





VOL. I.



SMITHSONIAN

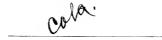
MISCELLANEOUS COLLECTIONS.

VOL. I.



"EVERY MAN IS A VALUABLE MEMBER OF SOCIETY WHO BY HIS OBSERVATIONS, RESEARCHES,

AND EXPERIMENTS PROCURES KNOWLEDGE FOR MEN." - SMITHSON.



WASHINGTON:
PUBLISHED BY THE SMITHSONIAN INSTITUTION.
1862.

PHILADELPHIA:
COLLINS, PRINTER.

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SMITHSONIAN MISCELLANEOUS COLLECTIONS.

DIRECTIONS

FGR

METEOROLOGICAL OBSERVATIONS,

AND THE

REGISTRY OF

PERIODICAL PHENOMENA.



WASHINGTON: SMITHSONIAN INSTITUTION. 1860.

PHILADELPHIA:
COLLINS, PRINTER, 705 JAYNE STREET.

DIRECTIONS

FOR

METEOROLOGICAL OBSERVATIONS,

ADOPTED BY THE SMITHSONIAN INSTITUTION

The following directions were originally drawn up for the use of the observers in correspondence with the Smithsonian Institution, by Professor Guyot, of the College of New Jersey, Princeton, and are now reprinted, with a series of additions, for more general distribution. The additions are indicated by brackets, [].

SECRETARY S. I.

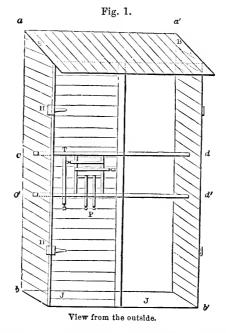
PLACING AND MANAGEMENT OF THE INSTRUMENTS.

THERMOMETER.

Placing.—Place the thermometer in the open air, and in an open space, out of the vicinity of high buildings, or of any obstacle that impedes the free circulation of the air. It should be so situated as to face the north, to be always in the shade, and be at least from nine to twelve inches from the walls of the building, and from every other neighboring object. The height from the ground may be from ten to fifteen feet, and, as far as possible, it should be the same at all the stations. The instrument should be protected against its own radiation to the sky, and against the light reflected by neighboring objects, such as buildings, the ground itself, and sheltered from the rain, snow, and hail. The following arrangement will fulfil these requirements (Fig. 1):—

Select a window situated in the first story, fronting the north, in a room not heated or inhabited; remove the lattice blinds, if there be any, and along the exterior jambs of the window place perpendicularly two pieces of board (ab-a'b'), projecting to

a distance of from twenty to twenty-four inches from the panes. At half this distance, ten or twelve inches from the panes, and at the height of the eye of the observer, when in the chamber, pass from one piece of board to the other two small wooden transverse bars (c, d, c', d'), each an inch broad, for the purpose of supporting the instruments. Upon the outer edge of the boards fasten, in the usual way (H H), the latticed blinds which were removed from the jambs, or two others provided for the That blind behind which the instruments are to be placed, is to serve as a screen, and must be fastened, almost entirely closed, so as to make a little more opening; the other will remain entirely open, to allow a free access of air and light, and is not to be closed except in great storms. The whole must be covered with a small inclined roof of boards (B E), placed at least fifteen or twenty inches above the instrument. part (J J), or the basis, may remain open.



[The foregoing is a convenient arrangement by which the observations can be taken without exposing the observer to the

weather. To prevent radiation from the room, the windows during the intervals of observations may be closed with an inside wooden shutter. . The outside of the lattice-work should be painted white, to reflect off the light and heat which may fall upon it.]

The thermometer must be placed exactly perpendicular, the middle of the scale being at the height of the eye against the

two small wooden bars, so that the top of the scale being fixed by a screw to the upper bar, the bulb may pass at least two or three inches beyond the lower bar. The instrument is attached to the last by a little metallic clasp. (Fig. 2.) It will thus be placed ten or twelve inches from the panes, from the screen, and the other parts of the window.

[In a later arrangement, a single transverse bar This being placed at the necessary height, is used. the thermometers are attached to it by small metal brackets, which support them at a distance from the bar of about two inches. The metal brackets are permanently screwed to the bar, and the thermometers are fastened to them by small finger-screws, by which they can be detached at pleasure. The order of placing

them is shown in the cut.]

Fig. 2.

Reading.—To read the thermometer, the eye must be placed exactly at the same height as the column of mercury. Unless this precaution is taken, there is a liability to errors, the greater in proportion to the thickness of the glass of the stem and the shortness of the degrees. The reading should be made at all times, and especially in the winter, through the panes, and without opening the window; otherwise the temperature of the chamber will inevitably influence the thermometer in the open air. The degrees must be read, and the fractions carefully estimated in tenths of degrees. After having rapidly taken the observation, another should be made to verify it. If there are several other instruments to observe, and the thermometer is to be read first, the first reading may be made some minutes before the hour; the second, after the reading of the psychrometer; and if there is a difference, the mean number is to be entered in the journal. When, notwithstanding the shelter, the bulb of the thermometer is moistened by rain or fog, or covered with ice or snow, it is necessary to wipe it rapidly, and not to record the degree until the instrument has been allowed to acquire the true temperature of the air.

Verification .- Verify the zero point, at the beginning and end of winter. For this purpose, fill a vessel with snow, immerse the bulb of the thermometer in the middle of it, so as to be surrounded on every side by a layer of several inches of snow, slightly pressed around the instrument. The stem must be placed exactly perpendicular, and covered with snow as far up as the freezing-point on the scale. Let it stand so for half an hour or more, and then read it, taking great care to place the eve at the same height as the summit of the mercurial column. If the top of the column does not coincide with the freezingpoint of the scale, the exact amount of the difference must be ascertained, and the correction immediately applied. At the same time enter in the journal, under its appropriate head, the day on which the experiment is made, its quantity, and the hour at which the application of it was commenced. It is necessary to add, that since the zero point of the thermometer is not that of the temperature of snow as it is frequently found when exposed to the atmosphere, but that of melting snow, the experiment must be made in a place above the temperature of freezing. Instead of snow, pounded ice may be employed.]

[Green's thermometers have an arrangement by which the tube can be slipped down the small quantity necessary to correct for this change. The end of the tube is fitted into a small plate of German silver, and this fastened by a serew to the scale. If, on testing the thermometer, the mercury be found to stand above 32°, free the screw one or two turns without taking it out, and push down the plate the necessary amount to bring the mercury to coincide. The thermometer must be handled with great care in making this adjustment, and it may be well, for additional security against accident, to loosen all the screws which fasten the bands around the tube; it will then slide in them more freely. After completing the adjustment, they may again be set moderately tight. The object of this adjustment being only to avoid the trouble of making a correction, it is not advisable to attempt it, if the observer thinks that he risks, in so doing, the safety of his instrument. As the tubes of these standard thermometers are kept for a considerable time before fixing the zero point, in most cases the moving will not be required. After the first year the zero point changes little, and practically, when exposed only to atmospheric influences, may be considered permanent.]

SELF-REGISTERING THERMOMETERS.

Placing.—These two thermometers, indicating the maxima and minima, are to be placed beside the common thermometer, in a horizontal position, with the bulbs opposite and free, on two small perpendicular supports uniting the two bars, as shown in Fig. 1.

Reading.—For the reading, place the eye in such a position that the visual ray may be perpendicular to the extremity of the index; enter the indications with the fractions of degrees, if there are any, and, after having verified them again, bring back, by means of the magnet, the indexes of the two thermometers to the summit of their respective columns.

Verification.—Compare the indications of the two thermometers frequently, and especially the spirit thermometer, with those of the common thermometer; verify the zeros at least twice a year, and, if there is a difference, adjust the zero anew, if the instrument permits, to eliminate the correction, as has been stated above for the simple thermometer, or take this correction into account in the register.

[The maximum thermometer is subject to derangement by the mercury getting to the side of the steel index and wedging it fast. When such is the case, put the bulb in ice, if it is necessary to bring the mercurial column so low, or cool it sufficiently to get all the mercury down that will pass the index; then move the magnet along the tube with a slight knocking or jarring motion, and try to get the index into the chamber at the top of the stem. If you get the index free of the wedge, but with mercury above it, heat the bulb until all the disjointed mercury and index are driven into the chamber, then keep the index up by the magnet, and the mercury will go back as the bulb cools. The great point of attention is to get and keep the index free of the wedge. The mercury being above is of little consequence, as it can readily be heated up into the chamber; in doing this, most watchfulness is required in not suffering the index to wedge

by the driving mercury. If the index is so wedged that it cannot be moved by these methods, then grasp the thermometer firmly in the hand, and swing it quickly, as if you wished to throw the mercury into the chamber at the top; the index, with more or less mercury, will be found in the chamber: if not, repeat the swinging until it is there. Then heat up the bulb until the mercury joins that in the chamber, keep the index up by the magnet, and let the mercury, by cooling, go back in unbroken line.

In using the magnet to move the index up into contact with the mercury, care must be taken not to urge it too strongly, or it may *enter* the mercury.

In using the spirit-thermometer, the same care is necessary as with the mercurial, since the index may sometimes be forced out of the spirit, entangling the vapor and the alcohol. When this is the case, the thermometer must be taken down and held vertically; a few taps or jars will bring the spirit together. The spirit-thermometer requires attention, also, in the following particular. The vapor above the column is apt, in time, to condense at the end of the tube, commonly at the very end. When the spirit-thermometer stands lower than the mercurial one, this may be suspected and looked for. When so found, the thermometer should be taken down and shaken until the alcohol runs down: it should then be kept in an upright position for some time, to drain. If it is found difficult to shake down the condensed vapor. the end of the tube may be carefully and slowly heated with a small lamp, or a small rod of heated iron held at a short distance, keeping the bulb and lower part as cold as possible; the alcohol by vaporization will then condense at the surface of the spirit in connection with the bulb. Occasionally, in cold climates, spiritthermometers are deranged by the air absorbed by the alcohol becoming free in the bulb at a low temperature. When this occurs, bring the thermometer to as low a temperature as may be convenient; then hold it in such a position that the air-bubble comes to the juncture of the bulb and tube, warm the bulb till all the air is in the tube; then, by shaking the thermometer, or by gentle knocking, the spirit will flow down, and the air speck come to the top.

This does not occur in spirit-thermometers that are closed with a vacuum, and the spirit at the time well freed from air.

In this case, however, the above-named difficulty from vaporization takes place more readily than when closed with air. These derangements of the spirit-thermometer are readily rectified, and only require occasional examination to detect them.

Both the maximum and minimum thermometers may be adjusted without the magnet, by raising one end sufficiently to allow the index to slide down by its own weight.*

The ordinary maximum thermometer (Rutherford's) not working well, even in the hands of many careful observers, has occasioned several attempts to make one without an index.

Mr. Green has lately contrived one. The object is effected by inclosing in the bulb a glass valve, which is floated by the mercury to the juncture of the bulb and tube. On an increase of heat the mercury from the bulb passes this valve, but on contraction from a decreasing temperature, the portion in the column is obstructed, and remains stationary, indicating the maximum point attained.

To set the instrument for another observation, it is held hulb downwards, and with a gentle jerk the mercury falls and joins that in the bulb; it is then placed horizontal in the usual way.

A movable valve-piece is introduced rather than a fixed obstruction or stricture, as in a new and ingenious maximum thermometer by Messrs. Negretti and Zambra, of London, in expectation that the observer will find greater ease and satisfaction in readjusting the instrument for observation.

Professor Phillips, of England, has also devised one. His plan is to cut off a portion of the column of mercury by an intervening small bubble of air. An increase of heat drives this detached portion forward, and leaves it there on a decrease of heat.

This form is also made by Mr. Green, and possesses some advantages peculiar to it; but, until experience decide otherwise, we doubt if it can be put in order after accidental derangement, by every observer. The former plans are not open to this objection.

^{*} The index of the spirit-thermometer is frequently made of a small cylinder of enamel, which cannot be moved by the magnet.

[†] These thermometers being new in plan, particular instructions in regard to suspending and setting them will be given with each instrument by the maker, Mr. James Green, New York.

PSYCHROMETER.

Placing.—The psychrometer, or wet-bulb thermometer, must be situated under the same conditions as the thermometer. It should be placed on the same wooden bars, several inches off, and ontside of the thermometer. (See Fig. 1.)

The bulbs should also be entirely free, and at a distance from the bars.

In ease of violent winds, the instrument may be sheltered by the movable blind, which may also serve as a fan to promote evaporation when the air is too still.

The cloth which surrounds the bulb ought to be of medium fineness, not too coarse; it should form a covering of equal thickness on all sides, and should not be drawn too closely upon the glass. Linen is preferable to cotton, which retains the dust. The covering should be changed every two or three months, and the bulb cleaned. [The linen may be washed, without removal, by means of a jet of clean water from a small syringe.]

Observation.—For the observation, take first a small vessel full of water, which should be left on the window, that the water may be at the temperature of the air; bring it near to the bulb, and immerse the bulb several times into the water. All the space between the bulb and the bottom of the seale must be wet, and care must be taken that the wrapping is thoroughly moistened, without, however, a too large drop remaining suspended at the bulb. The water used must be pure; the best is rain-water, filtered, because it does not hold any salt in solution, which might incrust the cloth after evaporation.

[In some arrangements of the psychrometer, the wet-bulb is kept constantly wet by conducting water to it from a small vessel, by capillary attraction, along a string of cotton wick. A series of comparative observations was made at this Institution, last summer, on these two modes of wetting the bulb, which gave the same result within a fraction of a degree from the mean of the records of a month. The observers connected with the Coast Survey prefer the method of dipping the covered bulb.]

After wetting the bulb, shut the window, and leave the psychrometer for a time.

While the wet bulb is slowly acquiring the temperature of

evaporation, the observer is occupied with other observations, though watching the psychrometer to make sure of the moment when it has become stationary. In summer, from four to ten minutes are needed for this, according to the size of the bulb; but in winter, when the water freezes on the bulb, it must be moistened from fifteen to thirty minutes before the observation, which should not be made until the ice around the bulb is quite formed and dry. The best way is to keep round the bulb a layer of ice, constant and uniform, which should be neither too thick nor too thin; then the observation may take place immediately. When the temperature is in the neighborhood of the freezing-point, the observation of the psychrometer requires very peculiar care; the reason of which we have elsewhere explained. During a fog, the wet-bulb thermometer may sometimes be higher than the dry-bulb; then the air is over-saturated, and contains, besides the vapor at its maximum of tension, water suspended in a disseminated liquid state. This is, however, not a frequent occurrence.

If the air is very still, it is well to increase the evaporation by setting the air in motion by a fan. If the wind is too strong, the instrument should be protected by the movable blind. The reading must be made rapidly, and, as much as possible, at a distance, and without opening the window; for the proximity of the observer, either by the heat radiating from his body, or by his breath, as well as the temperature and the hygrometrical state of the air issuing from the chamber, which is always different from that of the external air, especially in winter, would infallibly act upon the instruments, and would falsify the observation.

Verification.—The two thermometers must be carefully compared from time to time, and if a difference is found, the instruments must be adjusted, or it must be taken into the account, and the observations corrected when entered in the journal.

BAROMETER.

Placing.—The barometer should be placed in a room, of a temperature as uniform as possible; not heated, nor too much exposed to the sun. The instrument must be suspended at the height of the eye, near a window, in such a manner as to be lighted perfectly, without exposure either to the direct rays of

the sun, or to the currents of the air, which always take place at the joinings of the windows. When the barometer has to be fixed to the wall, as is the case with all the common stationary and wheel barometers, care must be taken to secure the tube in a position perfectly vertical, regulating it by the plumb-line, first in front, then at the sides, at least in two vertical planes cutting

Fig. 3. w 20

each other at right angles. When the instrument is so constructed as to take its equilibrium itself, as the Fortin barometers and those of J. Green, recently made under the direction of the Smithsonian Institution, it is enough to hang it on a strong hook. These conditions being fulfilled, the rest of the arrangement may be varied according to the nature of the localities. For the Fortin and Green barometers, the following arrangement is convenient, and may be almost everywhere adopted. (See Fig. 3.)*

A small oblong box $(a \ b)$, some inches longer than the barometer, and a little broader than its cistern, is firmly set against the wall $(w \ w')$, near the window, in such a manner as to open in a direction parallel to the panes; at the summit (a) it has a strong hook (h h'), which extends beyond the box about two or three inches, and on which the barometer is suspended. The instrument remains generally in the box, which is closed by a movable cover, and which protects it from external injuries, from dust, and from the direct radiation of warm bodies, or the currents of air from the window, and diminishes the effect of the too sudden variations of temperature. When it is to be observed, the barometer is taken by the upper end of the tube, and the suspending ring is made to slide towards the end of the

^{*} The standard barometer at the Smithsonian Institution is stationary and inclosed within a narrow case, the front and two sides of which open out by means of hinges so as fully to expose the instrument at the time of the observation.

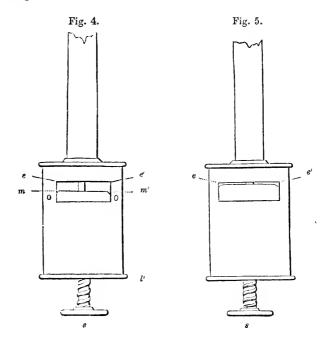
hook. The instrument is then in the full light of the window, in front of which the observer places himself; the summit of the mercurial column, as well as the surface of the mercury in the cistern, are completely lighted, and the reading becomes easy and certain. Moreover, the slight oscillating movement impressed on the instrument, by changing its place, breaks the adherence of the mercury to the glass, and thus prepares a good observation. After the reading, the barometer is again slipped gently into the box, and this is closed.

Observation.—The different operations of the barometer of constant level should be made in the following order:—

- a. Before all, incline the instrument gently, so as to render the mercurial column very movable; then, after having restored it to rest, strike several slight blows upon the casing, in such a manner as to impress on the mercury gentle vibrations. The adherence of the mercury to the glass will thus be destroyed, and the column will take its true equilibrium.
- b. Note the degree and the tenths of degrees of the thermometer attached to the instrument; for it will be seen that the heat of the observer's body soon makes it rise.
- c. Bring, by means of the adjusting serew (Fig. 4), the surface of the mercury to its constant level. In Green's first barometers, the metallic envelop of the eistern is pierced through $(o\ o')$, and allows the surface of the mercury contained in the glass cistern to be seen. The plane which passes through the upper edge $(e\ e')$ of this opening is the true level, or the zero of the scale, to which the surface of the mercury must be restored.

For this, take hold, with the left hand, of the lower edge of the eistern ($l\ l'$), taking great care not to disturb its vertical position; apply the right hand to the adjusting screw (s), and, turning it gently, bring by degrees the level surface of the mercury to the upper edge ($e\ e'$) of the opening of the cistern, until there remains between the two only an almost imperceptible line of light, as in the Fig. 5 ($e\ e'$). Then leave the instrument to itself, to re-establish its verticality, if it had been accidentally deranged, and placing the eye exactly at the height of the mercury, examine whether the contact is exact. For this operation, it is important to have a good light; the cistern ought to be placed higher than the lower edge of the window, so that the light may reach it directly. It is necessary also to take care

not to confound the slight line of light which marks the opposite edge of the eistern, with the light reflected by the surface of the mercury against the inner walls; the former is always sharp and well defined; the latter vague and indefinite. When, before adjusting the level, the mercury is higher than the upper edge, it is necessary to begin by lowering it beneath the level (see Fig. 4), so as to leave an interval of light, which is then gradually shut out, as has been described. When the observation is to be made in the night, place the lamp before, and not behind, the instrument, and somewhat higher than the eye; and if the wall itself is not light enough, place behind the cistern, or the top of the column, a viece of white paper, which reflects the light.



In the barometers with an ivory point, as the Fortin, Newman, and Green barometers, the extremity of this point is the zero of the scale, which must be brought into exact contact with the surface of the mercury. We commonly judge that this takes place when we see the actual rounded summit of the point co-

incide exactly with its image reflected below by the mercury. This method may be very good when the surface of the mercury is perfectly pure and brilliant; but this is very rare. It is generally dimmed by a slight layer of oxide, which makes the coincidence of the point with its image uncertain. It is safer to judge of the contact in a different manner. From the moment when the point does more than touch the surface, it forms around itself. by capillary action, a small depression, which, breaking the direction of the reflected rays, becomes immediately very easy to dis-It is enough, then, to raise the mercury so as slightly to immerse the point; then to lower it gradually until the little depression disappears. If care is taken to make a good light fall on that portion of the mercury which is under the point, and to use the aid of a magnifier, the adjustment of the point thus made becomes not only easy, but very certain, and the errors to which we are liable are almost insensible, for they do not exceed two or three hundredths of a millimetre, or a thousandth of an inch.

d. The level being thus adjusted to the zero of the scale, we proceed to observe the height of the summit of the column. Take hold of the instrument with the left hand, above the attached thermometer, without moving it from the vertical; strike several slight blows in the neighborhood of the top of the column; then, by means of the screw, lower the slide which carries the vernier, until the plane passing through the two lower opposite edges of it is exactly tangent to the summit of the meniscus—that is, the convexity which terminates the column. We know that this is the case when, placing the eye exactly at the height of the summit of the column, we still see the summit of the column, without there being any trace of light between the summit and the edge of the ring. To convince ourselves that the barometer has remained quite vertical during its operation, we leave it to itself, and when it is at rest, we look again to see whether the ring has remained tangential to the summit of the If it has not, the verticality has been disturbed; it must be adjusted anew. It is necessary, at the same time, to examine if the adjustment of the surface of the mercury in the cistern has remained the same. The attached thermometer will also be read anew, and if it indicates a temperature noticeably higher than at the commencement of the observation, a mean

value between the two indications must be adopted. An exact observer can never dispense with these verifications.

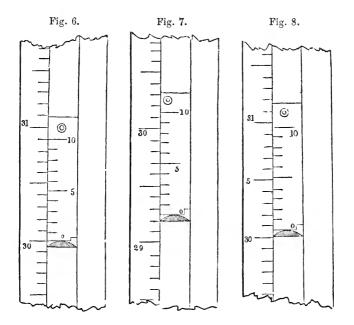
e. Nothing more, then, remains than to read the instrument. In the English barometers, the inches and tenths of inches are read directly on the scale, the hundredths and thousandths on the vernier. In the French barometers, with the metrical scale, the centimetres and millimetres are read on the scale, and the fractions of millimetres on the vernier. We begin by reading on the scale the number of inches and tenths of an inch, or of millimetres, there are, as far up as the line which corresponds to the lower edge of the vernier, and which marks the summit of the column. In the Green barometers, this line marks at the same time the zero of the vernier. If this line does not coincide with one of the divisions of the scale, we read the fraction of the following division on the vernier:—

The principle of the vernier is very simple. If we wish to obtain tenths, we divide into ten parts a space on the vernier comprising nine parts of the scale (see Fig. 6); each division of the vernier is thus found shorter by a tenth than each division of the scale. Now, if we start from the point where the zero of the vernier and its tenth division coincide exactly with the first and the ninth division of the scale, and if we cause the vernier to move gradually from the ninth to the tenth division of the scale, we shall see the first, the second, the third, and the other divisions of the vernier as far as the tenth, coincide successively with one of the divisions of the scale. Now, the divisions of the scale to which those of the vernier correspond, being equal parts, it follows that the space in question has been successively divided into ten parts, or tenths, by these successive coincidences. the scale bears millimetres, the vernier will give tenths of millimetres; if it has tenths of an inch, the vernier will give hundredths. By changing the proportions, it may be made to indicate by the vernier smaller fractions, as twentieths of millimetres, or five-hundredths of an inch, &c.

To read the vernier, we must look out for the line that coincides with one of the divisions of the scale; the number of this division of the vernier, proceeding from zero, indicates the number of tenths of millimetres, or of hundredths of an inch, which must be added to the whole number given by the scale. If none of the divisions of the scale coincides exactly, we estimate by

the eye, in decimals, the quantity by which the vernier must be lowered to obtain a coincidence, and this is added to the fraction already obtained. This will be hundredths of millimetres in the metrical barometer, and thousandths of inches in the English barometers.

The following figures will serve as an example; the instrument is an English barometer.



In Fig. 6 the regulating line, which is the lower edge of the vernier ring, coincides exactly with the line of thirty inches on the scale. The zero and the tenth division of the vernier are also in exact coincidence; that is to say, there is no fraction. We shall read then 30.000 inches.

In Fig. 7 the regulating line does not fall upon any of the divisions of the scale, but between twenty-nine inches and two-tenths and twenty-nine inches and three-tenths of an inch. There is then a fraction which must be read on the vernier. Seeking which of these divisions coincides with that of the scale, we find that it is the fifth; we shall write then 29.250 inches.

In Fig. 8 we see that the height falls between thirty inches

and thirty inches and one-tenth; no line of the vernier also coincides exactly; but the line 7 is a little above, the line 8 is a little below, one of the lines of the scale; the fraction falls, then, between seven and eight hundredths. Estimating in tenths the distance the vernier passes over between the coincidence of seven and that of eight, we thus obtain the tenths of an hundredth, or the thousandths. In this latter case, the distance above seven is less than the half; we shall then read 30.073. It will always be easy to judge whether the top approaches nearer the upper coincidence than the lower coincidence; in the former case, the fraction is greater than .005; in the latter it is smaller than .005. The error which will be committed in this estimate will remain less than .005; with practice and a little skill, it will hardly ever exceed .002, always supposing the scale is well graduated. For this reading, as well as for the others, it is particularly important to have the eye exactly at the height of the line to be determined.

The same process of reading is applied to the metrical scale; the vernier then gives tenths directly, and by estimate, the hundredths of millimetres. In the English instruments, the inches must be separated by a (.) and three decimals written, even when the last is a zero; e. g. 30.250, and not 30.25; the zero indicates that the thousandths have been taken into account, but that there are none. In the metrical scale put the (.) after the millimetres, and admit two decimals, e. g. 761.25.*

During the whole time of the observation of the barometer, the observer must endeavor to protect it as much as possible from the heat which radiates from his body. But the best way is to learn to observe rapidly. All the operations of which we have just spoken take longer to describe than to execute; one or two minutes, if the instrument be in place, three minutes if it is to be taken from its case and put back again, are sufficient for a practised observer to make a good observation

Altitude.—The height of the barometer above the ground, or above some fixed point, which may serve as an invariable point of reference, ought to be exactly determined. Such a point, for instance, may be the base of a public edifice, the level of low

^{*} For the method of reading the vernier of Green's standard barometer, see the description of the instrument, page 54.

water of a neighboring river, the ordinary level of the surfacewater of a canal, the upper part of a wharf in mason-work, &c. If the barometer has changed place, it is again necessary to measure exactly its height above the same point of reference; the latter will serve to fix the height of the barometer and of the station above the level of the ocean; this datum being of the greatest importance. Every change of this nature should be carefully noted in the journal.

It is greatly to be desired that the place of the barometer, once determined, should not be changed, either from one story to another, or from one house to another. If circumstances compel this to be done, we should begin, before taking it from its place, by raising the mercury in the cistern by means of the screw, so as to fill the cistern and the tube; it must then be gently taken from the hook, turned upside down, and carried with the cistern up, taking great care not to strike it against anything. If it were transported without these precautions, even from one chamber to another, great risk would infallibly be run of breaking it, or letting in air, and thus rendering it useless.

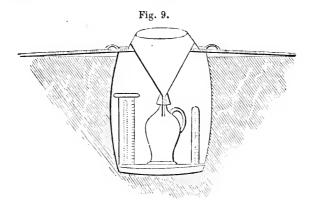
Verification.—From time to time the barometer should be so inclined as to cause the mercury to strike gently against the top of the tube. If it gives a dry and clear sound, it is free from air, and the instrument is in good condition. If the sound is flat and muffled, there is a little air in the barometric vacuum; and the fact should be noticed in the journal. Every occasion should be seized to compare it anew with a standard barometer, to ascertain whether it has undergone any change.

OMBROMETER.

Placing.—The ombrometer, or rain-gage, is a funnel, accompanied by a graduated cylindrical glass vessel, and by a reservoir. It should be placed in an open space. Trees, high buildings, and other obstacles, if too near, may have a considerable influence in increasing or diminishing the quantity of rain which falls into the funnel. The surface of the receiver should be placed horizontally about six inches above the ground. The most simple mode of establishing it is the following:—

Place in the ground a cask or barrel (Fig. 9), water-tight, the

top rising above the ground about three inches; cover it with boards slightly inclined in the form of a roof, which project on all sides beyond the edge of the barrel at least a foot. A circular opening in the middle receives the funnel, the borders of



which rest on the board. At the bottom of the barrel, to receive the water, is an earthen or metallic vessel, with a narrow neck, (an ordinary earthen jug will answer,) in which is placed the end of the funnel, exactly filling the opening. It must contain two or three quarts. The funnel is fastened by means of two clasps to the board, which must be covered up with sod, to make it like the ground itself. If circumstances render it necessary to place the ombrometer higher, the height must be carefully noted in the journal. If it is placed upon a sloping roof, it should be on the top, and not at the edges, or at the angles, and must be raised several feet above the roof itself.

Observation.—To make the observation, remove the funnel, and pour the water from the jug into the large graduated glass cylinder. The opening of the funnel being one hundred square inches, one inch of rain in depth gives one hundred cubic inches of water; and each division of the glass containing a cubic inch of water, each of them represents a hundredth of an inch of rain fallen into the ombrometer. These degrees are large enough to permit us to estimate the thousandths of an inch. The divisions of the smaller graduated glass cylinder will measure directly the thousandths of an inch, and it may serve, in case of accident, as a substitute for the larger onc. The two glass vessels may be

placed in the barrel itself, if it is of sufficient size. They must be placed in a reversed position, on two upright pegs, to let them drip out. As soon as the observation is made, it should be noted in pencil, not trusted to the memory; and written in the journal upon entering the house.

SNOW-GAGE.

Observation.—The snow-gage should be supported vertically, in an open place, between three short wooden posts, its opening being about two feet from the ground. It should be employed in the following manner:—

When only a very small quantity of snow falls, or of snow alternating with rain, or of dry and fine snow, driven by the wind, it should be collected in the snow-gage, as would be done in the ombrometer. But when the snow falls in a sufficient quantity to cover the ground more than an inch deep, the vessel must be emptied, and plunged, mouth downwards, into the snow, until the rim reaches the bottom. A plate of tinned iron, or a small board, may then be passed between the ground and the mouth of the gage, and the whole reversed. In this way a cylinder of snow, of which the base is superficially one hundred inches, will be cut out, and received into the vessel. The operation may be facilitated by placing on the ground a platform of strong board or plank, two or three feet square, on which the snow is received.

The place selected for this purpose must be one where the snow has not been heaped up, or swept away by the wind, and where it presents, as near as possible, the mean depth of the layer that has fallen. In order to take only the snow which may fall in the interval between two observations, the board should be swept after each measurement, and the place designated by stakes.

Reading.—In the reading of the graduated vessels, the general surface of the liquid must be considered as the true height, and not the edges, which are always raised along the walls of the vessel by capillary attraction.

The collected snow must be melted by placing the gage, covered with a board, to prevent evaporation, in a warm room;

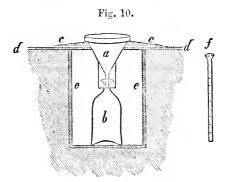
and the quantity of water produced measured by pouring it into the glass cylinder. It need hardly be said, that if rain and snow fall the same day, no account will be taken except of what the snow-gage receives, unless the ombrometer has been observed separately after the rain, and the snow-gage after the snow. Care must be taken, in these cases, not to count twice the same quantity of fallen water.

The rain-water and melted snow-water must be separately entered in the journal in the columns reserved for each.

During abundant rain-falls, it is well to measure the water more than once a day, or at least immediately after the rain; and the quantity of the rain fallen, together with the time it has lasted, is to be noted separately in the column of remarks.

When it freezes, it will be necessary to protect the receiver by filling in the interior of the barrel with straw.

[A series of observations have been made at the Smithsonian Institution with rain-gages of different sizes and different forms, the result of which, as far as the observations have been carried, is to induce a preference for the smallest gages. The one which was first distributed by the Institution and the Patent Office to the observers, is represented in Fig. 10. It consists of the



funnel a, terminated above by a cylindrical brass ring, bevelled into a sharp edge at the top, turned perfectly round in a lathe, and of precisely five inches diameter. The rain which falls within this ring is conducted into a two-quart bottle, b, placed below to receive it. To prevent any water which may run down on the outside of the funnel from entering the bottle, a short

tube is soldered on the lower part of the former and encloses the neck of the latter. The funnel and bottle are placed in a box or small cask e, e, sunk to the level of the ground, which is covered with a board d, d, having a circular hole in its centre to receive and support the funnel. To prevent the rain-drops which may fall on this board from spattering into the mouth of the funnel, some pieces of old cloth or carpet, e, e, may be tacked upon it.

The object of placing the receiving ring so near the surface of the earth, is, to avoid eddies caused by the wind, which might disturb the uniformity of the fall of rain.

In the morning, or after a shower of rain, the bottle is taken up and its contents measured in the graduated tube f, and the quantity in inches and parts recorded in the register. The gage, or tube, which was first provided for this purpose, will contain, when full, only one-tenth of an inch of rain, the divisions indicating hundredths and thousandths of an inch. As this, however, is found to be too small for convenience, another gage, which will contain an inch of rain, and indicating tenths and hundredths, will be sent to observers.

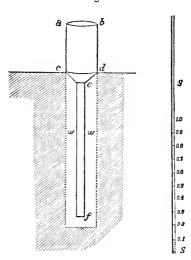
Another and simpler form of the gage has since been adopted by the Institution and the Patent Office, to send by mail to distant observers. It is one of those which have been experimented on at the Institution, and is a modification of a gage which was received from Scotland, and which has been recommended by Mr. Robert Russell.

It consists of—

- 1. A large brass cylinder a, b, c, d, two inches in diameter, to eatch the rain.
- 2. A smaller brass cylinder e, f, for receiving the water and reducing the diameter of the column, to allow of greater accuracy in measuring the height.
- 3. A whalebone scale s, s, divided by experiment, so as to indicate tenths and hundredths of an inch of rain.
- 4. A wooden cylinder w, w, to be inserted permanently in the ground for the protection and ready adjustment of the instrument.

To facilitate the transportation, the larger cylinder is attached to the smaller by a screw-joint at e.

Fig. 11.



Directions for use.—To put up this rain-gage for use: 1. Let the wooden cylinder be sunk into the ground in a level unsheltered place until its upper end is even with the surface of the earth. 2. Screw the larger brass cylinder on the top of the brass tube and place the latter into the hole in the axis of the wooden cylinder, as shown in the figure, and the arrangement is completed.

The depth of rain is measured by inserting the scale into the gage and noting the height to which it has been wetted by the water when it is withdrawn. In order, however, that the water may wet the scale, the superficial grease should be removed by rubbing it with a moist cloth, previous to use. In case the water cannot be made to adhere to the scale, a slip of pine or other wood may be made of the same size of the scale, and this inserted in its stead. The quantity of water may then be measured by applying the slip of wood to the scale.

Should the fall of rain be more than sufficient to fill the smaller tube, then the excess must be poured out into another vessel, and the whole measured in the small tube in portions.

Care should be taken to place the rain-gage in a level field or open space, sufficiently removed from all objects which would prevent the free access of rain, even when it is falling at the most oblique angle during a strong wind. A considerable space also around the mouth of the funnel should be kept free from plants, as weeds or long grass, and the ground so level as to prevent the formation of eddies or variations in the velocity of the wind.

To ascertain the amount of water produced from snow, a column of the depth of the fall of snow, and of the same diameter as the month of the funnel, should be melted and measured as so much rain.

The simplest method of obtaining a column of snow for this purpose is to procure a tin tube, about two feet long, having one end closed, and precisely of the diameter of the mouth of the gage.

With the open end downward, press this tube perpendicularly into the snow until it reaches the ground or the top of the ice, or last preceding snow; then take a plate of tin, sufficiently large to cover it, pass it between the mouth of the tube and the ground, and invert the tube. The snow contained in the tube, when melted, may be measured as so much rain. When the snow is adhesive, the use of the tin plate will not be necessary.

From measurements of this kind, repeated in several places when the depth of the snow is unequal, an average quantity may be obtained.

As a general average, it will be found that about ten inches of snow will make one of water.]

Mr. Guest, of Ogdensburgh, N. Y., recommends, from an experience of six years, the following as the best plan for ascertaining the amount of melted snow. Procure a cylindrical tin tube of the exact diameter of the mouth of the rain-gage and two or three feet long, so that the snow cannot be blown out. Place this vertically in a properly exposed position, and firmly secure it against the action of the wind, which would otherwise blow it over in a violent storm. After the snow has ceased to fall, bring the vessel with its contents into the house, near a fire, which will gradually melt the snow, and afterwards measure the water produced by means of the rain-gage.

WIND-VANE.

Placing.—The wind-vane should be set in a place as free and open as possible, away from every obstacle, and especially from high buildings. It should exceed in elevation, by at least eight or ten feet, the neighboring objects. To facilitate observations at night, the following arrangement may be adopted:—

The wind-vane is composed of a leaf of zinc about three feet in length, in the form of a butterfly's wing, exactly counterbalanced by a leaden ball. It is carried upon a cylindrical axis of pine wood, or of any other light and strong material, two inches in diameter, which, if possible, passes down through the roof into the observer's chamber, otherwise along the exterior wall of the building to a window. The axis terminates by a steel pivot turning freely on a cast-iron plate. This plate supports a dial divided into degrees, besides indicating the eight principal points of the compass. The axis carries an index placed in the same plane as the feather of the wind-vane, which enables us to read upon the dial, as well by night as by day, the direction of the wind. The whole rests on a strong wooden shelf, firmly fastened to the window by supports. Above, the rod is firmly fixed to a strong upright staff, or, better, on the roof, with strong braces, by means of a piece of wood containing friction rollers, which allow the shaft to turn freely and without effort. Similar pieces with friction rollers, placed at different distances along the wall, keep the axis vertical.

Great care must be taken to secure the perfect verticality of the shaft, and to this end it is necessary to fix it by a plumb-line in two different planes cutting each other at right angles. The index at the foot of the rod should be placed on the same side with the point of the wind-vane, and in the same plane as the feather. The pivot should turn very freely in the hole that receives it, and into which a drop of oil should be poured.

Finally, we must carefully adjust the points of the dial, which is supported with the iron plate, upon a board fastened upon a shelf by means of a strong screw. In making this adjustment by means of a compass, the magnetic variation of the locality must be taken into account; each observer should have the line of the true north traced on his window.

If the dial is exposed to the open air, it must be protected against the snow and bee, which would impede the play of the pivot and of the index. A small ring of wood placed around the pole, under one of the friction rollers, will prevent the windwane from being raised, and the pivot from being displaced during the most vicient winds.

[As a flat vane is always in a neutral line, a more accurate and sensitive one is made by fastening two plates together at an angle of about ten degrees, forming a long wedge. Thus,

The longer the vane, the shorter the pulsations, and the steadier the action will be. For a small sized vane, it may be ten or twelve inches wide, and four feet long.]

Observation.—The observation of this instrument demands some care. In winds of considerable strength the vane is never at rest, or fixed in the same direction; it oscillates incessantly, and its oscillations increase in amplitude with certain winds, and with the violence of the wind. We must then note the mean direction between the extremes. When the wind is very feeble, perhaps it may not have sufficient force to set the vane in motion; in this case, as when the air is calm, great mistakes might be made by registering the direction marked by the index; for its position indicates, not the direction of the existing wind, but that of the last wind that had the power to set the instrument in motion. When the index is immovable, and there is no oscillation, we must give up its indications, and refer to the movement of light bodies, as that of the leaves of trees and the smoke of chimneys, to determine the direction of these feeble currents of During the night the direction of the wind may be easily ascertained by raising the hand in the air, with one finger wet. The least motion in the air increases evaporation, and a sensation of cold is experienced on the side of the finger turned towards the wind.

The direction of the wind must be noted, following the eight principal points of the compass—north, northeast, east, southeast, south, southwest, west, and northwest. For the additional observations during storms, the degrees may be indicated, in order to follow more exactly the rotation of the wind, or at least

sixteen points of the compass, viz: N. NNE. NE. ENE. E. ESE. SE. SSE. S. SSW SW. WSW. W. WNW. NW. NNW.

The lower, or surface wind, often has a different direction from that which prevails in the upper regions of the atmosphere, and this is generally the case when the wind turns, and the weather is going to change, also during storms and great atmospheric movements. The direction, then, of the lower and the higher layers of clouds must be separately noted in the several columns of the journal reserved for this purpose. If the direction is the same in the whole extent of the atmosphere, the same letters will be marked in the three columns. If the absence of clouds does not permit us to judge how the wind is above, a dash must be substituted for the letter, indicating that the observation has been made. A blank always signifies an observation omitted.

To avoid an error in the estimate of the direction of the clouds, it will be well to observe their course between two fixed points, as a window frame, the fixed lines of which will facilitate the observation. Another very convenient method is to place a small mirror horizontally, with lines traced on it indicating the points of the compass; the image of the clouds passing over these will indicate their direction.

The manner in which the wind turns, or rather the order in which the winds succeed each other in the course of the day, must be watched very carefully. It will be seen that they commonly follow in regular order; they pass from the east by the south to the west, and from the west, by the north, to the east. Nevertheless, they sometimes go back in the opposite direction, particularly during storms. A little memorandum, summing up in a few words at the end of each day this course of the wind, together with the hours of the wind's changes, is very valuable. It may be entered in the column of remarks.

The *force* of the wind must be estimated as nearly as possible according to the following degrees:—

0. A perfect calm.

The simple initial letter of the wind, for instance N. (north), indicating its direction without any number, means a slight movement of the air hardly to be called a wind, and only just sufficient to allow an estimate of its direction.

- 1. A light breeze which moves the foliage, and sometimes fans the face.
- 2. A wind which moves the branches of the trees, somewhat retards walking, and causes more or less of a slight rustling sound in the open air.
- 3. A wind which causes strong boughs and entire trees to rock, makes walking against it difficult; which causes a stronger rustling sound to be heard, and which often blows in gusts, and carries light bodies up into the air.
- 4. A storm-wind, during which the trees are in constant motion; branches and boughs covered with foliage are broken off, and in a violent sterm sometimes even entire trees are broken, or uprooted; leaves, dust, &c., are continually borne up and carried far away; during which time there is an uninterrupted loud rustling sound, with strong gusts; walking windward is extremely difficult, and now and then chimneys, fences, &c., are thrown down, windows broken in, &c.

These degrees correspond nearly to the following numbers of Beaufort's scale, which is generally used among seamen:—

the same as 1. Light breeze,
 " " 4. Moderate breeze,
 " " 8. A fresh gale,
 " " 11. A storm-wind,

[The force of the wind is now estimated and registered according to the direction on the blank forms.]

SKY.

The blue color of the sky has an intimate connection with the hygrometrical state and the electrical tension of the air; it may be noted by the expressions, dark, light, and grayish.

Haze and dry mist.—The transparency of the air is often disturbed by a kind of vapor, which gives a whitish tint to the sky and dims the rays of the sun. This phenomenon, known in Europe under different names, appears frequently after long droughts; in this country it seems to characterize the Indian summer. In Europe, and elsewhere, an intensely dry mist, which is, probably, a different phenomenon, sometimes follows great earthquakes or volcanic eruptions. The observer will carefully

enter phenomena of this kind, and the circumstances under which they appear or disappear. If he has an opportunity, as in a high station, he should endeavor to ascertain if there is an upper limit, and what is the thickness of the layer of haze or dry mist. Observations made in the Alps prove that the atmosphere is often entirely free from it at a height of two thousand feet, when it is very intense in the plain. Does a thunder-storm or rain always cause it to disappear? Do the prairie fires have any relation with kindred phenomena? Does it appear more frequently in certain seasons than in others?

HYDRO-METEOROLOGICAL PHENOMENA.

DEW.

The dews, especially when they are abundant, and The white frosts, or frozen dew, particularly the first and last of the year, and their intensity, must be entered.

FOG.

Fog.—The moment must be noted when it forms and when it dissipates, as falling fog, rising fog; its density, as dense fog, slight fog.

Mists hanging over forests, moors, meadows, rivers, or the like

Notice must be carefully taken of the time of their appearance or disappearance; these are the most important facts in regard to them.

These fogs must not be confounded with the dry fog, which belongs to another class of phenomena, which have been spoken of above.

CLOUDS.

For noting these the observer must go out to a place entirely free, in case his residence has too confined a horizon.

The cloudiness or the quantity of clouds, after some practice,

CLOUDS. 29

can be easily estimated, in accordance with the following scale. Thus, we understand by—

- 0. A clear sky, entirely free from clouds;
- 10. The whole sky covered with clouds, or a dense fog, or rain; and by 1, 2, 3, 4, 5, 6, 7, 8, 9, the different degrees of cloudiness which lie between these:
- 1. Denotes, for instance, nine times as much blue sky as clouds;
- 5. An equal amount of clouds and blue sky;
- 9. Nine times more clouds than blue sky.

If, on account of the locality, it is impossible for the observer to estimate the quantity of clouds in this way, he can make use of the following expressions, which will mark at the same time the medium character of the aspect of the sky during each day:

Wel. Wholly clear; a sky entirely free from clouds.

- Cl. Clear; when at least two-thirds of the sky is unclouded.
- M. Medium; the clouded part of the sky nearly equal to the blue.
 - C. Cloudy; a larger part cloudy than clear.
 - Ov. Overcast; the clouds rarely broken.
 - Cov. Covered sky; without any visible spot of blue.

The form of the clouds will be indicated by the terminology of Howard.

According to this, they are distinguished by their external forms into three kinds: the cirrus, cumulus, and the stratus, to which belong four transition forms, the cirro-cumulus, the cirro-stratus, the cumulo-stratus, and the nimbus. The most remarkable of these forms may be characterized in the following manner:—

The *cirrus*, or cat-tail of the sailors, is composed of loose filaments, the whole of which sometimes resembles a pencil, sometimes early hair, sometimes a fine net, or a spider's web.

The cumulus, or summer cloud, the cotton-bale of the sailors, often shows itself under the form of a hemisphere resting on a horizontal base. Sometimes these half spheres are piled upon one another, forming those large accumulated clouds in the horizon which resemble, at a distance, mountains covered with snow.

The *stratus* is a horizontal band, which is formed at sunset and disappears at sunrise.

The cirro-cumulus are those small rounded clouds, which are

often called fleecy; when the sky is covered with clouds of that kind it is said to be mottled.

The cirro-stratus is composed of small bands, formed of closer filaments than those of the cirrus, for the rays of the sun often find it difficult to penetrate them. These clouds form horizontal beds, which, at the zenith, seem composed of a great number of loose clouds, while at the horizon a long and very narrow band is seen.

The *cumulo-stratus* is a mass of heaped up and dense cumuli. At the horizon they often assume a dark or bluish tint, and pass into the condition of *nimbi*, or rain clouds.

The *nimbus* is distinguished by its uniform gray tint, its fringe and indistinct edges; the clouds composing it are so blended that it is impossible to distinguish them.

But besides these principal forms, there are several intermediate, to which it is difficult to assign a name. They must be referred to the form which they most resemble.

They may be entered in the journal by means of the following abbreviations:—

St.	i. e.	Stratus.
Cu.	"	Cumulus.
Cir.	"	Cirrus.
Cir. st.	"	Cirro-stratus.
Cu. st.	"	Cumulo-stratus.
Cir. eu.	"	Cirro-cumulus.
Nim.	"	Nimbus.

If several of these forms are visible, the most frequent should be underlined, and the others should follow the order of their frequency. The distribution of the clouds in the sky should be noted, whether they are dispersed or accumulated in a special region of the heavens, in the horizon, at the zenith, &c

RAIN.

It is necessary to note as accurately as possible the hour at which the rain begins and ends; if it is a continued rain, or at intervals and in showers; if it is general or only partial, preceded, followed, or accompanied by fogs; the size of the drops and the force of the rain should be also noted. For these different cases, the following designations may be adopted:—

Rainy, when the fall of some drops and the appearance of the weather is such as to indicate the approach of rain.

Continued rain.

Interrupted rain.

Shower, which lasts not more than a quarter of an hour.

General rain, which prevails over the whole extent of the horizon.

Partial rain, which falls from the clouds that pass over only a small extent of country.

The force of the rain may be indicated by the following gradations:—

Drizzling rain, which falls in very small drops, almost like those of mist.

Slight or fine rain.

Moderate rain.

Heavy rain.

Violent rain, heavy and strong pelting rain.

The size of the drops seems to depend chiefly upon the height of the clouds, and consequently upon the seasons and the circumstances of the temperature.

The snow.—The period of the first and last snow, the size of the flakes, their forms.

Sleet, which consists in small balls of snow, white and opaque, commonly without a crust of ice, like the opaque nucleus found within hail-stones, falling more frequently in spring and in autumn.

Frozen rain drops should be distinguished from the preceding forms; they make little balls of transparent ice.

Hail.—Indicate the size, form and average weight of the hail-stones. The number of different strata observed in the larger stones. Whether any of them contain particles of sand or any other foreign matter. The extent and course of the phenomenon.

THUNDER-STORMS.

The time of beginning and ending of the storm must be indicated as exactly as possible; the point of the horizon whence it rises, the direction of the clouds, of the wind and its variations, and, if possible, the quantity of rain before and during the storm;

of hail, &c., which falls; note if it passes over the place of the observation, or at a distance; if it is accompanied, or not, with strong electrical detonations and numerous lightnings. It will be well to ascertain the state of the meteorological instruments every five minutes during the storm, especially of the barometer and the thermometer.

[At the Institution the barometer generally sinks during the coming on of a storm, and rises suddenly at the first fall of rain.]

In the journal, the occurrence of a storm will be indicated on the opposite page of the blank, with the hour when it took place. If special observations have been made with the instruments, they will also be entered on the opposite side of the sheet, taking care to note the day and the hour. If the observations require a more detailed description, it may be made on a separate sheet.

TORNADOES AND LAND-SPOUTS.

These whirlwinds, or violent and circumscribed storms, give rise to very complex phenomena, which are difficult to observe. All the meteorological circumstances, however, should be minutely noted; among others the following:—

The course of the barometer, which almost always sinks much and rapidly; that of the thermometer, which usually indicates an elevation of temperature; the region of the heavens in which the thunder-storm frequently accompanying them is formed; the form and color of the clouds; the direction and intensity of the wind; the frequency, the size, and the form of the lightnings; finally, the apparent shape of the land-spout, its variations, its course, and its effects upon the trees and upon the ground.*

ADDITIONAL OBSERVATIONS DURING STORMS.

Everybody knows the importance of a knowledge of the laws of those great movements of the atmosphere which embrace almost the whole extent of the continent. It is only in following them, step by step; by observing their different phases at different

^{*} For more detailed instructions upon the observations of land-spouts, see the Annuaire Météorol. de France, 1849, p. 225.

places, and by combining the facts obtained, that the meteorologist can be enabled to discover the laws which preside over these great phenomena. For this, the three regular observations a day are insufficient; it is then earnestly recommended to observers, who desire to contribute effectually to the solution of this great problem, not to content themselves with the prescribed number, but to add as many more as possible during the continuance of remarkable storms; noting not only the state of the instruments from hour to hour, if possible, but following with attention all the meteorological changes. These observations must be entered on the reverse of the sheet, under the head of Casual Phenomena, which is particularly reserved for this purpose.

The principal points to which attention should be directed are the following:—

The barometer announces by a considerable fall the approach of a storm. Then it begins to rise during its continuance, and only resumes its nominal equilibrium after its close. Remark especially the following points:—

Was the storm preceded by a noticeable or sudden rise previous to the fall;

Note the state of the barometer, and the time when the fall becomes more rapid;

Its state, and the time, when it is lowest and when the rise begins;

The highest point which it reaches during, or immediately after the storm.

If alternations of rising and falling take place, the fact should be mentioned and the time noted.

The thermometer.—The fluctuations of the thermometer in the same time as those of the barometer should also be noted, and their connection with the changes of the wind be observed.

The wind.—It is of the greatest importance to observe the course of the winds through the entire height of the atmosphere during the whole continuance of the storm, by means of the windvane and of the clouds in the different layers of the atmosphere.

The hour when the wind begins, and the direction whence it comes;

The moment of its greatest violence;

The instant it changes its direction, and when it takes the direction it keeps to the end of the storm.

It should be stated if the wind blows in a continuous manner or in squalls, and what is its force.

If there should be one or more moments of calm, the hour and duration will be indicated.

Great care must be taken at each observation to note also the direction of the different layers of clouds, which will very often be found different from that of the wind below, for the whole duration of the storm.

The clouds.—Are there certain forms of clouds which announce the approach of a storm? It is necessary, in this connection, to watch the formation of the cirrus, the cirro-cumulus, cirro-stratus, their arrangement in parallel lines, their course, and their directions. Note the quarter of the sky first covered with clouds; the moment when it is entirely covered; if there are later clear spots or not; the moment when the sky clears off.

The rain.—Note the hour at which the rain or the snow begins and ends; measure the quantity fallen while the storm lasts.

ACCIDENTAL METEORIC PHENOMENA.

These will be entered in the tables, in the place reserved for this purpose on the opposite side of the sheet. If the space is not sufficient for the description to be given, the phenomenon should be simply noted, and reference made to a separate account for details. Thus:—

The solar and lunar haloes—that is, the colored circles sometimes observed round the sun and moon. Distinguish the small ones, the ring of which measures only a few degrees, from the large or real haloes, the ring of which has a diameter of about forty-four degrees. It must be stated whether they are connected with other circles, as is sometimes the case. Care must be taken not to mistake a part of a grand halo for a rainbow. Note whether these appearances are, or are not, ordinarily followed by rain.

The Parhelia and Paraselenes (mock-suns and moons).—Describe exactly their forms and the state of the heavens at the moment of their appearance.

Rainbows, simple or double.

An extraordinary redness of the sky, either in the morning or

evening; the particular color of the sun and of the moon at their rising, especially in fair days.

Heat lightnings without thunder, and sometimes without clouds; indicate their direction and the aspect of the clouds in their neighborhood.

The Aurora Borealis, or northern light, for the observation of which the special instructions, page 48, must be followed.

Shooting-stars.—The observer must be particularly attentive to their frequency, during the periods near the 10th and 11th of August, and the 10th and 15th November, in which it is supposed that they are more numerous than at any other time. He will designate the quarter of the heavens from which they seem to issue, and their direction.

Fireballs.—Describe their aspect, their size, their course in the heavens, and note the exact hour of their appearance.

All the other luminous phenomena, which present any extraordinary appearance, should be noted down.

These descriptions should be made in simple and well-defined terms. The observer will take great care to enter scrupulously what he sees without drawing any conclusion, or attempting any explanation of the phenomenon. He ought to reflect that, in order to make a good observation, he must keep his mind in a state of perfect freedom in respect of any preconceived theory, and to consider the phenomenon before him as being one of the data for the foundation of the science, and that the knowledge of the truth will depend upon the fidelity of his observation.

TIME OF OBSERVATIONS.

The time of observations will be the mean time at each station The observations will be made three times daily, viz:—

The mean of these three hours will be very nearly the true mean, as it would be obtained by observation made every hour of the day and night.

The rain gage will be observed only once a day, unless very abundant rains should make a second measurement necessary.

The best time will be 2 o'clock p. m., the observation being made daily; if another hour is selected, it should, when once fixed, remain the same.

The maxima and minima thermometers will be read once a day, always at the same hour. The most suitable hour will be 9 o'clock in the evening.

If an observer desires to examine the daily oscillations of the barometer, he will also observe at 10 a. m. and 4 p. m., which give the daily maximum and minimum. It will be well to note also, at the same time, the state of the hygrometer.

If he desires to complete the data upon the diurnal course of the temperature, he will add observations of the thermometer at 10 a.m. and 6 p.m. In all cases it is desirable that, if an observer has leisure to increase the number of the hours of observations, he should fix them at equal intervals between the principal hours indicated above.

Besides these observations at regular hours, additional observations ought to be made during remarkable storms, as has been remarked above.

It is very important that the observations should be made at the exact hour, fixed by a well regulated watch. All the instruments should be read rapidly, so that the observations may be as simultaneous as possible.

The order in which they are to be observed will be as follows:-

A few minutes before the hour, observe the thermometer before opening the window; then wet the psychrometer. While it is taking the temperature of evaporation, note the height of the barometer, observe the wind, the course of the clouds, their quantity, the aspect of the sky, &c.; then read the temperature of the psychrometer.

The observations must be recorded for each instrument at the moment when they are made, without trusting anything to the memory. A strict rule should be laid down for one's self, to note exactly the indications of the instruments, without subjecting them mentally to any corrections or any reductions; these should not be applied until all the elements are at hand.

If the observer has been unavoidably hindered from making the observations at the exact hour, he will note in the column of hours the number of minutes of the delay. If he is obliged to procure a substitute, he must choose one accustomed to this kind of observation; but before entering his records, he will carefully examine them. To distinguish the observations made by his substitute, he will enter them in red ink.

As it is of the greatest importance that the series of observations should not be interrupted, and that there should be no omissions, each observer will do well to instruct beforehand one or more substitutes, who may be able upon occasion to take his place. If, in spite of these precautions, the observation has necessarily been omitted, its place will be left blank in the journal. In this case the observer must never fill up these blanks with calculations, according to his judgment; he should consider the conscientious observance of this rule indispensable to truth and good faith. He should remember, besides, that if he acts differently, he not only lessens the value of these results, but brings into doubt and disfavor the fidelity of his other observations, and takes from them what constitutes their greatest value for science—confidence.

THE REGISTER.

In the register the first page is devoted to regular observations; the second to additional observations, to periodical or extraordinary phenomena, and to monthly recapitulations. The headings of the columns indicate clearly the use of each.

For each instrument the columns follow each other in the order in which the observations are to be made, and one column is reserved to enter the observation just as it is made, and before any correction or reduction. As each sheet is to be regarded as an independent document, it should earry with it all that is necessary to correct the observations therein contained, and to render them authentic. Thus, the date of the year, the month, the precise locality, the latitude and longitude, the elevation of the instruments from the ground and above the sea, the nature and condition of the instruments which have been employed, and the amount of their corrections; finally, the signature of the observer should be repeated on every leaf. It will be sufficient, for this, to fill the blank spaces left after the different printed titles in the blank forms. The observer should the less neglect this important duty, as it is an affair of only a few strokes of the pen each

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month, without which his labor would run the hazard of losing its value.

Barometer.—The degree of the attached thermometer and the observed height of the barometer will be inscribed in the first two columns. This height will be reduced to freezing-point, or 32° Fahrenheit, or zero Centigrade, by means of tables, and the whole correction of the instrument will be applied to it. It will then be inscribed in the third column, entitled corrected height at freezing-point. These corrected heights, and never any others, must be employed to form the mean, which will be inscribed in the fourth column.

Thermometer.—In the thermometrical observations the quantities above zero will be always written without a sign; the negative quantities will be all individually marked with the sign minus (—), whether they follow each other or are isolated. In the first column, entitled daily mean, will be inscribed the mean of the three observations of the day, i. e. their sum divided by 3, admitting two decimals.

Psychrometer.—In the first two columns will be entered the indications of the dry and wet thermometer, after having applied to each of them the correction of the instruments, if there be any. By means of the psychrometrical tables will be found the force of the vapor and the degree of relative moisture, each of which has its column.

We have indicated above the manner of noting the direction of the winds.

As to the force of the surface wind, which alone can be estimated with some degree of precision, it will be expressed by adding to the letter which designates the direction, the figure indicating its force: e. g., N, without a figure, signifies a slight air, hardly perceptible, coming from the north; N_1 , a slight breeze; N_3 , a strong wind, &c. The other two columns will have only letters, or a dash (—) if the observation has not been possible.

The quantity of clouds, or the *cloudiness* estimated from zero, or a perfectly clear sky, to 10, sky entirely overcast, has a separate column.

It is the same with rain and melted snow, which will be separately entered. A third column is reserved for the total quantity

of both. The thickness of the layer of fallen snow may be indicated in inches and tenths.

As to the broad column for Casual Phenomena, although it is desirable, considering the small space the form of the table allows, to employ abbreviations to express the state of the sky and the different meteorological phenomena; nevertheless, we must limit ourselves to a small number, chosen from among the expressions which most frequently occur, such as those found at the bottom of the blank forms. If abbreviations are too much multiplied, we lose in clearness and certainty what we gain in conciseness. A meteorological journal should not resemble a page of algebra, where a badly formed letter or a misplaced sign renders the expression unintelligible.

For the additional observations the same rule should be followed.

In the space mentioned above, *periodical and extraordinary* phenomena will be inscribed, with their dates and the hour of their appearance.

Every change of position, or in the condition of the instruments, should be carefully entered, with the precise date at which it took place. If there has been none, instruments all in order will be entered. By the side of the indication of the correction of the instruments will be placed, correction applied or correction not applied, according as the observations contained in the sheet shall have been corrected or not. The finished sheet will be signed by the observer.

The reductions, the corrections, and the calculations of means, must be made day by day and at the end of each month with the greatest punctuality. The necessary tables will be placed at hand by the side of the journal, and each observation reduced, and the correction, if any, applied immediately.

This is not only the least troublesome method, but the only one which permits the observer to control the observations and the reductions, and to discover the accidental errors of the pen and of the reading in the record.

The observer cannot be too thoroughly convinced that a meteorological journal which contains only rough observations, is only half made; in this condition it is wholly unfit to serve any scientific purpose. The observations cannot be compared rigorously with each other, nor with those of other stations. The

only means for the observer to give its true value to his labor, is to make the corrections, the reductions, and the calculations of the means himself. It is for want of having thus been elaborated that voluminous collections of observations, the fruits of long years of toil, remain useless and forgotten in the dust of libraries, because the meteorologist finds it impossible to make use of them without first undertaking those calculations, the amount of which absolutely transcends the powers of an individual, and would discourage the most ardent zeal, while they would have cost the observer only an instant each day, if he had made them at the time of the observations.

The calculations desirable are as follows:-

- 1. Each barometrical observation must be reduced immediately to the temperature of zero Centigrade, or 32° Fahrenheit, by means of the tables, and the total correction of the barometer, if there is any, will be applied.
- 2. The diurnal means of the several instruments, resulting from the sum of the three observations made at these different hours, divided by three, must be entered each day in the respective columns, after the observation of 9 p. m. It is needless to say that these means should be drawn solely from observations reduced and corrected.
- 3. The monthly means for each hour separately—that is, the monthly mean of the observations of 7 a.m., and that of 2 p.m., and of the observations of 9 p.m.
- 4. The monthly means drawn from the means of each day; the monthly extremes of the instruments; the monthly amount of the rain, hail, or snow; the mean cloudiness of the sky; the prevailing wind, &c.
- 5. The annual means and amounts, and the respective extremes for the civil year.

It will be interesting to calculate, also, if the observer is so disposed, the mean of the seasons of the meteorological year, which begins December 1, to November 30, of the following civil year.

The meteorological seasons are, then :-

Winter-December, January, February.

Spring-March, April, May.

Summer—June, July, Angust.

Autumn-September, October, November.

In calculating all these different results, we should take, in order to be very exact, the means of the sums of all the observations during the period of time in question, by reason of the inequality of the length of the months.

The sums which form the basis of all these means should be inscribed in the tables in the place reserved for them.

The preceding calculations, after a little practice, will not appear difficult, and may be quickly performed; but it can hardly be too often urged upon the observer to make them without delay; otherwise, this task, which is slight if accomplished daily, would become very heavy, if left to accumulate for several months. It is only by making the correction himself that the observer can institute his own comparisons, and really study the course of the meteorological phenomena. His interest will increase still more with the feeling that he is coöperating in a great work, which concerns at once his whole country and the science of the world, and the success of which depends upon the accuracy, fidelity, and devotion of all who take part in it.

A copy of the observations of each month must be forwarded during the first week of the following month. It should be carefully collated by two persons, one of whom reads the figures aloud. Each observer will receive for this purpose a double series of blank forms, one of which will be retained by him.

Many of the phenomena connected with the state of the atmosphere are of great interest for comparative climatology, especially in a practical point of view. The periodical phenomena of vegetation and of the animal kingdom, such as the epoch of the appearance and the fall of the leaves, of the flowering and ripening of the more generally cultivated fruits; the seed time and harvest of plants; the coming and going of migratory birds; the first cry of the frogs, the appearance of the first insects, &c.; the moment of the closing of rivers, lakes, and canals by ice, and of their opening; the temperature of springs at different periods of the year; the temperature in the sun compared to that observed in the shade; that of the surface, and that below the surface of the ground. All observations of this kind are valuable.

The observer will find it very instructive to project curves which indicate the diurnal, monthly, or annual variations of tem-

peratures, of atmospheric pressure, of moisture, &c., as well as thermometrical, barometrical compasses, or circles, &c.

These graphic representations are of the greatest utility for the comparisons, speaking to the eye more clearly than simple figures.

Besides the above directions for keeping an ordinary Meteorological Journal, more special instructions for the study of peculiar meteorological phenomena are prepared by the Smithsonian Institution; as on

Thunder-storms, Tornadoes, and Water-spouts, Aurora Borealis, Parhelia, Parasalenes, Haloes, Rainbows, Temperature of the soil, Periodical phenomena of the vegetable and animal kingdoms, Graphic representations of meteorological phenomena, &c. If any observer should feel inclined to devote himself to the study of any one of these physical problems, he may receive, on application, the special instructions relating to the point which he wishes to investigate. [These instructions now form a part of this pamphlet.]

[The directions given in the preceding article are not intended to supersede those printed on the sheet of blank forms issued jointly by the Smithsonian Institution and the Patent Office, but to impart additional instruction, particularly to those who are furnished with a full set of instruments and desire to attain as much precision as possible.]

SPECIAL DIRECTIONS

TO THE

METEOROLOGICAL OBSERVERS

OF THE

SMITHSONIAN INSTITUTION.

In the reduction of the meteorological records presented to this Institution, much additional labor has resulted from the occasional omission in the registers, of some important facts, and in a want of perfect uniformity in noting the phenomena. We beg, therefore, to call attention to the following remarks:—

- 1. Failure to record latitude and longitude, name and station of the observer, and date on each sheet; the observer probably supposing it sufficient to insert them once on the first sheet sent, and so omitting them afterwards. This often renders it necessary to search back through all the series of registers to some one that contained them—perhaps in a former year. They should be inserted on every sheet.
- 2. Designating the same place by different names, thus rendering it impossible to distinguish whether it were one place or two, unless by accidentally noticing the similarity in the name of the observer or in the latitude and longitude. Such changes of name should be avoided when practicable, and when necessarily made special attention should be called to it.
 - 3. Diversity in the mode of recording the Barometer, as follows:
 - (a) Integers recorded in full, thus 29.35. (This is the proper mode.)
 - (b) Integers omitted when the same as in the entry next above, thus 38.
 - (c) Integers omitted when the same as in the entry next to the left.

- (d) Integers omitted when the same as in the entry next preceding in the order of time.
- (e) Integers omitted except where they are different from the usual ones at the place of observation.
- (f) Integers inserted occasionally and apparently without any system whatever.
- (g) A constant suppressed, and the excess or deficiency recorded, as + or -.

The proper mode is that indicated by (a).

- 4. Diversity in the mode of recording the Thermometer, when it is below zero, as follows:—
 - (a) Indicated by the sign minus placed before it, thus —16°. (This is the proper mode.)
 - (b) Indicated by the same sign placed after it, thus 160—.
 - (e) Indicated by writing it under a zero—thus $\frac{0}{16^{\circ}}$.
 - (d) Indicated by writing it after a zero, with a comma between, thus 0,16°.
 - (c) Indicated by the word 'below,' or the abbreviation b written before or after it—thus 16° below, 16° b, b 16°, or below 16°.

The first (a) is the proper mode.

- 5. Departure from the printed instructions in recording the degree of cloudiness, some observers reversing the figures and using 10 to denote a clear sky and 0, one entirely overeast; and others omitting the record altogether in the columns of cloudiness when the sky is clear, and in place of it sometimes inserting the word "clear" in the columns of "Remarks," or elsewhere. Both lead to error, and should be avoided—the zero should always be inserted "in the narrow column," as directed, when the sky is clear.
- 6. Diversity in the use of the character zero (0) in recording the motion of the clouds, as follows:—
 - (a) Used to signify a calm, or that there is no perceptible motion. (This is the correct use.)
 - (b) Used to signify that the sky is clear, instead of inserting it in the proper column.
 - (c) Used to signify that no observation was taken.

(d) Used to signify that the direction in which the upper current was moving could not be determined on account of the sky being either perfectly clear or entirely overcast.

The first (a) is the correct use.

- 7. Want of full and proper records of the direction of the wind, some observers recording the direction only after each change, and then omitting it so long as it continues the same, merely inserting a figure to denote the force. It is better to make the record in full. Other observers record the direction towards which the wind or clouds are moving instead of indicating that from which they come. A WIND from the North, or CLOUDS moving from the North, are to be denoted by N, and from the South by S, &c.
- 8. Different kinds of thermometers or different exposures used for the dry and wet-bulb thermometers, so that the observations are not comparable readily, if at all.
 - 9. Diversity in the use of the dash and the sign (") as follows:—
 - (a) To signify that the entry next above is to be repeated.
 - (b) To signify that the entry next to the left is to be repeated.
 - (c) To signify that the entry next preceding in the order of time is to be repeated.
- (d) To signify nothing at all, but merely to fill a blank. The use of these characters has caused much trouble in the reduction, and the true remedy would be to avoid them altogether, by making each record complete in itself.
- 10. Illegibility of the records, either from defective chirography or from being entered in pencil marks and partially erased.

CIRCULAR RELATIVE

TO

EARTHQUAKES.

The Smithsonian Institution is desirous of collecting information in reference to all phenomena having a bearing on the physical geography of this continent; and, in behalf of the Board of Regents, it is respectfully requested that you will furnish us with any information which you may possess, or be able to obtain, in regard to the earthquake which lately occurred in your neighborhood.

It will be interesting to determine the geographical limits of the disturbance, and to ascertain whether it was confined to any particular geological formation. If the direction of the shock was observed at a few places, the centre of commotion could be determined; and if the time were accurately known at different points, the velocity of the earth-wave could be calculated. Hence, an answer is requested to the following questions, viz:—

- 1. Was the agitation felt by yourself, or by any other person in your vicinity?
 - 2. What was the approximate time of the occurrence?
 - 3. What was the number, and duration, of the shocks?
 - 4. What was the direction of the motion?
- 5. What was the character of the disturbance? was it vertical, horizontal, or oblique? was it an actual oscillation? an upheaval and depression, or a mere tremor?
- 6. Was there any noise heard? and if so, what was its character?
- 7. Was the place of observation on soft ground, or on a hard foundation near the underlaying rocks of the district?

- 8. Were any facts observed having apparently an immediate or remote bearing on this phenomenon?
- 9. What was the intensity of the force in reference to producing motion in bodies and cracks in walls?

Note.—Please reply to the *first* question, if to no other—for an answer to it is necessary, in order to determine the limits of the commotion.

The direction of the impulse may have been ascertained by observing the direction in which molasses, or any viscid liquid, was thrown up against the side of a bowl. The remains of the liquid on the side of a vessel would indicate the direction some time after the shock occurred.

4

INSTRUCTIONS FOR OBSERVATIONS

OF THE

AURORA.*

GENERAL REMARKS.

Though the aurora borealis has received attention during a considerable portion of the last two centuries, definite information is still wanting on several points which may serve as the basis of a sound induction as to its cause. These relate particularly to the actual frequency of the appearance of the meteor; its comparative frequency in the different months of the year and different hours of the day; the connection of the appearance of the meteor with other atmospherical phenomena; the elevation and extent of visibility of the arch; and whether the same or different phases are presented to individuals at different stations at the same moment of time; finally, the precise influence of the arches, streams, &c., on the magnetic condition of the earth; and whether any unusual electrical effects can be observed during the appearance of the meteor.

Auroral phenomena may be divided into the following classes:-

- 1. A faint light in the north, without definite form or boundary.
 - 2. A diffused light, defined by an arch below.
 - 3. Floating patches of luminous haze—sometimes striated.
- 4. One or more arches, resembling the rainbow, of uniform white color, retaining the same apparent position for a considerable time, and varying in luminosity.

^{*} These instructions are principally adopted from those used in the Observatory at Toronto, Canada.

- 5. A dark segment, appearing under the arch.
- 6. Beams, rays, streamers, waves, transverse and serpentine bands, interrupted or checkered arches, frequently tinged with color, and showing rapid changes in form, place, and color.
 - 7. Auroral corona, or a union of beams south of the zenith.
 - 8. Dark clouds accompanying the diffuse light.
 - 9. Sudden appearance of haze over the whole face of the sky.

The following may serve as a scale of brightness:—

1. Faint. 2. Moderate. 3. Bright. 4. Very bright.

GENERAL DIRECTIONS.

- 1. Make a regular practice of looking for auroras every clear evening, from 8 to 10 o'clock, or later. Record the result, whether there be an aurora or not.
- 2. Note the time of observation, and compare the watch used with a good clock, as soon after as is convenient.
 - 3. Make a return of the latitude and longitude of the station.
 - 4. Note the class to which the auroral phenomenon belongs.
- 5. If it be an arch, note the time when the convex side reaches any remarkable stars, when it passes the zenith, disappears, &c.
- 6. If the arch be stationary for a time, mark its position among the stars on the accompanying map, so that its altitude may be determined.
- 7. If it be a streamer or beam, mark its position on the map, and the time of its beginning and ending.
- 8. If motion be observed in the beams, note the direction, whether vertically or horizontally, to the east or west.
- 9. Note the time of the formation of a corona, and its position among the stars.
- 10. Note the time of the appearance of any black clouds in the north near the aurora; also, if the sky be suddenly overcast with a mist at any time during the auroral display.
 - 11. Give the direction and force of the wind at the time.
 - 12. Note if any electrical effects are observed.
- 13. Note the effect upon a delicately suspended magnetic needle.

50 AURORA.

USE OF THE MAP.*

- 1. To define the place and the extent of the aurora, the observer should familiarize himself with the relative position of the stars in the northern sky, by frequent inspection of the accompanying map, or a celestial globe.
- 2. Let the observer place the map before him, with the constellations in the positions in which they actually appear at the time of the observation. This may be done by holding up a plumb-line between the eye and the pole star, noticing the stars which it cuts; then a light pencil drawn through these stars and the pole on the map will be the centre of the heavens, or place of the meridian at the moment.
- 3. Mark carefully the place among the stars of the arch of the aurora, and show its width by parallel curved lines. Make a note of the time.
- 4. Draw a light curved line, following, as nearly as can be judged, the outline of the arch down to the horizon, on each side.
- 5. If the arch changes its position, mark its new places at intervals, noting the time of each observation.
- 6. Letter each position A, B, C, &c., and note the time and other particulars on the back or margin of the map, or in the register.
- 7. Beams or coruscations, or streamers of white or colored light, may be marked by lines at right angles to the above, with arrow heads pointing towards the place among the stars to which they tend, or where they would meet, if prolonged.
- 8. To aid in the estimation of angular distances the spaces between certain conspicuous stars have been marked on the map, which will furnish a scale to assist the eye, when actual measurement may be impracticable.
- 9. The course of brilliant meteors, when they fall within the portion of the heavens included on the map, may be marked by a line, the length of which will show the path of the meteor; the course should be indicated by an arrow, and the time recorded.

The map, when filled, together with any written observations,

^{*} Copies of the map will be furnished by the Institution.

may be returned to the Smithsonian Institution, indorsed Meteorology.

MAGNETIC APPARATUS.

Few observers will probably be furnished with a regular set of magnetical instruments. A temporary apparatus may, however, be fitted up at comparatively little expense and trouble. For this purpose a steel plate, such as was used a few years since for ladies' busks, may be magnetized, and suspended edgewise in the vertical plane, by a few fibres of untwisted silk, in a box to prevent agitation by the air, furnished with a glass window on one side, through which observations may be made. To render the motions perceptible, a small mirror should be cemented on the side of the magnet opposite the window. In front of this mirror, and at the distance of ten or fifteen feet, an ordinary spyglass is fastened to a block, and under the glass, to the same block, a graduated scale, with arbitrary divisions marked upon it, is attached. The arrangement is such that the divisions of the scale may be seen through the telescope, reflected from the mirror, and consequently the slightest motion of the needle, and of the mirror cemented to it, gives a highly magnified apparent motion to the scale. The mirror may be formed of a flat piece of steel, highly polished by means of calcined magnesia; or, in default of a mirror of this kind, a piece of plate looking-glass may be employed, provided one can be procured sufficiently true. The suspension threads should be three or four feet long. instrument should not be placed very near large masses of iron, and care should be taken not to change the position of any articles of iron which are within the distance of fifteen or twenty feet, otherwise a change in the position of the needle will be produced. For a similar reason the box should be constructed without iron nails. The above described instrument will indicate changes in the direction of the magnetic meridian. similar instrument, deflected at right angles to the magnetic meridian by the torsion of two suspended threads, will furnish an apparatus for indicating changes of horizontal magnetic force.

ELECTRICAL APPARATUS.

To ascertain whether any change takes place in the electrical state of the atmosphere during the appearance of an aurora, the end of a long insulated wire, suspended from two high masts or two chimneys by means of silk threads, may be placed in connection with a delicate gold leaf electrometer. Any change in the electrical state of the atmosphere, simultaneous with the aurora, will be indicated by the divergence of the leaves. Two slips of gold-leaf attached by a little paste to the lower end of a thick wire, passing through a cork in a four-ounce vial, will answer for this purpose. The arrangement of the leaves will be best made by a bookbinder, who is expert in the management of gold-leaf.

[A continuous series of photographic registers of the motion of the magnetic needle is now kept up at the joint expense of the Coast Survey and this Institution, which will serve for comparison with any observations which may be made on the aurora.]

Prof. Olmsted, in a recent paper published by the Smithsonian Institution, classifies different auroras as follows:—

"Class I. This is characterized by the presence of at least three out of four of the most magnificent varieties of form, namely, arches, streamers, corona, and waves. The distinct formation of the corona is the most important characteristic of this class; yet, were the corona distinctly formed, without auroral arches or waves, or crimson vapor, it could not be considered as an aurora of the first class.

"Class II. The combination of two or more of the leading characteristics of the first class, but wanting in others, would serve to mark class the second. Thus the exhibition of arches and streamers, both of superior brilliancy, with a corona, while the waves and crimson columns were wanting, or of streamers with a corona, or of arches without a corona, without streamers or columns (if such a case ever occurs), we should designate as an aurora of the second class.

"Class III. The presence of only one of the more rare characteristics, either streamers or an arch, or irregular coruscations, but without the formation of a corona, and with but a

moderate degree of intensity, would denote an aurora of the third class.

"CLASS IV. In this class we place the most ordinary forms of the aurora, as a mere northern twilight, or a few streamers, with none of the characteristics that mark the grander exhibitions of the phenomenon."

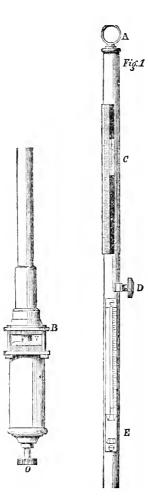
The same author remarks:-

"On the evening of the 27th of August, 1827, after a long absence of any striking exhibition of the aurora borealis, there commenced a series of these meteors, which increased in frequency and magnificence for the ten following years, arrived at a maximum during the years 1835, 1836, and 1837, and, after that period, regularly declined in number and intensity until November, 1848, when the series appeared to come to a close. The recurrence, however, of three very remarkable exhibitions of the meteor in September, 1851, and of another of the first class as late as February 19th, 1852, indicates that the close was not so abrupt as was at first supposed; but still there was a very marked decline in the number of great auroras after 1848, and there has been scarcely one of the higher class since 1853.

"A review of the history of the foregoing series of auroras appears to warrant the conclusion that it constituted a definite period, which I have ventured to call the "Secular Period," having a duration of little more than twenty years; increasing in intensity pretty regularly for the first ten years, arriving at its maximum about the middle of this period, and as regularly declining during the latter half of the same period."

If this view be correct, it would appear that but few brilliant displays of the aurora may be expected for a number of years to come.

GREEN'S STANDARD BAROMETER.

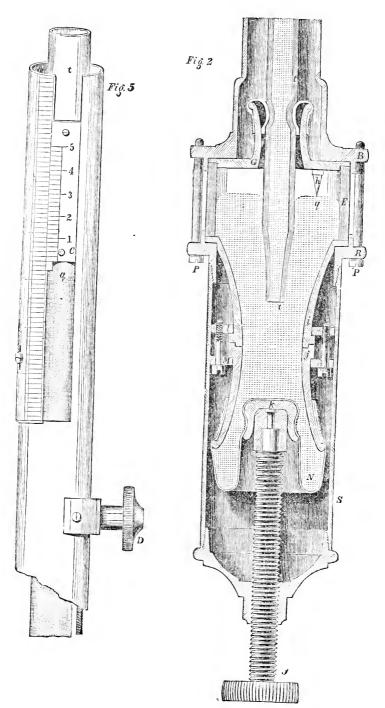


THE following is an account of Green's improved standard barometer, adopted by the Smithsonian Institution, for observers of the first class.

The barometer consists of a brass tube, (Fig. 1) terminating at top in a ring A, for suspension, and at bottom in a flange B, to which the several parts forming the cistern are attached.

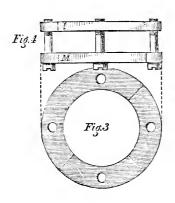
The upper part of this tube is cut through so as to expose the glass tube and mercurial column within, seen in Fig. 5. Attached at one side of this opening is a scale, graduated in inches and parts; and inside this slides a short tube c, connected to a rack-work arrangement, moved by a milled head D: this sliding tube carries a vernier in contact with the scale, which reads off to $\frac{1}{500}$ (.002) of an inch.

In the middle of the brass tube is fixed the thermometer E, the bulb of which being externally covered, but inwardly open, and nearly in contact



with the glass tube, indicates the temperature of the mercury in the barometer tube, not that of the external air. This central position of the thermometer is selected that the mean temperature of the whole column may be obtained; a matter of importance, as the temperature of the barometric column must be taken into account in every scientific application of its observed height.

The cistern (Fig. 2) is made up of a glass cylinder \mathbf{F} , which allows the surface of the mercury q to be seen, and a top plate \mathbf{G} , through the neck of which the barometer-tube t passes, and to which it is fastened by a piece of kid leather, making a strong but flexible joint. To this plate, also, is attached a small ivory point h, the extremity of which marks the commencement or zero of the scale above. The lower part, containing the mercury, in which the end of the barometer-tube t is plunged, is formed of two parts i j, held together by four screws and two divided rings l m, in the manner shown in the Figures 2, 3, and



To the lower piece j is fastened the flexible bag N, made of kid leather, furnished in the middle with a socket k. which rests on the end of the adjusting-screw O. These parts, with the glass cylinder F, are clamped to the flange B by means of four long screws P and the ring R; on the ring R screws the cap S, which covers the lower parts of the cistern, and supports at the end the adjusting-screw O. G, i, jand k, are of boxwood; the

other parts of brass or German silver. The screw O serves to adjust the mercury to the ivory point, and also, by raising the bag, so as to completely fill the cistern and tube with mercury, to put the instrument in condition for transportation.

In Fortin's barometer, and also Delcro's modification of it, a cement is used to secure the mercury against leakage at the joints. This, sooner or later, is sure to give way; and tested under the extremes of the thermometrical and hygrometrical range of this climate especially, has made this defect more evi-

This was removed by the substitution of iron in the place of wood; but it was soon found impracticable, in this form of cistern, to prevent damage from rust. These objections led to the present plan of construction, which effectually secures the joints without the use of any cement. The surfaces concerned are all made of a true figure, and simply clamped together by the screws, a very thin leather washer being interposed at the joints. This would not be permanent, however, but for the especial care taken in preparing the boxwood. The boxwood rings are all made from the centres of the wood, and concentric with its They are worked thin and then toughened, as well as made impervious to moisture, by complete saturation with shel-This is effected by immersing them in a suitable solution The air being withdrawn from the pores of the wood, in vacuo. is replaced by the lac. This, however, with the after-drying or baking, requires care; but when properly done, the wood is rendered all but unchangeable.

Another peculiarity consists in making the scale adjustable to correct for capillarity, so that the barometer may read exactly with the adopted standard, without the application

of any correction; and this, too, without destroying the character of the barometer as an original and standard instrument. Near the 30 inches line, Figure 6, is a line v, on the main tube; this last line is distant exactly thirty inches from the tip of the ivory point; therefore, when these lines coincide, or make one line, the scale is in true measurement position; or the 30 mark is exactly thirty inches from the tip of the ivory point in the cistern. In this position, the amount of correction due to capillarity being ascertained, the scale is then moved that quantity and clamped firm. The barometer will now give the readings



corrected for capillarity, and thus avoid at once the labor of applying a correction, and the risk of error from an accidental neglect of it.

It must be borne in mind that this correction applies only to the particular tube, and while preserved in good condition.

If this tube is injured and again used, or another tube put in its place, the scale should then be moved until the lines coincide, the amount of correction for the repaired or the new tube being estimated until a good comparison can be made directly or intermediately with the Smithsonian standard.

The connecting the parts i and j by rings and screws, Figs. 2, 3, and 4, rather than by a single screw cut on the edge, is an improvement, as the single wood-screw is apt, after a time, to adhere so firmly that it is often difficult, and sometimes impossible, with safety to the parts, to separate it.

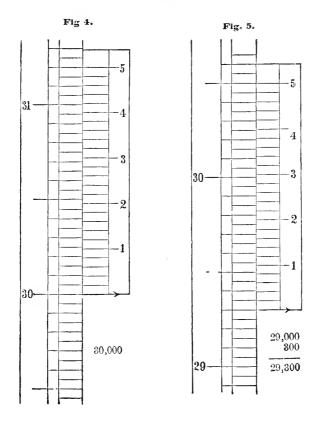
It is not advisable to disturb the cistern, unless it becomes difficult, from the oxide of mercury which gradually forms, to make the adjustment of the mercury to the ivory point, as there is more or less risk in doing so. Any one accustomed to such mechanical affairs, with due attention to the plan, can, however, take out the mercury from the cistern, refilter, clear the parts of adhering oxide, and replace them; the instrument all the time being kept vertical, with the cistern at top, as the mercury must not be allowed to come from the tube.

To insure a good vacuum by the complete expulsion of all air and moisture, the boiling of the mercury in the tube is done in vacuo; and care should be taken to preserve it in good condition.

To put up the barometer for observation, suspend the barometer by the ring A in a good light, near to and at the left side of a window, and, when practicable, in a room not liable to sudden variations of temperature. Record the temperature, and then, by the screw O, lower the mercury in the cistern until the surface is in the same plane with the extremity of the ivory point. As this extremity of the point is the zero of the scale, it is necessary, at each observation, to perfect this adjustment. It is perfect when the mercury just makes visible contact. If the surface is lowered a little, it is below the point; and if raised a small amount, a distinct depression is seen around the point. This depression is reduced to the least visible degree. A few trials will show that this adjustment can always be made to a thousandth of an inch.

The adjustment effected, bring the lower edge of the vernier C, Fig. 5, by means of the milled head D, into the same plane with the convex summit of the mercury in the tube. Looking through the opening, with the eye on a level with the top of the mercury in the tube, when the vernier tube is too low, the light

is cut off; when too high, the light is seen above the top of the mercury. It is right when the light is just cut off from the summit, the edge making a tangent to the curve. A piece of white paper placed behind, and also at the cistern, will be found to give a more agreeable light by day, and is, besides, necessary for night observations; the lamp being placed before the instrument and above the eye, to reflect the light.

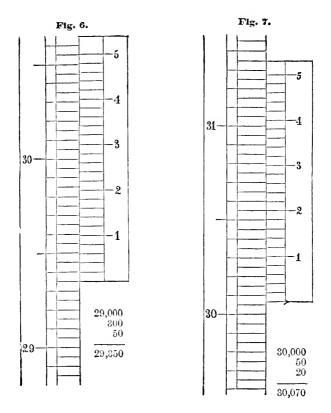


The method of reading off will perhaps be best explained by a few examples. Suppose, after completing the adjustments, the scale and vernier to be in the position shown in Fig. 4, on this page, it will be seen that the lowest or index line of the vernier coincides exactly with the line marked 30 on the scale. The reading, therefore, is 30.000 inches.

If, as in Fig. 5, we find the line of the vernier coinciding with the third line of the tenths above 29, we read 29.300.

If, as in Fig. 6, on this page, we find the index at 29 inches 3 tenths and 5 hundredths, we read 29.350.

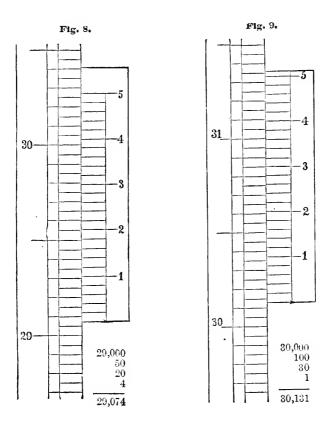
If, as in Fig. 7, we find the index at 30 inches no tenths 5 hundredths and something more, this additional quantity we



shall find by looking up the vernier scale, until we come to some one line on it, coinciding with a line on the other scale. In this instance it is the line marked 2, and indicates 2 hundredths, to be added to the other numbers, making 30.070.

If, as in Fig. 8, we find 29 inches no tenths 5 hundredths, and on the vernier the second line above that marked 2, is found to coincide with the scale, each of these short lines indicates 2

thousandths—consequently, are so counted; the reading s therefore 29.074.



Or it may be, as in Fig. 9, where we have 30 inches 1 tenth, and the line on the vernier mark 3 coinciding nearly, but not perfectly, with a line on the scale, it is a little too high; the 2 thousandth short line next above is, however, a like quantity too low; so the true reading must be the number between them—that is, 1 thousandth, making together 30.131.

These examples include all the combinations the scale allows. A little practice with the barometer, with reference to the examples, will soon enable the learner to read off the scale with facility. At first it will be best to write down the inches and

parts in full, as in the diagrams, not trusting the memory with the whole, until experience shall have given confidence.

Be careful never to lower the mercury in the cistern much below the necessary quantity, as it increases the risk of air entering the tube.

When the barometer is to be removed for transportation, or change of position, before taking it down, the mercury is to be screwed up until the cistern and tube are just full. If it is screwed more than this, the mercury may be forced through the joints of the cistern. It should then be inverted, and carried cistern-end upwards.

This instrument is well adapted for service as a mountain barometer, and when used as such, is packed in a leather case, with suitable straps for convenient carriage.

REGISTRY OF PERIODICAL PHENOMENA.

The Smithsonian Institution, being desirous of obtaining information with regard to the periodical phenomena of animal and vegetable life in North America, respectfully invites all persons who may have it in their power, to record their observations, and to transmit them to the Institution. These should refer to the first appearance of leaves and of flowers in plants; the dates of appearance and disappearance of migratory or hybernating animals, as mammals, birds, reptiles, fishes, insects, &c.; the times of nesting of birds, of moulting and littering of mammals, of utterance of characteristic cries among reptiles and insects, and anything else which may be deemed noteworthy.

The Smithsonian Institution is also desirous of obtaining detailed lists of all the animals and plants of any locality throughout this continent. These, when practicable, should consist of the scientific names, as well as of those in common use; but when the former are unknown, the latter may alone be given. It is in contemplation to use the information thus gathered, in deducing general laws relating to the geographical distribution of species of the animal and vegetable kingdoms of North America. Any specimens of natural history will also be acceptable. Directions for their preservation have been published by the Institution, and will be sent to all who may wish them.

The points in the phenomena of plants, to which attention should be directed, are:—

- 1. Frondescence, or leafing.—When the buds first open and exhibit the green leaf.
 - 2. Flowering .- When the anther is first exhibited :-
 - a. In the most favorable location;
 - b. General flowering of the species.

- 3. Fructification.—When the pericarp splits spontaneously in dehiscent fruits, or the indehiscent fruit is fully ripe.
 - 4. Fall of leaf.—When the leaves have nearly all fallen.

The dates of these various periods should be inserted in their appropriate columns.

When the observations for the year are complete, they should be returned to the Institution, with the locality and observer's name inserted in the blank at the head of the sheet.

PLANTS.

i mario.					
•	sence, ing.	Flow	ering.	ation	eaf,
List of Plants.	Frondescence or leafing.	a.	ь.	Fructification	Fall of leaf
Acer rubrum, L.—Red, or soft maple. Acer dasycarpum, Ehrh. — White, or silver maple. Acer saccharinum, L.—Sugar maple. Achillea millefolium, L.—Millefoil, or yarrow. Actæa rubra, Willd.—Red baneberry Actæa alba, Bigelow.— White baneberry; necklace weed. Exculus hippocastanum, L.—Horse chestnut. Escalus glabra, Willd.—Ohio buckeye. Æxculus flava, Ait.—Yellow buckeye. Ailantus glandulosa.—Tree of heaven; ailanthus glandulosa.—Tree of heaven; ailanthus glandulosa.—The willow buckeye. Amorpha fruticosa, L.—False indigo. Amorpha fruticosa, L.—False indigo. Amygdalus nana, L.—Flowering almond. Anemone nemorosa, L.—Wind flower; wood anemone. Aquilegia canadensis, L.—Wild columbine. Arctostaphylos wa-ursi, Spreng.—Bearberry. Asclepias cornuti, Decaisne.—Milkweed. Asimina triloba, Dunal.—Papaw. Azalea nudiflora, L.—Common red honeysuckle. Bignonia (Tecoma) radicans, Juss.—Trumpet creeper. Castanea vesca, L.—Chestnut. Carya alba.—Shag-bark, or shell-bark hickory. Cercis canadensis, L.—Red bud: Judas tree. Cerasus virginiana, DC.—Chokeberry. Cercasus virginiana, DC.—Chokeberry. Cercasus virginiana, DC.—Wild black cherry. Chionanthus virginica, L.—Fringe tree. Cimicifuga racemosa, Ell.—Black-suake root; rattlesnake root. Claytonia virginica, L.—Spring beauty. Clethra alnifolia.—White alder, or sweet pepper bush. Cornus florida, L.—Flowering dogwood* Crategus crus-galli, L.—Cockspur thorn. Cratagus coccinea, L.—Spring heauty. Clethra alnifolia.—White alder, or sweet pepper bush. Cornus florida, L.—Flowering dogwood* Crategus crus-galli, L.—Cockspur thorn. Cratagus coccinea, L.—Scarlet-fruited thorn. Cratagus coccinea, L.—Scarlet-fruited thorn. Cratagus coccinea, L.—Scarlet-fruited thorn. Cratagus coccinea, L.—Scarlet-fruited thorn. Crategus crus-galli, L.—Cockspur thorn. Crategus cr					

^{*} The time of the expansion of the real flower, not of the white involucre.

PLANTS—Continued.

	cence,	Flow	ering.	ation.	Paf.
List of Plants.	Frondescence, or leafing.	a.	ь.	Fructification	Fall of 19af
Gaylussacia resinosa, Torr. and Gray.—Black					
huckleberry					
Gerardia flara, L.—Yellow false foxglove					
Geranium maculatum, L.—Crane's bill					
Halesia tetraptera, Willd.—Snow-drop tree . Hepatica triloba, Chaix.—Round lobed liver-	1				
wort					
Houstonia carulea, Hook.—Bluets; innocence,	1				
&c	1				
Hypericum perforatum, L.—St. John's wort .					
Tris versicolor, L.—Large blue flag					
Kalmia latifolia, L.—Mountain laurel	ĺ				
Laurus benzoin, L.—(Benzoin odoriferum, Nees.)					
Spice bush; Benjamin bush					
Leucanthemum vulgare, Lam.—Ox-eye daisy;					
white weed					
Linnwa borealis, Gronov.—Twin flower					
Lobelia cardinalis, L.—Red cardinal flower .				- 1	
Lonicera tartarica, L.—Fereign spurs	1				
Lupinus perennis, L.—Wild lupine	i				
Liriodendron tulipifera, L.—Tulip tree; Ame-					
rican poplar					
				ļ	
lia; sweet bay					
Morus rubra, L.—Red mulberry					
Nympha a odorata, Ait.—Sweet-scented water	!			1	
lily				- 1	
Persica rulgaris, L.—Peach					
Podophyllum, L.—Mandrake; Mayapple					
Pontederia cordata, L.—Pickerel weed			1	ĺ	
Pogonio ophioglossoides, Nutt.—Adder's tongne					
Pyrus communis, L.—Common pear-tree					
Pyrus malus, L.—Common apple-tree					
Unercus alba, L.—White oak	1 1				
Ribes rubrum, L.—Currant					
Robinia pseud-acacia, L.—Common locust .	!	ļ		1	
Robinia viscosa, Vent.—Clammy locust					
Rubus villosus, Ait.—Blackberry					
Sambucus canadensis, L.—Common elder					
Sambucus nigra, L.—Black elder			1		
Sanguinaria canadensis, L.—Blood root					
Sarracenia purpurea, L.—Side-saddle flower .					
Saxifraga virginiensis, Michx. — Early saxi-				l	
frage			İ		
Smilacina bifolia, Ker.—Two-leaved Solomon-seal			1		
Syringa vulgaris, L.—Lilae		- 1			
Taraxacum dens-leonis, Desf.—Dandelion					
Tilia americana, L.—Bass wood; American			1		
lime, or linden)			
7/mus americana, L.—American elm					
iburnum lentago, L.—Sweet viburnum			- 1	- 1	

BIRDS

Birds.	Arrival in spring.	Commencement of nesting.	Commencement of incubation.	Appearance of young.	Departure in autuma.
Acanthylis pelasgia, Boie.—Chimney-bird . Agelaius phaniceus, L.—Red-winged blackbird Anser canadensis, L.—Wild goose					

Reptiles—first appearance, cries, and general peculiarities of habits.

Bufo americanus, and other species of toads.
Rana, the various kinds of frogs.
Hyla and Hylodes, the several kinds of tree-frogs.
Turtles, lizards, snakes.

FISHES—first appearance and spawning.

Salmo salar, L., salmon. Alosa, shad. Clapea, herring. Anguilla, eel. Acipenser, sturgeon.

INSECTS—their first appearance and cries.

Platyphyllum concavum, Harr., catydid. Cicada, locusts—the several kinds Ecanthus niveus, Harr., tree-crickets Grasshoppers, in their variety. Fire-flies.

GENERAL PHENOMENA OF CLIMATE.

Phenomena of a general character, of which the date of appearance cannot be mistaken, are very valuable. Series of years have in some cases been carefully observed, which would greatly add to the value of the current record, if forwarded with it. The following are of this class:—

- 1. Breaking up of ice in large rivers or bays.
- 2. Date of greatest rise and lowest fall of water in large rivers, especially when periodic, as in parts of the interior.
- 3. General leafing and fall of leaf in deciduous forests. In most parts of the North and interior these are well marked and easily designated periods.
- 4. Commencement of growth and the end of growth or destruction of grasses in general; as on plains or prairies.
- 5. First growth, flowering, and maturity, of important annual staples, with their period in days from the commencement to the end of vital action.

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Psychrometrical Table:

FOR DETERMINING THE

ELASTIC FORCE OF AQUEOUS VAPOR

. AND THE

RELATIVE HUMIDITY OF THE ATMOSPHERE

FROM

INDICATIONS OF THE WET AND THE DRY-BULB THERMOMETER FAHRENHEIT.

RV

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EASTON, PENNSYLVANIA.

WASHINGTON:
PUBLISHED BY THE SMITHSONIAN INSTITUTION.
1856.

THE following table is based on the formulæ of Reginault, as used by Prof. Guyot, in the preparation of his Psychrometrical Tables, for the Smithsonian Institution viz.:—

$$x = f - \frac{.480 (t - t')}{610 - t'} h$$
, for temperatures above the freezing-point, and $x = f - \frac{.480 (t - t')}{689 - t'} h$, for those below;

in which h represents the height of the barometer, t the temperature indicated by the dry bulb centigrade thermometer, t' that indicated by the wet bulb thermometer, f the elastic force of aqueous vapor in a saturated air at the temperature t', and x the actual force at the time of the observation.

Adapting these formulæ to the Fahrenheit thermometer, the former will read

$$x = f - \frac{.480 \times \frac{5}{9} (t - t')}{610 - \frac{5}{9} (t' - 32)} h = f - \frac{.480 (t - t')}{1130 - t'} h,$$

and the latter,

$$x = f - \frac{.480 \times \frac{5}{9}(t - t')}{689 - \frac{5}{9}(t' - 32)} h = f - \frac{.480(t - t')}{1240.2 - t'} h.$$

If we put h = 755 millimetres, = 29,725 English inches, these formulæ may be reduced for the latter measure to the following forms:—

$$x = f - \frac{14.268 (t - t')}{1130 - t'}$$
; and $x = f - \frac{14.268 (t - t')}{1240.2 - t'}$.

In using the table, look out the degree of the wet-bulb thermometer at the top, and the difference between the wet and dry bulb thermometers at the left. Under the former and opposite the latter, find, in their appropriate columns, the force of vapor, and the relative humidity.

euheit.			1				ERMOME					
Fabre		31°		80°		29°		S °		270	- 2	100
t — t' Fahreuheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1	·011 ·006	100 50 2	·012 ·006 ·001	100 52 6	·012 ·007 ·001	100 54 9	·013 ·007 ·002	100 55 12	·013 ·008 ·002	100 57 16	·014 ·008 ·003	100 59 19
it.		D	EGREES	OF TII	E WET	BULB '	rhermo	METER	— FАНКЕ	NHEIT		<u>' </u>
abrenhe	-2	25°	2	.10	2	23°	2	22°	2	21°	_2	:0°
t — t' Fabrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches,	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Fare of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 2	·015 ·009 ·003	100 60 22	·015 ·010 ·004	100 62 25	·016 ·010 ·005	100 63 28	·017 ·011 ·005	100 64 30	·017 ·012 ·006	100 66 33 1	·018 ·012 ·007 ·001	100 67 35 5
		D	EGREES	OF TII	E WET	BULB 1	THERMO	METER.	—FAHRI	ENHEIT		
renheit	-1	9°	-1	s°	-1	70	-1	6°	1	15°	-1	1°
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor. in inches.	Relative Humidity.
0° 1 1 1 1 1 2 2	·019 ·013 ·007 ·002	100 69 37 9	·020 ·014 ·008 ·003	100 70 40 12	·021 ·015 ·009 ·003	100 71 43 16	·022 ·016 ·010 ·004	100 72 45 19	·023 ·017 ·011 ·005	100 73 47 23	·024 ·018 ·012 ·006 ·001	100 74 49 26 3
ıt.		D	EGREES	OF TH	E WET	BULB T	HERMON	HETER.	FAHRE	NHEIT		
Fahrenbeit.	-1	3 °	-1	2 °	-1	1L°	-1	0 °		9°	9	3°
t — t' Fa	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 12 1 112 2 212	·025 ·019 ·013 ·007 ·002	100 75 51 29 6	·026 ·020 ·014 ·009 ·003	100 76 53 31 10	·027 ·021 ·015 ·010 ·004	100 77 55 34 13	·028 ·022 ·017 ·011 ·005	100 78 57 36 17	·029 ·024 ·018 ·012 ·006 ·001	100 79 58 39 20 2	·031 ·025 ·019 ·013 ·008 ·002	100 80 60 41 23 6

٠			DEGREES	S OF T	HE WET	BULB	THERM	OMETE	R.—FAIII	RENHE	T.	
breuhei		7°		6°	-:	5°	- 2	1 °	-:	3°		2°
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches,	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 2 2 2 2 2 2 3	·032 ·026 ·021 ·015 ·009 ·003	100 80 62 43 26 10	·033 ·028 ·022 ·016 ·011 ·005	100 81 63 46 29 13	·035 ·029 ·024 ·018 ·012 ·006 ·001	100 82 65 48 32 17 2	·036 ·031 ·025 ·019 ·014 ·008 ·002	100 83 66 50 34 20 5	·038 ·032 ·027 ·021 ·015 ·010 ·004	100 83 67 52 37 23 9	·040 ·034 ·028 ·023 ·017 ·011 ·006	100 84 68 53 39 26 12
eit.		D	EGREES	OF TI	IE WET	BULB	THERMO	METER	FAHR	ENHEI	г.	-
ahrenh	1	4	0									
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches,	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 12 1 1 1 2 2 2 2 2 2 2 2 4 4	-042 -036 -030 -025 -019 -013 -008 -002	100 84 69 55 42 28 16 4	·044 ·038 ·032 ·026 ·020 ·015 ·009 ·003	100 85 70 56 43 30 18 6	·046 ·040 ·034 ·028 ·022 ·017 ·011 ·005	100 85 71 57 45 32 21 9	-048 -042 -036 -030 -024 -019 -013 -007 -001	100 86 72 59 47 35 23 12 2	-050 -044 -038 -032 -027 -021 -015 -009 -003	100 86 73 60 49 37 26 15 6	·052 ·046 ·041 ·035 ·029 ·023 ·017 ·012 ·006	100 87 74 61 51 39 29 19
#		· D	EGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEĽ	г.	'
hrenhe	5	•	6	>	7	>	S	0	9	0	10	0
t t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c c} 0^{\circ} \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 3 \\ 4 \\ 4 \\ 4 \\ 5 \\ 5 \\ 4 \\ 4 \\ 5 \\ 5 \\ 6 \\ 2 \end{array}$	-055 -049 -043 -037 -031 -026 -020 -014 -008 -002	100 87 75 62 52 42 82 22 13 4	-057 -051 -045 -046 -034 -028 -022 -017 -011 -005	100 87 76 64 54 44 85 25 16	-060 -054 -048 -042 -036 -031 -025 -019 -013 -007 -002	100 88 77 66 56 46 87 27 19 10 2	-062 -057 -051 -045 -039 -033 -028 -022 -016 -010 -004	100 88 77 68 57 48 39 30 21 13 6	-065 -059 -054 -048 -042 -036 -030 -025 -019 -013 -007 -001	100 89 78 69 59 49 41 32 24 16 9	-068 -062 -057 -051 -045 -039 -033 -028 -022 -016 -010 -004	100 89 79 70 60 51 43 84 27 19 12 5

eit.		Г	EGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEIT		
t — t' Fahrenheit.	11	0	12	0	13	0	14	0	15	0	16	0
t - t' F	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c} 0 \\ \frac{1}{2} \\ 1 \\ \frac{1}{2} \\ 2 \\ \frac{1}{2} \\ 3 \\ \frac{1}{2} \\ 4 \\ \frac{1}{2} \\ 5 \\ \frac{1}{2} \\ 6 \\ \frac{1}{2} \\ 7 \\ 7 \\ \frac{1}{2} \end{array}$	-071 -066 -060 -054 -042 -037 -031 -025 -019 -019 -002	100 90 80 71 62 53 45 87 29 22 15 8	075 069 063 057 051 046 040 034 028 022 011 005	100 90 81 72 63 55 46 39 31 24 18 11	078 072 067 061 055 049 043 038 032 026 020 014 008 003	100 91 81 73 64 56 48 41 34 27 20 13 8	082 076 070 065 059 053 047 041 036 030 024 018 012 006 001	100 91 82 74 65 58 50 43 36 29 23 17 11 6	086 080 074 068 063 057 051 045 039 034 022 016 010 004	100 91 83 75 67 59 52 45 38 32 25 20 14 9 4	·090 ·084 ·078 ·072 ·061 ·055 ·049 ·043 ·032 ·026 ·020 ·014 ·008	100 91 83 75 68 60 53 47 40 84 28 22 17 12 7
beit.		D	EGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEI'	r.	
Fahrei	17	10	18	0	19	٥	20)°	21	l°	25	2 °
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Hunnidity.	Force of Valuation inches.	Relative Hamidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c} 0^{\circ} \\ \cdot \frac{1}{2} \\ 1 \\ 1 \\ \frac{1}{2} \\ 2 \\ 2 \\ \frac{1}{2} \\ 2 \\ \frac{1}{2} \\ 3 \\ \frac{1}{2} \\ 4 \\ 4 \\ \frac{1}{2} \\ 5 \\ \frac{1}{2} \\ 6 \\ 6 \\ \frac{1}{2} \\ 7 \\ 7 \\ \frac{1}{2} \\ 8 \\ \frac{1}{2} \\ 9 \\ \frac{1}{2} \\ 9 \\ \frac{1}{2} \\ 10 \\ \end{array}$	-094 -088 -082 -077 -071 -065 -059 -053 -042 -036 -030 -024 -018 -012 -007 -001	100 92 84 76 69 62 55 48 42 36 31 25 20 15 10	-098 -093 -087 -081 -075 -069 -064 -058 -052 -046 -040 -034 -023 -017 -011 -005	100 92 84 77 70 63 56 50 44 38 33 27 22 17 12 8	-103 -097 -091 -085 -080 -074 -068 -062 -056 -051 -044 -039 -033 -027 -021 -015 -010 -004	100 92 85 78 71 64 58 52 46 40 35 29 24 20 15 11 7	-108 -102 -096 -0996 -084 -079 -073 -067 -061 -055 -049 -043 -032 -026 -020 -014 -009	100 92 85 78 71 65 59 47 42 87 27 22 17 13 9 5	-113 -107 -101 -095 -089 -083 -077 -071 -060 -054 -048 -048 -047 -031 -025 -013 -007 -001	100 93 86 79 72 66 60 54 49 43 39 34 29 24 20 16 12 8 4	·118 ·112 ·106 ·100 ·094 ·088 ·082 ·077 ·071 ·065 ·059 ·053 ·048 ·042 ·030 ·024 ·018 ·012 ·006	100 93 86 79 73 67 61 56 51 40 36 31 27 22 18 14 11

reit.		D	EGREES	OF TI	E WET	BULB '	THERMO	METER	.—FAHRI	ENHEIT		_
— t' Fabrenheit.	28	B°	24	lo	25	0	20	3°	21	yo	28	30
t—t/F	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° $\frac{1}{2}$ 1 $1^{\frac{1}{2}}$	·123 ·117 ·111 ·105	100 93 86 80	·129 ·123 ·117 ·111	100 93 87 81	·135 ·129 ·123 ·117	100 93 87 82	·141 ·135 ·129 ·123	100 93 88 82	·147 ·141 ·135 ·129	100 93 88 82	·153 ·147 ·142 ·136	100 94 88 83
$\frac{2}{2}$ $\frac{21}{2}$ $\frac{3}{2}$	·100 ·094 ·088 ·082	$ \begin{array}{c c} 74 \\ 68 \\ 62 \\ 57 \end{array} $	·105 ·099 ·093 ·088	75 69 63 58	·111 ·105 ·099 ·093	75 70 64 59	·117 ·111 ·105 ·099	76 71 66 61	·123 ·117 ·111 ·106	77 72 67 62	·130 ·124 ·118 ·112	78 73 68 63
4 4½ 5 5½	·076 ·070 ·065 ·059	52 47 42 37	·082 ·076 ·070 ·064	53 48 44 39	·087 ·082 ·076 ·070	54 50 45 41	·093 ·088 ·082 ·076	56 51 47 43	·100 ·094 ·088 ·082	57 53 49 44	·106 ·100 ·094 ·089	58 54 50 46
$\begin{array}{c c} & & & & & & & & & & & & & & & & & & &$	·053 ·047 ·041 ·035	33 29 25 21	·058 ·053 ·047 ·041	35 31 27 23	·064 ·058 ·052 ·046	37 33 29 25	·070 ·064 ·058 ·052	39 35 31 27	·076 ·070 ·064 ·059	40 37 33 29	·083 ·077 ·071 ·065	42 38 35 31
8 81 9 91	·029 ·023 ·017 ·011	17 13 10 6	.035 .029 .023 .017	19 15 12 9	·041 ·035 ·029 ·023	21 18 14 11	·047 ·041 ·035 ·029	24 20 17 14	·053 ·047 ·041 ·035	26 22 19 16	·059 ·053 ·047 ·041	28 24 21 18
$ \begin{array}{ c c c c } \hline 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{3} \end{array} $.006	3	·012 ·006	6 3	·017 ·011 ·005	8 5 2	·023 ·017 ·011 ·005	11 8 5 2	·029 ·023 ·017 ·011	13 10 8 5	·036 ·030 ·024 ·018	15 13 10 7
12 $12\frac{1}{2}$							009	-	.006	2	·012 ·006	5 2

heit.		ľ	EGREES	OF TH	IE WET	BULB	THERMO)METER	.—FAIIR	ENHEL	Γ.	
— U Fahrenheit.	29	°	30)°.	31	Į°	32	<u>P</u> o	33	80	3.	10
t – V I	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches,	Relative Humidity.
0° 1 1 1 1 1 1 2	·160 ·154 ·148 ·142	100 94 89 84	·167 ·161 ·155 ·149	100 95 89 84	·174 ·168 ·162 ·156	100 95 89 85	·181 ·175 ·168 ·162	100 94 89 84	·188 ·182 ·175 ·169	100 95 89 84	·196 ·190 ·183 ·177	100 95 90 85
$ \begin{array}{c c} 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \end{array} $	·136 ·130 ·125 ·119	78 74 69 64	·143 ·137 ·131 ·126	79 74 70 65	·150 ·144 ·138 ·133	80 75 71 66	·155 ·149 ·142 ·136	79 74 70 65	·162 ·156 ·149 ·143	80 75 71 66	·170 ·164 ·157 ·151	80 76 71 67
$ \begin{array}{c c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array} $	·113 ·107 ·101 ·095	60 56 51 48	·120 ·114 ·108 ·102	61 57 53 49	·127 ·121 ·115 ·109	58 54 51	·129 ·123 ·116 ·110	61 57 53 49	·136 ·130 ·123 ·117	58 54 50	·144 ·138 ·131 ·124	63 59 55 51
$\begin{bmatrix} 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{bmatrix}$.089 .083 .077 .072	44 40 36 33	.096 .090 .084 .078	45 42 38 35	·103 ·097 ·091 ·085	47 43 40 37	·103 ·097 ·090 ·084	45 41 38 34	·110 ·104 ·097 ·091	46 43 39 36	·118 ·111 ·105 ·098	48 44 41 37
$ \begin{array}{c c} 8 \\ 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2} \end{array} $	•066 •060 •054 •048	30 26 23 21	·072 ·067 ·061 ·055	32 28 25 23	·079 ·074 ·068 ·062	34 30 27 25	·077 ·071 ·064 ·058	31 28 25 22	.084 .078 .071 .065	33 30 27 24	.092 .085 .079 .072	34 31 28 26
$ \begin{array}{c c} 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \end{array} $	·042 ·036 ·030 ·024	18 15 12 10	·049 ·043 ·037 ·031	$ \begin{array}{c c} 20 \\ 17 \\ 14 \\ 12 \end{array} $.056 .050 .044 .038	19 17 14	·051 ·045 ·038 ·032	19 16 14 11	•058 •052 •045 •039	21 18 16 13	.066 .059 .053 .046	23 20 18 15
$egin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \\ \end{array}$	•019 •013 •007 •001	7 5 2 0	·025 ·019 ·013 ·008	9 7 5 3	.032 .026 .020 .015	12 10 7 5	·025 ·019 ·012 ·006	$\begin{bmatrix} 9 \\ 6 \\ 4 \\ 2 \end{bmatrix}$	·032 ·026 ·019 ·013	11 8 6 4	·040 ·033 ·027 ·020	13 11 8 6
$ \begin{array}{c c} 14 \\ 14\frac{1}{2} \\ 15 \end{array} $			•002	1	.003	3	•••••	•••••			·014 ·007 ·001	$\begin{bmatrix} 4\\2\\0 \end{bmatrix}$

eit		D	EGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEIT	2.	
ahrenb	35	o°	36	°	37	7°	38	3° .	39)°	4()°
t — t' Fahrenheit.	Force of Vapor, in inches,	Relative Humidity.	Force of Vapor. in inches.	Relative Humidity.	Force of vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$\begin{array}{c} 0 \\ 0 \\ 1 \\ 1 \\ 1 \\ 2 \\ 2 \\ 2 \\ 1 \\ 2 \\ 2 \\ 2$	-204 -197 -191 -184 -178 -158 -152 -145 -139 -139 -113 -106 -109 -093 -087 -080 -074 -067 -061 -054 -048 -041 -035 -028 -022 -015 -008	100 95 90 85 81 76 68 63 60 56 52 49 45 42 39 36 33 30 27 25 22 21 17 15 13 10 8 6 4 4 1	·212 ·206 ·199 ·193 ·186 ·180 ·173 ·167 ·160 ·154 ·147 ·121 ·114 ·108 ·101 ·095 ·088 ·082 ·075 ·069 ·049 ·043 ·030 ·023 ·016 ·010 ·003	100 95 90 86 81 77 73 68 64 61 57 53 50 47 43 40 37 34 32 29 26 24 21 19 16 14 12 10 8 6 4 11 12 10 11 11 11 11 11 11 11 11 11	-221 -214 -208 -201 -195 -182 -175 -169 -162 -155 -149 -137 -130 -124 -117 -111 -103 -097 -090 -083 -077 -070 -064 -057 -051 -044 -038 -031 -025 -018 -012 -005	100 95 91 86 82 77 73 69 65 61 58 45 42 30 36 33 30 28 25 20 18 16 14 12 10 8 6 5	-229 -223 -216 -210 -203 -197 -190 -184 -177 -171 -164 -157 -151 -144 -138 -131 -125 -099 -092 -086 -069 -073 -066 -060 -053 -047 -040 -033 -027 -020 -014 -007 -001	100 95 91 86 82 78 74 70 66 62 55 52 49 46 43 32 29 27 24 22 20 18 16 14 12 10 8 7 5 3 4 6 6 18 18 18 18 18 18 18 18 18 18	-238 -232 -225 -219 -212 -206 -199 -193 -186 -180 -173 -166 -152 -146 -139 -133 -126 -120 -113 -107 -101 -094 -088 -081 -075 -068 -062 -055 -049 -042 -036 -023 -016 -010 -003	100 95 91 87 82 78 74 71 67 63 60 56 53 50 47 44 41 39 36 33 31 28 24 22 19 17 15 16 17 17 18 18 18 18 18 18 18 18 18 18	-248 -241 -235 -228 -222 -215 -209 -202 -196 -189 -163 -156 -150 -143 -137 -130 -124 -117 -110 -097 -091 -084 -097 -091 -045 -058 -051 -045 -032 -025 -019 -012 -006	100 95 91 87 83 79 75 71 68 64 61 57 54 45 43 40 37 85 22 23 21 19 10 8 7 5 4 4 11 12 10 8 11 11 11 11 11 11 11 11 11 11 11 11 1

eit.		1	DEGREES	OF TI	IE WET	BULB	THERMO	METER	FAHR	ENHEIT		
ahrenh	41	Lo	42	0	43	0	41.1	to	4.5	٥	40	0
t — ť Fáhrenheit.	Force of Vapor, in inches.	Relative Humidity.										
$ \begin{array}{c c} 0^{\circ} \\ 1^{\frac{1}{2}} \\ 1_{\frac{1}{2}} \end{array} $	·257 ·251 ·244 ·237	100 96 91 87	·267 ·261 ·254 ·248	100 96 92 88	·278 ·271 ·265 ·258	100 96 92 88	·289 ·282 ·275 ·269	100 96 92 88	·300 ·293 ·286 ·280	100 96 92 88	·311 ·305 ·298 ·291	100 96 92 89
$\frac{2}{2\frac{1}{2}}$ $\frac{3}{2}$	·231 ·224 ·218 ·211	83 79 76 72	·241 ·234 ·228 ·221	84 80 76 72	·251 ·245 ·238 ·232	84 80 77 73 70	·262 ·256 ·249 ·242 ·236	84 81 77 74 70	·273 ·267 ·260 ·253 ·247	85 81 78 74 71	·285 ·278 ·272 ·265 ·258	85 81 78 75 71
$ \begin{array}{c c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \\ 6 \end{array} $	·204 ·198 ·192 ·185 ·179	68 65 62 58 55	·215 ·208 ·202 ·195 ·189	69 66 62 59 56	·225 ·218 ·212 ·205 ·199	66 63 60 57	·229 ·223 ·216 ·210	67 64 61 58	·240 ·234 ·227 ·221	68 65 62 59	·252 ·245 ·239 ·282	68 65 63 60
$\begin{array}{c} 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 8 \end{array}$	·172 ·165 ·159 ·152	52 49 47 44	·182 ·175 ·169 ·162	53 50 48 45	·192 ·186 ·179 ·173	54 51 49 46	·203 ·196 ·190 ·183	55 52 50 47	·214 ·208 ·201 ·194	56 53 51 48	·226 ·219 ·212 ·206	57 54 52 49
$ \begin{array}{c} 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2} \end{array} $ 10	·146 ·139 ·132 ·126	41 39 36 34	·156 ·149 ·142 ·136	42 40 37 35	·166 ·159 ·153 ·146	43 41 39 36	·177 ·170 ·163 ·157	45 42 40 38	·188 ·181 ·175 ·168	46 43 41 39	·199 ·193 ·186 ·179	47 44 42 40 38
$10\frac{1}{2}$ 11 $11\frac{1}{2}$ 12	·120 ·113 ·106 ·100	31 29 27 25 23	·130 ·123 ·116 ·110 ·103	33 30 28 26	·140 ·133 ·127 ·120 ·113	34 32 30 28 26	·151 ·144 ·137 ·131 ·124	35 33 31 29 27	·162 ·155 ·148 ·142 ·135	37 34 32 30 28	·173 ·166 ·160 ·153 ·147	36 34 32 30
$egin{array}{c} 12rac{1}{2} \\ 13 \\ 13rac{1}{2} \\ 14 \\ 14rac{1}{2} \\ \end{array}$	·093 ·087 ·080 ·073 ·067	23 21 19 17 15	·097 ·090 ·083 ·077	24 22 20 19 17	·107 ·100 ·094 ·087	24 22 20 18	·124 ·118 ·111 ·104 ·098	25 23 22	·129 ·122 ·115 ·109	27 25 23 21	·140 ·133 ·127 ·120	28 26 25 23
$egin{array}{c c} 145 \\ 15 \\ 15\frac{1}{2} \\ 16 \\ 16\frac{1}{2} \\ \end{array}$	·061 ·054 ·048 ·041	13 12 10 9	.071 .064 .057 .051	15 13 12 10	·068 ·061	17 15 13 12	·091 ·085 ·078 ·072	20 18 17 15 13	·102 ·096 ·089 ·082	20 18 17 15	·114 ·107 ·101 ·094	21 20 18 16
$egin{array}{c c} 16rac{1}{2} \\ 17 \\ 17rac{1}{2} \\ 18 \\ 18rac{1}{2} \\ \end{array}$	·034 ·028 ·021 ·015	7 6 4 3	·044 ·038 ·031 ·024	9 7 6 5	·054 ·048 ·041 ·035	10 9 7 6	·065 ·058 ·052 ·045	112 111 9 8	.062 .069 .063 .056	14 12 11 10	·087 ·081 ·074 ·068	15 14 12 11
$egin{array}{c} 19 \ 19 \ 20 \ \end{array}$	·001	0	·018 ·011 ·005	3 2 1	·028 ·021 ·015 ·009	5 4 2 1	·039 ·032 ·026 ·019	7 5 4	·049 ·043 ·037 ·030	8 7 6 5	·061 ·054 ·048 ·041	10 9 7 6
$ \begin{array}{c c} 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \\ 22 \\ 201 \end{array} $.009	0	·013 ·006	2 2 1	·023 ·017 ·010 ·004	3 2 1	·035 ·028 ·022 ·015	5 4 3 2 1
$\begin{array}{c} 22 \\ 22 \\ 23 \\ 23 \\ 23 \\ 2 \end{array}$									7004	1	·008 ·002	1 0

heit.		D	EGREES	OF TH	E WET	BULB '	riiermo	METER	.—FAHRI	ENHEIT		
Fahren	47	10	48	90	49)°	50	0	51	٥	52	0
t — t' Fahrenbeit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	·323 ·316 ·310 ·303	100 96 92 89	•335 •329 •322 •315	100 96 92 89	·348 ·341 ·335 ·328	100 96 93 89	·361 ·354 ·348 ·341	100 96 93 89	·374 ·368 ·361 ·354	100 96 93 90	·388 ·382 ·375 ·369	10 9 9 9
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	·297 ·290 ·283 ·277	85 82 78 75	·309 ·302 ·296 ·289	85 82 79 76	·321 ·315 ·308 ·302	86 83 79 76	-334 -328 -321 -315	86 83 80 77	•348 •341 •335 •328	86 83 80 77	·362 ·355 ·349 ·342	8 8 8 7
$4 \\ 4\frac{1}{5} \\ 5\frac{1}{2}$	·270 ·264 ·257 ·251	72 69 66 63	·282 ·276 ·269 ·263	73 70 67 64	·295 ·288 ·282 ·275	73 70 67 65	·308 ·301 ·295 ·288	74 71 68 65	 321 315 308 302 	74 71 69 66	·336 ·329 ·322 ·316	77 6
$\frac{6}{6\frac{1}{2}}$ $\frac{7}{7\frac{1}{2}}$	·244 ·237 ·231 ·224	60 58 55 52	·256 ·249 ·243 ·236	61 59 56 53	·269 ·262 ·255 ·249	62 59 57 54	·282 ·275 ·268 ·262	63 60 58 55	·295 ·288 ·282 ·275	63 61 58 56	·309 ·302 ·296 ·289	()
8 8½ 9 9½	·218 ·211 ·204 ·198	50 48 45 43	·230 ·223 ·216 ·210	51 49 46 44	·242 ·236 ·229 ·222	52 50 47 45	·255 ·249 ·242 ·235	53 51 48 46	·269 ·262 ·255 ·249	54 51 49 47	·283 ·276 ·269 ·263	£ £
$\begin{bmatrix} 0 \\ 10 \\ 2 \\ 11 \\ 11 \\ 11 \\ 2 \end{bmatrix}$	·191 ·185 ·178 ·171	41 39 37 35	·203 ·197 ·190 ·183	42 40 38 36	·216 ·209 ·203 ·196	43 41 39 37	·229 ·222 ·216 ·209	44 42 40 38	·242 ·235 ·229 ·222	45 43 41 39	·256 ·249 ·243 ·236	4
2 2½ 3 3½	·165 ·158 ·152 ·145	33 31 29 27	·177 ·170 ·164 ·157	34 32 30 29	·189 ·183 ·176 ·170	35 33 32 30	·202 ·196 ·189 ·182	36 35 33 31	·216 ·209 ·203 ·196	37 36 34 32	·230 ·223 ·216 ·210	
$\begin{vmatrix} 4 \\ 14 \\ 5 \end{vmatrix}$ $\begin{vmatrix} 5 \\ 15 \\ 2 \end{vmatrix}$	·138 ·132 ·125 ·119	26 24 22 21	·150 ·144 ·137 ·131	27 25 24 22	·163 ·156 ·150 ·143	28 27 25 23	·176 ·169 ·163 ·156	29 28 26 25	·189 ·183 ·176 ·169	31 29 27 26	·203 ·197 ·190 ·183	
$16 \\ 16 \\ \frac{1}{2} \\ 17 \\ \frac{1}{2}$	·112 ·106 ·099 ·092	19 18 16 15	·124 ·118 ·111 ·104	21 19 18 16	·137 ·130 ·123 ·117	22 21 19 18	·149 ·143 ·136 ·130	23 22 21 19	·163 ·156 ·150 ·143	25 23 22 20	·177 ·170 ·163 ·157	
18 18½ 19 19½	·086 ·079 ·073 ·066	14 12 11 10	·098 ·091 ·085 ·078	15 14 13 11	·110 ·104 ·097 ·090	17 15 14 13	·123 ·116 ·110 ·103	18 17 15 14	·136 ·130 ·123 ·117	19 18 17 16	·150 ·144 ·137 ·130	4
$20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2}$	·059 ·053 ·046 ·040	9 8 7 6	·071 ·065 ·058 ·052	10 9 8 7	·084 ·077 ·071 ·064	12 11 10 8	·097 ·090 ·083 ·077	13 12 11 10	·110 ·103 ·097 ·090	14 13 12 11	·124 ·117 ·110 ·104	
22 22½ 23 23½	·033 ·027 ·020 ·013	3 2 2	·045 ·038 ·032 ·025	6 4 4 3	·057 ·051 ·044 ·038	7 6 5 5	·070 ·064 ·057 ·050	9 8 7 6	·083 ·077 ·070 ·064	10 9 8 7	·097 ·091 ·084 ·077	
24 24 <u>1</u> 25	·007 ·001	0	·019 ·012 ·005	$\begin{array}{c c} 2\\1\\0\end{array}$	·031 ·024 ·018	4 3 2	·044 ·037 ·030	5 4 3	·057 ·050 ·044	6 6 5	·071 ·064 ·057	

jį.		I	DEGREES	OF TI	IE WET	BULB	THERM	OMETEI	R.—FAHR	ENHEI	r.	
ahrenhe	53	0	54	ţo	55	,0	56	0	57	γο	58	30
t — t' Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.										
0°	•403 •396 •390 •383	100 96 93 90	·418 ·411 ·405 ·398	100 97 94 90	·433 ·427 ·420 ·413	100 97 94 90	·449 ·443 ·436 ·429	100 97 94 91	·466 ·459 ·452 ·446	100 97 94 91	·483 ·476 ·469 ·462	100 97 94 91
$ \begin{array}{c c} 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \end{array} $	•376 •370 •363 •357	87 84 81 78	·391 ·385 ·378 ·372	87 84 81 78	·407 ·400 ·394 ·387	87 84 82 79	·423 ·416 ·410 ·403	88 85 82 79	·489 ·433 ·426 ·419	88 85 82 80	·456 ·449 ·442 ·436	88 85 83 80
$egin{array}{c} 4 \\ 4rac{1}{2} \\ 5 \\ 5rac{1}{2} \end{array}$	-350 -343 -337 -330	75 72 70 67	·365 ·358 ·352 ·345	76 73 70 68	·380 ·374 ·367 ·360	76 73 71 68	·396 ·390 ·383 ·376	76 74 71 69	·413 ·406 ·399 ·392	77 74 72 69	·429 ·422 ·416 ·409	77 75 72 70
$\begin{bmatrix} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{bmatrix}$	·323 ·317 ·310 ·304	65 62 60 57	·338 ·332 ·325 ·319	65 63 61 58	·354 ·347 ·340 ·334	66 64 61 59	·370 ·363 ·356 ·350	66 64 62 60	·386 ·379 ·378 ·366	67 65 62 60	·403 ·396 ·389 ·383	67 65 63 61
$ \begin{array}{c c} 8 \\ 81 \\ 9 \\ 91 \\ \end{array} $	·297 ·290 ·284 ·277	55 53 51 49	·312 ·305 ·299 ·292	56 54 52 50	·327 ·321 ·314 ·307	57 55 53 51	·343 ·337 ·330 ·323	57 55 53 51	·359 ·353 ·346 ·340	58 56 54 52	·376 ·369 ·362 ·356	59 56 55 53
$ \begin{array}{ c c c c } \hline 10 \\ 10\frac{1}{2} \\ 11 \\ \hline 11\frac{1}{2} \\ \hline \end{array} $	·270 ·264 ·257 ·251	47 45 43 41	·285 ·279 ·272 ·265	48 46 44 42	·301 ·294 ·287 ·281	49 47 45 43	•316 •310 •303 •296	49 48 46 44	·333 ·326 ·319 ·313	50 48 47 45	·349 ·343 ·336 ·329	51 49 47 46
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	·244 ·237 ·231 ·224	39 38 36 34	·259 ·252 ·246 ·239	40 39 37 35	·274 ·268 ·261 ·254	41 40 38 36	·290 ·283 ·277 ·270	42 41 39 37	·306 ·300 ·293 ·286	43 41 40 38	·323 ·316 ·309 ·303	44 42 41 39
$egin{array}{c c} 14 \\ 14rac{1}{2} \\ 15 \\ 15rac{1}{2} \\ \end{array}$	·218 ·211 ·204 ·198	33 31 30 28	·232 ·226 ·219 ·212	34 32 31 29 28	•248 •241 •234 •228	35 33 32 30	•263 •257 •250 •243	36 34 33 31	·280 ·273 ·266 ·259	37 35 34 32	·296 ·289 ·283 ·276	38 36 35 33
$ \begin{array}{ c c c c } \hline 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \\ 18 \\ \end{array} $	·191 ·184 ·178 ·171	27 25 24 23	·206 ·199 ·193 ·186	27 25 24	·221 ·214 ·208 ·201	29 28 26 25	·237 ·230 ·223 ·217	30 29 27 26	·253 ·246 ·240 ·233	31 30 28 27	·270 ·263 ·256 ·249	32 31 29 28
$ \begin{array}{ c c c } & 18 \\ & 18\frac{1}{2} \\ & 19 \\ & 19\frac{1}{2} \\ & 20 \\ \end{array} $	·165 ·158 ·151 ·145	22 20 19 18	·179 ·173 ·166 ·160	23 22 20 19	·195 ·188 ·181 ·175	24 23 22 20	·210 ·204 ·197 ·190	25 24 23 21 20	·226 ·220 ·213 ·207	26 25 24 22	·243 ·236 ·229 ·223 ·216	27 26 25 23 22
$ \begin{array}{c c} 20 \\ 20 \\ 21 \\ 21 \\ 22 \end{array} $	·138 ·131 ·125 ·118 ·112	17 16 15 14 13	·153 ·146 ·139 ·133 ·126	18 17 16 15	·168 ·161 ·155 ·148 ·141	19 18 17 16 15	·183 ·177 ·170 ·164 ·157	19 18 17 16	·200 ·193 ·186 ·180 ·173	21 20 19 18 17	·216 ·210 ·203 ·196 ·190	21 20 19 18
$ \begin{array}{ c c c } & 22 \\ & 22 \\ & 23 \\ & 23 \\ & 24 \\ \end{array} $	·112 ·105 ·098 ·092 ·085	12 11 10 9	·126 ·120 ·113 ·106 ·100	13 12 11 10	·141 ·135 ·128 ·122 ·115	13 13 12 12	·150 ·144 ·137 ·131	15 14 14 14	·167 ·160 ·153 ·147	16 16 15 14	·183 ·176 ·169 ·163	18 18 17 16
$\begin{bmatrix} 24\\ 24\\ 25 \end{bmatrix}$	·079 ·072	8 7	·093 ·086	10 9	·108 ·101	11 10	124	12 12 11	·140 ·133	13 12	·156 ·150	14 13

hren	59	0	60°		. 61	0	62	20	68	3 °	6-	L°
t — V Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, iu inches.	Relative Humidity.	Force of Vapor, in inches.	Relative
0° 1	·500 ·493 ·487 ·480	100 97 94 91	·518 ·511 ·505 ·498	100 97 94 91	·537 ·530 ·523 ·517	100 97 94 91	·556 ·549 ·543 ·536	100 97 94 92	·576 ·569 ·563 ·556	100 97 94 92	·596 ·590 ·583 ·576	10 9 9
$\frac{2}{2\frac{1}{2}}$ $\frac{2}{3}$ $\frac{1}{3}$	·473 ·466 ·460 ·453	88 85 83 80	·491 ·485 ·478 ·471	88 86 83 81	·510 ·503 ·497 ·490	88 86 83 81	·529 ·523 ·516 ·509	89 86 84 81	•549 •542 •536 •529	89 87 84 82	•570 •563 •556 •550	8 8
$\frac{4}{4\frac{1}{2}}$ $\frac{5}{5\frac{1}{2}}$	·446 ·440 ·433 ·427	77 75 73 71	·464 ·458 ·451 ·444	77 75 78 71	·483 ·476 ·470 ·463	78 75 73 71	·502 ·496 ·489 ·483	78 77 75 72	•522 •516 •509 •502	79 77 75 72	•543 •586 •529 •523	777777777777777777777777777777777777777
$\begin{array}{c c} 6 & \\ 6\frac{1}{2} & \\ 7 & \\ 7\frac{1}{2} & \end{array}$	·420 ·413 ·407 ·400	68 66 63 61	·438 ·431 ·425 ·418	68 66 64 62	·457 ·450 ·443 ·487	69 67 65 63	·476 ·469 ·462 ·456	69 67 65 63	·496 ·490 ·482 ·476	70 68 66 64	·516 ·509 ·503 ·496	7 6 6
$8 \\ 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2}$	•393 •386 •380 •373	59 57 56 54	·411 ·405 ·398 ·391	58 56 54	·430 ·423 ·416 ·410	61 59 57 55	·449 ·442 ·436 ·429	59 57 55	·469 ·462 ·455 ·449	62 60 58 56	·489 ·483 ·476 ·469	6
$egin{array}{c c} 10 & & & \\ 10 rac{1}{2} & & & \\ 11 & & & \\ 11 rac{1}{2} & & & \\ \end{array}$	·367 ·360 ·353 ·347	$ \begin{array}{r} 52 \\ 50 \\ 48 \\ 46 \end{array} $	·385 ·378 ·371 ·365	53 51 49 47	·403 ·397 ·390 ·383	54 52 50 48	·422 ·416 ·409 ·402	54 52 50 49	·442 ·436 ·429 ·422	55 53 51 49	·463 ·456 ·449 ·443	10 10 10
$egin{array}{c} 12 \ 12 \ 13 \ 13 \ 13 \ 2 \ \end{array}$	·310 ·333 ·327 ·320	45 43 42 40	·358 ·351 ·345 ·338	46 44 42 41	·376 ·370 ·363 ·356	47 45 43 42	·396 ·389 ·382 ·376	48 46 44 42	·415 ·409 ·402 ·395	48 46 45 43	·436 ·429 ·422 ·416	4 4 4
$14 \\ 14 \\ 2 \\ 15 \\ 2 \\ 2 \\ 2 \\ 3 \\ 3 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 5 \\ 4 \\ 4 \\ 4 \\ 4$	·313 ·306 ·300 ·293	39 37 36 35	·331 ·324 ·318 ·311	39 38 37 35	·350 ·343 ·336 ·330	40 39 37 36	·369 ·362 ·356 ·349	41 40 38 37	·389 ·382 ·375 ·369	42 40 39 38	·409 ·402 ·396 ·389	4 4 4
$egin{array}{c} 16 \ 16 \ 17 \ 17 \ 1 \ 1 \ 2 \ \end{array}$	·287 ·280 ·273 ·267	33 32 30 29	·305 ·298 ·291 ·285	34 33 31 30	·323 ·316 ·310 ·303	35 34 32 31	·342 ·336 ·329 ·322	36 34 33 32	·362 ·355 ·349 ·342	36 35 34 33	·382 ·376 ·369 ·362	5
$18 \\ 18 \\ 19 \\ 19 \\ 19 \\ 19 \\ 1$	·260 ·253 ·247 ·240	28 27 26 25	·278 ·271 ·264 ·258	29 28 27 26	·296 ·290 ·283 ·276	30 29 28 26	·315 ·309 ·302 ·295	31 30 28 27	·335 ·328 ·322 ·315	32 30 29 28	·355 ·349 ·342 ·335	00000
$20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2}$	·234 ·227 ·220 ·213	23 22 21 20	·251 ·245 ·238 ·231	24 23 22 21	·270 ·263 ·256 ·250	25 24 23 22	·289 ·282 ·275 ·269	26 25 24 23	·308 ·302 ·295 ·288	27 26 25 24	·329 ·322 ·315 ·309	010101
$\begin{array}{c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \end{array}$	·207 ·200 ·193 ·187	19 19 18 17	·225 ·218 ·211 ·205	21 20 19 18	·243 ·236 ·230 ·223	22 21 20 19	·262 ·255 ·249 ·242	22 22 21 20	·282 ·275 ·268 ·262	23 22 22 21	·302 ·295 ·289 ·282	64 64 64 64
$24 \\ 24 \\ 25$	·180 ·173 ·167	16 15 14	·198 ·191 ·185	17 16 15	·216 ·209 ·203	18 17 16	·234 ·228 ·222	19 18 17	·255 ·248 ·241	20 19 18	·275 ·268 ·262	2 2 1

it.		D	EGREES	ог тн	E WET	BULB 7	HERMO!	METER	—FAHRI	ENHEIT	•	
— ť Fahrenheit.	65	0	66	0	67	0	68	0	69	0	70	,0
t-t'E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of · Vapor, in inches.	Relative Humidity.	Force of Vapor. in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
$ \begin{array}{c c} 0^{\circ} \\ \frac{1}{2} \\ 1 \\ 1\frac{1}{2} \\ 2 \\ 2\frac{1}{2} \\ 3 \end{array} $	·618 ·611 ·604 ·598 ·591 ·584 ·577	100 97 94 92 89 87 85	·639 ·633 ·626 ·619 ·612 ·606 ·599	100 97 95 92 90 88	·662 ·655 ·648 ·642 ·635 ·628 ·621	100 97 95 92 90 88 85	·685 ·678 ·671 ·665 ·658 ·651 ·644	100 97 95 92 90 88 86	·708 ·702 ·695 ·688 ·682 ·675 ·668	100 97 95 92 90 88	·733 ·726 ·720 ·713 ·706 ·700 ·693	100 97 95 92 90 88 85
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	·577 ·564 ·557 ·551 ·544 ·537	82 79 77 75 73 71	·599 ·592 ·586 ·579 ·572 ·566 ·559	85 83 80 78 76 74 72	·621 ·615 ·608 ·601 ·595 ·588 ·581	83 80 78 76 74	·638 ·631 ·624 ·617 ·611 ·604	83 81 79 77 75 73	·662 ·655 ·648 ·641 ·635 ·628	86 83 81 79 77 75 73	·686 ·680 ·673 ·666 ·659 ·652	83 81 79 77 75 73
$ \begin{array}{c c} 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 8 \\ 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2} \end{array} $	·530 ·524 ·517 ·510 ·504 ·497 ·490	69 66 64 63 61 59 58	•552 •545 •539 •532 •525 •519 •512	70 67 65 63 61 60 58	·574 ·568 ·561 ·554 ·548 ·541 ·534	70 67 65 64 62 60 59	·597 ·591 ·584 ·577 ·571 ·564 ·557	71 68 66 64 63 61 59	·621 ·614 ·608 ·601 ·594 ·588 ·581	71 68 67 65 63 62 60	·646 ·639 ·632 ·626 ·619 ·612 ·606	71 69 67 65 64 62 60
$ \begin{array}{ c c c c c } \hline 10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \\ 12 \\ \hline \end{array} $	·484 ·477 ·470 ·463 ·457	56 54 52 51 49	·505 ·498 ·492 ·485 ·478	56 55 53 52 50	·527 ·521 ·514 ·507 ·501	57 55 54 52 51	·550 ·544 ·537 ·530 ·523	58 56 54 53 51	·574 ·567 ·561 ·554 ·547	58 57 55 53 52	-599 -592 -585 -578 -572	59 57 56 54 52
$ \begin{array}{c c} 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \\ 14 \\ 14\frac{1}{2} \\ 15 \end{array} $	·450 ·443 ·437 ·430 ·423 ·417	48 46 45 43 42 41	·472 ·465 ·458 ·452 ·445 ·438	48 47 46 44 43 41	·494 ·487 ·481 ·474 ·467 ·460	49 48 46 45 43 42	·517 ·510 ·503 ·497 ·490 ·483	50 48 47 45 44 43	·541 ·534 ·527 ·520 ·514 ·507	50 49 48 46 45 43	·565 ·558 ·552 ·545 ·538 ·531	51 50 48 47 45 44
$ \begin{array}{c c} 15\frac{1}{2} \\ 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \end{array} $	·410 ·403 ·396 ·390 ·383	39 38 37 36 34	·432 ·425 ·417 ·410 ·404	39 38 36 35	·454 ·447 ·440 ·433 ·427	41 40 38 37 36	·476 ·470 ·463 ·456 ·450	42 40 39 38 37	·500 ·493 ·487 ·480 ·473	42 41 40 39 38	•525 •518 •511 •504 •498	43 42 41 39 38
$ \begin{array}{c c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \\ 20 \end{array} $	*376 *370 *363 *356 *350	33 32 31 30 29	·397 ·390 ·384 ·377 ·371	34 33 32 31 30	·420 ·413 ·407 ·400 ·393	35 34 33 32 31	·443 ·436 ·429 ·423 ·416	36 35 33 32 31	·467 ·460 ·453 ·446 ·440	36 35 34 33 32	·491 ·484 ·478 ·471 ·464	37 36 35 34 33
$ \begin{array}{c c} 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \end{array} $	343 -336 -330 -323 -316	28 27 26 25 24	•364 •358 •351 •344 •338	29 28 27 26 25	·386 ·380 ·373 ·366 ·360	30 29 28 27 26	·409 ·403 ·396 ·389 ·382	30 29 29 28 28 27	·433 ·426 ·419 ·413 ·406	31 30 29 28 28	·457 ·451 ·444 ·437 ·430	32 31 30 29 28
$ \begin{array}{c c} \hline $	-309	24 23 22 21 20	·331 ·324 ·317 ·311 ·304	24 23 23 22 21	·353 ·346 ·340 ·333 ·326	25 24 23 23 23 22	·376 ·369 ·362 ·356 ·349	26 25 24 23 22	·399 ·393 ·386 ·379 ·372	27 26 25 24 23	·424 ·417 ·410 ·404 ·397	27 27 26 25 24

heit.		1	EGREES	OF TI	E WET	BULB '	rhermo	METER.—FAHRENHEIT.					
abren	71	L°	7:	e°	73	B °	7-1	Į°	75	o	76		
t — t' Fabrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative	
0° 1 1 1 1 1	·759 ·752 ·745 ·739	100 98 95 93	·785 ·778 ·771 ·765	100 98 95 93	·812 ·805 ·798 ·792	100 98 95 93	·839 ·833 ·826 ·819	100 98 95 93	·868 ·861 ·854 ·847	100 98 95 93	·897 ·890 ·884 ·877	10 9 9 9	
01 01 01 01 01 01 01 01 01 01 01 01 01 0	·732 ·725 ·718 ·712	90 88 86 83	·758 ·751 ·745 ·738	90 88 86 84	·785 ·778 ·772 ·765	90 88 86 84	·812 ·805 ·799 ·792	91 88 86 84	·841 ·834 ·827 ·820	91 88 86 84	·870 ·863 ·856 ·850	8	
$\frac{4}{4\frac{1}{2}}$ $\frac{5}{5\frac{1}{2}}$	·705 ·698 ·691 ·685	81 79 77 75	·781 ·725 ·717 ·711	81 79 77 75	·758 ·751 ·744 ·738	82 80 78 76	·785 ·778 ·772 ·765	82 80 78 76	·813 ·807 ·800 ·793	82 80 78 76	·843 ·836 ·829 ·823	8	
$\frac{6}{6\frac{1}{2}}$ $\frac{7}{7\frac{1}{2}}$	·678 ·671 ·664 ·658	73 71 69 67	·704 ·697 ·691 ·684	73 71 69 67	·781 ·724 ·717 ·711	74 72 70 68	·758 ·751 ·745 ·738	74 72 70 69	·787 ·780 ·773 ·766	74 73 71 69	·816 ·809 ·802 ·795		
8 81 9 91	·651 ·644 ·638 ·631	66 64 62 61	·677 ·670 ·664 ·657	$66 \\ 64 \\ 62 \\ 61$	·704 ·697 ·691 ·684	66 65 63 61	·781 ·724 ·717 ·711	67 65 64 62	·759 ·753 ·746 ·739	$\begin{array}{c} 67 \\ 66 \\ 64 \\ 62 \end{array}$	·789 ·782 ·775 ·768		
$10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2}$	·624 ·617 ·610 ·604	59 58 56 54	•650 •643 •637 •630	59 58 56 54	·677 ·670 ·663 ·657	58 57 55	·704 ·698 ·691 ·684	59 57 56	·783 ·726 ·719 ·712	59 58 56	·762 ·755 ·748 ·741	(
$12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2}$	·597 ·590 ·584 ·577	53 51 50 49	·623 ·616 ·610 ·603	53 51 50 49	·650 ·643 ·637 ·630	54 52 51 50	·677 ·670 ·664 ·657	54 53 52 50	.705 .699 .692 .685	55 54 52 51	·735 ·728 ·721 ·714	1 6	
$14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2}$	·570 ·564 ·557 ·550	47 46 45 43	•596 •590 •583 •576	47 46 45 43	·623 ·616 ·609 ·603	48 47 46 45	·650 ·643 ·637 ·630	49 48 47 45	·678 ·671 ·665 ·658	50 48 47 46	·707 ·701 ·694 ·687	4	
$16 \\ 16 \\ 17 \\ 17 \\ 17 \\ 2$	·543 ·536 ·530 ·523	42 41 40 39	·569 ·562 ·556 ·549	42 41 40 39	·596 ·589 ·582 ·576	43 42 41 40	·623 ·616 ·610 ·603	44 43 42 41	·651 ·645 ·638 ·631	45 44 42 41	·680 ·674 ·667 ·660	4	
$18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2}$	·516 ·510 ·503 ·496	38 37 36 35	·542 ·536 ·529 ·522	38 37 36 35	·569 ·562 ·556 ·549	39 38 37 36	•596 •589 •582 •576	40 39 38 37	·624 ·617 ·611 ·603	40 39 38 37	·653 ·646 ·640 ·633	4.	
$20 \ 20 \ 21 \ 21 \ 21 \ 2$	·489 ·482 ·476 ·469	34 33 32 31	•515 •508 •502 •495	34 33 32 31	·542 ·535 ·528 ·522	35 34 33 32	•569 •562 •556 •549	36 35 34 33	·597 ·591 ·584 ·577	36 35 34 33	·626 ·620 ·613 ·606	4000	
22 22 <u>}</u> 23 23 <u>}</u> 23 <u>}</u>	·462 ·456 ·449 ·442	30 29 28 27	·488 ·482 ·475 ·468	31 30 29 28	·515 ·508 ·502 ·495	31 30 29 28	·542 ·535 ·528 ·522	32 31 30 29	·570 ·563 ·557 ·550	33 32 31 30	•599 •592 •586 •579	60 60	
$24 \over 24 \frac{1}{2} \\ 25$	·436 ·429 ·422	26 26 25	·461 ·455 ·448	27 26 25	·488 ·481 ·474	28 27 26	·515 ·508 ·502	28 27 26	·543 ·536 ·530	29 28 27	·572 ·565 ·559	2	

eit.		I	EGREES	OF TI	IE WET	BULB	THERMO	METER	R.—FAHR	ENHEI	r.	
ahrent	77	Y°	78	90	79	0	80	0	81	•	S	2°
t — U Fahrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	·927 ·920 ·914 ·907	100 98 95 93	•958 •951 •945 •938	100 98 95 93	·990 ·984 ·977 ·970	100 98 96 93	1.023 1.017 1.010 1.003	100 98 96 93	1.057 1.050 1.044 1.037	100 98 96 93	$\begin{array}{ c c c }\hline 1.092 \\ 1.085 \\ 1.079 \\ 1.072 \\\hline \end{array}$	100 98 96 94
$\frac{2}{2\frac{1}{2}}$	·900 ·893 ·886 ·880	91 89 87 85	·931 ·924 ·918 ·911	91 89 87 85	•963 •956 •950 •943	91 89 87 85	·996 ·989 ·983 ·976	91 89 87 85	1.030 1.023 1.016 1.010	91 89 87 85	1.065 1.058 1.051 1.045	91 89 87 86
$\begin{array}{c c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \\ \end{array}$	·873 ·866 ·859 ·853	83 81 79 77 75	·904 ·897 ·891 ·884 ·877	83 81 79 77 75	·936 ·929 ·923 ·916 ·909	83 81 79 77 75	·969 ·962 ·955 ·949	83 81 79 78	1.003 .996 .989 .982	83 81 80 78	1.038 1.031 1.024 1.017	84 82 80 78
$\begin{bmatrix} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \\ 8 \end{bmatrix}$	·846 ·839 ·832 ·825 ·819	73 72 70 68	·870 ·863 ·857 ·850	73 72 70 68	·902 ·895 ·889 ·882	74 72 70 69	•942 •935 •928 •921 •915	76 74 72 71 69	·976 ·969 ·962 ·955 ·948	76 74 73 71 69	1.010 1.004 .997 .990	76 75 73 71 70
8½ 9 9½ 10	·812 ·805 ·798	67 65 63 62	·843 ·836 ·829 ·823	67 65 63	·875 ·868 ·861 ·855	67 66 64 62	·908 ·901 ·894 ·887	68 66 64 63	·942 ·935 ·928 ·921	68 66 65 63	·976 ·970 ·963 ·956	68 67 65 64
$ \begin{array}{c c} & 10\frac{1}{2} \\ & 11 \\ & 11\frac{1}{2} \\ & 12 \end{array} $	·785 ·778 ·771 ·764	59 57 56	·816 ·809 ·802 ·796	60 59 57 56	·848 ·841 ·834 ·827	61 60 58 57	·881 ·874 ·867	61 60 59	·914 ·908 ·901 ·894	62 60 59 58	·949 ·942 ·936 ·929	62 61 59
12½ 13 13½ 14	·758 ·751 ·744	55 53 52 51	·789 ·782 ·775	55 53 52 51	·821 ·814 ·807 ·800	56 54 53 52	·854 ·847 ·840 ·833	56 55 53 52	·887 ·880 ·874 ·867	56 55 54	•922 •915 •908	58 57 56 54
$14\frac{1}{2} \\ 15 \\ 15\frac{1}{2}$	·781 ·724 ·717	49 48 47	·762 ·755 ·748	$ \begin{array}{r} 50 \\ 48 \\ 47 \end{array} $	·793 ·787 ·780	50 49 48	·826 ·820 ·813	51 50 49	·860 ·853 ·846	53 51 50 49	·902 ·895 ·888 ·881	53 52 51 50
$egin{array}{c c} 16 \\ 16\frac{1}{2} \\ 17 \\ 17\frac{1}{2} \\ 16 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17$	·710 ·704 ·697 ·690	46 45 44 42	·741 ·734 ·728 ·721	46 45 44 43	·773 ·766 ·760 ·753	47 46 45 44	·806 ·799 ·792 ·786	47 46 45 41	·840 ·833 ·826 ·819	48 47 46 45	·874 ·867 ·861 ·854	48 47 46 45
$ \begin{array}{c} 18 \\ 18\frac{1}{2} \\ 19 \\ 19\frac{1}{2} \end{array} $	·683 ·676 ·670 ·663	41 40 39 38	·714 ·707 ·700 ·694	42 41 40 39	·746 ·739 ·732 ·726	43 42 41 40	·779 ·772 ·765 ·758	43 42 41 40	·812 ·806 ·799 ·792	44 43 42 41	·847 ·840 ·833 ·827	44 43 42 41
$ \begin{array}{c} 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \end{array} $	·656 ·649 ·643 ·636	37 36 36 35	·687 ·680 ·673 ·667	38 37 36 35	·719 ·712 ·705 ·698	39 38 37 36	·752 ·745 ·738 ·731	39 38 37 36	·785 ·778 ·772 ·765	40 39 38 37	·820 ·813 ·806 ·799	40 39 38 38
$\begin{array}{c} 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \end{array}$	·629 ·622 ·615 ·609	34 33 32 31	·660 ·653 ·646 ·639	84 88 88 82	·692 ·685 ·678 ·671	35 34 33 32	·724 ·718 ·711 ·704	35 35 34 33	·758 ·751 ·744 ·738	36 35 34 34	·793 ·786 ·779 ·772	37 36 35 34
$ \begin{array}{c c} 24 \\ 24 \\ \hline 25 \end{array} $	·602 ·595 ·588	30 29 28	·633 ·626 ·619	31 30 29	·664 ·658 ·651	32 31 30	·697 ·690 ·684	32 31 30	·731 ·724 ·717	33 32 31	·765 ·759 ·752	33 32 31

nbeit							THERMO				I	
Fabre	83	0	84	ļ°	85	0	86		87		88	
t — t' Fabrenheit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, iu inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative
0° $1^{\frac{1}{2}}$ $1^{\frac{1}{2}}$	$\begin{array}{ c c c }\hline 1.128 \\ 1.121 \\ 1.114 \\ 1.108 \\\hline \end{array}$	100 98 96 94	1·165 1·158 1·151 1·145	100 98 96 94	1·203 1·196 1·189 1·183	100 98 96 94	1·242 1·235 1·228 1·222	100 98 96 94	1·282 1·275 1·269 1·262	100 98 96 94	1·324 1·317 1·310 1·303	10 9 9
$\frac{2}{2}$ $\frac{2}{2}$ $\frac{1}{2}$ $\frac{1}{2}$	1·101 1·094 1·087 1·080	91 90 88 86	1·138 1·131 1·124 1·117	92 90 88 86	1·176 1·169 1·162 1·155	92 90 88 86	1·215 1·208 1·201 1·194	92 90 88 86	1·255 1·249 1·241 1·235	92 90 88 86	1·296 1·290 1·283 1·276	9 9 8 8
$4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2}$	1.074 1.067 1.060 1.053	84 82 80 78	1·111 1·104 1·097 1·090	84 82 80 79	1·149 1·142 1·135 1·128	84 82 80 79	1·188 1·181 1·174 1·167	84 82 81 79	1·228 1·221 1·214 1·207	84 83 81 79	1·269 1·262 1·255 1·248	8 8 8 7
$\begin{array}{c} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{array}$	1.046 1.039 1.033 1.026	77 75 73 72	1.083 1.076 1.070 1.063	77 75 74 72	1·121 1·114 1·108 1·101	77 75 74 72	1·160 1·153 1·146 1·140	77 76 74 72	1·200 1·193 1·187 1·180	78 76 74 73	1.242 1.235 1.228 1.221	77 77 77
8 8 8 1 9 9 9	1.019 1.012 1.005 .999	70 69 67 66	1.056 1.049 1.042 1.036	70 69 67 66	1.094 1.087 1.080 1.074	71 69 68 66	1·133 1·126 1·119 1·112	71 69 68 66	1·173 1·166 1·159 1·153	71 70 68 67	1·214 1·208 1·201 1·194	7 7 6
10 10½ 11 11⅓	•992 •985 •978 •971	64 63 61 60	1.029 1.022 1.015 1.008	64 63 62 60	1.066 1.060 1.053 1.046	65 63 62 61	1·105 1·099 1·092 1·085	65 64 62 61	1·145 1·139 1·132 1·125	65 64 63 61	1·187 1·180 1·173 1·166	6
$12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{4}$	•965 •958 •951 •944	58 57 56 55	1.001 .995 .998 .981	59 58 56 55	1.039 1.032 1.026 1.019	59 58 57 56	1.078 1.071 1.065 1.058	58 57 56	1·118 1·111 1·105 1·098	60 59 57 56	1·159 1·153 1·146 1·139	5 5 5
14 14½ 15 15}	·937 ·931 ·924 ·917	54 52 51 50	•974 •967 •960 •954	54 53 52 50	1.012 1.005 .998 .991	55 53 52 51	1.051 1.044 1.037 1.030	55 54 52 51	1.091 1.084 1.077 1.070	55 54 53 52	1·132 1·125 1·118 1·111	10 10
$16^{1}_{16\frac{1}{2}}$ $17^{1}_{17\frac{1}{2}}$.910 .903 .896 .890	49 48 47 46	·947 ·940 ·933 ·926	49 48 47 46	·985 ·978 ·971 ·964	50 49 48 47	1.023 1.017 1.010 1.003	50 49 48 47	1.063 1.057 1.050 1.043	51 50 49 48	1·105 1·098 1·091 1·084	£ 4
18 18½ 19 19¾	*883 *876 *869 *862	45 44 43 42	•920 •913 •906 •899	45 44 43 42	·957 ·951 ·944 ·937	46 45 41 43	·996 ·989 ·983 ·976	46 45 44 43	1.036 1.029 1.023 1.016	47 46 45 44	1.077 1.071 1.064 1.057	4 4 4
20 20½ 20½ 21 21½	·855 ·849 ·842 ·835	41 40 39 38	·892 ·885 ·879 ·872	41 40 39 38	·930 ·923 ·916 ·910	42 41 40 39	·969 ·962 ·955 ·948.	42 41 41 40	1.009 1.002 .995 .988	43 42 41 40	1.050 1.043 1.036 1.029	4 4 4
22 221 221 23 231	·828 ·821 ·815 ·808	37 36 35 34	·865 ·858 ·851 ·845	38 37 36 35	·903 ·896 ·889 ·882	38 37 37 36	·942 ·935 ·928 ·921	39 38 37 36	·981 ·975 ·967 ·961	39 38 38 37	1.023 1.016 1.009 1.002	9 9
$24 \\ 24 \\ 24 \\ 25$	·800 ·794 ·787	34 33 32	·838 ·831 ·824	34 33 33	·875 ·869 ·862	35 34 33	·914 ·908 ·900	36 35 34	·954 ·947 ·940	36 35 35	·995 ·989 ·981	9 99

it.		I	DEGREES	OF TI	IE WET	BULB	THERMO	METER	.—FAHR	ENHEI'	r.	
- t' Fahrenheit.	89	0	90	0	91	0	92	°	93	0	94	ļo
t — t' E	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1	1·366	100	1·410	100	1·455	100	1.501	100	1.548	100	1·597	100
	1·359	98	1·403	98	1·448	98	1.494	98	1.541	98	1·590	98
	1·352	96	1·396	96	1·441	96	1.487	96	1.535	96	1·583	96
	1·346	94	1·389	94	1·434	94	1.480	94	1.528	94	1·576	94
$\begin{bmatrix} 2 \\ 2\frac{1}{2} \\ 3 \\ 3\frac{1}{2} \end{bmatrix}$	1·339	92	1·382	92	1·427	92	1·473	92	1.521	92	1.569	92
	1·332	90	1·375	90	1·420	90	1·466	90	1.514	91	1.562	91
	1·325	88	1·368	88	1·413	88	1·459	89	1.507	89	1.556	89
	1·318	86	1·362	86	1·406	87	1·453	87	1.500	87	1.549	87
$ \begin{array}{c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array} $	1·311	85	1.355	85	1.400	85	1.446	85	1·493	85	1.542	85
	1·304	83	1.348	83	1.393	83	1.439	83	1·486	84	1.535	84
	1·298	81	1.341	81	1.386	82	1.432	82	1·479	82	1.528	82
	1·291	80	1.334	80	1.379	80	1.425	80	1·473	80	1.521	80
$\begin{array}{c c} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{array}$	1.284	78	1·327	78	1·372	78	1·418	79	1.466	79	1.514	79
	1.277	77	1·321	77	1·365	77	1·411	77	1.459	77	1.507	77
	1.270	75	1·314	75	1·358	75	1·405	75	1.452	76	1.500	76
	1.263	73	1·307	74	1·352	74	1·398	74	1.445	74	1.493	74
$ \begin{array}{c c} 8 \\ 8 \\ \hline 9 \\ 9 \\ \hline 9 \\ \end{array} $	$\begin{array}{c c} 1.256 \\ 1.249 \\ 1.243 \\ 1.236 \end{array}$	72 70 69 67	1·300 1·293 1·286 1·279	72 71 69 68	1.345 1.338 1.331 1.324	72 71 69 68	1·391 1·384 1·377 1·370	73 71 70 68	1·438 1·431 1·424 1·417	73 71 70 69	1.487 1.480 1.473 1.466	73 72 70 69
$10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2}$	1·229	66	1.273	66	1·317	67	1.363	67	1·411	67	1·459	67
	1·222	65	1.266	65	1·311	65	1.356	65	1·404	66	1·452	66
	1·215	64	1.259	64	1·304	64	1.350	64	1·397	65	1·445	65
	1·208	62	1.252	62	1·297	63	1.343	63	1·390	63	1·439	64
$ \begin{array}{c c} 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array} $	1·202 1·195 1·188 1·181	59 58 57	1.245 1.238 1.231 1.224	61 60 59 57	1.290 1.283 1.276 1.269	61 60 59 58	1.336 1.329 1.322 1.315	62 60 59 58	1.383 1.376 1.369 1.363	62 61 60 59	1·432 1·425 1·418 1·411	62 61 60 59
14	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	56	1·217	56	1.262	57	1·308	57	1.356	58	1·404	58
14½		55	1·211	55	1.255	56	1·301	56	1.349	56	1·397	57
15		54	1·204	54	1.249	54	1·295	55	1.342	55	1·390	56
15½		53	1·197	53	1.242	53	1·288	54	1.335	54	1·383	55
16 $16\frac{1}{2}$ 17 $17\frac{1}{2}$	1·147 1·140 1·183 1·126	51 50 49 48	1·190 1·183 1·176 1·170	52 51 50 49	1·235 1·228 1·221 1·214	52 51 50 49	$\begin{array}{ c c c }\hline 1.281 \\ 1.274 \\ 1.267 \\ 1.260 \\\hline\end{array}$	53 52 51 50	1·328 1·321 1·314 1·308	53 52 51 50	1·377 1·370 1·363 1·356	54 53 52 51
$ \begin{array}{c c} 18 \\ 18 \\ 19 \\ 19 \\ 19 \\ 1 \end{array} $	1·119 1·112 1·105 1·099	47 46 45 44	1·163 1·156 1·149 1·142	48 47 •46 45	$ \begin{array}{ c c c c c } \hline 1.207 \\ 1.200 \\ 1.194 \\ 1.187 \\ \hline \end{array} $	48 47 46 45	1.253 1.246 1.239 1.233	49 48 47 46	1.301 1.294 1.287 1.280	49 48 47 46	1·349 1·342 1·335 1·328	50 49 48 47
$ \begin{array}{c c} 20 \\ 201 \\ 21 \\ 21\frac{1}{2} \end{array} $	1.092	44	1·135	44	1·180	44	1.226	45	1.273	45	1·321	46
	1.085	43	1·129	43	1·173	44	1.219	44	1.266	44	1·315	45
	1.078	42	1·122	42	1·166	43	1.212	43	1.259	44	1·308	44
	1.071	41	1·115	41	1·159	42	1.205	43	1.253	43	1·301	43
$ \begin{array}{ c c c c c } & 22 \\ & 22\frac{1}{2} \\ & 23 \\ & & 23\frac{1}{2} \end{array} $	1.065	40	1·108	41	1·153	41	1·198	42	1.246	42	1·294	43
	1.058	39	1·101	40	1·146	40	1·191	41	1.239	41	1·287	42
	1.051	39	1·094	39	1·139	89	1·185	40	1.232	41	1·280	41
	1.044	38	1·087	38	1·132	39	1·178	39	1.225	40	1·273	40
$ \begin{array}{r} 24 \\ 24\frac{1}{2} \\ 25 \end{array} $	1.037	37	1.080	38	1·125	38	1·171	38	1.218	39	1.266	39
	1.030	36	1.073	37	1·118	37	1·164	38	1.211	38	1.259	39
	1.023	36	1.067	36	1·111	37	1·157	37	1.204	38	1.253	38

eit.		D	EGREES	ог тн	E WET	BULB '	THERMO:	METER	FAHRI	· ENHEIT		
— t Fahrenheit.	95	0	96	0	97	•	98	0	99	0	100)°
t - t	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, iu inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.
0° 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.647 1.640 1.633 1.626	100 98 96 94	1.698 1.691 1.684 1.677	100 98 96 94	1.751 1.744 1.737 1.730	100 98 96 94	1·805 1·798 1·791 1·784	100 98 96 95	1.861 1.854 1.847 1.840	100 98 96 95	1:918 1:911 1:904 1:897	100 98 96 95
2 2 2 2 3 3	1.619 1.612 1.605 1.598	92 90 89 87	1.671 1.664 1.657 1.650	92 90 89 87	1.723 1.716 1.709 1.703	92 90 89 87	1·777 1·770 1·764 1·757	93 91 90 88	1.833 1.826 1.819 1.812	93 91 90 88	1.890 1.883 1.876 1.870	93 91 90 88
$\begin{array}{c} 4 \\ 4\frac{1}{2} \\ 5 \\ 5\frac{1}{2} \end{array}$	1.592 1.585 1.578 1.571	85 83 82 80	$egin{array}{c} 1.643 \\ 1.636 \\ 1.629 \\ 1.622 \\ \end{array}$	85 83 82 80	1.696 1.689 1.682 1.675	85 83 82 80	$ \begin{array}{c c} 1.750 \\ 1.743 \\ 1.736 \\ 1.729 \end{array} $	86 84 83 81	1·805 1·799 1·791 1·785	86 84 83 81	1.863 1.857 1.849 1.842	86 84 83 81
$\begin{bmatrix} 6 \\ 6\frac{1}{2} \\ 7 \\ 7\frac{1}{2} \end{bmatrix}$	1.564 1.557 1.550 1.543	78 77 75 73	1.615 1.608 1.602 1.595	78 77 76 74	1.668 1.661 1.654 1.647	78 77 76 74	1.722 1.715 1.708 1.701	79 78 77 75	1.778 1.771 1.764 1.757	79 78 77 76	1.835 1.828 1.821 1.814	79 78 77 76
$ \begin{array}{c} 8 \\ 8 \\ 9 \\ 9 \\ \hline 9 \\ \hline 2 \end{array} $	1.536 1.530 1.523 1.517	72 71 70 69	1.588 1.581 1.574 1.567	73 71 70 69	1.640 1.633 1.627 1.620	73 71 70 69	1.694 1.688 1.681 1.674	74 72 71 70	$\begin{array}{ c c c }\hline 1.750 \\ 1.743 \\ 1.736 \\ 1.729 \\\hline\end{array}$	74 73 72 70	1.807 1.800 1.793 1.786	74 73 72 70
$10 \\ 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2}$	1.509 1.502 1.495 1.488	68 66 65 63	1.560 1.553 1.546 1.539	68 66 65 63	1.613 1.606 1.599 1.592	68 66 65 64	1.667 1.660 1.653 1.646	69 67 66 64	$ \begin{array}{ c c c } \hline 1.722 \\ 1.715 \\ 1.708 \\ 1.702 \end{array} $	69 67 66 65	1·779 1·772 1·766 1·759	69 67 66 65
$\begin{array}{ c c c }\hline 12\\ 12\frac{1}{2}\\ 13\\ 13\frac{1}{2}\\ \end{array}$	1·481 1·474 1·468 1·461	62 61 60 59	1.532 1.526 1.519 1.512	62 61 60 59	1.585 1.578 1.571 1.564	63 62 61 60	1.639 1.632 1.625 1.618	63 62 61 60	1.695 1.688 1.681 1.674	64 63 62 61	1.752 1.745 1.738 1.731	64 63 62 61
$egin{array}{c c} 14 \\ 14rac{1}{2} \\ 15 \\ 15rac{1}{2} \end{array}$	1·454 1·447 1·440 1·433	58 57 56 55	1.505 1.498 1.491 1.484	58 57 56 55	1.558 1.551 1.544 1.537	59 58 57 56	1.611 1.605 1.598 1.591	59 58 57 56	1.667 1.660 1.653 1.646	60 59 58 57	1.724 1.717 1.710 1.703	60 59 58 57
$ \begin{array}{ c c c } & 16 \\ & 16 \frac{1}{2} \\ & 17 \\ & 17 \frac{1}{2} \end{array} $	1·426 1·419 1·412 1·405	54 53 52 51	1·477 1·470 1·464 1·457	54 53 52 51	1.530 1.523 1.516 1.509	55 54 53 52	1.584 1.577 1.570 1.563	55 54 53 52	1.639 1.632 1.625 1.619	56 55 54 53	1.696 1.689 1.682 1.676	56 55 54 53
$ \begin{array}{ c c c } & 18 \\ & 18 \\ & 19 \\ & 19 \\ & 19 \\ & 19 \\ & \end{array} $	1·399 1·392 1·385 1·378	50 49 48 47	$\begin{array}{ c c c }\hline 1.450 \\ 1.443 \\ 1.436 \\ 1.429 \\\hline\end{array}$	50 49 48 47	1.502 1.495 1.488 1.482	51 50 49 48	1.556 1.549 1.542 1.535	52 51 50 49	1.612 1.605 1.598 1.591	52 51 50 49	1.669 1.662 1.655 1.648	53 52 51 50
$ \begin{array}{ c c c c c } 20 \\ 20 \\ 21 \\ 21 \\ 21 \\ 2 \end{array} $	1·371 1·364 1·357 1·350	46 45 45 44	1·422 1·415 1·408 1·401	47 46 45 44	1·475 1·468 1·461 1·454	47 46 45 44	1.528 1.522 1.515 1.508	48 47 46 45	1.584 1.577 1.570 1.563		1.641 1.634 1.627 1.620	49 48 47 46
$\begin{array}{ c c c }\hline 22 \\ 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \\ \end{array}$	1·343 1·337 1·330 1·323	43 42	1·395 1·388 1·381 1·374	44 43 42 42	1·447 1·440 1·433 1·426		1.501 1.494 1.487 1.480	43	1.556 1.549 1.542 1.536		1.613 1.606 1.599 1.593	46 45 44 43
$\begin{array}{ c c } 24 \\ 24\frac{1}{2} \\ 25 \end{array}$	1·316 1·309 1·302	40	1·367 1·360 1·353		1·420 1·413 1·406	40	1·473 1·466 1·459		1.529 1.522 1.515	42 41 40	1.586 1.579 1.572	43 42 41

lejt.		· D	EGREES	OF TH	E WET	BULB '	THERMO	METER	.—FAHR	ENHEIT	r.	
ahrent	10	L°	10	2°	10	3°	104	1°	10	5°	10	6°
t — t' Fabrenbeit.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inches.	Relative Humidity.	Force of Vapor, in inclus.	Relative Humidity.
0° 1/2 1 1/2 2 2 1/2 3 3 1	1.977 1.970 1.963 1.956 1.949 1.942 1.935	100 98 96 95 93 91 90	2·037 2·030 2·023 2·016 2·009 2·002 1·995	100 98 96 95 93 91 90 88	2·098 2·092 2·085 2·078 2·071 2·064 2·057	100 98 96 95 93 91 90 88	2·162 2·155 2·148 2·141 2·134 2·127 2·120 2·113	100 98 96 95 93 91 90 88	2.226	100	2.293	100
3½ 4 4½ 5 5½ 6 6½	1.928 1.921 1.914 1.907 1.900 1.893 1.887	88 86 84 83 82 80 79	1.989 1.982 1.975 1.967 1.960 1.954 1.947 1.940	86 84 83 82 80 79	2.050 2.043 2.036 2.029 2.022 2.015 2.008 2.001	87 84 83 82 80 79 78	2·113 2·106 2·099 2·092 2·085 2·078 2·071 2·064	87 85 84 82 81 79 78				
$\begin{bmatrix} 7 \\ 7\frac{1}{2} \\ 8 \\ 8\frac{1}{2} \\ 9 \\ 9\frac{1}{2} \\ 10 \end{bmatrix}$	1.880 1.873 1.866 1.859 1.852 1.845	78 76 75 74 72 71 69	1.933 1.926 1.919 1.912 1.905 1.898	78 76 75 74 72 71 70	1.994 1.988 1.981 1.974 1.967	77 75 74 72 71 70	2.057 2.050 2.043 2.036 2.029 2.022	75 75 74 73 71 70				
$\begin{array}{c c} 10\frac{1}{2} \\ 11 \\ 11\frac{1}{2} \\ 12 \\ 12\frac{1}{2} \\ 13 \\ 13\frac{1}{2} \end{array}$	1.831 1.824 1.817 1.810 1.803 1.796 1.790	68 67 66 65 64 62 61	1.891 1.884 1.877 1.863 1.863 1.857 1.850	69 67 66 65 64 63 62	1.953 1.946 1.939 1.932 1.925 1.918 1.911	69 68 67 65 64 63 62	2.015 2.008 2.001 1.994 1.987 1.980 1.973	69 68 67 66 65 63 62				
$ \begin{array}{ c c c c } \hline 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \\ 16 \\ 16\frac{1}{3} \\ \hline \end{array} $	1·783 1·776 1·769 1·762 1·755 1·748	60 59 58 57 56 55	1.843 1.836 1.829 1.822 1.815 1.808	61 60 59 58 57 56	1.904 1.897 1.890 1.883 1.876 1.869	61 60 59 58 57 56	1.966 1.959 1.952 1.945 1.938 1.931	61 60 59 58 57 56				
$ \begin{array}{ c c c c } \hline 17^{1} \\ 17^{1}_{2} \\ 18 \\ 18^{1}_{2} \\ 19 \\ 19^{1}_{2} \end{array} $	1.741 1.734 1.727 1.720 1.713 1.706	54 53 52 52 51 50	1.801 1.794 1.787 1.780 1.778 1.766	55 54 53 52 51 50	1.862 1.856 1.849 1.842 1.835 1.828	55 54 53 53 52 51	1.924 1.917 1.910 1.903 1.896 1.889	55 55 54 53 52 51				
$ \begin{array}{ c c c c } \hline 20 \\ 20\frac{1}{2} \\ 21 \\ 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \end{array} $	1.699 1.692 1.685 1.679 1.672 1.665	49 48 47 47 46 45	1.759 1.752 1.745 1.738 1.732 1.725	49 48 48 47 46 45	1.821 1.814 1.807 1.800 1.793 1.786	50 49 48 48 47 46	1.882 1.875 1.868 1.861 1.854 1.847	50 49 49 48 47 46				
$ \begin{array}{c c} 23^{2} \\ 23\frac{1}{2} \\ 24 \\ 24\frac{1}{2} \\ 25 \end{array} $	1.658 1.651 1.644 1.637 1.630	44 43 43 42 41	1.718 1.711 1.704 1.697 1.690	44 44 43 42 42	1·779 1·772 1·765 1·759 1·751	45 45 44 43 43	1·840 1·833 1·826 1·819 1·812	46 45 44 43 43				

eit.		D	EGREES	OF TI	E WET	BULB	THERMO	METER	.— FAПК	ENHEI	г.	
Fahrenbeit	107°		108°		10	109°		110°		1°	112°	
t → t' F	Force of Vapor, in inches.	Relative Humidity.										
00	2.360	100	2.429	100	2.500	100	2.572	100	2.646	100	2.721	100

TABLES,

METEOROLOGICAL AND PHYSICAL,

PREPARED FOR

THE SMITHSONIAN INSTITUTION.

ВҰ

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THIRD EDITION,
REVISED AND ENLARGED.

WASHINGTON: SMITHSONIAN INSTITUTION. 1859.

PHILADELPHIA:

COLLINS, PRINTER, 705 JAYNE STREET.

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The Tables contained in this collection are divided into six series, as follows: -

- 1. Thermometrical Tables, marked A.
- II. Hygrometrical Tables, "B.
- III. Barometrical Tables, "C.
- IV. Hypsometrical Tables, "D.
- V. Meteorological Corrections, " E.
- VI. Miscellaneous Tables, "F.

Each series has an independent paging running through all the tables that it contains.

The letters A, B, C, D, E, F, at the bottom of each page, indicate the series, and the figure the folio of the series to which the page belongs.

The figure at the top of the page indicates the folio of the particular table of which the page is a part.

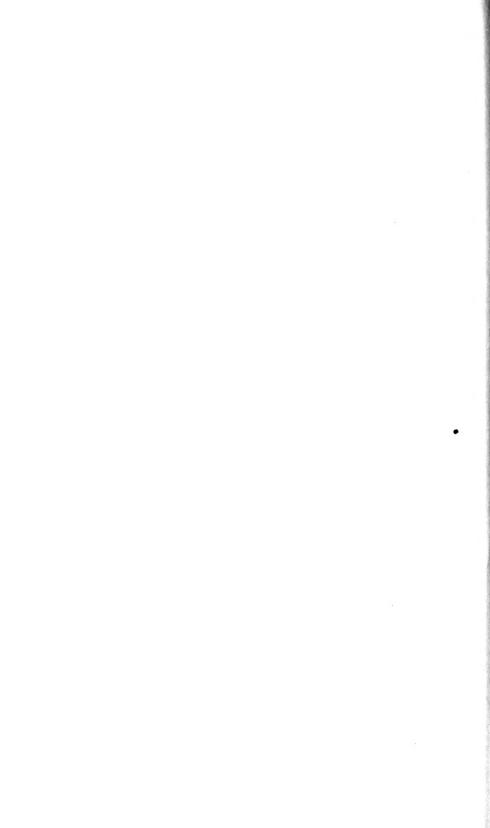
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METEOROLOGICAL TABLES.

I.

THERMOMETRICAL TABLES.



CONTENTS.

COMPARISON OF THE THERMOMETRICAL SCALES.

(The figures refer to the folio at the bottom of the page.)

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" X.	Value of any number of Degrees of Fahrenheit, expressed by a cor-
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"XIV.	Value of any number of Degrees of Reaumur, expressed by a cor-
// 3737	responding number of Centigrade Degrees,
" XV.	Value of any number of Degrees of Reaumur expressed by a cor-
	responding number of Degrees of Fahrenheit,
	A 3



PREFACE

TO THE FIRST EDITION.

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR,—

In compliance with your instructions, I have prepared the collection of Meteorological Tables contained in the following pages. I have endeavored to render it useful, not only to the observers engaged in the system of Meteorological Observations now in operation under the direction of the Smithsonian Institution, for whom it was immediately designed, but also to any Meteorologist who may desire to compare and to work out portions of the vast amount of Meteorological Observations already accumulated in the stores of science.

The reduction of the observations and the extensive comparisons, without which Meteorology can do but little, require an amount of mechanical labor which renders it impossible for most observers to deduce for themselves the results of their own observations. The difficulty is still further increased by the diversity of the thermometrical and barometrical scales which Meteorologists, faithful to old habits rather than to science and to reason, choose to retain, notwithstanding the additional labor they thus gratuitously assume to themselves. To relieve the Meteorologist of a great portion of this labor, by means of tables sufficiently extensive to render calculations and even interpolations unnecessary, is to save his time and his forces in favor of science itself, and thus materially contribute to its advancement. But most of the tables useful in Meteorology being scattered through many volumes, which are often not of easy access, this collection will be, it is hoped, acceptable to the friends of Meteorology, and will supply a want very much felt in this department of the physical sciences.

In the selection of the matter, I have been guided by the idea that the tables which I sought for my own use might also be those most likely to be wanted by others. But I wish the following to be considered as a first collection, containing only the tables most appropriate to the present purpose. They are, therefore, arranged in different and independent series, with distinct paging, but constituting together a frame-work into which any tables may be readily inserted when wanted, either to make the collection more complete, or to present a choice of tables calculated from somewhat different elements, or adapted to various methods of calculation.

The measurement of heights by means of the barometer being intimately connected with Meteorology, it was thought not inappropriate to admit into this collection Hypsometrical Tables, destined to render this kind of calculations more easy and more rapid, and thus to increase the taste for a method so useful in physical geography. I have preferred the tables of Delcros, as uniting in the greatest degree simplicity and accuracy. Those of Gauss, Bessel, and Baily may be given afterwards.

Every table contains directions for its use, when necessary; moreover, the indication of the elements used in its calculation, and of the source from which it has been taken. When no remark is made as to this last point, the table has been expressly calculated for this volume.

Very respectfully,

Your obedient servant,

A. GUYOT.

Cambridge, Mass., December 15th, 1851.

PREFACE

TO THE SECOND EDITION

To PROF. JOSEPH HENRY,

Secretary of the Smithsonian Institution.

SIR, —

In sending to you the Meteorological Tables composing the first edition of this volume, published in 1852, I expressed the desire that they be considered as a first collection, containing the tables most needed at the time by the meteorological observers engaged in the system carried on under the supervision of the Smithsonian Institution, but destined to be increased. It was in that expectation, I remarked, that the tables had been arranged in independent series, as a kind of framework, into which a larger number could readily be inserted. It seemed, indeed, highly desirable to offer to the Meteorologist and Physical Geographer, not only the tables they daily need for working out the results of their observations, but also such a variety of tables, computed from different elements, or by different methods, or adapted to different measures, as to enable every one to choose among them those that he most approves, and at the same time properly to compare and to appreciate the results obtained by others.

Thanks to the congenial spirit with which the elevated views of the founder of the Smithsonian Institution are carried out, that character of general usefulness is not wanting in the present volume. With your agreement, the present edition contains more than three times as much matter as the first; and a rapid indication of the additions will suffice to justify them, and to show that, in selecting or calculating the new tables, the object just mentioned was constantly kept in view

As to the tables in the first edition, I must remark that, several of them having been printed in my absence, the copy prepared for the printer, in which decimals had to be left out, failed to give always the nearest value. Though these errors are too small to have any importance whatsoever in Meteorology, a careful revision of all the tables on the original computations was made, and they were corrected in the present edition. The few actual misprints which were discovered are indicated in a table of errata to the first edition.

In the Thermometrical series six small tables have been added; they were prepared for converting into each other differential results given in degrees of any one of the three thermometrical scales, irrespective of their zero point.

The Hygrometrical series has been entirely reorganized. It only contained five tables, all in French measures, and the Appendix. composed of twenty-seven, arranged in three divisions. In the first are found ten tables, based on Regnault's hygrometrical constants, both in French and in English measures, in two corresponding sets, for the use of the psychrometer, the dew-point instruments, and for computing the weight of vapor in the air. The whole set in English measures, and Table V. in French measures, have been prepared for this edition. Being based on the best elements we now possess, they are given here for ordinary use. The second division contains the seven most important tables published in the Greenwich Observations, and Glaisher's extensive Psychrometrical Table. These tables being much used in England, and the results obtained by them exhibiting no inconsiderable differences from those derived from the preceding ones, they are indispensable for comparing these results. division, composed of ten miscellaneous tables, furnishes the means of comparing the different values of the force and the weight of vapor, especially those which have frequently been used in Germany, and also of reducing the indications of Saussure's Hair-Hygrometer to the ordinary seale of moisture. The Appendix has remained as in the first edition, but all the tables have been revised and corrected.

The Barometrical series, now in four divisions, has been increased from twelve to twenty-eight tables. Excepting three small tables for capillary action, all the new ones have been computed for this edition. The comparison, now so much needed, of the Russian barometer with the other scales, appears here for the first time.

The Hypsometrical series is almost entirely new. It contained only Deferos's table for barometric and Regnault's table for thermometric measurements, besides two auxiliary tables and the thirteen small tables of the Appendix. It now offers twenty-three tables for barometrical measurement of heights, in which all the principal formulæ and scales are represented; three for the measurement of heights by the thermometer, in French and in English measures; and a rich Appendix of forty-four tables, more extensive and convenient than those in the old set, which afford the means of readily converting into each other all the measures usually employed for indicating altitudes.

The series of Meteorological Corrections for periodic and non-periodic variations, for all parts of the world, mostly due to the untiring industry of Professor Dove, is an addition which will surely be appreciated by those who know how difficult access to the original tables is for most Meteorol-

ogists. A few tables have been added to Dove's collection, computed by Glaisher, Captain Lefroy, and by myself. Most of the tables refer to temperature, only two to moisture. Two tables of Barometrical Corrections have been placed in the Hypsometrical series, where they were needed, until they can be joined by others to make a set in this series, which still awaits new contributions, especially for these last two departments.

The Miscellaneous series is but begun. I have prepared a list of useful tables, which would be no doubt welcome to the lovers of Terrestrial Physics, and which may be published at some future occasion, if you should then find it expedient.

The present collection being designed, not for the scientific only, but for the observers at large, the propriety of the explicit and popular form of the explanations which accompany the tables, and of the directions for using them, will readily be understood.

I close by the remark, that, in every instance, the works from which the tables were taken have been carefully noted, and due credit given to their authors. For all the tables without author's names, I am myself responsible.

I remain, Sir,

Very respectfully, yours,

A. GUYOT.

PRINCETON, N. J., December, 1857.

PREFACE

TO THE THIRD EDITION.

A NEW series of Hygrometrical Tables, based on Regnault's Table of Elastic Forces of Vapor, has been published by Mr. Glaisher, in London, 1856. As, however, the Psychrometrical Table has not been computed from Regnault's formula, but by means of empirical factors, the results differ from those contained in Table VII. B. A table containing Glaisher's empirical factors, therefore, has been added, and will be found on page 144 B.

Table XVIII. of the Barometrical set, C, page 72, of the Second Edition, for reducing to the freezing point the Barometers with glass or wooden scales, copied from the Instructions of the Royal Society of London, and which is reprinted in most of the English works on Meteorology, having been found erroneous, a new table has been computed and substituted for it. As a large number of observers still use barometers with wooden scales, it was found advisable to enable them to make the needed interpolations at sight, by giving the corrections for every degree of the thermometer, from 0° to 100° Fahr., and for barometric heights ranging between 26 and 31 inches.

The small Table VI. D, page 48, of the Hypsometrical Tables by the writer, having been found useful for rapid computation of approximate results, a larger one of the same description, which allows to make at sight every interpolation, has been added, on page 92, as Table XIX'. The scientific traveller, wishing to determine, when ascending a mountain, the elevation of the physical or geological phenomena that he meets with, such as the stations of remarkable plants, limits of zones of vegetation,—the geologist who uses the aneroid barometer for geological sections,—the engineer who wishes to know, on the ground, approximately, his results,—will find it convenient to obtain the relative heights indicated by their instrument by a simple multiplication. The use of the table is explained page D 90.

Some of the decimals in the smaller Table VI. D, page 48, above mentioned, have been slightly altered in order to make both tables agree.

In set E of Meteorological Corrections, a table of corrections derived by Professor C. Dewey from the hourly observations of Professor Snell, at Amherst College, has been added, which will be of service especially to the numerous observers in New England and in the neighboring States.

The errata indicated in the Second Edition, and a few unimportant ones found since, have been corrected. No other changes have been made in this edition.

A. GUYOT.

I. – III.

GENERAL COMPARISON

 $_{
m OF}$

THE THERMOMETRICAL SCALES,

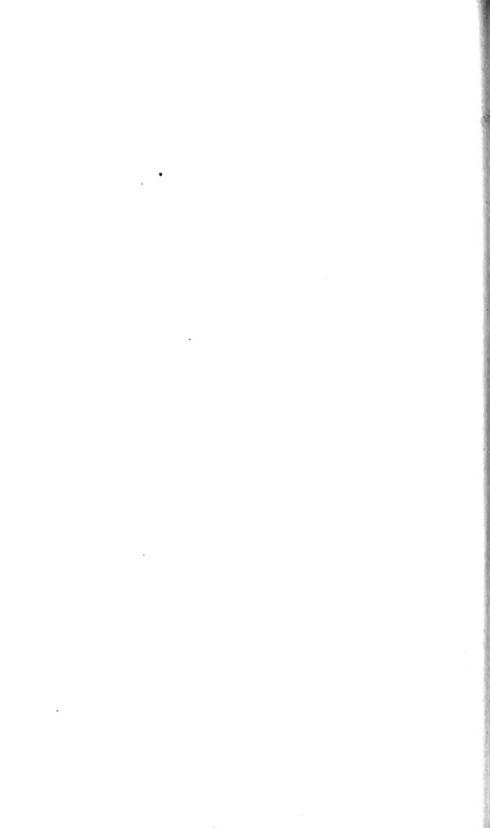
 \mathbf{OR}

TABLES

SHOWING THE CORRESPONDING VALUES OF EACH FULL DEGREE OF FAHRENHEIT'S,

CENTIGRADE, AND REAUMUR'S THERMOMETERS, FROM

+212° TO -39° FAHRENHEIT.



COMPARISON OF THE THERMOMETRICAL SCALES.

THE first three tables of this set give a simultaneous comparison of the three scales mostly used at present in Meteorology, and especially of the portion of the scales not comprised in the more extensive tables which follow them. They form thus a complement to these last tables; but as most of the temperatures contained in them do not occur in Meteorology, the comparison of the full degrees was found sufficient.

These three tables have been taken from E. L. Schubarth's Collection of Physical Tables. Berlin, 1836.

Tables IV. to IX. being more useful to the Meteorologist, the calculation has been carried out for every tenth of a degree. Tables VII. and IX. are from the *Annuaire Météorologique de France*; the others have been calculated.

A comparison of the Centigrade and Fahrenheit degrees near the boiling point, for every tenth of a degree, for the sake of the comparison of standard thermometers, will be found at the end of Table VI.

Tables X. to XV. will be found useful for comparing differential results, such as ranges of temperature, and any relative amount expressed in degrees of different scales, without reference to their respective zeros.

 x° Fahr. = $(x^{\circ} - 32^{\circ}) \frac{5}{9}$ Centig. = $(x^{\circ} - 32^{\circ}) \frac{4}{9}$ Reaum.

Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.
+212	+100.00	+80.00	+172	+77.78	+62.22	+132	+55.56	+44.44
211	99.44	79.56	171	77.22	61.78	131	55.00	44.00
210	98.89	79.11	170	76.67	61.33	130	54.44	43.56
209	98.33	78.67 78.22	169	76.11	60.89	129	53.89	43.11
208	97.78	75.22 77.78	168 167	75.56	60.44	128	53.33	42.67
207	97.22	77.33	166	75.00	60.00	127	52.78	42.22
206	96.67 96.11	76.89	165	74.44 73.89	59.56 59.11	126 125	52.22	41.78 41.33
205		76.44	164			1	51.67	
204	95.56	76.00	163	73.33	58.67	124 123	51.11	40.89
203	95.00	75.56	162	72.78	58.22		50.56	40.44
202	94.44	75.11	161	72.22	57.78	122	50.00	40.00
201	93.89	74.67	160	71.67	57.33	121 120	49.44	39.56
200	93.33	74.07	-	71.11	56.89		48.89	39.11
199	92.78	73.78	159	70.56	56.44	119	48.33	38.67
198	92.22	73.33	158	70.00	56.00	118	47.78	38.22
197	91.67	73.33 72.89	157	69.44	55.56	117	47.22	37.78
196	91.11		156	68.89	55.11	116	46.67	37.33
195	90.56	72.44	155	68.33	54.67	115	46.11	36.89
194	90.00	72.00	154	67.78	54.22	114	45.56	36.44
193	89.44	71.56	153	67.22	53.7 8	113	45.00	36.00
192	88.89	71.11	152	66.67	53.33	112	44.44	35.56
191	88.33	70.67	151	66.11	52.89	111	43.89	35.11
190	87.78	70.22	150	65.56	52.44	110	43.33	34.67
189	87.22	69.78	149	65.00	52.00	109	42.78	34.22
188	86.67	69.33	148	64.44 .	51.56	108	42.22	33.7S
187	86.11	68.89	147	63.89	51.11	107	41.67	33.33
186	85.56	68.44	146	63.33	50.67	106	41.11	32.89
185	85.00	68.00	145	62.78	50.22	105	40.56	32.44
184	84.44	67.56	144	62.22	49.78	104	40.00	32.00
183	83.89	67.11	143	61.67	49.33	103	39.44	31.56
182	83.33	66.67	142	61.11	48.89	102	38.89	31.11
181	82.78	66.22	141	60.56	48.44	101	38.33	30.67
180	82.22	65.78	140	60.00	48.00	100	37.78	30.22
179	81.67	65.33	139	59.44	47.56	99	37.22	29.78
178	81.11	64.89	138	58.89	47.11	98	36.67	29.33
177	80.56	64.44	137	58.33	46.67	97	36.11	28.89
176	80.00	64.00	136	57.78	46.22	96	35.56	28.44
175	79.44	63.56	135	57.22	45.78	95	35.00	28.00
174	78.89	63.11	134	56.67	45.33	94	34.44	27.56
173	78.33	62.67	133	56.11	44.89	93	33.89	27.11
	1					<u></u>		

 x° Fahr. = $(x^{\circ} - 32^{\circ}) \frac{5}{9}$ Centig. = $(x^{\circ} - 32^{\circ}) \frac{4}{9}$ Reaum.

			(•				
Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.	Fahren.	Centigrade.	Reaumur.
Lamon	Ochrighade.	1.cadinar.	1	Contigrador	110000111011			
			1				1	10.44
+92	+33.33	+26.67	+48	+ 8.89	+ 7.11	+ 4	-15.56	-12.44
91	32.78	26.22	47	8.33	6.67		-16.11	-12.89
90	32.22	25.78	46	7.78	6.22	2	-16.67 -17.22	-13.33 -13.78
89	31.67	25.33	45 44	7.22 6.67	5.78 5.33	0	-17.22 -17.78	-13.73 -14.22
88 87	31.11 30.56	24.89 24.44	43	6.11	4.89	- 1	-18.33	-14.22 -14.67
1	1	24.44	42	5.56	4.44	- 2	-18.89	-15.11
86	30.00	23.56	41	5.00	4.00	- 3	-19.44	-15.11 -15.56
85 84	29.44 28.89	23.11	40	4.44	3.56	- 4	-20.00	-16.00
83	28.33	22.67	39	3.89	3.11	- 4 - 5	-20.56	-16.44
1	1	22.22	38	3.33	2.67	- 6	-20.30 -21.11	-16.S9
82	27.78	21.78	37	2.78	2.22	- 7	-21.11	_17.33
81	27.22	21.75	36	2.78	1.78	- 8	-22.22	-17.78
80 79	26.67 26.11	20.89	35	1.67	1.33	- 9	-22.78	-18.22
78 78	25.56	20.39	34	1.11	0.89	-10	-23.33	-18.67
77	25.00	20.44	33	0.56	0.33	-11	-23.89	-19.11
II .	1	19.56	32	0.00	0.00	-12	-24.44	-19.56
76	24.44	19.50	31	- 0.56	- 0.44	-13	-25.00	-20.00
75 74	23.89	18.67	30	- 1.11	- 0.89	-13 -14	-25.56	-20.44
1	22.78	18.22	29	- 1.67	- 0.33 - 1.33	-15	-26.11	-20.44 -20.89
73 72	22.78	17.78	28	- 2.22	- 1.33 - 1.78	-16	-26.67	-20.33 -21.33
71	21.67	17.73	27	- 2.78	- 1.78 - 2.22	-17	-27.22	-21.78
70	21.11	16.89	26	- 3.33	- 2.67	-18	-27.78	-22.22
69	20.56	16.44	25	- 3.89	- 3.11	-19	-28.33	-22.67
68	20.00	16.00	24	- 4.44	- 3.56	-20	-28.S9	-23.11
67	19.44	15.56	23	- 5.00	- 4.00	-21	-29.44	-23.56
66	18.89	15.11	22	- 5.56	- 4.44	-22	-30.00	-24.00
65	18.33	14.67	21	- 6.11	- 4.89	-23	-30.56	-24.44
64	17.78	14.22	20	- 6.67	- 5.33	-24	-31.11	-24.89
63	17.22	13.78	19	- 7.22	- 5.78	-25	-31.67	-25.33
62	16.67	13.33	18	- 7.78	- 6.22	-26	-32.22	-25.78
61	16.11	12.89	17	- 8.33	- 6.67	-27	-32.78	-26.22
60	15.56	12.44	16	- 8.89	- 7.11	-28	-33.33	-26.67
59	15.00	12.00	15	- 9.44	- 7.56	-29	-33.S9	-27.11
58	14.44	11.56	14	-10.00	- 8.00	-30	-34.44	-27.56
57	13.89	11.11	13	-10.56	- 8.44	-31	-35.00	-28.00
56	13.33	10.67	12	-11.11	- 8.89	-32	-35.56	-28.44
55	12.78	10.22	11	-11.67	- 9.33	-33	-36.11	-28.89
54	12.22	9.78	10	-12-22	- 9.78	-34	-36.67	-29.33
53	11.67	9.33	9	-12.78	-10.22	-35	-37.22	-29.78
52	11.11	8.89	8	-13.33	-10.67	-36	-37.78	-30.22
51	10.56	8.44	7	-13.89	-11.11	-37	-38.33	-30.67
50	10.00	8.00	6	-14-44	-11.56	-38	-38.89	-31.11
49	9.44	7.56	5	-15.00	-12.00	-39	-39.44	-31.56
			For the C	entipuation se	a Table IV ar	d V		

For the Continuation see Table IV. and V.

II. COMPARISON OF THE CENTIGRADE THERMOMETER WITH REAUMUR'S AND FAHRENHEIT'S.

 x° Centig. = $(32 + \frac{9}{5} x^{\circ})$ Fahr. = $\frac{4}{5} x^{\circ}$ Reaum.

Centig.	Reaumur.	Fahrenheit.	Centig.	Reaumur.	Fahrenheit.	Centig.	Reaumur.	Fahrenheit.
+100	+80.0	+212.0	+83	+66.4	+181.4	+ 66	+52.8	+150.8
99	79.2	210.2	82	65.6	179.6	65	52.0	149.0
98	78.4	208.4	81	64.8	177.8	64	51.2	147.2
97	77.6	206.6	80	64.0	176.0	63	50.4	145.4
96	76.8	204.8	79	63.2	174.2	62	49.6	143.6
95	76.0	203.0	78	62.4	172.4	61	48.8	141.8
94	75.2	201.2	77	61.6	170.6	60	48.0	140.0
93	74.4	199.4	76	60.8	168.8	59	47.2	138.2
92	73.6	197.6	75	60.0	167.0	58	46.4	136.4
91	72.8	195.8	74	59.2	165.2	57	45.6	134.6
90	72.0	194.0	7 3	58.4	163.4	56	44.8	132.8
89	71.2	192.2	72	57.6	161.6	55	44.0	131.0
88	70.4	190.4	71	56.8	159.8	54	43.2	129.2
87	69.6	188.6	70	56.0	158.0	53	42.4	127.4
86	68.8	186.8	69	55.2	156.2	52	41.6	125.6
85	68.0	185.0	68	54.4	154.4	51	40.8	123.8
84	67.2	183.2	67	53.6	152.6	50	40.0	122.0

For the Continuation see Tables V. and VI.

III. COMPARISON OF REAUMUR'S THERMOMETER WITH FAHRENHEIT'S AND THE CENTIGRADE.

 x° Reaum. = $(32^{\circ} + \frac{9}{4} x^{\circ})$ Fahr. = $\frac{5}{4} x^{\circ}$ Centig.

Reaumur.	Fahrenheit.	Centigrade.	Reaumur.	Fahrenheit.	Centigrade.	Reaumur.	Fahrenheit.	Centigrade.
+80	+212.00	+100.00	+66	+180.50	+82.50	+52	+149.00	+65.00
79	209.75	98.75	65	178.25	81.25	51	146.75	63.75
78	207.50	97.50	64	176.00	80.00	50	144.50	62.50
77	205.25	96.25	63	173.75	78.75	49	142.25	61.25
76	203.00	95.00	62	171.50	77.50	48	140.00	60.00
75	200.75	93.75	61	169.25	76.25	47	137.75	58.75
7.1	198.50	92.50	60	167.00	75.00	46	135.50	57.50
73	196.25	91.25	59	164.75	73.75	45	133.25	56.25
72	194.00	90.00	58	162.50	72.50	44	131.00	55.00
71	191.75	88.75	57	160.25	71.25	43	128.75	53.75
70	189.50	87.50	56	158.00	70.00	42	126.50	52.50
69	187.25	86.25	55	155.75	68.75	41	124.25	51.25
68	185.00	85.00	54	153.50	67.50	40	122.00	50.00
67	182.75	83.75	53	151.25	66.25	39	119.75	48.75

For the Continuation see Tables VIII. and IX.

IV. - V.

COMPARISON

OF

FAHRENHEIT'S THERMOMETER

WITH

THE CENTIGRADE AND WITH THAT OF REAUMUR,

OR

TABLES

FOR CONVERTING THE DEGREES OF FAHRENHEIT INTO CENTIGRADE DEGREES AND INTO DEGREES OF REAUMUR;

Giving the corresponding values for each tenth of a degree, from $+122^{\circ}$ to -76° fahrenheit.



Degrees of					Tenths of	Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
1.100	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
+122	+50.00	+50.06	+50.11	+50.17	+50.22	+50.28	+50.33	+50.39	+50.44	+50.50
121	49.44	49.50	49.56	49.61	49.67	49.72	49.78	49.83	49.89	49.94
120	48.89	49.94	49.00	49.06	49.11	49.17	49.22	49.28	49.33	49.39
119	48.33	48.39	48.44	48.50	48.56	48.61	48.67	48.72	48.78	48.83
118	47.78	47.83	47.89	47.94	48.00	48.06	48.11	48.17	48.22	48.28
117	47.22	47.28	47.33	47.39	47.14	47.50	47.56	47.61	47.67	47.72
116	46.67	46.72	46.78	46.83	46.89	46.94	47.00	47.06	47.11	47.17
115	46.11	46.17	46.22	46.28	46.33	46.39	46.44	46.50	46.56	46.61
114	45.56	45.61	45.67	45.72	45.78	45.83	45.89	45.94	46.00	46.06
113	45.00	45.06	45.11	45.17	45.22	45.28	45.33	45.39	45.44	45.50
112	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.94
111	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.33	i
110	43.33	43.39	43.44	43.50	43.56	43.61	43.67	43.72	43.78	44.39 43.83
109	42.78	42.83	42.89	42.94	43.00	43.06	43.11	43.17	43.22	43.28
103	42.73	42.28	42.33	42.39		42.50	42.56	42.61		
103	42.22	42.25	42.55	42.39	42.44	42.50	42.50	42.01	42.67	42.72
107	41.67	41.72	41.78	41.83	41.89	41.94	42.00	42.06	42.11	42.17
106	41.11	41.17	41.22	41.28	41.33	41.39	41.44	41.50	41.56	41.61
105	40.56	40.61	40.67	40.72	40.78	40.83	40.89	40.94	41.00	41.06
104	40.00	40.06	40.11	40.17	40.22	40.28	40.33	40.39	40.44	40.50
103	39.44	39.50	39.56	39.61	39.67	39.72	39.78	39.83	39.89	39.94
102	38.89	90.04	20.00	90.00	00.77	39.17	39.22	39.28	39.33	00.00
102	li l	38.94	39.00	39.06	39.11	38.61	Ī	1		39.39
100	38.33	38.39	38.44	38.50	38.56		38.67	38.72 38.17	38.78	38.83
	37.78	37.83	37.89	37.94	38.00	38.06	38.11	1	38.22	38.28
99	37.22	37.28	37.33	37.39	37.44	37.50	37.56	37.61	37.67	37.72
98	36.67	36.72	36.78	36.83	36.89	36.94	37.00	37.06	37.11	37.17
97	36.11	36.17	36.22	36.28	36.33	36.39	36.44	36.50	36.56	36.61
96	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.06
95	35.00	35.06	35.11	35.17	35.22	35.28	35.33	35.39	35.44	35.50
94	34.44	34.50	34.56	34.61	34.67	34.72	34.78	34.83	34.89	34.94
93	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34.39
92	33.33	33.39	33.44	33.50	33.56	33.61	33.67	33.72	33.78	33.83
91	32.78	32.83	32.89	32.94	33.00	33.06	33.11	33.17	33.22	33.28
90	32.22	32.28	32.33	32.39	32.44	32.50	32.56	32.61	32.67	32.72
89	31.67	31.72	31.78	31.83	31.89	31.94	32.00	32.06	32.11	33.17
88	31.11	31.17	31.22	31.28	31.33	31.39	31.44	31.50	31.56	31.61
87	30.56	30.61	30.67	30.72	30.78	30.83	30.89	30.94	31.00	31.06
86	30.00	30.06	30.11	30.17	30.22	30.28	30.33	30.39	30.44	30.50
85	29.44	29.50	29.56	29.61	29.67	29.72	29.78	29.83	29.89	29.94
84 .	28.89	28.94	29.00	29.06	29.11	29.17	29.22	29.28	29.33	29.39
83	28.33	28.39	28.44	28.50	28.56	28.61	28.67	28.72	28.78	28.83
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
+82	Centig. +27.78	Centig. +27.83	Centig. +27.89	Centig. +27.94	Centig. +28.00	Centig. +28.06	Centig.	Centig. +28.17	Centig.	Centig.
81	27.22	27.28	27.33	27.39	27.44	27.50	+28.11 27.56	27.61	+28.22	+28.28
80	26.67	26.72	26.78	26.83	26.89	26.94	27.00	27.06	27.67	27.72 27.17
79	26.11	26.12	26.22	26.28	26.33	26.39	26.44	26.50	26.56	26.61
78	25.56	25.61	25.67	25.72	25.78	25.83	25.89	25.94	26.00	26.06
77	25.00	25.06	25.11	25.17	25.22	25.28	25.33	25.39	25.44	25.50
76	24.44	24.50	24.56	24.61	24.67	24.72	24.78	24.83	24.89	24.94
75	23.89	23.94	24.00	24.06	24.11	24.17	24.22	24.28	24.33	24.39
74	23.33	23.39	23.44	23.50	23.56	23.61	23.67	23.72	23.78	23.83
73	22.78	22.83	22.89	22.94	23.00	23.06	23.11	23.17	23.22	23.28
72	22.22	22.28	22.33	22.39	22.44	22.50	22.56	22.61	22.67	22.72
71	21.67	21.72	21.78	21.83	21.89	21.94	22.00	22.06	22.11	22.17
70	21.11	21.17	21.22	21.28	21.33	21.39	21.44	21.50	21.56	21.61
69	20.56	20.61	20.67	20.72	20.78	20.83	20.89	20.94	21.00	21.06
68	20.00	20.06	20.11	20.17	20.22	20.28	20.33	20.39	20.44	20.50
67	19.44	19.50	19.56	19.61	19.67	19.72	19.78	19.83	19.89	19.94
66	18.89	18.94	19.00	19.06	19.11	19.17	19.22	19.28	19.33	19.39
65	18.33	18.39	18.44	18.50	18.56	18.61	18.67	18.72	18.78	18.83
64	17.78	17.83	17.89	17.94	18.00	18.06	18.11	18.17	18.22	18.28
63	17.22	17.28	17.33	17.39	17.44	17.50	17.56	17.61	17.67	17.72
62	16.67	16.72	16.78	16.83	16.89	16.94	17.00	17.06	17.11	17.17
61	16.11	16.17	16.22	16.28	16.33	16.39	16.44	16.50	16.56	16.61
60	15.56	15.61	15.67	15.72	15.78	15.83	15.89	15.94	16.00	16.06
59	15.00	15.06	15.11	15.17	15.22	15.28	15.33	15.39	15.44	15.50
58	14.44	14.50	14.56	14.61	14.67	14.72	14.78	14.83	14.89	14.94
57	13.89	13.94	14.00	14.06	14.11	14.17	14.22	14.28	14.33	14.39
56	13.33	13.39	13.44	13.50	13.56	13.61	13.67	13.72	13.78	13.83
55	12.78	12.53	12.59	12.94	13.00	13.06	13.11	13.17	13.22	13.28
54	12.22	12.28	12.33	12.39	12.44	12.50	12.56	12.61	12.67	12.72
53	11.67	11.72	11.78	11.83	11.89	11.94	12.00	12.06	12.11	12.17
52	11.11	11.17	11.22	11.28	11.33	11.39	11.44	11.50	11.56	11.61
51	10.56	10.61	10.67	10.72	10.78	10.83	10.89	10.94	11.00	11.06
50	10.00	10.06	10.11	10.17	10.22	10.28	10.33	10.39	10.44	10.50
49	9.44	9.50	9.56	9.61	9.67	9.72	9.78	9.83	9.89	9.94
48	8.89	8.94	9.00	9.06	9.11	9.17	9.22	9.28	9.33	9.39
47	8.33	8.39	8.44	8.50	8.56	8.61	8.67	8.72	8.78	8.83
46	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.28
45	7.22	7.28	7.33	7.39	7.44	7.50	7.56	7.61	7.67	7.72
44	6.67	6.72	6.78	6.83	6.89	6.94	7.00	7.06	7.11	7.17
43	6.11	6.17	6.22	6.28	6.33	6.39	6.44	6.50	6.56	6.61
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of Fahren		Tenths of Degrees.										
heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
+42	Centig. +5.56	Centig. +5.61	Centig. +5.67	Centig. +5.72	Centig. +5.78	Centig. +5.83	Centig. +5.89	Centig. +5.94	Centig. +6.00	Centig. +6.06		
41	5.00	5.06	5.11	5.17	5.22	5.28	5.33	5.39	5.44	5.50		
40	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.83	4.89	4.94		
39	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39		
38	3.33	3.39	3.44	3.50	3.56	3.61	3.67	3.72	3.78	3.83		
37	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28		
36	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72		
35	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.17		
34	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61		
33	0.56	0.61	0.67	0.72	0.78	0.83	0.89	0.94	1.00	1.06		
32	0.00	0.06	0.11	0.17	0.22	0.28	0.33	0.39	0.44	0.50		
31	- 0.56	- 0.50	- 0.44	- 0.39	- 0.33	- 0.28	- 0.22	- 0.17	- 0.11	- 0.06		
30	- 1.11	- 1.06	- 1.00	- 0.94	- 0.89	- 0.83	- 0.78	- 0.72	- 0.67	- 0.61		
29	- 1.67	- 1.61	- 1.56	- 1.50	- 1.44	- 1.39	- 1.33	- 1.28	- 1.22	- 1.17		
28	- 2.22	- 2.17	- 2.11	- 2.06	- 2.00	- 1.94	- 1.89	- 1.83	- 1.78	1.72		
27	- 2.78	- 2.72	- 2.67	- 2.61	- 2.56	- 2. 50	- 2.44	- 2.39	- 2.33	- 2.28		
26	- 3.33	- 3.28	- 3.22	- 3.17	- 3.11	- 3.06	- 3.00	- 2.94	- 2.89	- 2. 83		
25	- 3.89	- 3.83	- 3.7 8	- 3.72	- 3.67	- 3.61	- 3.56	- 3.50	- 3.44	- 3.39		
24	- 4.44	4.39	- 4.33	- 4.28	- 4.22	- 4.17	- 4.11	- 4.06	- 4.00	- 3.94		
23	- 5.00	- 4.94	- 4.89	- 4.S3	- 4.7 8	- 4.72	- 4.67	- 4.61	→ 4.56	- 4.50		
22	- 5.56	- 5.50	- 5.44	- 5.39	- 5.33	- 5.28	- 5.22	- 5.17	- 5.11	- 5.06		
21	- 6.11	- 6.06	- 6.00	- 5.94	- 5.89	- 5.83	- 5.78	- 5.72	- 5.67	- 5.61		
20	- 6.67	- 6.61	- 6.56	- 6.50	- 6.44	- 6.39	- 6.33	- 6.28	- 6.22	- 6.17		
19	- 7.22	- 7.17	- 7.11	- 7.06	- 7.00	- 6.94	- 6.89	- 6.83	- 6.78	- 6.72		
18	- 7.78	- 7.72	- 7.67	- 7.61	- 7.56	- 7. 50	- 7.44	- 7.39	- 7.33	- 7.28		
17	- 8.33	- 8.28	- 8.22	- 8.17	- 8.11	- 8.06	- 8.00	- 7.94	- 7. 89	- 7.83		
16	- 8.89	- 8.83	- 8.78	- 8.72	- 8.67	- 8.61	- 8.56	- 8.50	- 8.44	- 8.39		
15	- 9.44	- 9.39	- 9.33	- 9.28	- 9.22	- 9.17	- 9.11	- 9.06	- 9.00	- 8.94		
14	-10.00	- 9.94	- 9.89	- 9.83 -10.39	- 9.78	-9.72	- 9.67	- 9.61	- 9.56	- 9.50		
13	-10.56	-11.50	-10.44	-10.39	-10.33	-10.28	-10.22	-10.17	-10.11	-10.06		
12	-11.11	-11.06	-11.00	-10.94	-10.89	-10.83	-10.78	-10.72	-10.67	-10.61		
11	-11.67	-11.61	-11.56	-11.50	-11.44	-11.39	-11.33	-11.28	-11.22	-11.17		
10	-12.22	-12.17	-12.11	-12.06	-12.00	-11.94	-11.89	-11.83	-11.78	-11.72		
9	-12.78	-12.72	-12.67	-12.61	-12.56	-12.50	-12.44	-12.39	-12.33	-12.28		
8	-13.33	-13.28	-13.22	-13.17	-13.11	-13.06	-13.00	-12.94	-12.89	-12.83		
7	-13.89	-13.83	-13.78	-13.72	-13.67	-13.61	-13.56	-13.50	-13.44	-13.39		
6	-14.44	-14.39	-14.33	-14.28	-14.22	-14.17	-14.11	-14.06	-14.00	-13.94		
5	-15.00	-14.94	-14.89	-14.83	-14.78	-14.72	-14.67	-14.61	-14.56	-14.50		
4	-15.56	-15.50	-15.44	-15.39	-15.33	-15.28	-15.22	-15.17	-15.11	-15.06		
3	-16.11	-16.06	-16.00	-15.94	-15.89	-15.83	-15.78	-15.72	-15.67	-15.61 		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Degrees of Fahren-					Tenths of	f Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig. -16.50.	Centig.	Centig. -16.39	Centig. -16.33	Centig16.28	Centig.	Centig. -16.17
+ 2	-16.67 -17.22	-16.61 -17.17	-16.56 -17.11	-17.06	-16.44 -17.00	$\begin{bmatrix} 16.39 \\ -16.94 \end{bmatrix}$	-16.89	-16.25 -16.83	-16.22 -16.78	-16.72
0	-17.22 -17.78	-17.77 -17.72	-17.11 -17.67	-17.61	-17.56	-17.50	-17.44	-17.39	-17.33	-17.28
- 0	-17.78	-17.S3	-17.89	-17.94	-18.00	-18.06	-18.11	-18.17	-18.22	-18.28
- 1	-18.33	-18.39	-18.44	-18.50	-18.56	-18.61	-18.67	-18.72	-18.78	-18.83
- 2	-18.89	-18.94	-19.00	-19.06	-19.11	-19.17	-19.22	-19.28	-19.33	-19.39
- 3	-19.44	-19.50	-19.56	-19.61	-19.67	-19.72	-19.78	-19.83	-19.89	-19.94
- 4	-20.00	-20.06	-20.11	-20.17	-20.22	-20.28	-20.33	-20.39	-20.44	-20.50
- 5	-20.56	-20.61	-20.67	-20.72	-20.78	-20.83	-20.89	-20.94	-21.00	-21.06
- 6	-21.11	-21.17	-21.22	-21.28	-21.33	-21.39	-21.44	-21.50	-21.56	-21.61
- 7	-21.67	-21.72	-21.78	-21.83	-21.89	-21.94	-22.00	-22.06	-22.11	-22.17
- 8	-22.22	-22.28	-22.33	-22.39	-22.44	-22.50	-22.56	-22.61	-22.67	-22.72
- 9	-22.78	-22.83	-22.89	-22.94	-23.00	-23.06	-23.11	-23.17	-23.22	-23.28
-10	-23.33	-23.39	-23.44	-23.50	-23.56	-23.61	-23.67	-23.72	-23.78	-23.83
-11	-23.89	-23.94	-24.00	-24.06	-24.11	-24.17	-24.22	-24.28	-24.33	-24.39
-12	-24.44	-24.50	-24.56	-24.61	-24.67	$\frac{1}{10}$ 24.72	-24.78	-24.83	-24.89	-24.94
-13	-25.00	-25.06	-25.11	-25.17	-25.22	-25.28	-25.33	-25.39	-25.44	-25.50
-14	-25.56	-25.61	-25.67	-25.72	-25.78	-25.83	-25.89	-25.94	-26.00	-26.06
-15	-26.11	-26.17	-26.22	-26.28	-26.33	-26.39	-26.44	-26.50	-26.56	-26.61
-16	-26.67	-26.72	-26.78	-26.S3	-26.S9	-26.94	-27.00	-27.06	-27.11	-27.17
-17	-27.22	-27.28	-27.33	-27.39	-27.44	-27.50	-27.56	-27.61	-27.67	-27.72
-18	-27.78	-27.S3	-27.89	-27.94	-28.00	-28.06	-28.11	-28.17	-28.22	-28.28
-19	-28.33	-28.39	-28.44	-28.50	-28.56	-28.61	-28.67	-28.72	-28.78	-28.83
-20	-28.89	-28.94	-29.00	-29.06	-29.11	-29.17	-29.22	-29.28	-29.33	-29.39
-21	-29.44	-29.50	-29.56	-29.61	-29.67	-29.72	-29.78	-29.83	-29.89	-29.94
-22	-30.00	-30.06	-30.11	-30.17	-30.22	-30.28	-30.33	-30.39	-30.44	-30.50
-23	-30.56	-30.61	-30.67	-30.72	-30.78	-30.83	-30.89	-30.94	-31.00	-31.06
-24	-31.11	-31.17	-31.22	-31.28	-31.33	-31.39	-31.44	-31.50	-31.56	-31.61
-25	-31.67	-31.72	-31.78	-31.83	-31.S9	-31.94	-32.00	-32.06	-32.11	-32.17
-26	-32.22	-32.28	-32.33	-32.39	-32.44	-32.50	-32.56	-32.61	-32.67	-32.72
-27	-32.78	-32.83	-32.89	-32.94	-33.00	-33.06	-33.11	-33.17	-33.22	-33.28
-28	-33.33	-33.39	-33.44	-33.50	-33.56	-33.61	-33.67	-33.72	-33.78	-33.83
-29	-33.89	-33.94	-34.00	-34.06	-34.11	-34.17	-34.22	-34.28	-34.33	-34.39
-30	-34.44	-34.50	-34.56	-34.61	-34.67	-34.72	-34.78	-34.83	-34.89	-34.94
-31	-35.00	-35.06	-35.11	-35.17	-35.22	-35.28	-35.33	-35.39	-35.44	-35.50
-32	-35.56	-35.61	-35.67	-35.72	-35.78	-35.83	-35.89	-35.94	-36.00	-36.06
-33	-36.11	-36.17	-36.22	-36.28	-36.33	-36.39	-36.44	-36.50	-36.56	-36.61
-31	-36.67	-36.72	-36.78	-36.S3	-36.89	-36.94	-37.00	-37.06	-37.11	-37.17
-35	-37.22	-37.28	-37.33	-37.39	-37.44	-37.50	-37.56	-37.61	-37.67	-37.72
-36	-37.78	-37.S3 	-37.89 	-37.94	-38.00 	-38.06 	-38.11	-38.17 	-38.22 	-38.28
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Degrees of Fahren-	Tenths of Degrees.										
heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	
-37	-38.33	-38.39	-38.44	-38.50	-38.56	-38.61	-38.67	-38.72	-38.78	-38.83	
-38	-38.89	-38.94	-39.00	-39.06	-39.11	-39.17	-39.22	-39.28	-39.33	-39.39	
-39	-39.14	-39.50	-39.56	-39.61	-39.67	-39.72	-39.78	-39.83	-39.89	-39.94	
-40	-40.00	-40.06	-40.11	-40.17	-40.22	-40.28	-40.33	-40.39	-40.44	-40.50	
-41	-40.56	-40.61	-40.67	-40.72	-40.78	-40.83	-40.89	-40.94	-41.00	-41.06	
-42	-41.11	-41.17	-41.22	-41.28	-41.33	-41.39	-41.44	-41.50	-41.56	-41.61	
-43	-41.67	-41.72	-41.78	-41.83	-41.89	-41.94	-42.00	-42.06	-42.11	-42.17	
-44	-42.22	-42.28	-42.33	-42.39	-42.44	-42.50	-42.56	-42.61	-42.67	-42.72	
-45	-42.78	-42.83	-42.89	-42.94	-43.00	-43.06	-43.11	-43.17	-43.22	-43.28	
-46	-43.33	-43.39	-43.44	-43.50	-43.56	-43.61	-43.67	-43.72	-43.78	-43.83	
-47	-43.89	-43.94	-44.00	-44.06	-44.11	-44.17	-44.22	-44.28	-44.33	-44.39	
-48	-44.44	-44.50	-44.56	-44.61	-14.67	-44.72	-44.78	-44.83	-44.89	-44.94	
-49	-45.00	-45.06	-45.11	-45.17	-45.22	-45.28	-45.33	-45.39	-45.44	-45.50	
-50	-45.56	-45.61	-45.67	-45.72	-45.78	-45.83	-45.89	-45.94	-46.00	-46.06	
-51	-46.11	-46.17	-46.22	-46.28	-46.33	-46.39	-46.44	-46.50	-46.56	-46.61	
7 0			10.00		10.00	10.01		1= 00			
-52	-46.67	-46.72	-46.78	-46.83	-46.89	-46.94	-47.00	-47.06	-47.11	-47.17	
-53	-47.22	-47.28	-47.33	-47.39	-47.44	-47.50	-47.56	-47.61	-47.67	-47.72	
-54 -55	-47.78 -48.33	-47.83	-47.89 -48.44	-17.94	-48.00	-48.06 -48.61	-48.11	-48.17 -48.72	-48.22 -48.78	-48.28 -48.83	
-56	-48.89	-48.39 -48.94	-49.00	-48.50 -49.06	-48.56 -49.11	-45.01 -49.17	-48.67 -49.22	-49.28	-49.33	-49.39	
-50	-40.09	-40.94	-49.00	-49.00	-49.11	-45.17	-49.22	-43.20	-45.55	-43.03	
-57	-49.44	-49.50	-49.56	-49.61	-49.67	-49.72	-49.78	-49.83	-49.89	-49.94	
-58	-50.00	-50.06	-50.11	-50.17	-50.22	-50.28	-50.33	-50.39	-50.44	-50.50	
-59	-50.56	-50.61	-50.67	-50.72	-50.78	-50.83	-50.89	-50.94	-51.00	-51.06	
-60	-51.11	-51.17	-51.22	-51.28	-51.33	-51.39	-51.44	-51.50	-51.56	-51.61	
-61	-51.67	-51.72	-51.78	-51.83	-51.S9	-51.94	-52.00	-52.06	-52.11	-52.17	
-62	-52.22	-52.28	-52.33	-52.39	-52.44	-52.50	-52.56	-52.61	-52.67	-52.72	
-63	-52.78	-52.83	-52.89	-52.94	-53.00	-53.06	-53.11	-53.17	-53.22	-53.28	
-64	-53.33	-53.39	-53.44	-53.50	-53.56	-53.61	-53.67	-53.72	-53.78	-53.83	
-65	-53.89	-53.94	-54.00	-54.06	-54.11	-54.17	-54.22	-54.28	-54.33	-54.39	
-66	-54.44	-54.50	-54.56	-54.61	-54.67	-54.72	-54.78	-54.83	-54.89	-54.94	
-67	_55.00	-55.06	55 11	25.15	_57.00	55.00	_55 99	-55.39	-55.44	-55.50	
-67 -68	-55.00 -55.56	-55.61	-55.11 -55.67	-55.17 -55.72	-55.22 -55.78	-55.28 -55.83	-55.33 -55.89	-55.94	-56.00	-56.06	
-69	-56.11	-56.17	-56.22	-56.28	-56.33	-56.39	-56.44	-56.50	-56.56	-56.61	
-70	-56.67	-56.72	-56.22 -56.78	-56.83	-56.89	-56.94	-57.00	-57.06	-57.11	-57.17	
-70 -71	-57.22	-50.72 -57.28	-57.33	-57.39	ı	-57.50	-57.56	-57.61	-57.67	-57.72	
	1	1				i					
-72	-57.78	-57.83	-57.89	-57.94	-58.00	-58.06	-58.11	-58.16	-58.22	-58.28	
-7 3	-58.33	-58.39	-58.44	-58.50	-58.56	-58.61	-58.67	-58.72	-58.78	-58.83	
-74	-58.89	-58.94	-59.00	-59.06	-59.11	-59.17	-59.22	-59.28	-59.33	-59.39	
-75 -76	$\begin{vmatrix} -59.44 \\ -60.00 \end{vmatrix}$	-59.50 -60.06	-59.56 -60.11	-59.61 -60.17	-59.67 -60.22	-59.72 -60.28	-59.78 -60.33	-59.83 -60.39	-59.89 -60.44	-59.94 -60.50	
		ļ	ļ 			1	-		l	ļ	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

Degrees of	Tenths of a Degree.												
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
+122	Reaumur. +40.00	Reaumur. +40.04	Reaumur. +40.09	Reaumur. +40,13	Reaumur +40.18	Reaumur. +40.22	Reaumur. +40.27	Reaumur. +40.31	Reaumur. +40.36	Reaumu +40,40			
	II.	!					l	i .	1				
121	39.56	39.60	39.64	39.69	39.73	39.78	39.82	39.87	39.91	39.96			
120	39.11	39.16	39.20	39.24	39.29	39.33	39.38	39.42	39.47	39.51			
119	38.67	38.71	38.76	38.80	38.84	38.89	38.93	38.98	39.02	39.07			
118	38.22	38.27	38.31	38.36	38.40	38.44	38.49	38.53	38.58	38.62			
117	37.78	37 82	37.87	37.91	37.96	38.00	38.04	38.09	38.13	38.18			
116	37.33	37.38	37.42	37.47	37.51	37.56	37.60	37.64	37.69	37.7			
115	36.89	36.93	36.98	37.02	37.07	37.11	37.16	37.20	37.24	37.2			
114	36.44	36.49	36.53	36.58	36.62	36.67	36.71	36.76	36.80	36.S			
113	36.00	36.04	36.09	36.13	36.18	36.22	36.27	36.31	36.36	36.4			
112	35.56	35.60	35.64	35.69	35.73	35.78	35.S2	35.87	35.91	35.9			
111	35.11	35.16	35.20	35.24	35.29	35.33	35,38	35.42	35.47	35.5			
110	34.67	34.71	34.76	34.80	34.84	34.89	34.93	34.98	35.02	35.0			
109	34.22	34.27	34.31	34.36	34.40	34.44	34.49	34.53	34.58	34.6			
108	33.78	33.82	33.87	33.91	33.96	34.00	34.04	34.09	34.13	34.1			
107	33.33	33.38	33.42	33.47	33.51	33.56	33.60	33.64	33.69	33.7			
106	32.89	32.93	32.98	33.02	33.07	33.11	33.16	33.20	33.24	33.2			
105	32.44	32.49	32.53	32.58	32.62	32.67	32.71	32.76	32.80	32.8			
104	32.00	32.04	32.09	32.13	32.18	32.22	32.27	32.31	32.36	32.4			
103	31.56	31.60	31.64	31.69	31.73	31.78	31.82	31.87	31.91	31.9			
100	01.11	91 10	01.00	01.04	21.00	01.00	91 90	91.40	01.47	01.7			
102	31.11	31.16	31.20	31.24	31.29	31.33	31.38	31.42	31.47	31.5			
101	30.67	30.71	30.76	30.80	30.84	30.89	30.93	30.98	31.02	31.0			
100	30.22	30.27	30.31	30.36	30.40	30.44	30.49	30.53	30.58	30.6			
99	29.78	29.82	29.87	29.91	29.96	30.00	30.04	30.09	30.13	30.1			
98	29.33	29.38	29.42	29.47	29.51	29.56	29.60	29.64	29.69	29.7			
97	28.89	28.93	28.98	29.02	29.07	29.11	29.16	29.20	29.24	29.2			
96	28.44	28.49	28.53	28.58	28.62	28.67	28.71	28.76	28.80	28.8			
95	28.00	28.04	28.09	28.13	28.18	28.22	28.27	28.31	28.36	28.4			
94	27.56	27.60	27.64	27.69	27.73	27.78	27.S2	27.87	27.91	27.9			
93	27.11	27.16	27.20	27.24	27.29	27.33	27.38	27.42	27.47	27.5			
92	26.67	26.71	26.76	26.80	26.84	26.89	26.93	26.98	27.02	27.0			
91	26.22	26.27	26.31	26.36	26.40	26.44	26.49	26.53	26.58	26.6			
90	25.78	25.82	25.87	25.91	25.96	26.00	26.04	26.09	26.13	26.1			
89	25.33	25.38	25.42	25.47	25.51	25.56	25.60	25.64	25.69	25.7			
88	24.89	24.93	24.98	25.02	25.07	25.11	25.16	25.20	25.24	25.2			
87	24.44	24.49	24.53	9150	2160	24.67	91 71	24.76	91 60	24.8			
86	24.44	24.49		24.58	24.62		24.71	1	24.80				
	li i		24.09	24.13	24.18	24.22	24.27	24.31	24.36	24.4			
85	23.56	23.60	23.64	23.69	23.73	23.78	23.82	23.87	23.91	23.9			
81	23.11	23.16	23.20	23.24	23.29	23.33	23.38	23.42	23.47	23.5			
83 82	$22.67 \\ 22.22$	22.71 22.27	$22.76 \\ 22.31$	22.S0 22.36	$22.84 \ 22.40$	22.S9 22.44	22.93 22.49	22.98 22.53	$23.02 \\ 22.58$	23.0° 22.6°			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

Degrees of		Tenths of a Degree.											
Fahren- heit.	0.	. 1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Reaumur.	Reaumur.	1	Reaumur.	1			1	Reaumur.				
+81	+21.78	+21.82	+21.87	+21.91	+21.96	+22.00	+22.04	+22.09	+22.13	+22.18			
80	21.33	21.38	21.42	21.47	21.51	21.56	21.60	21.64	21.69	21.73			
79	20.89	20.93	20.98	21.02	21.07	21.11	21.16	21.20	21.24	21.29			
78	20.44	20.49	20.53	20.58	20.62	20.67	20.71	20.76	20.80	20.84			
77	20.00	20.04	20.09	20.13	20.18	20.22	20.27	20.31	20.36	20.40			
76	19.56	19.60	19.64	19.69	19.73	19.78	19.82	19.87	19.91	19.96			
75	19.11	19.16	19.20	19.24	19.29	19.33	19.38	19.42	19.47	19.51			
74	18.67	18.71	18.76	18.80	18 84	18.89	18.93	18.98	19.02	19.07			
73	18.22	18.27	18.31	18.36	18.40	18.44	18.49	18.53	18.58	18.62			
72	17.78	17.82	17.87	17.91	17.96	18.00	18.04	18.09	18.13	18.18			
71	17.33	17.38	17.42	17.47	17.51	17.56	17.60	17.64	17.69	17.73			
70	16.89	16.93	16.98	17.02	17.07	17.11	17.16	17.20	17.24	17.29			
69	16.44	16.49	16.53	16.58	16.62	16.67	16.71	16.76	16.80	16.84			
68	16.00	16.04	16.09	16.13	16.18	16.22	16.27	16.31	16.36	16.40			
67	15.56	15.60	15.64	15.69	15.73	15.78	15.82	15.87	15.91	15.96			
66	15.11	15.16	15.20	15.24	15.29	15.33	15.38	15.42	15.47	15.51			
65	14.67	14.71	14.76	14.80	14.84	14.89	14.93	14.98	15.02	15.07			
64	14.22	14.27	14.31	14.36	14.40	14.44	14.49	14.53	14.58	14.62			
63	13.78	13.82	13.87	13.91	13 96	14.00	14.04	14.09	14.13	14.18			
62	13.33	13.38	13.42	13.47	13.51	13.56	13.60	13.64	13.69	13.73			
61	12.89	12.93	12.98	13.02	13.07	13.11	13.16	13.20	13.24	13.29			
60	12.44	12.49	12.53	12.58	12.62	12.67	12.71	12.76	12.80	12.84			
59	12.00	12.04	12.09	12.13	12.18	12.22	12.27	12.31	12.36	12.40			
58	11.56	11.60	11.64	11.69	11.73	11.78	11.82	11.87	11.91	11.96			
57	11.11	11.16	11.20	11.24	11.29	11.33	11.38	11.42	11.47	11.51			
56	10.67	10.71	10.76	10.80	10.84	10.89	10.93	10.98	11.02	11.07			
55	10.22	10.27	10.31	10.36	10.40	10.44	10.49	10.53	10.58	10.62			
54	9.78	9.82	9.87	9.91	9.96	10.00	10.04	10.09	10.13	10.18			
53	9.33	9.38	9.42	9.47	9.51	9.56	9.60	9.64	9.69	9.73			
52	8.89	8.93	8.98	9.02	9.07	9.11	9.16	9.20	9.24	9.29			
51	8.44	8.49	8.53	8.58	8.62	8.67	8.71	8.76	8.80	8.84			
50	8.00	8.04	8.09	8.13	8.18	8.22	8.27	8.31	8.36	8.40			
49	7.56	7.60	7.64	7.69	7.73	7.78	7.82	7.87	7.91	7.96			
48	7.11	7.16	7.20	7.24	7.29	7.33	7.38	7.42	7.47	7.51			
47	6.67	6.71	6.76	6.80	6.84	6.89	6.93	6.98	7.02	7.07			
46	6.22	6.27	6.31	6.36	6.40	6.44	6.49	6.53	6.58	6.62			
45	5.78	5.82	5.87	5.91	5.96	6.00	6.04	6.09	6.13	6.18			
44	5 33	5.38	5.42	5.47	5.51	5.56	5.60	5.64	5.69	5.73			
43	4.89	4.93	4.98	5.02	5.07	5.11	5.16	5.20	5.24	5.29			
42	4.44	4.49	4.53	4.58	4.62	4.67	4.71	4.76	4.80	4.84			
41	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.31	4.36	4.40			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

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Degrees of		Tenths of a Degree.										
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.		
+40	+ 3.56	+ 3.60	+ 3.64	+ 3.69	+ 3.73	+ 3.78	+ 3.82	+ 3.87	+ 3.91	+ 3.96		
39	3.11	3.16	3.20	3.24	3.29	3.33	3.38	3.42	3.47	3.51		
38	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07		
37	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.53	2.58	2.62		
36	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.13	2.18		
35	1.33	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73		
34	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29		
33	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84		
32	0.00	0.04	0.09	0.13	0.18	0.22	0.27	0.31	0.36	0.40		
31	- 0.44	- 0.40	- 0.36	- 0.31	- 0.27	- 0.22	- 0.1S	- 0.13	- 0.09	- 0.04		
30	- 0.89	- 0.84	- 0.80	- 0.76	- 0.71	- 0.67	- 0.62	- 0.58	- 0.53	- 0.49		
29	- 1.33	- 1.29	- 1.24	- 1.20	- 1.16	- 1.11	- 1.07	- 1.02	- 0.98	- 0.93		
28	- 1.78	- 1.73	- 1.69	- 1.64	- 1.60	- 1.56	- 1.51	- 1.47	- 1.42	- 1.38		
27	- 2.22	- 2.18	- 2.13	- 2.09	- 2.04	- 2.00	- 1.96	- 1.91	- 1.87	- 1.82		
26	- 2.67	- 2.62	- 2.58	- 2.53	- 2.49	- 2.44	- 2.40	- 2.36	- 2.31	- 2.27		
25	- 3.11	- 3.07	- 3.02	- 2.98	- 2.93	-2.89	- 2.84	- 2.80	- 2.76	-2.71		
24	- 3.56	- 3.51	- 3.47	- 3.42	- 3.38	- 3.33	- 3.29	- 3.24	- 3.20	- 3.16		
23	- 4.00	- 3.96	- 3.91	- 3.87	- 3.82	- 3.78	- 3.73	- 3.69	- 3.64	- 3.60		
22	- 4.44	- 4.40	- 4.36	- 4.31	- 4.27	-4.22	- 4.18	- 4.13	- 4.09	- 4.04		
21	- 4.89	- 4.84	- 4.SO	- 4.76	- 4.71	- 4.67	- 4.62	- 4.58	- 4.53	- 4.49		
20	- 5.33	- 5.29	- 5.24	- 5.20	- 5.16	- 5.11	- 5.07	- 5.02	- 4.98	- 4.93		
19	- 5.78	- 5.73	- 5.69	- 5.64	- 5.60	- 5.56	- 5.51	- 5.47	- 5.42	- 5.38		
18	- 6.22	- 6.18	- 6.13	- 6.09	- 6.04	- 6.00	- 5.96	- 5.91	- 5.87	- 5.82		
17	- 6.67	- 6.62	- 6.58	- 6.53	- 6.49	- 6.44	- 6.40	- 6.36	- 6.31	- 6.27		
16	7.11	7.07	- 7. 02	- 6.98	- 6.93	- 6.89	- 6.84	- 6.80	- 6.76	- 6.71		
15	- 7.56	- 7.51	- 7.47	- 7.42	- 7.3 8	- 7.33	- 7.29	- 7.24	- 7.20	- 7.16		
14	- 8.00	- 7.96	- 7.91	- 7.S7	- 7.S2	- 7.7 8	- 7.73	- 7.69	- 7.64	- 7.60		
13	- 8.14	- 8.40	- 8.36	- S.31	- 8.27	- S.22	- 8.18	- 8.13	- 8.09	- 8.04		
12	- 8.89	- 8.84	- 8.80	- 8.76	- 8.71	- 8.67	- 8.62	- 8.58	- 8.53	- 8.49		
11	- 9.33	- 9.29	- 9.24	- 9.20	- 9.16	- 9.11	- 9.07	- 9.02	- 8.98	- 8.93		
10	- 9.78	- 9.73	- 9.69	- 9.64	- 9.60	- 9.56	- 9.51	- 9.47	- 9.42	- 9.38		
9	-10.22	-10.18	-10.13	-10.09	-10.04	-10.00	- 9.96	- 9.91	- 9.87	- 9.82		
S	-10.67	-10.62	-10.58	-10.53	-10.49	-10.44	-10.40	-10.36	-10.31	-10.27		
7 6	-11.11 -11.56	-11.07 -11.51	-11.02 -11.47	-10.98 -11.42	-10.93 -11.38	-10.89 -11.33	-10.84 -11.29	-10.80 -11.24	$\begin{bmatrix} -10.76 \\ -11.20 \end{bmatrix}$	-10.71 -11.16		
5	-12.00	-11.96	-11.91	-11.87	-11.82	-11.78	-11.7 3	-11.69	-11.64	-11.60		
4	-12.44	-12.46	-12.36	-12.31	-12.27	-12.22	-12.18	-12.13	-12.09	-12.04		
3	-12.89	-12.84	-12.80	-12.76	-12.71	-12.67	-12.62	-12.58°	-12.53	-12.49		
2	-13.33	-13.29	-13.24	-13.20	-13.16	-13.11	-13.07	-12.02	-12.98	-12.93		
1	-13.78	-13.73	-13.69	-13.64	-13.60	-13.56	-13.51	-13.47	-13.42	-13.38		
+ 0	-14.22	-14.18	-14.13	-14.09	-14.04	-14.00	-13.96	-13.91	-13.S7	-13.82		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Degrees of		Tenths of a Degree.										
Fahren- he it.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur		
- 0	-14.22	-14.27	-14.31	-14.36	-14.40	-14.44	-14.49	-14.53	-14.58	-14.62		
- 1	-14.67	-14.71	-14.76	-14.80	-14.84	-14.89	-14.93	-14.98	-15.02	-15.07		
- 2	-15.11	-15.16	-15.20	-15.24	-15.29	-15.33	-15.38	-15.42	-15.47	-15.51		
- 3	-15.56	-15.60	-15.64	-15.69	-15.73	-15.78	-15.82	-15.87	-15.91	-15.96		
- 4	-16.00	-16.04	-16.09	-16.13	-16.18	-16.22	-16.27	-16.31	-16.36	-16.40		
- 5	-16.44	-16.49	-16.53	-16.58	-16.62	-16.67	-16.71	-16.76	-16.80	-16.84		
- 6	-16.89	-17.93	-16.98	-17.02	-17.07	-17.11	-17.16	-17.20	-17.24	-17.29		
- 7	-17.33	-17.38	-17.42	-17.47	-17.51	-17.56	-17.60	-17.64	-17.69	-17.73		
- 8	-17.78	-18.82	-17.87	-17.91	-17.96	-18.00	-18.04	-18.09	-18.13	-18.18		
- 9	-18.22	-18.27	-18.31	-18.36	-18.40	-18.44	-18.49	-18.53	-18.58	-18.62		
-10	-18.67	-18.71	-18.76	-18.80	-18.84	-18.89	-18.93	-18.98	-19.02	-19.07		
-11	-19.11	-19.16	-19.20	-19.24	-19.29	-19.33	-19.38	-19.42	-19.47	-19.51		
-12	-19.56	-19.60	-19.64	-19.69	-19.73	-19.78	-19.82	-19.87	-19.91	-19.96		
-13	-20.00	-20.04	-20.09	-20.13	-20.18	-20.22	-20.27	-20.31	-20.36	-20.40		
-14	-20.44	-20.49	-20.53	-20.58	-20.62	-20.67	-20.71	-20.76	-20.80	-20.84		
-15	-20.89	-20.93	-20.98	-21.02	-21.07	-21.11	-21.16	-21.20	-21.24	-21.29		
-16	-21.33	-21.38	-21.42	-21.47		-21.56	-21.60	-21.64	-21.69	-21.73		
-17	-21.78	-21.82	-21.87	-21.91	-21.96	-22.00	-22.04	-22.09	-22.13	-22.18		
-18	-22.22	-22.27	-22.31	-22.36	-22.40	-22.44	-22.49	-22.53	-22.58	-22.62		
-19	-22.67	-22.71	-22.76	-22.80	-22.84	-22.89	-22.93	-22.98	-23.02	-23.07		
-20	-23.11	-23.16	-23.20	-23.24	-23.29	-23,33	-23.38	-23.42	-23.47	-23.51		
-20 -21	-23.11 -23.56	-23.16 -23.60	-23.20 -23.64	-23.24 -23.69	-23.29 -23.73	-23.78	-23.82	-23.42 -23.87	-23.47 -23.91	-23.96		
-21 -22	-23.90 -24.00	-23.00 -24.04	-23.04 -24.09	-23.09 -24.13	-23.13 -24.18	-23.78 -24.22	-24.27	-23.37 -24.31	-24.36	-24.40		
-22 -23	-24.00 -24.44	-24.49	-24.09 -24.53	-24.13 -24.58	-24.13 -24.62	-24.67	-24.71	-24.76	-24.80	-24.84		
-24	-24.89	-24.49 -24.93	-24.98	-25.02	-25.07	-25.11	-25.16	-25.20	-25.24	-25.29		
-25	-25.33	-25.38	-25.42	-25.47	- 25.51	25.50	-25.60	-25.64	-25.69	-25.73		
-25 -26	-25.78	-25.85 -25.82	-25.42 -25.87	-25.47 -25.91	-25.96	-25.56 -26.00	-26.04	-26.09	-26.13	-26.18		
-20 -27	-26.22	-25.82 -26.27	-26.31	-26.36	-26.40	-26.44	-26.49	-26.53	-26.13 -26.58	-26.62		
-28	-26.22 -26.67	-26.27 -26.71	-26.31 -26.76	-26.80	-26.40 -26.84	-26.44 -26.89	-26.49 -26.93	-26.98	-20.93 -27.02	-27.07		
-29	-27.11	-20.71. -27.16	$\begin{bmatrix} -26.76 \\ -27.20 \end{bmatrix}$	-27.24	-20.34 -27.29	-27.33	-27.38	-20.33 -27.42	-27.47	-27.51		
	07.70	n= 00	25.01	0= 00	25.40	0* *0	0 = 00	07 07	97.01	0= 0C		
-30 -31	-27.56 -28.00	-27.60	-27.64	$-27.69 \\ -28.13$	-27.73	-27.78	-27.82 -28.27	-27.87 -28.31	-27.91 -28.36	-27.96 -28.40		
-31 -32	-28.00 -28.44	-28.04 -28.49		-28.13 -28.58	-28.18 -28.62	-28.22	-28.27 -28.71	-28.31 -28.76	-28.80	-28.40 -28.84		
-32 -33	-28.89	-28.49 -28.93	-28.53 -28.98	$-28.58 \\ -29.02$	-28.62 -29.07	-28.67 -29.11	-28.71 -29.16	-28.76 -29.20	-25.80 -29.24	-29.29		
-34	-29.33	-28.93 -29.38	-28.98 -29.42	-29.02 -29.47	-29.07 -29.51	-29.11 -29.56	-29.16 -29.60	-29.20 -29.64	-29.24 -29.69	-29.29 -29.73		
95	20. 70	20.22					00.04	90.00	00.10	90-10		
-35	-29.78	-29.82		-29.91	-29.96	-30.00	-30.04	-30.09	-30.13	-30.18		
-36 -37	-30.22	-30.27	-30.31	-30.36	-30.40	-30.44	-30.49	-30.53	-30.58	-30.62		
-37	-30.67	-30.71	-30.76	-30.80	-30.84	-30.89	-30.93	-30.98	-31.02	-31.07		
-38	-31.11	-31.16	-31.20	-31.24	-31.29	-31.33	-31.38	-31.42	-31.47	-31.51 -21.0 <i>c</i>		
-39 -40	$-31.56 \\ -32.00$	-31.60 -30.04	-31.64 -30.09	-31.69 -30.13	-31.73 -30.18	-31.78 -30.22	-31.82 -30.27	-31.87 -30.31	-31.91 -30.36	-31.96 -30.40		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		



VI.-VII.

COMPARISON

OF

THE CENTIGRADE THERMOMETER

WITH

THE THERMOMETERS OF FAHRENHEIT AND OF REAUMUR,

OR

TABLES

FOR CONVERTING CENTIGRADE DEGREES INTO DEGREES OF FAHRENHEIT AND OF REAUMUR;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM $+50^{\circ}$ TO -54° CENTIGRADE.

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	Tenths of Degrees.										
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	
+50	+122.00	+122.18	1		+122.72			+123.26	+123.44	+123.62	
49	120.20	120.38	120.56	120.74	120.92	121.10	121.28	121.46	121.64	121.82	
48	118.40	118.58	118.76	1	119.12	119.30	119.48	119.66	119.84	120.02	
47	116.60	116.78	116.96	117.14	117.32	117.50	117.68	117.86	118.04	118.22	
46	114.50	114.98	115.16	115.34	115.52	115.70	115.88	116.06	116.24	116.42	
45	113.00	113.18	113.36	113.54	113.72	113.90	114.08	114.26	114.44	114.62	
44	111.20	111.38	111.56	111.74	111.92	112.10	112.28	112.46	112.64	112.82	
43	109.40	109.58	109.76	109.94	110.12	110.30	110.48	110.66	110.84	111.02	
42	107.60	107.78	107.96	108.14	108.32	108.50	108.68	108.86	109.04	109.22	
41	105.80	105.98	106.16	106.34	106.52	106.70	106.58	107.06	107.24	107.42	
40	104.00	104.18	104.36	104.54	104.72	104.90	105.08	105.26	105.44	105.62	
39	102.20	102.38	102.56	102.74	102.92	103.10	103.28	103.46	103.64	103.82	
38	100.40	100.58	100.76	100.94	101.12	101.30	101.48	101.66	101.84	102.02	
37	98.60	98.78	98.96	99.14	99.32	99.50	99.68	99.86	100.04	100.22	
36	96.80	96.98	97.16	97.34	97.52	97.70	97.88	98.06	98.24	98.42	
35	95.00	95.18	95.36	95.54	95.72	95.90	96.08	96.26	96.44	96.62	
34	93.20	93.38	93.56	93.74	93.92	94.10	94.28	94.46	94.64	94.83	
33	91.40	91.58	91.76	91.94	92.12	92.30	92.48	92.66	92.84	93.02	
32	89.60	89.78	89.96	90.14	90.32	90.50	90.68	90.86	91.04	91.25	
31	87.80	87.98	88.16	88.34	88.52	88.70	88.88	89.06	89.24	89.42	
30	86.00	86.18	86.36	86.54	86.72	86.90	87.08	87.26	87.44	87.69	
29	84.20	84.38	84.56	84.74	84.92	85.10	85.28	85.46	85.64	85.83	
28	82.40	82.58	82.76	82.94	83.12	83.30	83.48	83.66	83.84	84.0	
27	80.60	80.78	80.96	81.14	81.32	81.50	81.68	81.86	82.04	82.2	
26	78.80	78.98	79.16	79.34	79.52	79.70	79.88	80.06	80.24	80.4	
25	77.00	77.18	77.36	77.54	77.72	77.90	78.08	78.26	78.44	78.6	
24	75.20	75.38	75.56	75.74	75.92	76.10	76.28	76.46	76.64	76.8	
23	73.40	73.58	73.76	73.94	74.12	74.30	74.48	74.66	74.84	75.0	
22	71.60	71.78	71.96	72.14	72.32	72.50	72.68	72.86	73.04	73.22	
21	69.80	69.98	70.16	70.34	70.52	70.70	70.88	71.06	71.24	71.45	
20	68.00	68.18	68.36	68.54	68.72	68.90	69.08	69.26	69.44	69.6	
19	66.20	66.38	66.56	66.74	66.92	67.10	67.28	67.46	67.64	67.83	
18	64.40	64.58	64.76	64.94	65.12	65.30	65.48	65.66	65.84	66.0	
17	62.60	62.78	62.96	63.14	63.32	63.50	63.68	63.86	64.04	64.25	
16	60.80	60.98	61.16	61.34	61.52	61.70	61.88	62.06	62.24	62.4	
15	59.00	59.18	59.36	59.54	59.72	59.90	60.08	60.26	60.44	60.63	
14	57.20	57.38	57.56	57.74	57.92	58.10	58.28	58.46	58.64	58.83	
13	55.40	1	55.76	55.94	56.12	56.30	56.48	56.66	56.84	57.0:	
12	53.60	53.78	53.96	54.14	54.32	54.50	54.68	54.86	55.04	55.2	
11	51.80	51.98	52.16	52.34	52.52	52.70	52.88	53.06	53.24	53.45	
·	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

		Tenths of Degrees.										
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.		Fahren.		
+10	+50.00	+50.18	+50.36	+50.54	+50.72	+50.90	+51.08	+51.26	+51.44	+51.62		
9	48.20	48.38	48.56	48.74	48.92	49.10	49.28	49.46	49.64	49.82		
8 7	46.40 44.60	46.58	46.76	46.94	47.12	47.30	47.48	47.66	47.84	48.02		
6	42.80	42.98	44.96 43.16	43.14	45.32 43.52	45.50 43.70	45.68 43.88	45.86	46.04	46.22		
о	42.50	42.95	45.10	40.04	45.52	43.70	45.55	44.06	44.24	44.42		
5	41.00	41.18	41.36	41.54	41.72	41.90	42.08	42.26	42.44	42.62		
4	39.20	39.38	39.56	39.74	39.92	40.10	40.28	40.46	40.64	40.82		
3	37.40	37.58	37.76	37.94	38.12	38.30	38.48	38.66	38.84	39.02		
2	35.60	35.7S	35.96	36.14	36.32	36.50	36.68	36.86	37.04	37.22		
1	33.80	33.98	34.16	34.34	34.52	34.70	34.88	35.06	35.24	35.42		
0	32.00	32.18	32.36	32.54	32.72	32.90	33.08	33.26	33.44	33.62		
- 0	32.00	31.82	31.64	31.46	31.28	31.10	30.92	30.74	30.56	30.38		
- 0 - 1	30.20	30.02	29.84	29.66	29.48	29.30	29.12	28.94	28.76	28.58		
- 2	28.40	28.22	28.04	27.86	27.68	27.50	27.32	27.14	26.96	26.78		
- 3	26.60	26.42	26.24	26.06	25.88	25.70	25.52	25.34	25.16	24.98		
- 4	24.80	24.62	24.44	24.26	24.08	23.90	23.72	23.54	23.36	23.18		
→ 5	23.00	22.82	22.64	22.46	22.28	22.10	21.92	21.74	21.56	21.38		
- 6	21.20	21.02	20.84	20.66	20.48	20.30	20.12	19.94	19.76	19.58		
- 7	19.40	19.22	19.04	18.86	18.68	18.50	18.32	18.14	17.96	17.78		
- 8	17.60	17.42	17.24	17.06	16.88	16.70	16.52	16.34	16.16	15.98		
- 9	15.80	15.62	15.44	15.26	15.08	14.90	14.72	14.54	14.36	14.18		
-10	14.00	13.82	13.64	13.46	13.28	13.10	12.92	12.74	12.56	12.38		
-11	12.20	12.02	11.84	11.66	11.48	11.30	11.12	10.94	10.76	10.58		
-12	10.40	10.22	10.04	9.86	9.68	9.50	9.32	9.14	8.96	8.78		
-13	8.60	8.42	8.24	8.06	7.88	7.70	7.52	7.34	7.16	6.98		
-14	6.80	6.62	6.44	6.26	6.08	5.90	5.72	5.54	5.36	5.18		
-15	5.00	4.82	4.64	4.46	4.28	4.10	3.92	3.74	3.56	3.38		
-16	3.20	3.02	2.84	2.66	2.48	2.30	2.12	1.94	1.76	1.58		
-17	1.40	1.22	1.04	0.86	0.68	0.50	0.32	0.14	- 0.04	- 0.22		
-18	- 0.40	- 0.58	- 0.76	- 0.94	- 1.12	- 1.30	- 1.48	- 1.66	- 1.84	- 2.02		
-19	- 2.20	- 2.38	- 2.56	- 2.74	- 2.92	- 3.10	- 3.28	- 3.46	- 3.64	- 3.82		
-20	- 4.00	- 4.18	- 4.36	- 4.54	- 4.72	- 4.90	- 5.08	- 5.26	5.44	5.69		
$-20 \\ -21$	- 5.80	- 5.98	- 6.16	- 4.34 - 6.34	- 4.72 - 6.52	-6.70	- 6.88	- 7.06	- 5.44 - 7.24	- 5.62 - 7.42		
$-21 \\ -22$	- 7.60	- 7.78	- 7.96	- 8.14	- 8.32	- 8.50	- 8.68	- 8.86	- 9.04	- 9.22		
-22 -23	- 9.40	- 9.58	- 9.76	- 9.94	-10.12	-10.30	-10.48	-10.66	-10.84	-11.02		
-24	-11.20	-11.38	-11.56	-11.74	-11.92	-12.10	-12.28	-12.46	-12.64	-12.82		
-25	-13.00	-13.18	-13.36	-13.54	-13.72	-13.90	-14.08	-14.26	-14.44	-14.62		
-26	-14.80	-14.98	-15.16	-15.34	-15.52	-15.70	-15.88	-16.06	-16.24	-16.42		
-27	-16.60	-16.78	-16.96	-17.14	-17.32	-17.50	-17.6S	-17.86	-18.04	-18.22		
-28	-18.40	-18.58	-18.76	-18.94	-19.12	-19.30	-19.48	-19.66	-19.84	-20.02		
-29	-20.20	-20.38	-20.56	-20.74	-20.92	-21.10	-21.28	-21.46	-21.64	-21.82		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

					Tenths of	Degrees.				
Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
-30	-22.00	-22.18	-22.36	-22.54	-22.72	-22.90	-23.08	-23.26	-23.44	-23.62
-31	-23.80	-23.98	-24.16	-24.34	-24.52	-24.70	-24.88	-25.06	-25.24	-25.42
-32	-25.60	-25.78	-25.96	-26.14	-26.32	-26.50	-26.68	-26.86	-27.04	-27.22
-33	-27.40	-27.58	-27.76	-27.94	-28.12	-28.30	-28.4 S	-28.66	-28.84	-29.02
-34	-29.20	-29.38	-29.56	-29.74	-29.92	-30.10	-30.28	-30.46	-30.64	-30.82
-35	-31.00	-31.18	-31.36	-31.54	-31.72	-31. 90	-32.08	-32.26	- 32.44	-32.62
-36	-32.80	-32.98	-33.16	-33.34	-33.52	-33.70	-33.88	-34.06	- 34.24	-34.42
-37	-34.60	-34.78	-34.96	-35.14	-35.32	-35.50	-35.68	-35.86	-36.04	-36.22
-38	-36.40	-36.58	-36.76	-36.94	-37.12	-37.30	-37.48	-37.66	-37. 84	-38.02
-39	-38.20	-38.38	-38.56	-38.74	-38.92	-39.10	-39.28	-39.46	-39.64	-39.82
-40	-40.00	-40.18	-40.36	-40.54	-40.72	-40.90	-41.0 S	-41.26	-41.44	-41.62
-41	-41.80	-41.98	-42.16	-42.34	-42.52	-42.70	-42.88	-43.06	-43.24	-43.42
-42	-43.60	-43.78	-43.96	-44.14	-44.32	-44.50	-44.68	-44.86	-45.04	-45.22
-43	-45.40	-45.58	-45.76	-45.94	-46.12	-46.30	-46.48	-46.66	-46.84	-47.02
-44	-47.20	-47.38	-47.56	-47.74	47.92	-48.10	-48.28	-48.46	-48.64	-48.82
1										
-45	-49.00	-49.18	-49.36	-49.54	-49.72	-49.90	-50.08	-50.26	-50.44	-50.62
-46	-50.80	-50.98	-51.16	-51.34	-51.52	-51.70	-51.88	-52.06	-52.24	-52.42
-47	-52.60	-52.78	-52.96	-53.14	-53.32	-53.50	-53.68	-53.86	-54.04	-54.22
-48	-54.40	-54.58	-54.76	-54.94	-55.12	-55.30	-55.48	-55.66	-55.84	-56.02
-49	-56,20	-56.38	-56.56	-56.74	-56.92	-57.10	-57.28	-57.46	-57.64	-57.82
10	33.23	00.00				1	1			
-50	-58.00	-58.18	-58.36	-58.54	-58.72	-58.90	-59.08	-59.26	-59.44	-59.62
-51	-59.80	-59.98	-60.16	-60.34	-60.52	-60.70	-60.88	-61.06	-61.24	-61.42
-52	-61.60	-61.78	-61.96	-62.14	-62.32	-62.50	-62.68	-62.86	-63.04	-63.22
-53	-63.40	-63.58	-63.76	-63.94	-64.12	-64.30	-64.48	-64.66	-64.84	-65.02
-54	-65.20	-65.38	-65.56	-65.74	-65.92	-66.10	-66.28	-66.46	-66.64	-66.82
	09.20	00.00	33100	39111	0.5102		33.20	1		

TABLE FOR COMPARING THE CENTIGRADE AND FAHRENHEIT'S THERMOMETERS NEAR THE BOILING POINT.

Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.									
100	212.00	212.18	212.36	212.54	212.72	212.90	213.08	213.26	213.44	213.62
99	210.20	210.38	210.56	210.74	210.92	211.10	211.28	211.46	211.64	211.82
98	208.40	208.58	208.76	208.94	209.12	209.30	209.48	209.66	209.84	210.02
97	206.60	206.78	206.96	207.14	207.32	207.50	207.68	207.86	208.04	208.22
96	204.80	204.98	205.16	205.34	205.52	205.70	205.88	206.06	206.24	206.42
95	203.00	203.18	203.36	203.54	203.72	203.90	204.08	204.26	204.44	204.62
i i										
94	201.20	201.38	201.56	201.7-1	201.92	202.10	202.28	202.46	202 64	202.82
93	199.40	199.58	199.76	199.94	200.12	200.30	200.48	200 66	200.84	201.02
92	197.60	197.78	197.96	198.14	198.32	198.50	198.68	198.86	199.04	199.22
91	195.80	195.98	196.16	196.34	196.52	196.70	196.88	197.06	197.24	197.42
90	194.00	194.18	194.36	194.51	194.72	194.90	195.08	195.26	195.44	195.62
89	192.20	192.38	192.56	192.74	192.92	193.10	193.28	193.46	193.61	193.82

Health H						Tenths of	Degrees.				
### ### ### ### ### ### ### ### ### ##	Centigrade Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$											Reaum.
38		II —	1-	i —	ı—	1-	_		ı—	<u>;</u> —	_
37				l .	ì	l .			ı	1	31.92
36 28.80 28.88 28.96 29.04 29.12 29.20 29.28 29.36 29.44 29.5 35 28.00 28.08 25.16 28.24 28.32 28.40 28.48 28.56 28.64 28.7 34 27.20 27.28 27.36 27.44 27.52 27.60 27.68 27.76 27.84 27.9 33 26.40 26.48 25.66 26.64 26.72 26.80 26.88 26.96 27.04 27.1 31 24.80 24.88 24.96 25.04 25.12 25.20 25.28 25.36 25.44 26.26 24.00 24.03 24.16 24.24 25.32 24.40 24.48 24.56 24.64 24.72 22.40 22.48 22.56 22.64 22.72 22.80 22.88 22.96 23.04 23.1 27 21.60 21.68 21.76 21.84 21.92 22.00 22.08 22.1	38	11	1	i	1	1		1	i	I	31.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	37	29.60	29.68	29.76	29.84	29.92	30.00	30.08	30.16	30.24	30.32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	36	28.80	28.88	28.96	29.04	29.12	29.20	29.28	29.36	29.44	29.52
33	35	28.00	28.08	28.16	28.24	28.32	28.40	28.48	28.56	28.64	28.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	34	27.20	27.28	27.36	27.44	27.52	27.60	27.68	27.76	27.84	27.92
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	33	26.40	26.48	26.56	26.64	26.72	26.80	26.88	26.96	27.04	27.12
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	32	25.60	25.68	25.76	25.84	25.92	26.00	26.08	26.16	26.24	26.32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	31	24.80	24.88	24.96	25.04	25.12	25.20	25.28	25.36	25.44	25.52
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	30	24.00	24.08	24.16	24.24	25.32	24.40	24.48	24.56	24.64	24.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	29	23.20	23.28	23.36	23.44	23.52	23.60	23.68	23.76	23.84	23.92
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	28	22.40	22.48	22.56	22.64	22.72	22.80	22.88	22.96	23.04	23.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	27	21.60	21.68	21.76	21.84	21.92	22.00	22.08	22.16	22.24	22.32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26	20.80	20.88	20.96	21.04	21.12	21.20	21.28	21.36	21.44	21.52
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	20.00	20.08	20.16	20.24	20.32	20.40	20.48	20.56	20.64	20.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	19.20	19.28	19.36	19.44	19.52	19.60	19.68	19.76	19.84	19.93
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	23	18.40	18.48	18.56	18.64	18.72	18.80	18.88	18.96	19.04	19.15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22	17.60	1	1	1	1	18.00	1	l .	18.24	18.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		III	16.88	1	17.04	17.12	1	F	17.36	1	17.55
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	16.00	16.08	16.16	16.24	16.32	16.40	16.48	16.56	16.64	16.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	15.20	15.28	15.36	15.44	15.52	15.60	15.68	15.76	15.84	15.92
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	18	14.40	14.48	14.56	14.64	14.72	14.80	14.88	14.96	15.04	15.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17	13.60	1		ŀ			i	1	14.24	14.32
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		£1	1		1	1		1	1		13.52
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	12.00	12.08	12.16	12.24	12.32	12.40	12.48	12.56	12.64	12.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14	11.20		1	1	I .	11.60	11.68	1	11.84	11.92
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	10.40	1	1	ı		10.80	I	1	11.04	11.15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11		1	1		l.	1	l l	ł	10.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11		1	1			1		ſ	9.55
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10	8.00	8.08	8.16	8.24	8.32	8.40	8.48	8.56	8.64	8.75
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9	7.20	1	1	7.44			1		7.84	7.99
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11	1	1	1	1		1	1	1	7.12
6 4.80 4.88 4.96 5.04 5.12 5.20 5.28 5.36 5.44 5.5 5 4.00 4.08 4.16 4.24 4.32 4.40 4.48 4.56 4.64 4.7 4 3.20 3.28 3.36 3.44 3.52 3.60 3.68 3.76 3.84 3.5 3 2.40 2.48 2.56 2.64 2.72 2.80 2.88 2.96 3.04 3.1 2 1.60 1.68 1.76 1.84 1.92 2.00 2.08 2.16 2.24 2.5 1 0.80 0.88 0.96 1.04 1.12 1.20 1.28 1.36 1.44 1.5 0 0.00 0.08 0.16 0.24 0.32 0.40 0.48 0.56 0.64 0.7		11	1	1	1	1		1	1	i	6.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$!!	1	1	1	1		1	L	1	5.59
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	4.00	4.08	4.16	4.24	4.32	4.40	4.48	4.56	4.64	4.7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4		4		1		1	1	l .		3.92
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	11	1	1	I	1		ı	1	1	3.12
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11	1	F.	1	I .			1	1	2.33
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11	1	1	l .	1	2	I .	i .	t	1.55
	0	0	0	0	0	0	0	0	0	0	0.75
		0.00	1.	2.	3.	4.	5.	6.	7.	8.	9.

VIII.-IX.

COMPARISON

OF

REAUMUR'S THERMOMETER

WITH

THE THERMOMETER OF FAHRENHEIT AND THE CENTIGRADE THERMOMETER,

03

TABLES

FOR CONVERTING DEGREES OF REAUMUR INTO DEGREES OF FAHRENHEIT AND INTO CENTIGRADE DEGREES;

GIVING THE CORRESPONDING VALUES FOR EACH TENTH OF A DEGREE, FROM $\pm 40^\circ$ TO $\pm 40^\circ$ REAUMUR.

		.,,			Tenths of	Degrees.			a	
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.	Fahren.
+40	1	+122.22		1			+123.35		+123.80	,
39	119.75	119.97	120.20	120.42	120.65	120.87	121.10	121.32	121.55	121.77
38	117.50	117.72	117.95	118.17	1		118.85	119.07	119.30	119.5
37	115.25	115.47	115.70	115.92	116.15	116.37	116.60	116.82	117.05	117.27
36	113.00	113.22	113.45	113.67	113.90	114.12	114.35	114.57	114.80	115.02
35	110.75	110.97	111.20	111.42	111.65	111.87	112.10	112.32	112.55	112.77
34	108.50	108.72	108.95	109.17	109.40	109.62	109.85	110.07	110.30	110.52
33	106.25	106.47	106.70	106.92	107.15	107.37	107.60	107.82	108.05	108.27
32	104.00	104.22	104.45	104.67	104.90	105.12	105.35	105.57	105.80	106.02
31	101.75	101.97	102.20	102.42	102.65	102.87	103.10	103.32	103.55	103.77
30	99.50	99.72	99.95	100.17	100.40	100.62	100.85	101.07	101.30	101.52
29	97.25	97.47	97.70	97.92	98.15	98.37	98.60	98.82	99.05	99.27
28	95.00	95.22	95.45	95.67	95.90	96.12	96.35	96.57	96.80	97.02
27	92.75	92.97	93.20	93.42	93.65	93.87	94.10	94.32	94.55	94.77
26	90.50	90.72	90.95	91.17	91.40	91.62	91.85	92.07	92.30	92.52
25	88.25	88.47	88.70	88.92	89.15	89.37	89.60	89.82	90.05	90.27
24	86.00	86.22	86.45	86.67	86.90	87.12	87.35	87.57	87.80	88.02
23	83.75	83.97	84.20	84.42	84.65	84.87	85.10	85.32	85.55	85.77
23	81.50	81.72	81.95	82.17	82.40	82.62	82.85	83.07	83.30	83.52
21	79.25	79.47	79.70	79.92	80.15	80.37	80.60	80.82	81.05	81.27
	00	22			00	-0.40		-0	~~ ~~	~0.0 0
20	77.00	77.22	77.45	77.67	77.90	78.12	78.35	78.57	78.80	79.02
19	74.75	74.97	75.20	75.42	75.65	75.87	76.10	76.32	76.55	76.77
18	72.50	72.72	72.95	73.17	73.40	73.62	73.85	74.07	74.30	74.52
17	70.25	70.47	70.70	70.92	71.15	71.37	71.60	71.82	72.05	72.27
16	68.00	68.22	68.45	68.67	68.90	69.12	69.35	69.57	69.80	70.02
15	65.75	65.97	66.20	66.42	66.65	66.87	67.10	67.32	67.55	67.77
14	63.50	63.72	63.95	64.17	64.40	64.62	64.85	65.07	65.30	65.52
13	61.25	61.47	61.70	61.92	62.15	62.37	62.60	62.82	63.05	63.27
12	59.00	59.22	59.45	59.67	59.90	60.12	60.35	60.57	60.80	61.02
11	56.75	56.97	57.20	57.42	57.65	57.87	58.10	58.32	58.55	58.77
10	54.50	54.72	54.95	55.17	55.40	55.62	55.85	56.07	56.30	56.52
Ð	52.25	52.47	52.70	52.92	53.15	53.37	53.60	53.82	54.05	54.27
8	50.00	50.22	50.45	50.67	50.90	51.12	51.35	51.57	51.80	52.02
7	47.75	47.97	48.20	48.42	48.65	48.87	49.10	49.32	49.55	49.77
6	45.50	45.72	45.95	46.17	46.40	46.62	46.85	47.07	47.30	47.5%
5	43.25	43.47	43.70	43.92	44.15	44.37	44.60	44.82	45.05	45.27
4	41.00	41.22	41.45	41.67	41.90	42.12	42.35	42.57	42.80	43.02
3	38.75	38.97	39.20	39.42	39.65	39.87	40.10	40.32	40.55	40.77
2	36.50	36.72	36.95	37.17	37.40	37.62	37.85	38.07	38.30	38.52
1	34.25	34.47	34.70	34.92	35.15	35.37	35.60	35.82	36.05	36.27
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

					Tenths o	f Degrees.	·			
Degrees of Reaumur.	l I	Ι,	2.	3.	4	5.	6.	7.	8.	
	0.	1.	2.	3.	4.	J.	0.		8.	9.
	Fahren.									
J+ 0	+32.00	+32.22	+32.45	+32.67	+32.90	+33.12	+33.35	+33.57	+33.80	+34.02
- 0	32.00	31.77	31.55	31.32	31.10	30.87	30.65	30.42	30.20	29.97
- 1	29.75	29.52	29.30	29.07	28.85	28.62	28.40	28.17	27.95	27.72
- 2	27.50	27.27	27.05	26.82	26.60	26.37	26.15	25.92	25.70	25.47
- 3	25.25	25.02	24.80	24.57	24.35	24.12	23.90	23.67	23.45	23.22
- 4	23.00	22.77	22.55	22.32	22.10	21.87	21.65	21.42	21.20	20.97
- 5	20.75	20.52	20.30	20.07	19.85	19.62	19.40	19.17	18.95	18.72
- 6	18.50	18.27	18.05	17.82	17.60	17.37	17.15	16.92	16.70	16.47
- 7	16.25	16.02	15.80	15.57	15.35	15.12	14.90	14.67	14.45	14.22
- 8	14.00	13.77	13.55	13.32	13.10	12.87	12.65	12.42	12.20	11.97
- 9	11.75	11.52	11.30	11.07	10.85	10.62	10.40	10.17	9.95	9.72
			l							
-10	9.50	9.27	9.05	8.82	8.60	8.37	8.15	7.92	7.70	7.47
-11	7.25	7.02	6.80	6.57	6.35	6.12	5.90	5.67	5.45	5.22
-12	5.00	4.77	4.55	4.32	4.10	3.87	3.65	3.42	3.20	2.97
-13	2.75	2.52	2.30	2.07	1.85	1.62	1.40	1.17	0.95	0.72
-14	0.50	0.27	0.05	- 0.17	- 0.40	-0.62	- 0.85	- 1.07	- 1.30	- 1.52
15	1 75	1.07	- 2.20	- 2.42	9.65	9 9 7	- 3.10	_ 9 99	9 5 5	0 **
-15	- 1.75 - 4.00	- 1.97	- 2.20 - 4.45	- 4.67	- 2.65	-2.87 -5.12	- 5.35	- 3.32 - 5.57	- 3.55 - 5.80	-3.77 -6.02
-16	1	- 4.22 - 6.47	i	- 4.67 - 6.92	- 4.90	-5.12 -7.37	- 7.60	- 5.57 - 7.82	- 8.05	
-17 -18	- 6.25 - 8.50	- 8.72	- 6.70 - 8.95	- 0.92 - 9.17	- 7.15 - 9.40	-9.62	- 9.85	-10.07	-10.30	- 8.27 -10.52
-18 -19	-10.75	-8.72 -10.97	-11.20	-3.17 -11.42	-11.65	-3.02 -11.87	-12.10	-12.32	-10.50 -12.55	-10.52 -12.77
-19	-10.75	-10.97	-11.20	-11.42	-11.05	-11.07	-12.10	-12.52	-12.99	-12.77
-20	-13.00	-13.22	-13.45	-13.67	-13.90	-14.12	-14.35	-14.57	-14.80	-15.02
-21	-15.25	-15.47	-15.70	-15.92	-16.15	-16.37	-16.60	-16.82	-17.05	-17.27
-22	-17.50	-17.72	-17.95	-18.17	-18.40	-18.62	-18.85	-19.07	-19.30	-19.52
-23	-19.75	-19.97	-20.20	-20.42	-20.65	-20.87	-21.10	-21.32	-21.55	-21.77
-24	-22.00	-22.22	-22.45	-22.67	-22.90	-23.12	-23.35	-23.57	-23.80	-24.02
-25	-24.25	-24.47	-24.70	-24.92	-25.15	-25.37	-25.60	-25.82	-26.05	-26.27
-26	-26.50	-26.72	-26.95	-27.17	-27.40	-27.62	-27.85	-28.07	-28.30	-28.52
-27	-28.75	-28.97	-29.20	-29.42	-29.65	-29.87	-30.10	-30.32	-30.55	-30.77
-28	-31.00	-31.22	-31.45	-31.67	-31.90	-32.12	-32.35	-32.57	-32.80	-33.02
-29	-33.25	-33.47	-33.70	-33.92	-34.15	-34.37	-34.60	-34. 82	-35.05	-35.27
-30	-35.50	-35.72	-35.95	-36.17	-36.40	-36.62	-36.85	-37.07	-37.30	-37.52
-30 -31	-37.75	-37.97	-38.20	-38.42	-38.65	-38.87	-39.10	-39.32	-39.55	-37.32 -39.77
-31 -32	-37.75 -40.00	-37.97 -40.22	-35.20 -40.45	-35.42 -40.67	-35.65 -40.90	-33.37 -41.12	-39.10 -41.35	-39.32 -41.57	-41.80	-39.77 -42.02
-32 -33	-42.25	-40.22 -42.47	-40.45 -42.70	-40.07 -42.92	-43.15	-43.37	-43.60	-41.57 -43.82	-44.05	-42.02 -44.27
- 1	-42.23 -44.50	-42.47 -44.72	-44.95	-45.17		-45.62	-45.85	-46.07	-44. 05	-46.52
9.3	11100	44.12	11.55	15.11	10.40	10.02	10.00	10.01	10.00	40.07
-35	-46.75	-46.97	-47.20	-47.42	-47.65	-47.87	-48.10	-48.32	-48.55	-48.77
-36	-49.00	-49.22	-49.45	-49.67	-49.90	-50.12	-50.35	-50.57	-50.80	-51.02
-37	-51.25	-51.47	-51.70	-51.92	-52.15	-52.3 7	-52.60	-52.82	-53.05	-53.27
-38	-53.50	-53.72	-53.95	-54.17	-54.40	-54.62	-54.85	-55.07	-55.30	-55.52
-39	-55.75	-55.97	-56.20	-56.42	-56.65	-56.87	-57.10	-57.32	-57.55	-57.77
							l			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

					Tenths of	Degrees.				
Degrees of Reaumur.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
1.0	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
±40	+50.00	+50.13	+50.25	±50.38	+50.50	±50.63	±50.75	±50.88	±51.00	+51.13
39	48.75	48.88	49.00	49.13	49.25	49.38	49.50	49.63	49.75	49.88
38	47.50	47.63	47.75	47.88	48.00	48.13	48.25	48.38	48.50	48.63
37	46.25	46.38	46.50	46.63	46.75	46.88	47.00	47.13	47.25	47.38
36	45.00	45.13	45.25	45.38	45.50	45.63	45.75	45.88	46.00	46.13
35	43.75	43.88	44.00	44.13	44.25	44.38	44.50	44.63	44.75	44.88
34	42.50	42.63	42.75	42.88	43.00	43.13	43.25	43.38	43.50	43.63
33	41.25	41.38	41.50	41.63	41.75	41.88	42.00	42.13	42.25	42.38
32	40.00	40.13	40.25	40.38	40.50	40.63	40.75	40.88	41.00	41.13
31	38.75	38.88	39.00	39.13	39.25	39.38	39.50	39.63	39.75	39.88
30	37.50	37.63	37.75	37.88	38.00	38.13	38.25	38.38	38.50	38.63
29	36.25	36.38	36.50	36.63	36.75	36.88	37.00	37.13	37.25	37.38
28	35.00	35.13	35.25	35.38	35.50	35.63	35.75	35.88	36.00	36.13
27	33.75	33.88	34.00	34.13	34.25	34.38	34.50	34.63	34.75	34.88
26	32.50	32.63	32.75	32.88	33.00	33.13	33.25	33.38	33.50	33.63
25	31.25	31.38	31.50	31.63	31.75	31.88	32.00	32.13	32.25	32.38
24	30.00	30.13	30.25	30.38	30.50	30.63	30.75	30.88	31.00	31.13
23	28.75	28.88	29.00	29.13	29.25	29.38	29.50	29.63	29.75	29.88
22	27.50	27.63	27.75	27.88	28.00	28.13	28.25	28.38	28.50	28.63
21	26.25	26.38	26.50	26.63	26.75	26.88	27.00	27.13	27.25	27.38
20	25.00	25.13	25.25	25.38	25.50	25.63	25.75	25.88	26.00	26.13
19	23.75	23.88	24.00	24.13	24.25	24.38	24.50	24.63	24.75	24.88
18	22.50	22.63	22.75	22.88	23.00	23.13	23.25	23.38	23.50	23.63
17	21.25	21.38	21.50	21.63	21.75	21.88	22.00	22.13	22.25	22.38
16	20.00	20.13	20.25	20.38	20.50	20.63	20.75	20.88	21.00	21.13
15	18.75	18.88	19.00	19.13	19.25	19.38	19.50	19.63	19.75	19.88
14	17.50	17.63	17.75	17.88	18.00	18.13	18.25	18.38	18.50	18.63
13	16.25	16.38	16.50	16.63	16.75	16.88	17.00	17.13	17.25	17.38
12	15.00	15.13	15.25	15.38	15.50	15.63	15.75	15.88	16.00	16.13
11	13.75	13.88	14.00	14.13	14.25	14.38	14.50	14.63	14.75	14.88
10	12.50	12.63	12.75	12.88	13.00	13.13	13.25	13.38	13.50	13.63
9	11.25	11.38	11.50	11.63	11.75	11.88	12.00	12.13	12.25	12.38
8	10.00	10.13	10.25	10.38	10.50	10.63	10.75	10.88	11.00	11.13
7	8.75	8.88	9.00	9.13	9.25	9.38	9.50	9.63	9.75	9.88
6	7.50	7.63	7.75	7.88	8.00	8.13	8.25	8.38	8.50	8.63
5	6.25	6.38	6.50	6.63	6.75	6.88	7.00	7.13	7.25	7.38
4	5.00	5.13	5.25	5.38	5.50	5.63	5.75	5.88	6.00	6.13
3	3.75	3.88	4.00	4.13	4.25	4.38	4.50	4.63	4.75	4.88
2	2.50	2.63	2.75	2.88	3.00	3.13	3.25	3.38	3.50	3.63
1	1.25	1.38	1.50	1.63	1.75	1.88	2.00	2.13	2.25	2.38
0	0.00	0.13	0.25	0.38	0.50	0.63	0.75	0.88	1.00	1.13
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

X. - XV.

TABLES

FOR

COMPARING THERMOMETRICAL DIFFERENCES

EXPRESSED IN DEGREES OF DIFFERENT SCALES,

IRRESPECTIVE OF THEIR ZERO POINT.

X. NUMBER OF DEGREES OF FAHRENHEIT \Longrightarrow NUMBER OF CENTIGRADE DEGREES.

4° Reaumur = 5° Centigrade = 9° Fahrenheit.

Degrees					Tenths of	a Degree.				
of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
0	0.00	0.06	0.11	0.17	0.22	0.28	0.33	0.39	0.44	0.50
1	0.56	0.61	0.67	0.72	0.78	0.83	0.89	0.91	1.00	1.06
2	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
3	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.22
4	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
5	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28
6	3.33	3.39	3.44	3.50	3.56	3.61	3.67	4.72	3.78	3.83
7	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39
8	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.83	4.89	4.94
9	5.00	5.06	5.11	5.17	5.22	5.28	5.32	5.39	5.44	5.50

XI. NUMBER OF DEGREES OF FAHRENHEIT = NUMBER OF DEGREES OF REAUMUR.

Degrees					Tenths of	a Degree.		,	,	
of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Reaumur.	Reaumur.	Reaumur	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur
0	0.00	0.04	0.09	0.13	0.18	0.22	0.27	0.31	0.36	0 40
1	0.44	0.49	0.53	0.58	0.62	0.67	0.71	0.76	0.80	0.84
2	0.89	0.93	0.98	1.02	1.07	1.11	1.16	1.20	1.24	1.29
3	1.33	1.38	1.42	1.47	1.51	1.56	1.60	1.64	1.69	1.73
4	1.78	1.82	1.87	1.91	1.96	2.00	2.04	2.09	2.13	2.18
5	2.22	2.27	2.31	2.36	2.40	2.44	2.49	2.53	2.58	2.62
6	2.67	2.71	2.76	2.80	2.84	2.89	2.93	2.98	3.02	3.07
7	3.11	3.16	3.20	3.24	3.29	3.33	3.38	3.42	3.47	3.51
8	3.56	3.60	3.64	3.69	3.73	3.78	3.82	3.87	3.91	3.96
9	4.00	4.04	4.09	4.13	4.18	4.22	4.27	4.31	4.36	4.40

XII. NUMBER OF CENTIGRADE DEGREES = NUMBER OF DEGREES OF REAUMUR.

					Tenths of	a Degree.				
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur	Reaumur.	Reaumur.	Reaumur.	Reaumur.	Reaumur.
0	0.00	0.08	0.16	0.24	0.32	0.40	0.48	0.56	0.64	0.72
1	0.80	0.88	0.96	1.04	1.12	1.20	1.28	1.36	1.44	1.52
2	1.60	1.68	1.76	1.84	1.92	2.00	2.08	2.16	2.24	2.32
3	2.40	2.48	2.56	2.64	2.72	2.80	2.88	2.96	3.04	3.12
4	3.20	3.28	3.36	3.44	3.52	3.60	3.68	3.76	3.84	3.92
5	4.00	4.08	4.16	4.24	4.32	4.40	4.48	4.56	4.64	4.72
6	4.80	4.88	4.96	5.04	5.12	5.20	5.28	5.36	5.44	5.52
7	5.60	5.68	5.76	5.84	5.92	6.00	6.08	6.16	6.24	6.32
8	6.40	6.48	6.56	6.64	6.72	6.80	6.88	6.96	7.04	7.12
9	7.20	7.28	7.36	7.44	7.52	7.60	7.68	7.76	7.84	7.92

XIII. NUMBER OF CENTIGRADE DEGREES \Longrightarrow NUMBER OF DEGREES OF FAHRENHEIT. 4° Reaumur $= 5^{\circ}$ Centigrade $= 9^{\circ}$ Fahrenheit.

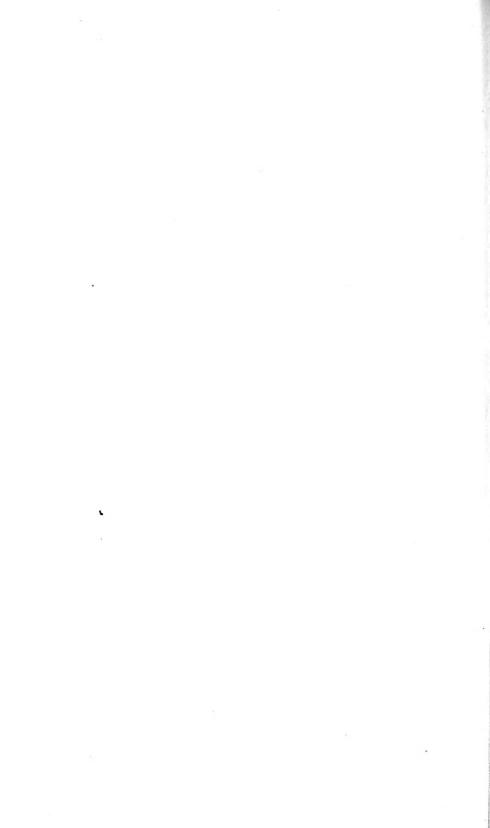
					Tenths of	a Degree.				
Centig. Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.
0	0.00	0.18	0.36	0.54	0.72	0.90	1.08	1.26	1.44	1.62
1	1.80	1.98	2.16	2.34	2.52	2.70	2.88	3.06	3.24	3.42
2	3.60	3.78	3.96	4.14	4.32	4.50	4.68	4.86	5.04	5.22
3	5.40	5.58	5.76	5.94	6.12	6.30	6.48	6.66	6.84	7.02
4	7.20	7.38	7.56	7.74	7.92	8.10	8.28	8.46	8.64	8.82
5	9.00	9.18	9.36	9.54	9.72	9.90	10.08	10.26	10.44	10.62
6	10.80	10.98	11.16	11.34	11.52	11.70	11.88	12.06	12.24	12.42
7	12.60	12.78	12.96	13.14	13.32	13.50	13.68	13.86	14.04	14.22
8	14.40	14.58	14.76	14.94	15.12	15.30	15.48	15.66	15.84	16.02
9	16.20	16.38	16.56	16.74	16.92	17.10	17.28	17.46	17.64	17.82

XIV. NUMBER OF DEGREES OF REAUMUR = NUMBER OF CENTIGRADE DEGREES.

Degrees				,	Tenths of	a Degree.				
of Reaum.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.	Centig.
0	0.00	0.12	0.25	0.37	0.50	0.62	0.75	0.87	1.00	1.12
1	1.25	1.37	1.50	1.62	1.75	1.87	2.00	2.12	2.25	2.37
2	2.50	2.62	2.75	2.87	3.00	3.12	3.25	3.37	3.50	3.62
3	3.75	3.87	4.00	4.12	4.25	4.37	4.50	4.62	4.75	4.87
4	5.00	5.12	5.25	5.37	5.50	5.62	5.75	5.87	6.00	6.12
5	6.25	6.37	6.50	6.62	6.75	6.87	7.00	7.12	7.25	7.37
6	7.50	7.62	7.75	7.87	8.00	8.12	8.25	8.37	8.50	8.62
7	8.75	8.87	9.00	9.12	9.25	9.37	9.50	9.62	9.75	9.87
8	10.00	10.12	10.25	10.37	10.50	10.62	10.75	10.87	11.00	11.12
9	11.25	11.37	11.50	11.62	11.75	11.87	12.00	12.12	12.25	12.37

XV. NUMBER OF DEGREES OF REAUMUR = NUMBER OF DEGREES OF FAHRENHEIT.

Degrees					Tenths of	a Degree.				
of Reaum.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.	Fahr.
0	0.00	0.22	0.45	0.67	0.90	1.12	1.35	1.57	1.80	2.02
1	2.25	2.47	2.70	2.92	3.15	3.37	3.60	3.82	4.05	4.27
2	4.50	4.72	4.95	5.17	5.40	5.62	5.85	6.07	6.30	6.52
3	6.75	6.97	7.20	7.42	7.65	7.87	8.10	8.32	8.55	8.77
4	9.00	9.22	9.45	9.67	9.90	10.12	10.35	10.57	10.80	11.02
5	11.25	11.47	11.70	11.92	12.15	12.37	12.60	12.82	13.05	13.27
6	13.50	13.72	13.95	14.17	14.40	14.62	14.85	15.07	15.30	15.52
7	15.75	15.97	16.20	16.42	16.65	16.87	17.10	17.32	17.55	17.77
8	.18.00	18.22	18.45	18.67	18.90	19.12	19.35	19.57	19.80	20.02
9	20.25	20.47	20.70	20.92	21.15	21.37	21.60	21.82	22.05	22.27



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HYGROMETRICAL TABLES.

Hygrometers, or instruments used for determining the amount of aqueous vapor present in the air, are of three classes. In the first, we find the hygrometers based on the absorption of moisture by hygroscopic substances, the best of which is Saussure's Hair-Hygrometer; in the second class, the Psychrometer, or wet-bulb thermometer, which gives the temperature of evaporation; in the third, the various instruments designed for ascertaining the temperature of the dew-point. From the data furnished by each of these instruments, and a table of the elastic forces of vapor at different temperatures, the humidity of the air can be deduced with more or less accuracy.

The use of the hygroscopic substances as hygrometers having been nearly given up on account of the inaccuracy of the results, the variability of the instruments, and the difficulty, if not impossibility, of making them comparable, the psychrometer and the dew-point instruments represent the two methods now usually employed in Meteorology. The following set, therefore, contains extensive tables, in French and English measures, for deducing the hygrometrical condition of the atmosphere from the indications of the Psychrometer and of the dew-point instruments, to which have been added tables of the weight of vapor, in a given space, at different temperatures, — an element often needed in Meteorology.

As, however, the results deduced from the same data furnished by the observations may considerably differ, according to the values of the elastic force of vapor, and the formulæ used in the computation, the tables have been arranged in two series.

The first series contains Regnault's table of the elastic forces of vapor, with tables of the three kinds above mentioned, together with a corresponding set in English measures. Tables V. to X. have been computed for this volume.

The second series gives the table of elastic forces of vapor deduced from Dalton's experiments, and adopted in the Greenwich Observations, together with the various tables based on it.

B

HYGROMETRICAL TABLES.

A third series of miscellaneous tables furnishes the means of comparing the different values of the elastic force and weight of vapor determined by various physicists, as well as the results of Saussure's Hair-Hygrometer, with those obtained by other methods.

An Appendix, containing tables for comparing the quantity of rain-water indicated in different measures, closes the set.

Though the first series of tables, based on Regnault's table of tensions, is recommended for ordinary use, as being derived from the determinations which seem to deserve the greatest degree of confidence, it was thought expedient to give also the Greenwich tables, which have been, and still are, so extensively used in England, in order to enable meteorologists to judge of the differences which exist between the results obtained by them and those deduced from the constants of Regnault and others.

$\label{eq:continuous_problem} P~R~A~C~T~I~C~A~L~~T~A~B~L~E~S~,$

1N

FRENCH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.



TABLE

OF

THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES,

BY REGNAULT.

This table contains the elastic forces of vapor corresponding to every tenth of a degree of temperature between —35° and +40° Centigrade, as determined by the experiments of V. Regnault, made by order of the French government, for the purpose of establishing the numerical value of the elements which enter into the computations concerning the steam-engine. These results are generally considered as the most accurate science possesses at present. They are published in the Mémoires de l'Institut, Tom. XXI.; and more correctly in Regnault's Etudes sur l'Hygrométrie, in the Annales de Chimie et de Physique. In Vol. XV. Regnault gives the table of elastic forces for every tenth of a degree from —10° to +35° Centigrade, which is reprinted in Table I. The numbers below —10° and above +35°, in the same table, have been taken from another table for every full degree, previously published in Vol. XI. p. 333 of the same periodical, and in the same volume of the Mémoires de l'Institut, extending from —32° to +230°.

It should be remarked, however, that the numbers below zero, in the two tables just mentioned, having been computed from different formulas of interpolation, slightly disagree. In order to establish a continuity, therefore, the numbers in Table I. corresponding to full degrees from -10° to -35° have been formed by starting from the value due to -10° in the larger table of Regnault, and subtracting from it the difference between -10° and -11° in the other table, in order to find the value of -11° , and so on, by subtracting successively the corresponding differences to -35° . For the fractions of degrees below -10° , the mean values have been adopted as sufficiently accurate for meteorological purposes.

I. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

By REGNAULT.

Tempera-					Tenths of	Degrees.				
ture Centigrade.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-35	0.221	0.219	0.216	0.214	0.211	0.209	0.207	0.204	0.202	0.199
-34	0.247	0.244	0.242	0.249	0.237	0.234	0.231	0.229	0.226	0.224
-33	0.275	0.272	0.269	0.267	0.264	0.261	0.258	0.255	0.253	0.250
-32	0.305	0.302	0.299	0.296	0.293	0.290	0.287	0.284	0.281	0.278
-31	0.337	0.334	0.331	0.327	0.324	0.321	0.318	0.315	0.311	.0.308
-30	0.371	0.368	0.364	0.361	0.357	0.354	0.351	0.347	0.344	0.340
-29	0.409	0.405	0.401	0.398	0.394	0.390	0.386	0.382	0.379	0.375
-28	0.449	0.445	0.441	0.437	0.433	0.429	0.425	0.421	0.417	0.413
-27	0.493	0.489	0.484	0.480	0.475	0.471	0.467	0.462	0.458	0.453
-26	0.540	0.535	0.531	0.526	0.521	0.516	0.512	0.507	0.502	0.498
-25	0.590	0.585	0.580	0.575	0.570	0.565	0.560	0.555	0.550	0.545
-24	0.645	0.639	0.634	0.628	0.623	0.617	0.612	0.606	0.601	0.595
-23	0.704	0.698	0.692	0.686	0.680	0.674	0.669	0.663	0.657	0.651
-22	0.768	0.762	0.755	0.749	0.742	0.736	0.730	0.723	0.717	0.710
-21	0.838	0.831	0.824	0.817	0.810	0.803	0.796	0.789	0.782	0.775
-20	0.912	0.905	0.897	0.890	0.882	0.875	0.868	0.860	0.853	0.845
-19	0.993	0.985	0.977	0.969	0.961	0.952	0.944	0.936	0.928	0.920
-18	1.080	1.071	1.063	1.054	1.045	1.036	1.028	1.019	1.010	1.002
-17	1.174	1.165	1.155	1.146	1.136	1.127	1.118	1.108	1.099	1.089
-16	1.275	1.265	1.255	1.245	1.235	1.224	1.214	1.204	1.194	1.184
-15	1.385	1.374	1.363	1.352	1.341	1.330	1.319	1.308	1.297	1.286
-14	1.503	1.491	1.479	1.468	1.456	1.444	1.432	1.420	1.409	1.397
-13	1.631	1.618	1.605	1.593	1.580	1.567	1.554	1.541	1.529	1.516
-12	1.768	1.754	1.741	1.727	1.713	1.699	1.686	1.672	1.658	1.645
-11	1.918	1.903	1.888	1.873	1.858	1.843	1.828	1.813	1.798	1.783
-10	2.078	2.062	2.046	2.030	2.014	1.998	1.982	1.966	1.950	1.934
- 9	2.261	2.242	2.223	2.204	2.186	2.168	2.150	2.132	2.114	2.096
- 8	2.456	2.436	2.416	2.396	2.376	2.356	2.337	2.318	2.299	2.280
- 7	2.666	2.645	2.624	2.603	2.582	2.561	2.540	2.519	2.498	2.477
- 6	2.890	2.867	2.844	2.821	2.798	2.776	2.754	2.732	2.710	2.688
- 5	3.131	3.106	3.082	3.058	3.034	3.010	2.986	2.962	2.938	2.914
- 4	3.387	3.361	3.335	3.309	3.283	3.257	3.231	3.206	3.181	3.156
- 3	3.662	3.634	3.606	3.578	3.550	3.522	3.495	3.468	3.441	3.414
- 2	3.955	3.925	3.895	3.865	3.836	3.807	3.778	3.749	3.720	3.691
- 1	4.267	4.235	4.203	4.371	4.140	4.109	4.078	4.047	4.016	3.985
- 0	4.600	4.565	4.531	4.497	4 463	4.430	4.397	4.364	4.331	4.299
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade					Tenths of	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 4.600	Millim, 4.633	Millim.	Millim. 4.700	Millim. 4.733	Millim. 4.767	Millim. 4.801	Millim. 4.836	Millim. 4.871	Millim. 4.905
1	4.940	4.975	5.011	5.047	5.082	5.118	5.155	5.191	5.228	5.265
2	5.302	5.340	5.378	5.416	5.454	5.491	5.530	5.569	5.608	5.647
3	5.687	5.727	5.767	5.807	5.848	5.889	5.930	5.972	6.014	6.055
4	6.097	6.140	6.183	6.226	6.270	6.313	6.357	6.401	6.445	6.490
5	6.534	6.580	6.625	6.671	6.717	6.763	6.810	6.857	6.904	6.951
6	6.998	7.047	7.095	7.144	7.193	7.242	7.292	7.342	7.392	7.442
7	7.492	7.544	7.595	7.647	7.699	7.751	7.804	7.857	7.910	7.964
8	8.017	8.072	8.126	8.181	8.236	8.291	8.347	8.404	8.461	8.517
9	8.574	8.632	8.690	8.748	8.807	8.865	8.925	8.985	9.045	9.105
10	9.165	9.227	9.288	9.350	9.412	9.474	9.537	9.601	9.665	9.728
11	9.792	9.857	9.923	9.989	10.054	10.120	10.187	10.255	10.322	10.389
12	10.457	10.526	10.596	10.665	10.734	10.804	10.875	10.947	11.019	11.090
13	11.162	11.235	11.309	11.383	11.456	11.530	11.605	11.681	11.757	11.832
14	11.908	11.986	12.064	12.142	12.220	12.298	12.378	12.458	12.538	12.619
15	12.699	12.781	12.864	12.947	13.029	13.112	13.197	13.281	13.366	13.451
16	13.536	13.623	13.710	13.797	13.885	13.972	14.062	14.151	14.241	14.331
17	14.421	14.513	14.605	14.697	14.790	14.882	14.977	15.072	15.167	15.262
18	15.357	15.454	15.552	15.650	15.747	15.845	15.945	16.045	16.145	16.246
19	16.346	16.449	16.552	16.655	16.758	16.861	16.967	17.073	17.179	17.285
20	17.391	17.500	17.608	17.717	17.826	17.935	18.047	18.159	18.271	18.383
21	18.495	18.610	18.724	18.839	18.954	19.069	19.187	19.305	19.423	19.541
22	19.659	19.780	19.901	20.022	20.143	20.265	20.389	20.514	20.639	20.763
23	20.888	21.016	21.144	21.272	21.400	21.528	21.659	21.790	21.921	22.053
24	22.184	22.319	22.453	22.588	22.723	22.858	22.996	23.135	23.273	23.411
25	23.550	23.692	23.834	23.976	24.119	24.261	24.406	24.552	24.697	24.842
26	24.988	25.138	25.288	25.438	25.588	25.738	25.891	26.045	26.198	26.351
27	26.505	26.663	26.820	26.978	27.136	27.294	27.455	27.617	27.778	27.939
28	28.101	28.267	28.433	28.599	28.765	28.931	29.101	29.271	29.441	29.612
29	29.782	29.956	30.131	30.305	30.479	30.654	30.833	31.011	31.190	31.369
30	31.548	31.729	31.911	32.094	32.278	32.463	32.650	32.837	33.026	33.215
31	33.406	33.596	33.787	33.980	34.174	34.368	34.564	34.761	34.959	35.159
32	35.359	35.559	35.760	35.962	36.165	36.370	36.576	36.783	36.991	37.200
33	37.410	37.621	37.832	38.045	38.258	38.473	38.689	38.906	39.124	39.344
34	39.565	39.786	40.007	40.230	40.455	40.680	40.907	41.135	41.364	41.595
35	41.827	42.059	42.293	42.527	42.763	43.000	43.238	43.477	43.717	43.959
36	44.201	44.445	44.690	44.936	45.183	45.431	45.681	45.932	46.184	46.437
37	46.691	46.947	47.203	47.462	47.721	47.981	48.243	48.506	48.770	49.035
38	49.302	49.570	49.839	50.110	50.382	50.655	50.929	51.205	51.481	51.759
39	52.039	52.320	52.602	52.885	53.170	53.456	53.743	54.032	54.322	54.613
40	54.906	55.200	55.496	55.793	56.091	56.391	56.692	56.994	57.293	57.603
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

GIVING IMMEDIATELY THE FORCE OF AQUEOUS VAPOR AND THE RELATIVE HUMIDITY FROM THE INDICATIONS OF THE PSYCHROMETER.

CALCULATED BY M. T. HAEGHENS.

In his Etudes sur l'Hygrométrie,* M. V. Regnault discusses the theoretical bases of the formula of the Psychrometer, given by M. August, which was,

$$x = f^{2} - \frac{0.568(t-t')}{640-t'} h$$

in which h represents the height of the barometer; t the temperature of the air given by the dry-bulb thermometer; t' the temperature of the wet-bulb thermometer; f' the force of aqueous vapor in the saturated air at a temperature equal to t'; x the elastic force of aqueous vapor which exists in the air at the time of the observation.

After having modified some of the numerical values, which form the coefficients, M. Regnault adopted this formula,

 $x = f' - \frac{0.429 (t - t')}{610 - t'} h.$

But comparative experiments, made by himself, showed that by substituting the coefficient 0.480 for that of 0.429, the calculated results, and those obtained by direct observation, agree perfectly in the fractions of saturation, which are greater than 0.40. This formula thus modified, or

 $x = f' - \frac{0.480 (t - t')}{610 - t'} h,$

has been used for calculating the following tables. In that part of the tables which supposes the wet-bulb to be covered with a film of ice, or below the freezing point, the value 610 — t', which represents the latent heat of aqueous vapor, has been changed into this: 610 + 79 - t' = 689 - t'.

The only hypothesis made, is that of a mean barometric pressure h, equal to 755 millimetres. If we take into account the causes of errors inherent to the psychrometer, and to the tables of the force of vapor, by means of which the absolute force of vapor is calculated, as well as to the differences of these tensions, taken at temperatures differing only by one tenth of a degree, it will be obvious that the correction due to the variations of barometric pressure can almost always be neglected. less, a separate table has been calculated, giving the correction to be applied to the numbers in the Psychrometrical Tables for the heights of the barometer between 650 and 800 millimetres. It will be found at the end of the tables.

The disposition of the tables is the following: —

The temperatures are noted in centigrade degrees; the elastic force of vapor in the air, or its pressure on the barometer, is expressed in millimetres of mercury; the rel-

^{*} Etudes sur l'Hygrométrie, par M. V. Regnault. Annales de Chimie et de Physique, 3^{me} Série, Tom X.V., 1845.

ative humidity is indicated in per cent. of the full saturation of the air at the corresponding temperature of the dry-bulb thermometer t.

The first vertical column contains the indications of the wet-bulb thermometer t', beginning with the temperatures below the freezing point, when the bulb is covered with ice, from -35° , and continuing from the freezing point up to $+35^{\circ}$ centigrade, the bulb being simply wet.

The second column gives the differences of the force of vapor for each tenth (0°.1) of a degree, between each full degree of the first column. It enables the observer to find out the correction for any fraction of a degree of the wet-bulb thermometer.

The following double columns give immediately the force of vapor and the relative humidity, corresponding to each degree of the wet-bulb, placed in the first column, on the same horizontal line, and to differences of the two thermometers, or to t-t', taken at every two tenths of a degree.

The horizontal column at the bottom indicates the mean difference, for each tenth of a degree, of the force of vapor contained in the same horizontal line. It gives the correction for the intermediate differences of the thermometers; 0.1, 0.3, 0.5, 0.7, 0.9, &c., &c.

To meet the wants arising from the extreme climate of North America, the tables of Mr. Haeghens have been extended from —15° to —35° centigrade, and from +30° to +35° of temperature of the wet-bulb, and to +40° of temperature of the dry-bulb thermometer. The forces of aqueous vapor of Regnault, as given in Table I., have been used for the calculations.

Use of the Tables.

Enter the tables with the difference of the two thermometers, or t-t', and with the temperature of the wet-bulb thermometer t', taking the first three pages, when the temperature of the wet-bulb is below the freezing point; and the following ones when it is above the freezing point.

Seek first the column at the head of which you find the difference of the thermometers; go down as far as the horizontal line, at the beginning of which you see the temperature of the wet-bulb thermometer; there you find the force of vapor, and the relative humidity corresponding to your observation.

Two corrections for fractions may be required for a complete calculation of the force of vapor; one for the fractions of degrees of the wet-bulb thermometer; another for the intermediate differences of the two thermometers, viz. for 0.1, 0.3, 0.5, 0.7, &c.

The first correction for fractions of degrees of the wet-bulb thermometer is found by multiplying the decimal fraction by the number placed in the second vertical column next to the whole degree, which number is the value of a tenth of a degree. The product must be *added* to the value of the full degree given in the table, when the temperature of the wet-bulb is above the freezing point; it must be *subtracted* when the temperature is below the freezing point, and receives the sign —. This correction is too important to be neglected.

The second correction, less important, for the intermediate differences of the ther-B

mometers, which are greater by one tenth than those indicated in the tables, is given in the horizontal column at the bottom of the page. It is *constant* and always *subtractive*.

Examples of Calculation.

Difference of thermometers, or $t - t' = 0^{\circ}.8$.

Temperature of the wet-bulb thermometer, $t' = 11^{\circ}.0$.

We find, page 18, for t-t', fifth double column; and for t', first column,

The force of vapor in the air $= 9^{mm}$.31.

Relative humidity,

= 90.

46

Difference of thermometers, or t-t', = 7°.2.

Wet-bulb thermometer, or t', $= 17^{\circ}.9$.

We find, page 24, for t - t', = 7°.2, and $t' = 17^{\circ}.0$, force of vapor $10^{\text{mm}}.02$.

Additive correction for fraction $0^{\circ}.9$, or $9 \times 0.09 = 0$.81.

Force of vapor in the air = 10 .83.

Relative humidity,

Difference of thermometers, $t - t' = 6^{\circ}.5$.

Wet-bulb thermometer, $t' = 23^{\circ}.6$.

We find, page 23, for $t' = 23^{\circ}.0$, and t - t', or difference, $= 6^{\circ}.4$, force of vapor $16^{\text{nam}}.94$; applying immediately the correction found at the bottom of the page for one tenth more difference, or $6^{\circ}.4 + 0.1 = 6^{\circ}.5$, we have,

Force of vapor = $16^{mm}.94 - 0.06$, or

16mm.88.

Additive correction for fraction 0.6 of the wet-bulb, $6 \times 0.13 = 0$.78.

Force of vapor in the air = 17 .66.

Relative humidity,

56.

The wet-bulb thermometer covered with ice.

Difference of thermometers, $t-t'=2^{\circ}.8$.

Wet-bulb thermometer (ice), $t' = -8^{\circ}.5$.

Page 17 gives for $t-t'=2^{\circ}.8$, and $t'=-8^{\circ}.0$, force of vapor = $1^{\text{mm}}.0$. Subtractive correction for fraction 0.5 of wet-bulb, $5 \times 0.019 = -0$.1.

Force of vapor in the air = 0 .9.

Relative humidity,

30.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

Wet- Bulb Thermo- meter t' Centi- grade	Mean														
Centi- grade	Differ-	0 °.	0	0°.	.2	0°.	4	0°.	6	0°.	8	10	.0		
Degrees.	ence for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.								
0	Millim.	Millim.		Millim.		Millim.		Millim		Millim.		Millim.			
-35	0.003	0.22	100	0.12	53										
-34	0.003	0.25	100	0.15	58	0.05	18								
-33	0.003	0.27	100	0.17	62	0.07	26								
-32	0.003	0.30	100	0.20	66	0.10	33								
-31		0.34	100	0.24	69	0.14	39	0.03	10						
	0.004		100					0.0-							
-30	0.004	0.37	100	0.27	71	0.17	44	0.07	17						
-29	0.004	0.41	100	0.31	74	0.21	46	0.11	25						
-28	0.004	0.45	100	0.35	76	0.25	53	0.15	31	0.04	9				
-27	0.005	0.49	100	0.39	78	0.29	57	0.19	36	0.09	17				
-26	0.005	0.54	100	0.44	80	0.34	60	0.24	41	0.13	23	0.03	6		
-25	0.003	0.59	100	0.49	81	0.39	63	0.29	46	0.18	29	0.08	12		
-24	0.005	0.64	100	0.54	82	0.35	66	0.23	50	0.15	34	0.03	19		
-23	0.006	0.70	100	0.60	84	0.50	69	0.40	53	0.24	39	0.14	25		
-22	0.006	0.77	100	0.67	85	0.56	71	0.46	5 7	0.36	39 44	0.19	31		
-21	0.007	0.84	100	0.74	86	1	73	0.53	60				36		
- 1	0.008	0.04	100	0.14	80	0.63	10	0.55	60	0.43	48	0.33	30		
-20	0.003	0.91	100	0.81	87	0.71	75	0.61	63	0.50	51	0.40	40		
-19	0.008	0.99	100	0.89	88	0.71	77	0.69	66	0.58		0.48	45		
-18	0.008	1.08	100	0.98	89	0.75	78	0.03	68	0.67	55 58	0.48	48		
-17	0.009	1.03	100	1.07	90	0.97	80	0.87	70				52		
-16	0.010	1.17	100	1.07	90	1.07	S1	1.97	70	0.76	61 63	0.66	55		
10	0.011	1.27	100	1.17	30	1.07	01	1.57	14	0.86	00	0.76	99		
-15	0.011	1.38	100	1.23	91	1.18	82	1.08	74	0.07	66	0.87	58		
-14	0.012	1.50	100	1.40	92	1.15	83	1.19	74 76	$\begin{bmatrix} 0.97 \\ 1.09 \end{bmatrix}$	68	0.99	61		
-13	0.013	1.63	100	1.53	92	1.42	84	1.13	77	1.09	70	1.11	63		
-12	0.014	1.77	100	1.66	93	1.56	85	1.46	78	1.35	71	1.11	65		
-11	0.015	1.92	100	1.81	93	1.71	86	1.61	80	1.50	73	1.40	67		
~	0.016	1.02	100	1.01			00	1.51	00	1.50	19	1.40	01		
-10	0.016	2.08	100	1.97	94	1.87	87	1.77	81	1.66	75	1.56	69		
- 9	0.019	2.26	100	2.16	94	2.05	88	1.95	82	1.85	76	1.74	71		
- 8	0.021	2.46	100	2.35	94	2.25	89	2.14	83	2.04	78	1.94	73		
- 7	0.023	2.67	100	2.56	94	2.46	89	2.35	84	2.25	79	2.15	74		
- 6	0.024	2.89	100	2.79	95	2.68	90	2.58	85	2.47	80	2.37	76		
	0.025			,0		2.30		2.30	~ ·						
- 5	0.040	3.13	100	3.03	95	2.92	90	2.82	86	2.71	81	2.61	77		
- 4	0.028	3.39	100	3.28	95	3.18	91	3.07	87	2.97	82	2.86	78		
- 3	0.029	3.66	100	3.56	96	3.45	92	3.35	87	3.24	83	3.14	79		
- 2	0.031	3.96	100	3.85	96	3.75	92	3.64	88	3.54	84	3.43	80		
- 1	0.033	4.27	100	4.16	96	4.06	92	3.95	89	3.85	85	3.74	81		
- 0	0.034	4.60	100	4.50	96	4.40	93	4.29	89	4.19	86	4.08	82		

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.05$ mm.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

Centigrade Degrees.	Mean Vertical Differ- ence for ach 0°.1.	To. Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative Humidity.	Force of Vapor.	Relative	10.	Rela-	20.	O Rela-	20.	
Centigrade Degrees. 0	ence for ach 0°. I.	Vapor.	tive Hu- mid-	Vapor.	tive Hu- mid-		tive			-	Rola-		
-35 -34 -33 -32	Millim.	Millim.		Millim.		I	mid- ity.	Force of Vapor.	tive Hu- mid- ity.	Force of Vapor.	tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
			,			Millim.		Millim.		Millim.		Millim.	
-30 -29 -28 -27 -26													
-25 -24 -23 -22 -21	0.006 0.006 0.007	0.04 0.09 0.16 0.23	5 12 18 24	0.05 0.12	6 13								
-20 -19 -18 -17 -16	0.008 0.008 0.009 0.010	0.30 0.38 0.46 0.56 0.66	30 34 39 43 47	0.20 0.28 0.36 0.46 0.56	18 25 30 35 39	0.09 0.17 0.26 0.35 0.45	9 15 21 26 31	0.07 0.16 0.25 0.35	6 13 18 24	0.05 0.15 0.25	4 11 16	0.04 0.14	3 9
-15 -14 -13 -12 -11	0.011 0.013 0.013 0.015 0.017	0.77 0.88 1.01 1.15 1.30	50 53 56 59 61	0.66 0.78 0.91 1.04 1.19	43 46 50 53 55	0.56 0.68 0.80 0.94 1.09	36 40 43 47 50	0.46 0.58 0.70 0.84 0.99	29 33 37 41 44	0.36 0.47 0.60 0.73 0.88	22 27 31 35 39	0.25 0.37 0.50 0.63 0.78	15 21 25 30 34
-10 - 9 - 8 - 7 - 6	0.018 0.019 0.021 0.023 0.024	1.46 1.64 1.83 2.04 2.26	63 66 68 69 71	1.35 1.53 1.73 1.94 2.16	58 61 63 65 67	1.25 1.43 1.62 1.83 2.06	52 56 58 61 63	1.15 1.33 1.52 1.73 1.95	47 51 54 56 59	1.04 1.22 1.42 1.63 1.85	42 46 49 52 55	0.94 1.12 1.31 1.52 1.74	38 41 45 48 51
- 5 - 4 - 3 - 2 - 1	0.025 0.028 0.029 0.030 0.031	2.50 2.76 3.03 3.33 3.64	73 74 75 77 78	2.40 2.65 2.93 3.22 3.53	69 70 72 73 75	2.30 2.55 2.82 3.12 3.43	65 67 68 70 71	2.19 2.45 2.72 3.01 3.32	61 63 65 66 68	2.09 2.34 2.61 2.91 3.22	57 59 61 63 65	1.98 2.24 2.51 2.80 3.11	53 55 58 60 62

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1=0.05~\mathrm{mm}$.

Below the Freezing-Point; the Bulb covered with a Film of Ice.

				t-	t', Diff	erence of	Wet ar	nd Dry Bu	ılb The	rmometer	·s.		
Wet- Bulb Thermo- meter	Mean Vertical Differ-	20	4	20	.6	2°.	8	30.	.0	3°	.2	3°	.4
Centigrade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative IIu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
-15	0.011	0.15	9	0.05	3	0.00	١.						
-14 -13	0.013	$0.27 \\ 0.39$	15 20	$0.16 \\ 0.29$	9 14	0.06	9	0.08	4				
-12	0.013	0.53	25	$0.29 \\ 0.42$	19	0.32	14	0.22	10	0.11	5	•	
-11	0.015	0.68	29	0.57	24	0.47	19	0.36	15	0.26	10	0.16	6
	0.016												
-10		0.83	33	0.73	28	0.63	24	0.52	20	0.42	16	0.32	12
- 9	0.018 0.019	1.02	37	0.91	33	0.81	28	0.70	24	0.60	20	0.50	17
- 8	0.019	1.21	40	1.10	36	1.00	32	0.90	28	G.79	25	0.69	21
- 7	0.021	1.42	44	1.31	40	1.21	36	1.11	32	1.00	29	0.90	26
- 6		1.64	47	1.54	43	1.43	40	1.33	36	1.22	33	1.12	30
_	0.024	1.00	50	1.77	46	1.67	43	1.57	40	1.46	36	1.36	33
- 5 4	0.025	$\frac{1.88}{2.13}$	50 52	$\frac{1.77}{2.03}$	49	1.92	46	1.82	43	1.71	40	1.61	37
- 3	0.027	$\frac{2.13}{2.40}$	55	$\frac{2.03}{2.30}$	52	2.19	48	2.09	45	1.99	43	1.88	40
- 2	0.029	2.70	57	2.59	54	2.49	51	2.38	48	2.28	46	2.17	43
- 1	0.031	3.01	59	2.90	56	2.80	54	2.69	51	2.59	48	2.48	46
						, A							
		3 °.	.6	3∘.	.8	40.	.0	40	.2	40	.4	40.	.6
		Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1.5	i		!										
-15 -14	1							l		1			
-13		ł		l		l						١.	
-12						1		l					
-11		0.05	2			i		1		1			
	0.016			1									
-10	0.018	0.21	8	0.11	4								
- 9	0.019	0.39	13	0.29	9	0.19	6	0.08	3			0.00	
- 8	0.021	0.58	18	0.48	14	0.38	11	0.27	8	0.17	5	$0.06 \\ 0.27$	2
- 7	0.022	0.79	22	0.69	19	0.59	16	0.48	13	$0.38 \\ 0.60$	10 15	0.27	7 12
- 6	0.024	1.01	26	0.91	23	0.81	20	0.70	17	0.00	19	0.49	1
- 5		1.25	30	1.15	27	1.01	24	0.94	22	0.83	19	0.73	16
- 4	0.025	1.50	34	1.40	31	1.30	28	1.19	26	1.09	23	0.98	20
- 3	0.027	1.78	37	1.67	34	1.57	32	1.46	29	1.36	27	1.25	24
- 2	0.029	2.07	40	1.96	37	1.86	35	1.75	33	1.65	30	1.54	28
- 1	0.031	2.38	43	2.27	40	2.17	38	2.06	36	1.96	34	1.85	31
		Man	n Homin	ontol Diff	omonaa	of Force	of Vano	r for each	001_	0.05 mm.			-

Wet-				t — 1	z', Diffe	rence of	Wet ar	nd Dry-Bu	lb The	rmometer	3.		
Bulb Thermo- meter.	Differ-	0	·.0	0°.	.2	0°.	4	0°.	6	0°.	.8	10	.0
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim		Millim.		Millim.		Millim.	
0	0.03	4.60	100	4.48	96	4.36	92	4.24	88	4.12	85	4.01	81
1	0.04	4.94	100	4.82	96	4.70	93	4.58	89	4.46	85	4.35	82
2	0.04	5.30	100	5.18	96	5.06	93	4.94	89	4.83	86	4.71	83
3	0.04	5.69	100	5.57	97	5.45	93	5.33	90	5.21	87	5.09	83
4 5	0.04	6.10	100 100	5.98 6.41	97	5.86 6.29	93 94	5.74 6.17	90	5.62 6.05	87 88	5.50 5.94	84
1 3	0.05	6.53	100	0.41	97	0.29	94	0.17	91	0.03	00	3.94	85
6	0.05	7.00	100	6.88	97	6.76	94	6.64	91	6.52	88	6.40	85
7	0.05	7.49	100	7.37	97	7.25	94	7.13	91	7.01	89	6.89	86
8	0.05	8.02	100	7.90	97	7.78	94	7.66	92	7.54	89	7.42	86
9	0.06	8.57	100	8.45	97	8.33	95	8.21	92	8.69	89	7.97	86
10	0.06	9.17	100	9.04	97	8.92	95	8.80	93	8.68	90	8.56	87
	0.06	"				0.02		0.00					
11		9.79	100	9.67	97	9.55	95	9.43	93	9.31	90	9.19	88
12	0.07	10.46	100	10.34	98	10.21	95	10.09	93	9.97	90	9.85	88
13	0.07	11.16	100	11.04	98	10.92	95	10.80	93	10.68	91	10.56	89
14	0.07 0.08	11.91	100	11.79	98	11.66	95	11.54	93	11.42	91	11.30	89
15	0.08	12.70	100	12.58	98	12.46	96	12.33	93	12.21	91	12.09	89
16	0.09	13.54	100	13.41	98	13.29	96	13.17	94	13.05	92	12.93	90
17	0.09	14.42	100	14.30	98	14.18	96	14.05	94	13.93	92	13.81	90
18	0.05	15.36	100	15.23	98	15.11	96	14.99	94	14.87	92	14.75	90
19	0.10	16.35	100	16.22	98	16.10	96	15.98	94	15.86	92	15.73	91
20	0.10	17.39	100	17.27	98	17.15	96	17.02	94	16.90	92	16.78	91
	0.11		_						- 1				
21	0.12	18.50	100	18.37	98	18.25	96	18.13	94	18.00	92	17.88	91
22	0.12	19.66	100	19.54	98	19.41	96	19.29	95	19.17	93	19.04	91
23	0.13	20.89	100	20.76	98	20.64	96	20.52	95	20.39	93	20.27	91
$\begin{array}{c c} 24 \\ 25 \end{array}$	0.14	22.18	100	22.06	98	21.94	97	21.81	95	21.69	93	21.57	92
49	0.14	23.55	100	23.43	98	23.30	97	23.18	95	23.05	93	22.93	92
26	0.14	24.99	100	24.86	98	24.74	97	24.62	95	24.49	93	24.37	92
27	0.15	26.51	100	26.38	98	26.26	97	26.13	95	26.01	93	25.88	92
28	0.16	28.10	100	27.98	98	27.85	97	27.73	95	27.60	93	27.48	92
29	0.17	29.78	100	29.66	98	29.53	97	29.41	95	29.28	94	29.16	92
30	0.18	31.55	100	31.42	98	31.30	97	31.17	95	30.05	94	30.92	93
'	0.19					- 50	-		-				
31	0.00	33.40	100	33.28	98	33.15	97	33.03	96	32.90	94	32.78	93
32	0.20	35.36	100	35.23	99	35.11	97	34.98	96	34.86	94	34.73	93
33	0.21	37.41	100	37.28	99	37.16	98	37.03	96	36.91	94	36.78	93
34	0.23	39.56	100	39.43	99	39.31	98	39.18	96	39.06	94	38.93	93
35	0.20	41.83	100	41.70	99	41.58	98	41.45	96	41.33	95	41.20	93
			'						<u>'</u>				

В

Wet-				t – 1	, Diffe	erence of	Wet a	ad Dry-Bi	ılb T he	rmometer	s.		
Bulb Thermo- meter.	Mean Vertical Differ-	1	.2	10,	4	1°.	6	10.	.8	2°.	.0	2°	.2
Centi- grade Degrees	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity,	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor,	Rela- tive Hu- mid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim,	_	Millim.		Millim.		Millim.		Millim.	
1	0.03	3.89 4.23	78	3.77	74	3.65	71	3.53	67	3.41	64	3.29	61
2	0.04	4.23	79 80	4.11 4.47	75 76	3.99	72	3.87	69	3.75	66	3.63	63
3	0.04	4.97	80	4.85	77	4.35 4.73	73 74	4.23 4.61	70 71	4.11	67	3.99	65
4	0.04	5.38	81	5.26	78	5.14	75	5.02	73	4.49	69 70	4.37	66
5	0.04	5.82	82	5.70	79	5.58	77	5.46	74	5.34	71	5.22	67 69
	0.05					0.00	••	0.10	• •	0.01	**	9.22	09
6	0.05	6.28	83	6.16	80	6.04	77	5.92	75	5.80	72	5.68	70
7	0.05	6.77	83	6.65	81	6.53	78	6.41	76	6.29	73	6.17	71
8	0.06	7.29	84	7.17	81	7.05	79	6.93	76	6.81	74	6.69	72
9	0.06	7.85	84	7.73	82	7.61	80	7.49	77	7.37	75	7.25	73
10		8.44	85	8.32	83	8.20	80	8.08	78	7.96	76	7.84	74
	0.06												
11	0.07	9.07	86	8.95	83	8.82	81	8.70	79	8.58	77	8.46	7 5
12	0.07	9.73	86	9.61	84	9.49	82	9.37	80	9.25	7 8	9.12	76
13	0.08	10.43	86	10.31	84	10.19	82	10.07	80	9.95	78	9.83	76
14	0.08	11.18	87	11.06	85	10.91	83	10.81	81	10.69	79	10.57	77
15	0.08	11.97	87	11.85	85	11.73	83	11.60	81	11.48	80	11.36	78
16	0.05	12.80	88	12.68	86	10.50							
17	0.09	13.69	88	13.57	86	12.56 13.44	84	12.44	82	12.32	80	12.19	7S
18	0.09	14.62	88	14.50	87	14.38	84 85	13.32	83 83	13.20 14.13	S1 S1	13.08	7 9
19	0.10	15.61	89	15.49	87	15.37	85	15.24	83	15.12	82	14.01 15.00	80 80
20	0.11	16.65	89	16.53	87	16.41	86	16.29	84	16.16	82	16.04	81
1	0.11				٠. ا	20171		10.23	0.4	10.10	02	10.04	01
21	0.10	17.76	89	17.63	88	17.51	86	17.39	84	17.27	83	17.14	81
22	0.12 0.12	18.92	90	18.80	ss	18.67	86	18.55	85	18.43	83	18.30	82
23	0.12	20.15	90	20.02	88	19.90	87	19.78	85	19.65	83	19.53	82
24	0.13	21.41	90	21.32	ss	21 20	87	21.07	85	20.95	84	20.82	82
25		22.81	90	22.68	89	22.56	87	22.44	86	22.31	84	22.19	83
- 1	0.14						l			- 1	- 1		
26	0.15	24.24	90	24.12	89	23.99	87	23.87	86	23.75	85	23.62	83
27	0.16	25.76	91	25.63	89	25.51	88	25.39	86	25.26	85	25.14	83
28	0.17	27.35	91	27.23	89	27.10	83	26.98	87	26.86	85	26.73	84
29 30	0.18	29.03	91	28.91	90	28.78	SS	28.66	87	28.53	85	28.41	84
50	0.19	30.80	91	30.67	90	30.55	89	30.42	87	30.30	86	30.17	84
31		32.65	91	32.53	90	32.40	89	32.28	٥	22.15	e. [20.00	0-
32	0.20	34.61		34.48	90	31.36	89	31.23	87 88	32.15 34.11	86	32.03 33.98	85
33	0.21	36.66		36.53	90	36.41	89	36.28	88	36.16	86	36.03	85 85
31	0.22	38.81		38.68	90	38.56		38.43	88	38.31	87	38.18	85
35	0.23	41.07	92	40.91	91	40.82	89	40.69	88	40.57	87	40.44	86

				t — t	', Diffe	rence of	Wet an	d Dry-Bu	lb The	rmometer	s.		
Wet- Bulb Thermo- meter. t'	Mean Vertical Differ-	2°	.4	2°.	6	2°.	8	3°.	0	3°.	2	3°.	4
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim		Millim.		Millim.		Millim.	
0	0.03	3.17	58	3.06	55	2.94	52	2.82	50	2.70	47	2.58	44
1	0.03	3.51	60	3.39	57	3.27	54	3.16	52	3.04	49	2.92	47
2	0.04	3.87	62	3.75	59	3.63	56	3.51	54	3.39	51	3.28	49
3	0.04	4.25	63	4.13	61	4.02	58	3.90	56	3.78	53	3.66	51
4	0.04	4.66	65	4.51	62	4.42	60	4.30	57	4.18	55	4.06	53
5	ļ	5.10	66	4.98	64	4.86	61	4.74	59	4.62	57	4.50	55
	0.05		C**		0-		CO	E 00	C1	= 00	F0	400	F.0
6	0.05	5.56	67	5.44	65	5.32	63	5.20	61	5.08 5.57	58	4.96	56
8	0.05	6.05 6.57	69 70	5.93 6 45	66 68	5.81 6.33	64	$\frac{5.69}{6.21}$	62 63	6.09	60 61	5.45 5.97	58 59
9	0.06	7.13	70	7.01	69	6.89	65 67	6.77	65	6.64	63	$\begin{array}{c} 5.97 \\ 6.52 \end{array}$	61
10	0.06	7.13	72	7.59	70		68	7.35	66	7.23	64	7.11	62
10	0.06	1.12	1-	1.00	70	7.47	00	1.00	00	1.20	0-1	7.11	04
11	0.00	8.34	73	8.22	71	8.10	69	7.98	67	7.86	65	7.74	63
12	0.07	9.00	74	8.88	72	8.76	70	8.64	68	8.52	66	8.40	64
13	0.07	9.71	75	9.58	73	9.46	71	9.34	69	9.22	67	9.10	66
14	0.07	10.45	75	10.33	73	10.21	72	10.08	70	9.96	68	9.84	67
15	0.08	11.24	76	11.12	74	10.99	72	10.87	71	10.75	69	10.63	67
1	0.08	****			• •	10.00		2010.			00	10.00	•
16		12.07	77	11.95	75	11.83	73	11.71	72	11.58	70	11.46	68
17	0.09	12.95	77	12.83	76	12.71	74	12.59	72	12.47	71	12.34	69
18	0.09	13.89	78	13.77	76	13.64	75	13.52	73	13.40	72	13.28	70
19	0.10	14.87	78	14.75	77	14.63	75	14.51	74	14.38	72	14.26	71
20	0.10	15.92	79	15.79	77	15.67	76	15.55	74	15.43	73	15.30	72
	0.11												
21	0.10	17.02	80	16.90	78	16.77	77	16.65	75	16.53	74	16.40	72
22	0.12	18.18	80	18.06	79	17.93	77	17.81	76	17.69	74	17.56	73
23	0.13	19.41	80	19.28	79	19.16	78	19.04	76	18.91	75	18.79	73
24	0.13	20.70	81	20.58	79	20.45	78	20.33	77	20.21	75	20.08	74
25		22.06	81	21.94	80	21.82	79	21.69	77	21.57	76	21.45	7 5
	0.14			-									
26	0.15	23.50	82	23.37	80	23.25	79	23.13	78	23.00	77	22.88	75
27	0.16	25.01	82	24.89	81	24.76	79	24.64	78	24.51	77	24.39	76
28	0.17	26.61	83	26.48	81	26.36	80	26.23	79	26.11	77	25.98	76
29	0.18	28.28	83	28.16	81	28.03	80	27.91	79	27.69	77	27.76	76
30	0.10	30.05	83	29.92	82	29.80	81	29.67	79	29.55	78	29.42	77
24	0.19	21.00		27.50		01.05	0.1	01 50	00	91 (0	m _O	27.00	
31 32	0.20	31.90	83	31.78	82	31.65	81	31.53	80 80	31.40 33.36	78 79	31.28 33.23	77 78
33	0.21	33.86 35.90	84 84	33.73 35.77	82	33.61	81 81	33.48 35.52	80	35.40	79 79	35.27	78
34	0.22	38.06	84	37.93	83 83	35.65 37.81	81	35.52 37.68	81	37.56	80	37.43	78
35	0.23	40.31	84	40.18	83	40.06	82	39.93	81	39.S1	so so	39.68	79
	- I	10.01	0.4	40.10	00	40.00	04	00.00	O.I.	99.01		99.00	

117				t — t	, Diffe	rence of	Vet an	d Dry-Bu	lb T her	mometer	3.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	3	.6	3°.	8	4 °.	0	4 °.	2	4 °.	4	4 °.	6
t' Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor,	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Mıllim.	
Õ	0.03	2.46	41	2.34	39	2.22	36	2.11	34	1.99	32	1.87	29
1	0.03	2.80	44	2.68	42	2.56	39	2.44	37	2.32	35	2.20	32
2	0.04	3.16	46	3.04	44	2.92	42	2.80	39	2.68	37	2.56	35
3		3.54	49	3.42	46	3.30	44	3.18	42	3.06	40	2.94	38
4	0.04	3.94	51	3.82	48	3.71	46	3.59	44	3.47	42	3.35	-10
5	0.04	4.38	52	4.26	50	4.14	48	4.02	46	3.90	44	3.78	42
	0.05	İ]				l	
6	0.05	4.84	54	4.72	52	4.60	50	4.48	48	4.36	46	4.24	41
7	0.05	5.33	56	5.21	54	5.09	52	4.97	50	4.85	48	4.73	46
8		5.85	57	5.73	56	5.61	54	5.49	52	5.37	50	5.25	48
9	0.06	6.40	59	6.28	57	6.16	55	6.04	53	5.92	52	5.80	50
10	0.06	6.99	60	6.87	58	6.75	57	6.63	55	6.51	53	6.39	52
	0.06					1	1	İ					
11	0.07	7.61	61	7.49	60	7.37	58	7.25	56	7.13	55	7.01	53
12	0.07	8.28	62	8.15	61	8.03	59	7.91	58	7.79	56	7.67	55
13	0.07	8.98	64	8.85	63	8.73	61	8.61	59	8.49	57	8.37	56
14	0.07	9.72	65	9.60	63	9.48	62	9.35	60	9.23	59	9.11	57
15	0.08	10.51	66	10.38	64	10.26	63	10.14	61	10.02	60	9.90	58
	0.08			1									
16	0.60	11.34	67	11.22	65	11.10	64	10.97	62	10.85	61	10.73	59
17	0.09	12.22	68	12.10	67	11.98	65	11.85	63	11.73	62	11.61	61
18	0.09	13.15	69	13.03	67	12.91	66	12.79	64	12.66	63	12.54	62
19	0.10	14.14	69	14.02	68	13.89	66	13.77	65	13.65	64	13.53	62
20	0.11	15.18	70	15.06	69	14.94	67	14.81	66	14.69	65	14.57	63
	0.11			[ŀ		1	İ	İ			
21		16.28	71	16.16	69	16.04	68	15.91	67	15.79	65	15.67	64
22	0.12	17.44	71	17.32	70	17.20	69	17.07	67	16.95	66	16.83	65
23	0.12	18.67	72	18.54	71	18.42	69	18.30	68	18.17	67	18.05	66
24	0.13	19.96	73	19.84	71	19.71	70	19.59	69	19.46	68	19.34	66
25	0.14	21.32	73	21.20	72	21.07	71	20.95	70	20.83	68	20.70	67
	0.14					ļ							
26	0.15	22.75	74	22.63	73	22.50	71	22.38	70	22.26	69	22.13	68
27	0.15	24.27	7-1	24.14	73	24.02	72	23.89	71	23.77	70	23.64	68
28	0.16	25.86	75	25.73	74	25.61	72	25.48	71	25.36	70	25.24	69
29	0.17	27.44	75	27.31	74	27.29	73	27.16	72	27.04	71	26.91	70
30	0.18	29.30	76	29.17	75	29.05	73	28.92	72	28.89	71	28.67	70
	0.19			1									1
31	0.20	31.15	36	31.03	75	30.90	74	30.78	73	30.65	72	30.53	71
32	0.20	33.10	77	32.97	76	32.85	75	32.72	73	32.60	72	32.47	71
33	0.21	35.15	77	35.02	76	34.90	75	31.77	7-1	31.65	73	34.52	72
34	0.23	37.30	77	37.17	76	37.05	75	36.92	74	36.80	73	36.67	72
35	0.23	39.56	78	39.43	77	39.31	76	39.18	74	39.06	73	38.93	72

				t – t	', Diffe	rence of	Wet an	ıd Dry∙Bu	lb The	rmometer	3.		
Wet- Bulb Thermo- meter.	Mean Vertical Differ	4 °	.8	5°.	0	5 °.	2	5°.	4	5°.	6	5∘.	8
Centigrade Begrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid ity.	Force of Vapor,	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity,	Force of Vapor,	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	_
0	0.03	1.75	27	1.63	25	1.51	23	1.39	21	1.27	19	1.15	17
1	0.04	2.08	30	1.97	28	1.85	26	1.73	24	1.61	22	1.49	20
2	0.04	2.44	33	2.32	31	2.20	29	2.08	27	1.96	25	1.85	23
3	0.04	2.82	36	2.70	34	2.58	32	2.46	30	2.34	28	2.22	26
4	0.04	3.23	38	3.11	36	2.99	34	2.87	33	2.75	31	2.63	29
5	·	3.66	40	3.54	39	3.42	37	3.30	35	3.18	33	3.06	32
	0.05					0.00	00			0.01		0.50	
6	0.05	4.12	43	4.00	41	3.88	39	3.76	37	3.64	36	3.52	34
7	0.05	4.61	45	4.49	43	4.37	41	4.25	40	4.13	38 40	4.01	36 39
8	0.06	5.13	47	5.01	45	4.89	43	4.77	,	5.20		4.53	
9	0.06	5.68	48	5.56	47	5.44	45	5.32	44	5.78	42	5.08	41
10	0.00	6.27	50	6.15	48	6.02	47	5.90	45	9.15	44	5.66	42
	0.06	6.00	52	6.77	50	6.65	49	6.53	47	6.40	46	6.28	44
11 12	0.07	6.89 7.55	53	7.43	52	7.31	50	7.18	49	7.06	47	6.94	46
13	0.07	8.25	55	8.13	53	8.01	52	7.88	50	7.76	49	7.64	47
15 14	0.07	8.99	56	8.87	54	8.75	53	8.62	51	8.50	50	8.38	49
15	0.08	9.78	57	9.65	55	9.53	54	9.41	53	9.29	51	9.17	50
19	0.08	3.10	37	5.05	33	3.55	94	3.41	30	0.20	31	3.11	50
16	0.00	10.61	58	10.49	57	10.36	55	10.24	54	10.12	53	10.00	51
17	0.09	11.49	59	11.37	58	11.24	56	11.12	55	11.00	54	10.88	53
18	0.09	12.42	60	12.30	59	12.17	58	12.05	56	11.93	55	11.81	54
19	0.10	13.40	61	13.28	60	13.16	59	13.04	57	12.91	56	12.79	55
20	0.11	14.44	62	14.32	61	14.20	60	14.08	58	13.95	57	13.83	56
1 20	0.11	11041	02	11.02	0.	11.20	0.0	1	00			20.00	
21		15.54	63	15.42	62	15.30	60	15.17	59	15.05	58	14.93	57
22	0.12	16.70	64	16.58	63	16.46	61	16.33	60	16.21	59	16.09	58
23	0.12	17.93	65	17.80	63	17.68	62	17.56	61	17.43	60	17.31	59
24	0.13	19.22	65	19.09	64	18.97	63	18.85	62	18.72	61	18.60	60
25	0.14	20.58	66	20.46	65	20.33	64	20.21	63	20.08	62	19.96	60
	0.14												
26	0.15	22.01	67	21.88	65	21.76	64	21.63	63	21.51	62	21.39	61
27	0.15	23.52	67	23.40	66	23.27	65	23.15	64	23.02	63	22.90	62
28	0.16 0.17	25.11	68	24.99	67	24.86	66	24.74	65	24.61	64	24.49	63
29	0.17	26.79	68	26.66	67	26.54	66	26.41	65	26.29	64	26.16	63
30	0.19	28.55	69	28.42	68	28.30	67	28.17	66	28.05	65	27.92	64
	0.19												
31	0.20	30.40	70	30.28	69	30.15	68	30.03	67	29.90	66	29.78	65
32	0.20	32.35	70	32.22	69	32.10	68	31.97	67	31.85	66	31.72	65
33	0.22	34.40	71	34.27	70	34.15	69	34.02	68	33.90	67	33.77	66
34	0.23	36.55	71	36.42	70	36.30	69	36.17	68	36.05	67	35.92	66
35		38.80	71	38.68	70								

Barbo	Wet-		${f t-t'}$, Difference of Wet and Dry-Bulb Thermometers.											
Particle Particle	Bulb Thermo- meter.	Bulb Mean Thermometer. t' Mean Vertical Differ-		. •••		6°.2		6°.4		6°.6		6°.8		.0
0	grade			munnu.	Force of Vapor.	tive Hu- mid-	Force of Vapor.	tive Hu- mid-		tive Hu- mid-		tive Hu- mid		Rela- tive Hu- mid- ity.
1 0.03 1.37 18 1.25 16 1.13 15 1.01 13 0.89 11 0.78 2 0.04 1.73 22 1.61 20 1.49 18 1.37 16 1.25 15 1.13 3 0.04 2.51 25 1.99 23 1.87 21 1.75 19 1.63 18 1.51 4 0.04 2.51 28 2.39 26 2.27 24 2.15 23 2.03 21 1.91 5 0.05 3.40 33 3.28 31 3.16 29 3.04 28 2.92 26 2.80 7 0.05 3.89 35 3.77 33 3.65 32 3.53 30 3.41 29 3.29 26 2.80 8 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 <t< td=""><td></td><td>Millim.</td><td>Millim.</td><td></td><td>Millim.</td><td></td><td>Millim.</td><td></td><td>Millim.</td><td></td><td>Millim.</td><td></td><td>Millim.</td><td></td></t<>		Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.03	1.04	15	0.92	13	0.80	11	0.68	9	0.56	8	0.44	6
1			1.37	18	1.25	16	1.13	15	1.01	13	0.89	11	0.78	10
3	1	1	1.73	22	1.61	20	1.49	18	1.37	16	1.25	15	1.13	13
4 0.04 2.51 28 2.39 26 2.27 24 2.15 23 2.03 21 1.91 6 0.05 3.40 33 3.28 31 3.16 29 3.04 28 2.92 26 2.80 7 0.05 3.89 35 3.77 33 3.65 32 3.53 30 3.41 29 3.29 8 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 31 3.80 9 0.06 4.96 39 4.84 38 4.71 36 4.59 35 4.47 33 3.92 31 3.80 10 0.06 4.96 39 4.84 38 4.71 36 4.59 35 5.47 31 3.85 11 0.06 6.16 43 6.04 41 5.92 40 5.80 39 5.68	3		2.11	25	1.99	23	1.87	21	1.75	19	1.63	18	1.51	16
5 0.05 2.94 30 2.82 28 2.70 27 2.58 25 2.46 24 2.34 6 0.05 3.40 33 3.28 31 3.16 29 3.04 28 2.92 26 2.80 7 0.05 3.89 35 3.77 33 3.65 32 3.53 30 3.41 29 3.29 8 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 31 3.80 9 0.06 4.96 39 4.84 38 4.71 36 4.59 35 4.47 33 4.35 10 0.06 5.54 41 5.42 40 5.30 39 5.68 37 5.56 11 0.07 6.82 44 6.70 43 6.58 42 6.46 41 6.34 39 6.22 13 <td< td=""><td>1</td><td>1</td><td>2.51</td><td>28</td><td>2.39</td><td>26</td><td>2.27</td><td>24</td><td>2.15</td><td>23</td><td>2.03</td><td>21</td><td>1.91</td><td>19</td></td<>	1	1	2.51	28	2.39	26	2.27	24	2.15	23	2.03	21	1.91	19
6 0.05 3.40 33 3.28 31 3.16 29 3.04 28 2.92 26 2.80 7 0.05 3.89 35 3.77 33 3.65 32 3.53 30 3.41 29 3.29 8 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 31 3.80 9 0.06 4.96 39 4.84 38 4.71 36 4.59 35 4.47 33 4.35 10 0.06 5.54 41 5.42 40 5.30 38 5.18 37 5.06 35 4.94 11 0.06 6.82 44 6.70 43 6.58 42 6.46 41 6.34 39 6.22 13 0.07 6.82 44 6.70 43 6.58 42 6.46 41 6.34 31 7.65 <td>5</td> <td></td> <td>2.94</td> <td>30</td> <td>2.82</td> <td>28</td> <td>2.70</td> <td>27</td> <td>2.58</td> <td>25</td> <td>2.46</td> <td>24</td> <td>2.34</td> <td>22</td>	5		2.94	30	2.82	28	2.70	27	2.58	25	2.46	24	2.34	22
7 0.05 3.89 35 3.77 33 3.65 32 3.53 30 3.41 29 3.29 8 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 31 3.80 9 0.06 4.96 39 4.84 38 4.71 36 4.59 35 4.47 33 4.35 10 0.06 5.54 41 5.42 40 5.30 38 5.18 37 5.06 35 4.94 11 0.07 6.16 43 6.04 41 5.92 40 5.80 39 5.68 37 5.56 12 0.07 6.82 44 6.70 43 6.58 42 6.46 41 6.34 39 6.22 13 0.07 7.52 46 7.40 45 7.28 43 7.16 42 7.03 41 6.91 </td <td></td> <td>0.05</td> <td></td> <td></td> <td></td> <td></td> <td>l</td> <td></td> <td>l</td> <td></td> <td></td> <td></td> <td></td> <td></td>		0.05					l		l					
8 0.05 3.59 35 3.77 33 3.65 32 3.53 30 3.41 29 3.29 9 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 31 3.80 10 0.06 4.96 39 4.84 38 4.71 36 4.59 35 4.47 33 3.92 31 3.80 10 0.06 5.54 41 5.42 40 5.30 38 5.18 37 5.06 35 4.94 11 0.06 6.16 43 6.04 41 5.92 40 5.80 39 5.68 37 5.56 12 0.07 6.82 44 6.70 43 6.58 42 6.64 41 6.31 6.22 13 7.16 42 7.03 41 6.91 14 0.08 8.26 47 7.40 45		0.05	3.40	33	3.28	31	3.16	29	3.04	28	2.92	26	2.80	25
8 0.06 4.41 37 4.28 35 4.16 34 4.04 33 3.92 31 3.80 10 0.06 4.96 39 4.84 38 4.71 36 4.59 35 4.47 33 4.35 10 0.06 5.54 41 5.42 40 5.30 38 5.18 37 5.06 35 4.94 11 0.07 6.16 43 6.04 41 5.92 40 5.80 39 5.68 37 5.56 12 0.07 6.82 44 6.70 43 6.58 42 6.46 41 6.34 39 6.22 13 0.07 7.52 46 7.40 45 7.28 43 7.16 42 7.03 41 6.91 14 0.08 8.26 47 8.14 46 8.02 45 7.90 44 7.77 43 7.65			3.89	35	3.77	33	3.65	32	3.53	30	3.41	29	3.29	28
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			4.41	37	4.28	35	4.16	34	4.04	33	3.92	31	3.80	30
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			4.96	39	4.84	38	4.71	36	4.59	35	4.47	33	4.35	32
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10		5.54	41	5.42	40	5.30	38	5.18	37	5.06	35	4.94	34
12 0.07 6.82 44 6.70 43 6.58 42 6.46 41 6.34 39 6.22 13 0.07 7.52 46 7.40 45 7.28 43 7.16 42 7.03 41 6.91 14 0.08 8.26 47 8.14 46 8.02 45 7.90 44 7.77 43 7.65 15 0.08 9.05 49 8.92 48 8.80 46 8.68 45 8.56 44 8.44 0.08 10.76 52 10.63 50 10.51 49 10.39 48 10.27 47 10.14 18 0.10 11.69 53 11.56 51 11.44 50 11.32 49 11.20 48 11.07 19 0.11 12.67 54 12.55 53 12.42 51 12.30 50 12.18 49 12.06 <		0.06									j			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.07					l i			39	í			36
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ì	1				42	1	41		39	}	38
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			1				1	43		42		41		40
15 0.08 9.05 49 8.92 48 8.80 46 8.68 45 8.56 44 8.44 16 0.09 9.88 50 9.75 49 9.63 48 9.51 47 9.39 45 9.27 17 0.09 10.76 52 10.63 50 10.51 49 10.39 48 10.27 47 10.14 18 0.10 11.69 53 11.56 51 11.44 50 11.32 49 11.20 48 11.07 19 0.11 12.67 54 12.55 53 12.42 51 12.30 50 12.18 49 12.06 20 11 13.71 55 13.58 54 13.46 53 13.34 52 13.22 50 13.09 21 0.12 14.81 56 14.68 55 14.56 54 14.44 53 14.31 52 <td>1</td> <td></td> <td></td> <td>47</td> <td></td> <td>46</td> <td></td> <td>45</td> <td>7.90</td> <td>44</td> <td>7.77</td> <td>43</td> <td>7.65</td> <td>41</td>	1			47		46		45	7.90	44	7.77	43	7.65	41
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	15	-	9.05	49	8.92	48	8.80	46	8.68	45	8.56	44	8.44	43
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.08						- 1						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.09				1	1	- 1	- 1	- 6				44
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.09			1				1				1	46
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.10	ì					. 1		- 1		- 1		47
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.11							- 1					48
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20		13.71	55	13.58	54	13.46	53	13.34	52	13.22	50	13.09	49
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	91	0.11	1401		14.00		14.50			٠. ا	1401		14.10	-,
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.12												51
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.12				- 1	- 1	- 1	- 1					52 53
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.13										- 1		53
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	i	0.14	1		1	- 1	1	- 1		- 1				54
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.14	13.54	0.5	13.71	"	13.33	31	13.40	30	13.34	33	13.22	94
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	26		21.26	60	21.14	59	21.01	58	20.89	57	20.77	56	20.61	55
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														56
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								- 1		- 1			1	57
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			- 1				- 1	~ -			1			57
31	- 1	0.18				- 1		- 1		· 1	- 1	1		58
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.19		0.5		~		٠. ا		33		50		30
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	31		29,65	64	29.53	63	29.40	62	29.28	61	29.15	60	29.03	59
33 0.21 33.64 65 33.51 64 33.39 63 33.26 62 33.14 61 33.01									I	1				59
03.01 00 03.01 01 00.01 00 00.11 01 00.01	1	0.21			t	1								60
						* 1							30.01	
35	35	ļ	- 1			- 1				- 1		l		

		${f t}-{f t}'$, Difference of Wet and Dry-Bulb Thermometers.											
Wet- Bulb Thermo- meter. t'	Mean Vertical Differ-	ertical 7°.2		7°.4		7°.6		7°.8		8°.0		8°.2	
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
	Millim.	Millim.		Millim.		Millim	_	Millim.		Millim.		Millim.	
0	0.03	0.32	4	0.20	3	0.09	1						
1	0.03	0.66	8	0.54	7	0.42	5	0.30	4	0.18	2	0.06	1
2	0.04	1.01	12	0.89	10	0.77	9	0.65	7	0.53	6 9	$0.41 \\ 0.79$	8
3	0.04	1.39	15	1.27	13	1.15	12	1.03	11	0.91 1.31	13	1.19	11
4	0.04	1.79 2.22	18 21	1.67 2.10	16 19	1.55	15 18	1.43 1.86	14 17	1.74	16	1.62	14
5	0.05	2.23	21	2.10	19	1.95	10	1.00	14	1.75	10	1.02	14
6	0.05	2.78	24	2.66	23	2.44	21	2.32	20	2.20	18	2.08	17
7	0.05	3.16	26	3.04	25	2.92	24	2.80	22	2.68	21	2.56	20
8	0.05	3.68	29	3.56	27	3.44	26	3.32	25	3.20	24	3.08	22
9	0.06	4.23	31	4.11	30	3.99	28	3.87	27	3.75	26	3.63	25
10	0.06	4.82	33	4.70	32	4.57	30	4.45	29	4.33	28	4.21	27
	0.06												
11	0.00	5.44	35	5.32	34	5.19	32	5.07	31	4.95	30	4.83	29
12	0.07	6.09	37	5.97	36	5.85	34	5.73	33	5.61	32	5.49	31
13	0.07	6.79	39	6.67	37	6.55	36	6.43	35	6.31	34	6.18	33
14	0.08	7.53	40	7.41	39	7.29	38	7.17	37	7.04	36	6.92	35
15		8.31	42	8.19	41	8.07	40	7.95	39	7.83	37	7.71	36
	0.08			0.03				0		0.00	20	0.50	90
16	0.09	9.14	43	9.02	42	8.90	41	8.78	40 42	8.66 9.53	39 40	8.53 9.41	38 39
17	0.09	10.02	45	$9.90 \\ 10.83$	44	$9.78 \\ 10.71$	43	$9.66 \\ 10.58$	42	10.46	40	10.34	59 41
18 19	0.10	10.95 11.93	46 47	11.81	$\frac{45}{46}$	11.69	45	11.56	44	11.44	43	11.32	42
20	0.10	12.97	48	12.85	47	12.72	46	$\frac{11.50}{12.60}$	45	12.48	44	12.36	43
20	0.11	12.91	40	12.09	41	12.12	40	12.00	40	12.40	44	12.00	40
21	0.11	14.07	50	13.94	49	13.82	48	13.70	47	13.58	46	13.45	45
22	0.12	15.22	51	15 10	50	14.98	49	14.85	48	14.73	47	14.61	46
23	0.12	16.45	52	16.32	51	16.20	50	16.08	49	15.95	48	15.83	47
24	0.13	17.73	52	17.61	52	17.49	51	17.36	50	17.24	49	17.12	48
25	0.14	19.09	53	18.97	52	18.85	52	18.72	51	18.60	50	18.47	49
	0.14				i		ı						
26	0.15	20.52	54	20.39	53	20.27	52	20.14	51	20.02	51	19.90	50
27	0.15	22.03	55	21.90	54	21.78	53	21.65	52	21.53	51	21.41	51
28	0.17	23.61	55	23.49	54	23.36	53	23.24	53	23.11	52	22.99	51
29	0.18	25.29	56	25.16	55	25.04	54	24.91	54	24.79	53	24.66	52
30		27.05	57	26.92	56	26.80	55	26.67	55	26.55	54	26.42	53
31	0.19	28.90	58	28.78	57	28.65	56	28.53	55	28.40	55	28.27	54
31	0.20	30.85	58 59	30.72	57 58	30.60	57	30.47	56	30.35	56	20.21	94
33		90.09	99	50.72	90	50.00	31	90.47	50	50.55	50		
34				- 1									
35													
						<u> </u>		Sar each O	!	<u> </u>	!	·	

		$\mathbf{t}-\mathbf{t}'$, Difference of Wet and Dry-Bulb Thermometers.											
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	8°	.4	8 °.	6	8 °.	8	9 °.	0	9°.	2	90.	1
Centi- grade Degrees	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
° 0	Mıllim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1 2	0.04	0.30	3	0.18	2	0.06	1						_
3	1	0.67	7	0.55	5	0.43	4	0.31	3	0.19	2	0.08	1
4	0.04	1.07	10	0.95	9	0.83	8	0.72	6	0.60	5	0.48	-1
5	0.04	1.50	13	1.38	12	1.26	11	1.14	10	1.02	8	0.90	7
6	0.05	1.96	16	1.84	15	1.72	14	1.60	13	1.48	12	1.36	10
7	0.05	2.44	19	2.32	17	2.20	16	2.08	15	1.96	14	1.84	13
8	0.05	2.96	21	2.84	20	2.72	19	2.60	18	2.48	17	2.36	16
9	0.06	3.51	24	3.39	23	3.27	21	3.15	20	3.03	19	2.91	18
10	0.06	4.09	26	3.97	25	3.85	24	3.73	23	3.61	22	3.49	21
	0.06			1.50	27		26	4.35	25	4.23	24	4.11	23
11	0.07	4.71	28	4.59	27	4.47	28	5.00	27	4.88	26	4.76	25
12	0.07	5.37	30	5.25		5.12	30	5.70	29	5.58	28	5.46	27
13	0.07	6.06	32	5.94	31	5.82		6.44	31	6.31	30	6.19	29
14	0.08	6.80	34	6.68	33	6.56	32			7.10	32	6.97	31
15	0.08	7.58	35	7.46	34	7.34	33	7.22	33	1.10	32	0.97	31
16	0.03	8.41	37	8.29	36	8.17	35	8.05	34	7.92	33	7.80	32
17	0.09	9.29	39	9.17	38	9.04	37	8.92	36	8.80	35	8.68	34
18	0.09	10.22	40	10.09	39	9.97	38	9.85	37	9.73	36	9.60	35
19	0.10	11.20	41	11.07	40	10.95	39	10.83	39	10.71	38	10.58	37
20	0.11	12.23	43	12.11	42	11.99	41	11.87	40	11.74	39	11.62	38
ii	0.11	1		l		1		1					
21	0.12	13.33	44	13.21	43	13.08	42	12.96	41	12.84	40	12.71	40
22	0.12	14.48	45	14.36	44	14.24	43	14.12	42	13.99	41	13.87	41
23	0.12	15.71	46	15.58	45	15.46	44	15.34	43	15,21	42	15.09	42
24	0.14	16.99	47	16.87	46	16.75	45	16.62	44	16.50	44	16.37	43
25	0.14	18.35	48	18.22	47	18.10	46	17.98	45	17.86	45	17.73	44
26	0.14	19.77	49	19.65	48	19.52	47	19.40	46	19.27	46	19.15	45
27	0.15	21.28	50	21.16	49	21.03	48	20.91	47	20.78	47	20.66	46
28	0.16	21.28	51	$\frac{21.10}{22.74}$	50	22.61	49	22.49	48	22.36	47	22.24	47
29	0.17	24.54	51	21.41	51	24.29	50	24.16	49	24.04	48	23.91	47
30	0.18		1	26.17	51	26.05	51	25.92	50	25.80	49	25.67	48
30	0.19	26.30	1 32	20.17	31	20.05	"	20.02	"	1			
31	0.19	28.16	53	28.03	52	27.91	51	27.78	51				
32	1	23.10	"	1 -5.00	"	1	"			1		1	
33		1				1	1	1	-	1	1	}	
34	1	1	1	1		1		1		1	1	1	
35		1	1	1		1		-		1		1	
	1			1		'	1	•	-	1	-!	·	·

В

Wet-		${f t-t'}$, Difference of Wet and Dry-Bulb Thermometers.												
Bulb Thermo- meter. t' Centi- grade Degrees.	Mean Vertical Differ- ence for each 0° 1.	9°.6		9°.8		10°	10°.0		10°.2		10°.4		.6	
		Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	
0	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.		
1 2 3														
- 1 5	0.04	0.36 0.78	3 6	0.24 0.66	2 5	0.12 0.54	1 4	0.42	3	0.30	2	0.18	1	
6	0.05 0.05	1.24	9	1.12	8	1.00	7	0.88	6	0.76	5	0.64	5	
7 8 9	0.05 0.06	1.72 2.24 2.79	12 15 17	$ \begin{array}{c c} 1 & 60 \\ 2.12 \\ 2.66 \end{array} $	11 14 16	1.48 2.00 2.54	10 13 16	1.36 1.88 2.42	9 12 15	1.24 1.76 2.30	8 11 14	1.12 1.64 2.18	7 10 13	
10	0.06	3.37	20	3.25	19	3.13	18	3.00	17	2.88	16	2.76	15	
11 12 13	0.07 0.07	3.98 4.64 5.33	$\frac{22}{24}$	3.86 4.52 5.21	21 23 25	3.74 4.40 5.09	$\frac{20}{22}$	3.62 4.28 4.97	19 22 24	3.50 4.15 4.85	18 21 23	3.38 4.03 4.73	18 20 22	
14 15	0.07 0.08	6.07 6.85	28 30	5.95 6.73	25 27 29	5.83 6.61	26 28	5.71 6.49	25 27	5.58 6.37	25 26	5.46 6.24	24 26	
16	0.08	7.68	31	7.56	31	7.44	30	7.31	29	7.19	28	7.07	27	
17 18 19	0.09	8.56 9.48 10.46	33 35 36	8.43 9.36 10.34	32 34 35	8.31 9.24 10.22	31 33 34	9.11 10.09	31 32 33	8.07 8.99 9.97	30 31 33	7.94 8.87 9.85	29 30 32	
20	0.11	11.50	37	11.37	36	11.25	36	11.13	35	11.01	34	10.88	33	
$\frac{21}{22}$	0.12 0.12	12.59 13.75 14.96	39 40 41	12.47 13.62 14.84	38 39 40	12.35 13.50 14.72	37 38 39	12.22 13.38 14.59	36 37 39	12.10 13.25 14.47	35 37 38	11.98 13.13 14.35	35 36 37	
24 25	0.13 0.14	16.25 17.61	42 43	16.13 17.48	41 42	16.00 17.36	40 42	15.88 17.24	40 41	15.76 17.12	39 40 ¢	15.63 16.99	38 39	
26 27	0.14 0.15	19.02 20.54	44	18.90 20.41	43	18.78	42	18.65 20.16	42	18.53 20.04	41	18.40	40	
28 29	0.16 0.17	20.54 22.12 23.79	45 46 47	20.41 22.00 23.66	44 45 46	20.29 21.87 23.54	43 44 45	20.16 21.75 23.41	43 44 45	20.04 21.62 23.29	42 43 44	19.91 21.50 23.16	41 42 43	
30	0.18	25.55	48	25.42	47	25.30	46							
31 32 33														
34 35														

Mean Horizontal Difference of Force of Vapor for each 0°.1 \Longrightarrow 0.06 mm.

Wet-				t t	, Diffe	erence of	Wet a	nd Dry-Bi	ılb The	rmometer	s.		
Bulb Thermo- meter. t'	Mean Vertical Differ-	10	°.8	110	.0	110	.2	110	.4	110	.6	110	.8
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.
0 1 2 3 4 5	Millim.	Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
6 7 8 9 10	0.05 0.05 0.06 0.06	0.52 1.00 1.52 2.06 2.64	4 7 9 12 14	0.40 0.88 1.40 1.94 2.52	3 6 9 11 14	0.28 0.76 1.27 1.82 2.40	5 8 10 13	0.16 0.64 1.15 1.70 2.28	1 4 7 10 12	0.52 1.03 1.58 2.16	3 6 9 11	0.40 0.91 1.46 2.04	2 5 8 11
11 12 13 14 15	0.07 0.07 0.07 0.08	3.26, 3.91 4.61 5.34 6.12	17 19 21 23 25	3.14 3.79 4.49 5.22 6.00	16 18 20 22 24	3.02 3.67 4.36 5.10 5.88	15 17 19 21 23	2.90 3.55 4.24 4.98 5.76	14 17 19 21 22	2.77 3.43 4.12 4.86 5.63	14 16 18 20 22	2.65 3.31 4.00 4.73 5.51	13 15 17 19 21
16 17 18 19 20	0.09 0.09 0.10 0.10	6.95 7.82 8.75 9.73 10.76	27 28 29 31 33	6.83 7.70 8.63 9.60 10.64	26 27 29 30 32	6.70 7.58 8.50 9.48 10.51	25 27 28 30 31	6.58 7.46 8.38 9.36 10.39	24 26 27 29 30	6.46 7.33 8.26 9.24 10.27	23 25 27 28 30	6.34 7.21 8.14 9.11 10.15	22 24 26 28 29
21 22 23 24 25	0.12 0.12 0.13 0.14	11.85 13.01 14.22 15.51 16.87	34 35 36 38 39	11.73 12.88 14.10 15.39 16.74	33 34 36 37 38	11.61 12.76 13.98 15.27 16.62	32 34 35 36 37	11.48 12.64 13.85 15.15 16.49	32 33 34 35 36	11.36 12.51 13.73 15.02 16.37	31 32 34 35 36	11.24 12.39 13.61 14.90 16.24	30 32 33 34 35
26 27 28 29 30	0.15 0.16 0.17	18.28 19.79 21.37 23.04	39 40 41 42	18.16 19.67 21.25 22.91	39 40 41 42	18.03 19.54 21.12	38 39 40	17.91 19.42 21.00	37 38 39	17.78 19.29 20.87	37 38 39	17.66 19.17 20.75	36 37 38
31 32 33 34 35													

Mean Horizontal Difference of Force of Vapor for each $0^{\circ}.1 = 0.06$ mm.

				t — t	', Diffe	rence of	Wet an	d Dry-Bu	lb The	rmometer	3,		
Wet- Bulb Thermo- meter.	Mean Vertical Differ-	12	?° .0	12°	.2	12	.4	12°	.6	120	.8	13°	.0
Centi- grade Degrees.	ence for each 0°.1.	Force of Vapor.	Relative Humid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0	Millim.	Millim.		Millim.		Millim	_	Millim.		Millim.		Millim.	
12	0.07	3.19	14	3.06	14	2.94	13	2.82	12	2.70	12	2.58	11
13	0.07	3.88	16	3.76	16	3.64	15	3.51	14	3.39	14	3.27	13
14	0.01	4.61	18	4.49	18	4.37	17	4.25	16	4.13	16	4.00	15
15	0.08	5.39	20	5.27	20	5.15	19	5.03	18	4.90	18	4.78	17
16	0.00	6.22	22	6.09	21	5.97	21	5.85	20	5.73	19	5.61	19
	0.09			i			1	l		1			
17	0.09	7.09	24	6.97	23	6.84	22	6.72	22	6.60	21	6.48	21
18	0.10	8.01	25	7.89	25	7.77	24	7.65	23	7.52	23	7.40	22
19	0.10	8.99	27	8.87	26	8.74	26	8.62	25	8.50	25	8.38	24
20	0.10	10.02	28	10.90	28	9.78	27	9.65	26	9.53	26	9.41	25
21	0.11	11.12	30	10.99	29	10.87	28	10.75	28	10.62	27	10.50	27
	0.12												
22	0.12	12.27	31	12.14	30	12.02	30	11.90	29	11.77	28	11.65	28
23	0.13	13.48	32	13.36	31	13.23	31	13.11	30	12.99	29	12.86	29
24	0.14	14.78	33.	14.65	33	14.53	32	14.40	31	14.28	31	14.16	30
25	0.14	16.11	35	15.99	34	15.87	33	15.74	33	15.62	32	15.50	31
26		17.54	36	17.42	35	17.29	34	17.17	34	17.04	33	16.92	33
	0.15												٠.
27	0.16	19.04	37	18.92	36	18.80	35	18.67	35	18.55	34	18.42	34
28		20 63	_ 38							li			
		13	.∘2	13°.	4	13°.	.6	13°.	.8	14°.	0		
		Millim.		Millim.		Millim.		Millim.		Millim.		Millim.	
1.0	j	2,46	10	2.34	10	2.22	9	2.09	8	1.97	8		
12 13	0.07	$\frac{2.46}{3.15}$	$\frac{10}{12}$	3.03	10	2.22	11	2.79	8 11	$\frac{1.97}{2.66}$	10		
	0.07	3.88	14	3.76	14	3.64	13	3.52	13	3.40	12		
14 15	0.08	4.66	16	4.54	16	4.42	15	4.29	15	4.17	14		
16	0.08	5.48	18	5.36	18	5.24	17	5.12	16	5.00	16		
10	0.09	9.40	10	0.00	10	0.21	1.	0.12	10	0.00	10		
17		6.36	20	6.23	19	6.11	19	5.99	18	5.87	17		
18	0.09	7.28	22	7.16	21	7.03	20	6.91	20	6.79	19		
19	0.10	8.25	23	8.13	22	8.01	22	7.89	21	7.76	21		
20	0.10	9.29	25	9.16	24	9.04	23	8.92	23	8.80	22		
21	0.11	10.38	26	10.25	25	10.13	25	10.01	24	9.89	24		
- I	0.12												
22		11.53	27	11.40	27	11.28	26	11.16	26	11.03	25		
23	0.12	12.74	28	12.62	28	12.49	27	12.37	27	12.25	26		- 10
24	0.13	14.02	30	13.90	29	13.77	29	13.65	28	13.53	27		
25	0.14	15.37	31	15.25	30	15.12	30	15.00	29	14.88	29		
26	0.14	16.80	32	16.67	31	16.55	31	16.42	30	16.30	30		

Correction for the Barometrical Height.

Height below.	12° Milli.	13°	14°										
Add. Subtr'ct	Milli.		14°										
Wet-Bulb above the Freezing Point.			1										
		77.11.											
		37.11.											
Millim. Millim. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli. Milli.	0.00	Milli.	Milli.										
	- 1	0.00	0.00										
	0.05	0.05	0.06										
	0.10	0.10	0.11										
	0.14	0.16	0.17										
$oxed{\parallel 735 \mid 775 \mid 0.02 \mid 0.03 \mid 0.05 \mid 0.06 \mid 0.08 \mid 0.10 \mid 0.11 \mid 0.13 \mid 0.14 \mid 0.16 \mid 0.18 \mid 0$	0.19	0.21	0.22										
$\left\ \begin{array}{cccccccccccccccccccccccccccccccccccc$	001	0.00	0.00										
	$0.24 \\ 0.29$	$\begin{bmatrix} 0.26 \\ 0.31 \end{bmatrix}$	0.28										
	0.34	0.36	$0.34 \\ 0.39$										
	0.38	0.42	0.35										
	0.43	0.47	0.50										
1.0 600 610 6			0.00										
$oxed{1}{700}$ " $oxed{0.04}$ 0.09 0.13 0.18 0.22 0.26 0.31 0.35 0.40 0.44 0.48 0	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$												
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$												
670 " 0.07 0.14 0.20 0.27 0.34 0.41 0.48 0.54 0.61 0.68 0.75 0	0.82	0.88	0.95										
	0.91	0.99	1.06										
			į										
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1.01	1.09	1.18										
	1	1											
Wet-bulb below the													
Freezing Point.													
EXAMPLE OF CALCUI	LAT	ON.											
755 755 0.00 0.00 0.00 0.00 0.00 Wet-bulb above the Freezing	Point												
750 760 0.00 0.01 0.01 0.02			. (
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		710 ^{mn}	n.										
740 770 0.01 0.02 0.03 0.04 0.05 The tables give for mean bard	ometr		nm.										
735 775 0.01 0.03 0.04 0.06 0.07 height 755 m. Force of vapor Additive correction for 710 mm. at		. = 9	- 1.										
730 780 0.02 0.04 0.05 0.07 0.09	ma 85.	2 = 0	,.ა∪										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$. = 9	9.71										
$\begin{bmatrix} 725 & 785 & 0.02 & 0.04 & 0.08 & 0.01 \\ 720 & 790 & 0.02 & 0.05 & 0.07 & 0.10 & 0.12 \end{bmatrix}$													
			- 1										
The mean barometrical pressu	The mean barometrical pressure, at a given												
prace, being known, it is easy to	place, being known, it is easy to make the above Psychrometrical Tables fitted for that place, by												
690 " 0.05 0.09 0.14 0.18 0.23 correction, to be applied to the nu													
680 " 0.05 0.11 0.16 0.21 0.26 bles, giving the force of vapor.													
670													
660 " $0.07 \mid 0.13 \mid 0.20 \mid 0.27 \mid 0.33$ of thermometers, a mean value, the	he de	umere viation	e of										
which will have little influence upo													
650 " 0.07 0.15 0.22 0.29 0.36 of the results.													

III.

TABLE

GIVING AT SIGHT THE RELATIVE HUMIDITY DEDUCED FROM THE INDICA-TIONS OF THE DEW POINT INSTRUMENTS.

By M. T. HAEGHENS.

This table, which has been published in the Annuaire Météorologique de France for 1850, page 86, and following, has been calculated by Mr. Haeghens, using Regnault's Tables of Elastic Forces of Vapor. It gives directly the relative humidity, when the hygrometrical observations have been made by means of dew point instruments like those of Daniell, Regnault, Bache, and others.

These hygrometers are destined to find out the temperature of the dew point, that is the temperature to which it would be necessary to lower the temperature of the air, in order that this air be completely saturated by the aqueous vapor which it contained at the time of the observation.

The force of vapor contained in the air, or its absolute humidity, is thus the maximum of force of vapor which corresponds to the temperature of the dew point; it is given directly in the Table I. of the Elastic Forces of Vapor, by Regnault.

The ratio of that maximum of force of vapor at the temperature of the dew point to the force of vapor which corresponds, in the same table, to the temperature of the surrounding air at the time of the observation, is the *relative humidity*. This ratio is given in hundredths in the following table, which relieves the observer of the trouble of calculating it.

Let t = temperature of the air surrounding the instrument.

t' = temperature of the dew point.

t-t'= the difference between these two temperatures.

The first column, on the left, contains the temperature of the air t, in centigrade degrees. The following ones, headed with the differences, t-t', between the temperatures of the air and of the dew point, give the relative humidity corresponding to the two elements.

	Temp. of the Air $= t$.	Dew point $= t'$.	Difference $t-t'$.	Relative Humidity.
Example:	10°.0	4°.4	5°.6	68

Should the temperature of the air t', or the difference t-t', fall between the numbers found in the columns, it is obvious, by glancing at the table, that an interpolation at sight will always be easy.

Temper-	ure of														
the air.	0°.0	0°.2	0°.4	0°.6	0°.8	1°.0	1°.2	1°.4	1°.6	1°.8	2°.0	2°.2	2°.4	2°.6	2°.8
Centig.	100	98	97	95	94	92	90	89	88	86	85	83	82	80	79
-8 -7	100	98	97	95	94	92	91	89	88	86	85	83	82	81	79
-6	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-5	100	98	97	95	94	92	91	89	88	87	85	84	82	81	80
-3	100	30	31	33	34	32	31	09	00	01	0.0	04	02	01	
-4	100	98	97	95	94	92	91	89	88	87	85	84	83	81	80
-3	100	98	97	95	94	92	91	90	88	87	85	84	83	81	80
-2	100	98	97	95	94	93	91	90	88	87	86	84	83	82	80
-1	100	98	97	95	94	93	91	90	89	87	86	85	83	82	81
0	100	98	97	96	94	93	91	90	89	87	86	85	83	82	81
+1	100	99	97	96	95	93	92	90	89	88	86	85	84	83	81
2	100	99	97	96	95	93	92	91	89	88	87	85	84	83	82
3	100	99	97	96	95	93	92	91	89	88	87	86	84	83	82
4	100	99	97	96	95	93	92	91	89	88	87	86	85	83	82
5	100 99 97 96 95 93 92 91 90 88 87 86 85														82
6	100	99	97	96	95	93	92	91	90	88	87	86	85	84	82
7	100	99	97	96	95	93	92	91	90	89	87	86	85	84	83
8	100	99	97	96	95	93	92	91	90	89	87	86	85	84	83
9	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
10	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
11	100	99	97	96	95	94	92	91	90	89	87	86	85	84	83
12	100	99	97	96	95	94	92	91	90	89	88	87	85	84	83
13	100	99	97	96	95	94	92	91	90	89	88	87	85	84	83
14	100	99	98	96	95	94	93	91	90	89	88	87	86	84	83
15	100	99	98	96	95	94	93	91	90	89	88	87	86	84	83
16	100	99	98	96	95	94	93	91	90	89	ss	87	86	85	84
17	100	99	98	96	95	94	93	91	90	89	88	87	86	85	84
18	100	99	93	96	95	94	93	92	90	89	88	87	86	85	84
19	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
20	100	99	98	96	95	94	93	92	91	89	88	87	86	85	84
21	100	99	93	96	95	94	93	92	91	90	88	87	86	85	84
22	100	99	98	96	95	94	93	92	91	90	89	87	86	85	84
23	100	99	98	96	95	94	93	92	91	90	89	88	86	85	84
24	100	99	98	97	95	94	93	92	91	90	89	88	87	85	84
25	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
26	100	99	93	97	95	94	93	92	91	90	89	88	87	86	85
27	100	99	98	97	95	94	93	92	91	90	89	88	87	86	85
28	100	99	93	97	95	94	93	92	91	90	89	88	87	86	85
29	100	99	93	97	96	94	93	92	91	90	89	88	87	86	85
30	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
31	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
32	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
33	100	99	98	97	96	94	93	92	91	90	89	88	87	86	85
34	100	99	98	97	96	95	93	92	91	90	89	88	87	86	85
35	100	99	98	97	96	95	93	92	91	90	89	88	87	86	85
В							3	1							

Temper-	$\mathbf{t} - \mathbf{t}' = ext{Difference}$ of Temperatures of the Dew Point and of the Air.														
ature of tne air.	20.0	20.2	0.04	30 C	00.0	10.0	10 0	10 1	10 C	10.0	70 A	70 a	50.4	50.0	
t =	3°.0	3°.2	3.°4	3°.6	3°.8	4°.0	4°.2	4°.4	4°.6	4°.8	5°.0	5°.2	5°.4	5°.6	5°.8
Centig.	78	77	75	74	73	72	71	69	68	67	66	65	64	63	62
-7	78	77	75	74	73	72	71	69	68	67	66	65	64	63	62
-6	78	77	76	74	73	72	71	69	68	67	66	65	64	63	62
-5	79	77	76	75	73	72	71	70	68	67	66	65	64	63	62
-4	79	77	76	75	74	73	71	70	69	68	67	66	64	63	62
-3	79	77	76	75	74	73	72	70	69	68	67	66	65	64	63
-2	79	78	77	76	74	73	72	71	70	69	68	66	65	64	63
-1	79	78	77	76	75	73	72	71	70	69	68	67	66	65	64
0	80	7 8	77	76	75	74	73	71	70	69	68	67	66	65	64
+1	80	79	78	77	75	74	73	72	71	70	69	68	66	65	64
2	SI	79	78	77	76	7 5	74	72	71	70	69	68	67	66	65
3	81	80	7 8	77	76	75	74	73	72	71	70	69	68	66	65
4	81	80	79	78	77	7 5	74	73	72	71	70	69	68	67	66
5	SI	80	79	78	77	76	75	73	72	71	70	69	68	67	66
6	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
7	81	80	79	7 8	77	76	75	74	73	72	71	70	69	68	67
8	81	80	79	78	77	76	75	74	73	72	71	70	69	68	67
8	82	80	79	78	77	76	75	74	73	72	71	70	69	68	67
10	82	81	80	78	77	76	75	74	73	72	71	70	69	68	67
11	82	81	80	79	78	76	75	74	73	72	71	70	70	69	68
12	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
13	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
14	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
15	82	81	80	79	78	77	76	75	74	73	72	71	70	69	68
16	82	81	80	79	78	77	76	75	74	73	72	71	71	70	69
17	83	81	80	79	78	77	76	75	74	73	73	72	71	70	69
18	83	82	81	80	79	78	77	76	75	74	73	72	71	70	69
19	83	82	81	80	79	78 78	77	76 76	75 75	74	73 73	72 72	71 71	70 70	69
20	83	82	81		79			-	ł			1		1	
21	83	82	81	80	79	78	77	76	75	74	73	72	71	70	70
22	83	82	81	80	79	78	77	76	75	74	73	73	72	71	70
23	83	82	81	80	79	78 70	77	76	75	74	74	73	72	71	70 70
24 25	83 84	82 83	81 82	80	79 80	78 79	77	77	76 76	75 75	74 74	73 73	72 72	71 71	70
26	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
26 27	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
28	84	83	82	81	80	79	78	77	76	75	74	73	72	71	70
29	84	83	82	81	80	79	78	77	76	75	75	74	73	72	71
30	84	83	82	SI	so	79	78	77	76	76	75	74	73	72	71
31	84	83	82	81	80	79	78	77	77	76	75	74	73	72	71
32	84	83	82	81	80	79	79	78	77	76	75	74	73	72	72
33	84	83	82	81	80	80	79	7 S	77	76	75	74	73	72	72
34	85	84	83	82	81	80	79	78	77	76	75	74	74	73	72
35	85	84	83	82	81	80	79	78	77	76	75	75	74	73	72
В							3	2							

Centis	Teniper-			t	- t' =	Differe	nce of '	rempera	tures o	f the De	w Poin	t and of	the Air	,		
-S	the air.	6°0	6°.2	6°.4	6°.6	6°.8	7°.0	7°.2	7°.4	7°.6	7°.8	8°.0	8°.2	8°.4	8°.6	8°.8
	-															
-5 61 60 59 58 58 57 56 55 54 53 52																
-4 62 61 60 59 58 57 56 55 54 53 52 51 50 49 -2 62 61 60 60 59 58 57 56 55 54 53 53 52 51 50 49 -1 63 62 61 60 60 59 58 57 56 55 54 53 53 52 51 50 49 -1 63 62 61 60 59 58 57 56 55 54 53 53 52 51 50 49 -1 63 62 61 60 59 58 57 56 55 54 53 32 52 51 50 49 -1 63 62 61 60 59 58 57 56 55 54 53 33 52 51 50 49 -1 63 62 61 61 60 59 58 57 56 55 54 53 33 52 51 50 -1 63 62 61 61 60 59 58 57 56 55 54 53 33 52 51 50 -1 63 62 61 61 60 59 58 57 56 55 54 53 33 52 51 50 -1 64 63 62 61 61 60 59 58 57 56 55 54 53 53 53 52 51 -1 65 64 63 62 62 60 60 59 58 57 56 55 55 54 53 53 52 51 -1 66 66 65 64 63 62 62 60 60 59 58 57 56 55 55 54 53 53 52 51 -1 66 66 65 64 63 62 62 61 60 59 58 57 56 55 55 54 53 53 52 -1 65 64 63 62 62 62 61 60 59 58 57 56 55 55 54 53 53 52 -1 65 64 63 62 62 61 60 59 58 57 56 55 55 54 53 53 52 -1 65 64 63 62 62 61 60 59 58 57 56 55 55 54 53 53 52 -1 65 64 63 62 62 61 60 59 58 57 56 55 55 54 53 53 52 -1 66 66 65 64 63 62 61 60 59 58 57 56 55 55 54 53 53 52 -1 66 66 65 64 63 62 61 60 59 58 57 56 55 55 54 53 -1 66 65 64 63 62 61 60 59 58 57 56 55 55 54 53 -1 66 65 64 63 62 61 60 59 58 57 56 55 55 54 53 -1 66 65 64 63 62 61 60 59 58 57 56 55 55 54 -1 66 65 64 63 62 62 61 60 59 58 57 56 55 55 54 -1 66 65 64 63 62 61 60 59 58 57 56 55 55 54 -1 66 65 64 63 62 61 60 59 58 57 56 55 55 -1 65 66 65 64 63 62 61 60 59 58 57 56 55 55 -1 66 65 64 63 62 61 60 59 58 57 56 55 55 -1 66 66 65 64 64 63 62 61 60 59 58 58 57 56 55 -1 66 66 65 64 64 63 62 61 60 59 58 58 57 56 55 -1 65 66 65 64 63 62 61 60 60 59 58 58 57 56 55 -1 66 66 65 64 64 63 62 61 60 60 59 58 58 57 56 55 -1 60 60 60 60 60 60 60 60 60 60 60 60 60	-6	61	60			57	56								ĺ	
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28	48	48	47	-16	46	45	45	44	44	43	42	42	41	41	40
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34	50	49	49	48	47	47	46	46	45	41	41	43	43	42	42
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TABLE IV.

FACTOR $_{\mathbf{F}}^{100}$, FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR FROM ITS ABSOLUTE HUMIDITY, GIVEN IN MILLIMETRES.

BY HAEGHENS.

The Relative Humidity, or the degree of moisture of the air, is the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $f_{\rm F}^{\times 100} = {
m Relative~Humidity~in~Hundredths}.$

But as $\frac{f \times 100}{F} = f \times \frac{100}{F}$, it is obvious that the operation indicated by the former expression, viz. $\frac{f \times 100}{F}$, would be reduced to a simple multiplication, if we had a table of the factors $\frac{100}{F}$. Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients to the tensions.

The following Table, taken from the Annuaire Météorologique de la France, for 1850, p. 79, gives the factor $\frac{100}{F}$ for every tenth of a degree from -10 to $+35^{\circ}$ Centigrade, corresponding to the Forces of Vapor in Table I.

USE OF THE TABLE.

The force of vapor contained in the air being given in millimetres, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the *Relative Humidity in Hundredths*.

Examples.

- 1. Suppose the temperature of the air to be $=24^{\circ}$ Centigrade.
 - " force of vapor in the air to be = 10.76 millimetres.

Opposite 24° is found in the table the factor 4.51.

Then $10.76 \times 4.51 = 48.5$, Relative Humidity in Hundredths.

- 2. Suppose the temperature of the air to be = 16.7.
 - " force of vapor in the air to be = 12.07.

Table gives for 16.7 the factor 7.07.

Then $12.07 \times 7.07 = 85.3$, Relative Humidity.

В

factor $\frac{100}{F}$, to compute the relative humidity.

=					Tenths o	Degrees.				
ir, ig.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	48.1	48.5	48.9	49.3	49.7	50.1	50.5	50.9	51.4	51.8
	44.2	44.6	45.0	45.4	45.7	46.1	46.5	46.9	47.3	47.7
3	40.7	41.1	41.4	41.7	42.1	42.4	42.8	43.1	43.5	43.9
.	37.5	37.8	38.1	38.4	38.7	39.0	39.4	39.7	40.0	40.4
	34.6	34.9	35.2	35.4	35.7	36.0	36.3	36.6	36.9	37.2
	31.9	32.2	32.4	32.7	33.0	33.2	33.5	33.8	34.0	34.3
	29.5	29.8	30.0	30.2	30.5	30.7	31.0	31.2	31.4	31.7
ľ	27.3	27.5	27.7	27.9	28.2	28.4	28.6	28.8	29.1	29.3
	25.3	25.5	25.7	25.9	26.1	26.3	26.5	26.7	26.9	27.1
	23.4	23.6	23.8	24.2	24.0	24.3	24.5	24.7	24.9	25.1
	21.7	21.9	22.1	22.2	22.4	22.6	22.8	22.9	23.1	23.3
	21.7	21.6	21.4	21.3	21.1	21.0	20.8	20.7	20.5	20.4
	20.2	20.1	20.0	19.8	19.7	19.5	19.4	19.3	19.1	19.0
- 1	18.9	18.7	18.6	18.5	18.3	18.2	18.1	18.0	17.8	17.7
	17.6	17.5	17.3	17.2	17.1	17.0	16.9	16.7	16.6	16.5
	16.4	16.3	16.2	16.1	15.9	15.8	15.7	15.6	15.5	15.4
- ii	15.3	15.2	15.1	15.0	14.9	14.8	14.7	14.6	14.5	14.4
	14.3	14.2	14.1	14.0	13.9	13.8	13.7	13.6	13.5	13.4
	13.4	13.3	13.2	13.1	13.0	12.9	12.8	12.7	12.6	12.6
	12.5	12.4	12.3	12.2	12.1	12.1	12.0	11.9	11.8	11.7
	11.7	11.6	11.5	11.4	11.4	11.3	11.2	11.1	11.1	11.0
	10.9	10.8	10.8	10.7	10.6	10.6	10.5	10.4	10.3	10.3
H	10.2	10.1	10.1	10.0	9.95	9.88	9.82	9.75	9.69	9.6
	9.56	9.50	9.44	9.38	9.32	9.26	9.20	9.13	9.08	9.0
- 11	8.96	8.90	8.84	8.79	8.73	8.67	8.62	8.56	8.51	8.4
	8.40	8.34	8.29	8.24	8.18	8.15	8.08	8.03	7.98	7.9
	7.87	7.82	7.77	7.72	7.68	7.63	7.58	7.53	7.48	7.4
	7.39	7.34	7.29	7.25	7.20	7.16	7.11	7.07	7.02	6.9
	6.93	6.89	6.85	6.80	6.76	6.72	6.68	6.63	6.59	6.5
	6.51	6.47	6.43	6.39	6.35	6.31	6.27	6.23	6.19	6.1
	6.12 5.75	6.08 5.71	6.04 5.68	6.00 5.64	5.97 5.61	5.93 5.58	5.89 5.54	$\frac{5.86}{5.51}$	5.82 5.47	5.7 5.4
	5.41	5.37	5.34	5.31	5.27	5.24	5.21	5.18	5.15	5.1
	5.09	5.06	5.02	4.99	4.96	4.93	4.90	4.87	4.85	4.8
	4.79	4.76	4.73	4.70	4.67	4.65	4.62	4.59	4.56	4.5
- 11	4.51	4.48	4.45	4.43	4.40	4.37	4.35	4.32	4.30	4.2
	4.25	4.22	4.20	4.17	4.15	4.12	4.10	4.07	4.05	4.0
	4.00	3.98	3.95	3.93	3.91	3.89	3.86	3.84	3.82	3.7
- 11	3.77	3.75	3.73	3.71	3.69	3.66	3.64	3.62	3.60	3.5
	3.56	3.51	3.52	3.50	3.48	3.46	3.44	3.42	3.40	3.3
	3.36	3.34	3.32	3.30	3.28	3.26	3.24	3.22	3.21	3.1
	3.17	3.15	3.13	3.12	3.10	3.08	3.06	3.05	3.03	3.0
	2.99	2.98	2.96	2.94	2.93	2.91	2.89	2.88	2.86	2.8
	2.83	2.81	2.80	2.78	2.77	2.75	2.73	2.72	2.70	2.6
	2.67	2.66	2.64	2.63	2.61	2.60	2.58	2.57	2.56	2.5
	2.53	2.51	2.50	2.49	2.47	2.46	2.44	2.43	2.42	2.4
İ	2.39	2.38	2.36	2.35	2.34		2.31	2.30	2.29	2.2

TABLE V.

WEIGHT OF VAPOR, IN GRAMMES,

contained in a cubic metre of saturated air under a barometric pressure of 760 millimetres, and at temperatures between -20° and $+40^\circ$ centigrade.

The theoretic density of aqueous vapor is very nearly 0.622, or $\frac{5}{8}$, of the density of the air at the same temperature and pressure. Regnault's experiments gave similar results. From this ratio the weight of the vapor contained in a given volume of air, the temperature and humidity of which are known, can be computed.

If we call

t =the temperature of the air;

f = the elastic force of the vapor contained in the air at the time of the observation; F = the maximum elastic force of vapor due to the temperature t, as given in the

p = the weight of the vapor contained in a litre of air at the temperature t, and with a force of vapor f;

P = the weight of vapor in a litre of air at the temperature t, and at full saturation, or F.

Then, $p = 0.622 \frac{1.293223^{\text{gr.}}}{1 + 0.00367t} \cdot \frac{f}{760^{\text{unn.}}}.$

In which 1.293223 grammes is the weight of a litre of dry air, at the temperature of zero Centigrade, and under a barometric pressure of 760 millimetres, according to the determination of Regnault; 0.00367, the coefficient of the expansion of the air as found by the same; 760 millimetres, the assumed normal barometric pressure.

The weight of a litre of air given by Regnault in the *Mémoires de l'Institut*, Tom. XXI. p. 157, is 1.293187 grammes; but by correcting a slight error of computation (see E. Ritter, *Mémoires de la Société Physique de Genève*, Tom. XIII. p. 361), it becomes, as given above, 1.293223 grammes.

In order to obtain the weight of vapor in a cubic metre, or 1000 litres, of saturated air, the formula becomes,

$$P = 0.622 \, \frac{1293.223^{\mathrm{gr.}}}{1 + 0.00367 \, t} \cdot \frac{F}{760^{\mathrm{mm.}}}$$

From this formula Table V, has been computed. The tensions due to the temperatures in the first column are placed opposite the weights of vapor; they are taken from Table I. It will be seen that, throughout the table, the number of grammes of vapor nearly corresponds to the number of millimetres of pressure expressing the tension.

The table of the weights of vapor given in Pouillet's Eléments des Physique, Tom. II. p. 707, being based on older values, gives results somewhat different. In that published by Becquerel, Eléments de Physique Terrestre, p. 354, Regnault's tensions and coefficient of expansion of the air have been used, but the value of the weight of vapor in a litre of air formerly determined by Biot and Arago, viz. 1.29954 grammes, has been retained.

В

V. WEIGHT OF VAPOR, IN GRAMMES,

CONTAINED IN A CUBIC METRE OF SATURATED AIR,

At Temperatures between —200 and $+\,400\,$ Centigrade.

Temperature	Force	Weight	Difference.	Temperature of	Force	Weight	Difference.
of Dew-Point.	of Vapor.	Vapor.	Difference.	Dew-Point.	of Vapor.	of Vapor.	Difference.
Centigrade.	Millimetres.	Grammes.	Grammes.	Centigrade.	Millimetres.	Grammes.	Grammes.
-20°	0.912	1.042	0.088	+10°	9.165	9.357	0.605
-19	0.993	1.130	0.094	11	9.792	9.962	0.639
-18	1.080	1.224	0.094	12	10.457	10.601	0.675
-17	1.174	1.325	0.109	13	11.162	11.276	0.712
-16	1.275	1.434	0.103	14	11.908	11.988	0.112
3.5	1 207	1 551	0.118	1.	10.000	10 200	0.751
-15	1.385	1.551	0.127	15	12.699	12.739	0.793
-14	1.503	1.678	0.134	16	13.536	13.532	0.835
-13	1.631	1.813	0.145	17	14.421	14.367	0.880
-12	1.768	1.957	0.157	18	15.357	15.247	0.926
-11	1.918	2.114		19	16.346	16.173	
-10	2.078	2.283	0.169	20	17.391	17.148	0.975
- 9	2.261	2.475	0.192	21	18.495	18.174	1.026
- 8	2.456	2.678	0.203	22	19.659	19.253	1.078
- 7	2.666	2.896	0.218	23	20.888	20.387	1.134
- 1 - 6	2.890	3.128	0.232	24	22.184	21.579	1.192
- 0	2.030	5.120			22.104	21.013	
- 5	3.131	3.376	0.248	25	23.550	22.831	1.252
- 4	3.387	3.638	0.262	26	24.988	24.144	1.313
- 3	3.662	3.919	0.281	27	26.505	25.524	1.380
- 2	3.955	4.217	0.298	28	28.101	26.971	1.447
- 1	4.267	4.534	0.317	29	29.782	28.489	1.519
			0.334				1.589
0	4.600	4.869	0.334	30	31.548	30.079	1.666
+ 1	4.940	5.209	0.341	31	33.405	31.744	1.747
2	5.302	5.571	0.361	32	35.359	33.491	1.827
3	5.687	5.953	0.383	33	37.410	35.317	1.913
4	6.097	6.360	0.406	34	39.565	37.230	1.913
_	0 =0 :	0.101	0.431			00.000	2.001
5	6.534	6.791	0.456	35	41.827	39.231	2.092
6	6.998	7.247	0.484	36	44.201	41.323	2.187
7	7.492	7.731	0.512	37	46.691	43.510	2.285
8	8.017	8.243	0.541	38	49.302	45.795	2.387
9	8.574	8.785	0.572	39	52.039	48.182	2.492
+10	9.165	9.357		+40	54.906	50.674	



PRACTICAL TABLES,

IN

ENGLISH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

VI.

TABLE OF THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, REDUCED FROM REGNAULT'S TABLE.

The values of the elastic force of vapor furnished by V. Regnault, which are found in Table 1. of this Hygrometrical set, are derived from a series of experiments conducted, during several years, with great care, consummate skill, and all the means of precision which are at the disposal of modern science. The methods of investigation, and all the steps in each experiment, were minutely described and submitted to the judgment of the scientific, successively in separate papers in several volumes of the Annales de Chimie et de Physique, and collectively in his final Report to the Minister of Public Works, (see above, p. 9,) which fills Volume XXI. of the Mémoires de l'Institut de France. The confidence which has been deservedly granted to these determinations by nearly all scientific men, is increased by the fact that one of the best physicists and experimenters in Germany, Professor Magnus, came, about the same time, to results so little different, that both tables, for most purposes, may be considered identical. (Compare below, Table XXII.) It seems, therefore, that these values ought to be used in our hygrometrical tables, as has been done in France, in preference to the older and less reliable determinations on which they are based.

Though Regnault's table of the elastic force of vapor is considered, even, it is believed, by a majority of scientific men in England, as the most reliable which science now possesses, the author is not aware that any extensive reduction of it to English measures, such as is wanted for meteorological purposes, has been as yet published; still less a series of tables based on these values. Such a set of hygrometrical tables in English measures, corresponding to the preceding one in French measures, is offered here, which, it is hoped, supplies a real want felt by a large number of meteorologists.

Table VI. is Regnault's Table of the Elastic Force of Vapor as given in Table I., reduced to English measures, in which the fourth decimal is given in order to secure the third, and otherwise to facilitate the computations. From these values Tables VII. to X. have been computed.

VI. ELASTIC FORCE OF AQUEOUS VAPOR,

Expressed in English Inches of Mercury for Temperatures of Fahrenheit.

REDUCED FROM REGNAULT'S TABLE.

	Force of	Vapor.		Force of	f Vapor.			Fore	e of V	apor.		Force o	f Vapor.
Temper- ature Fahren- heit.	Fenths of	Degrees.	Temper- ature Fahren- heit.	Tenths of	f Degrees	. atı Fah	pe r- ire ren- it.		s of I	egrees.	Temper- ature Fahren- heit.	Tenthso	f Degrees.
	0	0.5		0	0.5			0		0.5		0	0.5
	Eng. In.	Eng. In.		Eng. In.	Eng. In	.		Eng.	In. E	ng. In.		Eng. In.	Eng. In.
-31	0.0057	0.0085	-19	0.0171	0.016	7 -	8	0.02	97 (0.0290	+ 2	0.0476	1
-30	0.0092	0.0090	- 1S	0.0181	0.0176	3 -	7	0.03	312	0.0304	3	0.0498	0.0510
-29	0.0098	0.0095	-17	0.0190	0.018	5∥ -	6	0.03	327 (0.0319	4	0.0521	1
-28	0.0104	0.0101	-16	0.0200	0.019	5∥ -	5	0.03	343 (0.0335	5	0.0545	0.0558
-27	0.0110	0.0107	-15	0.0210	0.0203	5 -	4	0.03	359 (0.0351	6	0.0570	
-26	0.0117	0.0114	-14	0.0221	0.0216	5 -	3	0.03	376	0.0368	7	0.0597	0.0611
-25	0.0124	0.0120	-13	0.0232	0.022	7 -	2	0.03	95 (0.0386	8	0.0625	0.0639
-24	0.0131	0.0127	-12	0.0244	0.0238	3 -	1	0.0	1	0.0404	9	0.0654	1
-23	0.0138	0.0135	-11	0.0257	0.0250) -	0	0.04	34	0.0424	10	0.0684	
· - 22	0.0146	0.0142	-10	0.0270	0.026	3 +	0	0.04	134 (0.0444	11	0.0716	0.0732
-21	0.0154	0.0150	- 9	0.0283	0.027	6 +	1	0.04	154 (0.0465	12	0.0749	
-20	0.0163	0.0158	- 8	0.0297	0.0290	+ 0	2	0.04	176 (0.0487	+13	0.0783	0.0800
Temper- ature Fahren-					Те	nths of	Deg	rees.					
heit.	0.	1.	2.	3		4.		5.	G		7.	8.	9.
0	Eng. In.	Eng. In	n. Eng. I	n. Eng.	In. Er	ıg. In.	Eng	g. In.	Eng.	In. E	ng. In.	Eng. In.	Eng. In.
14	0.0818	0.082	2 0.082	26 0.08	530 0.	0834	0.0	837	0.0	841 0	.0845	0.0849	0.0853
15	0.0857	0.086	$1 \mid 0.086$	$65 \mid 0.08$	369 O	0873	0.0	877	0.0	$ssi \mid 0$.0885	0.0889	0.0893
16	0.0898	0.090	$2 \mid 0.090$	0.09	910 0.	0914	0.0	918	0.0	923 0	.0927	0.0931	0.0936
17	0.0940	0.094	4 0.094	9 0.09	953 0.	0958	0.0	962	0.0	967 0	.0971	0.0975	0.0980
18	0.0984	0.098	9 0.099	3 0.09	99S 0.	1002	0.1	007	0.1	012 0	.1016	0.1021	0.1025
19	0.1030	0.103	5 0.104	0.10	0.44	1049	0.1	054	0.10	059 0	.1064	0.1068	0.1073
20	0.1078	0.108	3 0.108	88 0.10	093 0.	1098	0.1	103	0.1	108 0	.1113	0.1118	0.1123
21	0.1128	0.113	3 0.113	8 0.11	$143 \mid 0.$	1148	0.1	153	0.1	159 0	.1164	0.1169	0.1174
22	0.1179	0.118	5 0.119	0 0.11	195 0.	1200	0.1	206	0.13	211 0	.1217	0.1222	0.1227
23	0.1233	0.1238	8 0.124	4 0.12	249 0.	1255	0.1	260	0.13	266 0	.1272	0.1277	0.1283
24	0.1289	0.129	5 0.130	1	1	1312	0.1	318	0.1	324 0	.1329	0.1335	0.1341
25	0.1347	0.135	3 0.135	69 0.13	36 5 0.	1371	0.1	377	0.13	383 0	.1389	0.1395	0.1401
26	0.1407	0.141	3 0.141	9 0.1	126 0.	1432	0.1	438	0.1	444 0	.1450	0.1457	0.1463
27	0.1469		1			1495		501	0.1		.1514	0.1521	0.1527
28	0.1534			- 1		1560		567	0.1	- 1	.1580	0.1587	0.1593
29	0.1600					1627		634	0.1		.1647	0.1654	0.1661
30	0.1668	1				1696		703	0.1		.1717	0.1724	0.1732
31	0.1739					1767		775	0.1		.1789	0.1796	0.1804
	0.	1.	2.	3		4.	- 7	5.	6	.	7.	8.	9.

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

rempera-					Tenths o	f Degrees.				
ture of Fahren- heit.	0.	I.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. I
32	0.1811	0.1818	0.1825	0.1833	0.1840	0.1847	0.1854	0.1861	0.1869	0.187
33	0.1883	0.1891	0.1898	0.1906	0.1913	0.1921	0.1928	0.1936	0.1944	0.195
34	0.1959	0.1967	0.1974	0.1982	0.1990	0.1998	0.2006	0.2013	0.2021	0.202
35	0.2037	0.2045	0.2053	0.2061	0.2070	0.2077	0.2086	0.2094	0.2102	0.211
36	0.2119	0.2127	0.2135	0.2144	0.2152	0.2161	0.2169	0.2178	0.2186	0.219
37	0.2204	0.2212	0.2221	0.2230	0.2238	0.2247	0.2256	0.2265	0.2273	0.228
38	0.2291	0.2300	0.2309	0.2318	0.2327	0.2336	0.2345	0.2354	0.2364	0.237
39	0.2382	0.2391	0.2400	0.2410	0.2419	0.2428	0.2438	0.2447	0.2457	0.246
40	0.2476	0.2485	0.2495	0.2504	0.2514	0.2524	0.2533	0.2543	0.2553	0.256
41	0.2572	0.2582	0.2592	0.2602	0.2612	0.2622	0.2632	0.2642	0.2652	0.266
42	0.2672	0.2682	0.2692	0.2702	0.2713	0.2723	0.2733	0.2744	0.2754	0.276
43	0.2775	0.2785	0.2796	0.2807	0.2817	0.2828	0.2839	0.2850	0.2860	0.287
44	0.2882	0.2893	0.2904	0.2915	0.2926	0.2937	0.2948	0.2960	0.2971	0.298
45	0.2993	0.3005	0.3016	0.3028	0.3039	0.3050	0.3062	0.3074	0.3085	0.309
46	0.3108	0.3120	0.3132	0.3144	0.3156	0.3168	0.3179	0.3191	0.3203	0.321
47	0.3228	0.3240	0.3252	0.3264	0.3276	0.3289	0.3301	0.3313	0.3326	0.333
48	0.3351	0.3363	0.3376	0.3388	0.3401	0.3414	0.3426	0.3439	0.3452	0.346
49	0.3477	0.3490	0.3503	0.3516	0.3529	0.3542	0.3556	0.3569	0.3582	0.359
50	0.3608	0.3622	0.3635	0.3648	0.3661	0.3675	0.3688	0.3702	0.3715	0.372
51	0.3743	0.3756	0.3770	0.3784	0.3798	0.3812	0.3826	0.3840	0.3854	0.386
52	0.3882	0.3896	0.3911	0.3925	0.3939	0.3954	0.3968	0.3983	0.3997	0.401
53	0.4027	0.4041	0.4056	0.4071	0.4086	0.4101	0.4116	0.4131	0.4146	0.416
51	0.4176	0.4191	0.4207	0.4222	0.4237	0.4253	0.4268	0.4284	0.4299	0.431
55	0.4331	0.4346	0.4362	0.4378	0.4394	0.4410	0.4426	0.4442	0.4458	0.447
56	0.4490	0.4507	0.4523	0.4539	0.4556	0.4572	0.4589	0.4605	0.4622	0.468
57	0.4655	0.4672	0.4689	0.4705	0.4722	0.4739	0.4756	0.4773	0.4791	0.480
58	0.4825	0.4842	0.4859	0.4876	0.4894	0.4912	0.4929	0.4947	0.4964	0.498
59	0.5000	0.5017	0.5035	0.5053	0.5071	0.5089	0.5107	0.5125	0.5143	0.516
60	0.5179	0.5198	0.5216	0.5234	0.5253	0.5271	0.5290	0.5301	0.5328	0.534
61	0.5365	0.5384	0.5403	0.5422	0.5441	0.5461	0.5480	0.5499	0.5519	0.553
62	0.5558		0.5597	0.5617	0.5636	0.5656	0.5676	0.5696		
63	0.5756	0.5777	0.5797	0.5817	0.5838	0.5858	0.5879	0.5899	0.5920	0.594
64	0.5962	0.5983	0.6004	0.6025	0.6046	0.6067	0.6088	0.6109	0.6131	0.615
65	0.6173	0.6195	0.6217	0.6238	0.6260	0.6282	0.6304	0.6325	0.6347	0.636
66	0.6392	0.6414	0.6436	0.6458	0.6481	0.6503	0.6525	0.6548	0 6571	0.659
67	0.6616	0.6639	0.6662	0.6685	0.6708	0.6731	0.6754	0.6777	0.6800	0.682
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Expressed in English Inches of Mercury for Temperatures of Fahrenheit.

empera-					Tenths of	Degrees.				
ture of Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In. 0.6989	Eng. In. 0.7012	Eng. In. 0.7036	Eng. In
68	0.6847	0.6870	0.6894	0.6917	0.6941	0.6965		0.7012 0.7255	0.7030	0.7308
69	$0.7084 \\ 0.7329$	0.7108 0.7354	0.7133 0.7379	0.7157	0.7181 0.7430	0.7206 0.7455	$0.7230 \\ 0.7480$	0.7506	0.7531	0.7557
70	0.7583	0.7609	0.7634	0.7405 0.7660	0.7486	0.7455	0.7430	0.7765	0.7791	0.7818
$\frac{71}{72}$	0.7844	0.7871	0.7897	0.7924	0.7951	0.7978	0.8005	0.8032	0.8059	0.8086
7 3	0.8113	0.8141	0.8168	0.8196	0.8223	0.8251	0.8279	0.8307	0.8335	0.836
74	0.8391	0.8419	0.8447	0.8476	0.8504	0.8533	0.8561	0.8590	0.8619	0.864
75	0.8676	0.8705	0.8735	0.8764	0.8793	0.8822	0.8852	0.8881	0.8911	0.894
7 6	0.8970	0.9000	0.9030	0.9060	0.9090	0.9120	0.9150	0.9180	0.9211	0.924
77	0.9272	0.9302	0.9333	0.9364	0.9395	0.9426	0.9457	0.9488	0.9519	0.955
7 8	0.9582	0.9613	0.9645	0.9677	0.9709	0.9740	0.9773	0.9805	0.9837	0.986
7 9	0.9902	0.9934	0.9967	1.0000	1.0033	1.0065	1.0099	1.0132	1.0165	1.019
80	1.0232	1.0265	1.0299	1.0332	1.0366	1.0400	1.0434	1.0468	1.0503	1.053
81	1.0572	1.0606	1.0641	1.0675	1.0710	1.0745	1.0780	1.0815	1.0851	1.088
82	1.0922	1.0957	1.0993	1.1028	1.1064	1.1100	1.1136	1.1172	1.1209	1.124
83	1.1281	1.1318	1.1354	1.1391	1.1428	1.1465	1.1502	1.1539	1.1576	1.161
84	1.1651	1.1689	1.1726	1.1764	1.1802	1.1840	1.1878	1.1916	1.1954	1.199
85	1.2031	1.2070	1.2108	1.2147	1.2186	1.2225	1.2264	1.2303	1.2342	į.
86	1.2421	1.2460	1.2500	1.2540	1.2580	1.2620	1.2660	1.2700	1.2740	1.278 1.319
87	1.2821	1.2862	1.2903	1.2944	1.2985	1.3026	1.3068	1.3109	1.3151	1.515
88	1.3234	1.3276	1.3318	1.3361	1.3403	1.3445	1.3488	1.3531	1.3573	1.361
89	1.3659	1.3703	1.3746	1.3789	1.3833	1.3877	1.3920	1.3964	1.4008	1.405
90	1.4097	1.4141	1.4186	1.4230	1.4275	1.4320	1.4365	1.4410	1.4456	1.450
91	1.4546	1.4592	1.4638	1.4684	1.4730	1.4776	1.4822	1.4869	1.4915	1.496
92	1.5008	1.5055	1.5102	1.5149	1.5197	1.5244	1.5291	1.5339	1.5387	1.548
00	1 5400	1 5501	1 ===0	1 5005	1.5000	1 500	1 5770	1 5000	1.5871	1.592
93	1.5482 1.5969	1.5531	1.5579	1.5627	1.5676	1.5724	1.5773	1.5822	1.6367	1.641
94		1.6018	1.6068	1.6117	1.6167	1.6217	1.6267	1.6317 1.6825	1.6876	1.692
95 96	1.6468 1.6980	1.6518 1.7032	1.6569	1.6620	1.6671	1.6722	1.6773 1.7295	1.6823	1.7401	1.745
90 97	1.7508	1.7561	1.7615	1.7137 1.7669	1.7189	1.7242 1.7777	1.7831	1.7886	1.7940	1.799
98	1.8050	1.8105	1.8160	1.7003	1.8271	1.8327	1.8382	1.8438	1.8494	1.85
99	1.8607	1.8664	1.8720	1.8777	1.8834	1.8891	1.8949	1.9006	1.9064	1.912
100	1.9179	1.9237	1.9295	1.9354	1.9412	1.9471	1.9530	1.9589	1.9648	1.970
101	1.9766	1.9826	1.9885	1.9945	2.0005	2.0065	2.0126	2.0186	2.0247	2.030
102	2.0368	2.0429	2.0490	1	2.0613	2.0675	2.0737	2.0798	2.0861	2.092
103	2.0985	2.1048	2.1110		2.1236	2.1299	2.1362	2.1426	2.1489	2.15
104	2.1617	2.1681	2.1745	2.1810	2.1874	2.1939	2.2004	2.2069	2.2135	2.220
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

VII.

PSYCHROMETRICAL TABLES,

GIVING, IN ENGLISH INCHES OF MERCURY, THE ELASTIC FORCE OF VAPOR CONTAINED

1N THE AIR, AND ITS RELATIVE HUMIDITY IN HUNDREDTHS;

DERIVED FROM THE INDICATIONS OF THE WET AND DRY BULB THERMOMETERS,

IN DEGREES OF FAHRENHEIT.

By A. Guyot.*

M. V. Regnault, in his Etudes sur l'Hygrométrie Annales de Chimie et de Physique, 3^{me} série, Tom. XV. p. 129, after having discussed the theoretical bases of the psychrometric formula given by August, and modified the numerical values of some of its coefficients, adopts the formula

$$x = f - \frac{0.480 (t - t')}{610 - t'} h$$

for temperatures above the freezing-point; and when the temperature of the wet thermometer is below the freezing-point, the bulb being covered with a film of ice,

$$x = f - \frac{0.480 (t - t')}{689 - t'} h,$$

В

^{*} While this table was going through the press, a similar one, prepared by Prof. T. H. Coffin for his private use, was published by the Smithsonian Institution, in order to meet an urgent demand from many quarters. Being based on the same formula, it gives the same results, except, perhaps, in degrees below 14° Fahrenheit, where the tables show slight discrepancies. These unimportant differences arise from the fact that Prof. Coffin's table was computed from Regnault's tensions, as given in the first edition of this collection, while the author's table is based on the table of tensions as given in this second edition, in which the values below 14° Fahrenheit have been somewhat modified, for reasons given above. The following table gives also the relative humidity with one more decimal, which makes the interpolations more easy; and a column of differences for finding the values for fractions of t'. A table for reducing the results to another barometric height is added at the end of the table.

in which

x represents the force of vapor in the air at the time of the observation;

t, the temperature of the air in Centigrade degrees, indicated by the dry thermometer;

t', the temperature of evaporation given by the wet thermometer;

f, the force of vapor in a saturated air at the temperature t';

h, the height of the barometer.

Substituting the Fahrenheit scale for the Centigrade, the formula, for temperatures above the freezing-point, reads

$$x = f - \frac{0.480 \times \frac{5}{9} (t - t')}{610 - \frac{5}{9} (t' - 32^{\circ})} h = f - \frac{0.480 (t - t')}{1130 - t'} h;$$

and below the freezing-point,

$$x = f - \frac{0.480 \times \frac{5}{9} (t - t')}{689 - \frac{5}{9} (t' - 32^{\circ})} h = f - \frac{0.480 (t - t')}{1240.2 - t'} h.$$

Making, further, h = 29.7 English inches, these formulæ become

$$x = f - \frac{0.480 (t - t')}{1130 - t'} 29.7 = f - \frac{14.256 (t - t')}{1130 - t'},$$

and

$$x = f - \frac{0.480 (t - t')}{1240.2 - t'} 29.7 = f - \frac{14.256 (t - t')}{1240.2 - t'}$$

The mean barometric pressure for which the table has been computed, viz. 29.7 inches, is, within a small fraction, the same as that adopted in Haeghens's Tables, No. II., which is 755 millimetres = 29.725 Eng. inches. As that slight difference in the barometric pressure cannot cause, in the most extreme cases, a difference exceeding two thousandths of an inch in the elastic forces, the results in the two tables may be considered identical.

That barometric pressure, corresponding, in our latitudes, to a mean altitude of 250 to 300 feet above the sea, is likely to suit, without correction, the largest number of meteorological stations. Should the mean height of the barometer, in consequence of the elevation of the station, much differ from that adopted in the table, a constant correction can be determined, to be applied to the numbers in the table. At the end, page 72, will be found a table which furnishes that correction for barometric heights between 20 and 31 inches, and for values of t - t' between 2° and 26° Fahrenheit.

The effect of the irregular variations of the barometer at the same station can, in most cases, be neglected; for the error due to that cause will scarcely ever exceed those which may arise from the uncertainty of the very elements on which the tables are based.

ARRANGEMENT OF THE TABLES.

The same arrangement as is found in the Psychrometrical for the Centigrade scale has been adopted.

The first column at the left contains the indications of the wet-bulb thermometer, from -31° to 105° Fahrenheit.

The second column gives the differences of the force of vapor for each tenth of a degree, between each two consecutive full degrees in the first column. It enables the observer easily to find the values for the fractions of degrees of the wet thermometer.

The following double columns furnish the forces of vapor and the relative humidity corresponding to each full degree of the wet-bulb thermometer given in the first column in the same horizontal line, and to the difference of the two thermometers, or t-t', found at the head of each column, for every half-degree from 0° to 26°.5. The relative humidity, or the fraction of saturation, is given in hundredths, which is near enough for meteorological purposes; but one decimal more has been added, though separated by a point, in order to facilitate the interpolations.

At the bottom of each page is found the mean difference, for each tenth of a degree, between the forces of vapor on the same line. It gives the means of finding the values for the intermediate differences of t - t', not found in the tables.

Use of the Tables.

Enter the tables with the difference of the two thermometers, or t-t', and the temperature of the wet-bulb thermometer, given by observation.

In the column headed by the observed difference of the thermometer, t-t', and on the horizontal line headed by the observed temperature of the wet thermometer, t', are found the force of vapor, and the relative humidity corresponding to these temperatures.

For the fractions of degrees of the wet thermometer, multiply the decimal fraction by the number placed in the second column between the full degree and the next, and add the product if the temperature is above, and subtract it if it is below zero Fahrenheit.

The intermediate values of t-t' not given in the table are found by *subtracting* the number in the line at the bottom of the page, multiplied by the number of additional tenths, from the value given in the table. This correction, being always very small, can usually be neglected.

For the relative humidity, interpolations at sight will generally suffice.

Examples.

Dry thermometer, $t = 50^{\circ}$ F. Wet thermometer, $t' = 43^{\circ}$ F. Difference, or $t - t' = 7^{\circ}$ F.

Page 58, we find for $t-t'=7^{\circ}$ in the third double column, and for $t'=43^{\circ}$ in the first column

Force of vapor in the air = 0.186 inch. Relative humidity in hundredths = 51

2. Dry thermometer, $t = 88^{\circ}.5$ F. Wet thermometer, $t' = 76^{\circ}.3$ F.

Difference, $t-t'=12^{\circ}.2$ F.

Page 63, Table gives for t - t' = 12 and $t' = 76^{\circ}$ = 0.735 inch.

Add for fraction of t' = 0.3, $0.003 \times 3 = 0.009$

Subtract for fraction of $t - t' = 0^{\circ}.2$, $.0013 \times 2 = -0.003$

Force of vapor in the air = 0.741 Relative humidity = 55

3. Dry thermometer, $t = -4^{\circ}.5 \text{ F.}$

Wet thermometer, $t' = 6^{\circ}.0 \text{ F}.$

Difference, $t - t' = 1^{\circ}.5 \text{ F.}$

Page 50, Table gives for $t-t'=1^{\circ}.5$ and $t'=-6^{\circ}=0.016$ inch.

Subtract for fraction of t' = 0.5, $0.0002 \times 5 = -0.001$ Force of vapor in the air = 0.015

Relative humidity = 45

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredths.

								and Dry				e.	
Wet- Bulb Thermo- meter	of Force		.0	00	.5	10	.0	1°	.5	2°	.0	20	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force o Vapor.	
0		Eng. In.		Eng. In	20.0	Eng. In.		Eng. In.		Eng. In		Eng. In	
-31 -30	.00005	0.009	100 100	0.003	36.0 39.6	1				1	1	i	
-30 -29	.00006	0.010	100	0.004	42.9			1				i	
-28	•00006	0.010	100	0.004	46.1	1		l	Ì	ŀ		İ	
-27	.00006	0.011	100	0.006	49.0			ł		1		1	1
	00000	0.011	100	0.000	43.0	ĺ							
9.0	.00006	0.012	100	0.006	710	Ì							
-26 -25	.00007	0.012	100	0.006	51.8		Į					i	
-24	.00007	0.012	100	0.007	54.4 56.8			i					
-23	.0000s	0.014	100	0.008	59.0	1						ſ	
-22	.00008	0.015	100	0.009	61.0					1	١.	I	
					01.0			l		ŀ		l	
	.00008										ĺ	1	ĺ
-21	.00008	0.015	100	0.010	62.6	0.004	26.9					1	
-20	.00008	0.016	100	0.011	64.2	0.005	30.3		ĺ			l .	
-19	.00009	0.017	100	0.012	65.9	0.006	33.5					l	
-18	.0001	0.018	100	0.012	67.5	0.007	36.6			1		l	
-17		0.019	100	0.013	69.0	0.008	39.5					ĺ	İ
	.0001											Ì	ĺ
-16		0.020	100	0.014	70.4	0.009	42.3					-	
-15	.0001	0.021	100	0.015	71.8	0.010	44.9	0.004	19.4				
-14	.0001	0.022	100	0.017	73.0	0.011	47.4	0.005	23.0				l
-13	.0001	0.023	100	0.018	74.3	0.012	49.8	0.007	26.4				
-12	.0001	0.024	100	0.019	75.4	0.013	51.9	0.008	29.5				
	.0001			İ		,							
-11		0.026	100	0.020	76.5	0.014	53.9	0.009	32.5				
-10	.0001	0.027	100	0.021	77.5	0.016	55.7	010.0	35.3	0.005	15.6		
- 9	.0001	0.028	100	0.023	78.5	0.017	57.7	0.012	33.3	0.006	19.1		
- 8	.0001	0.030	100	0.024	79.4	0.018	59.4	0.013	40.6	0.007	22.5		
- 7	.0001	0.031	100	0.026	80.3	0.020	61.1	0.014	43.0	0.009	25.7		
- 6	•0001	0.033	100	0.027	81.1	0.021	62.7	0.016	45.4	0.010	28.4	0.005	12.9
	.0002		ļ			1							
- 5		0.034	100	0.029	81.8	0.023	64.5	0.017	47.6	0.012	31.7	0.006	16.4
- 1	.0002	0.036	100	0.030	82.5	0.025	65.8	0.019		0.014	34.5	0.008	19.8
- 3	.0002	0.038	100	0.032	83.2	0.026	67.1	0.021	51.7	0.015	36.9	0.010	22.8
- 2	.0002	0.039	100	0.034	83.9	0.028	68.3	0.023	53.5	0.017	3 9.3	0.011	25.8
- 1	.0002	0.041	100	0.036	84.5	0.030	69.5	0.024	55.3	0.019	41.6	0.013	28.6
- 0	.0002	0.043	100	0.038	85.0	0.032	71.0	0.026	57.0	0.021	43.8	0.015	31.3
1]		,							1	
		Mea	n Horiz	ontal Diff	erence o	of Force	of Vapo	r for each	0°.1=	0.0012.			

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredths.

			1	t-				and Dry I					
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	0 °.		0 °.		1°.		1°.		2°.		2°.	5
t Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity,	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Foree of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity
0		Eng. In.	100	Eng. In.	85.0	Eng. In. 0.032	70.7	Eng. In. 0.026	57.0	Eng. In. 0.021	43.8	Eng. In 0.015	31.3
0	0.0002	0.043	100	0.038	85.6	0.034	71.8	0.028	58.6	0.023	46.0	0.017	33.9
1	.0002	0.045	100	0.040			73.0	0.023	60.2	0.025	48.0	0.019	36.4
2	.0002	0.047	100	0.042	86.2	0.036	74.0	0.031	61.8	0.023	50.0	0.022	38.8
3	.0002	0.050	100	0.044	86.7	0.038		0.035		0.027	52.0	0.024	41.2
4		0.052	100	0.046	87.2	0.041	75.0	0.055	63.3	0.050	04.0	0.024	71.2
	.0002												
5		0.055	100	0.049	87.7	0.043	76.0	0.038	64.7	0.032	53.8	0.026	43.4
6	.0002	0.057	100	0.051	88.2	0.046	76.9	0.040	66.0	0.034	55.3	0.029	45.2
7	.0003	0.059	100	0.054	88.6	0.048	77.7	0.043	67.1	0.037	56.8	0.031	47.0
8	.0003	0.062	100	0.057	89.0	0.051	78.4	0.045	68.2	0.040	58.2	0.034	48.8
9	.0003	0.065	100	0.059	89.4	0.054	79.1	0.048	69.2	0.043	59.6	0.037	50.5
	.0003	1											
10	.0003	0.068	100	0.062	89.8	0.057	79.7	0.051	70.1	0.046	61.0	0.040	52.2
11	.0003	0.071	100	0.066	90.1	0.061	80.4	0.054	71.1	0.049	62.3	0.043	53.S
12	.0003	0.075	100	0.069	90.4	0.063	81.0	0.058	72.1	0.052	63.5	0.046	55.3
13	.0003	0.078	100	0.072	90.7	0.067	81.6	0.061	73.0	0.056	64.8	0.050	56.8
14	.0004	0.082	100	0.076	91.0	0.071	82.3	0.065	73.9	0.059	65.9	0.054	58.2
14	ĺ												
	.0004			1				0.000		0.000	c= .	0.057	50.7
15	.0004	0.086	100	0.080	91.3	0.074	82.9	0.069	74.8	0.063	67.1	0.057	59.7
16	.0004	0.090	100	0.084	91.6	0.078	83.4	0.073	75.7	0.067	68.2	0.061	61.0
17	.0004	0.094	100	0.088	91.9	0.083	84.0	0.077	76.5	0.071	69.2	0.066	62.3
18	.0005	0.098	100	0.093	92.1	0.087	84.5	0.081	77.2	0.076	70.2	0.070	63.5
19	.0005	0.103	100	0.097	92.4	0.092	\$5.0	0.086	78.0	0.080	71.2	0.075	64.7
	.0005	ł		i									
20	1	0.108	100	0.102	92.6	0.096	85.5	0.091	78.7	0.085	72.1	0.079	65.8
21	•0005	0.113	100	0.107	92.9	0.101	86.0	0.096	79.4	0.090	73.0	0.084	66.9
22	•0005	0.118	100	0.112	93.1	0.107	86.4	0.101	80.0	0.095	73.8	0.089	68.0
23	•0005	0.123	100	0.118	93.3	0.112	86.8	0.106	80.7	0.100	74.6	0.095	68.9
24	.0006	0.129	100	0.123	93.6	0.117	87.2	0.112	81.2	0.106	75.4	0.100	69.9
25	.0006	0.135	100	0.129	93.8	0.123	87.6	0.118	81.8	0.112	76.1	0.106	70.7
	.0006					1						1	
26		0.141	100	0.135	91.0	0.129	88.0	0.123	82.4	0.117	76.8	0.112	71.6
20	.0006	0.147	100		94.1		88.3	1	1	0.124	1	0.118	72.5
28	.0006	0.147	100	1	94.3	1	88.7		83.4	1	78.2	0.125	73.3
29	.0007	0.160	}		94.5	1	1	1	83.9	1	78.8	0.131	74.0
30	.0007	0.167			94.7		89.3		84.3		79.4	0.138	74.8
31	.0007	0.174	i		1	1	}	1	84.8	1	80.0	0.145	75.6
91	i	1	100	"""									1
	1	<u>'</u>	!			•	<u> </u>	<u>. </u>		0.0000			
		Me	an Hor	izontal D	ifference	of Force	of Vap	or for eac	h 0°.1	= 0.0012.			

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t—i						ermomet		e.	
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	3°.	0	3°.	.5	4 °.	.0	4 °	.5	5°	.0	5°	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
0	0.0002	0.010	19.3	0.004	7.9			1					
1	.0002	0.012	22.3	0.006	11.3	l		l		ļ		ŀ	
2	.0002	0.014	25.3	0.008	14.7			İ					
3	.0002	0.016	28.1	0.010	17.8			l		1		ŀ	
4		0.018	30.8	0.013	20.9	0.007	11.4	l				İ	
	.0002]		ł							
5	.0002	0.021	33.4	0.015	23.8	0.010	14.6	[
6	!	0.023	35.6	0.018	26.3	0.012	17.5	0.006	9.0			l	
7	.0002	0.026	37.7	0.020	28.8	0.014	20.2	0.009	12.0				
8		0.028	39.8	0.023	31.2	0.017	22.9	0.011	15.0				
9	.0003	0.031	41.8	0.026	33.5	0.020	25.5	0.014	17.9	0.009	10.6		
	.0003												
10		0.034	43.8	0.029	35.7	0.023	28.0	0.017	20.6	0.012	13.6		
11	.0003	0.037	45.7	0.032	37.9	0.026	30.4	0.020	23.3	0.014	16.4	0.009	9.9
12	.0003	0.041	47.5	0.035	40.0	0.029	32.7	0.024	25.8	0.018	19.2	0.012	12.9
13	.0003	0.014	49.2	0.039	42.0	0.033	35.0	0.027	28.3	0.022	21.9	0.016	15.8
14	.0004	0.048	50.9	0.012	43.9	0.037	37.1	0.031	30.7	0.025	24.5	0.020	18.5
	.0004		1										
15		0.052	52.5	0.046	45.7	0.040	39.2	0.035	32.9	0.029	26.9	0.023	21.2
16	.0#04	0.056	54.1	0.050	47.5	0.044	41.2	0.039	35.1	0.033	29.3	0.027	23.7
17	0004	0.060	55.6	0.054	49.2	0.049	43.1	0.043	37.2	0.037	31.6	0.032	26.2
18	.0004	0.065	57.0	0.059	50.9	0.053	44.9	0.047	39.2	0.042	33.7	0.036	28.5
19	•0004	0.069	58.4	0.063	52.5	0.058	46.7	0.052	41.2	0.046	35.8	0.040	30.7
	.0005												
20		0.074	59.8	0.068	54.0	0.062	48.3	0.057	43.0	0.050	37.8	0.045	32.9
21	.0005	0.079	61.0	0.073	55.4	0.067	50.0	0.062	44.7	0.056	39.7	0.050	34.9
22	.0005	0.081	62.2	0.078	56.8	0.072	51.5	0.067	46.4	0.061	41.5	0.055	36. S
23	.0005	0.089	63.4	0.083	58.1	0.078	52.9	0.072	48.0	0.066	43.3	0.061	38.6
24	.0006	0.095	64.4	0.089	59.3	0.083	54.3	0.077	49.6	0.072	44.9	0.066	40.5
25	.0006	0.100	65.5	0.095	60.5	0.089	55.6	0.083	51.0	0.078	46.5	0.072	42.2
	•0006												
26		0.106	66.5	0.101	61.7	0.095	56.9	0.089	52.4	0.083	48.0	0.078	43.9
27	.0006	0.113	67.5	0.107	62.8	0.101	58.2	0.095	53.8	0.090	49.6	0.084	45.5
28	•0006	0.119	68.5	0.113	63.9	0.108	59.4	0.102	55.2	0.096	51.0	0.090	47.0
29	.0007	0.126	69.4	0.120	64.9	0.114	60.6	0.108	56.4	0.103	52.4	0.097	48.5
30	•0007	0.132	70.3	0.127	65.9	0.121	61.7	0.115	57.7	0.109	53.7	0.104	49.9
31	.0007	0.139	71.2	0.134	66.9	0.128	62.8	0.122	58.8	0.116	55.0	0.111	51.2
	!	Men	n Horiz	zontal Dif	Terence	of Force	of Vanc	or for eacl	h 0°.1 =	= 0.0012.	'		

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredths.

								•		ermomete ith a Film			
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	G°.	.0	6°.	5	70.	0	70.	.5	80.	•	80.	5
Fahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu-mid-ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Ilu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng In.	
12	0.0003	0.007	6.8							1			
13	.0004	0.010	9.9										
14	.0004	0.014	12.8	0.008	7.5								
15	.0004	0.018	15.7	0.012	10.4	0.006	5.4						
16		0.022	18.4	0.016	13.3	0.010	8.4						
17	.0004	0.026	21.0	0.020	16.0	0.015	11.3	0.009	6.7				
18	.0004	0.020	23.5	0.025	18.6	0.019	14.0	0.003	9.6	0.008	5.3		
19	.0005	0.035	25.8	0.029	21.2	0.013	16.6	0.013	12.3	0.003	8.2	0.006	4.5
20	.0005	0.040	28.1	0.023	23.5	0.028	19.0	0.013	15.0	0.012	11.0	0.000	7.
21	.0005	0.044	30.3	0.039	25.8	0.033	21.5	0.022	17.5	0.022	13.5	0.016	9.8
-1	.0005	0.044	00.0	0.055	20.0	0.055	21.0	0.021	11.5	0.022	10.0	0.010	0.0
22		0.050	32.3	0.044	28.0	0.038	23.8	0.032	19.8	0.027	16.0	0.021	12.
23	.0005	0.055	34.2	0.049	30.1	0.043	26.0	0.038	22.1	0.032	18.4	0.026	14.
21	.0005	0.060	36.1	0.055	32.1	0.049	28.1	0.043	24.4	0.038	20.7	0.032	17.
25	.0006	0.066	38.0	0.060	34.0	0.055	30.2	0.049	26.5	0.043	23.0	0.038	19.
26	.0006	0.072	39.8	0.066	35.9	0.061	32.2	0.055	28.6	0.049	25.1	0.043	21.8
	.0006	i						l		1			
27	.0006	0.078	41.5	0.073	37.8	0.067	34.0	0.061	30.6	0.055	27.2	0.050	23.9
28	.0007	0.085	43.2	0.079	39.5	0.073	35.9	0.067	32.5	0.062	29.1	0.056	25.9
29	.0007	0.091	44.8	0.085	41.1	0.080	37.6	0.074	34.2	0.068	31.0	0.063	27.9
30	.0007	0.098	46.2	0.092	42.7	0.086	39.2	0.081	35.9	0.075	32.8	0.069	29.
31		0.105	47.6	0.099	44.2	0.093	40.8	0.088	37.5	0.082	34.4	0.076	31.
		90	.0	9°	.5	100	0.0	100	·.5	110	0.0	110	.5
		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eug. In.		Eng. In.	
20		0.005	3.4	Ŭ .						Ĭ			
21	0.0005	0.010	6.1	0.005	2.7							1	
22	.0005	0.015	8.8	0.010	5.4	0.001	2.2						
23	.0005	0.021	11.4	0.015	8.0	0.009	4.9						
21	.0005	0.026	13.9	0.020	10.6	0.015	7.5	0.009	4.5				
25	.0006	0.032	16.2	0.026	13.1	0.020	10.0	0.015	7.1	0.009	4.2		
	.0006			1		ļ							
26		0.038	18.5	0.032	15.4	0.026	12.4	0.021	9.5	0.015	6.8	0.009	4.
27	.0006	0.014	20.7	0.038	17.7	0.032	14.7	0.027	11.9	0.021	9.2	0.015	6.
28	.0006	0.050	22.8	0.045	19.9	0.039	16.9	0.033	14.2	0.027	11.5	0.022	8.
29	.0007	0.057	24.9	0.051	21.9	0.045	19.0	0.040	16.3	0.034	13.7	0.028	11.
30	.0007	0.064	26.7	0.058	23.8	0.052	21.0	0.046	18.4	0.041	15.8	0.035	13.
31	.0007	0.071	28.5	0.065	25.7	0.059	22.9	0.053	20.3	0.048	17.8	0.042	15.
	l .		<u> </u>			1		I		= 0.0012.		1	

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t – t	t', o r Di	fference o	of Wet a	and Dry	Bulb Th	ermome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	0 °.	0	0 °.	5	10	.0	1°	.5	20	.0	2°	.5
Fahren- heit.	for each	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tivo Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.181	100	0.175	91.5	0.168	89.3	0.162	84.1	0.155	79.2	0.149	74.4
33	.0008	0.188	100	0.182	94.7	0.175	89.5	0.169	84.5	0.162	79.7	0.156	75.0
34	.0008	0.196	100	0.189	94.8	0.183	89.8	0.176	84.9	0.170	80.2	0.163	75.6
35	.0008	0.204	100	0.197	94.9	0.191	90.0	0.184	85.3	0.178	80.7	0.171	76.2
36	.0009	0.212	100	0.205	95.0	0.199	90.3	0.192	85.6	0.186	81.1	0.179	76.8
37		0.220	100	0.214	95.2	0.207	90.5	0.201	86.0	0.194	81.6	0.188	77.8
38	.0009	0.229	100	0.223	95.3	0.216	90.7	0.210	86.3	0.203	82.0	0.196	77.9
39	.0009	0.238	100	0.232	95.4	0.225	91.0	0.219	86.6	0.212	82.4	0.206	78.4
40	.0009	0.248	100	0.241	95.5	0.235	91.2	0.228	86.9	0.221	82.9	0.215	78.9
41	.0010	0.257	100	0.251	95.6	0.244	91.4	0.238	87.3	0.231	83.3	0.224	79.4
	.0010					*****			01.0	0.201	00.0	V	
42	.0010	0.267	100	0.260	95.7	0.254	91.6	0.247	87.5	0.241	83.6	0.234	79.8
43	.0010	0.278	100	0.271	95.8	0.264	91.8	0.258	87.8	0.251	84.0	0.245	80.3
44	.0011	0.288	100	0.282	95.9	0.275	92.0	0.268	88.1	0.262	84.3	0.255	80.7
45	.0011	0.299	100	0.293	96.0	0.286	92.1	0.280	88.3	0.273	84.7	0.266	81.1
46	.0011	0.311	100	0.304	96.1	0.297	92.3	0.291	88.6	0.284	85.0	0.278	81.5
	.0012							1					
47	.0012	0.323	100	0.316	96.2	0.310	92.5	0.303	88.8	0.297	85.3	0.290	81.9
48	.0013	0.335	100	0.329	96.2	0.322	92.6	0.315	89.0	0.309	85.6	0.302	82.2
49	.0013	0.348	100	0.341	96.3	0.335	92.7	0.328	89.3	0.321	85.9	0.315	82.6
50	.0013	0.361	100	0.354	96.4	0.348	92.9	0.341	89.5	0.334	86.1	0.328	82.9
51	.0014	0.374	100	0.368	96.5	0.361	93.0	0.354	89.7	0.348	86.4	0.341	83.2
52	•0014	0.388	100	0.332	96.5	0.375	93.2	0.368	89.9	0.362	86.7	0.355	83.6
53	.0014	0.403	100	0.396	96.6	0.389	93.3	0.383	90.1	0.376	86.9	0.370	83.9
54	•0015	0.418	100	0.411	96.7	0.404	93.4	0.398	90.2	0.391	87.2	0.385	84.2
55	.0015	0.433	100	0.426	96.7	0.420	93.5	0.413	90.4	0.407	87.4	0.400	84.4
56	.0016	0.449	100	0.442	96.8	0.436	93.6	0.429	90.6	0.422	87.6	0.416	84.7
	.0016												
57	0017	0.466	100	0.459	96.8	0.452	93.7	0.446	90.7	0.439	87.8	0.432	85.0
5 8	.0017 .0017	0.482	100	0.476	96.9	0.469	93.9	0.463	90.9	0.456	88.0	0.449	85.2
59	.0017	0.500	100	0.493	96.9	0.487	94.0	0.480	91.0	0.473	88.2	0.467	85.5
60	.0018 .0019	0.518	100	0.511	97.0	0.505	94.1	0.498	91.2	0.491	88.4	0.485	85.7
61	•0019	0.537	100	0.530	97.0	0.523	94.2	0.517	91.3	0.510	88.6	0.503	85.9
es.	•0019	0.556	100		0~ 1	0.540	ا م ا	0.500	01.	0 500	00.0	0 500	000
62	.0020	0.556 0.576	100	0.549	97.1	0.542	94.2	0.536	91.5	0.529	88.8	0.522	86.2
63	.0020	0.576	100	0.569	97.1	0.562	94.3	0.556	91.6	0.549	89.0	0.542	86.4
$\frac{64}{65}$.0021	0.596	100 100	0.589	97.2	0.583	94.4	0.576	91.7	0.569	89.1	0.563	86.6
66	.0022	0.617	100	$0.611 \\ 0.633$	97.2	0.604	94.5	0.597	91.9	0.591	89.3	$0.584 \\ 0.606$	86-8
67	•0023	0.662	100	0.655	97.3 97.3	$0.626 \\ 0.648$	94.6	0.619	$92.0 \\ 92.1$	$0.612 \\ 0.635$	89.5 89.6	0.606	87.0 87.2
01		0.002	100	0.000	31.5	0.048	94.7	0.642	92.1	0.053	09.0	0.040	01.2
		i ,											

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

				t t	, or Di	ffe reuce o	f Wet a	ınd Dry I	Bulb Th	ormomet	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force of Vapor	0 °.	0	٥٠.	5	1°.	0	1°.	5	2∘.	.0	2°.	.5
Fahren- heit.	for each 00.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.						
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	20.0	Eng In.	0
68	0.0023	0.685	100	0.678	97.3	0.671	94.7	0.665	92.2	0.658	89.8	$0.651 \\ 0.675$	87.3 87.5
69	.0024	0.708	100 100	0.702	97.4	$0.695 \\ 0.720$	94.8	$0.688 \\ 0.713$	$92.3 \\ 92.4$	$0.682 \\ 0.706$	89.9 90.0	0.699	87.7
70	.0025	0.733 0.758	100	$0.726 \\ 0.752$	97.4	0.745	95.0	0.738	92.5	0.731	90.2	0.725	87.9
72	.0026	0.784	100	0.778	97.5	0.771	95.0	0.764	92.7	0.757	90.3	0.751	88.0
	.0027	001	100	0.,,0		0	00.0						
73	.0028	0.811	100	0.805	97.5	0.798	95.1	0.791	92.7	0.784	90.4	0.778	88.2
74	.0028	0.839	100	0.832	97.6	0.826	95.2	0.819	92.8	0.812	90.6	0.805	88.3
75	.0029	0.868	100	0.861	97.6	0.854	95.2	0.847	92.9	0.841	90.7	0.834	88.5
76	.0030	0.897	100	0.890	97.6	0.883	95.3	0.877	93.0	0.870	90.8	0.863	88.6
77		0.927	100	0.920	97.7	0.914	95.4	0.907	93.1	0.900	90.9	0.893	88.8
78	.0031	0.958	100	0.951	97.7	0.945	95.4	0.938	93.2	0.931	91.0	0.924	88.9
79	.0032	0.990	100	0.983	97.7	0.977	95.5	0.970	93.3	0.963	91.1	0.956	89.0
80	.0033	1.023	100	1.016	97.7	1.010	95.5	1.003	93.4	0.996	91.2	0.989	89.2
81	.0034	1.057	100	1.050	97.8	1.044	95.6	1.037	93.4	1.030	91.3	1.023	89.3
82	.0035	1.092	100	1.085	97.8	1.079	95.6	1.072	93.5	1.065	91.4	1.058	89.4
	.0036												
83	.0037	1.128	100	1.121	97.8	1.115	95.7	1.108	93.6	1.101	91.5	1.094	89.5
84	.0038	1.165	100	1.158	97.8	1.152	95.7	1.145	93.6	1.138	91.6	1.131	89.6
85	.0039	1.203	100	1.196	97.9	1.189	95.8	1.183	93.7	1.176	91.7	1.169	89.7
86	.0040	1.242	100	1.235	97.9	1.228	95.8	1.222	93.8	1.215	91.8	1.208	89.8
87		1.282	100	1.275	97.9	1.268	95.9	1.263	93.8	1.256	91.9	1.249	90.0
88	.0041	1.323	100	1.317	97.9	1.310	95.9	1.303	93.9	1.296	92.0	1.289	90.1
89	.0042	1.366	100	1.359	97.9	1.352	95.9	1.345	94.0	1.339	92.0	1.332	90.2
90	-0044	1.410	100	1.403	98.0	1.396	96.0	1.389	94.0	1.382	92.1	1.375	90.3
91	•0045	1.455	100	h.448	98.0	1.441	96.0	1.434	94.1	1.427	92.2	1.420	90.3
92	•0046	1.501	100	1.494	98.0	1.487	96.1	1.480	94.1	1.473	92.3	1.466	90.4
	•0048							1		1			
93	0040	1.548	100	1.541	98.0	1.535	96.1	1.528	94.2	1.521	92.4	1.514	90.5
94	.0049	1.597	100	1.590	98.1	1.583	96.1	1.576	94.3	1	92.4	1.562	90.6
95	.0051	1.647	100	1.640	98.1	1.633	96.2	1.626	94.3	1.619	92.5	1.612	90.7
96	.0051	1.698	100	1.691	98.1	1.684	96.2	1.677	94.4	1.670	92.6	1.664	90.8
97	.0054	1.751	100	1.744	98.1	1.739	96.2	1.730	94.4	1.723	92.6	1.716	90.9
98	l	1.805	100	1.798	98.1	1.791	96.3	1.784	94.5	1.777	92.7	1.770	90.9
99	.0056	1.861	100	1.854	98.1	1.847	96.3	1.840	94.5	1.833	92.8	1.826	91.0
100	.0057	1.918	100	1.911	98.2	1.904	96.3	1.897	94.6	1.890	92.8	1.883	91.1
101	.0059	1.977	100	1.970	98.2	1.963	96.4	1.956	94.6	1.949	92.9	1.942	91.2
102	.0060	2.037	100	2.030	98.2	2.023	96.4	2.016	94.7	2.009	92.9	2.002	91.2
103	.0062	2.098	100	2.092	98.2	2.085	96.4	2.078	94.7	2.071	93.0	2.064	91.3
104	.0063	2.162	100	2.155	98.2	2.148	96.5	2.141	94.7	2.134	93.1	2.127	91.4
		Mea	n Horiz	ontal Diff	erence	of Force	of Vap	or for eac	h 00.1	= 0.0013.			

 ${\bf Temperature, Fahrenheit. -- Force\ of\ Vapor\ in\ English\ Inches. -- Relative\ Humidity\ in\ Hundredths.}$

				t —	t', or D	ifference	of Wet	and Dry	Bulb T	hermome	ters.		
Wet- Bulb Thermo- meter	of Force	3∘.	.0	3 °.	.5	40.	.0	40.	.5	5∘.	0	5∘.	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid ity.
0		Eng. In.	00.0	Eng. In.		Eng. In.	01.0	Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.142	69.8	0.136	65.3	0.129	61.0	0.123	56.S	0.116	52.7	0.110	48.8
33	.0007	0.149	70.5	0.143	66.1	0.136	61.9	0.130	57.7	0.123	5 3. 7	0.117	50.
34	.0008	0.157	71.2	0.150	66.9	0.144	62.8	0.137	58.6	0.131	54.7	0.121	51.
35	.0008	0.165	71.9	0.158	67.7	0.152	63.6	0.145	59.5	0.139	55.7	0.132	52.
36	.0003	0.173	72.6	0.166	68.5	0.160	64.5	0.153	60.5	0.147	56.7	0.140	53.
	.0008												
37	.0009	0.181	73.2	0.175	69.2	0.168	65.3	0.162	61.4	0.155	57.7	0.149	54.
38	.0009	0.190	73.8	0.183	69.9	0.177	66.1	0.170	62.3	0.164	58.7	0.157	55.
39	i i	0.199	74.4	0.192	70.6	0.186	66.9	0.179	63.2	0.173	59.7	0.166	56.
40	•0010	0.208	75.0	0.202	71.3	0.195	67.7	0.189	64.1	0.182	60.7	0.176	57.
41	.0010	0.218	75.6	0.211	72.0	0.205	68.4	0.198	65.0	0.192	61.7	0.185	58.
	.0010												
42	0310	0.228	76.2	0.221	72.6	0.215	69.1	0.208	65.7	0.202	62.4	0.195	59.
43	.0010	0.238	76.7	0.232	73.2	0.225	69.8	0.219	66.3	0.212	63.1	0.205	60.5
44	•0011	0.249	77.2	0.242	73.7	0.236	70.4	0.229	67.0	0.223	63.S	0.216	61.
45	.0011	0.260	77.7	0.253	74.3	0.247	71.0	0.240	67.6	0.234	64.6	0.227	61.
46	.0011	0.271	78.1	0.265	74.8	0.258	71.6	0.252	68.3	0.245	65.3	0.238	62.
40	.0012	0.211	73.1	0.203	14.0	0.233	11.0	0.202	00.0	0.240	00.0	0.230	04.
47	.00.12	0.283	78.6	0.277	75.3	0.270	72.2	0.264	68.9	0.257	66.0	0.250	63.
48	.0012	0.296	79.0	0.289	75.8	0.282	72.7	0.276	69.6	0.269	66.7	0.263	64.0
49	.0013	0.308	79.4	0.302	76.3	0.295	73.3	0.288	70.2	0.282	67.4	0.275	64.
50	•0013	0.303	79.8				73.8	0.301	70.2	0.295	68.1	0.238	65.
	.0013		1	0.315	76.7	0.308						i :	
51		0.335	80.2	0.328	77.2	0.321	74.3	0.315	71.4	0.308	68.7	0.302	66.
52	-0014	0.319	80.5	0.342	77.6	0.335	74.7	0.329	71.9	0.322	69.2	0.315	66.
1	.0014	0.363	80.9	0.342	78.0	0.350	75.2	0.343		0.336	69.8	0.330	67.5
53	.0015							1	72.5			1 1	
54	.0015	0.378	81.2	0.371	78.4	0.365	75.6	0.358	72.9	0.351	70.3	0.345	67.
55	.0016	0.393	81.6	0.387	78.8	0.380	76.1	0.373	73.4	0.367	70.8	0.360	68.
56	1	0.409	81.9	0.403	79.1	0.396	76.5	0.389	73.9	0.383	71.3	0.376	68.
-~	.0016	0.496	00.0	0.410	*0 -	0.113	#C 0	0.400	*4.0	0.000	F1 0	0.900	co
57	.0017	0.426	82.2	0.419	79.5	0.412	76.9	0.406	74.3	0.399	71.8	0.392	69.
58	.0017	0.443	82.5	0.436	79.8	0.429	77.2	0.123	74.8	0.416	72.3	0.409	69.9
59	.0018	0.160	82.8	0.453	80.2	0.447	77.6	0.440	75.1	0.433	72.7	0.427	70.
60	.0019	0.178	83.1	0.471	80.5	0.465	78.0	0.458	75.5	0.451	73.1	0.445	70.8
61		0.197	83.3	0.490	80.8	0.483	78.3	0.477	75.9	0.470	73.5	0.463	71.
00	.0019	0	0.0			, , , ,				0 150			
62	.0020	0.516	83.6	0.509	81.1	0.502	78.6	0.496	76.3	0.489	74.0	0.482	71.
63	.0020	0.536	83.8	0.529	81.4	0.522	79.0	0.516	76.6	0.509	74.3	0.502	72.
64		0.556	84.1	0.549	81.7	0.543	79.3	0.536	77.0	0.529	74.7	0.523	72.
65	.0021	0.577	84.3	0.570	81.9	0.564	79.6	0.557	77.3	0.550	75.1	0.544	72.
66	•0022	0.599	84.6	0.592	82.2	0.586	79.9	0.579	77.6	0.572	75.4	0.566	73.
67	.0023	0.622	84.8	0.615	82.4	0.608	80.2	0.601	78.0	0.595	75.8	0.588	73.
				ì		i l							

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t — t	', or Di	ifference o	of Wet :	and Dry 1	Bulb T l	nermomet	ers.		
Wet- Bulb hermo- meter	Mean Vertical Difference of Force	3∘.	0	3 °.	.5	4∘.	0	40.	.5	5 °.	0	5 °.	.5
t/ ahren- heit	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity.
0		Eng. In.	05.0	Eng. In.	00.7	Eng. In.	60.4	Eng. In.	*0.9	Eng. In.	FC 1	Eng. In.	
68	0.0024	0.644	85.0	0.638	82.7	0.631	80.4 80.7	0.624	78.3	0.618	76.1	0.611	74.
69	.0024	0.668	85.2	0.661	82.9	0.655		0.648	78.6	0.641	76.4	0.635	74.
70	.0025	0.693	85.4	0.686	83.2	0.679	81.0	0.672	78.8	0.666	76.S	0.659	71.
71	.0026	0.718	85.6	0.711	83.4	0.704	81.2	0.698	79.1	0.691	77.1	0.684	75.
72	00.75	0.744	85.8	0.737	83.6	0.731	81.5	0.724	79.4	0.718	77.4	0.710	75.
*0	.0027	0	86.0	0.764	83.8	0.757	81.7	0.751	79.7	0.711	77.6	0.797	
73	.0028	0.771	86.2	0.794	i i		81.9	0.731	79.9	$0.744 \\ 0.772$		0.737	75.
71	.0028	0.799			84.0	0.785					77.9	0.765	76.
75	.0029	0.827	86.3	0.820	84.2	0.814	82.2	0.807	80.2	0.800	78.2	0.793	76.
76	.0030	0.856	86.5	0.850	84.4	0.843	82.4	0.836	80.4	0.829	78.4	0.823	76.
77		0.887	86.7	0.880	84.6	0.873	82.6	0.866	80.6	0.860	78.7	0.853	76.
~ 0	.0031	0.010	86.8	0.911	84.8	0.904	82.8	0.897	80.8	0.890	78.9	0.884	77.
78	.0032	0.918						1				i	
79	.0033	0.949	87.0	0.943	85.0	0.936	83.0	0.929	81.1	0.922	79.2	0.916	77.
80	.0034	0.982	87.1	0.976	85.1	0.969	83.2	0.962	81.3	0.955	79.4	0.949	77.
81	.0035	1.016	87.3	1.010	85.3	1.003	83.4	0.996	81.5	0.989	79.7	0.982	77.
82		1.051	87.4	1.045	85.5	1.038	83.6	1.031	81.7	1.024	79.9	1.017	78.
00	.0036		O# #	1 000	0= 0	1.074	83.7	1.067	D1 0	1.060	80.1	1.050	78.
83	.0037	1.087	87.5	1.080	85.6	i		1	81.9	1		1.053	
84	.0038	1.124	87.7	1.117	85.8	1.111	83.9	1.104	82.1	1.096	80.3	1.090	78.
85	.0039	1.162	87.8	1.155	85.9	1.148	84.1	1.142	82.3	1.135	80.5	1.128	78.
86	•00 10	1.201	87.9	1.194	86.1	1.187	84.2	1.181	82.4	1.174	80.7	1.167	79.
87		1.242	88.1	1.235	86.2	1.228	84.4	1.222	82.6	1.215	80.9	1.208	79.
00	.0041		00.0	1.0~0	0.0.0	1 200	0.4.0	1 000	00.0	1 0	01.	1 0 10	-0
88	.0042	1.282	88.2	1.276	86.3	1.269	84.6	1.262	82.8	1.255	81.1	1.248	79.
89	.0044	1.325	88.3	1.318	86.5	1.311	84.7	1.304	83.0	1.297	81.3	1.291	79.
90	.0045	1.369	88.4	1.362	86.6	1.355	84.9	1.348	83.1	1.341	81.4	1.334	79.
91	.0046	1.413	88.5	1.407	86.7	1.400	85.0	1.393	83.3	1.386	81.6	1.379	80.
92		1.460	88.6	1.453	86.9	1.446	85.1	1.439	83.4	1.432	81.8	1.425	80.
93	.0047	1 500	88.7	1.500	87.0	1.493	85.3	1.486	83.6	1.480	82.0	1.473	80.
1	.0049	1.507				1		1 1	i	1			80.
91	.0050	1.556	88.8	1.549	87.1	1.542	85.4	1.535	83.8	1.528	82.1	1.521	
95	.0051	1.606	88.9	1.599	87.2	1.592	85.5	1.585	83.9	1.578	82.3	1.571	80.
96	.0052	1.657	89.0	1.650	87.3	1.643	85.7	1.636	84.0	1.629	82.4	1.622	80.
97	.0054	1.709	89.1	1.702	87.5	1.696	85.8	1.688	84.2	1.682	82.6	1.675	81.
98		1.761	89.2	1.757	87.6	1.750	85.9	1.743	84.3	1.736	82.7	1.729	81.
00	.0055	1 010	60.9	1 610	O 100 100	1.805	86.0	1.798	014	1 700	82.9	1 405	01
99	.0057	1.819	89.3	1.812	87.7	1		! !	84.4	1.792		1.785	81.
100	.0058	1.876	89.4	1.869	87.8	1.863	86.2	1.856	81.6	1.849	83.0	1.842	81.
101	.0060	1.935	89.5	1.928	87.9	1.921	86.3	1.91-1	84.7	1.907	83.2	1.900	81.
102	.0062	1.995	89.6	1.988	88.0	1.981	86.4	1.974	84.8	1.967	83.3	1.961	81.
103	.0063	2.057	89.7	2.050	88.1	2.043	86.5	2.036	84.9	2.029	83.4	2.022	81.
104	.0000	2.120	89.8	2.113	88.2	2.106	86 6	2.099	85.1	2.092	83.5	2.085	82

Temperature, Fahrenheit — Force of Vapor in English Inches. — Relative Humidity in Hundredths

				t 1	t', or D	ifference (of Wet	and Dry	Bulb T	he r mome	ters.		
Wet- Bulb Thermo- meter	Mean Vertical Difference of Force	6 °.	0	6∘.	5	70	.0	70.	.5	80.	.0	80	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor,	Rela- tive Hu- nid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid ity.
0		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.103	45.0	0.097	41.4	0.090	37.9	0.084	34.5	0.077	31.2	0.071	28.0
33	.0007	0.110	46.3	0.104	42.7	0.097	39.3	0.091	36.0	0.084	32.8	0.078	29.6
34	.0008	0.118	47.6	0.111	44.1	0.105	40.7	0.098	37.4	0.092	34.3	0.085	31.2
35	.0008	0.126	48.8	0.119	45.3	0.113	42.0	0.106	38.8	0.100	35.7	0.093	32.8
36	0000	0.134	50.0	0.127	46.6	0.121	43.3	0.114	40.2	0.108	37.2	0.101	34.5
37	.0009	0.142	51.1	0.136	47.8	0.129	44.6	0.123	41.6	0.116	38.6	0.109	35.7
38	•0009	0.142	52.2	0.133	49.0	0.125	45.9	0.131	42.9	0.115	40.0	0.118	37.5
39	.0009	0.160	53.3	0.144	50.1	0.147	47.1	0.140	44.1	0.123	41.3	0.113	38.
40	.0009	0.169	54.3	0.163	51.3	0.147	48.3	0.149	45.4	0.134	42.6	0.136	39.9
41	.0010	0.103	55.4	0.172	52.3	0.166	49.4	0.159	46.6	0.143	43.9	0.146	41.5
71	.0010	0.175	99.4	0.172	0.40	0.100	40.4	0.155	40.0	0.155	40.0	0.140	41.7
42		0.189	56.3	0.182	53.4	0.175	50.5	0.169	47.7	0.162	45.0	0.156	42
43	.0010	0.199	57.2	0.192	54.3	0.186	51.5	0.179	48.8	0.173	46.1	0.166	43.6
44	.0011	0.209	58.1	0.203	55.3	0.196	52.5	0.190	49.8	0.183	47.2	0.177	44.
45	.0011	0.220	59.0	0.214	56.2	0.207	53.5	0.201	50.8	0.194	48.3	0.188	45.8
46	.0011	0.232	59.8	0.225	57.0	0.219	54.4	0.212	51.8	0.206	49.3	0.198	46.9
	.0012	0.202	00.0	0.220	0	0.210		01212	01.0	0.200	10.0	0.100	10.0
47		0.241	60.6	0.237	57.9	0.231	55.2	0.224	52.7	0.217	50.2	0.211	47.9
48	.0012	0.256	61.3	0.249	58.7	0.243	56.1	0.236	53.6	0.230	51.2	0.223	48.8
49	.0013	0.269	62.0	0.262	59.4	0.255	56.9	0.249	54.5	0.242	52.1	0.236	49.7
50	.0013	0.252	62.7	0.275	60.2	0.268	57.7	0.262	55.3	0.255	52.9	0.249	50.6
51	.0013	0.295	63.4	0.288	60.9	0.282	58.4	0.275	56.1	0.269	53.7	0.262	51.3
	.0014												
52		0.309	64.1	0.302	61.6	0.296	59.2	0.289	56.8	0.282	54.6	0.276	52.3
53	.0014	0.323	64.7	0.317	62.3	0.310	59.9	0.303	57.6	0.297	55.3	0.290	53.2
54	.0015	0.338	65.3	0.332	62.9	0.325	60.6	0.318	58.3	0.312	56.1	0.305	53.9
55	.0015	0.354	65.9	0.347	63.5	0.340	61.2	0.334	59.0	0.327	56.8	0.320	54.9
56	.0016	0.369	66.5	0.363	64.1	0.356	61.9	0.349	59.7	0.343	57.5	0.336	55.
	.0017												
5 7	.0017	0.386	67.0	0.379	64.7	0.373	62.5	0.366	60.3	0.359	58.2	0.353	56.1
58	.0017	0.403	67.5	0.396	65.3	0.389	63.1	0.383	60.9	0.376	58.8	0.369	56.8
59	.0018	0.420	68.0	0.413	65.8	0.407	63.6	0.400	61.5	0.393	59.5	0.387	57.
60	.0018	0.438	68.5	0.431	66.3	0.425	64.2	0.418	62.1	0.411	60.1	0.405	58.
61	10010	0.457	69.0	0.450	66.9	0.443	64.7	0.436	62.7	0.430	60.7	0.423	58.7
62	.0019	0.476	69.5	0.469	67.4	0.462	65.3	0.456	63.2	0.449	61.3	0.442	59.5
63	.0020	0.476	70.0	0.489	67.8	0.482	65.8	0.436	63.8	0.449	61.8	0.442 0.462	59.9
64	.0021	0.495	70.4	0.489	68.3	0.482	66.3	0.475		0.489	62.4	0.483	60.
65	.0021	0.516	70.4	0.530	68.8	0.524	66.8	0.496	64.3 64.8	0.489	62.9	0.483	61.0
66	.0022	0.559	70.8	0.552		0.545	67.2	0.539		0.510	63.4	$0.504 \\ 0.525$	61.6
67	.0023	0.539			69.2	, ,			65.3			0.523	62.
01		0.951	71.6	0.575	69.6	0.568	67.7	0.561	65 .7	0.554	63.9	0.049	0.6.1

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

				t – t	, or Di	fference o	f Wet a	nd Dry I	Bulb Th	ermomet	ers.		
Wet- Bulb Chermo- meter t !	Mean Vertical Difference of Force	6 °.	0	6°	.5	70	.0	70	.5	80	.0	80	.5
Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity	Force of Vapor.	Rela tive IIu- mid- ity.
68		Eng. In. 0.604	72.0	Eng. In. 0.597	70.0	Eng. In. 0.591	68.1	Eng. In. 0.584	66.2	Eng. In, 0.577	64.4	Eng In. 0.571	62.6
69	0.0024	0.628	72.4	0.621	70.4	0.591	68.5	0.608	66.6	0.601	64.8	0.594	63.0
70	.0024	0.652	72.7	0.646	70.4	0.639	68.9	0.632	67.1	0.625	65.3	0.619	63.
71	•0025	0.678	73.1	0.671	71.2	0.664	69.3	0.657	67.5	0.651	65.7	0.644	64.
72	.0026	0.704	73.4	0.697	71.5	0.690	69.7	0.683	67.9	0.677	66.1	0.670	64.
	.0027	001	10.1	0.057	11.0	0.050	00	0.000	0,,,,	0.0	00.1	0.010	01.
73	.0028	0.730	73.8	0.724	71.9	0.717	70.1	0.710	68.3	0.703	66.5	0.697	64.
74	.0028	0.758	74.1	0.751	72.2	0.745	70.4	0.738	68.7	0.731	66.9	0.724	65.
7 5	.0029	0.787	71.4	0.780	72.6	0.773	70.8	0.766	69.0	0.760	67.3	0.753	65.
76	.0030	0.816	74.7	0.809	72.9	0.802	71.1	0.796	69.4	0.789	67.7	0.782	66.
77	•0030	0.846	75.0	0.839	73.2	0.832	71.4	0.826	69.7	0.819	68.1	0.812	66.
	.0031												ĺ
78	.0032	0.877	75.3	0.870	73.5	0.863	71.8	0.857	70.1	0.850	68.4	0.843	66.
79	.0033	0.909	75.6	0.902	73.8	0.895	72.1	0.888	70.4	0.882	68.8	0.875	67.
80	.0034	0.942	75.8	0.935	74.1	0.928	72.4	0.921	70.7	0.915	69.1	0.908	67.
81	.0035	0.976	76.1	0.969	74.4	0.962	72.7	0.955	71.0	0.948	69.4	0.942	67.
82		1.011	76.4	1.004	74.6	0.997	73.0	0.990	71.3	0.983	69.8	0.977	68.
	.0036												
83	.0037	1.046	76.6	1.040	74.9	1.033	73.3	1.026	71.6	1.019	70.1	1.012	68.
84	.0038	1.083	76.8	1.077	75.2	1.070	73.5	1.063	71.9	1.056	70.4	1.049	68.
85	.0038	1.121	77.1	1.114	75.4	1.108	73.8	1.101	72.2	1.094	70.7	1.087	69.
86	.0639	1.160	77.3	1.153	75.7	1.147	74.1	1.140	72.5	1.133	70.9	1.126	69.
87		1.201	77.5	1.194	75.9	1.187	74.3	1.181	72.7	1.174	71.2	1.167	69.
88	.0040	1.241	~~ ~	1 025	76.1	1.228	74.6	1.221	73.0	1.214	71.5	1.207	70.
89	.0042	1.284	77.7 78.0	1.235	76.4	1.270	74.8	1.263	73.3	1.256	71.8	1.250	70.
90	.0044	1.327						1.307		1.300	72.0	1.293	70.
91	.0045	1.372	78.2	1.321	76.6	1.314 1.359	75.0 75.3	1.352	73.5 73.7	1.345	72.3	1.338	70.
92	.0046	1.418	78.4	1.365	76.8	1.405	75.5	1.398	74.0	1.391	72.5	1.384	71.
34	.0047	1.413	78.6	1.412	77.0	1.409	19.9	1.595	14.0	1.551	12.0	1.004	11.
93		1.466	78.8	1.459	77.2	1.452	75.7	1.445	74.2	1.438	72.8	1.431	71.
94	.0049	1.514	79.0	1.507	77.4	1.501	75.9	1.494	74.4	1.487	73.0	1.480	71.
95	.0050	1.564	79.1	1.557	77.6	1.550	76.1	1.544	74.7	1.537	73.2	1.530	71.
96	•0051	1.615	79.3	1.608	77.8	1.602	76.3	1.595	74.9	1.588	73.4	1.581	72.
97	.0052	1.668	79.5	1.661	78.0	1.654	76.5	1.647	75.1	1.640	73.7	1.633	72.
98	.0054	1.722	79.7	1.715	78.2	1.708	76.7	1.701	75.3	1.694	73.9	1.688	72.
	.0056								- 1				
99		1.778	79.8	1.771	78.4	1.764	76.9	1.757	75.5	1.750	74.1	1.743	72.
100	.0057	1.835	80.0	1.828	78.5	1.821	77.1	1.814	75.7	1.807	74.3	1.800	72.
101	.0059	1.893	80.2	1.887	78.7	1.880	77.3	1.873	75.9	1.866	74.5	1.859	73.
102	•0060	1.954	80.3	1.947	78.9	1.940	77.4	1.933	76.1	1.926	74.7	1.919	73.
103	•0061	2.015	80.5	2.008	79.0	2.001	77.6	1.994	76.2	1.987	74.9	1.980	73.0
104	.0063	2.078	80.6	2.071	79.2	2.064	77.8	2.057	76.4	2.051	75.1	2.044	73.

 ${\bf Temperature, Fshrenheit. - Force \ of \ Vapor \ in \ English \ Inches. - Relative \ Humidity \ in \ Hundredths.}$

Wet- Bulb Thermo-	Mean Vertical Difference of Force of Vapor for each 0°.1.	00.0		9°.5		10°.0		10°.5		1100		1 110 7	
meter		9°.0				10.0		10.0		110.0		110.5	
Fahren- heit.		Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor	Relative Hu- nuid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eug. In.		Eng. In		Eng. In.		Eng. In		Eng. In.		Eng. In	
32	0 0007	0.061	25.0	0.058	22.0	0.051	19.2	0.045	16.4	0.038	13.8	0.032	11.5
33	.0007	0.071	26.7	0.065	23.8	0.058	21.0	0.052	18.3	0.045	15.7	0.039	13.
34	.0008	0.079	28.3	0.072	25.5	0.066	22.7	0.059	20.1	0.053	17.5	0.046	15.
35	.0008	0.087	29.9	0.080	27.1	0.074	24.4	0.067	21.8	0.061	19.3	0.054	16.
36	.0008	0.095	31.4	0.088	28.7	0.082	26.0	0.075	23.5	0.069	21.1	0.062	18.
37	.0009	0.103	33.0	0.096	30.3	0.090	27.6	0.083	25.2	0.077	22.8	0.070	20.
38	.0009	0.112	34.4	0.105	31.8	0.099	29.2	0.092	26.8	0.086	24.4	0.079	22.
39	.0009	0.121	35.9	0.114	33,3	0.108	30.7	0.101	28.4	0.094	26.1	0.088	23.8
40	.0010	0.130	37.3	0.123	34.8	0.117	32.2	0.110	29.9	0.104	27.6	0.097	25
41	.0010	0.139	38.6	0.133	36.2	0.126	33. 7	0.120	31.4	0.113	29.2	0.107	27.0
42	.0010	0.149	39.9	0.143	37.5	0.136	35.0	0.130	32.8	0.123	30.6	0.116	28.
43	.0010	0.160	41.1	0.153	38.7	0.146	36.3	0.140	34.1	0.133	32.0	0.127	29.8
44		0.170	42.3	0.163	39.9	0.157	37.6	0.150	35.4	0.144	33.3	0.137	31.5
45	.0011	0.181	43.4	0.175	41.1	0.168	38.8	0.161	36.7	0.155	34.6	0.148	32.
46	.0011	0.192	44.5	0.186	42.2	0.179	39.9	0.173	37.9	0.166	35.8	0.160	33.8
	.0012												
47	.0012	0.204	45.5	0.198	43.3	0.191	41.1	0.185	39.0	0.178	37.0	0.171	35.0
48	.0012	0.217	46.5	0.210	44.3	0.203	42.1	0.197	40.1	0.190	38.1	0.184	36.
49	.0012	0.229	47.5	0.222	45.3	0.216	43.2	0.209	41.2	0.203	39.2	0.196	37.2
50	.0013	0.242	48.4	0.235	46.3	0.229	44.2	0.222	42.2	0.216	40.2	0.209	38.3
51	.0013	0.255	49.3	0.249	47.2	0.242	45.2	0.236	43.2	0.229	41.2	0.222	39.3
52		0.269	50.2	0.263	48.1	0.256	46.1	0.249	44.1	0.243	42.2	0.236	40.5
53	.0015	0.284	51.1	0.277	49.0	0.270	47.0	0.264	45.1	0.257	43.2	0.250	41.5
54	•0015	0.298	51.9	0.292	49.8	0.285	47.9	0.279	46.0	0.272	44.1	0.265	42.3
55	.0015	0.314	52.7	0.307	50.7	0.300	48.7	0.294	46.8	0.287	45.0	0.281	43.2
56	.0016	0.330	53.5	0.323	51.4	0.316	49.5	0.310	47.7	0.303	45.9	0.296	44.
-~	.0016	0.346	54.3	0.339	52.2	0.333	50.3	0.326	48.5	0.319	46.7	0.313	44.9
57	.0017	_							49.2	0.336		0.330	
58 50	.0017	0.363	55.0 55.7	$0.356 \\ 0.373$	52.9	0.350	51.1	0.343	50.0	0.354	$47.5 \\ 48.2$	0.347	45.7
59	.0018	0.380	56.4	0.343	53.6	0.367	51.8	0.378	50.7	0.354	49.0	0.365	47.5
60	.0018	0.398			54.3	0.385	52.5	0.396	51.4	0.371	49.7	0.383	48.1
61	.0019	0.416	57.0	0.410	55.0	0.403	53.2						
62	.0020	0.436	57.6	0.429	55.6	0.422	53.9	0.416	52.1	0.409	50.4	0.402	48.8
63	.0020	0.455	58.2	0.449	56.3	0.442	54.5	0.435	52. 8	0.429	51.1	0.422	49.
64	.0021	0.476	58.8	0.469	56.9	0.462	55.1	0.456	53.4	0.449	51.8	0.112	50.2
65	.0021	0.497	59.3	0.490	57.5	0.483	55.8	0.477	54.1	0.470	52.4	0.463	50.8
66	.0022	0.519	59.9	0.512	58.0	0.505	56.3	0.498	54.7	0.492	53.1	0.485	51.
67	.0023	0.542	60.3	0.534	58.6	0.527	56.9	0.521	55.3	0.514	53.7	0.507	52.1

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

		${f t}-{f t}',$ or Difference of Wet and Dry Bulb Thermometers.												
Wet- Bulb	Mean Vertical Difference of Force of Vapor for each 0°.1.													
		9°.0		9°.5		100.0		10∘.5		110.0		110.5		
fahren- heit.		Force of Vapor.	mid-	Force of Vapor.	mid-	Force of Vapor.	Rela- tive Hu- mid-	Force of Vapor.	Rela- tive Hu- mid-	Force of Vapor,	mid-	Force of Vapor.	Rela- tive Ilu- mid-	
			ity.		ity.		ity.		ity.	ļ	ity.		ity.	
6 8		Eng. In. 0.564	60.8	Eng. In. 0.557	59.1	Eng. In. 0.550	57.4	Eng. In. 0.544	55.8	Eng Iu. 0.537	54.2	Eng. In. 0.530	52.7	
69	0.0024	0.588	61.3	0.581	59.6	0.574	58.0	0.567	56.4	0.561	51.8	0.554	53.3	
70	.0025	0.612	61.8	0.605	60.1	0.598	58.5	0.592	56.9	0.585	55.4	0.578	53.S	
71	.0025	0.637	62.3	0.630	60.6	0.624	59.0	0.617	57.4	0.610	55.9	0.603	54.4	
72	.0026	0.663	62.7	0.656	61.1	0.650	59.5	0.643	58.0	0.636	56.4	0.629	54.9	
.~	.0027	0.000		0.000		3,000	-							
73	0037	0.390	63.2	0.683	61.6	0.677	60.0	0.670	58.4	0.663	56.9	0.656	55.5	
74	.0027	0.718	63.6	0.711	62.0	0.704	60.5	0.697	58.9	0.691	57.4	0.684	56.0	
75	.0028	0.746	64.0	0.739	62.5	0.733	60.9	0.726	59.4	0.719	57.9	0.712	56.5	
76	.0029	0.775	64.4	0.769	62.9	0.762	61.3	0.755	59.8	0.748	58.4	0.741	56.9	
77	•0030	0.805	64.8	0.799	63.3	0.792	61.8	0.785	60.3	0.778	58.8	0.772	57.4	
	•0031													
78	.0032	0.836	65.2	0.829	63.7	0.823	62.2	0.816	60.7	0.809	59.2	0.802	57.8	
79	.0032	0.868	65.6	0.861	64.1	0.855	62.6	0.848	61.1	0.841	59.7	0.834	58.3	
80	.0034	0.901	66.0	0.894	64.5	0.897	63.0	0.881	61.5	0.874	60.1	0.867	58.7	
81	1	0.935	66.3	0.928	64.8	0.921	63.4	0.914	61.9	0.908	60.5	0.901	59.1	
82	•0035	0.970	66.7	0.963	65.2	0.956	63.7	0.949	62.3	0.943	60.9	0.936	59.5	
	.0036			1	ł									
83	.0037	1.006	67.0	0.999	65.5	0.992	64.1	0.985	62.7	0.978	61.3	0.972	59.9	
84	.0035	1.042	67.3	1.036	65.9	1.029	64.4	1.022	63.0	1.015	61.7	1.008	60.3	
85	.0039	1.080	67.7	1.073	66.2	1.067	64.8	1.060	63.4	1.053	62.0	1.046	60.7	
86	4	1.119	68.0	1.112	66.5	1.106	65.1	1.099	63.7	1.092	62.4	1.085	61.0	
87	•0040	1.160	68.3	1.153	66.8	1.146	65.4	1.140	64.1	1.133	62.7	1.126	61.4	
	.0041							1						
SS	.0042	1.200	68.6	1.194	67.1	1.187	65.8	1.180	64.4	1.173	63.1	1.166	61.7	
89	.0042	1.243	68.9	1.236	67.4	1.229	66.1	1.222	64.7	1.215	63.4	1.208	62.1	
90	.0045	1.286	69.1	1.279	67.7	1.273	66.4	1.266	65.0	1.259	63.7	1.252	62	
91	.0046	1.331	69.4	1.324	68.0	1.317	66.7	1.311	65.3	1.304	64.0	1.297	62.7	
92	.0040	1.377	69.7	1.370	68.3	1.363	67.0	1.357	65.6	1.350	64.3	1.343	63.1	
	.0047		20.0			!							00.4	
93	.0048	1.425	69.9	1.418	68.6	1.411	67.2	1.404	65.9	1.397	64.6	1.390	63.4	
94	.0050	1.473	70.2	1.466	68.8	1.459	67.5	1.452	66.2	1.446	64.9	1.439	63.7	
95	.0051	1.523	70.4	1.516	69.1	1.509	67.8	1.502	66.5	1.495	65.2	1.488	64.0	
96	.0053	1.574	70.7	1.567	69.4	1.560	68.0	1.553	66.7	1.546	65.5	1.539	64.2	
97	.0054	1.627	70.9	1.620	69.6	1.613	68.3	1.606	67.0	1.599	65.8	1.592	64.5	
98		1.681	71.2	1.674	69.8	1.667	68.5	1.660	67.3	1.653	66.0	1.646	64.8	
00	.0056	1 726	71 .	1 700	70.1	1 700	68.8	1 716	C~ -	1 700	66.9	1 700	6= 1	
99	.0057	1.736	71.4	1.729	70.1	1.722	i	1.716	67.5	1.709	66.3	1.702	65.1	
100	.0058	1.793	71.6	1.786	70.3	1.780	69.0	1.773	67.8	1.766	66.5	1.759	65.3	
101	.0060	1.852	71.8	1.845	70.5	1.838	69.3	1.831	68.0	1.824	66.8	1.817	65.6	
102	.0062	1.912	72.0	1.905	70.8	1.898	69.5	1.891	68.2	1.884	67.0	1.877	65.8	
103	.0063	1.974 2.037	•	1.967 2.030	71.0 71.2	$egin{array}{c} 1.960 \ 2.023 \ \end{array}$	69.7 69.9	1.953 2.016	68.5 68.7	1.946 2.009	67.3 67.5	1.939	66.	
104														

Temperature, Fahrenheit. -- Force of Vapor in English Inches. -- Relative Humidity in Hundredths.

Wet- Bulb Thermo- meter t Fahren- heit.	Mean Vertical Difference of Force of Vapor for each 0°.1.	$\mathbf{t}-\mathbf{t}',$ or Difference of Wet and Dry Bulb Thermometers.											
		12°.0		12°.5		13°.0		13°.5		140.0		140.5	
		Force of Vapor.	Relative Hu-mid-ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu mid ity
0		Eng. In.		Eng. In.		Eng In.		Eng. In.		Eng. In.		Eng. In.	
32	0.0007	0.025	8.8	0.019	6.4	0.012	4.1					1	
33	.0007	0.032	10.8	0.026	8.4	0.019	6.2	0.013	4.0				
34	.0007	0.040	12.7	0.033	10.4	0.027	8.2	0.020	6.0	0.014	4.1		
35	.0008	0.048	14.6	0.041	12.3	0.034	10.1	0.028	8.0	0.021	6.1	0.015	4.
36	0000	0.056	16.4	0.049	14.2	0.042	12.0	0.036	10.0	0.029	8.1	0.023	6.
37	.0008	0.064	18.2	0.057	16.0	0.051	13.9	0.044	11.9	0.038	10.0	0.031	8.
38	•0009	0.072	19.9	0.066	17.8	0.059	15.7	0.053	13.7	0.046	11.9	0.040	10.
39	•0009	0.081	21.6	0.075	19.5	0.068	17.5	0.062	15.5	0.055	13.7	0.049	11.
40	•0009	0.091	23.3	0.084	21.2	0.078	19.2	0.071	17.2	0.064	15.4	0.058	13.
41	•0010	0.100	24.9	0.094	22.8	0.087	20.8	0.081	18.9	0.074	17.1	0.067	15.
	.0010			1									
42	.0010	0.110	26.4	0.103	24.3	0.097	22.4	0.090	20.5	0.084	18.6	0.077	16.
43	.0010	0.120	27.8	0.114	25.8	0.107	23.9	0.100	22.0	0.095	20.1	0.087	18.
44	.0011	0.131	29.2	0.124	27.2	0.118	25.3	0.111	23.5	0.104	21.5	0.098	19.
45	.0011	0.142	30.5	0.135	28.6	0.129	26.7	0.122	24.9	0.115	22.9	0.109	21.
46		0.153	31.8	0.146	30.0	0.140	28.1	0.133	26.3	0.127	24.3	0.119	22.
47	.0012	0.165	33.0	0.158	31.2	0.152	29.3	0.145	27.6	0.138	25 7	0.132	24.
48	.0012	0.163 0.177	34.2	0.170	32.4	0.152	30.6	0.143	28.8	0.151	27.0	0.132	25.
49	.0013	0.177	35.3	0.183	33.5	0.176	31.7	0.170	30.0	0.163	28.3	0.157	26.
50	.0013	0.202	36.4	0.196	34.6	0.189	32.9	0.183	31.2	0.176	29.5	0.169	27.
51	•0014	0.216	37.5	0.209	35.7	0.202	34.0	0.196	32.3	0.189	30.7	0.183	29.
	.0014	0.210		0.200		0.202	0 2.0	0.100	02.0	0.100			
52		0.229	38.5	0.223	36.8	0.216	35.1	0.210	33.4	0.203	31.8	0.196	30.
53	.0014	0.244	39.5	0.237	37.8	0.231	36.1	0.224	34.5	0.217	32.9	0.211	31.
54	.0015	0.259	40.5	0.252	38.8	0.245	37.1	0.239	35.5	0.232	34.0	0.226	32.
55	.0015	0.274	41.5	0.267	39.8	0.261	38.1	0.254	36.5	0.247	35.0	0.241	33.
56	4	0.290	42.4	0.283	40.7	0.276	39.1	0.270	37.5	0.263	35.9	0.257	34.
57	.0016	0.306	43.2	0.299	41.6	0.293	40.0	0.286	38.4	0.280	36.9	0.273	35.
58	.0017	0.323	44.1	0.239	42.4	0.233	40.8	0.303	39.3	0.296	37.8	0.273	36.
59	.0017	0.340	44.9	0.334	43.3	0.327	41.7	0.320	40.1	0.230	38.7	0.307	37.
60	.0018	0.358	45.7	0.351	44.1	0.345	42.5	0.338	41.0	0.331	39.5	0.325	38.
61	.0018	0.376	46.4	0.370	44.9	0.363	43.3	0.356	41.8	0.350	40.3	0.343	38.
i	.0019												
62		0.396	47.2	0.389	45.6	0.382	44.1	0.376	42.6	0.369	11.2	0.362	39.
63	.0020	0.415	47.9	0.409	46.4	0.402	44.8	0.395	43.4	0.389	41.9	0.382	40.
64	.0021	0.436	48.6	0.429	47.1	0.422	45.6	0.416	44.1	0.409	42.7	0.402	41.
65	.0021	0.457	49.3	0.450	47.8	0.443	46.3	0.437	44.8	0.431	43.4	0.423	42.
66	.0022	0.478	49.9	0.472	48.4	0.465	47.0	0.458	45.5	0.452	44.1	0.445	42.
67	.0023	0.501	50.6	0.494	49.1	0.487	47.6	0.481	46.2	0.474	44.8	0.467	43.
i		1			I	1			ļ		J		

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t — 1	t', or D	ifference	of Wet	and Dry	Bulb Tl	he r mome	ters.		
meter	Mean Vertical Difference of Force	12°	.0	120	.5	139	.0	139	.5	14	•.0	14	·.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid- ity.
0		Eng. In.	51.0	Eng. In.	10.7	Eng. In	10.2	Eng. In. 0.503	46.9	Eng. In. 0.497	45.5	Eng In. 0.490	44.1
68 69	0.0024	$0.524 \\ 0.547$	$51.2 \\ 51.8$	$0.517 \\ 0.541$	49 .7 50.3	$0.510 \\ 0.534$	48.3	0.503 0.527	47.5	0.497	46.1	0.514	44.8
70	.0024	0.572	52.4	0.565	50.9	0.558	49.5	0.551	48.1	0.545	46.8	0.538	45.
71	.0025	0.597	52.9	0.590	51.5	0.583	50.1	0.577	48.7	0.570	47.4	0.563	46.
72	.0026	0.623	53.5	0.616	52.1	0.609	50.7	0.603	49.3	0.596	48.0	0.589	46.
	.0026												
73	.0027	0.650	54.0	0.643	52.6	0.636	51.3	0.629	49.9	0.623	48.6	0.616	47.
74	.0028	0.677	54.5	0.670	53.2	0.664	51.8	0.657	50.5	0.650	49.2	0.643	47.9
75	.0(129	0.705	55.0	0.699	53.7	0.692	52.3	0.685	51.0	$0.678 \\ 0.708$	49.7	0.672	48.
76	•0630	0.735	55.5	0.728	54.2	0.721	52.9	0.714	51.5 52.1	0.708	50.3 50.8	$0.701 \\ 0.731$	48.
77	.0031	0.765	56.0	0.759	54.7	0.752	53.4	0.745	92.1	0.755	50.0	0.751	49.
78	1	0.796	56.5	0.782	55.2	0.782	53.8	0.775	52.5	0.768	51.3	0.762	50.0
79	.0032	0.927	56.9	0.821	55.6	0.814	54.3	0.807	53.0	0.800	51.8	0.794	50.
80	.0033	0.860	57.3	0.853	56.1	0.847	54.8	0.840	53.5	0.833	52.2	0.826	51.0
81	.0034	0.894	57.8	0.887	56.5	0.880	55.2	0.874	53.9	0.867	52.7	0.860	51.
82	.0033	0.929	58.2	0.922	56.9	0.915	55.6	0.909	54.4	0.902	53.2	0.895	51.9
	.0036									0.00=		0.001	
83	.0037	0.965	58.6	0.958	57.3	0.951	56.1	0.944	54.8	0.937	53.6	0.931	52.
84	.0038	1.002	59.0	0.995	57.7	0.988	56.5	$0.981 \\ 1.019$	$55.2 \\ 55.6$	$0.974 \\ 1.012$	54.4 54.4	0.968 1.005	52.8
$\frac{85}{86}$.0639	1.039	59.4 59.7	1.033	58.1 58.5	1.026 1.065	56.8 57.2	1.019	56.0	1.051	54.S	1.044	53.6
87	.0040	1.119	60.1	1.112	58.8	1.105	57.6	1.099	56.4	1.092	55.2	1.085	54.0
01	.0041	1.113	00.1	1.112	00.0	1.103	31.0	1.055	50.1		00.2	1.000	
88		1.159	60.5	1.152	59.2	1.146	58.0	1.139	56.8	1.132	55.6	1.125	54
89	.0042	1.202	60.9	1.195	59.6	1.188	58.3	1.181	57.1	1.174	56.0	1.167	54.8
90	.0044	1.245	61.3	1.238	59.9	1.231	58.7	1.225	57.5	1.218	56.3	1.211	55.
91	.0045	1.290	61.6	1.283	60.2	1.276	59.0	1.269	57.9	1.263	66.7	1.256	55.0
92		1.336	61.9	1.329	60.6	1.322	59.4	1.315	58.2	1.309	57.0	1.302	55.
93	.0047	1.383	62.2	1.376	60.9	1.370	59.7	1.363	58.5	1.356	57.4	1.349	56.
94	.0049	1.432	62.5	1.425	61.2	1.418	60.0	1.411	58.9	1.404	57.7	1.397	56.
95	.0050	1.482	62.7	1.475	61.5	1.468	60.4	1.461	59.2	1.454	58.1	1.447	57.0
96	.0051	1.533	63.0	1.526	61.8	1.519	60.7	1.512	59.5	1.505	58.4	1.498	57.
97	.0052	1.585	63.3	1.578	62.1	1.571	61.0	1.564	59.8	1.558	58.7	1.551	57.
98	.0054	1.639	63.6	1.632	62.4	1.625	61.3	1.618	60.1	1.612	59.0	1.605	57.
	.0056					i				[
99	.0057	1.695	63.9	1	62.7	1.681	61.6	1.674	60.4	1.667	59.3	1.660	58.
100	.0059	1.752	64.2	1.745	63.0	1.738	62.0	1.731	60.7	1.724	59.6	1.717	58.
101	.0060	1.810	64.4	1.803	63.2	1.797	62.3	1.790	61.0	1.783	59.9	1.776	58.
102	.0062	1.870	61.7	1.863	63.5	1.857	62.6	1.850	61.3	1.843	60.2	1.836	59. 59.
103 104	.0063	1.932	64.9	1.925 1.988	63.8	1.918 1.981	62.9 63.2	1.911 1.974	61.5	1.904 1.967	60.4	1.897 1.960	59.
104	1	1.995	00.2	11.000	64.0	11.991	00.2	11.014	01.0	1.007	00.1	1.000	/

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wet-	Mean												
Bulb	Vertical Difference of Force of Vapor	150	0.0	15	∘.5	16	0.0	16	.5	17	0.0	17	.5
Fahren- heit.	for each	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- nid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela tive Hu- mid ity.
0		Eng. In.		Eng. In		Eng. In.		Eng. In.		Eng. In.		Eng. In.	
32													
33					,			l		ŀ		ŀ	
34						1		ŀ				ľ	
35				Ì				l		ł		1	
36	0.0000	0.016	4.4	ł				l		i		l	
37	0.0009	0.025	6.4	0.018	4.6							l	
38	.0009	0.033	8.3	0.027	6.5	0.020	4.8	0.014	3.2			l	
39	.0009	0.042	10.1	0.036	8.4	0.029	6.7	0.023	5.1	0.016	3.6	0.010	2.
40	.0009	0.051	11.9	0.045	10.1	0.038	8.5	0.032	6.9	0.025	5.4	0.019	3.
41	.0010	0.061	13 6	0.054	11.8	0.048	10.3	0.041	8.7	0.035	7.2	0.028	5.
	.0010												
42	.0010	0.071	15.1	0.064	13.4	0.058	11.9	0.051	10.3	0.044	8.8	0.038	7.
43	.0010	0.081	16.6	0.074	15.0	0.068	13.4	0.061	11.9	0.055	10.4	0.018	9.0
44	.0011	0.091	18.1	0.085	16.5	0.078	15.0	0.072	13.5	0.065	12.0	0.058	10.
45	.0011	0.102	19.6	0.096	18.0	0.089	16.5	0.083	15.0	0.076	13.5	0.069	12.
46		0.114	21.0	0.107	19.4	0.100	17.9	0.094	16.4	0.087	15.0	0.081	13.6
477	.0012	0.125	00.4	0.110	90.0	0.110	19.3	0.106	1~ 0	0.099	10 =	0.092	15
47	.0012	$0.125 \\ 0.137$	$\frac{22.4}{23.8}$	0.119 0.131	20.8 22.2	$0.112 \\ 0.124$	20.7	0.118	17.9 19.3	0.039	16.5 17.9	0.092 0.104	15.1 16.3
48 49	.0013	0.150	25.1	0.131	23.6	$0.124 \\ 0.137$	22.1	0.113	20.7	0.111	19.3	0.104	17.9
50	.0013	0.163	26.4	0.156	24.9	0.150	23.4	0.143	22.0	0.136	$\frac{13.3}{20.6}$	0.130	19.3
51	.0013	0.176	27.6	0.169	26.1	0.163	24.6	0.156	23.2	0.150	21.9	0.143	20.6
•	.0014	0.110	21.0	0.105	2011	0.100		0.100		0.100	21.0		
52		0.190	28.7	0.183	27.3	0.177	25.8	0.170	24.4	0.163	23.1	0.157	21.8
53	.0014 .0015	0.204	29.9	0.197	28.4	0.191	27.0	0.184	25.6	0.178	24.3	0.171	23.0
54	.0015	0.219	30.9	0.212	29.5	0.206	28.1	0.199	26.7	0.192	25.4	0.186	24.
55	.0013	0.234	32.0	0.228	30.6	0.221	29.2	0.214	27.8	0.208	26.5	0.201	25.2
56		0.250	33.0	0.243	31.6	0.237	30.2	0.230	28.9	0.223	27.6	0.217	26.3
57	.0016	0.266	210	0.900	20.6	0.253	31.2	0.246	29.9	0.240	50 C	0.233	27.5
5 7 58	.0017	0.253	34.0 34.9	$0.260 \\ 0.276$	32.6 33.5	$0.233 \\ 0.270$	32.2	$0.240 \\ 0.268$	30.8	$0.240 \\ 0.256$	$28.6 \\ 29.6$	0.233	28.3
59	.0017	0.300	35.S	$0.276 \\ 0.294$	34.4	$0.270 \\ 0.287$	33.1	0.280	31.8	$0.230 \\ 0.274$	30.5	0.249	29.3
60	.0018	0.318	36.7	0.234	35.3	0.305	34.0	0.298	32.7	0.274	31.4	0.285	30.:
61	.0019	0.336	37.5	0.330	36.2	0.323	34.9	0.316	33.6	0.310	32.4	0.303	31.2
0.1	.0019		5	3.660	50.2	0.020	31.0	3.010	35.0		52.4	3.303	
62		0.356	38.4	0.349	37.0	0.342	35.7	0.336	34.5	0.329	33.2	0.322	32.0
63	•0020	0.375	39.2	0.369	37.9	0.362	36.6	0.355	35.3	0.349	34.1	0.312	32.9
64	•0020	0.396	40.0	0.389	38.7	0.382	37.4	0.376	36.1	0.369	34.9	0.362	33.
65	.0021	0.417	40.7	0.410	39.4	0.403	38.2	0.396	36.9	0.390	35.7	0.383	34.5
66	.0022	0.438	41.5	0.431	40.2	0.425	38.9	0.418	37.7	0.411	36.5	0.405	35.
67	•0023	0.460	42.2	0.454	40.9	0.447	39.6	0.440	38.4	0.434	37.2	0.427	36.
				Í		1		i .					

 $\textbf{Temperature, Fahrenheit.} \\ \textbf{—Force of Vapor in English Inches.} \\ \textbf{—Relative Humidity in Hundredths.} \\$

				t — t	', or Di	fference o	of Wet	and Dry I	Bulb Th	nermomet	ers.		
meter	Mean Vertical Difference of Force	150	.0	15	.5	16°	.0	160	.5	170	.0	170	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid ity
68		Eng. In. 0.483	42.8	Eng. In. 0.477	41.6	Eng. In. 0.470	40.3	Eng. In. 0.463	39.1	Eng. In. 0.456	37.9	Eng. In. 0.450	36.5
69	0.0024	0.507	43.5	0.500	42.3	0.594	41.0	0.487	39.8	0.480	38.7	0.473	37.
	.0024			0.524	42.9	0.518	41.7	0.511	40.5	0.504	39.3	0.498	35.
70	.0025	0.531	44.2 44.8		43.6	0.543	42.4	0.536	41.2	0.529	40.0	0.523	38.
71	.0026	0.556		0.550							40.7	0.549	39.
72	.0027	0.582	45.4	0.576	44.2	0.569	43.0	0.562	41.5	0.555	40.7	0.549	99.
73	.0021	0.609	46.0	0.602	44.8	0.596	43.6	0.589	42.4	0.582	41.3	0.575	40.
74	.0028	0.637	46.6	0.630	45.4	0.623	44.2	0.616	43.0	0.610	41.9	0.603	40.
75	.0028	0.665	47.2	0.658	46.0	0.651	44.8	0.645	43.6	0.638	42.5	0.631	41.
	.0029			0.687	46.5	0.681	45.4	0.674	44.2	0.667	43.1	0.660	42.
76	.0030	0.694	47.7			0.031	45.9	0.704	44.8	0.697	43.6	0.690	42.
77	.0031	0.721	48.2	0.717	47.1	0.711	49.9	0.704	44.0	0.037	40.0	0.030	42.
78	.0031	0.755	48.8	0.748	47.6	0.741	46.4	0.735	45.3	0.728	44.2	0.721	43.
79	.0032	0.787	49.3	0.780	48.1	0.773	47.0	0.766	45.8	0.760	44.7	0.753	43.
80	.0033	0.737	49.8	0.730	48.6	0.806	47.5	0.799	46.4	0.792	45.3	0.786	44.
81	.0034	0.820	50.3	0.817	49.1	0.840	48.0	0.833	46.9	0.826	45.8	0.819	44.
	.0035				49.6	0.875		0.868	47.4	0.861	46.3	0.854	45.
82	.0036	0.888	50.7	0.881	49.6	0.875	48.5	0.505	41.4	0.501	40.5	0.554	40.
83	.0030	0.924	51.2	0.917	50.0	0.910	48.9	0.903	47.8	0.897	46.8	0.890	45.0
84	.0037	0.961	51.6	0.954	50.5	0.947	49.4	0.940	48.3	0.933	47.2	0.927	46.
85	.0038	0.998	52.1	0.992	50.9	0.985	49.8	0.978	48.7	0.971	47.7	0.964	46.0
86	.0039	1.037	52.5	1.030	51.3	1.024	50.3	1.017	49.2	1.010	48.1	1.003	47.
	.0040			ı	!	1.024	50.7	1.058	49.6	1.051	48.6	1.044	47.
87	.0041	1.078	52.9	1.071	51.8	1.004	50.7	1.055	49.0	1.031	40.0	1.044	-2.4.
88	.0041	1.118	53.3	1.111	52.2	1.105	51.1	1.098	50.0	1.091	49.0	1.084	48.0
89	.0042	1.161	53.7	1.154	52.6	1.147	51.5	1.140	50.4	1.133	49.4	1.126	48.
90	.0044	1.204	54.1	1.197	53.0	1.190	51.9	1.183	50.9	1.177	49.8	1.170	48.
91	.0045	1.249	54.5	1.242	53.4	1.235	52.3	1.228	51.2	1.221	50.2	1.215	49.
92	.0046		54.8	1.288	53.7	1.281	52.7	1.274	51.6	1.267	50.6	1.260	49.
94	.0048	1.295	94.0	1.200	33.7	1.231	32.1	1.274	91.0	1.207	50.0	1.200	43.
93	.0048	1.342	55.2	1.335	54.1	1.328	53.0	1.321	52.0	1.315	51.0	1.308	50.
94	.0049	1.390	55.5	1.384	54.4	1.377	53.4	1.370	52.4	1.363	51.4	1.356	50.
95	.0050	1.440	55.9	1.433	54.8	1.426	53.7	1.420	52.7	1.413	51.7	1.406	50.
96	.0051	1.491	56.2	1.484	55.1	1.477	54.1	1.471	53.1	1.464	52.1	1.457	51.
97	.0053	1.544	56.5	1.537	55.5	1.530	54.4	1.523	53.4	1.516	52.4	1.509	51.
98	.0054	1.598	56.8	1.591	55.8	1.584	54.8	1.525	53.8	1.570	52.8	1.563	51.
93	00=0	1.050	50.3	1.591	55.5	1.354	04.3	1.577	99.0	1.570		1.505	01.
99	.0056	1.653	57.2	1.646	56.1	1.639	55.1	1.633	54.1	1.626	53.1	1.619	52.
100	.0057	1.710	57.5	1.703	56.4	1.696	55.4	1.690	54.4	1.683	53.4	1.676	52.
101	.0059	1.769	57.S	1.762	56.7	1.755	55.7	1.748	54.7	1.741	53.7	1.734	52.
102	.0060	1.829	58.0	1.822	57.0		56.0	1.809	55.0	1.802	54.0	1.794	53.
102	.0062	1.890	58.3	1.883	57.3	1.876	56.3	1.869	55.3	1.863	54.3	1.856	53.
103	.0063	1.953	58.6	t	57.6	1.939	56.6	1.932	55.6	1.925	54.6	i	53.
104	<u> </u>	1.5.55	00.0	11.340	31.0	11.5.5	30.0	1.304	20.0	1 1.525	34.0	1 1.010	00.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

				t-1	t', or Di	fference o	of Wet	and Dry	Bulb Ti	hermome	ters.		
Wet- Bulb Thermo- meter t'	Mean Vertical Difference of Force	18	∘.0	18	°.5	19	° .0	19	∘.5	20	∘.0	20	°.5
Fahren- heit	of Vapor for each 0°.I.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Ilu- mid- ity	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu mid ity
0		Eng. In.		Eng. In		Eng. In.		Eug. In.		Eng. In.		Eng. In	
32		ł		Į.						1		l	İ
33	1	1		1			ĺ	İ		1		l	ĺ
$\frac{34}{35}$		l						1				l	
36				1						l			
***			ļ			j		1				i	ł
37								l			ĺ		
38						i					ļ	1	
39						ļ		ľ		1		ĺ	
40	0.0010	0.012	2.5	0.015		0.000		ļ					1
41	•0010	0.022	4.3	0.015	3.0	0.009	1.6	1		ĺ		i	
42		0.031	6.0	0.025	4.6	0.018	3.3	0.012	2.1			1	l
43	.0010	0.041	7.6	0.035	6.3	0.028	5.0	0.022	3.7	0.015	2.6		
44	.0011	0.052	9.2	0.045	7.9	0.039	6.6	0.032	5.4	0.026	4.3	0.019	3.
45	.0011 .0011	0.063	10.8	0.056	9.5	0.050	8.2	0.043	7.0	0.037	5.9	0.030	4.8
46		0.074	12.3	0.068	11.0	0.061	9.7	0.054	8.5	0.048	7.5	0.041	6.3
47	.0012	0.086	13.8	0.079	12.5	0.073	11.2	0.066	10.0	0.059	9.0	0.053	7.9
48	.0012	0.098	15.2	0.073	13.9	0.075	12.7	0.078	11.5	0.039	10.4	0.065	9.5
49	.0013	0.110	16.6	0.104	15.4	0.097	14.1	0.091	12.9	0.084	11.9	0.077	10.3
50	.0013	0.123	18.0	0.117	16.7	0.110	15.5	0.103	14.4	0.097	13.2	0.090	12.1
51	•0013	0.136	19.3	0.130	18.0	0.123	16.8	0.117	15.7	0.110	14.5	0.103	13
	•0014									-			
52	.0014	0.150	20.5	0.144	19.3	0.137	18.1	0.130	16.9	0.124	15.7	0.117	14.6
53	.0015	0.164	21.7	0.158	20.5	0.151	19.3	0.145	18.2	0.138	16.9	0.131	15.8
54 55	.0015	0.179	$\frac{22.9}{24.0}$	0.173 0.188	21.7 22.8	0.166 0.181	20.5	$0.159 \\ 0.174$	$19.3 \\ 20.5$	$0.152 \\ 0.168$	18.1 19.2	0.146	17.0
56	.0016	0.194	25.1	0.203	23.9	0.197	$\frac{21.6}{22.7}$	0.174	$\frac{20.5}{21.6}$	0.184	20.4	0.101	19.3
	.0016	0.210	2011	0.200	2010	0.131		01100		01101	2011		
57	1	0.226	26.1	0.220	24.9	0.213	23.8	0.206	22.7	0.200	21.5	0.193	20.4
58	•0017	0.243	27.1	0.236	25.9	0.230	24.8	0.223	23.7	0.217	22.6	0.210	21.5
59	.0017	0.260	28.1	0.254	26.9	0.247	25.8	0.240	24.7	0.234	23.6	0.227	22.6
60	.0018 .0019	0.278	29.0	0.271	27.9	0.265	26.8	0.258	25.7	0.251	24.6	0.245	23.6
61		0.296	30.0	0.290	28.8	0.283	27.7	0.276	26.6	0.270	25.5	0.263	24.5
62	.0019	0.316	30.9	0.309	29.7	0.302	28.6	0.295	27.5	0.289	26.5	0.282	25.4
63	.0020	0.335	31.7	0.328	30.6	0.322	29.5	0.315	28.4	0.308	27.4	0.302	26.4
64	•0020	0.355	32.6	0.349	31.5	0.342	30.4	0.335	29.3	0.329	28.2	0.322	27.2
65	•0021	0.376	33.4	0.370	32.3	0.363	31.2	0.356	30.1	0.350	29.1	0.343	28.1
66	.0022	0.398	34.2	0.391	33.1	0.385	32.0	0.378	30.9	0.371	29.9	0.364	28.9
67	.0023	0.420	34.9	0.414	33.8	0.407	32.8	0.400	31.7	0.393	30.7	0.387	29.7

Temperature, Fahrenheit. — Force of Vapor in English Inches — Relative Humidity in Hundredths.

				$\mathbf{t} - \mathbf{t}$, or Di	fference o	f Wet a	and Dry I	Bulb Th	ermomet	ters.		
	Mean Vertical Difference of Force	180	.0	180	.5	199	·.0	199	.5	200	•.0	20	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Humid
0		Eng. In.		Eng. In.	240	Eng. In.	~~~	Eng. In.	00.5	Eng. In.	01.4	Eng In.	20
68	0.0024	0.443	35.7	0.436	34.6	0.430	33.5	0.423	32.5	0.416	31.4	0.409	30.
69	.0025	0.467	36.4	0.460	35.3	0.453	34.2	0.446	33.2	0.440	32.2	0.433	31.
70	.0025	0.491	37.1	0.484	36.0	0.477	35.0	0.471	33.9	0.464	32.9	0.457	31. 32.
71	.0026	0.516	37.8	0.509	36.7	0.502	35.7	$0.496 \\ 0.522$	34.6 35.3	$0.489 \\ 0.515$	33.6 34.3	0.482 0.508	33.
72	.0026	0.542	38.5	0.535	37.4	0.528	36.3	0.522	59.5	0.515	94.5	0.505	00.
73	1	0.569	39.1	0.562	38.0	0.555	37.0	0.548	36.0	0.542	35.0	0.535	34.
74	.0027	0.596	39.7	0.589	38.7	0.583	37.7	0.576	36.6	0.569	35.7	0.562	34.
75	.0028	0.624	40.3	0.618	39.3	0.611	38.3	0.604	37.3	0.597	36.3	0.591	35.
76	.0029	0.654	40.9	0.647	39.9	0.640	38.9	0.633	37.9	0.627	36.9	0.620	35.
77	.0030	0.683	41.5	0.677	40.5	0.670	39.5	0.663	38.5	0.656	37.5	0.650	36.
• • •	.0031												
78	.0032	0.714	42.1	0.707	41.0	0.701	40.0	0.694	39.0	0.687	38.1	0.680	37.
79	.0032	0.746	42.6	0.739	41.6	0.732	40.6	0.726	39.6	0.719	38.6	0.712	37.
80	.0034	0.779	43.2	0.772	42.1	0.765	41.1	0.758	40.2	0.752	39.2	0.745	38.
81	.0035	0.813	43.7	0.806	42.7	0.799	41.7	0.792	40.7	0.785	39.7	0.779	38.
82		0.847	44.2	0.840	43.2	0.834	42.2	0.827	41.2	0.820	40.2	0.813	39.
	.0036									0.070		0.010	-00
83	.0036	0.883	14.7	0.876	43.7	0.869	42.7	0.863	41.7	0.856	40.7	0.849	39.
84	.0038	0.920	45.2	0.913	44.2	0.906	43.2	0.899	42.2	0.893	41.3	0.886	40.
85	.0639	0.958	45.6	0.951	44.6	0.944	43.7	0.937	42.7	0.930	41.8	0.923	40.
86	.0040	0.996	46.1	0.989	45.1	0.983	44.1	0.976	43.2	0.969	42.3	0.962	41.
87		1.037	46.5	1.030	45.6	1.023	44.6	1.017	43.6	1.010	42.7	1.003	41.
88	.0041	1.077	47.0	1.070	46.0	1.064	45.0	1.057	44.1	1.050	43.2	1.043	42.
89	.0042	1.119	47.4	1.113	46.4	1.106	45.5	1.099	44.5	1.092	43.6	1.085	42.
90	.0043	1.163	47.8	1.156	46.9	1.149	45.9	1.142	45.0	1.136	44.1	1.129	43.
91	.0045	1.208	48.2	1.201	47.3	1.194	46.3	1.187	45.4	1.180	44.5	1.173	43.
92	.0047	1.254	48.6	1.247	47.7	1.240	46.7	1.233	45.8	1.226	44.9	1.219	44.
-	.0048	1.201	10.0			1.210			1				
93		1.301	49.0	1.294	48.1	1.287	47.1	1.280	46.2	1.273	45.3	1.266	44.
94	.0049	1.349	49.4	1.342	48.4	1.335	47.5	1.329	46.6	1.322	45.7	1.315	44.
95	.0050	1.399	49.8	1.392	48.8	1.385	47.9	1.378	47.0	1.371	46.1	1.364	45.
96	.0051	1.450	50.1	1.443	49.2	1.436	48.3	1.429	47.3	1.422	46.5	1.415	45.
97	.0053	1.502	50.5	1.495	49.5	1.489	48.6	1.482	47.7	1.475	46.8	1.468	46.
98	.0054	1.556	50.8	1.549	49.9	1.543	49.0	1.536	48.1	1.529	47.2	1.522	46.
	.0055								40.4	1.50.		1 500	10
99	.0057	1.612	51.2	1.605	50.2	1.598	49.3	1.591	48.4	1.584	47.5	1.577	46.
100	.0058	1.669	51.5	1.662	50.6	1.655	49.7	1.648	48.8	1.641	47.9	1.634	47.
101	.0060	1.727	51.8	1.720	50.9	1.713	50.0	1.706	49.1	1.700	45.2	1.693	47.
102	.0062	1.787	52.2	1.780	51.2	1.773	50.3	1.766	49.4	1.759	48.6	1.753	47.
103	.0063	1.849	52.5	1.842	51.5	1.835	50.7	1.828	49.8	1.821 1.884	48.9 49.2	1.814	48. 48.
101	1	1.912	52.8	1.905	51.9	1.898	51.0	1.891	90.1	1.004	40.4	1.077	40.

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Mean Vertical ifference of Force of Vapor or each 0°.1.	Parce of Vapor.	Relative Humid- ity.	Force of Vapor.	mid- ity.	Force of Vapor.	mid- ity	Force of Vapor.	Relative Hu-midity.	Force of Vapor.	Rela-	Force of Vapor.	Relative Humid ity.
or each	Vapor.	tive Hu- mid- ity.	Vapor.	f Hu- mid- ity.	Vapor.	f Hu- mid- ity	Vapor.	tive Hu- mid- ity.	Vapor.	tive Hu- mid-	Vapor.	tive Hu- mid
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	0.013	2.0	l		ļ		l					
0.0011	0.023	3.7	0.017	2.6	0.010	1.6	1					
.0011	0.035	5.2	0.028	4.2	0.022	3.1	0.015	2.1				
.0012		ĺ				"						
0010	0.046	6.8	0.040	5.7	0.033	4.7	0.027	3.7	0.020	2.7	0.013	1.8
.0012	0.058	8.2	0.052	7.2	0.045	6.2	0.039	5.2	0.032	4.2	0.025	3.3
.0013	0.071	9.7	0.064	8.6	0.058	7.6	0.051	6.6	0.044	5.7	0.038	4.7
.0013	0.084	11.0	0.077	10.0	0.070	9.0	0.064	8.0	0.057	7.1	0.051	6.1
- 1	0.097	12.3	0.090	11.3	0.084	10.3	0.077	9.3	0.070	8.3	0.064	7.4
.0014	0.110	13.5	0.104	12.5	0.097	11.5	0.091	10.6	0.084	9.6	0.077	8.7
.0014	0.125	14.8	0.118	13.7	0.111	12.8	0.105	11.8	0.098	10.9	0.092	9.9
-0015	0.139	16.0	0.133	14.9	0.126	14.0	0.120	13.0	0.113	12.1	0.106	11.2
.0015	0.155	17.1	0.148	16.1	0.141	15.1	0.135	14.2	0.128	13.3	0.121	12.4
.0016	0.170	18.2	0.164	17.2	0.157	16.3	0.150	15.3	0.144	14.4	0.137	13.5
.0016	0.100	10 /	0.100		0.750		0.70=		0.100		0 7 7 0	
.0017			1		1			1	1			14.7
.0017	1						1					15.8 16.9
.0018	- 1		1									17.8
.0019		23.4									(18.8
.0019	1											
l	0.275	24.4	0.269	23.5	0.262	22.4	0.255	21.5	0.249	20.6	0.242	19.7
.0020	0.295	25.3		24.4	0.282	23.3	0.275	22.4	0.268	21.5	0.262	20.7
.0020		26.1	0.309	25.3		24.2	0.295	23.3	0.289	22.4	0.282	21.6
.0021			1			25.1	0.316				- 1	22.4
ł	l l										l l	23.3
.0022	0.550	25.7	0.373	27.8	0.367	26.8	0.360	25.9	0.353	25.0	0.346	24.2
.01	017 018 019 019 020 020 021	0.186 0.203 0.220 0.238 0.295 0.256 0.295 0.295 0.295 0.295 0.295 0.295 0.295 0.295 0.315 0.336 0.338	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					

PSYCHROMETRICAL TABLES.

 $\textbf{Temperature, Fahrenheit.} \\ \textbf{—} \textbf{Force of Vapor in English Inches.} \\ \textbf{—} \textbf{Relative Humidity in Hundredths.}$

				t – t	', or Di	ference o	f Wet a	nd Dry I	Bulb Th	ermomet	ers.		
meter	Mean Vertical Difference of Force	21°	.0	21°	.5	550	.0	22°	.5	230	.0	23°	.5
t' Fahren- heit.	of Vapor for each 0°.1.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Ilu- mid- ity.	Force of Vapor.	Relative Hu- mid- ity.
0		Eng. In.	20.	Eng. In.	20.5	Eng. In.	97 C	Eng. In.	26.7	Eng. In. 0.376	25.8	Eng. In. 0.369	25.0
68	0.0024	0.403	29.5	0.396	28.5	0.389	27.6	0.383			26.6	0.393	25.8
69	.0024	0.426	30.2	0.420	29.3	0.413	28.4	0.406	27.5	0.399	27.4	0.417	26.5
70	.0025	0.451	31.0	0.444	30.1	0.437	29.1	0.430	28.2	0.424	28.1	0.442	27.3
71	.0026	0.476	31.7	0.469	30.8	0.462	29.9	0.455	29.0	0.449			
72	.0020	0.501	32.4	0.495	31.5	0.488	30.6	0.481	29.7	0.475	28.8	0.468	28.0
	.0027			0.531	00.0	0 -1-	91.9	0.500	30.4	0.501	29.5	0.494	28.7
73	.0028	0.528	33.1	0.521	32.2	0.515	31.3	0.508		0.529	30.2	0.522	29.4
74	.0028	0.556	33.8	0.549	32.8	0.542	31.9	0.535	31.1	l .	30.9	0.550	30.0
75	.0029	0.584	34.4	0.577	33.5	0.570	32.6	0.564	31.7	0.557	31.5	0.579	30.7
76	-0030	0.613	35.0	0.606	34.1	0.599	33.2	0.593	32.3	0.586		0.609	31.3
77		0.643	35.6	0.636	34.7	0.629	33.8	0.623	33.0	0.616	32.1	0.609	91.6
	.0031		000	0.00	07.0	0.660	34.4	0.653	33.6	0.647	32.7	0.640	31.9
78	.0032	0.674	36.2	0.667	35.3		35.0	0.685	34.2	0.678	33.3	0.671	32.5
79	•0033	0.705	36.8	0.699	35.9	0.692		i	34.7	0.711	33.9	0.704	33.1
80	.0034	0.738	37.4	0.731	36.5	0.724	35.6	0.718		1	34.5	0.738	33.
81	.0035	0.772	37.9	0.765	37.0	0.758	36.1	0.751	35.3	0.745	35.0	0.772	34.2
82		0.806	38.4	0.800	37.6	0.793	36.7	0.786	35.8	0.779	55.0	0.772	04.2
0.0	.0036	0.040	39.0	0.835	38.1	0.329	37.2	0.822	36.4	0.815	35.5	0.808	34.7
83	.0037	0.842		0.872	38.6	0.865	37.7	0.858	36.9	0.852	36.1	0.845	35.2
84	.0038	0.879	39.5	1	ļ	1	38.2	0.896	37.4	0.889	36.6	0.882	35.8
. 85	.0039	0.917	40.0	0.910	39.1	0.903		l .	37.9	0.928	37.1	0.921	36.3
86	.0040	0.955	40.4	0.948	39.6	0.942	38.7	0.935	i .	0.968	37.5	0.961	36.
87		0.995	40.9	0.988	40.1	0.981	39.2	0.975	38.4	0.903	07.0	0.301	50.
	.0041		47.4	1.029	40.5	1.022	39.7	1.016	38.8	1.009	38.0	1.002	37.5
88	.0042	1.036	41.4	1.023	41.0	1.065	40.1	1.058	39.3	1.051	38.5	1.044	37.
89	.0044	1.078	41.8	1	41.4	1.108	40.6	1.101	39.7	1.094	38.9	1.088	38.
90	.0045	1.122	42.3	1.115	1	1.153	41.0	1.146	40.2	1.139	39.4	1.132	38.
91	.0046	1.166	42.7	1.160	41.9	1	41.4	1.192	40.6	1.185	39.8	1.178	39.
92		1.212	43.1	1.206	42.3	1.199	41.4	1.132	40.0	1.100		1.110	
0.2	.0048	1.260	43.5	1.253	42.7	1.246	41.9	1.239	41.0	1.232	40.2	1.225	39.
93	.0049	8	43.9	1	43.1	1.294	42.3	1	41.4	1.280	40.6	1.274	39.
94	.0050	1.308	44.3		43.5	1.344	42.7	1	41.8	1.330	41.0	1.323	40.
95	.0051	1.358	1	1.402	43.9	1.395	13.0	1	42.2		41.4	1.374	40.
96	.0053	N.	44.7		44.3	3	43.4		42.6		41.8	1.426	41.
97	.0054	1.461	45.1		44.6	1	43.8	1	43.0		42.2	1.480	41.
98		1.515	45.5	1.508	44.0	1.501	10.0	1.454	10.0	1			
99	.0056	1.570	45.8	1.563	45.0	1.556	44.2	1.550	43.4	1.543	42.6	1.536	41.
1	.0057	1.627	1		1	1	44.5		43.7		1	ă.	42.
100	.0059	1.686		1	L	1	44.9	1	1 .	1		1	42.
101	.0060	Я			1		45.2		1	1	1	1	42.
102	.0062	1.746	1		1	1			1 .	1	1	1	43
103	.0063	1.807					1 .		1		1 _	1.535	4
104	1	1.870	47.5	1.863	46.7	1.856	1 4000	11.049	1 10.1	1	1 - 1.0		

 ${\bf Temperature, F.hrenheit. - Force\ of\ Vapor\ in\ English\ Inches. - Relative\ Humidity\ in\ Hundredths.}$

Wet- Bulb Thermo-	Mean Vertical Difference		10.0	1 0	10.5	0.	50 A	0-		1 00		1	
meter t	of Force of Vapor		l°.0	224	1°.5	22.5	5°.0	25	0.5	20	0.0	26	3°.5
Fahren- heit.	for each 0°.1.	Force o Vapor.		Force of		Force o		Force of Vapor.		Force o		Force o	
0		Eng. In		Eng. Ir	1.	Eng. Ir	1.	Eng. In		Eng. In		Eng. In	1
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45				l		1		1		i		1	
46						1							
47										1		l	
48		0.019	2.4	0.012	1.5	1		İ		1		l	
49	0.0013	0.031	3.9	0.025	3.0	0.018	2.2	0.011	1.3	1	1	ł	
50	.0013	0.044	5.2	0.037	4.4	0.031	3.6	0.024	2.7	0.018	2.0	0.011	1.
51	.0013	0.057	6.5	0.051	5.7	0.044	4.9	0.037	4.1	0.031	3.3	0.024	2.
	.0014							i					
52	.0014	0.071	7.8	0.064	7.0	0.058	6.1	0.051	5.3	0.044	4.6	0.038	3.5
53 54	.0015	0.085	9.1	0.078	8.2	0.072	7.4	0.065	6.6	0.058	5.8	0.052	5.
55	.0015	0.100 0.115	10.3 11.5	0.093	9.4	0.086	8.6	0.080	7.8	0.073	7.0	0.067	6.
56	.0016	0.113	12.7	$0.108 \\ 0.124$	10.6 11.8	0.102	9.8	0.095 0.111	$9.0 \\ 10.2$	0.088	8.2	$0.082 \\ 0.097$	7.
"	.0016	0.130	12.7	0.124	11.5	0.117	11.0	0.111	10.2	0.104	9.4	0.097	8.
57		0.147	13.8	0.140	13.0	0.133	12.1	0.127	11.3	0.120	10.6	0.113	9.8
58	.0017	0.163	14.9	0.157	14.1	0.150	13.2	0.143	12.5	0.137	11.7	0.130	10.9
59	.0017	0.180	16.0	0.174	15.2	0.167	14.3	0.161	13.6	0.154	12.8	0.147	12.0
60	.0019	0.198	17.0	0.191	16.1	0.185	15.3	0.178	14.6	0.172	13.8	0.165	13.0
61		0.216	17.9	0.210	17.1	0.203	16.3	0.196	15.5	0.190	14.7	0.183	14.0
62	.0019	0.235	18.9	0.229	18.1	0.222	17.2	0.915	16 5	0.900	15 ~	0.202	15.0
63	•00-00	0.255 0.255	19.8	0.248	19.0	0.222	18.2	$0.215 \\ 0.235$	16.5 17.4	$0.209 \\ 0.228$	15.7 16.6	$0.202 \\ 0.222$	15.9
64	•0020	0.235 0.275	20.7	0.248	19.9	$\begin{array}{c} 0.242 \\ 0.262 \end{array}$	19.1	0.255	18.3	0.248	17.5	0.242	16.8
65	.0021	0.296	21.6	0.289	20.8	0.283	20.0	0.276	19.2	0.249	18.4	0.242	17.7
66	.0022	0.318	22.5	0.311	21.7	0.304	20.9	0.297	20.1	0.291	19.3	0.284	18.6
67	•0023 E	0.340	23.3	0.333	22.5	0.326	21.7	0.320	20.9	0.313	20.2	0.306	19.4

Temperature, Fahrenheit. — Force of Vapor in English Inches. — Relative Humidity in Hundredths.

Wat	Moon			t – t	', or Di	fference o	f Wet a	ind Dry I	Bulb Th	ermomet	ers.		
meter	Mean Vertical Difference of Force of Vapor	24°	.0	24	.5	250	.0	250	.5	26°	.0	26	·.5
t' ahren- heit.	for each 0°.1.	Force of Vapor.	Relative Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity.	Force of Vapor.	Rela- tive Hu- mid- ity	Force of Vapor.	Relative Hu mid ity.
0		Eng. In.	24.2	Eng. In.		Eng. In.	22.5	Eng. In.	21.0	Eng. In.	21.0	Eng In.	00
68	0.0024	0.363	24.2	0.356	23.3	0.349	22.5	0.342	21.8	0.336	21.8	0.329	20.
69	.0024	0.386	24.9	0.379	24.1	0.373	23.3	0.366	22.6	0.359	21.8 22.6	$0.352 \\ 0.377$	21.
70	.0025	$0.410 \\ 0.435$	25.7	0.403	24.9	$0.397 \\ 0.422$	$24.1 \\ 24.9$	0.390	23.3	$0.353 \\ 0.408$	23.3	0.377	21. 22.
71	.0026	9.461	26.4	0.428	25.6	0.422	25.6	$0.415 \\ 0.441$	$\frac{24.1}{24.8}$	0.434	$\frac{23.3}{24.1}$	0.402 0.427	23.
72	.0027	9.401	27.2	0.454	26.4	0.445	29.0	0.441	24.0	0.454	24.1	0.427	روند ا
73	1	0.488	27.9	0.481	27.1	0.474	26.3	0.467	25.5	0.461	21.8	0.454	24.
74	.0028	0.515	28.5	0.508	27.7	0.502	27.0	0.495	26.2	0.488	25.5	0.481	24.
75	.0028	0.543	29.2	0.537	28.4	0.530	27.6	0.523	26.8	0.516	26.1	0.510	25
76	.0029	0.572	29.8	0.566	29.1	0.559	28.3	0.552	27.4	0.545	26.8	0.539	26
77	.0030	0.602	30.5	0.595	29.7	0.589	28.9	0.582	28.0	0.575	27.4	0.568	26
	.0031												
7 8	.0032	0.633	31.1	0.626	30.3	0.619	29.5	0.613	28.7	0.606	28.0	0.599	27.
79	.0033	0.665	31.7	0.658	30.9	0.651	30.1	0.644	29.3	0.638	28.6	0.631	27.
80	.0034	0.697	32.3	0.691	31.5	0.684	30 .7	0.677	29.9	0.670	29.2	0.663	28
81	.0035	0.731	32.8	0.724	32.1	0.717	31.3	0.711	30.5	0.704	29.8	0.697	29
82	ŀ	0.766	33.4	0.759	32.6	0.752	31.8	0.745	31.0	0.738	30.4	0.732	29.
0.0	.0036	0.001	20.0	0 -0-	00.0	0.000	90 (0.701	91.6	0.774	30.9	0.767	30.
83	.0037	0.801	33.9	0.795	33.2	$0.788 \\ 0.824$	32.4 32.9	0.781	31.6	0.774	31.5	0.707	30.
84	.0038	0.838	34.5 35.0	0.831	33.7	$0.824 \\ 0.862$	33.4	$0.818 \\ 0.855$	$32.1 \\ 32.7$	0.811	32.0	0.842	31
85	.0039	0.914	35.5	0.869 0.908	34.2	0.901	33.9	0.894	33.2	0.887	32.5	0.880	31
86 87	.0040	0.954	36.0	0.947	35.2	0.940	34.4	0.934	33.7	0.927	33.0	0.920	32
01	.0041	0.554	30.0	0.947	33.2	0.540	94.4	0.334	99.1	0.521	00.0	0.020	0.2.
88		0.995	36.4	0.988	35.7	0.981	34.9	0.975	34.2	0.968	33.5	0.961	32
89	.0042	1.037	36.9	1.030	36.1	1.024	35.4	1.017	34.7	1.010	33.9	1.003	33.
90	.0044	1.081	37.4	1.074	36.6	1.067	35.8	1.060	35.1	1.053	34.4	1.046	33
91	.0045	1.125	37.8	1.118	37.1	1.112	36.3	1.105	35.6	1.098	34.9	1.091	34.
92	.0046	1.171	38.2	1.164	37.5	1.157	36.7	1.151	36.0	1.144	35.3	1.137	34
	.0048				Ì								
93	.0049	1.218	38.7	1.211	37.9	1.205	37.1	1.198	36.5	1.191	35.7	1.184	35.
94	.0050	1.267	39.1	1.260	38.3	1.253	37.5	1.246	36.9	1.239	36.2	1.232	35.
95	.0051	1.316	39.5	1.309	38.7	1.302	37.9	1.296	37.3	1.289	36.6 37.0	1.282 1.333	35. 36.
96	.0053	1.367	39.9	1.360	39.1	1.353	38.3	1.346	37.7	1.340	37.4	1.385	36
97	.0054	1.420	40.3	1.413	39.5	1.406	38.7 39.1	1.399 1.453	38.1 38.5	1.392 1.446	37.8	1.439	37
98	0050	1.473	40.7	1.467	39.9	1.460	39.1	1.405	90.9	1.440	37.0	1.403	37
99	.0056	1.529	41.1	1.522	40.3	1.515	39.5	1.508	38.9	1.501	38.2	1.494	37.
100	.0657	1.586	41.4	1.579	40.7	1.572	39.9	1.565	39.2	1.558	38.5	1.551	37
101	.0059	1.644	41.8	1.637	41.0	1.630	40.3	1.623	39.6	1.616	38.9	1.609	38
102	.0060	1.704	42.2	1.697	41.4	1.690	40.7	1.683	40.0	1.676	39.3	1.669	38
103	.0062	1.765	42.5	1.758	41.8	1.751	41.0	1.745	40.3	1.738	39.6	1.731	38.
104	.0063	1.828	42.8		42.1	1.814	41.4	1.807	40.7	1.800	40.0	1.793	39.

Correction for Barometrical Height above or below the Normal Height of 29.7 inches.

For				Diffe	rence of	Thermo	meters,	or t-t	. Fahrei	nheit.			
Baromet- rical Height.	20	40	6°	80	10°	12°	14°	16°	180	20°	22°	24°	26
					Wet I	Bulb abo	ve the F	reezing-	Point.		1	<u>'</u>	<u> </u>
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch
31.0	001	002	003	005	006	007	008	009	010	012	013	014	01
30.5	.001	.001	.002	.003	.004	.004	.005	.006	.006	.007	.008	.009	.00
30.0	000	000	001	001	001	002	002	002	002	003	003	003	00
29.5	+.000	+.000	+.001	+.001	+.001	+.001	+.001	+.001	+.002	i	+.002	+.002	+.00
29.0	100.	.001	.002	.003	.003	.004	.004	.005	.006	.006	.007	.008	.00
28.5	.001	.002	.003	.004	.005	.006	.007	.009	.010	.011	.012	.013	.01
28.0	.001	.003	.005	.006	.008	.009	.011	.012	.014	.015	.017	.018	.02
27.5	.002	.004	.006	.007	.010	.012	.014	.016	.018	.020	.022	.024	.02
27.0	.002	.005	.007	.009	012	.014	.017	.019	.022	.024	.027	.029	.03
26.5	.003	.006	.008	.011	.014	.017	.020	.023	.026	.029	.031	.034	.03
26.0	.003	.006	.010	.013	.016	.020	.023	.026	•030	.033	.036	.040	.0
25.5	100.	.007	.011	.014	.019	.022	.025	.030	.034	.037	.041	.045	.04
25.0	.004	.008	.012	.016	.021	.025	.028	.033	.038	.042	.046	.050	.03
24.0	.005	.010	.015	.020	.025	.030	.034	.040	.046	.051	.056	.061	.06
23.0	.006	.012	.018	.023	.030	.035	.041	.047	.054	.060	.066	.072	.07
22.0	.007	.013	.020	.027	.034	.041	.047	.054	.062	.069	.076	.083	.09
21.0	.008	.015	.023	.030	.038	.046	.053	.062	.070	.077	.085	.093	.10
20.0	+.008	+.017	+.026	+.034	+.043	+.051	+.059	+.069	+.078	+.086	+.095	+.104	+.1
			ulb belo					!	!	!	!	1	!
		Fre	ezing-l'o	int.			EXA	MPLI	E OF	CALC	CULA'	rion.	
31.0	001	002	003	004	006		7	Vet Bull	b above	the Frec	zing-Poi	nt.	
30.5	.001	.001	.002	.003	.003	t'	= 62°	F. t-	$-\mathbf{t}' =$	10°.	Barom	= 26.	5 in.
30.0	000	000	001	001	001	T	he larg	e table	s give f	ora mo	ean bar	0-	
29.5	+.000	+.000	+.000	+.001	+.001	met	rical he	ight of	27.9 ir	iches.	\mathbf{Force}	of	Inch
29.0	.001	.001	.002	.002	.003	Var							0.40
28.5	.001	.002	.003	.004	.005	1		correc	-		table, f		
				005		B =	= 26.5 i	nches,	ana 10	•	•	==	0.01
28.0	.001	.003	.004	.005	.007	}	Co	orrected	Force	of Vaj	por	. =	0.41
27.5	.002	.003	.005	.007	.009	,							•
27.0	.002	.004	.006	.008	.011							ı given	
26.5 26.0	.002	.005	.009	.012	.013							ove Psy	
25.5	.003	.007	.010	.013	.016							at plac	
20.0	.005	.001	1.010	.010	.010	l					,	constan	
25.0	.003	.007	.011	.015	.018							n the ta crection	
24.0	.004	.009		.018	.022							differen	
23.0	.005		1	.021	.026							ng the	
	.006	1	1	.024	.030			f the a				ing from	
22.0	11	1		1	1			••				• /	
22.0 21.0	.006	.014	.020	.027	.034	devi	ations	from t	hat me	ean wil	l little	-impai	r th
	11	+.015	1	l .	.034 +.038			from t f the re		ean wil	I little	impai	r

TABLE VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR FROM THE INDICATIONS, IN ENGLISH MEASURES, OF THE DEW-POINT INSTRUMENTS.

The object of every Dew-Point instrument is to ascertain, by causing a part of the apparatus to cool, the temperature at which the vapor contained in the air begins to condense, in the shape of light dew, on the cooled portion of the instrument. It is obvious that this is the temperature at which the atmosphere itself, if cooled likewise, would be fully saturated by the amount of vapor present in the air at the time of the observation.

The temperature of the dew-point being known, all the hygrometrical conditions of the air can be easily deduced from it.

The Absolute Humidity, or the total amount of vapor in the atmosphere, is expressed by the number, in the Tables of Elastic Forces of Vapor, due to that temperature.

The Relative Humidity, or the degree of moisture, being the ratio of the quantity of vapor actually contained in the air to the quantity it could contain if fully saturated, is expressed by the proportion

Relative Humidity: 1:: Force of Vapor at Dew-Point: Maximum Force of Vapor.

Calling the

Force of Vapor at the Temperature of the Dew-Point, f; Force of Vapor at the Temperature of the Air, F;

then

Relative Humidity $= \frac{f}{F}$.

It is thus found by dividing the force of vapor due, in the Table of Elastic Forces, to the temperature of the dew-point, by the maximum of the force of vapor due, in the same table, to the temperature of the air at the time of the observation. F being always greater than f, when the air is not saturated, the Relative Humidity is expressed by a fraction, which is termed the *fraction of saturation*. Making the point of saturation = 100, in order to obtain this fraction in hundredths, we have

Relative Humidity $=\frac{f \times 100}{F}$.

Example.

Suppose the

Temperature of the Air, or t, to be $= 43^{\circ} \text{ F.}$ Temperature of the Dew-Point, or t', to be $= 35^{\circ} \text{ F.}$ Difference between the two, or t - t', to be $= 8^{\circ} \text{ F.}$

Taking in Table VI. the Elastic Forces due to t and t', we have

Force of Vapor at $\mathbf{t}' = \frac{.2037 \times 100}{.2775} = 73.4$, Relative Humidity in Hundredths.

The following Table VIII. gives, in hundredths, the fraction of saturation, or Relative Humidity, corresponding to each degree of t', or of the temperature of the air, from 0° to 104°; and for every half degree of t—t', or of the difference between the temperature of the air and of the dew-point, from 0.°5 to 24.°5. Regnault's Table of Elastic Forces of Vapor, reduced to English measures, has been used in the computation.

Though the fraction of saturation expressed in hundredths indicates the Relative Humidity with sufficient accuracy, the thousandths have been added to facilitate, as remarked above in the preface to the Psychrometrical Tables, the interpolations for any number falling between those given in the table.

USE OF THE TABLE.

Example.

Temperature of Air, or t, being $= 62^{\circ}$ F. Temperature of the Dew-Point, or t', $= 53^{\circ}$ F. Difference, or t-t', $= 9^{\circ}$ F.

Find out the Relative Humidity.

In the column of temperatures, the first on the left, find 62°; on the same horizontal line, in the column headed 9°, is found 72.4, which is the Relative Humidity required.

Should it seem desirable to compute the Relative Humidity for values of t-t' not contained in the table, the factors given below in Table IX. may be used. It may be seen, however, that an interpolation at sight will always suffice for meteorological purposes.

VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR,

FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS.

Relative Humidity expressed in Hundredths, full Saturation being = 100.

remper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	tures of the	Air and o	f the Dew-	Point. — Fa	hrenheit.	
Fahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
0°	100.	97.7	95.4	93.2	91.0	88.9	86.8	84.8	82.8	80.9
1	100.	97.7	95.5	93.3	91.1	89.0	86.9	84.9	82.9	81.0
2	100.	97.7	95.5	93.3	91.2	89.1	87.0	85.0	83.0	81.1
3	100.	97.8	95.5	93.4	91.2	89.2	87.1	85.1	83.1	81.2
4	100.	97.8	95.6	93.4	91.3	89.2	87.2	85.2	83.2	81.3
5	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.3	81.4
6	109.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.3	81.5
7	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.3	83.4	81.5
8	100.	97.8	95.6	93.5	91.3	89.3	87.3	85.3	83.4	81.5
9	100.	97.8	95.6	93.5	91.3	89.3	87.3	85.3	83.4	81.5
10	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.4	81.5
11	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.4	81.6
12	100.	97.8	95.5	93.4	91.3	89.3	87.3	85.4	83.4	81.6
13	100.	97.8	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.6
14	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.7
15	100.	97.7	95.5	93.4	91.3	89.4	87.4	85.5	83.5	81.7
16	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.4	83.5	81.6
17	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.3	83.4	81.6
18	100.	97.7	95.5	93.4	91.3	89.3	87.3	85.3	83.4	81.3
19	100.	97.8	95.5	93.4	91.3	89.3	87.2	85.2	83.3	81.4
	0.0	0.5	1.0	1.5	2.0	2.5	3.0.	3.5	4.0	4.5

femper- ature of Air,		$\mathbf{t} - \mathbf{t}' = 1$	Difference o	f Tempera	tures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
0°	79.0	77.2	75.4	73.6	71.9	70.1	68.5	66.9	65.3	63.
1	79.1	77.3	75.5	73.7	72.0	70.2	68.6	67.0	65.4	63.8
2	79.2	77.4	75.6	73.8	72.1	70.3	68.7	67.1	65.5	64.0
3	79.3	77.5	75.7	73.9	72.2	70.5	68.8	67.2	65.6	64.
4	79.4	77.6	75.8	74.0	72.3	70.6	68.9	67.3	65.7	64.
5	79.5	77.7	75.9	74.1	72.4	70.7	69.1	67.4	65.8	64.
6	79.6	77.8	76.0	74.2	72.5	70.8	69.2	67.6	66.0	64.
7	79.6	77.8	76.0	74.3	72.6	70.9	69.3	67.7	66.1	64.
s	79.6	77.9	76.1	74.4	72.7	71.0	69.4	67.8	66.2	64.
9	79.7	77.9	76.1	74.4	72.7	71.1	69.5	67.9	66.3	64.
10	79.7	77.9	76.2	74.5	72.8	71.2	69.6	68.0	66.4	64.
11	79.7	78.0	76.2	74.5	72.8	71.2	69.6	68.0	66.5	64.
12	79.8	78.0	76.2	74.5	72.9	71.2	69.6	68.0	66.5	65.
13	79.8	78.0	76.3	74.6	72.9	71.3	69.6	68.1	66.5	65.
14	79.8	78.1	76.3	74.6	72.9	71.3	69.6	68.1	66.5	65.
15	79.8	78.1	76.3	74.6	72.9	71.3	69.7	68.1	66.6	65.
16	79.8	78.0	76.2	74.5	72.9	71.2	69.6	68.1	66.5	65.
17	79.7	77.9	76.1	74.5	72.8	71.2	69.6	68.0	66.5	65.
18	79.6	77.8	76.1	74.4	72.7	71.1	69.5	68.0	66.5	65.
19	79.6	77.8	76.0	74.3	72.7	71.1	69.5	68.0	66.4	65.
13				74.0		71.1	03.0	03.0	00.4	
	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.
0°	62.1	60.7	59.2	57.7	56.3	54.9	53.6	52.3	51.0	49.8
1	62.3	60.8	59.3	57.9	56.5	55.1	53.7	52.5	51.2	50.0
$\overline{2}$	62.4	61.0	59.5	58.1	500		53.9	52.7	51.4	50.
		01.0		90.1	56.6	55.3	00.0	02.1	01.1	00.
3	62.6	61.1	59.6	58.2	56.8	55.3 55.5	54.1	52.8	51.5	
3 4	$62.6 \\ 62.7$		1							50.
		61.1	59.6	58.2	56.8	55.5	54.1	52.8	51.5	50. 50.
-1	62.7	61.1 61.3	59.6 59.8	58.2 58.4	56.8 57.0	55.5 55.7	54.1 54.3	52.8 53.0	51.5 51.7	50.3 50.3
4 5	62.7 62.9	61.1 61.3 61.4	59.6 59.8 60.0	58.2 58.4 58.6	56.8 57.0 57.2	55.5 55.7 55.8	54.1 54.3 54.5	52.8 53.0 53.2	51.5 51.7 51.9	50.5 50.5 50.5
4 5 6	62.7 62.9 63.0	61.1 61.3 61.4 61.5	59.6 59.8 60.0 60.1	58.2 58.4 58.6 58.7	56.8 57.0 57.2 57.3	55.5 55.7 55.8 55.9	54.1 54.3 54.5 54.6	52.8 53.0 53.2 53.3	51.5 51.7 51.9 52.0	50.3 50.3 50.3 50.3
4 5 6 7	62.7 62.9 63.0 63.1	61.1 61.3 61.4 61.5 61.7	59.6 59.8 60.0 60.1 60.2	58.2 58.4 58.6 58.7 58.8	56.8 57.0 57.2 57.3 57.4	55.5 55.7 55.8 55.9 56.0	54.1 54.3 54.5 54.6 54.7	52.8 53.0 53.2 53.3 53.4	51.5 51.7 51.9 52.0 52.1	50.3 50.3 50.3 50.3 51.0
4 5 6 7 8	62.7 62.9 63.0 63.1 63.2	61.1 61.3 61.4 61.5 61.7 61.8	59.6 59.8 60.0 60.1 60.2 60.3	58.2 58.4 58.6 58.7 58.8 58.9	56.8 57.0 57.2 57.3 57.4 57.5	55.5 55.7 55.8 55.9 56.0 56.2	54.1 54.3 54.5 54.6 54.7 54.8	52.8 53.0 53.2 53.3 53.4 53.5	51.5 51.7 51.9 52.0 52.1 52.3	50.3 50.3 50.3 50.3 51.3
5 6 7 8 9	62.7 62.9 63.0 63.1 63.2 63.3	61.1 61.3 61.4 61.5 61.7 61.8	59.6 59.8 60.0 60.1 60.2 60.3 60.4	58.2 58.4 58.6 58.7 58.9 59.0	56.8 57.0 57.2 57.3 57.4 57.5 57.6	55.5 55.7 55.8 55.9 56.0 56.2 56.3	54.1 54.3 54.5 54.6 54.7 54.8 54.9	52.8 53.0 53.2 53.3 53.4 53.5 53.6	51.5 51.7 51.9 52.0 52.1 52.3 52.4	50.3 50.3 50.3 50.3 51.3 51.3
5 6 7 8 9	62.7 62.9 63.0 63.1 63.2 63.3	61.1 61.3 61.4 61.5 61.7 61.8 61.9	59.6 59.8 60.0 60.1 60.2 60.3 60.4	58.2 58.4 58.6 58.7 58.9 59.0	56.8 57.0 57.2 57.3 57.4 57.5 57.6	55.5 55.7 55.8 55.9 56.0 56.2 56.3	54.1 54.3 54.5 54.6 54.7 54.8 54.9	52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.8	51.5 51.7 51.9 52.0 52.1 52.3 52.4	50.3 50.3 50.3 50.3 51.3 51.3
5 6 7 8 9	62.7 62.9 63.0 63.1 63.2 63.3	61.1 61.3 61.4 61.5 61.7 61.8 61.9	59.6 59.8 60.0 60.1 60.2 60.3 60.4	58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2	56.8 57.0 57.2 57.3 57.4 57.5 57.6	55.5 55.7 55.8 55.9 56.0 56.2 56.3	54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1	52.8 53.0 53.2 53.3 53.4 53.5 53.6	51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6	50.3 50.3 50.3 50.3 51.3 51.3 51.3
5 6 7 8 9 10 11 12	62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5	61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1	59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6	58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3	56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9	55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6	54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2	52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 53.9 54.0	51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7	50.3 50.3 50.3 50.3 51.3 51.3 51.3 51.3
5 6 7 8 9 10 11 12 13	62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5	61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2	59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.7	58.2 58.4 58.6 58.7 58.8 59.9 59.0 59.1 59.2 59.3 59.3	56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0	55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6	54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3	52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 54.0 54.1	51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8	50.3 50.3 50.3 50.3 51.3 51.3 51.3 51.3 51.3
5 6 7 8 9 10 11 12 13 14	62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5 63.6	61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2 62.3	59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.7 60.8	58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3 59.4	56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1	55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6 56.7	54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4	52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 54.0 54.1 54.2	51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8 52.9	50.3 50.3 50.3 50.3 51.3 51.3 51.3 51.3 51.3
5 6 7 8 9 10 11 12 13 14	62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.5 63.6	61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.2 62.3 62.3	59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.5 60.6 60.6 60.7 60.8 60.8	58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3 59.4	56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1	55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6 56.6 56.7	54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4	52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 54.0 54.1 54.2 54.3	51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8 52.9 53.0 53.0	50.3 50.3 50.3 50.3 51.3 51.3 51.3 51.3 51.3 51.3
5 6 7 8 9 10 11 12 13 14	62.7 62.9 63.0 63.1 63.2 63.3 63.4 63.5 63.5 63.6 63.6	61.1 61.3 61.4 61.5 61.7 61.8 61.9 62.1 62.1 62.1 62.2 62.3	59.6 59.8 60.0 60.1 60.2 60.3 60.4 60.6 60.6 60.6 60.7 60.8	58.2 58.4 58.6 58.7 58.8 58.9 59.0 59.1 59.2 59.3 59.3 59.4	56.8 57.0 57.2 57.3 57.4 57.5 57.6 57.7 57.8 57.9 58.0 58.1	55.5 55.7 55.8 55.9 56.0 56.2 56.3 56.4 56.5 56.6 56.6 56.7	54.1 54.3 54.5 54.6 54.7 54.8 54.9 55.0 55.1 55.2 55.3 55.4	52.8 53.0 53.2 53.3 53.4 53.5 53.6 53.8 54.0 54.1 54.2	51.5 51.7 51.9 52.0 52.1 52.3 52.4 52.5 52.6 52.7 52.8 52.9	50.3 50.3 50.3 50.3 51.3 51.3 51.3 51.3 51.3

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	oifference o	f Temperat	cures of the	Air and o	f the Dew-	Point. — Fa	ahrenheit.	
Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.
0°	48.5	47.3	46.1	45.0	43.9	42.8	41.6	40.6	39.5	38.5
1	48.7	47.5	46.3	45.2	44.0	42.9	41.8	40.8	39.7	38.7
2	48.9	47.7	46.5	45.4	44.2	43.1	42.0	41.0	39.9	38.9
3	49.1	47.9	46.7	45.5	44.4	43.3	42.2	41.2	40.2	39.2
4	49.3	48.1	46.9	45.7	44.6	43.5	42.4	41.4	40.4	39.4
5	49.4	48.2	47.1	45.9	44.8	43.7	42.6	41.6	40.6	39.6
6	49.6	48.4	47.2	46.1	44.9	43.9	42.8	41.8	40.7	39.8
7	49.7	48.5	47.3	46.2	45.1	44.0	42.9	41.9	40.9	39.9
8	49.8	48.7	47.5	46.4	45.3	44.2	43.1	42.1	41.1	40.1
9	50.0	48.8	47.6	46.5	45.4	44.3	43.3	42.2	41.2	40.2
10	50.1	48.9	47.8	46.7	45.6	44.5	43.4	42.4	41.4	40.4
11	50.2	49.0	47.9	46.8	45.7	44.6	43.5	42.5	41.5	40.5
12	50.3	49.1	48.0	46.9	45.8	44.7	43.6	42.6	41.6	40.6
13	50.4	49.2	48.1	47.0	45.9	44.8	43.7	42.7	41.7	40.7
14	50.5	49.3	48.2	47.1	46.0	44.9	43.8	42.8	41.8	40.8
15	50.6	49.4	48.3	47.2	46.1	45.0	43.9	42.9	41.9	40.9
16	50.6	49.5	48.3	47.2	46.1	45.0	44.0	43.0	41.9	41.0
17	50.6	49.5	48.3	47.2	46.1	45.0	44.0	43.0	42.0	41.0
18	50.6	49.5	48.3	47.2	46.2	45.0	44.1	43.1	42.0	41.1
19	50.6	49.5	48.3	47.3	46.2	45.1	44.1	43.1	42.1	41.1
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.
0°	37.5	36.5	35.5	34.6	33.7	32.8	31.9	31.0	30.2	29.3
1	37.7	36.8	35.8	34.8	33.9	33.0	32.1	31.3	30.4	29.6
2	37.9	37.0	36.0	35.1	34.2	33.3	32.4	31.5	30.7	29.9
3	38.2	37.2	36.2	35.3	34.4	33.5	32.6	31.8	30.9	30.1
4	38.4	37.4	36.5	35.6	34.6	33.8	32.9	32.0	31.2	30.4
5	38.6	37.7	36.7	35.8	34.9	34.0	33.1	32.3	31.4	30.6
6	38.8	37.8	36.9	36.0	35.0	34.2	33.3	32.5	31.6	30.8
7	38.9	38.0	37.0	36.1	35.2	34.3	33.5	32.6	31.8	31.0
8	39.1	38.1	37.2	36.3	35.4	34.5	33.6	32.8	32.1	31.2
9	39.2	38.3	37.3	36.4	35.5	34.7	33.8	33.0	32.3	31.4
10	39.4	38.4	37.5	36.6	35.7	34.8	34.0	33.1	32.5	31.6
11	39.5	38.6	37.6	36.7	35.8	35.0	34.1	33.3	32.6	31.7
12	39.6	38.7	37.8	36.9	36.0	35.1	34.2	33.4	32.7	31.8
13	39.8	38.8	37.9	37.0	36.1	35.2	34.4	33.6	32.8	32.6
14	39.9	39.0	38.0	37.1	36.2	35.4	34.5	33.7	32.9	32.1
15	40.0	39.1	38.2	37.3	36.4	35.5	34.7	33.9	33.0	32.2
16	40.0	39.1	38.2	37.3	36.4	35.6	34.7	33.9	33.1	32.3
17	40.1	39.2	38.2	37.4	36.5	35.6	34.8	34.0	33.1	32.4
18	40.1	39.2	38.3	37.4	36.5	35.7	34.8	34.0	33.2	32.4
19	40.2	39.3	38.3	37.5	36.6	35.7	34.9	34.1	33.2	32 5

Temper- ature		$\mathbf{t} - \mathbf{t}' =$	Difference	of Tempera	tures of th	e Air and	of the Dew	-Point. — F	ahrenheit.	
of Air, Sahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.
20°	100.	97.8	95.6	93.4	91.3	89.2	87.2	85.2	83.2	81
21	100.	97.8	95.6	93.4	91.3	89.3	87.3	85.3	83.3	81
22	100.	97.8	95.6	93.5	91.4	89.3	87.3	85.4	83.4	81
23	100.	97.8	95.6	93.5	91.4	89.4	87.4	85.5	83.5	81
24	100.	97.8	95.7	93.5	91.5	89.5	87.5	85.5	83.6	81.
25	100.	97.8	95.7	93.6	91.5	89.5	87.6	85.6	83.7	81.
26	100.	97.8	95.7	93.6	91.6	89.6	87.7	85.7	83.8	82
27	100.	97.9	95.8	93.7	91.7	89.7	87.8	85.9	84.0	82.
28	100.	97.9	95.8	93.8	91.8	89.8	87.9	86.0	84.1	82.
29	100.	97.9	95.9	93.8	91.8	89.9	88.0	86.1	84.2	82.
30	100.	97.9	95.9	93.9	91.9	90.0	88.1	86.2	84.3	82.
31	100.	98.0	96.0	94.0	92.0	90.1	88.2	86.4	84.5	82.
32	100.	98.0	96.0	94.0	92.1	90.2	88.4	86.6	81.7	83.
33	100.	98.0	96.1	94.1	92.2	90.4	88.6	86.7	84.9	83.
34	100.	98.0	96.1	94.2	92.3	90.5	88.7	86.9	85.1	83.
35	100.	98.0	96.1	94.3	92.4	90.6	88.9	87.1	85.3	83.
36	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.1	85.4	83.
37	100.	98.1	96.2	94.3	92.5	90.7	88.9	87.2	85.4	83.
38	100.	98.1	96.2	94.3	92.5	90.7	89.0	87.2	85.5	83.
39	100.	98.1	96.2	94.3	92.5	90.7	89.0	87.2	85.5	83.
40	100.	98.1	96.2	94.4	92.5	90.8	89.0	87.3	85.6	83.
41	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.3	85.7	84.
42	100.	98.1	96.2	94.4	92.6	90.8	89.1	87.4	85.7	84.
43	100.	98.1	96.3	94.4	92.6	90.9	89.2	87.5	85.8	84.
44	100.	98.1	96.3	94.5	92.7	90.9	89.2	87.5	85.9	84.
45	100.	98.1	96.3	94.5	92.7	91.0	89.3	87.6	85.9	84.
46	100.	98.1	96.3	94.5	92.7	91.0	89.3	87.6	86.0	84.
47	100.	98.1	96.3	94.5	92.8	91.0	89.3	87.7	86.0	84.
48	100.	98.2	96.3	94.6	92.8	91.1	89.4	87.7	86.1	84.
49	100.	98.2	96.4	94.6	92.8	91.1	89.4	87.7	86.1	84.
50	100.	98.2	96.4	94.6	92.9	91.1	89.4	87.8	86.2	84.
51	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.8	86.2	84.
52	100.	98.2	96.4	94.6	92.9	91.2	89.5	87.9	86.3	84.
53	100.	98.2	96.4	94.7	92.9	91.2	89.6	87.9	86.3	84.
54	100.	98.2	96.4	94.7	93.0	91.3	89.6	88.0	86.4	84.
55	100.	98.2	96.5	94.7	93.0	91.3	89.7	88.0	86.4	84.
56	100.	98.2	96.5	94.7	93.0	91.4	89.7	88.1	86.5	84.
57	100.	98.2	96.5	94.8	93.1	91.4	89.7	88.1	86.5	85.
58	100.	98.2	96.5	94.8	93.1	91.4	89.8	88.2	86.6	85.0
59	100.	98.2	96.5	94.8	93.1	91.5	89.8	88.2	86.6	85.
60	100.	98.2	96.5	94.8	93.2	91.5	89.9	88.3	86.7	85.
61 62	100. 100.	98.3 98.3	96.5 96.6	94.9	93.2	91.5	89.9	88.3	86.7	85.
			96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.
- 1	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5

emper- ature		$\mathbf{t} - \mathbf{t}' = 1$	Difference (of Tempera	tures of th	e Air and o	of the Dew-	Point. — F	ahrenheit.	
of Air, ahren- heit.	0.0	0.5	1.0	1.5	2.0	2.5	3.0	3.5	4.0	4.5
62°	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.
63	100.	98.3	96.6	94.9	93.2	91.6	90.0	88.4	86.8	85.
64	100.	98.3	96.6	94.9	93.3	91.6	90.0	88.5	86.9	85.
65	100.	98.3	96.6	94.9	93.3	91.7	90.1	88.5	86.9	85.
66	100.	98.3	96.6	94.9	93.3	91.7	90.1	88.5	87.0	85.
67	100.	98.3	96.6	95.0	93.3	91.7	90.1	88.6	87.0	85.
68	100.	98.3	96.6	95.0	93.4	91.8	90.2	88.6	87.1	85.
69	100.	98.3	96.6	95.0	93.4	91.8	90.2	88.7	87.2	85.
70	100.	98.3	96.7	95.0	93.4	91.8	90.3	88.7	87.2	85.
71	100.	98.3	96.7	95.0	93.4	91.9	90.3	88.8	87.2	85.
72	100.	98.3	96.7	95.1	93.5	91.9	90.3	88.8	87.3	85.8
73	100.	98.3	96.7	95.1	93.5	91.9	90.4	88.8	87.3	85.
74	100.	98.3	96.7	95.1	93.5	91.9	90.4	88.9	87.4	85.
75	100.	98.3	96.7	95.1	93.5	92.0	90.4	88.9	87.4	86.
76	100.	98.3	96.7	95.1	93.6	92.0	90.5	89.0	87.5	86.0
77	100.	98.4	96.7	95.2	93.6	92.0	90.5	89.0	87.5	86.
78	100.	98.4	96.7	95.2	93.6	92.1	90.5	89.1	87.6	86.
79	100.	93.4	96.8	95.2	93.6	92.1	90.6	89.1	87.6	86.
so	100.	93.4	96.8	95.2	93.6	92.1	90.6	89.1	87.7	86
81	100.	98.4	96.8	95.2	93.7	92.1	90.6	89.2	87.7	86.
82	100.	98.4	96.8	95.2	93.7	92.2	90.7	89.2	87.8	86.:
83	100.	98.4	96.8	95.3	93.7	92.2	90.7	89.3	87.8	86.
84	100.	98.4	93.8	95.3	93.7	92.2	90.8	89.3	87.8	86
85	100.	93.4	96.8	95.3	93.8	92.3	90.8	89.3	87.9	86.
86	100.	98.4	96.8	95.3	93.8	92.3	90.8	89.4	87.9	86.
87	100.	98.4	96.9	95.3	93.8	92.3	90.9	89.4	88.0	86.6
88	100.	98.4	96.9	95.3	93.8	92.3	90.9	89.4	88.0	86.6
89	100.	98.4	96.9	95.4	93.9	92.4	90.9	89.5	88.1	86.7
90	100.	98.4	96.9	95.4	93.9	92.4	91.0	89.5	88.1	86.7
91	109.	93.4	96.9	95.4	93.9	92.4	91.0	89.6	88.2	86.8
92	100.	98.5	96.9	95.4	93.9	92.5	91.0	89.6	88.2	86.8
93	100.	98.5	96.9	95.4	93.9	92.5	91.1	89.6	88.2	86.9
94	100.	98.5	96.9	95.4	94.0	92.5	91.1	89.7	88.3	86.9
95	100.	98.5	97.0	95.5	91.0	92.5	91.1	89.7	88.3	57.0
96	100.	98.5	97.0	95.5	94.0	92.6	91.2	89.7	88.4	87.0
97	100.	98.5	97.0	95.5	94.0	92.6	91.2	89.8	88.4	87.0
93	100.	98.5	97.0	95.5	94.1	92.6	91.2	89.8	88.4	87.1
99	100.	93.5	97.0	95.5	94.1	92.7	91.3	89.9	88.5	87.1
100	100.	98.5	97.0	95.6	94.1	92.7	91.3	59.9	88.5	87.2
101	100.	98.5	97.0	95.6	94.1	92.7	91.3	89.9	88.6	87.2
102	100.	98.5	97.0	95.6	91.2	92.7	91.4	90.0	88.6	87.3
103	100.	98.5	97.0	95.6	94.2	92.8	91.4	90.0	88.7	87.3
104	100.	98.5	97.0	95.6	91.2	92.8	91.4	90.0	88.7	87.4
:		0.5								

Cemper- ature		$\mathbf{t} - \mathbf{t}' = 1$	Difference o	f Tempera	tures of the	e Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
20°	79.5	77.7	75.9	74.2	72.6	71.0	69.4	67.9	66.4	64.9
21	79.6	77.8	76.0	74.3	72.7	71.1	69.5	68.0	66.4	65.0
22	79.7	77.9	76.1	74.4	72.8	71.2	69.6	68.0	66.5	65.0
23	79.8	78.0	76.2	74.6	72.9	71.3	69.6	68.1	66.5	65.0
24	79.9	78.1	76.4	74.7	73.0	71.4	69.7	68.1	66.6	65.1
25	80.0	78.2	76.5	74.8	73.1	71.5	69.8	68.2	66.6	65.1
26	80.2	78.4	76.6	74.9	73.2	71.7	70.0	68.4	66.8	65.3
27	80.3	78.5	76.8	75.1	73.4	71.8	70.1	68.6	67.0	65.5
28	80.5	78.7	76.9	75.2	73.6	72.0	70.3	68.8	67.2	65.7
29	80.6	78.8	77.1	75.4	73.7	72.1	70.5	68.9	67.4	65.9
30	80.7	78.9	77.2	75.6	73.9	72.3	70.7	69.1	67.6	66.1
31	81.0	79.2	77.5	75.8	74.2	72.6	71.0	69.4	67.9	66.4
32	81.2	79.4	77.7	76.1	74.4	72.8	71.3	69.7	68.2	66.7
33	81.4	79.7	78.0	76.4	74.7	73.1	71.5	70.0	68.5	67.0
34	81.7	79.9	78.3	76.6	75.0	73.4	71.8	70.3	68.8	67.3
35	81.9	80.2	78.5	76.9	75.3	73.7	72.1	70.6	69.1	67.6
36	82.0	80.3	78.6	77.0	75.4	73.9	72.3	70.8	69.3	67.8
37	82.0	80.4	78.8	77.2	75.6	74.0	72.5	71.0	69.5	68.1
38	82.1	80.5	78.9	77.3	75.8	74.2	72.7	71.2	69.8	68.3
39	82.2	80.6	79.0	77.4	75.9	74.4	72.9	71.5	70.0	68.6
40	82.3	80.7	79.1	77.6	76.1	74.6	73.2	71.7	70.2	68.8
41	82.4	80.8	79.2	77.7	76.2	74.7	73.2	71.8	70.3	68.9
42	82.5	80.9	79.3	77.8	76.3	74.8	73.3	71.9	70.5	69.0
43	82.5	80.9	79.4	77.9	76.4	74.9	73.4	72.0	70.6	69.2
44	82.6	81.0	79.5	78.0	76.5	75.0	73.5	72.1	70.7	69.3
45	82.7	81.1	79.6	78.0	76.5	75.1	73.6	72.2	70.8	69.4
46	82.8	81.2	79.6	78.1	76.6	75.1	73.7	72.3	70.9	69.5
47	82.8	81.2	79.7	78.2	76.7	75.2	73.S	72.4	71.0	69.6
48	82.9	81.3	79.8	78.2	76.8	75.3	73.9	72.5	71.1	69.7
49	82.9	81.3	79.8	78.3	76.8	75.4	74.0	72.6	71.2	69.8
50	83.0	81.4	79.9	78.4	76.9	75.5	74.0	72.7	71.3	69.9
51	83.0	81.5	80.0	78.5	77.0	75.5	74.1	72.8	71.4	70.0
52	83.1	81.5	80.0	78.5	77.1	75.6	74.2	72.8	71.5	70.1
53	83.2	81.6	80.1	78.6	77.2	75.7	74.3	72.9	71.6	70.2
54	83.2	81.7	80.2	78.7	77.2	75.8	74.4	73.0	71.7	70.3
55 56	83.3 83.4	81.8 81.8	80.3 80.3	78.8 78.9	77.3	75.9 76.0	74.5 74.6	73.1 73.2	71.8 71.9	70.4
						İ				
57 58	$83.4 \\ 83.5$	81.9 82.0	80.4 80.5	78.9 79.0	77.5 77.6	76.1 76.2	74.7 74.8	73.3 73.4	72.0 72.1	70.6
59	83.6	82.0	80.6	79.1	77.7	76.2	74.9	73.5	72.2	70.9
60	83.6	82.1	80.6	79.2	77.7	76.3	75.0	73.6	72.3	71.0
61	83.7	82.2	80.7	79.2	77.8	76.4	75.0	73.7	72.4	71.0
62	83.7	82.2	80.8	79.3	77.9	76.5	75.1	73.8	72.4	71.1
	5.0	5.5				i				,

Temper- ature	•	$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	of Tempera	tures of the	e Air and o	of the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5
62°	83.7	82.2	80.8	79.3	77.9	76.5	75.1	73.8	72.4	71.1
63	83.8	82.3	80.8	79.4	78.0	76.6	75.2	73.9	72.5	71.2
64	83.9	82.4	80.9	79.5	78.1	76.7	75.3	74.0	72.6	71.3
65	83.9	82.4	81.0	79.6	78.1	76.8	75.4	74.0	72.7	71.4
66	84.0	82.5	81.1	79.6	78.2	76.8	75.5	74.1	72.8	71.5
67	84.0	82.6	81.1	79.7	78.3	76.9	75.6	74.2	72.9	71.6
68	84.1	82.6	81.2	79.8	78.4	77.0	75.7	74.3	73.0	71.7
69	84.2	82.7	81.3	79.9	78.5	77.1	75.7	74.4	73.1	71.8
70	84.2	82.8	81.3	79.9	78.5	77.2	75.8	74.5	73.2	71.9
71	84.3	82.8	81.4	80.0	78.6	77.3	75.9	74.6	73.3	72.0
72	84.3	82.9	81.5	80.1	78.7	77.3	76.0	74.7	73.4	72.1
73	84.4	83.0	81.5	80.1	78.7	77.4	76.1	74.8	73.5	72.2
74	84.5	83.0	81.6	80.2	78.8	77.5	76.2	74.9	73.6	72.3
75	84.5	83.1	81.7	80.3	78.9	77.6	76.2	74.9	73.7	72.4
76	84.6	83.1	81.7	80.4	78.9	77.7	76.3	75.0	73.7	72.5
77	84.6	83.2	81.8	80.4	79.0	77.7	76.4	75.1	73.8	72.6
78	84.7	83.3	81.9	80.5	79.1	77.S	76.5	75.2	73.9	72.7
79	84.7	83.3	81.9	80.6	79.1	77.9	76.6	75.3	74.0	72.8
80	84.8	83.4	82.0	80.6	79.2	78.0	76.7	75.4	74.1	72.9
81	84.9	83.5	82.1	80.7	79.3	78.0	76.7	75.5	74.2	73.0
82	84.9	83.5	82.1	80.8	79.4	78.1	76.8	75.5	74.3	73.0
83	85.0	83.6	82.2	80.8	79.4	78.2	76.9	75.6	74.4	73.1
84	85.0	83.6	82.3	80.9	79.5	78.3	77.0	75.7	74.5	73.2
85	85.1	83.7	82.3	81.0	79.6	78.4	77.1	75. 8	74.6	73.3
86	85.1	83.7	82.4	81.1	79.7	78.4	77.1	75.9	74.6	73.4
87	85.2	83.8	82.5	81.1	79.8	78.5	77.2	76.0	74.7	73.5
88	85.2	83.9	82.5	81.2	79.9	78.6	77.3	76.1	74.8	73.6
89	85.3	83.9	82.6	81.3	79.9	78.7	77.4	76.1	74.9	73.7
90	85.3	84.0	82.6	81.3	80.0	78.7	77.5	76.2	75.0	73.8
91	85.4	84.0	82.7	81.4	80.1	78.S	77.5	76.3	75.1	73.9
92	85.4	84.1	82.8	81.5	80.2	78.9	77.6	76.4	75.2	74.0
93	85.5	84.2	82.8	81.5	80.2	79.0	77.7	76.5	75.2	74.0
94	85.6	84.2	82.9	81.6	80.3	79.0	77.8	76.6	75.3	74.1
95	85.6	84.3	83.0	81.7	80.4	79.1	77.9	76.6	75.4	74.2
96	85.7	84.3	83.0	81.7	80.4	79.2	77.9	76.7	75.5	74.3
97	85.7	84.4	83.1	81.8	80.5	79.3	78.0	76.8	75.6	74.4
93	85.8	84.4	83.1	81.9	80.6	79.3	78.1	76.9	75.7	74.5
99	85.8	84.5	83.2	81.9	80.7	79.4	78.2	77.0	75.8	74.6
100	85.9	84.6	83.3	82.0	80.7	79.5	78.3	77.0	75.8	74.7
101	85.9	84.6	83.3	82.0	80.8	79.6	78.3	77.1	75.9	74.8
102	86.0	84.7	83.4	82.1	80.9	79.6	78.4	77.2	76.0	74.9
103	86.0	84.7	83.4	82.2	80.9	79.7	78.5	77.3	76.1	74.9
104	86.1	84.8	83.5	82.2	81.0	79.8	78.6	77.4	76.2	75.0
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	ifference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — Fa	hrenheit.	
of Air, Fahr n- heit.	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5
20°	63.5	62.1	60.6	59.3	58.0	56.6	55.4	54.1	52.9	51.7
21	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.2	53.0	51.8
22	63.5	62.1	60.7	59.4	58.0	56.7	55.5	54.2	53.0	51.8
23	63.6	62.1	60.7	59.4	58.0	56.7	55.5	54.3	53.0	51.9
24	63.6	62.1	60.7	59.4	58.1	56.8	55.5	54.3	53.1	51.9
25	63.6	62.1	60.7	59.4	58.1	56.8	55.6	54.4	53.1	52.0
26	63.8	62.3	60.9	59.6	58.3	57.0	55.7	54.5	53.3	52.1
27	61.0	62.5	61.1	59.8	58.5	57.2	55.9	54.6	53.4	52.2
28	64.2	62.7	61.3	60.0	58.6	57.3	56.0	54.8	53.5	52.3
29	64.4	63.0	61.5	60.2	58.8	57.5	56.2	54.9	53.7	52.4
30	64.6	63.2	61.8	60.4	59.0	57.7	56.3	55.1	53.8	52.6
31	64.9	63.5	62.1	60.7	59.3	58.0	56.6	55.4	54.1	52.9
32	65.2	63.8	62.4	61.0	59.6	58.3	57.0	55.7	54.4	53.2
33	65.5	64.1	62.7	61.3	59.9	58.6	57. 3	56.0	54.7	53.5
34	65.8	64.4	63.0	61.6	60.2	58.9	57.6	56.3	55.0	53.8
35	66.1	64.7	63.3	61.9	60.5	59.2	57.9	56.6	55.4	54.1
36	66.4	64.9	63.5	62.1	60.8	59.5	58.2	56.9	55.6	51.4
37	66.6	65.2	63.8	62.4	61.1	59.8	58.5	57.2	55.9	54.7
38	66.9	65.5	64.1	62.7	61.4	60.1	58.8	57.5	56.2	55.0
39	67.1	65.7	64.4	63.0	61.7	60.3	59.1	57.8	56.5	55.3
40	67.4	66.0	64.6	63.3	62.0	60.6	59.4	58.1	56.8	55.6
41	67.5	66.1	64.8	63.5	62.1	60.9	59.6	58.3	57.1	55.9
42	67.7	66.3	65.0	63.6	62.3	61.1	59.8	58.6	57.3	56.1
43	67.8	66.4	65.1	63.8	62.5	61.3	60.0	58.8	57.6	56.4
41	67.9	66.6	65.3	64.0	62.7	61.5	60.3	59.0	57.8	56.6
45	68.1	66.7	65.4	64.2	62.9	61.7	60.5	59.3	58.1	56.9
46	63.2	66 9	65.6	64.3	63.0	61.8	60.6	59.4	58.2	57.0
47	68.3	67.0	65.7	64.4	63.2	61.9	60.7	59.5	58.3	57.2
48	68.4	67.1	65.8	64.5	63.3	62.0	60.8	59.6	58.5	57.3
49	68.5	67.2	65.9	61.6	63.4	62.1	61.0	59.8	58.6	57.4
50	68.6	67.3	66.0	64.7	63.5	62.2	61.1	59.9	58.7	57.6
51	68.7	67.4	66.1	64.9	63.6	62.4	61.2	60.0	58.9	57.7
52	63.8	67.5	66.2	65.0	63.7	62.5	61.3	60.1	59.0	57.8
53	68.9	67.6	66.4	65.1	63.9	62.6	61.4	60.3	59.1	58.0
54	69.0	67.7	66.5	65.2	64.0	62.7	61.6	60.4	59.2	58.1
55	69.1	67.S	66.6	65.3	64.1	62.9	61.7	60.5	59.4	58.2
56	69.2	67.9	66.7	65.4	64.2	63.0	61.8	60.6	59.5	58.4
57	69.3	68.1	66.8	65.6	64.3	63.1	61.9	60.8	59.6	58.5
58	69.5	68.2	66.9	65.7	61.4	63.2	62.1	60.9	59.8	58.6
59	69.6	68.3	67.0	65.8	64.6	63.4	62.2	61.0	59.9	58 8
60	69.7	68.4	67.1	65.9	64.7	63.5	62.3	61.2	60.0	58.9
61	69.8	68.5	67.2	66.0	64.8	63.6	62.4	61.3	60.1	59.0
62	69.9	63.6	67.4	66.1	64.9	63.7	62.6	61.4	60.3	59.1
	10.0	10.5	11.0		12.0		13.0	13.5	14.0	

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}^{i} = \mathbf{I}$	Difference of	f Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	10.0	10.5	11.0	11.5	12.0	12.5	13.0	13.5	14.0	14.5
62°	69.9	68.6	67.4	66.1	64.9	63.7	62.6	61.4	60.3	59.1
63	70.0	68.7	67.5	66.2	65.0	63.8	62.7	61.5	60.4	59.3
64	70.1	68.8	67.6	66.3	65.1	64.0	62.8	61.6	60.5	59.4
65	70.2	68.9	67.7	66.5	65.3	64.1	62.9	61.8	60.6	59.5
66	70.3	69.0	67.8	66.6	65.4	64.2	63.0	61.9	60.8	59.7
67	70.4	69.1	67.9	66.7	65.5	64.3	63.2	62.0	60.9	59.8
68	70.5	69.2	68.0	66.8	65.6	64.4	63.3	62.1	61.0	59.9
69	70.6	69.3	68.1	66.9	65.7	64.5	63.4	62.3	61.1	60.0
70	70.7	69.4	68.2	67.0	65.8	64.7	63.5	62.4	61.3	60.2
71	70.8	69.5	68.3	67.1	65.9	64.8	63.6	62.5	61.4	60.3
72	70.9	69.6	68.4	67.2	66.0	64.9	63.7	62.6	61.5	60.4
73	71.0	69.7	68.5	67.3	66.2	65.0	63.9	62.7	61.6	60.5
74	71.1	69.8	68.6	67.4	66.3	65.1	64.0	62.8	61.7	60.7
75	71.1	69.9	68.7	67.5	66.4	65.2	64.1	63.0	61.9	60.8
76	71.2	70.0	68.8	67.6	66.5	65.3	64.2	63.1	62.0	60.9
77	71.3	70.1	68.9	67.8	66.6	65.5	64.3	63.2	62.1	61.0
78	71.4	70.2	69.0	67.9	66.7	65.6	64.4	63.3	62.2	61.1
79	71.5	70.3	69.1	68.0	66.8	65.7	64.5	63.4	62.3	61.3
80	71.6	70.4	69.2	68.1	66.9	65.8	64.7	63.6	62.5	61
81	71.7	70.5	69.3	68.2	67.0	65.9	64.8	63.7	62.6	61.5
82	71.8	70.6	69.4	68.3	67.1	66.0	64.9	63.8	62.7	61.6
83	71.9	70.7	69.5	68.4	67.2	66.1	65.0	63.9	62.8	61.8
84	72.0	70.8	69.6	68.5	67.3	66.2	65.1	64.0	62.9	61.9
85	72.1	70.9	69.7	68.6	67.4	66.3	65.2	64.1	63.0	62.0
86	72.2	71.0	69.8	68.7	67.5	66.4	65.3	64.2	63.2	62.1
87	72.3	71.1	69.9	68.8	67.7	66.5	65.4	64.4	63.3	62.2
88	72.4	71.2	70.0	68.9	67.8	66.6	65.5	64.5	63.4	62.3
89	72.5	71.3	70.1	69.0	67.9	66.8	65.7	64.6	63.5	62.5
90	72.6	71.4	70.2	69.1	68.0	66.9	65.8	64.7	63.6	62.6
91	72.7	71.4	70.3	69.2	68.1	67.0	65.9	64.8	63.7	62.7
92	72.8	71.5	70.4	69.3	68.2	67.1	66.0	64.9	63.9	62.8
93	72.9	71.6	70.5	69.4	68.3	67.2	66.1	65.0	64.0	62.9
94	72.9	71.7	70.6	69.5	68.4	67.3	66.2	65.1	64.1	63.0
95	73.0	71.8	70.7	69.6	68.5	67.4	66.3	65.2	64.2	63.2
96	73.1	71.9	70.8	69.7	68.6	67.5	66.4	65.4	64.3	63.8
97	73.2	72.0	70.9	69.8	68.7	67.6	66.5	65.5	64.4	63.4
98	73.3	72.1	71.0	69.9	68.8	67.7	66.6	65.6	64.5	63.5
99	73.4	72.3	71.1	70.0	68.9	67.8	66.7	65.7	64.6	63.6
100	73.5	72.4	71.2	70.1	69.0	67.9	66.8	65.8	64.8	63.7
101	73.6	72.5	71.3	70.2	69.1	68.0	67.0	65.9	64.9	63.9
102	73.7	72.6	71.4	70.3	69.2	68.1	67.1	66.0	65.0	64.0
103	73.8	72.7	71.5	70.4	69.3	68.2	67.2	66.1	65.1	64.1
104	73.9	72.8	71.6	70.5	69.4	68.3	67.3	66.2	65.2	64.2
	10.0	10.5		11.5				_		

hren- leit.	150		100	105	1 20	1 N F	100	10.	100	
ieit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	15
20°	50.6	49.5	48.4	47.3	46.2	45.1	44.1	43.1	42.1	4
21	50.6	49.5	48.4	47.3	46.2	45.1	44.2	43.2	42.2	4
22	50.7	49.5	48.4	47.4	46.3	45.2	44.2	43.2	42.2	41
23	50.7	49.6	48.5	47.4	46.3	45.2	44.2	43.3	42.3	41
24	50.7	49.6	48.5	47.4	46.4	45.3	44.3	43.3	42.3	41
25	50.8	49.7	48.5	47.5	46.4	45.4	44.3	43.3	42.4	41
26	50.9	49.3	48.6	47.6	46.5	45.4	44.4 *	43.4	42.4	41
27	51.0	49.9	48.7	47.7	46.6	45.5	44.5	43.5	42.5	41
28	51.1	50.0	48.8	47.7	46.7	45.6	44.6	43.6	42.6	4]
29	51.2	50.1	48.9	47.8	46.8	45.7	44.7	43.7	42.7	41
30	51.4	50.2	49.0	47.9	46.8	45.8	44.7	43.7	42.7	41
31	51.7	50.5	49.4	48.2	47.1	46.1	45.0	44.0	43.0	42
32	52.0	50.8	49.7	48.5	47.4	46.4	45.3	44.3	43.3	42
33	52.3	51.1	50.0	48.8	47.7	46.6	45.6	44.5	43.5	42
34	52.6	51.4	50.3	49.1	48.0	46.9	45.9	44.8	43.8	42
35	52.9	51.7	50.6	49.4	48.3	47.2	46.1	45.1	44.1	43
36	53.2	52.0	50.9	49.7	48.6	47.5	46.4	45.4	44.4	43
37	53.5	52.3	51.2	50.0	48.9	47.8	46.7	45.7	44.7	43
33	53.8	52.6	51.5	50.3	49.2	48.1	47.0	46.0	45.0	43
39	54.1	52.9	51.8	50.6	49.5	48.4	47.3	46.3	45.3	44
40	54.4	53.2	52.1	50.9	49.8	48.7	47.6	46.6	45.6	44
41	54.7	53.5	52.3	51.2	50.1	49.0	47.9	46.9	45.8	44
42	54.9	53.S	52.6	51.5	50.4	49.3	48.2	47.2	46.1	45
43	55.2	54.0	52.9	51.8	50.7	49.6	48.5	47.5	46.4	45
44	55.5	54.3	53.2	52.1	50.9	49.9	48.8	47.7	46.7	45
45	55.7	54.6	53.4	52.3	51.2	50.2	49.1	48.0	47.0	46
46	55.9	54.7	53.6	52.5	51.4	50.4	49.3	48.3	47.2	46
47	56.0	54.9	53.8	52.7	51.6	50.6	49.5	48.5	47.5	46
48	56.2	55.0	54.0	52.9	51.8	50.8	49.8	48.7	47.7	46
49	56.3	55.2	54.1	53.1	52.0	51.0	50.0	49.0	47.9	47
50	56.5	55.4	54.3	53.2	52.2	51.2	50.2	49.2	48.2	47
51	56.6	55.5	54.4	53.4	52.3	51.3	50.3	49.3	48.3	47
52	56.7	55.6	54.6	53.5	52.5	51.5	50.5	49.5	48.5	47
53	56.9	55.8	54.7	53.6	52.6	51.6	50.6	49.6	48.6	47
54	57.0	55.9	54.8	53.8	52.7	51.7	50.7	49.8	48.8	47
55	57.1	56.0	55.0	53.9	52.9	51.9	50.9	49.9	48.9	48
56	57.3	56.2	55.1	54.1	53.0	52.0	51.0	50.0	49.1	48
57	57.4	56.3	55.2	54.2	53.2	52.2	51.2	50.2	49.2	48
58	57.5	56.4	55.4	54.3	53.3	52.3	51.3	50.3	49.4	48
59	57.7	56.6	55.5	54.5	53.4	52.4	51.4	50.5	49.5	48
60	57.8	59.7	55.6	54.6	53.6	52.6	51.6	50.6	49.7	48
61	57.9	56.8	55.8	54.7	53.7	52.7	51.7	50.8	49.8	48
62	58.0	57.0	55.9	54.9	53.8	52.8	51.9	50.9	49.9	49

Temper-		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Tempera	tures of the	e Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.
62°	58.0	57.0	55.9	54.9	53.8	52.8	51.9	50.9	49.9	49.0
63	58.2	57.1	56.0	55.0	54.0	53.0	52.0	51.0	50.1	49.1
64	58.3	57.2	56.2	55.1	54.1	53.1	52.1	51.2	50.2	49.3
65	58.4	57.4	56.3	55.3	54.3	53.3	52.3	51.3	50.4	49.4
66	58.6	57.5	56.4	55.4	54.4	53.4	52.4	51.5	50.5	49.6
67	58.7	57.6	56.6	55.5	54.5	53.5	52.6	51.6	50.6	49.7
68	58.8	57.8	56.7	55.7	54.7	53.7	52.7	51.7	50.8	49.9
69	59.0	57.9	56.8	55.8	54.8	53.8	52.8	51.9	50.9	50.0
70	59.1	58.0	57.0	55.9	54.9	53.9	53.0	52.0	51.1	50.1
71	59.2	58.2	57.1	56.1	55.1	54.1	53.1	52.1	51.2	50.3
72	59.3	58.3	57.2	56.2	55.2	54.2	53.2	52.3	51.3	50.4
73	59.5	58.4	57.4	56.3	55.3	54.3	53.4	52.4	51.5	50.€
74	59.6	58.5	57.5	56.5	55.5	54.5	53.5	52.6	51.6	50.7
75	59.7	58.7	57.6	56.6	55.6	54.6	53.6	52.7	51.7	50.8
76	59.8	58.8	57.8	56.7	55.7	54.7	53.8	52.8	51.9	51.0
77	60.0	58.9	57.9	56.9	55.9	54.9	53.9	53.0	52.0	51.
78	60.1	59.1	58.0	57.0	56.0	55.0	54.0	53.1	52.2	51.2
79	60.2	59.2	58.1	57.1	56.1	55.1	54.2	53.2	52.3	51
80	60.3	59.3	58.3	57.3	56.3	55.3	54.3	53.4	52.4	51.5
81	60.5	59.4	58.4	57.4	56.4	55.4	54.5	53.5	52.6	51.7
82	60.6	59.6	58.5	57.5	56.5	55.5	54.6	53.6	52.7	51.8
83	60.7	59.7	58.6	57.6	56.6	55.7	54.7	53.8	52.8	51.9
84	60.8	59.8	58.8	57.8	56.8	55.8	54.8	53.9	53.0	52.1
85	60.9	59.9	58.9	57.9	56.9	55.9	55.0	54.0	53.1	52.2
86	61.1	60.0	59.0	58.0	57.0	56.1	55.1	54.2	53.2	52.3
87	61.2	60.2	59.1	58.1	57.2	56.2	55.2	54.3	53.4	52.5
88	61.3	60.3	59.3	58.3	57.3	56.3	55.4	54.4	53.5	52.6
89	61.4	60.4	59.4	58.4	57.4	56.5	55.5	54.6	53.7	52.7
90	61.6	60.5	59.5	58.5	57.6	56.6	55.6	54.7	53.8	52.9
91	61.7	60.7	59.6	58.7	57.7	56.7	55.8	54.8	53.9	53.0
92	61.8	60.8	59.8	58.8	57.8	56.9	55.9	55.0	54.1	53.2
93	61.9	60.9	59.9	58.9	57.9	57.0	56.0	55.1	54.2	53.3
94	62.0	61.0	60.0	59.0	58.1	57.1	56.2	55.2	54.3	53.4
95	62.1	61.1	60.1	59.2	58.2	57.2	56.3	55.4	54.5	53.6
96	62.3	61.3	60.3	59.3	58.3	57.4	56.4	55.5	54.6	53.7
97	62.4	61.4	60.4	59.4	58.4	57.5	56.5	55.6	54.7	53.8
98	62.5	61.5	60.5	59.5	58.6	57.6	56.7	55.8	54.9	54.0
99	62.6	61.6	60.6	59.6	58.7	57.7	56.8	55.9	55.0	54.1
100	62.7	61.7	60.7	59.8	58.8	57.9	56.9	56.0	55.1	54.2
101	62.8	61.9	60.9	59.9	58.9	58.0	57.1	56.2	55.3	54.4
102	63.0	62.0	61.0	60.0	59.1	58.1	57.2	56.3	55.4	54.5
103	63.1	62.1	61.1	60.1	59.2	58.3	57.3	56.4	55.5	54.6
104	63.2	62.2	61.2	60.3	59.3	58.4	57.5	56.6	55 .7	54.8
	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.

Temper- ature of Air,		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — Fa	hrenheit.	
Fabren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.
20°	40.2	39.3	38.4	37.5	36.6	35.8	34.9	34.1	33.3	32.5
21	40.3	39.4	38.4	37.6	36.7	35.8	35.0	34.2	33.4	32.6
22	40.3	39.4	38.5	37.6	36.8	35.9	35.1	34.3	33.5	32.
23	40.4	39.5	38.6	37.7	36.8	36.0	35.2	34.4	33.6	32.
24	40.4	39.6	38.6	37.8	36.9	36.1	35.2	34.4	33.6	32.
25	40.5	39.6	38.7	37.8	37.0	36.2	35.3	34.5	33.7	33.
26	40.5	39.7	38.8	37.9	37.0	36.2	35.4	34.6	33.8	33.
27	40.6	39.7	38.8	38.0	37.1	36.3	35.5	34.7	33.9	33.
28	40.7	39.8	38.9	38.0	37.2	36.3	35.5	34.7	34.0	23.
29	40.8	39.9	38.9	38.1	37.2	36.4	35.6	34.8	34.0	33.
30	40.8	39.9	39.0	38.1	37.3	36.5	35.7	34.9	34.1	33.
31	41.1	40.2	39.2	38.4	37.5	36.7	35.9	35.1	34.3	33.
32	41.3	40.4	39.5	38.6	37.7	37.0	36.1	35.3	34.5	33.
33	41.6	40.6	39.7	38.8	38.0	37.2	36.3	35.5	34.7	34.
34	41.8	40.9	39.9	39.1	38.2	37.4	36.5	35. 7	34.9	34.
35	42.1	41.1	40.2	39.3	38.4	37.7	36.7	35.9	35.1	34.
36	42.3	41.4	40.4	39.6	38.7	37.9	37.0	36.2	35.4	34.
37	42.6	41.7	40.7	39.8	38.9	38.2	37.2	36.4	35.6	34.
38	42.8	42.0	41.0	40.1	39.2	38.4	37.5	36.6	35.8	35.
39	43.1	42.3	41.3	40.4	39.5	38.6	37.7	36.9	36.0	35.
40	43.3	42.6	41.6	40.7	39.8	38.9	38.0	37.1	36.3	35.
41	43.7	42.9	41.9	41.0	40.0	39.1	38.3	37.4	36.5	35.
42	44.0	43.2	42.2	41.2	40.3	39.4	38.5	37.7	36.8	36.
43	44.3	43.4	42.5	41.5	40.6	39.7	38.8	38.0	37.1	36.
44	44.7	43.7	42.8	41.8	40.9	40.0	39.1	38.2	37.4	36.
45	45.0	44 0	43.1	42.1	41.2	40.3	39.4	38.5	37.7	36.
46	45.2	44.3	43.3	42.4	41.4	40.5	39.7	38.8	37.9	37.
47	45.5	44.5	43.6	42.6	41.7	40.8	39.9	39.1	38.2	37.
48	45.7	44.8	43.8	42.9	42.0	41.1	40.2	39.3	38.5	37.
49	46.0	45.0	44.1	43.2	42.2	41.3	40.5	39.6	38.7	37.
50	46.2	45.3	44.3	43.4	42.5	41.6	40.7	39.9	39.0	37.
51	46.4	45.4	44.5	43.6	42.7	41.8	40.9	40.1	39.2	38.
52	46.6	45.5	44.7	43.8	42.9	42.0	41.2	40.3	39.5	38.
53	46.7	45.8	44.9	44.0	43.1	42.2	41.4	40.5	39.7	38.9
54	46.9	46.0	45.1	44.2	43.3	42.4	41.6	40.8	39.9	39.
55	47.0	46.1	45.2	44.4	43.5	42.6	41.8	41.0	40.1	39.
56	47.2	46.3	45.4	44.5	43.6	42.8	42.0	41.1	40.3	39.
57	47.3	46.4	45.5	44.7	43.8	42.9	42.1	41.3	40.5	39.
58	47.5	46.6	45.7	44.8	43.9	43.1	42.3	41.4	40.6	39.8
59	47.6	46.7	45.8	45.0	44.1	43.2	42.4	41.6	40.8	40.0
60	47.8	46.9	46.0	45.1	44.2	43.4	42.5	41.7	40.9	40.
61	47.9	47.0	46.1	45.3	44.4	43.5	42.7	41.9	41.1	40.
62	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.
	20.0	20.5	21.0	21.5	22.0		23.0	23.5		

Temper- ature		$\mathbf{t} - \mathbf{t}' = \mathbf{I}$	Difference o	f Temperat	ures of the	Air and o	f the Dew-	Point. — F	ahrenheit.	
of Air, Fahren- heit.	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5
62°	48.1	47.2	46.3	45.4	44.5	43.7	42.8	42.0	41.2	40.4
63	48.2	47.3	46.4	45.5	44.7	43.8	43.0	42.2	41.4	40.6
64	48.4	47.5	46.6	45.7	44.8	44.0	43.1	42.3	41.5	40.7
65	48.6	47.6	46.7	45.8	45.0	44.1	43.3	42.5	41.7	40.9
66	48.7	47.8	46.9	46.0	45.1	44.3	43.4	42.6	41.8	41.0
67	48.8	47.9	47.0	46.1	45.3	44.4	43.6	42.8	42.0	41.2
68	48.9	48.0	47.2	46.3	45.4	44.6	43.7	42.9	42.1	41.3
69	49.1	48.2	47.3	46.4	45.6	44.7	43.9	43.1	42.3	41.5
70	49.2	48.3	47.4	46.6	45.7	44.9	44.0	43.2	42.4	41.6
71	49.4	48.5	47.6	46.7	45.9	45.0	44.2	43.4	42.6	41.8
72	49.5	48.6	47.7	46.9	46.0	45.2	44.3	43.5	42.7	41.9
73	49.6	48.8	47.9	47.0	46.1	45.3	44.5	43.7	42.9	42.1
74	49.8	48.9	48.0	47.1	46.3	45.4	44.6	43.8	43.0	42.2
75	49.9	49.0	48.2	47.3	46.4	45.6	44.8	44.0	43.1	42.4
76	50.1	49.2	48.3	47.4	46.6	45.7	44.9	44.1	43.3	42.5
77	50.2	49.3	48.5	47.6	46.7	45.9	45.1	44.2	43.4	42.6
7 8	50.3	49.5	48.6	47.7	46.9	46.0	45.2	44.4	43.6	42.8
79	50.5	49.6	48.7	47.8	47.0	46.2	45.3	44.5	43.7	43.0
80	50.6	49.7	48.9	48.0	47.2	46.3	45.5	44.7	43.9	43.1
81	50.8	49.9	49.0	48.1	47.3	46.5	45.6	44.8	44.0	43.2
82	50.9	50.0	49.2	48.3	47.4	46.6	45.8	45.0	44.2	43.4
83	51.0	50.1	49.3	48.4	47.6	46.8	45.9	45.1	44.3	43.3
84	51.2	50.3	49.4	48.6	47.7	46.9	46.1	45.3	44.5	43.7
85	51.3	50.4	49.6	48.7	47.9	47.0	46.2	45.4	44.6	43.8
86	51.4	50.6	49.7	48.8	48.0	47.2	46.4	45.6	44.8	44.0
87	51.6	50.7	49.8	49.0	48.1	47.3	46.5	45.7	44.9	44.1
88	51.7	50.8	50.0	49.1	48.3	47.5	46.6	45.8	45.0	44.8
89	51.9	51.0	50.1	49.3	48.4	47.6	46.8	46.0	45.2	44
90	52.0	51.1	50.3	49.4	48.6	47.7	46.9	46.1	45.3	44.6
91	52.1	51.3	50.4	49.5	48.7	47.9	47.1	46.3	45.5	44.7
92	52.3	51.4	50.5	49.7	48.8	48.0	47.2	46.4	45.6	44.8
93	52.4	51.5	50.7	49.8	49.0	48.2	47.4	46.6	45.8	45.0
94	52.5	51.7	50.8	50.0	49.1	48.3	47.5	46.7	45.9	45.1
95	52.7	51.8	50.9	50.1	49.3	45.4	47.6	46.8	46.1	45.8
96	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.0	46.2	45.4
97	52.9	52.1	51.2	50.4	49.5	48.7	47.9	47.1	46.3	45.6
98	53.1	52.2	51.4	50.5	49.7	48.9	48.1	47.3	46.5	45.7
99	53.2	52.3	51.5	50.6	49.8	49.0	48.2	47.4	46.6	45.9
100	53.4	52.5	51.6	50.8	50.0	49.1	48.3	47.5	46.8	46.0
101	53.5	52.6	51.8	50.9	50.1	49.3	48.5	47.7	46.9	46.2
102	53.6	52.8	51.9	51.1	50.2	49.4	48.6	47.8	47.1	46.3
103	53.8	52.9	52.0	51.2	50.4	49.6	48.8	48.0	47.2	46.4
104	53.9	53.0	52.2	51.3	50.5	49.7	48.9	48.1	47.3	46.6
	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.

TABLE IX.

factor $\frac{100}{F}$, for computing the relative humidity, or the degree of moisture of the air, expressed in hundredths, from its absolute

HUMIDITY GIVEN IN ENGLISH MEASURES.

The Relative Humidity, or the degree of moisture of the air, is, as explained above, the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call

The force of vapor contained in the air = f,

The maximum of the force of vapor at the temperature of the air = F,

The point of saturation = 100,

we have the proportion,

Relative Humidity: 100::f:F,

and

 $f_{F}^{\times 100} = \text{Relative Humidity in Hundredths}.$

But as $\frac{f \times 100}{F} = f \times \frac{100}{F}$, it is obvious that the operation indicated by the former expression, viz. $\frac{f \times 100}{F}$, would be reduced to a simple multiplication, if we had a table of the factors $\frac{100}{F}$. Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forces of Vapor, and substituting the quotients for the tensions, or forces of vapor.

The following Table gives the factor $\frac{100}{F}$ for every tenth of a degree from 0° to 104° Fahrenheit, corresponding to the Forces of Vapor in Table VI., or Regnault's table reduced to English measures.

USE OF THE TABLE.

The force of vapor contained in the air, or its absolute humidity, being given in English measures, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the *Relative Humidity in Hundredths*.

Examples.

- 1. Suppose the temperature of the air to be = 60° Fahrenheit.
 - " force of vapor in the air to be = .388 English inch.

Opposite 60° is found in the table the factor 193.1.

Then $0.388 \times 193.1 = 74.9$, Relative Humidity in Hundredths.

2. Suppose the temperature of the air to be $= 74^{\circ}.5$ Fahrenheit.

"force of vapor in the air to be = .650 English inch.

Table gives for 74°.5 the factor 117.2.

Then $0.650 \times 117.2 = 76.2$, Relative Humidity required.

IX. FACTOR $\frac{100}{F},$ FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE OF THE AIR,

EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY GIVEN IN ENGLISH INCHES.

Temper- ature of Air,					Tenths o	f Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	2306	2295	2285	2275	2264	2254	2243	2233	2222	2211
1	2201	2191	2181	2171	2162	2152	2142	2132	2122	2111
2	2101	2092	2083	2074	2064	2055	2045	2036	2026	2017
3	2007	1998	1990	1981	1972	1963	1954	1945	1936	1927
4	1918	1910	1901	1893	1885	1876	1868	1859	1851	1842
5	1834	1826	1818	1810	1802	1794	1786	1777	1769	1761
6	1753	1745	1738	1730	1722	1714	1707	1699	1691	1683
7	1675	1668	1660	1653	1646	1638	1631	1623	1616	1608
8	1600	1594	1587	1580	1572	1565	1558	1551	1544	1537
9	1529	1523	1516	1509	1503	1496	1489	1482	1475	1469
10	1462	1455	1449	1443	1436	1430	1423	1417	1410	1404
11	1397	1391	1385	1379	1373	1367	1361	1355	1348	1342
12	1336	1330	1324	1319	1313	1307	1301	1295	1289	1284
13	1278	1272	1267	1261	1255	1250	1244	1239	1233	1228
14	1222	1217	1211	1206	1200	1195	1189	1184	1178	1173
15	1167	1162	1157	1151	1146	1141	1136	1130	1125	1120
16	1114	1109	1104	1099	1094	1089	1084	1079	1074	1069
17	1064	1059	1055	1050	1045	1040	1035	1031	1026	1021
18	1016	1012	1007	1003	998.2	993.6	989.1	984.5	979.9	975.3
19	970.6	966.4	962.2	957.9	953.7	949.4	945.0	940.7	936.3	931.9
20	927.5	923.5	919.5	915.5	911.4	907.4	903.3	899.1	895.0	890.8
21	886.7	882.9	879.1	875.3	871.4	867.6	863.7	859.8	855.8	851.9
22	847.9	844.3	840.7	837.1	833.4	829.8	826.1	822.4	818.7	815.0
23	811.2	807.8	804.3	800.8	797.3	793.8	790.2	786.7	783.1	779.5
24	775.9	772.6	769.3	766.0	762.7	759.3	756.0	752.6	749.2	745.8
25	742.4	739.3	736.2	733.0	729.9	726.7	723.5	720.3	717.1	713.9
26	710.6	707.7	704.7	701.8	698.8	695.8	692.8	689.7	686.7	683.6
27	680.5	677.8	675.0	672.1	669.3	666.5	663.6	660.7	657.8	654.9
28	652.0	649.4	646.7	644.1	641.4	638.7	636.0	633.3	630.5	627.8
29	625.0	622.5	620.0	617.5	614.9	612.4	609.8	607.2	604.6	602.0
30	599.4	597.1	594.7	592.3	589.9	587.4	585.0	582.6	580.1	577.6
31	575.1	572.9	570.7	568.4	566.2	563.9	561.6	559.2	556.9	554.5
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Temper- ature of Air, Fahren- heit.	Tenths of Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
32°	552.2	550.0	547.8	545.7	543.6	541.4	539.3	537.2	535.1	533.		
33	530.9	528.8	526.8	524.7	522.7	520.6	518.6	516.5	514.5	512.		
34	510.5	508.5	506.5	504.5	502.5	500.5	498.6	496.6	494.7	492.		
35	490.8	488.9	487.0	485.1	483.2	481.3	479.4	477.5	475.6	473.		
36	471.9	470.1	468.2	466.4	464.6	462.8	461.0	459.2	457.4	455.		
37	453.8	452.0	450.3	448.5	446.8	445.0	443.3	441.6	439.9	438.		
38	436.4	434.7	433.1	431.4	429.7	428.0	426.4	424.7	423.1	421.		
39	419.8	418.2	416.6	415.0	413.4	411.8	410.2	408.6	407.0	405.		
40	403.9	402.4	400.8	399.3	397.8	396.2	394.7	393.2	391.7	290.		
41	388.7	387.2	385.8	384.3	382.9	381.4	380.0	378.5	377.1	375.		
42	374.3	372.9	371.5	370.0	368.6	367.3	365.9	364.5	363.1	361.		
43	360.4	359.0	357.6	356.3	354.9	353.6	352.3	350.9	349.6	348		
44	347.0	345.6	344.3	343.0	341.7	340.4	339.2	337.9	336.6	335		
45	334.1	332.8	331.6	330.3	328.1	327.8	326.6	325.4	324.1	322.		
46	321.7	320.5	319.3	318.1	316.9	315.7	314.5	313.3	312.2	311.		
47	309.8	308.7	307.5	306.4	305.2	304.1	302.9	301.8	300.7	299		
48	298.5	297.3	296.2	295.1	294.0	292.9	291.9	290.8	289.7	288		
49	287.6	286.5	285.4	284.4	283.3	282.3	281.3	280.2	279.2	278		
50	277.1	276.1	275.1	274.1	273.1	272.1	271.1	270.1	269.1	268.		
51	267.2	266.2	265.2	264.3	263.3	262.3	261.4	260.4	259.5	258.		
52	257.6	256.6	255.7	251.8	253.8	252.9	252.0	251.1	250.2	249.		
53	248.3	247.4	246.5	245.6	244.7	243.9	243.0	242.1	241.2	240.		
54	239.5	238.6	237.7	236.9	236.0	235.1	234.3	233.4	232.6	231		
55	230.9	230.1	229.2	228.4	227.6	226.8	225.9	225.1	224.3	223.		
-56	222.7	221.9	221.1	220.3	219.5	218.7	217.9	217.1	216.4	215.		
57	214.8	214.0	213.3	212.5	211.8	211.0	210.2	209.5	208.7	208.		
58	207.3	206.5	205.8	205.0	204.3	203.6	202.9	202.2	201.4	200.		
59	200.0	199.3	198.6	197.9	197.2	196.5	195.8	195.1	194.4	193.		
60 61	193.1 186.4	192.4 185.7	191.7 185.1	191.0 184.4	190.4 183.8	189.7 183.1	189.0 182.5	188.4 181.8	187.7 181.2	187. 180.		
97	100.4	109.1	103.1	104.4	100.0	100.1	102.0	101.0	101.4	100.		
62 63	179.9 173.7	179.3 173.1	178.7 172.5	178.0 171.9	177.4 171.3	176.8 170.7	176.2 170.1	175.6 169.5	174.9 168.9	174. 168.		
64	167.7	167.1	166.6	166.0	165.4	164.8	164.3	163.7	163.1	162.		
65	162.0	161.4	160.9	160.3	159.7	159.2	158.6	158.1	157.5	157.		
66	156.5	155.9	155.4	154.8	154.3	153.8	153.2	152.7	152.2	151.		
67	151.1	150.6	150.1	149.6	149.1	148.6	148.1	147.6	147.1	146.		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

Temperature of Air, Fahrenheit.	Tenths of Degrees.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
6s°	146.0	145.6	145.1	144.6	144.1	143.6	143.1	142.6	142.1	141.	
69	141.2	140.7	140.2	139.7	139.2	138.8	138.3	137.8	137.4	136.	
70	136.4	136.0	135.5	135.1	134.6	134.1	133.7	133.2	132.8	132.	
71	131.9	131.4	131.0	130.5	130.1	129.7	129.2	128.8	128.3	127.	
72	127.5	127.1	126.6	126.2	125.8	125.3	124.9	124.5	124.1	123.	
73	123.3	122.8	122.4	122.0	121.6	121.2	120.8	120.4	120.0	119.	
74	119.2	118.8	118.4	118.0	117.6	117.2	116.8	116.4	116.0	115.	
75	115.3	114.9	114.5	114.1	113.7	113.3	113.0	112.6	112.2	111.	
76	111.5	111.1	110.7	110.4	110.0	109.6	109.3	108.9	108.6	108.	
77	107.9	107.5	107.1	106.8	106.4	106.1	105.7	105.4	105.1	104.	
78	104.4	104.0	103.7	103.3	103.0	102.7	102.3	102.0	101.7	101.	
79	101.0	100.7	100.3	100.0	99.68	99.35	99.02	98.70	98.38	98.	
80	97.73	97.42	97.10	96.78	96.47	96.15	95.84	95.52	95.21	94.	
81	94.59	94.29	93.98	93.67	93.37	93.06	92.76	92.46	92.16	91.	
82	91.56	91.26	90.97	90.67	90.38	90.09	89.80	89.51	89.22	88.	
83	88.64	88.36	88.07	87.79	87.50	87.22	86.94	86.66	86.38	86.	
84	85.83	85.55	85.27	85.00	84.73	84.46	84.19	83.92	83.65	83.	
85	83.12	82.85	82.59	82.32	82.06	81.80	81.54	81.28	81.02	80.	
86	80.51	80.25	80.00	79.74	79.49	79.24	78.99	78.74	78.49	78.	
87	77.99	77.75	77.50	77.26	77.01	76.77	76.52	76.28	76.04	75.	
88	75.56	75.32	75.08	74.85	74.61	74.37	74.14	73.91	73.67	73.	
89	73.21	72.98	72.75	72.52	72.29	72.06	71.84	71.61	71.39	71.	
90	70.94	70.72	70.49	70.27	70.05	69.83	69.61	69.39	69.18	68.	
91	68.74	68.53	68.32	68.10	67.89	67.68	67.47	67.26	67.05	66.	
92	66.63	66.42	66.22	66.01	65.81	65.60	65.40	65.19	64.99	64.	
93	64.59	64.39	64.19	63.99	63.79	63.59	63.40	63.20	63.01	62.	
94	62.62	62.43	62.24	62.04	61.85	61.66	61.47	61.29	61.10	60.9	
95	60.72	60.54	60.35	60.17	59.98	59.80	59.62	59.43	59.25	59.0	
96	58.89	58.71	58.53	58.35	58.17	58.00	57.82	57.64	57.47	57.5	
97 98	57.12 55.40	56.94 55.23	56.77 55.06	56.60 54.90	56.42 54.73	56.25 54.56	56.08 54.40	55.91 54.23	55.74 54.07	55. 53.	
0.0	#0 m	F0 F0	70. 10	50.00	50.00	* 0.00		70 07	* 0 :-		
99	53.74	53.58	53.42	53.26	53.09	52.93	52.77	52.61	52.45	52.	
100 101	52.14 50.59	51.98 50.44	$51.82 \\ 50.29$	51.67 50.14	51.51 49.99	51.36 49.84	51.20 49.69	51.05 49.54	50.90 49.39	50.3	
101	49.10	48.95	48.80	48.66	48.51	48.37	48.22	48.08	47.94	49.5	
102	47.65	47.51	47.37	47.23	47.09	46.95	46.81	46.67	46.53	46.4	
104	46.26	46.12	45.99	45.85	45.72	45.58	45.45	45.31	45.18	45.0	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

TABLE X.

WEIGHT OF VAPOR, IN GRAINS TROY,

contained in a cubic foot of saturated air, under a barometric pressure of 30 english inches, at temperatures between 0° and 105° fahrenheit.

The weight of a litre of dry air at the temperature of zero Centigrade, or 32° Fahrenheit, and under a barometric pressure of 760 millimetres, as determined by the experiments of Regnault (Mémoires de l'Institut, Tom. XXI. p. 157), and corrected for a slight error of computation (see above, p. 38), is 1.293223 grammes. The coefficient of expansion of the air, according to the same physicist, is 0.00367 for 1° Centigrade; and the theoretic density of vapor is nearly 0.622, or $\frac{5}{8}$, of that of the air at the same temperature and pressure. From these elements the weight of the vapor contained in a determined volume of air, the temperature and humidity of which are known, can be deduced.

Reducing these values to English measures, 1 litre being =61.02705 cubic inches, and 1 gramme =15.43208 grains Troy, we have

1.293223 grammes = 19.9571208 grains,

and

61.027051 cubic inches: 19.9571208 grains:: 1 cubic inch: 0.32702 grain.

Therefore, the weight of a cubic foot of dry air, at 32° Fahrenheit, under a pressure of 760 millimetres, or 29.922 English inches, is = 0.32702 grain \times 1728 = 565.0923 grains Troy. Under a barometric pressure of 30 inches, it becomes

$$\frac{30}{29.922} \times 565.0923 = 566.5654$$
 grains.

The coefficient for the expansion of the air becomes 0.0020361 of its bulk for 1° Fahrenheit.

Now, if we call

t =the temperature of the air;

W =the weight of vapor in a saturated air at the temperature t;

F = the maximum of the force of vapor due to the temperature t, as given in the tables;

then the weight of the vapor contained in a cubic foot of saturated air is given by the formula

$$W = 0.622 \frac{566.5654 \text{ grains}}{1 + 0.002036 \times (t - 32^{\circ})} \cdot \frac{F}{30};$$

from which the values in Table X. have been computed. The forces of vapor due to the temperatures in the first column are those of Regnault, as given in Table VI.

It is evident, that, in order to find the weight of the vapor contained in the air at any state of humidity and pressure, it suffices to substitute for the normal values of $\frac{\mathbf{F}}{30}$ the force of vapor and the barometric pressure given by the observation.

X. WEIGHT OF VAPOR, IN GRAINS TROY,

contained in a cubic foot of saturated air, at temperatures between 0° and 105° fahrenheit.

1											
Temper- ature of Air, Fahren.	Force of Vapor in Eng. Inches.	Weight of Vapor in Grains.	Differ- ence.	Temper- ature of Air, Fahren.	Force of Vapor in Eng. Inches.	Weight of Vapor in Grains.	Differ- ence.	Temperature of Air, Fahren.	Force of Vapor in Eng, Inches.	Weight of Vapor in Grains.	Differ- ence.
o°	0.043	0.545		35°	0.204	2.379		70°	0.733	7.992	
1	0.045	0.569	0.024	36	0.212	2.469	0.090	71	0.758	8.252	0.261
2	0.048	0.595	0.025	37	0.220	2.563	0.093	72	0.784	8.521	0.268
3	0.050	0.621	0.027	38	0.229	2.659	0.097	73	0.811	8.797	0.276
4	0.052	0.649	0.028	39	0.238	2.759	0.100	74	0.839	9.081	0.284
			0.029				0.103				0.291
5	0.055	0.678		40	0.248	2.862		75	0.868	9.372	
6	0.057	0.708	0.030	41	0.257	2.967	0.106	76	0.897	9.670	0.298
7	0.060	0.739	0.031	42	0.267	3.076	0.109	77	0.927	9.977	0.307
8	0.062	0.772	0.033	43	0.277	3.189	0.113	78	0.958	10.292	0.315
9	0.065	0.806	0.034	44	0.288	3.306	0.116	79	0.990	10.616	0.324
	0.000	0.000	0.035		0.200	0.000	0.120			10.010	0.332
10	0.068	0.841		45	0.299	3.426		80	1.023	10.949	
11 1	0.072	0.878	0.037	46	0.311	3.550	0.124	81	1.057	11.291	0.342
12	0.075	0.916	0.038	47	0.323	3.679	0.129	82	1.092	11.643	0.352
13	0.078	0.957	0.040	48	0.335	3.811	0.133	83	1.128	12.005	0.361
14	0.082	0.999	0.042	49	0.348	3.948	0.137	84	1.165	12.376	0.371
	•••••	0.000	0.044	1	0.0.0	3.0 10	0.141		1.100	12.0.0	0.380
15	0.086	1.043		50	0.361	4.089		85	1.203	12.756	
16	0.090	1.090	0.046	51	0.374	4.234	0.145	86	1.242	13.146	0.390
17	0.094	1.139	0.049	52	0.388	4.383	0.149	87	1.282	13.546	0.400
18	0.098	1.190	0.051	53	0.403	4.537	0.154	88	1.323	13.957	0.411
19	0.103	1.243	0.053	54	0.418	4.696	0.159	89	1.366	14.378	0.421
	0.200		0.055			1.000	0.163		1.000	11.010	0.432
20	0.108	1.298		55	0.433	4.860		90	1.410	14.810	
21	0.113	1.355	0.057	56	0.449	5.028	0.168	91	1.455	15.254	0.443
22	0.118	1.415	0.059	57	0.466	5.202	0.174	92	1.501	15.709	0.455
23	0.123	1.476	0.062	58	0.482	5.381	0.179	93	1.548	16.176	0.467
24	0.129	1.540	0.064	59	0.500	5.566	0.185	94	1.597	16.654	0.479
			0.066				0.190				0.491
25	0.135	1.606		60	0.518	5.756		95	1.647	17.145	
26	0.141	1.674	0.068	61	0.537	5.952	0.196	96	1.698	17.648	0.503
27	0.147	1.745	0.070	62	0.556	6.154	0.202	97	1.751	18.164	0.516
28	0.153	1.817	0.073	63	0.576	6.361	0.208	98	1.805	18,693	0.529
29	0.160	1.892	0.075	64	0.596	6.575	0.214	99	1.861	19.235	0.542
			0.077				0.220			20.200	0.555
30	0.167	1.969		65	0.617	6.795		100	1.918	19.790	
31	0.174	2.046	0.077	66	0.639	7.021	0.226	101	1.977	20.357	0.567
32	0.181	2.126	0.080	67	0.662	7.253	0.232	102	2.037	20.938	0.582
33	0.188	2.208	0.082	68	0.685	7.493	0.239	103	2.099	21.535	0.596
34	0.196	2.292	0.084	69	0.708	7.739	0.246	104	2.162	22.146	0.611
35	0.204	2.379	0.087	70	0.733	7.992	0.253	105	2.227	22.771	0.625
										,	l

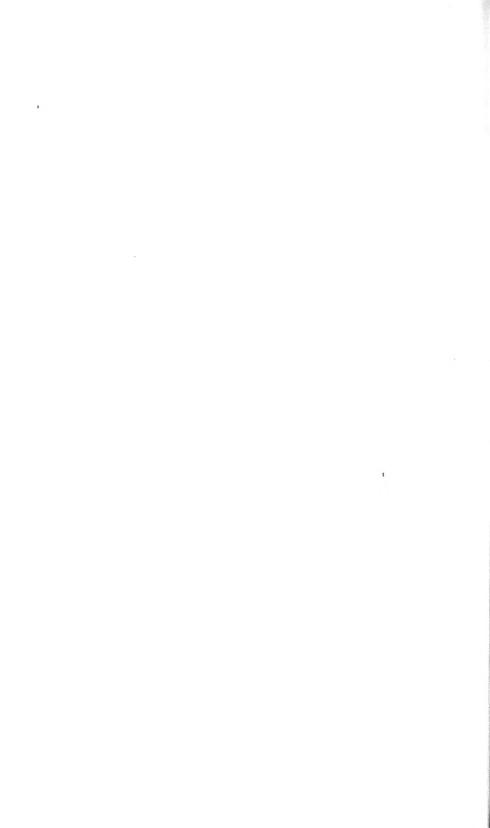


PRACTICAL TABLES,

IN

ENGLISH MEASURES,

BASED ON THE HYGROMETRICAL CONSTANTS ADOPTED IN THE GREENWICH OBSERVATIONS.



TABLE

OF

THE ELASTIC FORCES OF AQUEOUS VAPOR,

UNDER A PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, ADOPTED IN THE GREENWICH OBSERVATIONS.

This table contains the values of the elastic force of vapor for temperatures from 0° to 90° Fahrenheit, derived from Dalton's experiments by Biot's formula, by Anderson, and published in Edinburgh Encyclopædia, Art. Hygrometry. It is republished, without the last decimal, in the volumes of the Greenwich Magnetic and Meteorological Observations, and on it are based the various hygrometrical tables published by Mr. Glaisher, either in the Greenwich volumes, or separately, most of which will be found below, Tables XII. to XVII.

Since Dalton published his experiments, numerous attempts have been made by various skilful physicists to determine with greater accuracy the elastic force of vapor. Dr. Ure in England, Regnault in France, and Magnus in Germany, deserve in this respect a special notice.

The last two experimenters having arrived simultaneously at results nearly identical, and their experiments having been conducted with all the care that modern science requires, and the means that it can secure, their determinations seem to command an especial confidence, and to deserve the preference over all others. It is, therefore, much to be regretted that the usefulness of the following otherwise so valuable tables, the formation of which involved so much labor, is in a measure impaired by the fact that they were computed from elements which cannot be regarded as the most reliable we now possess.



XI.

TABLE

OF THE

ELASTIC FORCE OF AQUEOUS VAPOR,

UNDER A BAROMETRIC PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT.

From the Greenwich Observations.

Temper-					Tenths of	Degrees.				
ature Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
0	0.061	0.061	0.062	0.062	0.062	0.062	0.063	0.063	0.063	0.063
1	0.064	0.064	0.064	0.064	0.065	0.065	0.065	0.065	0.066	0.066
2	0.066	0.066	0.067	0.067	0.067	0.067	0.068	0.068	0.068	0.068
3	0.069	0.069	0.069	0.069	0.070	0.070	0.070	0.071	0.071	0.071
4	0.071	0.072	0.072	0.072	0.072	0.073	0.073	0.073	0.073	0.074
5	0.074	0.074	0.075	0.075	0.075	0.075	0.076	0.076	0.076	0.077
6	0.077	0.077	0.077	0.078	0.078	0.078	0.079	0.079	0.079	0.080
7	0.080	0.080	0.080	0.081	0.081	0.081	0.082	0.082	0.082	0.083
8	0.083	0.083	0.083	0.084	0.084	0.084	0.085	0.085	0.085	0.086
9	0.086	0.086	0.087	0.087	0.087	0.088	0.088	0.088	0.089	0.089
10	0.089	0.090	0.090	0.090	0.091	0.091	0.091	0.092	0.092	0.092
11	0.093	0.093	0.093	0.094	0.094	0.094	0.095	0.095	0.096	0.096
12	0.096	0.097	0.097	0.097	0.098	0.098	0.098	0.099	0.099	0.099
13	0.100	0.100	0.101	0.101	0.101	0.102	0.102	0.102	0.103	0.103
14	0.104	0.104	0.104	0.105	0.105	0.106	0.106	0.106	0.107	0.107
15	0.108	0.108	0.108	0.109	0.109	0.110	0.110	0.110	0.111	0.111
16	0.112	0.112	0.112	0.113	0.113	0.114	0.114	0.115	0.115	0.115
17	0.116	0.116	0.117	0.117	0.118	0.118	0.118	0.119	0.119	0.120
18	0.120	0.121	0.121	0.121	0.122	0.122	0.123	0.123	0.124	0.124
19	0.125	0.125	0.126	0.126	0.126	0.127	0.127	0.128	0.128	0.129
20	0.129	0.130	0.130	0.131	0.131	0.132	0.132	0.133	0.133	0.134
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

ELASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

Temper-					Teaths of	Degrees.				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
•	Eng. In.	Eng. In	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
21	0.134	0.135	0.135	0.136	0.136	0.137	0.137	0.138	0.138	0.139
22	0.139	0.140	0.140	0.141	0.141	0.142	0.142	0.143	0.143	0.144
23	0.144	0.145	0.145	0.146	0.146	0.147	0.147	0.148	0.148	0.149
24	0.150	0.150	0.151	0.152	0.152	0.152	0.153	0.153	0.154	0.155
25	0.155	0.156	0.156	0.157	0.157	0.158	0.158	0.159	0.160	0.160
26	0.161	0.161	0.162	0.163	0.163	0.164	0.164	0.165	0.165	0.166
27	0.167	0.167	0.168	0.168	0.169	0.170	0.170	0.171	0.172	0.172
28	0.173	0.173	0.174	0.175	0.175	0.176	0.177	0.177	0.178	0.178
29	0.179	0.180	0.180	0.181	0.182	0.182	0.183	0.184	0.184	0.185
30	0.186	0.186	0.187	0.188	0.188	0.189	0.190	0.190	0.191	0.192
91	0.192	0.193	0.194	0.194	0.195	0.196	0.197	0.197	0.198	0.198
31 32	0.192	0.193	0.194	0.194	0.193	0.190	0.197	0.191	0.195	0.198
33	0.199	0.207	0.201	0.201	0.202	0.203	0.204	0.212	0.203	0.213
34	0.207	0.207	0.205	0.209	0.210	0.210	0.211	0.212	0.213	0.21
	1	1 .		l .	0.217	0.218	0.219		t .	ľ
35	0.222	0.223	0.223	0.224	0.223	0.220	0.227	0.227	0.228	0.229
36	0.230	0.231	0.231	0.232	0.233	0.234	0.235	0.235	0.236	0.23
37	0.238	0.239	0.240	0.240	0.241	0.242	0.243	0.244	0.245	0.246
38	0.246	0.247	0.248	0.249	0.250	0.251	0.252	0.253	0.253	0.25
39	0.255	0.256	0.257	0.258	0.259	0.260	0.261	0.262	0.263	0.26;
40	0.264	0.265	0.266	0.267	0.268	0.269	0.270	0.271	0.272	0.27;
41	0.274	0.275	0.276	0.277	0.278	0.279	0.280	0.281	0.282	6.289
42	0.283	0.284	0.285	0.286	0.287	0.288	0.289	0.290	0.291	0.29
43	0.293	0.295	0.296	0.297	0.298	0.299	0.300	0.301	0.302	0.303
44	0.304	0.305	0.306	0.307	0.308	0.309	0.310	0.311	0.312	0.313
45	0.315	0.316	0.317	0.318.	0.319	0.320	0.321	0.322	0.323	0.32
	0.200	0.207	0.990	0.329	0.990	0.331	0.332	0 222	0.335	0.336
46	$0.326 \\ 0.337$	$0.327 \\ 0.338$	$0.328 \\ 0.339$	0.329	$0.330 \\ 0.342$	0.331	0.332 0.344	0.333 0.345	0.335	0.348
47 48	0.337	0.338	0.339	0.352	0.342	0.355	0.356	0.345	0.358	0.346
49	0.349	0.362	0.363	0.365	0.366	0.367	0.368	0.370	0.333	0.372
50	0.373	0.302	0.376	0.377	0.379	0.380	0.381	0.382	0.383	0.38
	3.013	0.010			,					
51	0.386	0.388	0.389	0.390	0.392	0.393	0.394	0.396	0.397	0.398
52	0.400	0.401	0.402	0.404	0.405	0.407	0.408	0.409	0.411	0.412
53	0.414	0.415	0.416	0.418	0.419	0.421	0.422	0.423	0.425	0.426
5 t 55	$0.428 \\ 0.442$	$\begin{array}{c c} 0.429 \\ 0.444 \end{array}$	0.431 0.445	0.432 0.447	0.434 0.449	0.435 0.450	$0.437 \\ 0.452$	$0.438 \\ 0.453$	0.440 0.455	0.441
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

ELASTIC FORCE OF AQUEOUS VAPOR.

From the Greenwich Observations.

Femper- ature					Tenths of	Degrees,				
Fahren- heit.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. I
56	0.458	0.459	0.461	0.462	0.464	0.465	0.467	0.469	0.470	0.473
57	0.473	0.475	0.476	0.478	0.480	0.481	0.483	0.485	0.486	0.488
58	0.489	0.491	0.493	0.494	0.496	0.498	0.499	0.501	0.503	0.50
59	0.506	0.508	0.509	0.511	0.513	0.515	0.516	0.518	0.520	0.52
60	0.523	0.525	0.527	0.528	0.530	0.532	0.534	0.536	0.537	0.539
61	0.541	0.543	0.544	0.546	0.548	0.550	0.552	0.554	0.555	0.557
62	0.559	0.561	0.563	0.565	0.567	0.568	0.570	0.572	0.574	0.57
63	0.578	0.580	0.582	0.584	0.586	0.588	0.590	0.591	0.593	0.59
64	0.597	0.599	0.601	0.603	0.605	0.607	0.609	0.611	0.613	0.61
65	0.617	0.619	0.621	0.623	0.626	0.628	0.630	0.632	0.634	0.63
00	0.000	0.040	0.642	0.644	0.646	0.648	0.651	0.050	0.055	0.65
66	0.638	0.640						0.653	0.655	1
67	0.659	0.661	0.664	0.666	0.668	0.670	0.672	0.674	0.677	0.67
68	0.681	0.684	0.686	0.688	0.690	0.692	0.695	0.697	0.699	0.70
69	0.704	0.706	0.708	0.711	0.713	0.715	0.717	0.720	0.722	0.72
70	0.727	0.729	0.732	0.734	0.736	0.739	0.741	0.744	0.746	0.74
71	0.751	0.753	0.756	0.758	0.761	0.763	0.766	0.768	0.771	0.77
72	0.776	0.778	0.781	0.783	0.785	0.787	0.790	0.792	0.795	0.79
73	0.801	0.803	0.806	0.809	0.811	0.814	0.817	0.819	0.822	0.82
74	0.827	0.830	0.832	0.835	0.838	0.840	0.843	0.846	0.849	0.85
75	0.854	0.857	0.860	0.862	0.865	0.868	0.871	0.873	0.876	0.87
76	0.882	0.885	0.887	0.890	0.893	0.896	0.899	0.902	0.905	0.908
77	0.910	0.913	0.916	0.919	0.922	0.925	0.928	0.931	0.934	0.93
- 11		1	I				I			
78	0.940	0.943	0.946	0.949	0.952	0.955	0.958	0.961	0.964	0.96
79 80	0.970 1.001	0.973 1.005	0.976 1.008	0.979 1.011	0.983 1.014	0.986 1.017	0.989 1.021	$0.992 \\ 1.024$	0.995 1.027	0.99 1.03
81	1.034	1.037	1.040	1.043	1.047	1.050	1.053	1.057	1.060	1.06
82	1.067	1.069	1.073	1.077	1.080	1.083	1.087	1.090	1.094	1.09
83	1.101	1.104	1.108	1.111	1.114	1.118	1.121	1.125	1.129	1.132
84	1.136	1.139	1.143	1.146	1.150	1.153	1.157	1.160	1.164	1.16
85	1.171	1.175	1.178	1.182	1.186	1.190	1.193	1.197	1.201	1.20
86	1.209	1.212	1.216	1.220	1.224	1.228	1.232	1.235	1.239	1.24
87	1.247	1.251	1.255	1.258	1.262	1.266	1.270	1.274	1.278	1.282
88	1.286	1.290	1.294	1.298	1.302	1.306	1.310	1.314	1.318	1.322
89	1.326	1.330	1.335	1.339	1.343	1.347	1.351	1.355	1.359	1.36
90	1.368	1.372	1.376	1.381	1.385	1.389	1.393	1.397	1.402	1.406
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

XII.

PSYCHROMETRICAL TABLE,

GIVING THE TEMPERATURE OF THE DEW-POINT, THE FORCE AND THE WEIGHT OF VAPOR IN THE ATMOSPHERE, AND ITS RELATIVE HUMIDITY, DEDUCED FROM THE INDICATIONS OF THE PSYCHROMETER, OR DRY AND WET BULB THERMOMETERS.

By James Glaisher.

This elaborate table, first published in London, in 1847, in pamphlet form, by J. Glaisher, of the Royal Observatory at Greenwich, is based on the tables of elastic forces of vapor deduced from Dalton's experiments, and given above, Table XI.

The weight of a cubic foot of dry air at 32° Fahrenheit, and under the barometric pressure of 30 inches, which has been adopted by Glaisher, and from which the weight of vapor in a cubic foot of air is derived, is the mean of the determinations obtained by Shuckburgh and by Biot and Arago, which is 563.2154 grains Troy; 563 being the number actually used in the calculations. See Preface to the Table, p. 13, and also the *Greenwich Meteorological Observations* for 1842, p. xlvi.

The coefficient of the expansion of air which has been employed is that determined by the experiments of Gay-Lussac, according to which the air expands 0.00375 of its bulk for 1° Centigrade, or $_{x_{3}}^{1}$ for 1° Fabrenheit.

All these values, as may be seen by comparing Tables VI. and XI. of the elastic forces, and also page 92, materially differ from those more recently determined with great care by Regnault, and on which are based the Psychrometrical Tables given above, page 50 et seq. This will account for the no inconsiderable differences often found between the results in the two tables derived from the same data. A few examples, taken from various parts of the tables, may be given here, in order to enable the meteorologist to judge of the amount of the discrepancies which may occur in the results when computed from different hygrometrical constants.

1. Suppose the temperature of the air indicated by the dry thermometer ter to be $= 10^{\circ} \text{ F.}$ The temperature of evaporation indicated by the wet thermometer $= 9^{\circ} \text{ F.}$ Difference 1° F.

Then, Glaisher's table gives,

The Force of Vapor = 0.065 inch. The Relative Humidity = 0.730

Guyot's table gives,

The Force of Vapor = 0.054 inch.

The Relative Humidity = 0.791

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PSYCHROMETRICAL TABLE.

2. By observation we have,

Dry Thermometer $= 50^{\circ}$ F.

Wet Thermometer $= 40^{\circ} \text{ F.}$

Difference $= 10^{\circ}$ F.

Then, by Glaisher's table, we find,

Force of Vapor = 0.186 inch.

Relative Humidity = 0.495

And by Guyot's table, we find,

Force of Vapor = 0.117 inch.

Relative Humidity = 0.322

3. The reading of the

Dry Thermometer is $= 90^{\circ}$ F.

Wet Thermometer is $= 70^{\circ}$ F.

Difference = 20° F.

By Glaisher's table we have,

Force of Vapor = 0.523 inch.

Relative Humidity = 0.381

And by Guyot's table,

Force of Vapor = 0.464 inch.

Relative Humidity = 0.329

The temperatures of the Dew-Point, given in Glaisher's tables, have been computed by means of the empirical factors given below, page 140, and in the manner there described. See Preface to the Table, page 11.

ARRANGEMENT OF THE TABLE.

In the first two columns, at the left, are found the indications, in degrees of Fahrenheit, of the dry and wet bulb thermometers. In the following columns, in their order, and opposite to each of the temperatures of the wet thermometer, are given the temperature of the dew-point; the force of vapor, in English inches; the weight of vapor, in grains, contained in a cubic foot of air; the amount of the same required for saturation; and the relative humidity in thousandths, corresponding to the difference of temperature between the two thermometers. The second half of the page, at the right, furnishes, in seven columns, the weight, in grains, of a cubic foot of air, under various barometric pressures from 28 to 31 inches, and in the different hygrometric conditions indicated by the differences of the two thermometers. These numbers have been computed in the manner described below, page 142.

The range of the table extends from 10° to 90° of the dry thermometer, or of the temperature of the air. From 10° to 34° Fahrenheit the results are calculated for every second, third, and fifth of a degree of the wet thermometer, and for extreme differences of the temperature of evaporation ranging from 2° to 5° below the temperature of the air. From 34° to 90° the results are given only for every full degree of the wet thermometer, and for extreme differences gradually increasing

PSYCHROMETRICAL TABLE.

from 5° to 27°. This range falls short of the wants of the extreme climate of North America, where temperatures above 90° and far below 10° are of usual occurrence over a great portion of the continent. The same may be said of the range of the differences between the two thermometers in the first part of the table. The double interpolation for the fractions of degrees of both thermometers being rather too large to be neglected, its application becomes inconvenient.

USE OF THE TABLE.

Enter the table with the observed temperatures of the dry and wet bulb thermometers. On the same line as the last, and in their appropriate columns, the results deduced from these data will be found.

Example.

The observation has given,

Temperature of the air by the dry thermometer $= 62^{\circ}$ F.

Temperature of evaporation by the wet-bulb thermometer = 53° F.

Page 129, find in the first column, headed Reading of the Dry Thermometer, the temperature of 62°, and in the second, that of the wet, 53°. On the line beginning with 53° are found, in their respective columns, the results deduced from these data, viz.:—

The temperature of the Dew-point $= 46^{\circ}.7$ F.

The force of vapor in the air = 0.333 inch.

The weight of vapor in a cubic foot of air = 3.72 grains.

The amount of vapor required for saturation = 2.53 grains.

The relative humidity in thousandths = 0.595

Res	ding Ther-	Temp.	Force		ght apor	Hu-		Weigh	t in Grai	ns of a Cu	ibic Foot	of Air.	
mon	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0 10	10.0	10.0	in. 0.089	gr. 1.11	gr. 0.00	1.000	gr. 550.1	gr. 560.0	gr. 569.8	gr. 579.6	gr. 589.4	gr. 599.2	gr. 609.0
10	9.8	8.3	0.084	1.05	0.06	0.946	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.6	6.6	0.079	0.98	0.13	0.883	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.4	4.9	0.074	0.92	0.19	0.829	550.2	560.1	569.9	579.7	589.5	599.3	609.1
	9.2	3.2	0.069	0.86	0.25	0.775	550.3	560.2	570.0	579.8	589.6	599.4	609.2
	9.0	1.5	0.065	0.81	0.30	0.730	550.3	560.3	570.0	579.8	589.6	599.4	609.3
11	11.0	11.0	0.093	1.15	0.00	1.000	548.9	558.7	568.5	578.3	588.1	597.9	607.7
1	10.8	9.3	0.087	1.08	0.07	0.939	548.9	558.7	568.5	578.3	588.1	597.9	607.7
	10.6	7.6	0.082	1.02	0.13	0.887	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.4	5.9	0.077	0.96	0.19	0.835	549.0	558.8	568.6	578.4	588.2	598.0	607.8
	10.2	4.2	0.072	0.90	0.25	0.783	549.0	558.8	568.6	578.4	588.2	598.0	607.S
	10.0	2.5	0.067	0.84	0.31	0.731	549.1	558.9	568.7	578.6	588.3	598.1	607.9
	9.8	0.8	0.063	0.78	0.37	0.679	549.1	558.9	568.7	578.6	588.3	598.1	607.9
12	12.0	12.0	0.096	1.19	0.00	1.000	547.7	557.5	567.2	577.0	586.8	596.6	606.4
	11.8	10.3	0.090	1.12	0.07	0.942	547.7	557.5	567.2	577.0	586.8	596.6	606.4
	11.6	8.6	0.085	1.05	0.14	0.883	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.4	6.9	0.080	0.99	0.20	0.832	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.2	5.2	0.075	0.93	0.26	0.782	547.8	557.6	567.3	577.1	586.9	596.7	606.5
	11.0	3.5	0.070	0.87	0.32	0.731	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.8	1.8	0.066	0.81	0.38	0.681	547.9	557.7	567.4	577.2	587.0	596.8	606.6
	10.6	0.1	0.061	0.76	0.43	0.639	547.9	557.7	567.4	577.2	587.0	596.8	606.6
13	13.0	13.0	0.100	1.24	0.00	1.000	546.5	556.3	566.0	575.S	585.5	595.3	605.0
	12.8	11.3	0.094	1.16	0.08	0.936	546.5	556.3	566.0	575.8	585.5	595.3	605.0
	12.6	9.6	0.088	1.08	0.16	0.871	546.6	556.4	566.1	575.9	585.6	595.4	605.1
1	12.4	7.9	0.083	1.02	0.22	0.823	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	12.2	6.2	0.077	0.97	0.27	0.783	546.7	556.5	566.2	576.0	585.7	595.5	605.2
1	12.0	4.5	0.073	0.91	0.33	0.734	546.7	556.5	566.2	576.0	585.7	595.5	605.2
	11.S	2.8	0.068	0.84	0.40	0.678	546.8	556.6	566.3	576.1	585.8	595.6	605.3
	11.6	1.1	0.064	0.79	0.45	0.637	546.8	556.6	566.3	576.1	585.8	595.6	605.3
14	14.0	14.0	0.104	1.28	0.00	1.000	545.3	555.0	564.7	574.4	584.2	594.0	603.7
li .	13.8	12.3	0.097	1.20	0.08	0.938	545.3	555.0	564.7	574.4	584.2	594.0	603.7
1	13.6	10.6	0.091	1.12	0.16	0.875	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.4	8.9	0.086	1.06	0.22	0.828	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.2	7.2	0.080	1.00	0.28	0.782	545.4	555.1	564.8	574.5	584.3	594.1	603.8
	13.0	5.5	0.075	0.93	0.35	0.727	545.5	555.2	564.9	574.6	584.4	594.2	603.9
	12.8	3.8	0.071	0.87	0.41	0.680	545.5	555.2	564.9	574.6	584.4	594.2	603.9
	12.6	2.1	0.066	0.82	0.46	0.641	545.6	555.3	565.0	574.7	584.5	594.2	603.9
15	15.0	15.0	0.108	1.32	0.00	1.000	544.0	553.8	563.5	573.2	582.9	592.6	602.3
	14.8	13.3	0.101	1.24	0.08	0.940	544.0	553.8	563.5	573.2	582.9	592.6	602.3
1	14.6	11.6	0.095	1.16	0.16	0.879	544.1	553.9	563.6	573.3	583.0	592.7	602.4
	14.4	9.9	0.089	1.10	0.22	0.833	544.1	553.9	563.6	573.3	583.0	592.7	602.4
	14.2	8.2	0.083	1.04	0.28	0.788	544.2	554.0		573.4	583.1	592.8	602.5
1	14.0	6.5	0.078	0.97	0.35	0.735	544.2	554.0	563.7	573.4	583.1	592.8	602.5
1	13.8	4.8	0.073	0.90	0.42	0.682	544.2		1		583.1	592.8	602.5
	13.6	3.1	0.069	0.85	0.47	0.644	544.3	554.1	563.8	573.5	583.2	592.9	602.6

	Reading f Ther-	Temp	Force		ight apor	Hu-		Weigh	t in Grai	ns of a C	ıbic Foot	of Air.	
m	ometer, Fahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
	0 00	100	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
16	16.0 15.8	16.0 14.3	0.112	1.37	0.00	1.000	542.8	552.5	562.2	571.9	581.6	591.3	601.0
ja ja	15.6	12.6	0.103	1.29	0.05	$0.942 \\ 0.883$	542.9 542.9	552.6	562.3	$572.0 \\ 572.0$	581.7	591.4	601.1 601.1
	15.4	10.9	0.093	1.14	0.10	0.832	543.0	552.6 552.7	562.3 562.4	572.0	581.7 581.8	591.4 591.5	601.1
i	15.2	9.2	0.032	1.07	0.23	0.332	543.0	552.7	562.4	572.1	581.8	591.5	601.2
1	15.0	7.5	0.081	1.00	0.37	0.730	543.0	552.7	562.4	572.1	581.S	591.5	601.2
H	14.8	5.8	0.076	0.94	0.43	0.686	543.1	552.8	562.5	572.1	581.9	591.6	601.3
	14.6	4.1	0.072	0.88	0.49	0.643	543.1	552.S	562.5	572.1	581.9	591.6	601.3
	1110	1	0.0,2		0.40	0.040	010.1	002.0	302.3	312.1	001.0	551.0	001.0
17	17.0	17.0	0.116	1.41	0.00	1.000	541.3	551.0	560.S	570.5	580.1	589.8	599.4
	16.8	15.3	0.109	1.33	0.08	0.943	541.3	551.0	560.8	570.5	580.1	589.8	599.4
	16.6	13.6	0.102	1.25	0.16	0.887	541.4	551.1	560.9	570.6	580.2	589.9	599.5
	16.4	11.9	0.096	1.17	0.24	0.830	541.4	551.1	560.9	570.6	580.2	589.9	599.5
	16.2	10.2	0.090	1.10	0.31	0.780	541.5	551.2	561.0	570.7	580.3	590.0	599.6
1	16.0	8.5	0.084	1.03	0.38	0.730	541.5	551.2	561.0	570.7	580.3	590.0	599.6
1	15.8	6.8	0.079	0.97	0.44	0.688	541.5	551.2	561.0	570.7	580.3	590.0	599.6
1	15.6	5.1	0.074	0.91	0.50	0.646	541.6	551.3	561.1	570.8	580.4	590.1	599.7
18	18.0	18.0	0.120	1.47	0.00	1.000	540.5	550.2	559.8	569.5	579.1	588.8	598.4
1	17.8	16.3	0.113	1.38	0.09	0.939	540.5	550.2	559.8	569.5	579.1	588.8	598.4
	17.6	14.6	0.106	1.29	0.18	0.878	540.6	550.3	559.9	569.6	579.2	588.9	598.5
1	17.4	12.9	0.099	1.21	0.26	0.824	540.6	550.3	559.9	569.6	579.2	588.9	598.5
1	17.2	11.2	0.093	1.14	0.33	0.776	540.7	550.4	560.0	569.7	579.3	589.0	598.6
	17.0	9.5	0.088	1.07	0.40	0.728	540.7	550.4	560.0	569.7	579.3	589.0	598.6
-	16.8	7.8	0.082	1.01	0.46	0.688	540.7	550.5	560.1	569.8	579.3	589.0	598.6
	16.6	6.1	0.077	0.95	0.52	0.647	540.8	550.6	560.2	569.9	579.4	589.1	598.7
19	19.0	19.0	0.125	1.52	0.00	1.000	539.3	E 10 A	558.5	568.2	577.8	587.5	597.1
18	18.8	17.3	0.125	1.43	0.00	0.941	539.3	548.9 548.9	558.5	568.2	577.8	587.5	597.1
	18.6	15.6	0.110	1.34	0.03	0.882	539.4	549.0	558.6	568.3	577.9	587.6	597.2
	18.4	13.9	0.103	1.26	0.26	0.829	539.4	549.0	558.6	568.3	577.9	587.6	597.2
li .	18.2	12.2	0.097	1.18	0.34	0.776	539.5	549.1	558.7	568.4	578.0	587.7	597.3
1	18.0	10.5	0.091	1.11	0.41	0.730	539.5	549.1	558.7	568.4	578.0	587.7	597.3
	17.8	8.8	0.085	1.04	0.48	0.684	539.6	549.2	558.8	568.5	578.1	587.8	597.4
	17.6	7.1	0.080	0.98	0.54	0.645	539.6	549.2	558.8	568.5	578.1	587.8	597.4
20		20.0	0.129	1.58	0.00	1.000	538.1	547.7	557.3	566.9	576.5	586.1	595.7
	19.8	18.3	0.121	1.48	0.10	0.937	538.2	547.8	557.4	567.0	576.6	586.2	595.8
	19.6	16.6	0.114	1.38	0.20	0.874	538.3	547.9	557.5	567.1	576.7	586.3	595.9
	19.4	14.9	0.107	1.30	0.28	0.823	538.3	l.	557.5	1	576.7	586.3	595.9
	19.2 19.0	li .	0.101	1.23	$0.35 \\ 0.43$	0.779	538.3	1	557.5	1	576.7	586.3	595.9
	18.8	11.5 9.8	0.094	1.15	0.43	0.728 0.684	538.4 538.4	548.0 548.0	557.6 557.6	567.2 567.2	576.8 576.8	586.4 586.4	596.0 596.0
	18.6	8.1	0.083	1.08	0.57	0.639	538.5	548.1	557.7	567.3	576.9	586.5	596.1
	18.4	11	0.033	0.95	0.63	0.601	538.5	548.1	557.7	567.3	576.9	586.5	596.1
	10.1	3.1		3.00	3.00	3.301				*****			
								}					
		}											} :
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of '	ding	Temp.	Force	Wei of V		Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
	neter, thr.	of Dew- Point,	of Vapor iu	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
21	21.0	21.0	in. 0.134	gr. 1.63	gr. 0.00	1.000	gr. 537.0	gr. 546.6	gr. 556.1	gr. 565. 7	gr. 575.3	gr. 584.9	gr. 594.5
-	20.8	19.3	0.126	1.53	0.10	0.939	537.0	546.6	556.1	565.7	575.3	584.9	594.5
	20.6	17.6	0.118	1.44	0.19	0.884	537.1	546.7	556.2	565.8	575.4	555.0	594.6
	20.4	15.9	0.111	1.36	0.27	0.835	537.1	546.7	556.2	565.8	575.4	585.0	594.6
	20.0					0 -0-						FOF 1	~0.4 ~
	20.2	14.2	0.104	1.28	0.35	0.785	537.2	546.8	556.3	565.9	575.5	585.1	594.7
	20.0	12.5	0.098	1.20	0.43	0.736	537.2	546.8	556.3	565.9	575.5	585.1	594.7
	19.8	10.8	0.092	1.12	0.51	0.687	537.3	546.9	556.4	566.0	575.6	585.2	594.8 594.8
	19.6 19.4	9.1	0.086	1.05 0.99	$0.58 \\ 0.64$	0.644	537.3 537.3	546.9 546.9	556.4 556.4	566.0 566.0	575.6 575.6	585.2 585.2	594.8
	19.4	14	0.031	0.99	0.04	0.007	991.9	540.5	930.4	300.0	373.0	303.2	334.0
22	22.0	22.0	0.139	1.69	0.00	1.000	535.7	545.3	554.9	564.5	574.0	583.6	593.1
	21.8	20.3	0.131	1.59	0.10	0.941	535.8	545.4	555.0	564.6	574.1	583.7	593.2
1	21.6	18.6	0.123	1.49	0.20	0.882	535.8	545.4	555.0	564.6	574.1	583.7	593.2
	21.4	16.9	0.115	1.40	0.29	0.828	535.9	545.5	555.1	564.7	574.2	583.8	593.3
	21.2	15.2	0.108	1.31	0.38	0.775	535.9	545.5	555.1	564.7	574.2	583.8	593.3
	21.0	13.5	0.102	1.23	0.46	0.728	536.0	545.6	555.2	564.8	574.3	583.9	593.4
	20.8	11.8	0.096	1.16	0.53	0.686	536.0	545.6	555.2	564.8	574.3	583.9	593.4
	20.6	10.1	0.090	1.09	0.60	0.645	536.1	545.7	555.3	564.9	574.4	584.0	593.5
	20.4	8.4	0.084	1.02	0.67	0.604	536.1	545.7	555.3	564.9	574.4	584.0	593.5
	20.2	6.7	0.079	0.96	0.73	0.568	536.1	545.7	555.3	564.9	574.4	584.0	593.5
								1					
23	23.0	23.0	0.144	1.75	0.00	1.000	534.6	544.2	553.7	563.3	572.8	582.4	591.9
	22.8	21.3	0.136	1.65	0.10	0.943	534.6	544.2	553.7	563.3	572.8	582.4	591.9
	22.6	19.6	0.127	1.55	0.20	0.886	534.7	544.3	553.8	563.4	572.9	582.5	592.0
	$22.4 \\ 22.2$	17.9 16.2	$\begin{vmatrix} 0.120 \\ 0.112 \end{vmatrix}$	1.45	$\begin{vmatrix} 0.30 \\ 0.39 \end{vmatrix}$	0.829	534.7	544.3	553.8 553.9	563.4 563.5	572.9 573.0	582.5 582.6	592.0 592.1
H	44.4	10.2	0.112	1.36	0.59	0.777	534.8	544.4	000.9	903.9	373.0	302.0	992.1
	22.0	14.5	0.106	1.28	0.47	0.731	534.8	544.4	553.9	563.5	573.0	582.6	592.1
	21.8	12.8	0.099	1.21	0.54	0.691	534.9	544.5	554.0	563.6	573.1	582.7	592.2
	21.6	11.1	0.093	1.13	0.62	0.646	534.9	544.5	554.0	563.6	573.1	582.7	592.2
	21.4	9.4	0.087	1.06	0.69	0.606	535.0	544.6	554.1	563.7	573.2	582.8	592.3
	21.2	7.7	0.082	1.00	0.75	0.571	535.0	544.6	554.1	563.7	573.2	582.8	592.3
	0.0	0.0	0.350	,	0.00	1,000				F.00.0			500.0
24	24.0	24.0	0.150	1.81	0.00	1.000	533.4	542.9	552.4	562.0	571.5	581.1	590.6 590.7
	23.8	22.5	$\begin{vmatrix} 0.142 \\ 0.135 \end{vmatrix}$	1.72	0.09	0.951	533.5	543.0		562.1	571.6 571.6	581.2 581.2	590.7
	$\begin{vmatrix} 23.6 \\ 23.4 \end{vmatrix}$	21.1 19.6	0.133	1.63 1.55	0.18	0.901	533.5	543.1 543.2	552.5 552.6	562.1	571.0	581.3	1
	23.4	18.2	0.127	1.46	0.26	0.807	533.6	1	1	562.2	571.7	581.3	590.8
	23.0	16.7	0.115	1.38	0.43	0.762	533.7	543.3	552.7	562.3	571.8	581.4	590.9
	22.8	15.2	1		0.50	0.724	1		1	562.3	1	1	1
	22.6	III.	0.103	1	0.57	0.685	l .	1		562.3	1	ł	590.9
	22.4	11	1	1	0.63	0.652	533.8		1	562.4		1	1
	22.2	10.8	1			0.634		1	1	562.4		1	

of '	ding Ther-	Temp.	Force of	We of V	ight apoi Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
	neter, ahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	- 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
25	25.0	25.0	0.155	1.87	0.00	1.000	532.3	541.8	551.3	560.8	570.3	579.8	589.3
	24.8	23.7	0.148	1.78	0.09	0.952	532.3	541.8	551.3	560.8	570.3	579.8	589.3
	24.6	22.4	0.141	1.70	0.17	0.909	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.4	21.2	0.135	1.62	0.25	0.867	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.2	19.9	0.129	1.55	0.32	0.829	532.4	541.9	551.4	560.9	570.4	579.9	589.4
	24.0	18.6	0.123	1.48	0.49	0.791	532.5	542.0	551.5	561.0	570.5	580.0	589.5
	23.8	17.3	0.117	1.41	0.46	0.754	532.5	542.0	551.5	561.0	570.5	580.0	589.5
	23.6	16.0	0.112	1.34	0.53	0.717	532.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.4	14.8	0.107	1.28	0.59	0.685	532.6	542.1	551.6	561.1	570.6	580.1	589.6
	23.2	13.5	0.102	1.22	0.65	0.653	532.6	542.1	551.6	561.1	570.6	580.1	589.6
26	26.0	26.0	0.161	1.93	0.00	1.000	531.1	540.6	550.0	559.5	569.0	578.5	588.0
20	25.8	24.8	0.154	1.85	0.08	0.959	531.1	540.7	550.0	559.6	569.1	578.6	588.1
	25.6	23.6	0.134	1.78	0.05	0.939 0.923	í	540.7	550.1	559.6	569.1	578.6	588.1
	25.4	22.3	0.141	1.70	0.13	0.881	531.2		550.1	559.6	569.1	578.6	588.1
	25.2	21.2	0.135	1.62	0.23	0.839	531.2 531.3	540.7 540.8	550.1	559.7	569.2	578.7	588.2
			0.100		0.01	0.000	331.0	01010	300.2	000.,	000.2	0.0	00012
	25.0	19.9	0.129	1.55	0.38	0.804	531.3	540.8	550.2	559.7	569.2	578.7	588.2
	24.8	18.7	0.123	1.48	0.45	0.767	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.6	17.5	0.118	1.41	0.52	0.731	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.4	16.2	0.112	1.35	0.58	0.700	531.4	540.9	550.3	559.8	569.3	578.8	588.3
	24.2	15.0	0.108	1.29	0.64	0.668	531.5	541.0	550.4	559.9	569.4	578.9	588.4
27	27.0	27.0	0.167	2.00	0.00	1.000	529.9	539.4	548.9	558.4	567.8	577.3	586.7
	26.7	25.2	0.156	1.88	0.12	0.940	529.9	539.4	548.9	558.4	567.8	577.4	586.8
1 [26.4	23.3	0.146	1.76	0.24	0.880	530.0	539.5	549.0	558.5	567.9	577.5	586.9
	26.1	21.5	0.137	1.64	0.36	0.820	530.1	539.6	549.1	558.6	568.0	577.6	587.0
	25.8	19.7	0.128	1.53	0.47	0.765	530.1	539.6	549.1	558.6	568.0	577.6	587.0
	25.5	17.8	0.119	1.43	0.57	0.715	530.2	539.7	549.2	558.7	568.1	577.7	587.1
	25.2	16.0	0.112	1.34	0.66	0.670	530.3	539.8	549.3	558.8	568.2	577.8	587.2
	24.9	14.2	0.104	1.26	0.74	0.630	530.3	539.8	549.3	558.8	568.2	577.8	587.2
	24.6	12.4	0.098	1.17	0.83	0.585	530.4	539.9	549.4	558.9	568.3	577.9	587.3
	24.3	10.5	0.091	1.09	0.91	0.545	530.5	540.0	549.5	559.0	568.3	577.9	587.3
28	28.0	28.0	0.173	2.07	0.00	1.000	528.7	538.1		ŀ	566.5	575.9	585.4
	27.7	1		1.95	ŀ	0.942	528.8	538.2	547.7	557.1	566.6	Į.	585.5
	27.4	24.6	0.153	1.84	0.23	0.889	528.9	538.3	547.8	557.2	566.7	576.1	585.6
1	27.1	22.9	0.144	1.73	0.34	0.836	528.9	538.3	547.8	557.2	566.7	576.1	585.6
	26.8	21.2	0.135	1.62	0.45	0.783	529.0	538.4	547.9	557.3	566.8	576.2	585.7
	26.5	19.4	0.126	1.52	0.55	0.734	529.1	538.5	548.0	557.4	566.9	576.3	585.8
	26.2	17.7	0.119	1.42	0.65	0.686	529.1	538.5	548.0	557.4	566.9	576.3	585.8
	25.9	16.0	0.112	1.34	0.73	0.648	529.2	538.6	548.1	557.5	567.0	576.4	585.9
	25.6	14.3	0.105	1.26	0.82	0.604	529.2	538.6	548.1	557.5	567.0	576.4	585.9
	25.3	12.6	0.098	1.18	0.89	0.571	529.2	538.6	548.1	557.5	567.0	576.4	585.9

	ading Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Grai	ns of a Cu	ibic Foot	of Air.	
mor	neter,	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
29	29.0	° 29.0	in. 0.179	gr. 2.14	gr. 0.00	1.000	gr. 527.6	gr. 537.0	gr. 546.5	gr. 555.9	gr. 565.3	gr. 574.7	gr. 584.1
29	28.7	27.5	0.170	2.03	0.11	0.949	527.7	537.1	546.6	556.0	565.4	574.8	584.2
	28.4	26.0	0.161	1.92	0.22	0.898	527.7	537.1	546.6	556.0	565.4	574.8	584.2
	28.1	24.5	0.152	1.82	0.32	0.851	527.8	537.2	546.7	556.1	565.5	574.9	584.3
	27.8	23.0	0.144	1.73	0.41	0.809	527.8	537.2	546.7	556.1	565.5	574.9	584.3
	27.5	21.5	0.137	1.64	0.50	0.766	527.9	537.3	546.7	556.2	565.6	575.0	584.5
	27.2	20.0	0.129	1.55	0.59	0.725	528.0	537.4	546.8	556.2	565.7	575.1	584.6
	26.9	18.5	0.122	1.47	0.67	0.687	528.0	537.4	546.8	556.3	565.7	575.2	584.6
	26.6	17.0	0.116	1.38	0.76	0.645	528.1	537.5	546.9	556.4	565.8	575.3	584.7
	26.3	15.5	0.110	1.30	0.84	0.617	528.1	537.5	546.9	556.4	565.8	575.3	584.7
0.0	80.0	20.0	0.186	2 21	0.00	1.000	526.5	535.9	545.3	554.7	564.1	573.5	582.9
30	30.0	30.0	0.130	$2.21 \\ 2.10$	0.11	0.951	526.5	535.9	545.3	554.7	564.1	573.5	582.9
	29.7 29.4	$\begin{vmatrix} 28.6 \\ 27.2 \end{vmatrix}$	0.168	2.00	0.11	0.905	526.6	536.0	545.4	554.8	564.2	573.6	583.0
	29.1	25.9	0.160	1.91	0.30	0.864	526.7	536.1	545.5	554.9	564.3	573.7	583.
	28.8	24.5	0.152	1.82	0.39	0.824	526.7	536.1	545.5	554.9	564.3	573.7	583.
	28.5	23.1	0.145	1.73	0.48	0.783	526.8	536.2	545.6	555.0	564.4	573.8	583.
	28.2	21.7	0.138	1.64	0.57	0.742	526.8	536.2	545.6	555.0	564.4	573.8	583.2
	27.9	20.3	0.131	1.56	0.65	0.706	526.9	536.3	545.7	555.1	564.5	573.9	583.3
	27.6	19.0	0.125	1.49	0.72	0.674	526.9	536.3	545.7	555.1	564.5	573.9	583.3
	27.3	17.6	0.118	1.42	0.79	0.643	527.0	536.4	545.8	555.2	564.6	574.0	583.4
31	31.0	31.0	0.192	2.29	0.00	1.000	525.4	534.7	544.1	553.5	562.9	572.3	581.
	30.7	29.9	0.185	2.20	0.09	0.961	525.4	534.7	544.1	553.5	562.9	572.3	581.
	30.4	28.8	0.178	2.12	0.17	0.926	525.5	534.8	544.2	553.6	563.0	572.4	581.5
	$\begin{vmatrix} 30.1 \\ 29.8 \end{vmatrix}$	27.7 26.6	0.171	2.04 1.95	$\begin{vmatrix} 0.25 \\ 0.34 \end{vmatrix}$	0.891	525.5 525.6	534.8 534.9	544.2 544.3	553.6 553.7	563.0 563.1	572.4 572.5	581.8
İ	29.5	25.5	0.158	1.87	0.42	0.817	525.6	534.9	544.3	553.7	563.1	572.5	581.9
	29.2	24.4	0.152	1.80	0.49	0.786	525.6	534.9	544.3	553.7	563.1	572.5	581.
	28.9	23.4	0.146	1.73	0.56	0.756	525.7	535.0	544.4	553.8	563.2	572.6	582.
	28.6	22.3	0.141	1.67	0.62	0.729	525.7	535.0	544.4	553.8	563.2	572.6	582.
	28.3	21.2	0.135	1.60	0.69	0.699	525.7	535.0	544.4	553.8	563.2	572.6	582.0
													500
32	32.0	32.0	0.199	2.37	0.00	1.000	524.2	533.5	542.9	552.3	561.6	570.9	580.
	31.6	30.8	0.191	2.27	0.10	0.958	524.3	533.6	543.0	552.4	561.7	571.0	580. 580.
	31.2	29.5	0.182	2.17	0.20	1		533.7	543.1	552.5	561.8	571.1 571.1	580.
	30.8 30.4	28.3 27.0	0.175 0.167	2.07 1.98	0.30	0.874 0.836	524.4 524.5	533.7 533.8	543.1 543.2	552.5 552.6	561.9	571.1	580.
	30.0	25.8	0.160	1.90	0.47	0.802	524.5	533.8	543.2	552.6	561.9	571.2	580.
	29.6	24.6	0.153	1		0.768		1	543.3	552.7	562.0	571.3	580.
	29.2		0.146	1	1	0.735	1	1	1	1	1	571.3	580.
	28.8	22.1	0.140	1.67		0.705	524.6	533.9	543.3	1	562.0	1	580.
1	28.4	20.8	0.133	1.60	0.77	0.675	524.7	534.0	543.4	552.8	562.1	571.4	580.

	ading Ther-	Temp.	Force	We of V	ight apor	Hn-		Weigh	t in Grai	as of a Cu	ibic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
33	$33.0 \\ 32.5$	33.0	$0.207 \\ 0.197$	$2.45 \\ 2.33$	$\begin{bmatrix} 0.00 \\ 0.12 \end{bmatrix}$	$1.000 \\ 0.951$	523.0 523.1	532.3	541.7	551.1	560.4 560.5	569.7 569.8	579.1 579.2
	32.0	30.2	0.187	2.22	$0.12 \\ 0.23$	0.906	523.1	532.5	541.8	551.2	560.6		579.3
	31.5	28.8	0.137	2.11	0.23	0.862	523.3	532.6 532.7	541.9	551.3	560.7	569.9 570.0	579.
	31.0	27.4	0.178	2.01	0.44	0.862	523.3		542.0	551.4	560.7	570.0	579.
	31.0	21.4	0.109	2.01	0.44	0.821	323.3	532.7	542.0	551.4	360.7	910.0	019.5
	30.5	26.0	0.161	1.91	0.54	0.780	523.4	532.8	542.1	551.5	560.8	570.1	579.5
	30.0	24.6	0.153	1.82	0.63	0.743	523.4	532.8	542.1	551.5	560.8	570.1	579.5
	29.5	23.2	0.145	1.74	0.71	0.711	523.5	532.9	542.2	551.6	560.9	570.2	579.6
	29.0	21.8	0.138	1.65	0.80	0.674	523.5	532.9	542.2	551.6	560.9	570.2	579.6
	28.5	20.4	0.131	1.57	0.88	0.641	523.6	533.0	542.3	551.7	561.0	570.3	579.7
34	34.0	34.0	0.214	2.53	0.00	1.000	521.9	531.2	540.6	549.9	559.2	568.5	577.8
0.1	33.5	32.7	0.204	2.42	0.11	0.957	522.0	531.4	540.7	550.0	559.3	568.6	577.9
	33.0	31.4	0.195	2.31	0.22	0.913	522.0	531.4	540.7	550.0	559.3	568.6	577.9
	32.5	30.1	0.186	2.21	0.32	0.874	522.1	531.5	540.8	550.1	559.4	568.7	578.0
	32.0	28.8	0.178	2.11	0.42	0.834	522.1	531.5	540.8	550.1	559.4	568.7	578.0
	31.5	27.5	0.170	2.01	0.52	0.795	522.2	531.6	540.9	550.2	559.5	568.8	578.
	31.0	26.2	0.162	1.91	0.62	0.755	522.3	531.7	541.0	550.3	559.6	568.9	578.
	30.5	24.9	0.155	1.83	0.70	0.724	522.3	531.7	541.0	550.3	559.6	568.9	578.2
	30.0	23.6	0.147	1.75	0.78	0.692	522.4	531.8	541.1	550.4	559.7	569.0	578.
	29.5	22.3	0.141	1.67	0.86	0.660	522.4	531.8	541.1	550.4	559.7	569.0	578.
	29.0	21.0	0.134	1.59	0.94	0.629	522.5	531.9	541.2	550.5	559.8	569.1	578.4
35	35	35.0	0.222	2.62	0.00	1.000	520.8	530.1	539.4	548.7	558.0	567.3	576.6
	34	32.5	0.203	2.40	0.22	0.916	520.9	530.2	539.5	548.8	558.1	567.4	576.
	33	30.0	0.186	2.19	0.43	0.836	521.0	530.3	539.6	548.9	558.3	567.5	576.8
	32	27.5	0.170	2.00	0.62	0.764	521.1	530.4	539.7	549.0	558.4	567.6	576.9
	31	25.0	0.155	1.83	0.79	0.698	521.2	530.5	539.8	549.1	558.5	567.7	577.0
	30	22.5	0.142	1.68	0.94	0.641	521.3	530.6	539.9	549.2	558.6	567.8	577.
	29	20.0	0.129	1.53	1.09	0.584	521.3	530.7	540.0	549.3	558.6	567.9	577.5
	28	17.5	0.117	1.39	1.23	0.531	521.4	530.8	540.1	549.4	558.7	568.0	577.
	27	15.0	0.108	1.27	1.35	0.485	521.5	530.9	540.2	549.5	558.7	568.1	577.
9.0	90	20.0	0.000	0.71	0.00	1.000	£10.5	#00 C	E90 0	5177	556.8	566.1	575.
36	36	36.0	0.230	$\begin{vmatrix} 2.71 \\ 2.48 \end{vmatrix}$	0.00	1.000	519.7	529.0	538.3	547.5	556.9	566.2	575.
	35	33.5	0.210		0.23	0.915	519.8		1	547.6		566.3	575.
	34	31.0	0.192 0.176	$\begin{vmatrix} 2.27 \\ 2.07 \end{vmatrix}$	0.44	0.838 0.764	519.9 520.0	529.2 529.3	538.5 538.6	547.7 547.8	557.0 557.1	566.4	575.
	33 32	$28.5 \\ 26.0$	0.176	1.89	0.84	0.764	520.0	529.4	538.7	547.9	557.2	566.5	575.
	31	23.5	0.147	1.74	0.97	0.642	520.2	529.5	538.8	548.0	557.3	566.6	575.
	30	21.0	0.134	1.58	1.13	0.583	520.3	529.6	538.9	548.1	557.4	566.7	576.
	29	18.5	0.122	1.45	1.26	0.535	520.4	529.7	539.0	548.2	557.5	566.8	576.
	28	16.0	0.112	1.32	1.39	0.487	520.5	529.8	539.1	548.3	557.6	566.9	576.
		1			ļ			1			1		

	iding	Temp.	Force	Wei of V		Hu-		Weight	t in Grain	ns of a Cu	ibic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.		of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	7 000	gr.	gr.	gr.	gr.	gr.	gr. 564.8	gr. 574.1
37	37 36	37.0 34.5	$0.238 \\ 0.218$	$2.80 \\ 2.56$	$\begin{bmatrix} 0.00 \\ 0.24 \end{bmatrix}$	1.000 0.914	518.6 518.7	$527.8 \ 527.9$	537.1 537.2	546.3 546.4	555.6 555.7	564.9	574.1
	35	32.0	0.218	2.35	0.45	0.839	518.8	528.0	537.3	546.5	555.8	565.0	574.3
	34	29.5	0.182	2.14	0.66	0.764	518.9	528.1	537.4	546.6	555.9	565.1	574.4
	33	27.0	0.167	1.96	0.84	0.700	519.0	528.2	537.5	546.7	556.0	565.2	574.5
	32	24.5	0.152	1.79	1.01	0.640	519.1	528.3	537.6	546.8	556.1	565.3	574.6
'	31	22.0	0.139	1.64	1.16	0.586	519.2	528.4	537.7	546.9	556.2	565.4	574.7
	30	19.5	0.127	1.50	1.30	0.536	519.3	528.5	537.8	547.1	556.3	565.5	574.8
	29	17.0	0.116	1.37	1.43	0.489	519.4	528.6	537.9	547.2	556.4	565.6	574.9
38	38	38.0	0.246	2.89	0.00	1.000	517.4	526.6	535.9	545.1	554.4	563.6	572.9
	37	35.5	0.226	2.65	0.24	0.917	517.5	526.7	536.0	545.2	554.5	563.7	573.0
	36	33.0	0.207	2.43	0.46	0.841	517.6	526.8	536.1	545.3	554.6	563.8	573.1
	35	30.5	0.189	2.22	0.67	0.768	517.7	526.9	536.2	545.4	554.7	563.9	573.2
	34	28.0	0.173	2.03	0.86	0.703	517.8	527.0	536.3	545.5	554.8	564.0	573.3
	33	25.5	0.158	1.85	1.04	0.640	517.9	527.1	536.4	545.6	554.9	564.1	573.4
	32	23.0	0.144	1.70	1.19	0.588	518.0	527.2	536.5	545.7	555.0	564.2	573.5
	31	20.5	0.132	1.54	1.35	0.533	518.1	527.3	536.6	545.8	555.1	564.3	573.6
	30	18.0	0.120	1.39	1.50	0.481	518.2	527.4	536.7	545.9	555.2	564.4	573.7
												1	
39	39	39.0	0.255	2.99	0.00	1.000	516.3	525.5	534.7	543.9	553.2	562.4	571.6
	38	36.5	0.234	2.74	0.25	0.917	516.4	525.6	534.8	544.0	553.3	562.5	571.7
	37	34.0	0.214	2.51	0.48	0.840	516.5	525.7	534.9	544.1	553.4	562.6	571.8
	36	31.5	0.196	2.30	0.69	0.769	516.6	525.8	535.0	544.2	553.5	562.7	571.9
	35	29.0	0.179	2.10	0.89	0.703	516.7	525.9	535.1	544.3	553.6	562.8	572.1
	34	26.5	0.164	1.91	1.08	0.639	516.8	526.0	535.2	544.4	553.7	562.9	572.2
	33	24.0	0.150	1.76	1.23	0.589	516.9	526.1	535.3	544.5	553.8	563.0	572.3
	32	21.5	0.137	1.60	1.39	0.535	517.0	526.2	535.4	544.6	553.9	563.1	572.4
	31	19.0	0.125	1.46	1.53	0.488	517.1	526.3	535.6	544.8	554.1	563.3	572.6
	30	16.5	0.114	1.32	1.67	0.442	517.2	526.4	535.7	544.9	554.2	563.4	572.7
												507.2	
40	40	40.0	0.264	1	0.00	1.000	515.2	524.4	533.6	542.8	552.0	561.2	570.4
1	39	37.8	0.245	2.86	0.23	0.926	515.3	524.5	533.7	542.9 543.0	552.1 552.2	561.3 561.4	570.5 570.6
	38 37	35.6 33.4	$0.227 \\ 0.210$,	0.44	0.858	515.4 515.5	524.6 524.7	1		552.3		
	36	31.2	0.210				515.6	1	1	1		1	
		1						1				561.7	570.9
	35	29.0	0.179	1	4		515.7	524.9 525.0	1	1			1
1	34 33	26.8 24.6	0.165	1		1	515.8 515.9	525.1			1	1	1
	32	22.4		1	1		516.0	525.2	1	1	1	[1
1	31	20.2	1			1	516.1	525.3		1	1	1	571.3
	30	18.0	T .		1		516.1	525.3		1	1	1	
		-											

Rea of '	ding Ther-	Temp.	Force	We of V	ight apor	Hu-		Weigh	t in Grain	as of a Ci	ıbic Foot	of Air.	
	neter, ihr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	3 1.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
41	41	41.0 38.8	$0.274 \\ 0.253$	3.19 2.96	$0.00 \\ 0.23$	1.000 0.928	514.1 514.2	523.3 523.4	532.5 532.6	541.6 541.7	550.8 550.9	560.0 560 1	569.2 569.3
1	39	36.6	0.235	2.74	0.45	0.859	514.3	523.5	532.7	541.8	551.0	560.2	569.4
	38	34.4	0.217	2.54	0.65	0.796	514.4	523.6	532.8	541.9	551.1	560.3	569.5
1	37	32.2	0.201	2.35	0.84	0.737	514.5	523.7	532.9	542.0	551.2	560.4	569.6
	36	30.0	0.186	2.16	1.03	0.677	514.6	523.8	533.0	542.1	551.3	560.5	569.7
							I						
	35	27.8	0.172	2.01	1.18	0.630	514.7	523.9	533.1	542.2	551.4	560.6	569.8
	34	25.6	0.158	1.85	1.34	0.580	514.8	524.0	533.2	542.3	551.5	560.7	569.9
	33	23.4	0.146	1.71	1.48	0.536	514.9	524.1	533.3	542.4	551.6	560.8	570.0
	32	21.2	0.135	1.58	1.61	0.495	514.9	524.1	533.3	542.5	551.7	560.9	570.1
-	31	19.0	0.125	1.46	1.73	0.458	515.0	524.2	533.4	542.6	551.8	561.0	570.2
42	42	42.0	0.283	3.30	0.00	1.000	513.0	522.2	531.3	540.5	549.6	558.8	567 9
	41	39.8	0.263	3.06	0.24	0.927	513.1	522.3	531.4	540.6	549.7	558.9	568.0
İ	40	37.6	0.243	2.83	0.47	0.858	513.2	522.4	531.5	540.7	549.9	559.0	568.1
	39	35.4	0.225	2.63	0.67	0.797	513.3	522.5	531.6	540.8	550.0	559.1	568.2
	38	33.2	0.208	2.43	0.87	0.736	513.4	522.6	531.7	540.9	550.1	559.2	568.3
l	37	31.0	0.192	2.24	1.06	0.679	513.5	522.7	531.8	541.0	550.2	559.3	568
		28.8			1.22	0 691	519 C	500 0		E (1 1	550.9	550 (568.5
- 1	36	1	0.178	2.08		0.631	513.6	522.8	531.9	541.1	550.3	559.4	568.6
	35	$26.6 \\ 24.4$	0.164	1.91	1.39 1.53	0.579 0.536	513.7 513.8	522.9	532.0	541.2	550.4 550.5	559.5 559.6	568.
	34 33	22.2	$0.152 \\ 0.140$	1.77 1.63	1.67	0.494	513.9	523.0 523.1	532.1 532.2	541.3 541.4	550.6	559.7	568.8
-	32	20.0	0.140	1.51	1.79	0.454	513.9	523.1	532.3	541.5	550.6	559.8	569.0
1	شد	20.0	0.129	1.91	1.75	0.400	513.5	920.1	332.3	941.9	330.0	999.0	303.0
43	43	43.0	0.293	3.41	0.00	1.000	511.8	520.9	530.1	539.3	548.4	557.5	566.7
1	42	40.8	0.272	3.16	0.25	0.927	511.9	521.0	530.2	539.4	548.6	557.7	566.9
1	41	38.6	0.252	2.93	0.48	0.859	512.0	521.1	530.3	539.5	548.7	557.8	567.0
	40	36.4	0.233	2.71	0.70	0.795	512.1	521.2	530.4	539.6	548.8	557.9	567.
	39	34.2	0.216	2.51	0.90	0.736	512.2	521.3	530.5	539.7	548.9	558.0	567.2
i	38	32.0	0.199	2.32	1.09	0.680	512.3	521.4	530.7	539.8	549.0	558.1	567.3
	37	29.8	0.184	2.15	1.26	0.630	512.4	521.5	530.8	539.9	549.1	558.2	567.4
	36	27.6	0.170	1.98	1.43	0.581	512.5	521.6	530.9	540.0	549.2	558.3	567.
	35	25.4	0.170	1.82	1.59	0.534	512.6	521.7	531.0	540.1	549.3	558.4	567.6
	34	23.2	0.145	1.69	1.72	0.495	512.7	521.8	531.1	540.2	549.4	558.5	567.7
	33	21.0	0.134	1.56	1.85	0.458	512.9	522.0	531.2	540.3	549.5	558.6	567.8
44	44	44.0	0.304	3.52	0.00	1.000	510.8	519.9	529.0	538.1	547.3	556.4	565.5
	43	41.8	0.282	3.27	0.25	0.929	510.9	520.0	529.1	538.2	547.5	556.5	565.7
	42	39.6	0.261	3.02	0.50	0.858	511.0		ı		547.6		1
	41	37.4	0.241	2.80	0.72	0.796	511.1	520.2	529.3	538.4	547.7	556.7	565.9
	40	35.2	0.223	2.60	0.92	0.739	511.2	520.3	529.4	538.5	547.8	556.8	566.0
	39	33.0	0.207	2.40	1.12	0.682	511.3	520.4	529.5	538.6	547.9	556.9	566.
	38	30.8	0.191		1.30			520.5	529.6	538.7	548.0	557.0	566.2
	37	28.6	0.191	2.22		$0.631 \\ 0.582$	511.4 511.5	520.6	529.6	538.8	548.1	557.1	566.3
	36	26.4	0.163	$\frac{2.05}{1.89}$	1.47	0.537	511.6	520.5	529.8	538.9	548.2	557.1	566.
	35	24.2	0.151	1.59	1.03	0.337	511.7	520.7	529.9	539.0	548.3	557.3	566.5
	34	22.0	0.131	1.62	1.90	0.460	1	520.8	1	539.1			566.6
!	01	22.0	0.103	1.02	1.50	0.400	011.7	020.0	000.0	000.1	0.00	00111	, 550.

	ding Ther-	Temp.	Force		ight apor	Hu-		Weigh	t in Graiı	as of a Ci	ahic Foot	of Air.	
mon	neter, thr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
45	0	45.0	in. 0.315	gr. 3.64	gr. 0.00	1.000	gr. 509.7	gr. 518.8	gr. 527.9	gr. 537.0	gr. 546.1	gr. 555.2	gr. 564.3
45	45	42.9	$0.315 \\ 0.292$	3.39	0.00	0.931	509.7	518.9	528.0	537.1	546.3	555-3	564.5
1	44	40.8	0.252 0.272	3.14	0.50	0.863	509.9	519.0	528.1	537.1	546.4	555.4	564.0
	43 42	38.7	0.272	2.92	0.72	0.802	510.0	519.1	528.2	537.3	546.5	555.5	564.
	41	36.6	0.235	2.70	0.72	0.302	510.0	519.2	528.3	537.4	546.6	555.6	564.
	40	34.5	0.233	2.52	1.12	0.692	510.1	519.3	528.4	537.5	546.7	555.7	564.
			1]			1			1	1		
	39	32.4	0.202	2.34	1.30	0.643	510.3	519.4	528 5	537.6	546.8	555.8	565.
	38	30.3	0.188	2.16	1.48	0.593	510.4	519.5	528.6	537.7	546.9	555.9	565.
	37	28.2	0.174	2.01	1.63	0.552	510.5	519.6	528.7	537.8	547.0	556.0	565.
	36	26.1	0.161	1.87	1.77	0.514	510.6	519.7	528.8	537.9	547.1	556.1	565.
	35	24.0	0.150	1.73	1.91	0.475	510.7	519.8	528.9	538.0	547.2	556.3	565.
46	46	46.0	0.326	3.76	0.00	1.000	508.6	517.7	526.7	535.S	544.9	554.0	563.
40	45	43.9	0.303	3.50	0.26	0.931	508.7	517.8	526.8	535.9	545.0	554.1	563.
	44	41.8	0.303	3.25	0.20	0.864	508.8	517.9	526.9	536.0	545.1	554.2	563.
	43	39.7	0.262	3.02	0.74	0.803	508.9	518.0	527.0	536.1	545.2	554.3	563.
İ	42	37.6	0.243	2.80	0.96	0.745	509.0	518.1	527.2	536.3	545.4	554.5	563.
ł	41	35.5	0.226	2.61	1.15	0.694	509.1	518.2	527.3	536.4	545.5	554.6	563.
i	i				1			1		i	1	554.7	
	40	33.4	0.210	2.42	1.34	0.643	509.2	518.3	527.4	536.5	545.6	554.8	563.
1	39	31.3	0.194	2.24	1.52	0.596	509.3	518.4	527.5	536.6	545.7		563.
	38	29.2	0.180	2.08	1.68	0.553	509.4	518.5	527.6	536.7	545.8	554.9	564
	37	27.1	0.167	1.93	1.83	0.514	509.5	518.6	527.7	536.8	545.9	555.0	564.
	36	25.0	0.155	1.79	1.97	0.476	509.5	518.6	527.7	536.8	545.9	555.0	564.
47	47	47.0	0.337	3.88	0.00	1.000	507.5	516.5	525.6	534.7	543.8	552.8	561.
	46	44.9	0.313	3.62	0.26	0.933	507.6	516.6	525.7	534.8	543.9	552.9	562.
	45	42.8	0.291	3.36	0.52	0.866	507.8	516.7	525.9	535.0	544.1	553.1	562.
	44	40.7	0.271	3.12	0.76	0.804	507.9	516.8	526.0	535.1	544.2	553.2	562.
	43	38.6	0.252	2.90	0.98	0.747	508.0	516.9	526.1	535.2	544.3	553.3	562.
	42	36.5	0.234	2.70	1.18	0.696	508.1	517.0	526.2	535.3	544.4	553.4	562.
ì	41					0.647	508.2	l	526.3	535.4	544.5	553.5	562.
	40	34.4	$0.217 \\ 0.201$	$2.51 \\ 2.32$	1.37 1.56	0.598	508.3	$517.1 \\ 517.2$	526.4	535.5	544.6	553.6	562.
	39	30.2	0.201	2.32	1.72	0.557	508.4	517.3	526.5	535.6	544.7	553.7	562.
	38	28.1	0.157	2.10	1.72	0.515	508.5	517.4	526.6	535.7	544.7	553.8	562.
	37	26.0	0.173	1.85	2.03	0.477	508.5	517.4	526.7	535.8	544.9	554.0	563.
48	48	48.0	0.349	4.01	0.00	1.000	506.4	515.4	524.5	533.5	542.6	551.6	560.
	47	45.9	0.324	3.73	0.28	0.930	506.5	515.5	524.6	533.7	542.8	551.8	560.
	46	43.8	0.302	3.47	0.54	0.865	506.6	515.6	524.7	533.8	542.9	551.9	561.
	45	41.7	0.281	3.23	0.78	0.805	506.7	515.7	524.8	533.9	543.0	552.0	561.
	44	39.6	0.261	3.00	1.01	0.748	506.8	515.8	524.9	534.0	543.1	552.1	561.
	43	37.5	0.242	2.79	1.22	0.696	506.9	515.9	525.0	534.1	543.2	552.2	561.
	42	35.4	0.225	2.60	1.41	0.648	507.0	516.0	525.1	534.2	543.3	552.3	561.
	41	33.3	0.223	2.40	1.41	0.598	507.0	516.1	525.2	534.4	543.5	552.5	561.
	40	31.2	0.209	2.24	1.77	0.558	507.1	516.2	525.3	534.5	543.5	552.5	561.
	39	29.1	0.184	2.24	1.94	0.538	507.3	516.3	525.4	534.6	543.6	552.6	561.
		27.0	0.180	1.92	2.09	0.316	507.4	1		1	l .	552.7	561.
	38							516.4	525.5	534.7	543.6	1337.7	

	ding Ther-	Temp.	Force	of V	ight apor	Hu-		Weigh	t in Grain	as of a Cu	bic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion ==		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.		of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
49	° 49	49.0	in. 0.361	gr. 4.14	gr. 0.00	1.000	gr. 505,3	gr. 514.3	gr. 523.3	gr. 532.3	gт. 541.4	gr. 550.4	gr. 559.
10	48	46.9	0.336	3.85	0.29	0.930	505.4	514.4	523.4	532.4	541.5	550.5	559.
	47	44.8	0.312	3.59	0.55	0.867	505.6	514.6	523.6	532.6	541.7	550.7	559.
	46	42.7	0.290	3.34	0.80	0.807	505.7	514.7	523.7	532.7	541.8	550.8	559.8
	45	40.6	0.270	3.10	1.04	0.749	505.9	514.9	523.8	532.9	542.0	551.0	560.
	44	38.5	0.251	2.88	1.26	0.696	506.0	515.0	523.9	533.0	542.1	551.1	560.
	43	36.4	0.233	2.68	1.46	0.647	506.1	515.1	524.0	533.1	542.2	551.2	560.
	42	34.3	0.216	2.49	1.65	0.601	506.2	515.2	524.1	533.2	542,3	551.3	560.
ŀ	41	32.2	0.201	2.32	1.82	0.560	506.3	515.3	524.2	533.3	542.4	551.4	560.
	40	30.1	0.186	2.14	2.00	0.517	506.3	515.3	524.3	533.4	542.5	551.5	560.
	39	28.0	0.173	1.99	2.15	0.481	506.4	515.4	524.4	533.5	542.6	551.6	560.
	38	25.9	0.160	1.84	2.30	0.444	506.4	515.4	524.4	533.5	542,6	551.6	560.
50	50	50.0	0.373	4.28	0.00	1.000	504.1	513.1	522.1	531.1	540.2	549.2	558.
1	49	48.0	0.349	3.99	0.29	0.932	504.2	513.2	522.2	531.2	540.3	549.3	558.
1	48	46.0	0.326	3.73	0.55	0.871	504.4	513.4	522.4	531.4	540.5	549.5	558.
ļ	47	44.0	0.304	3.48	0.80	0.813	504.5	513.5	522.5	531.5	540.6	549.6	558.
Ì	46	42.0	0.283	3.25	1.03	0.759	504.6	513.6	522.6	531.6	540.7	549.7	558.
1	45	40.0	0.264	3.03	1.25	0.708	504.8	513.8	522.8	531.8	540.9	549.9	558.
İ	44	38.0	0.246	2.82	1.46	0.659	504.9	513.9	522.9	532.0	541.0	550.0	559.
	43	36.0	0.230	2.63	1.65	0.614	505.1	514.1	523.1	532.1	541.2	550.2	559.
	42	34.0	0.214	2.45	1.83	0.572	505.2	514.2	523.2	532,2	541.3	550.3	559.
	41	32.0	0.199	2.28	2.00	0.533	505.3	514.3	523.3	532.3	541.4	550.4	559.
	40	30.0	0.186	2.12	2.16	0.495	505.4	514.4	523.4	532.4	541.5	550.5	559.
-,	39	28.0	0.173	1.97	2.31	0.460	505.5	514.5	523.5	532,5	541.6	550.6	559.
51	51	51.0	0.386	4.42	0.00	1.000	503.1	512.1	521.1	530.0	539.0	548.0	557.
	50 49	49.0	0.361	4.12	0.30	0.932	503.2	512.2	521.2	530.1	539.1	548.1	557.
l	48	47.0 45.0	0.337 0.315	3.85 3.60	$\begin{array}{c} 0.57 \\ 0.82 \end{array}$	0.871	503.3 503.4	512.3	521.3	530.3 530.4	539.3	548.3	557.
ŀ	47	43.0	0.293	3.36	1.06	$0.814 \\ 0.760$	503.5	512.4 512.5	$521.4 \\ 521.5$	530.5	539.4 539.5	548.4 548.5	557. 55 7 .
1	46	41.0	0.253 0.274	3.13	1.29	0.708	503.7	512.5	521.5	530.7	539.7	548.7	557. 557.
į	45	39.0	0.255	2.92	1.50	0.661	503.8	512.8	521.7	530.8	539.8	548.8	557.
	44	37.0	0.238	2.72	1.70	0.615	503.9	512.9	521.9	530.9	539.9	548.9	557.
İ	43	35.0	0.222	2.54	1.88	0.575	504.0	513.0	522.0	531.0	540.0	549.0	558.
	42	33.0	0.207	2.36	2.06	0.534	504.1	513.1	522.1	531.1	540.1	549.1	558.
1	41	31.0	0.192	2.20	2.22	0.498	504.2	513.2	522.2	531.2	540.3	549.3	558.
	40	29.0	0.179	2.05	2.37	0.464	504.3	513.3	522.3	531.3	540.4	549.4	558.
52	52	52.0	0.400	4.56	0.00	1.000	502.1	511.0	520.0	528.9	537.9	546.8	555.
	51	50.0	0.373	4.26	0.30	0.934	502.2	511.1	520.1	529.0	538.0	546.9	555.
1	50	48.0	0.349	3.98	0.58	0.873	502.4	511.3	520.3	529.2	538.2	547.1	556.
	49	46.0	0.326	3.72	0.84	0.816	502.5	511.4	520.4	529.3	538.3	547.2	556.
	48	44.0	0.304	3.47	1.09	0.761	502.6	511.5	520.5	529.4	538.4	547.3	556.
	47	42.0	0.283	3.23	1.33	0.709	502.8	511.7	520.7	529.6	538.6	547.5	556.
	46	40.0	0.264	3.02	1.54	0.662	502.9	511.8	520.8	529.7	538.7	547.6	556.
	45	38.0	0.246	2.81	1.75	0.616	502.9	511.9	520.9	529.8	538.8	547.8	556.
	44	36.0	0.230	2.63	1.93	0.577	503.1	512.0	521.0	529.9	539.0	548.0	557.
	43	34.0	0.214	2.44	2.12	0.535	503.2	512.1	521.1	530.0	539.1	548.1	557.
	42 41	32.0 30.0	0.199	2.28 2.13	2.28	0.500 0.467	503.3 503.4	512.3 512.4	521.3 521.4	530.2 530.3	539.2 539.3	548.2 548.3	55 7 .
	1	1, 50.0	7.100	4.19	2.49	3.307	203.4	014.4	041.4	200.0	202.0	340.0	3011

	ding Ther-	Temp.	Force	We of V	ight 'apor	Hu-		Weigh	t in Grain	as of a Ci	ıbie Foot	of Air.	
mon	neter, shr.	of Dew-	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura-		Height	of the Ba	rometer i	n English	h Inches	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	tion == 1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr,	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
53	53	53.0	0.414	4.71	0.00	1.000	500.9	509.8	518.8	527.7	536.7	545.6	554.6
	52	51.0	0.386	4.40	0.31	0.934	501.1	510.0 510.1	519.0	527.9	536.9	545 8 545.9	554.8 554.9
	51	49.0	$0.361 \\ 0.337$	4.11 3.84	$0.60 \\ 0.87$	0.873 0.815	501.2 501.4	510.1	519.1 519.3	528.0 528.2	537.0 537.2	546.1	555.1
	50 49	45.0	0.315	3.58	1.13	0.760	501.4	510.3	519.4	528.3	537.3	546.2	555.2
i	48	43.0	0.293	3.34	1.37	0.709	501.6	510.5	519.5	528.4	537.4	546.3	555.3
	i	i				1	l		:			. 8	!
	47	41.0	0.274	3.12	1.59	0.662	501.7	510.6	519 6	528.5	537.5	546.4	555.4
	46	39.0	0.255	2.91	1.80	0.618	501.8	510.7 510.9	519.7	528.6	537.6	546.5	555.5
	45	37.0 35.0	0.238 0.222	2.71	2.00	0.575	502.0 502.1	511.0	519.9 520.0	528.8 528.9	537.8 537.9	546.7 546.8	555.7 555.8
	44	33.0	0.222	2.53 2.35	2.16	0.499	502.1	511.0	520.0	528.9	538.0	546.9	555.9
	43 42	31.0	0.192	2.18	2.53	0.463	502.1	511.1	520.0	529.0	538.1	547.0	556.0
	42	31.0	0.102	2.10	2.00	0.409	002.2	011.1	02011	020.0	550.1	01110	00010
54	54	54.0	0.428	4.86	0.00	1.000	499.9	508.8	517.8	526.7	535.6	544.5	553.5
	53	52.0	0.400	4.54	0.32	0.934	500.0	508.9	517.9	526.8	535.7	544.6	553.6
	52	50.0	0.373	4.25	0.61	0.875	500.2	509.1	518.1	527.0	535.9	544.8	553.8
	51	48.0	0.349	3.96	0.90	0.815	500.3	509.2	518.2	527.1	536.0	544.9	553.9
	50	46.0	0.326	3.70	1.16	0.761	500.4	509.3	518.3	527.2	536.1	545.0	554.0
	49	44.0	0.304	3.45	1.41	0.709	500.6	509.5	518.5	527.4	536.3	545.2	554.2
	48	42.0	0.283	3.23	1.63	0.665	500.7	509.6	518.6	527.5	536.4	545.3	554.3
	47	40.0	0.264	3.01	1.85	0.619	500.8	509.7	518.7	527.6	536.5	545.4	554.4
	46	38.0	0.246	2.80	2.06	0.576	500.9	509.8	518.8	527.7	536.7	545.6	554.6
	45	36.0	0.230	2.61	2.25	0.537	501.0	509.9	518.9	527.8	536.8	545.7	554.7
	44	34.0	0.214	2.43	2.43	0.500	501.1	510.0	519.0	527.9	536.9	545.8	554.8
	43	32.0	0.199	2.27	2.59	0.467	501.1	510.0	519.1	528.0	537.0	545.9	554.9
	42	30.0	0.186	2.10	2.76	0.432	501.3	510.2	519.2	528.1	537.1	546.0	555.0
1	41	28.0	0.173	1.96	2.90	0.403	501.4	510.3	519.3	528.2	537.2	546.1	555.1
	40	26.0	0.161	1.82	3.04	0.375	501.5	510.4	519.4	528.3	537.3	546.2	555.2
	•												
55	55	55.0	0.442	5.02	0.00	1.000	498.8	507.7	516.6	525.5	534.4	543.3	552.2
	54	53.3	0.418	4.74	0.28	0.944	499.0	507.9	516.8	525. 7	534.6	543.5	552.4
,	53	51.6	0.394	4.46	0.56	0.888	499.1	508.0	516.9	525.8	534.7	543.6	552.5
	52	49.9	0.372	4.23	0.79	0.843	499.3	508.2	517.1	526.0	534.9	543.8	552.7
1	51	48.2	0.351	3.98	1.04	0.793	499.4	508.3	517.2	526.1	535.0	543.9	552.8
	50	46.5	0.331	3.76	1.26	0.749	499.5	508.4	517.3	526.2	535.1	544.0	552.9
!	49	44.8	0.312	3.55	1.47	0.707	499.7	508.6	517.5	526.3	535.3	544.2	553.1
'	48	43.1	0.295	3.34	1.68	0.665	499.8	508.7	517.6	526.5	535.4	544.3	553.3
	47	41.4	0.278	3.14	1.88	0.626	499.8	508.7	517.6	526.6	535.5	544.4	553.4
	46	39.7	0.262	2.97	2.05	0.591	499.9	508.8	517.7	526.7	535.6	544.5	553.5
	45	38.0	0.246	2.79	2.23	0.556	500.0	508.9	517.9	526.8	535.7	544.6	553.6
	44	36.3	0.232	2.64	2.38	0.526	500.1	509.0	518.0	526.9	535.8	544.7	553.7
	43	34.6	0.219	2.17	2.55	0.492	500.2	509.1	518.1	527.0	535.9	544.8	553.8
	42	32.9	0.206	2.32	2.70	0.462	500.3	509.2	518.2	527.1	536.0	544.9	553.9
	41	31.2	0.194	2.20	2.82	0.438	500.1	509.3	518.3	527.1	536.0	544.9	554.0
	40	29.5	0.182	2.07	2.95	0.412	500.5	509.3	518.4	527.2	536.1	545.0	554.1
	39	27.8	0.172	1.95	3.07	0.388	500.6	509.4	518.5	527.3	536.2	545.1	554.2
	38	26.1	0.161	1.93	3.19	0.365	500.7	509.5	518.6	527.4	536.2	545.1	554.2

of	ding	Temp.	Force		ight apor	Hu-		Weigh	t in Grai	ns of a Cı	ubic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic		midity, Satura- tion =		Height (of the Ba	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bie Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	o 56	56.0	in. 0.458	gr. 5.18	gr 0.00	1.000	gr. 497.7	gr. 506.6	gr.	gr.	gr.	gr.	gr.
56	55	54.3	0.432	4.89	0.29	0.944	497.9	506.8	515.5 515.7	524.4 524.6	533.2 533.4	542.1 542.3	551.0
	54	52.6	0.408	4.61	0.57	0.890	498.0	506.9	515.8	524.7	533.5	542.4	551.2 551.3
	53	50.9	0.385	4.37	0.81	0.844	498.2	507.1	516.0	524.9	533.7	542.4	551.5
	52	49.2	0.363	4.11	1.07	0.793	498.3	507.2	516.1	525.0	533.S	542.7	551.6
	51	47.5	0.343	3.87	1.31	0.747	498.4	507.3	516.2	525.1	533.9	542.8	551.7
	50	45.8	0.323	3.66	1.52	0.706	498.6	507.5	516.4	525.3	534.1	543.0	551.9
	49	44.1	0.305	3.45	1.73	0.666	498.6	507.5	516.4	525.3	534.2	543.1	552.0
	48	42.4	0.287	3.25	1.93	0.627	498.7	507.6	516.5	525.4	534.3	543.2	552.1
	47	40.7	0.271	3.07	2.11	0.593	498.8	507.7	516.6	525.5	534.4	543.3	552.2
	46	39.0	0.255	2.89	2.29	0.558	498.9	507.8	516.7	525.6	534.5	543.4	552.8
	45	37.3	0.240	2.73	2.45	0.527	499.0	507.9	516.8	525.7	534.6	543.5	552.4
	44	35.6	0.227	2.56	2.62	0.494	499.1	508.0	516.9	525.8	534.7	543.6	552.5
	43	33.9	0.213	2.41	2.77	0.465	499.2	508.1	517.0	525.9	534.8	543.7	552.6
	42	32.2	0.201	2.27	2.91	0.438	499.3	508.2	517.1	526.0	534.9	543.8	552.7
	41	30.5	0.189	2.14	3.04	0.413	499.4	508.3	517.2	526.1	535.0	543.9	552.8
	40	28.8	0.178	2.01	3.17	0.388	499.5	508.4	517.3	526.2	535.1	544.1	552.9
	39	27.1	0.167	1.89	3.29	0.365	499.5	508.4	517.3	526.2	535.1	544.1	552.9
57	57	57.0	0.473	5.34	0.00	1.000	496.6	505.5	514.4	523.2	532.1	540.9	549.8
	56	55.3	0.447	5.05	0.29	0.946	496.8	505.7	514.6	523.4	532.3	541.1	550.0
	55	53.6	0.422	4.76	0.58	0.891	496.9	505.8	514.7	523.5	532.4	541.2	550.1
	54	51.9	0.398	4.50	0.84	0.843	497.1	506.0	514.9	523.7	532.6	541.4	550.3
- 1	53	50.2	0.376	4.25	1.09	0.796	497.2	506.1	515.0	523.8	532.7	541.5	550.4
	52	48.5	0.355	4.00	1.34	0.749	497.3	506.2	515.1	523.9	532.8	541.6	550.5
	51	46.8	0.335	3.78	1.56	0.709	497.5	506.4	515.3	524.1	533.0	541.8	550.7
- 1	50	45.1	0.316	3.56	1.78	0.667	497.6	506.5	515.4	524.2	533.1	541.9	550.8
	49	43.4	0.298	3.36	1.98	0.629	497.7	506.6	515.5	524.3	533.2	542.0	550.9
	48	41.7	0.281	3.17	2.17	0.594	497.8	506.7	515.6	524.4	533.3	542.1	551.0
	47 46	40.0 38.3	$0.264 \\ 0.249$	2.99 2.81	$2.35 \\ 2.53$	$0.560 \\ 0.526$	497.9 498.0	506.8 506.9	515.7 515.8	524.5 524.6	533.4 533.5	542.2 542.3	551.2 551.3
	45	36.6	0.235	2.65	2.69	0.496	498.1	507.0	515.9	524.7	533.6	542.4	551.4
	44	34.9	0.221	2.50	2.84	0.468	498.2	507.1	516.0	524.S	533.7	542.5	551.5
	43	33.2	0.208	2.35	2.99	0.440	498.3	507.2	516.1	524.9	533.8	542.6	551.6
	42	31.5	0.196	2.21	3.13	0.414	498.3	507.2	516.1	524.9	533.S	542.6	551.6
	41	29.8	0.184	2.08	3.26	0.390	498.4	507.3	516.2	525.1	533.9	542.7	551.7
	40	28.1	0.173	1.96	3.38	0.367	498.5	507.4	516.3	525.2	534.0	542.8	551.8

	iding Ther-	Temp	Force	Wei of V	apor	Hu-		Weight	t in Grain	ıs of a Cu	ibic Foot	of Air.	
\mathbf{m} oı	neter, abr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1 000.	28.0	in. 28.5	in. 29.0	29.5	30.0	30.5	31.0
58	58	58.0	in. 0.489	gr. 5.51	gr_ 0.00	1.000	gr. 495.5	gr. 504.3	gr. 513.2	gr. 522.0	gr. 530.9	gr. 539.7	gr. 548.6
99	57	56.3	0.462	5.21	0.30	0.946	495.7	504.5	513.4	522.2	531.1	539.9	548.8
	56	54.6	0.437	4.92	0.59	0.893	495.8	504.6	513.5	522.3	531.2	540.0	548.9
	55	52.9	0.412	4.64	0.87	0.842	496.0	504.8	513.7	522.5	531.4	540.2	549.1
	54	51.2	0.389	4.39	1.12	0.797	496.1	504.9	513.8	522.7	531.6	540.4	549.3
	53	49.5	0.367	4.14	1.37	0.751	496.2	505.0	513.9	522.8	531.7	540.5	549
	52	47.8	0.346	3.90	1.61	0.708	496.4	505.2	514.1	523.0	531.9	540.7	549.6
	51	46.1	0.327	3.68	1.83	0.668	496.5	505.3	514.2	523.1	532.0	540.8	549.
	50	44.4	0.308	3.48	2.03	0.632	496.6	505.4	514.3	523.2	532.1	540.9	549.8
	49	42.7	0.290	3.28	2.23	0.595	496.7	505.5	514.4	523.3	532.2	541.0	549.9
	48	41.0	0.274	3.08	2.43	0.559	496.8	505.6	514.5	523.4	532.3	541.1	550.
	47	39.3	0.258	2.91	2.60	0.528	496.9	505.7	514.6	523.5	532.4	541.2	550.
	46	37.6	0.243	2.74	2.77	0.497	497.0	505.8	514.7	523.6	532.5	541.3	550.5
	45	35.9	0.229	2.58	2.93	0.469	497.1	505.9	514.8	523.7	532.6	541.4	550.
	44	34.2	0.216	2.43	3.08	0.441	497.2	506.0	514.9	523.8	532.7	541.5	550.
	43	32.5	0.203	2.29	3.22	0.416	497.3	506.1	515.1	523.9	532.8	541.6	550.
	42	30.8	0.191	2.15	3.36	0.390	497.4	506.2	515.2	524.1	532.9	541.7	550.
	41	29.1	0.180	2.03	3.48	0.368	497.5	506.3	515.3	524.2	533.0	541.8	550.
	40	27.4	0.169	1.91	3.60	0.347	497.5	506.3	515.3	524.2	533.0	541.8	550.
59	59	59.0	0.506	5.69	0.00	1.000	494.5	503.3	512.2	521.0	529.8	538.6	547.
	58	57.3	0.478	5.37	0.32	0.944	494.6	503.4	512.3	521.1	529.9	538.7	547.
	57	55.6	0.452	5.08	0.61	0.893	494.7	503.5	512.4	521.2	530.0	538.8	547.
	56	53.9	0.426	4.79	0.90	0.842	494.8	503.6	512.5	521.3	530.1	538.9	547.
	55	52.2	0.402	4.53	1.16	0.796	494.9	503.7	512.6	521.4	530.3	539.1	548.
	54	50.5	0.380	4.28	1.41	0.752	495.1	503.9	512.8	521.6	530.5	539.3	548.
	53	48.8	0.358	4.03	1.66	0.708	495.3	504.1	513.0	521.8	530.7	539.5	
	52	47.1	0.338	3.80	1.89	0.668	495.4	504.2	513.1	521.9	530.8	539.6	1
	51	45.4	0.319	3.60	2.09	0.633	495.5	504.3		522.0	ł	1	
	50	43.7	0.301	3.39	2.30	0.596	495.7	504.5	1	522.2	531.1	539.9	
	49	42.0	0.283	3.19	2.50	0.561	495.8	504.6	513.4	522.3		1	
	48	38.6	$0.267 \\ 0.252$	$\begin{vmatrix} 3.01 \\ 2.84 \end{vmatrix}$	$2.68 \\ 2.85$	0.529 0.499	495.9 496.0	504.7 504.8	513.5 513.6	522.4 522.5	531.3	540.1 540.2	549. 549.
	1.0	90.0	0.99~	9 E*	2 00	0.469	496.1	5010	513.7	522.6	531.5	540.3	549.
	46	36.9	0.237	2.67			1	504.9					-
	45	35.2	0.223	1		$\begin{vmatrix} 0.441 \\ 0.417 \end{vmatrix}$	496.2 496.3		1	1			
	41	33.5	0.210		1	0.417	496.4		1	522.5			1
	43 42	31.8	0.195	1			496.5	1					1
	42	28.4				í	1	1	t t)			
	40	26.7			1	4	496.6		1			1	
	10	20.7	0.103	1.09	9.04	0.020	490.0	909.1	514.0	52011	3.52.0		

	ding	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ubic Foot	of Air.	
mon	neter, ahr.	of Dew- Point,	of Vapor iu	In a Cubie	Reqd. for Sat'n	midity, Satura- tion =		Height	of the Ba	rometer i	in Englis	h Inches	
Dry.	Wet.	Fahr.	English Iuches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
60	0	60.0	in. 0.523	gr. 5.87	gr. 0.00	1.000	gr. 493.4	gr. 502.2	gr. 511.0	gr. 519.8	gr. 528.6	gr. 537.4	gr. 546.2
00	60 59	58.3	0.323	5.54	0.33	0.944	493.6	502.4	511.0	520.0	528.8	537.4	546.4
	58	56.6	0.467	5.24	0.63	0.893	493.7	502.5	511.3	520.1	528.9	537.7	546.5
	57	54.9	0.441	4.95	0.92	0.843	493.8	502.6	511.4	520.2	529.0	537.8	546.6
	56	53.2	0.416	4.68	1.19	0.797	494.0	502.8	511.6	520.4	529.2	538.0	546.8
	55	51.5	0.393	4.41	1.46	0.751	494.2	503.0	511.8	520.6	529.4	538.2	547.0
	54	49.8	0.371	4.17	1.70	0.710	494.4	503.2	512 0	520.8	529.6	538.4	547.2
	53	48.1	0.350	3.92	1.95	0.668	494.5	503.3	512.1	520.9	529.7	538.5	547.4
	52	46.4	0.330	3.70	2.17	0.630	494.7	503.4	512.3	521.1	529.9	538.7	547.6
	51	44.7	0.311	3.49	2.38	0.595	494.8	503.5	512.4	521.2	530.0	538.8	547.7
	50	43.0	0.293	3.29	2.58	0.561	494.8	503.6	512.5	521.3	530.1	538.9	547.8
	49	41.3	0.277	3.10	2.77	0.528	494.9	503.7	512.6	521.4	530.2	539.0	547.9
	48	39.6	0.261	2.93	2.94	0.499	495.0	503.8	512.7	521.5	530.3	539.1	548.0
	47	37.9	0.246	2.75	3.12	0.468	495.1	503.9	512.8	521.6	530.4	539.2	548.1
	46	36.2	0.231	2.60	3.27	0.443	495.2	504.0	512.9	521.7	530.5	539.3	548.2
	45	34.5	0.218	2.45	3.42	0.417	495.3	504.1	513.0	521.8	530.6	539.4	548.3
1	44	32.8	0.205	2.31	3.56	0.394	495.4	504.2	513.1	521.9	530.7	539.5	548.4
	43	31.1	0.193	2.17	3.70	0.370	495.5	504.3	513.2	522.0	530.8	539.6	548.5
	42	29.4	0.182	2.04	3.83	0.348	495.6	504.4	513.3	522.1	530.9	539.7	548.6
	41	27.7	0.171	1.92	3.95	0.327	495.6	504.4	513.3	522.1	530.9	539.7	548.7
61	61	61.0	0.541	6.06	0.00	1.000	492.3	501.1	509.9	518.7	527.5	536.3	545.1
"	60	59.3	0.511	5.72	0.34	0.944	492.5	501.3	510.1	518.9	527.7	536.5	545.3
- 1	59	57.6	0.483	5.40	0.66	0.891	492.6	501.4	510.2	519.0	527.8	536.6	545.4
	58	55.9	0.456	5.11	0.95	0.843	492.8	501.6	510.4	519.2	528.0	536.8	545.6
	57	54.2	0.431	4.83	1.23	0.797	493.0	501.8	510.6	519.4	528.2	537.0	545.8
	56	52.5	0.407	4.55	1.51	0.751	493.1	501.9	510.7	519.5	528.3	537.1	545.9
İ	55	50.8	0.383	4.30	1.76	0.710	493.3	502.1	510.9	519.7	528.5	537.3	546.1
	54	49.1	0.362	4.05	2.01	0.668	493.4	502.2	511.0	519.8	528.6	537.4	546.2
	53	47.4	0.342	3.83	2.23	0.632	493.5	502.3	511.1	519.9	528.7	537.5	546.3
	52	45.7	0.322	3.61	2.45	0.596	493.6	502.4	511.2	520.0	528.8	537.6	546.4
	51	44.0	0.301	3.40	2.66	0.561	493.8	502.6	511.4	520.2	529.0	537.8	546.6
	50	42.3	0.286	3.21	2.85	0.530	493.9	502.7	511.5	520.3	529.1	537.9	546.7
	49	40.6	0.270	3.02		0.498	494.0	502.8	1		529.2		546.8
	48	38.9	0.254	2.85	3.21	0.470	491.1	502.9	511.7	520.5	529.3	538.1	546.9
	47	37.2	0.240	2.69	3.37	0.444	494.2	503.0	511.8	520.6	529.4	538.2	547.0
	46	35.5	0.226	2.53	3.53	0.417	494.3	503.1	511.9	520.7	529.5	538.3	547.1
	45	33.8	0.213	2.38	3.68	0.393	494.4	503.2	512.0	520.8	529.6	1	547.2
	44	32.1	0.200	2 24	3.82	0.370	494.5	503.3	512.1	520.9	529.7	1	547.3
	43	30.4	0.183	2.11	3.95	0.348	494.6	503.4	1	521.0	529.8	538.6	547.4
	42	28.7	0.177	1.99	4.07	0.328	494.7	503.5	512.3	521.1	529.9	538.7	547.5
!	41	27.0	0.167	1.87	4.19	0.309	494.7	503.5	512.3	521.1	529.9	538.7	547.5

of '	ading Ther-	Temp.	Force of	of V	ight " /apor. Reqd.	IIu-		Weigh	t in Grain	ns of a C	abie Foot	t of Air.	
	meter, ahr.	Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion ==		Height	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
62	62	62.0	in. 0.559	gr. 6.25	gr. 0.00	1.000	gr. 491.2	gr. 499.9	gr.	gr.	gr.	gr.	gr.
02	61	60.3	0.528	5.91	0.34	0.946	491.4	500.1	508.7 508.9	517.5	526.3 526.5	535.1	543.9
	60	58.6	0.499	5.58	0.67	0.893	491.5	500.2	509.0	517.8	526.6	535.4	544.2
	59	56.9	0.472	5.27	0.98	0.843	491.7	500.4	509.2	518.0	526.8	535.6	544.4
	58	55.2	0.445	4.99	1.26	0.798	491.9	500.6	509.4	518.2	527.0	535.8	544.6
	57	53.5	0.421	4.70	1.55	0.752	492.0	500.7	509.5	518.3	527.1	535.9	544.7
	56	51.8	0.397	4.44	1.81	0.710	492.1	500.7	509.5	518.4	527.3	536.1	544.9
	55	50.1	0.375	4.19	2.06	0.670	492.2	500.9	509.7	518.5	527.4	536.2	545.0
	54	48.4	0.354	3.95	2.30	0.632	492.4	501.1	509.9	518.7	527.6	536.4	545.2
	53	46.7	0.333	3.72	2.53	0.595	492.5	501.3	510.1	518.9	527.7	536.5	545.5
	52	45.0	0.315	3.52	2.73	0.563	492.7	501.5	510.3	519.1	527.9	536.7	545.5
1	51	43.3	0.297	3.31	2.94	0.530	492.8	501.6	510.4	519.2	528.0	536.8	545.6
	50	41.6	0.280	3.13	3.12	0.501	492.9	501.7	510.5	519.3	528.1	536.9	545.
1	49	39.9	0.263	2.95	3.30	0.472	493.0	501.8	510.6	519.4	528.2	537.0	545.8
	48	38.2	0.248	2.77	3.48	0.443	493.1	501.9	510.7	519.5	528.3	537.1	545.9
	47	36.5	0.234	2.61	3.64	0.418	493.2	502.0	510.8	519.6	528.4	537.2	546.6
	46	34.8	0.220	2.47	3.78	0.395	493.3	502.1	510.9	519.7	528.5	537.3	546.
	45	33.1	0.207	2.32	3.93	0.371	493.3	502.1	511.0	519.7	528.6	537.3	546.
ı	44	31.4	0.195	2.18	4.07	0.349	493.4	502.2	511.0	519.8	528.6	537.4	546.
	43	29.7	0.184	2.06	4.19	0.330	493.4	502.2	511.1	519.8	528.6	537.4	546.
	42	28.0	0.173	1.94	4.31	0.311	493.5	502.3	511.2	519.9	528.7	537.5	546.
	41	26.3	0.163	1.83	4.42	0.293	493.6	502.4	511.3	520.0	528.8	537.6	546.
		22.0											ļ
63	63	63.0	0.578	6.45	0.00	1.000	490.2	498.9	507.7	516.4	525.2	533.9	542.7
	62	61.3 59.6	0.546	6.10	0.35	0.946	490.4	499.1	507.9	516.6	525.4	534.1	542.9
	61 60	57.9	0.516	5.76 5.44	0.69 1.01	0.893 0.843	490.5 490.7	499.2 499.4	508.0	516.7	525.5	534.2	543.0
	59	56.2	0.461	5.15	1.30	0.798	490.9	499.6	508.2 508.4	516.9 517.1	$525.7 \\ 525.9$	534.4 534.6	543.2 543.4
	- 11									i			
	58	54.5	0.435	4.86	1.59	0.753	491.0	499.7	508.5	517.2	526.0	534.7	543.5
1	57	52.8	0.411	4.59	1.86	0.712	491.1	499.8	508.6	517.3	526.2	534.9	543.7
	56 55	51.1 49.4	$0.388 \ 0.366$	4.33	$\frac{2.12}{2.36}$	$0.671 \\ 0.634$	491.2	499.9	508.7	517.4	526.3	535.0	543.8
	54	47.7	0.345	3.85	2.60	0.597	491.3	500.0 500.2	508.8 509.0	517.5 517.7	526.4 526.6	535.1 535.3	543.9
	H	-		-				-					
	53	46.0	0.326	3.63	2.82	0.563	491.7	500.4	509.2	518.0	526.8	535.5	544.3
	52 51	$\frac{41.3}{42.6}$	$0.307 \\ 0.289$	3.43	3.02	0.532	491.8	500.5	509.3	518.1	526.9	535.6	544.4
İ	50	40.9	$0.289 \\ 0.273$	$\frac{3.24}{3.05}$	$\frac{3.21}{3.40}$	$0.502 \\ 0.473$	491.9 492.0	500.6 500.7	509.4 509.5	518.2	527.0	535.7	544.5
	49	39.2	0.273	2.07	3.58	0.445	492.0	500.7	509.6	518.3 518.4	527.1 527.2	535.8 535.9	544.6 544.7
	48	37.5	0.242	2.71	3.74	0.420	492.2	500.9	509.7	518.5	527.3	536.0	544.8
1							-			i	l		
	47	35.8	0.228	2.56	3.89	0.397	492.3	501.0	509.8	518.6	527.4	536.1	541.9
	46	34.1	0.215	2.41	4.04	0.374	492.1	501.1	509.9	518.7	527.5	536.2	545.0
	45 44	32.4	$0.202 \\ 0.190$	$2.26 \\ 2.13$	4.19 4.32	$0.351 \\ 0.330$	492.5 492.5	501.2 501.2	510.0	518.8	527.6	536.3	545.1
	43	29.0	0.179	2.13	4.45	0.330	492.6	501.2	510.0 510.1	518.8 518.9	527.6 527.7	536.3 536.4	545.1 545.2
- 1	79	~J.U	0.168	1.87	4.58	3.010	402.0	001.9	210.1	010.9	041.1	990.4	040.2

of ?	iding Ther-	Temp.	Force	We of V	ight apor. Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	ibic Foot	of Air.	
	neter, ahr.	Dew-	of Vapor in	In a Cubic	for Sat'n.	midity, Satura-		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.			tion = 1 000.	28.0	in. 28.5	29.0	29.5	30.0	in. 3 0.5	31.0
0	6 4	0	in.	gr.	gr	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr.
64	63	$64.0 \\ 62.3$	0.597 0.565	$\begin{vmatrix} 6.65 \\ 6.29 \end{vmatrix}$	$0.00 \\ 0.36$	0.946	489.1 489.3	497.8	506.6 506.8	515.3 515.5	524.0 524.2	532. 7 532.9	541.5 541.7
	62	60.6	0.534	5.94	0.30	0.893	489.5	498.2	507.0	515.5	524.4	533.1	541.9
	61	58.9	0.504	5.61	1.04	0.843	489.7	498.4	507.0	515.7	524.4	533.3	542.1
	60	57.2	0.476	5.31	1.34	0.798	489.9	498.6	507.4	516.1	524.8	533.5	542.3
	59	55.5	0.450	5.01	1.64	0.753	490.0	498.7	507.4	516.2	524.9	533.6	542.4
į	58	53.8	0.425	4.73	1.92	0.711	490.1	498.8	507.6	516.3	525.1	533.8	542.6
Ì	57	52.1	0.401	4.47	2.18	0.672	490.2	498.9	507.7	516.4	525.2	533.9	542.7
	56	50.4	0.379	4.23	2.42	0.636	490.4	499.1	507.9	516.6	525.4	531.1	542.9
	55	48.7	0.357	3.98	2.67	0.598	490.5	499.2	508.0	516.7	525.5	531.2	543.0
1	54	47.0	0.337	3.75	2.90	0.564	490.7	499.4	508.2	516.9	525.7	534.4	543.2
	53	45.3	0.318	3.55	3.10	0.534	490.8	499.5	508.3	517.0	525.8	534.5	543.3
	52	43.6	0.300	3.34	3.31	0.502	490.9	499.6	508.4	517.1	525.9	534.6	543.4
	51	41.9	0.282	3.15	3.50	0.473	491.0	499.7	508.5	517.2	526.0	534.7	543.5
	50	40.2	0.266	2.96	3.69	0.445	491.2	499.9	508.7	517.4	526.1	534.9	543.7
	49	38.5	0.251	2.79	3.86	0.419	491.3	500.0	508.8	517.5	526.2	535.0	543.8
	48	36.8	0.236	2.63	4.02	0.396	491.4	500.1	508.9	517.6	526.3	535.1	543.9
	47	35.1	0.223	2.47	4.18	0.372	491.5	500.2	509.0	517.7	526.4	535.2	544.0
	46	33.4	0.210	2.33	4.32	0.351	491.6	500.3	509.1	517.8	526.5	535.3	544.1
	45	31.7	0.197	2.19	4.46	0.330	491.7	500.4	509.2	517.9	526.6	535.4	544.2
	44	30.0	0.156	2.06	4.59	0.310	491.7	500.4	509.2	517.9	526.6	535.4	544.2
	43	28.3	0.175	1.94	4.71	0.292	491.8	500.5	509.3	518.0	526.7	535.5	544.3
	42	26.6	0.164	1.83	4.82	0.275	491.9	500.6	509.4	518.1	526.8	535.6	544.4
65	65	65.0	0.617	6.87	0.00	1.000	488.1	496.8	505.5	514.2	522.9	531.6	540.3
	64	63.4	0.586	6.51	0.36	0.947	488.3	497.0	505.7	514.4	523.1	531.8	540.5
	63	61.8	0.555	6.17	0.70	0.898	488.5	497.2	505.9	514.6	523.3	532.0	540.7
1	62	60.2	0.527	5.85	1.02	0.851	488.7	497.4	506.1	514.8	523.5	532.2	540.9
!	61	58.6	0.499	5.55	1.32	0.808	488.9	497.6	506.3	515.0	523.7	532.4	541.1
	60	57.0	0.473	5.25	1.62	0.765	489.0	497.7	506.5	515.2	523.9	532.6	541.3
	59	55.4	0.449	4.98	1.89	0.725	489.1	497.8	506.6	515.3	524.0	532.7	541.5
	58	53.8	0.125	4.72	2.15	0.687	489.3	498.0	506.8	515.5	524.2	532.9	541.7
	57	52.2	0.402	4.47	2.40	0.651	489.4	498.1	505.9	515.6	524.3	533.0	541.8
	56	50.6	0.381	4.23	2.64	0.616	489.6	498.3	507.1	515.8	524.5	533.2	542.0
	55	49.0	0.361	4.01	2.86	0.584	489.7	498.4	507.2	515.9	524.6	533.3	542.1
	54	47.4	0.342	3.79	3.08	0.552	489.8	498.5	507.3	516.0	524.7	533.4	542.2
1	53	45.8	0.323	3.60	3.27	0.524	489.9	498.6	507.4	516.1	524.8	533.5	542.3
	52	44.2	0.306	3.39	3.48	0.493	490.0	198.7	507.5	516.2	524.9	533.6	542.4
	51	42.6	0.289	3.22	3.65	0.469	490.1	498.8	507.6	516.3	525.0	533.7	542.5
	50	41.0	0.274	3.04	3.83	0.442	490.2	498.9	507.7	516.4	525.1	533.8	542.6
	19	39.4	0.259	2.87	4.00	0.418	490.3	499.0	507.8	516.5	525.2	533.9	542.7
	48	37.8	0.245	2.72	4.15	0.396	490.3	499.0	507.8	516.5	525.2	533.9	542.7
	47	36.2	0.231	2.57	4.30	0.374	490.4	499.1	507.9	516.6	525.3	534.0	542.8
	46	34.6	0.219	2.43	4.41	0.354	490.5	499.2	508.0	516.7	525.4	534.1	542.9
	45	33.0	0.207	2.31	4.56	0.336	490.6	499.3	508.1	516.8	525.5	534.2	543.0
	41	31.4	0.195	2.17	4.70	0.316	490.7	499.4	508.2	516.9	525.6	534.3	543.1
	43	29 8	0.184	2.05	4.82	0.299	490.7	499.4	508.2	516.9	525.6	534.3	543.1
	42	28.2	0.171	1.94	4.93	0.283	490.8	499.5	508.3	517.0	525.7	534.4	543.2

Rea	ding Ther-	Temp.	Force	We of V	ight apor	Hn-		Weight	in Grain	ns of a Cu	ıbic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n	midity, Satura- tion =		Height 0	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr,	gr. 0.00	1.000	gr.	gr. 495.7	gr. 504.4	gr. 513.1	gr. 521.8	gr. 530.5	gr. 539.2
66	66	66.0	$0.638 \\ 0.605$	7.08	0.36	0.949	487.0 487.2	495.9	504.4	513.3	522.0	530.7	539.4
	65	62.8	0.574	6.72 6.35	0.73	0.897	487.3	496.0	504.0	513.4	522.0	530.8	539.5
	64	61.2	0.544	6.04	1.04	0.853	487.5	496.2	504.9	513.4	522.3	531.0	539.7
-	63	59.6	0.516	5.72	1.36	0.808	487.7	496.4	505.1	513.8	522.5	531.2	539 9
- 1	62	58.0				0.766		496.6	505.3	514.0	522.7	531.4	540.
- 1	61	33.0	0.489	5.42	1.66	0.766	487.9	490.0	303.3	514.0	322.7	991.4	340.
	60	56.4	0.464	5.14	1.94	0.726	488.0	496.7	505.4	514.1	522.8	531.5	540.5
	59	54.8	0.440	4.88	2.20	0.689	488.1	496.8	505.5	514.2	523.0	531.7	540.
	58	53.2	0.416	4.62	2.46	0.652	488.2	496.9	505.6	514.3	523.1	531.8	540.
	57	51.6	0.394	4.37	2.71	0.619	488.4	497.1	505.8	514.5	523.3	532.0	540.
	56	50.0	0.373	4.15	2.93	0.586	488.5	497.2	505.9	514.6	523.4	532.1	540.8
	55	48.4	0.354	3.92	3.16	0.553	488.6	497.3	506.1	514.8	523.5	532.2	541.
	54	46.8	0.335	3.72	3.36	0.525	488.8	497.5	506.3	515.0	523.7	532.4	541.
	53	45.2	0.317	3.51	3.57	0.496	488.9	497.6	506.4	515.1	523.8	532.5	541.
	52	43.6	0.300	3.33	3.75	0.470	489.0	497.7	506.5	515.2	523.9	532.6	541.
- 1	51	42.0	0.283	3.14	3.94	0.443	489.1	497.8	506.6	515.3	524.0	532.7	541.
	50	40.4	0.268	2.97	4.11	0.419	489.2	497.9	506.7	515.4	524.1	532.8	541.
	49	38.8	0.253	2.81	4.27	0.397	489.3	498.0	506.8	515.5	524.2	532.9	541.
	48	37.2	0.210	2.66	4.42	0.376	489.4	498.1	506.9	515.6	524.3	533.0	541.
	47	35.6	0.227	2.51	4.57	0.355	489.4	498.1	506.9	515.6	524.3	533.0	541.
	46	34.0	0.214	2.37	4.71	0.335	489.5	498.2	507.0	515.7	524.4	533.1	541.
-	45	32.4	0.214	2 24	4.84	0.336	489.6	498.3	507.1	515.8	524.5	533.2	542.
-	41	30.8	0.191	2.12	4.96	0.299	489.7	498.4	507.2	515.9	524.6	533.3	542.
	43	29.2	0.180	2.00	5.08	0.283	489.7	498.4	507.2	515.9	524.6	533.3	542.
67	67	67.0	0.659	7.30	0.00	1.000	485.9	494.6	503.3	512.0	520.6	529.3	538.
	66	65.4	0.626	6.93	0.37	0.949	486.1	491.8	503.5	512.2	520.8	529.5	538.
	65	63.8	0.593	6.55	0.75	0.897	486.3	495.0	503.7	512.4	521.0	529.7	538.
	64	62.2	0.563	6.23	1.07	0.853	486.5	495.2	503.9	512.6	521.2	529.9	538.
	63	60.6	0.534	5.91	1.39	0.810	486.7	495.4	504.1	512.8	521.4	530.1	538.
	62	59.0	0.506	5.60	1.70	0.767	486.8	495.5	504.2	512.9	521.6	530.3	539.
	61	57.4	0.480	5.31	1.99	0.728	486.9	495.6	504.3	513.0	521.7	530.4	539.
	60	55.8	0.455	5.04	2.26	0.691	487.1	495.8	504.5	513.2	521.9	530.6	539.
	59	54.2	0.431	4.77	2.53	0.653	487.2	495.9	504.6	513.3	522.0	530.7	539.
	53	52.6	0.408	4.52	12.78	0.619	487.3	496.0	504.7	513.4	522.1	530.8	539.
	57	51.0	0.386	4.28	3.02	0.586	487.5	496.2	504.9	513.6	522.3	531.0	539.
	56	49.4	0.366	4.05	3.25	0.555	487.6	496.3	,505.0	513.7	522.4	531.1	539.
	55	47.8	0.316	3.83	3.47	0.524	487.8	496.5	505.1	513.8	522.6	531.2	549.
	54	46.2	0.328	3.62	3.68	0.496	487.9	496.6	505.2	513.9	522.7	531.3	540.
	53	44.6	0.310	3.13	3.87	0.470	488.0	496.7	505.3	511.0	522.8	531.4	540.
	52	43.0	0.293	3.25	4.05	0.115	488.1	496.8	504.4	514.1	522.9	531.5	540.
	51	41.4	0.278	3.08	4.22	0.422	488.2	496.9	505.5	514.2	523.0	531.6	540.
		11	10.2.0	0.00	1								1
	50	39.5	0.263	2.91	4.39	0.399	488.4	1	505.7	514.4	523.1	531.8	540.

of	eading Ther-	Temp.	Force of	We of V	ight apor Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
mo	meter, lahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	of the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Air.	of aCu- bic Ft. of Air.	1 000.	in. 28.0	in. 28.5	29.0	in. 29.5	30.0	30.5	31.0
0	49	35.2	in. 0.248	gr 2.75	gr.	0.377	gr.	gr.	gr.	gr.	gr.	gr.	gr.
67	48	36.6	0.235	2.60	4.55	0.356	488.5 488.6	497.2 497.3	505.8 505.9	514.5 514.6	523.2 523.3	531.9 532.0	540.6 540.7
	47	35.0	0.222	2.46	1.84	0.337	488.7	497.4	505.9	514.7	523.4	532.1	540.8
	46	33.4	0.210	2.32	4.98	0.318	488.7	497.4	506.0	514.7	523.4	532.1	540.8
	45	31.8	0.198	2.19	5.11	0.301	488.8	497.5	506.1	514.8	523.5	532.2	540.9
	44	30.2	0.187	2.07	5.23	0.284	488.9	497.6	506.2	514.9	523.6	532.3	541.0
68	68	63.0	0.681	7.53	0.00	1.000	484.9	493.5	502.2	510.8	519.5	528.1	536.8
	67	66.4	0.646	7.15	0.38	0.949	485.1	493.8	502.5	511.1	519.7	528.4	537.1
	66	64.8	0.613	6.77	0.76	0.899	485.3	494.0	502.6	511.2	519.9	528.6	537.3
	65	63.2	0.582	6.43	1.10	0.854	485.5	494.2	502.8	511.4	520.1	528.8	537.5
1	64	61.6	0.552	6.10	1.43	0.810	485.7	494.4	503.0	511.6	520.3	529.0	537.7
1	63	60.0	0.523	5.78	1.75	0.768	485.8	494.5	503.1	511.8	520.5	529.2	537.9
1	62	58.4	0.496	5.47	2.06	0.726	485.9	494.6	503.3	512.0	520.7	529.4	538.1
	61	56.8	0.470	5.20	2.33	0.691	486.0	494.7	503.4	512.1	520.8	529.5	538.3
	60	55.2	0.445	4.93	2.60	0.655	486.2	494.9	503.6	512.3	521.0	529.7	538.5
	59	53.6	0.422	4.67	2.86	0.620	486.3	495.0	503.7	512.4	521.1	529.8	538.6
	58	52.0	0.400	4.42	3.11	0.587	486.4	495.1	503.8	512.5	521.2	529.9	538.6
	57	50.4	0.379	4.19	3.34	0.556	486.6	495.3	504.0	512.7	521.4	530.1	538.8
	56	48.8	0.358	3.96	3.57	0.526	486.7	495.4	504.1	512.8	521.5	530.2	538.9
l	55	47.2	0.339	3.75	3.78	0.498	486.8	495.5	504.2	512.9	521.6	530.3	539.0
	54	45.6	0.321	3.54	3.99	0.470	486.9	495.6	504.3	513.0	521.7	530.4	539.1
	53	44.0	0.304	3.35	4.18	0.445	487.0	495.7	504.4	513.1	521.8	530.5	539.2
	52	42.4	0.257	3.17	4.36	0.421	487.1	495.8	504.5	513.2	521.9	530.6	539.3
	51	40.8	0.272	3.00	4.53	0.399	487.2	495.9	504.6	513.3	522.0	530.7	539.4
il	50	39.2	0.257	2.84	4.69	0.377	487.3	496.0	504.7	513.4	522.1	530.8	539.5
	49	37.6	0.243	2.68	4.85	0.356	487.4	496.1	504.8	513.5	522.2	530.9	539.6
	48	36.0	0.230	2.54	4.99	0.337	487.5	496.2	504.9	513.6	522.3	531.0	539.7
1	47 46	34.4	$0.217 \\ 0.205$	$\begin{vmatrix} 2.40 \\ 2.27 \end{vmatrix}$	5.13 5.26	0.319 0.302	487.6	496.3	505.0	513.7	522.4	531.1	539.8 539.8
	45	31.2	0.194	2.15	5.38	0.302	487.7	496.3	505.0 505.1	513.7 513.8	522.4 522.5	531.1 531.2	539.9
	44	29.6	0.183	2.01	5.49	0.271	487.8	496.5	505.2	513.9	522.6	531.3	540.0
							10.10	1000					
69	69	69.0	0.701	7.76	0.00	1.000	483.8	492.4	501.1	509.7	518.3	527.0	535.6
	68	67.4	0.668	7.37	0.39	0.950	484.0	492.6	501.3	509.9	518.5	527.2	535.8
	67	65.8	0.634	7.00	0.76	0.902	484.2	492.8	501.5	510.1	518.7	527.4	536.0
	66	64.2	0.601	6.63	1.13	0.854	484.4	493.0	501.7	510.3	518.9	527.6	536.2
	65	62.6	0.570	6.29	1:47	0.810	484.6	493.2	501.9	510.5	519.1	527.8	536.4
	64	61.0	0.541	5.97	1.79	0.769	484.8	493.4	502.1	510.7	519.3	528.0	536.6
	63	59.4	0.513	5.65	2.11	0.728	485.0	493.6	502.3	510.9	519.5	528.2	536.8
	62	57.8	0.486	5.37	2.39	0.693	485.1	493.7	502.4	511.0	519.6	528.3	536.9
	61	56.2	0.461	5.09	2.67	0.657	485.1	493.7	502.6	511.2	519.8	528.5	537.1
	60	54.6	0.437	4.82	2.94	0.621	485.2	493.9	502.7	511.3	519.9	528.6	537.3
	59	53.0	0.414	4.57	3.19	0.589	485.4	494.1	502.8	511.5	520.1	528.8	537.5
1	5 8	51.4	0.392	4.33	3.43	0.558	485.5	494.2	502.9	511.6	520.2	528.9	537.6

of '	ding	Temp of	Force of	Wei of V	ght apor Reqd.	Hu- midity,				ıs of a Cu			
	neter, ahr.	Dew-	Vapor in	In a Cubic	for Sat'n.	Satura- tion =		Height o	f the Bar	rometer i	n English	Inches.	
Dry.	Wet.	Point, Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	in. 28.0	in. 28.5	29.0	29.5	30.0	in. 30.5	31.0
0	o 58	0 51 1	in. 0.392	gr. 4.33	gr. 3.43	0.558	gr. 485.5	gr. 494.2	gr. 502.9	gr. 511.6	gr. 520.2	gr. 528.9	gr. 537.6
69	57	51.4 49.8	0.371	4.09	3.67	0.527	485.7	494.4	503.1	511.8	520.4	529.1	537.8
	56	48.2	0.351	3.87	3.89	0.499	485.8	494.5	503.1	511.9	520.5	529.2	537.9
	55	46.6	0.332	3.66	4.10	0.472	485.9	494.6	503.3	512.0	520.6	529.3	538.0
	54	45.0	0.315	3.47	4.29	0.447	486.0	494.7	503.4	512.1	520.7	529.4	528.1
	53	43.4	0.298	3.29	4.47	0.424	486.1	494.8	503.5	512.2	520.8	529.5	538.2
	52	41.8	0.282	3.11	4.65	0.401	486.2	494.9	503.6	512.3	520.9	529.6	538.3
								.0		~~~ .	507.0	*20.5	- 500 A
	51	40.2	0.266	2.94	4.82	0.379	486.3	495.0	503.7	512.4	521.0	529.7	538.4
	50	38.6	0.252	2.78	4.98	0.358	486.4	495.1	503.8	512.5	521.1	529.8	538.5
	49	37.0	0.238	2.63	5.13	0.339	486.5	495.2	503 9	512.6	521.2	529.9	538.6
	48	35.4	0.225	2.49	5.27	0.321	486.6	495.3	504.0	512.7	521.3	530.0	538.7
	47	33.8	0.213	2.34	5.42	0.302	486.7	495.4	504.1	512.8	521.4	530.1	538.8
	46	32.2	0.201	2.20	5.56	0.284	486.8	495.5	504.2	512.9	521.5	530.2	538.9
	45	30.6	0.190	2.06	5.70	0.266	486.8	495.5	504.2	512.9	521.5	530.2	538.9
70	70	70.0	0.727	8.00	0.00	1.000	482.8	491.4	500.0	508.6	517.2	525.8	534.4
••	69	68.5	0.692	7.62	0.38	0.953	483.0	491.6	500.2	508.8	517.4	526.0	534.6
	68	67.0	0.659	7.26	0.74	0.907	483.2	491.8	500.4	509.0	517.6	526.2	534.8
	67	65.5	0.628	6.91	1.09	0.865	483.3	491.9	500.5	509.1	517.7	526.3	534.9
	66	64.0	0.597	6.57	1.43	0.822	483.5	492.1	500.7	509.3	517.9	526.5	535.1
	65	62.5	0.568	6.25	1.75	0.781	483.7	492.3	500.9	509.5	518.1	526.7	535.3
	61	61.0	0.541	5.95	2.05	0.744	483.8	492.4	501.0	509.6	518.3	526.9	535.5
	63	59.5	0.515	5.66	2.34	0.708	484.0	492.6	501.2	509.8	518.5	527.1	535.7
	62	58.0	0.489	5.38	2.62	0.672	484.2	492.8	501.4	510.0	518.7	527.3	535.9
	61	56.5	0.465	5.12	2.88	0.640	484.3	492.9	501.5	510.1	518.8	527.4	536.0
	60	55.0	0.442	4.87	3.13	0.609	484.4	493.0	501.6	510.2	518.9	527.5	536.1
	59	53.5	0.421	4.62	3.38	0.578	484.6	493.2	501.8	510.4	519.1	527.7	536.
	58	52.0	0.400	4.40	3.60	0.550	484.7	493.3	501.9	510.5	519.2	527.8	536.4
	57	50.5	0.380	4.18	3.82	0.522	484.8	493.4	502.0	510.6	519.3	527.9	536.5
	56	49.0	0.361	3.96	4.04	0.495	484.9	493.5	502.1	510.7	519.4	528.0	536.0
	55	47.5	0.343	3.76	4.24	0.470	485.1	493.7	502.3	510.9	519.6		536.8
	54	46.0	0.326	3.57	4.43	0.446	485.2	493.8	502.4	511.0	519.7)	
	53	44.5	0.309	3.40	4.60	0.425	485.3	493.9	1		519.8		537.0
	52	43.0	0.292	1		0.404	485.4	494.0	502.6	511.2	1	1	1
	51	41.5	0.279	3.07	4.93	0.384	485.5	494.1	502.7	511.3	1	i	
	50	40.0	0.264	2.81	5.19	0.351	485.5	494.1	502.7	511.3	520.0	528.6	537.
	49	38.5	1					1	1		1	1	
	48	37.0	1	1						1		1	1
	47	35.5		1	1	1	1	1			1		
	46	34.0		1	1	1			1	1	I.	1	1
	45	32.5	1				1		1	1		1	1
	44	31.0	1			1					1		537.
1	43	29.5	0.182	2.01	5.99	0.251	486.I	494.7	503.3	511.9	520.6	529.2	537.

of '	nding Ther-	Temp.	Force of		ight apor Reqd.	IIu-		Weigh	t in Grain	as of a Cu	ibic Foot	of Air.	
	neter, ahr.	Dew- Point,	Vapor in	In a Cubic	for Sat'n	midity, Satura- tion =		Height	of the Ba	rometer i	n Englis	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Air.	of a Cu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr	gr.	- 000	gr.	gr.	gr.	gr.	gr	gr	gr.
7 I	71	71.0	0.751	8.25	0.00	1.000	481.6	490.2	498.8	507.4	516.0	524.6	533.:
	70	69.5	0.715	7.86	0.39	0.953	481.8	490.4	499.0	507.6	516.2	524.8	533.
	69	68.0	0.681	7.48	0.77	0.907	482.0	490.6	499 2	507.8	516.4	525.0	533.
	68	66.5	0.648	7.13	1.12	0.865	482.2	490.8	499.4	508.0	516.6	525.2	533.
	67	65.0	0.617	6.79	1.46	0.823	482.4	491.0	499.6	508.2	516.8	525.4	534.
	66	63.5	0.588	6.45	1.80	0.782	482.6	491.2	499.8	508.4	517.0	525.6	534.
	65	62.0	0.559	6.14	2.11	0.744	482.8	491.4	500.0	508.6	517.2	525.8	534.
	64	60.5	0.532	5.85	2.40	0.709	483.0	491.6	500.2	508.8	517.4	526.0	534.
	63	59.0	0.506	5.56	2.69	0.674	483.1	491.7	500.3	508.9	517.5	526.1	534.
	62	57.5	0.481	5.28	2.97	0.640	483.2	491.8	500.4	509.0	517.7	526.3	534.
	61	56.0	0.458	5.03	3.22	0.609	483.3	491.9	500.5	509.1	517.8	526.4	535.
	60	54.5	0.435	4.78	3.47	0.579	483.5	492.1	500.7	509.3	518.0	526.6	535.
	59	53.0	0.414	4.54	3.71	0.550	483.6	492.2	500.8	509.4	518.1	526.7	535.
	58	51.5	0.393	4.31	3.94	0.522	483.8	492.4	501.0	509.6	518.3	526.9	535.
	57	50.0	0.373	4.10	4.15	0.497	483.9	492.5	501.1	509.7	518.4	527.0	535.
	56	48.5	0.355	3.89	4.36	0.471	484.0	492.6	501.2	509.9	518.5	527.1	535.
	55	47.0	0.337	3.69	4.56	0.447	484.1	492.7	501.3	510.0	518.6	527.2	535.
	54	45.5	0.320	3.51	4.74	0.425	484.2	492.8	501.4	510.1	518.7	527.3	535.
	53	41.0	0.301	3.33	4.92	0.404	484.3	492.9	501.5	510.2	518.8	527.4	535.
	52	42.5	0.288	3.16	5.09	0.383	481.4	493.0	501.6	510.3	518.9	527.5	536.
	51	41.0	0.274	3.00	5.25	0.364	484.5	493.1	501.7	510.4	519.0	527.6	536.
	50	39.5	0.260	2 85	5.40	0.345	484.6	493.2	501.8	510.5	519.1	527.7	536.
	49	33.0	0.246	2.70	5.55	0.327	484.7	493.3	501.9	510.6	519.2	527.8	536.
	48	36.5	0.234	2.57	5.68	0.312	484.7	493.3	501.9	510.6	519.2	527.8	536.
	47	35.0	0.222	2.44	5.81	0.296	484.8	493.4	502.0	510.7	519.3	527.9	536.
	46	33.5	0.210	2.31	5.94	0.280	484.9	493.5	502.1	510.8	519.4	528.0	536.
	45	32.0	0.199	2.19	6.06	0.265	485.0	493.6	502.2	510.9	519.5	528.1	536.
	44	30.5	0.159	2.08	6.17	0.252	485.0	493.6	502.2	510.9	519.5	528.1	536.
72	72	72.0	0.776	8.50	0.00	1.000	480.6	489.2	497.8	506.4	514.9	523.5	532.
	71	70.5	0.739	8.10	0.40	0.953	480.8	489.4	498.0	506.5	515.1	523.7	532.
	70	69.0	0.704	7.71	0.79	0.907	481.0	489.6	498.2	506.7	515.3	523.9	532.
	69	67.5	0.670	7.35	1.15	0.865	481.2	489.8	498.4	506.9	515.5	524.1	532.
	68	66.0	0.638	7.00	1.50	0.824	481.4	490.0	498.5	507.1	515.7	524.3	532.
	67	64.5	0.607	6.66	1.84	0.784	481.6	490.2	498.7	507.3	515.9	524.5	533.
	66	63.0	0.578	6.33	2.17	0.745	481.7	490.3	498.8	507.4	516.1	524.7	533.
	65	61.5	0.550	6.03	2.47	0.710	481.8	490.4	499.0	507.6	516.2	524.8	533.
	64	60.0	0.523	5.73	2.77	0.674	482.0	490.6	499.2	507.8	516.4	525.0	533.
	63	58.5	0.198	5.15	3.05	0.641	482.1	490.7	499.3	507.9	516.5	525.1	533.
	62	57.0	0.473	5.18	3.32	0.610	482.3	490.9	499.5	508.1	516.7	525.3	533.
	61	55.5	0.450	4.93	3.57	0.580	482.5	491.1	499.7	508.3	516.9	525.5	534.
	60	51.0	0.428	4.68	3.82	0.551	482.6	491.2	499.8	508.4	517.0	525.6	534.
	59	52.5	0.407	4.15	4.05	0.523		491.4	500.0	508.6	517.2	525.8	534.

of	ading Ther-	Temp	Force of		ight apor Reqd.	Hu-		Weigh	t in Grain	ns of a Cu	ibie Foot	of Air.	
	meter, ahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat n.	midity, Satura- tion =		Height o	of the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1 000.	28.0	in. 28.5	29.0	in. 29.5	in. 30.0	in 30.5	31.0
0	0	52.5	in. 0.407	gr.	gr	0.523	gr.	gr.	gr. 500.0	gr. 508.6	gr. 517.2	gr. 525.8	gr. 534.4
72	59	1		4.45	4.05		482.8	491.4		508.7	517.3	525.9	534.5
	58	51.0	0.386	4.23	4.27	0.498	482.9	491.5 491.6	500.1	508.8	517.4	526.0	534.6
	57	49.5	0.367	1	4.48	0.473	483.0			508.9	517.5	526.1	534.7
	56	48.0	0.349	3.82	4.68	0.449	483.1	491.7	500.3	509.0	517.6	526.2	534.8
	55		0.331	3.63	4.87	0.427	483.2	491.5 491.9	500.4	509.1	517.7	526.2	534.9
	54 53	45.0	0.315	3.45	5.05	0.406	483.3 483.3		500.6	509.2	517.8	526.3	535.0
	33	43.5	0.299	3.28	5.22	0.386	450.0	492.0	500.0	303.2	317.0	920.3	333.0
	52	42.0	0.283	3.11	5.39	0.366	483.5	492.1	500.7	509.3	517.9	526.4	535.
	51	40.5	0.269	2.95	5.55	0.347	483.6	492.2	500.8	509.4	518.0	526.5	535.
	50	39.0	0.255	2.80	5.70	0.329	483.7	492.3	500 9	509.5	518.1	526.6	535.
	49	37.5	0.242	2.66	5.84	0.313	483.8	492.4	501.0	509.6	518.2	526.7	535.
	48	36.0	0.230	2.52	5.98	0.296	483.8	492.4	501.0	509.6	518.2	526.7	535.
	47	34.5	0.218	2.39	6.11	0.281	453.9	492.5	501.2	509.7	518.3	526.8	535.
	46	33.0	0.207	2.27	6.23	0.267	484.0	492.6	501.3	509.8	518.4	526.9	535.
	45	31.5	0.196	2.16	6.34	0.254	484.1	492.7	501.3	509.9	518.5	527.1	535.
7 3	73	73.0	0.801	8.76	0.00	1.000	479.6	488.1	496.7	505.2	513.8	522.3	530.
	72	71.5	0.736	8.35	0.11	0.953	479.8	488.3	496.9	505.4	514.0	522.5	531.
	71	70.0	0.727	7.95	0.81	0.908	480.0	488.5	497.1	505.6	514.2	522.7	531.
	70	68.5	0.692	7.57	1.19	0.861	480.2	488.7	497.3	505.8	514.4	522.9	531.
	69	67.0	0.659	7.21	1.55	0.823	480.4	488.9	497.5	506.0	514.6	523.1	531.
	68	65.5	0.628	6.87	1.59	0.784	480.5	489.0	497.6	506.1	514.8	523.3	531.
	67	64.0	0.597	6.53	2.23	0.745	480.7	489.2	497.8	506.3	515.0	523.5	532.
	66	62.5	0.568	6.22	2.54	0.710	480.8	489.3	497.9	506.4	515.1	523.6	532.
	65	61.0	0.541	5.92	2.84	0.676	481.0	489.5	498.1	506.6	515.3	523.8	532.
	64	59.5	0.515	5.63	3.13	0.643	481.1	489.6	498.2	506.8	515.4	524.0	532.
	63	53.0	0.489	5.34	3.42	0.610	481.2	489.8	498.4	507.0	515.6	1	1
	62	56.5	0.465	5.09	3.67	0.581	481.4	490.0		507.2	515.8	521.4	533.
		55.0	0.442	4.84	3.92	0.553	481.6	490.2	498.8	507.4	516.0		533.
	60	53.5	0.421	4.59	4.17	0.524	481.7	490.3		507.5	516.1	524.7	533.
	59	52.0	0.400	4.37	4.39	0.499	481.8	490.4	499.0	507.6	516.2	521.8	533.
	58	50.5	0.380		4.60	0.475	482.0	490.6		507.8	516.4	1	
	57	49.0	0.361	3.94	4.82	0.450	482.1	490.7	1	507.9	1		533.
	56	47.5	0.343		5.02	0.427	482.2	-		508.0	516.6		
	55	46.0	0.326	1	5.20		482.3	1	1	508.1	516.7	1	1
	54	44.5	0.309	1		1	1			1			
	53	43.0	0.293	1	5.55	0.366			1	508.3	1		
	50	1, -	0.070	2.05	= ~1	0.240	100.0	101.0	100.0	500 4	517.0	505 6	594
	52	41.5	0.279	1		0.349			1	t .		1	
	51	40.0		1		i		1	1	1		1	
	50	38.5	0.251		1	1				1		1	
	49	37.0							1		1	1	i i
	48	35.5								i		1	1
	47	34.0	,			1	1			1			
	46	32.5	0.203	2.22	6.54	0.253	433.3	491.9	500.4	509.1	517.6	526.2	534

of '	iding Ther-	Temp.	Force		ight apor Reqd.	Hu-		Weigh	t in Grai	ns of a Cu	abic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for	midity, Satura- tion =		Height	of the Ba	rometer i	in Englis	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	in. 31.
0	0	710	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr	gr.	gr.
74	74 73	74.0 72.5	$0.827 \\ 0.787$	9.04 8.60	0.00	1.000 0.951	478.4	486.9 487.1	495.5	504.0	512.6 512.8	521.1 521.3	529 529
	72	71.0	0.751	8.20	0.84	0.907	478.8	487.3	495.7	504.4	513.0	521.5	530
	71	69.5	0.715	7.81	1.23	0.864	479.0	487.5	496.1	504.6	513.2	521.7	530
	70	68.0	0.681	7.44	1.60	0.823	479.2	487.7	496.3	504.8	513.4	521.9	530
	69	66.5	0.648	7.08	1.96	0.783	479.4	487.9	496.5	505.0	513.6	522.1	530
	68	65.0	0.617	6.75	2.29	0.747	479.6	488.1	496.7	505.2	513.8	522.3	530
	67	63.5	0.588	6.41	2.63	0.709	479.8	488.3	496.9	505.4	514.0	522.5	531
	66	62.0	0.559	6.10	2.94	0.675	480.0	488.5	497.1	505.6	514.2	522.7	531
l	65	60.5	0.532	5.81	3.23	0.643	480.1	488.7	497.3	505.9	514.4	522.9	531
	64	59.0	0.506	5.52	3.52	0.611	480.3	488.9	497.5	506.1	514.6	523.2	531
	63	57.5	0.481	5.24	3.80	0.580	480.5	489.1	497.7	506.3	514.8	523.4	532
Í	62	56.0	0.458	4.99	4.05	0.552	480.6	489.2	497.8	506.4	514.9	523.5	532
	61	54.5	0.435	4.75	4.29	0.525	480.7	489.3	497.9	506.5	515.0	523.6	532
	60	53.0	0.414	4.52	4.52	0.500	480.9	489.5	498.1	506.7	515.2	523.8	532
	59	51.5	0.393	4.29	4.75	0.475	481.0	489.6	498.2	506.8	515.3	523.9	532
Ì	58	50.0	0.373	4.08	4.96	0.451	481.1	489.7	498.3	506.9	515.4	524.0	532
ļ	57	48.5	0.355	3.86	5.18	0.427	481.2	489.8	498.4	507.0	515.5	524.1	532
	56	47.0	0.337	3.66	5.38	0.405	481.3	489.9	498.5	507.1	515.6	524.2	532
Ì	55	45.5	0.320	3.48	5.56	0.385	481.4	490.0	498.6	507.2	515.7	524.3	532
	54	44.0	0.304	3.32	5.72	0.367	481.5	490.1	498.7	507.3	515.8	524.4	533
1	53	42.5	0.288	3.15	5.89	0.348	481.6	490.2	498.8	507.4	515.9	524.5	533
	52	41.0	0.274	2.99	6.05	0.331	481.7	490.3	498.9	507.5	516.0	524.6	533
	51	39.5	0.260	2.83	6.21	0.313	481.8	490.4	499.0	507.6	516.1	524.7	533
1	50	38.0	0.246	2.69	6.35	0.298	481.9	490.5	499.1	507.7	516.2	524.8	533
1	49	36.5	0.234	2.55	6.49	0.282	481.9	490.5	499.1	507.7	516.2	524.8	533
- 1	48	35.0	0.222	2.42	6.62	0.268	482.0	490.6	499.2	507.8	516.3	524.9	533
	47	33.5	0.210	2.30	6.74	0.254	482.1	490.7	499.2	507.9	516.4	525.0	533
75	75	75.0	0.854	9.31	0.00	1.000	477.4	485.9	494.4	502.9	511.5	520.0	528
	74	73.5	0.814	8.87	0.44	0.953	477.6	486.1	494.6	503.1	511.7	520.2	528
	73 72	72.0	0.776	8.45	0.86	0.908	477.8	486.3	494.8	503.3	511.9	520.4	528
ĺ	71	70.5 69.0	0.739 0.704	8.05 7.67	1.26 1.64	$0.865 \\ 0.824$	478.0 478.2	486.5 486.7	495.0	503.5	512.1	$520.6 \\ 520.8$	529 529
	70	67.5	0.704	7.30	$\frac{1.04}{2.01}$	0.524 0.784	478.3	486.8	495.2 495.3	503.7 503.8	512.3 512.5	521.0	529
	69	66.0	0.638	6.95	2.36	0.746	478.5	487.0	495.5	504.0	512.5	521.0	529
	68	64.5	0.607	6.62	2.69	0.711	478.7	487.2	495.7	504.2	512.9	521.4	529
ļ	67	63.0	0.578	6.30	3.01	0.677	478.9	487.4	495.9	504.4	513.1	521.6	530
	66	61.5	0.550	5.99	3.32	0.643	479.1	487.6	496.1	504.6	513.3	521.8	530
	65	60.0	0.523	5.69	3.62	0.611	479.3	487.8	496.4	504.9	513.5	522.0	530
	64	58.5	0.498	5.42	3.89	0.582	479.5	488.0	496.6	505.1	513.7	522.2	530
	63	57.0	0.473	5.15	4.16	0.553	479.6	488.1	496.7	505.2	513.8	522.3	530
-	62	55.5	0.450	4.90	4.41	0.526	479.7	484.2	496.8	505.3	513.9	522.4	531

of mor	ading Ther- neter,	Temp of	Force of	of V	ight apor Reqd.	Hu- midity,					ibic Foot		
F	ahr.	Dew-	Vapor in	In a Cubic	for Sat'n.	Satnra- tion =		Height o	of the Bar	ometer 1	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	in. 29.0	in. 29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	0.500	gr.	gr.	gr.	gr.	gr.	gr.	gr.
75	62	55.5	0.450	4.90	4.41	0.526	479.7	488.2	496.8	505.3	513.9	522.4	531.0
	61	54.0	0.428	4.66	4.65	0.501	479.9	488.4	497.0	505.5	514.1	522.6	531.2
	60	52.5	0.407	4.43	4.88	0.476	480.0	488.5	497.1	505.6	514.2	522.7	531.3
	59	51.0	0.386	4.21	5.10	0.452	480.1	488.6	497.2	505.7	514.3	522.8	531.4
	58	49.5	0.367	4.00	5.31	0.429	480.3	488.8	497.4	505.9	514.5	523.0	531.6
	57	48.0	0.349	3.79	5.52	0.407	480.4	488.9	497.5	506.0	514.6	523.1	531.7
	56	46.5	0.331	3.60	5.71	0.387	480.5	489.0	497.6	506.1	514.7	523.2	531.8
	55	45.0	0.315	3.42	5.89	0.367	480.6	489.1	497.7	506.2	514.8	523.3	531.9
	54	43.5	0.299	3.25	6.06	0.349	480.7	489.2	497.8	506.3	514.9	523.4	532.0
	53	42.0	0.283	3.09	6.22	0.332	480.8	489.3	497.9	506.4	515.0	523.5	532.1
	52	40.5	0.269	2.93	6.38	0.315	480.8	489.3	497.9	506.4	515.0	523.5	532.1
	51	39.0	0.255	2.78	6.53	0.299	480.9	489.4	498.0	506.5	515.1	523.6	532.2
	50	37.5	0.242	2.64	6.67	0.284	481.0	489.5	498.1	506.6	515.2	523.7	532.3
	49	36.0	0.230	2.51	6.80	0.270	481.1	489.6	498.2	506.7	515.3	523.8	532.4
	48	34.5	0.218	2.39	6.92	0.257	481.2	489.7	498.3	506.8	515.4	523.9	532.5
		:											
***	76	76.0	0.882	9.60	0.00	1.000	476.3	484.8	493.3	501.8	510.3	518.8	527.
76	75	74.5	0.840	9.14	0.46	0.952	476.6	485.1	1	502.1	510.6	519.1	527.6
	74	73.0	0.801	8.71	0.40	0.907	476.8	485.3	493.6 493.8	502.1	510.8	519.3	527.8
	73	71.5	0.561	8.30	1.30	0.865		1	1	502.6		519.6	528.1
	72	70.0	0.703	7.90	1.70	0.823	477.0	485.5	494.0	502.8	511.1		528.3
	71	11	1	į.	2.07	1	477.2	485.7	494.3	1		$519.8 \\ 520.0$	528.
	70	$68.5 \\ 67.0$	$0.692 \\ 0.659$	7.53 7.17	2.43	0.784 0.747	477.4 477.6	485.9 486.1	494.5	503.0	511.5 511.7	520.0	528.
	10	07.0	0.033	7.17	2.40	0.747	477.0	400.1	494.7	303.2	311.7	920.2	02000
	69	65.5	0.628	6.83	2.77	0.711	477.8	486.3	494.9	503.4	511.9	520.4	528.9
	68	64.0	0.597	6.49	3.11	0.676	477.9	486.4	495.0	503.6	512.1	520.6	529.2
	67	62.5	0.568	6.16	3.44	0.642	478.1	486.6	465.2	503.8	512.3	520.8	529.
	66	61.0	0.541	5.88	3.72	0.613	478.2	486.7	495.3	503.9	512.4	520.9	529.3
	65	59.5	0.515	5.59	4.01	0.582	478.3	486.8	495.4	504.0	512.5	521.0	529.6
	64	58.0	0.489	5.31	4.29	0.553	478.5	487.0	495.6	504.2	512.7	521.2	529.8
	63	56.5	0.465	5.06	4.54	0.527	478.6	487.1	495.7	504.3	512.8	521.3	529.9
	62	55.0	0.442	4.81	4.79	0.501	478.8	487.3	495.9	504.5	513.0	521.5	530.
	61	53.5	0.421	4.57	5.03	0.476	479.0	487.5	496.1	504.7	513.2	521.7	530.3
	60	52.0	0.100	4.34	5.26	0.452	479.1	487.6	496.2	504.8	513.3	521.8	530.
	59	50.5	0.380	4.13	5.47	0.430	499.2	487.7	496.3	504.9	513.4	521.9	530.
	58	49.0	0.361	3.92	5.68	0.408	499.3	}	496.4	505.0	513.5	522.0	530.
	57	47.5	0.343		5.87	0.389	499.4	1		1	513.6	1	530.
	56	46.0	0.326			0.369	499.5		1	505.2	513.7	522.2	530.
	55	41.5	0.309	3.36	6.24	0.351	499.6	488.1	496.7	505.3	513.8	522.3	530.
	54	43.0	0.293			0.332	499.7			I.		522.4	
	53	41.5	0.279	i .		0.316	499.8	i		505.5		522.5	531.
	52	40.0	0.264		1	0.301	499.9		1	505.6		522.6	531.
	51	38.5	0.251			0.301	500.0	1	1	1		522.7	531.
	50	37.0	0.239		1	0.269	500.0	1		505.8	1	522.8	
	49	35.5	-			1	1		497.3		514.4	1	1

of '	ding Ther-	Temp.	Force		ight apor Reqd.	Hu-		Weigh	t in Graii	as of a Cu	abic Foot	of Air.	
	neter, thr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n	midity, Satura- tion =		Height (of the Ba	rometer i	n Englis	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Air.	bic Ft.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr	gr.		gr.	gr.	gr.	gr.	gr	gr.	gr.
77	77	77.0	0.910	9.89	0.00	1.000	475.3	483.8	492.3	500.8	509.2	517 7	526.
ļ	76	75.5	0.868	9.42	0.47	0.953	475.5	484.0	492.5	501.0	509.4	517.9	526.
1	75	74.0	0.827	8.99	0.90	0.909	475.7	484.2	492.7	501.2	509.6	518.1	526.
	74	72.5	0.787	8.57	1.32	0.867	475.9	484.4	492.9	501.4	509.9	518.4	526
1	73	71.0	0.751	8.15	1.74	0.824	476.1	484.6	493.1	501.6	510.1	518.6	527.
	72	69.5	0.715	7.77	2.12	0.786	476.3	484.8	493.3	501.8	510.3	518.8	527.
	71	68.0	0.651	7.40	2.49	0.748	476.5	485.0	493.5	502.0	510.5	519.0	527.
	70	66.5	0.648	7.04	2.85	0.712	476.7	485.2	493.7	502.2	510.7	519.2	527.
	69	65.0	0.617	6.71	3.18	0.678	476.9	485.4	493.9	502.4	510.9	519.4	527
	68	63.5	0.588	6.37	3.52	0.641	477.0	485.6	494.1	502.6	511.1	519.6	528.
	67	62.0	0.559	6.06	3.83	0.613	477.2	485.8	494.3	502.8	511.3	519.8	528
	66	60.5	0.532	5.77	4.12	0.583	477.4	486.0	494.5	503.0	511.5	520.0	528
	65	59.0	0.506	5.49	4.40	0.556	477.5	486.1	494.6	503.1	511.6	520.1	528
	64	57.5	0.481	5.21	4.68	0.527	477.7	486.3	494.8	503.3	511.8	520.3	528
	63	56.0	0.458	4.96	4.93	0.501	477.9	486.5	495.0	503.5	512.0	520.5	529
	62	54.5	0.435	4.70	5.19	0.476	478.0	486.6	495.1	503.7	512.1	520.6	529
	61	53.0	0.414	4.49	5.40	0.454	478.0	486.6	495.1	503.7	542.2	520.7	529
	60	51.5	0.393	4.26	5.63	0.431	478.1	486.7	495.2	503.8	512.3	520.8	529
	59	50.0	0.373	4.05	5.84	0.410	478.2	486.8	495.3	503.9	512.4	520.9	529
	58	48.5	0.355	3.85	6.04	0.389	478.3	486.9	495.4	504.0	512.5	521.0	529
	57	47.0	0.337	3.65	6.24	0.369	478.5	487.1	495.6	504.1	512.7	521.2	529
	56	45.5	0.320	3.47	6.42	0.351	478.6	487.2	495.7	504.2	512.8	521.3	529
	55	44.0	0.304	3.29	6.60	0.333	478.7	487.3	495.8	504.3	512.9	521.4	530
	51	42.5	0.288	3.13	6.76	0.317	478.8	487.4	495.9	504.4	513.0	521.5	530
	53	41.0	0.274	2.97	6.92	0.301	478.9	487.5	496.0	504.5	513.1	521.6	530
	52	39.5	0.260	2.82	7.07	0.235	479.0	487.6	496.1	504.6	513.2	521.7	530
	51	38.0	0.246	2.67	7.22	0.270	479.1	457.7	496.2	504.7	513.3	521.8	530
	50	36.5	0.234	2.53	7.36	0.256	479.1	487.7	496.2	504.7	513.3	521.8	530
78	78	78.0	0.940	10.19	0.00	1.000	474.1	482.5	491.0	499.1	508.0	516.4	524.
•	77	76.5	0.896	9.72	0.47	0.954	474.4	482.9	491.4	499.9	508.3	516.7	525
	76	75.0	0.854	9.25	0.94	0.908	474.7	483.2	491.6	500.1	508.6	517.1	525
	75	73.5	0.814	8.82	1.37	0.865	474.9	483.4	491.8	500.3	508.8	517.3	525
	71	72.0	0.776	8.40	1.79	0.821	475.2	483.7	492.1	500.6	509.1	517.6	526
	73	70.5	0.739	8.00		0.785	475.4	483.9	492.3	500.8	500.3	517.8	526
	72	69.0	0.704	7.62		0.748	475.6	484.1	492.5	501.0	509.5	518.0	526.
	71	67.5	0.670	7.25	2.94	0.711	-175.S	484.3	492.7	501.2	509.7	518.2	526.
	70	66.0	0.638	6.91	3.28	0.678	475.9	484.4	492.9	501.4	509.9	518.4	526
	69	64.5	0.607	6.58	3.61	0.646	476.1	484.6	493.1	501.6	510.1	518.6	527
	68	63.0	0.578	6.26	3.93	0.614	476.3	484.8	493.3	501.8	510.3	518.8	527
	67	61.5	0.550	5.96	4.23	0.585	476.4	484.9	493.4	501.9	510.1	518.9	527.
	66	60.0	0.523	5.66	4.53	0.555	476.6	485.1	493.6	502.1	510.6	519.1	527
	65	58.5	0.498	5.38	4.81	0.528	476.8	485.3	493.8	502.3	510.8	519.3	527

of '	iding Ther-	Temp.	Force	Wei of V	apor	Hu-		Weight	in Grain	ns of a Cu	ibic Foot	of Air.	
mor	nete r, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat n.	midity, Satura- tion =		Height o	f the Bar	ometer i	a English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Air.	of aCu- bic Ft. of Air.	1 000.	in. 28.0	in. 28.5	29.0	in. 29.5	in. 30.0	30.5	31.0
0	0	0 50 5	in. 0.498	gr. 5.38	gr.	0.500	gr.	gr.	gr.	gr.	gr. 510.8	gr. 519.3	gr. 527.8
78	65 64	58.5 57.0	0.455	5.12	$\frac{4.81}{5.07}$	$0.528 \\ 0.502$	476.8 476.8	485.3 485.3	493.8 493.9	502.3 502.4	510.9	519.4	527.9
	63	55.5	0.450	4.88	5.31	0.479	476.9	485.4	494.0	502.4	511.0	519.5	528.0
	62	54.0	0.428	4.63	5.56	0.454	477.1	485.6	494.2	502.7	511.2	519.7	528.2
	61	52.5	0.407	4.40	5.79	0.432	477.2	485.7	494.3	502.8	511.3	519.8	528.3
	60	51.0	0.386	4.18	6.01	0.409	477.3	485.8	494.4	502.9	511.4	519.9	528.4
	59	49.5	0.367	3.98	6.21	0.391	477.4	485.9	494.5	503.0	511.5	520.0	528.5
	58	48.0	0.349	3.78	6.41	0.371	477.5	486.0	494.6	503.1	511.6	520.1	528.6
	57	46.5	0.331	3.59	6.60	0.352	477.6	486.1	494.7	503.2	511.7	520.2	528.7
	56	45.0	0.315	3.41	6.78	0.335	477.8	486.3	494.8	503.3	511.9	520.4	528.9
	55	43.5	0.299	3.24	6.95	0.318	477.9	486.4	494.9	503.4	512.0	520.5	529.0
1	54	42.0	0.283	3.07	7.12	0.301	478.0	486.5	495.0	503.5	512.1	520.6	529.1
	53	40.5	0.269	2.92	7.27	0.287	478.1	486.5	495.0	503.5	512.1	520.6	529.1
	52	39.0	0.255	2.77	7.42	0.272	478.2	486.6	495.1	503.6	512.2	520.7	529.2
	51	37.5	0.242	2.63	7.56	0.258	478.3	486.7	495.2	503.7	512.3	520.8	529.3
79	79	79.0	0.970	10.50		1.000	473.1	481.5	490.0	498.4	506.9	515.3	523.8
	78	77.5	0.925	10.01	0.49	0.953	473.4	481.8	490.3	498.7	507.2	515.6	524.1
	77	76.0	0.882	9.54	0.96	0.909	473.7	482.1	490.6	499.0	507.5	515.9	524.4
	76	74.5	0.840	9.10	1.40	0.867	473.8	482.2	490.7	499.2	507.7	516.2	524.7
	75	73.0	0.801	8.66	1	0.825	474.0	482.4	490.9	499.4	507.9	516.4	524.9
	74 73	71.5	0.763	8.25 7.86		$\begin{vmatrix} 0.786 \\ 0.749 \end{vmatrix}$	474.3 474.5	482.7 482.9	491.2	499.7	508.2	516.7	525.2 525.4
ì	10	10.0	0.727	1.00	2.04	0.145	474.0	402.0	491.4	433.3	300.4	010.5	020.4
	72	68.5	0.692	7.48	3.02	0.712	474.7	483.1	491.6	500.1	508.6	517.1	525.6
}	71	67.0	0.659	7.12	3.38	0.678	474.9	483.4	491.9	500.4	508.8	517.3	525.8
	70	65.5	0.628	6.79	3.71	0.647	475.1	483.6	462.1	500.6	509.0	517.5	526.0
	69	64.0	0.597	6.45	4.05	0.614	475.3	483.8	492.3	500.8	509.2	517.7	526.2
	68	62.5	0.568	6.14	4.36	0.585	475.4	483.9	492.4	500.9	509.3	517.8	526.3
	67	61.0	0.541	5.84	4.66	0.556	475.6	484.1	492.6	501.1	509.5	518.0	526.5
	66	59.5	0.515	5.55	4.95	0.529	475.7	484.2	492.7	501.2	509.6	518.1	526.6
	65	58.0	0.489	5.28	5.22	0.503	475.8	484.3	492.8	501.3	509.8	518.3	526.8
	61	56.5	0.465	5.02		0.478	476.0	484.5	493.0	501.5	510.0	518.5	527.0
	63	55.0	0.442	4.78		0.455	476.1	484.6	493.1	501.6	510.1	518.6	527.1
	62	53.5	0.421	4.54		0.432	476.3	484.8	493.3	501.8	510.3	518.8	527.3
	61	52.0	0.400	4.31	6.19	0.410	476.4	484.9	493.4	501.9	510.4	518.9	527.4
	60	50.5	0.380	4.10	6.40	0.390	476.5	485.0	493.5	502.0	510.5	519.0	527.5
	59	49.0	0.361	3.90	6.60	0.371	476.6	485.1	493.6	502.1	510.6	519.1	527.6
	58	47.5	0.343			0.353	476.7	485.2	1	502.2	510.7		
	57	46.0	0.326		1	0.335	476.8		1	502.3		!	1
	56	41.5	0.309	3.3	l.	0.318	476.9		l .	502.4		1	1
1	55	43.0	0.293	3.17		0.301	477.0	1		502.5	}	1	
I	54	41.5	0.279	3.01	i	0.287	477.1	485.6		502.6	i .	1	1
I	53	40.0	1	t t	l.	1	477.2	1	1	502.7	1	1	
<u> </u>	52	38.5	0.251	2.73	7.78	0.260	477.3	485.8	494.3	502.8	511.3	1 919.8	528.3

	ding Ther-	Temp.	Force		ight apor	Hu-		Weight	t in Grain	ıs of a Cu	abic Foot	of Air.	
mor	neter, thr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height o	of the Ba	rometer i	n English	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bie Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.	1 000	gr.	gr.	gr.	gr.	gr.	gr.	gr
80	80	80.0 78.5	1.001 0.955	10.81 10.31	$0.00 \\ 0.50$	0.954	472.0	480.4	488.9	497.3	505.7 506.0	514.1	522.6 522.9
	79	77.0	0.933	9.83	0.98	0.909	472.5	480.9	489.4	497.9	506.3	514.7	523.2
	78 77	75.5	0.868	9.37	1.44	0.867	472.7	481.1	489.6	498.1	506.5	514.7	523.
		74.0	0.827	8.93	1.88	0.826	473.0	481.4	489.9	498.4	506.8	515.2	523.
	76	72.5	0.787	8.50	2.31	0.320	473.2	481.6	490.1	498.6	507.0	515.4	523.
	75 74	71.0	0.751	8.11	2.70	0.750	473.4	481.8	490.3	498.8	507.2	515.6	524.
	7 3	69.5	0.715	7.71	3.10	0.713	473.6	482.1	490.6	499.1	507.5	515.9	524.
	72	68.0	0.681	7.35	3.46	0.680	473.8	482.3	490.8	499.3	507.7	516.1	524.0
	71	66.5	0.648	6.99	3.82	0.647	474.0	482.5	491.0	499.5	507.9	516.3	524.
	70	65.0	0.617	6.66		0.616	474.2	482.7	491.2	499.7	508.1	516.5	525.
	69	63.5	0.588	6.33	4.48	0.586	474.4	482.9	491.4	499.9	508.3	516.7	525.
	68	62.0	0.559	6.03		0.558	474.5	483.0	491.5	500.0	508.4	516.8	525.
	67	60.5	0.532	5.74	5.07	0.531	474.7	483.2	491.7	500.2	508.6	517.0	525.
	66	59.0	0.506	5.45	5.36	0.504	474.9	483.4	491.9	500.4	508.8	517.2	525.
	65	57.5	0.481	5.18	5.63	0.479	475.0	483.5	492.0	500.5	508.9	517.3	525.
	64	56.0	0.458	4.93	5.96	0.456	475.2	483.7	492.2	500.7	509.1	517.5	526.
	63	54.5	0.435	4.69	6.12	0.434	475.3	483.8	492.3	500.8	509.2	517.6	526.
	62	53.0	0.414	4.46	6.35	0.413	475.4	483.9	492.4	500.9	509.3	517.7	526.
	61	51.5	0.393	4.23	6.58	0.391	475.5	484.0	492.5	501.0	509.4	517.8	526.
	60	50.0	0.373	4.02	6.79	0.372	475.6	484.1	492.6	501.1	509.5	517.9	526.
	59	48.5	0.355	3.82	6.99	0.353	475.7	484.2	492.7	501.2	509.6	518.0	526.
	58	47.0	0.337	3.63	7.18	0.336	475.9	484.4	492.9	501.4	509.8	518.2	526.
	57	45.5	0.320	3.45	7.36	0.319	476.0	484.5	493.1	501.5	509.9	518.3	526.
1	56	44.0	0.304	3.27	7.54	0.302	476.1	484.6	493.2	501.6	510.0	518.4	526.
	55	42.5	0.288	3.11	7.70	0.288	476.2	484.7	493.3	501.7	510.1	518.5	527.
	54	41.0	0.274	2.96	7.85	0.274	476.3	484.8	493.4	501.8	510.2	518.6	527.
	53	39.5	0.260	2.82	7.99	0.261	476.3	484.8	493.4	501.8	510.2	518.6	527.
81	81	81.0	1.034	11.14	0.00	1.000	471.0	479.4	487.8	496.2	504.6	513.0	521.
-	80	79.5	0.986	10.62	0.52	0.953	471.3	479.7	488.1	496.5	504.9	513.3	521.
	7 9	78.0	0.940	10.32		0.910	471.5	479.9	488.4	496.8	505.2	513.6	522.
	78	76.5	0.896	9.65	1.49	0.866	471.7	480.1	488.6	497.0	505.4	513.8	522.
	77	75.0	0.854	9.20		0.826	472.0	480.4	488.9	497.3	505.7	514.1	522.
	76	73.5	0.814	8.77		0.787	472.2	480.6	489.1	497.5		514.3	522.
	75	72.0	0.776	8.35		0.750	472.5	480.9	1	497.8	506.2	514.6	523.
	74	70.5	0.739	7.95	1	0.713	472.6	481.0	489.5	497.9	506.4	514.8	523.
	73	69.0	0.704	7.57		0.680	472.8	481.2	489.7	498.1	506.6	515.0	523.
	72	67.5	0.670	7.21	3.93	0.617	473.0	481.4	489.9	498.3	506.8	515.2	523.
	71	66.0	0.638	6.87	i	0.617	473.2	481.6	490.1	498.5	507.0	515.4	523.
	70	64.5	0.607	6.54	4.60	0.587	473.4	481.8	490.3	498.7	507.2	515.6	524.
	69	63.0	0.578	6.22		0.558	473.6	482.0	490.5	498.9	507.4	515.8	524.
	68	61.5	0.550	5.92	5.22	0.531	473.7	482.2	490.7	499.1	507.6	516.0	524.

	ading Ther-	Temp.	Force	Wei of V	apor	Hu-		Weight	t in Grain	ns of a Cu	bic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0 81	68	61.5	in. 0.550	gr. 5.92	gr. 5.22	0.531	gr. 473.7	gr. 482.2	gr. 490.7	gr. 499.1	gr. 507.6	gr. 516.0	gr. 524.5
0.	67	60.0	0.523	5.62	5.52	0.505	473.8	482.3	490.8	499.2	507.7	516.1	524.6
	66	58.5	0.498	5.31	5.83	0.477	474.0	482.5	491.0	499.4	507.9	516.3	524.8
	65	57.0	0.473	5.08	6.06	0.456	474.1	482.6	491.1	499.5	508.0	516.4	524.9
	64	55.5	0.450	4.84	6.30	0.434	474.3	482.8	491.3	499.7	508.2	516.6	525.1
	63	54.0	0.428	4.60	6.54	0.413	474.4	482.9	491.4	499.8	508.3	516.7	525.2
	62	52.5	0.407	4.37	6.77	0.392	474.5	483.0	491.5	499.9	508.4	516.8	525.3
	61	51.0	0.386	4.15	6.99	0.373	474.6	483.1	491.6	500.0	508.5	516.9	525.4
	60	49.5	0.367	3.95	7.19	0.355	474.7	483.2	491.7	500.1	508.6	517.0	525.5
	59	48.0	0.349	3.75	7.39	0.337	474.9	483.4	491.9	500.3	508.8	517.2	525.7
	58	46.5	0.331	3.56	7.58	0.320	475.0	483.5	492.0	500.4	508.9	517.3	525.8
	57	45.0	0.315	3.38	7.76	0.303	475.1	483.6	492.1	500.5	509.0	517.4	525.9
	56	43.5	0.299	3.21	7.93	0.289	475.2	483.7	492.2	500.6	509.1	517.5	526.0
	55	42.0	0.283	3.05	8.09	0.274	475.3	483.8	492.3	500.7	509.2	517.6	526.1
	54	40.5	0.269	2.90	8.24	0.260	475.3	483.8	492.3	500.7	509.2	517.6	526.1
82	82	82.0	1.067	11.47	0.00	1.000	470.0	478.4	486.8	495.2	503.5	511.9	520.3
	81	80.5	1.017	10.94	0.53	0.954	470.3	478.7	487.0	495.4	503.8	512.2	520.6
-	80	79.0	0.970	10.44	1.03	0.910	470.6	479.0	487.3	495.7	504.1	512.5	520.9
	79	77.5	0.925	9.95	1.52	0.868	470.7	479.1	487.5	495.9	504.3	512.7	521.1
1	78	76.0	0.882	9.49	1.98	0.827	471.0	479.4	487.8	496.2	504.6	513.0	521.4
11	77	74.5	0.840	9.03	2.44	0.787	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	76	73.0	0.801	8.60	2.87	0.750	471.5	479.9	488.3	496.7	505.1	513.5	521.9
	75	71.5	0.763	8.19	3.28	0.714	471.6	480.0	488.5	496.9	505.3	513.7	522.1
li	74	70.0	0.727	7.81	3.66	0.681	471.8	480.2	488.6	497.1	505.5	513.9	522.4
	73	68.5	0.692	7.43	4.04	0.648	472.0	480.4	488.8	497.3	505.7	514.1	522.6
1	72	67.0	0.659	7.08	4.39	0.618	472.2	480.6	489.0	497.5	505.9	514.3	522.8
	71	65.5	0.628	6.75	4.72	0.588	472.4	480.8	489.2	497.7	506.1	514.5	523.0
li	70	64.0	0.597	6.41	5.06	0.559	472.5	480.8	489.4	497.9	506.3	514.7	523.2
	69	62.5	0.568	6.10	5.37	0.532	472.6	481.0	489.5	498.0	506.4	514.8	523.3
1	68	61.0	0.541	5.81	5.66	0.507	472.8	481.2	489.7	498.2	506.6	515.0	523.5
	67	59.5	0.515	5.52	1	0.481	473.0	481.4	489.9	498.4	506.8	515.2	523.7
1	66	58.0	0.489	5.25	6.22	0.458	473.1	481.5	490.0	498.5	506.9	515.3	523.8
1	65	56.5	0.465	4.99	6.48	0.435	473.2	481.6	490.1	498.6	507.0	515.4	523.9
11	64	55.0	0.442	4.75	6.72	0.414	473.4	481.8	490.3	498.8	507.2	515.6	524.1
1	63	53.5	0.421	4.51	6.96	0.393	473.5	482.0	490.5	499.0	507.4	515.8	524.3
	62	52.0	0.400	4.29	7.18	0.374	473.6	482.1	490.6	499.1	507.5	515.9	524.4
	61	50.5	0.380	4.08	7.39	0.356	473.7	482.2	490.7	499.2	507.6	516.0	524.4
	60	49.0	0.361	1	7.60	0.337	473.8	1		1	507.7	1	524.5
1	59	47.5	0.343	3.68	7.79	0.320	473.9	1	1	1	507.8	516.2	524.6
1	58	46.0	0.326	3.50	1	0.305	474.0	1	1		507.9	516.3	524.7
1	57	44.5	0.309	3.32	1	0.289	474.1	1	1	1	508.0	516.4	524.8
	56	43.0	0.293	3.15		0.274	474.2				508.1	516.5	524.9
	55	41.5	0.279	2.99	8.48	0.260	474.3	482.8	491.3	499.8	508.2	516.6	525.1

	ding	Temp.	Force		ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
	neter, shr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height	of the Ba	rometer i	in Englisi	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	3 1.0
83	0	83.0	in. 1.101	gr. 11.82	gr. 0.00	1.000	gr. 468.8	gr. 477.2	gr. 485.5	gr. 493.9	gr. 502.3	gr. 510.6	gr. 519.0
03	83	81.5	1.050	11.27	0.55	0.953	469.1	477.5	485.8	494.2	502.6	511.0	519.4
	81	80.0	1.001	10.75	1.07	0.909	469.4	477.8	486.1	494.5	502.9	511.3	519.7
	80	78.5	0.955	10.25	1.57	0.868	469.7	478.1	486.4	494.8	503.2	511.6	520.0
	79	77.0	0.910	9.78	2.04	0.828	470.0	478.4	486.7	495.1	503.5	511.9	520.3
lì	78	75.5	0.868	9.31	2.51	0.786	470.3	478.7	487.0	495.4	503.8	512.2	520.6
	77	74.0	0.827	8.88	2.94	0.751	470.5	478.9	487.2	495.6	504.0	512.4	520.8
	76	72.5	0.787	8.45	3.37	0.715	470.6	479.0	487.4	495.8	504.2	512.6	521.0
	75	71.0	0.751	8.05	3.77	0.681	470.8	479.2	487.6	496.0	504.4	512.8	521.2
	74	69.5	0.715	7.66	4.16	0.647	471.0	479.4	487.8	496.2	504.6	513.0	521.4
	73	68.0	0.681	7.30	4.52	0.618	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	72	66.5	0.648	6.95	4.87	0.588	471.4	479.8	488.2	496.6	505.0	513.4	521.8
	71	65.0	0.617	6.62	5.20	0.560	471.6	480.0	488.4	496.8	505.2	513.6	522.0
	70	63.5	0.588	6.29	5.53	0.533	471.7	480.1	488.5	497.0	505.4	513.8	522.3
	69	62.0	0.559	5.99	5.83	0.507	471.9	480.3	488.7	497.2	505.6	514.0	522.5
	68	60.5	0.532	5.70	6.12	0.482	472.0	480.4	488.8	497.3	505.7	514.1	522.6
	67	59.0	0.506	5.42	6.40	0.459	472.2	480.6	489.0	497.5	505.9	514.3	522.8
	66	57.5	0.481	5.15	6.67	0.435	472.4	480.8	489.2	497.7	506.1	514.5	523.0
	65	56.0	0.458	4.90	6.92	0.414	472.4	480.8	489.3	497.8	506.2	514.6	523.1
	64	54.5	0.435	4.66	7.18	0.394	472.5	480.9	489.4	497.9	506.3	514.7	523.2
	63	53.0	0.414	4.43	7.39	0.375	472.7	481.1	489.6	498.1	506.5	514.9	523.4
	62	51.5	0.393	4.21	7.61	0.356	472.8	481.2	489.7	498.2	506.6	515.0	523.5
	61	50.0	0.373	4.00	7.82	0.339	472.9	481.3	489.8	498.3	506.7	515.1	523.6
	60	48.5	0.355	3.80	8.02	0.322	473.1	481.4	489.9	498.4	506.8	515.2	523.7
	59	47.0	0.337	3.60	8.22	0.305	473.2	481.5	490.0	498.5	506.9	515.3	523.8
	58	45.5	0.320	3.42	8.40	0.289	473.3	481.6	490.1	498.6	507.0	515.4	523.9
	57	44.0	0.304	3.25	8.57	0.276	473.4	481.7	490.2	498.7	507.1	515.5	524.0
	56	42.5	0.288	3.09	8.73	0.261	473.5	481.8	490.3	498.8	507.2	515.6	524.1
84	84	84.0	1.136	12.17	0.00	1.000	467.8	476.2	484.5	492.7	501.2	509.6	517.9
	83	82.5	1.083	11.61	0.56	0.954	468.1	476.4	484.8	493.2	501.5	509.8	518.2
	82	81.0	1.034	11.07	1.10	0.910	468.4	476.7	485.1	493.5	501.8	510.1	518.5
	81	79.5	0.986	10.55	1.62	0.867	468.6	476.9	485.4	493.7	502.1	510.5	518.8
	80	78.0	0.940 0.896	10.07 9.59	2.10	0.827 0.788	468.9	477.3	485.7	494.0 494.2	502.4	510.8 511.0	519.1 519.3
	79 78	75.0	0.854	9.14	2.58 3.03	0.788	469.1 469.4	477.5 477.8	485.9 486.1	494.5	502.6	511.3	519.7
	77	73.5	0.814	8.71	3.46	0.716	469.6	478.0	486.3	494.7	503.1	511.5	519.9
	76	72.0	0.776	8.30	3.87	0.682	469.8	478.2	486.5	494.9	503.3	511.7	520.1
	75	70.5	0.739	7.90	4.27	0.649	470.1	478.5	486.8	495.2	503.6	512.0	520.4
	74	69.0	0.704	7.53	4.64	0.619	470.3	478.7	487.0	495.4	503.8	512.2	520.6
	73	67.5	0.670	7.17	5.00	0.589	470.5	478.9	487.2	495.6	504.0	512.4	520.8
	72	66.0	0.638	6.83	1 1	0.561	470.6	479.0	487.4	495.8	504.2	512.6	521.0
	71	64.5	0.607	1	5.67	0.534	470.7			495.9		512.7	521.1

of '	iding Ther-	Temp	Force of	Wei of Va	ght apor Regd.	Hu-		Weight	in Grain	ns of a Cu	ibic Foot	of Air.	
	neter, ahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	in. 31.0
0	0	0	in. 0.607	gr. 6.50	gr. 5.67	0.534	gr. 470.7	gr. 479.1	gr. 487.5	gr. 495.9	gr. 504.3	gr. 512.7	gr. 521.1
84	71 70	64.5	0.578	6.18	5.99	0.508	470.9	479.3	487.7	496.1	504.5	512.9	521.3
	69	61.5	0.550	5.87	6.30	0.482	471.1	479.5	487.9	496.3	504.7	513.1	521.5
	68	60.0	0.523	5.59	6.58	0.459	471.2	479.6	488.0	496.4	504.8	513.2	521.6
	67	58.5	0.498	5.31	6.86	0.436	471.4	479.8	488.2	496.6	505.0	513.4	521.8
	66	57.0	0.473	5.05	7.12	0.415	471.6	480.0	488.3	496.7	505.2	513.6	522.1
	65	55.5	0.450	4.81	7.36	0.395	471.6	480.0	488.4	496.8	505.3	513.7	522.2
		54.0	0.428	157	7.60	0.375	471.7	480.1	488.5	496.9	505.4	513.8	522.3
	64	52.5	0.425	4.57	7.82	0.357	471.8	480.2	488.6	497.0	505.5	513.9	522.4
	63	51.0	0.386	4.13		0.339	471.9	480.4	488.8	497.2	505.7	514.0	522.5
	62 61	49.5	0.367	3.93		0.323	471.9	480.5	488.9	497.3	505.S	514.1	522.6
	60	48.0	0.349	3.73	8.44	0.306	472.2	480.6	489.0	497.4	505.9	514.2	522.7
	59	46.5	0.331	3.55		0.292	472.3	480.7	489.1	497.5	506.0	514.3	522.8
	58	45.0	0.315	3.37	8.80	0.277	472.4	480.8	489.2	497.6	506.1	514.4	522.9
	57	43.5	0.299	3.20	8.97	0.263	472.5	480.9	489.3	497.7	506.2	514.5	523.0
	31	45.0	0.233	9.20	0.5.	0.200	112.0	100.0	400.0	431	500.2		
		2.0			0.00	1 000			.00.	401.0	-00.1	700 5	516.8
85	85	85.0	1.171	12.53	l .	1.000	466.8	475.2	483.5	491.8	500.1	508.5	
	84	83.5	1.118	11.95	0.58	0.954	467.1	475.4	483.7	492.1	500.1	508.7	517.1
	83	82.0	1.067	11.40	1	0.910	467.3	475.6	484.0	492.4	501.0	509.0	517.4
	82	80.5	1.017	10.87		0.868	467.6	475.9	484.3	492.7	1	509.5	517.9
	81	79.0	0.970	10.38	1	0.829	467.8	476.1	484.5	492.9	501.2	509.8	517.5
	80	77.5	0.925	9.89	1	0.789	468.1	476.4	484.8	493.2	501.5	510.1	518.3
	79	76.0	0.882	9.43	3.10	0.753	468.4	476.7	485.1	493.5	301.3	310.1	310.6
	78	74.5	0.840	8.98	3.55	0.717	468.6	476.9	485.3	493.7	502.0	510.3	518.7
	77	73.0	0.801	8.55	3.98	0.682	468.7	477.1	485.5	493.9	502.2	510.5	518.9
	76	71.5	0.763	8.15	4.38	0.650	469.0	477.4	485.8	494.2	502.5	510.8	519.2
	75	70.0	0.727	7.76	4.77	0.619	469.2	477.6	486.0	494.4	502.7	511.0	519.
	74	68.5	0.692	7.39	5.14	0.589	469.4	477.8	486.2	494.6	502.9	511.2	519.6
	73	67.0	0.659	7.04	5.49	0.562	469.7	478.1	486.5	494.9	503.2	511.5	519.9
	72	65.5	0.628	6.71	5.82	0.536	469.9	478.3	486.7	495.1	503.4	511.7	520.1
	71	64.0	0.597	6.37	6.16	0.508	470.1	478.5	486.9	495.3	503.6	511.9	520.3
	70	62.5	0.568	6.07	1	0.484	470.3	478.7		495.5	1	1	520.
	69	61.0	0.541	5.77		0.460	470.5	1	1	1	Į.		1
	68	59.5	0.515	5.48	1	0.437	470.6	1	1	1	504.1	513.5	
	67	58.0					470.6		1		1		1
	66	56.5	1		7.57			1				1	521.
	65	55.0			7.81	1			1			512.8	521.
	64	53.5	0.421	4.40	8.04	0.359	470.9	479.3	487.7	496.1	504.5	512.9	521.
	63	52.0		1	8.27		1		1	1	1	1	
	62	50.5		1	1	1				1	1		l l
	61	49.0		1						1	1	1	
	60	47.5				i	1		1	1		1	
	59	46.0			1			1		1		· I	
	58	44.5		1		1	1		488.5		}		522.

of	ading Ther-	Temp.	Force	of V	ight apor	Hu-		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
	meter, ahr.	of Dew- Point,	Vapor in	In a Cubic	Reqd. for Sat'n.	midity, Satura- tion =		Height (of the Ba	rometer i	in Englisl	h Inches	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
0	0	0	in.	gr.	gr.		gr.	gr.	gr.	gr.	gr.	gr.	gr.
86	86	86.0	1.209	12.91	0.00	1.000	465.7	474.0	482.3	490.6	498.9	507.2	515.
	85	84.5	1.153	12.31	0.60	0.954	466.0	474.3	482.6	490.9	499.2	507.5	515.
	84	83.0	1.101	11.75	1.16	0.910	466.3	474.6	482.9	491.2	499.5	507.8	516.
	83	81.5	1.050	11.20	1 1	0.868	466.5	474.8	483.2	491.5	499.8	508.1	516.
	82	80.0	1.001	10.69	2.22	0.828	466.8	475.1	483.5	491.8	500.1	508.4	516.
	81	78.5	0.955	10.19		0.789	467.1	475.4	483.8	492.1	500.4	508.7	517.
	80	77.0	0.910	9.71	3.20	0.752	467.3	475.6	484.0	492.3	500.7	509.0	517.
	79	75.5	0.868	9.25	3.66	0.717	467.5	475.S	484.2	492.5	500.9	509.2	517
	78	74.0	0.827	8.82	4.09	0.683	467.8	476.1	484.5	492.8	501.2	509.5	517
	77	72.5	0.787	8.40	4.51	0.651	468.0	476.3	484.7	493.0	501.4	509.7	518
	76	71.0	0.751	8.00	4.91	0.619	468.2	476.5	484.9	493.2	501.6	509.9	518
	75	69.5	0.715	7.62	5.29	0.590	468.3	476.6	485.0	493.4	501.8	510.2	518
	74	68.0	0.681	7.26	5.65	0.562	468.5	476.8	485.2	493.6	502.0	510.4	518
	73	66.5	0.648	6.91	6.00	0.535	468.8	477.1	485.5	493.9	502.2	510.6	519
	72	65.0	0.617	6.58	6.33	0.509	468.9	477.2	485.6	494.0	502.4	510.8	519
	71	63.5	0.588	6.26	6.65	0.485	469.1	477.4	485.8	494.2	502.6	511.0	519
	70	62.9	0.559	5.95	6.96	0.461	469.2	477.5	485.9	494.3	502.7	511.1	519
	69	60.5	0.532	5.66	7.25	0.438	469.4	477.7	486.1	494.5	502.9	511.3	519
	68	59.0	0.506	5.38	7.53	0.417	469.6	477.9	486.3	494.7	503.1	511.5	519
	67	57.5	0.481	5.11	7.80	0.396	469.8	478.1	486.5	494.9	503.3	511.7	520
İ	56	56.0	0.458	4.87	8.04	0.377	469.9	478.2	486.6	495.0	503.4	511.8	520
	65	54.5	0.435	4.63	8.28	0.359	470.0	478.3	486.7	495.1	503.5	511.9	520
	64	53.0	0.414	4.40	8.51	0.341	470.1	478.4	486.8	495.1	503.6	512.0	520
İ	63	51.5	0.393	4.19	8.72	0.325	470.2	478.5	486.9	495.2	503.7	512.1	520
1	62	50.0	0.373	3.98	8.93	0.308	470.4	478.7	487.1	495.4	503.9	512.2	520
- 1	61	48.5	0.355	3.78	9.13	0.293	470.5	478.8	487.2	495.5	504.0	512.3	520
	60	47.0	0.337	3.59	9.32	0.278	470.6	478.9	487.3	495.6	504.1	512.4	520
	59	45.5	0.320	3.40	9.51	0.263	470.7	479.0	487.4	495.7	504.2	512.5	521
												,	
37	87	87.0	1.247	13.29	0.00	1.000	464.5	472.8	481.1	489.4	497.7	506.0	514
	86	85.5	1.190	12.68	0.61	0.954	464.8	473.1	481.4	489.7	498.0	506.3	514.
	85	84.0	1.136	12.10	1.19	0.910	465.1	473.4	481.7	490.0	498.3	506.6	514.
	84	82.5	1.083	11.54	1.75	0.868	465.4	473.7	482.0	490.3	498.6	506.9	515.
	83	81.0	1.034	11.01	2.28	0.828	465.7	474.0	482.3	490.6	498.9	507.2	515
	82	79.5	0.986	10.49	2.80	0.789	466.0	474.3	482.6	490.9	499.2	507.5	515
	81	78.0	0.940	10.01	3.28	0.753	466.3	474.6	482.9	491.2	499.5	507.8	516
	80	76.5	0.896	9.54	3.75	0.718	466.5	474.8	483.1	491.4	499.8	508.1	516
	79	75.0	0.854	9.09	4.20	0.684	466.8	475.1	483.5	491.8	500.1	508.4	516
	78	73.5	0.814	8.66	4.63	0.652	467.0	475.3	483.7	492.0	500.3	508.6	517
	77	72.0	0.776	8.24	5.05	0.620	467.2	475.5	483.9	492.2	500.5	508.8	517.
	76	70.5	0.739	7.85	5.44	0.591	467.3	475.6	484.0	492.3	500.7	509.0	517.
	75	69.0	0.704	7.48	5.81	0.563	467.5	475.8	484.2	492.5	500.9	509.2	517.
	74	67.5	0.670	7.12	6.17	0.536	467.7	476.0	484.4	492.7	501.1	509.4	517.

	ding Ther-	Temp.	Force	Wei of V	apor	Hu-		Weigh	t in Grain	ns of a Cu	ıbic Foot	of Air.	
	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n Euglish	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	28.5	29.0	29.5	30.0	30.5	31.0
87	° 74	67.5	in. 0.670	gr. 7.12	gr 6.17	0.536	gr. 467.7	gr. 476.0	gr. 484.4	gr. 492.7	gr. 501.1	gr. 509.4	gr. 517.8
01	73	66.0	0.638	6.78	6.51	0.510	467.9	476.2	484.6	492.9	501.1	509.6	518.0
1	72	64.5	0.607	6.46	6.83	0.486	468.1	476.4	484.8	493.1	501.5	509.8	518,2
	71	63.0	0.578	6.14	7.15	0.462	468.3	476.6	485.0	493.3	501.7	510.1	518.5
	70	61.5	0.550	5.85	7.44	0.440	468.4	476.7	485.1	493.5	501.9	510.3	518.7
	69	60.0	0.523	5.56	7.73	0.418	468.5	476.9	485.3	493.7	502.0	510.4	518.8
	68	58.5	0.498	5.28	8.01	0.397	468.7	477.I	485.5	493.9	502.2	510.6	519.0
	67	57.0	0.473	5.02	8.27	0.378	468.8	477.2	485.6	494.0	502.3	510.7	519.1
	66	55.5	0.450	4.77	8.52	0.359	468.9	477.3	485.7	494.1	502.4	510.7	519.2
	65	54.0	0.428	4.54	8.75	0.342	469.1	477.5	485.9	494.3	502.6	510.9	519.4
	64	52.5	0.407	4.33	8.96	0.326	469.2	477.6	486.1	494.4	02.7	511.0	519.5
	63	51.0	0.386	4.12	9.17	0.310	469.3	477.7	486.2	494.5	02.8	511.1	519.6
	62	49.5	0.367	3.91	9.38	0.294	469.4	477.8	486.3	494.6	⇒02.9	511.2	519.7
	61	48.0	0.349	3.71	9.58	0.279	469.6	477.9	486.5	494.8	503.1	511.4	519.9
	60	46.5	0.331	3.51	9.78	0.264	469.7	478.1	486.6	494.9	503.2	511.5	520.0
50	88	88.0	1.286	13.68	0.00	1.000	463.5	471.7	480.0	488.3	496.6	504.8	513.
88	87	86.5	1.228	13.06	0.62		463.8	472.0	480.3	488.6	496.9	505.1	513.
	86	85.0	1.171	12.46	1.22	1	464.2	472.4	480.7	489.0	497.3	505.6	513.9
	85	83.5	1.118	11.88	1.80		464.4	472.7	481.0	489.3	497.6	505.9	514.
	84	82.0	1.067	11.34	į.	1	464.7	473.0	481.3	489.6	497.9	506.2	514.
	83	80.5	1.017	10.81	1	1	465.0	473.3	481.6	489.9	498.2	506.5	514.
	82	79.0	0.970	10.31	3.37	1	465.2	473.5	481.8	490.1	498.4	506.7	515.
	81	77.5	0.925	9.83	3.85	0.718	465.5	473.S	482.1	490.4	498.7	507.0	515.
	80	76.0	0.882	9.37	4.31	0.685	465.8	474.1	482.4	490.7	499.0	507.3	515.
	79	74.5	0.840	8.93	4.75	0.653	466.1	474.4	482.7	491.0	499.3	507.6	515.
	78	73.0	0.801	8.50	5.18	0.621	466.3	474.6	482.9	491.2	499.5	507.8	516.
	77	71.5	0.763	8.09	5.59	0.591	466.4	474.7	483.0	491.3	499.7	508.0	516.
	76	70.0	0.727	7.71	5.97	0.563	466.6	474.9	483.2	491.5	499.9	508.2	516.
	75	68.5	0.692	7.34	6.34	0.537	466.8	475.1	483.4	491.7	500.1	508.4	516.
	74	67.0	0.659	6.99	6.69	0.511	467.0	475.3	483.6	491.9	500.3		1
	73	65.5	0.628	6.66	7.02	0.487	467.2	475.5	483.8	492.1	500.5	508.8	517.
	72	64.0	0.597	6.33	7.35	0.463	467.4	475.7	484.0	492.3			
	71	62.5	0.568	6.03	1	1	467.4	1	1	1	500.8		517.
	70	61.0	0.541	5.74	1		1		1	1		1	
	69	59.5	0.515	5.45	1	0.398	1	1	484.3			1	+
	68	58.0	0.489	5.18	8.50	0.378	467.9	476.2	484.5	492.9	501.3	509.6	518.
	67	56.5	0.465	4.93	1	1	1	1	1	1	501.5	1	1
	66	55.0	0.442	1		1	1	1	1		1	1	1
	65	53.5	0.421	4.47	1	1		1	1		1	1	
	64	52.0	0.400		1	1	1	i			1	1	ł
	63	50.5	0.380		1	1	1	1	1	1	1		1
	62	49.0	1			1			i .			510.4	
	61	47.5	0.343	3.62	2 10.06	0.265	468.8	477.2	485.5	493.8	502.2	510.5	518.

of '	ading Ther-	Temp.	Force		apor	Hu-		Weight	t in Grain	ıs of a Cı	ibic Foot	of Air.	
mor	neter, ahr.	of Dew- Point,	of Vapor in	In a Cubic	Reqd. for Sat'n	midity, Satura- tion =		Height o	of the Ba	rometer i	n Englisl	h Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.
0	0	0	in.	gr.	gr		gr.	gr.	gr.	gr.	gr.	gr.	gr.
89	89	89.0	1.326	14.08	0.00	1.000	462.4	470.6	478.9	487.1	495.4	503 6	511.
	88	87.5	1.266	13.44	0.64	0.954	462.7	470.9	479.2	487.4	495.7	503.9	512.
٠,	87	86.0	1.209	12.84	1.24	0.912	463.0	471.2	479.5	487.8	496.1	504.4	512
	86	84.5	1.153	12.24	1.84	0.869 0.830	463.3	471.5	479.8	488.1	496.4	504.7	513
	85	81.5	1.101	11.68 11.13	$2.40 \\ 2.95$	0.530	463.6	471.8 472.2	480.1	488.4	496.7	505.0 505.4	513
	84 83	80.0	1.001	10.62	3.46	0.754	464.0 464.2	472.5	480.8	489.1	497.4	505.7	513 514
	82	78.5	0.955	10.13	3.95	0.719	464.4	472.7	481.0	489.3	497.6	505.9	514
	81	77.0	0.910	9.66	4.42	0.686	464.7	473.0	481.3	489.6	497.9	506.2	514
	80	75.5	0.868	9.20	4.88	0.653	464.9	473.2	481.5	489.8	498.1	506.4	514
	79	74.0	0.827	8.77	5.31	0.623	465.2	473.5	481.8	490.1	498.4	506.7	515
	78	72.5	0.787	8.35	5.73	0.593	465.4	473.7	482.0	490.3	498.6	506.9	515
	77	71.0	0.751	7.96	6.12	0.565	465.6	473.9	482.2	490.5	498.8	507.1	515
	76	69.5	0.715	7.57	6.51	0.537	465.8	474.1	482.4	490.7	499.0	507.3	515
	75	68.0	0.681	7.21	6.87	0.512	466.0	474.3	482.6	490.9	499.2	507.5	515
	74	66.5	0.648	6.87	7.21	0.488	466.2	474.5	482.8	491.1	499.4	507.7	516
	73	65.0	0.617	6.54	7.54	0.465	466.3	474.6	482.9	491.2	499.6	507.9	516
	72	63.5	0.588	6.22	7.86	0.442	466.5	474.8	483.1	491.4	499.8	508.1	516
	71	62.0	0.559	5.91	8.17	0.420	466.7	475.0	483.3	491.7	500.0	508.3	516
	70	60.5	0.532	5.62	8.46	0.399	466.8	475.1	483.4	491.8	500.1	508.4	516
	69	59.0	0.506	5 35	8.73	0.380	467.0	475.3	483.6	492.0	500.3	508.6	517
	68	57.5	0.481	5.08	9.00	0.361	467.1	475.4	483.7	492.1	500.4	508.7	517
	67	56.0	0.458	4.84	9.24	0.343	467.2	475.5	483.8	492.2	500.5	508.8	517
	66	54.5	0.435	4.61	9.47	0.327	467.4	475.7	483.9	492.4	500.7	509.1	517
	65	53.0	0.414	4.39	9.69	0.312	467.5	475.8	484.1	492.5	500.8	509.2	517
	64	51.5	0.393	4.17	9.91	0.296	467.6	475.9	484.2	492.6	500.9	509.3	517
	63	50.0	0.373	3.96	10.12	0.281	467.7	476.1	484.3	492.7	501.0	509.4	517
	62	48.5	0.355	3.76	10.32	0.267	467.8	476.2	484.4	492.8	501.1	509.5	517
90	90	90.0	1.368	14.50	0.00	1.000	461.3	469.5	477.8	486.0	494.3	502.5	510
	89	88.5	1.306	13.84	0.66	0.954	461.6	469.8	478.1	486.3	494.6	502.8	511
	88	87.0	1.247	13.22	1.28	0.910	462.0	470.2	478.5	486.7	495.0	503.2	511
	87	85.5	1.190	12.61	1.89	0.870	462.3	470.5	478.8	487.0	495.3	503.5	511
	86	84.0	1.136	12.03	2.47	0.830	462.7	470.9	479.2	487.4	495.7	503.9	512
	85	82.5	1.083	11.47	3.03	0.791	463.0	471.2	479.5	487.7	496.0	504.2	512
	84	81.0	1.034	10.94	3.56	0.755	463.2	471.5	479.8	488.0	496.3	504.5	512
	83	79.5	0.986	10.43	1	i e	463.4	471.7	480.0	488.2	496.5	504.7	513
	82	78.0	0.940	9.95		0.686	463.7	472.0	480.3	488.5	496.8	505.0	513
	81	76.5	0.896	9.48	5.02	1	464.0	472.3	480.6	488.8	497.1	505.3	513
	80	75.0	0.854	9.03	1	0.622	464.2	472.5	480.7	488.9	497.3	505.5	513
	79	73.5	0.814	8.61	5.89	0.594	464.3	472.6	480.9	489.1	497.5	505.7	514
	78	72.0	0.776	8.20		ŀ	464.5	472.8	481.1	489.3	497.7	505.9	514
	77	70.5	0.739	7.80	6.70	0.538	464.7	473.0	481.3	489.5	497.9	506.1	014

of	ading Ther-	Temp	Force of	We of V	ight apor Reqd.	Hu-		Weigh	t in Grai	ıs of a Cı	ıbic Foot	of Air.	
	meter, ahr.	of Dew- Point,	Vapor in	In a Cubic	for Sat'n.	midity, Satura- tion =		Height o	f the Bar	ometer i	n English	Inches.	
Dry.	Wet.	Fahr.	English Inches.	Foot of Air.	of aCu- bic Ft. of Air.	1.000.	28.0	in. 28.5	29.0	29.5	30.0	30.5	31.0
90	o 77	70.5	in. 0.739	gr. 7.80	gr. 6.70	0.538	gr. 464.7	gr. 473.0	gr. 481.3	gr. 489.5	gr. 497.9	gr. 506.1	gr. 514.5
	76	69.0	0.704	7.43	7.07	0.512	465.0	473.3	481.6	489.8	498.2	506.4	514.8
	75	67.5	0.670	7.08	7.42	0.488	465.2	473.5	481.8	490.0	498.4	506.6	515.0
	74	66.0	0.638	6.74	7.76	0.465	465.4	473.7	482.0	490.2	498.6	506.8	515.2
1	73	64.5	0.607	6.42	8.08	0.443	465.6	473.9	482.2	490.4	498.8	507.0	515.4
	72	63.0	0.578	6.10	8.40	0.421	465.7	474.0	482.3	490.5	498.9	507.1	515.5
	71	61.5	0.550	5.81	8.69	0.400	465.9	474.2	482.5	490.7	499.1	507.3	515.7
	70	60.0	0.523	5.52	8.98	0.381	466.1	474.4	482.8	491.0	499.3	507.5	515.9
	69	58.5	0.498	5.25	9.25	0.362	466.2	474.5	482.9	491.1	499.4	507.6	516.0
	68	57.0	0.473	4.99	9.51	0.344	466.4	474.7	483.1	491.3	499.6	507.8	516.2
I	67	55.5	0.450	4.74	9.76	0.327	466.5	474.8	483.2	491.4	499.7	507.9	516.3
	66	54.0	0.428	4.52	9.98	0.312	466.6	474.9	483.3	491.5	499.8	508.0	516.4
	65	52.5	0.407	4.30	10.20	0.297	466.7	475.0	483.4	491.6	499.9	508.1	516.5
li	64	51.0	0.386	4.09	10.41		466.9	475.2	483.6	491.8	500.1	508.3	516.6
-	63	49.5	0.367	3.90	10.60	0.269	467.0	475.3	483.7	491.9	500.2	508.4	516.7

TABLE XIII.

FACTORS FOR COMPUTING THE FORCE OF VAPOR, FROM THE READINGS OF THE PSYCHROMETER, BY APJOHN'S FORMULA.

Dr. Apjohn's formula for deducing the force of vapor, and the temperature of the dew-point, from the readings of the Psychrometer, as given in the Proceedings of the Royal Irish Academy for 1840, is

$$f'' = f' - \frac{d}{88} \times \frac{h}{30},$$

when the readings of the wet-bulb thermometer are above 32° Fahr., in which formula

f'' = the force of vapor at the temperature of the dew-point in degrees of Fahr.,

f' = the force of vapor at the temperature of evaporation given by the wet-bulb thermometer,

d = the difference between the readings of the dry and wet thermometers,

h = the height of the barometer in English inches at the time of the observation. When the readings of the wet-bulb thermometer are *below* 32° Fahr., and the bulb is covered with ice, the formula becomes

$$f'' = f' - \frac{d}{96} \times \frac{h}{30}$$

The factors in the following table, which is taken from the Greenwich Observations for 1843, represent $\frac{d}{88} \times \frac{1}{30}$ and $\frac{d}{96} \times \frac{1}{30}$, computed for all differences between the wet and dry bulb thermometers, or values of d, from 0° to 21° .

USE OF THE TABLE.

To find out the force of vapor in the air, and the temperature of the dew-point, by means of these factors, let the factor corresponding to d, or the difference between the wet and dry thermometer in the first column, be multiplied into the observed height of the barometer, and subtract the result from the force of vapor, in Table XI., due to the temperature of evaporation, indicated by the wet-bulb thermometer; the rest is the force of vapor in the air at the time of the observation; and the temperature of the dew-point is that which is due to it in Table XI.

EXAMPLE.

The observation gives,

Dry-bulb thermometer = 79° Fahr., or the temperature of the air.

Wet-bulb " $=69^{\circ}$ " or temperature of evaporation.

Difference 10³

Height of barometer 29.7 English inches.

In the Table, 2d part, is found,—factor for a difference of $10^{\circ} = 0.00379 \times 29.7$, or height of barometer = 0.113, which, subtracted from the force of vapor due to 69° , in Table XI., = 0.704 - 0.113, gives force of vapor in the air = 0.591 inches, and temperature of the dew-point $62^{\circ}.5$.

When the temperature of the wet bulb is below 32° Fahrenheit, the factors in the first part of the Table must be used.

В

XIII. FACTOR $\frac{d}{96} imes \frac{1}{30}$, for computing the force of vapor by apjohn's formula.

Below 32° Fahrenheit; the Wet Bulb covered with a Film of Ice.

d, or Difference					Tenths of	f Degrees.				
of Wet and Dry Bulb Therm.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	0.00000	0.00003	0.00007	0.00010	0.00014	0.00017	0.00020	0.00024	0.00027	[0.0003]
1	.00034	.00037	.00041			.00051	.00054	.00058		.0006
2	.00068	.00071	.00075	.00078	.00081	.00085	.00088	.00092	.00095	.0009
3	.00102	.00105	.00109	.00112	.00116	.00119	.00122	.00126	ŀ	.0013
4	.00136	.00139	.00143	.00146	.00150	.00153	.00156	.00160	l	.0016
5	.00170	.00173	.00177	.00180	.00184	.00187	.00190	.00194	.00198	.0020
6	.00204	.00207	.00211	.00214	.00218	.00221	.00224	.00228	.00231	.0023
7	.00238	.00241	.00245		.00252	.00255	.00258	.00262		.0026
8	.00272	.00275	.00279	.00282	.00285	.00289	.00292	.00296		.0030
9	.00306	.00309	.00313	.00316	.00319	.00323	.00326	.00330		.0033
10	.00340	.00343	.00347	.00350	.00354	.00357	.00360	.00364	.00367	.0037

FACTOR $\frac{d}{88} \times \frac{1}{30}$.

Reading of Wet-Bulb Thermometer above 32° Fahrenheit.

d, or Difference					Tenths o	f Degrees.				
of Wet and Dry Bulb Therm.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
 0	0.00000	0.00004	0.00008	0.00011	0.00015	0.00019	0.00023	0.00027	0.00030	0.00031
1	.00038	.00042	.00046	.00049	.00053	.00057	.00061	.00064	.00068	.00072
2	.00076	.00080	.00083	.00087	.00091	.00095	.00098	.00102	.00106	.00110
3	.00114	.00118	.00121	.00125	.00129	.00132	.00137	.00140	.00144	.00148
4	.00151	.00135	.00159	.00163	.00167	.00171	.00174	.00178	.00182	.00186
5	.00189	.00193	.00197	.00201	.00205	.00209	.00212	.00216	.00220	.00224
6	.00228	.00231	.00235	.00239	.00242	.00246	.00250	.00254	.00258	.00261
7	.00265	.00269	.00273	.00277	.00280	.00284	.00288	.00292	.00295	.00299
8	.00303	.00307	.00311	.00315	.00318	.00322	.00326	.00330	.00333	.00337
9	.00341	.00345	.00349	.00352	.00356	.00360	.00364	.00368	.00371	.00375
10	.00379	.00383	.00386	.00390	.00394	.00398	.00401	.00405	.00409	.00412
11	.00416	.00420	.00424	.00428	.00432	.00436	.00439	.00443	.00447	.00451
12	.00454	.00458	.00462	.00466	.00470	.00474	.00477	.00481	.00485	.00489
13	.00493	.00496	.00500	.00504	.00508	.00511	.00515	.00519	.00522	.00526
14	.00530	.00534	.00538	.00541	.00545	.00549	.00553	.00556	.00560	.00564
15	.00568	.00572	.00576	.00580	.00584	.00587	.00591	.00595	.00598	.00602
16	.00606	.00610	.00614	.00618	.00622	.00625	.00629	.00633	.00636	.00640
17	.00644	.00648	.00652	.00655	.00659	.00663	.00666	.00670	.00674	.00678
18	.00682	.00686	.00690	.00693	.00697	.00701	.00704	.00708	.00712	.00716
19	.00720	.00724	.00728	.00731	.00735	.00739	.00742	.00746	.00750	.00754
20	.00758	.00761	.00765	.00769	.00773	.00777	.00780	.00781	.00788	.00792

TABLE XIV.

In the Greenwich Magnetic and Meteorological Observations for 1842 and 1843, Mr. Glaisher discussed the relation between the temperature of evaporation given by the Wet-bulb Thermometer and the temperature of the Dew-Point as given by Daniell's Hygrometer. Comparing the observations taken simultaneously every six hours with the Psychrometer, and with Daniell's Dew-Point Hygrometer, and dividing the average difference between the temperatures of the Wet and Dry bulb by the average difference of the temperature of the Dew-Point and of the Air, he obtained the empirical factors given in the following Table.

The observations from which they are deduced are those taken at the Observatory in the years 1841 to 1845, for the temperatures below 35° F., and in the years 1841 to 1843, for the temperatures above 35° F.

The observations made at Toronto Observatory, Canada West, in similar circumstances, in the years 1840 to 1842, were also compared in the same manner, and the factors derived from them showed a very close accordance for temperatures above 30° F., but were found smaller at temperatures below 30° F.

The errors in the temperature of the Dew-Point, which may result by using the Greenwich factors, though frequently within half a degree, often amount, however, to \pm 2 or 3 degrees, and, in extreme cases, to \pm 4 or 5 degrees, as shown in the volume of the *Greenwich Observations* for 1842, p. 60 of the *Abstracts*.

Use of the Table.

Multiply the difference between the Wet-bulb and Dry-bulb Thermometers by the factor standing in the Table opposite the reading of the Dry-bulb, and subtract the product from the reading of the Dry-bulb; the remainder will be the temperature of the Dew-Point.

Example. — Dry-bulb = 62° F.; Wet-bulb = 55° ; Difference = 7° .

Opposite 62°, in the first column, stands the factor 1.7, which multiplied by 7°, the difference, gives 11°.9, to be subtracted from the Dry-bulb; or $62^{\circ} - 11^{\circ}.9 = 50^{\circ}.1$, temperature of the Dew-Point.

XIV. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.
	8.5	35°	2.6	49°	2.2	63°	1.7	77°	1.5
22	8.5	36	2.6	50	2.1	64	1.7	78	1.5
23	8.5	37	2.5	51	2.1	65	1.7	79	1.5
24	7.3	38	2.5	52	2.0	66	1.6	80	1.5
25	6.4	39	2.5	53	2.0	67	1.6	81	1.5
26	6.1	40	2.4	54	2.0	68	1.6	82	1.5
27	5.9	41	2.4	55	2.0	69	1.5	83	1.5
28	5.7	42	2.4	56	1.9	70	1.5	84	1.5
29	5.0	43	2.4	57	1.9	71	1.5	85	1.5
30	4.6	41	2.3	58	1.9	72	1.5	86	1.5
31	3.6	45	2.3	59	1.8	73	1.5	87	1.5
32	3.1	46	2.3	60	1.8	74	1.5	88	1.5
33	2.8	47	2.2	61	1.8	75	1.5	89	1.5
34	2.6	48	2.2	62	1.7	76	1.5	90	1.5

XV. WEIGHT OF VAPOR, IN GRAINS TROY, CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN 0° AND 94° FAHRENHEIT.

From the Greenwich Observations.

Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.	Temper- ature of Air, Fahren.	Weight of Vapor, in Grains.
	0.78	19°	1.52	38°	2.89	57°	5.34	76°	9.60
1	0.81	20	1.58	39	2.99	58	5.51	77	9.89
2	0.84	21	1.63	40	3.09	59	5.69	78	10.19
3	0.87	22	1.69	41	3.19	60	5.87	79	10.50
4	0.90	23	1.75	42	3.30	61	6.06	80	10.81
5	0.93	24	1.81	43	3.41	62	6.25	81	11.14
6	0.97	25	1.87	44	3.52	63	6.45	82	11.47
7	1.00	26	1.93	45	3.64	64	6.65	83	11.82
. 8	1.04	27	2.00	46	3.76	65	6.87	84	12.17
9	1.07	28	2.07	47	3.88	66	7.08	85	12.53
10	1.11	29	2.14	48	4.01	67	7.30	86	12.91
11	1.15	30	2.21	49	4.14	68	7.53	87	13.29
12	1.19	31	2.29	50	4.28	69	7.76	88	13.68
13	1.24	32	2.37	51	4.42	70	8.00	89	14.08
14	1.28	33	2.45	52	4.56	71	8.25	90	14.50
15	1.32	34	2.53	53	4.71	72	8.50	91	14.91
16	1.37	35	2.62	54	4.86	73	8.76	92	15.33
17	1.41	36	2.71	55	5.02	74	9.04	93	15.76
18	1.47	37	2.80	56	5.18	75	9.31	94	16.22

XVI. FACTORS TO DEDUCE THE WEIGHT OF VAPOR CONTAINED IN A CUBIC FOOT OF AIR, AT THE TIME OF A GIVEN OBSERVATION, FROM THE INDICATIONS OF DEW-POINT INSTRUMENTS. — GREENW. Obs.

 $\mathbf{t} = \text{Temperature of Air}; \ \mathbf{t}'' = \text{Temperature of Dew-Point}.$

Difference or $\mathbf{t} - \mathbf{t}^{r}$.	Factors.	Difference or $\mathbf{t} - \mathbf{t}^{\mu}$.	Factors.	Difference or t — t".	Factors.	Difference or t — t".	Factors.	Difference or t—t".	Factors.
1	0.999	9	0.982	17	0.966	25	0.951	33	0.935
2	0.996	10	0.980	18	0.964	26	0.949	34	0.934
3	0.994	11	0.978	19	0.962	27	0.947	35	0.932
4	0.992	12	0.976	20	0.960	28	0.945	36	0.930
5	0.990	13	0.974	21	0.958	29	0.943	37	0.929
6	0.988	14	0.972	22	0.956	30	0.942	38	0.927
7	0.986	15	0.970	23	0.954	31	0.939	39	0.925
8	0.984	16	0.968	24	0.952	32	0.937	40	0.923

Use of Table XVI. — The difference between the temperatures of the air and of the Dew-Point being known, multiply the factor in the Table corresponding to that difference into the weight of a cubic foot of vapor at the temperature of the Dew-Point, as given in Table XV., and the product will be the weight of vapor in a cubic foot of air at the time of the observation.

Example. — Temperature of air = 60° F.; Dew-Point = 52° ; Diff. = 8° .

Table gives for a difference of 8°, factor 0.984; Table XV. gives weight of a cubic foot of vapor at temperature $52^{\circ} = 4.5^{\circ}.56$.

Hence, $0.984 \times 4.56 = 4^{gr}.49$, the weight of vapor required.

TABLE XVII.

FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR.

This table is composed of two tables found in the Greenwich Meteorological Observations for 1842, pages xlvi. and li.; the first containing the weight of a cubic foot of dry air, under a barometric pressure of 30 inches, at temperatures between 0° and 90° F.; the other giving the weight of a cubic foot of saturated air under the same barometric pressure and temperature, together with the excess of the first above the last.

The weight of a cubic foot of dry air, on which the tables are based, is assumed to be 563 grains Troy, being a mean value, in round numbers, between the determinations of Shuckburgh, which is 557.7295 grains, and that of Biot and Arago, 568.7013. The true mean is 563.2154, but 563 is the number used in the calculations.

The coefficient of the expansion of the air is that of Gay-Lussac, viz. 0.00375 for 1° Centigrade, or 0.002083 of its bulk for 1° Fahrenheit.

Use of the Table.

This table shows the amount of buoyancy imparted to the air by the addition of moisture; and from it, the temperature and the relative humidity of the air being known, the weight of a cubic foot of air, in the actual condition of the atmosphere at the time of an observation, can be deduced.

It suffices to take in the fourth column, headed "Excess," the quantity corresponding to the temperature of the air in the first, multiply it into the given Relative Humidity, and subtract the product from the number in the second column. The result will be the weight of a cubic foot of air at the existing temperature and moisture, under a barometric pressure of 30 inches.

This result will be reduced to its true value, under the barometric pressure given by the observation, by multiplying it by $\frac{\text{Height of Barometer}}{30}$.

Example.

The temperature of the air is 60° F.; the relative humidity, 0.852; the barometer reads 29 inches.

The table gives, for temperature of air, 60° ; excess, $3.35 \times 0.852 = 2.85$, which, subtracted from 531.91 in the second column, = 529.12, weight of a cubic foot of air under 30 inches of pressure; and $529.12 \times \frac{29 \text{ inch}}{30} = 511.48$, the weight of a cubic foot of air in the given conditions of temperature, moisture, and barometric pressure.

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В

XVII. FOR COMPARING THE WEIGHT OF A CUBIC FOOT OF DRY AND OF SATURATED AIR,

AT TEMPERATURES BETWEEN 0° AND 90° FAHRENHEIT.

From the Greenwich Observations.

			1	1							
Temper- ature Fahren.	foot of	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.	Temper- ature Fahren.	Weight of a cubic foot of Dry Air.	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.	Temper- ature Fahren.	Weight of a cubic foot of Dry Air	Weight of a cubic foot of Saturat- ed Air.	Excess of Dry Air.
		0-1	Grains				Grains.		Cuoles	Gi.	
0	Grains.	Grains.		0	Grains.	Grains.		0	Grains.	Grains.	Grains.
0	603.21	602.77	0.44	30	565.35	564.08	1.27	60	531.97	528.62	3.35
1	601.87	601.40	0.47	31	564.17	562.86	1.31	61	530.93	527.48	3.45
2	609.52	600.03	0.49	32	563.00	561.64	1.36	62	529.88	526.32	3.56
3	599.20	598.69	0.51	33	561.84	560.42	1.42	63	528.84	525.17	3.67
4	597.87	597.34	0.53	34	560.67	559.20	1.47	64	527.81	524.03	3.78
_		****	0.54	0.5		~ ~ 0 0 0 0		0.2	¥20.00	500.00	0.00
5	596.55	596.01	0.54	35	559.51	558.01	1.50	65	526.88	522.90	3.88
6	595.24	594.69	0.55	36	558.35	556.79	1.56	66	525.76	521.75	4.01
7	593.94	593.36	0.58	37	557.21	555.61	1.60	67	524.75	520.61	4.14
8	592.63	592.04	0.59	38 .	556.05	554.40	1.65	68	523.72	519.46	4.26
9	591.33	590.72	0.61	39	554.91	553.20	1.71	69	522.70	518.29	4.41
10	500.04	F00 40	001	40				-0	~01 ~0	512 12	4.50
10	590.04	589.40	0.64	40	553.77	552.00	1.77	70	521.70	517.17	4.53
11	538.75	588.07	0.68	41	552.65	550.80	1.84	71	520.70	516.02	4.68
12	587.48	586.78	0.70	42	551.52	549.63	1.89	72	519.69	514.87	4.82
13	586.21	585.49	0.72	43	550.39	548.44	1.95	73	518.70	513.75	4.95
14	584.94	584.18	0.75	44	549.27	547.26	2.01	74	517.70	512.61	5.09
15	509 C*	F00 00	0.40	45	540.30	7 10 00	0.10		510 51	511 16	5 05
15	583.67	582.89	0.78 0.80	45	548.16	546.06	2.10	75	516.71	511.46	5.25
16	582.41	581.61	0.82	46	547.05	544.88	2.17	76	515.73	510.32	5.41 5.56
17	581.15	580.33	ł 1	47	545.97	543.75	2.22	77	514.74	509.18	
18	579.91	579.06	0.85	48	544.85	542.55	2.30	78	513.77	508.04	5.73
19	578.67	577.79	0.88	49	543.75	541.36	2.39	79	512.80	506.91	5.89
20	577.44	576.54	0.90	50	542.65	540.21	2.44	80	511.82	505.74	6.08
21	576.21	575.27	0.94	51	541.55	539.04	2.51	81	510.87	504.61	6.26
22	574.98	574.01	0.97	52	540.48	537.87	2.61	82	509.89	503.45	6.44
23	573.76	572.76	1.00	53	539.41	536.71	2.70	83	508.93	502.32	6.61
24	572.55	571.50	1.05	54	538.33	535.55	2.78	84	507.97	501.16	6.81
-1	5.2.00	0.1.00	1.00	04	300.00	200.00		J-1	301101	201.10	0.01
25	571.33	570.26	1.07	55	537.27	534.39	2.88	85	507.03	500.05	6.98
26	570.13	569.01	1.12	56	536.19	533.22	2.97	86	506.07	498.87	7.20
27	568.92	567.77	1.15	57	535.12	532.06	3.06	87	505.11	497.71	7.40
28	567.73	566.53	1.20	58	534.07	530.92	3.15	88	504.19	496.58	7.61
29	566.54	565.31	1.23	59	533.03	529.77	3.26	89	503.25	495.44	7.81
30	565.35	564.08	1.27	60	531.97	528.62	3.35	90	502.32	494.28	8.04
				"							
	•	1		1				·			

TABLE XIV'.

Mr. Glaisher published in London, in 1856, another series of Hygrometrical Tables, which were unknown to the writer when the Second Edition of this volume was issued. They are based on Regnault's Table of Elastic Forces of Vapor, and on the coefficient of the expansion of the air as determined by the same physicist. Psychrometrical Table, however, is not computed from Regnault's formula, but by first finding out, in the manner described on page 140, the temperatures of the dewpoint from the readings of the Psychrometer, by means of the empirical factors given below, in Table XIV', and then taking the corresponding values of the force of vapor from Regnault's table. These factors have been derived from the combination of all simultaneous observations of the dry and wet bulb thermometers with those of Daniell's hygrometer, taken at the Royal Observatory, Greenwich, from the year 1841 to 1854, with some observations taken at high temperatures in India, and others at low and medium temperatures at Toronto; they are, therefore, more correct than those given in Table XIV. page 140. The results in this new Psychrometrical Table, nevertheless, by no means entirely coincide with those given by the formula, as a comparison with those in Table VII. will show.

XIV'. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. — GLAISHER.

0.70			Fahren.	Factors.	Therm. Fabren.	Factors.	Dry-Bulb Therm. Fahren.	Factors.
	0		0	2.14	0	7.00	0	
8.78	28	5.12	46	2.14	64	1.83	82	1.67
			1		1		11	1.67
								1.66
			11 .					1.65
8.76	32	3.32	50	2.06	68	1.79	86	1.65
					-			
			11				1	1.64
								1.64
8.62	1		53		71	1.76	11 1	1.63
8.50	36	2.50	54	1.98	72	1.75	90	1.63
8.34	37	2.42	55	1.96	73	1.74	91	1.62
8.14	38	2.36	56	1.94	74	1.73	92	1.62
7.88	39	2.32	57	1.92	75	1.72	93	1.61
7.60	40	2.29	58	1.90	76	1.71	94	1.60
7.28	41	2.26	59	1.89	77	1.70	95	1.60
6.92	42	2.23	60	1.88	78	1.69	96	1.59
					İ			
6.53	43	2.20	61	1.87	79	1.69	97	1.59
6.08	44	2.18	62	1.86	80	1.68	98	1.58
5.61	45	2.16	63	1.85	81	1.68	99	1.58
5.12	46	2.14	64	1.83	82	1.67	100	1.57
	8.34 8.14 7.88 7.60 7.28 6.92 6.53 6.08 5.61	8.78 30 8.77 31 8.76 32 8.75 33 8.70 34 8.62 35 8.50 36 8.34 37 8.14 38 7.88 39 7.60 40 7.28 41 6.92 42 6.53 43 6.08 44 5.61 45	8.78 30 4.15 8.77 31 3.70 8.76 32 3.32 8.75 33 3.01 8.70 34 2.77 8.62 35 2.60 8.50 36 2.50 8.34 37 2.42 8.14 38 2.36 7.88 39 2.32 7.60 40 2.29 7.28 41 2.26 6.92 42 2.23 6.53 43 2.20 6.08 44 2.18 5.61 45 2.16	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$



FOR

COMPARING THE HYGROMETRICAL RESULTS OBTAINED BY DIFFERENT AUTHORITIES.

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MISCELLANEOUS TABLES.

The object of these Tables is to afford the means of comparing the different determinations of the hygrometrical elements which have been obtained, or adopted, by various physicists, especially the values of the elastic forces of vapor given in other tables than those contained in the preceding pages.

Table XVIII., giving the elastic forces of vapor, expressed in millimetres of mercury, for Centigrade temperatures, was calculated by August from Dalton's experiments, and reduced to French measures in the translation of Kaemtz's *Meteorology*, by Chas. Martins, page 70, from which it has been taken. On these values are based the first psychrometrical tables published by August, in Berlin, 1825.

Table XIX. is the table computed by Kaemtz from his own experiments. It is found, reduced to French measures, in the same volume, page 68.

Table XX. furnishes the results of the experiments made by Professor Magnus, in Berlin, and published in Poggendorf's *Annalen*, Tom. LXI. p. 226, and also in the *Annales de Chimie et de Physique*, 3^{me} série, Tom. XII. p. 88, from which this table was copied.

Table XXI. has been published by the Committee of Physics and Meteorology of the Royal Society, in their Report on the Objects of Scientific Inquiry in these Sciences, London, 1840, p. 89. The values which it contains are not derived from new experiments, but are probably computed from those existing at that time.

Table XXII. furnishes a synoptic view of the differences in the values of the force of vapor adopted by various authorities, prepared with the view of facilitating their comparison. A reference to their respective origin will be found below, page 152.

Table XXIII., showing the weight, in grammes, of the vapor contained in a cubic metre of saturated air, at different temperatures, is taken from Pouillet's *Eléments de Physique*, Tom. II. p. 707.

Table XXIV. gives the weights as derived from August's experiments, in Kaemtz's Vorlesungen über Meteorologie. The table is copied from the French translation, by Martins, page 73. The tensions have been added, opposite the weights, and are extracted from August's table.

Table XXV. is found in Biot's Traité de Physique, Tom. I. p. 533.

XVIII. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR EVERY TENTH OF A CENTIGRADE DEGREE.

CALCULATED BY AUGUST.

Centigrade					Tenths of	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
-31	0.45	0.45	0.45	0.44	0.44	0.43	0.43	0.42	0.42	0.41
-30	0.50	0.49	0.49	0.48	0.48	0.47	0.47	0.46	0.46	0.45
-29	0.54	0.54	0.54	0.53	0.53	0.52	0.52	0.51	0.51	0.50
-28	0.59	0.58	0.58	0.57	0.57	0.56	0.56	0.55	0.55	0.54
-27	0.63	0.63	0.63	0.62	0.62	0.61	0.61	0.60	0.60	0.59
-26	0.70	0.69	0.68	0.68	0.67	0.66	0.66	0.65	0.64	0.64
-25	0.77	0.76	0.75	0.75	0.74	0.73	0.73	0.72	0.71	0.71
-24	0.83	0.83	0.82	0.82	0.81	0.80	0.80	0.79	0.78	0.78
-23	0.90	0.89	0.88	0.88	0.87	0.86	0.86	0.85	0.84	0.84
-22	0.99	0.98	0.97	0.96	0.95	0.95	0.94	0.93	0.92	0.91
-21	1.06	1.05	1.04	1.04	1.03	1.02	1.02	1.01	1.00	1.00
-20	1.15	1.14	1.13	1.12	1.11	1.11	1.10	1.09	1.08	1.07
-19	1.26	1.25	1.24	1.23	1.22	1.21	1.20	1.18	1.17	1.16
-18	1.33	1.32	1.31	1.31	1.30	1.29	1.29	1.28	1.27	1.27
-17	1.44	1.43	1.42	1.41	1.40	1.39	1.38	1.36	1.35	1.34
-16	1.56	1.54	1.53	1.52	1.51	1.50	1.49	1.47	1.46	1.45
-16 -15	1.69	1.68	1.67	1.65	1.64	1.63	1.61	1.60	1.59	1.57
-15 -14	1.80	1.79	1.78	1.77	1.76	1.75	1.74	1.72	1.71	1.70
-14 -13	1.96	1.73	1.93	1.91	1.59	1.88	1.86	1.85	1.83	1.82
-13 -12	2.12	2.10	2.09	2.07	2.05	2.04	2.02	2.01	1.99	1.98
-12	۵.۱.۵	2.10	2.03	2.01	2.00	2.01			2.00	
-11	2.30	2.28	2.26	2.25	2.23	2.21	2.19	2.17	2.16	2.1
-10	2.48	2.46	2.44	2.43	2.41	2.39	2.37	2.35	2.34	2.32
- 9	2.66	2.64	2.62	2.61	2.59	2.57	2.55	2.53	2.52	2.50
- 8	2.86	2.84	2.82	2.80	2.78	2.76	2.74	2.72	2.70	2.68
- 7	3.09	3.06	3.04	3.02	3.00	2.97	2.95	2.93	2.91	2.88
- 6	3.32	3.29	3.27	3.25	3.23	3.20	3.18	3.16	3.14	3.1
- 5	3.56	3.56	3.54	3.51	3.48	3.46	3.43	3.40	3.37	3.3
- 4	3.83	3.80	3.78	3.75	3.72	3.70	3.67	3.64	3.61	3.59
- 3	4.11	4.07	4.05	4.02	3.99	3.97	3.94	3.91	3.88	3.80
- 2	4.40	4.37	4.34	4.32	4.29	4.26	4.23	4.20	4.17	4.1
- 1	4.71	4.68	4.65	4.62	4.59	4.56	4.53	4.49	4.46	4.43
– 0	5.05	*5.01	4.98	4.95	4.91	4.88	4.85	4.81	4.78	4.7
+ 0	5.05	5.09	5.12	5.16	5.19	5.23	5.27	5.30	5.34	5.3
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade					Tenths of	Degrees.				
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millm
° 1	5.41	5.45	5.49	5.52	5.56	5.60	5.64	5.68	5.72	5.75
2	5.80	5.84	5.88	5.92	5.96	6.00	6.04	6.08	6.13	6.17
3	6.20	6.24	6.29	6.33	6.37	6.41	6.46	6.50	6.54	6.59
4	6.63	6.68	6.72	6.77	6.81	6.86	6.90	6.95	6.99	7.04
5	7.08	7.13	7.18	7.23	7.28	7.33	7. 38	7.43	7.48	7.58
6	7.58	7.63	7.68	7.74	7.79	7.84	7.89	7.94	7.99	8.03
7	8.10	8.15	8.21	8.26	8.32	8.37	8.43	8.48	8.53	8.59
8	8.64	8.70	8.76	8.82	8.87	8.93	8.99	9.05	9.11	9.17
9	9.23	9.30	9.36	9.43	9.50	9.57	9.63	9.70	9.77	9.84
10	9.90	9.96	10.02	10.08	10.14	10.20	10.25	10.31	10.37	10.43
11	10.49	10.56	10.63	10.69	10.76	10.83	10.90	10.96	11.03	11.10
12	11.17	11.24	11.31	11.38	11.45	11.52	11.59	11.66	11.73	11.80
13	11.86	11.94	12.02	12.10	12.18	12.26	12.34	12.42	12.50	12.58
14	12.66	12.74	12.82	12.90	12.98	13.05	13.13	13.21	13.29	13.37
15	13.44	13.52	13.61	13.69	13.77	13.86	13.94	14.02	14.11	14.19
16	14.28	14.37	14.47	14.56	14.65	14.74	14.84	14.93	15.02	15.11
17	15.20	15.29	15.38	15.46	15.55	15.64	15.73	15.82	15.90	15.99
18	16.08	16.17	16.27	16.36	16.45	16.54	16.64	16.73	16.82	16.91
19	17.01	17.13	17.25	17.37	17.49	17.61	17.73	17.85	17.97	18.09
20	18.20	18.31	18.43	18.54	18.65	18.76	18.88	18.99	19.10	19.21
21	19.33	19.45	19.56	19.68	19.80	19.92	20.03	20.15	20.27	20.39
22	20.51	20.63	20.76	20.88	21.01	21.13	21.25	21.38	21.50	21.68
23	21.75	21.88	22.00	22.13	22.26	22.38	22.51	22.63	22.76	22.89
24	23.01	23.13	23.24	23.36	23.48	23.60	23.71	23.83	23.95	24.07
25	24.18	24.34	24.50	24.67	24.83	24.99	25.15	25.32	25.48	25.6
26	25.81	25.97	26.13	26.28	26.44	26.60	26.76	26.92	27.07	27.23
27	27.39	27.55	27.71	27.86	28.02	28.18	28.34	28.50	28.65	28.81
28	28.96	29.13	29.29	29.46	29.63	29.79	29.96	30.13	30.30	30.46
29	30.63	30.81	30.98	31.16	31.33	31.51	31.69	31.86	32.01	32.21
30	32.39	32.57	32.76	32.94	33.13	33.31	33.50	33.68	33.87	34.05
31	34.24	34.43	34.63	34.82	35.02	35.21	35.40	35.60	35.79	35.99
32	36.18	36.38	36.59	36.79	36.99	37.20	37.40	37.60	37.80	38.01
33	38.21	38.43	38.64	38.86	39.08	39.29	39.51	39.73	39.94	40.16
34	40.38	40.60	40.82	41.04	41.26	41.49	41.71	41.93	42.15	42.37
35	42.59	42.82	43.05	43.28	43.51	43.74	43.97	41.20	44.43	44.66
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

XIX. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

BY KAEMTZ.

Temper- ature Centi- Grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor,
	Millim.		Millim.	0	Millim.	0	Millim.	0	Millim.
-25	0.68	-12	1.92	0	4.58	12	10.24	24	21.43
-24	0.72	-11	2.05	1	4.92	13	10.91	25	22.74
-23	0.79	-10	2.21	2	5.26	14	11.62	26	24.16
-22	0.86	- 9	2.39	3	5.64	15	12.38	27	25.56
-21	0.92	- 8	2.57	4	6.01	16	13.17	28	27.07
-20	1.01	- 7	2.78	5	6.45	17	14.03	29	28.67
-19	1.10	- 6	2.98	6	6.90	18	14.93	30	30.36
-18	1.20	- 5	3.20	7	7.38	19	15.86	31	32.17
-17	1.29	- 4	3.45	8	7.89	20	16.87	32	33.95
-16	1.40	- 3	3.70	9	8.41	21	17.91	33	35.95
-15	1.51	- 2	3.97	10	9.00	22	19.04	34	37.99
-14	1.62	- 1	4.26	11	9.58	23	20.21	35	40.15
-13	1.76	0	4.58	12	10.24	24	21.43	36	42.40

XX. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY, FOR CENTIGRADE TEMPERATURES.

BY MAGNUS.

Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.	Temper- ature Centi- grade	Force of Vapor.	Temper- ature Centi- grade.	Force of Vapor.
0	Millim.	0	Millim.	0	Millim.	0	Millim.	0	Millim.
-20	0.916	-7	2.671	6	6.939	19	16.345	32	35.419
-19	0.999	-6	2.886	7	7.436	20	17.396	33	37.473
-18	1.089	-5	3.115	8	7.964	21	18.505	34	39.630
-17	1.186	-4	3.361	9	8.525	22	19.675	35	41.893
-16	1.290	-3	3.624	10	9.126	23	20.909	36	44.268
-15	1.403	-2	3.905	11	9.751	24	22.211	37	46.758
-14	1.525	-1	4.205	12	10.421	25	23.582	38	49.368
-13	1.655	0	4.525	13	11.130	26	25.026	39	52.103
-12	1.796	+1	4.867	14	11.882	27	26.547	40	54.964
-11	1.947	2	5.231	15	12.677	28	28.148	41	57.969
-10	2.109	3	5.619	16	13.519	29	29.832	42	61.109
- 9	2.284	4	6.032	17	14.409	30	31.602	43	64.396
- 8	2.471	5	6.471	18	15.351	31	33.464	44	67.833

XXI. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY, FOR TEMPERATURES OF FAHRENHEIT.

From the Royal Society's Report.

Temperature of	Force of	Temperature of	Force of	Temperature of	Force of	Temperature of	Force of
Air.	Vapor.	Air.	Vapor.	Air.	Vapor.	Air.	Vapor.
Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng Inches.	Fahrenheit.	Eng. Inches.	Fahrenheit.	Eng. Inches
0°	0.051	31°	0.179	62°	0.551	93°	1.514
1	0.053	32	0.186	63	0.570	94	1.562
2	0.056	33	0.193	64	0.590	95	1 610
3	0.058	34	0.200	65	0.611	96	1.660
4	0.060	35	0.208	66	0.632	97	1.712
5	0.063	36	0.216	37	0.654	98	1.764
6	0.066	37	0.224	68	0.676	99	1.819
7	0.069	38	0.233	69	0.699	100	1.874
8	0.071	39	0.242	70	0.723	101	1.931
9	0.074	40	0.251	71	0.748	102	1.990
10	0.078	41	0.260	72	0.773	103	2.050
11	0.081	42	0.270	73	0.799	104	2.112
12	0.084	43	0.280	74	0.826	105	2.176
13	0.088	44	0.291	75	0.854	106	2.241
14	0.092	45	0.302	76	0.882	107	2.307
15	0.095	46	0.313	77	0.911	108	2.376
16	0.099	47	0.324	78	0.942	109	2.447
17	0.103	48	0.336	79	0.973	110	2.519
18	0.107	49	0.349	80	1.005	111	2.593
19	0.112	50	0.361	81	1.036	112	2.669
20	0.116	51	0.375	82	1.072	113	2.747
21	0.121	52	0.389	83	1.106	114	2.826
22	0.126	53	0.402	84	1.142	115	2.908
23	0.131	54	0.417	85	1.179	116	2.992
24	0.136	55	0.432	86	1.217	117	3.078
25	0.142	56	0.447	87	1.256	118	3.166
26	0.147	57	0.463	88	1.296	119	3.257
27	0.153	58	0.480	89	1.337	120	3.349
28	0.159	59	0.497	90	1.380	121	3.444
29	0.165	60	0.514	91	1.423	122	3.542
30	0.172	61	0.532	92	1.468	123	3.641
31	0.179	62	0.551	93	1.514	124	3.743

TABLE XXII.

FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR ADOPTED BY DIFFERENT AUTHORITIES.

The following synoptic view of the values of the elastic force of vapor adopted by various authorities, furnishes the means of readily comparing them, and of appreciating the amount of the differences which they exhibit. The values are given both in English and in French measures.

Dalton's values are copied from the Edinburgh Encyclopædia, Art. Hygrometry. Those adopted in the Greenwich Observations are found in the same article, and also in the volumes published annually by that Observatory. Biot's table of tensions is, in fact, the same, computed by Pouillet from Dalton's results, by Biot's formula, and published in Biot's Traité de Physique, Tom. I. p. 531. Dr. Ure's results are taken from his Memoir in the Philosophical Transactions for 1818, p. 347. In the column headed "Daniell" are given the forces of vapor as found in the table published in his Meteorological Essays, 2d edition, p. 596, a table computed by Galbraith, from Dr. Ure's experiments, by the formula of Ivory.

For the columns headed Royal Society, August, Kaemtz, Magnus, and Regnault, see above, p. 147.

XXII. FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTIC FORCE OF AQUEOUS VAPOR, ADOPTED BY DIFFERENT AUTHORITIES.

FORCE OF VAPOR EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES $\hspace{1.5cm} \text{OF FAHRENHEIT.}$

Temper-				Force of	Vapor acc	ording to				Temper
ature of Air, Fahren- heit.	Dalton.	Green- wich Observa- tions.	Ure.	Daniell.	Royal Society.	August.	Kaemtz.	Magnus.	Regnault.	ature of Air, Fahren heit.
0	Eng. ln.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	0
0	0.064	0.061		0.068	0.051	0.053	0.048	0.044	0.043	0
10	0.090	0.089		0.098	0.078	0.082	0.074	0.070	0.068	10
20	0.129	0.129		0.140	0.116	0.124	0.112	0.108	0.108	20
30	0.186	0.186		0.200	0.172	0.184	0.166	0.164	0.167	30
32	0.200	0.199	0.200	0.216	0.186	0.199	0.180	0.178	0.181	32
40	0.263	0.264	0.250	0.280	0.251	0.269	0.244	0.245	0.248	40
50	0.375	0.373	0.360	0.400	0.361	0.390	0.354	0.359	0.361	50
60	0.524	0.523	0.516	0.560	0.516	0.547	0.505	0.517	0.518	60
70	0.721	0.727	0.726	0.770	0.723	0.766	0.710	0.733	0.733	70
80	1.000	1.001	1.010	1.060	1.005	1.058	0.988	1.025	1.023	80
90	1.360	1.368	1.360	1.430	1.380	1.412	1.354	1.412	1.410	90
95	1.580	1.594	1.640	1.636	1.562	1.677	1.581	1.649	1.647	95
100	1.860	1.852	1.860		1.874			1.921	1.918	100

FORCE OF VAPOR EXPRESSED IN MILLIMETRES FOR CENTIGRADE TEMPERATURES.

Temper-				Force of	Vapor acc	ording to				Temper
ature of Air, Centi- grade.	Dalton.	Green- wich Observa- tions.	Biot.	Daniell.	Royal Society.	August.	Kaemtz.	Magnus.	Regnault.	ature of Air, Centi- grade.
	Millim.	Millim.	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	-
-20			1.33			1.15	1.01	0.91	0.91	-20
-15	1.93	1.88	1.88	2.11	1.60	1.69	1.51	1.40	1.38	-15
-10	2.64	2.62	2.63	2.92	2.34	2.48	2.21	2.11	2.08	-10
- 5	3.66	3.66	3.66	4.01	3.33	3.56	3.20	3.11	3.13	- 5
0	5.08	5.06	5.06	5.49	4.72	5.05	4.58	4.52	4.60	0
+ 5	6.93	6.95	6.95	7.42	6.60	7.08	6.45	6.47	6.53	+ 5
10	9.52	9.48	9.47	10.16	9.17	9.90	9.00	9.13	9.16	10
15	12.88	12.85	12.84	13.79	12.62	13.44	12.38	12.68	12.70	15
20	17.17	17.30	17.31	18.34	17.17	18.20	16.87	17.40	17.39	20
25	23.11	23.12	23.09	24.51	23.14	24.18	22.74	23.58	23.55	25
30	30.73	30.70	30.64	32.33	30.91	32.39	30.36	31.60	31.55	30
35	40.13	40.47	40.40	41.55	40.89	42.59	40.15	41.89	41.83	35
40	10.10	10.11	53.00		53.64	42.93	40.13	54.96	54.91	40

XXIII. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN -20° and $+40^{\circ}$ centigrade. - poullet.

Temper- ature of Dew-Point	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor,	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	Millim	Grammes.
-20°	1.3	1.5	11°	10.1	10.3	26°	24.4	23.8
-15	1.9	2.1	12	10.7	10.9	27	25.9	25.1
-10	2.6	2.9	13	11.4	11.6	28	27.4	26.4
- 5	3.7	4.0	14	12.1	12.2	29	29.0	27.9
0	5.0	5.4	15	12.8	13.0	30	30.6	29.4
+ 1	5.4	5.7	16	13.6	13.7	31	32.4	31.0
2	5.7	6.1	17	14.5	14.5	32	34.3	32.6
3	6.1	6.5	18	15.4	15.3	33	36.2	34.3
4	6.5	6.9	19	16.3	16.2	34	38.3	36.2
5	6.9	7.3	20	17.3	17.1	35	40.4	38.1
6	7.4	7.7	21	18.3	18.1	36	42.7	40.2
7	7.9	8.2	22	19.4	19.1	37	45.0	42.2
8	8.4	8.7	23	20.6	20.2	38	47.6	44.4
9	8.9	9.2	24	21.8	21.3	39	50.1	46.7
10	9.5	9.7	25	23.1	22.5	40	53.0	49.2

XXIV. WEIGHT OF VAPOR, IN GRAMMES, CONTAINED IN A CUBIC METRE OF SATURATED AIR, AT TEMPERATURES BETWEEN -25° AND $+36^\circ$ CENTIGR. - KAEMTZ.

Temper- ature of Dew-Point.	Force of Vapor,	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.	Temper- ature of Dew-Point.	Force of Vapor.	Weight of Vapor.
Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.	Centigrade.	Millim.	Grammes.
-25°	0.77	0.93	-4°	3.83	4.37	16°	14.28	14.97
-24	0.83	1.01	-3	4.11	4.70	17	15.20	15.84
-23	0.90	1.10	-2	4.40	5.01	18	16.08	16.76
-22	0.99	1.19	-1	4.71	5.32	19	17.01	17.75
-21	1.06	1.26	0	5.05	5.66	20	18.20	18.77
					j	İ		
-20	1.15	1.38	+1	5.41	6.00	21	19.33	19.82
-19	1.26	1.47	2	5.80	6.42	22	20.51	20.91
-18	1.33	1.60	3	6.20	6.84	23	21.75	22.09
-17	1.44	1.74	4	6.63	7.32	24	23.01	23.36
-16	1.56	1.84	5	7.08	7.77	25	24.18	24.61
-15	1.69	2.00	6	7.58	8.25	26	25.81	25.96
-14	1.80	2.14	7	8.10	8.79	26	27.39	27.34
-13	1.96	2.33	8	8.64	9.30	28	28.96	28.81
-12	2.12	2.48	9	9.23	9.86	29	30.63	30.35
-11	2.30	2.63	10	9.90	10.57	30	32.39	31.93
-10	2.48	2.87	11	10.49	11.18	31	34.24	33.65
- 9	2.66	3.08	12	11.17	11.53	32	36.18	35.45
- 8	2.86	3.30	13	11.86	12.57	33	38.21	37.20
- 7	3.09	3.53	14	12.66	13.33	34	40.38	39.12
- 6	3.32	3.80	15	13.44	14.17	35	42.59	41.13
- 5	3.56	4.08	16	14.28	14.97	36	44.96	43.17

XXV. FORCES OF VAPOR AND RELATIVE HUMIDITY,

corresponding to the degrees of saussure's hair-hygrometer, at the temperature of 10° centigrade.

From the Experiments of Gay-Lussac.

The force of vapor is expressed in hundredths, the tension at full saturation being represented by 100.

Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of II ir-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths.	Degrees of Hair-Hy- grometer.	Force of Vapor.	Relative Humidity in Thou- sandths
	0.00	0.000	0	17.10		0	49.79	
$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$	0.00	0.000	34	17.10	0.177	67 68	43.73 44.89	}
2	0.45		35 36	18.30	0.177	69	46.04	
3	1.35		37	18.92		70	47.19	0.172
4	1.80		38	19.54		71	48.51	0.172
5	2.25	0.022	39	20.16		72	49.82	0.500
6	2.71	0	40	20.78	0.208	73	51.14	
7	3.18		41	21.45		74	52.45	
8	3.64		42	22.12		75	53.76	0.538
9	4.10		43	22.79		76	55.25	
10	4.57	0.046	44	23.46		77	56.74	
11	5.05		45	24.13	0.241	78	58.24	
12	5.52		46	24.86		79	59.73	
13	6.00		47	25.59		80	61.22	0.612
14	6.48		48	26.32		81	62.89	
15	6.96	0.070	49	27.06		82	64.57	
16	7.46		50	27.79	0.278	83	66.24	
17	7.95		51	28.58		84	67.92	
18	8.45		52	29.38		85	69.59	0.696
19	8.95		53	30.17		86	71.49	
20	9.45	0.094	54	30.97		87	73.39	
21	9.97		55	31.76	0.318	88	75.29	
22	10.49		56	32.66		89	77.19	
23	11.01		57	33.57		90	79.09	0.791
24	11.53		58	34.47		91	81.09	
25	12.05	0.120	59	35.37		92	83.08	
26	12.59		60	36.28	0.363	93	85.08	
27	13.14		61	37.31		94	87.07	
23	13.69		62	35.34		95	89.06	0.891
29	14.23		63	39.36		96	91.25	
30	14.78	0.148	64	40.39		97	93.44	
31	15.36		65	41.42	0.414	98	95.63	
32	15.94		66	42.58		99	97.81	
33	16.52		67	43.73		100	100.00	1.000

XXVI.

TABLE

FOR

DEDUCING THE RELATIVE HUMIDITY IN HUNDREDTHS, FROM THE INDICATIONS OF SAUSSURE'S HAIR-HYGROMETER;

Calculated from the Experiments of Melloni.

By M. T. HAEGHENS.

The Hair-Hygrometer of Saussure having been formerly used for long series of observations, and being still employed by some meteorologists, notwithstanding the imperfection of this instrument, on account of its giving directly the relative humidity without calculation, it was desirable to ascertain the correspondence of the degrees of that hygrometer with the relative humidity expressed in hundredths, as in the preceding table. Though these instruments compared with each other, show very often great discrepancies in their indications, yet a large number of them agree sufficiently well with the experiments of Melloni, August, and others, to allow the following table of comparison to be constructed, which table may be considered as giving good approximations. For the calculation of it, Mr. Haeghens used the results of Melloni, which agree also satisfactorily with a series of observations very carefully made by M. Deleros. See Annuaire Météorologique de la France, pour 1850.

RELATIVE HUMIDITY IN HUNDREDTHS.

Degrees of Saussure's Hygrome-		Degrees of Saussure's Hygrometer. Units.										
ter. Tens,	θ.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity	Humidity		
0	0	0	1	1	2	3	3	4	4	5		
1	5	6	6	7	8	8	9	10	11	11		
2	12	12	13	14	15	16	17	18	18	19		
3	19	20	21	22	23	24	24	25	26	26		
4	27	27	28	28	29	30	31	32	33	34		
5	35	36	37	37	38	39	40	41	42	43		
6	44	45	46	47	49	50	51	52	53	55		
7	56	57	58	59	61	62	63	65	66	68		
8	69	70	72	73	75	77	78	79	81	82		
					1							
9	83	85	87	88	9ı	91	93	95	97	98		
10	100							•		•		

TABLE XXVII.

The following Table shows the Relative Humidity, in hundredths, corresponding to the degrees of Saussure's Hair-Hygrometer, as determined by various physicists. It is found in Kaemtz, *Vorlesungen über Meteorologie*, page 100; also in the French translation by Martins, *Cours de Météorologie*, page 80.

XXVI. RELATIVE HUMIDITY, CORRESPONDING TO THE DEGREES OF SAUSSURE'S HAIR-HYGROMETER.

Saturation = 100.

Degrees of		Relative Humidi	ty according to		Degrees of
Hair- Hygrometer.	Gay-Lussac.	Prinsep.	August.	Melloni.	Hair- Hygrometer.
100°	100.0	100.0	100.0	100.0	100°
95	89.1	88.7	94.0	90.8	95
90	79.1	78.2	86.0	83.1	90
85	69.6	68.3	79.0	76.5	85
so	61.2	59.2	71.0	68.9	80
75	53.8	50.6	64.0	62.0	75
70	47.2	43.6	56.0	55.6	70
65	41.4	37.2	48.0	49.6	65
60	36.3	31.5	41.0	44.0	60
55	31.8	26.3	36.0	39.1	55
50	27.8	21.8	31.0	34.6	50
45	24.1	17.7	27.0	29.8	45
40	20.8	14.3	23.0	27.0	40
35	17.7	11.4	19.0	23.8	35
30	14.8	9.1	16.0	19.0	30
25	12.0	7.1	13.0	16.4	25
20	9.4	4.9	10.0	11.7	20
15	7.0	3.0	7.0	8.3	15
10	4.6	1.6	4.0	5.0	10
5	2.2	0.6	2.0	2.6	5
0	0.0	0.0	0.0	0.0	0

В



APPENDIX

TO

THE HYGROMETRICAL TABLES.

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TABLES

FOR

COMPARING THE QUANTITIES OF RAIN-WATER.

THE three kinds of measures which are most in use for noting the quantities of rain and melted snow, are the Centimetres and Millimetres in France, the Paris or French inches and lines in Germany, and the English inches and decimals in England, America, and also in Russia, the Russian foot being the same as the English foot. The following tables will facilitate the comparison of these various measures with each other.

A glance at the tables will show that the first column on the left contains the numbers to be converted, and the heads of the following columns the fractions of these numbers, or units, each of which is one tenth of those in the first column. Shorter tables, at the bottom, give, when necessary, the value of proportional parts still smaller than those found in the larger tables.

Example.

Let 13 Centimetres be converted into French inches and lines.

Take, in Table II., the line beginning with 10 Centimetres in the first column, follow that line as far as the column headed 3 Centimetres, and there will be found the number of 4 inches 9.63 lines, which is the corresponding value in French inches of 10 + 3, or 13 Centimetres.

If the number is followed by a fraction, as for instance, 13.5 Centimetres, or 135 Millimetres, we find, —

French Inches, Lines, In the larger table 13 Centimetres = 4.9,63In the smaller table at the bottom 5 Millimetres = Or $\overline{13.5}$ Centimetres = 4.11,846

When the measures which are to be compared are both subdivided into decimal parts, the equivalents of the numbers greater than 9.9 may be found by moving the decimal point.

Example.

Let 346.7 Centimetres be converted into English inches.

In Table I., in the column headed 4, on the fourth line,

we find 3.4 Centimetres = 1.3386 English inches.

Moving the decimal point by two places we have

340 Centimetres = 133.86 English inches.

Then, in the column headed 7, on the

line beginning with 6, we find 6.7 Centimetres = 2.64

Making together 346.7 Centimetres = 136.50 English inches. В

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	-11					Centimetr			Inch.			
Centi-					1	1	Mill	imetres.	· · · · · · · · · · · · · · · · · · ·	1	1	1
metres	.	0.		1.	2.	3.	4.	5.	6.	7.	8.	9.
		Eng. Inc	,	g.Inch		1 0	_			Eng.Inch	1 -	
0		0.000		.0394			1	1	1	0.2756	1	1
1		0.393		4331	1	1	1		1	0.6693		0.748
2		0.787	1	8268		. 1		i i		1.0630	1.1024	1.1418
3		1.181		2205			ì	i	1	1.4567		1.535
4	I	1.5743	1	6142	1	1		1		1.8504	1.8898	1.929
5		1.968	- 1	$0079 \\ 4016$	i			1	1	2.2441	2.2835	2.322
6		2.3623	_ _				1		2.5985	2.6378	2.6772	2.716
7 8		2.7560 3.149	1	7953	1	1			1	3.0316	3.0709	3.110
9	H	-		1890				1		3.4253	3.4646	3.504
	- 11	3.543	1 0.	5827	3.6221	+3.6615	3.7009	3.7402	3.7796	3.8190	3.8583	3.897
II. CO	N V	ERSIO	N 01	F CE		RES INT				IES, AN	D DECIM	IALS.
Centi-	_						Un	its.				
netres.		0.	1	.	2.	3.	4.	5.	6.	7.	8.	9.
	Fr.	In. Lin.	Fr.In.	Lin. I	Fr.In. Lin.	Fr.In. Lin.	Fr. In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin.	Fr.In. Lin
0						1. 1,30						3. 3,9
10		. 8,33			4. 5,20			5. 6,49				
20	7	4,66	7. 9	9,09	8. 1,53	8. 5,96						
30	11	. 0,99	11. 5	5,42	11. 9,85	12. 2,29	12. 6,72	12.11,15	13. 3,59	13. 8,02	14. 0,45	14. 4,8
40	14	. 9,32	15. 1	1,75	15. 6,18	15.10,62	16. 3,05	16. 7,48	16.11,92	17. 4,35	17. 8,78	18. 1,2
50	18	. 5,65	18.10	0,08	19. 2,51	19. 6,95	19.11,38	20. 3,81	20. 8,25	21. 0,68	21. 5,11	21. 9,5
60						23. 3,28						
70	25	.10,31	26. 2	2,74	26. 7,17	26.11,61	27. 4,04	27. 8,47	28. 0,90	28. 5,34	28. 9,77	29. 2,2
80	29	6,64	29.11	l,07 3	30. 3,50	30. 7,93	31. 0,37	31. 4,80	31. 9,23	32. 1,67	32. 6,10	32.10,5
90	33	. 2,97	33. 7	,40 3	33.11,83	34. 4,26	34. 8,70	35. 1,13	35. 5,56	35.10,00	36. 2,43	36 6,8
			Fr.ln. l 36.11	- 11	1	Fr. In. Lin. 73.10.59	1 1	Fr.In. Lin. 110.9,89	1 1	Fr.In. Lin. 147.9,18	Centim. 500	Fr.In. Lin 184.8,4
	(CONVE	ERSIO	ON O	F CENT	IMETRE	S INTO	FRENCH	LINES	AND DE	CIMALS.	
Centi-							U	nits.				
metres.		0.		1.	2.	3.	4.	5.	6.	7.	8.	9.
		Fr. Line	- 1	Lines.	1	Fr. Lines		1	Fr. Lines.		Fr. Lines.	ı
0		0.00	- 1	4.43	8.87			22.16	26.60	31.03	35.46	39.90
10		44.33	1	8.76	53.20			66.49	70.93	75.36	79.79	84.23
20		88.66	1	3.09	97.53			110.82	115.26	119.69	124.12	128.56
30		132.99	- 1	7.42	141.85	1		155.15	159.59	164.02	168.45	172.89
40		177.32	1	1.75	186.18	190.62	195.05	199.48	203.92	208.35	212.78	217.22
50		221.63		6.08	230.51	234.95	239.38	243.81	248.25	252.68	257.11	261.5
60		265.98	- 1	0.41	274.84	1	1	288.14	292.58	297.01	301.44	305.87
70		310.31	- 1	4.74	319.17	1	1	332.47	336.90	341.34	345.77	350.20
80 90		354.6	- 1	9.07	363.50	1	1	376.80	381.23	385.67	390.10	394.53
90	1	398.97		3.40			<u> </u>	421.13	425.56	430.00	434.43	438.86
	- Ii				1	METRES	T	1				
		0,	_ _ :	1.	2.	3.	4.	5.	6.	7.	8.	9.
		Fr. Line		Lines.	Fr. Lines 0.887	Fr. Lines 1.330	Fr. Lines 1.773	Fr. Lines. 2.216	Fr. Lines. 2.660	Fr. Lines. 3.103	Fr. Lines. 3.546	Fr. Lines 3.990

I English Inch = 2.53995 Centimetres.

English					U	nits.				
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centim.	Centim.		Centim.	1	1	Centim.	Centim.	Centim.	Centim
0	0.00	2.54		7.62	1		15.24	17.78	20.32	22.80
10	25.40	27.94	1	33.02		1	40.64	43.18	45.72	48.26
20	50.80	53.34	1	58.42	1		66.04	68.58	71.12	73.6
30	76.20	78.74	1	83.82		1	91.44	93.98	96.52	99.0
40	101.60	104.14		109.22	1		116.84	119.38	121.92	124.4
50	127.00	129.54		134.62	1	1	142.24	144.78	147.32	149.80
60	152.40	154.94	1	160.02	1	1	167.64	170.18	172.72	175.20
70	177.80	180.34	1	185.42	!		193.04	195.58	198.12	200.6
80	203.20	205.74	Į.	210.82	1	1	218.44	220.98	223.52	226.00
90	228.60	231.14		236.22	i .	I.	243.84	246.38	248.92	251.40
100	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.8
	200.00	201.00	221.15	20= 0=	200	303.00	201.00	00= ==	200	
110	279.39	281.93		287.01	289.55	1	294.63	297.17	299.71	302.23
120	301.79	307.33		312.41	314.95	1	320.03	322.57	325.11	327.63
130	330.19	332.73	1	337.81	340.35	1	345.43	347.97	350.51	353.03
140	355.59	358.13	360.67	363.21	365.75	368.29	370.83	373.37	375.91	378.43
150	380.99	383.53	386.07	358.61	391.15	I .	396.23	398.77	401.31	403.83
160	406.39	408.93	411.47	414.01	416.55	1	421.63	424.17	426.71	429.25
170	431.79	434.33	436.87	439.41	441.95		447.03	449.57	452.11	454.63
180	457.19	459.73	462.27	464.81	467.35	1	472.43	474.97	477.51	480.03
190	482.59	485.13	487.67	490.21	492.75	495.29	497.83	500.37	502.91	505.45
200	507.99	510.53	513.07	515.61	518.15	520.69	523.23	525.77	528.31	530.85
	1				Tenths of	f an Inch.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Centim. 0.000	Centim. 0.254	Centim. 0.508	Centim. 0.762	Centim. 1.016	Centim. 1.270	Centim. 1.524	Centim. 1.778	Centim. 2.032	Centim. 2.286
IV	7. CONVE	ERSION			CHES 11			ICHES A	ND LIN	ES.
					Uni	ts.				
Eng. Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
F	r.In. Lin F	r.In. Lin F	r.In. Lin. F	r.In. Lin I	2r. In. Lin. 1	Fr.In. Lin	Fr.In. Lin	Fr.In. Lin	Fr.In. Lin	Fr In Liv
	0. 0,00		r.In. Lin. F 1.10,52							
0		0.11,26	1.10,52	2. 9,78	3. 9,04	4. 8,30	5. 7,56	6. 6,82	7. 6,08	8. 5,3
0 10	0. 0,00	0.11,26 $0.3,85$	1.10,52 1. 3,11	2. 9,78 2. 2,37	3. 9,04 13. 1,63	4. 8,30 14. 0,89	5. 7,56 15. 0,15	6. 6,82 15.11,41	7. 6,08 16.10,67	8. 5,3 17. 9,9
0 10 20	0. 0,00 9. 4,59 1	0.11,26 $0.3,85$ $0.8,45$	1.10,52 1. 3,11 20. 7,71	2. 9,78 2. 2,37 21. 6,97	3. 9,04 13. 1,63 22. 6,23	4. 8,30 14. 0,89 23. 5,49	5. 7,56 15. 0,15 24. 4,75	6, 6,82 15,11,41 25, 4,01	7. 6,08 16.10,67 26. 3,27	8. 5,3 17. 9,9 27. 2,5
0 10 20 1 30	0. 0,00 9. 4,59 1 8. 9,19 1	$egin{array}{ccc} 0.11,26 \ 0. & 3,85 \ 1. \ 9. & 8,45 \ 2. & 1,04 \ 3. \ \end{array}$	1.10,52 $1.3,11$ $20.7,71$ $20.0,30$	2. 9,78 2. 2,37 21. 6,97 30.11,56	3. 9,04 13. 1,63 22. 6,23 31.10,82	4. 8,30 14. 0,89 23. 5,49 32.10,08	5. 7,56 15. 0,15 24. 4,75 33. 9,34	6. 6,82 15.11,41 25. 4,01 34. 8,60	7. 6,08 16.10,67 26. 3,27 35. 7,86	8. 5,3 17. 9,93 27. 2,53 36. 7,13
0 10 20 1 30 40	0. 0,00 9. 4,59 18. 9,19 18. 1,78 28. 1,78	0.11,26 0. 3,85 1 9. 8,45 2 9. 1,04 3. 5,64	1.10,52 1. 3,11 20. 7,71 30. 0,30 39. 4,90	2. 9,78 2. 2,37 21. 6,97 30.11,56 40. 4,16	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46	8. 5,3 17. 9,99 27. 2,59 36. 7,19 45.11,79
0 10 20 30 40 50 4	0. 0,00 9 9. 4,59 10 8. 9,19 13 8. 1,78 25 7. 6,38 33	0.11,26 0. 3,85 1.04	1.10,52 1. 3,11 20. 7,71 20. 0,30 39. 4,90 48. 9,49	2. 9,78 2. 2,37 21. 6,97 30.11,56 40. 4,16 49. 8,75	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27	5. 7,56 15. 0,15 24. 4,75 83. 9,34 43. 1,94 52. 6,53	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05	8. 5,3 17. 9,93 27. 2,53 36. 7,13 45.11,73 55. 4,33
0 10 20 30 40 50 60	9. 4,59 16 8. 9,19 19 88. 1,78 29 67. 6,38 38 6.10,97 4	0.11,26 0. 3,85 1.04 9. 8,45 2.9. 1,04 3. 5,64 7.10,23 4. 2,83 5. 3	1.10,52 1. 3,11 20. 7,71 30. 0,30 39. 4,90 48. 9,49 48. 2,09 5	2. 9,78 2. 2,37 21. 6,97 30.11,56 40. 4,16 9. 8,75 9. 1,35	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42 50. 8,01	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27 60.11,87	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94 52. 6,53 31.11,13	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79 62.10,39	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05 63. 9,65	8. 5,3 17. 9,9 27. 2,5 36. 7,1 45.11,7 55. 4,3 64. 8,9
0 10 20 20 40 50 60 70 80 7	0. 0,00 9. 4,59 10 88. 9,19 11 88. 1,78 22 87. 6,38 36 60,10,97 47 66. 3,57 57 8,16 66 5. 0,76 76 76 76 76 76 76 76	0.11,26 0. 3,85 1.9. 8,45 2.1,04 3. 5,64 3. 5,64 7.10,23 4.7. 2,83 5. 7,42 6. 0,02 7. 0,02	1.10,52 1. 3,11 1. 3,11 1. 0, 7,71 20, 0,30 39, 4,90 48, 9,49 48, 2,09 57, 6,68 66,11,28 7	2. 9,78 2. 2,37 21. 6,97 30.11,56 30. 4,16 49. 8,75 9. 1,35 8. 5,94 7.10,54	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42 50. 8,01 50. 0,61 69. 5,20 78. 9,80	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46 79. 9,06	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94 52. 6,53 51.11,13 71. 3,72 80. 8,32	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84	8. 5,3 17. 9,93 27. 2,5 36. 7,13 45.11,7 55. 4,3 64. 8,9 74. 1,5 83. 6,1
0 10 20 30 40 50 60 70 80 90 8	0. 0,00 9. 4,59 10 88. 9,19 11 178 22 17. 6,38 33 16.10,97 47 16. 3,57 57 57 58,16 16 16 16 16 16 16 16	0.11,26 0. 3,85 1.04 9. 8,45 9. 1,04 3. 5,64 7.10,23 4.7. 2,83 5. 7,42 6. 0,02 7. 4,61 8	1.10,52 1. 3,11 20. 7,71 20. 0,30 39. 4,90 48. 9,49 48. 2,09 57. 6,68 6.11,28 7. 6,68 6.11,28 7. 6,68 6. 3,87	2. 9,78 2. 2,37 21. 6,97 20.11,56 30. 4,16 9. 8,75 9. 1,35 8. 5,94 7.10,54 7. 3,13	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80 78. 9,80	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27 60.11,87 60.11,87 67. 4,46 79. 9,06 89. 1,65	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94 52. 6,53 51.11,13 71. 3,72 80. 8,32 90. 0,91	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58 91. 0,17	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84 91.11,43	8. 5,3 17. 9,93 27. 2,5 36. 7,13 45.11,7 55. 4,3 64. 8,9 74. 1,5 83. 6,1 92.10,6
0 10 20 30 40 50 60 70 80 90 8	0. 0,00 9. 4,59 18. 9,19 19. 1,78 20. 1,78	0.11,26 0. 3,85 1.04 9. 8,45 9. 1,04 3. 5,64 7.10,23 4.7. 2,83 5. 7,42 6. 0,02 7. 4,61 8	1.10,52 1. 3,11 20. 7,71 20. 0,30 39. 4,90 48. 9,49 48. 2,09 57. 6,68 6.11,28 6. 3,87 6. 3,87 6. 3,87	2. 9,78 2. 2,37 21. 6,97 20.11,56 30. 4,16 9. 8,75 9. 1,35 8. 5,94 7.10,54 7. 3,13	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80 88. 2,39 Eag.Inch. E	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27 60.11,87 60.11,87 67. 4,46 79. 9,06 89. 1,65	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94 52. 6,53 51.11,13 71. 3,72 80. 8,32 90. 0,91 Eng.Inch.	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58 91. 0,17 Fr.In. Lin.	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84 91.11,43	8. 5,3 17. 9,93 27. 2,53 36. 7,13 45.11,73 55. 4,33 64. 8,93 74. 1,50 83. 6,10 92.10,69
0 10 20 30 40 50 40 50 60 70 80 90 8	0. 0,00 9. 4,59 18. 9,19 19. 1,78 20. 1,78	0.11,26 0. 3,85 9. 8,45 9. 1,04 3. 5,64 3. 5,64 7. 2,83 5. 7,42 6. 0,02 7. 4,61 8. In. Lin. [E	1.10,52 1. 3,11 20. 7,71 20. 0,30 39. 4,90 48. 9,49 48. 2,09 57. 6,68 6.11,28 6. 3,87 6. 3,87 6. 3,87	2. 9,78 12. 2,37 11. 6,97 10. 11,56 10. 4,16 10. 4,	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80 88. 2,39 Eag.Inch. E	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46 79. 9,06 89. 1,65 67.In. Lin 281.5,85	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94 52. 6,53 51.11,13 71. 3,72 80. 8,32 90. 0,91 Eng.Inch.	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58 91. 0,17	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84 91.11,43 Eng.Inch.	8. 5,3- 17. 9,9: 27. 2,5; 36. 7,1: 45.11,7: 55. 4,3: 64. 8,9: 74. 1,5: 83. 6,1: 92.10,6: Fr.In. Lin
0 10 20 30 40 50 40 50 60 70 80 90 8	0. 0,00 9. 4,59 18. 9,19 19. 1,78 20. 1,78	0.11,26 0. 3,85 9. 8,45 9. 1,04 3. 5,64 3. 5,64 7. 2,83 5. 7,42 6. 0,02 7. 4,61 8. In. Lin. [E	1.10,52 1. 3,11 20. 7,71 20. 0,30 39. 4,90 48. 9,49 48. 2,09 57. 6,68 6.11,28 6. 3,87 6. 3,87 6. 3,87	2. 9,78 12. 2,37 11. 6,97 10. 11,56 10. 4,16 10. 4,	3. 9,04 13. 1,63 22. 6,23 31.10,82 41. 3,42 50. 8,01 60. 0,61 69. 5,20 78. 9,80 88. 2,39 Eng.Inch. 1	4. 8,30 14. 0,89 23. 5,49 32.10,08 42. 2,68 51. 7,27 60.11,87 70. 4,46 79. 9,06 89. 1,65 67.In. Lin 281.5,85	5. 7,56 15. 0,15 24. 4,75 33. 9,34 43. 1,94 52. 6,53 51.11,13 71. 3,72 80. 8,32 90. 0,91 Eng.Inch.	6. 6,82 15.11,41 25. 4,01 34. 8,60 44. 1,20 53. 5,79 62.10,39 72. 2,98 81. 7,58 91. 0,17 Fr.In. Lin.	7. 6,08 16.10,67 26. 3,27 35. 7,86 45. 0,46 54. 5,05 63. 9,65 73. 2,24 82. 6,84 91.11,43 Eng.Inch.	8. 5,3- 17. 9,93 27. 2,58 36. 7,13 45.11,73 55. 4,31 64. 8,91 74. 1,50 83. 6,10 92.10,69

В

V. CONVERSION OF FRENCH INCHES INTO CENTIMETRES.

I French Inch = 2.7070 Centimetres.

French Inches.	Units.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	
0	0.00	2.71	5.41	8.12	10.83	13.53	16.24	18.95	21.66	24.36	
10	27.07	29.78	32.48	35.19	37.90	40.60	43.31	46.02	48.73	51.43	
20	54.14	56.85	59.55	62.26	64.97	67.67	70.38	73.09	75.80	78.50	
30	81.21	83.92	86.62	89.33	92.04	94.74	97.45	100.16	102.87	105.57	
40	108.28	110.99	113.69	116.40	119.11	121.81	124.52	127.23	129.94	132.64	
50	135.35	138.06	140.76	143.47	146.18	148.88	151.59	154.30	157.01	159.71	
			1		ĺ				:		
60	162.42	165.13	167.83	170.54	172.25	175.95	178.66	181.37	184.08	186.78	
70	189.49	192.20	194.90	197.61	200.32	203.02	205.73	208.44	211.15	213.85	
80	216.56	219.27	221.97	224.68	227.39	230.09	232.80	235.51	238.22	240.92	
90	243.63	246.34	249.04	251.75	254.46	257.16	259.87	262.58	265.29	267.99	
100	270.70	273.41	276.11	278.82	281.53	284.23	286.94	289.65	292.36	295.06	
110	297.77	300.48	303.18	305.89	308.60	311.30	314.01	316.72	319.42	322.13	
120	324.84	327.55	330.25	332.96	335.67	338.37	341.08	343.79	346.49	349.20	
130	351.91	354.62	357.32	360.03	362.74	365.44	368.15	370.86	373.56	376.27	
140	378.98	381.69	384.39	387.10	389.81	392.51	395.22	397.93	400.63	403.34	
150	406.05	408.76	411.46	414.17	416.88	419.58	422.29	425.00	427.70	430.41	
	ļ										
160	433.12	435.83	438.53	441.24	443.95	446.65	449.36	452.07	454.77	457.48	
170	460.19	462.90	465.60	468.31	471.02	473.72	476.43	479.14	481.84	484.55	
180	487.26	489.97	492.67	495.38	498.09	500.79	503.50	506.21	508.91	511.62	
190	514.33	517.04	519.74	522.45	525.16	527.86	530.57	533.28	535.98	538.69	
200	541.40	544.11	546.81	549.52	552.23	554.93	557.64	560.35	563.05	565.76	

CONVERSION OF FRENCH LINES INTO CENTIMETRES.

1 French Line = 0.22558 Centimetre.

French Lines.	Tenths of a Line.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	Centim.	
0	0.000	0.023	0.045	0.068	0.090	0.113	0.135	0.158	0.180	0.203	
1	0.226	0.248	0.271	0.293	0.316	0.338	0.361	0.383	0.406	0.429	
2	0.451	0.474	0.496	0.519	0.541	0.564	0.587	0.609	0.632	0.654	
3	0.677	0.699	0.722	0.744	0.767	0.790	0.812	0.835	0.857	0.880	
4	0.902	0.925	0.947	0.970	0.993	1.015	1.038	1.060	1.083	1.195	
5	1.128	1.150	1.173	1.196	1.218	1.241	1.263	1.286	1.308	1.331	
6	1.353	1.376	1.399	1.421	1.444	1.466	1.489	1.511	1.534	1.557	
7	1.579	1.602	1.624	1.647	1.669	1.692	1.714	1.737	1.760	1.782	
8	1.805	1.827	1.850	1.872	1.895	1.917	1.940	1.963	1.985	2.008	
9	2.030	2.053	2.075	2.098	2.120	2.143	2.166	2.188	2.211	2.233	
10	2.256	2.278	2.301	2.324	2.346	2.369	2.391	2.414	2.436	2.459	
11	2.481	2.504	2.527	2.549	2.572	2.594	2.617	2.639	2.662	2.684	
12	2.707	2.730	2.752	2.775	2.797	2.820	2.842	2.865	2.887	2.910	

I French Inch = 1.065765 English Inch.

French Inches.	Units.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
				Eng.Inch.							
0	0.000				4.263	5.329	6.395				
10	10.658		1	13.855	14.921	15.986	17.052	18.118		20.250	
20.	21.315	22.381	23.447	24.513	25.578	26.644	27.710	28.776	29.841	30.907	
30	31.973	33.039	34.104	35.170	36.236	37.302	38.368	39.433	40.499	41.565	
40	42.631	43.696	44.762	45.828	46.894	47.959	49.025	50.091	51.157	52.222	
50	53.288	54.354	55.420	56.486	57.551	58.617	59.683	60.749	61.814	62.880	
	:										
60	63.946	65.012	66.077	67.143	68.209	69.275	70.340	71.407	72.472	73.538	
70	74.604	75.669	76.735	77.801	78.867	79.932	80.998	82.064	83.130	84.195	
80	85.261	86.327	87.393	88.458	89.524	90.590	91.656	92.722	93.787	94.853	
90	95.919	96.985	98.050	99.116	100.182	101.248	102.314	103.379	104.445	105.511	
100	106.576	107.642	108.708	109.774	110.840	111.905	112.971	114.037	115.103	116.168	
110	117.234	118.300	119.366	120.431	121.497	122.563	123.629	124.695	125.760	126.826	
120	127.892	128.958	130.023	131.089	132.155	133.221	134.286	135.352	136.418	137.484	
130	138.549	139.615	140.681	141.747	142.813	143.878	144.944	146.010	147.076	148.141	
140	149.207	150.273	151.339	152.404	153.470	154.536	155.602	156.667	157.733	158.799	
150	159.865	160.931	161.996	163.062	164.128	165.194	166.259	167.325	168.391	169.457	
160	170.522	171.588	172.654	173.720	174.785	175.851	176.917	177.983	179.049	180.114	
170				184.377					189.706		
180	11 1			195.035			198.232	199.298	200.364	201.430	
190	4			205.693							
200	11	214.219									

CONVERSION OF FRENCH LINES INTO ENGLISH INCHES.

1 French Line = 0.088814 English Inch.

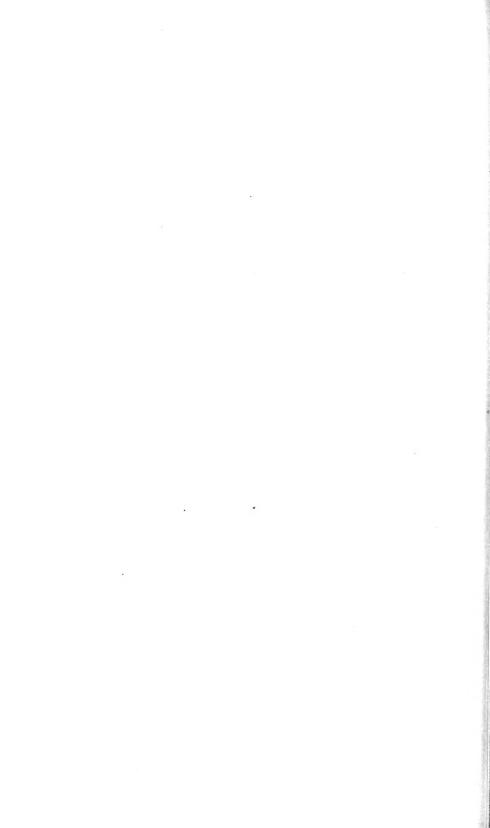
French Lines.	Tenths of a Line.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Eng.Inch.	Eug.Inch.	Eng.Inch.	Eng. Inch.	Eng Inch.	Eng.Inch.	Eng Inch.	Eng.Inch.	Eng. Inch.	Eng Incl	
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0533	0.0622	0.0711	0.0799	
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687	
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2309	0.2398	0.2487	0.2576	
3	0.2664	0.2753	0.2842	0.2931	0.3020	0.3108	0.3197	0.3286	0.3375	0.3464	
4	0.3553	0.3641	0.3730	0.3819	0.3908	0.3997	0.4085	0.4174	0.4263	0.4352	
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240	
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.6128	
7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.7016	
8	0.7105	0.7194	0.7283	0.7372	0.7460	0.7549	0.7638	0.7727	0.7816	0.790	
9	0.7993	0.8082	0.8171	0.8260	0.8349	0.8437	0.8526	0.8615	0.8704	0.879	
10	0.8881	0.8970	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.968	
11	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.056	
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.145	



METEOROLOGICAL TABLES.

III.

BAROMETRICAL TABLES.



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a		Baily



COMPARISON

ŌΕ

THE BAROMETRICAL SCALES,

OR

TABLES

FOR CONVERTING THE INDICATIONS OF THE ENGLISH, METRICAL, OLD FRENCH, AND RUSSIAN BAROMETERS INTO EACH OTHER.



COMPARISON

OF

THE BAROMETRICAL SCALES.

The following tables are intended for converting into each other the four most important Barometrical Scales. They are sufficiently detailed to save the labor of any calculation or even of interpolation for the ordinary wants of Meteorology. But before making use of them, for comparing the observations taken with barometers of different scales, it is necessary to reduce the observed heights to the temperature of the freezing point, or to any other temperature, provided it be the same for all, by means of the tables calculated for this purpose, and which will be found below. The reason of it may be readily understood.

The length of the bars of metal, or of other substances, which represent the standard measures of length which obtain among different nations, varying with the temperature, it was necessary to determine a fixed point of temperature at which they really ought to have the length adopted as the standard unit of measure. This temperature is the *normal* temperature of the standard, and the length of the standard-bar, at this temperature, is the *true* length of it.

If the normal temperature of the various standards used for dividing Barometrical Scales were the same, the heights of the barometrical column, taken with these scales, could be compared directly, provided the scales be made of the same substance, brass, for instance, because their variations above or below this normal temperature would remain parallel with each other. But unfortunately it is not so. The English Yard is a standard at the temperature of 62° Fahrenheit; the Old French Toise, at 13° Reaumur; the Metre, at the freezing point, or zero Centigrade. Thus metallic rods intended to represent these various units of measure give the true or standard length only when at these respective temperatures; at any other temperature they are longer or shorter than the standard, and their subdivisions, inches, lines, or millimetres, partake of the error.

It is obvious, therefore, that the barometrical heights, taken with different scales, cannot be compared *directly* by means of the following tables, which give the relation between these scales at their respective *normal* temperatures. For suppose the temperature of the three barometers to be the freezing point, or 32° Fahrenheit,

the scale of the Metrical Barometer alone will actually represent the standard length, and the millimeters will have the true length; while the inches and lines of the Old French and of the English Barometers will be too short, causing thus the barometrical column to appear too high. If the temperature of the instruments be 62° Fahrenheit, the divisions of the English Barometer will have the true standard length, and those of the Old French Barometer nearly so; but the millimeters of the Metrical Barometer will be too long, causing the barometrical column to appear too low. It is to neutralize the effect of those inequalities arising from the expansion of the scale that it is necessary, before comparing the observations taken with the three barometers, to reduce them to the same temperature. This is done by means of the tables above mentioned, for reducing the barometer to the freezing point, which suppose the scales to be of brass from top to bottom, and which take into account the expansion or contraction they undergo by the variations of temperature.

But in doing so, we must be aware that the accuracy of the comparison depends in part upon the correctness of the indications of the attached thermometers, which determine the amount of the correction to be applied for reducing the barometers to the freezing point. If the thermometers do not agree, an error is introduced which will affect the height of the reduced columns, and the final comparison. Therefore the correction of the attached thermometers ought to be ascertained and applied to them before the reduction is made; or if this correction is unknown, it will be well to place the instruments to be compared in the most favorable conditions for taking the same temperature, and then to take the temperature given by one of the thermometers to reduce both barometers. If the correction of the attached thermometer has not been applied before the reduction, it will be contained, after the reduction, in the total correction of the instrument. If it be so, this circumstance must be indicated.

In computing the following tables, the value of the Metre, as determined by Capt. Kater, (Philosoph. Transact. for 1818, p. 109, and Baily's Astronomical Tables, p. 192,) has been adopted, viz. 1 Metre, at 0° Centigrade = 39.37079 English inches, at 62° Fahrenheit. The relation of the Metre (legal) to the Old French system of measures is known to be 1 Metre = 443.296 French or Paris lines. From these equations are derived the elements used in the computations, which are found at the head of each table.

Besides the larger Tables I. – VIII., a set of smaller ones, Tables IX. – XVI., has been added, which will be found useful for comparing Barometrical differences, such as ranges, amount of variation in a given time, &c., expressed in measures of different scales, in which only small quantities occur that are not found in the large tables.

I. - II.

COMPARISON

OF

THE ENGLISH BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

TABLES

FOR CONVERTING ENGLISH INCHES INTO MILLIMETRES, AND INTO FRENCH OR PARIS LINES AND DECIMALS;

GIVING THE VALUES CORRESPONDING TO EVERY TENTH OF AN INCH, FROM 9
TO 19 INCHES; AND TO EVERY HUNDREDTH, FROM
19 TO 31.5 ENGLISH INCHES.

USE OF TABLE I.

Example.

The English Barometer reads 20.657 inches. What would be the corresponding height in the Metrical Barometer?

In Table I., first column on the left, look out the line of 20 inches 6 tenths; on that line, in the sixth column, headed 5 hundredths, is found the value in millimetres for

At the bottom of the page, for
$$0.007$$
 " $= 0.18$ " Or for 20.657 " $= 524.68$ "

which would be the reading of the Metrical Barometer.

This example may serve for all tables, throughout the volume, which are constructed on the same plan.

1 English Inch = 25.39954 Millimetres.

P11.1.					Tenths o	f an Inch.				
English Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
9	228.60	231.14	233.68	236.22	238.76	241.30	243.84	246.38	248.92	251.46
10	254.00	256.54	259.08	261.62	264.16	266.70	269.24	271.78	274.32	276.85
11	279.39	281.93	284.47	287.01	289.55	292.09	294.63	297.17	299.71	302.25
12	304.79	307.33	309.87	312.41	314.95	317.49	320.03	322.57	325.11	327.65
13	330 19	332.73	335.27	337.81	340.35	342.89	345.43	347.97	350.51	353.05
14	355.59	358.13	360.67	363.21	365.75	368.29	370.83	373.37	375.91	378.45
15	380.99	383.53	386.07	388.61	391.15	393.69	396.23	398.77	401.31	403.85
16	406.39	408.93	411.47	414.01	416.55	419.09	421.63	424.17	426.71	429.25
17	431.79	434.33	436.87	439.41	441.95	444.49	447.03	449.57	452.11	454.65
18	457.19	459.73	462.27	464.81	467.35	469.89	472.43	474.97	477.51	480.05
English nches and				1	Hundredth	of an In	ch.			
tenths	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim	Millim	Millim	Mıllim.
19.0	482.59	482.85	483.10	483.35	483.61	483.86	484.12	484.37	484.62	484.88
1	485.13	485.39	485.64	485.89	486.15	486.40	486.66	486.91	487.16	487.42
2	487.67	487.93	488.18	488.43	488.69	488.94	489.20	489.45	489.70	489.96
3	490.21	490.47	490.72	490.97	491.23	491.48	491.74	491.99	492.24	492.50
4	492.75	493.01	493.26	493.51	493.77	494.02	494.28	494.53	494.78	495.04
5	495.29	495.55	495.80	496.05	496.31	496.56	496.81	497.07	497.32	497.58
6	497.83	498.08	498.34	498.59	498.85	499.10	499.35	499.61	499.86	500.12
7	500.37	500.62	500.88	501.13	501.39	501.64	501.89	502.15	502.40	502.66
8	502.91	503.16	503.42	503.67	503.93	504.18	504.43	504.69	504.94	505.20
9	505.45	505.70	505.96	506.21	506.47	506.72	506.97	507.23	507.48	507.74
20 .0	507.99	508.24	508.50	508.75	509.01	509.26	509.51	509.77	510.02	510.28
1	510.53	510.78	511.04	511.29	511.55	511.80	512.05	512.31	512.56	512.82
2	513.07	513.32	513.58	513.83	514.09	514.34	514.59	514.85	515.10	515.36
3	515.61	515.86	516.12	516.37	516.63	516.88	517.13	517.39	517.64	517.90
4	518.15	518.40	518.66	518.91	519.17	519.42	519.67	519.93	520.18	520.44
5	520.69	520.94	521.20	521.45	521.71	521.96	522.21	522.47	522.72	522.98
6	523.23	523.48	523.74	523.99	524.25	524.50	524.75	525.01	525.26	525.52
7	525.77	526.02	526.28	526.53	526.79	527.04	527.29	527.55	527.80	528.06
8	528.31	528.56	528.82	529.07	529.33	529.58	529.83	530.09	530.34	530.60
9	530.85	531.10	531.36	531.61	531.87	532.12	532.37	532.63	532.88	533.14
				Thousar	ndths of an	Inch.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	8 0.	10 0	0.13	0.15	0.18	0.20	0.23

English					Hundredth	s of an Inc	h.			
nches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Mıllim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millir
21.0	533.39	533.64	533.90	534.15	534.41	534.66	534.91	535.17	535.42	535.6
1	535.93	536.18	536.44	536.69	536.95	537.20	537.45	537.71	537.96	538 2
2	538.47	538.72	538.98	539.23	539.49	539.74	539.99	540.25	540.50	540.7
3	541.01	541.26	541.52	541.77	542.03	542.28	542.53	542.79	543.04	543.3
4	543.55	543.80	544.06	544.31	544.57	544.82	545.07	545.33	545.58	545.8
5	546.09	546.34	546.60	546.85	547.11	547.36	547.61	547.87	548.12	548.3
6	548.63	548.88	549.14	549.39	549.65	549.90	550.15	550.41	550.66	550.9
7	551.17	551.42	551.68	551.93	552.19	552.44	552.69	552.95	553.20	553.4
8	553.71	553.96	554.22	554.47	554.73	554.98	555.23	555.49	555.74	556.0
9	556.25	556.50	556.76	557.01	557.27	557.52	557.77	558.03	558.28	558.5
22.0	558.79	559.04	559.30	559.55	559.81	560.06	560.31	560.57	560.82	561.0
1	561.33	561.58	561.84	562.09	562.35	562.60	562.85	563.11	563.36	563.6
2	563.87	564.12	564.38	564.63	564.89	565.14	565.39	565.65	565.90	566.1
3	566.41	566.66	566.92	567.17	567.43	567.68	567.93	568.19	568.44	568.7
4	568.95	569.20	569.46	569.71	569.97	570.22	570.47	570.73	570.98	571.2
5	571.49	571.74	572.00	572.25	572.51	572.76	573.01	573.27	573.52	573.7
6	574.03	574.28	574.54	574.79	575.05	575.30	575.55	575.81	576.06	576.3
7	576.57	576.82	577.08	577.33	577.59	577.84	578.09	578.35	578.60	578.8
8	579.11	579.36	579.62	579.87	580.13	580.38	580.63	580.89	581.14	581.4
9	581.65	581.90	582.16	582.41	582.67	582.92	583.17	583.43	583.68	583.9
3.0	584.19	584.44	584.70	584.95	585.21	585.46	585.71	585.97	586.22	586.4
1	586.73	586.98	587.24	587.49	587.75	588.00	588.25	588.51	588.76	589.0
2	589.27	589.52	589.78	590.03	590.29	590.54	590.79	591.05	591.30	591.5
3	591.81	592.06	592.32	592.57	592.83	593.08	593.33	593.59	593.84	594.1
4	594.35	594.60	594.86	595.11	595.37	595.62	595.87	596.13	596.38	596.6
5	596.89	597.14	597.40	597.65	597.91	598.16	598.41	598.67	598.92	599.1
6	599.43	599.68	599.94	600.19	600.45	600.70	600.95	601.21	601.46	601.7
7	601.97	602.22	602.48	602.73	602.99	603.24	603.49	603.75	604.00	604.20
8	604.51	604.76	605.02	605.27	605.53	605.78	606.03	606.29	606.54	606.79
9	607.05	607.30	607.56	607.81	608.06	608.32	608.57	608.83	609.08	609.3
1.0	609.59	609.84	610.10	610.35	610.60	610.86	611.11	611.37	611.62	611.8
1	612.13	612.38	612.64	612.89	613.14	613.40	613.65	613.91	614.16	614.4
2	614.67	614.92	615.18	615.43	615.68	615.94	616.19	616.45	616.70	616.9
3	617.21	617.46	617.72	617.97	618.22	618.48	618.73	618.99	619.24	619.4
4	619.75	620.00	620.26	620.51	620.76	621.02	621.27	621.53	621.78	622.0
				Thoma	andths of a	n Inah				

				Thousandt	hs of an Inc	h.			
0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
0.0	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23

English				I	Hundredths	of an Inc	h.			
nches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
24.5	622.29	622.54	622.80	623.05	623.30	623.56	623.81	624.07	624.32	624.57
6	624.83	625.08	625.34	625.59	625.84	626.10	626.35	626.61	626.86	627.11
7	627.37	627.62	627.88	628.13	628.38	628.64	628.89	629.15	629.40	629.63
8	629.91	630.16	630.42	630.67	630.92	631.18	631.43	631.69	631.94	632.19
9	632.45	632.70	632.96	633.21	633.46	633.72	633.97	634.23	634.48	634.73
25.0	634.99	635.24	635.50	637.75	636.00	636.26	636.51	636.77	637.02	637.27
1	637.53	637.78	638.04	638.29	638.54	338.80	639.05	639.31	639.56	639.8
2	640.07	640.32	640.58	640.83	641.08	641.34	641.59	641.85	642.10	642.3
3	642.61	642.86	643.12	643.37	643.62	643.88	644.13	644.39	644.64	644.89
4	645.15	645.40	645.66	645.91	646.16	646.42	646.67	646.93	647.18	647.45
5	647.69	647.94	648.20	648.45	648.70	648.96	649.21	649.47	649.72	649.97
6	650.23	650.48	650.74	650.99	651.24	651.50	651.75	652.01	652.26	652.5
7	652.77	653.02	653.28	653.53	653.78	654.04	654.29	654.55	654.80	655.03
8	655.31	655.56	655.82	656.07	656.32	656.58	656.S3	657.09	657.34	657.59
9	657.85	658.10	658.36	658.61	658.86	659.12	659.37	659.63	659.88	660.13
26 .0	660.39	660.64	660.90	661.15	661.40	661.66	661.91	662.17	662.42	662.63
1	662.93	663.18	663.44	663.69	663.94	664.20	664.45	664.71	664.96	665.23
2	665.47	665.72	665.98	666.23	666.48	665.74	666.99	667.25	667.50	667.7
3	668.01	668.26	668.52	668.77	669.02	669.28	669.53	669.79	670.04	670.29
4	670.55	670.80	671.06	671.31	671.56	671.82	672.07	672.33	672.58	672.83
	200 00	200			07.170					
5	673.09	673.34	673.60	673.85	674.10	674.36	674.61	674.87	675.12	675.37
6	675.63	675. 88	676.14	676.39	676.64	676.90	677.15	677.41	677.66	677.91
7	678.17	678.42	678.68	678.93	679.18	679.44	679.69	679.95	680.20	680.45
8 9	680.71 683.25	680.96 683.50	681.22 683.76	681.47 684.01	681.72 684.26	681.98 684.52	$682.23 \\ 684.77$	682.49 685.03	$682.74 \\ 685.28$	682.99 685.58
3	000.20	003.30	033.70	004.01	004.20	004.04	004.77	000.00	000-20	000.00
27.0	685.79	686.04	686.30	686.55	686.80	687.96	687.31	687.57	687.82	688.07
1	688.33	688.58	688.84	689.09	689.34	689.60	689.85	690.11	690.36	690.61
2	690.87	691.12	691.38	691.63	691.88	692.14	692.39	692.65	692.90	693.15
3	693.41	693.66	693.92	694.17	694.42	694.68	694.93	695.19	695.44	695.69
4	695.95	696.20	696.46	696.71	696.96	697.22	697.47	697.73	697.98	698.23
5	698.49	698.74	699.00	699.25	699.50	699.76	700.01	700.27	700.52	700.77
6	701.03	701.28	701.54	701.79	702.04	702.30	702.55	702.81	703.06	703.31
7	703.57	703.82	704.08	704.33	704.58	704.84	705.09	705.35	705.60	705.83
8	706.11	706.36	706.62	706.87	707.12	707.38	707.63	707.89	708.14	708.39
9	708.65	708.90	709.16	709.41	709.66	709.92	710.17	710.43	710.68	710.93

0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23

English					Hundredth	s of an Inc	h.	 		
Inches and tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
28.0	711.19	711.44	711.70	711.95	712.20	712.46	712.71	712.97	713.22	713.4
1	713.73	713.98	714.24	714.49	714.74	715.00	715.25	715 51	715.76	716.0
2	716.27	716.52	716.78	717.03	717.28	717.54	717.79	718.04	718.30	718.5
3	718.81	719.06	719.31	719.57	719.82	720.08	720.33	720.58	720.84	721.0
-1	721.35	721.60	721.85	722.11	722.36	722.62	722.87	723.12	723.38	723.6
5	723.89	724.14	724.39	724.65	724.90	725.16	725.41	725.66	725.92	726.1
6	726.43	726.68	726.93	727.19	727.44	727.70	727.95	728.20	728.46	728.7
7	728.97	729.22	729.47	729.73	729.98	730.24	730.49	730.74	731.00	731.2
8	731.51	731.76	732.01	732.27	732.52	732.78	733.03	733.28	733.54	732.7
9	734.05	734.30	734.55	734.81	735.06	735.32	735.57	735.82	736.08	736.3
29.0	736.59	736.84	737.09	737.35	737.60	737.86	738.11	738.36	738.62	738.8
1	739.13	739.38	739.63	739.89	740.14	740.40	740.65	740.90	741.16	741.4
2	741.67	741.92	742.17	742.43	742.68	742.94	743.19	743.44	743.70	743.9
3	744.21	744.46	744.71	744.97	745.22	745.48	745.73	745.98	746.24	746.4
4	746.75	747.00	747.25	747.51	747.76	748.02	748.27	748.52	748.78	749.0
5	749.29	749.54	749 79	750.05	750.30	750.56	750.81	751.06	751.32	751.5
6	751.83	752.08	752.33	752.59	752.84	753.10	753.35	753.60	753.86	754.1
7	754.37	754.62	754.87	755.13	755.38	755.64	755.89	756.14	756.40	756.6
8	756.91	757.16	757.41	757.67	757.92	758.18	758.43	758.68	758.94	759.1
9	759.45	759.70	759.95	760.21	760.46	760.72	760.97	761.22	761.48	761.7
30.0	761.99	762.24	762.49	762.75	763.00	763.26	763.51	763.76	764.02	764.2
1	764.53	764.78	765.03	765.29	765.54	765.80	766.05	766.30	766.56	766.8
2	767.07	767.32	767.57	767.83	768.08	768.34	768.59	768.84	769.10	769.3
3	769.61	769.86	770.11	770.37	770.62	770.88	771.13	771.38	771.64	771.8
4	772.15	772.40	772.65	772.91	773.16	773.42	773.67	773.92	774.18	774.4
5	774.69	771.94	775.19	775.45	775.70	775.96	776.21	776.46	776.72	776.9
6	777.23	777.48	777.73	777.99	778.24	778.50	778.75	779.00	779.26	779.5
7	779.77	780.02	780.27	780.53	780.78	781.04	781.29	781.54	781.80	782.0
S	782.31	782.56	782.81	783.07	783.32	783.58	783.83	784.08	784.34	784.5
9	784.85	785.10	785.35	785.61	785.86	786.12	786.37	786.62	786.88	787.1
1.0	787.39	787.64	787.89	788.15	788.40	788.66	788.91	789.16	789.42	789.6
1	789.93	790.18	790.43	790.69	790.94	791.20	791.45	791.70	791.96	792.2
2	792.47	792.72	792.97	793.23	793.48	793.74	793.99	794.24	794.50	794.7
3	795.01	795.26	795.51	795.77	796.02	796.28	796.53	796.78	797.04	797.2
4	797.55	797.80	798.05	798.31	798.56	798.82	799.07	799.32	799.58	799.8
	ļ		l	Thous	sandths of	an Inch.	1	1	<u> </u>	l
0.	1.	2.	3.	4.		5.	6.	7.	8.	9.
0.0	0.03	0.05	0.08	0.1	0 0.	13	0.15	0.18	0.20	0.23

1 English Inch = 11.2595 French or Paris Lines.

					Tenths o	f an Inch.				
English Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par lines.			Par.lines,	4	Par line		. Par.lines		Par lines
11	123.85	124.98	126.11	127.23	128.36	129.48			132.86	133.99
12	135.11	136.24	137.37	138.49	139.62	140.74)	144.12	145.25
13	146.37	147.50	148.63	149.75	150.88	152.00			155.38	156.51
14	157.63	158.76	159.88	161.01	162.14	163.26	1		166.64	167.77
15	168.89	170.02	171.14	172.27	173 40	174.52		176.77	177.90	179.03
16	180.15	181.28	182.40	183.53	184.66	185.78	186.91	188.03	189.16	190.29
				Hundre	edths of an	Inch.				
0.	1.	2.	3.	4.	_	5.	6.	7.	8.	9.
0.000	0.113	0.225	0.338	0.45	50 0.	563	0.676	0.788	0.991	1.013
English				1	Iundredth	s of an In	ch.			
Inches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par lines	. Par.lines	Par lines	Par.lines.	Par.lines
17.0	191.41	191.52	191.64	191.75	191.86	191.97	192.09	192.20	192.31	192.42
1	192.54	192.65	192.76	192.85	192.99	193.10	193.21	193.33	193.44	193.55
2	193.66	193.78	193.89	194.00	194.11	194.23	194.34	191.45	194.56	194.68
3	194.79	194.90	195.01	195.13	195.24	195.35	195.46	195.58	195.69	195.80
4	195.92	196.03	196.14	196.25	196.37	196.48	196.59	196.70	196.82	196.93
5	197.04	197.15	197.27	197.38	197.49	197.60	197.72	197.83	197.94	198.05
6	198.17	198.28	198.39	198.50	198.62	198.73	198.84	198.96	199.07	199.18
7	199.29	199.41	199.52	199.63	199.74	199.86	199.97	200.08	200.19	200.31
8	200.42	200.53	200.64	200.76	200.87	200.98	201.09	201.21	201.32	201.43
9	201.55	201.66	201.77	201.88	202.00	202.11	202.22	202.33	202.45	202.56
18.0	202.67	202.78	202.90	203.01	203.12	203.23	203.35	203.46	203.57	203.68
1	203.80	203.91	204.02	204.13	204.25	204.36	204.47	204.59	204.70	204.81
2	204.92	205.04	205.15	205.26	205.37	205.49	205.60	205.71	205.82	205.94
3	206.05	206.16	206.27	206.39	206.50	206.61	206.72	206.84	206.95	207.06
4	207.17	207.29	207.40	207.51	207.63	207.74	207.85	207.96	208.08	208.19
5	208.30	208.11	208.53	208.64	208.75	208.86	208.98	209.09	209.20	209.31
6	209.43	209.54	209.65	209.76	209.88	209.99	210.10	210.21	210.33	210.44
7	210.55	210.67	210.78	210.89	211.00	211.12	211.23	211.34	211.45	211.57
8	211.68	211.79	211.90	212.02	212.13	212.24	212.35	212.47	212.58	212.69
9	212.80	212.92	213.03	213.14	213.25	213.37	213.48	213.59	213.71	213.82
19.0	213.93	214.04	214.16	214.27	214.38	214.49	214.61	214.72	214.83	214.94
1	215.06	215.17	215.28	215.39	215.51	215.62	215.73	215.84	215.96	216.07
2	216.18	216.29	216.41	216.52	216.63	216.75	216.86	216.97	217.08	217.20
3	217.31	217.42	217.53	217.65	217.76	217.87	217.98	218.10	218.21	218.32
4	218.43	218.55	218.66	218.77	218.88	219.00	219.11	219.22	219.34	219.45
5	219.56	219.67	219.79	219.90	220.01	220.12	220.24	220.35	220.46	220.57
6	220.69	220.80	220.91	221.02	221.14	221.25	221.36	221.47	221.59	221.70
7	221.81	221.92	222.01	222.15	222.26	222.38	222.49	222.60	222.71	222.83
s	222.94	223.05	223.16	223.28	223.39	223.50	223.61	223.73	223.84	223.95
9	221.06	221.18	224.29	224.40	224.51	224.63	224.74	224.85	224.96	225.08

1 English Inch = 11.2595 French or Paris Lines.

English				1	lundredths	of an Inc	h.			
nches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
20.0	225.19	225.30	225.42	225.53	225.64	225.75	225.87	225.98	226.09	226.2
1	226.32	226.43	226.54	226.65	226.77	226.88	226.99	227.10	227.22	227.3
2	227.44	227.55	227.67	227.78	227.89	228.00	228.12	228.23	228.34	228.4
3	228.57	228.68	228.79	228.91	229.02	229.13	229.24	229.36	229.47	229.5
4	229.69	229.81	229.92	230.03	230.14	230.26	230.37	230.48	230.59	230.7
5	230.82	230.93	231.01	231.16	231.27	231.38	231.50	231.61	231.72	231.8
6	231.95	232.06	232.17	232.28	232.40	232.51	232.62	232.73	232.85	232.9
7	233.07	233.18	233.30	233.41	233.52	233.63	233.75	233.86	233.97	234.0
8	234.20	234.31	234.42	234.54	234.65	234.76	234.87	234.99	235.10	235.5
9	235.32	235.44	235.55	235.66	235.77	235.89	236.00	236.11	236.22	236.
21.0	236.45	236.56	236.67	236.79	236.90	237.01	237.13	237.24	237.35	237.
1	237.58	237.69	237.80	237.91	238.03	238.14	238.25	238.36	238.48	238.
2	238.70	238.81	238.93	239.04	239.15	239.26	239.38	239.49	239.60	239.
3	239.83	239.94	240.05	240.17	240.28	240.39	240.50	240.62	240.73	240.8
4	240.95	241.07	241.18	241.29	241.40	241.52	241.63	241.74	241.85	241.9
5	242.08	242.19	242.30	242.42	242.53	242.64	242.75	242.87	242.98	243.0
6	243.21	243.32	243.43	243.54	243.66	243.77	243.88	243.99	244.11	244.5
7	244.33	244.44	244.56	244.67	244.78	244.89	245.01	245.12	245.23	245.3
s	245.46	245.57	245.68	245.79	245.91	246.02	246.13	246.25	246.36	246
9	246.58	246.70	246.81	246.92	247.03	247.15	247.26	247.37	247.48	247.6
22.0	247.71	247.82	247.93	248.05	248.16	248.27	248.38	248.50	248.61	248.7
1	248.83	248.95	249.06	249.17	249.29	249.40	249.51	249.62	249.74	249.8
2	249.96	250.07	250.19	250.30	250.41	250.52	250.64	250.75	250.86	250.9
3	251.09	251.20	251.31	251.42	251.54	251.65	251.76	251.88	251.99	252.
4	252.21	252.33	252.44	252.55	252.66	252.78	252.89	253.00	253.11	253.5
5	253.34	253.45	253.56	253.68	253.79	253.90	254.01	254.13	254.24	254.3
6	254.46	254.58	254.69	254.80	254.92	255.03	255.14	255.25	255.37	255.4
7	255.59	255.70	255.82	255.93	256.04	256.15	256.27	256.38	256.49	256.6
8	256.72	256.83	256.94	257.05	257.17	257.28	257.39	257.50	257.62	257.3
9	257.84	257.96	258.07	258.18	258.29	258.41	258.52	258.63	258.74	258.8
23.0	258.97	259.08	259.19	259.31	259.42	259.53	259.64	259.76	259.87	259.9
1	260.09	260.21	260.32	260.43	260.54	260.66	260.77	260.88	261.00	261.1
2	261.22	261.33	261.45	261.56	261.67	261.78	261.90	262.01	262.12	262.2
3	262.35	262.46	262.57	262.68	262.80	262.91	263.02	263.13	263.25	263.3
4	263.47	263.58	263.70	263.81	263.92	264.04	264.15	264.26	264.37	264.4
5	264.60	264.71	264.82	264.94	265.05	265.16	265.27	265.39	265.50	265.6
6	265.72	265.84	265.95	266.06	266.17	266.29	266.40	266.51	266.62	266.7
7	266.85	266.96	267.08	267.19	267.30	267.41	267.53	267.64	267.75	267.8
8	267.98	268.09	268.20	268.31	268.43	268.54	268.65	268.76	268.88	268.9
9	269.10	269.21	269.33	269.44	269.55	269.67	269.78	269.89	270.00	270.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

English				I	Iundredths	of an Incl	1.			
nches and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.liues.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines
24.0	270.23	270.34	270.45	270.57	270.68	270.79	270.90	271.02	271.13	271.24
1	271.35	271.47	271.58	271.69	271.80	271.92	272.03	272.14	272.25	272.3
2	272.48	272.59	272.71	272.82	272.93	273.04	273.16	273.27	273.38	273.49
3	273.61	273.72	273.83	273.94	274.06	274.17	274.28	274.39	274.51	274.63
4	274.73	274.84	274.96	275.07	275.18	275.29	275.41	275.52	275.63	275.73
5	275.86	275.97	276.08	276.20	276.31	276.42	276.53	276.65	276.76	276.8
6	276.98	277.10	277.21	277.32	277.43	277.55	277.66	277.77	277.88	278.00
7	278.11	278.22	278.33	278.45	278.56	278.67	278.79	278.90	279.01	279.1
8	279.24	279.35	279.46	279.57	279.69	279.80	279.91	280.02	280.14	280.2
9	280.36	280.47	280.59	280.70	280.81	280.92	281.04	281.15	281.26	281.38
25 .0	281.49	281.60	281.71	281.83	281.91	282.05	282.16	282.28	282.39	282.50
1	282.61	282.73	282.84	282.95	283.06	283.18	283.29	283.40	283.51	283.63
2	283.74	283.85	283.96	284.08	284.19	284.30	284.41	284.53	284.64	284.7
3	284.87	284.98	285.09	285.20	285.32	285.43	285.51	285.65	285.77	285.8
4	285.99	286.10	286.22	286.33	286.44	286.55	286.67	286.78	286.89	287.0
5	287.12	287.23	287.34	287.16	287.57	287.68	287.79	287.91	288.02	288.1
6	288.24	288.36	288.47	288.58	288.69	288.81	288.92	289.03	289.14	289.2
7	289.37	289.48	289.59	289.71	289.82	2 89.93	290.04	290.16	290.27	290.3
8	290.50	290.61	290.72	290.83	290.95	291.06	291.17	291.28	291.40	291.5
9	291.62	291.73	291.85	291.96	292.07	292.18	292.30	292.41	292.52	292.6
26 .0	292.75	292.86	292.97	293.08	293.20	293.31	293.42	293.54	293.65	293.7
1	293.87	293.99	294.10	294.21	294.32	294.44	294.55	291.66	294.77	294.8
2	295.00	295.11	295.22	295.34	295.45	295.56	295.67	295.79	295.90	296.0
3	296.12	296.24	296.35	296.16	296.58	296.69	296.80	296.91	297.03	297.1
4	297.25	297.36	297.48	297.59	297.70	297.81	297.93	298.04	298.15	298.2
5	293.38	298.49	298.60	298.71	298.83	298.94	299.05	299.17	299.28	299.3
6	299.50	299.62	299.73	299.84	299.95	300.07	300.18	300.29	300.40	300.5
7	300.63	300.74	300.85	300.97	301.08	301.19	301.30	301.42	301.53	301.6
8	301.75	301.87	301.98	302.09	302.20	302.32	302.43	302.54	302.66	302.7
9	302.88	302.99	303.11	303.22	303.33	303.44	303.56	303.67	303.78	303.8
27 .0	304.01	304.12	304.23	304.34	304.46	304.57	304.68	301.79	304.91	305.0
1	305.13	305.25	305.36	305.47	305.58	305.70	305.81	305.92	306.03	306.1
2	306.26	306.37	306.48	306.60	306.71	306.82	306.93	307.05	307.16	307.2
3	307.38	307.50	307.61	307.72	307.83	307.95	308.06	308.17	308.29	308.4
4	308.51	308.62	308.74	308.85	308.96	309.07	309.19	309.30	309.41	309.5
5	309.61	309.75	309.86	309.97	310.09	310.20	310.31	310.42	310.54	310.6
6	310.76	310.87	310.99	311.10	311.21	311.33	311.44	311.55	311.66	311.7
7	311.59	312.00	312.11	312.23	312.34	312.45	312.56	312.68	312.79	312.9
8	313.01	313.13	313.21	313.35	313.46	313.58	313.69	313.80	313.91	314.0
9	314.14	314.25	314.37	314.48	314.59	314.70	314.82	314.93	315.04	315.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 English Inch = 11.2595 French or Paris Lines.

English Inches and				I	Inndredth	s of an Inc	h.			
Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	1		Par.lines.			1			
28.0	315.27	315.38	315.49	315.60	315.72	315.83	315.94	316.05	316.17	316.28
1	316.39	316.50	316.62	316.73	316.84	316.95	317.07	317.18	317.29	317.4
2	317.52	317.63	317.74	317.86	317.97	318.08	318.19	318.31	318.42	318.5
3	318.61	318.76	318.87	318.98	319.09	319.21	319.32	319.43	319.54	319.6
4	319.77	319.88	319.99	320.11	320.22	320.33	320.45	320.56	320.67	320.7
5	320.90	321.01	321.12	321.23	321.35	321.46	321.57	321.68	321.80	321.9
6	322.02	322.13	322.25	322.36	322.47	322.58	322.70	322.81	322.92	323.0
7	323.15	323.26	323.37	323.49	323.60	323.71	323.52	323.94	324.05	324.1
8	324.27	324.39	324.50	324.61	324.72	324.84	324.95	325.06	325.17	325.2
9	325.40	325.51	325.62	325.74	325.85	325.96	326.08	326.19	326.30	326.4
29 .0	326.53	326.61	326.75	326.86	326.98	327.09	327.20	327.31	327.43	327.5
1	327.65	327.76	327.88	327.99	328.10	328.21	328.33	328.44	328.55	328.6
2	328.78	328.89	329.00	329.12	329.23	329.34	329.45	329.57	329.68	329.7
3	329.90	330.02	330.13	330.24	330.35	330.47	330.58	330.69	330.80	330.9
4	331.03	331.14	331.25	331.37	331.48	331.59	331.70	331.82	331.93	332.0
5	332.16	332.27	332.38	332.49	332.61	332.72	332.83	332.94	333.06	333 .1
6	333.28	333.39	333.51	333.62	333.73	333.84	333.96	334.07	334.18	334.2
7	334.41	334.52	334.63	334.74	334.86	334.97	335.08	335.20	335.31	335.43
8	335.53	335.65	335.76	335.S7	335.98	336.10	336.21	336.32	336.43	336.5
9	336.66	336.77	33 6. 88	337.00	337.11	337.22	337.33	337.45	337.56	337.6
30 .0	337.78	337.90	338.01	338.12	338.24	338.35	338.46	333.57	338.69	338.8
1	338.91	339.02	339.14	339.25	339.36	339.47	339.59	339.70	339.81	339.9
2	310.04	340.15	340.26	340.37	340.49	340.60	340.71	340.83	340.94	341.0
3	341.16	341.28	341.39	341.50	341.61	341.73	341.84	341.95	342.06	342.13
4	342.29	342.40	342.51	342.63	342.74	342.85	342.96	343.08	343.19	343.30
5	313.41	343.53	343.64	343.75	343.87	343.98	344.09	344.20	344.32	344.4
6	314.51	341.65	311.77	344.88	344.99	345.10	345.22	345.33	345.44	345.5
7	345.67	345.78	345.89	346.00	346.12	346.23	346.34	346.45	346.57	346.68
8	346.79	346.91	347 02	347.13	347.24	347.36	347.47	347.58	347.69	347.8
9	347.92	348.03	348.14	348.26	348.37	348.48	348.59	348.71	348.82	348.93
31.0	349.04	349.16	349.27	349.38	349.49	349.61	349.72	349.83	349.95	350.0
1	350.17	350.28	350.40	350.51	350.62	350.73	350.85	350.96	351.07	351.18
2	351.30	351.41	351.52	351.63	351.75	351.86	351.97	352.08	352.20	352.3
3	352.42	352.53	352.65	352.76	352.87	352.99	353.10	353.21	353.32	353.4
-4	353.55	353.66	353.77	353.89	354.00	354.11	354.22	354.34	354.45	354.50
5	351.67	354.79	354.90	355.01	355.12	355.24	355.35	355.46	355.57	355.69
6	355.80	355.91	356.03	356.14	356.25	356.36	356.48	356.59	356.70	356.8
				Thousan	dths of an	Inch.				
0.	1.	2.	3.	4.	;	5.	6.	7.	8.	9.
0.000	0.011	0.023	0.034	_\	-			0.079	0.090	0.101

III. - IV.

COMPARISON

OF

THE METRICAL BAROMETER

WITH

THE ENGLISH AND THE OLD FRENCH BAROMETERS,

OR

TABLES

FOR CONVERTING MILLIMETRES INTO ENGLISH INCHES AND DECIMALS, AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY MILLIMETRE FROM 250 TO 600; AND TO EVERY TENTH OF A MILLIMETRE FROM 600 TO 800 MILLIMETRES.

 \mathbf{C}



1 Metre = 39.37079 English Inches.

Millime- tres.		,			Millimetre	es. Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6	. 7	·	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. I	n. Eng.	In. Eng.	In	Eng. In.	Eng. In.
250	9.843	9.882	9.921	9.961	10.000	10.0				10.158	10.197
260	10.236	10.276	10.315	10.355	10.394	10.43	33 10.4	73 10.5	512	10.551	10.591
270	10.630	10.669	10.709	10.748	10.788	10.82	27 10.8	66 10.9	906	10.945	19.984
280	11.024	11.063	11.103	11.142	11.181	11.23	1	1		11.339	11.378
290	11.418	11.457	11.496	11.536	11.575	11.61	14 11.6	54 11.6	693	11.732	11.772
300	11.811	11.851	11.890	11.929	11.969	12.00	08 12.0	47 12.0	087	12.126	12.166
310	12.205	12.244	12.284	12.323	12.362	12.40	2 12.4	41 12.4	181	12.520	12.559
320	12.599	12.638	12.677	12.717	12.756	12.79	5 12.8	35 12.8	374	12.914	12.953
3 30	12.992	13.032	13.071	13.110	13.150	13.18	89 13.2	29 13.2	268	13.307	13.547
340	13.386	13.425	13.465	13.504	13.544	13.58	3 13.6	22 13.6	662	13.701	13.740
3 50	13.780	13.819	13.859	13.898	13.937	13.97	1	- 1	- 1	14.095	14.134
360	14.173	14.213	14.252	14.292	14.331	14.37	-	1		14.488	14.528
370	14.567	14.607	14.646	14.685	14.725	14.76		1		14.882	14.922
380	14.961	15.000	15.040	15.079	15.118	15.15	8 15.1	97 15.2	236	15.276	15.315
390	15.355	15.494	15.433	15.473	15.512	15.55	51 15.59	91 15.6	530	15.670	15.709
400	15.748	15.788	15.827	15.866	15.906	15.94	5 15.9	85 16.0)24	16.063	16.103
410	16.142	16.181	16.221	16.260	16.300	16.33	9 16.3	78 16.4	118	16.458	16.496
420	16.536	16.575	16.614	16.654	16.693	16.73	3 16.7	72 16.8	11	16.851	16.890
430	16.929	16.969	17.008	17.048	17.087	17.12	6 17.10	66 17.2	205	17.244	17.284
440	17.323	17.362	17.402	17.441	17.481	17.52	0 17.5	59 17.5	99	17.638	17.677
450	17.717	17.756	17.796	17.835	17.874	17.91	4 17.9	53 17.9	92	18.032	18.071
460	18.111	18.150	18.189	18.229	18.268	18.30	7 18.3	47 18.3	86	18.426	18.465
470	18.504	18.544	18.583	18.622	18.662	18.70	11 18.7	10 18.7	80	18.819	18.859
480	18.898	18.937	18.977	19.016	19.055	19.09	5 19.13	34 19.1	74	19.213	19.252
490	19.292	19.331	19.370	19.410	19.449	19.48	9 19.5	28 19.5	67	19.607	19.646
500	19.685	19.725	19.764	19.804	19.843	19.88				20.000	20.040
510	20.079	20.118	20.158	20.197	20.237	20.27	1	1	1	20.394	20.433
520	20.473	20.512	20.552	20.591	20.630	20.67	- 1		- 1	20.788	20.827
530 540	20.867 21.260	20.906 21.300	20.945 21.339	20.985 21.378	$21.024 \\ 21.418$	$21.06 \\ 21.45$	1	1 '	- 1	$21.181 \\ 21.575$	21.221 21.615
550	21.654	21.693	91 4 99	91 ****	21.811	91 0=			20 .	91 060	22.008
560	22.048	22.087	21.733 22.126	21.772 22.166	22,205	$21.85 \\ 22.24$	1	l l	- 1	21.969 22.363	22.402
570	22.441	22.481	22.520	22.559	22.599	22.24				$\frac{22.505}{22.756}$	22.402
580	22.835		22.914			23.03		1 23.1	- 1	23.150	23.189
590	23.229	23.268	23.308	23.347	23.386	23.42	i	1	- 1	23.544	23.583
1				Tenths	of Millime	etres.		1			
0.	1.	2.	3.	4.	5	i.	6.	7.	Ī	8.	9.
0.000	0.004	0.008	0.012	0.01	6 0.0)20	0.024	0.028	0.	.031	0.035

 $1~{\rm Metre} = 39.37079~{\rm English~Inches}.$

Millime-					Tenths of 1	Millimetres	·			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. 1
600	23.622	23.626	23.630	23.634	23.638	23.642	23.646	23.650	23.654	23.63
601	23.662	23.666	23.670	23.674	23.678	23.682	23.685	23.689	23.693	23.69
602	23.701	23.705	23.709	23.713	23.717	23.721	23.725	23.729	23.733	23.73
603	23.741	23.745	23.748	23.752	23.756	23.760	23.764	23.768	23.772	23.7
601	23.780	23.784	23.788	23.792	23.796	23.800	23.804	23.808	23.811	23.8
605	23.819	23.823	23.827	23.831	23.835	23.839	23.843	23.847	23.851	23.8
606	23.859	23.863	23.867	23.871	23.874	23.878	23.882	23.886	23.890	23.8
607	23.898	23.902	23.906	23.910	23.914	23.918	23.922	23.926	23.930	23.9
608	23.937	23.941	23.945	23.949	23.953	23.957	23.961	23.965	23.969	23.9
609	23.977	23.981	23.985	23.989	23.993	23.996	24.000	24.004	24.008	24.0
610	24.016	24.020	24.024	24.028	24.032	24.036	24.040	24.044	24.048	24.0
611	24.056	24.059	24.063	24.067	24.071	24.075	24.079	24.083	24.087	24.0
612	24.095	24.099	24.103	24.107	24.111	24.115	24.119	24.122	24.126	24.1
613	24.134	24.138	24.142	24.146	24.150	24.154	24.158	24.162	24.166	24.1
614	24.174	24.178	24.182	24.185	24.189	24.193	24.197	24.201	24.205	24.2
615	24.213	24.217	24.221	24.225	24.229	24.233	24.237	24.241	24.245	24.2
616	24.252	24.256	24.260	24.264	24.268	24.272	24.276	24.280	24.284	24.2
617	24.292	24.296	24.300	24.304	24.308	24.311	24.315	24.319	24.323	24.3
618	24.331	24.335	24.339	24.343	24.347	24.351	24.355	24.359	24.363	24.3
619	24.371	24.374	24.378	24.382	24.386	24.390	24.394	24.398	24.402	24.4
620	24.410	24.414	24.418	24.422	24.426	24.430	24.434	24.437	24.441	24.4
621	24.449	24.453	24.457	24.461	24.465	24.469	24.473	24.477	24.481	24.4
622	24.489	24.493	24.197	24.500	24.504	24.508	24.512	24.516	24.520	24.5
623	24.528	24.532	24.536	24.540	24.544	24.548	24.552	24.556	24.559	24.5
624	24.567	24.571	24.575	24.579	24.583	24.587	24.591	24.595	24.599	24.6
625	24.607	24.611	24.615	24.619	24.622	24.626	24.630	24.634	24.638	24.6
626	24.646	24.650	24.654	24.658	24.662	24.666	24.670	24.674	24.678	24.6
627	24.685	24.689	24.693	24.697	24.701	24.705	24.709	24.713	24.717	24.7
628	24.725	24.729	24.733	24.737	24.741	24.745	24.748	24.752	24.756	24.7
629	24.764	24.768	24.772	24.776	24.780	24.784	24.788	24.792	24.796	24.8
630	24.804	24.808	24.811	24.815	24.819	24.823	24.827	24.831	24.835	24.8
631	24.843	24.847	24.851	24.855	24.859	24.863	24.867	24.871	24.874	24.8
632	24.882	24.886	24.890	24.894	24.898	24.902	24.906	24.910	24.914	24.9
633	24.922	24.926	24.930	24.934	24.937	24.941	24.945	24.949	24.953	24.9
634	24.961	24.965	24.969	24.973	24.977	24.981	24.985	24.989	24.993	24.99
635	25.000	25.004	25.008	25.012	25.016	25.020	25.024	25.028	25.032	25.0
636	25.040	25.044	25.048	25.052	25.056	25.060	25.063	25.067	25.071	25.0
637	25.079	25.083	25.087	25.091	25.095	25.099	25.103	25.107	25.111	25.11
638	25.119	25.123	25.126	25.130	25.134	25.138	25.142	25.146	25.150	25.15
639	25.158	25.162	25.166	25.170	25.174	25.178	25.182	25.185	25.189	25.19
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches

Millime-					Tenths of	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In
640	25.197	25.201	25.205	25.209	25.213	25.217	25.221	25.225	25.229	25.23
641	25.237	25.241	25.245	25.248	25.252	25 256	25.260	25.264	25.268	25.27
642	25.276	25.280	25.284	25.288	25.292	25.296	25.300	25.304	25.308	25.31
643	25.315	25.319	25.323	25.327	25.331	25.335	25.339	25.343	25.347	25.35
644	25.355	25.359	25.363	25.367	25.371	25.374	25.378	25.382	25.386	25.39
645	25.394	25.398	25.402	25.406	25.410	25.414	25.418	25.422	25.426	25.43
646	25.434	25.437	25.441	25.445	25.449	25.453	25.457	25.461	25.465	25.46
647	25.473	25.477	25.481	25.485	25.489	25.493	25.497	25.500	25.504	25.50
648	25.512	25.516	25.520	25.524	25.528	25.532	25.536	25.540	25.544	25.54
649	25.552	25.556	25.560	25.563	25.567	25.571	25.575	25.579	25.583	25.58
650	25.591	25.595	25.599	25.603	25.607	25.611	25.615	25.619	25.623	25.62
651	25.630	25.634	25.638	25.642	25.646	25.650	25.654	25.658	25.662	25.66
652	25.670	25.674	25.678	25.682	25.686	25.689	25.693	25.697	25.701	25.70
653	25.709	25.713	25.717	25.721	25.725	25.729	25.733	25.737	25.741	25.74
654	25.748	25.752	25.756	25.760	25.764	25.768	25.772	25.776	25.780	25.78
655	25.788	25.792	25.796	25.800	25.804	25.808	25.811	25.815	25.819	25.82
656	25.827	25.831	25.835	25.839	25.843	25.847	25.851	25.855	25.859	25.86
657	25.867	25.871	25.874	25.878	25.882	25.886	25.890	25.894	25.898	25.90
65S	25.906	25.910	25.914	25.918	25.922	25.926	25.930	25.934	25.937	25.94
659	25.945	25.949	25.953	25.957	25.961	25.965	25.969	25.973	25.977	25.98
660	25.985	25.989	25.993	25.997	26.000	26.004	26.008	26.012	26.016	26.02
661	26.024	26.028	26.032	26.036	26.040	26.044	26.048	26.012	26.056	26.06
1	26.063	26.025		26.036	26.079	26.083		26.091		26.09
662	1		26.071				26.087		26.095	
663 664	26.103 26.142	26.107 26.146	26.111 26.150	26.115 26.154	26.119 26.158	$26.123 \\ 26.162$	26.126 26.166	26.130 26.170	26.134 26.174	26.13 26.17
	20.222	20.725	20 - 22	20.202		00.000	20.225	22.222	20.5==	
665	26.182	26.186	26.189	26.193	26.197	26.201	26.205	26.209	26.213	26.21
666	26 221	26.225	26.229	26.233	26.237	26.241	26.245	26.249	26.252	26.25
667	26.260	26.264	26.268	26.272	26.276	26.280	26.284	26.288	26.292	26.29
668 669	26.300 26.339	26.304 26.343	26.308 26.347	26.311 26.351	26.315 26.355	26.319 26.359	26.323 26.363	26.327 26.367	26.331 26.371	26.33 26.37
670	26.378	26.382	26.386	26.390	26.394	26.398	26.402	26.406	26.410	26.41
671	26.418	26.422	26.426	26.430	26.434	26.437	26.441	26.445	26.449	26.45
672	26.457	26.461	26.465	26.469	26.473	26.477	26.481	26.485	26.489	26.49
673	26.197	26.500	26.504	26.508	26.512	26.516	26.520	26.524	26.528	26.53
674	26.536	26.540	26.544	26.548	26.552	26.556	26.560	26.563	26.567	26.57
675	26.575	26.579	26.583	26.587	26.591	26.595	26.599	26.603	26.607	26.61
676	26.615	26.619	26.623	26.626	26.630	26.634	26.638	26.642	26.646	26.650
677	26.654	26.658	26.662	26.666	26.670	26.674	26.678	26.682	26.686	26.68
678	26.693	26.697	26.701	26.705	26.709	26.713	26.717	26.721	26.725	26.72
679	26.733	26.737	26.741	26.745	26.749	26.752	26.756	26.760	26.764	26.76
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-					Tenths of 1	dillimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng In.	Eng. In	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. I
680	26.772	26.776	26.780	26.784	26.788	26.792	26.796	26.800		26.80
681	26.812	26.815	26.819	26.823	26.827	26.831	26.835	26.839	26.843	26.84
682	26.851	26.855	26.859	26.863	26.867	26.871	26.875	26.878	26.882	26.88
683	26.890	26.894	26.898	26.902	26.906	26.910	26.914	26.918	26.922	26.92
684	26.930	26.934	26.937	26.941	26.945	26.949	26.953	26.957	26.961	26.96
685	26.969	26.973	26.977	26.981	26.985	26.989	26.993	26.997	27.000	27.00
686	27.008	27.012	27.016	27.020	27.024	27.028	27.032	27.036	27.040	27.0-
687	27.048	27.052	27.056	27.060	27.063	27.067	27.071	27.075	27.079	27.08
658	27.087	27.091	27.095	27.099	27.103	27.107	27.111	27.115	27.119	27.12
689	27.126	27.130	27.134	27.138	27.142	27.146	27.150	27.154	27.158	27.16
690	27.166	27.170	27.174	27.178	27.182	27.186	27.189	27.193	27.197	27.20
691	27.205	27.209	27.213	27.217	27.221	27.225	27.229	27.233	27.237	27.2
692	27.245	27.249	27.252	27.256	27.260	27.264	27.268	27.272	27.276	27.28
693	27.284	27.288	27.292	27.296	27.300	27.304	27.308	27.312	27.315	27.31
694	27.323	27.327	27.331	27.335	27.339	27.343	27.347	27.351	27.355	27.35
695	27.363	27.367	27.371	27.375	27.378	27.382	27.386	27.390	27.394	27.39
696	27.402	27.406	27.410	27.414	27.418	27.422	27.426	27.430	27.434	27.43
697	27.441	27.445	27.449	27.453	27.457	27.461	27.465	27.469	27.473	27.47
698	27.481	27.485	27.489	27.493	27.497	27.500	27.504	27.508	27.512	27.51
699	27.520	27.524	27.528	27.532	27.536	27.540	27.544	27.548	27.552	27.5
700	27.560	27.563	27.567	27.571	27.575	27.579	27.583	27.587	27.591	27.59
701	27.599	27.603	27.607	27.611	27.615	27.619	27.623	27.626	27.630	27.63
702	27.638	27.612	27.646	27.650	27.654	27.658	27.662	27.666	27.670	27.67
703	27.678	27.682	27.686	27.689	27.693	27.697	27.701	27.705	27.709	27.7
704	27.717	27.721	27.725	27.729	27.733	27.737	27.741	27.745	27.749	27.7
705	27.756	27.760	27.764	27.768	27.772	27.776	27.780	27.784	27.788	27.79
706	27.796	27.800	27.804	27.808	27.812	27.815	27.819	27.823	27.827	27.8
707	27.835	27.839	27.843	27.847	27.851	27.855	27.859	27.863	27.867	27.8
708	27.875	27.878	27.882	27.886	27.890	27.894	27.898	27.902	27.906	27.9
709	27.914	27.918	27.922	27.926	27.930	27.934	27.938	27.941	27.945	27.9
710	27.953	27.957	27.961	27.965	27.969	27.973	27.977	27.981	27.985	27.98
711	27.993	27.997	28.001	28.004	28.008	28.012	28.016	28.020	28.024	28.0
712	28.032	28.036	28.010	28.044	28.048	28.052	28.056	28.060	28.063	28.00
713	28.071	28.075	28.079	28.083	28.087	28.091	28.095	28.099	28.103	28.10
714	28.111	28.115	28.119	28.123	28.126	28.130	28.134	28.138	į.	i
715	28.150	28.154	28.158	28.162	28.166	28.170	28.174	28.178	28.182	28.18
716	28.189	28.193	28.197	28.201	28.205	28.209	28.213	28.217	28.221	28.23
717	28.229	28.233	28.237	28.241	28.245	28.249	28.252	28.256	28.260	28.20
718	28.268	28.272	28.276	28.280	28.284	28.288	28.292	28.296	28.300	28.30
719	28.308	28.312	28.315	28.319	28.323	28.327	28.331	28.335	28.339	28.3
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 39.37079 English Inches.

Millime-					Tenths of	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. Ir
720	28.347	28.351	28.355	28.359	28.363	28.367	28.371	28.375	28.378	28.38
721	28.386	28.390	28.394	28.398	28.402	28.406	28.410	28.414	28.418	28.42
722	28.426	28.430	28.434	28.438	28.441	28.445	28.449	28.453	28.457	28.46
723	28.465	28.469	28.473	28.477	28.481	28.485	28.489	28.493	28.497	28.50
724	28.504	28.508	28.512	28.516	28.520	28.524	28.528	28.532	28.536	28.54
725	28.544	28.548	28.552	28.556	28.560	28.564	28.567	28.571	28.575	28.57
726	28.583	28.587	28.591	28.595	28.599	28.603	28.607	28.611	28.615	28.61
727	28.623	28.627	28.630	28.634	28.638	28.642	28.646	28.650	28.654	28.65
728	28.662	28.666	28.670	28.674	28.678	28.682	28.686	28.689	28.693	28.69
72 9	28.701	28.705	28.709	28.713	28.717	28.721	28.725	28.729	28.733	28.73
730	28.741	28.745	28.749	28.752	28.756	28.760	28.764	28.768	28.772	28.77
731	28.780	28.784	28.788	28.792	28.796	28.800	28.804	28.808	28.812	28.81
732	28.819	28.823	28.827	28.831	28.835	28.839	28.843	28.847	28.851	28.85
733	28.859	28.863	28.867	28.871	28.875	28.878	28.882	28.886	28.890	28.89
734	28.898	28.902	28.906	28.910	28.914	28.918	28.922	28.926	28.930	28.93
735	28.938	28.941	28.945	28.949	28.953	28.957	28.961	28.965	28.969	28.97
736	28.977	28.981	28.985	28.989	28.993	28.997	29.001	29.004	29.008	29.01
737	29.016	29.020	29.024	29.028	29.032	29.036	29.040	29.044	29.048	29.05
738	29.056	29.060	29.064	29.067	29.071	29.075	29.079	29.083	29.087	29.09
739	29.095	29.099	29.103	29.107	29.111	29.115	29.119	29.123	29.127	29.13
740	29.134	29.138	29.142	29.146	29.150	29.154	29.158	29.162	29.166	29.17
741	29.174	29.178	29.182	29.186	29.190	29.193	29.197	29.201	29.205	29.20
742	29.213	29.217	29.221	29.225	29.229	29.233	29.237	29.241	29.245	29.24
743	29.252	29.256	29.260	29.264	29.268	29.272	29.276	29.280	29.284	29.24
744	29.292	29.296	29.300	29.304	29.308	29.312	29.315	29.319	29.323	29.32
	29.331	29.335	29.339	29.343	00.04*	29.351	29.355	29.359	00.000	20.20
745	29.331	29.335	29.378	29.343	29.347 29.386	29.391	29.394	29.398	29.363	29.36
746	29.410					29.430			29.402	29.40
747	29.449	29.414 29.453	29.418	29.422 29.461	29.426	29.469	29.434 29.473	29.438	29.441	29.44
748 749	29.449	29.493	29.457 29.497	29.461	29.465 29.504	29.508	29.473	29.477 29.516	29.481 29.520	29.48 29.52
750	90 590	20 520	90 590	90 5 10	20 5 4 4	29.548	00 550	20 550	90 #00	20.50
750	29.528 29.567	29.532 29.571	29.536	29.540	29.544		29.552	29.556	29.560	29.56
751 752	29.607	29.611	29.575 29.615	29.579 29.619	29.583 29.623	29.587 29.627	29.591 29.630	29.595 29.634	29.599 29.638	29.60
753	29.646	29.650	29.654	29.658	29.662	29.666	29.670	29.674	29.678	29.64
754	29.686		29.693	29.697	29.701	29.705	29.709	29.713		29.683 29.72
755	29.725	29.729	29.733	29.737	29.741	29.745	29.749	29.753	29.756	29.76
756	29.764	29.768	29.772	29.776	29.780	29.784	29.788	29.792	29.796	29.800
757	29.804	29.808	29.812	29.815	29.819	29.823	29.827	29.831	29.835	29.839
758	29.843	29.847	29.851	29.855	29.859	29.863	29.867	29.871	29.875	29.878
759	29.882	29.886	29.890	29.894	29.898	29.902	29.906	29.910	29.914	29.91

1 Metre = 39.37079 English Inches.

Millime-					Tenths of	Millime	tres.				
tres.	0.	1.	2.	3.	4.	5	. 6		7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng In.	Eng. In.	Eng.		In.	Eng. In	Eng. In.	Eng. In
760	29.922	29.926	29.930	29.934	29.938	29.9	41 29.9	145	29.949	29.953	29.95
761	29,961	29.965	29.969	29.973	29.977	29.9	81 29.9	85	29.989	29.993	29.99
762	30.001	30.004	30.008	30.012	30.016	30.0	20 30.0	21 :	30.028	30.032	30.03
763	30.040	30.011	30.048	30.052	30.056	30.0	$60 \mid 30.6$	64	30.067	30.071	30 07
764	30.079	30.033	30.087	30.091	30.095	30.0	99 30.1	103	30.107	30.111	30.11
765	30.119	30.123	30.127	30.130	30.134	30.1	f	42	30.146	30.150	30.15
766	30.153	30.162	30.166	30.170	30.174	30.1	- 1	- 1	30.156		30.19
767	30.197	30.201	30.205	30.209	30.213	30.2	1	21 3	30.225	30.229	30.23
768	30.237	30.241	30.245	30.249	30.253	30.2	$56 \mid 30.2$	60	30.264	30.268	30.27
769	30.276	30.280	30.284	30.288	30.292	30.2	96 30.3	: 00	30.304	30.308	30.31
770	30.316	30.319	30.323	30.327	30.331	30.3	35 30.3	39 :	30.343	30.347	30.35
771	30.355	30.359	30.363	30.367	30.371	30.3	75 30.3	79	30.382	30.386	30.39
772	30.394	30.398	30.402	30.406	30.410	30.4	14 30.4	18 :	30.422	30.426	30.43
773	30.434	30.438	30.441	30.445	30.449	30.4	53 30.4	57 5	30.461	30.465	30.46
774	30.473	30.477	30.481	30.485	30.489	30.49	93 30.4	97 :	30.501	30.504	30.50
775	30.512	30.516	30.520	30.524	30.528	30.5	32 30.5	36	30.540	30.544	30.54
776	30.552	30.556	30.560	30.561	30.567	30.5	71 30.5	75 3	30.579	30.583	30.58
777	30.591	30.595	30.599	30.603	30.697	30.6	$11 \mid 30.6$	15 8	30.619	30.623	30.62
778	30.630	30.634	30.638	30.642	30.646	30.6	$50 \mid 30.6$	54 3	80.658	30,662	30.66
779	30.670	30.674	30.678	30.682	30.686	30.69	90 30.6	93 8	30.697	30.701	30.70
7 80	30.709	30.713	30.717	30.721	30.725	30.7	29 30.7	33	30.737	30.741	30.74
781	30.749	30.753	30.756	30.760	30.761	30.70	68 30 .7	72	30.776	30.780	30.78
782	30.788	30.792	30.796	30.500	30.804	30.80	$08 \mid 30.8$	12 3	30.816	30.819	30.82
783	30.827	30.831	30.835	30.839	30.843	30.8	47 30.8	51 3	30.855	30.859	30.86
784	30.867	30.871	30.875	30.579	30.882	30.8	86 30.8	90 3	30.894	30.898	30.90
785	30.906	30.910	30.914	30.918	30.922	30.93			30.934	1	30.94
7 86	30.945	30.949	30.953	30.957	30.961	30.90			30.973		30.98
787	30.985	30.989	30.993	30.997	31.001	31.00	1		31.012	1	31.02
788	31.024	31.028	31.032	31.036	31.040	31.0			31.052	i	31.06
789	31.064	31.067	31.071	31.075	31.079	31.08	83 31.0	87 3	31.091	31.095	31.09
790	31.103	31.107	31.111	31.115	31.119	31.13		- 1	31.130	1	31.13
791	31.142	31.146	31.150	31.154	31.158	31.10		- 1	31.170	1	31.17
792	31.182	31.186	31.190	31.193	31.197	31.20			31.209	1	31.21
793	31.221	31.225	31.229	31.233	31.237	31.2		- 1	1.249	31.253	31.25
994	31.260	31.264	31.268	31.272	31.276	31.28		- 1	1.288	31.292	31.29
795	31.300	31.304	31.308	31.312	31.316	31.3		1	1.327	31.331	31.33
796	31.339	31.343	31.347	31.351	31.355	31.33		63 3	1.367	31.371	31.37
797	31.379	31.382	31.386	31.390	31.394	31.39	$98 \mid 31.4$	02 3	1.406	31.410	31.41
79S	31.418	31.422	31.426	31.430	31.434	31.43	i		1.445	31.449	31.45
799	31.157	31.461	31.465	31.469	31.473	31.47	1		1.485	31.489	31.49
800	31.497	31.501	31.505	31.508	31.512	31.5	16 31.5	20 3	1.524	31.528	31.53:
				Hundredtl	ns of Millin	metres.					
0.	1.	2.	3.	4.	5	·	6.	7		8.	9.
.0000	.0001	.0008	.0012	- 	—i—						

1 Millimetre = 0.443296 French or Paris Line.

Millimetres					Millimetr	es. Uni	ts.			
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines	Par.lines	Par.lines	Par.lines.	Par.line	es. Par.lines	Par.lines.	Par.lines.	Par.lines.
300	132.99	133.43	133.88	134.32	134.76	135.2	1 135.65	136.09	136.54	136.98
310	137.42	137.87	138.31	138.75	139.19	139.6	4 140.08	140.52	140.97	141.41
320	141.85	142.30	142.74	143.18	143.63	144.0	7 144.51	1	145.40	145.84
330	146.29	146.73	147.17	147.62	148.06	148.5	1		149.83	150.28
340	150.72	151.16	151.61	152.05	152.49	152.9	4 153.38	153.82	154.27	154.71
350	155.15	155.60	156.04	156.48	156.93	157.3	1	1	158.70	159.14
360	159.59	160.03	160.47	160.92	161.36	161.8	1	1	163.13	163.58
370	164.02	164.46	164.91	165.35	165.79	166.2	1	1	167.57	168.01
380	168.45	168.90	169.34	169.78	170.23	170.6	7 171.11	171.56	172.00	172.44
390	172.89	173.33	173.77	174.22	174.66	175.1	0 175.55	175.99	176.43	176.88
400	177.32	177.76	178.20	178.65	179.09	179.5	3 179.99	180.42	180.86	181.31
410	181.75	182.19	182.64	183.08	183.52	183.9	7 184.41	184.85	185.30	185.74
420	186.18	186.63	187.07	187.51	187.96	188.4	0 188.8	189.29	189.73	190.17
430	190.62	191.06	191.50	191.95	192.39	192.8	3 193.28	193.72	194.16	194.61
440	195.05	195.49	195.94	196.38	196.82	197.2	7 197.7	198.15	198.60	199.04
450	199.48	199.93	200.37	200.81	201.26	201.7	0 202.1-	202.59	203.03	203.47
460	203.92	204.36	204.80	205.25	205.69	206.1	3 206.58	207.02	207.46	207.91
470	208.35	208.79	209.24	209.68	210.12	210.5	7 211.01	211.45	211.90	212.34
480	212.78	213.23	213.67	214.11	214.56	215.0	0 215.4	1 215.88	216.33	216.77
490	217.22	217.66	218.10	218.54	218.99	219.4	3 219.83	7 220.32	220.76	221.20
500	221.65	222.09	222.53	222.98	223.42	223.8	66 224.3	224.75	225.19	225.64
510	226.08	226.52	226.97	227.41	227.85	228.8	$0 \mid 228.7$	1 229.18	229.63	230.07
520	230.51	230.96	231.40	231.84	232.29	232.7	$73 \mid 233.1^{\circ}$	$7 \mid 233.62$	234.06	234.50
530	234.95	235.39	235.83	236.28	236.72	237.1	6 237.6	1 238.05	238.49	238.94
540	239.38	239.82	240.27	240.71	241.15	241.6	60 242.0	1 242.48	242.93	243.37
5 50	243.81	244.26	244.70	245.14	245.59	246.0	3 246.4	7 246.92	247.36	247.80
560	248.25	248.69	249.13	249.57	250.01	250	16 250.9	$1 \mid 251.35$	251.79	252.24
570	252.68	253.12	253.57	254.01	254.45	254.9			1	256.67
580	257.11	257.55	258.00	258.44	258.88	259.3	1	1		261.10
590	261.54	261.99	262.43	262.87	263.32	263.7	76 264.2	0 264.65	265.09	265.53
		<u> </u>		Tenths	of Millim	etres.				
0.	1.	2.	3.	4.	1 6	i.	6.	7.	8.	9.
0.000	0.044	0.089	0.133	0.17	7. 0.5	222	0.266	0.310	0.355	0.399
	1		1	Hundred	ths of Mill	imetres.				
0.000	0.004	0.009	0.013	0.018	8 0.0	22	0.027	0.031	0.035	0.040

1 Millimetre = 0.443296 French Line.

Millime-				'	Tenths of I	Hillimetres	•			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
600	265.98	266.02	266.07	266.11	266.15	266.20	266.24	266.29	266.33	266.3
601	266.42	266.47	266.51	266.55	266.60	266.64	266.69	266.73	266.78	266.8
602	266.86	266.91	266.95	267.00	267.04	267.09	267.13	267.17	267.22	267.2
603	267.31	267.35	267.40	267.44	267.48	267.53	267.57	267.62	267.66	267.7
604	267.75	267.80	267.84	267.88	267.93	267.97	268.02	268.06	268.11	268.1
605	265.19	268.24	268.28	268.33	268.37	268.42	268.46	268.50	268.55	268.5
606	268.64	268.68	268.73	268.77	268.81	268.86	268.90	268.95	268.99	269.0
607	269.08	269.13	269.17	269.21	269.26	269.30	269.35	269.39	269.44	269
608	269.52	269.57	269.61	269.66	269.70	269.75	269.79	269.83	269.88	269.9
609	269.97	270.01	270.06	270.10	270.14	270.19	270.23	270.28	270.32	270.5
610	270.41	270.45	270.50	270.54	270.59	270.63	270.68	270.72	270.77	270.8
611	270.85	270.90	270.94	270.99	271.03	271.08	271.12	271.16	271.21	271.2
612	271.30	271.34	271.39	271.43	271.47	271.52	271.56	271.61	271.65	271.
613	271.74	271.78	271.83	271.87	271.92	271.96	272.01	272.05	272.10	272.
614	272.18	272.23	272.27	272.32	272.36	272.41	272.45	272.49	272.54	272.
615	272.63	272.67	272.72	272.76	272.80	272.85	272.89	272.94	272.98	273.0
616	273.07	273.11	273.16	273.20	273.25	273.29	273.34	273.38	273.42	273.
617	273.51	273.56	273.60	273.65	273.69	273.74	273.78	273.82	273.87	273.9
618	273.96	274.00	274.05	274.09	274.13	274.18	274.22	274.27	274.31	274.
619	274.40	274.44	274.49	274.53	274.58	274.62	274.67	274.71	274.75	274.8
620	274.84	274.89	274.93	274.98	275.02	275.07	275.11	275.15	275.20	275.2
621	275.29	275.33	275.38	275.42	275.46	275.51	275.55	275.60	275.64	275.0
622	275.73	275.77	275.82	275.86	275.91	275.95	276.00	276.04	276.08	276.
623	276.17	276.22	276.26	276.31	276.35	276.38	276.44	276.48	276.53	276.
624	276.62	276.66	276.71	276.75	276.79	276.84	276.88	276.93	276.97	277.0
625	277.06	277.10	277.15	277.19	277.24	277.28	277.33	277.37	277.41	277.
626	277.50	277.55	277.59	277.64	277.58	277.72	277.77	277.81	277.86	277.
627	277.95	277.99	278.04	278.08	278.12	278.17	278.21	278.26	278.30	278.
628	278.39	278.43	278.48	278.52	278.57	278.61	278.66	278.70	278.74	278.
629	278.83	278.88	278.92	278.97	279.01	279.05	279.10	279.14	279.19	279.
630	279.28	279.32	279.37	279.41	279.45	279.50	279.54	279.59	279.63	279.
631	279.72	279.76	279.81	279.85	279.90	279.94	279.99	280.03	280.07	280,
632	280.16	280.21	280.25	280.30	280.34	280.38	280.43	280.47	280.52	280.
633	280.61	280.65	280.70	280.74	280.78	280.83	280.87	280.92	280.96	281.0
634	281.05	281.09	281.14	281.18	281.23	281.27	281.32	281.36	281.40	281.
635	281.49	281.54	281.58	281.63	281.67	281.71	281.76	281.80	281.85	281.
636	281.91	281.98	282.02	282.07	282.11	282.16	282.20	282.25	282.29	282.3
637	282.38	282.42	282.47	282.51	282.56	282.60	282.65	282.69	282.73	282.
638	282.82	282.87	282.91	282.96	283.00	283.04	283.09	283.13	283.18	283.2
639	283.27	283.31	283.35	283.40	283.44	283.49	283.53	283.58	283.62	283.
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

 $1 \ {\rm Millimetre} = 0.443296 \ {\rm French \ Line}.$

fillime-				,	Tenths of I	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lin
640	283.71	283.75	283.80	283.84	283.89	283.93	283.98	284.02	284.06	284.1
641	284.15	284.20	284.24	284.29	284.33	284.37	284.42	284.46	284.51	284.
642	284.60	284.64	284.68	284.73	284.77	284.82	284.86	284.91	284.95	284.9
643	285.04	285.08	285.13	285.17	285.22	285.26	285.31	285.35	285.39	285.
644	285.48	285.53	285.57	285.62	285.66	285.70	285.75	285.79	285.84	285.8
645	285.93	285.97	286.01	286.06	286.10	286.15	286.19	286.24	286.28	286.
646	286.37	286.41	286.46	286.50	286.55	286.59	286.64	286.68	286.72	286.
647	286.81	286.86	286.90	286.95	286.99	287.03	287.08	287.12	287.17	287.5
648	287.26	287.30	287.34	287.39	287.43	287.48	287.52	287.57	287.61	287.0
649	287.70	287.74	287.79	287.83	287.88	287.92	287.96	288.01	288.05	288.
650	288.14	288.19	288.23	288.28	288.32	288.36	288.41	288.45	288.50	288.
651	288.59	288.63	288.67	288.72	288.76	288.81	288.85	288.90	288.94	288.
652	289.03	289.07	289.12	289.16	289.21	289.25	289.29	289.34	289.38	289.
653	289.47	289.52	289.56	289.61	289.65	289.69	289.74	289.78	289.83	289.8
654	289.92	289.96	290.00	290.05	290.09	290.14	290.18	290.23	290.27	290.
655	290.36	290.40	290.45	290.49	290.54	290.58	290.62	290.67	290.71	290.
656	290.80	290.85	290.89	290.94	290.98	291.02	291.07	291.11	291.16	291.
657	291.25	291.29	291.33	291.38	291.42	291.47	291.51	291.56	291.60	291.
658	291.69	291.73	291.78	291.82	291.87	291.91	291.95	292.00	292.04	292.0
659	292.13	292.18	292.22	292.26	292.31	292.35	292.40	292.44	292.49	292.
660	292.58	292.62	292.66	292.71	292.75	292.80	292.84	292.89	292.93	292.9
661	293.02	293.06	293.11	293.15	293.20	293.24	293.28	293.33	293.37	293.
662	293.46	293.51	293.55	293.59	293.64	293.68	293.73	293.77	293.82	293.8
663	293.91	293.95	293.99	294.04	294.08	294.13	294.17	294.22	294.26	294.
664	294.35	294.39	294.44	294.48	294.53	294.57	294.61	294.66	294.70	294.
665	294.79	294.84	294.88	294.92	294.97	295.01	295.06	295.10	295.15	295.
666	295.24	295.28	295.32	295.37	295.41	295.46	295.50	295.55	295.59	295.
667	295.68	295.72	295.77	295.81	295.86	295.90	295.94	295.99	296.03	296.0
668	296.12	296.17	296.21	296.25	296.30	296.34	296.39	296.43	296.48	296.
669	296.56	296.61	296.65	296.70	296.74	296.79	296.S3	296.88	296.92	296.
670	297.01	297.05	297.10	297.14	297.19	297.23	297.27	297.32	297.36	297.
671	297.45	297.50	297.54	297.58	297.63	297.67	297.72	297.76	297.81	297.8
672	297.89	297.94	297.98	298.03	298.07	298.12	298.16	298.21	298.25	298.5
673	298.34	298.38	298.43	298.47	298.52	298.56	298.60	298.65	298.69	298.
674	298.78	298.83	298.87	298.91	298.96	299.00	299.05	299.09	299.14	299.1
675	299.22	299.27	299.31	299.36	299.40	299.45	299.49	299.54	299.58	299.6
676	299.67	299.71	299.76	299.80	299.85	299.89	299.93	299.98	300.02	300.0
677	300.11	300.16	300.20	300.24	300.29	300.33	300.38	300.42	300.47	300.5
678	300.55	300.60	300.64	300.69	300.73	300.78	300.82	300.86	300.91	300.9
679	301.00	301.04	301.09	301.13	301.18	301.22	301.26	301.31	301.35	301.
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

illima					Tenths of I	Millimetres				
illime- tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	1	Par.lines.		Par.lines.			Par.lines.			1
680	301.44	301.49	301.53	301.57	301.62	301.66	301.71	301.75	301.80	301.8
681	301.88	301.93	301.97	302.02	302.06	302.11	302.15	302.19	302.24	302.2
682	302.33	302.37	302.42	302.46	302.51	302.55	302.59	302.64	302.68	302.7
683	302.77	302.82	302.86	302.90	302.95	302.99	303.04	303.08	303.13	303.1
684	303.21	303.26	303.30	303.35	303.39	303.44	303.48	303.52	303.57	303.6
685	303.66	303.70	303.75	303.79	303.83	303.88	303.92	303.97	304.01	304.0
686	304.10	304.15	304.19	304.23	304.28	304.32	304.37	304.41	304.46	304.5
687	304.54	304.59	304.63	304.68	304.72	304.77	304.81	304.85	304.90	304.9
688	304.99	305.03	305.08	305.12	305.16	305.21	305.25	305.30	305.34	305.3
689	305.43	305.48	305.52	305.56	305.61	305.65	305.70	305.74	305.79	305.8
690	305.87	305.92	305.96	306.01	306.05	306.10	306.14	306.18	306.23	306.2
691	306.32	306.36	306.41	306.45	306.49	306.54	306.58	306.63	306.67	306.7
692	306.76	306.81	306.85	306.89	306.94	306.98	307.03	307.07	307.12	307.1
693	307.20	307.25	307.29	307.34	307.38	307.43	307.47	307.51	307.56	307.6
694	307.65	307.69	307.74	307.78	307.82	307.87	307.91	307.96	308.00	308.0
605	308.09	308.13	308.18	308.22	308.27	308.31	308.36	308.40	308.45	308.4
695	308.53			ļ.		308.76	308.80	308.84	308.89	308.9
696		308.58	308.62	308.67	308.71 309.15	309.20	309.24	309.29	309.33	309.3
697	308.98	309.02	309.07	309.11		309.64	309.69	309.73	309.78	309.8
698 699	309.42 309.86	309.46 309.91	309.51 309.95	309.55 310.00	309.60 310.04	310.09	310.13	310.17	310.22	310.2
700	310.31	310.35	310.40	310.44	310.48	310.53	310.57	310.62	310.66	310.7
701	310.75	310.79	310.84	310.88	310.93	310.97	311.02	311.06	311.11	311.1
702	311.19	311.24	311.28	311.33	311.37	311.42	311.46	311.50	311.55	311.5
703	311.64	311.68	311.73	311.77	311.81	311.86	311.90	311.95	311.99	312.0
704	312.08	312.12	312.17	312.21	312.26	312.30	312.35	312.39	312.43	312.4
705	312.52	312.57	312.61	312.66	312.70	312.75	312.79	312.83	312.88	312.9
706	312.97	313.01	313.06	313.10	313.14	313.19	313.23	313.28	313.32	313.3
707	313.41	313.45	313.50	313.54	313.59	313.63	313.68	313.72	313.76	313.8
703	313.85	313.90	313.94	313.99	314.03	314.08	314.12	314.16	314.21	314.2
709	314.30	314.34	314.39	314.43	314.47	314.52	314.56	314.61	314.65	314.7
710	314.74	314.78	314.83	314.87	314.92	314.96	315.01	315.05	315.09	315.1
711	315.18	315.23	315.27	315.32	315.36	315.41	315.45	315.49	315.54	315.5
712	315.63	315.67	315.72	315.76	315.80	315.85	315.89	315.94	315.98	316.0
713	316.07	316.11	316.16	316.20	316.25	316.29	316.34	316.38	316.42	316.4
711	316.51	316.56	316.60	316.65	316.69	316.73	316.78	316.82	316.87	l
715	316.96	317.00	317.05	317.09	317.13	317.18	317.22	317.27	317.31	317.3
716	317.40	317.44	317.49	317.53	317.13	317.62	317.67	317.71	317.75	317.8
717	317.84	317.89	317.43	317.98	318.02	318.06	318.11	318.15	318.20	318.2
718	318.29	318.33	318.38	318.42	318.46	318.51	318.55	318.60	318.64	318.6
719	318.73	318.77	318.82	318.86	318.91	318.95	319.00	319.04	319.08	319.1
	0.	1.	2.	3.	4.		6.	7.	8.	9.

1 Millimetre = 0.443296 French Line.

Millime-				,	Tenths of	Millimetres				
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines,	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
720	319.17	319.22	319.26	319.31	319.35	319.39	319.44	319.48	319.53	319.57
721	319.62	319.66	319.70	319.75	319.79	319.84	319.88	319.93	319.97	320.0:
722	320.06	320.10	320.15	320.19	320.24	320.28	320.33	320.37	320.41	320.40
723	320.50	320.55	320.59	320.64	320.68	320.72	320.77	320.81	320.86	320.9
724	320.95	320.99	321.03	321.08	321.12	321.17	321.21	321.26	321.30	321.3
725	321.39	321.43	321.48	321.52	321.57	321.61	321.66	321.70	321.74	321.7
726	321.83	321.88	321.92	321.97	322.01	322.05	322.10	322.14	322.19	322.2
727	322.28	322.32	322.36	322.41	322.45	322.50	322.54	322.59	322.63	322.6
728	322.72	322.76	322.81	322.85	322.90	322.94	322.99	323.03	323.07	323.1
729	323.16	323.21	323,25	323.30	323.34	323.38	323.43	323.47	323.52	323.5
730	323.61	323.65	323.69	323.74	323.78	323.83	323.87	323.92	323.96	324.0
731	324.05	324.09	324.14	324.18	324.23	324.27	324.32	324.36	324.40	324.4
732	324.49	324.54	324.58	324.63	324.67	324.71	324.76	324.80	324.85	324.8
733	324.94	324.98	325.02	325.07	325.11	325.16	325.20	325.25	325.29	325.3
734	325.38	325.42	325.47	325.51	325.56	325.60	325.65	325.69	325.73	325.7
735	325.82	325.87	325.91	325.96	326.00	326.04	326.09	326.13	326.18	326.2
736	326.27	326.31	326.35	326.40	326.44	326.49	326.53	326.58	326.62	326.6
737	326.71	326.75	326.80	326.84	326.89	326.93	326.98	327.02	327.06	327.1
738	327.15	327.20	327.24	327.29	327.33	327.37	327.42	327.46	327.51	327.5
739	327.60	327.64	327.68	327.73	327.77	327.82	327.86	327.91	327.95	327.9
740	328.04	328.08	328.13	328.17	328.22	328.26	328.30	328.35	328.39	328.4
741	328.48	328.53	328.57	328.62	328.66	328.70	328.75	328.79	328.84	328.8
742	328.93	328.97	329.01	329.06	329.10	329.15	329.19	329.24	329.28	329.3
743	329.37	329.41	329.46	329.50	329.55	329.59	329.63	329.68	329.72	329.7
744	329.81	329.86	329.90	329.95	329.99	330.03	330.08	330.12	330.17	330.2
745	330.26	330.30	330.34	330.39	330.43	330.48	330.52	330.57	330.61	330.6
746	330.70	330.74	330.79	330.83	330.88	330.92	330.96	331.01	331.05	331.1
747	331.14	331.19	331.23	331.28	331.32	331.36	331.41	331.45	331.50	331.5
748	331.59	331.63	331.67	331.72	331.76	331.81	331.85	331.90	331.94	331.9
749	332.03	332.07	332.12	332.16	332.21	332.25	332.29	332.34	332.38	332.4
750	332.47	332.52	332.56	332.60	332.65	332.69	332.74	332.78	332.83	332.8
751	332.92	332.96	333.00	333.05	333.09	333.14	333.18	333.23	333.27	333.3
752	333.36	333.40	333.45	333.49	333.54	333.58	333.62	333.67	333.71	333.7
753	333.80	333.85	333.89	333.93	333.98	334.02	334.07	334.11	334.16	334.2
754	334.25	334.29	334.33	334.38	334.42	334.47	334.51	334.56	334.60	334.6
755	334.69	334.73	334.78	334.82	334.87	334.91	334.95	335.00	335.04	335.0
756	335.13	335.18	335.22	335.26	335.31	335.35	335.40	335.44	335.49	335.5
757	335.58	335.62	335.66	335.71	335.75	335.80	335.84	335.89	335.93	335.9
758	336.02	336.06	336.11	336.15	336.20	336.24	336.28	336.33	336.37	336.4
759	336.46	336.51	336.55	336.59	306.64	336.68	336.73	336.77	336.82	336. 8
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Millimetre = 0.443296 French Line

Millime-				7	Tenths of I	Millimetres				
Millime- tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.lines.	Par.line
760	336.90	336.95	336.99	337.04	337.08	337.13	337.17	337.22	337.26	337.30
761	337.35	337.39	337.44	337.48	337.53	337.57	337.61	337.66	337.70	337.7
762	337.79	337.84	337.88	337.92	337.97	338.01	338.06	338.10	338.15	338.19
763	338.23	338.28	338.32	338.37	338.41	338.46	338.50	338.55	338.59	338.6
764	338.68	338.72	338.77	338.81	338.86	338.90	338.94	338.99	339.03	339.0
765	339.12	339.17	339.21	339.25	339.30	339.34	339.39	339.43	339.48	339.5
766	339.56	339.61	339.65	339.70	339.74	339.79	339.83	339.87	339.92	339.9
767	340.01	340.05	340.10	340.14	340.19	340.23	340.27	340.32	340.36	340.4
768	340.45	340.50	340.54	340.58	340.63	340.67	340.72	340.76	340.81	340.8
769	340.89	340.94	340.98	341.03	341.07	341.12	341.16	341.20	341.25	341.2
770	341.34	341.38	341.43	341.47	341.52	341.56	341.60	341.65	341.69	341.7
771	341.78	341.83	341.87	341.91	341.96	342.00	342.05	342.09	342.14	342.1
772	342.22	342.27	342.31	342.36	342.40	342.45	342.49	342.53	342.58	342.6
773	342.67	342.71	342.76	342.80	342.85	342.89	342.93	342.98	343.02	343.0
774	343.11	343.16	343.20	343.24	343.29	343.33	343.38	343.42	343.47	343.5
775	343.55	343.60	343.64	343.69	343.73	343.78	343.82	343.86	343.91	343.9
776	314.00	344.04	344.09	344.13	344.17	344.22	344.26	344.31	344.35	344.4
777	344.44	344.49	344.53	344.57	344.62	344.66	344.71	344.75	344.80	344.8
778	344.88	344.93	344.97	345.02	345.06	345.11	345.15	345.19	345.24	345.28
779	345.33	345.37	345.42	345.46	345.50	345.55	345.59	345.64	345.68	345.73
780	345.77	345.82	345.86	345.90	345.95	345.99	346.04	346.08	346.13	346.1
781	346.21	346.26	346.30	346.35	346.39	346.44	346.48	346.52	346.57	346.6
782	346.66	346.70	346.75	346.79	346.83	346.88	346.92	346.97	347.01	347.0
7 83	347.10	347.15	347.19	347.23	347.28	347.32	347.37	347.41	347.46	347.50
784	347.54	347.59	347.63	347.68	347.72	347.77	347.81	347.85	347.90	347.9
785	347.99	348.03	348.08	348.12	348.16	348.21	348.25	348.30	348.34	348.3
786	348.43	348.47	348.52	348.56	348.61	348.65	348.70	348.74	348.79	348.8
787	348.87	348.92	348.96	349.01	349.05	349.10	349.14	349.18	349.23	349.2
788	349.32	349.36	349.41	349.45	349.49	349.54	349.58	349.63	349.67	349.7
789	349.76	349.80	349.85	349.89	349.94	349.98	350.03	350.07	350.12	350.1
790	350.20	350.25	350.29	350.34	350.38	350.43	350.47	350.51	350.56	350.6
791	350.65	350.69	350.74	350.78	350.82	350.87	350.91	350.96	351.00	351.0
7 92	351.09	351.13	351.18	351.22	351.27	351.31	351.36	351.40	351.44	351.4
793	351.53	351.58	351.62	351.67	351.71	351.76	351.80	351.84	351.89	351.9
794	351.98	352.02	352.07	352.11	352.15	352.20	352.24	352.29	352.33	352.3
795	352.42	352.46	352.51	352.55	352.60	352.64	352.69	352.73	352.77	352.8
796	352.86	352.91	352.95	353.00	353.04	353.09	353.13	353.17	353.22	353.2
797	353.31	353.35	353.40	353.44	353.48	353.53	353.57	353.62	353.66	353.7
798	353.75	353.79	353.84	353.88	353.93	353.97	354.02	354.06	354.10	354.1
799	354.19	354.24	354.28	354.33	354.37	354.42	354.46	354.50	354.55	354.5
800	354.64	354.68	354.73	354.77	354.81	354.86	354.90	354.95	354.99	355.0
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

V. - VI.

COMPARISON

OF

THE OLD FRENCH BAROMETER

WITH

THE ENGLISH AND THE METRICAL BAROMETERS,

OR.

TABLES

FOR CONVERTING FRENCH OR PARIS LINES INTO ENGLISH INCHES AND DECIMALS, AND INTO MILLIMETRES;

GIVING THE VALUES CORRESPONDING TO EVERY PARIS LINE FROM 120 TO 216 LINES, OR FROM 10 TO 18 INCHES; AND TO EVERY TENTIL OF A LINE FROM 216 TO 348 LINES, OR FROM 18 TO 29 FRENCH INCHES.

TABLE V.

MM. J. J. Pohl and J. Schabus have published, in the number for March, 1852, of the Proceedings of the Imperial Academy of Vienna, Class of Mathematics and Natural Philosophy, a set of short Thermometrical and Barometrical Reduction Tables, among which is found a table for the reduction of the Old French Barometrical Scale into the English. As this table shows slight discrepancies from the one given in the following pages, it may not be out of place to state that they arise from an accidental error in the equation used by MM. Pohl and Schabus in computing their table. Adopting, as they do, Bird's value of the metre, viz.

1 metre = 39.37062 English inches,

the value of the Paris line is

1 Paris line = 0.088813 English inches.

But the table seems to have been computed by using the equation

1 Paris line = 0.088823 English inches,

which gives, at the end of the table,

 $348 \text{ lines} \times .088823 = 30.9104 \text{ English inches},$

instead of

$$348$$
 " $\times .088813 = 30.9069$ " "

thus causing an error

which, of course, gradually diminishes in lower numbers.

1 Paris Line = 0.088814 English Inch.

			1 P	aris Line =	= 0.088814	English I	nch.			
French or Paris Lines.					Uı	nits.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
10 Inch.	Eng. In.	Eng In.	Eng. In.	Eng. In.	Eng In	Eng. In.	Eng. In	. Eng. In	Eng In.	Eng. In
120	10.658	10.746	10.835	10.924	11.013	11.102	11.191	11.27	$9 \mid 11.368$	11.45
130	11.546	11.635	11.723	11.812	11.901	11.990	12.079	12.16	3 12.256	12.34
140	12.434	12.523	12.612	12.700	12.789	12.878	12.967	13.05	$6 \mid 13.144$	13.23
150	13.322	13.411	13.500	13.589	13.677	13.766	13.855	13.94	1 14.033	14.12
160	14.210	14.299	14.388	14.477	14.565	14.654	14.74	14.83	2 14.921	15.01
170	15.098	15.187	15.276	15.365	15.454	15.542	15.631	15.72	15.809	$^{\perp}$ 15.89
180	15 987	16.075	16.164	16.253	16.342	16.431	16.519			16.78
190	16.875	16.963	17.052	17.141	17.230	17.319	17.408	1		17.67
200	17.763	17.852	17.940	18.029	18.118	18.207	18.296			18.56
210	18.651	18.740	18.829	18.917	19.006	19.095	19.184			19.45
					Ter	ths.			-	
Paris Lines.	0.	1.	2.	3,	4.	5,	6.	7.	8.	9.
18 Inch.	Eng. In.	Eng. In.	Eng In.	Eng In	Eng. In.	Eng. In.	Eng. In	Eng. Ir	Eng. In.	Eng. Ir
216	19.184	19.193	19.202	19.210	19.219	19.228	19.237			19.26
217	19.273	19.252	19.290	19.299	19.308	19.317	19.326	19.33	5 19.344	. 19.35
218	19.361	19.370	19.379	19.388	19.397	19.406	19.415			19.44
219	19.450	19.459	19.468	19.477	19.486	19.495	19.504	19.51		19.53
220	19.539	19.548	19.557	19.566	19.575	19.583	19.592			19.61
221	19.628	19.637	19.646	19.655	19.663	19.672	19.681	19.690		19.708
222	19.717	19.726	19.734	19.743	19.752	19.761	19.770	19.779	19.788	10.70
223	19.806	19.814	19.823	19.832	19.840	19.850				19.79
224	19.894	19.903	19.912	19.921	19.930	19.939	19.859 19.948	1		19.888
									1	19.97
225	19.983	19.992	20.001	20.010	20.019	20.028	20.036	20.043		20.06
226	20.072	20.081	20.090	20.099	20.107	20.116	20.125	20.13-		20.15:
227	20.161	20.170	20.179	20.187	20.196	20.205	20.214	20.223	20.232	20.24
19 Inch.	20 250	20 250	20 20#	20 2=2	22 22 7					
228	20.250	20.258	20.267	20.276	20.285	20.294	20.303			20.330
229	20.338	20.347	20.356	20.365	20.374	20.383	20.392	20.401		20.418
230	20.427	20.436	20.445	20.454	20.463	20.472	20.481	20.489	1	20.507
231	20.516	20.525	20.534	20.543	20.552	20.560	20.569	20.578	20.587	20.596
232	20.605	20.614	20.623	20.631	20.640	20.649	20.658	20.667	20.676	20.683
233	20.694	20.703	20.711	20.720	20.729	20.738	20.747	20.756	20.765	20.77
234	20.782	20.791	20.800	20.809	20.818	20.827	20.836	20.845	20.554	20.862
235	20.871	20.880	20.889	20.898	20.907	20.916	20.925	20.933		20.951
236	20.960	20.969	20.978	20.987	20.996	21.005	21.013	21.022		21.040
237	21.049	21.058	21.067	21.076	21.084	21.093	21.102			21.129
233	21.138	21.147	21.155	21.164	21.173	21.182	21.191	21.200		21.218
239	21.227	21.235	21.244	21.253	21.262		21.280			21.306
				Hundr	edths of a	Line.				
0.	1.	2.	3.	4.	5	.	6.	7.	8.	9.
c00.	.001	.002	.003	.004	.00		005	.006	.007	.008

1 Paris Line = 0.083814 English Inch.

French or					Tenths	of a Line.				
ParisLines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. Ir
240	21.315	21.321	21.333	21.342	21.351	21.360	21.369	21.378	21.386	21.39
241	21.404	21.413	21.422	21.431	21.440	21.449	21.457	21.466	21.475	21.48
242	21.493	21.502	21.511	21.520	21.529	21.537	21.546	21.555	21.564	21.573
243	21.582	21.591	21.600	21.608	21.617	21.626	21.635	21.644	21.653	21.66
244 245	21.671 21.759	21.679 21.768	21.688 21.777	21.697 21.786	21.706 21.795	21.715 21.804	21.724 21.813	21.733 21.822	21.742 21.830	21.75 21.83
246	21.848	21.857	21.866	21.875	21.884	21.893	21.902	21.910	21.919	21.928
247	21.937	21.946	21.955	21.964	21.973	21.981	21.990	21.999	22.008	22.01
248	22.026	22.035	22.044	22.053	22.061	22.070	22.079	22.088	22.097	22.10
249	22.115	22.124	22.132	22.141	22.150	22.159	22.168	22.177	22 186	22.19
250	22.203	22.212	22.221	22.230	22.239	22.248	22.257	22.266	22.275	22.28
251	22.292	22.301	22.310	22.319	22.328	22.337	22.346	22.354	22.363	22.37
31 In. =						l				
252	22.381	22.390	22.399	22.408	22.417	22.426	22.434	22.443	22.452	22.46
253	22.470	22.479	22.488	22.497	22.505	22.514	22.523	22.532	22.541	22.55
251	22.559	22.568	22.577	22.585	22.594	22.603	22.612	22.621	22.630	22.63
255	22.648	22.656	22.665	22.674	22.683	22.692	22.701	22.710	22.719	22.728
256	22.736	22.745	22.754	22.763	22.772	22.781	22.790	22.799	22.807	22.810
257	22.825	22.834	22.843	22.852	22.861	22.870	22.878	22.887	22.896	22.90
258	22.914	22.923	22.932	22.941	22.950	22.958	22.967	22.976	22.985	22.99
259	23.003	23.012	23.021	23.029	23.038	23.047	23.056	23.065	23.074	23.08
260	23.092	23.101	23.109	23.118	23.127	23.136	23.145	23.154	23.163	23.17
261	23.180	23.189	23.198	23.207	23.216	23.225	23.234	23.243	23.252	23.26
262	23.269	23.278	23.287	23.296	23.305	23.314	23.323	23.331	23.340	23.349
263	23.358	23.367	23.376	23.385	23.394	23.402	23.411	23.420	23.429	23.438
2 In. =	2.0									
264	23.447	23.456	23.465	23.474	23.482	23.491	23.500	23.509	23.518	23.523
265	23.536	23.545	23.553	23.562	23.571	23.580	23.589	23.598	23.607	23.616
266	23.625	23.633	23.642	23.651	23.660	23.669	23.678	23.687	23.696	23.70-
267 268	23.713	23.722	23.731	23.740	23.749	23.758	23.767	23.776	23.784	23.793
269	23.802 23.891	23.811 23.900	$23.820 \\ 23.909$	23.829 23.918	23.838 23.926	$\begin{array}{c} 23.847 \\ 23.935 \end{array}$	23.855 23.944	23.864 23.953	23.873 23.962	23.883 23.971
270	23.980	23.989	23.998	24.006	24.015	24.024	24.033	24.042	24.051	24.060
271	21.069	24.077	24.086	24.095	24.104	24.113	24.122	24.131	24.140	24.149
272	24.157	24.166	24.175	24.184	24.193	24.202	24.211	24.220	24.228	24.237
273	24.246	24.255	24.264	24.273	24.133	21.291	24.300	24.308	24.317	24.326
274	24.335	24.344	24.353	24.362	24.371	24.379	24.388	24.397	24.406	24.415
275	24.424	24.433	24.442	24.450	24.459	21.468	24.477	24.486	24.495	24.504
				Hundre	dths of a	Line.			<u>'</u>	
0.	1.	2.	3.	4.	5	. (3.	7.	8.	9.
					_ 1	1				-

1 Paris Line = 0.088814 English Inch.

French or					Tenths o	f a Line.		Tenths of a Line.													
ParisLines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.											
23 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.											
276	24.513	24.522	24.530	24.539	24.548	24.557	24.566	24.575	24.584	24.593											
277	24.601	24.610	24.619	24.628	24.637	24.646	24.655	24.664	24.673	24.681											
278	24.690	24.699	24.708	24.717	24.726	24.735	24.744	24.752	24.761	21.770											
279	24.779	24.788	24.797	24.806	24.815	24.824	24.832	24.841	24.850	24.859											
280	24.868	24.877	24.886	24.895	24.903	24.912	24.921	24.930	24.939	24.948											
281	24.957	24.966	24.974	24.983	24.992	25.001	25.010	25.019	25.028	25.037											
282	25.046	25.054	25.063	25.072	25.081	25.090	25.099	25.108	25.117	25.125											
283	25.134	25.143	25.152	25.161	25.170	25.179	25.188	25.197	25.205	25.214											
284	25.223	25.232	25.241	25.250	25.259	25.268	25.276	25.285	25.294	25.303											
285	25.312	25.321	25.330	25.339	25.348	25.356	25.365	25.374	25.383	25.392											
286	25.401	25.410	25.419	25.427	25.436	25.445	25.454	25.463	25.472	25.481											
287	25.490	25.498	25.507	25.516	25.525	25.534	25.543	25.552	25.561	25.570											
24 In. =	25.50	05 504	25 500	05 005	25 014	25 229	07 000	07.647	25.649	25.658											
288	25.578	25.587	25.596	25.605	25.614	25.623	25.632	25.641 25.729	25.738	25.747											
289	25.667	25.676	25.685 25.774	25.694 25.783	25.703 25.792	25.712 25.800	25.721 25.809	25.818	25.827	25.836											
$\begin{array}{c} 290 \\ 291 \end{array}$	25.756 25.845	25.765 25.854	25.863	25.785 25.872	25.880	25.889	25.898	25.907	25.916	25.925											
291	25.934	25.943	25.951	25.960	25.969	25.978	25.987	25.996	26.005	26.014											
293	26.023	26.031	26.040	26.049	26.058	26.067	26.076	26.085	26.094	26.102											
	Ì																				
294	26.111	26.120	26.129	26.138	26.147	26.156	26.165	26.173	26.182	26.191											
295	26.200	26.209	26.218	26.227	26.236	26.245	26.253	26.262	26.271	26.280											
296	26.289	26.298	26.307	26.316	26.324	26.333	26.342	26.351	26.360	26.369											
297	26.378	26.387	26.396	26.404	26.413	26.422	26.431	26.440	26.449	26.458											
298	26.467	26.475	26.484	26.493	26.502	26.511	26.520	26.529	26.538	26.547											
299	26.555	26.564	26.573	26.582	26.591	26.600	26.609	26.618	26.626	26.635											
25 In. =							22 222	20.00	20 -15	00 70											
300	26.644	26.653	26.662	26.671	26.680	26.689	26.697	26.706	26.715	26.724											
301	26.733	26.742	26.751	26.760	26.769	26.777	26.786	26.795	26 804	26.813 26.902											
302	26.822	26.831	26.840	26.848	26.857	26.866	26.875	26.884	26.893 26.982	26.902 26.991											
303	26.911	26.920	26.928	26.937	26.946	26.955	26.964 27.053	26.973 27.062	27.071	27.079											
304 305	26.999 27.088	27.008 27.097	27.017 27.106	27.026 27.115	27.035 27.124	27.044 27.133	27.142	27.002	27.159	27.168											
303	21.000	27.097	27.100	27.115	27.124	24.155	27.142	21.150	211195	2,											
306	27.177	27.186	27.195	27.204	27.213	27.221	27.230	27.239	27.248	27.257											
307	27.266	27.275	27.284	27.293	27.301	27.310	27.319	27.328	27.337	27.346											
308	27.355	27.364	27.372	27.381	27.390	27.399	27.408	27.417	27.426	27.435											
309	27.441	27.452	27.461	27.470	27.479	27.488	27.497	27.506	27.515	27.523											
310	27.532	27.541	27.550	27.559	27.568	27.577	27.586	27.595	27.603	27.612											
311	27.621	27.630	27.639	27.648	27.657	27.666	27.674	27.683	27.692	27.701											
		1	1	Hundr	edths of a	Line.															
0.	1.	2.	3.	4.	5	5.	6.	7.	8.	9.											
				_	1																

1 Paris Line = 0.088814 English Inch.

French or ParisLines.	Tenths of a Line.												
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
26 Inches.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In			
312	27.710	27.719	27.728	27.737	27.745	27.754	27.763	27.772	27.781	27.79			
313	27.799	27.808	27.817	27.825	27.834	27.843	27.852	27.861	27.870	27.87			
314	27.888	27.896	27.905	27.914	27.923	27.932	27.941	27.950	27.959	27.96			
315	27.976	27.985	27.994	28.003	28.012	28.021	28.030	28.039	28.047	28.05			
316	28.065	28.074	28.083	28.092	28.101	28.110	28.119	28.127	28.136	28.14			
317	28.154	28.163	28.172	28.181	28.190	28.198	28.207	28.216	28.225	28.23			
318	28.213	28.252	28.261	28.269	28.278	28.287	28.296	28.305	28.314	28.32			
319	28.332	28.341	28.349	28.358	28.367	28.376	28.385	28.394	28.403	28.41			
320	28.420	28.429	28.438	28.447	28.456	28.465	28.474	28.483	28.492	28.50			
321	28.509	28.518	28.527	28.536	28.545	28.554	28.563	28.571	28.580	28.58			
322	28.598	28.607	28.616	28.625	28.634	28.643	28.651	28.660	28.669	28.67			
323	28.687	28.696	28.705	28.714	28.722	28.731	28.740	28.749	28.758	28.76			
27 In. =				ļ									
324	28.776	28.785	28.793	28.802	28.811	28.820	28.829	28.838	28.847	28.85			
325	28.865	28.873	28.882	28.891	28.900	28.909	28.918	28.927	28.936	28.94			
326	28.953	28.962	28.971	28.980	28.989	28.998	29.007	29.016	29.024	29.03			
327	29.042	29.051	29.060	29.069	29.078	29.087	29.095	29.104	29.113	29.12			
328	29.131	29.140	29.149	29.158	29.167	29.175	29.184	29.193	29.202	29.21			
. 329	29.220	29.229	29.238	29.246	29.255	29.264	29.273	29.282	29.291	29.30			
330	29.309	29.318	29.326	29.335	29.341	29.353	29.362	29.371	29.380	29.38			
331	29.397	29.406	29.415	29.424	29.433	29.442	29.451	29.460	29.468	29.47			
332	29.486	29.495	29.504	29.513	29.522	29.531	29.540	29.548	29.557	29.56			
333	29.575	29.584	29.593	29.602	29.611	29.619	29.628	29.637	29.646	29.65			
334	29.664	29.673	29.682	29.691	29.699	29.708	29.717	29.726	29.735	29.74			
335	29.753	29.762	29.770	29.779	29.788	29.797	29.806	29.815	29.824	29.83			
28 In. =													
336	29.842	29.850	29.859	29.868	29.877	29.886	29.895	29.904	29.913	29.92			
337	29.930	29.939	29.948	29.957	29.966	29.975	29.984	29.992	30.001	30.01			
338	30.019	30.028	30.037	30.046	30.055	30.064	30.072	30.081	30.090	30.09			
339	30.108	30.117	30.126	30.135	30.143	30.152	30.161	30.170	30.179	30.18			
340	30.197	30.206	30.215	30.223	30.232	30.241	30.250	30.259	30.268	30.27			
341	30.286	30.294	30.303	30.312	30.321	30.330	30.339	30.348	30.357	30.36			
342	30.374	30.383	30.392	30.401	30.410	30.419	30.428	30.437	30.445	30.45			
343	30.463	30.472	30.481	30.490	30.499	30.508	30.516	30.525	30.534	30.54			
344	30.552	30.561	30.570	30.579	30.588	30.596	30.605	30.614	30.623	30.63			
345	30.641	30.650	30.659	30.667	30.676	30.685	30.694	30.703	30.712	30.72			
346	30.730	30.739	30.747	30.756	30.765	30.774	30.783	30.792	30.801	39.81			
347	30.818	30.827	30.836	30.845	30.854	30.863	30.872	30.881	30.890	30.89			
318 In. =	30.907	30.916	30.925	30.934	30.943	30.952	30.961	30.969	30.978	30.98			

C

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1.

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.0062

9.

.0080

1 Paris Line = 2.255829 Millimetres.

French or ParisLines.					Un	its.									
Tens.	0.	1.	2.	3.	4.	5.	6		7.	8.	9.				
10 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin	ı. Milli	m.	Millim.	Millim.	Millim.				
120	270.70	272.96	275.21	277.47	279.72	281.9	8 284	23	286.49	288.75	291.00				
130	293.26	295.51	297.77	300.03	302 28	304.5	4 306.	79	309.05	311.30	313.56				
140	315.82	318.07	320.33	322.58	324.84	327.1	0 329.	35	331.61	333.86	336.12				
150	338.37	340.63	342.89	345.14	347.40	349.6	5 351.	91	354.17	356.42	358.68				
160	360.93	363.19	365.44	367.70	369.96	3 7 2.2	21 374.	47	376.72	378.98	381.24				
170	383.49	385.75	388.00	390.26	392.51	394.7	7 397.	03	399.28	401.54	403.79				
180	406.05	408.30	410.56	412.82	415.07	417.3	3 419.	58	421.84	424.10	426.35				
190	428.61	430.86	433.12	435.37	437.63	439.8	9 442.	14	444.40	446.65	448.91				
200	451.17	453.42	455.68	457.93	460.19	462.4	4 464.	70	466.96	469.21	471.47				
210	473.72	475.98	478.24	480.49	482.75	485.0	0 487.	26	489.51	491.77	494.03				
		Tenths of a Line.													
Paris Lines.	0.	1.	2.	3.	4.	5.	6		7.	8.	9.				
18 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim	n. Milli	m.	Millim.	Millim.	Millim.				
216	487.26	487.48	487.71	487.94	488.16	488.3	9 488.	61	488.84	489.06	489.29				
217	489.51	489.74	489.97	490.19	490.42	490.6	490.	87	491.09	491.32	491.55				
218	491.77	492.00	492.22	492.45	492.67	492.9	0 493.	12	493.35	493.58	493.80				
219	494.03	494.25	494.48	494.70	494.93	495.1	5 495.	38	495.61	495.83	496.06				
220	496.28	496.51	496.73	496.96	497.18	497.4	1 497.	64	497.86	498.09	498.31				
221	498.54	498.76	498.99	499.21	499.44	499.6	7 499.	89	500.12	500.34	500.57				
222	500.79	501.02	501.25	501.47	501.70	501.9	2 502.	15	502.37	502.60	502.82				
223	503.05	503.28	503.50	503.73	503.95	504.1	8 504.	40	504.63	501.85	505.08				
224	505.31	505.53	505.76	505.98	506.21	506.4	3 506.	66	506.88	507.11	507.34				
225	507.56	507.79	508.01	508.24	508.46	508.6	9 508.	91	509.14	509.37	509.59				
226	509.82	510.04	510.27	510.49	510.72	510.9	5 511.	17	511.40	511.62	511.85				
227	512.07	512.30	512.52	512.75	512.98	513.2	0 513.	43	513.65	513.88	514.10				
19 Inch.															
228	514.33	514.55	514.78	515.01	515.23	515.4	6 515.	68	515.91	516.13	516.36				
229	516.58	516.81	517.04	517.26	517.49	517.7		94	518.16	518.39	518.61				
230	518.84	519.07	519.29	519.52	519.74	519.9	7 520.	19	520.42	520.65	520.87				
231	521.10	521.32	521.55	521.77	522.00	522.2	2 522.	45	522.68	522.90	523.13				
232	523.35	523.58	523.80	524.03	524.25	524.4	8 524.	71	524.93	525.16	525.38				
233	525.61	525.83	526.06	526.28	526.51	526.7		96	527.19	527.41	527.64				
234	527.86	528.09	528.32	528.54	528.77	528.9	9 529.	22	529.44	529.67	529.89				
235	530.12	530.35	530.57	530.80	531.02	531.2		- 1	531.70	531.92	532.15				
236	532.38	532.60	532.83	533.05	533.28	533.5		- 1	533.95	534.18	534.41				
237	534.63	534.86	535.08	535.31	535.53	535.7		0.0	536.21	536.44	536.66				
233	536.89	537.11	537.34	537.56	537.79	538.0	- 1	- 1	538.17	1	538.92				
239	539.14	539.37	539.59	539.82	540.05			- 1	540.72	540.95	541.17				
				Tent	hs of a Li	ne.									
0.	1.	2.	3.	4.	5		6.		7.	8.	9.				
0.00	0.23	0.45	0.68	0.90) 1.	13	1.35	1	.58	1.80	2.03				

1 Paris Line = 2.255829 Millimetres.

Paris or					Tenths o	fa Line.				
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
20 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
240	541.40	541.62	541.85	512.08	542.30	542.53	542.75	542.98	543.20	543.4
241	543.65	543.88	544.11	544.33	544.56	544.78	545.01	545.23	545.46	545.6
242	545.91	546.14	546.36	546.59	546.81	547.04	547.26	547.49	547.72	547.9
243	548.17	548.39	548.62	543.94	549.67	549.29	549.52	549.75	549.97	550.2
244	550.42	550.65	550.87	551.10	551.32	551.55	551.78	552.00	552.23	552.
245	552.68	552.90	553.13	553.35	553.58	553.81	554.03	554.26	554.48	554.7
246	554.93	555.16	555.39	555.61	555.S4	556.06	556.29	556.51	556.74	556.9
247	557.19	557.42	557.64	557.87	558.09	558.32	558.54	558.77	558.99	559.2
248	559.45	559.67	559.90	560.12	560.35	560.57	560.80	561.02	561.25	561
249	561.70	561.93	562.15	562.38	562.60	562.83	563.05	563.28	563.51	563.
250	563.96	564.18	564.41	564.63	564.86	565.09	565.31	565.54	565.76	565.9
251	566.21	566.44	566.66	566.89	567.12	567.34	567.57	567.79	568.02	568.
21 Inches.										
252	568.47	568.69	568.92	569.15	569.37	569.60	569.82	570.05	570.27	570.
253	570.72	570.95	571.18	571.40	571.63	571.85	572.08	572.30	572.53	572.
254	572.98	573.21	573.43	573.66	573.SS	574.11	574.33	574.56	574.79	575.0
255	575.24	575.46	575.69	575.91	576.14	576.36	576.59	576.82	577.04	577.
256	577.49	577.72	577.94	578.17	578.39	578.62	578.85	579.07	579.30	579.
257	579.75	579.97	580.20	580.42	580.65	580.88	581.10	581.33	581.55	581.
258	582.00	582.23	582.46	582.68	582.91	583.13	583.36	583.58	583.81	584.0
259	584.26	584.49	584.71	584.94	585.16	585.39	585.61	585.84	586.06	586.
260	586.52	586.74	586.97	587.19	587.42	587.64	587.87	588.09	588.32	588.
261	588.77	589.00	589.22	589.45	589.67	589.90	590.12	590.35	590 58	590.
262	591.03	591.25	591.48	591.70	591.93	592.16	592.38	592.61	592.83	593.
263	593.28	593.51	593.73	593.96	594.19	594.41	594.64	594.86	595.09	595.
22 Inches.						Ĭ				
264	595.54	595.76	595.99	596.22	596.44	596.67	596.89	597.12	597.34	597.
265	597.79	598.02	598.25	598.47	598.70	598.92	599.15	599.37	599.60	599.8
266	600.05	600.28	600.50	600.73	600.95	601.18	601.40	601.63	601.86	602.0
267	602.31	602.53	602.76	602.98	603.21	603.43	603.66	603.89	604.11	604.
268	604.56	604.79	605.01	605.24	605.46	605.69	605.92	606.14	606.37	606.
269	606.82	607.04	607.27	607.49	607.72	607.95	608.17	608.40	608.62	608.
270	609.07	609.30	609.52	609.75	609.98	610.20	610.43	610.65	610.88	611.
271	611.33	611.56	611.78	612.01	612.23	612.46	612.68	612.91	613.13	613.
272	613.59	613.81	614.04	614.26	614.49	614.71	614.94	615.16	615.39	615.
273	615.84	616.07	616.29	616.52	616.74	616.97	617.19	617.42	617.65	617.8
274	618.10	618.32	618.55	618.77	619.00	619.23	617.19	617.42	619.90	620.
275	620.35	620.58	620.80	621.03	621.26	621.48	621.71	621.93	622.16	622.
	•			Hundre	edths of a	Line.	t .	1		1
0.	1.	2.	3.	4.	. ;	5.	6.	7.	8.	9.
0.000	0.023	0.045	0.068	3 0.09	90 0.	113	0.135	0.158	0.180	0.20

1 Paris Line = 2.255829 Millimetres.

Paris or					Tenths o	f a Line.				
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
23 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
276	622.61	622.83	623.06	623.29	623.51	623.74	623.96	624.19	624.41	624.64
277	624.86	625.09	625.32	625.54	625.77	625.99	626.22	626.44	626.67	626.89
278	627.12	627.35	627.57	627.80	628.02	628.25	628.47	628.70	628.93	629.15
279	629.38	629.60	629.83	630.05	630.28	630.50	630.73	630.96	631.18	631.41
280	631.63	631.86	632.08	632.31	632.53	632.76	632.99	633.21	633.44	633.66
281	633.89	634.11	634.34	634.56	634.79	635.02	635.24	635.47	635.69	635.92
282	636.14	636.37	636.59	636.82	637.05	637.27	637.50	637.72	637.95	638.17
283	638.40	638.63	638.85	639.08	639.30	639.53	639.75	639.98	640.20	640.43
284	640.66	640.88	641.11	641.33	641.56	641.78	642.01	642.23	643.46	642.69
285	642.91	643.14	643.36	643.59	643.81	644.04	644.26	644.49	644.72	644.9
286	645.17	645.39	645.62	645.84	646.07	646.30	646.52	646.75	646.97	647.20
287	647.42	647.65	647.87	648.10	648.33	648.55	648.78	649.00	649.23	649.43
4 Inches.										
288	649.68	649.90	650.13	650.36	650.58	650.81	651.03	651.26	651.48	651.71
289	651.93	652.16	652.39	652.61	652.84	653.06	653.29	653.51	653.71	653.96
290	654.19	654.42	654.64	654.87	655.09	655.32	655.54	655.77	656.00	656.23
291	656.45	656.67	656.90	657.12	657.35	657.57	657.80	658.03	658.25	658.48
292	658.70	658.93	659.15	659.38	659.60	659.83	660.06	660.28	660.51	660.73
293	660.96	661.18	661.41	661.63	661.86	662.09	662.31	662.54	662.76	662.99
20.4	000 01	000 44	000.00	000.00	004.10	004.04	001.55	004 *0	007.00	00.0
294	663.21	663.44	663.66	663.89	664.12	664.34	664.57	664.79	665.02	665.2
295	665.47	665.70	665.92	666.15	666.37	666.60	666.82	667.05	667.27	667.5
296	667.73	667.95	668.18	668.40	668.63	668.85	669.08	669.30	669.53	669.70
297	669.98	670.21	670.43	670.66	670.88	671.11	671.33	671.56	671.79	672.0
298	672.24	672.46	672.69	672.91	673.14	673.36	673.59	673.82	674.04	674.2
299	674.49	674.72	674.94	675.17	675.40	675.62	675.85	676.07	676.30	676.5
5 Inches.										
300	676.75	676.97	677.20	677.43	677.65	677.88	678.10	678.33	678.55	678.78
301	679.00	679.23	679.46	679.68	679.91	680.13	680.36	680.58	680.81	681.0
302	681.26	681.49	681.71	681.94	682.16	682.39	682.61	682.84	683.07	683.2
303	683.52	683.74	683.97	684.19	684.42	684.64	684.87	685.10	685.32	685.5
304	685.77	686.00	686.22	686.45	686.67	686.90	687.13	687.35	687.58	657.8
305	688.03	688.25	688.48	688.70	688.93	689.16	689.38	689.61	689.83	690.0
306	690.28	690.51	690.73	690.96	691.19	691.41	691.64	691.86	692.09	692.3
307	692.54	692.77	692.99	693.22	693.44	693.67	693.89	694.12	694.34	694.5
308	694.80	695.02	695.25	695.47	695.70	695.92	696.15	696.37	696.60	696.8
309	697.05	697.28	697.50	697.73	697.95	698.18	698.40	698.63	698.86	699.0
310	699.31	699.53	699.76	699.98	700.21	700.43	700.66	700.89	701.11	701.3
311	701.56	701.79	702.01	702.24	702.47	702.69	702.92	703.14	703.37	703.5
				Hundr	edths of a	Line.				
0.	1.	2.	3.	4		5.	6.	7.	8.	9.
0.000	0.023	0.045	0.06	s 0.0	90 0.	113	0.135	0.158	0.180	0.20

1 Paris Line = 2.255829 Millimetres.

Paris or					Tenths	of a Line.				
French Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
26 Inches.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
312	703.82	704.04	704.27	704.50	704.72	704.95	705.17	705.40	705.62	705.85
313	706.07	706.30	706.53	706.75	706.98	707.20	707.43	707.65	707.88	708.10
314	708.33	708.56	708.78	709.01	709.23	709.46	709.68	709.91	710.13	710.36
315	710.59	710.81	711.04	711.26	711.49	711.71	711.94	712.17	712.39	712.62
316	712.84	713.07	713.29	713.52	713.74	713.97	714.20	714.42	714.65	714.87
317	715.10	715.32	715.55	715.77	716.00	716.23	716.45	716.68	716.90	717.13
318	717.35	717.58	717.80	718.03	718.26	718.48	718.71	718.93	719.16	719.38
319	719.61	719.84	720.06	720.29	720.51	720.74	720.96	721.19	721.41	721.64
320	721.87	722.09	722.32	722.54	722.77	722.99	723.22	723.44	723.67	723.90
321	724.12	724.35	724.57	724.80	725.02	725.25	725.47	725.70	725.93	726.15
322	726.38	726.60	726.83	727.05	727.28	727.50		727.96	728.18	728.41
323	728.63	728.86	729.08	729.31	729.54	729.76	729.99	730.21	730.44	730.66
27 Inches.	120.00	,20.00	120.00	120.01	120.01	123.10	120.00	100.21	100.11	100.00
324	730.89	731.11	731.34	731.57	731.79	732.02	732.24	732.47	732.69	732.92
325	733.14	733.37	733.60	733.82	734.05	734.27	734.50	734.72	734.95	735.17
326	735.40	735.63	735.85	736.08	736.30	736.53	736.75	736.98	737.20	737.43
327	737.66	737.88	738.11	738.33	738.56	738.78		739.24	739.46	739.69
328	739.91	740.14	740.36	740.59	740.81	741.04		741.49	741.72	741.94
329	742.17	742.39	742.62	742.84	743.07	743.30	743.52	743.75	743.97	744.20
330	744.42	744.65	744.87	745.10	745.33	745.55	745.78	746.00	746.23	746.45
331	746.68	746.90	717.13	747.36	747.58	747.81	748.03	748.26	748.48	748.71
332	748.94	749.16	749.39	749.61	749.84	750.06	750.29	750.51	750.74	750.97
333	751.19	751.42	751.64	751.87	752.09	752.32	752.54	752.77	753.00	753.22
334	753.45	753.67	753.90	754.12	754.35	754.57	754.80	755.03	755.25	755.48
335 24 Inches.	755.70	755.93	756.15	756.38	756.61	756.83	757.06	757.28	757.51	757.73
336	757.96	758.18	758.41	758.64	758.86	759.09	759.31	759.54	759.76	759.99
337	760.21	760.41	760.67	760.89	761.12	761.34	761.57	761.79	762.02	762.24
338	762.47	762.70	762.92	763.15	763.37	763.60		764.05	764.27	764.50
339	764.73	764.95	765.18	765.40	765.63	765.85	766.08	766.31	766.53	766.76
340	766.98	767.21	767.43	767.66	767.88	768.11	768.34	768.56	768.79	769.01
341	769.24	769.46	769.69	769.91	770.14	770.37	770.59	770.82	771.04	771.27
342	771.49	771.72	771.94	772.17	772.40	772.62	772.85	773.07	773.30	773.52
343	773.75	773.97	774.20	774.43	774.65	774.88	1	775.33	775.55	775.78
344	776.01	776.23	776.46	776.68	776.91	777.13		777.58	777.81	778.04
345	778.26	778.49	778.71	778.94	779.16	779.39	1	779.84	780.07	780.29
346	780.52	780.74	780.97	781.19	781.42	781.64	781.87	782.10	782.32	782.55
347	782.77	783.00	783.22	783.45	783.67	783.90	784.13	784.35	784.58	784.80
29 Inches.						1				
313	785.03	785.25	785.48	785.71 Hundre	edths of a	1786.16 Line.	786.38	786.61	786.83	787.00
0.	1.	2.	3.	4	.	5.	6.	7.	8.	9.
0.000	0.023	0.045	0.06	6 0.0	90 0	113	0.135	0.158	0.180	0.203

VII. - VIII.

COMPARISON

OF

THE RUSSIAN BAROMETER

WITH

THE METRICAL AND THE OLD FRENCH BAROMETERS,

OR

TABLES

FOR CONVERTING RUSSIAN HALF-LINES INTO MILLIMETRES,

AND INTO FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY HALF-LINE FROM 440 TO 540, OR FROM 22 TO 27 INCHES; AND TO EVERY TENTH, FROM 540 TO 610 HALF-LINES, OR FROM 27 TO 30.5 ENGLISH INCHES.

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RUSSIAN BAROMETER.

A LEGULAR system of Meteorological Observations has been established by order of the Russian government throughout the extensive regions placed under its sway, and a vast amount of observations made in Europe, in Asia, and in North America have already been published. The scale of the barometer employed in this system is divided in units, each of which is equal to one half of a Russian, or English decimal line, that is, 1=0.05 of an inch, 600 half-lines of the Russian Barometer being =30 inches of the English Barometer.

The conversion of this scale, which is the English scale, slightly modified in its form, is easy. It suffices to divide the Russian heights by two, and to put back, by one figure, the decimal point, in order to have them converted into English inches and decimals. This transformation is so easy to effect, that a peculiar table for it would seem superfluous.

The normal temperature of the standard being the same as that of the English, that is, 13°½ Reaumur, or 62° Fahrenheit, the reduction of the Russian Barometer to the freezing point can be made by means of the table for reducing the English Barometers. But the attached thermometer being that of Reaumur, its indications must be first converted into degrees of Fahrenheit.

Tables VII. and VIII., which follow, have been computed in order to render more easy the comparison and the use of the Barometrical Observations recorded in the large collection, published annually by order of the Emperor of Russia, under the name of Annuaire Météorologique et Magnétique du Corps des Ingénieurs des Mines.

1 Russian Half-Line = 1.269977 Millimetres.

Russian				Uni	its or Russ	ian Half-Li	nes.			
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
22 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
440	558.79	560.06	561.33	562.60	563.87	565.14	566.41	567.68	568.95	570.2
450	571.49	572.76	574.03	575.30	576.57	577.84	579.11	580.38	581.65	582.9
460	584.19	585.46	586.73	588.00	589.27	590.54	591.81	593.08	594.35	595.6
470	596.89	598.16	599.43	600.70	601.97	603.24	604.51	605.78	607.05	608.3
480	609.59	610.86	612.13	613.40	614.67	615.94	617.21	618.48	619.75	621.0
24.5 In.						l				
490	622.29	623.56	624.83	626.10	627.37	628.64	629.91	631.18	632.45	633.7
500	634.99	636.26	637.53	638.80	640.07	641.34	642.61	643.88	645.15	646.
510	647.69	648.96	650.23	651.50	652.77	654.04	655.31	656.58	657.85	659.1
520	660.39	661.66	662.93	664.20	665.47	666.74	668.01	669.28	670.55	671.8
530	673.09	674.36	675.63	676.90	678.17	679.44	680.71	681.98	683.25	684.5
Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
27 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
540	685.79	685.91	686.04	686.17	686.30	686.42	686.55	686.68	686.80	686.9
541	687.06	687.18	687.31	687.44	687.57	687.69	687.82	687.95	688.07	688.2
542	688.33	688.45	688.58	688.71	688.84	688.96	689.09	689.22	689.34	689.4
543	689.60	689.72	689.85	689.98	690.11	690.23	690.36	690.49	690.61	690.7
544	690.87	690.99	691.12	691.25	691.38	691.50	691.63	691.76	691.88	692.0
545	692.14	692.26	692.39	692.52	692.65	692.77	692,90	693.03	693.15	693.2
546	693.41	693.53	693.66	693.79	693.91	694.04	694.17	694.30	694.42	694.5
547	694.68	694.80	694.93	695.06	695.19	695.31	695.44	695.57	695.69	695.8
548	695.95	696.07	696.20	696.33	696.46	696.58	696.71	696.84	696.96	697.0
549	697.22	697.34	697.47	697.60	1	697.85	697.98	698.11	698.23	698.3
27.5 In.	031.22	097.04	037.47	097.00	697.73	097.33	037.93	093.11	093.23	050.0
550	698.49	698.61	698.74	698.87	699.00	699.12	699.25	699.38	699.50	699.6
551	699.76	699.88	700.01	700.14	700.27	700.39	700.52	700.65	700.77	700.9
552	701.03	701.15	701.28	701.41	701.54	701.66	700.32	701.92	702.04	702.1
11		ì				!		i	l .)
553	702.30	702.42	702.55	702.68	702.81	702.93	703.06	703.19	703.31	703.4
554	703.57	703.69	703.82	703.95	704.08	704.20	704.33	704.46	704.58	704.7
555	704.84	704.96	705.09	705.22	7 05 . 35	705.47	705.60	705.73	705.85	705.9
556	706.11	706.23	706.36	706.49	706.62	706.74	706.87	707.00	707.12	707.2
557	707.38	707.50	707.63	707.76	707.89	708.01	708.14	708.27	708.39	708.5
558	708.65	708.77	708.90	709.03	709.16	709.28	709.41	709.54	709.66	709.7
559 28 Inch.	709.92	710.14	710.27	710.40	710.53	710.65	710.78	710.81	710.93	711.0
560	711.19	711.31	711.44	711.57	711.70	711.82	711.95	712.08	712.20	712.3
561	712.46	712.58	712.71	712.84	712.97	713.09	713.22	713.35	713.47	713.6
562	713.73	713.85	713.98	714.11	714.24	714.36	714.49	714.62		714.8
563	715.00	715.12	715.25	714.11					l 1	716.1
564	716.27	716.12	716.52	716.65	715.51 716.78	715.63 716.90	715.76 717.03	715.89 717.16	716.01 717.28	716.1
565	717.54	717.66	717.79	717.92	718.04	718.17	718.30	718.43	718.55	718.6
566	718.81	718.93						719.70	l	
15			719.06	719.19	719.31	719.44	719.57		719.82	719.9
567	720.08	720.20	720.33	720.46	720.58	720.71	720.84	720.97	721.09	721.2
568	721.35	721.47	721.60	721.73	721.85	721.98	722.11	722.24	722.36	722.4
569	722.62	722.74	722.87	723.00	723.12	723.25	723.38	723.51	723.63	723.7

1 Russian Half-Line = 1.269977 Millimetre.

Russian					Ter	iths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
28.5 Inch.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
570	723.89	724.01	724.14	724.27	724.39	724.52	724.65	724.78	724.90	725.0
571	725.16	725.28	725.41	725.54	725.66	725.79	725.92	726.05	726.17	726.3
572	726.43	726.55	726.68	726.81	726.93	727.06	727.19	727.32	727.44	727.5
573	727.70	727.82	727.95	728.08	728.20	728.33	728.46	728.59	728.71	728.8
574	728.97	729.08	729.21	729.34	729.46	729.59	729.73	729.85	729.97	730.1
575	730.24	730.36	730.49	730.62	730.74	730.87	731.00	731.13	731.25	731.3
576	731.51	731.63	731.76	731.89	732.01	732.14	732.27	732.40	732.52	732.6
577	732.78	732.90	733.03	733.16	733.28	733.41	733.54	733.67	733.79	733.9
57 8	734.05	734.17	734.30	734.43	734.55	734.68	734.S1	734.94	735.06	735.1
579	735.32	735.44	735.57	735.70	735.82	735.95	7 36.08	736.21	736.33	736.4
29 Inch.	*00 *0	**************************************	* 00.04	****	mom 00		****			
580	736.59	736.71	736.84	736.97	737.09	737.22	737.35	737.48	737.60	737.7
581	737.86	737.98	738.11	738.24	738.36	738.49	738.62	738.75	738.87	739.0
582	739.13	739.25	739.38	739.51	739.63	739.76	739.89	740.02	740.14	740.2
583	740.40	740.52	740.65	740.78	740.90	741.03	741.16	741.29	741.41	741.5
584	741.67	741.79	741.92	742.05	742.17	742.30	742.43	742.56	742.68	742.8
585	742.94	743.06	743.19	743.32	743.44	743.57	743.70	743.83	743.95	744.0
586	744.21	744.33	744.46	744.59	744.71	744.84	744.97	745.10	745.22	745.3
587	745.48	745.60	745.73	745.86	745.98	746.11	746.24	746.37	746.49	746.6
588	746.75	746.87	747.00	747.13	747.25	747.38	747.51	747.64	747.76	747.8
589 29.5 In.	748.02	748.14	748.27	748.40	748.52	748.65	748.78	748.91	749.03	749.1
590	749.29	749.41	749.54	749.67	749.79	749.92	750.05	750.18	750.30	750.4
591	750.56	750.68	750.81	750.94	751.06	751.19	751.32	751.45	751.57	751.7
592	751.83	751.95	752.08	752.21	752.33	752.46	752.59	752.72	752.84	752.9
593	753.10	753.22	753.35	753.48	753.60	753.73	753.86	753.99	754.11	754.2
594	754.37	754.49	754.62	754.75	754.87	755.00	755.13	755.26	755.38	755.5
595	755.64	755.76	755.89	756.02	756.14	756.27	756.40	756.53	756.65	756.7
596	756.91	757.03	757.16	757.29	757.41	757.54	757.67	757.80	757.92	758.0
597	758.18	758.30	758.43	758.56	758.68	758.81	758.94	759.07	759.19	759.3
598	759.45	759.57	759.70	759.84	759.96	760.09	760.21	760.34	760.46	760.5
599	760.72	760.84	760.97	761.10	761.22	761.35	761.48	761.61	761.73	761.S
30 Inch.										
600	761.99	762.11	762.24	762.37	762.49	762.62	762.75	762.88	763.00	763.13
601	763.26	763.38	763.51	763.64	763.76	763.89	764.02	764.15	764.27	764.4
602	764.53	764.65	764.78	764.91	765.03	765.16	765.29	765.42	765.54	765.6
603	765.80	765.92	766.05	766.18	766.30	766.43	766.56	766.69	766.81	766.9
604	767.07	767.19	767.32	767.45	767.57	767.70	767.83	767.96	768.08	768.2
605	768.34	768.46	768.59	768.72	768.84	768.97	769.10	769.23	769.35	769.48
606	769.61	769.73	769.85	769.99	770.11	770.24	770.37	770.50	770.62	770.75
607	770.88	771.00	771.13	771.26	771.38	771.51	771.64	771.77	771.89	772.02
608 609	772.15	772.27	772.40	772.53	772.65	772.78	772.91 774.18	773.03	773.16	773.29
000	773.42	773.54	773.67	773.80	773.92	774.05	114.15	774.30	774.43	774.50
				Hu	indredths.					
0.000	0.013	0.025	0.038	0.051	ı 0.06	63 0.0	076 0	.089	0.102	0.114

1 Russian Half-Line = 0.562976 Paris Line.

Russian					Units or R	ussian Half	Lines.			
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
22 Inch.	Par. line.	Par line.	Par. line	Par line.	Par line.	Par line.	Par. line.	Par. line	Par line	Par. line
440	247.71	248.27	248.84	249.40	249.96	250.52	251.09	251.65	252.21	252.78
450	253.34	253.90	254.47	255.03	255.59	256.15	256.72	257.28	257.84	258.41
460	258.97	259.53	260.09	260.66	261.22	261.78	262.35	262.91	263.47	264.04
470	264.60	265.16	265.72	266.29	266.85	267.41	267.98	268.54	269.10	269.67
480	270.23	270.79	271.35	271.92	272.48	273.04	273.61	274.17	274.73	275.30
24.5 In.						ĺ	ĺ			
490	275.86	276.42	276.98	277.55	278.11	278.67	279.24	279. S0	280.36	280.93
500	281.49	282.05	282.61	283.18	283.74	284.30	284.87	285.43	285.99	286.50
510	287.12	287.68	288.24	288.81	289.37	289.93	290.50	291.06	291.62	292.18
520	292.75	293.31	293.87	294.44	295.00	295.56	296.13	296.69	297.25	297.81
530	298.38	298.94	299.50	300.07	300.63	301.19	301.76	302.32	302.88	303.4
Russian					Ten	ths.				
Half-Lines	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
27 Inch.	Par. line	Par line.	Par. line.	Par. line.	Par. line.	Par line.	Par line.	Par. line	Par line	Par. line
540	304.01	304.06	304.12	304.18	304.23	304.29	304.34	304.40	304.46	304.51
541	304.57	304.63	304.68	304.74	304.80	304.85	304.91	304.96	305.02	305.08
542	305.13	305.19	305.25	305.30	305.36	305.41	305.47	305.53	305.58	305.64
543	305.70	305.75	305.81	305.86	305.92	305.98	306.03	306.09	306.15	306.20
544	306.26	306.32	306.37	306.43	306.48	306.54	306.60	306.65	306.71	306.77
545	306.S2	306.88	306.93	306.99	307.05	307.10	307.16	307.22	307.27	307.38
546	307.38	307.44	307.50	307.55	307.61	307.67	307.72	307.78	307.84	307.89
547	307.95	303.00	308.06	308.12	308.17	308.23	308.29	308.34	308.40	308.48
548	308.51	308.57	308.62	308.68	308.74	308.79	308.85	308.90	308.96	309.03
549	309.07	309.13	309.19	309.24	309.30	309.36	309.41	309.47	309.52	309.58
27.5 In.	000.01	000110	300.10	000.21	000.00	000.00	000.11	000111	000.02	000.00
550	309.64	309.69	309.75	309.81	309.86	309.92	309.97	310.03	310.09	310.1-
551	310.20	310.26	310.31	310.37	310.42	310.48	310.54	310.59	310.65	310.71
552	310.76	310.82	310.88	310.93	310.99	311.04	311.10	311.16	311.21	311.27
553	311.33	311.38	311.44	311.49	311.55	311.61	311.66	311.72	311.78	311.88
554	311.89	311.95	312.00	312.06	312.11	312.17	312.23	312.28	312.34	312.40
555	312.45	312.51	312.56	312.62	312.68	312.73	312.79	312.85	312.90	312.96
556	313.01	313.07	313.13	313.18	313.24	313.30	313.35	313.41	313.47	313.52
557	313.56	313.63	313.69	313.75	313.80	313.86	313.92	313.97	314.03	314.08
558	314.14	314.20	314.25	314.31	314.37	314.42	314.48	314.53	314.59	314.63
559	314.70				1			315.10		
28 Inch.	914.70	314.76	314.82	314.87	314.93	314.99	315.04	313.10	315.15	315.21
560	315.27	315.32	315.38	315.44	315.49	315.55	315.60	315.66	315.72	315.77
561	315.83	315.89	315.94	316.00	316.05	316.11	316.17	316.22	316.28	316.34
562	316.39	316.45	316.51	316.56	316.62	316.67	316.73	316.79	316.84	316.90
563	316.96	317.01	317.07		317.18	317.24	317.29	317.35	317.41	317.46
564	317.52	317.57	317.63	317.12 317.69	317.74	317.24	317.29	317.91	317.41	318.03
565	318.08	318.14	318.19	318.25	318.31	318.36	318.42	318.48	318.53	318.59
566	318.64	318.70	318.76	318.81	318.87	318.93	318.98	319.04	319.09	319.15
				1				319.60		319.71
- 11	319.21	319 <i>96</i>	319 32							
567 568	319.21 319.77	319.26 319.83	319.32 319.88	319.38 319.94	319.43 320.00	319.49 320.05	319.55 320.11	320.16	$319.66 \\ 320.22$	320.28

COMPARISON OF THE RUSSIAN AND OLD FRENCH BAROMETERS.

1 Russian Half-Line = 0.562976 Paris Line.

Russian										
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
28.5 Inch.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line
570	320.90	320.95	321.01	321.07	321.12	321.18	321.23	321.29	321.35	321.40
571	321.16	321.52	321.57	321.63	321.68	321.74	321.80	321.85	321.91	321.97
572	322.02	322.08	322.13	322.19	3 2 2.25	322.30	322.36	322.42	322.47	322.53
573	322.59	322.64	322.70	322.75	322.81	322.87	322.92	322.98	323.04	323.09
574	323.15	323.20	323.26	323.32	323.37	323.43	323.49	323.54	323.60	323.65
575	323.71	328.77	323.82	323.88	323.94	323.99	324.05	324.11	324.16	324.22
576	324.27	324.33	324.39	324.44	324.50	324.56	324.61	324.67	324.72	324.78
577	324.84	324.89	324.95	325.01	325.06	325.12	325.17	325.23	325.29	325.3
578	325.40	325.46	325.51	325.57	325.63	325.68	325.74	325.79	325.85	325.9
579	325.96	326.02	326.08	326.13	326.19	326.24	326.30	326.36	326.41	326.47
29 Inch.										
580	326.53	326.58	326.64	326.69	326.75	326.81	326.86	326.92	326.98	327.03
581	327.09	327.15	327.20	327.26	327.31	327.37	327.43	327.48	327.54	327.60
582	327.65	327.71	327.76	327.82	327.88	327.93	327.99	328.05	328.10	328.10
583	328.22	328.27	328.33	328.38	328.44	328.50	328.55	328.61	328.67	328.7
584	328.78	328.83	328.89	328.95	329.00	329.06	329.12	329.17	329.23	329.2
585	329.34	329.40	329.45	329.51	329.57	329.62	329.68	329.74	329.79	329.8
586	329.90	329.96	330.02	330.07	330.13	330.19	330.24	330.30	330.35	330.4
587	330.47	330.52	330.58	330.64	330.69	330.75	330.80	330.86	330.92	330.9
588	331.03	331.09	331.14	331.20	331.26	331.31	331.37	331.42	331.48	331.5
589	331.59	331.65	331.71	331.76	331.82	331.87	331.93	331.99	332.04	332.1
29.5 In. 590	332.16	332.21	332.27	332.32	332.38	332.44	332.49	332.55	332.61	332.6
591	332.72	332.78	332.83	332.89	332.94	333.00		333.11		ł
1		- 1					333.06		333.17	333.2
592	333.28	333.34	333.39	333.45	333.51	333.56	333.62	333.68	333.73	333.79
593 594	333.84 334.41	333.90 334.46	333.96 334.52	334.01 334.58	334.07 334.63	334.13 334.69	334.18 334.75	334.24 334.80	334.30 334.86	334.3 334.9
595	334.97	335.03	335.08	335.14	335.20	335.25	335.31	335.36	335.42	335.4
596	335.53	335.59	335.65	335.70	335.76	335.82	335.87	335.93	335.98	336.0
597	336.10	336.15	336.21	336.27	336.32	336.38)	336.49		336.60
- 1							336.43		336.55	
598	336.66	336.72	336.77	336.83	336.88	336.94	337.00	337.05	337.11	337.1
599 30 Inch.	337.22	337.28	337.34	337.39	337.45	337.50	337.56	337.62	337.67	337.73
600	337.79	337.84	337.90	337.95	338.01	338.07	338.12	338.18	338.24	338.29
601	338.35	338.40	338.46	338.52	338.57	338.63	338.69	338.74	338.S0	338.86
602	338.91	338.97	339.02	339.08	339.14	339.19	339.25	339.31	339,36	339.42
603	339.47	339.53	339.59	339.64	339.70	339.76	339.81	339.87	339.92	339.98
11	340.04					340.32			340.49	
604	040.04	340.09	340.15	340.21	340.26	940.92	340.38	310.43	940.49	340.5
605	340.60	340.66	340.71	340.77	340.83	340.88	340.94	340.99	341.05	341.1
606	311.16	341.22	341.28	341.33	341.39	341.44	341.50	341.56	341.61	341.67
607	341.73	341.78	341.84	341.90	341.95	342.01	342.06	342.12	342.18	342.23
603	342.29	342.35	312.40	342.46	342.51	342.57	342.63	342.68	342.74	342.80
609	342.85	342.91	342.96	313.02	343.08	343.13	343.19	343.25	343.30	343.36
				Ifi	andredths.					
0.000	0.006	0.011	0.017	0.02	2 0.0	e 0.0	034 0	.039	0.045	0.051



IX. - XVI.

COMPARISON

OF

BAROMETRICAL DIFFERENCES

EXPRESSED IN MEASURES OF DIFFERENT SCALES,

OR

TABLES

FOR CONVERTING ENGLIST/ INCHES, MILLIMETRES, PARIS LINES, AND RUSSIAN HALF-LINES INTO EACH OTHER.

 \mathbb{C}



IX. CONVERSION OF ENGLISH INCHES INTO MILLIMETRES.

1 English Inch = 25.39954 Millimetres.

English				П	undredths	of an Inc	h.			
Inctes and Tenths.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0.0	0.000	0.254	0.508	0.762	1.016	1.270	1.524	1.778	2.032	2.286
0.1	2.540	2.794	3.048	3.302	3.556	3.810	4.064	4.318	4.572	4.826
0.2	5.080	5.334	5.588	5.842	6.096	6.350	6.604	6.858	7.112	7.366
0.3	7.620	7.874	8.128	8.382	8.636	8.890	9.144	9.398	9.652	9.906
0.4	10.160	10.414	10.668	10.922	11.176	11.430	11.684	11.938	12.192	12.446
0.5	12.700	12.954	13.208	13.462	13.716	13.970	14.224	14.478	14.732	14.986
0.6	15.240	15.494	15.748	16.002	16.256	16.510	16.764	17.018	17.272	17.526
0.7	17.780	18.034	18.288	18.542	18.796	19.050	19.304	19.558	19.812	20.066
0.8	20.320	20.574	20.828	21.082	21.336	21.590	21.844	22.098	22.352	22.606
0.9	22.860	23.114	23.368	23.622	23.876	24.130	24.384	24.638	24.892	25.146
1.0	25.400	25.654	25.908	26.162	26.416	26.670	26.924	27.178	27.432	27.685
1.1	27.939	28.193	28.447	28.701	28.955	29.209	29.463	29.717	29.971	30.225
1.2	30.479	30.733	30.987	31.241	31.495	31.749	32.003	32.257	32.511	32.765
1.3	33.019	33.273	33.527	33.781	34.035	34.289	34.543	34.797	35.051	35.305
1.4	35.559	35.813	36.067	36.321	36.575	36.829	37.083	37.337	37.591	37.845
1.5	38.099	38.353	38.607	38.861	39.115	39.369	39.623	39.877	40.131	40.385
1.6	40.639	40.893	41.147	41.401	41.655	41.909	42.163	42.417	42.671	42.925
1.7	43.179	43.433	43.687	43.941	44.195	44.449	44.703	44.957	45.211	45.465
1.8	45.719	45.973	46.227	46.481	46.735	46.989	47.243	47.497	47.751	48.005

X. CONVERSION OF ENGLISH INCHES INTO FRENCH OR PARIS LINES. $1 \ {\rm English \ Inch} = 11.259515 \ {\rm Paris \ Lines}.$

English				1	Inndredths	of an Inc	h.			
Inches and Tentlis.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line
0.0	0.000	0.113	0.225	0.338	0.450	0.563	0.676	0.788	0.901	1.013
0.1	1.126	1.239	1.351	1.464	1.576	1.689	1.802	1.914	2.027	2.139
0.2	2.252	2.364	2.477	2.590	2.702	2.815	2.927	3.040	3.153	3.265
0.3	3.378	3.490	3.603	3.716	3.828	3.941	4.053	4.166	4.279	4.391
0.4	4.504	4.616	4.729	4.842	4.954	5.067	5.179	5.292	5.405	5.517
0.5	5.630	5.742	5.855	5.968	6.080	6.193	6.305	6.418	6.531	6.643
0.6	6.756	6.868	6.981	7.093	7.206	7.319	7.431	7.544	7.656	7.769
0.7	7.882	7.994	8.107	8.219	8.332	8.445	8.557	8.670	8.782	8.895
0.8	9.008	9.120	9.233	9.345	9.458	9.571	9.683	9.796	9.908	10.021
0.9	10.134	10.246	10.359	10.471	10.584	10.697	10.809	10.922	11.034	11.147
1.0	11.260	11.372	11.485	11.597	11.710	11.822	11.935	12.048	12.160	12.273
1.1	12.385	12.498	12.611	12.723	12.836	12.948	13.061	13.174	13.286	13.399
1.2	13.511	13.624	13.737	13.849	13.962	14.074	14.187	14.300	14.412	14.525
1.3	14.637	14.750	14.863	14.975	15.088	15.200	15.313	15.426	15.538	15.651
1.4	15.763	15.876	15.988	16.101	16.214	16.326	16.439	16.551	16.664	16.777
1.5	16.889	17.002	17.114	17.227	17.340	17.452	17.565	17.677	17.790	17.903
1.6	18:015	18.128	18.240	18.353	18.466	18.578	18.691	18,803	18.916	19.029
1.7	19.141	19.254	19.366	19.479	19.592	19.704	19.817	19.929	20.042	20.155
1.8	20.267	20.380	20.492	20.605	20.717	20.830	20.943	21.055	21.168	21.280

XI. CONVERSION OF MILLIMETRES INTO ENGLISH INCHES.

1 Metre = 39.37079 English Inches.

Millime-				7	Tenths of a	Millimetr	e.			
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. I
0	0.0000	0.0039	0.0079	0.0118	0.0157	0.0197	0.0236	0.0276	0.0315	0.035
1	0.0394	0.0433	0.0472	0.0512	0.0551	0.0591	0.0630	0.0669	0.0709	0.074
2	0.0787	0.0827	0.0866	0.0906	0.0945	0.0984	0.1024	0.1063	0.1102	0.114
3	0.1181	0.1220	0.1260	0.1299	0.1339	0.1378	0.1417	0.1457	0.1496	0.153
4	0.1575	0.1614	0.1654	0.1693	0.1732	0.1772	0.1811	0.1850	0.1890	0.192
5	0.1969	0.2008	0.2047	0.2087	0.2126	0.2165	0.2205	0.2244	0.2283	0.232
6	0.2362	0.2402	0.2441	0.2480	0.2520	0.2559	0.2598	0.2638	0.2677	0.271
7	0.2756	0.2795	0.2835	0.2874	0.2913	0.2953	0.2992	0.3032	0.3071	0.311
8	0.3150	0.3189	0.3228	0.3268	0.3307	0.3347	0.3386	0.3425	0.3465	0.350
9	0.3543	0.3583	0.3622	0.3661	0.3701	0.3740	0.3780	0.3819	0.3858	0.389
10	0.3937	0.3976	0.4016	0.4055	0.4095	0.4134	0.4173	0.4213	0.4252	0.429
11	0.4331	0.4370	0.4410	0.4449	0.4488	0.4528	0.4567	0.4606	0.4646	0.468
12	0.4724	0.4764	0.4803	0.4843	0.4882	0.4921	0.4961	0.5000	0.5039	0.507
13	0.5118	0.5158	0.5197	0.5236	0.5276	0.5315	0.5354	0.5394	0.5433	0.547
14	0.5512	0.5551	0.5591	0.5630	0.5669	0.5709	0.5748	0.5788	0.5827	0.586
15	0.5906	0.5945	0.5984	0.6024	0.6063	0.6102	0.6142	0.6181	0.6221	0.626
16	0.6299	0.6339	0.6378	0.6417	0.6457	0.6496	0.6536	0.6575	0.6614	0.665
17	0.6693	0.6732	0.6772	0.6811	0.6851	0.6890	0.6929	0.6969	0.7008	0.704
18	0.7087	0.7126	0.7165	0.7205	0.7244	0.7284	0.7323	0.7362	0.7402	0.744
19	0.7480	0.7520	0.7559	0.7599	0.7638	0.7677	0.7717	0.7756	0.7795	0.783
20	0.7874	0.7914	0.7953	0.7992	0.8032	0.8071	0.8110	0.8150	0.8189	0.822
21	0.8268	0.8307	0.8347	0.8386	0.8425	0.8465	0.8504	0.8543	0.8583	0.862
22	0.8662	0.8701	0.8740	0.8780	0.8819	0.8858	0.8898	0.8937	0.8977	0.901
23	0.9055	0.9095	0.9134	0.9173	0.9213	0.9252	0.9292	0.9331	0.9370	0.941
24	0.9149	0.9488	0.9528	0.9567	0.9606	0.9646	0.9685	0.9725	0.9764	0.980
25	0.9843	0.9882	0.9921	0.9961	1.0000	1.0040	1.0079	1.0118	1.0158	1.019
26	1.0236	1.0276	1.0315	1.0355	1.0394	1.0433	1.0473	1.0512	1.0551	1.059
27	1.0630	1.0669	1.0709	1.0748	1.0788	1.0827	1.0866	1.0906	1.0945	1.098
28	1.1024	1.1063	1.1103	1.1142	1.1181	1.1221	1.1260	1.1299	1.1339	1.137
29	1.1418	1.1457	1.1496	1.1536	1.1575	1.1614	1.1654	1.1693	1.1732	1.177
30	1.1811	1.1851	1.1890	1.1929	1.1969	1.2008	1.2047	1.2087	1.2126	1.216
31	1.2205	1.2244	1.2284	1.2323	1.2362	1.2402	1.2441	1.2481	1.2520	1.255
32	1.2599	1.2638	1.2677	1.2717	1.2756	1.2796	1.2835	1.2874	1.2914	1.295
33	1.2992	1.3032	1.3071	1.3110	1.3150	1.3189	1.3229	1.3268	1.3307	1.334
34	1.3386	1.3425	1.3465	1.3504	1.3544	1.3583	1.3622	1.3662	1.3701	1.374
35	1.3780	1.3819	1.3859	1.3898	1.3937	1.3977	1.4016	1.4055	1.4095	1.413
36	1.4173	1.4213	1.4252	1.4292	1.4331	1.4370	1.4410	1.4449	1.4488	1.452
37	1.4567	1.4607	1.4646	1.4685	1.4725	1.4764	1.4803	1.4843	1.4882	1.492
38	1.4961	1.5000	1.5040	1.5079	1.5118	1.5158	1.5197	1.5236	1.5276	1.531
39	1.5355	1.5394	1.5433	1.5473	1.5512	1.5551	1.5591	1.5630	1.5670	1.570
40	1.5748	1.5788	1.5827	1.5866	1.5906	1.5945	1.5985	1.6024	1.6063	1.610
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

XII. CONVERSION OF MILLIMETRES INTO FRENCH OR PARIS LINES.

1 Millimetre = 0.443296 Paris Line.

fillime-		Tenths of a Millimetre. 0. 1. 2. 3. 4. 5. 6. 7. 8. 9.									
tres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
0	Par. line. 0.000	Par. line. 0.044	Par. line. 0.089	Par. line. 0.133	Par. line. 0.177	Par. line. 0.222	Par. line. 0.266	Par. line. 0.310	Par. line 0.355	Par. lin	
1	0.443	0.488	0.532	0.576	0.621	0.665	0.709	0.754	0.798	0.84	
2	0.887	0.931	0.975	1.020	1.061	1.108	1.153	1.197	1.241	1.28	
3	1.330	1.374	1.419	1.463	1.507	1.552	1.596	1.640	1.685	1.73	
4	1.773	1.818	1.862	1.906	1.950	1.995	2.039	2.083	2.128	2.17	
5	2.216	2.261	2.305	2.349	2.394	2.438	2.482	2.527	2.571	2.61	
6	2.660	2.704	2.748	2.793	2.837	2.881	2.926	2.970	3.014	3.03	
7	3.103	3.147	3.192	3.236	3.280	3.325	3.369	3.413	3.458	3.50	
8	3.546	3.591	3.635	3.679	3.724	3.768	3.812	3.857	3.901	3.9	
9	3.990	4.034	4.078	4.123	4.167	4.211	4.256	4.300	4.344	4.38	
10	4.433	4.477	4.522	4.566	4.610	4.655	4.699	4.743	4.788	4.83	
11	4.876	4.921	4.965	5.009	5.054	5.098	5.142	5.187	5.231	5.27	
12	5.320	5.364	5.408	5.453	5.497	5.541	5.586	5.630	5.674	5.71	
13	5.763	5.807	5.851	5.896	5.940	5.984	6.029	6.073	6.117	6.16	
14	6.206	6.250	6.295	6.339	6.383	6.428	6.472	6.516	6.561	6.60	
15	6.649	6.694	6.738	6.782	6.827	6.871	6.915	6.960	7.004	7.04	
16	7.093	7.137	7.181	7.226	7.270	7.314	7.359	7.403	7.447	7.49	
17	7.536	7.580	7.625	7.669	7.713	7.758	7.802	7.846	7.891	7.93	
18	7.979	8.024	8.068	8.112	8.157	8.201	8.245	8.290	8.334	8.37	
19	8.423	8.467	8.511	8.556	8.600	8.644	8.689	8.733	8.777	8.82	
20	8.866	8,910	8.955	8.999	9.043	9.088	9.132	9.176	9.221	9.26	
21	9.309	9.354	9.398	9.442	9.487	9.531	9.575	9.620	9.664	9.70	
22	9.753	9.797	9.841	9.886	9.930	9.974	10.018	10.063	10.107	10.15	
23	10.196	10.240	10.284	10.329	10.373	10.417	10.462	10.506	10.550	10.59	
24	10.639	10.683	10.728	10.772	10.816	10.861	10.905	10.949	10.994	11.08	
25	11.082	11.127	11.171	11.215	11.260	11.304	11.348	11.393	11.437	11.48	
26	11.526	11.570	11.614	11.659	11.703	11.747	11.792	11.836	11.880	11.92	
27	11.969	12.013	12.058	12.102	12.146	12.191	12.235	12.279	12.324	12.36	
28	12.412	12.457	12.501	12.545	12.590	12.634	12.678	12.723	12.767	12.81	
29	12.856	12.900	12.944	12.989	13.033	13.077	13.122	13.166	13.210	13.25	
30	13.299	13.343	13.388	13.432	13.476	13.521	13.565	13.609	13.654	13.69	
31	13.742	13.786	13.831	13.875	13.919	13.964	14.008	14.052	14.097	14.14	
32	14.185	14.230	14.274	14.318	14.363	14.407	14.451	14.496	14.540	14.58	
33	14.629	14.673	14.717	14.762	14.806	14.850	14.895	14.939	14.983	15.02	
34	15.072	15.116	15.161	15.205	15.249	15.294	15.338	15.382	15.427	15.47	
35	15.515	15.560	15.604	15.648	15.693	15.737	15.781	15.826	15.870	15.91	
36	15.959	16.003	16.047	16.092	16.136	16.180	16.225	16.269	16.313	16.35	
37	16.402	16.446	16.491	16.535	16.579	16.624	16.668	16.712	16.757	16.80	
38	16.845	16.890	16.934	16.978	17.023	17.067	17.111	17.156	17.200	17.24	
39	17.289	17.333	17.377	17.422	17.466	17.510	17.555	17.599	17.643	17.6 8	
40	17.732	17.776	17.820	17.865	17.909	17.953	17.998	18.042	18.086	18.13	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

1 Paris Line = 2.255829 Millimetres.

Paris					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.000	0.226	0.451	0.677	0.902	1.128	1.353	1.579	1.805	2.030
1	2.256	2.481	2.707	2.933	3.158	3.384	3.609	3.835	4.060	4.286
2	4.512	4.737	4.963	5.188	5.414	5.640	5.865	6.091	6.316	6.542
3	6.767	6.993	7.219	7.444	7.670	7.895	8.121	8.347	8.572	8.798
4	9.023	9.249	9.474	9.700	9.926	10.151	10.377	10.602	10.828	11.054
5	11.279	11.505	11.730	11.956	12.181	12.407	12.633	12.858	13.084	13.309
	li									
6	13.535	13.761	13.986	14.212	14.437	14.663	14.888	15.114	15.340	15.565
7	15.791	16.016	16.242	16.468	16.693	16.919	17.144	17.370	17.595	17.821
8	18.047	18.272	18.498	18.723	18.949	19.175	19.400	19.626	19.851	20.077
9	20.302	20.528	20.754	20.979	21.205	21.430	21.656	21.882	22.107	22.333
10	22.558	22.784	23.009	23.235	23.461	23.686	23.912	24.137	24.363	24.589
11	24.814	25.040	25.265	25.491	25.716	25.942	26.168	26.393	26.619	26.844
12	27.070	27.296	27.521	27.747	27.972	28.198	28.423	28.649	28.875	29.100
13	29.326	29.551	29.777	30.003	30.228	30.454	30.679	30.905	31.130	31.356
14	31.582	31.807	32.033	32.258	32.485	32.711	32.936	33.162	33.387	33.613
15	33.837	34.063	34.289	34.514	34.740	34.965	35.191	35.417	35.642	35.868
16	36.093	36.319	36.544	36.770	36.996	37.221	37.447	37.672	37.898	38.124
17	38.349	38.575	38.800	39.026	39.251	39.477	39.703	39.928	40.154	40.379
18	40.605	40.831	41.056	41.282	41.507	41.733	41.958	42.184	42.410	42.635

XIV. CONVERSION OF FRENCH OR PARIS LINES INTO ENGLISH INCHES. $1 \ {\rm Paris \ Line} = 0.088814 \ {\rm English \ Inch}.$

Paris					Tenths o	f a Line.				
Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In	Eng. In.	Eng. In.	Eng. In.	Eng. In.	Eng. In.
0	0.0000	0.0089	0.0178	0.0266	0.0355	0.0444	0.0533	0.0622	0.0711	0.0799
1	0.0888	0.0977	0.1066	0.1155	0.1243	0.1332	0.1421	0.1510	0.1599	0.1687
2	0.1776	0.1865	0.1954	0.2043	0.2132	0.2220	0.2309	0.2398	0.2487	0.2576
3	0.2664	0.2753	0.2842	0.2931	0.3020	0.3108	0.3197	0.3286	0.3375	0.3464
4	0.3553	0.3641	0.3730	0.3819	0.3908	0.3997	0.4085	0.4174	0.4263	0.4352
5	0.4441	0.4530	0.4618	0.4707	0.4796	0.4885	0.4974	0.5062	0.5151	0.5240
6	0.5329	0.5418	0.5506	0.5595	0.5684	0.5773	0.5862	0.5951	0.6039	0.6128
7	0.6217	0.6306	0.6395	0.6483	0.6572	0.6661	0.6750	0.6839	0.6927	0.7016
8	0.7105	0.0300	0.7283	0.7372	0.7460	0.7549	0.7638	0.0033	0.7816	0.7904
9	0.7993	0.8082	0.7283	0.7372	0.7400	0.1343	0.7033	0.8615	0.7310	0.7304
10	0.7993	0.8082	0.9059	0.9148	0.9237	0.9325	0.9414	0.9503	0.9592	0.9681
				i						
11	0.9770	0.9858	0.9947	1.0036	1.0125	1.0214	1.0302	1.0391	1.0480	1.0569
12	1.0658	1.0746	1.0835	1.0924	1.1013	1.1102	1.1191	1.1279	1.1368	1.1457
13	1.1546	1.1635	1.1723	1.1812	1.1901	1.1990	1.2079	1.2168	1.2256	1.2345
14	1.2434	1.2523	1.2612	1.2700	1.2789	1.2878	1.2967	1.3056	1.3144	1.3233
15	1.3322	1.3411	1.3500	1.3589	1.3677	1.3766	1.3855	1.3944	1.4033	1.4121
16	1.4210	1.4299	1.4388	1.4477	1.4565	1.4654	1.4743	1.4832	1.4921	1.5010
17	1.5098	1.5187	1.5276	1.5365	1.5454	1.5542	1.5631	1.5720	1.5809	1.5898
18	1.5987	1.6075	1.6164	1.6253	1.6342	1.6431	1.6519	1.6608	1.6697	1.6786

XV. CONVERSION OF RUSSIAN HALF-LINES INTO MILLIMETRES.

1 Russian Half-Line = 1.269977 Millimetres.

Russian					Ten	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.000	0.127	0.254	0.381	0.508	0.635	0.762	0.889	1.016	1.143
1	1.270	1.397	1.524	1.651	1.778	1.905	2.032	2.159	2.286	2.413
2	2.540	2.667	2.794	2.921	3.048	3.175	3.302	3.429	3.556	3.683
3	3.810	3.937	4.064	4.191	4.318	4.445	4.572	4.699	4.826	4.953
4	5.080	5.207	5.334	5.461	5.588	5.715	5.842	5.969	6.096	6.223
5	6.350	6.477	6.604	6.731	6.858	6.985	7.112	7.239	7.366	7.493
						ĺ				
6	7.620	7.747	7.874	8.001	8.128	8.255	8.382	8.509	8.636	8.763
7	8.890	9.017	9.144	9.271	9.398	9.525	9.652	9.779	9.906	10.033
8	10.160	10.287	10.414	10.541	10.668	10.795	10.922	11.049	11.176	11.303
9	11.430	11.557	11.684	11.811	11.938	12.065	12.192	12.319	12.446	12.573
10	12.700	12.827	12.954	13.081	13.208	13.335	13.462	13.589	13.716	13.843
11	13.970	14.097	14.224	14.351	14.478	14.605	14.732	14.859	14.986	15.113
12	15.240	15.367	15.494	15.621	15.748	15.875	16.002	16.129	16.256	16.383
13	16.510	16.637	16.764	16.891	17.018	17.145	17.272	17.399	17.526	17.653
14	17.780	17.907	18.034	18.161	18.288	18.415	18.542	18.669	18.796	18.923
15	19.050	19.177	19.304	19.431	19.558	19.685	19.812	19.939	20.066	20.193
16	20.320	20.447	20.574	20.701	20.828	20.955	21.082	21.209	21.336	21.463
17	21.590	21.717	21.844	21.971	22.098	22.225	22.352	22.479	22.606	22.733
18	22.860	22.987	23.114	23.241	23.368	23.495	23.622	23.749	23.876	24.003

XVI. CONVERSION OF RUSSIAN HALF-LINES INTO PARIS LINES.

¹ Russian Half-Line = 0.562976 Paris Line.

Russian					Ter	ths.				
Half-Lines.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. line	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.	Par. line.
0	0.000	0.056	0.113	0.169	0.225	0.281	0.338	0.394	0.450	0.507
1	0.563	0.619	0.676	0.732	0.788	0.844	0.901	0.957	1.013	1.070
2	1.126	1.182	1.239	1.295	1.351	1.407	1.464	1.520	1.576	1.633
3	1.689	1.745	1.802	1.858	1.914	1.970	2.027	2.083	2.139	2.196
4	2.252	2.308	2.364	2.421	2.477	2.533	2.590	2.646	2.702	2.759
5	2.815	2.871	2.927	2.984	3.040	3.096	3.153	3.209	3.265	3.322
6	3.378	3.434	3.490	3.547	3.603	3.659	3.716	3.772	3.828	3.885
7	3.941	3.997	4.053	4.110	4.166	4.222	4.279	4.335	4.391	4.448
8	4.501	4.560	4.616	4.673	4.729	4.785	4.842	4.898	4.954	5.010
9	5.067	5.123	5.179	5.236	5.292	5.348	5.405	5.461	5.517	5.573
10	5.630	5.686	5.742	5.799	5.855	5.911	5.968	6.024	6.080	6.136
11	6.193	6.249	6.305	6.362	6.418	6.474	6.531	6.587	6.643	6.699
12	6.756	6.812	6.868	6.925	6.981	7.037	7.093	7.150	7.206	7.262
13	7.319	7.375	7.431	7.488	7.544	7.600	7.656	7.713	7.769	7.825
14	7.882	7.938	7.994	8.051	8.107	8.163	8.219	8.276	8.332	8.388
15	8.445	8.501	8.557	8.614	8.670	8.726	8.782	8.839	8.895	8.951
16	9.008	9.064	9.120	9.177	9.233	9.289	9.345	9.402	9.458	9.514
17	9.571	9.627	9.683	9.739	9.796	9.852	9.908	9.965	10.021	10.077
18	10.134	10.190	10.246	10.302	10.359	10.415	10.471	10.528	10.584	10.640



TABLES

FOR

REDUCING BAROMETRICAL OBSERVATIONS,

TAKEN AT ANY TEMPERATURE,

TO THE TEMPERATURE OF THE FREEZING POINT.



TABLES

FOR

REDUCING THE BAROMETRICAL OBSERVATIONS TAKEN AT ANY TEMPERATURE TO THE TEMPERATURE OF THE FREEZING POINT.

The variations of the mercurial column in a stationary barometer are due to two causes, the changes of atmospheric pressure and the variations of temperature of the mercury, which affect the length of the column by changing its density. tions of atmospheric pressure, which alone the barometer is destined to ascertain, are therefore hidden, and their observation falsified by the expansion or contraction of the mercury due to changes of temperature. For, supposing that, while the atmospheric pressure remains the same, the temperature of the instrument becomes lower, the mercurial column will become shorter, and the barometer will appear to fall; if the pressure becomes less, but the temperature increases, the expansion of the mercury will tend to compensate the diminution of pressure, and the barometer may remain stationary, or even may rise, while it ought to be falling; in other cases the action of temperature will tend to increase the amount of the changes of the barometrical height. It is therefore evident that successive observations, with the same barometer, do not give directly the actual changes of atmospheric pressure, unless they have been taken exactly at the same temperature, a case which, in practice, seldom occurs. Likewise simultaneous observations, taken with various barometers, do not give directly the actual differences of the absolute pressure of the atmosphere above the instruments. To obtain the true barometrical heights, that is, the action of the atmospheric pressure alone, the influence of the temperature must first be eliminated from the observed heights. This is done by reducing, by means of the following Tables, the various barometrical columns to the length they would have at a given temperature, which is the same for all. For the sake of convenient comparison, the freezing point has been almost universally adopted as the standard temperature to which all observations are to be reduced.

Construction of the Tables.

In all the following Tables the barometers are supposed to be furnished with brass scales, extending from the surface of the mercury in the cistern to the top of the mercurial column. The correction to be applied is therefore composed of two elements: the correction for the expansion of the mercury, and that for the expansion of the scale; both of which ought to be, and have been, taken into account.

Indeed, the correction for the expansion of mercury is not sufficient to reduce the readings to the height which the barometer would indicate, under the same pressure, at the temperature of the freezing point. For when the temperature rises the mercurial column expands; but then the scale also grows longer, and this will tend to lower the reading of the height. The correction for the expansion of the mercury

 \mathbf{C}

must thus be diminished by the amount of that of the scale, that is, by nearly $\frac{1}{10}$, this being the proportion between the expansion of brass and that of mercury.

It is also the expansion of the scale which causes an apparent anomaly in the Tables for the Reduction of the English and Old French Barometers. It can be seen, that, though the observations are to be reduced to the freezing point, or to 32° Fahrenheit and zero Reaumur, the Tables give still a correction for observations taken at that temperature. The reason of it is, that the normal length of the English and Old French standards has not been determined at the temperature of the freezing point, as is the case with the metre, but respectively at the temperatures of 62° Fahrenheit and 13° Reaumur. It is thus only at these temperatures that the scales graduated with these standards have their true length. Above and below, the inches of the scales are longer or shorter than the inches of the standards. At the freezing point, therefore, the correction for the expansion of the mercury is null, but that for the expansion of the scale is not. The scale being too short, the reading will be too high, and a subtractive correction must still be applied, which will be gradually compensated at lower temperatures by the now additive correction of the mercurial column. Thus the point of no correction will occur at 28°.5 Fahrenheit, instead of 32°, in the English Barometer, and at -1°.5 Reaumur, instead of zero, in the Old French.

Schumacher has calculated and published in his Collection of Tables, &c., and in his Jahrbuch for 1836, 1837, and 1838, extensive tables for the reduction of the English, Old French, and Metrical Barometers, using the following general formula:—

Let h = observed height.

" t = temperature of the attached thermometer.

" T = temperature to which the observed height is to be reduced.

" m = expansion, in volume, of mercury.

" l = linear expansion of brass.

" ϑ = normal temperature of the standard scale.

The reduction to the freezing point will be given by the formula, -

$$h \cdot \frac{m(t-T)-l(t-\vartheta)}{1+m(t-T)}$$

The following tables, which may be found more convenient for ordinary use, have been calculated from the same formula. Table XVII., published in the Instructions of the Royal Society of London, is mostly abstracted from the table of Schumacher. It gives the reduction of the English Barometer, adopting the following values:—

Let h = observed height in English inches.

" t = temperature of attached thermometer in degrees of Fahrenheit.

" m = expansion, in volume, of mercury for one degree Fahrenheit = 0.0001001.

" l = linear expansion of brass for one degree Fahrenheit = 0.0000104344.

The normal temperature of standard being $=62^{\circ}$.

The reduction to 32° Fahrenheit will be given then by the formula,

$$-h \cdot \frac{m(t-32)-l(t-62)}{1+m(t-32)}$$
.

The elements for the other tables are found at the head of each.

XVII.

ENGLISH BAROMETER.

TABLE

GIVING THE CORRECTION TO BE APPLIED TO ENGLISH BAROMETERS,

WITH BRASS SCALES EXTENDING FROM THE CISTERN TO THE TOP OF
THE MERCURIAL COLUMN, FOR REDUCING THE OBSERVATIONS
TO THIRTY-TWO DEGREES FAHRENHEIT.

TABLE XVII.

The following Table, calculated after that of Schumacher, has been adopted by the Committee of Physics and Meteorology of the Royal Society of London. It gives immediately the correction for every degree of Fahrenheit, and for every half-inch from 20 up to 31 inches. The scale of the barometer is supposed to be of brass, extending from the cistern to the top of the mercurial column. The difference of expansion of brass and mercury is taken into account. The standard temperature of the yard being 62° Fahr., and not 32° Fahr., the difference of expansion of the scale and of the mercurial column carries the point of no correction down to 29° Fahr. Therefore, from 29° up the correction must be subtracted from, from 29° down it must be added to, the observed height.

Examples of Calculation.

Barometer, observed height, 30.231
Attached thermometer 82° Fahr.

See in the last page the column of 30 inches; go down as far as the horizontal line corresponding with 82° in the first vertical column, which contains the temperatures; you will find there the correction —.143. We have thus:—

Barometer, observed height,	•	•	•	30.231
Subtractive correction for 82° Fahr.,	•	•	•	 0.143
Barometer at 32° Fahr.,	•	•	•	30.088
Barometer, observed height,	•	•	•	29.743
Attached thermometer 25° Fahr.				
The column of 29.5 inches opposite to 25°	Fahr.	gives	an	
additive correction of,	•	•	•	+0.009
Barometer at 32° Fahr.,	•			29.752

It will be easy to apply also the correction for fractions of a degree Fahrenheit; for example:—

Barometer, observed height, 28.358
Attached thermometer 71.3

In the column of 28.5 inches, we find that the difference between the correction for 71° and that for 72° is .003; dividing this difference proportionally to the fraction, we have for three tenths of a degree a correction of —.001, which added to —.108, the correction for 71°, makes a total correction of,

And barometer at 32° Fahr., . . . 28.249

--.109

Degrees				Englisl	Inches.				Degree
of Fah- renheit.	20	20.5	21	21.5	22	22.5	23	23.5	of Fal renhei
0	+.051	+.053	+.054	+.055	+.056	+.058	+.059	+.060	0
ì	.049	.051	.052	.053	.054	.056	.057	.058	ľi
2	.048	.049	.050	.051	.052	.054	.055	.056	2
3	.046	.047	.048	.049	.050	.052	.053	.054	3
4 5	.044	.045 .043	.046 .044	.047 .045	.048	.050 .048	.051 .049	.052 .050	4 5
6	+.040	+.042	+.042	+.044	+.044	+.046	+.047	+.048	6
7	.039	.040	.041	.042	.042	.044	.044	.046	7
8 9	.037	.038	.039 .037	.040	.041	.041	.042	.043	8 9
10	.033	.034	.035	.036	.039 .03 7	.039 .037	.040	.041	10
11	+.031	+.032	+.033	+.034	+.035	+.035	+.036	+.037	11
12	.030	.030	.031	.032	.033	.033	.034	.035	12
13 14	.028 .026	.029 .027	.029 .027	.030	.031	.031	.032	.033	13
15	.024	.025	.026	.026	.029 .027	.029 .027	.030 .028	.031	14 15
16	+.022	+.023	+.024	+.024	+.025	+.025	+.026	+.026	16
17	.021	.021	.022	.022	.023	.023	.024	.024	17
18 19	.019 .017	.019 .018	.020 .018	.020	.021	.021	.022	.022	18
20	.015	.016	.016	.016	.019 .017	.017	.018	.020 .018	19 20
21	+.014	÷.014	+.014	+.015	+.015	+.015	+.015	+.016	21
22	.012	.012	.012	.013	.013	.013	.013	.014	22
$\frac{23}{24}$.010 .008	.010	.010	.011	.011	.011	.011	.012	23
25	.006	.008 .007	.009	.007	.009 .007	.007	.009	.010	24 25
26	+.005	+.005	+.005	+.005	+.005	+.005	+.005	+.005	26
27	.003	.003	.003	.003	.003	.003	.003	.003	27
28 29	.001 001	.001	.001 001	.001 001	.001	001 001	.001 001	.001	28 29
30	.003	001 .003	.003	.003	001 .003	.003	.003	001 .003	30
31	005	005	005	005	005	005	005	005	31
32	.006	.006	.007	.007	.007	.007	.007	.007	32
33 34	.008	.008	.008	.009	.009	.009	.009	.010	33
35	.010 $.012$.010 .012	.010 .012	.011 .013	.011 .013	.011 .013	.011 .013	.012	34 35
36	013	014	014	014	015	015	016	-016	36
37	.015	.016	.016	.016	.017	.017	.018	.018	37
38 39	.017 .019	.017	.018	.018 .020	.019	.019 .021	.020 .022	.020	38 39
40	.021	.019 .021	.020 .022	.020	.021 .023	.021	.022	.022 .024	40
4 l	022	023	024	024	025	025	026	026	41
42	.024	.025	.025	.026	.027	.027	.028	.028	42
43 44	.026 $.028$.027 .029	0.027 0.029	.028 .030	.029 .031	.029 .031	.030 $.032$.031	43 44
45	.030	.030	.029	.032	.033	.033	.032	.035	45
46	031	032	033	034	035	035	036	037	46
47	.033	.034	.035	.036	.036	.037	.038	.039	47
48	.035 $.037$.036	.037	.038	.038	.039	.040	.041	48
		.038	.039	.040	.040	.041	.042	.043	49 50
50 C	.038	.039	.040	.041	.042	043	.044	.045	

Degrees			•	English	Inches.				Degrees
of Fah- renheit.	20	20.5	21	21.5	22	22.5	23	23.5	of Fah- renheit.
51	040	041	042	043	044	045	046	047	51
52	.042	.043	.044	.045	.046	.047	.048	.049	52
53	.044	.045	.046	.047	.048	.049	.050	.052	53
54	.046	.047	.048	.049	.050	.051	.052	.054	54
55	.047	.049	.050	.051	.052	.053	.055	.056	55
56	049	050	052	053	054	055	057	058	56
57	.051	.052	.054	.055	.056	.057	.059	.060	57
58	.053	.054	.055	.057	.058	.059	.061	.062	58
59	.055	.056	.057	.059	.060	.061	.063	.064	59
60	.056	.058	.059	.061	.062	.063	.065	.066	60
61	058	060	061	062	064	065	067	068	61
62	.060	.061	.063	.064	.066	.067	.069	.070	62
63	.062	.063	.065	.066	.068	.069	.071	.072	63
64	.063	.065	.067	.068	.070	.071	.073	.075	64
65	.065	.067	.068	.070	.072	.073	.075	.077	65
66	067	069	070	072	074	075	077	079	66
67	.069	.071	.072	.074	.076	.077	.079	.081	67
68	.071	.072	.074	.076	.078	.079	.081	.083	68
69	.072	.074	.076	.078	.080	.081	.083	.085	69
70	.074	.076	.078	.080	.082	.083	.085	.087	70
71 72 73 74 75	076 .078 .079 .081 .083	078 .080 .081 .083 .085	080 .082 .083 .085 .087	082 .084 ·.085 .087 .089	083 .085 .087 .089	085 .087 .089 .091 .093	087 .089 .091 .093 .095	089 .091 .093 .095 .098	71 72 73 74 75
76	085	087	089	091	093	095	097	100	76
77	.087	.089	.091	.093	.095	.097	.100	.102	77
78	.088	.091	.093	.095	.097	.099	.102	.104	78
79	.090	.092	.095	.097	.099	.101	.104	.106	79
80	.092	.094	.096	.099	.101	.103	.106	.108	80
81	094	096	098	101	103	105	108	110	81
82	.095	.098	.100	.103	.105	.107	.110	.112	82
83	.097	.100	.102	.104	.107	.109	.112	.114	83
84	.099	.101	.104	.106	.109	.111	.114	.116	84
85	.101	.103	.106	.108	.111	.113	116	.118	85
86	103	105	108	110	113	115	118	120	86
87	.104	.107	.109	.112	.115	.117	.120	.123	87
88	.106	.109	.111	.114	.117	.119	.122	.125	88
89	.108	.111	.113	.116	.119	.121	.124	.127	89
90	.110	.112	.115	.118	.121	.123	.126	.129	90
91	111	114	-117	120	122	125	128	131	91
92	.113	.116	.119	.122	.124	.127	.130	.133	92
93	.115	.118	.121	.124	.126	.129	.132	.135	93
94	.117	.120	.122	.125	.128	.131	.134	.137	94
95	.118	.121	.124	.127	.130	.133	.136	.139	95
96	120	123	126	129	132	135	138	141	96
97	.122	.125	.128	.131	.134	.137	.140	.143	97
98	.124	.127	.130	.133	.136	.139	.142	.145	98
99	.125	.129	.132	.135	.138	.141	.144	.147	99
100	.127	.130	.134	.137	140	.143	.146	.150	100

Degrees				English	Inches.			*	Degrees
of Fahrenheit.	24	24.5	25	25.5	26	26.5	27	27.5	of Fah- renheit.
0	+.061	+.063	+.064	+.065	+.067	+.068	+.069	+.071	°
1	.059	.061	.062	.063	.064	.065	.067	.068	1
2	.057	.058	.060	.061	.062	.063	.064	.066	2
3	.055	.056	.057	.059	.060	.061	.062	.063	3
4 5	.053 .051	.054 .052	.055 .053	.056 .0 54	.057 .055	.058 .056	.059 .057	.061 .058	4 5
6	+.049	+.050	+.051	+.052	+.053	+.054	+.055	+.056	6
7	.046	.047	.048	.049	.050	.051	.052	.053	7
8 9	.044	.045	.046	.047	.048	.049	.050	.051	8
10	.042	.043 .041	.044	.045 .042	.046	.046 .044	.047 .045	.048	10
11	+.038	+.039	+.039	+.040	+.041	+.042	+.042	+.043	11
12	.036	.036	.037	.038	.039	.039	.040	.041	12
13	.033	.034	.035	.036	.036	.037	.038	.038	13
14	.031	.032	.033	.033	.034	.035	.035	.036	14
15	.029	.030	.030	.031	.032	.032	.033	.033	15
16	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	16
17	.025	.025	.026	.026	.027	.027	.028	.028	17
18 19	.023	.023	.024	.024	.025	.025	.025	.026	18
20	.021	.021	.021	.022	.022	.023	.023 .021	.024	19
	.010	.019		.020	.020	.020		.021	20
21	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	21
22 23	.014 .012	.014	.015	.015	.015	.016	.016	.016	22
24	.012	.012 .010	.012	.013 .010	.013	.013	.013 .011	.014	23 24
25	.008	.008	.008	.008	.008	.008	.009	.009	25
26	+.005	+.006	+.006	+.006	+.006	+.006	+.006	+.006	26
27	.003	.003	.003	.003	.004	.004	.004	.004	27
28	.001	.001	100.	.001	.001	.001	.001	.001	28
29	001	001	001	001	001	001	001	001	29
30	.003	.003	.003	.004	.004	.004	.004	.004	30
31 32	005	006	006	006	006	006	006	006	31
33	.008	.008 .010	.008 .010	.008	.008	.008	.008	.009	32
34	.012	.010	.010	.013	.011 .013	.013	.013	.011	33 34
35	.014	.014	.015	.015	.015	.015	.016	.016	35
36	016	017	017	017	017	018	018	019	36
37	.018	.019	.019	.019	.020	.020	.021	.021	37
38 39	.020	.021	.021	.022	.022	.023	.023	.023	38
40	.023 .025	.023 .025	.024 .026	.024	.024	.025 .027	.025 .028	.026	39
	.020	.023	.020	.020	.027	.027	.028	.028	40
41 42	027 .029	027	028	029	029	030	030	031	41
43	.029	.030	.030	.031	.031 .034	.032	.033 .035	.033	42 43
44	.033	.034	.035	.035	.034	.037	.037	.038	44
45	.035	.036	.037	.038	.038	.039	.040	.041	45
46	038	038	039	040	041	042	042	043	46
47	.040	.041	.041	.042	.043	.044	.045	.046	47
48	.042	.043	.044	.045	.045	.046	.047	.048	48
49 50	.044	.045	.046	.047	.048	.049	.050	.050	49
30	1040	.047	.048	.049	.050	.051	.052	.053	50

Degrees				English	Inches.				Degrees
of Fah- renheit.	24	24.5	25	25.5	26	26.5	27	27.5	of Fah- renheit.
51	048	049	050	051	052	053	054	055	51
52	.050	.052	.053	.054	.055	.056	.057	.058	52
53	.053	.054	.055	.056	.057	.058	.059	.060	53
54	.055	.056	.057	.058	.059	.060	.062	.063	54
55	.057	.058	.059	.060	.062	.063	.064	.065	55
56	059	060	061	063	064	065	066	068	56
57	.061	.062	.064	.065	.066	.068	.069	.070	57
58	.063	.065	.066	.067	.069	.070	.071	.073	58
59	.065	.067	.068	.070	.071	.072	.074	.075	59
60	.068	.069	.070	.072	.073	.075	.076	.077	60
61	070	071	073	074	075	077	078	080	61
62	.072	.073	.075	.076	.078	.079	.081	.082	62
63	.074	.076	.077	.079	.080	.082	.083	.085	63
64	.076	.078	.079	.081	.082	.084	.086	.087	64
65	.078	.080	.082	.083	.085	.086	.088	.090	65
66	080	082	084	085	087	089	090	092	66
67	.083	.084	.086	.088	.089	.091	.093	.095	67
68	.085	.086	.088	.090	.092	.094	.095	.097	68
69	.087	.089	.090	.092	.094	.096	.098	.100	69
70	.089	.091	.093	.095	.096	.098	.100	.102	70
71	091	093	095	097	099	101	102	104	71
72	.093	.095	.097	.099	.101	.103	.105	.107	72
73	.095	.097	.099	.101	.103	.105	.107	.109	73
74	.097	.099	.102	.104	.106	.108	.110	.112	74
75	.100	.102	.104	.106	.108	.110	.112	.114	75
76	102	104	106	108	110	112	114	117	76
77	.104	.106	.108	.110	.112	.115	117	.119	77
78	.106	.108	.110	.113	.115	.117	.119	.122	78
79	.108	.110	.113	.115	.117	.119	.122	.124	79
80	.110	.113	.115	.117	.119	.122	.124	.126	80
81	112	115	117	119	122	124	126	129	81
82	.114	.117	.119	.122	.124	.126	.129	.131	82
83	.117	.119	.121	.124	.126	.129	.131	.134	83
84	.119	.121	.124	.126	.129	.131	.134	.136	84
85	.121	.123	.126	.128	.131	.133	.136	.139	85
86	123	126	128	131	133	136	138	141	86
87	.125	.128	.130	.133	.136	.138	.141	.143	87
88	.127	.130	.133	.135	.138	.141	.143	.146	88
89	.129	.132	.135	.137	.140	.143	.146	.148	89
90	.131	.134	.137	.140	.142	.145	.148	.151	90
91	134	136	139	142	145	148	150	153	91
92	.136	.139	.141	.144	.147	.150	.153	.156	92
93	.138	.141	.144	.147	.149	.152	.155	.158	93
94	.140	.143	.146	.149	.152	.155	.157	.161	94
95	.142	.145	.148	.151	.154	.157	.160	.163	95
96	144	147	150	153	156	159	162	165	96
97	.146	.149	.152	.156	.159	.162	.165	.168	97
98	.148	.152	.155	.158	.161	.164	.167	.170	98
99	.151	.154	.157	.160	.163	.166	.169	.173	99
100	.153	.156	.159	.162	.165	.169	.172	.175	100

egrees of				English Inche	es.			Degrees o
Fahren- heit.	28	28.5	29	29.5	30	30.5	31	Fahren heit.
0	+.072	+.073	+.074	+.076	+.077	+.078	+.080	0
1	.069	.071	.072	.073	.074	.076	.077	0
2	.067	.068	.069	.070	.074	.073	.074	1
3	.064	.065	.067	.068	.069	.070	.071	3
4	.062	.063	.064	.065	.066	.067	.068	4
5	.059	.060	.061	.062	.063	.065	.066	5
6	+.057	+.058	+.059	+.060	+.061	+.062	+.063	6
7	.054	.055	.056	.057	.058	.059	.060	7
8	.052	.053	.054	.054	.055	.056	.057	8
9	.049	.050	.051	.052	.053	.054	.054	9
10	.047	.047	.048	.049	.050	.051	.052	10
11	+.044	+.045	+.046	+.046	+.047	+.048	+.049	11
12	.042	.042	.043	.044	.045	.045	.046	12
13	.039	.040	.040	.041	.042	.043	.043	13
14	.037	.037	.038	.038	.039	.040	.040	14
15	.034	.035	.035	.036	.036	.037	.038	15
16	+.032	+.032	+.033	+.033	+.034	+.034	+.035	16
17	.029	.030	.030	.031	.031	.032	.032	17
18	.026	.027	.027	.028	.028	.029	.029	18
19	.024	.024	.025	.025	.026	.026	.027	19
20	.021	.022	.022	.023	.023	.023	.024	20
21	+.019	+.019	+.020	+.020	+.020	+.021	+.021	21
22	.016	.017	.017	.017	.018	.018	.018	22
23	.014	.014	.014	.015	.015	.015	.015	23
24	.011	.012	.012	.012	.012	.012	.013	24
25	.009	.009	.009	.009	.009	.010	.010	25
26	+.006	+.006	+.007	+.007	+.007	+.007	+.007	26
27	.004	.004	.004	.004	.004	.004	.004	27
28	.001	.001	.001	.001	.001	.001	.001	28
29	061	001	001	001	001	001	001	29
30	.004	.004	.004	.004	.004	.004	.004	30
31	006	006	007	007	007	007	007	31
32	.009	.009	.009	.009	.009	.010	.010	32
33	.011	.012	.012	.012	.012	.012	.012	33
34	.014	.014	.014	.015	.015	.015	.015	34
35	.016	.017	.017	.017	.018	.018	.018	35
36 37	019	019	020	020	020	021	021	36
48	.021	.022	.022	.022	.023	.023	.024	37
39	.024 $.026$.024	.025	.025	.026	.026	.026	38
40	.029	.027 .029	.027 .030	.028 .030	.028 .031	.029 .031	.029	39 40
41	031	032	033	- 033	-021	034	035	41
42	.034	.034	.035	03 3 .036	034 .036	.034	.037	41 42
43	.036	.037	.038	.038	.039	.040	.040	43
44	.039	.040	.040	.041	.042	.040	.043	44
45	.041	.042	.043	.044	.044	.045	.046	45
46	044	045	045	046	047	048	049	46
47	.046	.047	.048	.049	.050	.051	.051	47
48	.049	.050	.051	.052	.052	.053	.054	48
49 50	.051	.052	.053	.054	.055	.056	.057	49
	.054	.055	.056	.057	.058	.059	.060	50

Fahren- heit. 51 52 53 54 55 56 57	056 .059 .061 .064 .066	057 .060	29	29.5	30	30.5	0.1	Fahren- hei t .
52 53 54 55 56	.059 .061 .064	.060			1	30.0	31	
52 53 54 55 56	.059 .061 .064	.060	058	059	060	061	062	51
54 55 56	.061 .064		.061	.062	.063	.064	.065	52
55 56		.063	.064	.065	.066	.067	.068	53
56	.066	.065	.066	.067	.068	.070	.071	54
		.068	.069	.070	.071	.072	.073	55
57 11	069	070	071	073	074	075	076	56
	.071	.073	.074	.075	.076	.078	.079	57
58 59	.074	.075	.077	.078	.079	.081	.082	58
60	.076 .079	.078	.079	.080	.082 .085	.083 .086	.085	59 60
61	001	000	004	000	007	000	000	
62	081 .084	083	084	086	087	089	090	61
63	.084	.085	.087	.088	.090 .093	.091	.093	62
64	.089	.090	.092	.091	.095	.094	.098	64
65	.091	.093	.095	.096	.098	.100	.101	65
66	094	096	097	099	101	102	104	66
67	.096	.098	.100	.102	.103	.105	.107	67
68	.099	.101	.102	.104	.106	.108	.109	68
69	.101	.103	.105	.107	.109	.110	.112	69
70	.104	.106	.108	.109	.111	.113	.115	70
71	106	108	110	112	114	116	118	71
72	.109	.111	.113	.115	.117	.119	.120	72
73	.111	.113	.115	.117	.119	.121	.123	73
74	.114	.116	.118	.120	.122	.124	.126	74
75	.116	.118	.120	.122	.125	.127	.129	75
76	119	121	123	125	127	129	131	76
77	.121	.123	.126	.128	.130	.132	.134	77
78	.124	.126	.128	.130	.133	.135	.137	78
79 80	.126 .129	.128 .131	.131 .13 3	.133 .136	.135 .138	.137 .140	.140 .143	79 80
.	191	104	100	100	141	140	-145	
81 82	131 .134	134 .136	136 .138	138 .141	141 .143	143 .146	145 .148	81 82
83	.134	.139	.138	.143	.145	.148	.151	83
84	.139	.141	.144	.146	.149	.151	.154	84
85,	.141	.144	.146	.149	.151	.154	.156	85
86	144	146	- .149	151	154	156	159	86
87	.146	.149	.151	.154	.157	.159	.162	87
88	.149	.151	.154	.157	.159	.162	.165	88
89	.151	.154	.156	.159	.162	.165	.167	89
90	.153	.156	.159	.162	.164	.167	.170	90
91	156	159	162	165	167	170	- 173	91
92	.158	.161	.164	.167	.170	.172	.175	92
93	.161	.164	.167	.170	.172	.175	.178	93
94 95	.163 .166	.166 .169	.169 .172	.172 .175	.175 .178	.177 .180	.180 .183	94 95
00	100	177	174	170	101	100	100	0.0
96 97	168 .171	171 .174	174 .177	178 .180	181 .183	183 .186	186 .189	96 97
98	.173	.174	.177	.183	.183	.186	.189	98
99	.176	.179	.182	.185	.188	.191	.194	99
100	.178	.181	.184	.188	.191	.194	.197	100

TABLE XVIII.

FOR REDUCING THE INDICATIONS OF ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO THE FREEZING POINT.

In most of the common barometers the scale is engraved upon a short plate of brass, or of ivory, fixed upon the wooden frame of the instrument. In such a case, the compound expansion of the two substances can only be guessed at, and the correction to be applied to the observations for reducing them to the freezing point cannot be determined with precision. As a near approximation for such imperfect instruments, the following table may be used. In computing this table, the expansion of glass, which is less than that of brass and greater than that of wood, has been substituted for that of brass, as an approximate value for a scale composed of these last two substances. The table thus gives the true correction, in English inches, for the barometers, the graduation of which is engraved on the glass tube itself. It answers equally for any English barometer with wooden scale, whatever be the substance of which the short plate bearing the graduation is made.

CORRECTIONS TO BE APPLIED TO ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO REDUCE THE OBSERVATIONS TO THE FREEZING POINT.

Attached Chermom-				Ba	rometer in	n English	Inches.				
eter, Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31
	+.076		1.070	. 000	. 000	1.000	1.005	1.000	+.088	+.089	+.090
0		+.077	+.079	+.080	+.082	+.083	+.085	+.086	+.085	+.089	+.088
1	+.073 $+.071$	$+.075 \\ +.072$	$+.076 \\ +.074$	+.078	+.079 +.076	+.080	+.082	+.080	+.083	+.083	+.085
2	+.06S	+.072	+.074	+.075	+.074	+.075	+.079	+.078	+.079	+.080	+.082
- 11	+.066	+.067	+.069	+.070	+.071	+.072	+.074	+.075	+.076	+.077	+.079
4	1.000	1.007	₩,009	7.070	7.071	7.072	1.074	7.075	+.070	1.077	1.013
5	+.064	+.065	+.066	+.067	+.068	+.070	+.071	+.072	+.073	+.074	+.076
6	+.061	+.062	+.063	+.065	+.066	+.067	+.068	+.069	+.070	+.072	+.073
7	+.059	+.060	+.061	+.062	+.063	+.064	+.065	+.067	+.068	+.069	+.070
8	+.056	+.057	+.058	+.059	+.060	+.061	+.063	+.064	+.065	+.066	+.067
	+.054	+.055	+.056	+.057	+.058	+.059	+.060	+.061	+.062	+.063	+.064
,	+.051	+.052	+.053	+.054	+.055	+.056	+.057	+.058	+.059	+.060	+.061
	+.049	+.050	+.051	+.051	+.052	+.053	+.054	+.055	+.056	+.057	+.058
	+.046	+.047	+.048	+.049	+.050	+.051	+.052	+.052	+.053	+.054	+.055
	+.044	+.045	+.045	+.046	+.047	+.048	+.049	+.050	+.050	+.051	+.052
	+.041	+.042	+.043	+.044	+.044	+.045	+.046	+.047	+.048	+.048	+.049
.	+.039	+.039	+.040	+.041	+.042	+.042	+.043	+.044	+.045	+.045	+.046
	+.036	+.037	+.038	+.038	+.039	+.040	+.040	+.041	+.042	+.043	+.043
	+.034	+.034	+.035	+.036	+.036	+.037	+.038	+.038	+.039	+.040	+.040
1	+.031	$\pm .032$	+.032	+.033	+.034	+.034	+.035	+.036	+.036	+.037	+.037
	+.029	+.029	+.030	+.030	+.031	+.032	+.032	+.033	+.033	+.034	+.034
]]	+.026	+.027	+.027	+.028	+.028	+.029	+.029	+.030	+.030	+.031	+.031

Barometer with Glass or Wooden Scale.

Attached Thermom-				Baro	ometer in	English I	nches.				
eter, Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31
•	+.024	+.024	+.025	+.025	+.026	+.026	+.027	+.027	+.028	+.028	+.028
21	+.021	+.024	+.023	+.023	+.022	+.023	+.024	+.024	1		+.025
22	+.019	+.019	+.022	+.020	+.022	+.023	+.021	+.024	+.025 +.022	+.025 + .022	+.023
$\begin{bmatrix} 23 \\ 24 \end{bmatrix}$	+.016	+.017	+.017	+.017	+.018	+.018	+.018	+.019	+.019	+.019	+.020
25	+.014	+.014	+.014	+.015	+.015	+.015	+.016	+.016	+.016	+.016	+.01
26	+.011	+.012	+.012	+.012	+.012	+.013	+.013	+.013	+.013	+.013	+.01
27	+.009	+.009	+.009	+.009	+.010	+.010	+.010	+.010	+.010	+.011	+.01
28	+.006	+.007	+.007	+.007	+.007	+.007	+.007	+.007	+.007	+.008	+.00
29	+.004	+.004	+.004	+.004	+.004	+.004	+.004	+.005	+.005	+.005	+.00
30	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.002	+.00
31	001	001	001	001	001	001	001	001	001	001	00
32	003	004	004	004	004	004	004	004	004	004	00
33	006	006	006	006	006	007	007	007	007	007	00
34	008	009	009	009	009	009	009	010	010	010	01
35	011	011	011	012	012	012	012	012	013	013	01
36	013	014	014	014	014	015	015	015	015	016	01
37	016	016	017	017	017	017	018	018	018	019	01
38	018	019	019	019	020	020	020	021	021	022	02
39	021	021	022	022	022	023	023	024	034	024	02
40	023	024	024	025	025	026	026	026	027	027	02
41	026	026	027	027	028	028	029	029	030	030	03
42	028	029	029	030	030	031	032	032	033	033	03
43	031	031	032	033	033	034	033	035	036	036	03
44	033	034	035	035	036	036	036	038	038	039	04
45	036	036	037	038	038	039	039	041	041	042	04
46	038	039	040	040	041	042	042	043	044	045	04
47	041	041	042	043	044	045	044	046	047	048	04
48	043	044	045	046	047	047	047	049	050	051	05
49	046	046	047	048	049	050	050	052	053	054	05
50	048	049	050	051	052	053	054	055	056	056	05
51	051	052	053	054	055	055	056	057	058	059	060
52	053	054	055	056	057	058	059	060	061	062	06
53	056	057	058	059	060	061	062	063	064	065	066
54	058	059	060	061	063	064	065	066	067	068	069
55	061	062	063	064	065	066	068	069	070	071	075
56	063	064	065	067	068	069	070	071	073	074	075
57	065	067	068	069	071	072	073	074	076	077	078
58	068	069	071	072	073	074	076	077	078	080	08
59	070	072	073	074	076	077	079	080	081	083	0S
60	073	074	076	077	079	080	081	083	084	085	087

Barometer with Glass or Wooden Scale.

Barometer with Glass or Wooden Scale.											
Attached Thermom- eter,	Barometer in English Inches.										
Fahren- heit.	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31
61	075	077	078	080	081	083	084	086	087	088	090
62	078	079	081	082	084	085	087	088	090	091	093
63	080	082	083	085	086	088	090	091	093	094	096
64	083	084	086	088	089	091	092	094	096	097	099
65	035	087	089	090	092	093	095	097	098	100	102
66	088	089	091	093	094	096	098	100	101	103	104
67	090	092	094	095	097	099	101	102	104	106	108
68	093	094	096	098	100	102	103	105	107	109	110
69	095	097	099	101	102	104	106	108	110	112	113
70	098	099	101	103	105	107	109	111	113	114	116
71	100	102	104	106	108	110	112	114	115	117	119
72	103	105	106	108	110	112	114	116	118	120	122
73	105	107	109	111	113	115	117	119	121	123	125
74	107	110	112	114	116	118	120	122	124	126	128
75	110	112	114	116	118	121	123	125	127	129	131
76	112	115	117	119	121	123	125	128	130	132	134
77	115	117	119	121	124	126	128	130	133	135	137
78	117	120	122	124	126	129	131	133	135	138	140
79	120	122	124	127	129	131	134	136	138	141	143
80	122	125	127	129	132	134	136	139	141	143	146
81	125	127	130	132	134	137	139	142	144	146	149
82	127	130	132	135	137	139	142	144	147	149	152
83	130	132	135	137	140	142	145	147	150	152	155
84	132	135	137	140	142	145	147	150	152	155	158
85	135	137	140	142	145	147	150	153	155	158	160
86	137	140	142	145	148	150	153	155	158	161	163
87	139	142	145	148	150	153	156	158	161	164	166
88	142	145	147	150	153	156	158	161	164	167	169
89	144	147	150	153	156	158	161	164	167	169	172
90	147	150	 153	155	158	161	164	167	169	172	175
91	149	152	155	158	161	164	167	169	172	175	178
92	152	155	158	161	163	166	169	172	175	178	181
93	154	157	160	163	166	169	172	175	178	181	184
91	157	160	163	166	169	172	175	178	181	184	187
95	159	162	165	168	171	174	178	181	184	187	190
96	162	165	168	171	174	177	180	183	186	190	193
97	164	167	170	174	177	180	183	186	189	192	196
98	167	170	173	176	179	183	186	189	192	195	199
99	169	172	175	179	182	185	188	192	195	198	201
100	171	175	178	181	 185	188	191	194	1 98	201	204

XIX.

METRICAL BAROMETER.

TABLE

FOR

REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO
THE TOP; CALCULATED FROM 260 TO 865 MILLIMETRES,
AND FOR EACH DEGREE CENTIGRADE.
By M. T. Delcros.



TABLE XIX.

This table has been calculated by using the following coefficients of dilatation:—
Brass, linear dilatation, from Laplace and Lavoisier for 100° C. = 0.0018782.

Mercury, dilatation in volume, from Dulong and Petit for 100° C. = 0.0180180.

Dilatation of the mercurial column for 100° C. . . . = 0.0161398.

Dilatation of the mercurial column for 1° C. . . . = 0.0001614.

Observed height reduced to freezing point,

$$H = h - h \ (0.0001614). \quad T = h - h \left(\frac{T}{6196}\right).$$

The second term of this last formula is given by the table, when the temperature T and the height h of the barometer are known; this correction must be *subtracted* from the observed height h, when the temperature is above freezing point; it is to be added when the temperature is below zero, or freezing point.

This table allows the barometrical heights taken at the highest summits, and in the deepest mines, to be corrected.

Examples of Calculation. Barometer, observed height, 567.49 Temperature of the barometer, +12°.7. Second page, $\begin{cases} \text{for } 10.0 = 0.912 \\ \text{for } 2.0 = 0.182 \\ \text{for } 0.7 = 0.064 \end{cases}$ Total, = 1.158Subtractive correction, - 1.16 Barometer at zero, 566.33 Barometer, observed height, 454.17 Temperature of the barometer, -7°.8. First page, $\begin{cases} \text{for } 7.0 = 0.514 \\ \text{for } 0.8 = 0.059 \end{cases}$ Total, = 0.573Additive correction, Barometer at zero,

Height of the	TEMPERATURE CENTIGRADE.											
of the Barome- ter.	1°	2°	3°	4°	5°	6°	70	80	90			
Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin			
260	0.042	0.084	0.126	0.168	0.210	0.252	0.294	0.336	0.37			
265	0.043	0.086	0.128	0.171	0.214	0.257	0.299	0.342	0.38			
270	0.044	0.087	0.131	0.174	0.218	0.261	0.305	0.349	0.39			
275	0.044	0.089	0.133	0.178	0.222	0.266	0.311	0.355	0.39			
280	0.045	0.090	0.136	0.181	0.226	0.271	0.316	0.362	0.40			
285	0.046	0.092	0.138	0.184	0.230	0.276	0.322	0.368	0.41			
290	0.047	0.094	0.140	0.187	0.234	0.281	0.328	0.374	0.42			
295	0.048	0.095	0.143	0.190	0.238	0.286	0.333	0.381	0.42			
300	0.048	0.097	0.145	0.194	0.242	0.291	0.339	0.387	0.43			
305	0.049	0.098	0.148	0.197	0.246	0.295	0.345	0.394	0.44			
310	0.050	0.100	0.150	0.200	0.250	0.300	0.350	0.400	0.45			
315	0.051	0.102	0.152	0.203	0.254	0.305	0.356	0.407	0.45			
320	0.052	0.103	0.155	0.207	0.258	0.310	0.361	0.413	0.46			
325	0.052	0.105	0.157	0.210	0.262	0.315	0.367	0.420	0.47			
330	0.053	0.106	0.160	0.213	0.266	0.320	0.374	0.426	0.47			
335	0.054	0.108	0.162	0.216	0.270	0.324	0.379	0.432	0.48			
340	0.055	0.110	0.165	0.219	0.274	0.329	0.384	0.439	0.49			
345	0.056	0.111	0.167	0.223	0.278	0.334	0.390	0.445	0.50			
350	0.056	0.113	0.169	0.226	0.282	0.339	0.395	0.452	0.50			
355	0.057	0.115	0.172	0.229	0.286	0.344	0.401	0.458	0.51			
360	0.058	0.116	0.174	0.232	0.290	0.349	0.407	0.465	0.52			
365	0.059	0.118	0.177	0.236	0.294	0.353	0.412	0.471	0.53			
370	0.060	0.119	0.179	0.239	0.299	0.358	0.418	0.478	0.53			
375	0.060	0.121	0.182	0.242	0.303	0.363	0.424	0.484	0.54			
380	0.061	0.123	0.184	0.245	0.307	0.368	0.429	0.491	0.55			
385	0.062	0.124	0.186	0.249	0.311	0.373	0.435	0.497	0.55			
390	0.063	0.126	0.189	0.252	0.315	0.378	0.441	0.504	0.566			
395	0.064	0.127	0.191	0.255	0.319	0.382	0.446	0.510	0.57			
400	0.065	0.129	0.194	0.258	0.323	0.387	0.452	0.516	0.58			
405	0.065	0.131	0.196	0.261	0.327	0.392	0.457	0.523	0.588			
410	0.066	0.132	0.198	0.265	0.331	0.397	0.463	0.529	0.596			
415	0.067	0.134	0.201	0.268	0.335	0.402	0.469	0.536	0.60			
420	0.068	0.136	0.203	0.271	0.339	0.407	0.474	0.542	0.610			
425	0.068	0.137	0.206	0.274	0.343	0.411	0.480	0.549	0.617			
430	0.069	0.139	0.208	0.278	0.347	0.416	0.486	0.555	0.625			
435	0.070	0.140	0.211	0.281	0.351	0.421	0.491	0.562	0.632			
440	0.071	0.142	0.213	0.284	0.355	0.426	0.497	0.568	0.639			
445	0.072	0.144	0.215	0.287	0.359	0.431	0 503	0.574	0.646			
450	0.073	0.145	0.218	0.290	0.363	0.436	0.508	0.581	0.654			
455	0.073	0.147	0.220	0.294	0.367	0.441	0.514	0.587	0.661			
	110	2°	3°	4 °	5°	6 2	7°	8 2	9°			

Height	TEMPERATURE CENTIGRADE.											
of the Barome- ter.	1°	2°	3°	4°	5°	6 °	7°	8°	9°			
Millim.	Millim.	Millim. 0.1485	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.			
460	0.0742		0.2227	0.2970	0.371	0.445	0.520	0.594	0.668			
465	0.0750	0.1501	0.2251	0.3002	0.375	0.450	0.525	0.600	0.675			
470	0.0759	0.1517	0.2276	0.3034	0.379	0.455	0.531	0.607	0.683			
475	0.0767	0.1533	0.2300	0.3066	0.383	0.460	0.537	0.613	0.690			
480	0.0775	0.1549	0.2324	0.3099	0.387	0.465	0.542	0.620	0.697			
485	0.0783	0.1565	0.2348	0.3131	0.391	0.470	0.548	0.626	0.704			
490	0.0791	0.1582	0.2373	0.3163	0.395	0.474	0.554	0.633	0.712			
495	0.0800	0.1598	0.2397	0.3195	0.399	0.479	0.559	0.639	0.719			
500	0.0807	0.1614	0.2421	0.3228	0.403	0.484	0.565	0.646	0.726			
505	0.0815	0.1630	0.2445	0.3260	0.407	0.489	0.570	0.652	0.734			
510	0.0823	0.1646	0.2469	0.3293	0.412	0.494	0.576	0.658	0.741			
515	0.0831	0.1662	0.2493	0.3325	0.416	0.499	0.582	0.665	0.748			
520	0.0839	0.1679	0.2518	0.3357	0.420	0.504	0.587	0.671	0.755			
525	0.0847	0.1695	0.2542	0.3389	0.424	0.508	0.593	0.678	0.763			
530	0.0855	0.1711	0.2566	0.3422	0.428	0.513	0.599	0.684	0.770			
535	0.0863	0.1727	0.2590	0.3454	0.432	0.518	0.604	0.691	0.777			
540	0.0872	0.1743	0.2615	0.3486	0.436	0.523	0.610	0.697	0.784			
545	0.0879	0.1759	0.2639	0.3518	0.440	0.528	0.616	0.704	0.792			
550	0.0888	0.1775	0.2663	0.3551	0.444	0.533	0.621	0.710	0.799			
555	0.0896	0.1791	0.2687	0.3583	0.448	0.537	0.627	0.717	0.806			
560	0.0904	0.1808	0.2712	0.3615	0.452	0.542	0.633	0.723	0.813			
565	0.0912	0.1824	0.2736	0.3647	0.456	0.547	0.638	0.730	0.821			
570	0.0920	0.1840	0.2760	0.3680	0.460	0.552	0.644	0.736	0.828			
575	0.0928	0.1856	0.2784	0.3712	0.464	0.557	0.650	0.742	0.835			
580	0.0936	0.1872	0.2808	0.3744	0.468	0.562	0.655	0.749	0.842			
585	0.0944	0.1888	0.2833	0.3777	0.472	0.566	0.661	0.755	0.850			
590	0.0952	0.1904	0.2857	0.3809	0.476	0.571	0.667	0.762	0.857			
595	0.0960	0.1921	0.2881	0.3841	0.480	0.576	0.672	0.768	0.864			
600	0.0968	0.1937	0.2905	0.3874	0.484	0.581	0.678	0.775	0.872			
605	0.0976	0.1953	0.2929	0.3906	0.488	0.586	0.683	0.781	0.879			
610	0.0985	0.1969	0.2954	0.3938	0.492	0.591	0.689	0.788	0.886			
615	0.0993	0.1985	0.2978	0.3930	0.496	0.595	0.695	0.794	0.893			
620	0.1001	0.2001	0.3002	0.4003	0.500	0.600	0.700	0.800	0.901			
625	0.1001	0.2017	0.3026	0.4035	0.504	0.605	0.706	0.807	0.908			
630	0.1017	0.2034	0.3050	0.4067	0.508	0.610	0.712	0.813	0.915			
635	0.1025	0.2050	0.3074	0.4099	0.512	0.615	0.717	0.820	0.922			
640	0.1023	0.2066	0.3099	0.4033 0.4132	0.516	0.620	0.717	0.826	0.922			
645	0.1033	0.2082	0.3033	0.4164	0.520	0.625	0.729	0.833	0.937			
650	0.1041	0.2098	0.3147	0.4196	0.524	0.629	0.734	0.839	0.944			
655	0.1043	0.2114	0.3172	0.4229	0.529	0.634	0.740	0.846	0.951			
660	0.1065	0.2130	0.3196	0.4261	0.533	0.639	0.746	0.852	0.959			
	1°	2 °	3°	40	5 °	6 °	70	80	9 °			

	Height				TEMPERA	TURE CEN	NTIGRADE.			
665 0.1073 0.2146 0.3220 0.4293 0.537 0.644 0.751 0.859 0.966 670 0.1081 0.2163 0.3244 0.4326 0.541 0.659 0.767 0.865 0.976 673 0.1099 0.2193 0.3248 0.4358 0.515 0.654 0.763 0.871 0.986 680 0.1097 0.2193 0.3292 0.4390 0.549 0.658 0.768 0.878 0.983 690 0.1110 0.2221 0.3311 0.4455 0.557 0.668 0.774 0.884 0.993 690 0.1112 0.22260 0.3389 0.4520 0.565 0.673 0.785 0.891 1.000 695 0.1130 0.2260 0.3389 0.4520 0.565 0.678 0.791 0.901 1.022 700 0.1130 0.22260 0.3389 0.4520 0.569 0.683 0.797 0.991 1.022 710	of the Barome- ter.	1°	2°	3°	40	5°	6°	7°	8°	90
670 0.1081 0.2163 0.3244 0.4326 0.541 0.649 0.757 0.865 0.977 673 0.1089 0.2179 0.3268 0.4358 0.515 0.654 0.763 0.571 0.986 680 0.1097 0.2193 0.3292 0.4390 0.519 0.658 0.763 0.571 0.986 685 0.1106 0.2211 0.3317 0.4423 0.553 0.663 0.774 0.884 0.996 690 0.1114 0.2227 0.3317 0.4455 0.557 0.668 0.780 0.891 1.006 695 0.1122 0.2233 0.3365 0.4487 0.561 0.673 0.785 0.897 1.010 700 0.1130 0.2260 0.3385 0.4520 0.5655 0.678 0.791 0.904 1.017 710 0.1146 0.2232 0.3418 0.4524 0.573 0.683 0.791 0.917 1.031 711	Millim.		1	1	1				1	Millim.
675 0.1089 0.2179 0.3268 0.4358 0.545 0.654 0.763 0.871 0.986 680 0.1097 0.2195 0.3292 0.4390 0.549 0.658 0.768 0.578 0.988 685 0.1106 0.2211 0.3317 0.4423 0.553 0.663 0.774 0.884 0.992 685 0.1104 0.2227 0.3341 0.4455 0.557 0.668 0.780 0.891 1.006 699 0.1122 0.2223 0.3365 0.4187 0.561 0.673 0.785 0.891 1.010 700 0.1130 0.2260 0.3389 0.4520 0.565 0.678 0.791 0.904 1.017 700 0.1136 0.2220 0.3144 0.4552 0.569 0.683 0.797 0.910 1.02 710 0.1162 0.2324 0.3186 0.4616 0.577 0.691 0.808 0.923 1.032 720	1						1			
650 0.1097 0.2195 0.3292 0.4390 0.549 0.658 0.768 0.878 0.985 655 0.1106 0.2211 0.3317 0.4423 0.553 0.663 0.774 0.884 0.993 690 0.1114 0.2227 0.3311 0.4455 0.557 0.668 0.780 0.891 1.005 693 0.1122 0.2230 0.3365 0.4187 0.661 0.673 0.781 0.997 1.010 700 0.1130 0.2260 0.3365 0.4187 0.665 0.678 0.791 0.994 1.010 700 0.1130 0.2260 0.3365 0.4520 0.665 0.678 0.791 0.991 1.002 710 0.1166 0.2276 0.3414 0.4552 0.569 0.683 0.797 0.910 1.02 710 0.1162 0.2334 0.3486 0.4648 0.581 0.697 0.833 0.3330 1.044 725		l I	1							
655 0.1106 0.2211 0.3317 0.4423 0.553 0.663 0.774 0.884 0.996 690 0.1114 0.2227 0.3341 0.4455 0.557 0.668 0.780 0.891 1.000 695 0.1122 0.2233 0.3365 0.4487 0.561 0.673 0.785 0.897 1.010 700 0.1136 0.2266 0.3414 0.4552 0.569 0.683 0.797 0.910 1.027 710 0.1146 0.2292 0.3138 0.4584 0.573 0.683 0.797 0.910 1.022 710 0.1162 0.2324 0.3486 0.4648 0.581 0.697 0.813 0.930 1.052 720 0.1162 0.2324 0.3310 0.4680 0.555 0.702 0.813 0.930 1.067 733 0.1176 0.2356 0.3535 0.4713 0.599 0.777 0.825 0.943 1.066 740						i				1
690 0.1114 0.2227 0.3341 0.4455 0.557 0.668 0.780 0.891 1.002 695 0.1122 0.2233 0.3365 0.4487 0.561 0.673 0.785 0.897 1.016 700 0.1130 0.2260 0.3389 0.4520 0.565 0.678 0.791 0.904 1.017 703 0.1138 0.2276 0.3414 0.4552 0.569 0.683 0.797 0.910 1.02 7110 0.1164 0.2292 0.3438 0.4584 0.573 0.688 0.923 1.03 720 0.1162 0.2324 0.3186 0.4618 0.585 0.702 0.819 0.936 1.057 730 0.1170 0.2340 0.3510 0.4680 0.585 0.702 0.819 0.936 1.052 733 0.1186 0.2372 0.3555 0.4715 0.593 0.717 0.830 0.941 1.066 740 0.1104										
655 0.1122 0.2233 0.3365 0.4487 0.561 0.673 0.785 0.897 1.010 700 0.1130 0.2260 0.3389 0.4520 0.565 0.678 0.791 0.904 1.012 705 0.1134 0.2276 0.3414 0.4552 0.569 0.683 0.797 0.910 1.02 710 0.1146 0.2292 0.3438 0.4584 0.573 0.688 0.802 0.911 1.031 715 0.1154 0.2303 0.3462 0.4616 0.577 0.691 0.808 0.923 1.032 720 0.1162 0.2324 0.3180 0.351 0.661 0.557 0.691 0.888 0.923 1.032 725 0.1170 0.2340 0.3510 0.4680 0.555 0.702 0.819 0.936 1.052 730 0.1176 0.2325 0.3553 0.4717 0.597 0.717 0.830 0.949 1.062	685	0.1106	0.2211	0.3317	0.4423	0.555	0.005	0.774	0.004	0.995
700 0.1130 0.2260 0.3389 0.4520 0.565 0.678 0.791 0.904 1.017 705 0.1138 0.2276 0.3414 0.4552 0.569 0.633 0.797 0.910 1.02- 710 0.1146 0.2292 0.3438 0.4584 0.573 0.688 0.802 0.917 1.031 715 0.1154 0.2303 0.3486 0.4616 0.577 0.691 0.808 0.923 1.032 720 0.1170 0.2340 0.3510 0.4680 0.581 0.697 0.813 0.933 1.052 730 0.1176 0.2340 0.3551 0.4680 0.585 0.702 0.819 0.936 1.052 730 0.1186 0.2372 0.3553 0.4713 0.589 0.707 0.825 0.943 1.060 740 0.1104 0.2389 0.3583 0.4777 0.597 0.717 0.836 0.955 1.072 740	690	0.1114	0.2227	0.3341	0.4455	0.557	0.668	0.780	0.891	1.002
703 0.1138 0.2276 0.3414 0.4552 0.569 0.683 0.797 0.910 1.02 710 0.1146 0.2292 0.3433 0.4584 0.573 0.688 0.802 0.917 1.031 715 0.1154 0.2308 0.3462 0.4616 0.577 0.691 0.808 0.923 1.032 720 0.1162 0.2324 0.3486 0.4648 0.581 0.697 0.813 0.936 1.056 723 0.1178 0.2356 0.3510 0.4680 0.585 0.702 0.819 0.936 1.066 733 0.1178 0.2356 0.3583 0.4777 0.597 0.712 0.830 0.949 1.066 740 0.1104 0.2389 0.3583 0.4777 0.597 0.717 0.836 0.955 1.075 745 0.1200 0.2405 0.3607 0.4809 0.601 0.721 0.842 0.962 1.052 750	695	0.1122	0.2233	0.3365	0.4487	0.561	0.673	0.785	0.897	1.010
710 0.1146 0.2292 0.3438 0.4584 0.573 0.688 0.802 0.917 1.031 715 0.1154 0.2308 0.3462 0.4616 0.577 0.691 0.808 0.923 1.035 720 0.1162 0.2324 0.3486 0.4648 0.581 0.697 0.813 0.930 1.046 725 0.1170 0.2340 0.3510 0.4680 0.585 0.702 0.819 0.936 1.052 730 0.1176 0.2340 0.3553 0.4713 0.589 0.707 0.825 0.943 1.060 735 0.1186 0.2372 0.3583 0.4777 0.597 0.717 0.830 0.949 1.062 740 0.1104 0.2389 0.3583 0.4777 0.597 0.717 0.836 0.955 1.07 745 0.1202 0.2405 0.3607 0.4809 0.601 0.721 0.842 0.962 1.052 755	700	0.1130	0.2260	0.3389	0.4520	0.565	0.678	0.791	0.904	1.017
715 0.1154 0.2303 0.3462 0.4616 0.577 0.691 0.808 0.923 1.036 720 0.1162 0.2324 0.3486 0.4648 0.581 0.697 0.813 0.930 1.046 725 0.1170 0.2340 0.3510 0.4680 0.555 0.702 0.819 0.936 1.052 730 0.1178 0.2356 0.3535 0.41713 0.589 0.707 0.825 0.943 1.060 735 0.1186 0.2372 0.3559 0.4745 0.593 0.712 0.830 0.949 1.068 740 0.1104 0.2389 0.3583 0.4777 0.597 0.717 0.836 0.955 1.072 740 0.1104 0.2389 0.3631 0.4842 0.605 0.726 0.847 0.962 1.082 755 0.1210 0.2437 0.3631 0.4842 0.605 0.726 0.847 0.962 1.082 760	705	0.1138	0.2276	0.3414	0.4552	0.569	0.683	0.797	0.910	1.024
720 0.1162 0.2324 0.3486 0.4648 0.581 0.697 0.813 0.930 1.046 725 0.1170 0.2340 0.3510 0.4680 0.585 0.702 0.819 0.936 1.052 730 0.1178 0.2356 0.3535 0.4713 0.589 0.707 0.825 0.943 1.066 735 0.1186 0.2372 0.3559 0.4745 0.593 0.712 0.330 0.949 1.068 740 0.1104 0.2389 0.3553 0.4777 0.597 0.717 0.836 0.955 1.077 745 0.1202 0.2401 0.3631 0.4842 0.605 0.726 0.847 0.968 1.085 750 0.1210 0.2421 0.3631 0.4842 0.605 0.726 0.847 0.968 1.087 760 0.1227 0.2453 0.3680 0.4906 0.613 0.731 0.842 0.962 1.082 760	710	0.1146	0.2292	0.3438	0.4584	0.573	0.688	0.802	0.917	1.031
720 0.1162 0.2324 0.3486 0.4648 0.581 0.697 0.813 0.930 1.046 725 0.1170 0.2340 0.3510 0.4680 0.585 0.702 0.819 0.936 1.052 730 0.1178 0.2356 0.3535 0.4713 0.589 0.707 0.825 0.943 1.066 735 0.1186 0.2372 0.3559 0.4745 0.593 0.712 0.330 0.949 1.068 740 0.1104 0.2389 0.3553 0.4777 0.597 0.717 0.836 0.955 1.077 745 0.1202 0.2401 0.3631 0.4842 0.605 0.726 0.847 0.968 1.085 750 0.1210 0.2421 0.3631 0.4842 0.605 0.726 0.847 0.968 1.087 760 0.1227 0.2453 0.3680 0.4906 0.613 0.731 0.842 0.962 1.082 760	715	0.1154	0.2303	0.3462	0.4616	0.577	0.691	0.808	0.923	1.039
725 0.1170 0.2340 0.3510 0.4680 0.585 0.702 0.819 0.936 1.052 730 0.1178 0.2356 0.3535 0.4713 0.589 0.707 0.825 0.943 1.060 735 0.1186 0.2372 0.3559 0.4745 0.593 0.712 0.830 0.949 1.062 740 0.1104 0.2389 0.3583 0.4777 0.597 0.717 0.836 0.955 1.073 745 0.1202 0.2405 0.3607 0.4809 0.601 0.721 0.842 0.962 1.082 750 0.1210 0.2421 0.3655 0.4874 0.609 0.731 0.853 0.975 1.097 755 0.1218 0.2447 0.3655 0.4874 0.609 0.731 0.853 0.975 1.097 760 0.1227 0.2453 0.3680 0.4943 0.617 0.741 0.864 0.988 1.111 775	1									1.046
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740 0.1104 0.2389 0.3583 0.4777 0.597 0.717 0.836 0.955 1.077 745 0.1202 0.2405 0.3607 0.4809 0.601 0.721 0.842 0.962 1.082 750 0.1210 0.2421 0.3631 0.4842 0.605 0.726 0.847 0.968 1.082 755 0.1218 0.2437 0.3655 0.4874 0.609 0.731 0.853 0.975 1.092 760 0.1227 0.2453 0.3680 0.4906 0.613 0.736 0.859 0.981 1.104 765 0.1235 0.2469 0.3704 0.4939 0.617 0.741 0.864 0.988 1.111 770 0.1243 0.2466 0.3725 0.4971 0.621 0.746 0.870 0.994 1.118 775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.122 780		0.1178	0.2356	0.3535	0.4713	0.589	0.707	0.825	0.943	1.060
745 0.1202 0.2405 0.3607 0.4809 0.601 0.721 0.842 0.962 1.082 750 0.1210 0.2421 0.3631 0.4842 0.605 0.726 0.847 0.968 1.085 755 0.1218 0.2437 0.3655 0.4874 0.609 0.731 0.853 0.975 1.097 760 0.1227 0.2453 0.3680 0.4906 0.613 0.736 0.859 0.981 1.109 765 0.1235 0.2469 0.3704 0.4939 0.617 0.741 0.864 0.988 1.111 770 0.1243 0.2486 0.3723 0.4971 0.621 0.746 0.870 0.994 1.118 775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.126 785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790	735	0.1186	0.2372	0.3559	0.4745	0.593	0.712	0.830	0.949	1.068
745 0.1202 0.2405 0.3607 0.4809 0.601 0.721 0.842 0.962 1.082 750 0.1210 0.2421 0.3631 0.4842 0.605 0.726 0.847 0.968 1.085 755 0.1218 0.2437 0.3655 0.4874 0.609 0.731 0.853 0.975 1.097 760 0.1227 0.2453 0.3680 0.4906 0.613 0.736 0.859 0.981 1.109 765 0.1235 0.2469 0.3704 0.4939 0.617 0.741 0.864 0.988 1.111 770 0.1243 0.2486 0.3723 0.4971 0.621 0.746 0.870 0.994 1.118 775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.126 785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790		0.7704	0.0000	0.0500		0 505	0	0.000	0.055	1.0~
750 0.1210 0.2421 0.3631 0.4842 0.605 0.726 0.847 0.968 1.085 755 0.1218 0.2437 0.3655 0.4874 0.609 0.731 0.853 0.975 1.097 760 0.1227 0.2453 0.3680 0.4906 0.613 0.736 0.859 0.981 1.104 765 0.1235 0.2469 0.3704 0.4939 0.617 0.741 0.864 0.988 1.111 770 0.1243 0.2486 0.3723 0.4971 0.621 0.746 0.870 0.994 1.118 775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.126 780 0.1259 0.2518 0.3777 0.5036 0.629 0.755 0.881 1.007 1.135 785 0.1267 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795										
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765 0.1235 0.2469 0.3704 0.4939 0.617 0.741 0.864 0.988 1.111 770 0.1243 0.2486 0.3728 0.4971 0.621 0.746 0.870 0.994 1.118 775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.126 780 0.1259 0.2518 0.3777 0.5036 0.629 0.755 0.881 1.007 1.135 785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790 0.1275 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.158 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805										
770 0.1243 0.2486 0.3728 0.4971 0.621 0.746 0.870 0.994 1.118 775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.126 780 0.1259 0.2518 0.3777 0.5036 0.629 0.755 0.881 1.007 1.135 785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790 0.1275 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.155 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810	700	0.1227	0.2499	0.3030	0.4300	0.013	0.750	0.000	0.501	1.104
775 0.1251 0.2502 0.3752 0.5003 0.625 0.750 0.876 1.001 1.126 780 0.1259 0.2518 0.3777 0.5036 0.629 0.755 0.881 1.007 1.135 785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790 0.1275 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.155 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815	765	0.1235	0.2469	0.3704	0.4939	0.617	0.741	0.864	0.988	1.111
780 0.1259 0.2518 0.3777 0.5036 0.629 0.755 0.881 1.007 1.133 785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790 0.1275 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.155 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825	770	0.1243	0.2486	0.3728	0.4971	0.621	0.746	0.870	0.994	1.118
785 0.1267 0.2534 0.3801 0.5068 0.633 0.760 0.888 1.014 1.146 790 0.1275 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.155 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.166 810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825	775	0.1251	0.2502	0.3752	0.5003	0.625	0.750	0.876	1.001	1.126
790 0.1275 0.2550 0.3825 0.5100 0.637 0.765 0.893 1.020 1.148 795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.155 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2633 0.3994 0.5326 0.666 0.799 0.932 1.065 1.198 830	780	0.1259	0.2518	0.3777	0.5036	0.629	0.755	0.881	1.007	1.133
795 0.1283 0.2566 0.3849 0.5132 0.641 0.770 0.898 1.026 1.155 800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2653 0.3994 0.5326 0.6666 0.799 0.932 1.065 1.198 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835	785	0.1267	0.2534	0.3801	0.5068	0.633	0.760	0.888	1.014	1.140
800 0.1291 0.2582 0.3874 0.5165 0.646 0.775 0.904 1.033 1.162 805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.198 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.218 840	790	0.1275	0.2550	0.3825	0.5100	0.637	0.765	0.893	1.020	1.148
805 0.1299 0.2598 0.3898 0.5197 0.650 0.780 0.909 1.039 1.168 810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.198 830 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.198 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845	795	0.1283	0.2566	0.3849	0.5132	0.641	0.770	0.898	1.026	1.155
810 0.1307 0.2615 0.3922 0.5230 0.654 0.784 0.915 1.046 1.177 815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.198 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.225 850	800	0.1291	0.2582	0.3874	0.5165	0.646	0.775	0.904	1.033	1.162
815 0.1315 0.2621 0.3946 0.5262 0.658 0.789 0.921 1.052 1.184 820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.198 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.225 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.235 855	805	0.1299	0.2598	0.3898	0.5197	0.650	0.780	0.909	1.039	1.169
820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.196 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.227 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.246 860	810	0.1307	0.2615	0.3922	0.5230	0.654	0.784	0.915	1.046	1.177
820 0.1323 0.2647 0.3970 0.5294 0.662 0.794 0.926 1.059 1.191 825 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.196 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.227 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.246 860	815	0.1315	0.2621	0.3946	0.5262	0.658	0.789	0.921	1.052	1.184
825 0.1331 0.2653 0.3994 0.5326 0.666 0.799 0.932 1.065 1.198 830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.227 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.248 860 0.1388 0.2776 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256							*****			
830 0.1340 0.2679 0.4019 0.5358 0.670 0.804 0.938 1.072 1.206 835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.218 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.225 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.246 860 0.1388 0.2776 0.4164 0.5552 0.694 0.833 0.972 1.110 1.256 865 0.1396 0.2792 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256	i	i i		l	1		1	i e		l
835 0.1348 0.2695 0.4043 0.5391 0.674 0.809 0.943 1.078 1.216 840 0.1356 0.2712 0.4067 0.5423 0.678 0.813 0.949 1.085 1.226 845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.227 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.235 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.246 860 0.1388 0.2776 0.4164 0.5552 0.694 0.833 0.972 1.110 1.246 865 0.1396 0.2792 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256	1			1					i .	1.206
845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.227 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.243 860 0.1388 0.2776 0.4164 0.5552 0.694 0.833 0.972 1.110 1.243 865 0.1396 0.2792 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256				[i i		1.213
845 0.1364 0.2728 0.4091 0.5455 0.682 0.818 0.955 1.091 1.227 850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.243 860 0.1388 0.2776 0.4164 0.5552 0.694 0.833 0.972 1.110 1.243 865 0.1396 0.2792 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256	810	0.1256	0.9719	0.1067	0.5499	0.679	0.819	0 0 10	1.085	1 99/
850 0.1372 0.2744 0.4116 0.5488 0.686 0.823 0.960 1.097 1.233 855 0.1380 0.2760 0.4140 0.5520 0.690 0.828 0.966 1.104 1.243 860 0.1388 0.2776 0.4164 0.5552 0.694 0.833 0.972 1.110 1.243 865 0.1396 0.2792 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256	1	II .	1				i	1		
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865 0.1396 0.2792 0.4188 0.5584 0.698 0.838 0.977 1.117 1.256		()	1					ł	t .	1.249
10 00 00 FO FO FO FO FO	865	0.1396		0.4188		1	0.838		1.117	1.256
		10	2°	3°	40		6 °	70	8°	9°

XX.

METRICAL BAROMETER.

TABLE

FOR

REDUCING TO THE FREEZING POINT THE BAROMETRICAL COLUMN,

measured by Brass scales, extending from the cistern to the top; calculated for the heights between 605 and 800 millimetres, and for every tenth of a degree, from 0° to + and - 35° centigrade. By M. T. Haeghens.

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TABLE. XX.

This table has been calculated by using the same coefficients of dilatation as in the preceding table, viz.:—

Brass, linear dilatation, from Laplace and Lavoisier for 100°C. = 0.0018782.

Mercury, dilatation in volume, from Dulong and Petit for 100°C. = 0.0180180.

Dilatation of the mercurial column for 100°C. . . . = 0.0161398.

Dilatation of the mercurial column for 1°C. . . . = 0.0001614.

This table, calculated for the reduction of long series of meteorological observations, gives immediately the value of the correction for each tenth of a degree up to 35° C. above, and down to 35° C. below, the freezing point, and for mercurial columns extending from 605 to 800 millimetres.

Examples of Calculation.

For finding the correction, seek in the horizontal column, headed *barometer*, at the head of the pages, the corresponding height of the barometer; it will be found, p. 31, barometer 755^{mm} (from 752.50 to 757.50); next seek in the first vertical column, containing the temperatures, 17°, follow then horizontally this line as far as the column of 8 tenths, and you find there 2.17 millimetres, which is the correction, or the quantity to be subtracted for reducing the observed height to zero. We have thus:—

	В	Sarom	eter a	t zero.	_	752.00
Subtractive correction	for $+1$	7°.8 =	= .	•		— 2.17
Observed height,				•		$754.17^{\mathrm{mm.}}$

If the temperature is below zero, the correction will be additive.

Observed height,					•	•	729.72
Temperature of the	attae	hed t	herm	omete	r, —8	8°.4.	
Additive correction,	•		•				+0.99
		В	arom	eter a	t zero	,	730.71

mm.

	BAROMETER: 605 ^{mm} . (from 602.51 to 607.50).											
Centigrade Degrees.				-	Tenths o	f Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.		
-	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim,		
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09		
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19		
2	0.20	0.21	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28		
3	0.29	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38		
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48		
5	0.49	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58		
6	0.59	0.60	0.61	0.62	0.63	0.63	0.64	0.65	0.66	0.67		
7	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77		
8	0.78	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87		
9	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97		
10	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.05	1.06		
11	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16		
12	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26		
13	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36		
14	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46		
15	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55		
16	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.65		
17	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75		
18	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85		
19	1.86	1.87	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94		
20	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04		
21	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14		
22	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24		
23	2.25	2.26	2.27	2.28	2.29	2.29	2.30	2.31	2.32	2.33		
24	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43		
25	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53		
26	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63		
27	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.71	2.72		
28	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82		
29	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92		
30	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02		
31	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12		
32	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21		
33	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31		
34	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41		
35	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 610 ^{mm} . (from 607.51 to 612.50).														
Centi- grade Degrees.		Tenths of Degrees.													
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
-	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.					
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09					
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19					
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29					
3	0.30	0.31	0.32	0.32	0.33	0.34	0.35	0.36	0.37	0.38					
4	0.39	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48					
5	0.49	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58					
6	0.59	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68					
7	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78					
8	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88					
9	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.96	0.97					
10	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07					
11	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17					
12	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27					
13	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37					
14	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47					
15	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57					
16	1.58	1.59	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66					
17	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76					
18	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86					
19	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96					
20	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06					
21	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16					
22	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.23	2.24	2.25					
23	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35					
24	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45					
25	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55					
26	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65					
27	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75					
28	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85					
29	2.86	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94					
30	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04					
31	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14					
32	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24					
33	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34					
34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44					
35	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.55	3.54					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					

BAROMETER: 615^{mm} . (from 612.51 to 617.50).

Centigrade De rees

Tenths of Degrees.

grade Jeg r ees.	Tenths of Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim.	Millim.	Millim.	Millim.	Millim,	Millim,	Millim.	Millim.	Millim.	Millim.		
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09		
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19		
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29		
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39		
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49		
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59		
6	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.68		
7	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78		
8	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88		
9	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98		
10	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08		
11	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18		
12	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28		
13	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38		
14	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48		
15	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58		
16	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68		
17	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78		
18	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88		
19	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98		
20	1.99	2.00	2.01	2.01	2.02	2.03	2.04	2.05	2.06	2.07		
21	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17		
22	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27		
23	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37		
24	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47		
25	2.48	2.19	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57		
26	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67		
27	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77		
28	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87		
29	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97		
30	2.98	2.99	3.00	3.01	3.02	3.03	3.01	3.05	3.06	3.07		
31	3.08	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17		
32	3.18	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27		
33	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.36		
34	3.37	3.33	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46		
35	3.47	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 620 ^{mm.} (from 617.51 to 622.50)														
Centigrade grade Degrees.		Tenths of Degrees.													
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim 0.08	Millim. 0.09					
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19					
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29					
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39					
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49					
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59					
6	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69					
7	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79					
8	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89					
9	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99					
10	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09					
11	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19					
12	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29					
13	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39					
14	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49					
15	1.50	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59					
16	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69					
17	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79					
18	1.80	1.81	1.82	1.83	1.84	-1.85	1.86	1.87	1.88	1.89					
19	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99					
20	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09					
21	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19					
22	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29					
23	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39					
24	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49					
25	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59					
26	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69					
27	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79					
28	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89					
29	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	2.99					
30	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09					
31	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19					
32	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29					
33	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39					
34	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49					
35	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58	3.59					
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					

	BAROMETER: 625 ^{mm} . (from 622.51 to 627.50).													
Centi- grade Degrees.		Tenths of Degrees,												
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim 0.08	Millim 0.09				
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19				
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29				
3	0.30	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39				
4	0.40	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49				
5	0.50	0.51	0.52	0.53	0.54	0.55	0.56	0.58	0.59	0.60				
6	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70				
7	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80				
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90				
9	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00				
10	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10				
11	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20				
12	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30				
13	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40				
14	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50				
15	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60				
16	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70				
17	1.71	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81				
18	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91				
19	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01				
20	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11				
21	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21				
22	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31				
23	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41				
24	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51				
25	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61				
26	2.62	2.63	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71				
27	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80	2.81				
28	2.82	2.83	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92				
29	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02				
30	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12				
31	3.13	3.14	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22				
32	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32				
33	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42				
34	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52				
35	3.53	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.61	3.62				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

		В	AROMI	ETER:	630 ^{mm} ·	(from	627.51	to 632.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim, 0.04	Millim. 0.05	Millim.	Millim. 0.07	Millim. 0.08	Millim.
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19
2	0.20	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40
4	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50
5	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60
6	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70
7	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80
8	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01
10	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11
11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21
12	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31
13	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41
14	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.52
15	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62
16 .	1.63	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72
17	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82
18	1.83	1.84	1.85	1.86	1.87	.1.88	1.89	1.90	1.91	1.92
19	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02
20	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13
21	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23
22	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33
23	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43
24	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53
25	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63
26	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.73	2.74
27	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
28	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94
29	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04
30	3.05	3.06	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14
31	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24
32	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32	3.34	3.35
33	3.36	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45
34	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.55
35	3.56	3.57	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.65
	0.	1.	2.	3.	4.	5,	6.	7.	8.	9.

Centigrade grade Jegrees.						BAROMETER: 635 ^{mm} . (from 632.51 to 637.50).												
Ì	Tenths of Degrees.																	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.								
0	Millim.	Millim.	Millim,	Millim.	Millim.	Millim,	Millim.	Millim,	Millim,	Millim								
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09								
1	0.10	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19								
2	0.20	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30								
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40								
4	0.41	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50								
5	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60								
6	0.61	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71								
7	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81								
8	0.52	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91								
9	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01								
10	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12								
	1 10	1 14	1 15	1.16	1.77	1 10	1.10	1.00	1.01	1.00								
11	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22								
12	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32								
13	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.42								
14 15	1.43 1.54	1.45 1.55	1.46 1.56	1.47	1.48 1.58	1.49 1.59	1.50 1.60	1.51	1.52 1.62	1.53								
16	1.64	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73								
17	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.88								
18	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94								
19	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.04								
20	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14								
21	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.2								
22	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35								
23	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.43								
24	2.46	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.5								
25	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.6								
26	2.66	2.67	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.70								
27	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.80								
28	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.9								
29	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.0								
30	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.1								
31	3.18	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.2								
32	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.3								
33	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.4								
34	3.48	3.49	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.5								
35	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.6								
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.								

Centi-						(1101111		o 642.5		
grade egrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	۹.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim, 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millon 0.09
1	0.10	0.11	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40
4	0.41	0.42	0.43	0.44	0.45	0.46	0.48	0.49	0.50	0.51
5	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61
6	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71
7	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.80	0.81	0.82
8	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92
9	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02
10	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.11	1.12	1.13
11	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23
12	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33
13	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42	1.43	1.4
14	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.5
15	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.6
16	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.74	1.75
17	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
18	1.86	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.93
19	1.96	1.97	1.98	1.99	2.00	2.01	2.02	2.03	2.05	2.06
20	2.07	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16
21	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26
22	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.36	2.33
23	2.38	2.39	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
24	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.5
25	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.68
26	2.69	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78
27	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.83
28	2.59	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.99
29	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09
30	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.19
31	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.30
32	3.31	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.4
33	3.41	3.42	3.13	3.44	3.45	3.46	3.47	3.48	3.49	3.50
34	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58	3.59	3.6
35	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69	3.70	3.7
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		BA	AROME	ETER:	645 ^{mm} .	(from 6	642.51 t	o 647.5	0).	
Centi- grade Degrees.					Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
1	0.10	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.31	0.32	0.33	0.34	0.35	0.36	0.37	0.39	0.40	0.41
4	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51
5	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61
6	0.62	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82
8	0.83	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93
9	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03
10	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13
11	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24
12	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34
13	1.35	1.36	1.37	1.38	1.39	1.41	1.42	1.43	1.44	1.45
14	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55
15	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.63	1.64	1.66
16	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76
17	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85	1.86
18	1.87	1.88	1.89	1.91	1.92	1.93	1.94	1.95	1.96	1.97
19	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07
20	2.08	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17	2.18
21	2.19	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28
22	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38
23	2.39	2.40	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49
24	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59
25	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70
26	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78	2.79	2.80
27	2.51	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.90
28	2.92	2.93	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01
29	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10	3.11
30	3.12	3.13	3.14	3.15	3.16	3.18	3.19	3.20	3.21	3.22
31	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.30	3.31	3.32
32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42
33	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53
34	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.61	3.62	3.63
35	3.64	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.72	3.73
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROM	ETER :	650 ^{mm}	(from	647.51	to 652.5	0).	
Centi- grade Degrees.		•			Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim 0.09
1	0 11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41
4	0.42	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51
5	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72
7	0.73	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83
8	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93
9	0.94	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04
10	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14
11	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25
12	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35
13	1.36	1.37	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46
14	1.47	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.56
15	1.57	1.58	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67
16	1.68	1.69	1.70	1.71	1.72	1.73	1.74	1.75	1.76	1.77
17	1.78	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88
18	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.98
19	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.07	2.08	2.09
20	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19
21	2.20	2.21	2.22	2.24	2.25	2.26	2.27	2.28	2.29	2.30
22	2.31	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40
23	2.41	2.42	2.43	2.44	2.46	2.47	2.48	2.49	2.50	2.51
24	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61
25	2.62	2.63	2.61	2.65	2.67	2.68	2.69	2.70	2.71	2.72
26	2.73	2.84	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
27	2.83	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.92	2.93
28	2.94	2.95	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3 03
29	3.04	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14
30	3.15	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.23	3.24
31	3.25	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34	3.35
32	3.36	3 37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45
33	3.46	3.47	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.56
34	3.57	3 58	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66
35	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROME	TER:	655 ^{mm} .	(from 6	652.51 to	o 657.50	0).	
Centi- grade Degrees				-	Tenths of	Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Mıllim. 0.03	Millim, 0.04	Millim.	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35 *	0.36	0.37	0.38	0.39	0.40	0.41
4	0.42	0.43	0.44	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62
6	0.63	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73
7	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.83	0.84
8	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94
9	0.95	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05
10	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15
11	1.16	1.17	1.18	1.20	1.21	1.22	1.23	1.24	1.25	1.26
12	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36
13	1.37	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47
14	1.48	1.49	1.50	1.51	1.52	1.53	1.54	1.55	1.57	1.58
15	1.59	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68
16	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79
17	1.80	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.89
18	1.90	1.91	1.92	1.94	1.95	1.96	1.97	1.98	1.99	2.00
19	2.01	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10
20	2.11	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.20	2.21
21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.31	2.32
22	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40	2.41	2.42
23	2.43	2.44	2.45	2.46	2.47	2.48	2.50	2.51	2.52	2.53
24	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63
25	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74
26	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
27	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95
28	2.96	2.97	2.98	2.99	3.00	3.01	3.02	3.03	3.05	3.06
29	3.07	3.08	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16
30	3.17	3.18	3.19	3.20	3.21	3.22	3.24	3.25	3.26	3.27
31	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35	3.36	3.37
32	3.38	3.39	3.40	3.42	3.43	3.44	3.45	3.46	3.47	3.48
33	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58
34	3.59	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69
35	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3.77	3.79	3.80
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER :	660 ^{mm} .	(from	657.51 t	o 662.5	0).	
Centi- grade Degrees.				***	Tenths o	f Degrees.				
•	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim, 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.21	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.41	0.42
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52
5	0.53	0.54	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74
7	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.84
8	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.95
9	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.06
10	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16
11	1.17	1.18	1.19	1.20	1.21	1.23	1.24	1.25	1.26	1.27
12	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37
13	1.39	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48
14	1.49	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59
15	1.60	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.69
16	1.70	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80
17	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
18	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99	2.00	2.01
19	2.02	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.12
20	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23
21	2.24	2.25	2.26	2.27	2.28	2.29	2.30	2.31	2.32	2.33
22	2.34	2.35	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.44
23	2.45	2.46	2.47	2.48	2.49	2.50	2.51	2.53	2.54	2.55
24	2.56	2.57	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65
25	2.66	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.76
26	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87
27	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97
28	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.06	3.07	3.08
29	3.09	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.19
30	3.20	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29
31	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40
32	3.41	3.42	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.51
33	3.52	3.53	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.61
34	3.62	3.63	3.64	3.65	3.66	3.68	3.69	3.70	3.71	3.72
35	3.73	3.74	3.75	3.76	3.77	3.78	3.79	3.80	3.81	3.82
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

 $\overline{\mathbf{C}}$

		В.	AROMI	ETER :	665 ^{mm}	(from	662.51	to 667.5	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31
3	0.32	0.33	0.34	0.35	0.37	0.38	0.39	0.40	0.41	0.42
4	0.43	0.44	0.45	0.46	0.47	0.48	0.49	0.51	0.52	0.53
5	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63
6	0.64	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73	0.74
7	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.85
8	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.95	0.96
9	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06
10	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17
11	1.18	1.19	1.20	1.21	1.22	1.23	1.25	1.26	1.27	1.28
12	1.29	1.30	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.39
13	1.40	1.41	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49
14	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59	1.60
15	1.61	1.62	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71
16	1.72	1.73	1.74	1.75	1.76	1.77	1.78	1.79	1.80	1.81
17	1.83	1.84	1.85	1.86	1.87	1.88	1.89	1.90	1.91	1.92
18	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.02	2.03
19	2.04	2.05	2.06	2.07	2.08	2.09	2.10	2.11	2.13	2.14
20	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.22	2.23	2.24
21	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.35
22	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44	2.45	2.46
23	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.54	2.56	2.57
24	2.58	2.59	2.60	2.61	2.62	2.63	2.64	2.65	2.66	2.67
25	2.68	2.69	2.71	2.72	2.73	2.74	2.75	2.76	2.77	2.78
26	2.79	2.80	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89
27	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00
28	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.09	3.10
29	3.11	3.12	3.13	3.15	3.16	3.17	3.18	3.19	3.20	3.21
30	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.30	3.31	3.32
31	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.42
32	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.51	3.52	3.53
33	3.54	3.55	3.56	3.57	3.59	3.60	3.61	3.62	3.63	3.64
34	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75
35	3.76	3.77	3.78	3.79	3.80	3.81	3.82	3.83	3.84	3.85
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	TER ·	670 ^{mm} ·	(from	667.51 t	o 672.50	0.)	
Centigrade Degrees.					Tenths of	Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim.	Millim. 0.04	Millim. 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1 2	0.11	0.12	0.13 0.24	0.14 0.25	0.15	0.16 0.27	0.17 0.28 0.39	0.18 0.29 0.40	0.20	0.21
3 4 5	$0.32 \\ 0.43 \\ 0.54$	$0.34 \\ 0.44 \\ 0.55$	$0.35 \\ 0.45 \\ 0.56$	$0.36 \\ 0.47 \\ 0.57$	$0.37 \\ 0.48 \\ 0.58$	0.38 0.49 0.60	0.39 0.50 0.61	0.40 0.51 0.62	0.41 0.52 0.63	0.42 0.53 0.64
6 7	0.65 0.76	0.66 0.77	0.67 0.78	0.68 0.79	0.69 0.80	0.70 0.81	0.71 0.82	0.73 0.83	0.74 0.84	0.75 0.85
8 9 10	0.87 0.97 1.08	0.88 0.98 1.09	0.89 1.00 1.10	0.90 1.01 1.11	0.91 1.02 1.13	0.92 1.03 1.14	0.93 1.04 1.15	0.94 1.05 1.16	0.95 1.06 1.17	0.96 1.07 1.18
11 12	1.19	1.20 1.31	1.21 1.32	1.22 1.33	1.23 1.34	1.24 1.35	1.25 1.36	1.27 1.37	1.28	1.29 1.40
13 14	1.41 1.51	1.42 1.53	1.43 1.54	1.44 1.55	1.45 1.56	$1.46 \\ 1.57$	1.47 1.58	1.48 1.59	1.49 1.60	1.50 1.61
15 16	1.62	1.63	1.64 1.75	1.66	1.67	1.68	1.69 1.80	1.70	1.71	1.72
17 18 19	1.84 1.95 2.06	1.85 1.96 2.07	1.86 1.97 2.08	1.87 1.98 2.09	1.88 1.99 2.10	1.89 2.00 2.11	1.90 2.01 2.12	1.91 2.02 2.13	1.92 2.03 2.14	1.94 2.04 2.15
20	2.16	2.17	2.18	2.20	2.21 2.31	2.22	2.23	2.24 2.35	2.25	2.26
22 23	2.38 2.49 2.60	2.39 2.50	2.40 2.51 2.62	2.41 2.52 2.63	2.42 2.53 2.64	2.43 2.54	2.44 2.55 2.66	2.46 2.56 2.67	2.47 2.57 2.68	2.48 2.59 2.69
24 25	2.70	2.61 2.71	2.73	2.74	2.75	2.65 2.76	2.77	2.78	2.79	2.80
26 27 28	2.81 2.92 3.03	2.82 2.93 3.04	2.83 2.94 3.05	2.84 2.95 3.06	2.86 2.96 3.07	2.87 2.97 3.08	2.88 2.99 3.09	2.89 3.00 3.10	2.90 3.01 3.11	2.91 3.02 3.13
29 30	3·14 3·24	3.15 3.26	3.16 3.27	3.17 3.28	3.18 3.29	3.19 3.30	3.20 3.31	3.21 3.32	3.22 3.33	3.23 3.34
31 32 33	3.35 3.46 3.57	3.36 3.47 3.58	3.37 3.48 3.59	3.39 3.49 3.60	3.40 3.50 3.61	3.41 3.52 3.62	3.42 3.53 3.63	3.43 3.54 3.64	3.44 3.55 3.66	3.45 3.56 3.67
34 35	3.68 3.79	3.69 3.80	3.70 3.81	3.71 3.82	3.72 3.83	3.73 3.84	3.74 3.85	3.75 3.86	3.76 3.87	3 77 3.88
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROME	TER:	675 ^{mm} .	(from 6	572.51 t	o 677.50	0).	
Centi- grade Degrees.					Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.02	0.03	0.04	0.05	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.17	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32
3	0.33	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53
5	0.54	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.64
6	0.65	0.66	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75
7	0.76	0.77	0.78	0.80	0.81	0.82	0.83	0.84	0.85	0.86
8	0.87	0.88	0.89	0.90	0.92	0.93	0.94	0.95	0.96	0.97
9	0.98	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07	1.08
10	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19
11	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.29	1.30
12	1.31	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.41
13	1.42	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51
14	1.53	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62
15	1.63	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73
16	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82	1.83	1.84
17	1.85	1.86	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95
18	1.96	1.97	1.98	1.99	2.00	2.02	2.03	2.04	2.05	2.06
19	2.07	2.08	2.09	2.10	2.11	2.12	2.14	2.15	2.16	2.17
20	2.18	2.19	2.20	2.21	2.22	2.23	2.24	2.26	2.27	2.28
21	2.29	2.30	2.31	2.32	2.33	2.34	2.35	2.36	2.38	2.39
22	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47	2.48	2.49
23	2.51	2.52	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.60
24	2.61	2.63	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.71
25	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.81	2.82
26	2.83	2.84	2.85	2.87	2.88	2.89	2.90	2.91	2.92	2.93
27	2.94	2.95	2.96	2.97	2.99	3.00	3.01	3.02	3.03	3.04
28	3.05	3.06	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15
29	3.16	3.17	3.18	3.19	3.20	3.21	3.22	3.24	3.25	3.26
30	3.27	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.36	3.37
31	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.46	3.48
32	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.56	3.57	3.58
33	3.60	3.61	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69
34	3.70	3.72	3.73	3.74	3.75	3.76	3.77	3.78	3.79	3.80
35	3.81	3.82	3.83	3.85	3.86	3.87	3.88	3.89	3.90	3.91
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

 $\overline{\mathbf{C}}$

		В	AROMI	ETER :	680 ^{mm.}	(from	677.51 t	o 682.50	0).	
Centigrade Degrees.			·····		Tenths of	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim. 0.00	Millim, 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.26	0.27	0.29	0.30	0.31	0.32
3	0.33	0.34	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43
4	0.44	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54
5	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.63	0.64	0.65
6	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76
7	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.85	0.86	0.87
8	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.97	0.98
9	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.08	1.09
10	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.19	1.20
11	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.30	1.31
12	1.32	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42
13	1.43	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53
14	1.54	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.62	1.64
15	1.65	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.73	1.75
16	1.76	1.77	1.78	1.79	1.80	1.81	1.82	1.83	1.84	1.85
17	1.87	1.88	1.89	1.90	1.91	1.92	1.93	1.94	1.95	1.96
18	1.98	1.99	2.00	2.01	2.02	2.03	2.04	2.05	2.06	2.07
19	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.16	2.17	2.18
20	2.20	2.21	2.22	2.23	2.24	2.25	2.26	2.27	2.28	2.29
21	2.30	2.32	2.33	2.34	2.35	2.36	2.37	2.38	2.39	2.40
22	2.41	2.43	2.44	2.45	2.46	2.47	2.48	2.49	2.50	2.51
23	2.52	2.54	2.55	2.56	2.57	2.58	2.59	2.60	2.61	2.62
24	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.71	2.72	2.73
25	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83	2.84
26	2.85	2.86	2.88	2.89	2.90	2.91	2.92	2.93	2.94	2.95
27	2.96	2.97	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06
28	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
29	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.26	3.27	3.28
30	3.29	3.30	3.31	3.33	3.34	3.35	3.36	3.37	3.38	3.39
31	3.40	3.41	3.42	3.44	3.45	3.46	3.47	3.48	3.49	3.50
32	3.51	3.52	3.53	3.54	3.56	3.57	3.58	3.59	3.60	3.61
33	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.70	3.71	3.72
34	3.73	3.74	3.75	3.76	3.78	3.79	3.80	3.81	3.82	3.83
35	3.84	3.85	3.86	3.87	3.89	3.90	3.91	3.92	3.93	3.94
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROMI	ETER :	685 ^{mm.}	(from	682.51 t	o 687.50	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim, 0.03	Millim. 0.04	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21
2	0.22	0.23	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.32
3	0.33	0.34	0.35	0.36	0.38	0.39	0.40	0.41	0.42	0.43
4	0.44	0.45	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.54
5	0.55	0.56	0.57	0.59	0.60	0.61	0.62	0.63	0.64	0.65
6	0.66	0.67	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76
7	0.77	0.78	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87
8	0.88	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98
9	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09
10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.21
11	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.32
12	1.33	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.42	1.43
13	1.44	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53	1.54
14	1.55	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65
15	1.66	1.67	1.68	1.69	1.70	1.71	1.72	1.74	1.75	1.76
16	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.87
17	1.88	1.89	1.90	1.91	1.92	1.93	1.95	1.96	1.97	1.98
18	1.99	2.00	2.01	2.02	2.03	2.05	2.06	2.07	2.08	2.09
19	2.10	2.11	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20
20	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.30	2.31
21	2.32	2.33	2.34	2.35	2.37	2.38	2.39	2.40	2.41	2.42
22	2.43	2.44	2.45	2.47	2.48	2.49	2.50	2.51	2.52	2.53
23	2.54	2.55	2.56	2.58	2.59	2.60	2.61	2.62	2.63	2.64
24	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.74	2.75
25	2.76	2.78	2.79	2.80	2.81	2.82	2.83	2.84	2.85	2.86
26	2.87	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97
27	2.99	3.00	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08
28	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.18	3.20
29	3.21	3.22	3.23	3.24	3.25	3.26	3.27	3.28	3.29	3.31
30	3.32	3.33	3.34	3.35	3.36	3.37	3.38	3.39	3.41	3.42
31	3.43	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.52	3.53
32	3.54	3.55	3.56	3.57	3.58	3.59	3.60	3.62	3.63	3.64
33	3.65	3.66	3.67	3.68	3.69	3.70	3.71	3.73	3.74	3.75
34	3.76	3.77	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86
35	3.87	3.88	3.89	3.90	3.91	3.92	3.94	3.95	3.96	3.97
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROME	ETER:	690 ^{mm} .	(from	687.51	to 692.5	0).	
Centi- grade Degrees.					Tenths o	f Degrees.		,		************
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.04	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim 0.10
1	0.11	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21
$_2$	0.22	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.32
3	0.33	0.35	0.36	0.37	0.38	0.39	0.40	0.41	0.42	0.43
4	0.45	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55
5	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.65	0.66
6	0.67	0.68	0.69	0.70	0.71	0.72	0.74	0.75	0.76	0.77
7	0.78	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87	0.88
8	0.89	0.90	0.91	0.92	0.94	0.95	0.96	0.97	0.98	0.99
9	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08	1.09	1.10
10	1.11	1.12	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21
11	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.33
12	1.34	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.43	1.44
13	1.45	1.46	1.47	1.48	1.49	1.50	1.51	1.53	1.54	1.55
14	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.66
15	1.67	1.68	1.69	1.70	1.72	1.73	1.74	1.75	1.76	1.77
16	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.88
17	1.89	1.90	1.92	1.93	1.94	1.95	1.96	1.97	1.98	1.99
18	2.00	2.02	2.03	2.04	2.05	2.06	2.07	2.08	2.09	2.10
19	2.12	2.13	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22
20	2.23	2.24	2.25	2.26	2.27	2.28	2.29	2.31	2.32	2.33
21	2.34	2.35	2.36	2.37	2.38	2.39	2.41	2.42	2.43	2.44
22	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.55
23	2.56	2.57	2.58	2.59	2.61	2.62	2.63	2.64	2.65	2.66
24	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.76	2.77
25	2.78	2.80	2.81	2.82	2.83	2.84	2.85	2.86	2.87	2.88
26	2.90	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00
27	3.01	3.02	3.03	3.04	3.05	3.06	3.07	3.08	3.10	3.11
28	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22
29	3.23	3.24	3.25	3.26	3.27	3.29	3.30	3.31	3.32	3.33
30	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.42	3.43	3.44
31	3.45	3.46	3.47	3.49	3.50	3.51	3.52	3.53	3.54	3.55
32	3.56	3.57	3.59	3.60	3.61	3.62	3.63	3.64	3.65	3.66
33	3.68	3.69	3.70	3.71	3.72	3.73	3.74	3.75	3.76	3.78
34	3.79	3.80	3.81	3.82	3.83	3.84	3.85	3.86	3.88	3.89
35	3.90	3.91	3.92	3.93	3.94	3.95	3.96	3.98	3.99	4.00
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	$695^{\mathrm{mm.}}$	(from 6	592.51 to	697.50)).	
Centi- grade Degrees.					Tenths of	Degrees.		,		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim
0	0.00	0.01	0.02	0.03	0.04	0.06	0.07	0.08	0.09	0.10
1	0.11	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.20	0.21
2	0.22	0.24	0.25	0.26	0.27	0.28	0.29	0.30	0.31	0.33
3	0.34	0.35	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44
4	0.45	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54	0.55
5	0.56	0.57	0.58	0.59	0.61	0.62	0.63	0.64	0.65	0.66
6	0.67	0.68	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77
7	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.89
8	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.98	0.99	1.00
9	1.01	1.02	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11
10	1.12	1.13	1.14	1.16	1.17	1.18	1.19	1.20	1.21	1.22
11	1.23	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33
12	1.35	1.36	1.37	1.38	1.39	1.40	1.41	1.42	1.44	1.45
13	1.46	1.47	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56
14	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.66	1.67
15	1.68	1.69	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.78
16	1.79	1.81	1.82	1.83	1.84	1.85	1.86	1.87	1.88	1.90
17	1.91	1.92	1.93	1.94	1.95	1.96	1.97	1.99	2.00	2.01
18	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.12
19	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21	2.22	2.23
20	2.24	2.25	2.27	2.28	2.29	2.30	2.31	2.32	2.33	2.34
21	2.36	2.37	2.38	2.39	2.40	2.41	2.42	2.43	2.45	2.46
22	2.47	2.48	2.49	2.50	2.51	2.52	2.53	2.55	2.56	2.57
23	2.58	2.59	2.60	2.61	2.62	2.64	2.65	2.66	2.67	2.68
24	2.69	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.79
25	2.80	2.82	2.83	2.84	2.85	2.86	2.87	2.88	2.89	2.91
26	2.92	2.93	2.94	2.95	2.96	2.97	2.98	3.00	3.01	3.02
27	3.03	3.04	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13
28	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.23	3.24
29	3.25	3.26	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.35
30	3.37	3.38	3.39	3.40	3.41	3.42	3.43	3.44	3.45	3.47
31	3.48	3.49	3.50	3.51	3.52	3.53	3.54	3.56	3.57	3.58
32	3.59	3.60	3.61	3.62	3.63	3.65	3.66	3.67	3.68	3.69
33	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.78	3.79	3.80
34	3.81	3.83	3.84	3.85	3.86	3.87	3.88	3.89	3.90	3.91
35	3.93	3.94	3.95	3.96	3.97	3.98	3.99	4.00	4.02	4.03
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROMI	ETER :	700 ^{mm} .	(from	69 7 .5 1 t	o 702.5	0).	
Centigrade Degrees.		-			Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim, 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim. 0.10
1	0.11	0.12	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.21
2	0.23	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33
3	0.34	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44
4	0.45	0.46	0.47	0.49	0.50	0.51	0.52	0.53	0.54	0.55
5	0.56	0.58	0.59	0.60	0.61	0.62	0.63	0.64	0.66	0.67
6	0.68	0.69	0.70	0.71	0.72	0.73	0.75	0.76	0.77	0.78
7	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87	0.88	0.89
8	0.90	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.01
9	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.10	1.11	1.12
10	1.13	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.23
11	1.24	1.25	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34
12	1.36	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.45	1.46
13	1.47	1.48	1.49	1.50	1.51	1.53	1.54	1.55	1.56	1.57
14	1.58	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68
15	1.69	1.71	1.72	1.73	1.74	1.75	1.76	1.77	1.79	1.80
16	1.81	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91
17	1.92	1.93	1.94	1.95	1.97	1.98	1.99	2.00	2.01	2.02
18	2.03	2.04	2.06	2.07	2.08	2.09	2.10	2.11	2.12	2.14
19	2.15	2.16	2.17	2.18	2.19	2.20	2.21	2.23	2.24	2.25
20	2.26	2.27	2.28	2.29	2.30	2.32	2.33	2.34	2.35	2.36
21	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.45	2.46	2.47
22	2.49	2.50	2.51	2.52	2.53	2.54	2.55	2.56	2.58	2.59
23	2.60	2.61	2.62	2.63	2.64	2.66	2.67	2.68	2.69	2.70
24	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.81
25	2.82	2.84	2.85	2.86	2.87	2.88	2.89	2.90	2.91	2.93
26	2.94	2.95	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04
27	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15
28	3.16	3.17	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.27
29	3.28	3.29	3.30	3.31	3.32	3.33	3.34	3.36	3.37	3.38
30	3.39	3.40	3.41	3.42	3.43	3.45	3.46	3.47	3.48	3.49
31	3.50	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.59	3.60
32	3.62	3.63	3.64	3.65	3.66	3.67	3.68	3.69	3.71	3.72
33	3.73	3.74	3.75	3.76	3.77	3.78	3.80	3.81	3.82	3.83
34	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.92	3.93	3.94
3.5	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.03	4.04	4.06
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

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		В.	AROME	ETER :	705 ^{mm}	(from	702.51	to 707 .5	0).	0.10 0.22 0.33 0.44 0.56 0.67 0.79 0.90 1.01 1.13 1.24 1.35 1.47 1.58 1.70 1.81 1.92 2.04 2.15 2.26 2.38 2.49 2.61 2.72 2.83 2.95 3.06
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim, 0.00	Millim. 0.01	Millim.	Millim. 0.03	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim, 0.09	Millim 0.10
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.22
2	0.23	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0 33
3	0.34	0.35	0.36	0.38	0.39	0.40	0.41	0.42	0.43	0.44
4	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56
5	0.57	0.58	0.59	0.60	0.61	0.63	0.64	0.65	0.66	0.67
6	0.68	0.69	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.79
7	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.88	0.89	0.90
8	0.91	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.00	1.01
9	1.02	1.04	1.05	1.06	1.07	1.08	1-09	1.10	1.12	1
10	1.14	1.15	1.16	1.17	1.18	1.19	1.21	1.22	1.23	1.24
11	1.25	1.26	1.27	1.29	1.30	1.31	1.32	1.33	1.34	1.35
12	1.37	1.38	1.39	1.40	1.41	1.42	1.43	1.45	1.46	1.47
13	1.48	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58
14	1.59	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70
15	1.71	1.72	1.73	1.74	1.75	1.76	1.78	1.79	1.80	1.81
16	1.82	1.83	1.84	1.85	1.87	1.88	1.89	1.90	1.91	1.92
17	1.93	1.95	1.96	1.97	1.98	1.99	2.00	2.01	2.03	2.04
.18	2.05	2.06	2.07	2.08	2.09	2.11	2.12	2.13	2.14	2.15
19	2.16	2.17	2.18	2.20	2.21	2.22	2.23	2.24	2.25	2.26
20	2.28	2.29	2.30	2.31	2.32	2.33	2.34	2.36	2.37	2.38
21	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.49
22	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.58	2.59	2.61
23	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70	2.71	2.72
24	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.81	2.82	2.83
25	2.84	2.86	2.87	2.88	2.89	2.90	2.91	2.92	2.94	2.95
26	2.96	2.97	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.06
27	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.15	3.16	3.17
28	3.19	3.20	3.21	3.22	3.23	3.24	3.25	3.27	3.28	3.29
29	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40
30	3.41	3.42	3.44	3.45	3.46	3.47	3.48	3.49	3.50	3.52
31	3.53	3.54	3.55	3.56	3.57	3.58	3.60	3.61	3.62	3.63
32	3.64	3.65	3.66	3.68	3.69	3.70	3.71	3.72	3.73	3.74
33	3.75	3.77	3.78	3.79	3.80	3.81	3.82	3.83	3.85	3.86
34	3.87	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96	3.97
35	3.98	3.99	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.08
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	710 ^{mm} ·	(from	707.51 t	o 712.50	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin
0	0.00	0.01	0.02	0.03	0.05	0.06	0.07	0.08	0.09	0.10
1	0.11	0.13	0.14	0.15	0.16	0.17	0.18	0.19	0.21	0.22
2	0.23	0.24	0.25	0.26	0.28	0.29	0.30	0.31	0.32	0.33
3	0.34	0.36	0.37	0.38	0.39	0.40	0.41	0.42	0.44	0.45
4	0.46	0.47	0.48	0.49	0.50	0.52	0.53	0.54	0.55	0.56
5	0.57	0.58	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.68
6	0.69	0.70	0.71	0.72	0.73	0.74	0.76	0.77	0.78	0.79
7	0.80	0.81	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.91
8	0.92	0.93	0.94	0.95	0.96	0.97	0.99	1.00	1.01	1.02
9	1.03	1.04	1.05	1.07	1.08	1.09	1.10	1.11	1.12	1.13
10	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.23	1.24	1.25
11	1.26	1.27	1.28	1.29	1.31	1.32	1.33	1.34	1.35	1.36
12	1.38	1.39	1.40	1.41	1.42	1.43	1.44	1.46	1.47	1.48
13	1.49	1.50	1.51	1.52	1.54	1.55	1.56	1.57	1.58	1.59
14	1.60	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70	1.71
15	1.72	1.73	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.82
16	1.83	1.84	1.86	1.87	1.88	1.89	1.90	1.91	1.93	1.94
17	1.95	1.96	1.97	1.98	1.99	2.01	2.02	2.03	2.04	2.05
18	2.06	2.07	2.09	2.10	2.11	2.12	2.13	2.14	2.15	2.17
19	2.18	2.19	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.28
20	2.29	2.30	2.31	2.33	2.34	2.35	2.36	2.37	2.38	2.40
21	2.41	2.42	2.43	2.44	2.45	2.46	2.48	2.49	2.50	2.51
22	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.60	2.61	2.62
23	2.64	2.65	2.66	2.67	2.68	2.69	2.70	2.72	2.73	2.74
24	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.83	2.84	2.85
25	2.86	2.88	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97
26	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07	3.08
27	3.09	3.11	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20
28	3.21	3.22	3.23	3.24	3.25	3.27	3.28	3.29	3.30	3.31
29	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40	3.41	3.43
30	3.44	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53	3.54
31	3.55	3.56	3.58	3.59	3.60	3.61	3.62	3.63	3.64	3.66
32	3.67	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77
33	3.78	3.79	3.80	3.82	3.83	3.84	3.85	3.86	3.87	3.88
34	3.90	3.91	3.92	3.93	3.94	3.95	3.96	3.98	3.99	4.00
35	4.01	4.02	4.03	4.05	4.06	4.07	4.08	4.09	4.10	4.11
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

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		В	AROMI	ETER:	715 ^{mm.}	(from 7	712.51 to	717.50	0). 								
Centi- grade Degrees.					Tenths of	Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.							
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millin							
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.10							
1	0.12	0.13	0.14	0.15	0.16	0.17	0.18	0.20	0.21	0.22							
2	0.23	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.32	0.33							
3	0.35	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45							
4	0.46	0.47	0.48	0.50	0.51	0.52	0.53	0.54	0.55	0.57							
5	0.58	0.59	0.60	0.61	0.62	0.63	0.65	0.66	0.67	0.68							
6	0.69	0.70	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.80							
7	0.81	0.82	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91							
8	0.92	0.93	0.95	0.96	0.97	0.98	0.99	1.00	1.02	1.03							
9	1.04	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.13	1.14							
10	1.15	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.25	1.26							
11	1.27	1.28	1.29	1.30	1.32	1.33	1.34	1.35	1.36	1.37							
12	1.38	1.40	1.41	1.42	1.43	1.44	1.45	1.47	1.48	1.49							
13	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59	1.60							
14	1.62	1.63	1.64	1.65	1.66	1.67	1.68	1.70	1.71	1.72							
15	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.81	1.82	1.83							
	105	1 00	1.87	1.88	1.89	1.90	1.92	1.93	1.94	1.95							
16	1.85	1.86	1.98	2.00	2.01	2.02	2.03	2.04	2.05	2.07							
17	1.96	1.97	2.10	2.11	2.12	2.13	2.15	2.16	2.17	2.18							
18	2.08	2.09 2.20	2.10	$\frac{2.11}{2.23}$	$\frac{2.12}{2.24}$	2.15	2.13	2.10	2.28	2.30							
$\frac{19}{20}$	2.19 2.31	2.32	2.33	2.23	2.35	2.37	2.38	2.39	2.40	2.41							
-0	2.01	2.02	2.00	2.01						İ							
21	2.42	2.43	2.45	2.46	2.47	2.48	2.49	2.50	2.52	2.53							
22	2.54	2.55	2.56	2.57	2.58	2.60	2.61	2.62	2.63	2.64							
23	2.65	2.67	2.68	2.69	2.70	2.71	2.72	2.74	2.75	2.76							
24	2.77	2.78	2.79	2.80	2.82	2.83	2.84	2.85	2.86	2.87							
25	2.89	2.90	2.91	2.92	2.93	2.94	2.95	2.97	2.98	2.99							
26	3.00	3.01	3.02	3.04	3.05	3.06	3.07	3.08	3.09	3.10							
27	3.12	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22							
28	3.23	3.24	3.25	3.27	3.28	3.29	3.30	3.31	3.32	3.34							
29	3.35	3.36	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45							
30	3.46	3.47	3.49	3.50	3.51	3.52	3.53	3.54	3.55	3.57							
31	3.58	3.59	3.60	3.61	3.62	3.64	3.65	3.66	3.67	3.68							
32	3.69	3.70	3.72	3.73	3.74	3.75	3.76	3.77	3.79	3.80							
33	3.81	3.82	3.83	3.84	3.85	3.87	3.88	3.89	3.90	3.91							
34	3.92	3.94	3.95	3.96	3.97	3.98	3.99	4.00	4.02	4.03							
35	4.04	4.05	4.06	4.07	4.09	4.10	4.11	4.12	4.13	4.14							
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.							

		В	AROME	ETER:	720 ^{mm.}	(from	717.51 t	o 722.50).								
Centi- grade Degrees.					Tenths o	f Degrees.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.						
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.03	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim.	Millim. 0.10						
1	0.12	0.13	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22						
2	0.23	0.24	0.26	0.27	0.28	0.29	0.30	0.31	0.33	0.34						
3	0.35	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.45						
4	0.46	0.48	0.49	0.50	0.51	0.52	0.53	0.55	0.56	0.57						
5	0.58	0.59	0.60	0.62	0.63	0.64	0.65	0.66	0.67	0.69						
, 6	0.70	0.71	0.72	0.73	0.74	0.76	0.77	0.78	0.79	0.80						
7	0.81	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.91	0.92						
8	0.93	0.94	0.95	0.96	0.98	0.99	1.00	1.01	1.02	1.03						
9	1.05	1.06	1.07	1.08	1.09	1.10	1.12	1.13	1.14	1.15						
10	1.16	1.17	1.19	1.20	1.21	1.22	1.23	1.24	1.26	1.27						
11	1.28	1.29	1.30	1.31	1.32	1.34	1.35	1.36	1.37	1.38						
12	1.39	1.41	1.42	1.43	1.44	1.45	1.46	1.48	1.49	1.50						
13	1.51	1.52	1.53	1.55	1.56	1.57	1.58	1.59	1.60	1.62						
14	1.63	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73						
15	1.74	1.75	1.77	1.78	1.79	1.80	1.81	1.82	1.84	1.85						
16	1.86	1.87	1.88	1.89	1.91	1.92	1.93	1.94	1.95	1.96						
17	1.98	1.99	2.00	2.01	2.02	2.03	2.05	2.06	2.07	2.08						
18	2.09	2.10	2.11	2.13	2.14	2.15	2.16	2.17	2.18	2.20						
19	2.21	2.22	2.23	2.24	2.25	2.27	2.28	2.29	2.30	2.31						
20	2.32	2.34	2.35	2.36	2.37	2.38	2.39	2.41	2.42	2.43						
21	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.52	2.53	2.54						
22	2.56	2.57	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66						
23	2.67	2.68	2.70	2.71	2.72	2.73	2.74	2.75	2.77	2.78						
24	2.79	2.80	2.81	2.82	2.84	2.85	2.86	2.87	2.88	2.89						
25	2.91	2.92	2.93	2.94	2.95	2.96	2.97	2.99	3.00	3.01						
26	3.02	3.03	3.04	3.06	3.07	3.08	3.09	3.10	3.11	3.13						
27	3.14	3.15	3.16	3.17	3.18_	3.20	3.21	3.22	3.23	3.24						
28	3.25	3.27	3.28	3.29	3.30	3.31	3.32	3.34	3.35	3.36						
29	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45	3.46	5.47						
30	3.49	3.50	3.51	3.52	3.53	3.54	3.56	3.57	3.58	3.59						
31	3.60	3.61	3.63	3.64	3.65	3.66	3.67	3.68	3.70	3.71						
32	3.72	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.81	3.82						
33	3.83	3.85	3.86	3.87	3.88	3.89	3.90	3.92	3.93	3.94						
34	3.95	3.96	3.97	3.99	4.00	4.01	4.02	4.03	4.04	4.06						
35	4.07	4.08	4.09	4.10	4.11	4.13	4.14	4.15	4.16	4.17						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.						

		В.	BAROMETER: 725 ^{mm.} (from 722.51 to 727.50).										
Centi- grade Degrees.					Tenths o	f Degrees,				•			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			
	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millin			
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.08	0.09	0.11			
1	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22			
2	0.23	0.25	0.26	0.27	0.28	0.29	0.30	0.32	0.33	0.3-			
3	0.35	0.36	0.37	0.39	0.40	0.41	0.42	0.43	0.44	0.46			
4	0.47	0.48	0.49	0.50	0.51	0.53	0.54	0.55	0.56	0.57			
5	0.59	0.60	0.61	0.62	0.63	0.64	0.66	0.67	0.68	0.69			
6	0.70	0.71	0.73	0.74	0.75	0.76	0.77	0.78	0.80	0.8			
7	0.82	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.9			
s	0.94	0.95	0.96	0.97	0.98	0.99	1.01	1.02	1.03	1.0			
9	1.05	1.06	1.08	1.09	1.10	1.11	1.12	1.14	1.15	1.10			
10	1.17	1.18	1.19	1.21	1.22	1.23	1.24	1.25	1.26	1.28			
11	1.29	1.30	1.31	1.32	1.33	1.35	1.36	1.37	1.38	1.39			
12	1.40	1.42	1.43	1.44	1.45	1.46	1.47	1.49	1.50	1.5			
13	1.52	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.6			
14	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.7			
15	1.76	1.77	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.80			
16	1.87	1.88	1.90	1.91	1.92	1.93	1.94	1.95	1.97	1.9			
17	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.08	2.0			
18	2.11	2.12	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.2			
19	2.22	2.23	2.25	2.26	2.27	2.28	2.29	2.31	2.32	2.3			
20	2.34	2.35	2.36	2.38	2.39	2.40	2.41	2.42	2.43	2.4			
21	2.46	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.55	2.5			
22	2.57	2.59	2.60	2.61	2.62	2.63	2.64	2.66	2.67	2.68			
23	2.69	2.70	2.71	2.73	2.74	2.75	2.76	2.77	2.78	2.80			
24	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89	2.90	2.9			
25	2.93	2.94	2.95	2.96	2.97	2.98	3.00	3.01	3.02	3.0			
26	3.04	3.05	3.07	3.08	3.09	3.10	3.11	3.12	3.14	3.13			
27	3.16	3.17	3.18	3.19	3.21	3.22	3.23	3.24	3.25	3.20			
28	3.28	3.29	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38			
29	3.39	3.41	3.42	3.43	3.44	3.45	3.46	3.48	3.49	3.50			
30	3.51	3.52	3.53	3.55	3.56	3.57	3.58	3.59	3.60	3.6			
31	3.63	3.64	3.65	3.66	3.67	3.69	3.70	3.71	3.72	3.73			
32	3.74	3.76	3.77	3.78	3.79	3.80	3.81	3.83	3.84	3.83			
33	3.86	3.87	3.88	3.90	3.91	3.92	3.93	3.94	3.96	3.97			
34	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06	4.07	4.08			
35	4.10	4.11	4.12	4.13	- 4.14	4.15	4.17	4.18	4.19	4.20			
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.			

		В.	AROMI	ETER:	730 ^{mm.}	(from	727.51 t	o 732.5	0).	
Centigrade Grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
$\stackrel{\circ}{0}$	Millim. 0.00	Millim. 0.01	Millim.	Millim. 0.01	Millim.	Millim 0.06	Millim. 0.07	Millim. 0.08	Millim.	Millim. 0.11
1	0.12	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.22
2	0.24	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34
3	0.35	0.37	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46
4	0.47	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58
5	0.59	0.60	0.61	0.62	0.64	0.65	0.66	0.67	0.68	0.70
6	0.71	0.72	0.73	0.74	0.75	0.77	0.78	0.79	0.80	0.81
7	0.82	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93
8	0.94	0.95	0.97	0.98	0.99	1.00	1.01	1.03	1.04	1.05
9	1.06	1.07	1.08	1.10	1.11	1.12	1.13	1.14	1.15	1.17
10	1.18	1.19	1.20	1.21	1.23	1.24	1.25	1.26	1.27	1.28
11	1.30	1.31	1.32	1.33	1.34	1.35	1.37	1.38	1.39	1.40
12	1.41	1.43	1.44	1.45	1.46	1.47	1.48	1.50	1.51	1.52
13	1.53	1.54	1.56	1.57	1.58	1.59	1.60	1.61	1.63	1.64
14	1.65	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76
15	1.77	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	1.87
16	1.89	1.90	1.91	1.92	1.93	1.94	1.96	1.97	1.98	1.99
17	2.00	2 01	2.03	2.04	2.05	2.06	2.07	2.09	2.10	2.11
18	2.12	2.13	2.14	2.16	2.17	2.18	2.19	2.20	2.22	2.23
19	2.24	2.25	2.26	2.27	2.29	2.30	2.31	2.32	2.33	2.34
20	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44	2.45	2.46
21	2.47	2.49	2.50	2.51	2.52	2.53	2.54	2.56	2.57	2.58
22	2.59	2.60	2.62	2.63	2.64	2.65	2.66	2.67	2.69	2.70
23	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.79	2.80	2.82
24	2.83	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.92	2.93
25	2.95	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04	3.05
26	3.06	3.08	3.09	3.10	3.11	3.12	3.13	3.15	3.16	3.17
27	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.26	3.28	3.29
28	3.30	3.31	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.41
29	3.42	3.43	3.44	3.45	3.46	3.48	3.49	3.50	3.51	3.52
30	3.53	3.55	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64
31	3.65	3.66	3.68	3.69	3.70	3.71	3 72	3.73	3.75	3.76
32	3.77	3.78	3.79	3.81	3.82	3.83	3.84	3.85	3.86	3.88
33	3.89	3.90	3.91	3.92	3.94	3.95	3.96	3.97	3.98	3.99
34	4.01	4.02	4.03	4.04	4.05	4.06	4.07	4.09	4.10	4.11
35	4.12	4.14	4.15	4.16	4.17	4.18	4.19	4.21	4.22	4.23
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

 $\overline{\mathbf{C}}$

Centi-			Tenths of Degrees.											
grade Degrees.					Tenens o	Degrees.	1			ī				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
c	Millim. 0.00	Millim.	Millim.	Millim. 0.04	Millim.	Millim.	Millim.	Millim.	Millim.	Millii 0.1				
0	0.00	0.01	0.02	0.04	0.03	0.00	0.07	0.00	0.03	0.1				
1	0.12	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.21	0.2				
2	0.24	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.3				
3	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.4				
4	0.47	0.49	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.5				
5	0.59	0.61	0.62	0.63	0.64	0.65	0.66	0.68	0.69	0.7				
6	0.71	0.72	0.74	0.75	0.76	0.77	0.78	0.79	0.81	0.8				
7	0.83	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.9				
8	0 95	0.96	0.97	0.98	1.00	1.01	1.02	1.03	1.04	1.0				
9	1.07	1.08	1.09	1.10	1.12	1.13	1.14	1.15	1.16	1.1				
10	1.19	1.20	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.2				
11	1.30	1.32	1.33	1.34	1.35	1.36	1.37	1.39	1.40	1.4				
12	1.42	1.44	1.45	1.46	1.47	1.48	1.49	1.51	1.52	1.5				
13	1.54	1.55	1.57	1.58	1.59	1.60	1.61	1.63	1.64	1.6				
14	1.66	1.67	1.69	1.70	1.71	1.72	1.73	1.74	1.76	1.7				
15	1.78	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.87	1.8				
16	1.90	1.91	1.92	1.93	1.95	1.96	1.97	1.98	1.99	2.0				
17	2.02	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.1				
18	2.14	2.15	2.16	2.17	2.18	2.19	2.21	2.22	2.23	2.2				
19	2.25	2.27	2.28	2.29	2.30	2.31	2.33	2.34	2.35	2.3				
20	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.46	2.47	2.4				
21	2.49	2.50	2.51	2.53	2.54	2.55	2.56	2.57	2.59	2.6				
22	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.69	2.70	2.7				
23	2.73	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.82	2.8				
24	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.9				
25	2.97	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.0				
26	3.08	3.10	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.1				
27	3.20	3.21	3.23	3.24	3.25	3.26	3.27	3.29	3.30	3.3				
28	3.32	3.33	3.35	3.36	3.37	3.38	3.39	3.40	3.42	3.4				
29	3.44	3.45	3.46	3.48	3.49	3.50	3.51	3.52	3.54	3.5				
30	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	3.65	3.6				
31	3.68	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.7				
32	3.80	3.81	3.82	3.83	3.84	3.86	3.87	3.88	3.89	3.9				
33	3.91	3.93	3.94	3.95	3.96	3.97	3.99	4.00	4.01	4.0				
34 35	4.03	3.05 4.16	4.06 4.18	4.07 4.19	4.08 4.20	4.09 4.21	4.10 4.22	4.12 4.24	4.13 4.25	$\begin{array}{ c c }\hline 4.1\\ 4.2\end{array}$				
			·											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

		BAROMETER: 740 ^{min} (from 737.51 to 742.50).										
Centi- grade Degrees.					Tenths of	Degrees.						
	0.	L	2.	3.	4.	5.	6.	7.	8.	9.		
° 0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Millim. 0.04	Millim.	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.09	Millim 0.11		
1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.21	0.23		
2	0.24	0.25	0.26	0.27	0.29	0.30	0.31	0.32	0.33	0.35		
3	0.36	0.37	0.38	0.39	0.41	0.42	0.43	0.44	0.45	0.47		
4	0.48	0.49	0.50	0.51	0.53	0.54	0.55	0.56	0.57	0.59		
5	0.60	0.61	0.62	0.63	0.64	0.66	0.67	0.68	0.69	0.70		
6	0.72	0.73	0.74	0.75	0.76	0.78	0.79	0.80	0.81	0.82		
7	0.84	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94		
8	0.96	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.06		
9	1.07	1.09	1.10	1.11	1.12	1.13	1.15	1.16	1.17	1.18		
10	1.19	1.21	1.22	1.23	1.24	1.25	1.27	1.28	1.29	1.30		
11	1.31	1.33	1.34	1.35	1.36	1.37	1.39	1.40	1.41	1.42		
12	1.43	1.45	1.46	1.47	1.48	1.49	1.50	1.52	1.53	1.54		
13	1.55	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66		
14	1.67	1.68	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78		
15	1.79	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90		
16	1.91	1.92	1.93	1.95	1.96	1.97	1.98	1.99	2.01	2.02		
17	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.11	2.13	2.14		
18	2.15	2.16	2.17	2.19	2.20	2.21	2.22	2.23	2.25	2.26		
19	2.27	2.28	2.29	2.31	2.32	2.33	2.34	2.35	2.36	2.38		
20	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47	2.48	2.50		
21	2.51	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.60	2.62		
22	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.72	2.74		
23	2.75	2.76	2.77	2.78	2.79	2.81	2.82	2.83	2.84	2.85		
24	2.87	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.97		
25	2.99	3.00	3.01	3.02	3.03	3.05	3.06	3.07	3.08	3.09		
26	3.11	3.12	3.13	3.14	3.15	3.17	3.18	3.19	3.20	3.21		
27	3.22	3.24	3.25	3.26	3.27	3.28	3.30	3.31	3.32	3.33		
28	3.34	3.36	3.37	3.38	3.39	3.40	3.42	3.43	3.44	3.45		
29	3.46	3.48	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.57		
30	3.58	3.60	3.61	3.62	3.63	3.64	3.65	3.67	3.68	3.69		
31	3.70	3.71	3.73	3.74	3.75	3.76	3.77	3.79	3.80	3.81		
32	3.82	3.83	3.85	3.86	3.87	3.88	3.89	3.91	3.92	3.93		
33	3.94	3.95	3.97	3.98	3.99	4.00	4.01	4.02	4.04	4.05		
34 35	4.06 4.18	4.07 4.19	4.08 4.20	4.10 4.22	4.11 4.23	4.12 4.24	4.13 4.25	4.14 4.26	4.16 4.28	4.17 4.29		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

		В	BAROMETER: 745 ^{mm.} (from 742.51 to 747.50).									
Centi- grade Degrees.					Tenths of	Degrees.						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
0	Millim. 0.00	Millim.	Millim, 0.02	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.08	Millim. 0.10	Millin 0.11		
1	0.12	0.13	0.14	0.16	0.17	0.18	0.19	0.20	0.22	0.23		
2	0.24	0.25	0.26	0.28	0.29	0.30	0.31	0.32	0.34	0.35		
3	0.36	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.46	0.47		
4	0.48	0.49	0.51	0.52	0.53	0.54	0.55	0.57	0.58	0.59		
5	0.60	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71		
6	0.72	0.73	0.75	0.76	0.77	0.78	0.79	0.81	0.82	0.83		
7	0.84	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.94	0.95		
8	0.96	0.97	0.99	1.00	1.01	1.02	1.03	1.05	1.06	1.07		
9	1.08	1.09	1.11	1.12	1.13	1.14	1.15	1.17	1.18	1.19		
10	1.20	1.21	1.23	1.24	1.25	1.26	1.27	1.29	1.30	1.31		
11	1.32	1.33	1.35	1.36	1.37	1.38	1.39	1.41	1.42	1.43		
12	1.44	1.45	1.47	1.48	1.49	1.50	1.52	1.53	1.54	1.53		
13	1.56	1.58	1.59	1.60	1.61	1.62	1.64	1.65	1.66	1.67		
14	1.68	1.70	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79		
15	1.80	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91		
16	1.92	1.94	1.95	1.96	1.97	1.98	2.00	2.01	2.02	2.03		
17	2.04	2.06	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.15		
18	2.16	2.18	2.19	2.20	2.21	2.22	2.24	2.25	2.26	2.27		
19	2.28	2.30	2.31	2.32	2.33	2.34	2.36	2.37	2.38	2.39		
20	2.40	2.42	2.43	2.44	2.45	2.46	2.48	2.49	2.50	2.51		
21	2.53	2.54	2.55	2.56	2.57	2.59	2.60	2.61	2.62	2.63		
22	2.65	2.66	2.67	2.68	2.69	2.71	2.72	2.73	2.74	2.75		
23	2.77	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.87		
24	2.89	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	2.99		
2.5	3.01	3.02	3.03	3.04	3.05	3.07	3.08	3.09	3.10	3.11		
26	3.13	3.14	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.23		
27	3.25	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34	3.35		
28	3.37	3.38	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.48		
29	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.57	3.58	3.60		
30	3.61	3.62	3.63	3.64	3.66	3.67	3.68	3.69	3.70	3.72		
31	3.73	3.74	3.75	3.76	3.78	3.79	3.80	3.81	3.82	3.84		
32	3.85	3.86	3.87	3.88	3.90	3.91	3.92	3.93	3.94	3.96		
33	3.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.06	4.08		
34	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.18	4.20		
35	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.29	4.30	4.32		
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		

	BAROMETER: 750 ^{mm} (from 747.51 to 752.50).														
Centi- grade Degrees.					Tenths of	Degrees.									
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
° 0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Mıllim. 0.04	Millim.	Millim. 0.06	Millim. 0.07	Millim, 0.08	Millim. 0.10	Millin 0.11					
1	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.23					
2	0.24	0.25	0.27	0.28	0.29	0.30	0.31	0.33	0.34	0.35					
3	0.36	0.38	0.39	0.40	0.41	0.42	0.44	0.45	0.46	0.47					
4	0.48	0.50	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.59					
5	0.61	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.71					
6	0.73	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.84					
7	0.85	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.96					
8	0.97	0.98	0.99	1.00	1.02	1.03	1.04	1.05	1.07	1.08					
9	1.09	1.10	1.11	1.13	1.14	1.15	1.16	1.17	1.19	1.20					
10	1.21	1.22	1.23	1.25	1.26	1.27	1.28	1.30	1.31	1.32					
11	1.33	1.34	1.36	1.37	1.38	1.39	1.40	1.42	1.43	1.44					
12	1.45	1.46	1.48	1.49	1.50	1.51	1.53	1.54	1.55	1.56					
13	1.57	1.59	1.60	1.61	1.62	1.63	1.65	1.66	1.67	1.68					
14	1.69	1.71	1.72	1.73	1.74	1.76	1.77	1.78	1.79	1.80					
15	1.82	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.92					
16	1.94	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.03	2.05					
17	2.06	2.07	2.08	2.09	2.11	2.12	2.13	2.14	2.15	2.17					
18	2.18	2.19	2.20	2.21	2.23	2.24	2.25	2.26	2.28	2.29					
19	2.30	2.31	2.32	2.34	2.35	2.36	2.37	2.38	2.40	2.41					
20	2.42	2.43	2.45	2.46	2.47	2.48	2.49	2.51	2.52	2.53					
21	2.54	2.55	2.57	2.58	2.59	2.60	2.61	2.63	2.64	2.65					
22	2.66	2.68	2.69	2.70	2.71	2.72	2.73	2.75	2.76	2.77					
23	2.78	2.80	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89					
24	2.91	2.92	2.93	2.94	2.95	2.97	2.98	2.99	3.00	3.01					
25	3.03	3.04	3.05	3.06	3.07	3.09	3.10	3.11	3.12	3.14					
26	3.15	3.16	3.17	3.18	3.20	3.21	3.22	3.23	3.24	3.26					
27	3.27	3.28	3.29	3.30	3.32	3.33	3.34	3.35	3.37	3.38					
28	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.47	3.49	3.50					
$\begin{vmatrix} 29 \\ 30 \end{vmatrix}$	3.51 3.63	3.52	3.54 3.66	3.55 3.67	3.56 3.68	$3.57 \\ 3.69$	3.58	3.60	3.61	3.62					
90		3.04	0.00	i	9.00	5.03	3.70	3.72	3.73	3.74					
31	3.75	3.76	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86					
32	3.87	3.89	3.90	3.91	3.92	3.93	3.95	3.96	3.97	3.98					
33	3.99	4.01	4.02	4.03	4.04	4.06	4.07	4.08	4.09	4.10					
34 35	4.12	4.13 4.25	4.14 4.26	4.15	4.16 4.29	4.18 4.30	$4.19 \\ 4.31$	$\frac{4.20}{4.32}$	4.21 4.33	$4.22 \\ 4.35$					
	0.	1.	2.	3.	4.	5.									
	٠.	**	~•	9.	'#•	<i>y</i> .	6.	7.	8.	9.					

	BAROMETER: 755°°° (from 752.51 to 757.50).													
Centi- grade Degrees.					Tenths of	Degrees.								
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.				
0	0.00	0.01	0.02	0.04	0.05	0.06	0.07	0.09	0.10	0.11				
1	0.12	0.13	0.15	0.16	0.17	0.18	0.19	0.21	0.22	0.23				
2	0.24	0.26	0.27	0.28	0.29	0.30	0.32	0.33	0.34	0.35				
3	0.37	0.38	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48				
4	0.49	0.50	0.51	0.52	0.54	0.55	0.56	0.57	0.58	0.60				
5	0.61	0.62	0.63	0.65	0.66	0.67	0.68	0.69	0.71	0.72				
6	0.73	0.74	0.76	0.77	0.78	0.79	0.80	0.82	0.83	0.84				
7	0.85	0.87	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96				
8	0.97	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.08				
9	1.10	1.11	1.12	1.13	1.15	1.16	1.17	1.18	1.19	1.21				
10	1.22	1.23	1.24	1.26	1.27	1.28	1.29	1.30	1.32	1.33				
,,	1.34	7.05	1.36	1.38	1.39	1.40	1.41	1 49	1.44	1 45				
11	1.46	1.35 1.47	1.49	1.50	1.51	1.52	1.41 1.54	1.43 1.55	1.56	1.45 1.57				
12 13	1.58	1.60	1.49	1.62	1.63	1.65	1.66	1.67	1.68	1.69				
14	1.55	1.72	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82				
15	1.83	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94				
	- 0 -				2.00		2.00	201	2 0 "	0.00				
16	1.95	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06				
17	2.07	2.08	2.10	2.11 2.23	$2.12 \\ 2.24$	2.13 2.25	2.14	2.16	2.17 2.29	2.18				
18	2.19 2.32	$2.21 \\ 2.33$	2.22 2.34	2.35	2.36	2.38	2.27 2.39	2.28 2.40	2.41	2.30 2.42				
$\frac{19}{20}$	2.32	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.41	2.55				
20	2.11	2.40	2.40	2.4.	2.43	2.00	2.01	2.02	2.00	2.00				
21	2.56	2.57	2.58	2.60	2.61	2.62	2.63	2.64	2.66	2.67				
22	2.68	2.69	2.71	2.72	2.73	2.74	2.75	2.77	2.78	2.79				
23	2.80	2.81	2.83	2.84	2.85	2.86	2.88	2.89	2.90	2.91				
24	2.92	2.94	2.95	2.96	2.97	2.99	3.00	3.01	3.02	3.03				
25	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.13	3.14	3.16				
26	3.17	3.18	3.19	3.20	3.22	3.23	3.24	3.25	3.27	3.28				
27	3.29	3.30	3.31	3.33	3.34	3.35	3.36	3.38	3.39	3.40				
28	3.41	3.42	3.44	3.45	3.46	3.47	3.49	3.50	3.51	3.52				
29	3.53	3.55	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64				
30	3.66	3.67	3.68	3.69	3.70	3.72	3.73	3.74	3.75	3.77				
31	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89				
32	3.90	3.91	3.92	3.94	3.95	3.96	3.97	3.98	4.00	4.01				
33	4.02	4.03	4.05	4.06	4.07	4.08	4.09	4.11	4.12	4.13				
34	4.14	4.16	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.25				
35	4.26	4.28	4.29	4.30	4.31	4.33	4.34	4.35	4.36	4.37				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

		В.	AROME	ETER :	760 ^{mm.}	(from	757.51 t	o 762.5	0). 	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim.	Mıllim.	Millim.	Millim. 0.04	Millim, 0.05	Millim.	Millim.	Millim. 0.09	Millim. 0.10	Millin 0.11
	0.00	0.01	0.02	0.01	0.00	0.00	0.00	0.00	0.20	0.11
1	0.12	0.13	0.15	0.16	0.17	0.18	0.20	0.21	0.22	0.23
2	0.25	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	0.36
3	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.47	0.48
4	0.49	0.50	0.52	0.53	0.54	0.55	0.56	0.58	0.59	0.60
5	0.61	0.63	0.64	0.65	0.66	0.67	0.69	0.70	0.71	0.72
6	0.74	0.75	0.76	0.77	0.79	0.80	0.81	0.82	0.83	0.85
7	0.86	0.87	0.88	0.90	0.91	0.92	0.93	0.94	0.96	0.97
8	0.98	0.99	1.01	1.02	1.03	1.04	1.05	1.07	1.08	1.09
9	1.10	1.12	1.13	1.14	1.15	1.17	1.18	1.19	1.20	1.21
10	1.23	1.24	1.25	1.26	1.28	1.29	1.30	1.31	1.32	1.34
11	1.35	1.36	1.37	1.39	1.40	1.41	1.42	1.44	1.45	1.46
12	1.47	1.48	1.50	1.51	1.52	1.53	1.55	1.56	1.57	1.58
13	1.59	1.61	1.62	1.63	1.64	1.66	1.67	1.68	1.69	1.71
14	1.72	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83
15	1.84	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95
16	1.96	1.97	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07
17	2.09	2.10	2.11	2.12	2.13	2.15	2.16	2.17	2.18	2.20
18	2.21	2.22	2.23	2.24	2.26	2.27	2.28	2.29	2.31	2.32
19	2.33	2.34	2.36	2.37	2.38	2.39	2.40	2.42	2.43	2.44
20	2.45	2.47	2.48	2.49	2.50	2.51	2.53	2.54	2.55	2.56
21	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66	2.67	2.69
22	2.70	2.71	2.72	2.74	2.75	2.76	2.77	2.78	2.80	2.81
23	2.82	2.83	2.85	2.86	2.87	2.88	2.89	2.91	2.92	2.93
24	2.94	2.96	2.97	2.98	2.99	3.01	3.02	3.03	3.04	3.05
25	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15	3.16	3.18
26	3.19	3.20	3.21	3.23	3.24	3.25	3.26	3.28	3.29	3.30
27	3.31	3.32	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.42
28	3.43	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53	3.54
29	3.56	3.57	3.58	3.59	3.61	3.62	3.63	3.64	3.66	3.67
30	3.68	3.69	3.70	3.72	3.73	3.74	3.75	3.77	3.78	3.79
31	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91
32	3.93	3.94	3.95	3.96	3.97	3.99	4.00	4.01	4.02	4.04
33	4.05	4.06	4.07	4.08	4.10	4.11	4.12	4.13	4.15	4.16
34	4.17	4.18	4.20	4.21	4.22	4.23	4.24	4.26	4.27	4.28
35	4.29	4.31	4.32	4.33	4.34	4.35	4.37	4.38	4.39	4.40
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В.	AROME	ETER:	765 ^{mm.}	(from	762.51	to 7 67.5	0).			
Centigrade Degrees	Tenths of Degrees.											
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.		
$\stackrel{\circ}{0}$	Millim, 0.00	Millim. 0.01	Millim. 0.02	Mıllim. 0.04	Millim.	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim, 0.10	Millim. 0.11		
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.23		
2	0.25	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.35	0.36		
3	0.37	0.38	0.40	0.41	0.42	0.43	0.44	0.46	0.47	0.48		
4	0.49	0.51	0.52	0.53	0.54	0.56	0.57	0.58	0.59	0.61		
5	0.62	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73		
6	0.74	0.75	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85		
7	0.86	0.88	0.89	0.90	0.91	0.93	0 94	0.95	0.96	0.98		
8	0.99	1.00	1.01	1.02	1.04	1.05	1.06	1.07	1.09	1.10		
9	1.11	1.12	1.14	1.15	1.16	1.17	1.19	1.20	1.21	1.22		
10	1.23	1.25	1.26	1.27	1.28	1.30	1.31	1.32	1.33	1.35		
11	1.36	1.37	1.38	1.40	1.41	1.42	1.43	1.44	1.46	1.47		
12	1.48	1.49	1.51	1.52	1.53	1.54	1.56	1.57	1.58	1.59		
13	1.61	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72		
14	1.73	1.74	1.75	1.77	1.78	1.79	1.80	1.82	1.83	1.84		
15	1.85	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96		
16	1.98	1.99	2.00	2.01	2.02	2.04	2.05	2.06	2.07	2.09		
17	2.10	2.11	2.12	2.14	2.15	2.16	2.17	2.19	2.20	2.21		
18	2.22	2.23	2.25	2.26	2.27	2.28	2.30	2.31	2.32	2.33		
19	2.35	2.36	2.37	2.38	2.40	2.41	2.42	2.43	2.44	2.46		
20	2.47	2.48	2.49	2.51	2.52	2.53	2.54	2.56	2.57	2.58		
21	2.59	2.61	2.62	2.63	2.64	2.65	2.67	2.68	2.69	2.70		
22	2.72	2.73	2.74	2.75	2.77	2.78	2.79	2.80	2.82	2.83		
23	2.84	2.85	2.86	2.88	2.89	2.90	2.91	2.93	2.94	2.95		
24	2.96	2.98	2.99	3.00	3.01	3.03	3.04	3.05	3.06	3.07		
25	3.09	3.10	3.11	3.12	3.14	3.15	3.16	3.17	3.19	3.20		
26	3.21	3.22	3.23	3.25	3.26	3.27	3.28	3.30	3.31	3.32		
27	3.33	3.35	3.36	3.37	3.38	3.40	3.41	3.42	3.43	3.44		
28	3.46	3.47	3.48	3.49	3.51	3.52	3.53	3.54	3.56	3.57		
29	3.58	3.59	3.61	3.62	3.63	3.64	3.65	3.67	3.68	3.69		
.30	3.70	3.72	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.82		
31	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94		
32	3.95	3.96	3.98	3.99	4.00	4.01	4.03	4.04	4.05	4.06		
33	4.07	4.09	4.10	4.11	4.12	4.14	4.15	4.16	4.17	4.19		
34	4.20	4.21	4.22	4.24	4.25	4.26	4.27	4.28	4.30	4.31		
35	4.32	4.33	4.35	4.36	4.37	4.38	4.40	4.41	4.42	4.43		
	0.	1.	2.	3.	4.	5,	6.	7.	8.	9.		

 $\overline{\mathbf{C}}$

		В	AROME	TER:	770 ^{mm} ·	(from 7	67.51 t	o 772. 50	0).	
Centi- grade Degrees.					Tenths o	Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
0	Millim. 0.00	Millim. 0.01	Millim. 0.02	Mıllim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.07	Millim. 0.09	Millim. 0.10	Millim. 0.11
1	0.12	0.14	0.15	0.16	0.17	0.19	0.20	0.21	0.22	0.24
2	0.25	0.26	0.27	0.29	0.30	0.31	0.32	0.34	0.35	0.36
3	0.37	0.39	0.40	0.41	0.42	0.43	0.45	0.46	0.47	0.48
4	$\hat{0}.50$	0.51	0.52	0.53	0.55	0.56	0.57	0.58	0.60	0.61
5	0.62	0.63	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.73
6	0.75	0.76	0.77	0.78	0.80	0.81	0.82	0.83	0.85	0.86
7	0.87	0.88	0.89	0.91	0.92	0.93	0.94	0.96	0.97	0.98
8	0.99	1.01	1.02	1.03	1.04	1.06	1.07	1.08	1.09	1.11
9	1.12	1.13	1.14	1.16	1.17	1.18	1.19	1.21	1.22	1.23
10	1.24	1.26	1.27	1.28	1.29	1.30	1.32	1.33	1.34	1.35
11	1.37	1.38	1.39	1.40	1.42	1.43	1.44	1.45	1.47	1.48
12	1.49	1.50	1.52	1.53	1.54	1.55	1.57	1.58	1.59	1.60
13	1.62	1.63	1.64	1.65	1.67	1.68	1.69	1.70	1.72	1.73
14	1.74	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85
15	1.86	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98
16	1.99	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10
17	2.11	2.13	2.14	2.15	2.16	2.17	2.19	2.20	2.21	2.22
18	2.24	2.25	2.26	2.27	2.29	2.30	2.31	2.32	2.34	2.35
19	2.36	2.37	2.39	2.40	2.41	2.42	2.44	2.45	2.46	2.47
20	2.49	2.50	2.51	2.52	2.54	2.55	2.56	2.57	2.58	2.60
21	2.61	2.62	2.63	2.65	2.66	2.67	2.68	2.70	2.71	2.72
22	2.73	2.75	2.76	2.77	2.78	2.80	2.81	2.82	2.83	2.85
23	2.86	2.87	2.88	2.90	2.91	2.92	2.93	2.95	2.96	2.97
24	2.98	3.00	3.01	3.02	3.03	3.04	3.06	3.07	3.08	3.09
25	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19	3.21	3.22
26	3.23	3.24	3.26	3.27	3.28	3.29	3.31	3.32	3.33	3.34
27	3.36	3.37	3.38	3.39	3.41	3.42	3.43	3.44	3.45	3.47
28	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.57	3.58	3.59
29	3.60	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.70	3.72
30	3.73	3.74	3.75	3.77	3.78	3.79	3.80	3.82	3.83	3.84
31	3.85	3.87	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96
32	3.98	3.99	4.00	4.01	4.03	4.04	4:05	4.06	4.08	4.09
33	4.10	4.11	4.13	4.14	4.15	4.16	4.18	4.19	4.20	4.21
34	4.23	4.24	4.25	4.26	4.28	4.29	4.30	4.31	4.32	4.34
35	4.35	4.36	4.37	4.39	4.40	4.41	4.42	4.44	4.45	4.46
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

C

,	BAROMETER: 775 ^{mm.} (from 772.51 to 777.50). Tenths of Degrees.													
Centi- grade Degrees.					Tenths of	Degrees.								
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	Millim.	Millim.	Millim.	Millim.	Millim	Millim.	Millim.	Millim.	Millim.	Millim				
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11				
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24				
2	0.25	0.26	0.23	0.29	0.30	0.31	0.33	0.34	0.35	0.36				
3	0.38	0.39	0.40	0.41	0.43	0.44	0.45	0.46	0.48	0.49				
4	0.50	0.51	0.53	0.54	0.55	0.56	0.58	0.59	0.60	0.61				
5	0.63	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74				
6	0.75	0.76	0.78	0.79	0.80	0.81	0.83	0.84	0.85	0.86				
7	0.88	0.89	0.90	0.91	0.93	0.94	0.95	0.96	0.98	0.99				
8	1.00	1.01	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.11				
9	1.13	1.14	1.15	1.16	1.18	1.19	1.20	1.21	1.23	1.24				
10	1.25	1.26	1.28	1.29	1.30	1.31	1.33	1.34	1.35	1.36				
11	1.38	1.39	1.40	1.41	1.43	1.44	1.45	1.46	1.48	1.49				
12	1.50	1.51	1.53	1.54	1.55	1.56	1.58	1.59	1.60	1.61				
13	1.63	1.64	1.65	1.66	1.68	1.69	1.70	1.71	1.73	1.74				
14	1.75	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86				
15	1.88	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99				
16	2.00	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11				
17	2.13	2.14	2.15	2.16	2.18	2.19	2.20	2.21	2.23	2.24				
18	2.25	2.26	2.28	2.29	2.30	2.31	2.33	2.34	2.35	2.36				
19	2.38	2.39	2.40	2.41	2.43	2.44	2.45	2.46	2.48	2.49				
20	2.50	2.51	2.53	2.54	2.55	2.56	2.58	2.59	2.60	2.61				
21	2.63	2.64	2.65	2.66	2.68	2.69	2.70	2.71	2.73	2.74				
22	2.75	2.76	2.78	2.79	2.80	2.81	2.83	2.84	2.85	2.86				
23	2.88	2.89	2.90	2.91	2.93	2.94	2.95	2.96	2.98	2.99				
24	3.00	3.01	3.03	3.04	3.05	3.06	3.08	3.09	3.10	3.11				
25	3.13	3.14	3.15	3.16	3.18	3.19	3.20	3.21	3.23	3.24				
26	3.25	3.26	3.28	3.29	3.30	3.31	3.33	3.34	3.35	3.36				
27	3.38	3.39	3.40	3.41	3.43	3.44	3.45	3.46	3.48	3.49				
28	3.50	3.51	3.53	3.54	3.55	3.56	3.58	3.59	3.60	3.61				
29	3.63	3.64	3.65	3.66	3.68	3.69	3.70	3.72	3.73	3.74				
30	3.75	3.77	3.78	3.79	3.80	3.82	3.83	3.84	3.85	3.87				
31	3.88	3.89	3.90	3.92	3.93	3.94	3.95	3.97	3.98	3.99				
32	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09	4.10	4.12				
33	4.13	4.14	4.15	4.17	4.18	4.19	4.20	4.22	4.23	4.24				
34	4.25	4.27	4.28	4.29	4.30	4.32	4.33	4.34	4.35	4.37				
35	4.38	4.39	4.40	4.42	4.43	4.44	4.45	4.47	4.48	4.49				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				

Ĉ

		В	AROME	ETER:	780 ^{mm.}	(from	777.51 t	o 7 82.50	0).	
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.21	0.23	0.24
2	0.25	0.26	0.28	0.29	0.30	0.31	0.33	0.34	0.35	0.37
3	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.47	0.48	0.49
4	0.50	0.52	0.53	0.54	0.55	0.57	0.58	0.59	0.60	0.62
5	0.63	0.64	0.65	0.67	0.68	0.69	0.70	0.72	0.73	0.74
6	0.76	0.77	0.78	0.79	0.81	0.82	0.83	0.84	0.86	0.87
7	0.88	0.89	0.91	0.92	0.93	0.94	0.96	0.97	0.98	0.99
8	1.01	1.02	1.03	1.04	1.06	1.07	1.08	1.10	1.11	1.12
9	1.13	1.15	1.16	1.17	1.18	1.20	1.21	1.22	1.23	1.25
10	1.26	1.27	1.28	1.30	1.31	1.32	1.33	1.35	1.36	1.37
									1 40	
11	1.38	1.40	1.41	1.42	1.44	1.45	1.46	1.47	1.49	1.50
12	1.51	1.52	1.54	1.55	1.56	1.57	1.59	1.60	1.61	1.62
13	1.64	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75
14	1.76	1.78	1.79	1.80	1.81	1.83	1.84	1.85	1.86	1.88
15	1.89	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00
16	2.01	2.03	2.04	2.05	2.06	2.08	2.09	2.10	2.11	2.13
17	2.14	2.15	2.17	2.18	2.19	2.20	2.22	2.23	2.24	2.25
18	2.27	2.28	2.29	2.30	2.32	2.33	2.34	2.35	2.37	2.38
19	2.39	2.40	2.42	2.43	2.44	2.45	2.47	2.48	2.49	2.51
20	2.52	2.53	2.54	2.56	2.57	2.58	2.59	2.61	2.62	2.63
21	2.64	2.66	2.67	2.68	2.69	2.71	2.72	2.73	2.74	2.76
22	2.77	2.78	2.79	2.81	2.82	2.83	2.85	2.86	2.87	2.88
23	2.90	2.91	2.92	2.93	2.95	2.96	2.97	2.98	3.00	3.01
24	3.02	3.03	3.05	3.06	3.07	3.08	3.10	3.11	3.12	3.14
25	3.15	3.16	3.17	3.19	3.20	3.21	3.22	3.24	3.25	3.26
20	3.27	3.29	9 90	3.31	9 00	201	3.35	9 92	9.0*	9 90
26		3	3.30	3.44	3.32	3.34	3.35 3.47	3.36	3.37	3.39
27 28	$\frac{3.40}{3.52}$	3.41 3.54	$\frac{3.42}{3.55}$	3.44	$\frac{3.45}{3.58}$	$\frac{3.46}{3.59}$	3.47	$3.49 \\ 3.61$	$3.50 \\ 3.63$	3.51
28	3.65	3.66	3.68	3.69	3.70	3.71	3.73	3.74	3.75	3.64 3.76
30	3.78	3.79	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89
	5.10				0.00					0.00
31	3.90	3.92	3.93	3.94	3.95	3.97	3.98	3.99	4.00	4.02
32	4.03	4.04	4.05	4.07	4.08	4.09	4.10	4.12	4.13	4.14
33	4.15	4.17	4.18	4.19	4.20	4.22	4.23	4.24	4.26	4.27
34	4.28	4.29	4.31	4.32	4.33	4.34	4.36	4.37	4.38	4.39
35	4.41	4.42	4.43	4.44	4.46	4.47	4.48	4.49	4.51	4.52
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

		В	AROME	ETER:	785 ^{mm.}	(from	782.51 t	o 7 87.5	0).	
Centi grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.11
1	0.13	0.14	0.15	0.16	0.18	0.19	0.20	0.22	0.23	0.24
2	0.25	0.27	0.28	0.29	0.30	0.32	0.33	0.34	0.35	0.37
3	0.38	0.39	0.41	0.42	0.43	0.44	0.46	0.47	0.48	0.49
4	0.51	0.52	0.53	0.54	0.56	0.57	0.58	0.60	0.61	0.62
5	0.63	0.65	0.66	0.67	0.68	0.70	0.71	0.72	0.73	0.75
6	0.76	0.77	0.79	0.80	0.81	0.82	0.84	0.85	0.86	0.87
7	0.89	0.90	0.91	0.92	0.94	0.95	0.96	0.98	0.99	1.00
8	1.01	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.11	1.13
9	1.14	1.15	1.17	1.18	1.19	1.20	1.22	1.23	1.24	1.25
10	1.27	1.28	1.29	1.30	1.32	1.33	1.34	1.36	1.37	1.38
11	1.39	1.41	1.42	1.43	1.44	1.46	1.47	1.48	1.50	1.51
12	1.52	1.53	1.55	1.56	1.57	1.58	1.60	1.61	1.62	1.63
13	1.65	1.66	1.67	1.69	1.70	1.71	1.72	1.74	1.75	1.76
14	1.77	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.88	1.89
15	1.90	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01
10	2.03	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14
16	2.05	2.17	2.18	2.19	2.20	2.22	2.23	2.24	2.26	2.27
17 18	2.13	2.29	2.31	2.32	2.33	2.34	2.36	2.37	2.38	2.39
19	2.41	2.42	2.43	2.45	2.46	2.47	2.48	2.50	2.51	2.52
20	2.53	2.55	2.56	2.57	2.58	2.60	2.61	2.62	2.64	2.65
21	2.66	2.67	2.69	2.70	2.71	2.72	2.74	2.75	2.76	2.77
22	2.79	2.80	2.81	2.83	2.84	2.85	2.86	2.88	2.89	2.90
23	2.73	2.93	2.94	2.95	2.96	2.98	2.99	3.00	3.02	3.03
24	3.04	3.05	3.07	3.08	3.09	3.10	3.12	3.13	3.14	3.15
25	3.17	3.18	3.19	3.21	3.22	3.23	3.24	3.26	3.27	3.28
26	3.29	3.31	3.32	3.33	3.34	3.36	3.37	3.38	3.40	3.41
27	3.42	3.43	3.45	3.46	3.47	3.48	3.50	3.51	3.52	3.53
28	3.55	3.56	3.57	3.59	3.60	3.61	3.62	3.64	3.65	3.66
29	3.67	3.69	3.70	3.71	3.72	3.74	3.75	3.76	3.78	3.79
30	3.80	3.81	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91
31	3.93	3.94	3.95	3.97	3.98	3.99	4.00	4.02	4.03	4.04
32	4.05	4.07	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4.17
33	4.18	4.19	4.21	4.22	4.23	4.24	4.26	4.27	4.28	4.30
34	4.31	4.32	4.33	4.35	4.36	4.37	4.38	4.40	4.41	4.42
35	4.43	4.45	4.46	4.47	4.49	4.50	4.51	4.52	4.54	4.55
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

C

		B.	AROMI	ETER:	790 ^{mm}	(from	787.51 t	o 792.50	0).	
Centi- grade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
° 0	Millim. 0.00	Millim. 0.01	Millim, 0.03	Millim. 0.04	Millim. 0.05	Millim. 0.06	Millim. 0.08	Millim.	Millim. 0.10	Millim 0.11
1	0.13	0.14	0.15	0.17	0.18	0.19	0.20	0.22	0.23	0.24
2	0.26	0.27	0.28	0.29	0.31	0.32	0.33	0.34	0.36	0.37
3	0.38	0.40	0.41	0.42	0.43	0.45	0.46	0.47	0.48	0.50
4	0.51	0.52	0.54	0.55	0.56	0.57	0.59	0.60	0.61	0.62
5	0.64	0.65	0.66	0.68	0.69	0.70	0.71	0.73	0.74	0.75
6	0.77	0.78	0.79	0.80	0.82	0.83	0.84	0.85	0.87	0.88
7	0.89	0.91	0.92	0.93	0.94	0.96	0.97	0.98	0.99	1.01
8	1.02	1.03	1.05	1.06	1.07	1.08	1.10	1.11	1.12	1.13
9	1.15	1.16	1.17	1.19	1.20	1.21	1.22	1.24	1.25	1.26
10	1.28	1.29	1.30	1.31	1.33	1.34	1.35	1.36	1.38	1.39
11	1.40	1.42	1.43	1.44	1.45	1.47	1.48	1.49	1.50	1.52
12	1.53	1.54	1.56	1.57	1.58	1.59	1.61	1.62	1.63	1.64
13	1.66	1.67	1.68	1.70	1.71	1.72	1.73	1.75	1.76	1.77
14	1.79	1.80	1.81	1.82	1.84	1.85	1.86	1.87	1.89	1.90
15	1.91	1.93	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03
16	2.04	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.15
17	2.17	2.18	2.19	2.21	2.22	2.23	2.24	2.26	2.27	2.28
18	2.30	2.31	2.32	2.33	2.35	2.36	2.37	2.38	2.40	2.41
19	2.42	2.44	2.45	2.46	2.47	2.49	2.50	2.51	2.52	2.54
20	2.55	2.56	2.58	2.59	2.60	2.61	2.63	2.64	2.65	2.66
21	2.68	2.69	2.70	2.72	2.73	2.74	2.75	2.77	2.78	2.79
22	2.81	2.82	2.83	2.84	2.86	2.87	2.88	2.89	2.91	2.92
23	2.93	2.95	2.96	2.97	2.98	3.00	3.01	3.02	3.03	3.05
24	3.06	3.07	3.09	3.10	3.11	3.12	3.14	3.15	3.16	3.17
25	3.19	3.20	3.21	3.23	3.24	3.25	3.26	3.28	3.29	3.30
26	3.32	3.33	3.34	3.35	3.37	3.38	3.39	3.40	3.42	3.43
27	3.44	3.46	3.47	3.48	3.49	3.51	3.52	3.53	3.54	3.56
28	3.57	3.58	3.60	3.61	3.62	3.63	3.65	3.66	3.67	3.68
29	3.70	3.71	3.72	3.74	3.75	3.76	3.77	3.79	3.80	3.81
30	3.83	3.84	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94
31	3.95	3.97	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.07
32	4.08	4.09	4.11	4.12	4.13	4.14	4.16	4.17	4.18	4.19
33	4.21	4.22	4.23	4.25	4.26	4.27	4.28	4.30	4.31	4.32
34	4.34	4.35	4.36	4.37	4.39	4.40	4.41	4.42	4.44	4.45
35	4.46	4.48	4.49	4.50	4.51	4.53	4.54	4.55	4.56	4.58
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

	BAROMETER: 795 ^{mm.} (from 792.51 to 797.50).									
Centigrade Degrees.					Tenths o	f Degrees.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Mıllim.	Millim.	Millim.
0	0.00	0.01	0.03	0.04	0.05	0.06	0.08	0.09	0.10	0.12
1	0.13	0.14	0.15	0.17	0.18	0.19	0.21	0.22	0.23	0.24
2	0.26	0.27	0.28	0.30	0.31	0.32	0.33	0.35	0.36	0.37
3	0.38	0.40	0.41	0.42	0.44	0.45	0.46	0.47	0.49	0.50
4	0.51	0.53	0.54	0.55	0.56	0.58	0.59	0.60	0.62	0.63
5	0.64	0.65	0.67	0.68	0.69	0.71	0.72	0.73	0.74	0.76
6	0.77	0.78	0.80	0.81	0.82	0.83	0.85	0.86	0.87	0.89
7	0.90	0.91	0.92	0.94	0.95	0.96	0.98	0.99	1.00	1.01
8	1.03	1.04	1.05	1.06	1.08	1.09	1.10	1.12	1.13	1.14
9	1.15	1.17	1.18	1.19	1.21	1.22	1.23	1.24	1.26	1.27
10	1.28	1.30	1.31	1.32	1.33	1.35	1.36	1.37	1.39	1.40
11	1.41	1.42	1.44	1.45	1.46	1.48	1.49	1.50	1.51	1.53
12	1.54	1.55	1.57	1.58	1.59	1.60	1.62	1.63	1.64	1.66
13	1.67	1.68	1.69	1.71	1.72	1.73	1.75	1.76	1.77	1.78
14	1.80	1.81	1.82	1.83	1.85	1.86	1.87	1.89	1.90	1.91
15	1.92	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	2.04
16	2.05	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.16	2.17
17	2.18	2.19	2.21	2.22	2.23	2.25	2.26	2.27	2.28	2.30
18	2.31	2.32	2.34	2.35	2.36	2.37	2.39	2.40	2.41	2.43
19	2.44	2.45	2.46	2.48	2.49	2.50	2.51	2.53	2.54	2.55
20	2.57	2.58	2.59	2.60	2.62	2.63	2.64	2.66	2.67	2.68
21	2.69	2.71	2.72	2.73	2.75	2.76	2.77	2.78	2.80	2.81
22	2.82	2.84	2.85	2.86	2.87	2.89	2.90	2.91	2.93	2.94
23	2.95	2.96	2.98	2.99	3.00	3.02	3.03	3.04	3.05	3.07
24	3.08	3.09	3.11	3.12	3.13	3.14	3.16	3.17	3.18	3.19
25	3.21	3.22	3.23	3.25	3.26	3.27	3.28	3.30	3.31	3.32
26	3.34	3.35	3.36	3.37	3.39	3.40	3.41	3.43	3.44	3.45
27	3.46	3.48	3.49	3.50	3.52	3.53	3.54	3.55	3.57	3.58
28	3.59	3.61	3.62	3.63	3.64	3.66	3.67	3.68	3.70	3.71
29	3.72	3.73	3.75	3.76	3.77	3.79	3.80	3.81	3.82	3.84
30	3.85	3.86	3.88	3.89	3.90	3.91	3.93	3.94	3.95	3.96
31	3.98	3.99	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09
32	4.11	4.12	4.13	4.14	4.16	4.17	4.18	4.20	4.21	4.22
33	4.23	4.25	4.26	4.27	4.29	4.30	4.31	4.32	4.34	4.35
34	4.36	4.38	4.39	4.40	4.41	4.43	4.44	4.45	4.47	4.48
35	4.49	4.50	4.52	4.53	4.54	4.56	4.57	4.58	4.59	4.61
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centigrade Degrees. 0 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Millim. 0.00 0.13 0.26 0.39 0.52 0.65 0.77 0.90 1.03 1.16 1.29	Millim, 0.01 0.14 0.27 0.40 0.53 0.66 0.79 0.92 1.05 1.17 1.30	2. Millim, 0.03 0.15 0.28 0.41 0.54 0.67 0.80 0.93 1.06 1.19	Millim. 0.04 0.17 0.30 0.43 0.56 0.68 0.81 0.94 1.07	Millim. 0.05 0.18 0.31 0.44 0.57 0.70 0.83 0.96	5. Millim. 0.06 0.19 0.32 0.45 0.58 0.71	Millim. 0.0S 0.21 0.34 0.46 0.59 0.72	7. Millim. 0.09 0.22 0.35 0.48 0.61 0.74	8. Mdlim. 0.10 0.23 0.36 0.49 0.62 0.75	9. Millim. 0.12 0.25 0.37 0.50 0.63 0.76
0	Millim. 0.00 0.13 0.26 0.39 0.52 0.65 0.77 0.90 1.03 1.16 1.29 1.42 1.55	Millim. 0.01 0.14 0.27 0.40 0.53 0.66 0.79 0.92 1.05 1.17 1.30	Millim, 0.03 0.15 0.28 0.41 0.54 0.67 0.80 0.93 1.06 1.19	Millim. 0.04 0.17 0.30 0.43 0.56 0.68 0.81	Millim. 0.05 0.18 0.31 0.44 0.57 0.70	Millim. 0.06 0.19 0.32 0.45 0.58 0.71	Millim. 0.08 0.21 0.34 0.46 0.59	Millim. 0.09 0.22 0.35 0.48 0.61	Millim, 0.10 0.23 0.36 0.49 0.62	Millim. 0.12 0.25 0.37 0.50 0.63
0	0.00 0.13 0.26 0.39 0.52 0.65 0.77 0.90 1.03 1.16 1.29 1.42 1.55	0.01 0.14 0.27 0.40 0.53 0.66 0.79 0.92 1.05 1.17 1.30	0.03 0.15 0.28 0.41 0.54 0.67 0.80 0.93 1.06 1.19	0.04 0.17 0.30 0.43 0.56 0.68 0.81 0.94	0.05 0.18 0.31 0.44 0.57 0.70 0.83	0.06 0.19 0.32 0.45 0.58 0.71	0.08 0.21 0.34 0.46 0.59	0.09 0.22 0.35 0.48 0.61	0.10 0.23 0.36 0.49 0.62	0.12 0.25 0.37 0.50 0.63
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.26 0.39 0.52 0.65 0.77 0.90 1.03 1.16 1.29	0.27 0.40 0.53 0.66 0.79 0.92 1.05 1.17	0.28 0.41 0.54 0.67 0.80 0.93 1.06 1.19	0.30 0.43 0.56 0.68 0.81 0.94	0.31 0.44 0.57 0.70 0.83	0.32 0.45 0.58 0.71	0.34 0.46 0.59	0.35 0.48 0.61	$0.36 \\ 0.49 \\ 0.62$	0.37 0.50 0.63
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.39 0.52 0.65 0.77 0.90 1.03 1.16 1.29	0.40 0.53 0.66 0.79 0.92 1.05 1.17	0.41 0.54 0.67 0.80 0.93 1.06 1.19	0.43 0.56 0.68 0.81 0.94	0.44 0.57 0.70	0.45 0.58 0.71	0.46 0.59	0.48 0.61	0.49 0.62	0.50 0.63
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.52 0.65 0.77 0.90 1.03 1.16 1.29	0.53 0.66 0.79 0.92 1.05 1.17 1.30	0.54 0.67 0.80 0.93 1.06 1.19	0.56 0.68 0.81 0.94	0.57 0.70 0.83	0.58 0.71	0.59	0.61	0.62	0.63
5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.65 0.77 0.90 1.03 1.16 1.29 1.42 1.55	0.66 0.79 0.92 1.05 1.17 1.30	0.67 0.80 0.93 1.06 1.19	0.68 0.81 0.94	0.70 0.83	0.71			t .	
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.77 0.90 1.03 1.16 1.29 1.42 1.55	0.79 0.92 1.05 1.17 1.30	0.80 0.93 1.06 1.19	0.81 0.94	0.83		0.72	0.74	0.75	0.76
7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.90 1.03 1.16 1.29 1.42 1.55	0.92 1.05 1.17 1.30	0.93 1.06 1.19	0.94		0.04			ì	
7 8 9 10 11 12 13 14 15 16 17 18 19 20	1.03 1.16 1.29 1.42 1.55	1.05 1.17 1.30	1.06 1.19		0.96	0.84	0.85	0.87	0.88	0.89
8 9 10 11 12 13 14 15 16 17 18 19 20	1.16 1.29 1.42 1.55	1.17 1.30	1.19	1.07	0.00	0.97	0.98	0.99	1.01	1.02
9 10 11 12 13 14 15 16 17 18 19 20	1.42 1.55	1.30	1		1.08	1.10	1.11	1.12	1.14	1.15
11 12 13 14 15 16 17 18 19 20	$1.42 \\ 1.55$			1.20	1.21	1.23	1.24	1.25	1.27	1.28
12 13 14 15 16 17 18 19 20	1.55		1.32	1.33	1.34	1.36	1.37	1.38	1.39	1.41
12 13 14 15 16 17 18 19 20	1.55	1.43	1.45	1.46	1.47	1.48	1.50	1.51	1.52	1.54
13 14 15 16 17 18 19 20		1.56	1.58	1.59	1.60	1.61	1.63	1.64	1.65	1.67
14 15 16 17 18 19 20	1.68	1.69	1.70	1.72	1.73	1.74	1.76	1.77	1.78	1.79
15 16 17 18 19 20	1.81	1.82	1.83	1.85	1.86	1.87	1.89	1.90	1.91	1.92
17 18 19 20	1.94	1.95	1.96	1.98	1.99	2.00	2.01	2.03	2.04	2.05
17 18 19 20	2.07	2.08	2.09	2.10	2.12	2.13	2.14	2.16	2.17	2.18
18 19 20	2.20	2.21	2.22	2.23	2.25	2.26	2.27	2.29	2.30	2.31
19 20	2.32	2.34	2.35	2.36	2.38	2.39	2.40	2.41	2.43	2.44
20	2.45	2.47	2.48	2.49	2.50	2.52	2.53	2.54	2.56	2.57
21	2.58	2.60	2.61	2.62	2.63	2.65	2.66	2.67	2.69	2.70
21	2.71	2.72	2.74	2.75	2.76	2.78	2.79	2.80	2.81	2.83
22	2.84	2.85	2.87	2.88	2.89	2.91	2.92	2.93	2.94	2.96
23	2.97	2.98	3.00	3.01	3.02	. 3.03	3.05	3.06	3.07	3.09
24	3.10	3.11	3.12	3.14	3.15	3.16	3.18	3.19	3.20	3.22
25	3.23	3.24	3.25	3.27	3.28	3.29	3.31	3.32	3.33	3.34
26	3.36	3.37	3.38	3.40	3.41	3.42	3.43	3.45	3.46	3.47
27	3.49	3.50	3.51	3.52	3.54	3.55	3.56	3.58	3.59	3.60
28	3.62	3.63	3.64	3.65	3.67	3.68	3.69	3.71	$\frac{3.55}{3.72}$	3.73
29	3.74	3.76	3.77	3.78	3.80	3.81	3.82	3.83	3.85	3.86
30	3.87	3.89	3.90	3.91	3.93	3.94	3.95	3.96	3.98	3.99
.	4.00	4.00	4.00		4.0-		4.00	4.00	4	4.30
31	4.00	4.02	4.03	4.04	4.05	4.07	4.08	4.09	4.11	4.12
32	4.13	4.14	4.16	4.17	4.18	4.20	4.21	4.22	4.24	4.25
33	4.26	4.27	4.29	4.30	4.31 4.44	4.33	4.34 4.47	4.35 4.48	4.36	4.38
34 35	$4.39 \\ 4.52$	4.40 4.53	4.42 4.55	4.43 4.56	4.44	4.45 4.58	4.47	4.48	4.49 4.62	$4.51 \\ 4.64$
		1.	2.	3.	4.	5.	6.	7.	8.	9.

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XXI.

OLD FRENCH BAROMETER.

TABLE

FOR

REDUCING TO THE FREEZING POINT THE OBSERVATIONS TAKEN WITH OLD FRENCH BAROMETERS,

PROVIDED WITH BRASS SCALES, EXTENDING FROM THE CISTERN 10 THE TOP OF THE MERCURIAL COLUMN; CALCULATED FROM 240 TO 345

LINES, OR FROM 23 INCHES 4 LINES TO 28 INCHES 9 LINES.

BY KAEMTZ.

TABLE XXI.

This table is taken from Kaemtz's Lehrbuch der Meteorologie, Vol. II. p. 236. To render it more useful, the first page, giving the corrections for Barometrical Heights between 240 and 280 Paris lines, has been added.

The values adopted by Kaemtz for reducing the Old French Barometer are the following: —

Let h =observed height in French lines.

- " t = temperature of attached thermometer in degrees of Reaumur.
- " $m = \text{expansion of mercury between 0 and } 80^{\circ} \text{ Reaumur} = 0.018018.$
- " $l = \text{linear expansion of brass between 0 and 80}^{\circ}$ Reaumur = 0.0018782.

The normal temperature of standard being $= 13^{\circ}$ Reaumur.

And the formula becomes, -

$$-h \cdot \frac{m \times t - l \cdot (t - 13)}{1 + m \times t}$$

The Table gives the corrections only for full degrees and for every fifth line; but the intermediate values can easily be found by an interpolation at sight.

Example of Reduction.

Observed height	•	•	•	•	•	•	=	325.32 lines.
Attached thermome	eter					•	=	12.5 Reaumur.
In the line beginning w	ith 12	2°, an	d in t	he v	ertica	ıl colun	ın he	eaded 325 lines,
we find,	Cor	rectio	n for	1	2°	= -0	.89 1	ines.
	Inte	erpola	tion f	or	0°.5	= -0	.03	"
	Cor	rectio	on for	1	2°.5	= -0	.92	"
And we have,								
	Obs	erved	heig	ht,		325	.32	66
	Cor	rectio	n for	12°	.5,	-0	.92	"
He	ight a	at the	freez	ing	point	$= \overline{324}$.40 1	ines.

Normal Temperature of the Scale = 13° Reaumur.

Attached Thermom- eter.			I	Sarometer in	Paris Line	s,			Attached Thermon
Degrees of Reaumur.	240	245	250	255	260	265	270	275	Degrees o Reaumui
-15	Par. Lines. +0.65	Par Lines.	Par. Lines. +0.68	Par. Lines. +0.69	Par. Lines. +0.70	Par Lines	Par. Lines. +0.73	Par. Lines. +0.75	° -15
-14	0.60	0.61	0.63	0.64	0.65	0.67	0.68	0.69	-14
-13	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	-13
-12	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	-12
-11	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.52	-11
-10	0.41	0.42	0.43	0.44	0.44	0.45	0.46	0.47	-10
- 9	+0.36	+0.37	+0.38	+0.38	+0.39	+0.40	+0.41	+0.41	- 9
- 8	0.31	0.32	0.33	0.33	0.34	0.35	0.35	0.36	- 8
- 7	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.30	- 7
- 6	0.22	0.22	0.23	0.23	0.24	0.24	0.24	0.25	- 6
- 5	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	- 5
- 4	+0.12	+0.12	+0.13	+0.13	+0.13	+0.13	+0.14	+0.14	4
- 3	0.07	0.07	0.08	0.08	0.08	0.08	0.08	0.08	- 3
- 2	+0.02	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	- 2
- 1	-0.02	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1
0	-0.07	-0.07	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	0
+ 1	-0.12	-0.12	-0.13	-0.13	-0.13	-0.13	-0.14	-0.14	+ 1
2	0.17	0.17	0.18	0.18	0.18	0.19	0.19	0.19	2
3	0.22	0.22	0.23	0.23	0.24	0.24	0.24	0.25	3
4	0.27	0.27	0.28	0.28	0.29	0.29	0.30	0.30	4
5	0.31	0.32	0.33	0.33	0.34	0.35	0.35	0.36	5
+ 6	-0.36	-0.37	-0.38	-0.38	-0.39	-0.40	-0.41	-0.41	+ 6
7	0.41	0.42	0.43	0.44	0.44	0.45	0.46	0.47	7
8	0.46	0.47	0.48	0.49	0.50	0.51	0.52	0.52	8
9	0.51	0.52	0.53	0.54	0.55	0.56	0.57	0.58	9
10	0.55	0.57	0.58	0.59	0.60	0.61	0.62	0.64	10
+11	-0.60	-0.61	-0.63	-0.64	-0.65	-0.67	-0.68	-0.69	+11
12	0.65	0.66	0.68	0.69	0.70	0.72	0.73	0.75	12
13	0.70	0.71	0.73	0.74	0.76	0.77	0.79	0.80	13
14	0.75	0.76	0.78	0.79	0.81	0.82	0.84	0.86	14
15	0.80	0.81	0.83	0.84	0.86	0.88	0.89	0.91	15
+16	-0.84	-0.86	-0.88	-0.90	-0.91	-0.93	-0.95	-0.97	+16
17	0.89	0.91	0.93	0.95	0.97	0.98	1.00	1.02	17
18	0.94	0.96	0.98	1.00	1.02	1.04	1.06	1.08	18
19	0.99	1.01	1.03	1.05	1.07	1.09	1.11	1.13	19
20	1.04	1.06	1.08	1.10	1.12	1.14	1.17	1.19	20
+21	-1.08	-1.11	-1.13	-1.15	-1.17	-1.20	-1.22	-1.24	+21
22	1.13	1.16	1.18	1.20	1.23	1.25	1.27	1.30	22
23	1.18	1.20	1.23	1.25	1.28	1.30	1.33	1.35	23
24	1.23	1.25	1.28	1.31	1.33	1.36	1.38	1.41	24
25	1.28	1.30	1.33	1.36	1.38	1.41	1.44	1.46	25

Normal Temperature of the Scale $= 13^{\circ}$ Reaumur.

Attached Thermom- eter.			Baron	neter in Paris	Lines.			Attached Thermom- eter.
Degrees of Reaumur.	280	285	290	295	300	305	310	Degrees of Reaumur.
0	Par. Lines.	Par. Lines.	Par. Lines.	1	Par, Lines.	Par. Lines.	Par. Lines.	0
-15	+0.77	+0.78	+0.79	+0.81	+0.82	+0.84	+0.85	-15
-14	0.71	0.73	0.74	0.75	0.76	0.77	0.79	-14
-13	0.65	0.67	0.68	0.69	0.70	0.71	$0.72 \\ 0.66$	-13
-12	0.60 0.54	0.61	$0.62 \\ 0.56$	0.63 0.57	0.64	0.65 0.59	0.60	-12 -11
-11		I .	0.50	0.57		l	0.54	-11 -10
-10	0.48	0.49	0.50	0.51	0.52	0.53	0.94	-10
- 9	+0.43	+0.44	+0.44	+0.45	+0.46	+0.46	+0.47	- 9
- 8	0.37	0.38	0.38	0.39	0.40	0.40	0.41	- 8
- 7	0.31	0.32	0.32	0.33	0.34	0.34	0.35	- 7
- 6	0.26	0.26	0.26	0.27	0.27	0.28	0.28	- 6
- 5	0.20	0.20	0.21	0.21	0.21	0.22	0.22	- 5
- 4	+0.14	+0.15	+0.15	+0.15	+0.15	+0.16	+0.16	- 4
- 3	0.09	0.09	0.09	0.09	0.09	0.09	0.09	- 3
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	- 2
- î	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1
ō	-0.08	-0.09	-0.09	-0.09	-0.09	-0.09	-0.09	0
_		0.14	0.15	0.75		0.15	0.10	
+ 1	-0.14	-0.14	-0.15	-0.15	-0.15	-0.15	-0.16	+ 1
2	0.20	0.20	0.21	0.21	0.21	$0.22 \\ 0.28$	$0.22 \\ 0.28$	3
3	0.26	0.26	$0.27 \\ 0.32$	0.27	0.27	0.25	0.25	4
4 5	$0.31 \\ 0.37$	0.32	0.32	0.33	0.33 0.40	0.40	0.33	5
3	0.57		0.00	0.00	0.10	0.10		
+ 6	-0.43	-0.43	-0.44	-0.45	-0.46	-0.46	-0.47	+ 6
7	0.48	0.49	0.50	0.51	0.52	0.53	0.53	7
8	0.54	0.55	0.56	0.57	0.58	0.59	0.60	8
9	0.60	0.61	0.62	0.63	0.64	0.65	0.66	9
10	0.65	0.66	0.68	0.69	0.70	0.71	0.72	10
+11	-0.71	-0.72	-0.74	-0.75	-0.76	-0.77	-0.79	+11
12	0.77	0.78	0.80	0.81	0.82	0.84	0.85	12
13	0.82	0.84	0.85	0.87	0.88	0.90	0.91	13
14	0.88	0.90	0.91	0.93	0.94	0.96	0.98	14
15	0.94	0.95	0.97	0.99	1.00	1.02	1.04	15
+16	-0.99	-1.01	-1.03	-1.05	-1.07	-1.08	-1.10	+16
17	1.05	1.07	1.09	1.11	1.13	1.15	1.16	17
18	1.11	1.13	1.15	1.17	1.19	1.21	1.23	18
19	1.16	1.18	1.13	1.23	1.25	1.27	1.29	19
20	1.22	1.24	1.27	1.29	1.31	1.33	1.35	20
. 07					,	,	1	
+21	-1.28	-1.30	-1.33	-1.35	-1.37	-1.39	-1.42	+21
22	1.34	1.36	1.38	1.41	1.43	1.45	1.48	22
23	1.39	1.41	1.44	1.47	1.49	1.52	1.54	23
24	1.45	1.47	1.50	1.53	1.55	1.58	1.60	24
25	1.50	1.53	1.56	1.59	1.61	1.64	1.67	25

Normal Temperature of the Scale = 13° Reaumur.

Attached Thermometer.			Barom	eter in Paris	Lines.			Attached Thermom- eter,
Degrees of Reaumur.	315	320	325	330	335	340	345	Degrees of Reaumur
° -15	Par. Lines.	Par. Lines.	Par. Lines. +0.89	Par. Lines. +0.90	Par. Lines. +0.92	Par. Lines. +0.93	Par. Lines. +0.95	° -15
-14	0.80	0.81	0.83	0.84	0.85	0.86	0.88	-14
-13	0.74	0.75	0.76	0.78	0.78	0.79	0.81	-13
-12	0.67	0.68	0.69	0.70	0.71	0.73	0.74	-12
-11	0.61	0.62	0.63	0.64	0.65	0.66	0.67	-11
-10	0.54	0.55	0.56	0.57	0.58	0.59	0.60	-10
- 9	+0.48	+0.49	+0.50	+0.50	+0.51	+0.52	+0.53	- 9
- 8	0.42	0.42	0.43	0.44	0.44	0.45	0.46	- 8
- 7	0.35	0.36	0.36	0.37	0.37	0.38	0.39	- 7
- 6	0.29	0.29	0.30	0.30	0.31	0.31	0.32	- 6
- 5	0.22	0.23	0.23	0.24	0.24	0.24	0.25	- 5
- 4	+0.16	+0.16	+0.17	+0.17	+0.17	+0.17	+0.18	- 4
- 3	0.10	0.10	0.10	0.10	0.10	0.10	0.11	- 3
- 2	+0.03	+0.03	+0.03	+0.03	+0.03	+0.03	+0.04	- 2
- 1	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	- 1
0	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10	-0.10	0
+ 1	-0.16	-0.16	-0.16	-0.17	-0.17	-0.17	-0.17	+ 1
2	0.22	0.23	0.23	0.23	0.24	0.24	0.24	2
3	0.29	0.29	0.30	0.30	0.31	0.31	0.31	3
4	0.35	0.36	0.36	0.37	0.37	0.38	0.38	4
5	0.42	0.42	0.43	0.44	0.44	0.45	0.45	5
+ 6	-0.48	-0.49	-0.49	-0.50	-0.51	-0.52	-0.53	+ 6
7	0.54	0.55	0.56	0.57	0.58	0.59	0.60	7
8	0.61	0.62	0.63	0.64	0.65	0.66	0.67	8
9	0.67	0.68	0.69	0.70	0.71	0.72	0.74	9
10	0.74	0.75	0.76	0.77	0.78	0.79	0.81	10
+11	-0.80	-0.81	-0.82	-0.84	-0.85	-0.86	-0.88	+11
12	0.86	0.88	0.89	0.90	0.92	0.93	0.95	12
13	0.93	0.94	0.96	0.97	0.99	1.00	1.02	13
14 15	$0.99 \\ 1.05$	1.01	1.02 1.09	1.04	1.05	1.07	1.09	14
19	1.05	1.07	1.09	1.10	1.12	1.14	1.16	15
+16	-1.12	-1.14	-1.15	-1.17	-1.19	-1.21	-1.23	+16
17	1.18	1.20	1.22	1.24	1.26	1.28	1.30	17
18	1.25	1.27	1.29	1.31	1.33	1.35	1.37	18
19	1.31	1.33	1 35	1.37	1.39	1.41	1.44	19
20	1.37	1.40	1.42	1.44	1.46	1.48	1.51	20
+21	-1.44	-1.46	-1.48	-1.51	-1.53	-1.55	-1.58	+21
22	1.50	1.53	1.55	1.57	1.60	1.62	1.65	22
23	1.57	1.59	1.62	1.64	1.67	1.69	1.72	23
24	1.63	1.66	1.68	1.71	1.73	1.76	1.79	24
25	1.69	1.72	1.75	1.78	1.80	1.83	1.86	25



TABLES

FOR CORRECTING THE

DEPRESSION OF THE BAROMETRICAL COLUMN

DUE TO CAPILLARY ACTION.

CORRECTION FOR CAPILLARY ACTION.

It is known that the effects of capillary action are not the same in different liquids. In a tube plunged in water, the liquid in the tube rises higher than the level of the water in the vessel, and terminates by a concave surface, which is called a concare meniscus. In a tube plunged in mercury the liquid in the tube stands lower than the mercury in the vessel, and terminates by a convex surface, or a convex meniscus. It is thus evident that the mercurial column in the tube of a Barometer does not rise to its true height, and that it needs to be corrected for the depression due to capillarity, before it indicates the real pressure of the atmosphere.

La Place, in the *Mécanique Céleste*, Tom. IV., has shown that the value of that correction depends upon the form of the meniscus, and gave a formula to compute it. As this form varies in tubes of different bores, so does the depression, which diminishes as the diameter of the tube increases. The form of the meniscus, however, was supposed to be the same in tubes of the same diameter, and constant in the same tube; and on this supposition the tables generally used for correcting the capillary action have been computed. But more accurate observations have proved that, owing to various causes not yet all well understood, the form of the meniscus is often different in tubes of the same diameter, and that it is even variable in the tube of the same instrument.

It thus became necessary to construct new tables, taking into consideration, in a given case, both the diameter of the tube and the form of the meniscus. Such tables, with a double entry, have been given by Schleiermacher, in the Bibliothèque Universelle de Genève, Tom. VIII.; by Bravais, in the Annales de Physique et de Chimie, Tom. V. p. 508; and by Deleros. The numbers in these tables agree very closely; but as Deleros's table is more extended than that of Schleiermacher, and in a more convenient form than that of Bravais, it is given below, together with a reduction of it to English measures, for the ordinary use.

The other tables may serve for comparison.

Table XXII., from the Report of the Committee of Physics and Meteorology of the Royal Society of London, 1840, gives the correction to be applied to English barometers for capillary action in boiled and unboiled tubes. It takes into account the diameter of the tube, but not the variations of the height of the meniscus, or of the convexity which terminates the barometrical column. This last element is supposed to be in its normal state, and constant.

Tables XXIII. and XXIV., by Delcros, in the Annuaire Météorologique de France, for 1849, give the means of finding the true correction to be applied to metrical barometers for capillary action.

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The first shows the normal height of the meniscus when in contact with the air (as is the case in the inferior branch of a siphon barometer), and in the barometric vacuum at the top of the column, in tubes of different bores. It enables the observer to judge better of its variations.

Table XXIV. has been calculated by Delcros after the formulas of Schleiermacher, making the constant x equal to 6^{mm} .5278, being the mean value between that of Gay-Lussac = 6^{mm} .5262, and that of Schleiermacher = 6^{mm} .5295. It gives the amount of the capillary action in millimetres of mercury, taking into account both the size of the bore, or the internal radius of the tube, which will be found in the vertical argument, and the height of the meniscus, given in the horizontal argument. The internal radius of the tube is supposed to be known; the height of the meniscus, or the vertical distance from the base, that is, from the sharp line where the mercury ceases to be in contact with the walls of the tube, to the very top of the convexity, can be ascertained by measuring it several times by means of the vernier.

Example: — Suppose the internal radius of the tube to be $3^{mm}.2$, and the height of the meniscus to be $0^{mm}.8$; seek in the first vertical column the number $3^{mm}.2$; follow then the horizontal line as far as the vertical column headed $0^{mm}.8$, you find there the number $0^{mm}.776$, which is the amount of the depression due to capillary action, or the value of the correction to be added to the observation.

Table XXV. is taken from Pouillet's Eléments de Physique, Vol. II. p. 698 (1853). Table XXVI. is found in Gehler's Physicalisches Wörterbuch, and in Schubarth, Physicalische Tabellen, p. 21.

Table XXVII., which is Delcros's table reduced into English measures, gives the means of correcting with more accuracy the indications of the English barometers. For its use, see, above, the explanation to Table XXIV.

Table XXVIII. is from Baily's Astronomical Tables.

XXII. TABLE FOR THE CORRECTION TO BE ADDED TO ENGLISH BAROMETERS FOR CAPILLARY ACTION.

D:	Correction for							
Diameter of Tube.	Unboiled Tubes.	Boiled Tubes.						
Inch.	Inch.	Inch.						
0.60	0.004	0.002						
0.50	0.007	0.003						
0.45	0.010	0.005						
0.40	0.014	0.007						
0.35	0.020	0.010						
0.30	0.028	0.014						
0.25	0.040	0.020						
0.20	0.060	0.029						
0.15	0.088	0.044						
0.10	0.142	0.070						

XXIII. TABLE OF THE HEIGHT OF THE MENISCUS OF THE BAROMETRICAL COLUMN.

Internal Radius of the Tube in		Normal Height of the Meniscus in Millimetres.							
Millimetres.	In the Air.	In the Vacuum.							
1 2 3 4 5 6 7	0.427 0.795 1.079 1.287 1.413 1.488 1.524	0.34 0.64 0.86 1.03 1.13 1.19 1.22							

Vertical Argument = Internal Radius of Tube. Horizontal Argument = Height of Meniscus in Millimeters.

Radius of	the Tube in Milli- metres.	-	0.0	1.4	1.6	1.8	2.0	2.5	4.2	6 8 8	3.0	3.5	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.5	5 4	2.6	 89.	0.9	6.2	6.4	9.9	8.9	7.0
	1.8	Millim,	3	3	3	3	3	3	3	3 3	3	3	3	3	3	*	3	3	3	3	3	0.418	0.376	0.338	0.304	0.273	0.246	0.221	0.500	0.180	0.163
	1.7	Millim.	3	3	3	3	3	3	3	# #	3	3	3	¥	0.887	0.790	0.705	0.630	0.563	0.504	0.452	0.405	0.364	0.327	0.294	0.264	0.238	0.214	0.193	0.174	0.158
	1.6	Millim.	3	3	3	3	3	z	3	: : 	¥	1.238	1.095	0.970	0.861	0.766	0.682	0.609	0.544	0.486	0.436	0.330	0.350	0.315	0.283	0 254	0.229	0.506	0 186	0.168	0.152
	1.5	Millim.	3	3	3	3	3	ä	3	: :	1.368	1.203	1.061	0.938	0.831	0.738	0.657	0.585	0.522	0.467	0.418	0.374	0.336	0.301	0.271	0.243	0.219	0.197	0.178	0.160	0.145
	1.4	ĮĮ.	3	3	3	3	3	3	3	1.511	1.322	1.161	1.021	0.901	0.797	0.707	0.628	0.559	0.499	0.445	0.398	0.356	0.319	0.287	0.257	0.231	0.508	0.187	0.169	0.153	0.138
	1.3	Millim.	3	3	3	3	3	3	ย	1.676 1.456	1.270	1.112	0.976	0.860	0.760	0.673	0.597	0.531	0.473	0.422	0.377	0.337	0.305	0.271	0.243	0.219	0.197	0.177	0.160	0.144	0.130
ья.	1.2	Millim.	3	3	3	3	3	3	1.866	1.608	1.210	1.057	0.926	0.814	0.718	0.635	0.563	0.500	0.445	0.397	0.354	0.317	0.284	0.255	0.228	0.205	0.185	0.166	0.150	0.135	0.122
Height of the Meniscus in Millimetres	1.1	Millim.	3	3	3	ž	u	2.087	1.780	1.528	1.143	0.995	0.871	0.764	0.673	0.594	0.526	0.467	0.416	0.370	0.330	0.295	0.264	0.237	0.213	0.191	0.172	0.154	0.139	0.126	0.114
iscus in]	1.0	Millim.	3	:	z	3	2.348	1.978	1.680	1.436 1.235	1.068	0.928	0.810	0.710	0.624	0 551	0.487	0.432	0.384	0.342	0.305	0.272	0.244	0.218	0.196	0.176	0.158	0.142	0.128	0.116	0.105
f the Mer	0.0	Millim.	3	3	3	2.662	2.209	1.851	1.565	1.332	0.985	0.855	0.745	0.652	0.572	0.504	0.446	0.395	0.351	0.312	0.278	0.248	0.222	0.199	0.178	0.160	0 144	0.130	0.117	0.105	0.095
Height o	0.8	Millim.	3	z	3.050	2.483	2.046	1.705	1.436	1.218	968.0	0.776	0.675	0.590	0.517	0.455	0.402	0.356	0.316	0.281	0 250	0.224	0.200	0.179	0.160	0.144	0.129	0.116	0 105	0.095	0.085
	0.7	Millim.	3	3.542	2.812	2.270	1.859	1.541	1.292	0.932	0.800	0.691	0.601	0.524	0.459	0.404	0.356	0.315	0.580	0.249	0.221	0.198	0.177	0.158	0.142	0.127	0.114	0.103	0.033	0.084	0.075
	9.0	Millim.	4.190	3.218	2.528	2.024	1.648	1.360	1.135	0.958	0 698	0.603	0.523	0.455	0.399	0.350	0.309	0.273	0.242	0.215	0.192	0 171	0.153	0.137	0.122	0.110	0.099	0.089	0.080	0.072	0.065
	0.5	Millim. 5.085	3.758	2.825	2.196	1.746	1.413	1.161	0.966	0.813	0.591	0.509	0.441	0.384	0.336	0.295	0.260	0.230	0.204	0.181	0.161	0.144	0.128	0.115	0.103	0.092	0.083	0.074	0.067	0.061	0.055
	0.4	Millim. 4.396	3.162	2.363	1.820	1.437	1.158	0.948	0.787	0.560	0.478	0.412	0.356	0.310	0.271	0.238	0.310	0.185	0.164	0.146	0.130	0.116	0.103	0.092	0.083	0.074	0.067	0.060	0.054	0.049	0.044
	0.3	Millim. 3.516	_		1.404		0.885			0.502	0.362	0.312	_	0	0.205		0.158			0.110	0.098				0.062	0.056	0.050			0.037	0.033
	0.3			1.256	_	_		_		0.337				_		0.120	_		_				0.025			0.037			0.057		0.033
	0.1	Millim. 1.268	0.876	0 638	0.484	0.378	0.302	0.245	0.203	0.170	0.122	0.105	0.091	0.079	0.069	090.0	0.053	0.047	0.045	0.037	0.033	0.029	0 026	0.023	0.021	0.019	0.017	0.015	0.01	0.012	0.011
Radius of	in Milli- metres.	1.0	67	1:4	1.6	1.8	5.0	2.5	5.4	2, 2, & &	3.0	3.5	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4		ю. ю	0.9	6.2	6.4	9.9	8.9	7.0

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FROM POUILLET.

Internal Diameter of Tube.	Depression.	Differences.	Internal Diameter of Tube.	Depression.	Differences.	Internal Diameter of Tube	Depression.	Differences
Millimetres.	Millimetres.	Millimet.	Millimetres.	Millimetres.	Millimet.	Millimetres.	Millimetres.	Millimet.
2.00 2.50 3.00 3.50 4.00	4.579 3.595 2.902 2.415 2.053	0.985 0.692 0.487 0.362 0.301	8.50 9.00 9.50 10.00 10.59	0.604 0.534 0.473 0.419 0.372	0.070 0.061 0.054 0.047 0.042	15.00 15.50 16.00 16.50 17.00	0.127 0.112 0.099 0.087 0.077	0.015 0.013 0.012 0.010 ·
4.50 5.00 5.50 6.00 6.50	1.752 1.507 1.306 1.136 0.995	0.245 0.201 0.170 0.141 0.118	11.00 11.50 12.00 12.50 13.00	0.330 0.293 0.260 0.230 0.204	0.037 0.033 0.030 0.026 0.023	17.50 18.00 18.50 19.00 19.50	0.068 0.060 0.053 0.047 0.041	0.008 0.007 0.006 0.006
7.00 7.50 8.00	0.877 0.775 0.684	0.102 0.091 0.080	13.50 14.00 14.50	0.181 0.161 0.143	0.020 0.018 0.016	20.00 20.50 21.00	0.036 0.032 0.028	0.004 0.004

XXVI. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

Internal		Depression	according t	0	Internal	:	Depression	according t	to
Diameter of Tube.	La Place	Young.	Ivory.	Cavendish.	Diameter of Tube.	La Place.	Young	Ivory.	Cavendish
Millimetres.	Millim.	Millim.	Millim.	Millim.	Millimetres.	Millim.	Millim.	Millim.	Millim.
2.00	4.454	4.887	4.888	4.472	11.50	0.315			
2.50	3.568				12.00	0.281	0.242	0.253	0.200
3.00	2.918	2.986	2.988	3.054	12.50	0.250			
3.50	2.442		}		13.00	0.223	0.188	0.196	0.170
4.00	2.068	2.063	2.066	2.187	13.50	0.198		İ	
		1							
4.50	1.774		}		14.00	0.176	0.144	0.152	0.150
5.00	1.534	1.510	1.513	1.735	14.50	0.156			
5.50	1.337				15.00	0.137	0.111	0.118	0.131
6.00	1.171	1.139	1.134	1.377	15.50	0.121			
6.50	1.030				16.00	0.107	0.088	0.087	
7.00	0.909	0.869	0.868	1.073	16.50	0.094			
7.50	0.803	0.005	0.505	1.075	17.00	0.034	0.068	0.071	i i
8.00	0.503	0.669	0.673	0.820	17.50	0.033	0.003	0.071	1
8.50	0.632	0.003	0.073	0.020	18.00	0.064	0.053	0.054	
9.00	0.562	0.517	0.521	0.608	18.50	0.056	0.055	0.034	
9.00	0.502	0.517	0.521	0.003	10.50	0.050			
9.50	0.500				19.00	0.049	0.041	0.042	
10.00	0.445	0.402	0.406	0.406	19.50	0.043			
10.50	0.397				20.00	0.038	0.031	0.031	
11.00	0.354	0.311	0.316	0.270	20.50	0.034			ĺ
11.50	0.315				21.00	0.030	0.024	0.024	

XXVII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, REDUCED INTO ENGLISH INCHES FROM DELCROS'S TABLE.

Internal Diam- eter				Heigh	nt of Me	niscus i	n Thou	sandths	of an I	English	Inch.			
of Tube.	5	10	15	20	25	30	35	40	45	50	55	60	65	70
Eng. In.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch
0.10	0.040	0.076	0.109	0.136	0.155									
0.12	.027	.053	.076	.097	.114									
0.14	.019	.038	.056	.071	.085	0.097								
0.16	.015	.029	.042	.055	.066	.076	0.084							
0.18	.011	.022	.033	.043	.052	.060	.067	0.073						
0.20	.009	.018	.026	.034	.042	.049	.055	.060	0.064					
0.22	.007	.014	.021	.028	.034	.040	.045	.049	.053	0.057				
0.24	.006	.012	.017	.023	.028	.033	.037	.041	.045	.048	0.050			
0.26	.005	.010	.014	.019	.023	.027	.031	.035	.038	.040	.043	0.045		
0.28	.004	.008	.012	.016	.019	.023	.026	.029	.032	.034	.036	.038		
0.30	.003	.007	.010	.013	.016	.019	.022	.025	.027	.029	.031	.033	0.034	
0.32	.003	.006	.009	.011	.014	.016	.019	.021	.023	.025	.027	.028	.030	
0.34	.002	.005	.007	.010	.012	.014	.016	.018	.020	.022	.023	.024	.026	
0.36	.002	.004	.006	.008	.010	.012	.014	.016	.017	.019	.020	.021	.022	
0.38	.002	.004	.005	.007	.009	.010	.012	.013	.015	.016	.017	.018	.019	
0.40	.002	.003	.005	.006	.008	.009	.010	.012	.013	.014	.015	.016	.017	
0.42	.001	.003	.004	.005	.007	.008	.009	.010	.011	.012	.013	.014	.015	0.01
0.44	.001	.002	.004	.005	.006	.007	.008	.009	.010	.011	.011	.012	.013	.01
0.46	.001	.002	.003	.004	.005	.006	.007	.008	.008	.009	.010	.011	.011	.01
0.48	.001	.002	.003	.004	.004	.005	.006	.007	.007	.008	.009	.009	.010	.0
0.50	.001	.002	.002	.003	.004	.004	.005	.006	.006	.007	.008	.008	.008	.00
0.52	.001	.001	.002	.003	.003	.004	.005	.005	.006	.006	.007	.007	.007	.00
0.54	.001	.001	.002	.002	.003	.003	.004	.004	.005	.005	.006	.006	.006	.00
	5	10	15	20	25	30	35	40	45	50	55	60	65	70

XXVIII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, EXPRESSED IN ENGLISH INCHES. — Baily.

Diameter	Depr	ession accordii	ng to	Diameter	Depression according to					
of Tube.	lvory.	Young.	La Place.	of Tube.	lvory.	Young.	La Place.			
Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng. Inch.	Eng Inch.	Eng. Inch.	Eng. Inch			
0.05	0.2949	0.2964	0	0.35	0.0212	0.0196	0.0216			
0.10	.1404	.1424	.1394	0.40	.0154	.0139	.0159			
0.15	.0865	.0880	.0854	0.45	.0112	.0100	.0117			
0.20	.0583	.0589	.0580	0.50	.0082	.0074	.0087			
0.25	•0409	.0404	.0412	0.60	.0043	.0045	.0046			
0.30	.0293	.0280	.0296	0.70	.0023		.0024			
0.35	0.0212	0.0196	0.0216	0.80	0.0012	0	0.0013			

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IV.

HYPSOMETRICAL TABLES.



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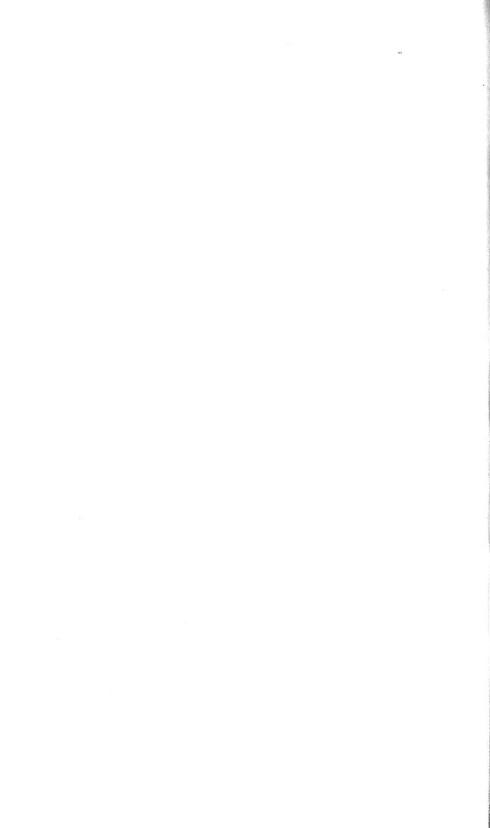
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BAROMETRICAL

MEASUREMENT OF HEIGHTS,

OR

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

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HYPSOMETRICAL TABLES

FOR

COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

Numerous determinations of altitude are one of the great desiderata of physical science, and no more ready means for obtaining them is at the disposal of the scientific man than the Barometer. A traveller, furnished with the improved and convenient instruments we can now command, and with some experience in using them, can take a large number of barometric observations for determining heights, at the cost of little trouble or time. It is, however, quite otherwise with the computations by which the results are obtained. The prospect of that tedious and time-robbing labor not only too often cools the zeal of the observer, but a vast amount of data actually collected remain of no avail from the want of having been computed.

The object of this much enlarged set of Hypsometrical Tables is to facilitate the task of the computer. It contains practical tables adapted to the three usual barometrical scales, and, among them, No. I., II., and V. are so disposed as to dispense with the use of logarithms, and to reduce the computation to the simplest arithmetical operations. The others suppose the use of logarithms, a method which may still be preferred by some observers.

As these various tables represent the development of the principal formulæ which have been proposed, the computer is enabled to compare the results obtained by each of them, and to select that which he most approves.

These formulæ may be referred to two classes, the respective types of which are Laplace's and Bessel's formulæ.

Laplace, in the Mécanique Céleste, Tom. IV. p. 292, gave a complete solution of the problem, and proposed a formula which soon superseded the older and less accurate formulæ of De Luc, Shuckburgh, and others. The coefficients which enter in it were derived from the best determinations of the needed physical constants which science could then furnish, the most important of which are the relative weight of the air and of the mercury, and the rate of expansion of air by heat. The first was assumed to be $\frac{1}{10^467}$, according to the experiments of Biot and Arago; and the barometrical coefficient deduced from it, 18317 metres. This coefficient was, however, empirically increased to 18336 metres, in order to adjust the results of the formula to those furnished by the careful trigonometrical measurements made by Ramond for the purpose of testing its correctness. It becomes 18393 metres when including the correction due to the effect of the decrease of gravity with the height on the density of the mercurial column and of the air. The coefficient expressing the expansion of the air by heat, as determined by Gay-Lussac, viz. 0.00375 of its bulk for one Centigrade degree, was adopted, but Laplace increased it to 0.004, in order to take into the account the effect of the greater expansive power of the vapors contained in the atmosphere.

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These values have been retained in the different formulæ proposed later by Gauss, in Schumacher's Jahrbuch for 1840, by Schmidt, Mathem. und Physische Geographie, II. p. 205, and by Baily, Astronomical Tables, p. 183, which, therefore, only change the form without changing the results. D'Aubuisson, in his formula and tables, Traité de Géognosie, p. 488, only reduced the barometrical coefficient to its theoretical value, which he determined to be 18365 metres, leaving unchanged the other coefficients of Laplace's formula.

Bessel first introduced, in his formula, Astronomische Nachrichten, No. 356, a separate correction for the effect of moisture. The correction for the temperature of the air is computed in his tables for two values of the coefficient, that of Gay-Lussac, 0.00375, and that of Rudberg, 0.00365. Laplace's barometrical coefficient is retained, but the correction for the decrease of gravity is considerably modified.

In Elie Ritter's formula, in the Mémoires de la Societé de Physique de Genève, Tom. XIII. p. 343, the corrections for temperature and moisture are also separated; but other values of the barometrical and thermometrical coefficients, derived from Regnault's determinations, are used, and a new method is proposed for applying the correction due to the expansion of air, which is made proportional to the square of the difference between the observed temperatures at each station.

Baeyer's formula, recently published in Poggendorf's Annalen der Physik und Chemie, Tom. XCVIII. p. 371, does not belong to either of the two classes just mentioned; for while it keeps Laplace's barometrical and thermometrical coefficients, it corrects the effect of temperature by a method analogous to that of Ritter, and it entirely neglects the effect of aqueous vapor.

In the following set the tables of Delcros, Guyot, and Loomis develop the formula of Laplace. The much larger tables of Delcros render unnecessary those of Oltmanns, which are yearly reprinted in the Annuaire du Burcau des Longitudes. Instead of Gauss's tables will be found the tables of Dippe, which are computed from the same formula, but are more extended. Baily's tables close the first series. The tables of Plantamour, computed from Bessel's formula, are given here in preference to Bessel's tables, because Plantamour substituted for Laplace's barometrical coefficient that derived from the probably more accurate determination of the relative weight of the air and mercury by Regnault, viz. 18404.8 metres. E. Ritter's tables, computed from his own formula, give perhaps, in extreme cases, better results; but as, in ordinary circumstances, the altitudes obtained do not much differ from those furnished by the less complicated tables of Plantamour, they were not reprinted here.

The miscellaneous tables which follow furnish useful materials for solving several questions connected with the barometrical measurements.

Regnault's table of Barometric Pressures corresponding to Temperatures of the Boiling Point of Water, revised by Moritz, and its reduction to English measures, will be found a valuable addition for thermometrical measurements of heights.

The Appendix to the Hypsometrical Tables now offers, in a new form, a complete series of tables for the comparison of the different measures of length generally used for indicating altitudes, the convenience of which will be fully appreciated by those who have attempted to collect and to use the abundant contributions furnished by all civilized nations to that branch of geographical science.

TABLES

FOR

DETERMINING DIFFERENCES OF LEVEL BY BAROMETRICAL OBSERVATIONS.

COMPUTED FROM THE COMPLETE FORMULA OF LAPLACE.

By M. T. DELCROS.

Construction of the Tables.

If we take z = difference of level of the two barometers, a = earth's mean radius = 6366200 metres,L = mean latitude between the two stations.

and further: -

At Station.
$$\begin{cases} h = \text{observed height of the barometer,} \\ T = \text{temperature of the barometer,} \\ t = \text{temperature of the air,} \\ t' = \text{observed height of the barometer,} \\ T' = \text{temperature of the barometer,} \\ t' = \text{temperature of the air,} \end{cases}$$

and if we make finally H = h + h'. $\left(\frac{T - T'}{6196}\right)$,

we shall have, according to Laplace, the following general and complete equation: -

If have, according to Laplace, the following general and complete equal
$$z=18336 \text{ metres} imes \left\{ \begin{array}{l} \left(1+\frac{2\cdot(t+t')}{1000}\right) \\ \left(1+0.0028371 \cos. 2. \text{ L}\right) \\ \left(\left(1+\frac{z}{a}\right)\cdot \text{ Log. }\left(\frac{h}{H}\right)+\frac{z}{a} \text{ 0.868589} \right) \end{array} \right\}$$

after the proper transformations this equation becomes

$$z = \text{Log.} \left(\frac{h}{H} \right) \text{ 18336 metres} \times \left\{ \begin{array}{l} \left(1 + \frac{2. \ (l + l')}{1000} \right) \\ \left(1 + 0.0028371 \text{ cos. 2. L} \right) \\ \left(1 + \frac{\left(\log. \left(\frac{h}{H} \right) + 0.868589 \right). \frac{z}{a}}{\text{Log.} \left(\frac{h}{H} \right)} \right) \end{array} \right\}$$
D

introducing into this expression the value in metres of a, the earth's mean radius, making $z = \text{Log.}\left(\frac{h}{H}\right)$ 18336 and Log. $\left(\frac{h}{H}\right) = \left(\frac{z}{18336}\right)$, which can be done without sensible error, the above formula takes the following form, sufficiently accurate for practical purposes:—

$$z = \text{Log.}\left(\frac{h}{H}\right)$$
. 18336 metres $\times \left\{ \begin{array}{l} \left(1 + \frac{(2.\ (t+t'))}{1000}\right) \\ \left(1 + 0.0028371 \text{ cos. 2. L}\right) \\ \left(1 + \frac{z + 15926}{6366200}\right) \end{array} \right\}$

the four factors of which can easily be developed in tables, as has been done by Mr. Oltmanns. But though this savant chose to develop also the second factor, I found it better not to do so, partly because the calculation of it is very easy, and also or account of the great extent it would have been necessary to give to this table, in order to avoid troublesome interpolations.

In the calculation of h'. $\left(\frac{T-T'}{6196}\right)$, Mr. Oltmanns used the constant coefficient of the absolute expansion of the mercurial column; I took that of the relative expansion of the mercury and of the brass scale. It is obvious, therefore, that if the scale of the barometer employed was of wood, glass, iron, or of another substance, it would be necessary to make use of as many different coefficients, and the Table II. could not be used. Moreover, Oltmanns combined the last two factors of the general formula in one single table with double entry. This table I have calculated, extending it sufficiently to avoid a double interpolation; but as it seemed to me much too extensive, I substituted for it Tables III. and IV., which are more condensed, without rendering any troublesome interpolation necessary.

I carried the calculation of these tables beyond the limits at which Oltmanns chose to stop, in order that they may answer for the most extreme cases.

At the head of each table will be found the factor of which it is the development; this makes any other explanation superfluous.

All these tables give, at sight, the numbers wanted; only when very great precision is desired, a slight interpolation, at sight, and very easy to apply, may be required. My principal object was to relieve the computer of the troublesome and annoying labor of interpolations.

I added to these four tables the small Table V., taken from the *Annuaire du Bureau des Longitudes* of Paris. It will be seldom used.

When calculating differences of level, in the same order, with the tables, and by the complete formula of Laplace, the results thus obtained never differ by more than one decimetre in the most extreme cases. The following example will illustrate this statement. I take the observation made in a balloon, by Gay-Lussac, at Paris, as an extreme case, which is very well adapted to manifest the errors of the tables, if there were any, by comparing the results obtained by means of them with those of the direct calculation according to the complete formula of Laplace, from which they are derived.

D

Example of Calculation by the complete Formula of Laplace and by the Tables
Height of the Balloon of Gay-Lussac.

The observation gave: -

Balloon
$$h' = 328.80$$
 $T' = -9.5$ $t' = -9.5$ $t' = -9.5$ Paris $h = 765.68$ $T = +30.8$ $t = +30.8$ $t = +30.8$ $t = +30.8$ The set of the set of

 $(A + a + \beta + v + \delta) = 6986.74$ Altitude barom. Paris = 48.70

Altitude of balloon = 7035.44 by the formula of Laplace.

25.03

Log. = +1.3984372

 $\delta = +$

Now let us calculate by the tables, placing side by side the corresponding results given by the formula of Laplace.

Balloon
$$h' = 328.80$$
 $T' = -9.5$ $t' = -9.5$
Paris $h = 765.68$ $T = +30.8$ $t = +30.8$

with $\begin{cases} h' = 328.80 \\ h = 765.68 \end{cases}$ Table I. gives $\begin{cases} 1478.4 \\ 8209.8 \end{cases}$ By the formula of Eaplace we found:

$$A = \frac{6731.4}{6679.79}$$
with $(T' - T) = -40^{\circ}.3$, Table II. gives $a = -52.0$

$$(A + a) = \frac{6679.4}{6679.79}$$
with $A = 48^{\circ}.50^{\circ}$, Table III. gives $A = -2.3$ $A = 2.53$

$$A = \frac{677.26}{6679.79}$$
with $A = 48^{\circ}.50^{\circ}$, Table III. gives $A = -2.3$ $A = 2.53$

$$A = \frac{6677.26}{6677.26}$$
with $A = \frac{6677.26}{6677.26}$
with $A = \frac{6677.26}{6677.26}$
with $A = \frac{6961.71}{6961.6}$

$$A = \frac{6961.71}{6961.71}$$
with $A = \frac{6961.71}{6986.7}$
Altitude of barometer at Paris $A = \frac{6986.7}{7035.44}$
Therefore altitude of balloon $A = \frac{6986.7}{7035.44}$

Two results which are sensibly identical. This ought not to astonish us; the tables being the exact development of the formula, they ought to give the same results, provided in both cases nothing has been neglected, and the four factors have been calculated in the same relative order.

Delcros.

Disposition and Use of the Tables.

The disposition of the tables is the following: -

In Table I., the first column on the left contains the height of the barometer in millimetres, corrected for the error of the instrument.

The second column headed N (number), gives in metres the first two figures of the number corresponding to each height of the barometer in the first column; the third column, headed 0.0, gives the remaining figures for the full number of millimetres; the following columns give the remaining figures for the same number of millimetres and each decimal fraction of a millimetre which may follow it. The value of the hundredths is to be found in the last column.

Example: - Height of Barometer = 761.00.

We look out in the first column for the number 761, and we find on the same line in the second column, 81; in the third column, headed 0.0, or full number, 61.1. The corresponding number is thus 8161.1 metres.

Height of barometer = 761.35.

The second column gives 81; the column headed 0.3 gives, on the same line, 64.2. The corresponding number is then 8164.2. Adding the value of five hundredths of millim., being 0^m.5, as indicated in the last column, we have 8164.7 metres, corresponding to 761.35 millim.

The other four tables need no further explanation.

To calculate, by means of the tables, a difference of level from two barometrical observations, proceed in the following manner:—

- 1. Take the height of the barometer at the lower station, or h, and seek in Table I. the number corresponding to this height. Seek likewise the number corresponding to the height of the barometer at the upper station. Subtract the second from the first. The remainder is the approximate difference of level between the two stations. Then apply the following corrections.
 - 2. Correction to be applied for the temperature of the barometers.

If T' be the temperature of the attached thermometer at the upper station, and T that of the attached thermometer at the lower station, take the difference, or T' - T, and seek in Table II. the number corresponding to this difference.

When T' is smaller than T, that is, when the temperature of the attached thermometer of the upper station is lower than that of the lower station, the correction is to be *subtracted* from the approximate height; when T' is greater than T, it is to be *added*.

3. Correction for the temperature of the air.

The first correction having been applied, multiply the number obtained, or N, by the double sum of the temperatures of the air at both stations, and divide the product by 1000; the number thus found, or the quantity expressed by $\frac{N}{1000}$. 2 (t + t) is the correction in metres which is to be *added* to the preceding number N.

- 4. Tables III. and IV. give two corrections; the first due to the decrease of gravitation in latitude, which is to be added when the mean latitude of the places of observation is between the 45th parallel and the equator; and to be subtracted when it is between the same parallel and the poles, as indicated at the head of the columns. The second correction, due to the decrease of gravitation on the vertical line, is always additive.
- 5. Table V. gives another small correction to be added in the case of the lower station being very elevated above the level of the ocean.

Examples of Calculation.

Measurement of the Height of Guanaxuato. By M. de Humboldt.

Barometer at the upper station, Barometer at the level of the sea, D $h' = 600.95 \quad T' = 2\hat{1}.3 \quad t' = 2\hat{1}.3$ $h = 763.15 \quad T = 25.3 \quad t = 25.3$

BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table I. gives the corresponding numbers,		$\begin{cases} h = 8 \\ h' = 6 \end{cases}$	3183.5 3280.8
Table II. gives for T' — T,	Difference,	-	1902.7 5.2
$\frac{N}{1000}$. 2 $(t+t')=1.897\times 93.2$,	Difference,		$\frac{1897.5}{176.8} = N$
	Sum,	·_	2074.3
Table III. gives for mean latitude of 21°, Table IV. gives for decrease of gravitation	in the vertical line	+ e, +	4.3 6.0
Hence altitude of Guanaxuato above the o	cean,	2	2084.6

Measurement of the height of Mont Blanc, August 29, 1844. By MM. Bravais and Martins.

Barometer at one metre below the summit, h'=424.05 T' = -4.2 t'=-7.6 Barometer of the Observatory of Geneva, h=729.65 T = -18.6 t=-19.3

Table I. gives for numbers corresponding to		$\begin{cases} h = 7826.0 \\ h' = 3504.4 \end{cases}$
I	Difference,	$\overline{4321.6}$
Table II. gives for T' — T,		— 29.3
· I	Difference,	$\overline{4292.3} = N$
$\frac{N}{1000}$. 2 $(t + t') = 4292 \times 23.4 =$		+ 100.4
s	bum,	${4392.7}$
Table III. gives for the mean latitude of 46°	,	- 0.4
п	Difference,	4392.3
Table IV. for decrease of gravitation in the	vertical line	+ 13.7
Table V. for the elevation of the lower static	on,	+ 0.5
s	Jum,	4406.5
Elevation of the lower barometer above the	ocean,	407.0
Hence elevation of upper barometer above the	he ocean,	4813.5
Finally, height of the summit of Mont Blanc		n, 4814.5

TABLE I. — Giving A = 18336 \times log. H or h..., argument H or h in Millimetres.

				11115 12	10000 X	105, 11 0,	r h, arg	, ameno 11	1	· · · · · · · · · · · · · · · · · · ·		
Barometer H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
288	4	23.4	26.2	28.9	31.7	34.4	37.2	40.0	42.7	45.5	48.2	1 0.3
289	4	51.0	53.8	56.5	59.3	62.0	64.8	67.5	70.3	73.0	75.8	2 0.5
290	4	78.5	81.3	84.0	86.7	89.5	92.2	95.0	97.7			3 0.8
290	5		1				1			00.4	03.2	4 1.1
291	5	05.9	08.7	11.4	14.1	16.8	19.6	22.3	25.0	27.8	30.5	5 1.4
292	5	33.2	36.0	38.7	41.4	44.1	46.8	49.6	52.3	55.0	57.7	6 1.6
293	5	60.5	63.2	65.9	68.6	71.3	74.0	76.7	79.5	82.2	84.9	7 1.9
294	5	87.6	90.3	93.0	95.7	98.4	1			02:2	0 1.0	8 2.2
294	6	01.0	00.0	1	""	00.1	01.1	03.8	06.5	09.2	11.9	9 2.4
295	6	14.6	17.3	20.0	22.7	25.4	28.1	30.8	33.5	36.2	38.9	0,2.1
296	6	41.6	44.3	47.0	49.6	52.3	55.0	57.7	60.4	63.1	65.8	
297	6	68.4	71.1	73.8	76.5	79.1	81.8	84.5	87.2	89.9	92.5	
	1	1		10.0	10.5	19.1	31.3	04.9	07.2	33.3	92.9	
298	6	95.2	97.9	00.5	03.2	05.0	08.6	11.0	120	16.6	10.2	
298	7	91.0	045	1		05.9		11.2	13.9	16.6	19.2	
299	7	21.9	24.5	27.2	29.9	32.5	35.2	37.S	40.5	43.2	45.8	
				1					00	00 -		
300	7	48.5	51.1	53.8	56.4	59.1	61.7	64.4	67.0	69.7	72.3	
301	7	75.0	77.6	80.3	82.9	85.5	88.2	90.8	93.5	96.1	98.7	ļ
302	8	01.4	04.0	06.6	09.3	11.9	14.5	17.2	19.8	22.4	25.1	l
303	8	27.7	30.3	33.0	35.6	38.2	40.8	43.5	46.1	48.6	51.3	!
304	8	54.0	56.6	59.2	61.8	64.4	67.0	69.6	72.3	74.9	77.5	
305	8	80.1	82.7	85.3	87.9	90.5	93.1	95.7	98.3			
305	9		1							01.0	03.6	
306	9	06.2	08.8	11.4	14.0	16.6	19.2	21.8	24.4	27.0	29.6	1 0.3
307	9	32.1	34.7	37.3	39.9	42.5	45.1	47.7	50.3	52.9	55.5	2 0.5
308	9	58.0	60.6	63.2	65.8	68.4	70.9	73.5	76.1	78.7	81.3	3 0.8
309	9	83.9	86.4	89.0	91.6	94.1	96.7	99.3		-		4 1.0
309	10								01.9	04.4	07.0	5 1.3
310	10	09.6	12.1	14.7	17.3	19.8	22.4	25.0	27.5	30.1	32.7	6 1.5
311	10	35.2	37.8	40.3	42.9	45.5	48.0	50.6	53.1	55.7	58.2	7 1.8
312	10	60.8	63.3	65.9	68.4	71.0	73.5	76.1	78.6	81.2	83.7	8 2.1
313	10	86.3	88.8	91.4	93.9	96.4	99.0					9 2.3
313	11							01.5	04.1	06.6	09.1	0 12.0
314	11	11.7	14.2	16.7	19.3	21.8	24.3	26.9	29.4	31.9	34.5	
315	11	37.0	39.5	42.0	44.6	47.1	49.6	52.1	54.7	57.2	59.7	
316	11	62.2	64.8	67.3	69.8	72.3	74.8	77.3	79.9	82.4	84.9	
317	11	87.4	89.9	92.4	94.9	97.4	99.9			-		
317	12		20.0			~ , · x		02.4	05.0	07.5	10.0	
318	12	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0	32.5	35.0	
319	12	37.5	40.0	42.5	45.0	47.5	50.0	52.4	54.9	57.4	59.9	
320	12	62.4	64.9	67.4	69.9	72.3	74.8	77.3	79.8	82.3	84.8	
320	12	87.2	89.7	92.2	94.7	92.1	99.6	11.9	19.0	02.0	04.0	
1 11	1 1	31.2	33.1	32.4	34.1	32.1	33.0	02.1	016	07.1	00 =	
321	13	19.0	115	170	10.1	21.9	9.4		04.6	07.1	09.5	
322	13	12.0	14.5	17.0	19.4		24.4	26.8	29.3	31.8	34.2	
323	13	36.7	39.2	41.6	44.1	46.6	49.0	51.5	53.9	56.4	58.9	
324	13	61.3	63.8	66.2	68.7	71.1	73.6	76.1	78.5	81.0	83.4	
325 325	13 14	85.9	88.3	90.8	93.2	95.7	98.1	00.5	03.0	05.4	07.9	
Barom- eter Hor h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

326 to 364mm.

					34	0 10 0	364 ^{mn}	·					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for	Parts r eacl
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	-	Metr
326	14	10.3	12.8	15.2	17.6	20.1	22.5	25.0	27.4	29.8	32.3	1	
327	14	34.7	37.2	39.6	42.0	44.5	46.9	49.3	51.7	54.2	56.6	2	0.5
328	14	59.0	61.5	63.9	66.3	68.7	71.2	73.6	76.0	78.4	80.9	3	0.7
329	14	83.3	85.7	88.1	90.5	92.9	95.4	97.8	[4	1.0
329	15								00.2	02.6	05.0	5	1.2
330	15	07.4	09.9	12.3	14.7	17.1	19.5	21.9	24.3	26.7	29.1	6	1.5
331	15	31.5	33.9	36.3	38.7	41.2	43.6	46.0	48.4	50.8	53.2	7	1.7
332	15	55.6	58.0	60.4	62.8	65.1	67.5	69.9	72.3	74.7	77.1	8	2.0
333	15	79.5	81.9	84.3	86.7	89.1	91.4	93.8	96.2	98.6		9	2.2
333	16						1				01.0	1	
334	16	03.4	05.8	08.1	10.5	12.9	15.3	17.7	20.0	22.4	24.8		
335	16	27.2	29.6	31.9	34.3	36.7	39.1	41.4	43.8	46.2	48.8		
336	16	50.9	53.3	55.7	58.0	60.4	62.8	65.1	67.5	69.9	72.2	1	0.2
337	16	74.6	77.0	79.3	81.7	84.0	86.4	88.8	91.1	93.5	95.8	2	0.4
338	16	98.2										3	0.7
338	17		00.5	02.9	05.2	07.6	10.0	12.3	14.7	17.0	19.4	4	1.0
339	17	21.7	24.1	26.4	28.8	31.1	33.4	35.8	38.1	40.5	42.8	5	1.2
340	17	45.2	47.5	49.8	52.2	54.5	56.9	59.2	61.5	63.9	66.2	6	1.5
341	17	68.6	70.9	73.2	75.6	77.9	80.2	82.6	84.9	87.2	89.5	7	1.7
342	17	91.9	94.2	96.5	98.9							8	1.9
342	18					01.2	03.5	05.8	08.2	10.5	12.8	9	2.2
343	18	15.1	17.4	19.8	22.1	24.4	26.7	29.0	31.4	33.7	36.0		
344	18	38.3	40.6	42.9	45.2	47.6	49.9	52.2	54.5	56.8	59.1		
345	18	61.4	63.7	66.0	68.3	70.6	73.0	75. 3	77.6	79.9	82.2		
346	18	84.5	86.8	89.1	91.4	93.7	96.0	98.3		1			
346	19								00.6	02.9	05.2		
347	19	07.5	09.6	12.0	14.3	16.6	18.9	21.2	23.5	25.8	28.1		
348	19	30.4	32.7	34.9	37.2	39.5	41.8	44.1	46.4	48.6	50.9		
349	19	53.2	55.5	57.8	60.1	62.3	64.6	66.9	69.2	71.5	7 3. 7		
350	19	76.0	78.3	80.6	82.8	85.1	87.4	89.6	91.9	94.2	96.5	1	0.2
351	19	98.7										2	0.4
351	20		01.0	03.3	05.5	07.8	10.1	12.3	14.6	16.8	19.1	3	0.7
352	20	21.4	23.6	25.9	28.2	30.4	32.7	34.9	37.2	39.5	41.7	4	0.9
353	20	44.0	46.2	48.5	50.7	53.0	55.2	57.5	59.7	62.0	64.2	5	1.1
354	20	66.5	68.7	71.0	73.2	75.5	77.7	80.0	82.2	84.5	86.7	6	1.3
355	20	89.0	91.2	93.4	95.7	97.9						7	1.6
355	21						00.2	02.4	04.6	06.9	09.1	8	1.8
356	21	11.4	13.6	15.8	18.1	20.3	22.5	24.8	27.0	29.2	31.5	9	2.1
357	21	33.7	35.9	38.2	40.4	42.6	44.8	47.1	49.3	51.5	53.7		
358	21	56.0	58.2	60.4	62.6	64.9	67.1	69.3	71.5	73.7	76.0		
359	21	78.2	80.4	82.6	84.8	87.0	89.3	91.5	93.7	95.9	98.1		
360	22	00.3	02.5	04.8	07.0	09.2	11.4	13.6	15.8	18.0	20.2		
361	22	22.4	24.6	26.8	29.0	31.2	33.4	35.6	37.9	40.1	42.3		
362	22	44.5	46.7	48.9	51.0	53.2	55.4	57.6	59.8	62.0	64.2		
363	22	66.4	68.6	70.8	73.0	75.2	77.4	79.6	81.8	83.9	86.1		
364	22	88.3	90.5	92.7	94.9	97.1	99.3		00.7	0.5.0			
364	23 ——							01.4	03.6	05.8	08.0	_	
Barom- eter Tor h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for	arts each mm

365 to 403mm.

	-					10 4		,					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for	arts each 1mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.		Metr.
365	23	10.2	12.4	14.5	16.7	18.9	21.1	23.2	25.4	27.6	29.8		0.2
366	23	32.0	34.1	36.3	38.5	40.7	42.8	45.0	47.2	49.3	51.5	2	0.4
367	23	53.7	55.9	58.0	60.2	62.4	64.5	66.7	68.9	71.0	73.2	3	0.6
368	23	75.4	77.5	79.7	81.8	84.0	86.2	88.3	90.5	92.6	94.8	4	0.9
369	23	97.0	99.1					00.0	00.0	02.0		5	1.1
369	24			01.3	03.4	05.6	07.7	09.9	12.1	14.2	16.4	6	1.3
370	24	18.5	20.6	22.8	24.9	27.1	29.2	31.4	33.5	35.7	37.8	7	1.5
371	24	40.0	42.1	44.3	46.4	48.6	50.7	52.9	55.0	57.2	59.3	8	1.7
372	24	61.5	63.6	65.8	67.9	70.1	72.2	74.3	76.5	78.6	80.8	1 1	1.9
373	24	82.9	85.0	87.2	89.3	91.4	93.6	95.7	97.8	99.9	00.0	"	1.0
373	25	02.0	00.0	01.2	0010	31.1	30.0	30.1	31.0	33.3	02.1		
374	25	04.2	06.3	08.4	10.6	12.7	14.8	16.9	19.0	21.2	23.3		
374	20	04.2	00.0	00.4	10.0	12.1	14.0	10.5	15.0	21.2	20.0		
975	25	25.4	27.5	29.6	31.8	33.9	26.0	90 1	10.0	19.4	115		
375	ļ	1			1	l .	36.0	38.1	40.2	42.4	44.5		
376	25	46.6	48.7	50.8	53.0	55.1	57.2	59.3	61.4	63.6	65.7		
377	25	67.8	69.9	72.0	74.1	76.2	78.3	80.5	82.6	84.7	86.8		
378	25	88.9	91.0	93.1	95.2	97.3	99.4						
378	26							01.5	03.6	05.7	07.8		
379	26	09.9	12.0	14.1	16.2	18.3	20.4	22.5	24.6	26.7	28.8		- 1
380	26	30.9	33.0	35.1	37.2	39.3	41.3	43.4	45.5	.47.6	49.7		
381	26	51.8	53.9	56.0	58.1	60.2	62.2	64.3	66.4	68.5	70.6		- 1
382	26	72.7	74.8	76.9	78.9	81.0	83.1	85.2	87.3	89.3	91.4		
383	26	93.5	95.6	97.7	99.7								
383	27					01.8	03.9	06.0	08.1	10.1	12.2	1	0.2
384	27	14.3	16.4	18.4	20.5	22.6	24.6	26.7	28.8	30.9	32.9	2	0.4
385	27	35.0	37.1	39.1	41.2	43.2	45.3	47.4	49.4	51.5	53.5	3	0.6
386	27	55.6	57.7	59.7	61.8	63.8	65.9	68.0	70.0	72.1	74.1	4	0.9
387	27	76.2	78.3	80.3	82.4	84.4	86.5	88.6	90.6	92.7	94.7	5	1.1
388	27	96.8	98.8							-		6	1.3
388	28	l		00.9	02.9	05.0	07.0	09.1	11.1	13.2	15.2	7	1.5
389	28	17.3	19.3	21.4	23.4	25.5	27.5	29.6	31.6	33.7	35.7	8	1.7
390	28	37.8	39.8	41.9	43.9	46.0	48.0	50.0	52.1	54.1	56.2	9	1.9
391	28	58.2	60.2	62.3	64.3	66.3	68.3	70.4	72.4	74.4	76.5		!
392	28	78.5	80.5	82.6	84.6	86.6	88.6	90.7	92.7	94.7	96.8		
393	28	98.8				ı							
393	29		00.8	02.8	04.9	06.9	08.9	10.9	12.9	15.0	17.0		
394	29	19.0	21.0	23.0	25.1	27.1	29.1	31.1	33.1	35.2	37.2		
395	29	39.2	41.2	43.2	45.2	47.2	49.2	51.3	53.3	55.3	57.3		
396	29	59.3	61.3	63.3	65.3	67.3	69.3	71.4	73.4	75.4	77.4		i
397	29	79.4	81.4	83.4	85.4	87.4	89.4	91.5	93.5	95.5	97.5		1
398	29	99.5				····		-1.0	20.0	20.0			
398	30		01.5	03.5	05.5	07.5	09.5	11.5	13.5	15.5	17.5		
399	30	19.5	21.5	23.5	25.5	27.5	29.4	31.4	33.4	35.4	37.4		1
999	30	10.0	21.0	20.0	-5.5	-1	20.4	91.4	99.4	3314	91.4		
400	30	39.4	41.4	43.4	45.4	47.4	49.4	51.3	53.3	55.3	57.3		
400	30	59.3	61.3	63.3	65.2	67.2	69.2	71.2	73.2	75.1	77.1		
II.	- 1	79.1	81.1	83.1	85.0	87.0	89.0	91.0					
402 403	30 30	98.9	01.1	39.1	00.0	01.0	09.0	91.0	93.0	94.9	96.9		
Barom-	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Pa	rts each
or h.								,,,		,		0.01	mm.
D						19							_

403 to 442mm.

					400	3 to 4	44					
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Part for ea 0.01 m
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Me
403	31		00.9	02.8	04.8	06.8	08.7	10.7	12.7	14.7	16.6	110
404	31	18.6	20.6	22.5	24.5	26.5	28.4	30.4	32.4	34.4	36.3	2 0
405	31	38.3	40.3	42.2	44.2	46.1	48.1	50.1	52.0	54.0	55.9	3 0
406	31	57.9	59.9	61.8	63.8	65.7	67.7	69.7	71.6	73.6	75.5	4 0.
407	31	77.5	79.5	81.4	83.4	85.3	87.3	89.3	91.2	93.2	95.1	5 1
408	31	97.1	99.0									6 1
408	32		1	01.0	02.9	04.9	06.8	08.8	10.7	12.7	14.6	7 1
409	32	16.6	18.5	20.5	22.4	24.4	26.3	28.2	30.2	32.1	34.1	8 1.
410	32	36.0	37.9	39.9	41.8	43.8	45.7	47.6	49.6	51.5	53.5	9 1.
411	32	55.4	57.3	59.3	61.2	63.2	65.1	67.0	69.0	70.9	72.9	
412	32	74.8	76.7	78.7	80.6	82.5	84.4	86.4	88.3	90.2	92.2	
413	32	94.1	96.0	97.9	99.9	02.0	04.4	00.4	00.0	30.2	02.2	1
413	33	34.1	30.0	31.3	33.3	01.8	03.7	05.6	07.5	09.5	11.4	
- 1		100	15.0	17.1	10.1		ı				Į	ĺ
414	33	13.3	15.2	17.1	19.1	21.0	22.9	24.8	26.7	28.7	30.6	
415	33	32.5	34.4	36.3	38.3	40.2	42.1	44.0	45.9	47.9	49.8	
416	33	51.7	53.6	55.5	57.4	59.3	61.2	63.2	65.1	67.0	68.9	
417	33	70.8	72.7	74.6	76.5	78.4	80.3	82.3	84.2	86.1	88.0	
418	33	89.9	91.8	93.7	95.6	97.5	99.4				_	
418	3-1		1			!	l	01.3	03.2	05.1	07.0	
419	34	08.9	.10.S	12.7	14.6	16.5	18.4	20.3	22.2	24.1	26.0	
420	34	27.9	29.8	31.7	33.6	35.5	37.3	39.2	41.1	43.0	44.9	
421	34	46.8	48.7	50.6	52.5	54.4	56.2	58.1	60.0	61.9	63.8	
422	34	65.7	67.6	69.5	71.4	73.3	75.1	77.0	78.9	80.8	82.7	1 0.
423	34	84.6	86.5	88.4	90.2	92.1	94.0	95.9	97.8	99.6		2 0.
423	35						ł				01.5	3 0.
424	35	03.4	05.3	07.2	09.0	10.9	12.8	14.7	16.6	18.4	20.3	4 0.
												5 1.
425	35	22.2	24.1	25.9	27.8	29.6	31.5	33.4	35.2	37.1	38.9	6 1.
426	35	40.8	42.7	44.5	46.4	48.3	50.1	52.0	53.9	55.S	57.6	7 1.
427	35	59.5	61.4	63.2	65.1	67.0	68.8	70.7	72.6	74.5	76.3	8 1.
428	35	78.2	80.1	81.9	83.8	85.6	87.5	89.4	91.2	93.1	94.9	9 1.
429	35	96.8	98.6	01.0	00.0	00.0	01.5	03.4	31.2	30.1	0 1.0	311.
429		30.0	30.0	00.5	02.3	04.2	06.0	07.9	09.7	11.6	13.4	
	36	159	12.1	i	20.8				28.2	30.1	31.9	
430	36	15.3	17.1	19.0	ì	22.7	24.6	26.4		48.5	50.4	
431	36	33.8	35.6	37.5	39.3	41.2	43.0	44.8	46.7		1	
432	36	52.2	54.0	55.9	57.7	59.6	61.4	63.2	65.1	66.9	68.8	
433	36	70.6	72.4	74.3	76.1	78.0	79.8	81.6	83.5	85.3	87.2	
434	36	89.0	90.8	92.7	94.5	96.3	98.1		0	00.0	0	
434	37	0	00.					00.0	01.8	03.6	05.5	
435	37	07.3	09.1	11.0	12.8	14.6	16.4	18.3	20.1	21.9	23.8	
436	37	25.6	27.4	29.2	31.1	32.9	34.7	36.5	38.3	40.2	42.0	
437	37	43.8	45.6	47.5	49.3	51.1	52.9	51.8	56.6	58.4	60.3	
438	37	62.1	63.9	65.7	67.6	69.4	71.2	73.0	74.8	76.7	78.5	
439	37	80.3	82.1	83.9	85.7	87.5	89.3	91.2	93.0	94.8	96.6	
440	37	98.4	1									
440	3S		00.2	02.0	03.8	05.6	07.5	09.3	11.1	12.9	14.7	
441	38	16.5	18.3	20.1	21.9	23.7	25.5	27.3	29.1	30.9	32.7	
442	38	34.5	36.3	38.1	39.9	41.7	43.5	45.3	47.1	48.9	50.7	-
Birom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for ea 0.01m

443 to 482mm.

Barom-					Т	enth of	Millimeti	·e.				Parts
eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for eac 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Met
443	38	52.5	54.3	56.1	57.9	59.7	61.4	63.2	65.0	66.8	68.6	
444	38	70.4	72.2	74.0	75.8	77.6	79.3	81.1	82.9	84.7	86.5	
445	38	88.3	90.1	91.9	93.7	95.5	97.2	99.0	1			
445	39						1		00.8	02.6	04.4	
446	39	06.2	08.0	09.8	11.5	13.3	15.1	16.9	18.7	20.4	22.2	
447	39	24.0	25.8	27.6	29.3	31.1	32.9	34.7	36.5	38.2	40.0	
448	39	41.8	43.6	45.4	47.1	48.9	50.7	52.5	54.3	56.0	57.8	
449	39	59.6	61.4	63.1	64.9	66.7	68.4	70.2	72.0	73.8	75.5	
450	39	77.3	79.1	80.8	82.6	84.3	86.1	87.9	89.6	91.4	93.1	
451	39	94.9	96.7	98.4	1							
451	40				00.2	02.0	03.7	05.5	07.3	09.1	10.8	
452	40	12.6	14.4	16.1	17.9	19.6	21.4	23.2	24.9	26.7	28.4	
453	40	30.2	32.0	33.7	35.5	37.2	39.0	40.8	42.5	44.3	46.0	
454	40	47.8	49.5	51.3	53.0	54.8	56.5	58.3	60.0	61.8	63.5	
455	40	65.3	67.0	68.8	70.5	72.3	74.0	75.8	77.5	79.3	81.0	1 0.2
456	40	82.8	84.5	86.3	88.0	89.8	91.5	93.2	95.0	96.7	98.5	2 0.3
457	41	00.2	01.9	03.7	05.4	07.2	08.9	10.6	12.4	14.1	15.9	3 0.5
458	41	17.6	19.3	21.1	22.8	24.6	26.3	28.0	29.8	31.5	33.3	4 0.7
459	41	35.0	36.7	38.5	40.2	41.9	43.6	45.4	47.1	48.8	50.6	5 0.9
460	41	52.3	54.0	55.8	57.5	59.2	60.9	62.7	64.4	66.1	67.9	6 1.0
461	41	69.6	71.3	73.1	74.8	76.5	78.2	80.0	81.7	83.4	85.2	7 1.9
462	41	86.9	88.6	90.3	92.1	93.8	95.5	97.2	98.9			8 1.4
462	42						1			00.7	02.3	9 1.6
463	42	04.1	05.8	07.5	09.3	11.0	12.7	14.4	16.1	17.9	19.6	
464	42	21.3	23.0	24.7	26.4	28.1	29.8	31.6	33.3	35.0	36.7	
465	42	38.4	40.1	41.8	43.5	45.2	46.9	48.7	50.4	52.1	53.8	
466	42	55.5	57.2	58.9	60.6	62.3	64.0	65.S	67.5	69.2	70.9	
467	42	72.6	74.3	76.0	77.7	79.4	81.1	82.8	84.5	86.2	87.9	
468	42	89.6	91.3	93.0	94.7	96.4	98.1	99.8				
468	43	}							01.5	03.2	04.9	
469	43	06.6	08.3	10.0	11.7	13.4	15.1	16.8	18.5	20.2	21.9	
470	43	23.6	25.3	27.0	28.7	30.4	32.0	33.7	35.4	37.1	38.8	
471	43	40.5	42.2	43.9	45.6	47.3	48.9	50.6	52.3	54.0	55.7	
472	43	57.4	59.1	60.8	62.5	64.2	65.8	67.5	69.2	70.9	72.6	
473	43	74.3	76.0	77.7	79.3	81.0	82.7	84.4	86.1	87.7	89.4	
474	43	91.1	92.8	94.5	96.1	97.8	99.5					
474	44							01.2	. 02.9	04.5	06.2	
475	44	07.9	09.6	11.2	12.9	14.6	16.2	17.9	19.6	21.3	22.9	
476	44	24.6	26.3	27.9	29.6	31.3	33.9	35.6	37.3	39.0	40.6	ĺ
477	44	41.3	43.0	44.6	46.3	48.0	49.6	51.3	53.0	54.7	56.3	
478	4.1	58.0	59.7	61.3	63.0	64.7	66.3	68.0	69.7	71.4	73.0	
479	44	74.7	76.4	78.0	79.7	81.3	83.0	84.7	86.3	88.0	89.6	
480	44	91.3	93.0	94.6	96.3	97.9	99.6		1			1
480	45							01.3	02.9	04.6	06.2	
491	45	07.9	09.5	11.2	12.8	14.5	16.1	17.7	19.4	21.0	22.7	
482	45	24.3	25.9	27.6	29.2	30.9	32.5	34.2	35.8	37.5	39.1	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac

483 to 524mm.

	,			T) (O 3		,		1		T
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres,	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
483	45	40.8	42.4	44.1	45.7	47.4	49.0	50.7	52.3	54.0	55.6	1 0.2
484	45	57.3	58.9	60.6	62.2	63.9	65 5	67.1	68.8	70.4	72.1	2 0.3
485	45	73.7	75.3	77.0	78.6	80.3	81.9	83.6	85.2	86.9	88.5	3 0.5
486	45	90.2	91.8	93.5	95.1	96.8	98.4					4 0.6
486	46							00.0	01.7	03.3	05.0	5 0.8
487	46	06.6	08.2	09.9	11.5	13.1	14.7	16.4	18.0	19.6	21.3	6 1.0
488	46	22.9	24.5	26.2	27.8	29.4	31.0	32.7	34.3	35.9	37.6	7 1.1
489	46	39.2	40.8	42.4	44.1	45.7	47.3	48.9	50.5	52.2	53.8	8 1.3
490	46	55.4	57.0	58.6	60.3	61.9	63.5	65.1	66.7	68.4	70.0	9 1.4
491	46	71.6	73.2	74.9	76.5	78.1	79.7	81.4	83.0	84.6	86.3	İ
492	46	87.9	89.5	91.1	92.8	94.4	96.0	97.6	99.2			
492	47									00.9	02.5	
493	47	04.1	05.7	07.3	08.9	10.5	12.1	13.8	15.4	17.0	18.6	
494	47	20.2	21.8	23.4	25.0	26.6	28.2	29.9	31.5	33.1	34.7	
495	47	36.3	37.9	39.5	41.1	42.7	44.3	45.9	47.5	49.1	50.7	
496	47	52.3	53.9	55.5	57.1	58.7	60.3	61.9	63.5	65.1	66.7	
497	47	68.3	69.9	71.5	73.1	74.7	76.3	78.0	79.6	81.2	82.8	
498	47	84.4	86.0	87.6	89.2	90.8	92.4	94.0	95.6	97.2	98.8	
499	48	00.4	02.0	03.6	05.2	06.8	08.3	09.9	11.5	13.1	14.7	Ì
1												
500	48	16.3	17.9	19.5	21.1	22.7	24.2	25.8	27.4	89.0	30.6	
501	48	32.2	33.S	35.4	37.0	38.6	40.1	41.7	43.3	44.9	46.5	
502	48	48.1	49.7	51.3	52.9	54.5	56.0	57.6	59.2	60.8	62.4	
503	48	64.0	65.6	67.2	68.7	70.3	71.9	73.5	75.1	76.6	78.2	
504	48	79.8	81.4	83.0	84.5	86.1	87.7	89.3	90.9	92.4	94.0	
505	48	95.6	97.2	98.7								
505	49				00.3	01.9	03.4	05.0	06.6	08.2	09.7	
506	49	11.3	12.9	14.4	16.0	17.6	19.1	20.7	22.3	23.9	25.4	
507	49	27.0	28.6	30.1	31.7	33.3	34.8	36.4	38.0	39.6	41.1	
508	49	42.7	44.3	45.8	47.4	49.0	50.5	52.1	53.7	55.3	56.8	
509	49	58.4	60.0	61.5	63.1	64.6	66.2	67.8	69.3	70.9	72.4	
510	49	74.0	75.6	77.1	78.7	80.2	81.8	83.4	84.9	86.5	88.0	
511	49	89.6	91.2	92.7	94.3	95.8	97.4	99.0		ì		
511	50								00.5	02.1	03.6	
512	50	05.2	06.7	08.3	09.8	11.4	12.9	14.5	16.0	17.6	19.1	
513	50	20.7	22.2	23.8	25.3	26.9	28.4	30.0	31.5	33.1	34.6	
514	50	36.2	37.7	39.3	40.8	42.4	43.9	45.5	46.0	48.6	50.1	
515	50	51.7	53.2	54.8	56.3	57.9	59.4	61.0	62.5	64.1	65.6	
516	50	67.2	68.7	70.3	71.8	73.4	74.9	76.4	78.0	79.5	81.1	
517	50	82.6	84.1	85.7	87.2	88.7	90.2	91.8	93.3	94.8	96.4	
518	50	97.9	99.4									
518	51			01.0	02.5	04.1	05.6	07.1	08.7	10.2	11.8	
519	51	13.3	14.8	16.4	17.9	19.4	20.9	22.5	24.0	25.5	27.1	
520	51	28.6	30.1	31.7	33.2	34.7	36.2	37.8	39.3	40.8	42.4	
521	51	43.9	45.4	47.0	48.5	50.0	51.5	53.1	54.6	56.1	57.7	
522	51	59.2	60.7	62.2	63.8	65.3	66.8	68.3	69.8	71.4	72.9	
523	51	74.4	75.9	77.5	79.0	80.5	82.0	83.6	85.1	86.6	88.2	
524	51	89.7	91.2	92.7	94.3	95.8	97.3	98.8		İ		
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm.

524 to 565mm.

Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for	ar t s eacl Imm
Milli.	Metr.	Metres.	Metres.	Metres,	Metres,	Metres	Metres.	Metres.	Metres.	Metres,	Metres.	I	Metr
524	52						l		00.3	01.9	03.4		
525	52	04.9	06.4	07.9	09.4	10.9	12.4	14.0	15.5	17.0	18.5		
526	52	20.0	21.5	23.0	24.5	26.0	27.5	29.1	30.6	32.1	33.6		
527	52	35.1	36.6	38.1	39.6	41.1	42.6	41.2	45.7	47.2	48.7		
528	52	50.2	51.7	53.2	54.7	56.2	57.7	59.3	60.8	62.3	63.S		
529	52	65.3	66.8	68.3	69.8	71.3	72.8	74.3	75.8	77.3	78.8	1	0.
530	52	80.3	81.8	83.3	84.8	86.3	87.8	89.3	90.8	92.3	93.8	2	θ.
531	52	95.3	96.8	98.3	99.8							3	0.
531	53					01.3	02.8	04.3	05.8	07.3	08.8	4	0.
532	53	10.3	11.8	13.3	14.8	16.3	17.8	19.3	20.8	22.3	23.8	5	0.
533	53	25.3	26.8	28.3	29.8	31.3	32.7	34.2	35.7	37.2	38.7	6	0.
531	53	40.2	41.7	43.2	14.7	46.2	47.6	49.1	50.6	52.1	53.6	7	1.
535	53	55.1	56.5	58.1	59.6		62.5	64.0	65.5	67.0	68.5	8	1.
536	1	70.0	71.5	73.0		61.1	i	78.9	80.4	81.8	83.3	9	
	53		1		74.4	75.9	77.4						
537	53	84.8	86.3	87.8	89.2	90.7	92.2	93.7	95.2	96.6	98.1		
538	53	99.6		02.0	0.0	0	0.0	00.5	100		120		
538	54		01.1	02.6	04.0	05.5	07.0	08.5	10.0	11.4	12.9		
539	54	14.4	15.9	17.4	18.8	20.3	21.8	23.3	24.8	26.2	27.7		
540	54	29.2	30.7	32.1	33.6	35.1	36.5	38.0	39.5	41.0	42.4		
541	54	43.9	45.4	46.8	48.3	49.8	51.2	52.7	54.2	55.7	57.1	ĺ	
542	54	58.6	60.1	61.5	63.0	64.5	66.0	67.4	68.9	70.4	71.8		
543	54	73.3	74.8	76.2	77.7	79.1	80.6	82.1	83.5	85.0	86.4		
544	54	87.9	89.4	90.8	92.3	93.7	95.2	96.7	98.1	99.6			
544	55						1				01.0		
545	55	02.5	04.0	05.4	06.9	08.4	09.8	11.3	12.8	14.3	15.7		
546	55	17.2	18.7	20.1	21.6	23.0	24.5	26.0	27.4	28.9	30.3		
547	55	31.8	33.3	34.7	36.1	37.6	39.0	40.5	41.9	43.4	41.8		
548	55	46.3	47.7	49.2	50.6	52.1	53.5	55.0	56.4	57.9	59.3		
549	55	60.8	62.2	63.7	65.1	66.6	68.0	69.5	70.9	72.4	73.8		
550	55	75.3	76.7	78.2	79.6	81.1	82.5	84.0	85.4	86.9	88.3		
551	5.5	89.8	91.2	92.7	94.1	95.6	97.0	98.4	99.9				
551	56				1		l			01.3	02.8	1	0.
552	56	04.2	05.6	07.1	08.5	10.0	11.4	12.8	14.3	15.7	17.2	2	0.
553	56	18.6	20.0	21.5	22.9	24.4	25.8	27.2	28.7	30.1	31.6	3	0.
554	56	33.0	34.4	35.9	37.3	38.8	40.2	41.6	43.1	41.5	46.0	4	0.
555	56	47.1	48.8	50.3	51.7	53.1	54.5	56.0	57.4	58.8	60.3	5	0.
556	56	61.7	63.1	61.6	66.0	67.4	68.8	70.3	71.7	73.1	74.6		0.
557	56	76.0	77.4	78.9	80.3	81.7	83.1	81.6	86.0	87.4	88.9	7	ı.
558	57	90.3	91.7	93.2	91.6	96.0	97.4	98.9	00.0			$ \mathbf{s} $	1.
558	57	30.0	""	0.5.2	51.0	33.0	374	00.0	00.3	01.7	03.2	9	
559	57	04.6	06.0	07.4	08.9	10.3	11.7	13.1	14.5	16.0	17.4		
	H	18.8	20.2	21.6	23.1	1	25.9	27.3	28.7	30.2	31.6		
560	57	1	ł	35.S	1	1	•	l .			ţ		
561	57	33.0	34.4	l .	37.3	38.7	40.1	41.5	42.9	44.4	45.8		
562	57	47.2	48.6	50.0	51.4	52.8	54 2	55.7	57.1	58.5	59.9		
563	57	61.3	62.7	61.1	65.5	66.9	68.3	69.8	71.2	72.6	74.0		
564	57	75.4	76.8	78.2	79.6	81.0	82.4	83.9	85.3	86.7	88.1		
565 ———	57	89.5 	90.9	92.4	93.8	95.2	96.6	98.0	99.4				
Barom- eter H or h	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	for 0,01	

565 to 605 mm.

	1			ı						1	1	1
B trom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
565	58									00.8	02.2	
566	58	03.6	05.0	06.4	07.8	09.2	10.6	12.1	13.5	14.9	16.3	
567	58	17.7	19.1	20.5	21.9	23.3	24.7	26.1	27.5	28.9	30.3	1
568	58	31.7	33.1	34.5	35.9	37.3	38.7	40.1	41.5	42.9	44.3	
569	58	45.7	47.1	48.5	49.9	51.3	52.7	54.1	55.5	56.9	58.3	
570	58	59.7	61.1	62.5	63.9	65.3	66.7	68.1	69.5	70.9	72.3	
571	58	73.7	75.1	76.5	77.9	79.3	80.6	82.0	83.4	84.8	86.2	
572	58	87.6	89.0	90.4	91.8	93.2	94.5	95.9	97.3	98.7		
572	59										00.1	
573	59	01.5	02.9	04.3	05.7	07.1	08.4	09.8	11.2	12.6	14.0	
574	59	15.4	16.8	18.2	19.6	21.0	22.3	23.7	25.1	26.5	27.9	
575	59	29.3	30.7	32.1	33.4	34.8	36.2	37.6	39.0	40.3	41.7	
576	59	43.1	44.5	45.9	47.2	48.6	50.0	51.4	52.8.	54.1	55.5	1 0.1
577	59	56.9	58.3	59.7	61.0	62.4	63.8	65.2	66.6	67.9	69.3	2 0.3
578	59	70.7	72.1	73.5	74.8	76.2	77.6	79.0	80.4	81.7	83.1	3 0.4
579	59	84.5	85.9	87.2	88.6	90.0	91.3	92.7	94.1	95.5	96.8	4 0.5
580	59	98.2	99.6									5 0.7
580	60			00.9	02.3	03.7	05.0	06.4	07.8	09.2	10.5	6 0.8
581	60	11.9	13.3	14.6	16.0	17.4	18.7	20.1	21.5	22.9	24.2	7 1.0
582	60	25.6	27.0	28.3	29.7	31.1	32.4	33.8	35.2	36.6	37.9	8 1.1
583	60	39.3	40.7	42.0	43.4	44.7	46.1	47.5	48.8	50.2	51.5	9 1.2
584	60	52.9	54.3	55.6	57.0	58.4	59.7	61.1	62.5	63.9	65.2	
585	60	66.6	68.0	69.3	70.7	72.0	73.4	74.8	76.1	77.5	78.8	
586	60	80.2	81.6	82.9	84.3	85.6	87.0	88.4	89.7	91.1	92.4	
587	60	93.8	95.1	96.5	97.8	99.2						
587	61						00.5	01.9	03.2	04.6	05.9	
588	61	07.3	08.6	10.0	11.3	12.7	14.0	15.4	16.7	18.1	19.4	
589	61	20.8	22.1	23.5	24.8	26.2	27.5	28.9	30.2	31.6	32.9	
590	61	34.3	35.6	37.0	38.3	39.7	41.0	42.4	43.7	45.1	46.4	
591	61	47.8	49.1	50.5	51.8	53.2	54.5	55.9	57.2	58.6	59.9	
592	61	61.3	62.6	64.0	65.3	66.7	68.0	69.3	70.7	72.0	73.4	
593	61	74.7	76.0	77.4	78.7	80.1	81.4	82.7	84.1	85.4	86.8	
594	61	88.1	89.4	90.8	92.1	93.5	94.8	96.1	97.5	98.8		
594	62	1									00.2	
595	62	01.5	02.8	04.2	05.5	06.9	08.2	09.5	10.9	12.2	13.6	
596	62	14.9	16.2	17.6	18.9	20.2	21.5	22.9	24.2	25.5	26.9	
597	62	28.2	29.5	30.9	32.2	33.6	34.9	36.2	37.6	38.9	40.3	
598	62	41.6	42.9	44.3	45.6	46.9	48.2	49.6	50.9	52.2	53.6	
599	62	54.9	56.2	57.6	58.9	60.2	61.5	62.9	64.2	65.5	66.9	
600	62	68.2	69.5	70.8	72.2	73.5	74.8	76.1	77.4	78.8	80.1	
601	62	81.4	82.7	84.1	85.4	86.7	88.0	89.4	90.7	92.0	93.4	
602	62	94.7	96.0	97.3	98.7				-	1	i	
602	63					00.0	01.3	02.6	03.9	05.3	06.6	
C)3	63	07.9	09.2	10.5	11.9	13.2	14.5	15.8	17.1	18.5	19.8	
604	63	21.1	22.4	23.7	25.1	26.4	27.7	29.0	30.3	31.7	33.0	
605	63	34.3	35.6	36.9	38.2	39.5	40.8	42.2	43.5	44.8	46.1	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.

606 to 647mm.

			1		000		47	I				
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr.
606	63	47.4	48.7	50.0	51.3	52.6	53.9	55.3	56.6	57.9	59.2	
607	63	60.5	61.8	63.1	64.5	65.8	67.1	68.4	69.7	71.1	72.4	
608	63	73.7	75.0	76.3	77.6	78.9	80.2	81.5	82.8	84.1	85.4	
609	63	86.7	88.0	89.3	90.6	91.9	93.2	94.6	95.9	97.2	98.5	
610	63	99.8				1						ĺ
610	64		01.1	02.4	03.7	05.0	06.3	07.6	08.9	10.2	11.5	1
611	61	12.8	14.1	15.4	16.7	18.0	19.3	20.7	22.0	23.3	24.6	
612	64	25.9	27.2	28.5	29.8	31.1	32.4	33.7	35.0	36.3	37.6	
613	64	38.9	40.2	41.5	42.8	44.1	45.4	46.7	48.0	49.3	50.6	
614	64	51.9	53.2	54.5	55.8	57.1	58.3	59.6	60.9	62.2	63.5	
615	6.1	64.8	66.1	67.4	68.7	70.0	71.2	72.5	73.8	75.1	76.4	l
616	64	77.7	79.0	80.3	81.6	82.9	84.2	85.5	86.8	88.1	89.4	ĺ
617	64	90.7	92.0	93.3	94.6	95.9	97.1	98.4	99.7			
617	65						1			01.0	02.3	
618	65	03.6	04.9	06.2	07.4	08.7	10.0	11.3	12.6	13.8	15.1	
619	65	16.4	17.7	19.0	20.3	21.6	22.8	24.1	25.4	26.7	28.0	
620	65	29.3	30.6	31.9	33.1	34.4	35.7	37.0	38.3	39.5	40.8	
621	65	42.1	43.4	44.7	45.9	47.2	48.5	49.8	51.1	52.3	53.6	1 0.1
622	65	54.9	56.2	57.5	58.7	60.0	61.3	62.6	63.9	65.1	66.4	2 0.2
623	65	67.7	69.0	70.3	71.5	72.8	74.1	75.4	76.7	77.9	79.2	3 0.4
624	65	80.5	81.8	83.0	84.3	85.6	86.8	88.1	89.4	90.7	91.9	4 0.5
							l					5 0.6
625	65	93.2	94.5	95.8	97.0	98.3	99.6					6 0.8
625	66						l	00.9	02.2	03.4	01.7	7 0.9
626	66	06.0	07.3	08.5	09.8	11.1	12.3	13.6	14.9	16.2	17.4	8 1.0
627	66	18.7	20.0	21.2	22.5	23.8	25.0	26.3	27.6	28.9	30.1	9 1.1
628	66	31.4	32.7	33.9	36.2	56.4	37.7	39.0	40.2	41.5	42.7	
629	66	44.0	45.3	46.5	47.8	49.1	50.3	51.6	52.9	54.2	55.4	
630	66	56.7	58.0	59.2	60.5	61.7	63.0	64.3	65.5	66.8	68.0	
631	66	69.3	70.6	71.8	73.1	74.4	75.6	76.9	78.2	79.5	80.7	
632	66	82.0	83.2	84.5	85.7	87.0	88.2	89.5	90.7	92.0	93.2	
633	66	94.5	95.8	97.0	98.3	99.5						
633	67						00.8	02.1	03.3	04.6	05.8	
634	67	07.1	08.4	09.6	10.9	12.1	13.1	14.7	15.9	17.2	18.4	
635	67	19.7	20.9	22.2	23.4	24.7	25.9	27.2	28.4	29.7	30.9	
636	67	32.2	33.4	34.7	35.9	37.2	38.4	39.7	40.9	42.2	43.4	
637	67	44.7	45.9	47.2	48.4	49.7	50.9	52.2	53.4	54.7	55.9	
638	67	57.2	58.4	59.7	60.9	62.2	63.4	64.7	65.9	67.2	68.4	
639	67	69.7	70.9	72.2	73.4	74.7	75.9	77.1	78.4	79.6	80.9	
640	67	82.1	83.3	84.6	85.8	87.1	88.3	89.6	90.8	92.1	93.3	
641	67	94.6	95.8	97.1	98.3	99.6						
641	68				1		00.S	02.0	03.3	04.5	05.8	
612	68	07.0	08.2	09.5	10.7	12.0	13.2	14.4	15.7	16.9	18.2	
643	68	19.4	20.6	21.9	23.1	24.3	25.5	26.8	28.0	29.2	30.5	
644	68	31.7	32.9	34.2	35.4	36.7	37.9	39.1	40.4	41.6	42.9	
645	68	44.1	45.3	46.6	47.8	49.0	50.2	51.5	52.7	53.9	55.2	
646	68	56.4	57.6	58.9	60.1	61.3	62.5	63.8	65.0	66.2	67.5	
647	68	68.7	69.9	71.2	72.4	73.6	74.8	76.1	77.3	78.5	79.8	
B trom- eter H or h.	N	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm

648 to 689mm.

5=	1				046	10 0	1			[i .
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres,	Metres.	Metres.	Metres.	Metres.	Metres,	Metres.	Metr.
648	68	81.0	82.2	83.5	84.7	85.9	87.1	88.4	89.6	90.8	92.1	
649	68	93.3	94.5	95.8	97.0	98.2	99.4					
649	69							00.7	01.9	03.1	04.4	į
650	69	05.6	06.8	08.0	09.3	10.5	11.7	12.9	14.1	15.4	16.6	
651	69	17.8	19.0	20.2	21.5	22.7	23.9	25.1	26.3	27.6	28.8	
652	69	30.0	31.2	32.4	33.7	34.9	36.1	37.3	38.5	39.8	41.0	
653	69	42.2	43.4	44.6	45.9	47.1	48.3	49.5	50.7	52.0	53.2	
654	69	54.4	55.6	56.8	58.1	59.3	60.5	61.7	62.9	64.2	65.4	
655	69	66.6	67.8	69.0	70.2	71.4	72.6	73.9	75.1	76.3	77.5	
656	69	78.7	79.9	81.1	82.4	83.6	84.8	86.0	87.2	88.5	89.7	
657	69	90.9	92.1	93.3	94.5	95.7	96.9	98.2	99.4			
657	70	00.0			0.5.5					00.6	01.8	
658	70	03.0	04.2	05.4	06.6	07.8	09.0	10.3	11.5	12.7	13.9	
659	70	15.1	16.3	17.5	18.7	19.9	21.1	22.4	23.6	24.8	26.0	
660	70	27.2	28.4	29.6	30.8	32.0	33.2	34.4	35.6	36.8	38.0	1 0.1
661	70	39.2	40.4	41.6	42.8	44.0	45.2	46.4	47.6	48.8	50.0	$2 \mid 0.2 \mid$
662	70	51.2	52.4	53.6	54.8	56.0	57.2	58.5	59.7	60.9	62.1	3 0,4
663	70	63.3	64.5	65.7	66.9	68.1	69.3	70.5	71.7	72.9	74.1	4 0.5
664	70	75.3	76.5	77.7	78.9	80.1	81.2	82.4	83.6	84.8	86.0	$5 \mid 0.6 \mid$
665	70	87.2	88.4	89.6	90.8	92.0	93.2	94.4	95.6	96.8	98.0	6 0.7
666	70	99.2										7 0.8
666	71		00.4	01.6	02.8	04.0	05.2	06.4	07.6	08.8	10.0	8 1.0
667	71	11.2	12.4	13.6	14.8	16.0	17.1	18.3	19.5	20.7	21.9	9 1.1
668	71	23.1	24.3	25.5	26.7	27.9	29.0	30.2	31.4	32.6	33.8	
669	71	35.0	36.2	37.4	38.6	39.8	40.9	42.1	43.3	44.5	45.7	
670	71	46.9	48.1	49.3	50.5	51.7	52.8	54.0	55.2	56.4	57.6	
671	71	58.8 70.6	60.0	61.2	62.3	63.5	64.7	65.9	67.1	68.2	69.4	
672	71	82.5	71.8	73.0	74.2	75.4	76.5	77.7	78.9	80.1	81.3	
673	71	94.3	83.7 95.5	84.9 96.7	$\begin{array}{c} 86.0 \\ 97.8 \end{array}$	$87.2 \\ 99.0$	88.4	89.6	90.8	91.9	93.1	i
674 674	71 72	94.0	93.3	30.7	97.0	99.0	00.2	01.4	02.6	03.7	04.9	
675	72	06.1	07.3	08.5	09.6	10.8	12.0	13 2	14.4	15.5	16.7	
676	72	17.9	19.1	20.3	21.4	22.6	23.8	25.0	26.2	27.3	28.5	
677	72	29.7	30.9	32.0	33.2	34.4	35.5	36.7	37.9	39.1	40.2	
678	72	41.4	42.6	43.8	44.9	46.1	47.3	48.5	49.7	50.8	52.0	1
679	72	53.2	54.4	55.5	56.7	57.9	59.0	60.2	61.4	62.6	63.7	
680	72	64.9	66.1	67.2	68.4	69.6	70.7	71.9	73.1	74.3	75.4	
681	72	76.6	77.8	78.9	80.1	81.3	82.4	83.6	84.8	86.0	87.1	1 0.1
682	72	88.3	89.5	90.6	91.8	93.0	94.1	95.3	96.5	97.7	98.8	2 0.2
683	73	00.0	01.2	02.3	03.5	04.6	05.8	07.0	08.1	09.3	10.4	3 0.3
684	73	11.6	12.8	13.9	15.1	16.2	17.4	18.6	19.7	20.9	22.0	4 0.5
685	73	23.2	24.4	25.5	26.7	27.8	29.0	30.2	31.3	32.5	33.6	5 0.6
686	73	34.8	36.0	37.1	38.3	39.4	40.6	41.8	42.9	44.1	45.2	6 0.7
687	73	46.4	47.6	48.7	49.9	51.0	52.2	53.4	54.5	55.7	56.8	7 0.8
688	73	58.0	59.2	60.3	61.5	62.6	63.8	65.0	66.1	67.3	68.4	8 0.9
689	73	69.6	70.7	71.9	73.0	74.2	75.3	76.5	77.6	78.8	79.9	9 1.1
Barom- eter H or h	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
D "						I						

690 to 730mm.

						to 7						
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0,01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Meti
690	73	81.1	82.3	83.4	84.6	85.7	86.9	88.1	89.2	90.4	91.5	
691	73	92.7	93.8	95.0	96.1	97.3	98.4	99.6				
691	74						1		00.7	01.9	03.0	
692	74	04.2	05.3	06.5	07.6	08.8	09.9	11.1	12.2	13.4	14.5	
693	74	15.7	16.8	18.0	19.1	20.3	21.4	22.6	23.7	24.9	26.0	ĺ
694	74	27.2	28.3	29.5	30.6	31.8	32.9	34.1	35.2	36.4	37.5	l
695	74	38.7	39.8	41.0	42.1	43.3	44.4	45.5	46.7	47.8	49.0	1
696	74	50.1	51.2	52.4	53.5	54.7	55.S	56.9	58.1	59.2	60.4	
697	74	61.5	62.6	63.8	64.9	66.1	67.2	68.3	69.5	70.6	71.8	
698	74	72.9	74.0	75.2	76.3	77.5	78.6	79.7	80.9	82.0	83.2	
699	74	84.3	85.4	86.6	87.7	88.9	90.0	91.1	92.3	93.4	94.6	
700	74	95.7	96.8	98.0	99.1	ŀ						
700	75					00.3	01.4	02.5	03.7	04.8	06.0	
701	75	07.1	08.2	09.4	10.5	11.6	12.7	13.9	15.0	16.1	17.3	
702	75	18.4	19.5	20.7	21.8	23.0	24.1	25.2	26.4	27.5	28.7	İ
703	75	29.8	30.9	32.1	33.2	34.3	35.4	36.6	37.7	38.8	40.0	
704	75	41.1	42.2	43.4	44.5	45.6	46.7	47.9	49.0	50.1	51.3	
705	75	52.4	53.5	54.7	55.8	56.9	58.0	59.2	60.3	61.4	62.6	
706	75	63.7	64.8	66.0	67.1	68.2	69.3	70.5	71.6	72.7	73.9	
707	75	75.0	76.1	77.2	78.4	79.5	80.6	81.7	82.8	84.0	85.1	
708	75	86.2	87.3	88.5	89.6	90.7	91.8	93.0	94.1	95.2	96.4	
709	75	97.5	98.6	99.7	1	İ	1					
709	76			ļ	00.9	02.0	03.1	04.2	05.3	06.5	07.6	
710	76	08.7	09.8	10.9	12.1	13.2	14.3	15.4	16 5	17.7	18.8	
711	76	19.9	21.0	22.1	23.3	24.4	25.5	26.6	27.7	28.9	30.0	
712	76	31.1	32.2	33.3	34.4	35.5	36.6	37.8	38.9	40.0	41.1	1 0.1
713	76	42.2	43.3	44.4	45.6	46.7	47.S	48.9	50.0	51.2	52.3	2 0.3
714	76	53.4	54.5	55.6	56.8	57.9	59.0	60.1	61.2	62.4	63.5	3 0.3
715	76	64.6	65.7	66.8	67.9	69.0	70.1	71.3	72.4	73.5	71.6	4 0
716	76	75.7	76.8	77.9	79.0	80.1	81.2	82.4	83.5	84.6	85 7	5 0.3
717	76	86.8	87.9	89.0	90.1	91.2	92.3	93.5	94.6	95.7	96.8	6 0.7
718	76	97.9	99.0				l	1				7 0.8
718	77			00.1	01.2	02.3	03.4	04.6	05.7	06.8	07.9	8 0.9
719	77	09.0	10.1	11.2	12.3	13.4	14.5	15.7	16.8	17.9	19.0	9 1.0
720	77	20.1	21.2	22.3	23.4	24.5	25.6	26.7	27.8	28.9	30.0	
721	77	31.1	32.2	33.3	31.4	35.5	36.6	37.7	38.8	39.9	41.0	
722	77	42.1	43.2	41.3	45.4	46.5	47.6	48.7	49.8	50.9	52.0	
723	77	53.1	54.2	55.3	56.4	57.5	58.6	59.8	60.9	62.0	63.1	
724	77	64.2	65.3	66.4	67.5	68.6	69.6	70.7	71.8	72.9	71.0	
725	77	75.1	76.2	77.3	78.4	79.5	80.6	81.7	82.8	83.9	85.0	
726	77	86.1	87.2	88.3	89.4	90.5	91.6	92.7	93.8	94.9	96.0	
727	77	97.1	98.2	99.3								
727	78			1	00.4	01.5	02.5	03.6	04.7	05.8	06.9	
728	78	08.0	09.1	10.2	11.3	12.4	13 5	14.6	15.7	16.8	17.9	
729	78	19.0	20.1	21.2	22.3	23.4	24.4	25.5	26.6	27.7	28.8	
730	78	29.9	31.0	32.1	33.3	34.3	35.3	36.4	37.5	38.6	39.7	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01 mm

731 to 770mm.

			7									
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for eac 0.01mm
Milli.	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
731	78	40.8	41.9	43.0	44.1	45.2	46.2	47.3	48.4	49.5	50.6	
732	78	51.7	52.8	53.9	54.9	56.0	57.0	58.2	59.3	60.3	61.4	1
733	78	62.5	63.6	64.7	65.8	66.9	67.9	69.0	70.1	71.2	72.3	
734	78	73.4	74.5	75.6	76.6	77.7	78.8	79.9	81.0	82.0	83.1	
735	78	84.2	85.3	86.4	87.5	88.6	89.6	90.7	91.8	92.9	94.0	İ
736	78	95.1	96.2	97.3	98.3	99.4						
736	79					1	00.5	01.6	02.7	03.7	04.8	}
737	79	05.9	07.0	08.1	09.1	10.2	11.3	12.4	13.5	14.5	15.6	
738	79	16.7	17.8	18.9	.19.9	21.0	22.1	23.2	24.3	25.3	26.4	
739	79	27.5	28.6	29.6	30.7	31.8	32.8	33.9	35.0	36.1	37.1	
				_								
740	79	38.2	39.3	40.4	41.4	42.5	43.6	44.7	45.8	46.8	47.9	
741	79	49.0	50.1	51.1	52.2	53.3	54.3	55.4	56.5	57.6	58.6	1
742	79	59.7	60.8	61.8	62.9	64.0	65.0	66.1	67.2	68.3	69.3	
743	79	70.4	71.5	72.6	73.6	74.7	75.8	76.9	78.0	79.0	80.1	
714	79	81.2	82.3	83.3	84.4	85.5	86.5	87.6	88.7	89.8	90.8	1
745	79	91.9	93.0	94.0	95.1	96.1	97.2	98.3	99.3			
745	80	00.5	00.0	0.4.0		22.0	0-0		- 0.0	00.4	01.4	
746	80	02.5	03.6	04.6	05.7	06.8	07.8	08.9	10.0	11.1	12.3	
747	80	13.2	14.3	15.3	16.4	17.4	18.5	19.6	20.6	21.7	22.7	
748	80	23.8	24.9	25.9	27.0	28.0	29.1	30.2	31.2	32.3	33.3	
749	80	34.4	35.5	36.5	37.6	38.7	39.7	40.8	41.9	43.0	44.0	
		45.3	40.0	47.0			-0-					
750	80	45.1	46.2	47.3	48.4	49.4	50.5	51.6	52.6	53.7	54.7	
751	80	55.7	56.8	57.8	58.9	59.9	61.0	62.1	63.1	64.2	65.2	
752	80	66.3	67.4	68.4	69.5	70.5	71.6	72.7	73.7	74.8	75.8	
753	80	76.9	78.0	79.0	80.1	81.1	82.2	83.3	84.3	85.4	86.4	
754	80	87.5 98.0	88.5	89.6	90.6	91.7	92.7	93.8	94.8	95.9	96.9	1 0.1
755	80	95.0	99.1	00.1	01.0	00.0	00.0	0.4	05.4	00		2 0.2
755	81	08.6	09.6	10.7	01.2	02.2	03.3	04.4	05.4	06.5	07.5	3 0.3
756	81	19.1	20.1	21.2	$11.7 \\ 22.2$	$12.8 \\ 23.3$	13.8 24.3	$\frac{14.9}{25.4}$	15.9	17.0	18.0	4 0.4
757	81	29.6	30.6	31.7	32.7	33.8	34.8	35.9	26.4 36.9	27.5 38.0	28.5	5 0.5
758 759	81	40.1	41.1	42.2	43.2	44.3	45.3	46.4		48.5	39.0	$\begin{array}{c c} 6 & 0.6 \\ \hline \end{array}$
155	01	40.1	41.1	42.0	40.4	44.0	40.0	40.4	47.4	40.0	49.5	7 0.7
760	sı	50.6	51.6	52.7	53.7	54.8	55.8	56.9	57.9	59.0	60.0	8 0.8
761	81	61.1	62.1	63.2	64.2	65.3	66.3	67.3	68.4	69.4	70.5	9 0.9
761	81	71.5	72.5	73.6	74.6	75.7	76.7	77.8	78.8	79.9	80.9	
763	81	82.0	83.0	84.1	85.1	86.2	87.2	88.2	89.3	90.3	91.4	
764	81	92.4	93.4	94.5	95.5	96.6	97.6	98.6	99.7	30.0	J1-1	
764	82		33.4		30.0	٠٠.٠		30.0		00.7	01.8	
765	82	02.8	03.8	04.9	05.9	07.0	08.0	09.0	10.1	11.1	12.2	
766	82	13.2	14.2	15.3	16.3	17.4	18.4	19.4	20.5	21.5	22.6	
767	82	23.6	24.6	25.7	26.7	27.8	28.8	29.8	30.9	31.9	33.0	
768	82	34.0	35.0	36.1	37.1	38.2	39.2	40.2	41.3	42.3	43.4	
769	82	44.4	45.4	46.5	47.5	48.5	49.5	50.6	51.6	52.6	53.7	
770	82	54.7	55.7	56.8	57.8	58.8	59.8	60.9	61.9	62.9	64.0	
Barom- eter H or h.	N.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01mm.
D						28						

771 to \$10mm.

Barometer H or h.	N.			i -		1		1	1	1	1	
		0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each 0.01 mm
	Metr.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metr
771	82	65.0	66.0	67.1	68.1	69.2	70.2	71.2	72.3	73.3	74.4	
772	82	75.4	76.4	77.5	78.5	79.5	80.5	81.6	82.6	83.6	84.7	
773	82	85.7	86.7	87.8	88.8	89.8	90.8	91.9	92.9	93.9	95.0	
774	82	96.0	97.0	98.0	99.1		}	1	1	ĺ		
774	83	22.2				00.1	01.1	02.1	03.1	04.2	05.2	
775	83	06.2	07.2	08.3	09.3	10.3	11.3	12.4	13.4	14.4	15.5	
776	83	16.5	17.5	18.5	19.6	20.6	21.6	22.6	23.6	24.7	25.7	ĺ
777	83	26.7	27.7	28.8	29.8	30.8	31.8	32.9	33.9	34.9	36.0	
778	83	37.0	38.0	39.0	40.1	41.1	42.1	43.1	44.1	45.2	46.2	
779	83	47.2	48.2	49.2	50.3	51.3	52.3	53.3	54.3	55.4	56.4	
780	83	57.4	58.4	59.4	60.5	61.5	62.5	63.5	64.5	65.6	66.6	
781	83	67.6	68.6	69.6	70.7	71.7	72.7	73.7	74.7	75.8	76.8	
782	83	77.8	78.8	79.8	80.9	81.9	82.9	83.9	84.9	86.0	87.0	
783	83	88.0	89.0	90.0	91.1	92.1	93.1	94.1	95.1	96.2	97.2	
784	83	98.2	99.2									
784	84			00.2	01.2	02.2	03.2	04.3	05.3	06.3	07.3	
785	84	08.3	09.3	10.3	11.4	12.4	13.4	14.4	15.4	16.5	17.5	
786	84	18.5	19.5	20.5	21.5	22.5	23.5	24.6	25.6	26.6	27.6	
787	84	28.6	29.6	30.6	31.6	32.6	33.6	34.7	35.7	36.7	37.7	
788	84	38.7	39.7	40.7	41.7	42.7	43.7	44.8	45.8	46.8	47.8	
789	84	48.8	49.8	50.8	51.8	52.8	53.8	54.9	55.9	56.9	57.9	
790	84	58.9	59.9	60.9	61.9	62.9	63.9	65.0	66.0	67.0	68.0	
791	84	68.9	69.9	70.9	71.9	72.9	73.9	75.0	76.0	77.0	78.0	1 0.1
792	84	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	2 0.2
793	84	89.0	90.0	91.0	92.0	93.0	94.0	95.1	96.1	97.1	98.1	3 0.3
794	84	99.1										4 0.4
794	85		00.1	01.1	02.1	03.1	04.1	05.1	06.1	07.1	08.1	5 0.5
795	85	09.1	10.1	11.1	12.1	13.1	14.1	15.1	16.1	17.1	18.1	6 0.6
796	85	19.1	20.1	21.1	22.1	23.1	24.1	25.1	26.1	27.1	28.1	7 0.7
797	85	29.1	30.1	31.1	32.1	33.1	34.1	35.1	36.1	37.1	38.1	8 0.8
798	85	39.1	40.1	41.1	42.1	43.1	44.1	45.1	46.1	47.1	48.1	9 0.9
799	85	49.1	50.1	51.1	52.0	53.0	54.1	55.0	56.0	57.0	58.0	
800	85	59.0	60.0	61.0	62.0	63.0	64.0	65.0	66.0	67.0	68.0	
801	85	69.0	70.0	70.9	71.9	72.9	73.9	74.9	75.9	76.9	77.9	
802	85	78.9	79.9	80.9	81.9	82.9	83.9	84.9	85.8	86.8	87.8	
803	85	88.8	89.8	90.8	91.8	92.8	93.8	94.8	95.8	96.7	97.7	
804	85	98.7	99.7	- 1	-			-				
804	86	- 1		00.7	01.7	02.7	03.7	04.7	05.7	06.6	07.6	
805	86	08.6	09.6	10.6	11.6	12.6	13.6	14.6	15.5	16.5	17.5	
806	86	18.5	19.5	20.5	21.5	22.5	23.4	24.4	25.4	26.4	27.4	
807	86	28.4	29.4	30.4	31.3	32.3	33.3	34.3	35.3	36.3	37.3	
808	86	38.3	39.2	40.2	41.2	42.2	43.2	44.2	45.1	46.1	47.1	
809	86	48.1	49.1	50.1	51.1	52.0	53.0	54.0	55.0	56.0	57.0	
810	86	57.9	58.9	59.9	60.9	61.9	62.8	63.8	64.8	65.8	66.8	
Barom- eter		0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Parts for each

TABLE II. Correction for Difference of Temperature of Attached Thermometers.

Temperature of Barometers at Station { Upper = T' Lower = T.

						(LOWEL -			
T' - T	Correct	T' - T	Correct.	T' - T	Correct.	T' — T	Correct.	T' - T	Correct.
Centig.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.	Centigrade.	Metres.
0.0	0.0	8.0	10.3	16.0	20.6	24.0	30.9	32.0	41.3
0.0	0.3	8.2	10.6	16.2	20.9	24.0	31.2	32.2	41.5
0.1	0.5	8.4	10.8	16.4	21.1	24.4	31.5	32.4	41.8
0.6	0.8	8.6	11.1	16.6	21.4	24.6	31.7	32.6	42.0
0.8	1.0	8.8	11.3	16.8	21.7	24.8	32.0	32.8	42.3
1.0	1.3	9.0	11.6	17.0	21.9	25.0	32.2	33.0	42.5
1.2	1.5	9.2	11.9	17.2	22.2	25.2	32.5	33.2	42.8
1.4	1.8	9.4	12.1	17.4	22.4	25.4	32.7	33.4	43.1
1.6	2.1	9.6	12.4	17.6	22.7	25.6	33.0	33.6	43.3
1.8	2.3	9.8	12.6	17.8	22.9	25.8	33.3	33.8	43.6
2.0	2.6	10.0	12.9	18.0	23.2	26.0	33.5	34.0	43.8
2.2	2.8	10.2	13.1	18.2	23.5	26.2	33.8	34.2	44.1
2.4	3.1	10.4	13.4	18.4	23.7	26.4	34.0	34.4	44.3
2.6	3.4	10.6	13.7	18.6	24.0	26.6	34.3	34.6	44.6
2.8	3.6	10.8	13.9	18.8	24.2	26.8	34.6	34.8	44.9
3.0	3.9	11.0	14.2	19.0	24.5	27.0	34.8	35.0	45.1
3.2	4.1	11.2	14.5	19.2	24.8	27.2	35.1	35.2	45.4
3.4	4.4	11.4	14.7	19.4	25.0	27.4	35.3	35.4	45.6
3.6	4.6	11.6	15.0	19.6	25.3	27.6	35.6	35.6	45.9
3.8	4.9	11.8	15.2	19.8	25.5	27.8	35.8	35.8	46.2
4 0	5.2	12.0	15.5	20.0	25.8	28.0	36.1	36.0	46.4
4.2	5.4	12.2	15.8	20.2	26.0	28.2	36.4	36.2	46.7
4.4	5.7	12.4	16.0	20.4	26.3	28.4	36.6	36.4	46.9
4.6	5.9	12.6	16.3	20.6	26.6	28.6	36.9	36.6	47.2
4.8	6.2	12.8	16.5	20.8	26.8	28.8	37.1	36.8	47.4
5.0	6.4	13.0	16.8	21.0	27.1	29.0	37.4	37.0	47.7
5.2	6.7	13.2	17.0	21.2	27.3	29.2	37.6	37.2	48.0
5.4	7.0	13.4	17.3	21.4	27.6	29.4	37.9	37.4	48.2
5.6	7.2	13.6	17.5	21.6	27.8	29.6	38.2	37.6	48.5
58	7.5	13.8	17.8	21.8	28.1	29.8	38.4	37.8	48.7
6.0	7.7	14.0	18.0	22.0	28.4	30.0	38.7	38.0	49.0
6.2	8.0	14.2	18.3	22.2	28.6	30.2	38.9	38.2	49.2
6.4	8.3	14.4	18.5	22.4	28.9	30.4	39.2	38.4	49.5
6.6	8.5	14.6	18.8	22.6	29.1	30.6	39.5	38.6	49.8
6.8	8.8	14.8	19.0	22.8	29.4	30.8	39.7	38.8	50.0
7.0	9.0	15.0	19.3	23.0	29.7	31.0	40.0	39.0	50.3
7.2	9.3	15.2	19.6	23.2	29.9	31.2	40.2	39.2	50.5
7.4	9.5	15.4	198	23.4	30.2	31.4	40.5	39.4	50.8
7.6	9.8	15.6	20.1	23.6	30.4	31.6	40.7	39.6	51.1
7.8	10.1	15.8	20.3	23.8	30.7	31.8	41.0	39.8	51.3
8.0	10.3	16.0	20.6	24.0	30.9	32.0	41.3	40.0	51 6

This Table supposes the scale to be of *brass* from the top to the cistern. If it were of glass or of wood, the argument T' — T ought to be diminished at the ratio of 54 to 62.

In computing by the formula of Laplace, we begin by reducing the barometers to the same temperature by means of the following formula: $II = h' + h' \left(\frac{T' - T}{6196}\right)$. Table II. saves this trouble, and gives, in metres, the correction due to the difference of temperature of the barometers.

TABLE III. CORRECTION FOR DECREASE OF GRAVITATION IN LATITUDE.

 $\beta = (0.0028371 \text{ cosin. 2 L}). (\Lambda + \alpha + \beta).$

The Argument is the Mean Latitude between the two Stations.

rude.				Co	rrection, in	metres, for			
Subtr'ct	1000	2000	3000	4000	5000	6000	7000	8000	9000
90	9.0	57	9.5	11.9	110	17.0	10.0	99.7	25.7
I.		l 1				l	1		25.6
					1	1	ł		25.5
		1				1			25.4
						I	1		ł
			1			1			25.3 25.1
1			1			1			25.1
					1	1			24.8
		1				l			
1		1				l			24.5
						l			24.3 24.0
			, i						
I II						I			23.7
l il		1			1	I .			23.3
									22.9
11			. 1						22.5
1 18			1						22.1
11									21.6
11								1	21.2
									20.7
11					1				20.1
			1						19.6
11							1		19.0
11			1						18.4
	1		- 1					1	17.7
li li									17.1
								1	16.4
									15.7
	1		1						15.0
l II	1								14.3
71	- 1		1			1 1			13.5
- 11									12.8
- 18	1				1				12.0
- 11								- 1	11.2
- 1					1			4	10.4
								1	9.6
- 11									8.7
- (1	1	- 1							7.9
ll ll	1								7.0
- 1			t t						6.2
li li	- 1	1	1						5.3
- 11	- 1	1							4.4
l)		I							3.5
- 1)	1								2.7
- (J							1.8
- (1									0.9
45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	Stion. Subtrict 90 89 88 87 86 85 84 83 82 81 80 79 78 77 76 75 74 73 72 71 70 69 68 67 66 65 64 63 62 61 60 59 58 57 56 55 54 53 52 51 50 49 48 47 46 45	stion. Subtr'et 90 2.8 89 2.8 89 2.8 86 2.8 85 2.8 85 2.8 85 2.8 85 2.7 80 2.7 81 2.7 80 2.7 80 2.7 81 2.7 80 2.7 79 2.6 78 2.5 76 2.5 75 2.5 74 73 2.4 72 2.3 71 2.2 70 2.2 69 2.1 68 2.0 67 2.0 66 1.9 65 1.8 64 1.7 63 1.7 62 1.6 61 1.5 60 1.4 59 1.3 58 1.2 57 1.1 56 1.1 55 1.0 54 0.9 53 0.8 52 0.7 51 0.6 50 0.5 49 0.4 48 0.3 47 0.2 46 0.1	ction. Subtr'et 90 2.8 5.7 89 2.8 5.7 87 2.8 5.6 86 2.8 5.6 85 2.8 5.6 84 2.8 5.5 83 2.7 5.5 82 2.7 5.4 81 2.7 5.4 80 2.7 5.3 79 2.6 5.2 78 2.5 5.1 76 2.5 5.1 76 2.5 5.1 76 2.5 5.1 76 2.5 77 2.5 5.1 76 2.5 4.9 74 2.4 4.8 73 2.4 4.7 72 2.3 4.6 71 2.2 4.3 69 2.1 4.2 68 2.0 4.1 67 2.0 3.9 66 1.9 3.8 65 1.8 3.6 64 1.7 3.3 62 1.6 3.2 61 1.5 3.0 60 1.4 2.8 59 1.3 57 1.1 2.3 56 1.1 55 1.0 1.9 54 0.9 1.7 53 0.8 1.6 52 0.7 1.4 54 0.9 1.7 53 0.8 1.6 52 0.7 1.4 54 0.9 1.7 53 0.8 1.6 52 0.7 1.4 54 0.9 0.4 48 0.3 0.6 47 0.2 0.4 48 0.3 0.6 47 0.2 0.4 48 0.3 0.6 47 0.2 0.4 48 0.3 0.6 47 0.2 0.4 48 0.3 0.6	ction. Subtreet 1000 2000 3000 90 2.8 5.7 8.5 89 2.8 5.7 8.5 87 2.8 5.6 8.5 86 2.8 5.6 8.4 85 2.8 5.6 8.4 84 2.8 5.5 8.3 83 2.7 5.5 8.2 82 2.7 5.4 8.2 81 2.7 5.4 8.1 80 2.7 5.3 8.0 79 2.6 5.2 7.9 78 2.6 5.2 7.8 77 2.5 5.1 7.6 76 2.5 5.0 7.5 75 2.5 4.9 7.4 74 2.4 4.8 7.2 73 2.4 4.7 7.0 72 2.3 4.6 6.9 71 2.2 4.5	oction. Subtret. 1000 2000 3000 4000 90 2.8 5.7 8.5 11.3 89 2.8 5.7 8.5 11.3 88 2.8 5.7 8.5 11.3 87 2.8 5.6 8.5 11.3 86 2.8 5.6 8.4 11.2 85 2.8 5.6 8.4 11.2 84 2.8 5.5 8.3 11.1 83 2.7 5.5 8.2 11.0 82 2.7 5.4 8.2 10.9 81 2.7 5.4 8.2 10.9 81 2.7 5.3 8.0 10.7 79 2.6 5.2 7.9 10.5 78 2.6 5.2 7.9 10.5 78 2.6 5.2 7.8 10.4 77 2.5 5.1 7.6 10.2 76 <td>ction. Subtr'et 1000 2000 3000 4000 5000 90 2.8 5.7 8.5 11.3 14.2 89 2.8 5.7 8.5 11.3 14.1 87 2.8 5.6 8.5 11.3 14.1 86 2.8 5.6 8.4 11.2 14.0 85 2.8 5.6 8.4 11.2 14.0 84 2.8 5.5 8.3 11.1 13.9 83 2.7 5.5 8.2 11.0 13.8 82 2.7 5.4 8.2 10.9 13.6 81 2.7 5.4 8.2 10.9 13.6 81 2.7 5.4 8.2 10.9 13.6 81 2.7 5.3 8.0 10.7 13.3 79 2.6 5.2 7.9 10.5 13.1 78 2.6 5.2 7.9 10.5 13.1</td> <td> Subtr'et</td> <td> Stion. </td> <td> Stion. </td>	ction. Subtr'et 1000 2000 3000 4000 5000 90 2.8 5.7 8.5 11.3 14.2 89 2.8 5.7 8.5 11.3 14.1 87 2.8 5.6 8.5 11.3 14.1 86 2.8 5.6 8.4 11.2 14.0 85 2.8 5.6 8.4 11.2 14.0 84 2.8 5.5 8.3 11.1 13.9 83 2.7 5.5 8.2 11.0 13.8 82 2.7 5.4 8.2 10.9 13.6 81 2.7 5.4 8.2 10.9 13.6 81 2.7 5.4 8.2 10.9 13.6 81 2.7 5.3 8.0 10.7 13.3 79 2.6 5.2 7.9 10.5 13.1 78 2.6 5.2 7.9 10.5 13.1	Subtr'et	Stion.	Stion.

TABLE IV. CORRECTION FOR DECREASE OF GRAVITATION ON A VERTICAL LINE.

$$\delta = \left(\frac{A + \alpha + \beta + \nu + 15296}{6366200}\right) \times A \left(+ \alpha + \beta + \nu \right).$$

Argument = $(A + \alpha + \beta + \nu)$.

Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond. Correction Positive.	Approximate Difference of Level.	Correspond Correction Positive.
Metres.	Metres,	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
100	0.2	2100	6.0	4100	12.9	6100	21.1
200	0.5	2200	6.3	4200	13.3	6200	21.6
300	0.8	2300	6.6	4300	13.7	6300	22.0
400	1.0	2400	6.9	4400	14.1	6400	22.5
500	1.3	2500	7.3	4500	14.5	6500	22.9
il i							
600	1.6	2600	7.6	4600	14.9	6600	23.4
700	1.8	2700	7.9	4700	15.3	6700	23.9
800	2.1	2800	8.3	4800	15.7	6800	24.3
900	2.4	2900	8.6	4900	16.1	6900	24.8
1000	2.7	3000	8.9	5000	16.5	7000	25.3
1						Ì	
1100	2.9	3100	9.3	5100	16.9	7100	25.7
1200	3.2	3200	9.6	5200	17.3	7200	26.2
1300	3.5	3300	10.0	5300	17.7	7300	26.7
1400	3.8	3400	10.3	5400	18.1	7400	27.2
1500	4.1	3500	10.7	5500	18.5	7500	27.7
1							
1600	4.4	3600	11.1	5600	19.0	7600	28.1
1700	4.7	3700	11.4	5700	19.4	7700	28.6
1800	5.0	3800	11.8	5800	19.8	7800	29.1
1900	5.3	3900	12.2	5900	20.3	7900	29.6
2000	5.6	4000	12.5	6000	20.7	8000	30.1
]						

TABLE V. Correction for the Elevation of the Lower Station above Ocean. $Argument = Height \ of \ Barometer \ at \ Lower \ Station.$

		He	eight of Baron	neter at Lowe	er Station in	Millimetres.		
Difference of Level.	400	450	500	550	600	650	700	750
Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
1000	1.7	1.4	1.1	0.9	0.6	0.4	0.2	0.0
2000	3.4	2.8	2.2	1.7	1.3	0.8	0.4	0.1
3000	5.1	4.2	3.3	2.6	1.9	1.3	0.7	0.1
4000	6.8	5.6	4.4	3.4	2.5	1.7	0.9	0.1
5000	8.5	6.9	5.5	4.3	3.1	2.1	1.1	0.1
6000	10.3	8.3	6.7	5.2	3.8	2.5	1.3	0.2
7000	12.0	9.7	7.8	6.0	4.4	2.9	1.5	0.2
8000	13.7	11.1	8.9	6.9	5.0	3.4	1.8	0.2
9000	15.4	12.5	10.0	7.7	5.7	3.8	2.0	0.3

II.

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

BY A. GUYOT.

Tables which, like the preceding ones by Delcros, in metrical measures, are sufficiently extensive to save the necessity of interpolations, relieve the computer of most of his trouble, and considerably reduce the chances of error in the computations. They thus render to science itself a real service, by inducing observers to determine a larger number of points, and to secure the accuracy of the results by repeating their observations at the same point in various atmospheric circumstances, both of which they can do without fear of being overwhelmed by the labor of the computation.

Similar tables are here offered to the observers who use instruments graduated to English measures. Like those of Delcros, the new tables are based on Laplace's formula, with a slight modification of only one constant. They dispense with the use of logarithms, and give the differences of level corresponding to every thousandth of an inch from 12 to 31 inches by means of the simplest arithmetical operations, so that the data being prepared and corrected, the computation of an elevation takes but a few minutes, and is done with scarcely any chance of error.

Laplace's formula and constants were adopted for the computation of the tables in preference to others found in the following sets for reasons which a few words will explain.

It has been remarked, page 9, that, in consequence of Laplace's constants having been retained in Gauss's, Schmidt's, and Baily's formulæ, they all give similar results; but that Bessel's formula differs in separating the correction due to the moisture of the air from that due to its temperature, while in Laplace's, and in the formulæ just mentioned, both are united. To introduce a separate correction for the expansion of aqueous vapor is, in the writer's view, a doubtful improvement. The laws of the distribution and transmission of moisture through the atmosphere are too little known, and its amount, especially in mountain regions, is too variable, and depends too much upon local winds and local condensation, to allow a reasonable hope of obtaining the mean humidity of the layer of air between the two stations by means of hygrometrical observations taken at each of them. These doubts are confirmed by the experience of the author and of many other observers, which shows that, on an average, Laplace's method works not only as well as the other, but more uniformly well. At any rate, the gain, if there is any, is not clear enough to compensate for the undesirable complication of the formula.

Though the several co-efficients of Laplace's formula need perhaps to be modified according to more recent and probably more accurate determinations of the physical constants on which they depend, as has been proposed by Plantamour, E. Ritter, and lately by the writer himself in a paper read before the American Association for the Advancement of Science at their meeting in Montreal, they have been retained in preparing the following tables, partly because it was found that the errors due to

the various co-efficients nearly compensate each other; partly on the ground that, until a severe test, by means of actual comparative measurements made for the purpose, has shown the expediency of these modifications, it seemed desirable to adhere to the old constants, and thus to preserve a uniformity in the results with the tables of Oltmans, Delcros, Gauss, Baily, and others, which have already been extensively used. The substitution of the co-efficient 0.00260, expressing, according to Schmidt's computation (Mathem. und Physic. Geogr., II. p. 202), the variation of gravity in latitude, for the value 0.002837, does not sensibly alter the altitudes obtained.

The close agreement of the determinations furnished by Laplace's formula, in barometrical measurements carefully conducted, made in favorable circumstances, and during the warm season, with those obtained from repeated trigonometrical observations, or by the spirit-level, strongly testifies in favor of its general correctness. A few striking examples will suffice to show it.

The altitude of Mont Blanc, measured by the barometer, by MM. Bravais and Martins, on the 29th of August, 1844, and computed by Delcros, by means of nine corresponding stations situated on all sides of the mountain (see Annuaire Météorologique de France, for 1851, p. 274), was found to be 4810 metres. The altitude of the same point, being the mean of seven of the most elaborate and reliable geodetic measurements, which cost nearly twenty years of labor, is 4809.6 metres.

For smaller elevations the formula seems to answer equally well.

The barometrical measurement of Mount Washington, in New Hampshire, by the author, on the 8th and 9th of August, 1851, gave, by Deleros's Tables, for the mean of eight observations, taken at different hours of the day, 5466.7 English feet above Gorham, N. H., 6285.7 above high tide, and 6291.7 feet above the mean level of the ocean in Portland harbor. In August, 1852, W. A. Goodwin, Civil Engineer, starting from Gorham Railroad Station, found, by the spirit-level, Mount Washington to be 6285.5 feet above mean tide. In September, 1853, Captain T. J. Cram, of the Topographical Engineers, executed, in behalf of the Coast Survey, a careful measurement with the spirit-level, on the same line, for the purpose of testing the various methods of measuring altitudes, and found Mount Washington to be 6293 English feet above the mean level of the ocean.

In lower latitudes the formula showed equally good results. By a barometrical measurement in July, 1856, the altitude of the highest peak of the Black Mountain, North Carolina, about Lat. 36°, was found by the author to be 6701 English feet; and that of the highest Mountain House 5248 feet. In September, 1857, Major T. C. Turner, Chief Engineer of the Morganton Railroad, ran a line of levels from the same point which was used as the lower station for the barometrical measurement, to the top of the highest peak, and found its altitude to be 6711 English feet, and that of the Mountain House 5246 feet. Other points on the line agreed equally well.

Such an agreement, in so considerable elevations, is all that can be desired.

These figures show conclusively, that, when the errors which may arise from the great variability of the data furnished by the instruments have been removed by a repetition, in various states of the atmosphere, and by a proper combination of simultaneous observations at stations not too distant from each other, those which remain and may be attributed to the formula cannot be considerable. But, on the other

hand, we have no right to expect such results from single observations, taken, perhaps, in unsettled weather, without paying any regard to the time of the day at which they were made, to the distance or the non-simultaneity of the corresponding observations, or to other unfavorable circumstances. It is too well known that in such cases large errors may and do actually occur; but for these the formula ought not to be held responsible.

ARRANGEMENT OF THE TABLES.

If we call

 $h = \text{the observed height of the barometer} \atop \tau = \text{the temperature of the barometer} \atop t = \text{the temperature of the air}$ at the lower station;

h'= the observed height of the barometer t'= the temperature of the barometer t'= the temperature of the air

If we make, further,

 $Z=\,$ the difference of level between the two barometers ;

L = the mean latitude between the two stations;

H= the height of the barometer at the upper station reduced to the temperature of the barometer at the lower station; or,

 $H = h' \{1 + 0.00008967 (\tau - \tau')\};$

The expansion of the mercurial column, measured by a brass scale, for 1° Fahrenheit = 0.00008967;

The increase of gravity from the equator to the poles = 0.00520048, or 0.00260 to the 45th degree of latitude;

The earth's mean radius = 20,886,860 English feet;

Then, Laplace's formula, reduced to English measures, reads as follows:

$$Z = \log \frac{h}{H} \times 60158.6 \text{ English feet} \left\{ egin{aligned} \left(1 + rac{t + t' - 64}{900}
ight). \\ \left(1 + 0.00260\cos 2 L
ight). \\ \left(1 + rac{z + 52252}{20886860} + rac{h}{10443130}
ight). \end{aligned}
ight.$$

Table I. gives, in English feet, the value of $\log H$ or $h \times 60158.6$ for every hundredth of an inch, from 12 to 31 inches in the barometer, together with the value of the additional thousandths, in a separate column. These values have been diminished by a constant, which does not alter the difference required.

Table II. gives the correction 2.343 feet \times $(\tau - \tau')$ for the difference of the temperatures of the barometers at the two stations, or $\tau - \tau'$. As the temperature at the upper station is generally lower, $\tau - \tau'$ is usually positive, and the correction negative. It becomes positive when the temperature of the upper barometer is higher, and $\tau - \tau'$ negative. When the heights of the barometers have been reduced to the same temperature, or to the freezing point, this table will not be used.

Table IV. shows the correction $D'\frac{z+52252}{20886860}$ to be applied to the approximate altitude for the decrease of gravity on a vertical acting on the density of the mercurial column. It is always additive.

Table V. furnishes the small correction $\frac{h}{10443430}$ for the decrease of gravity on a vertical acting on the density of the air; the height of the barometer h at the lower station representing its approximate altitude. Like the preceding correction, it is always additive.

Use of the Tables.

In Table I. find first the numbers corresponding to the observed heights of the barometer h and h'. Suppose, for instance, h=29.345 in.; find in the first column on the left the number 29.3; on the same horizontal line, in the column headed .04, is given the number corresponding to 29.34=28121.7; in the last column but one on the right, we find for .005=4.5, or for 29.345=28126.2. Take likewise the value of h', and find the difference.

If the barometrical heights have not been previously reduced to the same temperature, or to the freezing point, apply to the difference the correction found in Table II. opposite the number representing $\tau - \tau'$; we thus obtain the approximate difference of level, D.

For computing the correction due to the expansion of the air according to its temperature, or $D \times \left(\frac{t+t'-64}{900}\right)$, make the sum of the temperatures, subtract from that sum 64; multiply the rest into the approximate difference D, and divide the product by 900. This correction is of the same sign as (t+t'-64). By applying it, we obtain a second approximate difference of level, D'.

In Table III., with D' and the mean latitude of the stations, find the correction for variation of gravity in latitude, and add it to D', paying due attention to the sign.

In Table IV. with D', and in Table V. with D' and the height of the barometer at the lower station, take the corrections for the decrease of gravity on a vertical, and add them to the approximate difference of level.

The sum thus found is the true difference of level between the two stations, or Z; by adding the elevation of the lower station above the level of the sea, when known, we obtain the *altitude* of the upper station.

The use of the small table, VI., by means of which approximate differences of level can be obtained by a single multiplication, is explained below, page 90.

Example 1.

Measurement of Mount Washington, New Hampshire, by A. Guyot, August 8th, 1851, 4 p. m.; the barometer at the lower station being at 825 English feet above the mean level of the sea; at the upper station at one foot below the summit.

The observation gave,

Gorham,
$$h=29.272$$
 in. $\tau=70^{\circ}.70$ F. $t=72^{\circ}.05$ F. Mount Washington, $h'=24.030$ " $\tau'=54^{\circ}.52$ F. $t'=50^{\circ}.54$ F. $\tau-\tau'=16^{\circ}.38$ F. $t'=50^{\circ}.54$ F. $t'=50^{\circ}$

BAROMETRICAL MEASUREMENT OF HEIGHTS.

Table I. gives for $h = 29.272$ inches,	
Difference,	
Table II. gives for $\tau - \tau' = 16^{\circ}.38$	— 37.64
Approximate difference of level, $D=$	5,117.76
$\frac{D \times (t + t' - 64)}{900} = \frac{5118 \times 58.6}{900} =$	333.19
Second approximate difference, $D'=$	5,450.95
Table III. gives for $D'=5450$ and Lat. 44°	0.50
Table IV. gives for $D'=5450$	14.94
Table V. gives for $h = 29.27$	0.00
Barometer below summit,	1.00
Mount Washington above Gorham, or $$	5,465.39
Barometer at Gorham above sea level	825.00
Mount Washington above the sea, or altitude,	6,290.39 Eng. ft.

Example 2.

Measurement of the highest peak of the Black Mountain, in North Carolina, July 11th, 1856, by A. Guyot.

By observation we have at,

36		Attached Thermometer.	
		$\tau = 64^{\circ}.58 \text{ F}.$	
Highest Peak,	h' = 23.662 "	$\tau' = 61^{\circ}.88 \text{ F.}$	$t' = 59^{\circ}.36 \text{ F.}$
	τ –	$-\tau' = \overline{2^{\circ}.70} \text{ F.}$	120°.70 F.
			— 64°
		t + t' -	$64 = \overline{56^{\circ}.7} \text{ F.}$
Table I. gives	for $h = 24.934$.		23,870.4
	Differenc	e,	1.368.0
Table II. gives			
14010 11. 5170.			
		nate difference, D =	
	$\frac{D \times (t + t' - 6)}{900}$	$\frac{4)}{2} = \frac{1362 \times 56.7}{900} =$	= 85.8
	Second approxim	nate difference, D^\prime =	= 1,447.5
Table III. give	es for $D'=1448$ an	${ m id}\;{ m Lat.}\;36^{\circ}$	1.2
Table IV. give	es for $D'=1448$		3.8
Table V. give	s for $D'=1448$ and	ad $h=25$	0.7
Highest peak	above Mountain Hou	use, or $Z=$	= $1,453.2$
Black Mounta	iń, highest peak abo	ve the sea, or altitud	e, 6,701.6 Eng. ft.

Ξ.

TABLES

FOR COMPUTING THE DIFFERENCE IN THE HEIGHT OF TWO PLACES FROM BAROMETRICAL OBSERVATIONS.

I. $\mathbf{D} = 60158.58 \times \log H$ or h. Argument, the observed Height of the Barometer at either Station.

Barometer	Eng. Inch.	12.0	12.1	12.2	12.3	12.4		12.5	12.6	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	
ths	Inch.		F	Feet.	1 2.1	4.2		3 6.2	8.3	5 10.4	6 12.5	7 14.6	8 16.6	9 18.7				_
=		1 .					-		_		_							-
	60.	Eng. Feet. 4958.6	5173.8	5387.2	5599.0	5809.0		6017.4	6224.0	6429.2	6632.7	6834.5	703-1.9	7233.8	7431.1	7627.0	7821.4	
	.03	Eng. Feet. 4937.0	5152.4	5367.0	5578.9	5788.1		5996.6	6203.5	6408.8	6612.4	6814.4	7014.9	7213.9	7411.4	7607.4	7802.0	
	.07	Eng. Feet. 4915.4	5130.9	5344.7	5556.8	5767.2		5975.8	6182.8	6388.3	6592.1	6794.3	6995.0	7194.1	7391.8	7587.9	7782.6	
	90.	Eng. Feet. 4893.7	5109.4	5323.4	5535.7	5746.2		5955.0	6162.2	6367.8	6571.8	6774.1	6975.0	7174.3	7372.1	7568.4	7763.2	
of an Inch.	.05	Eng. Feet. 4872.1	6.7803	5302.1	5514.5	5725.3		5934.2	6141.6	6347.3	6551.5	6754.0	6955.0	7154.4	7352.3	7548.8	7743.8	
Hundredths of an Inch.	10.	Eng. Feet. 4850.4	5066.4	5280.7	5493.4	5704.3		5913.4	6120.9	6326.8	6531.1	6733.8	6934.9	7134.5	7332.6	7529.2	7724.4	
	.03	Eng. Feet. 4828.7	5044.9	5259.4	5472.2	5683.2		5892.6	6100.2	6306.3	6510.8	6713.6	6914.9	7114.6	7312.9	7509.6	7704.9	
	.03	Eng. Feet. 4806.9	5023.4	5238.0	5452.0	5662.2		5871.7	9.6709	6285.8	6490.4	6693.4	8.1689	7.094.7	7293.1	7490.0	1685.4	
	10.	Eng. Feet. 4785.2	8.1003	5216.6	5429.8	5641.2		5850.8	6058.8	6265.2	6470.0	6673.2	6874.7	7074.8	7273.3	7470.4	0.9997	
	00.	Eng. Feet.	4980.2	5195.2	5408.5	5620.1		5829.9	6038.1	6214.6	6449.6	6652.9	6854.7	7054.9	7253.6	7450.8	7646.5	
Barometer	Eng. Inch.	12.0	12.1	12.2	12.3	12.4		12.5	12.6	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	

Barometer					Hundredth	Hundredths of an Inch.					Thou	sandths	Barometer
in Eng. Iuch.	00.	10.	.09	.03	10.	.05	90.	.03	80.	60.	o ≓ ———	r an nch.	of an in Inch. Eng. Inch.
	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng Feet.			
13.5	7840.8	1260.1	7879.4	7898.7	7918.0	7937.3	7956.6	7975.8	7995.1	8014.3		,	13.5
13.6	8033.6	8052.8	8071.9	8091.1	8110.3	8129.4	8148.6	8167.7	8186.8	8205.9		Feet.	13.6
13.7	8225.0	8244.0	8263.1	8282.1	8301.1	8320.1	8339.1	8358.1	8377.1	8396.0	_	1.9	13.7
13.8	8415.0	8433.9	8452.8	8471.7	8.190.6	8509.4	8528.3	8547.1	8565.9	8584.8	ঝ	3.8	13.8
13.9	8603.6	8622.3	8641.1	8659.9	8678.6	8697.4	8716.1	8734.8	8753.5	8772.2	က	5.6	13.9
14.0	8790.8	8809.5	8828.2	8846.8	8865.4	8884.0	8902.6	8921.2	8939.7	8958.3	4	7.5	14.0
14.1	89768	8995.4	9013.9	9032.4	8020.8	9069.3	9087.8	9106.2	9154.6	9143.0	rO	6.4	14.1
14.2	9161.4	8.6216	9198.2	9216.6	9234.9	9253.3	9271.6	9289.9	9308.2	9326.5	9	11.3	14.2
14.3	9344.7	9363.0	9381.3	9399.5	9417.7	9436.0	9454.2	9472.3	9490.5	9508.7	~	13.2	14.3
14.4	9526.8	9545.0	9563.1	9581.2	9599.3	£.7196	9635.5	9653.5	9671.6	9.6896	00	15.0	14.4
14.5	9707.6	9725.7	9743.7	9761.7	9779.6	9797.6	9815.6	9833.5	9851.4	9869.3	6	17.0	14.5
14.6	9887.2	9905.1	9923.0	6.0166	9958.7	9976.5	1.1666	10012.2	10030.0	10047.8			14.6
14.7	10065.5	10083.3	10101.1	10118.8	10136.6	10154.3	10172.0	10189.7	10207.4	10225.1			14.7
14.8	10242.7	10260.4	10278.0	10295.7	10313.3	10330.9	10348.5	10366.1	10383.6	10401.2	_	1.7	14.8
14.9	10418.7	10436.3	10453.8	10471.3	10488.8	10506.3	10523.7	10541.2	10558.6	10576.0	61	3.4	14.9
15.0	10593.4	10610.8	10628.2	10645.6	10662.9	10680.3	10697.6	10715.0	10732.3	10749.6	က	5.1	15.0
15.1	10766.9	10784.1	10801.5	10818.7	10836.0	10853.2	10870.5	10887.7	10904.9	10922.1	7	8.9	15.1
15.2	10939.3	10956.5	10973.6	10990.8	11008.0	11025.1	11042.2	11059.3	11076.4	11093.5	10	8.5	15.2
15.3	111110.6	11127.7	111144.7	11161.8	11178.8	11195.8	11212.8	11229.8	11246.8	11263.8	9	10.5	15.3
15.4	11280.8	11297.8	11314.7	11331.6	11348.6	11365.5	11382.4	11399.3	11416.2	11433.0	7	11.9	15.4
15.5	11449.9	11466.7	11453.6	11500.4	11517.2	11534.0	11550.8	11567.6	11584.4	11601.1	တ	13.6	15.5
15.6	11617.9	11634.6	11651.4	11668.1	11684.8	11701.5	11718.2	11734.9	11751.6	11768.2	6	15.3	15.6
15.7	11784.9	11801.5	11818.2	11834.8	11851.4	0.89811	11884.6	119011	11917.7	11934.3		-	15.7
15.8	11950.8	11967.3	11983.8	12000.4	12016.9	12033.3	12049.8	12066.3	12082.7	12099.2			15.8
15.9	12115.6	12132.0	12148.4	12164.8	12181.2	12197.6	12214.0	12230.4	12246.7	12263.1	_		15.9

				Hundredth	Hundredths of an Inch.					Thous	Thousandths of an	Barometer in
	10.	€ .	.03	10.	.05	90.	40.	80.	60.	II.	ch.	Eng. Inch.
Eng. Fect.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Fret.	Eng Feet.	Eng. Feet.	Eng Feet.			
12279.6	12295.9	12312.2	12328.5	12344.8	12561.1	12377.4	12393.6	12109.9	12426.1			16.0
12442.4	12458.6	12474.8	12491.0	12507.2	12523.4	12539.6	12555.7	12571.9	12588.0		reet.	16.1
12604.2	12620.3	12636.4	12652.5	12668.6	12684.7	12700.S	12716.8	12732.9	12748.9	_	1.6	16.2
12765.0	12781.0	12797.0	12813.0	12829.0	12845.0	12861.0	12876.9	12892.9	12908.8	લ	3.1	16.3
12924.8	12940.7	12956.6	12972.5	12988.4	13004.3	13020.2	13036.0	13051.9	13067.7	က	4.7	16.4
3083.6	13099.4	13115.2	13131.0	13146.8	13162.6	13178.4	13194.2	13210.0	13225.7	7	6.3	16.5
(3241.5	13257.2	13272.9	13288.6	13301.3	13320.0	13335.7	13351.4	13367.1	13382.7	13	7.8	16.6
13398.4	13414.0	13429.6	13445.2	13.160.8	13476.4	13492.0	13507.6	13523.2	13538.7	9	6.4	16.7
13554.3	13569.8	13585.4	13600.9	13616.4	13631.9	13647.4	13662.9	13678.4	13693.9	~	11.0	16.8
13709.4	13724.8	13740.3	13755.7	13771.1	13786.5	13801.9	13817.3	13832.7	13848.1	œ	12.5	16.9
3863.5	13878.8	13894.2	13909.6	13924.9	13940.2	13955.6	13970.9	13986.2	14001.5	6.	14:1	17.0
14016.8	14032.0	14047.3	14062.6	14077.8	14093.0	14108.3	14123.5	14138.7	14153.9			17.1
14169.1	14184.3	14199.4	14214.6	14229.8	14244.9	14260.1	14275.2	14290.3	14305.5			17.2
14320.6	14335.7	14350.8	14365.8	14380.9	14396.0	14411.0	14426.1	14441.1	14456.2			17.3
14471.2	14486.2	14501.2	14516.2	14531.2	14546.1	14561.1	11576.1	14591.0	14605.9	-	1.5	17.4
14620.9	14635.8	14650.7	14665.6	14680.5	14695.4	14710.3	14725.2	14740.1	14754.9	67	5.9	17.5
14769.8	14784.6	14799.4	14814.3	14829.1	14843.9	14858.7	14873.5	14888.2	14903.0	<u>ස</u>	1.1	17.6
14917.8	14932.5	14947.3	14962.0	14976.8	14991.5	15006.2	15020.9	15035.6	15050.3	7	5.S	17.7
15065.0	15079.6	15094.3	15109.0	15123.6	15138.2	15152.9	15167.5	15182.1	15196.7	ıo	7.3	17.8
15211.3	15225.9	15240.5	15255.0	15269.6	15284.2	15298.7	15313.3	15327.8	15342.4	9	8.8	17.9
15356.8	15371.3	15385.8	15400.3	15114.8	15429.3	154437	15458.2	15472.7	15487.1	7	10.2	18.0
5501.5	15516.0	15530.4	15544.8	15559.2	15573.6	15588.0	15602.4	15616.8	15631.2	œ	11.7	18.1
5645.5	15659.9	15674.2	15688.5	15702.9	15717.2	15731.5	15745.8	15760.1	15774.4	6	13.1	18.2
628876	15802.9	15817.2	15831.4	15845.7	15859.9	15874.2	15888.4	15902.6	15916.8			18 3
15931.0	15945.2	15959.4	15973.6	15987.8	9.10091	16016.1	16030.2	16044.4	16058.5	_		18.4

Barometer					Hundredths of an Inch.	of an Inch.					Thous	Thousandths	Barometer
in Eng. Inch.	00.	10.	3.0.	€⊕•	\$0.	.05	90.	.0.	8.9.	60.	14	Inch.	Eng. Inch.
	Eng Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Fect.	Eng. Feet.	Eng. Feet.	Eng. Feet.			9
5.5	16072.6	16086.8	16100.9	16115.0	16129.1	16143.2	16157.3	16171.3	16185.4	16199.5		Foot	18.5
9.8	16213.5	16227.6	16241.6	16255.6	16269.7	16283.7	16297.7	16311.7	16325.7	16339.6		• • • • • • • • • • • • • • • • • • • •	18.6
2 2	16353.5	16367.5	16381.5	16395.4	16409.4	16423.3	16437.2	16451.2	16165.1	16479.0	-	1.4	18.7
. o	16199.9	16506.8	16520.7	16534.6	16548.5	16562.3	16576.2	16590.0	16603.9	16617.8	ଚୀ	2.7	18.8
15.9	16631.5	16645.4	16659.2	16673.0	16686.8	16700.6	16714.4	16728.1	16741.9	16755.7	အ	1.	18.9
0 0 1	16220	6.283.9	16,596.9	16810.6	16824.3	16838.1	16851.8	16865.5	16879.2	16892.8	-	5.1	19.0
10.01	16406.5	16920.2	16933.9	16947.5	16951.2	16974.9	16988.5	17002.1	17015.8	17029.4	10	6.8	19.1
6.01	150 (2.0	17056.6	17070.9	17083.8	17097.4	17110.9	17124.5	17138.1	17151.6	17165.2	9	8:1	19.2
9.01	17178 4	17199.9	17205.8	17219.3	17232.8	17246.3	17259.8	17273.3	17286.8	17300.3	7	9.5	19.3
1.61	173137	17327.2	17340.6	17354.1	17367.5	17380.9	17394.4	17407.8	17421.2	17434.6	œ	10.9	19.4
10	17160	17161.1	8.17.171	17488.9	17501.6	17515.0	17528.3	17541.7	17555.0	17568.4	6	12.2	19.5
9 01	175817	17595.0	17603.3	17621.7	17635.0	17648.2	17661.5	17671.8	17688.1	17701.4			9.61
20.01	177116	1757.9	1.14771	17754.4	17767.6	17780.8	17794.1	17807.3	17820.5	17833.7			19.7
3 9 9	17846.9	17860.1	17873.3	17886.5	17899.6	17912.8	17926.0	17939.1	17952.2	17965.4			19.8
19.9	17978.5	17991.6	18004.8	18017.9	18031.0	18044.1	18057.2	18070.3	18083.4	18096.4	-	:: ::	19.9
0.06	18109.5	18122.6	18135.6	18148.7	18161.7	18174.8	18187.8	18200.8	18213.8	18226.8	¢1	5.6	20.0
001	18939.8	18952.8	18265.8	15278.8	18291.8	18304.8	18317.7	18330.7	18343.6	18356.6	က	3.9	20.1
6 06	18369.5	18350.5	18395.4	18408.3	15421.2	18434.1	18447.0	18459.9	18472.8	18185.7	7	5.1	20.5
806	18198.5	18511.4	18524.3	18537.1	18550.0	18562.8	18575.7	18588.5	18601.3	18614.1	70	6.4	20.3
20.4	18626.9	18639.7	18652.5	18665.3	18678.1	18690.9	18703.6	18716.4	18729.1	18741.9	9	7.7	20.4
50.5	18754.6	18767.4	18780.1	18792.9	18805.6	18818.3	18831.0	18843.7	18856.4	18869.1	1-	0.6	20.5
9 0 6	18881.8	18891.5	18907.2	18919.9	18932.5	18945.2	18957.8	18970.5	18983.1	18995.7	oo	10.3	20.6
20.0	19003.3	19021.0	19033.6	19046.2	19058.8	19071.4	19083.9	19096.5	19109.1	19121.7	6	11.6	20.7
8.06	19134.2	19146.8	19159.3	19171.9	19184.4	19196.9	19209.5	19222.0	19234.5	19247.0			20.8
	1 0 100			* #0000	10000	0.0000	10001	10000	10950	0 14601			0 00

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Barometer	Eng. Inch.	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	22.0	22.1	22.3	22.3	22.4	22.5	22.6	22.7	22.8	95.9	23.0	23.1	23.2	23.3	23.4
Thousandths	Inch.	Feet.	1.2	2.4	3.6	4.8	6.0	7.5	8.4	9.7	10.9				1:1	2.3	3.4	4.6	5.7	6.8	8.0	9.1	10.2			
Tho			П	61	က	7	.c	9	7	00	<u></u>				_	61	ಣ	7	50	9	7	œ	6			
	60.	Eng. Feet. 19496.0	19619.6	19742.6	19865.0	19986.9	20108.2	20228.9	20349.1	20468.7	20587.8	20706.3	20824.4	20941.9	21058.8	21175.3	21291.1	21406.5	21521.4	21635.8	21749.7	21863.0	21976.0	22088.4	22200.4	22311.8
	80.	Eng. Feet. 19483.6	19607.3	19730.3	19852.8	19974.7	20096.1	20216.9	20337.1	20456.8	20575.9	20694.5	20812.6	20930.1	21047.1	21163.6	21279.5	21395.0	21509.9	21624.4	21738.3	21851.7	21964.7	22077.2	22189.2	22300.7
	.03	Eng. Feet. 19471.2	19594.9	19718.0	19840.6	19962.6	20083.9	20204.8	20325.1	20444.8	20564.0	20682.7	20501.8	20918.4	21035.4	21152.0	21268.0	21383.5	21498.5	21613.0	21727.0	21840.4	21953.4	22066.0	22178.0	22289.6
	90.	Eng. Feet. 19458.8	19582.6	19705.8	19828.4	19950.4	20071.8	20192.7	20313.1	20432.9	20552.1	20670.8	20789.0	20906.7	21023.8	21140.4	21256.4	21371.9	21487.0	21601.6	21715.6	21829.1	21942.1	22054.7	22166.8	22278.4
Hundredths of an Inch.	.05	Eng. Feet. 19446.4	19570.2	19693.5	19816.1	19938.2	20059.7	20180.7	20301.1	20420.9	20540.2	20659.0	20777.2	20894.9	21012.1	21128.7	21244.8	21360.4	21475.5	21590.1	21704.2	21817.7	21930.8	22043.5	22155.6	22267.3
Hundredth	0.	Eng. Feet.	19557.9	19681.2	19803.9	19926.0	20047.6	20168.6	20289.1	20409.0	20528.3	20647.1	20765.4	20883.2	21000.4	21117.1	21233.2	21348.9	21464.0	21578.7	21692.8	21806.4	21919.6	22032.3	22144.5	22256.2
	.03	Eng. Feet.	19545.5	19668.9	19791.6	19913.9	20035.5	20156.5	20277.0	20397.0	20516.4	20635.3	20753.6	20871.4	20988.7	21105.4	21221.6	21337.3	21452.5	21567.2	21681.4	21795.1	21908.3	22021.0	22133.3	22245.0
	.03	Eng Feet. 19409.1	19533.1	19656.6	19779.4	19901.7	20023.3	20144.4	20265.0	20385.0	20504.5	20623.4	20741.8	20859.7	20977.0	21093.8	21210.1	21325.8	21441.1	21555.8	21670.1	21783.7	21897.0	22009.8	22122.1	22233.9
	10.	Eng. Feet.	19520.8	19644.3	19767.1	19889.5	20011.2	20132.3	20253.0	20373.0	20492.6	20611.5	20732.0	20847.9	20965.3	21082.1	21198.5	21314.2	21429.6	21544.3	21658.7	21772.4	21885.6	21998.5	22110.8	22222.7
	00.	Eng. Feet.	19508.4	19632.0	19754.9	19877.3	19999.1	20120.3	20241.0	20361.1	20480.7	20599.7	20718.2	20836.2	20953.6	21070.5	21186.9	21302.6	21418.1	21532.9	21647.3	21761.0	21874.3	21987.2	22099.6	22211.5
Barometer	Eng. Inch.	91.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	23.0	23.1	23.2	23.3	23.4

Barometer					Hundredths of an Inch.	of an Inch.					Thou	andths	Barometer
in Eng. Inch.	00.	10.	30 •	.03	10.	.03	90.	20.	80.	.00	54	Inch.	Eng. Inch.
	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Fect.	Eng Feet.	Eng Feet.	Eng Feet	Eng. Feet			
23.5	22322.9	22334.0	22345.2	22356.3	22367.4	22378.4	22389.5	22400.6	22411.7	22422.8			23.5
23.6	22433.8	22444.9	22156.0	22467.0	22478.1	22489.1	22500.2	22511.2	22522.3	22533.3		F	23.6
23.7	22544.3	22555.4	22566.4	22577.1	22588.4	22599.4	22610.4	22621.4	22632.4	22643.4	-	Feet	23.7
93.8	22654.3	22665.3	22676.3	22687.2	22698.2	22709.1	22720.1	22731.0	22742.0	22752.9	~	1.1	23.8
23.9	22763.8	22774.8	22785.7	22796.6	22807.5	22818.4	22829.4	22840.3	22851.2	22862.0	63	c:	23.9
016	99873.0	99883.9	22894.7	22905.6	22916.5	22927.4	22938.2	22949.1	22960.0	22970.8	ಣ	3.5	24.0
0.1.7	22981.7	22992.5	23003.3	23014.2	23025.0	23035.8	23046.6	2:057.5	23068.3	23079.1	7	65.4	24.1
21.2	23089.9	23100.7	23111.4	23122.2	23133.0	23143.8	23154.5	23165.3	23176.1	23186.8	က	5.4	24.2
51.3	23197.6	23208.3	23219.1	23229.8	23240.5	23251.3	23262.0	23272.7	23283.4	23294.2	9	6.5	24.3
24.4	23301.9	23315.6	23326.3	23337.0	23347.6	23358.3	23369.0	23379.7	23390.3	23401.0	7	7.5	24.4
21.5	93411.7	23422.3	23433.0	23443.7	25454.3	23464.9	23475.6	23486.2	23496.8	23507.4	00	8.6	24.5
24.6	23518.1	23528.7	23539.3	23549.9	23560.5	23571.1	23551.7	23592.3	23602.9	23613.5	6	9.7	24.6
24.7	23624.1	23634.6	23645.2	23655.8	23666.3	23676.9	23687.5	23698.0	23708.6	23719.1			24.7
24.8	23729.7	23740.2	23750.7	23761.2	23771.7	23782.3	23792.8	23803.3	23813.8	23824.3			21.8
24.9	23834.8	23845.3	23855.7	23866.2	23876.7	23887.2	23897.7	23908.2	23918.6	23929.1	_	1.0	24.9
25.0	23939.5	23949.9	23960.4	23970.8	23981.3	23991.7	24002.1	24012.5	24023.0	24033.4	61	2.1	25.0
25.1	24043.8	24054.2	21064.6	24075.0	24085.4	24095.7	24106.1	24116.5	24126.9	24137.2	က	3.1	25.1
25.2	24147.6	24158.0	24168.3	24178.7	24189.0	24199.4	24209.7	24220.1	24230.4	24240.8	- +	4.1	25.2
25.3	24251.1	24261.4	24271.8	24282.1	24292.4	24302.7	24313.0	24323.3	24333.6	24343.9	20	5.1	25.3
25.4	21354.2	24364.5	21374.7	24385.0	24395.3	24405.5	24415.8	24426.1	24436.3	24446.6	9	6.2	25.4
25.5	24456.8	21167.0	24477.3	24187.5	24497.8	24508.0	24518.2	24528.4	24538.7	24548.9	~	7.2	25.5
25.6	24559.1	24569.3	24579.5	24589.7	24599.9	24610.0	24620.2	21630.4	24640.6	24650.7	œ	8:3	25.6
25.7	24660.9	21671.1	24681.2	2 1691.1	24701.5	24711.7	24721.8	2 (732.0	24742.1	24752.3	6	0.3	25.7
25.8	24762.4	24772.5	24782.6	24792.8	24802.9	24813.0	24823.1	24833.2	24843.3	24853.4			25.8
95.0	91863 5	9 22516	9 1883.7	9 1503.7	8.5001.6	0.21016	0.1991.0	2 193 1.0	24944.1	24954.1			25.9

Thousandths Barometer	Eng. Inch.	et. 26.0	26.1	1.0 26.2	2.0 26.3	2.9 26.4	3.9 26.5	4.9 26.6	5.9 26.7	6.9 26.8	7.8 26.9	8.8 27.0	27.1	27.2	27.3	0.9 27.4	1.9 27.5	2.8 27.6	3.7 27.7		5.6 27.9	6.5 28.0	7.5 28.1		28.3	28.4
nousand	Inch	Feet.		_	2 2			5		9		s		_		- -				5			8			
_ <u>E</u>		1 + 10	-	_					_				-	ಣ	6										s	-
	69.	Eng. Feet 25054.5	25154.4	25254.0	25353.1	25451.9	25550.4	25648.5	25746.2	25843.5	25940.5	26037.2	26133.4	26229.3	26324.9	26420.1	26514.9	26609.5	26703.7	26797.6	26891.0	26981.3	27077.1	27169.6	27261.8	27353.7
	80.	Eng. Feet. 25044.5	25144.4	25244.0	25343.2	25442.1	25540.5	25638.7	25736.4	25×33.8	25930.8	26027.5	26123.8	26219.8	26315.3	26410.6	26505.5	26600.0	26694.3	26788.2	26881.7	26975.0	27067.8	27160.4	27252.6	27344.5
	20.	Eng. Feet. 25034.4	25134.5	25234.1	25333.3	25432.2	25530.7	25628.9	25726.7	25824.0	25921.1	26017.9	26114.2	26210.2	26305.8	26401.1	26496.0	26590.6	26684.9	26778.8	26872.3	26965.6	27058.6	27151.2	27243.4	27335.3
	90.	Eng. Feet. 25024.4	25124.5	25224.1	25323.4	25422.3	25520.9	25619.1	25716.9	25814.3	25911.4	26008.2	26104.6	26200.6	26296.3	26391.6	26486.5	26581.2	26675.5	26769.5	26863.0	26956.3	27049.3	27141.9	27234.2	27326.2
Hundredths of an Inch.	.03	Eng. Feet. 25014.4	25114.5	25214.2	25313.5	25412.4	25511.0	25609.3	25707.1	25804.6	25901.7	25998.6	26095.0	26191.0	26286.7	26382.1	26477.1	26571.7	26666.1	26760.1	26853.7	26947.0	27040.0	27132.7	27225.0	27317.0
Hundredth	0	Eng. Feet. 25004.4	25104.5	25204.2	25303.6	25402.6	25501.2	25599.5	25697.4	25794.6	25892.1	25988.5	26085.3	26181.4	26277.2	26372.5	26467.6	26562.3	26656.7	26750.7	26844.3	26937.7	27030.7	27123.4	27215.7	27307.8
	.03	Eng. Feet. 2499-1.3	25094.5	25194.3	25293.7	25392.7	25491.4	25589.7	25687.6	25785.1	25882.3	25979.2	26075.7	26171.8	26267.6	26363.0	26458.1	26552.8	26647.2	26741.3	26835.0	26928.4	27021.5	27114.2	27206.5	27298.6
	.03	Eng. Feet. 24984.3	25084.5	25184.3	25283.8	25382.8	25481.5	25579.8	25677.8	25775.4	25872.6	25969.6	26066.1	26162.2	26258.0	26353.5	26448.6	26543.3	26637.8	26731.9	26825.6	26919.0	27012.2	27104.9	27197.3	27289.4
	10.	Eng. Feet. 24974.2	25074.5	25174.4	25273.8	25372.9	25171.7	25570.0	25668.1	25765.6	25862.9	25959.9	26056.5	26152.6	26248.5	26344.0	26439.1	26533.9	26628.4	26722.5	26816.3	26909.7	27002.9	27095.6	27188.1	27280.2
	00.	Eng. Feet. 24964.2	25064.5	25164.4	25263.9	25363.0	25461.8	25560.2	25658.3	25755.9	25853.2	25950.2	26046.8	26143.0	26238.9	26334.4	26429.6	26524.4	26618.9	26713.1	26806.9	26900.4	26993.6	27086.4	27178.9	27271.0
Barometer	Eng. Inch.	26.0	26.1	26.2	26.3	26.4	26.5	56.6	26.7	8.92	56.9	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	28.0	28.1	28.5	28.3	1.86

Barometer					Hundredths of an Inch.	of an Inch.					Thous	Thousandths	Barometer in
in Eng. Inch.	00.	10.	.03	.03	10.	.05	90.	.07	80.	60.	: <u>4</u>	 14	Eng. Inch.
	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng. Feet.	Eng Feet.			200
28.5	27362.9	27372.0	27381.2	27390.4	27399.5	27408.7	27417.8	27.127.0	7/430.1	7.6+1.7	_	Feet.	0.07
28.6	27454.4	27463.5	27472.6	27481.8	27490.9	27500.0	27509.1	27518.2	27527.4	27536.5			58.6
28.7	27515.6	27554.7	27563.8	27572.9	27582.0	27591.1	27600.2	27609.3	27618.3	27627.4	_	6.0	28.7
28.8	27636.5	27645.5	27654.6	27663.7	27672.7	27681.8	27690.8	27699.9	27708.9	27717.9	67	s.	28.8
28.9	27727.0	27736.0	27745.1	27754.1	27763.1	27772.2	27781.2	27790.3	27799.2	27808.3	က	2.7	28.9
_	0 -10-6	0 96846	97535 9	97811.9	97853.9	27862.2	27871.2	27880.2	27889.1	27898.1	7	3.6	29.0
0.67	5.11.72	1 91026	97995 0	97934.0	97943.0	27951.9	27960.9	27969.8	27975.8	27987.7	ī.	£.5	29.1
6 06	97006 7	98003 6	98014.6	28023.5	28032.1	25041.4	28050.3	28059.2	28068.2	28077.1	9	5.4	29.5
2.65	0.98086	6.60052	28103.8	28112.8	28121.7	28130.6	28139.5	28148.4	28157.3	28166.2	1	6.3	29.3
1.66	28175.1	25184.0	28192.9	28201.7	28210.6	28219.5	28228.4	28237.2	28246.1	28254.9	œ	7.5	29.4
	5 63656	95979 6	98981 n	8 06686	6.9998	98308.0	28316.9	28325.7	28334.5	28343,4	6	8.1	29.5
9 06	982599	0.19386	8.8369.8	28378.7	28387.5	28396.3	28405.1	28413.9	28422.7	28431.5			29.6
20.0	28410.3	28149.1	28457.9	28466.7	28475.4	28484.2	28493.0	28501.8	28510.6	28519.3			29.7
or	28528.1	25536.9	28545.6	28554.4	28563.2	28571.9	28580.7	28589.4	28598.2	28606.9			29.8
29.9	28615.7	28624.4	25633.2	28641.9	28650.6	28659.3	28668.1	28676.8	28685.5	28694.2	1	9.8	29.9
30.0	98209.9	98711.6	28720.3	28729.0	28737.7	28746.4	28755.1	28763.8	28772.5	28781.1	Ç1	1.7	30.0
30.1	28789.8	28798.5	28807.2	28815.9	28824.5	28833.2	28841.9	28850.5	28859.2	25867.9	က	5.6	30.1
30.2	28876.5	28585.2	25893.8	28902.5	28911.1	28919.8	28928.4	25937.0	28945.7	28954.3	7	5.4	30.5
30.3	28962.9	28971.5	28980.1	28988.8	28997.4	29006.0	29014.6	29023.2	29031.7	29040.3	20	<u>ਹ</u>	30.3
30.4	29048.9	29057.5	29066.1	29074.7	29083.3	29091.8	29100.4	29109.0	29117.6	29126.2	9	5.5	30.4
30.5	29134.7	29143.3	29151.9	29160.4	29169.0	29177.6	29186.1	29194.7	29203.2	29211.8	7	6.0	30.5
9.08	29290.3	6,8556.6	29237.4	29245.9	29251.4	29262.9	29271.5	29280.0	29288.5	29297.0	00	6.9	90.0
30.7	29305.5	29314.0	29322.5	29331.1	29339.6	29348.1	29356.6	29365.1	29373.5	29382.0	6	7.7	30.7
30.8	29390.5	29399.0	29 107.5	29416.0	29424.4	29432.9	29441.4	29449.8	29458.3	29 166.8			30.8
30.9	29175.2	29483.7	29 192.1	29500.6	29509.0	29517.5	29525.9	29534.3	29542.8	29551.2			30.9

II. Correction for \(r -- \tau'\), or Difference of the Temperature of the Barometers at the Two Stations.

This Correction is negative when the attached Thermometer at the Upper Station is lowest; positive, when the attached Thermometer at the Upper Station is highest.

Correction in Eng. Feet.	213.2	214.3	215.5	216.7	217.9	219.0	220.2	221.4	222.5	223.7		224.9	226.1	227.2	228.4	229.6	230.7	231.9	233.1	231.3	
				_													 				
F ₩	91.0	91.5	92.0	92.5	93.0	93.	94.0	94.5	95.0	95.5		0.96	96.5	97.0	97.5	98.0	 98.5	99.0	99.5	100.0	
Correction in Eng.	189.7	190.9	192.1	193.3	194.4	195.6	196.8	197.9	199.1	200.3		201.5	202.6	203.8	205.0	206.1	 207.3	208.5	209.7	210.8	
τ — τ' Fahren- heit.	81.0	81.5	82.0	82.5	83.0	83 73	84.0	84.5	85.0	85.5		86.0	86.5	87.0	87.5	88.0	88.5	89.0	89.5	90.0	
Correc- tion in Eng. Feet.	166.3	167.5	168.7	169.8	171.0	172.2	173.4	174.5	175.7	176.9		178.0	179.2	180.4	181.6	182.7	183.9	185.1	186.2	187.4	
$r \longrightarrow \tau'$ Fahren- heit.	71.0	71.5	72.0	72.5	73.0	73.5	74.0	74.5	75.0	75.5		26.0	76.5	77.0	77.5	78.0	 78.5	79.0	79.5	80.0	
Correc- tion in Eng. Feet.	142.9	144.1	145.2	146.4	147.6	148.8	1.49.9	151.1	152.3	153.4		154.6	155.8	157.0	158.1	159.3	160.5	161.6	162.8	164.0	
τ — τ' Fabren- beit.	61.0	61.5	62.0	62.5	63.0	 7	64.0	64.5	65.0	65.5		0.99	66.5	67.0	67.5	0.89	68.5	0.69	69.5	70.0	
Correction in Eng. Feet.	119.5	120.6	121.8	123.0	124.2	125.3	126.5	127.7	128.8	130.0		131.2	132.4	133.5	134.7	135.9	137.0	138.2	139.4	140.6	
τ — τ' Fahren- heit.	51.0	51.5	52.0	52.5	53.0	7.0 6.0 7.0	54.0	54.5	55.0	55.5		26.0	56.5	57.0	57.5	58.0	58.5	59.0	59.5	0.09	
Correction in Eng. Fret.	96.0	97.2	98.4	9.66	100.7	6.101	103.1	104.2	105.4	106.6	4	107.8	108.9	110.1	111.3	112.4	113.6	114.8	116.0	117.1	
τ — τ' Fahren- heit.	41.0	41.5	45.0	42.5	43.0	13.5	14.0	44.5	45.0	45.5		16.0	46.5	47.0	47.5	48.0	48.5	49.0	49.5	50.0	_
Correc- tion in Eng. Feet.	72.6	73.8	75.0	76.1	77.3	78.5	79.6	80.8	85.0	83.2		84.3	85.5	86.7	87.8	89.0	90.5	91.4	92.5	93.7	
τ — τ' Fahren- heit.	31.0	31.5	32.0	32.5	33.0	33.5	31.0	34.5	35.0	35.5		36.0	36.5	37.0	37.5	38.0	38.5	39.0	39.5	40.0	
Correc- tion in Eng. Feet.	49.2	50.4	51.5	52.7	53.9	55.1	56.5	57.4	58.6	59.7		6.09	62.1	63.2	64.4	65.6	8.99	6.79	69.1	70.3	
τ — τ' Fahren- heit.	21.0	21.5	22.0	22.5	23.0	23.5	24.0	24.5	25.0	25.5		26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0	
Correc- tion in Eng. Feet.	25.8	26.9	28.1	29.3	30.5	31.6	35.8	34.0	35.1	36.3		37.5	38.7	39.8		42.5	43.3	44.5	45.7	46.9	
τ — τ' Fahren- heit.	0.11	11.5	12.0	12.5	13.0	13.5	14.0	14.5	15.0	15.5	1	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5	20.0	
Correc- tion in Eng. Feet.	2.3	3.5	4.7	5.9	7.0	8:3	9.4	10.5	11.7	12.9	1	14:1	15.2	16.4	17.6	18.7	19.9	21.1	22.3	23.4	
r — r' Fahren- heit.	0.1	1.5	5.0	2.5	3.0	3.03	4.0	4.5	5.0	5.5		0.9	6.5	7.0	7.5	8.0	x .c.	0.6	9.5	10.0	

CORRECTION FOR THE DIFFERENCE OF GRAVITY IN VARIOUS LATITUDES.

Correction positive from Latitude 00 to 450. Negative from 450 to 900.

pproxi- mate												Lat	Latitude.												Approxi- mate Differ-
Differ- ence of Level.	°06	ရုံ တို့ ရုံ	°98	° 178	° 3	008	120	26°	740	28°	200 2	99°	24° 9	26° 2 64° (3000	° %	34°	36.	88 89 89 89	40°	42°	440	45°	of of Level.
10.5	Poot	Feet	F. Page	Root	Post	Foot	Feet.	Foot	Foot.	Feref.	Foot.	Feet.	Feet. 1	Feet.	Feet.	Feet	Feet	Feet.	Feet.	Feet.	Feet	Feet.	Feet.	Feet.	Eng. Feet
1000 I		2.6	2.6	2.5	2.5	2.4	2.4	23		9. 1.:		_					-	1.0	8.0	9.0	0.5	0.3	0.1	0	1000
2000	5.5	5.5	5.1	5.1	5.0	4.9	1.7	4.6	7.7	4.5	4.0	3.7	3.5	65.50	5.9	5.6	e.	1.9	1.6	1.3	6.0	0.5	0.5	0	2000
3000	3.	2.8	7.7	7.6	7.5	3.5	7:1	6.9	9.9	6.3	0.9	5.6	5.5	90	7:7	3.9	3.4	5.9	2.4	1.9	1:1	8.0	0.3	0	3000
0000		10.4	10.3	10.5	10.0	8.6	9.5	9.5	80	8.4	8.0	7.5	7.0	6.4	5.8	5.5	9.1	3.9	85 61	2.5	1.8	1.1	1.0	0	4000
2000	13.0	13.0	12.9	12.7	12.5	12.2	11.9	11.5	11.0	10.5	10.0	9.4	8.1	8.0	7.3	6.5	5.7	4.9	4.0	3.1	5.3	1.4	0.5	0	2000
0009	15.6	15.6	15.4	15.3	15.0	14.7	14.3	13.8	13.2	12.6	11.9	11.2	10.4	9.6	8.7	7.8	8.9	s.s	3.	.s	5.7	1.6	0.5	0	0009
2000	18.2	18.2		17.8	17.5	17.1	9.91	16.1	15.4	14.7	13.9	13.1	12.2	11.2	10.2	9.1	8.0	8.9	5.6	7.7	3.5	1.9	9.0	0	2000
8000	20.8	20.7		20.3	20.0	19.5	19.0	18.4	17.6	16.8	15.9	15.0	13.9	12.8	9.11	10.4	9.1	7.8	6.4	5.0	3.6	2.2	0.7	0	8000
0006	23.4	23.3		22.9	22.5	22.0	21.4	20.7	19.8	18.9	17.9	16.8	15.7	14.4	13.1	11.7	10.3	80	7.2	5.7	7	2.4	8.0	0	0006
10000	26.0	25.9	25.7	25.4	25.0	24.4	23.8	23.0	22.0	21.0	19.9	18.7	17.4	16.0	34.5	13.0	11.4	9.7	8.0	6.3	4.5	5.7	0.0	0	10000
1000	28.6	28.5	28.3	28.0	27.5	26.9	26.1	25.3	2 1.3	23.1	21.9	20.6	19.1	17.6	16.0	14.3	12.5	10.7	s.	6.9	5.0	3.0	1.0	0	11000
2000	31.2	31.1			30.0	29.3	28.5	1934 F	26.5	25.2	23.9	22.4	20.9	19.5	17.4	15.6	13.7	11.7	9.6	7.5	5.4	3,3	1:1	0	12000
3000	33.8	33.7		33.1	32.5	31.8	30.9	29.8	28.7	27.3	25.9	24.3	55.6	8.02	18.9	16.9	14.8	12.7	10.4	8.5	5.9	3.5	1:5	0	13000
000	36.4	36.3	36.0	35.6	35.0	34.2	33.3	32.1	30.9	29.4	27.9	26.2	24.4	22.4	20.4	18.2	16.0	13.6	11.2	s s	6.3	3.8	1.3	0	14000
15000	39.0	38.9		38.1	37.5	9.98	35.6	31.4	33.1	31.6	29.9	28.1	26.1	0.43	21.8	19.5	17.1	9.41	12.1	9.4	8.9	1:	1.4	0	15000
00091	41.6	11.5	5.1	10.7	10.0	39.1	38.0	36.7	35.3	33.7	31.9	29.9	27.8	25.6	23.3	20.8	18.2	15.6	12.9	10.1	7.2	6.4	1.5	0	16000
2000	44.2	11.1	13.8	13.5	12.5	41.5	10.1	39.0	37.5	35.8	33.9	31.8	29.6	27.2	24.7	22.1	19.4	9.91	13.7	10.7	7.7	4.6	1.5	0	17000
8000	46.8	46.7	46.3	45.8	45.0	14.0	45.8	41.3	39.7	37.9	35.8	33.7	31.3	28.8	2.97	23.4	20.5	17.5	14.5	11.3	8.1	4.9	9.1	0	18000
0006	19.4	49.3	48.9	18.3	17.5	16.4	15.1	43.6	41.9	40.0	37.8	35.5	33.1	30.4	27.6	24.7	21.7	18.5	15.3	12.0	9.8	5.5	1.7	0	19000
0000	52.0	51.9		50.9	50.0	48.9	47.5	15.9	T++	12.1	39.8	37.4	34.8	32.0	29.1	26.0	8:27	19.5	16.1	12.6	9.0	5.4	1.s	0	20000
21000	54.6		54.1	53.4	52.5	51.3	49.9	ç;	46.3	57	8:	39.3	36.5	33.6	30.5	27.3	23.9	20.5	16.9	13.2	9.5	5.7	1.9	0	21000
52000	57.2			55.9	55.0	53.7	52.3	50.5	5.5	46.3	13.8	=======================================	38.3	35.2	32.0	28.6	25.1	21.4	17.7	13.8	6.6	0.9	5.0	0	22000
23000	59.8	59.7			57.5	56.3	54.6	52.8	50.7	8	15.8	13.0	10.0	36.8	33.4	29.9	26.3	22.4	18.5	14.5	10.4	6.5	2.1	0	23000
24000	62.4			0.19	0.09	58.6	57.0	55.1	52.9	50.5	17.8	14.9	41.8	38.1	34.9	31.2	27.4	23.4	19.3	15.1	8.01	6.5	2:5	0	24000
00000	65.0		1 9		2 69	61.1	013	44	10	29 62	0	0 0	5	- 0	6 76	100	30	6 1 6	90.1	15.7	6	3	6	0	95000

IV.	Correction For	CTION	V. Co	CORRECTION FOR THE LOWER STATION	ION FOR THE STATION.	R THI		Неібит об тив Positive.	тне	VI. III	EIGHT	OF A C	OLUI	INCH IN	IR, COI	rrespondin Barometer	NDING	To O.	NE TE	HLN
Approxi- mate Dif-		Decrease of Gravity on a Vertical.	II	Height of the Barometer, in English Inches, at Lower Station.	he Barou Low	eter, in er Station	English J	nehes, at		Barometer Reading			Tem	erature .	of the Ai	Temperature of the Air, Fahrenheit, being	theit, bei	gu gu		
ference of Level.	•	+500	91	20	08	₹ ₹	₹8	98	9 0	in English Inches.	40 °	450	.0g	55°	°09	. 29	200	500	° 💝	85 °
Eng Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.		Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
1000	2.5	3.9	1.6	<u></u>	1.0	8.0	9.0	0.4	0.5	18.5	9.44.6	146.1	147.7	1.19.3	150.9	152.5	154.0	155.7	157.2	158.8
2000	5.2	9.9	3.1	2.5	5.0	1.5	1.1	0.7	0.3	19.0	140.8	142.3	143.8	1.15.1	146.9	148.4	150.0	151.5	153.1	154.6
3000	7.9	9.3	4.7	3.8	3.0	2.3	1.7	1.1	0.5	19.5	137.1	138.6	140.1	141.6	143.1	144.6	1.911	147.6	149.1	150.6
4000	10.8	12.2	6.3	5.1	4.0	3.1	2.5	1.1	0.7	20.0	133.7	135.2	136.6	138.1	139.6	141.0	142.5	143.9	145.4	1.16.9
2000	13.7	15.2	7.8	6.4	5.0	3.8	5.8	1.8	8.0	20.5	130.5	131.9	133.3	134.7	136.1	137.6	139.0	140.4	141.8	143.3
0009	16.7	18.3	9.4	9.7	0.9	9.4	3.3	5.1	1.0	21.0	127.3	128.7	130.1	131.5	132.9	134.3	135.7	137.0	138.4	139.8
2000	19.9	21.5	11.0	8.9	7.1	5.4	3.9	2.5	1.2	21.5	124.3	125.7	127.0	128.4	129.7	131.1	132.4	133.8	135.1	136.5
8000	23.1	24.7	12.5	10.2	8.1	6.5	4.4	2.8	1.3	22.0	121.5	122.9	124.2	125.5	126.8	128.2	129.5	130.8	132.2	133.5
0006	26.4	28.1	14.1	11.4	9.1	6.9	5.0	3.5	1.5	22.5	118.8	120.1	121.4	122.7	124.0	125.3	126.6	127.9	129.2	130.5
10000	29.8	31.5	15.7	12.7	10.1	7.7	5.5	3.5	1.7	23.0	116.2	117.5	118.8	120.0	121.3	122.6	123.8	125.1	126.4	127.7
11000	33.3	35.1	17.2	14.0	11.1	8.5	6.1	3.9	1.8	23.5	113.7	115.0	116.2	117.5	118.7	120.0	121.2	122.5	123.7	124.9
12000	36.9	38.7	18.8	15.3	15.1	6.5	9.9	4.2	5.0	24.0	111.3	112.6	113.8	115.0	116.2	117.4	9.811	6.611	121.1	122.3
13000	40.6	42.5	20.4	16.5	13.1	10.0	7.2	9.4	5.5	24.5	109.1	110.3	111.5	112.6	113.8	115.0	116.2	117.3	9.811	8.611
14000	44.4	46.3	21.9	17.8	14.1	10.8	7.7	4.9	2.3	25.0	106.9	108.1	109.3	110.4	9.111	112.8	113.9	115.1	116.3	117.4
15000	48.3	50.3	23.5	1.61	15.1	11.5	œ ::	5.3		25.5	104.8	105.9	107.1	108.2	109.3	110.5	111.6	112.8	113.9	115.1
16000	52.3	54.3	25.1	20.3	1.91	12.3	8.8	5.6	5.7	26.0	102.7	103.9	105.0	106.1	107.2	108.4	109.5	110.6	111.7	112.8
17000	56.4	58.4	56.6	21.6	17.1	13.1	6.4	0.9	e.i &	26.5	100.9	105.0	103.1	104.2	105.3	106.4	107.5	9.801	109.7	110.8
18000	60.5	62.6	28.2	22.9	18.1	13.8	6.6	6.3	3.0	27.0	0.66	1001	101.2	102.3	103.3	101.4	105.5	9.901	9.201	108.7
19000	64.8	67.0	8.62	24.1	19.5	14.6	10.5	6.7		27.5	97.2	98.2	99.3	100.3	101.4	102.5	103.5	104.6	105.6	106.7
20000	69.2	71.4	31.3	25.4	20.5	15.4	11.0	0.7	3.3	28.0	95.4	96.5	97.5	986	9.66	1001	101.7	102.8	103.8	8.401
21000	73.6	75.9	32.9	26.7	21.2	16.1	11.6	7.4	3.5	28.5	93.8	94.8	95.8	6.96	97.9	6.86	6.66	100.9	101.9	10::01
22000	78.2	80.5	34.5	28.0	22.2	16.9	12.1	7.7	3.7	29.0	92.1	93.1	94.1	95.1	96.2	97.2	98.5	99.3	100.5	101.3
23000	82.9	85.2	36.0	29.5	23.5	17.7	12.7	8.1	3.8	29.5	90.06	91.6	95.6	93.6	91.5	95.5	96.5	97.5	98.5	99.5
24000	87.6	90.0	37.6	30.5	24.2	18.5	13.2	8.4	1.0	30.0	89.1	90.0	91.0	95.0	92.9	93.9	6.16	95.9	8.96	87.8
25000	92.5	6.16	39.1	31.8	25.2	19.2	13.8	8.8	4.1	30.5	87.6	88.5	89.5	90.4	91.4	92.3	93.3	94.2	95.2	96.1

III.

TABLE

FOR

COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER.

By Prof. Elias Loomis.

This table was computed from the formula of Laplace, modified in accordance with the results of more recent determinations.

Suppose that we have observed

At the lower station.
$$\begin{cases} H, \text{ the height of the barometer,} \\ T, \text{ the temperature of the barometer,} \\ t, \text{ the temperature of the air,} \end{cases}$$
 At the upper station.
$$\begin{cases} h', \text{ the height of the barometer,} \\ T', \text{ the temperature of the barometer,} \\ t', \text{ the temperature of the air.} \end{cases}$$

Represent by s the height of the lower station above the level of the sea, by L the latitude of the place, and by h the observed height h' reduced to the temperature T.

The difference of level x between the two stations is given by the formula,

$$x = 60158. 6 \text{ ft.} \times \log_{\frac{1}{h}} \times \left\{ \begin{cases} \left(1 + \frac{t + t' - 64}{900}\right) \\ \left(1 + 0.00265 \cos_{\frac{1}{h}} 2 \text{ L}\right) \\ \left(1 + \frac{x + 52251}{2088629} + \frac{s}{1044315}\right) \end{cases} \right\}$$

But h represents the height h' reduced from the temperature T' to the temperature T. The expansion of mercury for 1° Fahr. is 0.0001000; that of the brass which forms the scale of the barometer is 0.0000104; the difference is 0.0000896. we have $h = h' \{1 + 0.0000896 (T - T')\}$.

Therefore,

D

60158. 6 ft. log.
$$\frac{H}{h}$$
 = 60158.6 ft. log. $\frac{H}{h'}$ — 2.3409 ft. (T — T').

Part I. of the accompanying Table furnishes in English feet the value of the expression 60158.6 log. H for heights of the barometer from 11 to 31 inches; only they have all been diminished by the constant 27541.5 feet which does not change the difference

60158.6 log. H — 60158.6 log.
$$h$$
.

Part II. furnishes the correction - 2.3409 (T - T') depending upon the difference T — T' of the temperatures of the barometers at the two stations. This cor-49

rection is generally negative. It would be positive if T - T' were negative; that is, if the temperature T' of the barometer at the upper station exceeded the temperature T at the lower station.

Part III. gives the correction $A \times 0.00265$ cos. 2 L, to be applied to the approximate altitude A, and which arises from the variation of gravity from the latitude of 45 degrees, to the latitude L of the place of observation. This correction has the same sign as cos. 2 L; that is, it is positive from the equator to 45 degrees, and negative from 45 degrees to the pole.

Part IV. gives the correction $A \times \frac{A+52251}{2088629}$, which is always to be added to the approximate height A, and which is due to the diminution of gravity on the vertical.

Part V. furnishes for the approximate difference of level A the small correction $A \times \frac{s}{10444315}$ corresponding to several values of the height s of the lower station. But in place of s there has been substituted as the argument of the table, the height H of the barometer at this station.

Method of Computation.

Take from Part I. the two numbers corresponding to the observed barometric heights H and h'. From their difference subtract the correction 2.3409 (T — T') found in Part II. with the difference T — T' of the thermometers attached to the barometers. We thus obtain an approximate altitude a.

We then calculate the correction $a^{\frac{t+t'-64}{900}}$ for the temperature of the air, by multiplying the nine-hundredth part of a by the sum of the temperatures t and t' diminished by 64. This correction is of the same sign as t+t'-64. We thus obtain a second approximate altitude A.

With A and the latitude of the place L, we seek in Part III. the correction $A \times 0.00265$ cos. 2 L arising from the variation of gravity with the latitude.

For the approximate height A, Part IV. gives the correction $A \times \frac{A+52251}{20888629}$ arising from the diminution of gravity on a vertical. This correction is always additive.

Finally, when the height s of the lower station is considerable, the small correction $A \times \frac{s}{10444315}$ may be found in Part V. This correction is always additive.

Example 1.

M. Humboldt made the following observations on the mountain of Guanaxuato, in Mexico, in Latitude 21°, viz.

	Upper station.	Lower station near the sea.
Thermometer in open air,	$t' = 70^{\circ}.3$	$t=77^{\circ}.5$
Thermometer to barometer,	$T' = 70^{\circ}.3$	$T = 77^{\circ}.5$
Barometer,	h' = 23.66	H = 30.046

Required the difference in the height of the two stations.

for $H = 30.046$ inches	27649.7
Part I. gives $\begin{cases} \text{for H} = 30.046 \text{ inches} \\ \text{for } h = 23.66 \text{ inches} \end{cases}$	21406.9
Difference	$\overline{6242.8}$
Part II. gives for $T - T' = 7^{\circ}.2$,	16.9
Approximate altitude a,	${6225.9}$
$\frac{a}{900} (t + t' - 64) = 6.918 \times 83.8,$	+579.7
Second approximate altitude A,	6805.6
Part III. gives for $A=6806$, and $L=21^{\circ}$,	+13.3
Part IV. gives for 6806,	+19.3
Height above the sea,	6838.2 feet.

Example 2.

M. Gay Lussac in his celebrated balloon ascent in 1805, found his barometer to indicate 12.945 English inches, the temperature being 14°.9 Fahrenheit. The barometer at Paris at the same time indicated 30.145 English inches with a temperature of 87°.44 Fahrenheit. Required the elevation of the balloon above Paris.

$R \rightarrow I$. (for $H = 30.145$ inches,	27735.6
Part I. gives $\begin{cases} \text{ for H} = 30.145 \text{ inches,} \\ \text{ for } h' = 12.945 \text{ inches,} \end{cases}$	5650.4
Difference,	22085.2
Part II. gives for $T - T' = 72^{\circ}.54$,	169.9
Approximate altitude a ,	21915.3
$\frac{a}{900}(t+t'-64) = 24.35 \times 38.34,$	+933.6
Second approximate altitude A,	22848.9
Part III. gives for $A=22848$, and $L=48^{\circ}\ 50'$	-8.2
Part IV. gives for 22848,	+82.1
Height of balloon above Paris,	22922.8 feet.

		Arg	ument, tl	ne observed		T I.	ometer at ei	ther Stat	ion.		
Inches.	Feet.	Diff.	Inches.	Feet.	Diff.	Inches.	Feet.	Diff.	Inches.	Feet.	Diff.
11.0	1396.9		16.0	11186.3		21.0	18291.0		26.0	23871.0	
11.1	1633.3	236.4	16.1	11349.1	162.8	21.1	18415.1	124.1	26.1	23971.3	100.3
11.2	1867.6	234.3	16.2	11510.9	161.8	21.2	18538.7	123.6	26.2	24071.2	99.9
11.3	2099.9	232.3	16.3	11671.7	160.8	21.3	18661.6	122.9	26.3	24170.7	99.5
11.4	2330.1	230.2	16.4	11831.5	159.8	21.4	18784.0	122.4	26.4	24269.8	99.1
11.5	2558.3	228.2	16.5	11990.3	158.8	21.5	18905.8	121.8	26.5	24368.6	98.8
11.6	2784.5	226.2	16.6	12148.2	157.9	21.6	19027.0	121.2	26.6	24467.0	98.4
11.7	3008.7	224.2	16.7	12305.1	156.9	21.7	19147.7	120.7	26.7	24565.1	98.1
11.8	3231.1	222.4	16.8	12461.0	155.9	21.8	19267.8	120.1	26.8	24662.7	97.6
11.9	3451.6	220.5	16.9	12616.1	155.1	21.9	19387.4	119.6	26.9	24760.0	97.3
12.0	3670.2	218.6	17.0	12770.2	154.1	22.0	19506.4	119.0	27.0	24857.0	97.0
12.1	3887.0	216.8		12923.5	153.3		l	118.5	27.1	24953.6	96.6
		215.0	17.1		152.3	22.1	19624.9	118.0	8	1	96.2
12.2	4102.0	213.3	17.2	13075.8	151.5	22.2	19742.9	117.4	27.2	25049.8	95.9
12.3	5315.3	211.6	17.3	13227.3	150.6	22.3	19860.3	116.9	27.3	25145.7	95.5
12.4	4526.9	209.8	17.4	13377.9	149.7	22.4	19977.2	116.4	27.4	25241.2	95.2
12.5	4736.7	208.2	17.5	13527.6	148.9	22.5	20093.6	115.8	27.5	25336.4	94.8
12.6	4944.9	206.5	17.6	13676.5	148.0	22.6	20209.4	115.4	27.6	25431.2	94.5
12.7	5151.4	205.0	17.7	13824.5	147.2	22.7	20324.8	114.8	27.7	25525.7	94.2
12.8	5356.4	203.3	17.8	13971.7	146.3	22.8	20439.6	114.4	27.8	25619.9	93.8
12.9	5559.7	201.7	17.9	14118.0	145.6	22.9	20554.0	113.8	27.9	25713.7	93.4
13.0	5761.4	200.2	18.0	14263.6	144.7	23.0	20667.8	113.3	28.0	25807.1	93.2
13.1	5961.6	198.7	18.1	14408.3	144.0	23.1	20781.1	112.9	28.1	25900.3	92.8
13.2	6160.3	197.2	18.2	14552.3	143.1	23.2	20894.0	112.4	28.2	25993.1	92.5
13.3	6357.5	195.7	18.3	14695.4	142.4	23.3	21006.4	111.9	28.3	26085.6	92.1
13.4	6553.2	194.3	18.4	14837.8	141.6	23.4	21118.3	111.4	28.4	26177.7	91.9
13.5	6747.5	192.8	18.5	14979.4	140.9	23.5	21229.7	110.9	28.5	26269.6	91.5
13.6	6940.3	191.4	18.6	15120.3	140.0	23.6	21340.6	110.5	28.6	26361.1	91.2
13.7	7131.7	190.0	18.7	15260.3	139.4	23.7	21451.1	110.0	28.7	26452.3	90.9
13.8	7321.7	188.6	18.8	15399.7	138.6	23.8	21561.1	109.5	28.8	26543.2	90.5
13.9	7510.3	187.3	18.9	15538.3	137.9	23.9	21670.6	109.1	28.9	26633.7	90.3
14.0	7697.6	186.0	19.0	15676-2	137.1	24.0	21779.7	108.7	29.0	26724.0	89.9
14.1	7883.6	184.6	19.1	15813.3	136.5	24.1	21888.4	108.2	29.1	26813.9	89.6
14.2	8068.2	183.3	19.2	15949.8	135.7	24.2	21996.6	107.7	29.2	26903.5	89.3
14.3	8251.5	182.1	19.3	16085.5	135.0	24.3	22104.3	107.3	29.3	26992.8	89.1
14.4	8433.6	180.8	19.4	16220.5	134.3	24.4	22211.6	106.8	29.4	27081.9	88.7
14.5	8614.4	179.6	19.5	16354.8	133.7	24.5	22318.4	106.4	29.5	27170.6	88.4
14.6	8794.0	179.0	19.6	16488.5	132.9	24.6	22424.8	106.4	29.6	27259.0	88.1
14.7	8972.3	175.3	19.7	16621-4	132.3	24.7	22530.8	105.6	29.7	27347.1	87.8
14.8	9149.5		19.8	16753.7		24.8	22636.4	105.1	29.8	27434.9	87.6
14.9	9325.5	176.0	19.9	16885.3	131.6 131.0	24.9	22741.5		29.9	27522.5	87.2
15.0	9500.3	174.8	20.0	17016.3		25.0	22846.3	104.8	30.0	27609.7	86.9
15.1	9673.8	173.5	20.1	17146.6	130.3	25.1	22950.6	104.3	30.1	27696.6	86.7
15.2	9846.2	172.4	20.2	17276.3	129.7	25.2	23054.4	103.8	30.2	27783.3	
15.3	10017.5	171.3	20.3	17405-3	129.0	25.3	23157.9	103.5	30.3	27869.7	86.4
15.4	10187.7	170.2	20.4	17533.7	128.4	25.4	23261.0	103.1	30.4	27955.7	86.0
15.5	10356.8	169.1	20.5	17661-4	127.7	25.5	23363.6	102.6	30.5	28041.5	85.8
15.6	10524.8	168.0	20.6	17788-6	127.2	25.6	23465.9	102.3	30.6	28127.1	85.6
15.7	10691.8	167.0	20.7	17915-1	126.5	25.7	23567.7	101.8	30.7	28212.3	85.2
15.8	10857.7	165.9	20.8	18041.0	125.9	25.8	23669.2	101.5	30.8	28297.3	85.0
15.9	11022.5	164.8	20.9	18166.3	125.3	25.9	23770.3	101.1	30.9	28382.0	84.7
16.0	11186.3	163.8	21.0	18291.0	124.7	26.0	23871.0	100.7	31.0	28466.4	84.4

PART II.

Correction due to T — T', or the Difference of the Temperatures of the Barometers at the two Stations.

This Correction is Negative when the Temperature at the Upper Station is lowest, and vice vers i.

This correction is regarded when the reinfertation as the Opper Station is better, and correcting the Correction of Correcting the Correcting the Correcting the Correction of Correcting the Correction of Correcting the Correction of Correcting the Correction of Correc												
T — T'.	tion.	T — T'.	tion.	T — T'.	tion.	T - T'.	tion.	T — T'.	tion.	T — T'.	tion.	
Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	Fah't.	Feet.	
•		0		0						0		
1	2.3	14	32.8	27	63.2	40	93.6	53	124.1	66	154.5	
2	4.7	15	35.1	28	65.5	41	96.0	54	126.4	67	156.8	
3	7.0	16	37.5	29	67.9	42	98.3	55	128.7	68	159.2	
4	9.4	17	39.8	30	70.2	43	100.7	56	131.1	69	161.5	
5	11.7	18	42.1	31	72.6	44	103.0	57	133.4	70	163.9	
6	14.0	19	44.5	32	74.9	45	105.3	58	135.8	71	166.2	
7	16.4	20	46.8	33	77.3	46	107.7	59	138.1	72	168.6	
8	18.7	21	49.2	34	79.6	47	110.0	60	140.4	73	170.9	
9	21.1	22	51.5	35	81.9	48	112.4	61	142.8	74	173.3	
10	23.4	23	53.8	36	84.3	49	114.7	62	145.1	75	175.6	
11	25.8	24	56.2	37	86.6	50	117.0	63	147.5	76	177.9	
12	28.1	25	58.5	38	89.0	51	119.4	64	149.8	77	180.3	
13	30.4	26	60.9	39	91.3	52	121.7	65	152.2	78	182.6	
			T III.	2.2	PAI			PAR	T V.			
			the Chang			.			** 1 7 1 .6			

1				PART				PART			\mathbf{P}^{A}	RT	V.				ļį.
l				lue to t				IV.	_					C / 1 T			
١		Lat	titude o	of the P	lace of	Observ	ation.	Correction for	Corr	ection		the He Station		tne L	ower		
		Po N	ositive egative	from I from	at. 00 Lat. 45	to 450 ○ to 9(; ,o.	Decrease of Gravity			Alwa	ys Pos	itive.				il
1				Lati	tude.			on a	***		D	neter at	Tomos	. Otatio			
İ		00	100	200	300	400	450	Vertical. Always	He	ignt or	вагоп	ieter at	Lower	rotatic	л.		l
l	App. Alt.	900	800	700	600	500	450	Positive.	16 in.	18 in.	20 in.	22 in.	24 in.	26 in.	28 in.	App.	l
I	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	
}	1000	2.6	2.5	2.0	1.3	0.5	0	2.5	1.6	1.3	1.0	0.8	0.6	0.4	0.2	1000	ľ
١	2000	5.3	5.0	4.1	2.6	0.9	0	5.2	3.1	2.5	2.0	1.5	1.1	0.7	0.3	2000	li
l	3000	7.9	7.5	6.1	4.0	1.4	0	7.9	4.7	3.8	3.0	2.3	1.7	1.1	0.5	3000	
١	4000	10.6	10.0	8.1	5.3	1.8	0	10.8	6.3	5.1	4.0	3.1	2.2	1.4	0.7	4000	
ļ	5000	13.2	12.4	10.1	6.6	2.3	0	13.7	7.8	6.4	5.0	3.8	2.8	1.8	0.8	5000	
ì	6000	15.9	14.9	12.2	7.9	2.8	0	16.7	9.4	7.6	6.0	4.6	3.3	2.1	1.0	6000	
1	7000	18.5	17.4	14.2	9.3	3.2	0	19.9	11.0	8.9	7.1	5.4	3.9	2.5	1.2	7000	li
l	8000	21.2	19.9	16.2	10.6	3.7	0	23.1	12.5	10.2	8.1	6.2	4.4	2.8	1.3	8000	I
1	9000	23.8	22.4	18.3	11.9	4.1	0	26.4	14.1	11.4	9.1	6.9	5.0	3.2	1.5	9000	
1	10000	26.5	24.9	20.3	13.2	4.6	0	29.8	15.7	12.7	10.1	7.7	5.5	3.5	1.7	10000	
١	11000	29.1	27.4	22.3	14.6	5.1	0	33.3	17.2	14.0	11.1	8.5	6.1	3.9	1.8	11000	
1	12000	31.8	29.9	24.4	15.9	5.5	0	36.9	18.8	15.3	12.1	9.2	6.6	4.2	2.0	12000	
1	13000	34.4	32.4	26.4	17.2	6.0	0	40.6	20.4	16.5	13.1	10.0	7.2	4.6	2.2	13000	H
ı	14000	37.1	34.9	1	18.5	6.4	0	44.4	21.9	17.8	14.1	10.8	7.7	4.9	2.3	14000	l
1	15000	39.7	37.3	30.4	19.9	6.9	0	48.3	23.5	19.1	15.1	11.5	8.3	5.3	2.5	15000	1
1	16000	42.4		1	21.2	7.1	0	52.3	25.1	20.3	16.1	12.3	8.8	5.6	2.7	16000	H
İ	17000	45.0	42.3	$^{+}_{-34.5}$	22.5	7.8	0	56.4	26.6	21.6	17.1	13.1	9.4	6.0	2.8	17000	
l	18000	47.7	1	1	23.8	8.3	0	60.5	28.2	22.9	18.1	13.8	9.9	6.3	3.0	18000	۱
1	19000	50.3		38.6	25.2	8.7	0	64.8	29.8	24.1	19.2	14.6	10.5	6.7	3.2	19000	ď
1	20000	53.0	49.8	40.6	26.5	9.2	0	69.2	31.3	25.4	20.2	15.4	11.0	7.0	3.3	20000	۱
1	21000	55.6				9.7	0	73.6	32.9	26.7	21.2	16.1	11.6	7.4	3.5	21000	H
	22000	58.3	-			10.1	0	78.2	34.5	28.0	22.2	16.9	12.1	7.7	3.7	22000	,
	23000	60.9				10.6	0	82.9	36.0	29.2	23.2	17.7	12.7	8.1	3.8	23000	
	24000	63.6	1	!		11.0	0	87.6	37.6	30.5	24.2	18.5	13.2	8.4	4.0	24000	,
	25000			50.7	33.1	11.5	0	92.5	39.1	31.8	25.2	19.2	13.8	8.8	4.1	25000	,
	1							**									-1

IV.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANY OTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

The following tables, published by M. C. Diffe, in the Astronomische Nachrichten, No. 1056, November, 1856, are a modification and extension of Gauss's tables, published in Schumacher's Jahrbuch, for 1836 and the following years, which are based on the formula of Laplace. In this new form they answer a double purpose. They give the means of solving a problem which often occurs in Meteorology, viz.: The difference of elevation between two stations, and the temperature of the air at both, being known, to reduce the height of the barometer at one of the stations to the height it would have at the other. They are likewise adapted to the computation of heights from barometrical observations.

The formula of Laplace, which has been used, the Metres being reduced to Toises, and the Centigrade degrees to degrees of Reaumur, reads as follows:

$$h = 940\overline{7.73} \left(1 + \frac{t+t'}{400}\right) \left(1 + a \cos 2 \phi\right) \left(1 + \frac{h}{r}\right) \left\{\log \frac{b}{b'} + 2 \log \left(1 + \frac{h}{r}\right)\right\}.$$

Where t and t' = the temperatures of the air, in degrees of Reaumur, at the lower and upper station,

b and b' = the height of the barometer, in any scale, reduced to the freezing point, at the lower and upper station,

h = the difference of level, in toises, between the two stations,

r = the distance, in toises, of the lower station to the centre of the Earth,

 ϕ = the latitude of the place of observation,

a = the increase of gravity from the equator to the poles.

Making, besides, m = the modulus of the common logarithms, the formula becomes, with sufficient accuracy,

$$\log b - \log b' = h \left\{ \frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t + t'}{400}} - \frac{2 m}{r} \right\} \cdot \frac{1}{1 + a \cos 2 \phi} \cdot \frac{1}{1 + \frac{h}{r}}.$$

Assuming τ , or the radius of the Earth, at 45° latitude = 3266631 toises, and a = 0.002595, instead of 0.002845 adopted in Gauss's tables, and making

$$u = \log b - \log b',$$

$$a = \log \left(\frac{1}{9407.73} \cdot \frac{1}{1 + \frac{t + t'}{400}} - \frac{2m}{r}\right),$$

$$c = -m a \cos 2\phi,$$

$$c' = -\frac{mh}{r},$$

then the reduction of the height of the barometer to another level is given by the formula,

BAROMETRICAL MEASUREMENT OF HEIGHTS.

1.
$$\log u = \log h + a + c + c';$$

$$2. \quad \log b = \log b' + u.$$

Table I. contains the values of a for the argument t+t'; 10 units are to be subtracted from the characteristic.

Table II. gives the values of c for the argument ϕ , or the correction for the change of gravity in latitude, which is negative from 0° to 45°, positive from 45° to 90°.

Table III. furnishes the values of e' for the argument h in toises, or the correction for the decrease of gravity on the vertical. Both in Tables II. and III. the values of c and c' are given in units of the fifth decimal place.

The difference of elevation of the two stations is given by the formula,

1.
$$u = \log b - \log b',$$

2.
$$\log h = \log u + A + c + c'$$
,

in which A is the arithmetical complement of a, and the corrections c and c' receive contrary signs. For the sake of convenience, the values of A have been placed in Table II, and in Table III. the correction for A is found in another column, with the more convenient argument $v = \log u + \Lambda$.

If the heights of the barometers have not been reduced to the freezing point, then, B and B' being the unreduced heights of the barometers, and T and T' the temperature of the attached thermometer in degrees of Reaumur,

$$b:b'=rac{\mathrm{B}}{1+rac{\mathrm{T}}{4440}}:rac{\mathrm{B}'}{1+rac{\mathrm{T}'}{4440}}$$

and making $\frac{m}{4440} = \beta$,

$$u = \log b - \log b' = (\log B - \beta T) - (\log B' - \beta T').$$

Instead of $\beta = 0.000098$, we can write with sufficient accuracy 0.00010.

Use of the Tables.

These tables can be used in any latitude, and for any barometrical scale; but the indications of the barometers must be reduced to the freezing point; and the temperatures of the air must be given in degrees of Reaumur. The tables suppose the use of logarithms with 5 decimals, such as those of Lalande, and give the results in toises.

I. For Reducing Barometrical Observations to another Level.

Given h in toises, t, t', ϕ , and b or b'. To find b or b'.

In Table I. with the argument t + t', take a, In Table II. with the argument ϕ , take c, In Table III. with the argument h, take c',

the last two corrections being given in units of the fifth decimal, making

$$\log h + a + c + c' - 10$$
 (whole units) = $\log u$.

Then we have

for a level lower by h toises, $\log b = \log b' + u$; for a level higher by h toises, $\log b' = \log b - u$.

If h, or the difference of elevation, is given in metres, take c', which is always negative, from Table III. (for A) with the argument $v = \log h + 9.71$, and write

$$\log u = 9.71018 + \log h + a + c + c' - 10$$
 (whole units).

Then again is $\log b = \log b' + u$.

Example 1.

Suppose the height of the barometer, reduced to the freezing point, to be b' =295.39 Paris lines; the temperature of the air $t'=11^{\circ}.8$ Reaumur, and the latitude $\phi = 51^{\circ} 48'$; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer, reduced to the freezing point, at a station lower by h = 498.2 to see?

In the case $t = t' + 4^{\circ}.98 = 16^{\circ}.78$, and $t + t' = 28^{\circ}.58$.

Then

Table I. for 28°.58 gives
$$a = 5.99538$$
Table II. for 51° 48′ gives $c = +0.00026$
Table III. for 498 toises gives $c' = -0.00007$

$$\log u = 8.69297 - 10$$

$$u = 0.04931$$

$$\log b = 2.47040$$

$$\log b = 2.51971$$
Barometer at the lower station $b = 330.90$ Paris lines.

Example 2.

Suppose the reduced barometer b' = 598.6 millimetres; the temperature of the air $t'=18^{\circ}.0$ Centigrade = 14°.4 Reaumur; the difference of elevation h=2217metres; $\phi = 3^{\circ}$. The temperature of the air at the lower station $t = 27^{\circ}.5$ Centigrade = 22°.0 Reaumur, and t + t' = 36°.4 Reaumur.

Then
$$\log h = \begin{cases} \log 2217 = 3.34577 \\ + 9.71018 \\ \hline 3.05595 \end{cases} \quad v = 3.06 \\ a = 5.98750 \\ c = -0.00112 \\ c' = -0.00015 \\ \log u = 9.04218 - 10 \\ u = 0.11020 \\ \log b' = 9.77714 \\ \log b = 9.88734 \\ Barometer at the lower station $b = 771.5$ millimetres.$$

For Computing Differences of Elevation from Barometrical Observations.

Given the unreduced height of the barometer at the lower and upper station, B and B'; the temperatures of the attached thermometers, T and T'; the temperatures of the air, t and t'; and the latitude, ϕ .

To find h, or the difference of elevation between the two stations.

Subtract (log B' - 10 T') from (log B - 10 T), paying due attention to the nature of the signs of T and T', and taking the numbers 10 T and 10 T' as units of the fifth decimal. Calling then $(\log B - 10 T) - (\log B' - 10 T') = u$, or if the heights of the Barometers are reduced to the freezing point, $\log b - \log b' = u$, take,

In Table I., A with the argument t + t', and make $v = \log u + A$. In Table II., with the argument ϕ , take c reversing the sign.

In Table III., for A, with the argument v, take c', which, in this case, is always positive; then, remembering that the values of c and c' are given in units of the fifth decimal, we have,

$$\begin{array}{lll} v + c + c' & = \log h \text{ in toises,} \\ v + c + c' + 0.28982 = \log h \text{ in metres,} \\ v + c + c' + 0.80584 = \log h \text{ in English feet.} \end{array}$$

Example 1.

L. station B = 329.013 Paris lines; T =
$$+15.88$$
 R.; $t = +15.96$ R.; $\phi = 45.32$.
U. station B' = 268.215 Paris lines; T' = $+8.40$ R.; $t = +7.92$ R.
 $t + t' = 23.88$ R.

$$\log B = 2.51722 - 10 \times 15.88 = 2.51563$$

$$\log B' = 2.42848 - 10 \times 8.4 = 2.42764$$

$$u = 0.08799$$

$$\log u = 8.94443$$

$$A = 3.99982$$

$$v = 2.94425$$

$$c = -0.00002$$

$$c' = +0.00012$$

$$\log h = 2.94435$$

$$h = 879.74 \text{ toises.}$$

Example 2.

```
L. station B = 763.15 millimetres; T = t = 25.3 Cent. = 20.24 R.; \phi = 21.0 U. station B' = 600.95 millimetres; T' = t' = 21.3 Cent. = 17.04 R.
                                                           t + t' = 37.28 \,\mathrm{R}.
                \log B = 9.88261 - 10 \times 20.24 =
                                                               9.88059
                \log B' = 9.77884 - 10 \times 17.04 =
                                                               9.77714
                                                               0.10345
                                                 \log u =
                                                               9.01473
                                                     A =
                                                               4.01337
                                                               3.02810
                                                     v =
                                                     c = +0.00084
                                                     c' = +0.00014
                                                              3.02908 for toises.
                                                 \log h =
                                                               0.28982
                                                 \log h =
                                                               3.31890 for metres.
                                                 \log h =
                                                               3.02908 for toises.
                                                               0.30584
```

 $\log h =$

h = 1069.3 toises = 2084.0 metres = 6837.9 English feet.

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3.83492 for English feet.

I. Argument: Sum of the Temperatures of the Air in Degrees of Reaumur.

		Correction for				Correction for	
t+t'				t+t'		1	
Reaumur.	a	Difference.	\mathbf{A}	Reaumur.	a	Difference.	A
-60°	6.09617	100	3.90383	-20°	6.01776	115	3.95224
-59	6.09489	128	3.90511	-19	6.04661	1	3.95339
-58	6.09362	127	3.90638	-18	6.04547	114	3.95453
-57	6.09235	127	3.90765	-17	6.04434	113	3.95566
-56	6.09108	127 126	3.90\$92	-16	6.04320	114	$\boldsymbol{3.95680}$
-55	6.08982		3.91018	-15	6.01207		3.95793
-54	6.08856	126	3.91144	-14	6.04094	113	3.95906
-53	6.08730	126	3.91270	-13	6.03981	113	3.96019
-52	6.08605	125	3.91395	-12	6.03869	112	3.96131
-51	6.08480	125 124	3.91520	-11	6.03757	112	3.96243
-50	6.08356		3.91644	-10	6.03645		3.96355
- 19	6.08231	125	3.91769	- 9	6.03533	112	3.96467
-48	6.03108	123	3.91892	- 8	6.03422	111	3.96578
-47	6.07984	124	3.92016	- 7	6.03311	111	3.96689
-46	6.07861	123 123	3.92139	- 6	6.03201	110	3.96799
-45	6.07738		3.92262	- 5	6.03090		3.96910
-44	6.07616	122	3.92384	- 4	6.02980	110	3.97020
-43	6.07494	122	3.92506	- 3	6.02871	109	3.97129
-42	6.07372	122	3.92628	- 2	6.02761	110	3.97239
-41.	6.07250	122	3.92750	- 1	6.02652	109	3.97348
-40	6.07129		3.92871	0	6.02543		3.97457
-39	6.07009	120	3.92991	+ 1	6.02434	109	3.97566
-38	6.06888	121	3.93112	2	6.02326	108	3.97674
-37	6.06768	120	3.93232	3	6.02217	109	3.97783
-36	6.06648	120 119	3.93352	4	6.02109	108	3.97891
-35	6.06529		3.93471	5	6.02002		3.97998
-31	6.06410	119	3.93590	6	6.01895	107	3.98105
-33	6.06291	119	3.93709	7	6.01787	108	3.98213
-32	6.06173	118	3.93827	8	6.01680	107	398320
-31	6.06055	118	3.93945	9	6.01574	106	3.98426
-30	6.05937	110	3.94063	10	6.01468	106	3.98532
-29	6.05819	118	3.94181	11	6.01362	106	3.98638
-28	6.05702	117	3.94298	12	6.01256	106	3.98744
-27	6.05585	117	3.94415	13	6.01150	105	3.98850
-26	6.05469	116	3.94531	14	6.01045	105	3.98955
-25	6.05352		3.94648	15	6.00940	105	3.99060
-24	6.05236	116	3.94764	16	6.00835	105	3.99165
-23	6.05121	115	3.94879	17	6.00731	104	3.99269
-22	6.05005	116	3.94995	18	6.00626	105	3.99374
-21	6.04890	115	3.95110	19	6.00522	104	3.99478
-20	6.01776	114	3.95224	+20	6.00418	104	3.99582

(Continued.)

								Onte	nued.)							
t +	· t'			Correct	ion for	r			t+t'			Co	rrection f	or		
Reaun	1	a		Differe	ence.		A		Reaumur.		a	I	Difference.		A	
+20	· -	6.00	118	-	_	3	99582	-	+40°	5.0	 983	93		4.0	1607	
21		6.00:		10	3		99685		41		982		99	i	1706	
22		6.002		10:	3		99788		42		981		99		1805	
	1			10	4							J	98	1		
23	- 1	6.001		10	2		99892	- 11	43		980	j	99		1903	
24	·	6.000)06	10	3	3.	99994		44	5.	979	98	98	4.0	2002	
25		5.999		10	2		00097		45		979		97		2100	
26		5.998	801	10		4.	00199		46	5.	978	03	98	4.0	2197	
27		5.996	599	10		4.	00301		47	5.9	977	05	97	4.0	2295	
28		5.993	597	1		4.	00403	i	48	5.	976	808		4.0	2392	
29		5.99	195	10		4.	00505		49	5.9	975	11	97 97	4.0	2489	
30		5.998	394		.	4.	00606		50	5.	974	114		4.0	2586	
31		5.992	293	10	- 1	4.	00707		51	5.	973	317	97	4.0	2683	
32		5.991	192	10	}	4.	00808	-	52	5.	972	221	96	4.0	2779	
33		5.990		10	1		00909		53	1	971		97		2876	
34		5.989		10	1		01009		54	1	970		96 95	1	2972	
35		5.988	390	10	'	4.	01110		55	5.	969	333	90	4.0	3067	
36		5.987		10	- 1		01210	- 1	56		968		96		3163	
37		5.986		9	9		01309		57	5.96742			95		4.03258	
38		5.983		10	0		01409		58		966	1	96		3354	
39		5.98		9	9		01508		59		965		95	F	4.03449	
II.	. La			- COR			FOR	a.		VEI	RT1		- Corr	For A,	arg. v,	
ϕ	c	φ	φ	c	φ	φ	c	φ	$-\left\ \begin{array}{c} - \\ h \end{array} \right\ $	c	_	h	c'	v	c'	
-		0			0	-			_						-	
0	-113+	90	15	-98+	75	30	-56+	60	100		1	1600	21	1.8	1	
1	113	89	16	96	74	31	53	59	□ 200)	3	1700	23	1.9	1	
2	112	88	17	93	73	3 2	49	58	300)	4	1800	24	2.0	1	
3	112	87	18	91	72	33	46	57	400)	5	1900	25	2.1	2	
4	112	86	19	89	71	34	42	56	500)	7	2000	27	2.2	2	
			l .			l								2.3	3	
5	111	85	20	86	70	35	39	55	600)	8	2100	28	2.4	3	
6	110	84	21	84	69	36	35	54	700		9	2200	29	2.5	4	
7	109	83	22	81	68	37	31	53	800) 1	1	2300	31	2.6	5	
8	103	82	23	78	67	38	27	52	1	1	2	2400	32	2.7	7	
9	107	81	24	75	66	39	23	51	- 11		3	2500	33	2.8	8	
				-	-									2.9	11	
10	106	80	25	72	65	40	20	50	1100	1	5	2600	35	3.0	13	
11	104	79	26	69	61	41	16	49	- 14	- 1	6	2700	36	3.1	17	
12	103	78	27	66	63	42	12	48		_	7	2800	37	3.2	21	
13	101	77	28	63	62	43	8	47	H	- 1	9	2900	39	3.3	27	
14	101	76	29	60	61	44	4	46	- []	1	0	3000	40	3.4	33	
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1,-	00.		90	501	cΛ	4.5		4.5	1,000		, I	3500	177		53	
15	-98+	75	30	-56+	60	45	-0+	45	1600	2	1	3000	47	3.6	- 53	

V.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

In No. 1088 of the Astronomische Nachrichten, published in June, 1857, Dr. Dippe gives the following set of Tables for reducing barometrical observations to another level, and for computing heights. These tables, being based, as the preceding ones (IV.), on the formula of Laplace, and computed with the same constants, give results nearly identical, but dispense with the use of logarithms.

USE OF THE TABLES.

The tables suppose the height of the barometer to be expressed in French inches or Paris lines, and the temperature in degrees of Reaumur; they give the differences of level in French toises.

The signs used have the following signification: -

At Lower Station. $\begin{cases} B = \text{Observed Height of Barometer in Paris lines.} \\ T = \text{Attached Thermometer in degrees of Reaumur.} \\ b = \text{Barometer reduced to the freezing point.} \\ t = \text{Temperature of the air, detached Thermometer.} \end{cases}$ At Upper Station. $\begin{cases} B' = \text{Observed Height of Barometer.} \\ T' = \text{Attached Thermometer.} \\ b' = \text{Barometer at the freezing point.} \\ t' = \text{Temperature of the air.} \\ \phi = \text{Latitude of the place.} \\ h = \text{Difference of elevation between the two stations.} \end{cases}$

I. For Reducing Barometrical Observations to another Level.

Given, h in toises, t, t', ϕ , and b or b'. To find b or b'.

Make first
$$2 \tau = \frac{t+t}{2}$$
 and τ , and

 \mathbf{D}

In Table I., with the argument 2τ , take τ' ; In Table III., with the arguments h and τ , take C; In Table IV., with the arguments h and ϕ , take C';

Make, further,

$$u = h + C + C'$$
 and $\frac{u}{100} \tau'$;

And if b' be given, and b required,

In Table II., with the argument b, take H;

then is

$$H = H' + (u - \frac{u}{100} \tau'),$$

and the height of the barometer, in Table II., due to H, is b required.

If b be given, and b' required for a level higher by h toises, then,

In Table II., with the argument b, take H'.

Make, further,

$$H' = H - (u - \frac{u}{100} \tau'),$$

and b' is the height of the barometer in Table II., corresponding to H'.

Example 1.

Suppose the height of the barometer reduced to the freezing point to be b'=295.39 Paris lines; the temperature of the air $t'=11^{\circ}.8$ Reaumur; and the latitude $\phi = 51^{\circ}.48$; the increase of heat downwards being 1° Reaumur for 100 toises. What is the height of the barometer reduced to the freezing point, at a station lower by h = 498.2 to ses?

In this case,
$$t'=11^{\circ}.8$$
; $t=11^{\circ}.8+4^{\circ}.98$; $t+t'=28^{\circ}.58$; $2\tau=\frac{t+t}{2}=14^{\circ}.29$; $\tau=7^{\circ}.15$; and according to Table I. $\tau'=+6.67$.

With h and τ , in Table III., we find C = -1.4With h and ϕ , in Table IV., we find C' = + 0.3

We add
$$h = 498.2$$
 and we have $u = 497.1$; $u = 4.971$ $\tau' = +6.67$ $-\frac{u}{100} \tau' = -33.15$ 0.2983 0.298 0.34 With b' , in Table II., we find H' 0.2983 0.34 0.34 0.34 0.35 0.34 0.35 0.34 0.35

With b', in Table II., we find H' =H =831.81

Finally, with H, in Table II., we find b = 330.91 Paris lines, which is the required height of the barometer at the lower station. Gauss's tables (IV.) would give b =330.90 lines.

Example 2.

Suppose b'=330.46 Paris lines; $t'=-12^{\circ}.3$ Reaumur; h'=92.7 toises; $\phi = 62^{\circ}$.

In this case, assuming t = t',

$$2\tau = \frac{t+t'}{2} = -12^{\circ}.3; \ \tau = -6.15;$$

and according to Table I.

$$r' = -6.55.$$

With h and τ , in Table III., take C = -0.2

With h and ϕ , in Table IV., take C' = + 0.1

Add
$$h = 92.7$$

We have $u = 92.6$
 $-\frac{u}{100}\tau' = +6.07$
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With b', in Table II., take H' =

$$H = 924.89$$

With H, in Table II., we find b = 338.53 Paris lines. Gauss's tables (IV.) would give b = 338.54 lines.

II. For Computing Differences of Elevation from Barometrical Observations.

Suppose to be given B, B', T, T', t, t', ϕ ; required h.

Make first
$$\tau = \frac{t+t'}{4}$$
 and $T-T'$.

Then in Table II., with the argument { B take H, B' take H',

and make

$$u = (H - H') + \frac{H - H'}{100} \tau - (T - T'),$$

in which each full degree of T - T' corresponds to a toise.

Further, in Table III., with u and τ , take C reversing the sign;

in Table IV., with u and ϕ , take C' reversing the sign;

in Table V., with T - T' and τ , take C' with the signs of T - T'.

Then the difference of elevation required is

$$h = u + C + C' + C''.$$

If the heights of the barometer, reduced to the freezing point, or b and b', are given,

then in Table II., with the argument, $\begin{cases} b \text{ take H} \\ b' \text{ take H'}, \end{cases}$

and make

$$u = H - H' + \frac{H - H'}{100} \tau.$$

Further, in Table III., take C reversing the sign; in Table IV., take C' reversing the sign;

and

$$h = u + C + C'.$$

Example 1.

Suppose to be given,

In Table II. with B take H = 864.9
"with B' take H' = 291.2
H — H' = 573.7

$$\frac{\text{II} - \text{II}'}{100} \tau = 49.06$$

 $\frac{11 - \text{II}'}{100} = 5.737$
 $\frac{11 - \text{II}'}{100} = 5.737$
 $\frac{11 - \text{II}'}{100} = \frac{1.7}{2.87}$
 $\frac{1.7 - \text{II}'}{100} = \frac{1.7}{2.9}$
 $\frac{1.7 - \text{II}'}{100} = \frac{2.9}{49.06}$
 $\frac{1.7 - \text{II}'}{100} = \frac{2.9}{49.06}$

In Table III., with u and τ , take C = +1.8 In Table IV., with u and ϕ , take C' = -0.2 In Table V., with T - T' and τ take C" = 0.0

Difference of elevation, or h = 623.66 to ses.

Gauss's Tables give 623.64 toises.

Example 2.

Suppose to be given,

$$b = 342.68$$
 Paris lines; $t = -10^{\circ}.38$ Reaumur; $\phi = 65^{\circ}.$ $b' = 285.47$ Paris lines; $t' = -14^{\circ}.94$ Reaumur; $T - T' = 0^{\circ}.$ R.

$$t + t' = -25^{\circ}.32$$

 $\tau = -6.33$

In Table II. with
$$b$$
 take $H = 974.58$
"with b' take $H' = 228.28$
 $H - H' = 746.30$

$$H - H' = 746.30$$
 $II - II'$
 $100 \tau = -47.24$
 $u = 699.06$
 $II - II'$
 $\tau = -47.24$
 $u = 699.06$
 $II - II'$

In Table III., with
$$u$$
 and τ , take $C = +1.8$
In Table IV., with u and ϕ , take $C' = -1.2$

h = 699.66

Gauss's Tables give h = 699.72 toises.

V.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION, BY M. C. DIPPE.

Table I. - Argument, the observed Height of the Barometer at either Station.

Barom-					Tenths	of a Line.				
eter iu Paris Lines.	0	1	2	3	4	5	6	7	8	9
B or B'		<u>'</u>			II or II' i	n Toises =		·		
270	0.7	2.2	3.7	5.2	6.7	8.2	9.7	11.2	12.8	14.3
271	15.8	17.3	18.8	20.3	21.8	23.3	24.8	26.3	27.8	29.3
272	30.8	32.3	33.8	35.3	36.8	38.3	39.8	41.3	42.8	44.3
273	45.8	47.3	48.8	50.3	51.8	53.3	54.8	56.3	57.8	59.3
274	60.8	62.2	63.7	65.2	66.7	68.2	69.7	71.2	72.7	74.1
275	75.6	77.1	78.6	80.1	81.6	83.1	84.5	86.0	87.5	89.0
23 Inch.	ĺ					ĺ				
276	90.5	91.9	93.4	94.9	96.4	97.9	99.3	100.8	102.3	103.8
277	105.2	106.7	108.2	109.7	111.1	112.6	114.1	115.6	117.0	118.5
278	120.0	121.4	122.9	124.4	125.8	127.3	128.8	130.2	131.7	133.2
279	134.6	136.1	137.6	139.0	140.5	142.0	143.4	144.9	146.3	147.8
280	149.3	150.7	152.2	153.6	155.1	156.5	158.0	159.5	160.9	162.4
281	163.8	165.3	166.7	168.2	169.6	171.1	172.5	174.0	175.4	176.9
282	178.3	179.8	181.2	182.7	184.1	185.6	187.0	188.5	189.9	191.4
283	192.8	194.2	195.7	197.1	198.6	200.0	201.4	202.9	204.3	205.8
284	207.2	208.6	210.1	211.5	213.0	214.4	215.8	217.3	218.7	220.1
285	224.6	223.0	224.4	225.9	227.3	228.7	230.2	231.6	233.0	234.5
286	235.9	237.3	238.7	240.2	241.6	243.0	244.4	245.9	247.3	248.7
287	250.1	251.6	253.0	254.4	255.8	257.3	258.7	260.1	261.5	262.9
24 Inch.										
288	264.4	265.8	267.2	268.6	270.0	271.4	272.9	274.3	275.7	277.1
289	278.5	279.9	281.3	282.8	284.2	285.6	287.0	288.4	289.8	291.2
290	292.6	294.0	295.4	296.8	298.3	299.7	301.1	302.5	303.9	305.3
291	306.7	308.1	309.5	310.9	312.3	313.7	315.1	316.5	317.9	319.3
292	320.7	322.1	323.5	324.9	326.3	327.7	329.1	330.5	331.9	333.3
293	334.7	336.1	337.5	338.9	340.2	341.6	343.0	344.4	345.8	347.2
294	348.6	350.0	351.4	352.8	354.2	355.5	356.9	358.3	359.7	361.1
295	362.5	363.9	365.2	366.6	368.0	369.4	370.8	372.2	373.5	374.9
296	376.3	377.7	379.1	380.4	381.8	383.2	384.6	385.9	387.3	388.7
297	390.1	391.5	392.8	394.2	395.6	397.0	398.3	399.7	401.1	402.4
298	403.8	405.2	406.5	407.9	409.3	410.7	412.0	413.4	414.8	416.1
299	417.5	418.9	420.2	421.6	423.0	424.3	425.7	427.1	428.4	429.8
25 Inch			ł							
300	431.1	432.5	433.9	435.2	436.6	437.9	439.3	440.7	442.0	443.4
301	441.7	446.1	447.5	448.8	450.2	451.5	452.9	454.2	455.6	456.9
302	458.3	459.6	461.0	462.3	463.7	465.0	466.4	467.8	469.1	470.5
303	471.8	473.1	474.5	475.8	477.2	478.5	479.9	481.2	482.6	483.9
304	485.3	486.6	487.9	489.3	490.6	492.0	493.3	494.7	496.0	497.3
305	498.7	500.0	501.4	502.7	504.0	505.4	506.7	508.0	509.4	510.7
306	512.0	513.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0

TABLE I. Continued.

Barom-					Tenths	of a Line.				
eter in Paris Lines.	0	1	2	3	4	5	6	7	8	9
306	512.0	513.4	514.7	516.0	517.4	518.7	520.1	521.4	522.7	524.0
307	525.4	526.7	528.0	529.4	530.7	532.0	533.4	534.7	536.0	537.4
308	538.7	540.0	541.3	542.6	544.0	545.3	546.6	547.9	549.3	550.6
309	551.9	553.2	554.6	555.9	557.2	558.5	559.8	561.2	562.5	563.8
310	565.1	566.4	567.8	569.1	570.4	571.7	573.0	574.3	575.6	576.9
311	578.3	579.6	580.9	582.2	583.5	584.8	586.1	587.5	588.8	590.1
26 Inch.	0.0.0	0.5.0	000.3	902.2	000.0	904.0	930.1	907.9	900.0	390.1
312	591.4	592.7	594.0	595.3	596.6	597.9	599.2	600.6	601.9	603.2
313	604.5	605.8	607.1	608.4	609.7	611.0	612.3	613.6	614.9	616.2
314	617.5	618.8	620.1	621.4	622.7	624.0	625.3	1		1
	П		1	1				626.6	627.9	629.2
315	630.5	631.8	633.1	634.4	635.7	637.0	638.3	639.5	640.8	642.1
316	643.4	644.7	646.0	647.3	648.6	649.9	651.2	652.5	653.8	655.1
317	656.3	657.6	658.9	660.2	661.5	662.8	664.1	665.4	666.6	667.9
318	669.2	670.5	671.8	673.1	674.3	675.6	676.9	678.2	679.5	680.8
319	652.0	683.3	684.6	685.9	687.2	688.4	689.7	691.0	692.3	693.6
320	694.8	696.1	697.4	698.7	699.9	701.2	702.5	703.8	705.0	706.3
321	707.6	708.9	710.1	711.4	712.7	713.9	715.2	716.5	717.7	719.0
322	720.3	721.6	722.8	724.1	725.4	726.6	727.9	729.2	730.4	731.7
323	733.0	734.2	735.5	736.7	738.0	739.3		İ	1	1
323 27 Inch.	100.0	104.2	155.5	100.1	133.0	159.5	740.5	741.8	743.1	744.3
324	745.6	746.8	748.1	749.4	750.6	751.9	753.2	754.4	755.7	756.9
325	758.2	759.4	760.7	761.9	763.2	764.5	765.7			1
	770.7	772.0	773.2		1	777.0		767.0	768.2	769.5
326	11	l .	1	774.5	775.7		778.2	779.5	780.7	782.0
327	783.2	784.5	785.7	787.0	788.2	789.5	790.7	792.0	793.2	794.5
328	795.7	797.0	798.2	799.4	800.7	801.9	803.2	804.4	805.7	806.9
329	808.2	809.4	810.6	811.9	813.1	814.4	815.6	816.8	818.1	819.3
330	820.6	821.8	823.0	824.3	825.5	826.7	828.0	S29.2	830.4	831.7
331	832.9	834.2	835.4	836.6	837.9	839.1	840.3	841.6	842.8	844.0
332	815.2	846.5	847.7	848.9	850.2	851.4	852.6	853.9	855.1	856.3
333	857.5	858.8	860.0	861.2	862.4	863.7	864.9	866.1	867.3	868.6
334	869.8	871.0	872.2	873.4	874.7	875.9	877.1	878.3	879.6	880.8
335	882.0	883.2	884.4	885.7	886.9	888.1	889.3	890.5	891.7	593.0
353 28 Inch	002.0	000.2	004.4	000.1	030.5	000.1	009.3	030.5	091.7	030.0
336	894.2	895.4	896.6	897.8	899.0	900.3	901.5	902.7	903.9	905.1
337	906.3	907.5	908.7	909.9	911.2	912.4	913.6	914.8	916.0	917.2
	918.4	919.6	920.8	922.0	923.3			926.9	928.1	1
338	11	1	1			924.5	925.7			929.3
339	930.5	931.7	932.9	934.1	935.3	936.5	937.7	938.9	940.1	941.3
340 341	942.5 954.5	943.7	944.9 956.9	946.1 958.1	947.3 959.3	948.5 960.5	949.7	950.9 962.9	952.1 964.1	953.3 965.3
941	334.3	330.1	330.3	330.1	333.3	300.3	301.7	302.3	304.1	909.9
342	966.5	967.7	968.9	970.1	971.3	$972\ 5$	973.7	974.8	976.0	977.2
343	978.4	979.6	980.8	982.0	983.2	984.4	985.6	986.8	957.9	989.1
344	990.3	991.5	992.7	993.9	995.1	996.2	997.4	998.6	999.8	1001.0
315	1002.2	1003.4	1004.5	1005.7	1006.9	1008.1	1009.3	1010.5	1011.6	1012.8
346	1014.0	1015.2	1016.4	1017.5	1018.7	1019.9	1021.1	1022.3	1023.4	1024.6
347	1025.8	1027.0	1028.1	1029.3	1030.5	1031.7	1032.8	1034.0	1035.2	1036.4
29 Inch									-	
348	1037.5	1038.7	1039.9	10 (1.1	1042.2	1043.4	1014.6	1045.8	1046 9	1018.1

TABLE II.

CORRECTION FOR THE TEMPERATURE OF THE AIR.

Argument, $2\tau = \frac{t+t'}{2}$.

2 τ -25 -24 -23	-14.29 -13.64 -13.00	0.65 0.64	2 τ -12 -11 -10	-6.38 -5.82 -5.26	0.56 0.56	2 τ + 1 2 3	+0.50 0.99 1.48	0.49 0.49	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	7' + 6.54 6.98 7.41	0.44 0.43
-22 -21 -20	-12.36 -11.73 -11.11	0.64 0.63 0.62	- 9 - 8	-4.71 -4.17 -3.63	0.55 0.54 0.54	4 5 6	1.96 2.44 2.91	0.48 0.48 0.47	17 18 19	7.83 8.26 8.68	0.42 0.43 0.42
-19 -18 -17 -16	-10.50 - 9.89 - 9.29 - 8.70	0.61 0.61 0.60 0.59 0.59	- 6 - 5 - 4 - 3	-3.09 -2.56 -2.04 -1.52	0.54 0.53 0.52 0.52 0.51	7 8 9 10	3.38 3.85 4.31 4.76	0.47 0.47 0.46 0.45 0.45	20 21 22 23	9.09 9.50 9.91 10.31	0.41 0.41 0.41 0.40 0.40
-15 -14 -13 -12	- 8.11 - 7.53 - 6.95 - 6.38	0.58 0.58 0.57	$\begin{vmatrix} -2 \\ -1 \\ 0 \\ +1 \end{vmatrix}$	-1.01 -0.50 0.00 +0.50	0.51 0.50 0.50	11 12 13 +14	5.21 5.66 6.10 $+6.54$	0.45 0.44 0.44	24 25 26 +27	10.71 11.11 11.50 +11.89	0.40 0.39 0.39

TABLE III. FOR C.

Arguments, h and τ .

In computing Heights reverse the signs of C. — Arguments, τ and u.

h, (u)	1			τ, in Deg	rees of Rea	umur =			
Toises.	-16 °	-12°	-8°	_4°	0°	+4°	+8°	+12°	+160
50	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
100	0.2	0.2	0.2	0.2	0.3	0.3	0.3	0.3	0.3
150	0.3	0.3	0.4	0.4	0.4	0.4	0.4	0.4	0.4
200	0.4	0.5	0.5	0.5	0.5	0.5	0.6	0.6	0.6
250	0.5	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.7
300	0.7	0.7	0.7	0.7	0.8	0.8	0.8	0.9	0.9
350	0.8	0.8	0.8	0.9	0.9	0.9	1.0	1.0	1.1
400	0.9	0.9	1.0	1.0	1.0	1.1	1.1	1.2	1.2
450	1.0	1.1	1.1	1.1	1.2	1.2	1.3	1.3	1.4
500	1.1	1.2	1.2	1.3	1.3 .	1.4	1.4	1.5	1.5
550	1.2	1.3	1.4	1.4	1.5	1.5	1.6	1.6	1.7
600	1.4	1.4	1.5	1.6	1.6	1.7	1.7	1.8	1.9
650	1.5	1.6	1.6	1.7	1.8	1.8	1.9	1.9	2.0
700	1.6	1.7	1.8	1.8	1.9	2.0	2.0	2.1	2.2
750	1.7	1.8	1.9	2.0	2.0	2.1	2.2	2.3	2.3
800	1.9	2.0	2.0	2.1	2.2	2.3	2.4	2.4	2.5
850	2.0	2.1	2.2	2.3	2.3	2.4	2.5	2.6	2.7
900	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9
950	2.3	2.4	2.5	2.6	2.7	2.7	2.9	3.0	3.1
1000	2.4	2.5	2.6	2.7	2.8	2.9	3.1	3.2	3.3

 $\label{eq:Table IV. For C'.}$ correction in toises for the change of gravity in latitude.

In computing Heights, reverse the signs of C'. Arguments φ and u.

Lati	tude.			A	proximat	e Differen	ce of Lev	el, in Tois	es.		
_	+	100	200	300	400	500	600	700	800	900	1000
0	90	0.3	0.5	0.8	1.0	1.3	1.6	1.8	2.1	2.3	2.6
5	85	0.3	0.5	0.8	1.0	1.3	1.5	1.8	2.0	2.3	2.6
10	80	0.2	0.5	0.7	1.0	1.2	1.5	1.7	2.0	2.2	2.4
15	75	0.2	0.4	0.7	0.9	1.1	1.3	1.6	1.8	2.0	2.3
20	70	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0
25	65	0.2	0.3	0.5	0.7	0.8	1.0	1.2	1.3	1.5	1.7
30	60	0.1	0.3	0.4	0.5	0.6	0.8	0.9	1.0	1.2	1.3
35	55	0.1	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.9
36	54	0.1	0.2	0.2	0.3	0.4	0.5	0.6	0.6	0.7	0.8
37	53	0.1	0.1	0.2	0.3	0.4	0.5	0.5	0.6	0.6	0.7
38	52	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.5	0.6	0.6
39	51	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.5
40	50	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5
41	49	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.3	0.4
42	48	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.3
43	47	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.2
44	46	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1
45	45	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Table V. for $C^{\prime\prime}$.

Arguments τ and T — T'. To be used only in computing Heights.

T — T'			Correcti	on for T—	T', in Toi	ses, with t	he same s	$ign; \tau =$		
Reaumur.	-12°	-10°	-8°	-6 °	-4°	-2 °	O o	+2°	+40	+6°
0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0
2	0.4	0.3	0.3	0.3	0.2	0.2	0.2	0.1	0.1	0.0
3	0.6	0.5	0.5	0.4	0.4	0.3	0.2	0.2	0.1	0.1
4	0.8	0.7	0.6	0.5	0.5	0.4	0.3	0.2	0.2	0.1
5	1.0	0 9	0.8	0.7	0.6	0.5	0 4	0.3	0.2	0.1
6	1.1	1.0	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.1
7	1.3	1.2	1.1	0.9	0.8	0.7	0.6	0.4	0.3	0.2
8	1.5	1.4	12	1.1	0.9	0.8	0.6	0.5	0.3	0.2
9	1.7	1.6	1.4	1.2	1.1	09	0.7	0.6	0.4	0.2
10	1.9	1.7	1.5	1.4	1.2	1.0	0.8	0.6	0.4	0.2

Correction	for	T - T	with	contraru	sion.	-	_

T — T'	+8°	+10°	+12°	+140	T — T'	+8°	+10°	+120	+14°
1	0.0	0.0	0.0	0.0	6	0.0	0.1	0.2	0.3
2	0.0	0.0	0.1	0.1	7	0.0	0.1	0.2	0.3
3 .	0.0	0.0	0.1	0.1	8	0.0	0.1	0.2	0.4
4	0.0	0.0	0.1	0.2	9	0.0	0.1	0.2	0.1
5	0.0	0.1	0.2	0.2	10	0.0	0.1	0.3	0.4

LAPLACE'S FORMULA FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS, MODIFIED BY BABINET.

In the Comptes Rendus de l'Académie des Sciences for March, 1851, M. Babinet proposes the following modification of Laplace's formula, the object of which is to dispense both with the use of logarithms and with tables of any kind.

Laplace's formula is,

$$z = 18393 \text{ metres (log H} - \log h) \left[1 + \frac{2 (T + t)}{1000} \right],$$

z being the difference of level between the two stations,

H, the height of barometer at the lower station,

h, the height of barometer at the upper station,

T, temperature of air at the lower station,

t, temperature of air at the upper station.

The two barometers are supposed to be reduced to the same temperature. The small correction for the latitude is omitted.

For elevations less than 1000 metres, and even for much greater elevations, if approximate results only are needed, the formula may be transformed into the following:

$$z = 16000 \text{ metres } \frac{\mathrm{II} - h}{\mathrm{II} + h} \left[1 + \frac{2 \left(\mathrm{T} + t \right)}{1000} \right].$$

Example 1.

Suppose,

at lower station, barometer at zero Cent. = 755^{mm} ; temperature of air 15° Cent. at upper station, barometer at zero Cent. = 745^{mm} ; temperature of air 10° Cent.

$${
m H}-h=10^{
m mm.}$$
 ${
m T}+t=25^{\circ}{
m Cent.}$ ${
m H}+h=1500^{
m mm.}$ $2~({
m T}+t)={}_{
m T}^5{}_{
m 0}^{\circ}{}_{
m T}=.05.$ $z=16000{}_{
m T}{}_{
m S}^{\circ}{}_{
m 0}{}_{
m T} imes(1.05)=112~{
m metres.}$

Then

Laplace's formula, by Delcros's tables, would give 111.6 metres.

Example 2.

Suppose,

at lower station, barometer at zero Cent. = 730^{mm.}; temperature of air 20° Cent. at upper station, barometer at zero Cent. = 635^{mm.}; temperature of air 15° Cent.

$$H - h = 95^{mm}$$
. $T + t = 35^{\circ}$ Cent. $H + h = 1365^{mm}$. $2 (T + t) = \frac{75}{1000} = .07$.

Then

$$z = 16000_{\frac{95}{1365}} \times (1.07) = 1191.5$$
 metres.

Laplace's formula, by Delcros's tables, would give 1191.1 metres.

For greater elevations an intermediate station may be supposed.

Babinet's formula reduced to English measures becomes,

$$z = 52494 \text{ English feet } \frac{\text{II} - h}{\text{II} + h} \left[1 + \frac{(\text{T} + t - 64)}{900} \right];$$

but as, in this form, it loses the simplicity of its coefficient, it will be found, on trial, that its use requires rather more computing than the author's tables (II.), p. 38, which give more accurate results.

VII.

TABLES

FOR COMPUTING THE DIFFERENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER. - BAILY.

Bailly, in his Astronomical Tables and Formulæ, page 111, gives the following final formula:

$$\begin{split} x &= 60345.51 \left\{ 1 + .0011111 \left(t + t' - 64^{\circ} \right) \right\} \\ &\times \log \text{ of } \left\{ \frac{\beta}{\beta'} \times \frac{1}{1 + .0001 \left(\tau - \tau' \right)} \right\} \times \left\{ 1 + .002695 \cos 2 \phi \right\}. \end{split}$$

Where ϕ = the latitude of the place,

 β = the height of the barometer, au = the temperature, Fahrenheit, of the mercury, t = the temperature, Fahrenheit, of the air, t at the lower station.

 β' = the height of the barometer, β' = the neight of the parameter, τ' = the temperature, Fahrenheit, of the mercury, at the upper station.

t' = the temperature, Fahrenheit, of the air.

The numerical values assumed are as follows: -

The constant barometrical coefficient = 60158.53 English feet.

The expansion of moist air for 1° Fahrenheit = .0022222.The expansion of mercury for 1° Fahrenheit = .0001001.

The increase of gravitation from Equator to Poles = .00539.

= 20898240 English feet. The radius of the Earth at ϕ

The height of lower station assumed = 4000 English feet.

Make A = the log of the first term, in English feet.

B = the log of 1 + .0001 $(\tau - \tau')$.

C =the log of the last term.

 $D = \log \beta - (\log \beta' + B).$

Then, by the tables which follow, the logarithm of the difference of altitude in English feet

 $= A + C + \log D.$

Baily's Tables have been recomputed and extended by Downes, for Lee's Collection of Tables and Formulæ (2d edit. pp. 84, 85). These new tables are given here as revised by Mr. Downes for this volume.

I. THERMOMETERS IN THE OPEN AIR.

+ t'	A	t+t'	A	t+t'	A	t+t'	A	t+t'	A
。 1	4.74913	° 37	4.76742	° 73	4.78497	0 109	4.80183	° 145	4.81807
2	4.74965	38	4.76791	74	4.78544	110	4.80229	146	4.81851
3	4.75016	39	4.76841	75	4.78592	111	4.80275	147	4.81896
4	4.75068	40	4.76891	76	4.78640	112	4.80321	148	4.81940
5	4.75120	41	4.76940	77	4.78687	113	4.80367	149	4.81984
6	4.75171	42	4.76990	78	4.78735	114	4.80413	150	4.82028
7	4.75223	43	4.77039	79	4.78782	115	4.80458	151	4.82072
8	4.75274	44	4 77089	80	4.78830	116	4.80504	152	4.82116
9	4.75326	45	4.77138	81	4.78877	117	4.80550	153	4.82160
10	4.75377	46	4.77187	82	4.78925	118	4.80595	154	4.8220
	4 65 400	17	4 ##000	83	4 50050	110	4.80641	155	1.0004
11	4.75429	47	4.77236	1	4.78972	119	4.80641 4.80686	156	4.82248
12	4.75480	48	4.77285	84 85	4.79019 4.79066	120 121	4.80686	156	4.8229
13	4.75531	49 50	4.77335	86	4.79066	121	4.80731	157	4.8233
14	4.75582	51	4.77384 4.77433	87	4.79113	122	4.80822	159	4.8242
15	4.75633	91	4.77400	61	4.75100	120	4.00022	133	4.0242
16	4.75684	52	4.77482	88	4.79207	124	4.80867	160	4.8246
17	4.75735	53	4.77530	89	4.79254	125	4.80913	161	4.82510
18	4.75786	54	4.77579	90	4.79301	126	4.80958	162	4.8255
19	4.75837	55	4.77628	91	4.79348	127	4.81003	163	4.8259
20	4.75888	56	4.77677	92	4.79395	128	4.81048	164	4.82640
21	4.75938	57	4.77725	93	4 79442	129	4.81093	165	4.8268
22	4.75989	58	4.77774	94	4.79489	130	4.81138	166	4.82727
23	4.76040	59	4.77823	95	4.79535	131	4.81183	167	4.82770
24	4.76090	60	4.77871	96	4.79582	132	4.81228	168	4.8281
25	4.76141	61	4.77919	97	4.79628	133	4.81273	169	4.8285
26	4.76191	62	4.77968	98	4.79675	134	4.81317	170	4.82900
27	4.76241	63	4.75016	99	4.79721	135	4.81362	171	4.8294
28	4.76292	64	4.78065	100	4.79768	136	4.81407	172	4.8298
29	4.76342	65	4.78113	101	4.79814	137	4.81452	173	4.8302
30	4.76392	66	4.78161	102	4.79861	138	4.81496	174	4.83072
31	4.76442	67	4.78209	103	4.79907	139	4.81541	175	4.83118
32	4.76492	68	4.78257	104	4.79953	140	4.81585	176	4.83158
33	4.76542	69	$\boldsymbol{4.78305}$	105	4.79999	141	4.81630	177	4.8320
34	4.76592	70	4.78353	106	4.80045	142	4.81674	178	4.8324
35	4.76642	71	4.78401	107	4.80091	143	4.81719	179	4.8328
36	4.76692	72	4.78449	108	4.80137	144	4.81763	180	4.83330

	II.	Аттасне	THERMON	IETER.			ATITUDE OF PLACE.
ττ΄	В	$\tau - \tau'$	В	au- au'	В	φ	C
0	0.00000	0 20	0.00087	o 40	0.00174	0	0.00117
1	0.00004	21	0.00091	41	0.00174	5	0.00117
2	0.00009	22	0.00096	42	0.00178	10	0.00113
3	0.00013	23	0.00100	43	0.00187	15	0.00110
4	0.00017	24	0.00104	44	0.00191	20	0.00090
5	0.00022	25	0.00109	45	0.00195	25	0.00075
6	0.00026	26	0.00113	46	0.00200	30	0.00078
7	0.00030	27	0.00117	47	0.00204	35	0.00040
8	0.00035	28	0.00122	48	0.00208	40	0.00020
9	0.00039	29	0.00126	49	0.00212	45	0.00000
10	0.00043	30	0.00130	50	0.00217	50	9.99980
11	0.00048	31	0.00135	51	0.00217	55	9.99980
12	0.00043	32	0.00139	52	0.00221	60	9.99960
13	0.00056	33	0.00133	53	0.00223	65	9.99925
14	0.00061	34	0.00148	54	0.00234	70	9.99910
	0.00005	0.5	0.001#2		0.00000		
15	0.00065	35	0.00152	55	0.00238	75	9.99900
16	0.00069	36	0.00156	56	0.00243	80	9.99890
17 18	0.00074 0.00078	37	0.00161 0.00165	57 58	0.00247	85	9.99885
19	0.00078	38	0.00169	58 59	0.00251 0.00256	90	9.99883
1.5	0.00000	0.0	0.00103	90	0.00200		

EXAMPLE.

	Upper Station.	Lower Station.
Thermometer in open air,	t' = 70.4,	t = 77.6.
Attached Thermometer,	au' = 70.4,	$\tau = 77.6$.
Barometer,	$\beta' = 23.66$ inches,	$\beta = 30.05$ inches.
Latitude of the place	$\phi = 21^{\circ}$.	
B = 0.00031	$\log D = 9.0$	1502
$\log \beta' = 1.37401$	C = 0.0	00087
1.37432	A = 4.8	81940
$\log \beta = 1.47784$	$\overline{3.8}$	83529
D = 0.10352	=68	43.7 English feet.

VIII.

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS,

BASED ON BESSEL'S FORMULA.

BY E. PLANTAMOUR.

[These Tables, computed by Professor E. Plantamour, Director of the Observatory at Geneva, Switzerland, are found in Vol. XIII. Part 1, of the Mémoires de la Société de Physique, &c. de Genève, p. 63, together with the following explanations.]

In No. 356 of the Astronomische Nachrichten, Bessel published a paper on the measurement of heights by means of the barometer, in which he deduces a formula which contains a factor depending on the humidity of the air. This formula is:

$$\log \frac{P}{P'} = \frac{(g) \cdot H' - H}{L(1 + KT)} \left[1 - a \frac{0.002561}{\sqrt{PP'}} \cdot 10^{-0.0279712 \text{ T}} - 0.0000625826 \text{ T}^2 \right],$$

where the various quantities have the following signification: -

h being the elevation of the lower station, and

h' the elevation of the upper station above the level of the sea,

a = the radius of the Earth,

$$H = \frac{a h}{a + h},$$

$$H' = \frac{a h'}{a + h'};$$

P = the weight of the atmosphere at the lower station,

P' = the weight of the atmosphere at the upper station,

the unit of weight assumed being the pressure of a column of mercury

BAROMETRICAL MEASUREMENT OF HEIGHTS.

of 336.905 Paris lines, at the temperature of the freezing point, or zero Reaumur, and under the 45th degree of latitude.

(g) = the gravity, at the level of the sea, in the mean latitude between the two places of observation.

Therefore, calling ϕ the latitude,

 $(g) = 1 - 0.0026257 \cos \phi,$

L = the constant barometrical coefficient depending on the relative density of the mercury and of the air,

K = the coefficient of the expansion of the air,

T = the mean temperature of the layer of air between the lower and upper station,

a = the fraction of saturation of the same layer.

The second term in the parenthesis, destined to take into account the aqueous vapor in the air, was obtained by assuming that the elastic force of vapor for a temperature T is represented, in unit of weight, by the expression,

$$p = 0.0067407 \times 10^{-0.0279712} \text{ T} - 0.0000625826 \text{ T}^2$$
.

Multiplying the second member by 336.905 we find the expression of the elastic force of vapor that Laplace deduced from Dalton's experiments. Substituting, in the computation, Regnault's results, the numerical value of these coefficients is somewhat changed, and we find then

$$p = 0.0060527 \times 10^{-0.0301975} \,\mathrm{T} - 0.000080170 \,\mathrm{T}$$
.

Bessel's tables give the difference of elevation in toises. The logarithm of the difference is obtained by the sum of four logarithms. The same form is preserved in the following tables; but the differences of elevation are given in metres.

The term due to the expansion of the air is computed in Bessel's tables for two values of the coefficient, viz. that of Gay-Lussac, 0.00375, and that of Rudberg, 0.003648; in the new tables it is only computed for that of Regnault, 0.003665.

The relative density of dry air at the freezing point, under a barometrical pressure of 0^m.76, and at the 45th degree of latitude, and of mercury in the same circumstances, adopted by Bessel, is that determined by the experiments of Biot and Arago, viz.

The value of that constant derived from Regnault's experiments has been substituted. Regnault found the weight of a litre of dry air, at zero Centigrade, under a pressure of $0^{\rm m}$.76, and at the latitude of Paris, to be 1.293187 grammes, which, reduced to the gravity of the 45th degree of latitude, becomes 1.292732 grammes. The weight of a litre of mercury, at zero Centigrade, he found to be 13596 grammes; the ratio is thus:

$$D = \frac{1}{10517.3}$$

or about $\frac{1}{200}$ smaller than the value adopted by Bessel. If the constant coefficient L is expressed by $L = \frac{0^{m_*}.76}{D \cdot \mu}$, μ being the modulus of the common logarithms, its numerical value becomes

$$L = 18404^{m} \cdot .8$$
.

In order to reduce the formula into tables, Bessel caused it to undergo several modifications, which we have followed, introducing the values of the constants above mentioned.

Let b and b' be the heights of the barometer, expressed in the metrical scale, at the two stations; t and t', the temperatures of the mercury measured with a brass scale; we have,

$$P = \frac{b}{0^{m} \cdot 76} \cdot (g) \cdot \left(\frac{a}{a+h}\right)^{2} \frac{(1+0.00001879 t)}{(1+0.00018018 t)}$$

and

$$P' = \frac{b'}{0^{m} \cdot .76} \cdot (g) \cdot \left(\frac{a}{a + b'}\right)^2 \frac{(1 + 0.00001879 \, t')}{(1 + 0.00018018 \, t')}.$$

Therefore,

$$\log P = \log b + \log (g) - \log 0^{m} \cdot .76 - \frac{2 \text{ II } \mu}{a} - \mu t \left[0.00018018 - 0.00001879 \right],$$

$$\log P' = \log b' + \log (g) - \log 0^{m} \cdot 76 - \frac{2 H' \mu}{a} - \mu t' [0.00018018 - 0.00001879].$$

If we call B, B' the heights of the barometer reduced to the freezing point, which we obtain by making

$$\log B = \log b - t \cdot 0.000070095$$
; $\log B' = \log b' - t' \cdot 0.000070095$,

$$\log \frac{P}{P'} = \log B - \log B' + \frac{H' - H}{7329755},$$

and with sufficient accuracy,

$$\checkmark P P' = \frac{\sqrt{B B'}}{0^{m} 76}$$
.

Substituting these expressions in the formula, it becomes,

$$\log B - \log B' = \frac{(g) \cdot H' - H}{L (1 + K T)} \left[1 - \frac{L (1 + K T)}{(g) \cdot 7329755} - \frac{\alpha \cdot 0.001748}{V B B'} \cdot 10^{0.0301975 T} - 0.000080170 T^{2} \right].$$

If we set instead of a the half sum $\frac{a+a}{2}$ of the fraction of saturation observed at both stations, we find, after some transformations,

BAROMETRICAL MEASUREMENT OF HEIGHTS.

$$\begin{split} \log \mathrm{B} - \log \mathrm{B'} &= \frac{(g) \; (\mathrm{H'-H)} \; (397.25 - \mathrm{KT})}{398.25 \; . \; \mathrm{L} \; (1+\mathrm{KT})} \; \times \\ & \left[1 - \frac{(a+a') \; . \; 0.34807}{(397.25 - \mathrm{KT}) \; \sqrt{\mathrm{BB'}}} \; . \; 10^{\; 0.0301975 \; \mathrm{T} \; - \; 0.000080170 \; \mathrm{T^2}} \right] \end{split}$$

Making further,

$$V = \frac{398.25}{397.25 - KT} L (1 + KT),$$

$$W = \frac{0.34807}{397.25 - KT}$$
. 10 $^{0.0301975\,T - 0.000080170\,T^2}$,

we shall have for the logarithm of the approximate difference of level between the two stations H' -- H,

$$\log (H' - H) = \log [\log B - \log B'] + \log V + \log \frac{1}{1 - W \frac{a + a'}{V B B'}} + \log \frac{(g)}{1}.$$

Table I. gives the values of log V and log W, both of which only depend on the temperature; the argument is the sum of the temperature of the air, τ and τ' , observed at both stations, supposing $\tau + \tau' = 2 \text{ T}$.

Table II. gives the factor depending on the humidity of the air; with the argument

W. $\log \frac{(a+a')}{\sqrt{BB'}}$,

we obtain

$$\log \frac{1}{1 - W \frac{(a+a')}{\sqrt{B B'}}} = \log V'.$$

Table III. gives the factor depending on the latitude for every degree, viz.

$$\log G' = \log \frac{1}{(g)}.$$

The logarithm of the approximate difference is thus given by the sum of four logarithms. To obtain the exact elevation, the small correction found in Table IV. must be added to the number corresponding to that logarithm. For we have, with the necessary accuracy,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$
.

Table IV. gives, for every 200 metres, the quantity $\frac{H^2}{a}$; the number in the table corresponding to $\frac{H'^2}{a}$ must be *added* to the approximate elevation; and the number corresponding to $\frac{H^2}{a}$ must be subtracted from the same.

USE OF THE TABLES.

Reduce first the observed height of the barometer at both stations to the freezing point by means of the usual tables, or by the logarithmic formula,

$$\log B = \log b - t \cdot 0.00007, \quad \log B' = \log b' - t' \cdot 0.00007;$$

b and b' being, in fractions of metre, the observed heights at the temperatures t and t' marked by the attached thermometers; and B and B' the reduced height at the lower and upper station.

Take the difference of log B and log B', and find, in the tables of the common logarithms, the logarithm of that difference, viz. log (log B — log B'); find also the logarithm of the product \checkmark B B', or

$$\log \checkmark B B' = \frac{\log B + \log B'}{2}.$$

Make further the sum $\tau + \tau'$ of the temperature of the air at both stations, and likewise the sum of a + a' of the fraction of saturation.

Then, in Table I., with argument $\tau + \tau'$, take $\log V$ and $\log W$; further, to $\log W$ add $\log (a + a')$, and subtract $\log \checkmark BB'$; and with the logarithm thus obtained as argument, take in Table II. $\log V'$.

Table III. with the mean latitude of the stations gives log G'.

H' — H being the approximate difference of level between the two stations, we have

$$\log (II' - H) = \log (\log B - \log B') + \log V + \log V' + \log G'.$$

The altitude of the lower station being known, we deduce from H' - H the approximate altitude, H', of the upper station; h', the exact altitude, or h' - h, the difference of elevation, is given by the formula,

$$h' - h = H' - H + \frac{H'^2}{a} - \frac{H^2}{a}$$

Table IV. gives the values of $\frac{H^2}{a}$ and $\frac{H^2}{a}$ for the values of H' or H for every 200 metres.

Example 1.

Computing the height of St. Bernard, taking Geneva, 407 metres above the level of the sea, as the lower station. The observation gives,

St. Bernard above the level of the sea h' = 2473.0 metres.

Example 2.

Computing the height of Mont Blanc from the observations of Bravais and Martins, on the 29th of August, 1844, taking St. Bernard (2473.0 metres) as the lower station. The observation gives,

				m . D. T.	·					
				TABLE					TABL	
		Argu	ment =	τ + τ'. Cer	ntigrade Deg	rees.			Arg't. =	Height.
τ + τ'.	log. V.	log. W.	τ + τ'.	log. V.	log. W.	τ + τ'.	log. V.	log. W.	H'. H.	+
0			0			0			Metres.	Metres.
-24	4.24644	6.5362	+15	4.27783	7.1692	+54	4.30711	7.7033	200	0.01
-23	4.24728	6.5441	+16	4.27861	7.1839	+55	4.30784	7.7160	400	0.03
-22	4.24811	6.5620	+17	4.27938	7.1985	+56	4.30856	7.7287	600	0.06
-21	4.24894	6.5797	+18	4.28016	7.2131	+57	4.30929	7.7413	800	0.10
-20	4.24977	6.5974	+19	4.28093	7.2275	+58	4.31001	7.7539	1000	0.16
-19	4.25059	6.6157	+20	4.28170	7.2420	+59	4.31073	7.7664	1200	0.23
-18	4.25142	6.6341	+21	4.28247	7.2564	+60	4.31145	7.7789	1400	0.31
-17	4.25225	6.6521	+22	4.28323	7.2708	+61	4.31217	7.7914	1600	0.40
-16	4.25307	6.6700	+23	4.28400	7.2850	+62	4.31288	7.8038	1800	0.51
-15	4.25389	6.6879	+24	4.28477	7.2993	+63	4.31360	7.8161	2000	0.63
-14	4.25471	6.7057	+25	4.28553	7.3135	+64	4.31432	7.8285	2200	0.76
-13	4.25553	6.7232	+26	4.28629	7.3276	+65	4.31503	7.8407	2400	0.90
-12	4.25634	6.7407	+27	4.28705	7.3417	+66	4.31574	7.8530	2600	1.06
-11	4.25716	6.7581	+28	4.28781	7.3557				2800	1.23
-10	4.25797	6.7755	+29	4.28857	7.3697				3000	1.41
- 9	4.25878	6.7926	+30	4.28933	7.3837				3200	1.61
- 8	4.25959	6.8096	+31	4.29008	7.3975				3400	1.82
- 7	4.26040	6.8266	+32	4.29084	7.4114	l .	•		3600	2.04
- 6	4.26121	6.8436	+33	4.29159	7.4252				3800	2.27
- 5	4.26202	6.8603	+34	4.29234	7.4389				4000	2.51
- 4	4.26282	6.8770	+35	4.29319	7.4526				4200	2.77
- 3	4.26362	6.8935	+36	4.29384	7.4662				4400	3.04
- 2	4.26443	6.9100	+37	4.29459	7.4798				4600	3.32
- 1	4.26523	6.9263	+38	4.29534	7.4933	ı			4800	3.62
0	4.26603	6.9426	+39	4.29608	7.5068				5000	3.93
+ 1	4.26682	6.9581	+40	4.29683	7.5202				5200	4.25
+ 2	4.26762	6.9736	+41	4.29757	7.5336				5400	4.58
+ 3	4.26841	6.9889	+42	4.29831	7.5470				5600	4.93
+ 4	4.26921	7.0043	+43	4.29905	7.5602				5800	5.28
+ 5	4.27000	7.0195	+44	4.29979	7.5735				6000	5.65
+ 6	4.27079	7.0347	+45	4.30053	7.5867				6200	6.04
+ 7	4.27157	7.0499	+46	4.30127	7.5999	·		{	6400	6.43
+ 8	4.27236	7.0650	+47	4.30200	7.6130			1	6600	6.84
+ 9	4.27315	7.0800	+48	4.30273	7.6260				6800	7.26
+10	4.27393	7.0950	+49	4.30347	7.6390				7000	7.70
	4.00:00	- 1000								
+11	4.27471	7.1099	+50	4.30420	7.6519				7200	8.14
+12	4.27550	7.1248	+51	4.30493	7.6648				7400	8.60
+13	4.27628	7.1397	+52	4.30566	7.6777					
+14	$4.27705 \\ 4.27783$	7.1545	+53	4.30639	7.6905					
15	4.41103	7.1692	+54	4.30711	7.7033					
L		•			1			1	Ų.	1

					li li				
		TAB	LE II.				TABL	E III	.
	Arg	gument = lo	og. W. $\frac{(z+z)}{\sqrt{B}}$;' <u>)</u> •			Argument =	= Latit	ude.
Argum't.	log. V¹.	Argum't.	log. V'.	Argum't.	log. V'.	φ.	log. G'.	¢.	log. G'.
6.5	0.00014	7.70	0.00218	8.09	0.00538	0	+0.00114	0 40	+0.00020
6.6	0.00014	7.71	0.00218	8.10	0.00550	1	+0.00114	41	+0.00016
6.7	0.00022	7.72	0.00229	8.11	0.00563	2	+0.00114	42	+0.00012
6.8	0.00022	7.73	0.00234	8.12	0.00576	3	+0.00114	43	+0.00008
6.9	0.00034	7.74	0.00239	8.13	0.00590	4	+0.00113	44	+0.00004
7.0	0.00043	7.75	0.00245	8.14	0.00604	5	+0.00112	45	0.00000
7.1	0.00055	7.76	0.00251	8.15	0.00618	6	+0.00112	46	-0.00004
7.2	0.00069	7.77	0.00256	8.16	0.00632	7	+0.00111	17	-0.00008
7.3	0.00087	7.78	0.00262	8.17	0.00647	8	+0.00110	48	-0.00012
7.4	0.00109	7.79	0.00269	8.18	0.00662	9	+0.00109	49	-0.00016
]			1					
7.41	0.00112	7.80	0.00275	8.19	0.00678	10	+0.00107	50	-0.00020
7.42	0.00114	7.81	0.00281	8.20	0.00694	11	+0.00106	51	-0.00024
7.43	0.00117	7.82	0.00288	8.21	0.00710	12	+0.00104	52	-0.00028
7.44	0.00120	7.83	0.00295	8.22	0.00727	13	+0.00103	53	-0.00031
7.45	0.00123	7.84	0.00302	8.23	0.00744	14	+0.00101	54	-0.00035
7.46	0.00125	7.85	0.00309	8.24	0.00761	15	+0.00099	55	-0.00039
7.47	0.00128	7.86	0.00316	8.25	0.00779	16	+0.00097	56	-0.00043
7.48	0.00131	7.87	0.00323	8.26	0.00798	17	+0.00095	57	-0.00046
7.49	0.00134	7.88	0.00331	8.27	0.00816	18	+0.00092	58	-0.00050
7.50	0.00138	7.89	0.00338	8.28	0.00835	19	+0.00090	59	-0.00054
7.51	0.00141	7.90	0.00346	8.29	0.00855	20	+0.00087	60	-0.00057
7.52	0.00141	7.91	0.00354	8.30	0.00875	21	+0.00085	61	-0.00060
7.53	0.00147	7.92	0.00363	8.31	0.00896	22	+0.00082	62	-0.00064
7.54	0.00141	7.93	0.00371	8.32	0.00917	23	+0.00079	63	-0.00067
7.55	0.00151	7.94	0.00380	8.33	0.00939	24	+0.00076	64	-0.00070
									0.000=0
7.56	0.00158	7.95	0.00389	8.34	0.00961	25	+0.00073	65	-0.00073
7.57	0.00162	7.96	0.00398	8.35	0.00983	26	+0.00070	66	-0.00076 -0.00079
7.58	0.00165	7.97	0.00407	l		27	+0.00067	67 68	-0.00079
7.59	0.00169	7.98	0.00417	1		28 29	+0.00064	69	-0.00082 -0.00085
7.60	0.00173	7.99	0.00427	1		29	+0.00000	0.9	-0.00033
7.61	0.00177	8.00	0.00437			30	+0.00057	70	-0.00087
7.62	0.00181	8.01	0.00447	1		31	+0.00054	71	-0.00090
7.63	0.00186	8.02	0.00457	1		32	+0.00050	72	-0.00092
7.64	0.00190	8.03	0.00468	1		33	+0.00046	73	-0.00094
7.65	0.00194	8.04	0.00479			34	+0.00043	74	-0.00097
7.66	0.00199	8.05	0.00490			35	+0.00039	75	-0.00099
7.67	0.00193	8.06	0.00502	1		36	+0.00035	76	-0.00101
7.68	0.00204	8.07	0.00513	1		37	+0.00031	77	-0.00102
7.69	0.00213	8.08	0.00525	1		38	+0.00028	78	-0.00104
7.70	0.00218	8.09	0.00538			39	+0.00024	79	-0.00106
		l		1		40	+0.00020	80	-0.00107

CORRECTION

FOR THE HOUR OF THE DAY AND THE SEASON OF THE YEAR AT WHICH THE OBSERVATIONS HAVE BEEN TAKEN.

In all the preceding tables, the mean temperature of the layer of air between the two stations is assumed to be given by the half-sum of the temperatures observed at each station, or by $\frac{t+t'}{2}$. Experience, however, has proved that this assumption is not true under all meteorological circumstances, and that, not to speak of more irregular influences, the temperature expressed by $\frac{t+t'}{2}$ differs in + or - from the true mean temperature by a quantity which considerably varies with the hour of the day, the season of the year, and the elevation at which the observations are taken. The amount of the correction for the temperature of the air, as given by the various formulas, thus needs to be modified accordingly. In the absence of the data necessary for establishing the law of the decrease of heat on the vertical in the various layers of the atmosphere, at the different periods of the day and of the year, and in different latitudes, which alone would furnish the means of determining the true value of this correction in these various circumstances, the following empirical tables enable us to form a judgment of the importance of that correction.

Tables IX. and X. are taken from Berghaus, Grundriss der Geographie, p. 91, and in the Tables accompanying the same work, p. 71. The correction to be applied for the hour of the day at which the observations have been taken, is found by multiplying the approximate height obtained by the factors in Table IX., giving to the correction the sign of the factor. This table and the following are calculated to be used in the climate of Germany, and for elevations not much exceeding 5,000 feet. The influence of the seasons on the correction is not taken into the account; judging from Table X., the correction may be, perhaps, too small for the summer months, and may better answer for the autumn. Using these factors, we obtain for the differences of level, in toises, placed at the head of each column, in Table X., the correction corresponding to each hour, from 6 A. M. to 10 P. M.

TABLE IX.

Hour.	Factor.	Hour.	Factor.	Hour.	Factor.
A. M. 6 7 8 9 10	+0.0075 +0.0050 +0.0025 -0.0005 -0.0035 -0.0044	Noon. P. M. 1 2 3 4 5	-0.0054 -0.0057 -0.0059 -0.0045 -0.0031 -0.0011	P. M. 5 6 7 8 9	$-0.0011 \\ +0.0013 \\ +0.0022 \\ +0.0032 \\ +0.0043 \\ +0.0054$

CORRECTION FOR THE HOUR OF THE DAY.

TABLE X.

ARGUMENT, THE HOUR, AND THE APPROXIMATE HEIGHT IN TOISES.

				Correct	ion, in To	ises, for				
Hour.	100	200	300	400	500	600	700	800	900	Ilour.
A. M. 6	+0.7	+1.5	+2.2	+3.0	+3.7	+4.5	+5.2	+6.0	+6.7	6 A. M.
7	+0.5	+1.0	+1.5	+2.0	+2.5	+3.0	+3.5	+4.0	+4.5	7
8	+0.2	+0.5	+0.7	+1.0	+1.2	+1.5	+1.8	+2.0	+2.3	8
9	-0.0	-0.1	-0.1	-0.2	-0.2	-0.3	-0.3	-0.4	-0.4	9
10	-0.3	-0.7	-1.0	-1.4	-2.1	-2.4	-2.8	-3.1	-3.5	10
11	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-3.1	-3.6	-4.0	11
Noon.	-0.5	-1.1	-1.6	-2.2	-2.7	-3.3	-3.8	-4.4	-4.9	Noon.
P. M. 1	-0.6	-1.1	-1.7	-2.3	-2.8	-3.4	-4.0	-4.5	-5.1	1 P. M.
2	-0.6	-1.2	-1.8	-2.4	-3.0	-3.5	-4.1	-4.7	-5.3	2
3	-0.4	-0.9	-1.3	-1.8	-2.2	-2.7	-3.1	-3.6	-4.0	3
4	-0.3	-0.6	-0.9	-1.2	-1.5	-1.8	-2.1	-2.4	-2.7	4
5	-0.1	-0.2	-0.3	-0.4	-0.5	-0.6	-0.7	-0.8	-0.9	5
6	+0.1	+0.2	+0.4	+0.5	+0.5	+0.8	+0.9	+1.0	+1.1	6
7	+0.2	+0.4	+0.7	+0.9	+1.1	+1.3	+1.6	+1.8	+2.0	7
8	+0.3	+0.6	+0.9	+1.3	+1.6	+1.9	+2.2	+2.5	+2.9	8
9	+0.4	+0.8	+1.3	+1.7	+2.1	+2.6	+3.0	+3.4	+3.8	9
10	+0.5	+1.1	+1.6	+2.1	+2.7	+3.2	+2.8	+4.3	+4.8	10

Table XI. is found in the Résumé des Observations Thermométrique et Barométriques faites à Genève et au Grand St. Bernard pendant les dix années 1841 à 1850, a very elaborate paper by Professor E. Plantamour, Director of the Observatory at Geneva, published in Vol. XIII. of the Mémoires de la Société de Physique de Genève. The author, after having determined the difference of elevation between Geneva (407.0 metres above the level of the sea) and the Great St. Bernard, by means of the corresponding observations, made during these 10 years, and using his own tables given above, reversed the problem. Assuming the difference of level thus found, viz. 2066 metres, to be the true height of the layer of air between the two stations, and its weight being given by the barometrical observations, he deduced from these data its mean density, and from the density its mean temperature at every even hour in every month of the year. Comparing these mean temperatures with those given at the same hours by the half-sum of the temperatures taken at the upper and the lower station, he found the differences contained in Table XI., which are the corrections to be applied to the half-sums of the temperatures to obtain, in this particular case, the true mean temperatures. The second part of the table has been computed by multiplying each temperature in the first by 7.5 metres, in order to show the value of that correction in barometrical measurements.

TABLE XI.

CORRECTION TO BE APPLIED TO THE HALF-SUMS OF THE TEMPERATURES OF THE AIR, OBSERVED AT GENEVA AND AT THE GREAT ST. BERNARD, TO OBTAIN THE TRUE MEAN TEMPERATURE OF THE AIR BETWEEN THE TWO STATIONS.

				C	errection	, in Cen	tigrade I	egrees, f	or				
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-0.5	0	-3.0	-3.9	° -4.1	° -4.4	° -4.4	° -3.8	-2.7	° -1.6	0 -0.4	0+0.7	° -2.5
2	-0.3	-1.5	-2.8	-3.7	-4.0	-1.4	-4.4	-3.8	-2.7	-1.5	-0.4	+0.7	-2.3
4	+0.4	-0.6	-1.6	-2.5	-2.7	-3.4	-3.6	-2.9	-1.7	-0.7	+0.4	+1.3	-1.5
6	+1.2	+0.7	-0.2	-0.9	-1.3	-2.1	-3.0 -2.2	-2.9	-0.5	+0.4	+1.3	+2.1	-0.3
8	+1.5	+1.4	+0.6	0.0	0.0	-0.6	-0.7	-0.5	+0.3	+1.3	+1.7	+2.6	+0.6
10	+1.7	+1.5	+1.2	+0.6	+0.7	+0.5	-0.1	+0.1	+0.8	+1.7	+1.8	+2.6	+1.1
Mid-			,										
night.	+1.9	+1.8	+1.9	+1.3	+1.8	+1.6	+0.9	+1.2	+1.3	+2.3	+2.1	+2.5	+1.7
2	+2.0	+2.2	+2.5	+1.9	+2.2	+2.0	+1.5	+2.0	+1.9	+2.5	+2.4	+2.6	+2.2
4	+2.3	+2.5	+2.6	+1.8	+1.7	+1.4	+1.1	+1.8	+2.1	+2.5	+2.7	+2.9	+2.1
6	+2.0	+2.0	+1.7	+0.7	+0.4	+0.1	0.0	+0.7	+1.5	+1.7	+2.3	+2.9	+1.3
8	+1.5	+1.1	0.0	-1.3	-2.0	-2.2	-2.4	-1.7	-0.4	+0.6	+1.7	+2.5	-0.3
10	+0.4	-0.4	-2.0	-3.1	-3.5	-3. 8	-3.7	-3.1	-2.0	-1.0	+0.3	+1.3	-1.7
Mean,	+1.2	+0.8	+0.1	-0.8	-0.9	-1.2	-1.5	-0.9	-0.2	+0.7	+1.3	+2.1	0.0
miean,					Cor	rection, i	n Metres	s, for					
Hour.	Jan.	Feb.	March.	April.	Cor	June.	n Metres	, for	Sept.	Oct.	Nov.	Dec.	Year
Hour.	Jan.				May.	June.	July.	Aug.					
Hour.	Jan 3.7	-12.7	-22.5	-29.2	May.	June.	July.	Aug.	-20.2	-12.0	- 3.0	+ 5.2	-18.
Hour.	Jan 3.7 - 1.5	-12.7 -11.2	-22.5 -21.0	-29.2 -27.7	May30.7 -30.0	June33.0 -33.0	July33.0 -33.0	Aug28.5 -28.5	-20.2 -19.5	-12.0 -11.2	- 3.0 - 1.5	+ 5.2 + 5.2	-18. -17.
Hour. Noon. 2 4	Jan 3.7 - 1.5 + 3.0	-12.7 -11.2 - 4.5	-22.5 -21.0 -12.0	-29.2 -27.7 -18.7	May30.7 -30.0 -20.2	June33.0 -33.0 -25.5	July33.0 -33.0 -27.0	Aug28.5 -28.5 -21.7	-20.2 -19.5 -12.7	-12.0 -11.2 - 5.2	- 3.0 - 1.5 + 3.0	+ 5.2 + 5.2 + 9.7	-18. -17. -11.
Hour. Noon. 2 4 6	Jan. - 3.7 - 1.5 + 3.0 + 9.0	-12.7 -11.2 -4.5 $+5.2$	-22.5 -21.0 -12.0 - 1.5	-29.2 -27.7 -18.7 - 6.7	May. -30.7 -30.0 -20.2 - 9.7	June33.0 -33.0 -25.5 -15.7	July. -33.0 -33.0 -27.0 -16.5	Aug. -28.5 -28.5 -21.7 -12.0	-20.2 -19.5 -12.7 - 3.7	-12.0 -11.2 - 5.2 + 3.0	- 3.0 - 1.5 + 3.0 + 9.7	+ 5.2 + 5.2 + 9.7 +15.7	-18. -17. -11. - 2.
Hour. Noon. 2 4	Jan 3.7 - 1.5 + 3.0	-12.7 -11.2 - 4.5	-22.5 -21.0 -12.0 - 1.5 + 4.5	-29.2 -27.7 -18.7	May. -30.7 -30.0 -20.2 - 9.7 0.0	June33.0 -33.0 -25.5	July33.0 -33.0 -27.0	Aug28.5 -28.5 -21.7	-20.2 -19.5 -12.7	-12.0 -11.2 - 5.2	- 3.0 - 1.5 + 3.0 + 9.7 +12.7	+ 5.2 + 5.2 + 9.7	-18. -17. -11. - 2.: + 4.
Hour. 2 4 6 8 10 Mid-	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5	May. -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7	July. -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7	Aug. -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5	-18. -17. -11. - 2. + 4. + 8.
Hour. Noon. 2 4 6 8 10 Midnight.	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2	$ \begin{array}{r} -22.5 \\ -21.0 \\ -12.0 \\ -1.5 \\ + 4.5 \\ + 9.0 \\ +14.5 \end{array} $	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7	May. -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7	July. -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7	Aug. -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5	-18.* -17.* -11.* - 2.* + 4.* + 8.* +12.*
Noon. 2 4 6 8 10 Midnight. 2	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7	$ \begin{array}{r} -29.2 \\ -27.7 \\ -18.7 \\ -6.7 \\ 0.0 \\ +4.5 \\ +9.7 \\ +14.2 \end{array} $	May. -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +15.0	July. -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 +11.2	Aug. -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5	-18.* -17.* -11.* - 2.* + 4.* + 8.\$ +12.* +16.\$
Noon. 2 4 6 8 10 Midnight. 2 4	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5	$ \begin{array}{r} -29.2 \\ -27.7 \\ -18.7 \\ -6.7 \\ 0.0 \\ +4.5 \\ +9.7 \\ +14.2 \\ +13.5 \end{array} $	-30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7	-33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +15.0 +10.5	-33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2	-28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5	$ \begin{array}{r} -20.2 \\ -19.5 \\ -12.7 \\ -3.7 \\ +2.2 \\ +6.0 \\ +9.7 \\ +14.2 \\ +15.7 \end{array} $	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7 +18.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7	-18. -17. -11. - 2. + 4. + 8. +12. +16. +15.
Hour. 2 4 6 8 10 Mid- night. 2 4 6	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2 +15.0	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7 +15.0	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5 +12.7	$ \begin{array}{r} -29.2 \\ -27.7 \\ -18.7 \\ -6.7 \\ 0.0 \\ +4.5 \\ +9.7 \\ +14.2 \\ +13.5 \\ +5.2 \end{array} $	May. -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +10.5 + 0.7	July. -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2 0.0	-28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7 +11.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7 +18.7 +12.7	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7 +21.7	-18. -17. -11. - 2. + 4. + 8. +12. +16.: + 9.
Noon. 2 4 6 8 10 Mid-night. 2 4 6 8	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2 +15.0 +11.2	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7 +15.0 + 8.2	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5 +12.7 0.0	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5 + 5.2 - 9.7	May. -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0 -15.0	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +10.5 + 0.7 -16.5	July. -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2 0.0 -18.0	Aug. -28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2 -12.7	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7 +11.2 - 3.0	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7 +18.7 + 12.7 + 4.5	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +20.2 +17.2 +12.7	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +19.5 +21.7 +21.7 +18.7	
Hour. 2 4 6 8 10 Mid-night. 2 4 6	Jan. - 3.7 - 1.5 + 3.0 + 9.0 +11.2 +12.7 +14.5 +15.0 +17.2 +15.0	-12.7 -11.2 - 4.5 + 5.2 +10.5 +11.2 +13.5 +16.5 +18.7 +15.0 + 8.2	-22.5 -21.0 -12.0 - 1.5 + 4.5 + 9.0 +14.5 +18.7 +19.5 +12.7 0.0	-29.2 -27.7 -18.7 - 6.7 0.0 + 4.5 + 9.7 +14.2 +13.5 + 5.2 - 9.7	May. -30.7 -30.0 -20.2 - 9.7 0.0 + 5.2 +13.5 +16.5 +12.7 + 3.0	June. -33.0 -33.0 -25.5 -15.7 - 4.5 + 3.7 +12.0 +10.5 + 0.7	July. -33.0 -33.0 -27.0 -16.5 - 5.2 - 0.7 + 6.7 + 11.2 + 8.2 0.0	-28.5 -28.5 -21.7 -12.0 - 3.7 + 0.7 + 9.0 +15.0 +13.5 + 5.2	-20.2 -19.5 -12.7 - 3.7 + 2.2 + 6.0 + 9.7 +14.2 +15.7 +11.2	-12.0 -11.2 - 5.2 + 3.0 + 9.7 +12.7 +17.2 +18.7 +18.7 + 12.7 + 4.5	- 3.0 - 1.5 + 3.0 + 9.7 +12.7 +13.5 +15.7 +18.0 +20.2 +17.2	+ 5.2 + 5.2 + 9.7 +15.7 +19.5 +19.5 +18.7 +19.5 +21.7 +21.7	-18. -17. -11. - 2. + 4. + 8. +12. +16.3

The elevation of a place in the interior of a continent where regular meteorological observations are made, may be ascertained by taking the yearly means of the barometer reduced to the freezing point, and of the temperature of the air, as data for the upper station, and the yearly means of the reduced barometer and of the free thermometer at the level of the sea, as the data for the lower station. The Hypsometric Tables then will give the difference of level. As observation, however, has shown that the mean height of the barometer at the level of the sea is not the same in all latitudes, it is necessary to take for such a comparison the mean height of the barometer which belongs to the latitude of the station the elevation of which is to be computed, or that which is nearest to it.

Table XII., published by Schouw, in Poggendorf's Annalen, and in the Comptes Rendus de l'Académie des Sciences, Tom. III. p. 573, gives in Paris lines the mean height of the barometer in various latitudes. The reduction into millimetres is from Martins's French translation of Kaemtz's Meteorology, p. 278; the corresponding values in English inches, and the new stations, Savannah, Ga., Philadelphia, Pa., and Cambridge, Mass., have been added. The mean heights last mentioned have been derived from three years of observations at Savannah, by Dr. John F. Posey, from June, 1853, to June, 1856, published in the American Almanae; from four years of hourly observations at Girard College, Philadelphia, by Prof. A. D. Bache; and from ten years of observations at Cambridge Observatory. They have been reduced to a common absolute standard and to mean tide-water at the respective places.

These mean barometric heights, corrected for the variation of gravity in latitude, according to the proposition of Poggendorf, by the formula b=b 45 (1 — 0.0025935 cos 2 ϕ), where b is the height of the barometer in latitude ϕ , and b 45 the corresponding height at the forty-fifth degree of latitude, are found in another column. For computing the elevations, the uncorrected heights are to be used.

The mean barometric pressure, as shown by Table XIII. from Kaemtz's *Précis de Météorologie*, French translation, p. 281, is not the same in all seasons, and the monthly means differ by a quantity which also varies with the latitude. If, therefore, the height of an inland station is to be ascertained from the barometrical means of one or more months only, the computation must be made with the mean pressure in the corresponding months at the level of the sea; or if this is not known, the yearly means taken from Table XII. must be corrected for the difference between the monthly means of the given month, or months, and the annual mean in the same latitude, as derived from the comparison of the numbers in Table XIII.

Example.

Suppose an inland station, in latitude 40° N.; the mean barometric pressure for July is 26.30 inches, and its elevation is to be computed from it.

Table XII. gives for latitude 40° , at Philadelphia, reduced to the level of the sea, 30.053 inches. Table XIII. gives as the mean for July, at the same place, 759.80 millimetres, and for the year, 760.25 millimetres (both not reduced to the level of the sea), difference — 0.45 millimetres = — 0.017 English inches, which is to be subtracted from the annual mean, 30.053, to reduce it to the mean of July; or

30.053 - 0.017 = 30.036. This last number is to be used in the computation, with the mean temperature of July at both stations.

Towards the tropical regions, the irregular or non-periodic variations of the barometer, which in high and middle latitudes are so considerable as to render simultaneous observations indispensable for the measurement of heights, gradually decrease and nearly cease to exist, while the monthly and daily periodic variations, which are small in high latitudes, considerably increase. Within the tropics, therefore, the oscillations of the barometer being far more uniform, observations made during a short period of time, or even single observations, may be used for computing heights, without corresponding observations, by referring them to the mean pressure at the level of the sea as to a constant, provided this last has been corrected for the monthly and daily periodic variation at the place.

Table XIII. furnishes the means of applying the correction for the monthly variation, as described above. Table XIV., which gives the mean height of the barometer at all hours of the day in various latitudes, enables the observer to correct the data according to the hour at which the observations have been taken. This table is from Kaemtz's Vorlesungen über Meteorologie, French translation, p. 249. The column Bossekop is from the observations of the French Scientific Expedition in the North; the column Philadelphia, from the observations at Girard College, has been added.

The correction for the hourly variation is found by taking the difference between the mean of the hour of observation and the daily mean, and correcting accordingly, with due regard to the signs, either the yearly mean at the sea level, or the observation at the upper station.

Example.

The barometer at Caracas, latitude 10° 30′ N., on the 20th of August, at 4 o'clock P. M., reads 680.57 millimetres.

which is the number to be used for the computation of the height of Caracas. In this case, however, the monthly correction, being derived from a higher latitude, may be too small. Both corrections can of course be applied, with contrary signs, to the observation at Caracas, leaving then the mean height at the level of the sea as a constant.

TABLE XII.

MEAN HEIGHT OF THE BAROMETER,

IN VARIOUS LATITUDES, REDUCED TO THE LEVEL OF THE SEA, AND TO THE FREEZING POINT.

		In Mill	imetres	In Englis	h Inches.	In Par	is Lines.
Places.	Latitude.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.	Observed.	Corrected for Gravity.
Cape of Good Hope,	33 S.	763.01	762.20	30.041	30.008	338.24	337.88
Rio Janeiro, Brazil,	23 S.	764.03	762.65	30.080	30.026	338.69	338.08
Christiansborg, Guinea,	5 30N.	760.10	758.16	29.925	29.850	336.95	336.09
La Guayra, Venezuela,	10	760.17	758.32	29.928	29.855	336.98	336.16
St. Thomas, W. Indies,	19	760.51	758.95	29.942	29.881	337 13	336.44
Macao, China,	23	762.99	761.61	30.040	29.986	338.23	337.62
Teneriffe, Canary Isles,	28	764.21	763.10	30.087	30.044	338.77	333.28
Savannah, Georgia,	32	764.59	763.74	30.102	30.070	338.93	338.57
Funchal, Madeira,	32 30	765.18	764.34	30.126	30.093	339.20	338.83
Tripoli, Northern Africa,	33	767.41	766.60	30.214	30.182	340.19	339.83
Palermo, Sicily,	38	762.95	762.47	30.038	30.019	338.21	338.00
Philadelphia, Penn.	40	763.35	763.00	30.053	30.040	338.38	338.23
Naples, Italy,	41	762.34	762.06	30.014	30.003	337.94	337.82
Cambridge, Mass.	42	762.44	762.24	30.018	30.010	337.99	337.90
Florence, Italy,	43 30	761.93	761.81	29.997	29.993	337.76	337.71
Avignon, France,	44	762.02	761.95	30.001	29.998	337.80	337.77
Bologna, Italy,	44 30	762.18	762.13	30.007	30.005	337.87	337.85
Padua, Italy,	45	762.18	762.18	30.007	30.007	337.87	337.87
Paris, France,	49	761.41	761.68	29.978	29.988	337.53	837.65
London, England,	51 30	760.96	761.41	29.960	29.978	337.33	337.53
Altona, Denmark,	53 30	760.42	761.01	29.938	29.961	337.09	337.35
Dantzig, Prussia,	54 30	760.10	760.76	29.925	29.952	336.95	337.24
Königsberg, Prussia,	54 30	760.49	761.14	29.941	29.967	337.12	337.41
Apenrade, Denmark,	55	759.58	760.71	29.906	29.950	336.72	337.22
Edinburgh, Scotland,	56	758.25	759.00	29.853	29.582	336.13	336-46
Christiania, Norway,	60	758.64	759.63	29.868	29.908	336.30	336.74
Hardanger, Norway,	60	756.94	757.04	29.801	29.841	335.55	335.99
Bergen, Norway,	60	757.01	758.00	29.804	29.844	335.58	336.02
Reikiavig, Iceland,	64	752.00	753.20	29.607	29.654	333.36	333.89
Godthaab, S. Greenland,	64	751.94	753.13	29.605	29.651	333.83	333.56
Eyafiord, Iceland,	66	753.59	754.89	29.669	29.721	334.06	234.64
Godhavn, Disco, Greenl.	68	753.76	755.16	29.677	29.731	334.14	334.76
Upernavik, N. Greenl.	73	755.18	756.80	29.732	29.796	334.77	335.49
Melville Isl., Arct. Amer.		757.08	758.75	29.807	29.872	335.61	336.35
Spitzbergen,	75 30	756.76	758.48	29.794	29.862	335.17	336.23

XIII. MEAN HEIGHT OF THE BAROMETER, IN ALL MONTHS OF THE YEAR, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sea.

Places,	HAVANA.	CAL- CUTTA.	MACAO.	CAIRO.	SA- VANNAH.	PHILA- DELPHIA.	CAM- BRIDGE.	PARIS.	St. PE-
Latitude,	230 9'	220 331	22° 11′	30° 2′	320 5/	39° 58′	42° 23′	48° 50′	590 56'
Jan.	765.24	761.57	767.93	762.40	762.80	760.97	761.37	758.86	762.54
Feb.	760.15	758.86	767.01	"	763.76	759.63	760.90	759.09	763.10
March,	760.98	756.24	766.08	759.43	763.05	760.51	759.09	756.33	760.76
April,	759.58	753.83	761.93	760.10	763.10	760.05	759.37	755.18	761.19
May,	758.19	750.81	761.64	758.23	763.39	759.09	759.63	755.61	760.94
June,	760.67	748.10	757.31	754.42	764.37	759.22	758.91	757.28	759.83
July,	760.67	747.54	757.91	753.90	764.02	759.80	760.34	756.52	758.25
Aug.	757.33	748.53	757.91	754.06	765.54	760.54	761.11	756.74	759.94
Sept.	757.46	751.83	762.22	756.70	763.36	761.25	761.83	756.61	761.19
Oct.	758.19	755.25	763.37	759.70	763.13	760.68	761.07	754.42	760.82
Nov.	761.25	758.37	766.17	760.76	763.41	760.49	760.85	755.75	758.05
Dec.	763.62	760.59	768.65	761.82	761.12	760.82	760.80	755.09	760.22
Year,	760.28	754.54	763.18	758.32	763.41	760.25	760.44	756.46	760.57

XIV. MEAN HEIGHT OF THE BAROMETER, AT ALL HOURS OF THE DAY, IN VARIOUS LATITUDES.

Not reduced to the Level of the Sea.

			Not re	duced to th	e Level of th	e Sea.			
Places,	Pacific Ocean.	CUMANA.	La Guayra.	CAL- CUTTA.	PHILADEL- PHIA.	Padua.	HALLE	St. Pe- tersburg	Bossekop
Latitude,	00 0'	10° 28′N.	10° 36′n.	22° 35′N.	39° 58′N.	45° 24′N.	51° 29′N.	59° 56′n.	69° 58'N
Observers,	Horner.	Hum- boldt.	Boussin- gault.	Balfour.	Bache.	Ciminello.	Kaemtz.	Kupffer.	Bravais.
	Millim,	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
Midnight,	752.17	756.86	759.64	758.80	760.49	757.01	753.23	759.35	754.90
1	752.20	756.53	759.34	758.62	760.46	756.90	753.14	"	"
2	751.77	756.21	759.05	758.57	760.41	756.84	753.05	759.32	754.79
3	751.63	755.89	758.81	758.49	760.34	756.78	752.99	"	66
4	751.32	755.66	758.68	758.47	760.39	756.74	752.99	759.32	754.70
5	751.65	755.79	758.85	758.44	760.49	756.75	753.34	"	66
6	751.95	756.18	759.32	758.68	760.75	756.79	753.12	759.39	754.68
7	752.48	756.58	759.94	759.16	761.00	756.89	753.24	"	
8	752.95	756.98	760.50	759.88	761.15	757.01	753.37	759.49	754.75
9	753.16	757.31	759.63	760.11	761.22	757.08	753.44	66	44
10	753.15	757.32	760.50	760.19	761.17	757.14	753.46	759.51	754.96
11	752.80	757.01	759.99	760.09	760.97	757.07	753.40	"	66
Noon,	752.35	756.57	759.41	759.61	760.56	757.02	753.29	759.47	755.01
1	751.87	755.99	758.91	759.22	760.13	756.85	753.11	66	66
2	751.55	755.47	758.41	758.39	759.83	756.67	752.99	759.38	754.96
3	751.15	755.14	758.12	758.12	759.65	756.54	752.89	66	"
4	751.02	754.96	758.05	757.91	759.65	756.47	753.84	759.32	754.82
5	751.31	755.14	758.10	757.93	759.70	756.46	752.86	66	"
6	751.71	755.41	758.40	758.01	759.85	756.50	752.91	759.31	754.87
7	751.93	755.81	758.90	758.02	760.08	756.63	753.02	"	66
8	752.35	756.21	759.19	758.54	760.31	756.79	753.14	759.32	754.89
9	752.74	756.59	759.69	759.24	760.49	756.92	753.24	"	"
10	752.85	756.87	759.93	759.33	760.59	757.02	753.31	759.36	754.92
11	752.86	757.15	759.98	759.09	760.72	757.02	753.29		
Mean,	752.13	756.33	759.22	758.87	760.43	756.83	753.19	759.38	754.85

Table XIV. shows that, after all irregular variations of the barometer have been eliminated, there remains a double period of rise and fall within the twenty-four hours, and that the amplitude of these daily oscillations is greatest within the tropics, and goes on diminishing towards the polar regions.

According to Kaemtz, the mean time of the daily maxima and minima, or the mean tropic hours for the northern hemisphere, are as follows:—

The minimum of the afternoon is reached at 4.05 P. M.

The maximum of the evening is reached at 10.11 P. M.

The minimum of the night is reached at 3.45 A. M.

The maximum of the morning is reached at 9.37 A. M.

Even in temperate and high latitudes these diurnal variations, though small, must be taken into account, if great accuracy is required, in reducing corresponding observations made at a somewhat different hour to the time of the observation at the station the height of which is to be determined. But in so doing, it must be remembered that the times of the minima and maxima change with the seasons, as is shown by Table XV. from Kaemtz, p. 251 of the French translation.

XV. TROPIC HOURS OF THE DAILY VARIATION OF THE BAROMETER AT HALLE. LAT. $51^{\circ}~30'~\mathrm{N}.$

Month.	Minimum, P. M.	Maximum, P. M.	Minimum, A. M.	Maximum, A. M.	Month.	Minimum, P. M.	Maximum, P. M.	Minimum, A. M.	Maximum,
	h.	h.	h.	h.		h.	h.	h.	h.
Jan.	2.81	9.17	4.91	9.91	July,	5.21	11.04	3.04	8.73
Feb.	3.43	9.46	3.86	9.66	Aug.	4.86	10.66	3.06	8.96
March,	3.82	9.80	3.87	10.10	Sept.	4.55	10.45	3.45	9.71
April,	4.46	10.27	3.53	9.53	Oct.	4.17	10.24	3.97	10.07
May,	5.43	10.93	3.03	9.13	Nov.	3.52	9.85	4.68	10.08
June,	5.20	10.93	2.83	8.73	Dec.	3.15	9.11	4.91	10.18

This shifting of the times of maxima and minima with the seasons diminishes with the latitude, and tends to disappear towards the equator, with the inequality of the days and nights. The elevation above the level of the sea also causes a change in the tropic hours of the daily variation which is not yet sufficiently studied.

Table XIV. gives evidence that the amplitude of the hourly oscillation is greatest under the equator, and gradually decreases towards the pole. Kaemtz computes its mean value in various latitudes and at the level of the sea, as follows:—

XV'. AMPLITUDE OF DAILY VARIATIONS IN VARIOUS LATITUDES.

	Latitude.	Variation.	Latitude.	Variation.	Latitude.	Variation	Latitude	Variation.
	° ′ 0 0	Millim. 2.28	23 55	Millim. 1.80	° ′ 39 4	Millim.	52 33	Millim. 0.45
	5 26 N.	2.26	29 28	1.58	43 34	0.90	57 17	0.23
L	17 52	2.03	34 26	1.35	48 1	0.67	62 25	0.00

The amplitude also decreases with the elevation, at least in our latitudes; it was found to be on the Faulhorn, in Switzerland, 9000 feet above the sea level, 0.27 millimetres, while it was 0.90 millimetres at Geneva.

TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANOTHER LEVEL.

To reduce barometric means taken at a given elevation to the height they would have if taken at the level of the sea, or barometric observations made at different elevations to a common level, in order to eliminate the influence of altitude in the comparison of barometric pressures, is a problem, the solution of which is often needed in meteorology.

For a complete and accurate reduction, embracing all cases, Tables IV. and V., by Dippe, given above, pages 54 et seq., may be used. But when the difference of height between the two stations, or above the sca-level, does not exceed a few hundred feet, the small tables XVI. to XIX., in three different scales, will be found more convenient.

Tables XVI. and XVII. have been computed from the constants of Laplace's formula, the barometric coefficient, including the correction for the decrease of gravity on a vertical, being respectively 60,345.51 English feet and 56,621.83 Paris feet; and the coefficient for expansion of moist air 0.00222 and 0.005.

In Table XVIII. the coefficient 18,420 metres, deduced from Regnault's experiments (see *Proceedings of the Amer. Assoc. for Adv. of Science*, 1857), and his coefficient for expansion of dry air, 0.003665, increased to 0.0039, in order to include the effect of moisture, have been used.

USE OF THE TABLES.

The correction for reducing the barometer to the level of the sea is found by the formula

$$C = \frac{f}{N} \times \frac{h'}{h}$$

where C is the correction required; f, the elevation of the station; N, the number in the tables; h', the reading of the barometer; h, the normal height of barometer at the sea-level.

Example.

At Cambridge Observatory, Massachusetts, at 71.34 English feet above mean tide, the mean barometer is = 29.939 inches; the mean temperature 47°.3 Fahrenheit; what would be the height at the level of the sea?

In Table XVI. we take for $47^{\circ}.3 = 90.49$, or, in order to get the correction in a fraction of an inch, 904.9.

Then

$$C = \frac{71.34}{904.9} \times \frac{29.939}{30} = 0.079$$
, correction required;

and

29.939 + 0.079 = 30.018 inches, height of the barometer at the level of the sea.

It will be seen that the quantity represented by the second member can be neglected without causing a sensible error in the correction. In this case the error does not amount to .001; it scarcely would reach .002 for 250 feet of elevation; so that the reduction can be made in most cases by a simple division; viz. $\frac{f}{N}$.

KVI. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR CORRESPONDING TO A TENTH OF AN ENGLISH INCH IN THE BAROMETER, AT TEMPERATURES BETWEEN 32° AND 100° FAHRENHEIT,

The Barometric Pressure at the Lower Station being = 30 English Inches.

Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temper- ature of Air, Fahren.	Height in English Feet.	Temperature of Air, Fahren.	Height in English Feet.
32°	87.51	46°	90.23	60°	92.95	74°	95.67	87°	98.20
33	87.70	47	90.42	61	93.15	75	95.87	88	98.40
34	87.90	48	90.62	62	93.34	76	96.06	89	98.59
35	88.09	49	90.81	63	93.53	77	96.26	90	98.79
36	88.28	50	91.01	64	93.73	78	96.45	91	98.98
37	88.48	51	91.20	65	93.92	79	96.65	92	99.17
38	88.67	52	91.40	66	94.12	80	96.84	93	99.37
39	88.87	53	91.59	67	94.31	81	97.04	94	99.56
40	89.06	54	91.78	68	94.51	82	97.23	95	99.76
41	89.26	55	91.98	69	94.70	83	97.42	96	99.95
42	89.45	56	.92.17	70	94.90	84	97.62	97	100.15
43	89.65	57	92.37	71	95.09	85	97.81	98	100.34
44	89.84	58	92.56	72	95.29	86	98.01	99	100.54
45	90.03	59	92.76	73	95.48	87	98.20	100	100.73

XVII. HEIGHT, IN FRENCH FEET, OF A COLUMN OF AIR CORRESPONDING TO A PARIS LINE IN THE BAROMETER, AT TEMPERATURES OF THE AIR BETWEEN 0° AND 34° REAUMUR,

The Barometric Pressure at the Lower Station being = 337 Paris Lines.

Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet.	Temper- ature of Air, Reaumur.	Height in French Feet
0°	73.08	7°	75.63	14°	78.19	21°	80.75	2s°	83.31
1	73.44	8	76.00	15	78.56	22	81.11	29	83.67
2	73.81	9	76.36	16	78.92	23	\$1.48	30	84.04
3	74.17	10	76.73	17	79.29	24	81.85	31	84.40
4	74.54	11	77.10	18	79.65	25	82.21	32	84.77
5	74.90	12	77.46	19	80.02	26	82.58	33	85.13
6	75.27	13	77.83	20	80.38	27	82.94	34	85.50

XVIII. HEIGHT, IN METRES, OF A COLUMN OF AIR CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT TEMPERATURES BETWEEN $0^{\circ} \ \ \text{AND} \ \ 39^{\circ} \ \ \text{CENTIGRADE},$

The Barometric Pressure at the Lower Station being = 760 Millimetres.

Temper- ature of Air, Centigr	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.	Temperature of Air, Centigr.	Height in Metres.	Temper- ature of Air, Centigr.	Height in Metres.
0°	10.54	s°	10.86	16°	11.19	24°	11.52	32°	11.85
1	10.58	9	10.91	17	11.23	25	11.56	33	11.89
2	10.62	10	10.95	18	11.28	26	11.60	3-1	11.93
3	10.66	11	10.99	19	11.32	27	11.64	35	11.97
4	10.70	12	11.03	20	11.36	28	11.69	36	12.01
5	10.74	13	11.07	21	11.40	29	11.73	37	12.06
6	10.78	14	11.11	22	11.44	30	11.77	38	12.10
7	10.82	15	11.15	23	11.48	31	11.81	39	12.14

Table XIX. gives, in metrical measure, the values of a millimetre in the barometer at different elevations and Centigrade temperatures. The values are derived from Laplace's constants, as in Tables XVI. and XVII.

This table may be used, as the preceding ones, for reducing barometrical observations to the level of the sea, and also to any other level by a similar process.

Example.

Suppose the barometer to read 700 millimetres at the altitude of 750 metres, the temperature of air being = 16° Centigrade; what would be the reading at a station lower by 350 metres, assuming the temperature of the air downwards to increase at the rate of 1° Centigrade for 185 metres?

The temperature of air at lower station will be $16^{\circ} + 1^{\circ}.9 = 17^{\circ}.9$

The approximate height of barometer about 73 centimetres.

Then, in Table XIX, we find for 16° and 70 centimetres, 12.15 for 17°.9 and 73 centimetres, 11.73

> Mean 11.94

And

 $\frac{300}{11.94} = 29.31$, or barometer at lower station 700 + 29.31 = 729.31 millimetres.

Delcros's tables, with these data, would give for the difference of level 349.76, instead of 350 metres; the corresponding error in the height of the barometrical column does not exceed 0.08 millimetre, and thus remains within the limits of error which may be expected in an ordinary observation.

The principal object of this table, however, is to furnish the scientific traveller with the means of readily computing on the spot approximate differences of level, by simply multiplying the difference between the readings of the barometer at each station by the half sum of the numbers in the table corresponding to the data given by the observations.

Example.

Suppose the barometer at the lower station to read 732.5, and at the upper station 703.2 millimetres; the temperature of the air being respectively 18° and 16° Centigrade.

The difference of the barometers, supposed to be reduced to the same temperature, is 29.3 millimetres.

Then, Table XIX. gives for 18° Centigrade and 73 centimetres, for 16° Centigrade and 70 centimetres, 12.15 11.94 Half sum, or mean,

And, $29.3 \times 11.94 = 349.8$ metres = difference of level required.

By the large tables of Delcros, we find for the same data 350.1 metres.

This table can be considered as a complement to Delcros's tables, and may save the traveller the trouble of carrying the larger tables.

A similar table in English measures is found above, at the end of the author's larger tables (Table VI.), page 48 of this series, and another, more extensive one, below, page 92, the use of which is explained by the examples just given.

XIX- HEIGHT, IN METRES, OF A COLUMN OF AIR, CORRESPONDING TO A MILLIMETRE IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Temper- ature of			Barome	eter at the	Lower Stat	tion, Readi	ng in Cent	imetres.		
Air, Centig.	76	75	74	73	72	71	70	69	68	67
0	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0	10.52	10.66	10.80	10.94	11.10	11.26	11.42	11.59	11.75	11.9
2	10.60	10.74	10.89	11.03	11.19	11.35	11.51	11.68	11.85	12.0
4	10.69	10.83	10.97	11.12	11.28	11.44	11.60	11.77	11.94	12.1
6	10.77	10.91	11.06	11.20	11.37	11.53	11.69	11.86	12.04	12.2
8	10.85	11.00	11.15	11.29	11.46	11.62	11.78	11.96	12.13	12.3
10	10.94	11.08	11.23	11.38	11.55	11.71	11.87	12.05	12.22	12.4
12	11.02	11.17	11.32	11.47	11.63	11.80	11.97	12.14	12.32	12.5
14	11.11	11.25	11.41	11.55	11.72	11.89	12.06	12.23	12.41	12.6
16	11.19	11.34	11.49	11.64	11.81	11.98	12.15	12.33	12.51	12.7
18	11.27	11.43	11.58	11.73	11.90	12.07	12.24	12.42	12.60	12.7
20	11.36	11.51	11.67	11.82	11.99	12.16	12.33	12.51	12.69	12.8
22	11.44	11.60	11.75	11.90	12.08	12.25	12.42	12.61	12.79	12.9
24	11.53	11.68	11.84	11.99	12.17	12.34	12.51	12.70	12.88	13.0
26	11.61	11.77	11.93	12.08	12.26	12.43	12.61	12.79	12.98	13.1
28	11.70	11.85	12.01	12.17	12.35	12.52	12.70	12.88	13.07	13.2
30	11.78	11.94	12.10	12.25	12.43	12.61	12.79	12.98	13.16	13.3
32	11.86	12.02	12.18	12.34	12.52	12.70	12.88	13.07	13.26	13.4
34	11.95	12.11	12.27	12.43	12.61	12.79	12.97	13.16	13.35	13.5
36	12.03	12.19	12.36	12.52	12.70	12.88	13.06	13.25	13.45	13.6
38	12.12	12.28	12.44	12.60	12.79	12.97	13.15	13.35	13.54	13.7
emper-				Ba	rometer in	Centimetr	es.			
ture of	66	65	61	63	62	61	60	59	58	57
Centig.		6.9			02					97
0	Metres. 12.11	Metres. 12.30	Metres. 12.49	Metres. 12.69	Metres. 12.89	Metres. 13.10	Metres. 13.32	Metres. 13.55	Metres. 13.78	Metre 14.0
2	12.21	12.40	12.59	12.79	13.00	13.21	13.43	13.66	13.89	14.1
4	12.31	12.50	12.69	12.89	13.10	13.31	13.54	13.77	14.00	14.2
6	12.40	12.60	12.79	13.00	13.20	13.42	13.64	13.88	14.11	14.30
8	12.50	12.69	12.89	13.10	13.31	13.52	13.75	13.98	14.22	14.4
10	12.60	12.79	12.99	13.20	13.41	13.63	13.86	14.09	14.34	14.59
12	12.69	12.89	13.09	13.30	13.51	13.73	13.96	14.20	14.45	14.70
14	12.79	12.99	13.19	13.40	13.62	13.84	14.07	14.31	14.56	14.81
16	12.89	13.09	13.29	13.50	13.72	13.94	14.18	14.42	14.67	14.93
18	12.98	13.19	13.39	13.61	13.82	14.05	14.28	14.53	14.78	15.0
20	13.08	13.28	13.49	13.71	13.93	14.15	14.39	14.63	14.89	15.15
22	13.18	13.38	13.59	13.81	14.03	14.26	14.50	14.74	15.00	15.26
24	13.27	13.48	13.69	13.91	14.13	14.36	14.60	14.85	15.11	15.37
26	13.37	13.58	13.79	14.01	14.24	14.47	14.71	14.96	15.22	15.48
28	13.47	13.68	13.89	14.11	14.34	14.57	14.82	15.07	15.33	15.60
30	13.57	13.78	13.99	14.22	14.44	14.68	14.92	15.18	15.44	15.7
32	13.66	13.87	14.09	14.32	14.55	14.78	15.03	15.28	15.55	15.83
34	13.76	13.97	14.19	14.44	14.65	14.89	15.14	15.39	15.66	15.93
- 11	13.86	14.07	14.29	14.52	14.75	14.99	15.24	15.50	15.77	16.08

XIX'. HEIGHT, IN ENGLISH FEET, OF A COLUMN OF AIR, CORRESPONDING TO A TENTH OF AN INCH IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

Barometer				Ten	peratur	e of the A	ir, Fahr	enheit, b	eing			
Reading in English Inches.	400	450	50°	55°	60°	65°	70°	75°	800	85°	90°	95
22.0	121.5	122.8	124.2	125.5	126.8	128.2	129.5	130.8	132.1	133.5	134.8	136
22.2	120.4	121.7	123.1	124 4	125.7	127.0	128.3	129.6	130.9	132.2	133.6	134
22.4	119.3	120.6	121.9	123.2	124.6	125.9	127.2	128.5	129.8	131.1	132.4	133
22.6	118.2	119.5	120.8	122.1	123.4	124.7	126.0	127.3	128.6	129.9	131.2	132
22.8	117.2	118.5	119.8	121.1	122.3	123.6	124.9	126.2	127.5	128.8	130.0	131
23.0	116.2	117.5	118.7	120.0	121.3	122.6	123.8	125.1	126.4	127.6	129.9	130
23.2	115.2	116.5	117.7	119.0	120.2	121.5	122.7	124.0	125.3	126.5	127.8	129
23.4	114.2	115.5	116.7	118.0	119.2	120.5	121.7	123.0	124.2	125.4	126.7	127
23.6	113 2	114.4	115.7	116.9	118.1	119.4	120.6	121.8	123.1	124.3	125.5	126
23.8	112.3	113.5	114.8	116.0	117.2	118.4	119.7	120.9	122.1	123.3	124.6	125
24.0	111.4	112.6	113.8	115.0	116.2	117.4	118.7	119.9	121.1	122.3	123.5	124
24.2	110.5	111.7	112.9	114.1	115.3	116.5	117.7	118.9	120.1	121.3	122.5	123
24.4	109.5	110.7	111.9	113.1	114.3	115.5	116.7	117.9	119.1	120.3	121.5	122
24.6	108.6	109.8	111.0	112.2	113.4	114.6	115.8	116.9	118.1	119.3	120.5	121
24.8	107.8	108.9	110.1	111.3	112.5	113.7	114.8	116.0	117.2	118.4	119.5	120
25.0	106.9	108.1	109.2	110.4	111.6	112.7	113.9	115.1	116.2	117.4	118.6	119
25.2	106.0	107.2	108.4	109.5	110.7	111.8	113.0	114.1	115.3	116.5	117.6	118
25.4	105.2	106.4	107.5	108.7	109.8	111.0	112.1	113.3	114.4	115.6	116.7	117
25.6	104.4	105.5	106.7	107.8	108.9	110.1	111.2	112.4	113.5	114.6	115.8	116
25.8	103.6	104.7	105.8	107.0	108.1	109.2	110.4	111.5	112.6	113.8	114.9	116
26.0	102.8	103.9	105.0	106.1	107.3	108.4	109.5	110.6	111.8	112.9	114.0	115
26.2	102.0	103.1	104.2	105.3	106.5	107.6	108.7	109.8	110.9	112.0	113.1	114
26.4	101.2	102.3	103.4	104.6	105.7	106.8	107.9	109.0	110.1	111.2	112.3	113
26.6	100.5	101.6	102.7	103.8	104.9	106.0	107.1	108.2	109.3	110.4	111.4	112
26.8	99.7	100.8	101.9	103.0	104.1	105.2	106.3	107.4	108.5	109.5	110.6	111
27.0	99.0	100.1	101.2	102.2	103.3	104.4	105.5	106.6	107.6	108.7	109.8	110
27.2	98.3	99.3	100.4	101.5	102.6	103.6	104.7	105.8	106.8	107.9	109.0	110
27.4	97.5	98.6	99.7	100.7	101.8	102.9	103.9	105.0	106.1	107.1	108.2	109
27-6	96.8	97.9	98.9	100.0	101.1	102.1	103.2	104.2	105.3	106.3	107.4	108
27.8	96.1	97.2	98.2	99.3	100.3	101.4	102.4	103.5	104.5	105.6	106.6	107
28.0	95.4	96.5	97.5	98.6	99.6	100.6	101.7	102.7	103.8	104.8	105.9	106
28.2	94.8	95.8	96.8	97.9	98.9	99.9	101.0	102.0	103.0	104.1	105.1	106
28.4	94.1	95.1	96.1	97.2	98.2	99.2	100.2	101.3	102.3	103.3	104.3	105
28.6	93.4	94.4	95.5	96.5	97.5	98.5	99.5	100.6	101.6	102.6	103.6	104
28.8	92.8	93.8	94.8	$95.\overline{8}$	96.8	97.8	98.8	99.8	100.8	101.8	102.8	103
29.0	92.1	93.1	94.1	95.1	96.2	97.2	98.2	99.2	100.2	101.2	102.2	103
29.2	91.5	92.5	93.5	94.5	95.5	96.5	97.5	98.5	99.5	100.5	101.5	102
29.4	90.9	91.9	92.9	93.9	94.8	95.8	96.8	97.8	98.8	998	100.8	101
29.6	90.3	91.3	92.2	93.2	94.2	95.2	96.2	97.2	98.2	99.1	100.1	101
29.8	89.7	90.6	91.6	92.6	93.6	94.5	95.5	96.5	97.5	98.5	99.4	100
30.0	89.1	90.0	91.0	92.0	92.9	93.9	94.9	95.9	96.8	97.8	98.8	99
30.2	88.5	89.4	90.4	91.4	92.3	93.3	94.3	95.2	96.2	97.2	98.1	99
30.4	87.9	88.8	89.8	90.8	91.7	92.7	93.6	94.6	95.6	96.5	97.5	98

When the Barometrical means to be used have been derived from observations taken at such hours of the day as, if combined, do not give the true mean pressure, they must be reduced to the true means by using the Tables XX. and XXI. These tables give the corrections to be applied to the hourly means, in each month, for reducing them to the means which would have been given by observations made at each of the twenty-four hours. The correction for any given set of hours is found by taking the mean of the corrections due to each of the combined hours, paying due attention to the signs. Table XX. has been computed from the hourly observations made under the superintendence of Professor A. D. Bache, at Girard College, Philadelphia. Table XXI. is from the Greenwich Observations, by Glaisher.

XX.

NORTH AMERICA. — PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Barometric Pressure of the respective Days, Months, and of the Year.

Barometer in English Inches.

Midnight. + 1	+.002 +.001 007 008 003 003 009 021	007 003 +.002 +.003 004 013 023 026	002 001 +.009 +.009 +.002 011 020	001 +.006 +.005 +.002 007	+.003 +.007 +.007 +.003 006 019 026	+.007 +.010 +.007 +.002 007 022	+.001 +.004 +.003 010 019	001 +.004 +.005 +.001 005 017	+.005 +.010 +.009 +.005 006 016	+.007 +.011 +.011 +.007 003 012	+.007 +.011 +.007 +.003 006 012	010 011 016 014 010 008 015	1nch. 0024 +.0007 +.0030 +.0036 +.0038 0050 0147
Midnight. + 1	+.002 +.001 007 008 003 003 009 021 032 040	009 007 003 +.002 +.003 .000 004 013 023	007 002 001 +.009 +.002 011 020	004 001 +.006 +.005 +.002 007 020 029	002 +.003 +.007 +.007 +.003 006 019 026	+.003 +.007 +.010 +.007 +.002 007 022	007 +.001 +.004 +.003 010 019	003 001 +.004 +.005 +.001 005 017	002 +.005 +.010 +.009 +.005 006 016	+.007 +.007 +.011 +.011 +.007 003 012	+.003 +.007 +.011 +.007 +.003 006 012	010 011 016 014 010 008 015	0024 +.0007 +.0030 +.0036 +.0038 0050 0147
1 + 2 - 3 - 4 - 5 - 6 - 7 - 8 - 9	+.001 007 008 003 003 009 021 032 040	007 003 +.002 +.003 004 013 023 026	002 001 +.009 +.009 +.002 011 020	001 +.006 +.005 +.002 007 020 029	+.003 +.007 +.007 +.003 006 019 026	+.007 +.010 +.007 +.002 007 022	+.001 +.004 +.003 010 019	001 +.004 +.005 +.001 005 017	+.005 +.010 +.009 +.005 006 016	+.007 +.011 +.011 +.007 003 012	+.007 +.011 +.007 +.003 006 012	011 016 014 010 008 015	+.0007 +.0030 +.0036 +.0038 0050 0147
2	007 008 003 003 009 021 032 040	003 +.002 +.003 .000 004 013 023	001 +.009 +.009 +.002 011 020 028	+.006 +.005 +.002 007 020 029	+.007 +.007 +.003 006 019 026	+.010 +.007 +.002 007 022	+.004 +.003 .000 010 019	+.004 +.005 +.004 005 017	+.010 +.009 +.005 006 016	+.011 +.011 +.007 003 012	+.011 +.007 +.003 006 012	016 014 010 008 015	+.0030 +.0036 +.0038 0050 0147
3 - 4 - 5 - 6 - 7 - 8 - 9 -	008 003 003 009 021 032 040	+.002 +.003 .000 004 013 023	+.009 +.009 +.002 011 020 028	+.005 +.002 007 020 029	+.007 +.003 006 019 026	+.007 +.002 007 022	+.003 010 019	+.005 +.004 005 017	+.009 +.005 006 016	+.011 +.007 003 012	+.007 +.003 006 012	014 010 008 015	+.0036 +.0038 0050 0147
4 - 5 - 6 - 7 - 8 - 9	003 003 009 021 032 040	+.003 .000 004 013 023 026	+.009 +.002 011 020 028	+.002 007 020 029	+.003 006 019 026	+.002 007 022	.000 010 019	+.004 005 017	+.005 006 016	+.007 003 012	+.003 006 012	010 008 015	+.0038 0050 0147
5 -6 -7 -8 -9 -	003 009 021 032 040	.000 004 013 023 026	+.002 011 020 028	007 020 029	006 019 026	007 022	010 019	005 017	006 016	003 012	006 012	008 015	0050 0147
6 - 7 - 8 -	009 021 032 040	004 013 023 026	011 020 028	020 029	019 026	022	019	017	016	012	012	015	0147
7 - 8 - 9 -	021 032 040	013 023 026	020 028	029	026								
8 -	032 040	023 026	028			024	025	023	023	_ 091	010		0000
9 -	040	026		034						021	019	023	0222
9 -	040	026		034		000	000	000	000	000	000	0.30	0000
- 1				1 1							1		1
10 -	041							1				3	
			1										i e
11 -	023	019	016	023	018	019	019	022	021	014	017	011	0185
Noon.	+ 006	004	002	008	006	010	012	012	009	+.001	+.006	+.005	0037
110011.				+.006									+.0107
	,		1								l .		+.0240
			1										+.0287
"	1.004	1.004	1.001	1.004	1.020	11015	1.020		1.021	1.020	1.000	001	1.020.
4 +	+.031	+.032	+.034	+.042	+.032	+.027	+.027	+.027	+.030	+.028	+.027	+.030	+.0306
5 +	+.024	+.024	+.025	+.036	+.034	+.030	+.028	+.029	+.027	+.021	+.018	+.026	+.0267
6 +	+.015	+.014	+.016	+.031	+.027	+.023	+.028	+.028	+.023	+.012	+.005	$\pm .021$	+.0202
7 +	+.003	+.006	+.007	+.022	+.016	+.018	+.021	+.018	+.016	+.001	002	+.018	+.0123
		0.00	000		. 000	. 010		. 000	. 00-	000	00.1	. 010	
													+.0010
·													0027
	(0065
11	+.002	011	017	010	019	005	002	002	004	009	003	+.005	0064
_					201		20:	0.00	•				
, ,			i	001				1					+ .001
												+.008	
9,12,3,9	.000	001	001	002	 004	004	004	004	004	 003	001	+.005	002

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XXI. England. — Greenwich. Lat. 51° 29′ N.; Long. 0° 0′. Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Barometric Pressure for the respective Months.—Glaisher.

English Inches.

Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midn	.000	001	002	008	005	.000	006	010	005	005	011	004	005
1	.001	.004	.013	.000	.002	.004	.000	.000	.000	.004	005	.001	.002
2	.002	.008	.020	.007	.004	.005	.003	.007	.005	.010	.003	.006	.007
3	.005	.012	.023	.010	.005	.004	.005	.011	.010	.015	.008	.010	.009
4	.011	.014	.022	.011	.005	.001	.005	.014	.012	.020	.013	.012	.012
5	.015	.015	.019	.011	.006	002	.006	.011	.014	.022	.016	.014	.012
6	.015	.012	.012	.006	.006	006	.002	.005	.010	:018	.015	.011	.009
7	.010	.007	.005			010	004	.000	.001	.008	.010	.006	.003
, ,													
8	.003	.000	004	00s	.003	012	008	007	006	003	.003	.004	003
9		}	010					ı		I	ł	ł.	1 1
10	i .	i .	015					l		l	007		012
11	1	1	015					ı		ı	ì	1	1 1
	.014	.010	.010	.011	.000	1000	1000	1000	.010	.011		.010	1022
Noon	005	_ 012	010	- 008	- 002	- 006	006	005	- 005	010	.002	009	006
1	.002		005			003		.000		003	.007	1	001
2	.002	.003	.000	.003	.003	.003	.001	.003	.004	.004	-011	.008	.004
3	.003	.005	003	.009	.006	.007	.005	.005	.008	.004	.010	.010	.004
9	.004	.000	003	•009	.000	.007	•000	.005	•003	.005	.010	•010	.000
4	.002	.008	.005	.004	.010	.013	.009	.009	.010	.003	.008	.009	.007
5	.002	.006	.004	.014	.014	.013	.013	.011	.011	.000		.006	.008
6	003	.002	.000	.014	.014	.017	.013	.011	.006	1	.000	.002	.006
7	1	004		ì		.014		.005		003	1	002	.000
,	005	004	006	007	.010	*014	.010	*009	.000	003	000	~.003	1000
8	_ 006	_ 006	012	_ 005	.000	.008	00.1	005	_ 005	_ 011	_ 012	_ 006	_ 005
9	1		015	1	1	!		010					
10		l .	013		i	,		015		l	1	ł) !
	l	t .	012 010		ı	,				l .		l .	
11	004	005	010	012	005	002	012	015	011	009	017	009	009
											1		
6. 6	.006	.007	.006	.008	.011	.005	.008	.008	.008	.006	.007	.006	.008
7. 7	.002	.002		005	.008	.002	.003	.002	.000	.000		.002	.001
8. 8	002		008		l	l	002		006		004	001	1 1
0.0													
9. 9	007	008	013	010	006	004	005	009	010	012	011	009	009
10.10	007		014										i I
7. 2. 9	.003	1	003	i .		l	l .	002	ł.	1	.001	.002	.001
					,,,,,,	.501		.502					
6. 2. 8	.005	.003	.000	.001	.003	.002	.002	.001	.003	.004	.005	.004	.003
6. 2.10	.005	.003	.000	1		002	l .	002	.001	.003	.002	.003	.001
6. 2. 6	.006	ł	J	.007		005		.006	.007	.006	ŀ	.007	.006
3. 2. 0								1.550		1.550			
7. 2	.007	.005	.003	.000	.004	001	001	.002	.002	.006	.010	.007	.003
8. 2	.004	1	002	1		í	003	ł	001	.000	.007	.006	.001
8. 1	.002	i		006	1	l	006		003	003	.005	.003	002
7. 1	.006			003		l	003	i	.000	.002	.008	.004	.001
								}					
9.12.3.9	004	005	008	005	002	002	003	004	004	007	002	004	004
·							<u> </u>						

XXII. TABLE TO REDUCE, BY INTERPOLATION,

THE OBSERVATIONS TO THE SAME ABSOLUTE TIME.

DECIMALS OF AN HOUR.

Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.	Min.	Decimal.
								l			
1	.017	11	.183	21	.350	31	.517	41	.683	51	.850
2	.033	12	.200	22	.367	32	.533	42	.700	52	.867
3	.050	13	.217	23	.383	33	.550	43	.717	53	.883
4	.067	14	.233	24	.400	34	.567	44	.733	54	.900
						1					
5	.083	15	.250	25	.417	35	.583	45	.750	55	.917
6	.100	16	.267	26	.433	36	.600	46	.767	56	.933
7	.117	17	.283	27	.450	37	.617	47	.783	57	.950
8	.133	18	.300	28	.467	38	.633	48	.800	58	.967
9	.150	19	.317	29	.483	39	.650	49	.817	59	.983
						1				1	
10	.167	20	.333	30	.500	40	.667	50	.833	60	1.000

TABLE FOR CORRECTION OF CURVATURE AND REFRACTION.

From a mountain, when furnished with a barometer, or with an apparatus for determining the temperature of boiling water, and a pocket level, an observer can find the elevations of distant points, which are in sight, but lower than the mountain itself on which he stands. He has only to seek, with the level, the point on the slope of the mountain which corresponds to the point at a distance that he wishes to determine, and to take there a barometrical, or a boiling point observation. This observation is to be calculated in the usual way, but the result must be corrected for the curvature of the surface of the globe, and for the atmospheric refraction, by means of the following Table.

This method, which furnishes the means of multiplying, without much trouble, the measurements of heights, gives approximations which are sufficient for most of the purposes of Physical Geography. It may even seem preferable to direct measurements for determining the mean elevation of certain physical lines, which are best estimated when seen from a distance; such as the upper limit of the growth of trees, the limits of different kinds of vegetation, that of permanent snow, that of the mean elevation of the crest of a mountain range, &c.

Table XXIII. is taken from Captain Lee's Collection of Tables and Formulæ, 2d edit., page 81.

XXIII. CORRECTIONS FOR CURVATURE AND REFRACTION.

Showing the Difference of the Apparent and True Level, in feet and decimals, for Distances in feet and miles.

	c	Correction in F	eet.		c	orrection in F	eet.
Distances				Distances			1
in Feet.	For Curvature.	For Re- fraction.	For Curva- ture and Refraction.	in Miles.	For Curvature.	For Re- fraction.	For Curva- ture and Refraction.
100	.00024	.00004	.00020	1 1	.0417	.0060	.0357
150	.00054	.00008	.00046	1 2	.1668	.0238	.1430
200	.00094	.00013	.00083	1 1 2 3 4	.3752	.0536	.3216
250	.00149	.00021	.00128	1	.6670	.0953	.5717
300	.00215	.00031	.00184	11/2	1.5008	.2144	1.2864
350	.00293	.00042	.00251	2	2.6680	.3811	2.2869
400	.00383	.00055	.00328	$2\frac{1}{2}$	4.1688	•5955	3.5733
450	.00484	.00069	.00415	3	6.0030	.8561	5.1469
500	.00598	.00085	.00513	$3\frac{1}{2}$	8.1708	1.1673	7.0035
550	.00724	.00103	.00621	4	10.6720	1.5246	9.1474
600	.00861	.00123	.00738	$4\frac{1}{2}$	13.5468	1.9295	11.5773
650	.01010	.00144	.00866	5	16.6750	2.3821	14.2929
700	.01172	.00167	.01005	5½	20.1769	2.8824	17.2945
750	.01345	.00192	.01153	6	24.0120	3.4303	20.5817
800	.01531	.00219	.01312	$6\frac{1}{2}$	28.1809	4.0258	24.1551
850	.01728	.00247	.01481	7	32.6830	4.6690	28.0143
900	.01938	.00277	.01661	71/2	37.5190	5.3599	32.1591
950	.02159	.00308	.01851	8	42.6880	6.0997	36.5883
1000	.02392	.00333	.02059	81/2	48.1910	6.8844	41.3066
1050	.02638	.00377	.02261	9	54.0270	7.7181	46.3089
1100	.02895	.00414	.02481	$9^1_{\bar{2}}$	60.1971	8.5996	51.5975
1150	.03164	.00452	.02712	10	66.7000	9.5286	57.1714
1200	.03445	.00492	.02953	11	80.7070	11.5296	69.1774
1250	.03738	.00534	.03204	12	96.0480	13.7211	82.3269
1300	.04043	.00578	.03465	13	112.7230	16.1033	96.6197
1350	.04361	.00623	.03738	14	130.7320	18.6760	112.0560
1400	.04689	.00670	.04019	15	150.0750	21.4393	128.6357
1450	.05030	.00719	.04311	16	170.7520	24.3931	146.3589
1500	.05383	.00769	.04614	17	192.7630	27.5376	165.2254
1550	.05748	.00821	.04927	18	216.1086	30.8727	185.2359
1600	.06125	.00875	.05250	19	240.7870	34.3981	206.3889
1650	.06514	.00931	.05583	20	266.8000	38-1143	228.6857
1700	.06914	.00988	.05926				
1750 1800	.07327 .07752	.01047	.06280	j			
1500	.01134	.01107	.06645				
1850	.08188	.01170	.07018				
1900 1950	.08637	.01234	.07403				
2000	.09098	.01300	.07798				
2000	.09570	.01367	.08203				

THERMOMETRICAL

MEASUREMENT OF HEIGHTS,

OR

TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM OBSERVATIONS OF THE TEMPERATURE OF BOILING WATER.

THERMOMETRICAL MEASUREMENT OF HEIGHTS.

TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of the vapors produced from it gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles, and the water boils. The temperature at which, in the open air, water boils, thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the higher the station where an observation is taken, the lower the temperature at which water boils at that station will be.

The difference of elevation between two places, therefore, can be deduced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and, the atmospheric pressures at both places being known, to compute the difference of level by a formula, or by the tables given above for computing heights from barometrical observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometrical observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water gives only indirectly the atmospheric pressure, which is given directly by the barometer. This method is thus liable to all the chances of error which may affect the measurements by means of the barometer, besides adding to them new ones peculiar to itself, the principal of which, not to speak of the differences exhibited in the various tables of the force of vapor, is the difficulty of ascertaining with the necessary accuracy the true temperature of boiling water. In the present state of thermometry it would hardly be safe, indeed, to answer, in the most favorable circumstances, for quantities so small as hundredths of degrees, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and the substance of the vessel containing the water, the nature of the water itself, the place at which the bulb of the thermometer is placed, whether in the current of steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric

D 96'

pressure. Owing to these various causes, an observation of the boiling point, differing by one tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimetres in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one tenth of a millimetre, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer, or thermobarometer, is of the greatest utility to travellers traversing distant or rough countries, on account of its being more conveniently transported, and much less liable to accidents than the mercurial barometer. The best form for it is that contrived and described by Regnault in the *Annales de Chimie et de Physique*, Tom. XIV. p. 202. It consists of an accurate thermometer with long degrees, subdivided into tenths, whose bulb is placed, about 2 or 3 centimetres above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp. The whole instrument when closed is about 6 inches long; when drawn out for observation, about 14 inches.

Table XXIV. of barometric pressures corresponding to temperatures of boiling water, has been calculated by Regnault from his Tables of Forces of Vapor, and published in the *Annales de Chimie et de Physique*, Tom. XIV. p. 206. It gives, in millimetres of mercury, the barometric pressures corresponding to every tenth of a Centigrade degree; for greater convenience, the values for every hundredth have been added.

The accuracy of this table has been tested by direct observation by Mr. Wisse, a traveller competent in such matters, who noted down simultaneously the temperatures of the boiling point of water and the height of the barometer, in various parts of the Andes, up to the summit of the volcano of Pichincha, including in his observations barometrical pressures ranging from 752 to 430 millimetres of mercury. The agreement between the barometric pressures given here by Regnault and those found by Wisse are very satisfactory, the differences never exceeding a few tenths of a millimetre. See *Annales de Chimie et de Physique*, Tom. XXVIII. p. 123.

Table XXV. is the same table, revised by A. Moritz, who, in a communication to the Académie des Sciences, in October, 1856, called the attention to some slight errors of computation in Regnault's table, and gave the corrected numbers for every whole degree from 40° to 102° Centigrade. Those numbers are given here from 80° upwards, as published in the *Journal de l'Institut*; the values for every tenth of a degree, and their differences, have been computed to fit the table for practical use. The comparison of the two tables will show that the corrections mostly amount to a few hundredths, and never exceed one tenth of a millimetre.

Table XXVI. is table XXV. reduced to English measures.

1										
Centig.			,		Iundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
85.0	433.04	433.21	433.38	433.55	433.72	433.89	434.07	434.24	434.41	434.58
85.1	434.75	434.92	435.09	435.26	435.43		435.78	435.95	436.12	436.29
85.2	436.46	436.63	436.80	436.97	437.14		437.49	437.66	437.83	438.00
85.3	438.17	438.34	438.51	438.69	438.86	1	439.20	439.37	439.55	439.72
85.4	439.89	440.06	440.23	440.41	440.58	440.75	440.93	441.10	441.27	441.45
85.5	441.62	441.79	441.97	442.14	442.31	442.48	442.66	442.83	443.00	443.18
85.6	443.35	443.52	443.70	443.87	444.05	444.22	444.39	444 57	444.74	444.92
85.7	445.09	445.26	445.44	445.61	445.79	445.96	446.14	446.31	446.49	446.67
85.8	446.84	447.01	447.19	447.36	447.54	447.71	447.89	448.06	448.24	448.41
85.9	448.59	448.76	448.94	449.11	449.29	449.46	449.64	449.81	449.99	450.16
86.0	450.34	450.52	450.69	450.87	451.04	451.22	451.40	451.57	451.75	451.92
86.1	452.10	452.28	452.45	452.63	452.81	452.98	453.16	453.34	453.52	453.69
86.2	453.87	454.05	454.22	454.40	454.58	454.75	454.93	455.11	455.29	455.46
86.3	455.64	455.82	456.00	456.17	456.35	456.53	456.71	456.89	457.06	457.24
86.4	457.42	457.60	457.78	457.96	458.14	458.31	458.49	458.67	458.85	459.03
86.5	459.21	459.39	459.57	459.75	459.93	460.10	460.28	460.46	460.64	460.82
86.6	461.00	461.18	461.36	461.54	461.72	461.90	462.08	462.26	462.44	462.62
86.7	462.80	462 98	463.16	463.34	463.52	463.70	463.88	464.06	464.24	464.42
86.8	464.60	464.78	464.96	465.14	465.32	465.50	465.69	465.87	466.05	466.23
86.9	466.41	466.59	466.77	466.95	467.13	467.31	467.50	467.68	467.86	468.04
87.0	468.22	468.40	468.58	468.77	468.95	469.13	469.31	469.49	469.68	469.86
87.1	470.04	470.22	470.41	470.59	470.77	470.95	471.14	471.32	471.50	471.69
87.2	471.87	472.05	472.24	472.42	472.60	472.78	472.97	473.15	473.33	473.52
87.3	473.70	473.88	474.07	474.25	474.44	474.62	474.80	474.99	475.17	475.36
87.4	475.54	475.72	475.91	476.09	476.28	476.46	476.64	476.83	477.01	477.20
87.5	477.38	477.56	477.75	477.93	478.12	478.30	478.49	478.67	478.86	479.04
87.6	479.23	479.41	479.60	479.78	479.97	480.15	480.34	480.52	480.71	480.89
87.7	481.08	481.27	481.45	481.64	481.82	482.01	482.20	482.38	482.57	482.75
87.S	482.94	483.13	483.31	483.50	483.69	483.87	484.06	484.25	484.44	484.62
87.9	484.81	485.00	485.19	485.37	485.56	485.75	485.94	486.13	486.31	486.50
88.0	486.69	486.88	487.07	487.25	487.44	487.63	487.82	488.01	488.19	488.38
88.1	488.57	488.76	488.95	489.13	489.32	489.51	489.70	489.89	490.07	490.26
88.2	490.45	490.64	490.83	491.02	491.21	491.39	491.58	491.77	491.96	492.15
88.3	492.34	492.53	492.72	492.91	493.10	493.29	493.48	493.67	493.86	494.05
88.4	494.24	494.43	494.62	494.81	495.00	495.19	495.39	495.58	495.77	495.96
88.5	496.15	496.34	496.53	496.72	496.91	497.10	497.30	497.49	497.68	497.87
88.6	498.06	498.25	498.44	498.64	498.83	499.02	499.21	499.40	499.60	499.79
88.7	499.98	500.17	500.36	500.56	500.75	500.94	501.13	501.32	501.52	501.71
88.8	501.90	502.09	502.28	502.48	502.67	502.86	503.05	503.24	503.44	503.63
88.9	503.82	504.01	504.21	504.40	504.60	504.79	504.98	505.18	505.37	505.57
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

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Centig.				ŀ	lundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.
89.0	505.76	505.95	506.15	506.34	506.54	506.73	506.92	507.12	507.31	507.51
89.1	507.70	507.89	508.09	508.28	508.48	508.67	508.87	509.06	509.26	509.45
89.2	509.65	509.84	510.04	510.23	510.43	510.62	510.82	511.01	511.21	511.40
89.3	511.60	511.80	511.99	512.19	512.38	512.58	512.78	512.97	513.17	513.36
89.4	513.56	513.76	513.95	514.15	514.35	514.54	514.74	514.94	515.14	515.33
89.5	515.53	515.73	515.92	516.12	516.32	516.51	516.71	516.91	517.11	517.30
89.6	517.50	517.70	517.90	518.09	518.29	518.49	518.69	518.89	519.08	519.28
89.7	519.48	519.68	519.88	520.07	520.27	520.47	520.67	520.87	521.06	521.26
89.8	521.46	521.66	521.86	522.06	522.26	522.46	522.66	522.86	523.05	523.25
89.9	523.45	523.65	523.85	524.05	524.25	524.45	524.65	524.85	525.05	525.25
90.0	525.45	525.65	525.85	526.05	526.25	526.45	526.65	526.85	527.05	527.25
90.1	527.45	527.65	527.85	528.05	528.25	528.45	528.66	528.86	529.06	529.26
90.2	529.46	529.66	529.86	530.07	530.27	530.47	530.67	530.87	531.08	531.28
90.3	531.48	531.68	531.88	532.09	532.29	532.49	532.69	532.89	533.10	533.30
90.4	533.50	533.70	533.91	534.11	534.31	534.51	534.72	534.92	535.12	535.33
90.5	535.53	535.73	535.94	536.14	536.35	536.55	536.75	536.96	537.16	537.37
90.6	537.57	537.77	537.98	538.18	538.39	538.59	538.79	539.00	539.20	539.41
90.7	539.61	539.81	540.02	540.22	540.43	540.63	540.84	541.04	541.25	541.45
90.8	541.66	541.87	542.07	542.28	542.48	542.69	542.90	543.10	543.31	543.51
90.9	543.72	543.93	544.13	544.34	544.54	544.75	544.96	545.16	545.37	545.57
91.0	545.78	545.99	546.19	546.40	546.61	546.81	547.03	547.23	547.44	547.64
91.1	547.85	548.06	548.26	548.47	548.68	548.88	549.09	549.30	549.51	549.71
91.2	549.92	550.13	550.34	550.54	550.75	550.96	551.17	551.38	551.58	551.79
91.3	552.00	552.21	552.42	552.63	552.84	553.04	553.25	553.46	553.67	553.88
91.4	554.09	554.30	554.51	554.72	554.93	555.14	555.35	555.56	555.77	555.98
91.5	556.19	556.40	556.61	556.82	557.03	557.24	557.45	557.66	557.87	558.08
91.6	558.29	558.50	558.71	558.92	559.13	559.34	559.55	559.76	559.97	560.18
91.7	560.39	560.60	560.81	561.03	561.24	561.45	561.66	561.87	562.09	562.30
91.8	562.51	562.72	562.93	563.15	563.36	563.57	563.78	563.99	564.21	564.42
91.9	564.63	564.86	565.06	565.27	565.48	565.69	565.91	566.12	566.33	566.55
92.0	566.76	566.97	567.19	567.40	567.61	567.85	568.04	568.25	568.46	563.63
92.1	568.89	569.10	569.32	569.53	569.75	569.96	570.17	570.39	570.60	570.82
92.2	571.03	571.24	571.46	571.67	571.89	572.10	572.32	572.53	572.75	572.96
92.3	573.18	573.40	573.61	573.83	574.04	574.26	574.48	574.69	574.91	575.12
92.4	575.34	575.56	575.77	575.99	576.20	576.42	576.64	576.85	577.07	577-28
92.5	577.50	577.72	577.93	578.15	578.37	578.58	578.80	579.02	579.24	579.45
92.6	579.67	579.89	580.10	580.32	580.54	580.75	580.97	581.19	581.41	581.62
92.7	581.84	582.06	582.28	582.49	582.71	582.93	583.15	583.37	583.58	583.80
92.8	584.02	584.24	584.46	584.68	584.90	585.11	585.33	585.55	585.77	585.99
92.9	586.21	586.43	586.65	586.87	587.09	587.31	587.53	587.75	587.97	588.19
	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.

Centig.				I	Hundredth	s of a Degi	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
93.0	Millim. 588.41	Millim. 588.63	Millim. 588.85	Millim. 589.07	Millim. 589.29	Millim. 589.51	Millim, 589.73	Millim. 589.95	Millim. 590.17	Millim. 590.39
93.1	590.61	590.83	591.05	591.27	591.49		591.94	592.16	592.38	1
93.2	592.82	593.04	593.26	593.49	593.71	593.93	594.15	594.37	594.60	592.60 594.82
93.3	595.04	595.26	595.48	595.71	595.93		596.37	596 59	596.82	597.04
93.4	597.26	597.48	597.71	597.93	598.15	598.37	598.60	598.82	599.04	599.27
93.5	599.49	599.71	599.94	600.16	600.38	600.60	600.83	601.05	601.27	601.50
93.6	601.72	601.94	602.17	602.39	602.62	602.84	603.07	603.29	603.52	603.74
93.7	603.97	604.19	604.42	604.64	604.87	605.09	605.32	605.54	605.77	605.99
93.8	606.22	606.45	606.67	606.90	607.12	607.35	607.58	607.80	608.03	608.25
93.9	608.48	608.71	608.93	609.16	609.38	609.61	609.84	610.06	610.29	610.51
94.0	610.74	610.97	611.19	611.42	611.65	611.87	612.10	612.33	612.56	612.78
94.1	613.01	613.24	613.47	613.69	613.92	614.15	614.38	614.61	614.83	615.06
94.2	615.29	615.52	615.75	615.97	616.21	616.43	616.66	616.89	617.12	617.35
94.3	617.58	617.81	618.04	618.27	618.50	618.72	618.95	619.18	619.41	619.64
94.4	619.87	620.10	620.33	620.56	620.79	621.02	621.25	621.48	621.71	621.94
94.5	622.17	622.40	622.63	622.86	623.09	623.32	623.56	623.79	624.02	624.25
94.6	624.48	624.71	624.94	625.17	625.40	625.63	625.87	626.10	626.33	626.56
94.7	626.79	627.02	627.25	627.49	627.72	627.95	628.18	628.41	628.65	628.88
94.8	629.11	629.34	629.58	629.81	630.04	630.27	630.51	630.74	630.97	631.21
94.9	631.44	631.67	631.91	632.14	632.38	632.61	632.84	633.08	633.31	633.55
95.0	633.78	634.01	634.25	634.48	634.72	634.95	635.18	635.42	635.65	635.89
95.1	636.12	636.35	636.59	636.82	637.06	637.29	637.53	637.76	638.00	638.23
95.2	638.47	638.71	638.94	639.18	639.41	639.65	639.89	640.12	640.36	640.59
95.3	640.83	641.07	641.30	641.54	641.77	642.01	642.25	642.48	642.72	642.95
95.4	643.19	643.43	643.67	643.90	644.14	644.38	644.62	644.86	645.09	645.33
95.5	645.57	645.81	646.05	646.28	646.52	646.76	647.00	647.24	647.47	647.71
95.6	647.95	648.19	648.43	648.67	648.91	649.14	649.38	649.62	649.86	650.10
95.7	650.34	650.58	650.82	651.06	651.30	651.53	651.77	652.01	652.25	652.49
95.8	652.73	652.97	653.21	653.45	653.69	653.93	654.17	654.41	654.65	654.89
95.9	655.13	655.37	655.61	655.85	656.09	656.33	656.58	656.82	657.06	657.30
96.0	657.54	657.78	658.02	658.26	658.50	658.74	658.99	659.23	659.47	659.71
96.1	659.95	660.19	660.43	660.68	660.92	661.16	661.40	661.64	661.89	662.13
96.2	662.37	662.61	662.86	663.10	663.34	663.58	663.83	664.07	664.31	664.56
96.3	664.80	665.04	665.29	665.53	665.78	666.02	666.26	666.51	666.75	667.00
96.4	667.24	667.48	667.73	667.97	668.22	668.46	668.71	668.93	669.20	669.44
96.5	669.69	669.93	670.18	670.42	670.67	670.91	671.16	671.40	671.65	671.99
96.6	672.14	672.39	672.63	672.88	673.12	673.37	673.62	673.86	674.11	674.35
96.7	674.60	674.85	675.09	675.34	675.59	675.83	676.08	676.33	676.58	676.82
96.8	677.07	677.32	677.57	677.81	678.06	678.31	678.56	678.81	679.05	679.30
96.9	679.55	679.80	680.05	680.29	680.54	680.79	681.04	681.29	681.53	681.78
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

Centig.				H	lundredths	of a Degr	ee.			
Degrees.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim.	Millim
97.0	682.03	682.28	682.53	682.78	683.03	683.27	683.52	683.77	684.02	684.2
97.1	684.52	684.77	685.02	685.27	685.52	685.77	686.02	686.27	686.52	686.7
97.2	687.02	687.27	687.52	687.77	688.02	688.27	688.53	688.78	689.03	689.29
97.3	689.53	689.78	690.03	690.28	690.53	690.78	691.04	691.29	691.54	691.7
97.4	692.04	692.29	692.54	692.80	693.05	693.30	693.55	693.80	694.06	694.3
97.5	694.56	694.81	695.06	695.32	695.57	695.82	696.07	696.32	696.58	696.S
97.6	697.08	697.33	697.59	697.84	698.09	698.34	698.60	698.85	699.10	699.3
97.7	699.61	699.86	700.12	700.37	700.63	700.88	701.13	701.39	701.64	701.9
97.8	702.15	702.40	702.66	702.91	703.17	703.42	703.68	703.93	704.19	704.4
97.9	704.70	704.96	705.21	705.47	705.72	705.98	706.24	706.49	706.75	707.0
98.0	707.26	707.52	707.77	708.03	708.28	708.54	708.80	709.05	709.31	709.5
98.1	709.82	710.08	710.33	710.59	710.85	711.10	711.36	711.62	711.88	712.13
98.2	712.39	712.65	712.91	713.16	713.42	713.68	713.94	714.20	714.45	714.7
98.3	714.97	715.22	715.49	715.75	716.01	716.26	716.52	716.78	717.04	717.30
98.4	717.56	717.82	718.08	718.34	718.60	718.85	719.11	719.37	719.63	719.8
98.5	720.15	720.41	720.67	720.93	721.19	721.45	721.71	721.97	722.23	722.4
98.6	722.75	723.01	723.27	723.53	723.79	724.05	724.31	724.57	724.83	725.0
98.7	725.35	725.61	725.87	726.13	726.39	726.65	726.92	727.18	727.44	727.7
98.8	727.96	728.22	728.48	728.75	729.01	729.27	729.53	729.79	730.06	730.3
98.9	730.58	730.84	731.11	731.37	731.63	731.89	732.16	732.42	732.68	732.93
99.0	733.21	733.47	733.74	734.00	734.27	734.53	734.79	735.06	735.32	735.59
99.1	735.85	736.11	736.38	736.64	736.91	737.17	737.44	737.70	737.97	738.2
99.2	738.50	738.77	739.03	739.30	739.56	739.83	740.10	740.36	740.63	740.89
99.3	741.16	741.43	741.69	741.96	742.23	742.49	742.76	743.03	743.30	743.5
99.4	743.83	744.10	744.36	744.63	744.90	745.16	745.43	745.70	745.97	746.2
99.5	746.50	746.77	747.04	747.30	747.57	747.84	748.11	748.38	748.64	748.9
99.6	749.18	749.45	749.72	749.99	750.26	750.52	750.79	751.06	751.33	751.69
99.7	751.87	752.14	752.41	752.68	752.95	753.22	753.49	753.76	754.03	754.30
99.8	754.57	754.84	755.11	755.38	755.65	755.92	756.20	756.47	756.74	757.0
99.9	757.28	757.55	757.82	758.10	758.37	758.64	758.91	759.18	759.46	759.73
100.0	760.00	760.27	760.55	760.S2	761.09	761.36	761.64	761.91	762.18	762.40
100.1	762.73	763.00	763.28	763.55	763.82	764.09	764.37	764.64	764.91	765.19
100.2	765.46	765.73	766.01	766.28	766.56	766.83	767.10	767.38	767.65	767.9
100.3	768.20	768.47	768.75	769.02	769.30	769.57	769.85	770.12	770.40	770.6
100.4	770.95	771.23	771.50	771.78	772.05	772.33	772.61	772.88	773.16	773.43
100.5	773.71	773.99	774.26	774.54	774.82	775.09	775.37	775.65	775.93	776.20
100.6	776.48	776.76	777.04	777.31	777.59	777.87	778.15	778.43	778.70	778.98
100.7	779.26	779.54	779.82	780.09	780.37	780.65	780.93	781.21	781.48	781.70
100.8	782.04	782.32	782.60	782.88	783.16	783.43	783.71	783.99	784.27	784.5
100.9 101.0	784.83 787.63	785.11 787.91	785.39 788.19	785.67 788.47	785.95 788.75	786.23 789.03	786.51 789.31	786.79 789.59	787.07 789.87	787.3 790.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

TABLE XXV.

BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

BY REGNAULT, REVISED BY MORITZ.

Boiling Point, Centigrade.	Barometer in Millimetres,	Differ- ence,	Boiling Point, Centigrade.	Barometer in Millimetres,	Differ- ence.	Boiling Point, Centigrade.	Barometer in Millimetres.	Differ- ence.
80.0 80.1 80.2 80.3 80.4 80.5 80.6 80.7 80.8 80.9	351.62 356.06 357.50 358.96 360.41 361.87 363.34 364.81 366.29 367.77	1.44 1.45 1.45 1.46 1.46 1.47 1.47 1.48	83.0 83.1 83.2 83.3 83.4 83.5 83.6 83.7 83.8 83.9	400.07 401.66 403.26 404.87 406.48 408.10 409.72 411.35 412.98 414.62	1.60 1.60 1.61 1.61 1.62 1.62 1.63 1.63	86.0 86.1 86.2 86.3 86.4 86.5 86.6 86.7 86.8 86.9	450.30 452.06 453.83 455.60 457.38 459.17 460.96 462.75 464.55 466.36	1.76 1.77 1.77 1.78 1.78 1.79 1.80 1.80
81.0 81.1 81.2 81.3 81.4	369.26 370.75 372.25 373.75 375.25	1.49 1.49 1.50 1.51 1.51	84.0 84.1 84.2 81.3 84.4	416.26 417.91 419.57 421.23 422.89	1.64 1.65 1.66 1.66 1.67	87.0 87.1 87.2 87.3 87.4	468.17 469.99 471.82 473.65 475.49	1.81 1.92 1.83 1.83 1.84 1.84
81.5 81.6 81.7 81.9 81.9	376.77 378.28 379.81 381.33 382.87	1.52 1.52 1.53 1.53 1.54	84.5 84.6 84.7 84.8 84.9	424.56 426.24 427.92 429.61 431.30	1.68 1.69 1.69 1.70	87.5 87.6 87.7 87.8 87.9	477.33 479.18 481.04 482.90 484.76	1.85 1.86 1.86 1.67 1.87
82.1 82.2 82.3 82.4	385.95 387.49 389.05 390.61	1.54 1.55 1.55 1.56 1.56	85.1 85.2 85.3 85.4	434.71 436.42 438.13 439.85	1.70 1.71 1.72 1.72 1.73	88.1 88.2 88.3 88.4	488.52 490.40 492.29 494.19	1.89 1.89 1.89 1.90
82.5 82.6 82.7 82.8 82.9 83.0	392.17 393.74 395.31 396.89 398.48 400.07	1.57 1.57 1.58 1.58 1.59	85.5 85.6 85.7 85.8 85.9 86.0	441.58 443.31 445.05 446.80 448.55 450.30	1.73 1.74 1.74 1.75 1.76	88.5 88.6 88.7 88.8 88.9 89.0	496.09 498.00 500.92 501.81 503.77 505.70	1.91 1.92 1.92 1.93 1.93

			11		1	11		+
Boiling Point,	Barometer in	Differ-	Boiling Point,	Barometer in	Differ-	Boiling Point,	Barometer in	Differ
Centigrade.	Millimetres.	ence.	Centigrade.	Millimetres.	ence.	Centigrade.	Millimetres.	ence.
			0					
89.0	505.70	1.94	93.0	588.33	2.20	97.0	681.93	
89.1	507.65	1.94	93.1	590.53	2.20	97.1	684.42	2.49
89.2	509.59		93.2	592.74	2.21	97.2	686.92	2.50
89.3	511.54	1.95	93.3	594.96		97.3	689.42	2.5
89.4	513.50	1.96 1.97	93.4	597.18	2.22	97.4	691.94	2.5
89.5	515.47	1.97	93.5	599.41	2.24	97.5	694.46	0.5
89.6	517.44	-	93.6	601.65	2.24	97.6	696.98	2.5
89.7	519.42	1.98	93.7	603.89	2.24	97.7	699.52	2.5
89.8	521.40	1.98	93.8	606.14	2.25	97.8	702.06	2.5
89.9	523.39	1.99 2.00	93.9	608.40	2.26	97.9	704.62	2.5
90.0	525.39	2.00	94.0	610.66	0.07	98.0	707.17	
90.1	527.40	2.00	94.1	612.93	2.27	98.1	709.74	2.5
90.2	529.41	2.01	94.2	615.21	2.28	98.2	712.31	2.5
90.3	531.42	2.02	94.3	617.50	2.29	98.3	714.90	2.5
90.4	533.44	2.02 2.03	94.4	619.79	2.29 2.30	98.4	717.49	2.5
90.5	535.47	0.01	94.5	622.09	2.31	98.5	720.08	
90.6	537.51	2.04	94.6	624.39	}	98.6	722.69	2.6
90.7	539.55	2.01	94.7	626.71	2.31	98.7	725.30	2.6
90.8	541.60	2.05	94.8	629.93	2.32	98.8	727.93	2.6
90.9	543.65	2.05 2.06	94.9	631.36	2.33	98.9	730.55	2.6
91.0	545.71	0.07	95.0	633.69	2.04	99.0	733.19	
91.1	547.78	2.07	95.1	636.03	2.34	99.1	735.84	2.6
91.2	549.86	2.07	95.2	638.38	2.35	99.2	738.49	2.6
91.3	551.94	2.08	95.3	640.74	2.36	99.3	741.15	2.6
91.4	554.03	2.09 2.09	95.4	643.10	2.36 2.37	99.4	743.82	2.6
91.5	556.12	2.10	95.5	645.48		99.5	746.50	
91.6	558.22	2.10	95.6	647.86	2.38 2.39	99.6	749.18	2.6
91.7	560.33	2.11	95.7	650.24	2.39	99.7	751.87	2.6
91.8	562.44	2.11	95.8	652.63	2.39	99.8	754.57	2.7
91.9	564.56	2.12	95.9	655.04	2.40	99.9	757.28	2.7 2.7
92.0	566.69	0.10	96.0	657.44	0.40	100.0	760.00	0
92.1	568.82	2.13	96.1	659.86	2.42	100.1	762.73	2.7
92.2	570.96	2.14	96.2	662.28	2.42	100.2	765.46	2.7
92.3	573.11	2.15 2.15	96.3	664.71	2.43	100.3	768.20	2.7
92.4	575.27	2.15	96.4	667.15	2.44	100.4	770.95	2.7
92.5	577.43	9.17	96.5	669.59	9.45	100.5	773.71	
92.6	579.59	2.17	96.6	672.05	2.45	100.6	776.47	2.7
92.7	581.77	2.17	96.7	674.51	2.46	100.7	779.25	2.7
92.8	583.95	2.18	96.8	676.97	2.47	100.8	782.03	2.7
92.9	586.14	2.19	96.9	679.45	2.47	100.9	784.82	2.7
93.0	588.33	2.19	97.0	681.93	2.48	101.0	787.62	2.8

TABLE XXVI.

BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

REDUCED FROM REGNAULT'S TABLE, REVISED BY MORITZ.

Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.
0 185.0 185.1 185.2 185.3 185.4	17.048 17.085 17.122 17.160 17.197	0.037 .037 .037 .037	0 188.0 188.1 188.2 188.3 188.4	18.195 18.235 18.274 18.314 18.353	0.039 .039 .039 .040	0 191.0 191.1 191.2 191.3 191.4	19.407 19.448 19.490 19.532 19.573	0.042 .042 .042 .042	0 194.0 194.1 194.2 194.3 194.4	20.685 20.729 20.773 20.817 20.861	0.044 .044 .044 .044
185.5 185.6 185.7 185.8 185.9	17.235 17.272 17.310 17.348 17.355	.038 .038 .038 .038	188.5 188.6 188.7 188.8 188.9	18.393 18.432 18.472 18.512 18.552	.040 .040 .040 .040	191.5 191.6 191.7 191.8 191.9	19.615 19.657 19.699 19.741 19.783	.042 .042 .042 .042	194.5 194.6 194.7 194.8 194.9	20.905 20.949 20.993 21.038 21.082	.044 .044 .044 .044
186.0 186.1 186.2 186.3 186.4	17.423 17.461 17.499 17.537 17.575	.008 .038 .038 .038	189.0 189.1 189.2 189.3 189.4	18.592 18.632 18.672 18.712 18.753	.040 .040 .040 .040	192.0 192.1 192.2 192.3 192.4	19.825 19.868 19.910 19.952 19.995	.042 .042 .042 .042 .042	195.0 195.1 195.2 195.3 195.4	21.126 21.171 21.216 21.260 21.305	.045 .045 .045 .045
186.5 186.6 186.7 186.9	17.614 17.652 17.690 17.729 17.767	.038 .038 .038 .038	189.5 189.6 189.7 189.8 189.9	18.793 18.833 18.874 18.914 18.955	.040 .040 .041 .041	192.5 192.6 192.7 192.8 192.9	20.037 20.080 20.123 20.166 20.208	.043 .043 .043 .043	195.5 195.6 195.7 195.8 195.9	21.350 21.395 21.440 21.485 21.530	.045 .045 .045 .045
187.0 187.1 187.2 187.3 187.4	17.806 17.844 17.883 17.922 17.961	.039 .039 .039 .039	190.0 190.1 190.2 190.3 190.4	18.996 19.036 19.077 19.118 19.159	.041 .041 .041 .041	193.0 193.1 193.2 193.3 193.4	20.251 20.294 20.338 20.381 20.424	.043 .043 .043 .043	196.0 196.1 196.2 196.3 196.4	21.576 21.621 21.666 21.712 21.758	.045 .045 .046 .046
187.5 187.6 187.7 187.8 187.9 188.0	18.000 18.039 18.078 18.117 18.156 18.195	.039 .039 .039 039 0.039	190.5 190.6 190.7 190.8 190.9 191.0	19.200 19.241 19.283 19.324 19.365 19.407	.041 .041 .041 .041	193.5 193.6 193.7 193.8 193.9 194.0	20.467 20.511 20.554 20.598 20.641 20.685	.043 .043 .044 .044	196.5 196.6 196.7 196.8 196.9 197.0	21.803 21.849 21.895 21.941 21.987 22.033	.046 .046 .046 .046 0.046

Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren.	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren	Barom- eter in English Inches.	Differ- ence.	Boiling Point, Fahren	Barom- eter in English Inches.	Difference.
0	0.2 000		0	22.040		0	25.000	,	0	00.100	
197.0	22.033	0.046	201.0	23.943	0.049	205.0	25.990	0.053	209.0	28.180	0.057
197.1	22.079	.046	201.1	23.993	.050	205.1	26.043	.053	209.1	28.237	.057
197.2	22.125	.046	201.2	24.042	.050	205.2	26.096	.053	209.2	28.293	.057
197.3	22.172	.046	201.3	24.092	.050	205.3	26.149	.053	209.3	28.350	.057
197.4	22.218	.046	201.4	24.142	.050	205.4	26 202	.053	209.4	28.407	.057
197.5	22.264		201.5	24.191		205.5	26.255		209.5	28.464	
197.6	22.311	.047	201.6	24.241	.050	205.6	26.309	.053	209.6	28.521	.057
197.7	22.358	.047	201.7	24.291	•050	205.7	26.362	.054	209.7	28.579	.057
197.8	22.404	-047	201.8	24.341	•050	205.8	26.416	.054	209.8	28.636	.057
197.9	22.451	.047	201.9	24.391	•050	205.9	26.470	.054	209.9	28.693	.057
10	22.701	-047	201.0	211001	-050	200.5	20.410	•054	200.0	20.035	.058
198.0	22.498		202.0	24.442	0-0	206.0	26.523		210.0	28.751	
198.1	22.545	.047	202.1	24.492	•050	206.1	26.577	•054	210.1	28.809	.058
198.2	22.592	.047	202.2	21.542	•050	206.2	26.631	.054	210.2	28.866	.058
198.3	22.639	.047	202.3	24.593	•050	206.3	26.685	.054	210.3	28.924	.058
198.4	22.686	.047	202.4	24.644	•05 ł	206.4	26.740	.054	210.4	28.982	.05S
		.047			.051			-054			.058
198.5	22.734	0.17	202.5	24.691	.051	206.5	26.794		210.5	29.040	
198.6	22.781	.047	202.6	24.745		206.6	26.848	•054	210.6	29.098	.058
198.7	22.829	.047	202.7	24.796	.051	206.7	26.903	•054	210.7	29.156	.058
198.8	22.576	.048	202.8	24.847	.051	206.8	26.957	.055	210.8	29.215	.058
198.9	22.924	.048	202.9	24.898	•051	206.9	27.012	•055	210.9	29.273	.058
		.048			.051			.055			•059
199.0	22.971	.048	203.0	24.949	.051	207.0	27.066	0.5	211.0	29.331	0.50
199.1	23.019	.049	203.1	25.000	.051	207.1	27.121	•055	211.1	29.390	.059
199.2	23.067		203.2	25.051	.051	207.2	27.176	•055	211.2	29.449	.059
199.3	23.115	.048	203.3	25.103		207.3	27.231	•055	211.3	29.508	.059
199.4	23.163	.048 .048	203.4	25.154	.051	207.4	27.286	.055	211.4	29.566	.059
199.5	23.211		203.5	25.206		207.5	07 041		011.5	20.60=	1000
199.6	23.259	.048	203.6	25.257	.052	207.6	27.341 27.397	.055	211.5	29.625	.059
199.7		.048	203.7	25.309	.052	207.7		.055	211.6	29.684	.059
	23.308	.048	203.7		.052		27.452	•055	211.7	29.744	.059
199.8	23.356	.048		25.361	.052	207.8	27.507	.056	211.8	29.803	.059
199.9	23.405	.049	203.9	25.413	.052	207.9	27.563	•056	211.9	29.862	.059
200.0	23.453		204.0	25.465		208.0	27.618		212.0	29.922	
200.1	23.502	.049	204.1	25.517	.052	208.1	27.674	.056	212.1	29.981	.060
200.2	23.550	.049	204.2	25.569	.052	208.2	27.730	.056	212.2	30.041	.060
200.3	23.599	•049	204.3	25.621	.052	208.3	27.786	.056	212.3	30.101	•060
200.4	23.648	.049	204.4	25.674	.052	208.4	27.842	.056	212.4	30.161	.060
		•049			.052			.056		20.101	.060
200.5	23.697	.049	204.5	25.726	.053	208.5	27. 898	.056	212.5	30.221	.060
200.6	23.746	.049	204.6	25.779	.053	208.6	27.954	.056	212.6	30.281	
200.7	23.795	.049	204.7	25.831	.053	208.7	28.011	.056	212.7	30.341	.060
200.8	23.845		204.8	25.884	.053	208.8	28.067		212.8	30.401	•060
200.9	23.894	.049 0.049	204.9	25.937	0.053	208.9	28.123	.056 0.057	212.9	30.461	.060
201.0	23.943	0.049	205.0	25.990	0.000	209.0	28.180	0.007	213.0	30.522	0.060



APPENDIX

70

THE HYPSOMETRICAL TABLES.

COMPARISON OF THE DIFFERENT MEASURES OF LENGTH MOST GENERALLY USED FOR INDICATING ALTITUDES.

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COMPARISON

OF THE MEASURES OF LENGTH MOST GENERALLY USED FOR INDICATING ALTITUDES.

It is too well known that the measures used in scientific researches among civilized nations are not uniform, as the convenience of all would require. In France the metre is employed; in England and North America, the yard and its third part, the English foot; in Germany, most commonly, the Old French or Paris foot, the sixth part of the French toise called the *Toise du Pérou*; at the same time, however, though not so extensively, the Rhine foot, in Denmark and Holland, and especially in Prussia, where it has been declared, under the name of Prussian foot, the legal measure in that kingdom; in Austria, the klafter of Vienna and its sixth part, the foot of Vienna; in Switzerland, the Swiss or federal foot, which has been adjusted to the metrical system, and is three tenths of a metre; and so on.

The numerous altitudes ascertained, either by private efforts, or in connection with the public works, and quite especially with the extensive geodetic operations carried on by the governments of these various countries for the survey of a regular map, are expressed in the measures respectively adopted by each of them. These heights, however, before they can be compared, require to be uniformly reduced to any one of these measures. Their relation to each other, therefore, is given here, together with numerous reduction tables, designed to save both the useless expenditure of time and the almost unavoidable errors arising from so numerous reductions.

The exact relation of the standard measures above mentioned is not easily ascertained, and the numbers given by the best authorities by no means always agree; for the manufacture of exact copies of a standard scale, and the accurate comparison of it, require considerable skill, and belong to the most delicate operations of physics. The numbers used for computing the following tables have been adopted, after a careful review of the authorities, as the most reliable. A few words on the most important original legal standards of measures may not be unwelcome. For further details on the subject the reader is referred principally to Dove's work, Maas und Messen, 2d edition, Berlin, 1835.

The principal original, legal standards are the following: -

1. The Toise du Pérou, the old French standard, made in 1735, in Paris, by Langlois, under the direction of Godin, is a bar of iron which has its standard length at the temperature of 13° Reaumur. It is known as the Toise du Pérou, because it was used by the French Academicians Bouguer and La Condamine in their measurement

of an arc of the meridian in Peru. What follows will show that it may almost be called the only common standard, to which all the others are referred for comparison.

- 2. The Metre is a standard bar of platina, made by Lenoir in Paris, which has its normal length at the temperature of zero Centigrade, or the freezing point. Its length is intended to make it a natural standard, and to represent the ten-millionth part of the terrestrial arc comprised between the equator and the pole, or of a quarter of the meridian. The length of this arc given by the measurement ordered for the purpose by the Assemblée Nationale, of the arc of the meridian between Barcelona, through France, to Dunkirk, combined with the measurements previously made in Peru and in Lapland, gave for the distance of the equator from the pole 5,130,740 toises, with an ellipticity of $\frac{1}{334}$, and for the length of the metre 443.29596 lines of the toise du Perou, assumed to be 443.296 lines, or 3 feet 11.296 lines. This last quantity was declared in 1799 to be the length of the legal metre, and vrai et définitif, and is the length of Lenoir's platina standard. Later and more extensive measurements in various parts of the globe, however, seem to indicate that this quantity is somewhat too small. The latest and most exact results we now possess, combined and computed by Bessel, would make the quarter of the meridian 10,000,856 metres, and the metre = 443.29979 Paris lines; Schmidt's computation would make it 443.29977 lines, and both numbers are confirmed by Airy's results. The legal metre is thus, in fact, as Dove remarks, a legalized part of the toise du Pérou, and this last remains the primitive standard. But it must be added that a natural standard, in the absolute sense of the word, is a utopian one, which ever-changing Nature never will give us. The metre is, for all practical purposes, what it was intended to be, a natural standard; though it must be confessed that, in practice, the question is not whether and how far a standard is a natural or a conventional one, but how readily and accurately it can be obtained, or recovered when lost.
- 3. The English Standard Yard is a brass bar, made by Bird in 1760, which was declared, by act of Parliament, 1st May, 1825, the legal measure of length when at the temperature of 62° Fahrenheit, under the name of Imperial Standard. Another standard, sometimes also called Parliamentary Standard, was made by Bird in 1758. Sir George Shuckburgh found both to be nearly identical, at least within 0.0002 of an inch. (Philos. Trans. for 1798, p. 170.)

Another scale of brass, however, made by Troughton for Sir George Shuckburgh, described in the *Philosophical Transactions for* 1798, and known as Shuckburgh's scale, obtained among scientific men, perhaps, a higher degree of authority, on account of the great accuracy of its division, and of its apparatus, devised by Troughton, for delicate comparisons. That scale was used by Captain Kater, in 1818, in his researches for determining the length of the pendulum beating a second at London, and also the length of the metre, expressed in English inches of the imperial standard. (*Phil. Trans. for* 1818.)

Numerous attempts to determine the relation between the English and the French measures show no inconsiderable discrepancies in their results. Omitting the older comparisons with the toise, we give here the value of the metre in English imperial inches, as resulting from the most reliable comparisons.

A standard scale made and divided by Troughton, and in all particulars identical

with Shuckburgh's scale, was brought to France in 1801 by Pictet. The comparison of it with the standard metre, made by Prony, Legendre, and Méchain, gave, after due reduction of the two standards to their respective normal temperatures,

1 metre at 32° Fahr. = 39.371 English imperial inches at 62° Fahr.

This determination was adopted for all reductions in Kelly's *Universal Cambist*, and in the French translation of the work, published in Paris in 1823.

A new comparison was made with great care by Captain H. Kater, in 1818. (See *Philos. Trans. for* 1818, p. 103.) The standards used were a brass scale metre, by Fortin, terminated with parallel planes (*mètre à bouts*), and a bar of platina on which the length of the metre was marked by two very fine lines (*mètre à traits*). Both were compared with Shuckburgh's scale, and a double series of experiments gave as the mean result:

Brass metre at 32° Fahr. = 39.37076 inches of Shuckburgh's scale at 62° Fahr.

Platina metre at 32° Fahr. = $\frac{39.37081}{39.37079}$ " " " " "

On this value of the metre are based the reduction tables by Matthieu, published yearly in the *Annuaire du Bureau des Longitudes*; and it has come into general use, both in Europe and in this country.

Captain Kater gives besides, in the same paper, p. 109, note, the value of the metre compared with Bird's Parliamentary standard as being

1 metre at 32° F. = 39.37062 imp. inches of Bird's Parliamentary standard at 62° F. This value has been adopted by Dove, as being the legal one, in his reduction tables in his work, *Maas und Messen*, p. 175, &c., and by many German authorities.

According to Baily's experiments, made in 1835, when engaged in constructing a new standard for the Royal Astronomical Society (Memoirs R. Ast. Soc., Vol. IX.), the value of the metre is (Lee, Collection of Tables and Formulæ, p. 62)

1 metre at 32° F. = 39.370092 imperial standard inches at 62° F.

The original legal standards having been lost in the fire which destroyed, several years ago, the Parliament Houses, an act of Parliament provided for the construction of new ones; but as the report of the committee having charge of the construction of the new British standard has not yet been published, the discussion of the subject must be postponed.

The value adopted in the following tables, is that determined by Captain Kater, viz. 1 metre = 39.37079 English inches.

It may not be out of place to remark that Schumacher, in the first edition of his Sammlung von Hülfstafeln, used the value 1 metre = 39.3827 English inches, as given in the Base du Système Métrique; but this number, which expresses the relation of both standards when at the freezing point, becomes 39.37079 when they are respectively reduced to their normal temperatures. Schumacher's tables, therefore, must be corrected accordingly.

4. The actual standard of length of the United States is a brass scale of eighty-two inches in length, prepared for the Coast Survey of the United States, by Troughton of London, meant to be identical with the English Imperial Standard, and deposited in the office of weights and measures. The temperature at which it is a standard is 62° Fahrenheit, and the yard measure is between the 27th and 63d inches of the

scale. (See Report on the Construction and Distribution of Weights and Measures, by Prof. A. D. Bache, 1857.)

Hassler, first Superintendent of the United States Coast Survey, made an elaborate comparison of eleven different standard metres with the brass scale of eighty-two inches, by Troughton. Three of the standard metres, certified to be correct by high authorities, seem to deserve especial confidence: - 1. An iron metre, presented to Mr. Hassler by Tralles, which was one of the three that Tralles had made by Lenoir at the same time with those distributed to the committee on the weights and measures. 2. Another metre of iron, also by Lenoir, verified by Bouvard and Arago, and declared by them to be identical with the original. 3. A platina standard by Fortin, verified by Arago, and found to be $\frac{1}{1000}$ of a millimetre too long, for which error allowance was made. Their comparison with the Troughton scale at the temperature of the freezing point gave:

- 1. Iron metre of Tralles = 39.3809171 inches of the Troughton scale.
- 2. Iron metre of Lenoir = 39.3799487
- 3. Platina metre of Fortin = 39.3804194

Or, correcting for expansion, and reducing them to their respective standard temperatures:

- = 39.36850= 39.36754 = 39.36789 English inches of the Troughton scale of 82 inches at 62° F. 1. Iron metre of Tralles at 32° F. 2. Iron metre of Lenoir at 32° F. = 39.36754
- 3. Platina metre of Fortin at 32° F. = 39.36789

Hassler, in his Report to Congress on Weights and Measures, in 1832, adopts the first value, viz.:

1 metre at 32° F. = 39.3809171 inches of the Troughton scale at 32° F; and the Troughton scale was declared the United States standard, from which copies were to be made.

This value materially differs from those given by other careful comparisons, while, on the other hand, the close accordance of the numbers corresponding to the various standard metres proves the accuracy of Hassler's method and comparison. It is, therefore, difficult not to ascribe, with Baily, this discrepancy to some inaccuracy in the length of the Troughton scale of 82 inches. But as that scale has been declared the standard of length of the United States, it seems better to call it, as is done in the Coast Survey Reports, the American yard, and its subdivisions the American foot and inch, and to consider it as a new standard, similar to, but not identical with, the English imperial standard. The value of the metre expressed in American standard inches is given in the Coast Survey Report for 1853, as

1 metre at 32° F. = 39.36850535 United States standard inches at 62° F.

We learn from the Report on Weights and Measures, by Prof. A. D. Bache, 1857, p. 18, that two copies of the new British standards, now in progress of construction, viz. a bronze standard, No. 11, and a malleable iron standard, No. 57, have been presented by the British government to the United States. A series of careful comparisons, made in 1856, by Mr. Saxton, under the direction of Prof. A. D. Bache, of the British bronze standard, No. 11, with the Troughton scale of eighty-two inches, showed that the British bronze standard yard is shorter than the American yard by 0.00087 inch.

Comparisons of the American standards with new French standards, recently presented to the United States by the French government, are still in progress.

For the present, however, it seems best to adhere to the value of the metre, expressed in American standard inches, adopted by the Coast Survey as given above. From this value the separate tables, which will be found below, for the reduction of the American yard and foot, were computed.

- 5. The Klafter of Vienna is a silver line let into a prismatic bar of iron, on which the length of the klafter was engraved by Voigtländer. It has its normal length at 13° Reaumur, and was declared by law, in 1816, the standard Klafter of Vienna. On the same silver line the French toise is marked, from the standard toise sent, in 1760, by La Caille and La Condamine to the Observatory of Vienna. According to a recent and very careful comparison by Struve (Mem. of the Austrian Acad., Vol. V., I. p. 117), the value of the klafter of Vienna is 0.9730317 toise du Pérou.
- 6. The *Prussian Foot* is marked on a standard iron bar, 3 feet long, made by Pistor in Berlin; it is a standard at the temperature of 13° Reaumur. The length of the Prussian foot was declared by law to be = 139.13 lines of the toise du Pérou.
- 7. A Mexican Vara, the standard length, brought from Mexico at the close of the war, by Major Turnbull of the Topographical Engineers, was presented to the Office of Weights and Measures. This standard was made by soldering sheet-brass upon the tinned surface of an iron bar. A careful comparison of its length with the American standard was made under the direction of Prof. Bache, which gave its length to be = 32.9682 inches at 58°.7 Fahrenheit, or 32.9680 when reduced to 62° Fahrenheit.

The relation of that particular Mexican standard to the Spanish standard not being known, it was thought better to adopt, for the present, the value of the Spanish Vara, and of its third part, the Castilian foot, found in Thionville, *Traité des Poids et Mesures*, &c., in Balbi's *Abrégé de Géographie*, viz. 1 vara = 0.847965 metre.

From the fundamental equations indicated above have been derived all those which have been used for computing the reduction tables given in the Appendix. At the head of each table will be found the value from which it was computed.

The tables are so arranged as to give *directly* the reduction of any whole number not exceeding three or four figures, and larger numbers within the limits needed for altitudes, by means of a *single* addition.

Example.

Reduce 25,351 English feet into metres.

In Table XVI., on the line beginning with 25,000 and in the column headed 300, take for 25,300 = 7711.30 metres.

In the second part of the table, on the line beginning with 50, and in column headed 1, take for 51 = 15.54 English feet 25,351 = 7726.84

The fractions, which seldom occur, are treated as whole numbers, taking care only properly to move the decimal point.

Tables XL. to XLIV. will be found convenient for converting fractional parts of a toise or of a foot into each other.

TO CONVERT

FRENCH TOISES

INTO DIFFERENT MEASURES OF LENGTH

I. CONVERSION OF FRENCH TOISES INTO METRES.

1 Toise = 1.94903631 Metre.

Toises.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.000	1.949	3.898	5.847	7.796	9.745	11.694	13.643	15.592	17.5
10	19.490	21.439	23.388	25.337	27.287	29.236	31.185	33.124	35.073	37.0
20	38.981	40.930	42.879	44.828	46.777	48.726	50.675	52.624	54.573	56.5
30	58.471	60.420	62.369	64.318	66.267	68.216	70.165	72.114	74.063	76.0
40	77.961	79.911	81.860	83.809	85.758	87.707	89.656	91.605	93.554	95.5
50	97.452	99.401	101.350	103.299	105.248	107.197	109.146	111.095	113.044	114.9
60	116.942	118.891	120.840	122.789	124.738	126.687	128.636	130.585	132.534	134.4
70	136.433	138.382	140.331	142.280	144.229	146.178	148.127	150.076	152.025	153.9
80	155.923	157.872	159.821	161.770	163.719	165.668	167.617	169.566	171.515	173.4
90	175.413	177.362	179.311	181.260	183.209	185.158	187.108	189.057	191.006	192.9
Thousands.					Hun	dreds.				
nousanas.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metre
0	0.00	194.90	389.81	584.71	779.61	974.52	1169.42	1364.33	1559.23	1754.
1000	1949.04	2143.94	2338.84	2533.75	2728.65	2923.55	3118.46	3312.36	3507.27	3702.
2000					4677.69	1	1	5262.40	1	į .
3000	5847.11	6042.01	6236.92	6431.82	6626.72	6821.63	7016.53	7211.44	7406.34	7601.
4000	7796.15	7991.05	8185.95	8380.86	8575.76	8770.66	8965.57	9160.47	9355.38	9550.
5000	9745.18	9940.09	10135.0	10329.9	10524.8	10719.7	10914.6	11109.5	11304.4	11499
	и. со	NVERSI	ON OF		INTO FI	RENCH (OR PARI	S FEET	•	
					Un	its.				
Toises. Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par Feet	Par Feet	Par.Feet.	Par. Feet	Par. Feet.	Par Feet.	Par.Feet.	Par. Feet	Par Feet	Par Fe
0	0.00	6	12	18	24	30	36	42	48	54
10	60	66	72	78	84	90	96	102	108	114
20	120	126	132	138	144	150	156	162	168	174
30	180	186	192	198	204	210	216	222	228	23-1
40	240	246	252	2 58	264	270	276	282	288	294
50	300	306	312	318	324	330	336	342	348	354
	360	366	372	378	384	390	396	402	408	414
60	11	1	100	438	414	450	456	462	468	474
60 70	420	426	432	4.00	717	100	100			313
	420 480	426 486	432 492	498	504	510	516	522	528	534

1 Toise = 6.3945916 English Feet.

Toises.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. feet.	Eng. feet.	Eng feet.	Eng feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng feet.	Eng feet.	Eng feet.
0	0.000	6.395	12.789	19.184	25.578	31.973	38.368	44.762	51.157	57.551
10	63.946	70.340	76.735	83.130	89.524	95.919	102.313	108.708	115.103	121.497
20	127.892	134.286	140.681	147.076	153.470	159.865	166.259	172.654	179.049	185.443
30	191.S38	198.232	204.627	211.021	217.416	223.811	230.205	236.600	242.994	249.389
40	255.784	262.178	268.573	274.967	281.362	287.757	294.151	300.546	306.940	313.335
50	319.729	326.124	332.519	338.913	345.308	351.702	358.097	364.492	370.886	377.281
60	383.675	390.070	396.465	402.859	409.254	415.648	422.043	428.438	434.832	441.227
70	447.621	454.016	460.410	466.805	473.200	479.594	485.989	492.383	498.778	505.173
80	511.567	517.962	524.356	530.751	537.146	543.540	549.935	556.329	562.724	569.119
90	l i			1		607.486	1	1		i
					Hund					
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet.		Eng. feet.	Eng. feet.	Eng. feet.	Eng feet.		Eng feet.	Eng feet.
0	0.0	639.5	1278.9	1918.4	2557.8	3197.3	3836.8	4476.2	5115.7	5755.1
1000	6394.6	7034.0	7673.5	8313.0	8952.4	9591.9	10231.3	10870.8	11510.3	12149.7
2000	12789.2	13428.6	14068.1	14707.6	15347.0	15986.5	16625.9	17265.4	17904.9	18544.3
3000	19183.8	19823.2	20462.7	21102.1	21741.6	22381.1	23020.5	23660.0	24299.4	24938.9
4000	25578.1	26217.8	26857.3	27496.7	28136.2	28775.7	29415.1	30054.6	30694.0	31333.5
5000	31972.9	32612.4	33251.9	33891.3	34530.8	35170.2	35809.7	36449.2	37088.6	37728.1
	IV. COI	NVERSIO			942205 Am	INTO A erican Feet		N FEET	•	
Toises.			1	_	l _	1 _	1 _	1		
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
•	Am Feet.			Am. Feet.		1	Am Feet	i .	l .	1
0	0.000		12.788	19.183		31.971	38.365	44.760	51.154	l
10	63.942	i	76.731	83.125		ı	102.308		l	
20	li .	134.279		147.067		ı	166.250			1
30	11	198.221	204.615			223.798	1	236.586		
40	255.769	262.163	268.557	274.951	281.346	287.740	294.134	300.528	306.923	313.317
50	319.711	326.105	332.499	338.894	345.288	351.682	358.076	364.470	370.865	377.259
60	383.653	390.047	396.442	402.836	409.230	415.624	422.018	428.413	434.807	441.201
70	447.595	453.990	460.384	466.778	473.172	479.566	485.961	492.355	498.749	505.143
80	511.538	517.932	524.326	530.720	537.114	543.509	549.903	556.297	562.691	569.085
90	575.480	581.874	588.268	594.662	601.057	607.451	613.845	620.239	626.633	633.028
Wh					Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am. Feet	Am Feet	Am Feet	Am Feet.	Am. Feet.	Am Feet	Am Feet.	Am Feet		Am. Feet
0	0.0	1					3836.5	4476.0	5115.4	l .
1000	6394.2	1		1	1	1	10230.8	[ı	ŀ
2000		13427.9		14706.7		15985.5		17264.4		
3000						22379.8				
4000						28774.0				
5000	31971.1	32610.5	33249.9	33889.4	34528.8	35168.2	35507.6	36447.0	37086.5	37725

TO CONVERT

METRES

INTO DIFFERENT MEASURES OF LENGTH.

1 LEGAL METRE = 443.296 FRENCH OR PARIS LINES.

V. CONVERSION OF METRES INTO TOISES AND DECIMALS.

1 Metre = 0.513074074 Toise.

Metres. Thousands.	Hundreds.										
	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.	
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.	
0	0.00	51.31	102.61	153.92	205.23	256.54	307.84	359.15	410.46	461.7	
000	513.07	564.38	615.69	667.00	718.30	769.61	820.92	872.23	923.53	974.8	
2000	1026.15	1077.46	1128.76	1180.07	1231.38	1282.69	1333.99	1385.30	1436.61	1487.9	
3000	1539.22	1590.53	1641.84	1693.14	1744.45	1795.76	1847.07	1898 37	1949.68	2000.9	
4000	2052.30	2103.60	2154.91	2206.22	2257.53	2308.83	2360.14	2411.45	2462.76	2514.0	
5000	2565.37	2616.68	2667.98	2719.29	2770.60	2821.91	2873.21	2924.52	2975.83	3027.1	
6000	3078.44	3129.75	3181.06	3232.37	3283.67	3334.98	3386.29	3437.60	3488.90	3540.2	
7000	3591.52	3642.83	3694.13	3745.44	3796.75	3848.06	3899.36	3950.67	4001.98	4053.28	
8000	4104.59	4155.90	4207.21	4258.51	4309.82	4361.13	4412.44	4463.74	4515.05	4566.30	
9000	4617.67	4668.97	4720.28	4771.59	4822.90	4874.20	4925.51	4976.82	5028.13	5079.43	
Metres.	Units.										
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	
0	0.000	0.513	1.026	1.539	2.052	2.565	3.078	3.592	4.105	4.618	
10	5.131	5.644	6.157	6.670	7.183	7.696	8.209	8.722	9.235	9.748	
20	10.261	10.775	11.288	11.801	12.314	12.827	13.340	13.853	14.366	14.879	
30	15.392	15.905	16.418	16.931	17.445	17.958	18.471	18.984	19.497	20.010	
46	20.523	21.036	21.549	22.062	22.575	23.088	23.601	24.114	24.628	25.141	
50	25.654	26.167	26.680	27.193	27.706	28.219	28.732	29.245	29.758	30.271	
60	30.784	31.298	31.811	32.324	32.837	33.350	33.863	34.376	34.889	35.402	
70	35.915	36.428	36.941	37.454	37.967	38.481	38.994	39.507	40.020	40.533	
80	41.046	41.559	42.072	42.585	43.098	43.611	44.124	44.637	45.151	45.664	
90	46.177	46.690	47.203	47.716	48.229	48.742	49.255	49.768	50.281	50.794	

 $1\ \mathrm{Metre} = 3.078444\ \mathrm{Paris}\ \mathrm{Feet}.$

Metres. Tens.	Metres. Units.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr. Feet.	Fr Feet.	Fr. Fee	
0	0.00	3.08	6.16	9.24	12.31	15.39	18.47	21.55	24.63	27.7	
10	30.78	33.86	36.94	40.02	43.10	46.18	49.26		55.41	58	
20	61.57	64.65	67.73		1	76.96	80.04		86.20	l .	
30	92.35	95.43	98.51	1	1	107.75	110.82	113.90	116.98	1	
40	123.14	126.22	129.29	132.37	135.45	138.53	141.61	144.69	147.77	150.9	
50	153.92	157.00	160.08	163.16	166.24	169.31	172.39	175.47	178.55	181.6	
60	184.71	187.79	190.86	193.94	197.02	200.10	203.18	206.26	209.33	212	
70	215.49	218.57	221.65	224.73	227.80	230.88	233.96	237.04	240.12	243.2	
80	246.28	249.35	252.43	255.51	258.59	261.67	264.75	267.82	270.90	273.9	
90	277.06	280.14	283.22	286.30	289.37	292.45	295.53	298.61	301.69	304.7	
100	307.84	310.92	314.00	317.08	320.16	323.24	326.32	329.39	332.47	335.5	
110	338.63	341.71	344.79	347.86	350.94	354.02	357.10	360.18	363.26	366.3	
120	369.41	372.49	375.57	378.65	381.73	384.81	387.88	390.96	394.04	397.	
130	400.20	403.28	406.35	409.43	412.51	415.59	418.67	421.75	424.83	427.9	
140	430.98	434.06	437.14	440.22	443.30	446.37	449.45	452.53	455.61	458.6	
150	461.77	464.85	467.92	471.00	474.08	477.16	480.24	483.32	486.39	489.	
160	492.55	495.63	498.71	501.79	504.86	507.94	511.02	514.10	517.18		
170	523.34	526.41	529.49	532.57	535.65	538.73	541.81	544.88	547.96	551.0	
180	554.12	557.20	560.28	563.36	566.43	569.51	572.59	575.67	578.75	581.8	
190	584.90	587.98	591.06	594.14	597.22	600.30	603.38	606.45	609.53	612.6	
200	615.69	618.77	621.85	624.92	628.00	631.08	631.16	637.24	640.32	643.3	
210	646.47	649.55	652.63	655.71	658.79	661.87	664.94	668.02	671.10	674.1	
220	677.26	680.34	683.41	686.49	689.57	692.65	695.73	698.81	701.89	704.9	
230	708.04	711.12	714.20	717.28	720.36	723.43	726.51	729.59	732.67	735.7	
240	738.83	741.90	744.98	748.06	751.14	754.22	757.30	760.38	763.45	766.	
250	769.61	772.69	775.77	778.85	781.92	785.00	*00 A0	701.16	*0.1.9.1	707 (
260	800.40	803.47	806.55	809.63	812.71	815.79	788.08 818.87	791.16 821.94	794.24 825.02	797.3 828.1	
270	831.18	834.26	837.34	840.42	843.49	846.57	849.65	852.73	855.81	858.8	
280	861.96	865.04	868.12	871.20	874.28	877.36	880.43	883.51	886.59	889.6	
290	892.75	895.83	898.91	901.98	905.06	908.14	911.22	914.30	917.38	920	
200	000 80	026.61	020 80	020 77	005.05	000 00	0.10.00	0.05.00	0.10 10	051.5	
300	923.53	926.61 957.40	929.69 960.47	932.77 963.55	935.85 966.63	938.93			948.16	951.2	
310 320	954.32 985.10	988.18					972.79 1003.57		978.95	982.0	
330	1		i 1		1028.20						
340	1046.67	1049.75	1052.83	1055.91	1028.20	1062.06	1065.14	1068.22	1071.30	1074.3	
350					1089.77						
360					1120.55						
370					1151.34						
380	1160 81	1172.50	1175 97	1179 01	1182.12	1185 90	1186 05	1101.97	1104-44	1100.	
390					1212.91						
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	

1 Metre = 3.078444 Paris Feet.

Metres. Tens.	Metres. Units.										
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	
		Fr. Feet.			Fr. Feet.						
400	[]				1243.69	1	l .	1			
410	11 1				1274.48	t .			1	ł	
420	11 :				1305.26			1		i	
430	11 1				1336.04				1348.36	ĺ	
440	1354.52	1357.59	1360.67	1363.75	1366.83	1369.91	1372.99	1376.06	1379.14	1382.	
450	1385.30	1388.38	1391.46	1394.54	1397.61	1400.69	1403.77	1406.85	1409.93	1413.	
460	1416.08	1419.16	1422.24	1425.32	1428.40	1431.48	1434.55	1437.63	1440.71	1443.	
470	1446.87	1449.95	1453.03	1456.10	1459.18	1462.26	1465.34	1468.42	1471.50	1474.	
480	1477.65	1480.73	1483.81	1486.89	1489.97	1493.05	1496.12	1499.20	1502.28	1505.	
490	1508.44	1511.52	1514.59	1517.67	1520.75	1523.83	1526.91	1529.99	1533.07	1536.	
500	1539.22	1542.30	1545.38	1548.46	1551.54	1554.61	1557.69	1560.77	1563.85	1566.	
510					1582.32						
520	1)-				1613.10						
530	11 1				1643.89						
540	11				1674.67				1686.99		
==0	1602 14	1606 22	1600 20	1709 99	1705.46	1700 54	1711 61	171 4 60	1717 77	1790	
550		1		1	1736.24						
560	[]				1767.03						
570 500					1797.81		· ·		1810.13		
580 590	11				1828.60		i		1840.91		
590	1310.23	1013.30	1022.44	1020.02	1020.00	1031.07	1394.19	1007.00	1040.31	1043.	
600	1847.07	1850.14	1853.22	1856.30	1859.38	1862.46	1865.54	1868.62	1871.69	1874.	
610	1877.85	1880.93	1884.01	1887.09	1890.16	1893.24	1896.32	1899.40	1902.48	1905.	
620	1908.64	1911.71	1914.79	1917.87	1920.95	1924.03	1927.11	1930.18	1933.26	1936.	
630	1939.42	1942.50	1945.58	1948.66	1951.73	1954.81	1957.89	1960.97	1964.05	1967.	
640	1970.20	1973.28	1976.36	1979.44	1982.52	1985.60	1988.67	1991.75	1994.83	1997.	
650	2000.99	2004.07	2007.15	2010.22	2013.30	2016.38	2019.46	2022.54	2025.62	2028.	
660	81 1			1	2044.09	i					
670	!				2074.87	,		ı		l	
680					2105.66					l	
690	11			1	2136.44					l	
700	2154 91	2157.99	2161.07	2164.15	2167.22	2170 20	2173.38	2176.46	2179.54	2182	
710					2198.01	9					
720					2228.79						
730			1	1	2259.58	1				í	
740					2290.36						
750	2308.83	2311.91	2314.99	2318.07	2321.15	2324.23	2327.30	2330.38	2333.46	2336.	
760	11		1	ł	2351.93		i		1	1	
770					2382.72						
780					2413.50						
790					2444.28						
					l	·					

1 Metre = 3.078444 Paris Feet.

Metres.					Metres.	Units.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
000	11	Fr. Feet.		1	Fr. Feet.		Fr. Feet.		Fr Feet.	
800	11			2471.99		1	2481.23			1
810	11			2502.77	1		2512.01	1		į.
820	II	2527.40		2533.56	1		2542.79	1	1	1
$830 \\ 840$	H	2558.19 2588.97		2564.34 2595.13	i	ı	2573.58 2604.36	l		1
850	2616.68	2619.76	2622.83	2625.91	2628.99	2632.07	2635,15	2638.23	2641.30	2644.3
860	11	1		2656.70	l		1	ł	i	1
870	14	2		2687.48	l.		1	(1
880	13	ı		2718.27	[2727.50	1		1
890	13	i		2749.05			1	1		t
900	2770.60	2773.68	2776.76	2779.83	2782.91	2 7 85.99	2789.07	2792.15	2 7 95.23	2798.
910	2801.38	2804.46	2807.54	2810.62	2813.70	2816.78	2819.85	2822.93	2826.01	2829.
920				2841.40						
930	2862.95	2866.03	2869.11	2872.19	2875.27	2878.35	2881.42	2884.50	2887.58	2890.
940	2893.74	2896.82	2899.89	2902.97	2906.05	2909.13	2912.21	2915.29	2918.36	2921.
950				2933.76						
960	2955.31	2958.38	2961.46	2964.54	2967.62	2970.70	2973.78	2976.86	2979.93	2983.
970				2995.33						
980				3026.11						
990	3047.66	3050.74	3053.82	3056.89	3059.97	3063.05	3066.13	3069.21	3072.29	3075.
Metres.	French F	eet. M	etres. F	rench Feet	t. Metr	es. Fre	nch Feet.	Metre	s. Fren	ich Feet
1000	3078.	44 5	000	15392.22	90	00 27	7706.00	13000	100	019.78
2000	6156.	+i	1	18470.67	- 11		0784.44	14000	1	098.22
3000	9235.	- 11		21549.11	11		3862.89	15000		176.67
4000	12313.	- 11		24627.56	ll l		6941.33	16000		255.11
				,	Decim	etres.				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Fr Feet.	Fr Feet.	Fr.Feet.	Fr.Feet.	Fr Feet.	Fr.Feet	Fr. Feet.	Fr. Feet.	Fr.Feet.	Fr Fee
0	0.0000	0.3078	0.6157	0.9235	1.2314	1.5392		2.1549	2.4628	
1	3.0784	3.3863	3.6941	4.0020	4.3098	4.6177	4.9255	5.2334	5.5412	1
2		6.4647				7.6961			8.6196	
3				10.1589						
4	12.3138	12.6216	12.9295	13.2373	13.5452	13.8530	14.1608	14.4687	14.7765	15.08
5	15.3922	15.7001	16.0079	16.3158	16.6236	16.9314	17.2393	17.5471	17.8550	18.16
6				19.3942						
7				22.4726						
8				25.5511						
					28.9374					

1 Metre = 3.28089917 English Feet.

					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
		Eng. Feet.			Eng. Feet.		Eng Feet.		_	
0	0.0	3.28	6.56	9.84	13.12	16.40	19.69	22.97	26.25	29.53
10	32.81	36.09	39.37	42.65	45.93	49.21	52.49	55.78	59.06	62.3
20	65.62	68 90	72.18	75.46	78.74	82.02	85.30	88.58	91.87	95.15
30	98.43	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	127.96
40	131.24	134.52	137.80	141.08	144.36	147.64	150.92	154.20	157.48	160.76
50	164.01	167.33	170.61	173.89	177.17	180.45	183.73	187.01	190.29	193.57
60	196.85	200.13	203.42	206.70	209.98	213.26	216.54	219.82	223.10	226.38
70	229.66	232.94	236.22	239.51	242.79	246.07	249.35	252.63	255.91	259.19
$_{80}$	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.00
90	295.28	298.56	301.84	305.12	308.40	311.69	314.97	318.25	321.53	324.8
100	328.09	331.37	334.65	337.93	341.21	344.49	347.78	351.06	354.34	357.65
110	360.90	364.18	367.46	370.74	374.02	377.30	380.58	383.87	387.15	390.4
120	393.71	396.99	400.27	403.55	406.83	410.11	413.39	416.67	419.96	423.2
130	426.52	429.80	433.08	436.36	439.64	442.92	446.20	449.48	452.78	456.0
140	459.33	462.61	465.89	469.17	472.45	475.73	479.01	482.29	485.57	488.8
	102.10	107.10	400 50	F01.00	-0- 0C	500 54	E11 00	717 10	710.00	501.0
150	492.13	495.42	498.70	501.98	505.26	508.54	511.82	515.10	518.38	521.6
160	524.94	528.22	531.51	534.79 567.60	538.07	541.35 574.16	544.63 577.44	547.91 580.72	551.19	554.4
170	557.75	561.03	564.31	600.40	570.88 603.69	606.97	610.25	613.53	584.00	587.28 620.09
180 190	590.56 623.37	593.84 626.65	597.12 629.93	633.21	636.49	639.78	643.06	646.34	616.81 649.62	652.90
190	020.07	020.05	025.55	055.21	050.45	000.10	045.00	040.54	043.02	002.50
200	656.18	659.46	662.74	666.02	669.30	672.58	675.87	679.15	682.43	685.7
210	688.99	692.27	695.55	698.83	702.11	705.39	708.67	711.96	715.24	718.55
220	721.80	725.08	728.36	731.64	734.92	738.20	741.48	744.76	748.05	751.33
230	754.61	757.89	761.17	764.45	767.73	771.01	774.29	777.57	7 80.85	784.13
240	787.42	790.70	793.98	797.26	800.54	803.82	807.10	810.38	813.66	816.9
250	820.22	823.51	826.79	830.07	833.35	836.63	839.91	843.19	846.47	849.7
260	853.03	856.31	859.60	862.88	866.16	869.44	872.72	876.00	879.28	882.5
270	885.84	889.12	892.40	895.69	898.97	902.25	905.53	908.81	912.09	915.33
280	918.65	921.93	925.21	928.49	931.78	935.06	938.34	941.62	944.90	948.1
290	951.46	954.74	958.02	961.30	964.58	967.87	971.15	974.43	977.71	980.9
900	001.97	007 75	990.83	994.11	907 30	1000.67	1002.06	1007 21	1010.52	1013.S
300	984.27	987.55		1026.92		1033.48	l	1040.05	1043.33	1046.6
310	1017.08 1049.89	1020.36 1053.17	1	1020.92		1066.29	l	1072.85		l
320 330	1039.59		1089.26			ı	1102.38			į.
340	1115.51						1135.19			l
					ĺ					
350	1148.31	1	1	1158.16		1164.72	1		1174.56	l
360	1181.12	1	1187.69	1			1200.81	1204.09	1207.37	1210.6
370	1213.93	i .	1220.49	1223.78	ł.	1230.34	1	1236.90	1240.18	1243.4
380	1246.74	1	1253.30	1		1263.15	1266.43 1299.24	1269.71 1302.52	1272.99 1305.80	1276.2 1309.0
390	1279.55	1282.83	1286.11	1289.39	1292.67	1295.96	1299.24	1502.52	1505.50	
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

D

400 to 799.

Metres.					Metres.	(Units.)				
Mettes.	0.	1.	2.	3.	4.	5.	6.	7.	s.	9.
400	Eng.Feet. 1312.36	Eng.Feet. 1315.64	Eng. Feet. 1318.92	Eng.Feet. 1322.20			Eng. Feet.		Eng. Feet.	
	1					1328.76	ì	1	i	l.
410	1345.17	1348.45	1351.73	1355.01		1361.57	1	1	1	
420	1377.98	1381.26	1384.54	1387.82		1394.38	1397.66	1400.94	1404.22	
$\frac{430}{440}$	1410.79 1443.60	1414.07 1446.88	1417.35 1450.16	1420.63 1453.44		1427.19 1460.00	1430.47 1463.28	$1433.75 \\ 1466.56$	1437.03 1469.84	1440.8 1473.1
4-10	1445.00	1440.00	1490.10	1499:44	1400.72	1400.00	1405.25	1400.00	1409.54	1470.1
450	1476.40	1479.69	1482.97	1486.25	1489.53	1492.81	1496.09	i	1502.65	1505.9
460	1509.21	1512.49	1515.78	1519.06	1522.34	1525.62	1528.90	1532.18	1535.46	1535.7
470	1542.02	1545.30	1548.58	1551.87	1555.15	1558.43	1561.71	1564.99	1568.27	1571.5
480	1574.83	1578.11	1581.39	1584.67	1587.96	1591.23	1594.52	1597.80	1601.08	1604.3
490	1607.64	1610.92	1614.20	1617.48	1620.76	1624.05	1627.33	1630.61	1633.89	1637.1
500	1640.45	1643.73	1647.01	1650.29	1653.57	1656.85	1660.13	1663.42	1666.70	1669.9
510	1673.26	1676.54	1679.82	1683.10		1689.66	1692.94		1699.51	1702.7
520	1706.07	1709.35	1712.63	1715.91	i	1722.47	1725.75	1729.03	1732.31	1735.6
530	1738.88	1742.16	1745.44		1	1755.28	1758.56	1	1765.12	1768.4
540	1771.69	1774.97	1778.25	1781.53	1784.81	1788.09	1791.37	1794.65	1797.93	1801.2
550	1804.49	1807.78	1811 06	1814.34	1917 60	1820.00	1824.18	1827.46	1830.74	18911
560	1837.30	1840.58	1843.87		1850.43	l l	1856.99	1860.27	1863.55	1866.8
570	1870.11	1873.39	1876.67	1879.96	1883.24			1893.08	1896.36	
580	1902.92	1906 20	1909.48	1912.76		1919.33	1922.61	1925.89	1929.17	1932.4
590	1935.73	1939.01	1942.29	1945.57			1955.42	1958.70	1961.98	1965.2
-00	- 0 00 7 .	-0-4-03							1004 50	*****
600	11	1971.82		1978.38					1994.79	1998.0
610	2001.35	}	2007.91				1	2024.31		2030.8
620	1	2037.44	2040.72	2044.00	2047.28		2053.84			2063.6
630	2066.97	2070.25	2073.53	2076.81		2083.37				2096.4
640	2099.78	2103.06	2106.34	2109.62	2112.90	2116.18	2119.46	2122.74	2126.02	2129.3
650	2132.58	2135.87	2139.15	2142.43	2145.71	2148.99	2152.27	2155.55	2158.83	2162.1
660	2165.39	2168.67	2171.96	2175.24	2178.52	2181.80	2185.08	2188.36	2191.64	2194.9
670	2198.20	2201.48	2204.76	2208.05		1			2224.45	
650	2231.01	2234.29	2237.57	2240.85			2250.70			2260.5
690	2263.82	2267.10	2270.38	2273.66	2276.94	2280.22	2283.51	2286.79	2290.07	2293.3
700	2296.63	2299.91	2303.19	2306.47	2309.75	2313.03	2316.31	2319.60	2322.88	2326.1
710	2329.44		2336.00	2339.28				2352.40		2358.9
720	2362.25	2365.53	2368.81	2372.09			2381.93			2391.7
730	2395.06	2398.34	2401.62	2404.90	2108.18	2411.46	2414.74	2418.02	2421.30	2424.5
740				2437.71						2457.3
750	2460.67	2463.96	2467.24	2470.52	2473.80	2477.08	2480.36	2483.64	2486.92	2490.2
760	11	2496.76		2503.33						
770	11	2529.57		2536.14				1		
780	2559.10	2562.38		2568.94	1	2575.51	l	2582.07		
790		2595.19						2614.88		
•										

800 to 1199.

					Metres.	(Units.)				
Metros.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. Feet.				1 ~	Eng.Feet.				
800	2624.72	2628.00	2631.28	2634.56	i	2641.12	2644.40		1	2654.2
810	2657.53	2660.81	2664.09	2667.37	1	2673.93	2677.21	2680.49	i	2687.0
820	2690.34	2693.62	2696.90	2700.18		2706.74			1	1
830	2723.15	2726.43	2729.71	2732.99	i	2739.55	2742.83	2746.11	2749.39	2752.6
840	2755.96	2759.24	2762.52	2765.80	2769.08	2772.36	2775.64	2778.92	2782.20	2785.4
850	2788.76	2792.05	2795.33	2798.61	2801.89	2805.17	2808.45	2811.73	2815.01	2818.
860	2821.57	$2\overline{8}24.85$	2828.14	2831.42	2834.70	2837.98	2841.26	2844.54	2847.82	2851.
870	2854.38	2857.66	2860.94	2864.22	2867.51	2870.79	2874.07	2877.55	2880.63	2883.9
880	2887.19	2890.47	2893.75	2897.03	2900.31	2903.60	2906.88	2910.16	2913.44	2916.7
890	2920.00	2923.28	2926.56	2929.84	2933.12	2936.40	2939.6 9	2942.97	2946.25	2949.
900	2952.81	2956.09	2959.37	2962.65	2965.93	2969.21	2972.49	2975.78	2979.06	2982.3
910	2985.62	2988.90	2992.18	2995.46	1	3002.02	3005.30	3008.58	3011.87	3015.
920	3018.43	3021.71	3024.99	3028.27		3034.83	3038.11	3041.39	3044.67	3047.9
930	3051.24	3054.52	3057.80	3061.08	1	3067.64	3070.92	1	3077.43	3080.
940	3084.05	3087.33	3090.61	3093.89		3100.45	3103.73	3107.01	3110.29	3113.
950	3116.85	3120.14	3123.42	3126.70	2129 98	3133.26	3136.54	3139.82	3143.10	3146.
960	3149.66	3152.94	3156.22	3159.51		3166.07	3169.35	1	3175.91	3179.
970		3185.75	3189.03			3198.S8	3202.16	3205.44	3208.72	3212.0
	3182.47						3234.97	3238.25		3244.8
980	3215.28		3221.84	3225.12		3231.69		3271.06	3241.53	
990	3248.09	3251.37	3254.65	3 257. 93	3201.21	3264.49	3267.78	3271.00	3274.34	3277.0
1000	3280.90	3284.18	3287.46	3290.74	3291.02	3297.30	3300.58	3303.87	3307.15	3310.
1010	3313.71	3316.99	3320.27	3323.55	3326.83	3330.11	3333.39	3336.67	3339.96	3343.2
1020	3346.52	3349.80	3353.08	3356.36	3359.64	3362.92	3366.20	3369.48	3372.76	3376.0
1030	3379.33	3382.61	33S5.S9	3389.17	3392.45	3395.73	3399.01	3402.29	3405.57	3408.8
1040	1	3415.42			3425.26		3431.82	3435.10	3438.38	3441.6
1050	3444.94	344S.22	3451.51	3454.79	3458.07	3461.35	3464.63	3467.91	3471.19	3474
1060		3481.03	3484.31	3487.60	3490.88		3497.44	3500.72	3504.00	3507.2
1070		3513.84		3520.40	3523.69		3530.25	3533.53	3536.81	3540.0
1080	3543.37			3553.21	3556.49		,		3569.62	3572.9
1090	3576.18	3579.46	3582.74		3589.30		1	1	,	3605.7
1100	3608.99	3612.27	3615.55	3618.83	3622.11	3695 30	3628.67	3631.96	3635.24	3638.5
1110	1 1	3645.08	3648.36		3654.92					3671.3
1120	3674.61	3677.89		3684.45	3687.73		j		3700.85	3704.1
1130	3707.42	3710.70			3720.54		3727.10		3733.66	3736.9
1140	3740.22	3743.51	3746.79		3753.35		1	1	1	3769.7
1150	2772 00	9776 91	9770.60	ეუდი იი	9796 10	3789.44	2702 70	2706 00	2700 90	ვვტი =
1150	1						1	}		3802.5
1160	1	3809.12			3818.97		3825.53		1	3835.3
1170		3841.93				1	3858.34		i	3868.1
1180 1190	N I	3874.74 3907.55	3878.02 3910.83		3884.58 3917.39		3891.15 3923.96	3894.43 3927.24		3900.9 3933.8
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1200 to 1599.

					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
1200	Eng.Feet.	Eng. Feet.		Eng. Feet.						1
1200	1			3946.92	1	1	3956.76	1	3963.33	
1210	1	3973.17	3976.45	1	1	3986.29		1	3996.14	1
1220	4002.70	4005.98	4009.26	4012.54	l	4019.10	4022.38	4025.66	4028.94	4032.2
1230 1240	4035.51	4038.79 4071.60	4042.07 4074.88	4045.35 4078.16	1	4051.91 4084.72	4055.19 4088.00	4058.47 4091.28	4061.75 4094.56	4097.8
1250	4101.12	4104.40	4107.69	4110.97	111 (95	4117.53	4120.81	4124.09	4127.37	4130.6
1260	4133.93	4137.21	4140.49	4143.78	1	4150.34	4153.62	4156.90	4160.18	4163.4
1270	4166.74	4170.02					4186.43	4189.71	4192.99	
1280	4199.55	4202.83	4173.30 4206.11	4209.39		4183.15 4215.96	4219.24	4139.71 4222.52	4225.80	4229.0
1290	4232.36		4238.92	4242.20		4248.76	4219.24	4255.33	4258.61	
1300	4265.17	4268.45	4271.73	4275.01	1978 90	4281.57	4284.85	1988 1 (4291.42	129.17
1310	4297.98	4301.26	4304.54			4314.38	4317.66	4320.94	4324.23	4327.5
1320	4330.79	4334.07	4337.35	4340.63		4347.19	4350.47	4353.75	4357.03	4360.3
1330	4363.60	4366.88	4370.16	4373.44	4376.72		4383.28	4386.56		4393.1
1340	4396.40	4399.69	4402.97	4406.25	4409.53		4416.09	4419.37	1	4425.9
1350	4429.21	4432.49	4435.78	4439.06	4442.34	1115.60	4448.90	1159 18	4455.46	1 (58.7
1360	4462.02	4465.30	4468.58	4471.87	4475.15		4481.71	4484.99	4488.27	4491.5
1370	4494.83	4498.11	4501.39	4504.67			4514.52	- 1	ì	4524.3
1380	4527.64	4530.92	4534.20	4537.48	4540.76		4547.33	4550.61	J	4557.1
1390	4560.45	4563.73	4567.01	4570.29	4573.57	1	4580.14			4589.9
1400	4593.26	4596.54	4599.82	4603.10	4606.38	4609.66	4612.94	4616,23	4619.51	4622.7
1410	4626.07	4629.35	4632.63	4635.91	4639.19			,		4655.6
1420	4658.88	4662.16	4665.44	4668.72	4672.00			1		4688.4
1430	4691.69	4694.97	4698.25	4701.53	4704.81		4711.37			4721.2
1440	4724.49	4727.78	4731.06	4734.34	4737.62		4744.18		-	4754.0
1450	4757.30	4760.58	4763.87	4767.15	4770.43	4773.71	4776.99	4780.27	4783.55	4786.8
1460	4790.11	4793.39	4796.67	4799.96	4803.24			1	- 1	1819.6
1470	4822.92	4826.20	4829.48		4836.05			- 1		4852.4
1480	4855.73	4859.01	4862.29	4865.57	4868.85		1 1	4878.70	4881.98	4885.2
1490	4888.54	4891.82	4895.10	4898.38	4901.66	4904.94	4908.23	4911.51	4914.79	4918.0
1500	4921.35	4924.63	4927.91	4931.19	4934.47	4937.75	4941.03	4944.31	4947.60	4950.8
1510	4954.16	4957.44	4960.72	4964.00	4967.28	4970.56	4973.84	4977.12	4980.40	4983.6
1520	4986.97	4990.25	4993.53	4996.81	5000.09	5003.37	5006.65	5009.93	5013.21	5016.4
1530	5019.78	5023.06	5026.34	5029.62	5032.90	5036.18	5039.46	5042.71	5046.02	5049.3
1540	5052.58	5055.87		1				5075.55		
1550	5085.39	5088.67	5091.96	5095.24	5098.52	5101.80	5105.08	5108.36	5111.64	5114.9
1560	5118.20	5121.48	5121.76	5128.05	5131.33	5134.61	5137.89	5141.17	5144.45	5147.7
1570	5151.01	5154.29	5157.57	5160.85	5161.14	5167.42	5170.70	5173.98	5177.26	5180.5
1580	5183.82	5187.10	5190.38	5193.66	5196.94	5200.23	5203.51	5206.79	5210.07	5213.3
1590	5216.63	5219.91	5223.19	5226.47	5229.75	5233.03	5236.32	5239.60	5242.88	5246.1
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1600 to 2000.

					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. Feet.		Eng. Feet.			Eng.Feet.				
1600	5249.44	5252.72	1	5259.28		5265.84	1	1	i	
1610	5282.25	5285.53	5288.81	5292.09	1	5298.65	1	1	1	
1620	5315.06	5318.34	5321.62	5324.90	Í	5331.46		5338.02	5341.30	1
1630	5347.87	5351.15	5354.43	5357.71		5364.27	1	5370.53	5374.11	1
1640	5380.67	5383.96	5387.24	5390.52	5393.80 	5397.08	5400.36	5403.64	5406.92	5410.20
1650	5413.48	5416.76	5420.05	5423.33	5426.61	5429.89	5433.17	5436.45	5439.73	5443.01
1660	5446.29	5449.57	5452.85	5456.14	5459.42	5462.70	5465.98	5469.26	5472.54	5475.82
1670	5479.10	5482.38	5485.66	5488.94	5492.23	5495.51	5498.79	5502.07	5505.35	5508.63
1680	5511.91	5515.19	5518.47	5521.75	5525.03	5528.32	5531.60	5534.88	5538.16	5541.44
1690	5544.72	5548.00	5551.28	5554.56	5557.84	5561.12	5564.40	5567.69	5570.97	5574.25
1700	5577.53	5580.81	5584.09	5587.37	5590 65	5593.93	5597.21	5600.49	5603.78	5607.06
1710	5610.34	5613.62	5616.90	1		5626.74	5630.02	5633.30	1	5639.87
1720	5643.15	5646.43	5649.71	5652.99		5659.55	5662.83	5666.11	5669.39	5672.67
1730	5675.96	5679.24	5682.52	5685.80		5692.36	5695.64	5698.92	5702.20	5705.48
1740	5708.76	5712.05	5715.33	5718.61		5725.17	5728.45	5731.73	5735.01	5738.29
1750	5741.57	5744.85	5748.14	1	5754.70	1	5761.26	5764.54		5771.10
1760	5774.38	5777.66	5780.94	5784.23		5790.79	5794.07	5797.35	5800.63	5803.91
1770	5807.19	5810.47	5813.75	5817.03		5823.60	5826.88	5830.16		5836.72
1780	1 1	5843.28	1	5849.84		5856.40	5859.69	5862.97	5866.25	5869.53
1790	5872.81	5876.09	5879.37	5882.65	5885.93	5889.21	5892.49	5895.78	5899.06	5902.34
1800	5905.62	5908.90	5912.18	5915.46	5918.74	5922.02	5925.30	5928.58	5931.87	5935.15
1810	5938.43	5941.71	5944.99	5948.27	5951.55	5954.83	5958.11	5961.39	5964.67	5967.96
1820	5971.24	5974.52	5977.80	5981.08	5984.36	5987.64	5990.92	5994.20	5997.48	6000.76
1830	6004.05	6007.33	6010.61	6013.89	6017.17	6020.45	6023.73	6027.01	6030.29	6033.57
1840	6036.85	6040.14	6043.42	6046.70	6049.98	6053.26	6056.54	6059.82	6063.10	6066.38
1850	6069.66	6072.94	6076.23	6079.51	6082.79	6086.07	6089.35	6092.63	6095.91	6099.19
1860	6102.47	6105.75	6109.03	1	6115.60		6122.16	6125.44	6128.72	6132.00
1870	6135.28	6138.56		6145.12		6151.69	6154.97	6158.25	6161.53	6164.81
1880	6168.09	6171.37	6174.65	6177.93	6181.21	6184.49	6187.78	6191.06	6194.34	6197.62
1890	6200.90	6201.18	6207.46	6210.74	6214.02	6217.30	6220.58	6223.87	6227.15	6230.43
1900	6233.71	6236.99	6240.27	6243.55	6246.83	6250.11	6253.39	6256.67	6259.96	6263.24
1910	6266.52		i		6279.64		6286.20		6292.76	6296.05
1920	6299.33	6302.61		1	6312.45		6329.01		6325.57	6328.85
1930	6332.14				6345.26		6351.82	i	6358.38	6361.66
1940	6364.94	1	1		6378.07		6384.63	!	6391.19	6394.47
1950	6397.75	6401.03	6101 39	6407 60	6410.88	81 1 1 1 2 3	6417.44	6420.72	6454.00	6427.28
1960	6430.56		6437.12			6446.97	6450.25	1	6456.81	6460.09
1970	6463.37		6469.93		6476.49		6483.06		6489.62	6492.90
1980	6496.18		6502.74		6509.30		6515.87		6522.43	6525.71
1990	6528.99	6532.27				6545.39	6548.67		6555.24	6558.52
2000	6561.80	6565.08	6568.36		6574.92		6581.48		6588.05	6591.33
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
			~ .	9.	***	٠.	· ·	••		

					Metres.	(Units)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
		Eng.Feet.					0	Eng.Feet	Eng.Feet	
2000	6561.80	6565.08	6568.36	6571.64	6574.92	6578.20	6581.48		6588.05	6591.3
2010	6594.61	6597.89		6604.45		6611.01	6614.29		6620.85	6624.1
2020	6627.42	6630.70	6633.98	6637.26	6640.54	6643.82	6647.10	6650.38	6653.66	6656.9
2030	6660.23	6663.51	6666.79	6670.07	6673.35	6676.63	6679.91	6683.19	6686.47	6689.7
2040	6693.03	6696.32	6699.60	6702.88	6706.16	6709.44	6712.72	6716.00	6719.28	6722.5
2050	6725.84	6729.12	6732.41	6735.69	6738.97	6742.25	6745.53	6748.81	6752.09	6755.3
2060	6758.65	6761.93	6765.21	6768.49	6771.78	6775.06	6778.34	6781.62	6784.90	6788.1
2070	6791.46	6794.74		6801.30	1 i	6807.87	6811.15	6814.43	6817.71	6820.9
2080	6524.27	6827.55		6834.11	1	6840.67	6843.96	6847.24	6850.52	6853.8
2090	6857.08	6860.36		6866.92		6873.48	6876.76		6883.33	1
2100	6889.89	6893.17	6906 15	6899. 7 3	6002 01	6906.29	6909.57	C019 05	6916.14	6919.4
	il I	6925.98		6932.54				1	6948.94	6952.2
2110	6922.70	6958.79				6939.10	6942.38	6945.66		6985.0
2120	6955.51				6968.63	6971.91	6975.19	6978.47	6981.75	
2130 2140	6988.32 7021.12	6991.60 7024.41		7030.97	7001.44	7004.72 7037.53	7008.00 7040.81	7011.28	7014.56 7047.37	7017.8
2150	7053.93	7057.21	7060.49	7063.78	7067.06	7070.34	7073.62	7076.90	7080.18	7083.4
2160	7086.74	7090.02	7093.30	7096.58	7099.87	7103.15	7106.43	7109.71	7112.99	7116.2
2170	7119.55	7122.83	7125.11	7129.39	7132.67	7135.96	7139.24	7142.52	7145.80	7149.0
2180	7152.36	7155.64	7158.92	7162.20	7165.48	7168.76	7172.05	7175.33	7178.61	7181.8
2190	7185.17	7188.45	7191.73	7195.01	7198.29	7201.57	7204.85	7208.14	7211.42	7214.7
2200	7217.98	7221.26	7224.54	7227.82	7231.10	7234.38	7237.66	7240.94	7244.23	7247.5
2210	7250.79	7254.07	7257.35	7260.63	7263.91	7267.19	7270.47	7273.75	7277.03	7280.3
2220	7283.60	7286.88	7290.16	7293.44	7296.72	7300.00	7303.28	7306.56	7309.84	7313.1
2230	7316.41	7319.69	7322.97		7329.53	7332.81	7336.09	7339.37	1	7345.9
2240	7349.21	7352.49	7355.78		7362.34	7365.62	7368.90	7372.18	i	7378.7
2250	7382.02	7385.30	7388.58	7201 87	7395.15	7398.43	7401.71	7101.00	7408.27	7411.5
2260	7414.83	7418.11	7421.39	7424.67		7431.24	7434.52	7437.S0	7441.08	7444.3
2270	7447.64	7450.92	7454.20	1	7460.76	7464.05	7467.33	7470.61	7473.89	7477.1
2280	7480.45	7483.73	7487.01	7490.29	i	7496.85	7500.14	7503.42	7506.70	1
$\frac{2280}{2290}$	7513.26	7516.54	7519.82		7526.38	7529.66	7532.94	1	7539.51	7542.7
2222										
2300	7516.07	7549.35	7552.64	!	7559.19	7562.47	7565.75		7572.32	7575.6
2310	7578.88	7582.16	7585.44	7588.72		7595.28	7598.56	7601.84	7605.12	7608.4
2320	7611.69	7614.97	7618.25			7628.09	7631.37	7634.65		7641.2
2330							7664.18			
2340	7677.30	7680.58	7683.87	7687.15	7690.43	7693.71	7696.99	7700.27	7703.55	7706.8
2350	7710.11	7713.39	7716.67	7719.96	7723.24	7726.52	7729.80	7733.08	7736.36	7739.6
2360	7742.92	7746.20	7749.48	7752.76	7756.05	7759.33	7762.61	7765.89	7769.17	7772.4
2370	7775.73	7779.01	7782.29	7785.57	7788.85	7792.14	7795.42	7798.70	7801.98	7805.2
2380	7808.54		7815.10		1		1		7834.79	l .
2390	7841.35	7844.63	7847.91	7851.19	7854.47	785 7. 75	7861.03	7864.32	7867.60	7870.8
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

2400 to 2799.

VIetres.					Metres.	(Units)				
vietres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
						Eng.Feet.				
2400	7874.16	7877.44		J	7887.28	7890.56	7893.84	7897.12	7900.41	7903.6
2410	7906.97	7910.25	7913.53	7916.81	7920.09	7923.37	7926.65	7929.93	7933.21	7936.5
2420	7939.78	7943.06	7916.34	7949.62	7952.90	7956.18	7959.46	7962.74	7966.02	7969.
2430	7972.59	7975.87	7979.15	7982.43	7985.71	7988.99	7992.27	7995.55	7998.83	8002.
2440	8005.39	8008.67	8011.96	8015.24	8018.52	8021.80	8025.08	8028.36	8031.64	8034.
2450	8038.20	8041.48	8044.76	8048.05	8051.33	8054.61	8057.89	8061.17	8061.45	8067.
2460	8071.01	8074.29	8077.57	8080.85	8084.14	8087.42	8090.70	8093.98	8097.26	8100.
2470	8103.82	8107.10	8110.38	8113.66	8116.94	8120.22	8123.51	8126.79	8130.07	8133.
2480	8136.63	8139.91		8146.47	1		8156.32		\$162.88	8166.
2490	8169.44	8172.72		1	8182.56		8189.12	ĺ	8195.69	8198.
2500	8202.25	8205.53	8208.81	8212.09	S215.37	8218 65	8221.93	8225.21	8228.50	8231.
2510	8235.06	8238.34		4	8248.18		8254.74		8261.30	1
2520	8267.87	8271.15		8277.71		8284.27	8287.55		8294.11	8297.
2530	8300.67	8303.96		8310.52	8313.80		8320.36		8326.92	t
2540	8333.48	8336.76		8343.33	8346.61	8349.89	8353.17		8359.73	8363.
2040	0999.40	0330.70	0040.00	2949.99	3940.01	0949.09	0000.17	0990:49	0000.10	2303.
2550	8366.29	8369.37	8372.85	8376.14	8379.42	8382.70	8385.98	8389.26	8392.54	8395.
2560	8399.10	8402.38	8405.66	8408.94	8412.23	8415.51	8418.79	8422.07	8425.35	8428.
2570	8431.91	8435.19	8438.47	8441.75	8445.03	8448.32	8451.60		8458.16	8461.
2580	8464.72	\$468.00		8474.56	8477.84	1	8484.41		8490.97	8494.
2590	8497.53	8500.81	8504.09	8507.37	8510.65	Į.	8517.21	1	8523.78	8527.
2600	8530.34	8533.62	8536.90	8540.18	8543.46	8546.74	8550.02	8553.30	8556.58	8559.
2610	8563.15	8566.43		l .	8576.27	8579.55	l		8589.39	ł
2620	8595.96	8599.24		8605.80	8609.08	8612.36	1	ĺ	8622.20	8625.
2630	8628.76	8632.05		8638.61	8641.89	8645.17			8655.01	8658.
2640	8661.57	8664.85		Í	8674.70	8677.98	8681.26	1	\$687.82	8691.
2010	0001.01	0001100	0000111	0011.42	0014.10	0011.50	0001.20	0004.04	0001102	0031.
2650	8694.38	8697.66	8700.94	8704.23	8707.51	8710.79	8714.07	8717.35	8720.63	8723.
2660	8727.19	8730.47	8733.75	8737.03	8740.32	8743.60	8746.88	8750.16	8753.44	8756.
2670	8760.00	8763.28	8766.56	8769.84	8773.12	8776.41	8779.69	8782.97	8786.25	8789.
2680	8792.81	8796.09	8799.37	8802.65	8805.93	8809.21	8812.50	8815.78	8819.06	8822.
2690	8825.62	8828.90	8832.18	8835.46	8838.74	8842.02	8845.30	8848.59	8851.87	8855.
2700	8858.43	8861.71	8864.99	8868.27	8871.55	8874.83	8878.11	8881.39	8884.67	8887.
2710	8891.24	8894.52			1	8907.64	1		8917.48	8920.
2720	8926.05	8927.33	8930.61			8940.45	8943.73		8950.29	8953.
2730	8956.85	8960.14				8973.26	1 1		8983.10	8986.
2740	\$989.66	8992.94					9009.35	9012.63		
2750	9022.47	9025.75	9029.03	9035 35	9035 60	9038 88	9042.16	9045.44	9048.72	9052.
2760	9055.28	1		9065.12		9035.69	9074.97	9078.25		9084.
2770	9088.09	9091.37)				9117.
2780	9120.90	- 1		9097.93	1	9104.50	9107.78	9111.06		9150.
2790	9153.71	9124.18 9156.99)	9130.74 9163.55		9137.30 9170.11	9140.59 9173.39	9143.S7 9176.68	1	9183.
	0.	1.	2.	3.	4.	5.	6,	7.	9.	9.

2800 to 3000.

					Metres.	(Units.)				
Metres.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	-									
2800		Eng.Feet. 9189.80								
2810	11	9222.61			ľ	1		1	1	
2820	il	9255.42	1		J		1	l	1	
2830		9288.23								
2840	11	9321.03	1							
2040	0011110	0021.00	0024.02	3321.00	3000.00	3554.10	2007.44	3540.12	3344.00	2041.20
2850	9350.56	9353.84	9357.12	9360.41	9363.69	9366.97	9370.25	9373.53	9376.81	9380.09
2860	II.	9386.65		1	j .					
2870	III.	9419.46	1				1			
2880	13	9452.27								
2890	9481.80	9485.08	9488.36	9491.64	9494.92	9498.20	9501.48	9504.76	9508.05	9511.33
2900	9514.61	9517.89	9521.17	9524.45	9527.73	9531.01	9534.29	9537.57	9540.85	9544.14
2910	9547.42	9550.70	9553.98	9557.26	9560.54	9563.82	9567.10	9570.38	9573.66	9576.94
2920	9580.23	9583.51	9586.79	9590.07	9593.35	9596.63	9599.91	9603.19	9606.47	9609.75
2 930	9613.03	9616.32	9619.60	9622.88	9626.16	9629.44	9632.72	9636.00	9639.28	9642.56
2940	9645.84	9649.12	9652.41	9655.69	9658.97	9662.25	9665.53	9668.81	9672.09	9675.37
								·		
2950	9678.62	9681.93	9685.21	9688.50	9691.78	9695.06	9698.34	9701.62	9704.90	9708.18
2960	9711.46	9714.74	9718.02	9721.30	9724.59	9727.87	9731.15	9734.43	9737.71	9740.99
2970	11	9747.55		1 1			1		1 1	
2980	ł1 I	9780.36					1 1			
2990	1).	9813.17	1	1						
3000	9842.70	9845.98	9849.26	9852.54	9855.82	9859.10	9862.38	9865.66	9868.94	9872.23

Proportional Parts.

Metres.					Decin	netres.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng.Feet.	Eng.Feet.	Eng Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet.	Eng.Feet	Eng.Feet	Eng.Feet.	Eng Feet.
0	0.0000	0.3281	0.6562	0.9843	1.3124	1.6404	1.9685	2.2966	2.6247	2.9528
1	3.2809	3.6090	3.9371	4.2652	4.5933	4.9213	5.2494	5.5775	5.9056	6.2337
2	6.5618	6.8899	7.2180	7.5461	7.8742	8.2022	8.5303	8.8584	9.1865	9.5146
3	9.8427	10.1708	10.4989	10.8270	11.1551	11.4831	11.8112	12.1393	12.4674	12.7955
4	13.1236	13.4517	13.7798	14.1079	14.4360	14.7640	15.0921	15.4202	15.7483	16.0764
5	16.4045	16.7326	17.0607	17.3888	17.7169	18.0449	18.3730	18.7011	19.0292	19.3573
6	19.6854	20.0135	20.3416	20.6697	20.9978	21.3258	21.6539	21.9820	22.3101	22.6382
7	22.9663	23.2944	23.6225	23.9506	24.2787	24.6067	24.9348	25.2629	25.5910	25.9191
8	26.2472	26.5753	26.9034	27.2315	27.5596	27.8876	28.2157	28.5438	28.8719	29.2000
9	29.5281	29.8562	30.1843	30.5124	30.8405	31.1685	31.4966	31.8247	31.1528	32.4809
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.

1 Metre = 3.28070878 American Feet.

Metres.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am Feet	Am Feet	Am Feet	Am Feet	Am Feet	Am.Feet	Am, Feet	Am. Feet	Am.Feet	Am Feet
0	0.0	328.I	656.1	984.2	1312.3	1640.4	1968.4	2296.5	2624.6	2952.6
1000	3280.7	3608.8	3936.9	4264.9	4593.0	4921.1	5249.1	5577.2	5905.3	6233.3
2000	6561.4	6889.5	7217.6	7545.6	7873.7	8201.8	8529.8	8857.9	9186.0	9514.1
3000	9842.1	10170.2	10498.3	10826.3	11154.4	11482.5	11810.6	12138.6	12466.7	12794.8
4000	13122.8	13450.9	13779.0	14107.0	14435.1	14763.2	15091.3	15419.3	15747.4	16075.5
5000	16403.5	16731.6	17059.7	17387.8	17715.S	18043.9	18372.0	18700.0	19028.1	19356.2
6000	19684.3	20012.3	20340.4	20668.5	20996.5	21324.6	21652.7	21980.7	22308.8	22636.9
7000	22965.0	23293.0	23621.1	23949.2	24277.2	24605.3	24933.4	25261.5	25589.5	25917.6
8000	26245.7	26573.7	26901.8	27229.9	27558.0	27886.0	28214.1	28542.2	28870.2	29198.3
9000	29526.4	29854.4	30182.5	30510.6	30838.7	31166.7	31494.8	31822.9	32150.9	32479.0
					Uni	ita				
	1)				C II.	its.				
Tens.	-		0	9				-		
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	O. Am Feet	1. Am Feet	2. Am Feet							9.
0		Am Feet 3.281			4.	5.				
0 10	Am Feet	Am Feet	Am Feet	Am Feet.	4. Am.Feet	5. Am Feet.	Am Feet	Am.Feet.	Am Feet.	Am. Feet
0 10 20	Am Feet 0.000	Am Feet 3.281 36.088 68.895	Am Feet 6.561 39.369 72.176	Am Feet. 9.842 42.649 75.456	4. Am.Feet 13.123 45.930 78.737	5. Am Feet. 16.404	Am Feet 19.684	Am.Feet. 22.965	Am Feet. 26.246	Am. Feet 29.526
0 10 20 30	Am Feet 0.000 32.807	Am Feet 3.281 36.088 68.895	Am Feet 6.561 39.369 72.176	Am Feet. 9.842 42.649	4. Am.Feet 13.123 45.930 78.737	5. Am Feet. 16.404 49.211 82.018	Am Feet 19.684 52.491 85.298	Am.Feet. 22.965 55.772 88.579	Am Feet. 26.246 59.053	Am Feet 29.526 62.333 95.141
0 10 20	Am Feet 0.000 32.807 65.614	Am Feet 3.281 36.088 68.895 191.702	Am Feet 6.561 39.369 72.176 104.983	Am Feet. 9.842 42.649 75.456	4. Am.Feet 13.123 45.930 78.737 111.544	Am Feet. 16.404 49.211 82.018 114.825	Am Feet 19.684 52.491 85.298 118.106	Am.Feet. 22.965 55.772 88.579	Am Feet. 26.246 59.053 91.860 124.667	Am. Feet 29.526 62.333 95.14 127.948
0 10 20 30	Am Feet 0.000 32.807 65.614 98.421 131.228	Am Feet 3.281 36.088 68.895 191.702 134.509	Am Feet 6.561 39.369 72.176 104.983 137.790	Am Feet. 9.842 42.649 75.456 108.263 141.070	4. Am.Feet 13.123 45.930 78.737 111.544	Am Feet. 16.404 49.211 82.018 114.825 147.632	Am Feet 19.684 52.491 85.298 118.106 150.913	Am.Feet. 22.965 55.772 88.579 121.386 154.193	Am Feet. 26.246 59.053 91.860 124.667	Am. Feet 29.526 62.333 95.14 127.948 160.755
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421 131.228	Am Feet 3.281 36.088 68.895 191.702 134.509	Am Feet 6.561 39.369 72.176 104.983 137.790 170.597	Am Feet. 9.842 42.649 75.456 108.263 141.070 173.878	4. Am. Feet 13.123 45.930 78.737 111.544 144.351 177.158	5. Am Feet. 16.404 49.211 82.018 114.825 147.632 180.439	Am Feet 19.684 52.491 85.298 118.106 150.913	Am.Feet. 22.965 55.772 88.579 121.386 154.193	Am Feet. 26.246 59.053 91.860 124.667 157.474	Am Feet 29.526 62.33; 95.14 127.948 160.75;
0 10 20 30 40	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035 196.843	Am Feet 3.281 36.088 68.895 191.702 134.509 167.316	Am Feet 6.561 39.369 72.176 104.983 137.790 170.597 203.404	Am Feet. 9.842 42.649 75.456 108.263 141.070 173.878 206.685	4. Am.Feet 13.123 45.930 78.737 111.544 144.351 177.158 209.965	5. Am Feet. 16.404 49.211 82.018 114.825 147.632 180.439 213.246	Am Feet 19.684 52.491 85.298 118.106 150.913 183.720 216.527	Am.Feet. 22.965 55.772 88.579 121.386 154.193 187.000 219.807	Am Feet. 26.246 59.053 91.860 124.667 157.474 190.281	Am Feet 29.526 62.33; 95.14 127.948 160.753 193.565 226.369
0 10 20 30 40 50 60	Am Feet 0.000 32.807 65.614 98.421 131.228 164.035 196.843 229.650	Am Feet 3.281 36.088 68.895 191.702 134.509 167.316 200.123 232.930	Am Feet 6.561 39.369 72.176 104.983 137.790 170.597 203.404 236.211	Am Feet. 9.842 42.649 75.456 108.263 141.070 173.878 206.685 239.492	4. Am.Feet 13.123 45.930 78.737 111.544 144.351 177.158 209.965	5. Am Feet. 16.404 49.211 82.018 114.825 147.632 180.439 213.246 246.053	Am Feet 19.684 52.491 85.298 118.106 150.913 183.720 216.527 249.334	Am.Feet. 22.965 55.772 88.579 121.386 154.193 187.000 219.807 252.615	Am Feet. 26.246 59.053 91.860 124.667 157.474 190.281 223.088	Am. Feet 29.520 62.333 95.14 127.940 160.753 193.563 226.360 259.170

IX. CONVERSION OF METRES INTO RHINE OR PRUSSIAN FEET AND DECIMALS.

1 Metre = 3 1861995 Rhine Feet.

Metres.					Hun	dreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Rhine Ft.	Rhine Ft	Rhine Ft	Rhine Ft	Rhine Ft.	Rhine Ft	Rhine Ft.	Rhine Ft.	Rhine Ft.	Rhine Ft.
0	0.0	318.6	637.2	955.9	1274.5	1593.I	1911.7	2230.3	2549.0	2867.6
1000	3186.2	3504.8	3823.4	4142.1	4460.7	4779.3	5097.9	5416.5	5735.2	6053.8
2000	6372.4	6691.0	7009.6	7328.3	7646.9	7965.5	8284.1	8602.7	8921.4	9240.0
3000	9558.6	9877.2	10195.8	10514.5	10833.1	11151.7	11470.3	11788.9	12107.6	12426.2
4000	12744.8	13063.4	13382.0	13700.7	14019.3	14337.9	14656.5	14975.1	15293.8	15612.4
5000	15931.0	16249.6	16568.2	16886.9	17205.5	17524.1	17842.7	18161.3	18480.0	18798.6
6000	19117.2	19435.8	19754.4	20073.1	20391.7	20710.3	21028.9	21347.5	21666.2	21984.8
7000	22303.4	22622.0	22940.6	23259.3	23577.9	23896.5	24215.1	24533.7	24852.4	25171.0
8000	25489.6	25808.2	26126.S	26445.5	26764.1	27082.7	27401.3	27719.9	28038.6	28357.2
9000	II i	i .				30268.9				

PARIS OR FRENCH FEET

INTO DIFFERENT MEASURES OF LENGTH.

X. CONVERSION OF PARIS OR FRENCH FEET INTO TOISES.

1 French Foot = 0.1666666 Toise.

French Feet.					Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	Toises.	Toises-
0	0.00	16.67	33.33	50.00	66.67	83.33	100.00	116.67	133.33	150.00
1000	166.67	183.33	200.00	216.67	233.33	250.00	266.67	283.33	300.00	316.67
2000	333.33	350.00	366.67	383.33	400.00	416.67	433.33	450.00	466.67	483.33
3000	500.00	516.67	533.33	550.00	566.67	583.33	600.00	616.67	633.33	650.00
4000	666.67	683.33	700.00	716.67	733.33	750.00	766.67	783.33	800.00	816.67
5000	833.33	850.00	866.67	883.33	900.00	916.67	933.33	950.00	966.67	983.33
6000	1000.00	1016.67	1033.33	1050.00	1066.67	1083.33	1100.00	1116.67	1133.33	1150.00
7000	1166.67	1183.33	1200.00	1216.67	1233.33	1250.00	1266.67	1283.33	1300.00	1316.67
8000	1333.33	1350.00	1366.67	1383.33	1400.00	1416.67	1433.33	1450.00	1466.67	1483.33
9000	1500.00	1516.67	1533.33	1550.00	1566.67	1583.33	1600.00	1616.67	1633.33	1650.00
10000	1666.67	1683.33	1700.00	1716.67	1733.33	1750.00	1766.67	1783.33	1800.00	1816.67
11000	1833.33	1850.00	1866.67	1883.33	1900.00	1916.67	1933.33	1950.00	1966.67	1983.33
12000	2000.00	2016.67	2033.33	2050.00	2066.67	2083.33	2100.00	2116.67	2133.33	2150.00
13000	2166.67	2183.33	2200.00	2216.67	2233.33	2250.00	2266.67	2283.33	2300.00	2316.67
14000	2333.33	2350.00	2366.67	2383.33	2400.00	2416.67	2433.33	2450.00	2466.67	2483.33
15000	2500.00	2516.67	2533.33	2550.00	2566.67	2583.33	2600.00	2616.67	2633.33	2650.00
16000	2666.67	2683.33	2700.00	2716.67	2733.33	2750.00	2766.67	2783.33	2800.00	2816.67
17000	2833.33	2850.00	2866.67	2883.33	2900.00	2916.67	2933.33	2950.00	2966.67	2953.33
18000	3000.00	3016.67	3033.33	3050.00	3066.67	3083.33	3100.00	3116.67	3133.33	3150.00
19000	3166.67	3183.33	3200.00	3216.67	3233.33	3250.00	3266.67	3283.33	3300.00	3316.67
20000	3333.33	3350.00	3366.67	3383.33	3400.00	3416.67	3433.33	3450.00	3466.67	3483.33
21000	3500.00	3516.67	3533.33	3550.00	3566.67	3583.33	3600.00	3616.67	3633.33	3650.00
22000	3666.67	3683.33	3700.00	3716.67	3733.33	3750.00	3766.67	3783.33	3800.00	3816.67
23000	3833.33	3850.00	3866.67	3883.33	3900.00	3916.67	3933.33	3950.00	3966.67	3983.33
24000	4000.00	4016.67	4033.33	4050.00	4066.67	4083.33	4100.00	4116.67	4133.33	4150.00
25000	4166.67	4183.33	4200.00	4216.67	4233.33	4250.00	4266.67	4283.33	4300.00	4316.67
26000	4333.33	4350.00	4366.67	4383.33	1400.00	4416.67	4433.33	4150.00	4466.67	4483.33

XI. CONVERSION OF PARIS OR FRENCH FEET INTO METRES.

1 Paris Foot = 0.32483943 Metres.

French Feet.					Hune	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	000.00		64.97	97.45	1	162.42	194.90	1	1	1
1000	324.84	357.32		422.29	1	487.26	519.74	i .		1
2000	649.68	682.16		1	1	812.10		1	1	1
3000 4000	974.52	1	1039.49			1	1	1	1234.39	
4000	1299.36	1991.54	1364.33	1396.81	1429.29	1461.78	1494.26	1526.75	1559.23	1591.7
5000	1624.20	1656.68	1689.16	1721.65	1754.13	1786.62	1819.10	1851.58	1884.07	1916.5
6000	1949.04	4			1	2111.46	1	1	1	1
7000	2273.88	1	2338.84	1	1	2436.30	1	1	1	1
8000	2598.72		2663.68	1	1	2761.14	1		2858.59	1
9000	2923.55			1	1	3085.97			1	1
10000	3248.39	3280.88	3313.36	3345 85	3378.33	3410.81	3113.30	3175 78	3508 27	35.10.7
11000	11	1 .	1		1	3735.65	I		1	
12000	11	3930.56	1		1	4060.49		l .	i .	1
13000	l)	4255.40			ľ	4385.33				
14000	4547.75	4580.24			1	4710.07	1	1		-
15000	1879 50	1005.00	1027 56	1070.01	5000 50	5095 01	5007 10	7000 00	7190 46	51046
16000	ř.	l .				5035.01				
17000		5229.91 5554.75	1	1	1	5359.85	1		5457.30	
18000	5847.11	5879.59	1	I	5977.05	5684.69)		6106.98	
19000	6171.95		1	1	6301.88			i	6431.82	
20000	6 106 70	6500.0*	0501 50	C*04.04	CC0C #0	0070.01	0001 00	070130	C== C CC	C#00.1
21000	I .			1		6659.21			i	1
22000	6821.63				6951.56				7081.50	
23000	7146.47	7178.95		1	7276.40				7406.34	1
24000	7471.31 7796.15				7601.24 7926.08	7633.73 7958.57			7731.18 8056.02	
27000	2120.00	0170 4	030505	2010	2270 02	2222 43	201 # 00	0.40.00	0000000	0.170.0
25000 26000	! !					8283.41			1	
27000						8608.24			1	
27000	8770.66	0909.19	5555.05	8808.12			8900.07	2990.09	9030.94	9003.0
Tens.					Un	its.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.0000	0.3248	0.6497	0.9745	1.2994	1.6242	1.9490	2.2739	2.5987	2.923
10	3.2484	3.5732	3.8981	4.2229	4.5478	4.8726	5.1974	5.5223	5.8471	6.171
20	6.4968	6.8216		7.4713	7.7961	8.1210		8.7707		
30						11.3694				
40	12.9936	13.3184	13.6433	13.9681	14.2929	14.6178	14.9426	15.2675	15.5923	15.917
50	16.2420	16.5668	16.8916	17.2165	17.5413	17.8662	18.1910	18.5158	18.8407	19.165
60						21.1146				
70						24.3630				
80						27.6114				
90						30.8597				

1 French Foot = 1.06576527 English Feet.

			1 Frenci	h Foot =	1.06576527	English Fe	et.			
French Feet.					Hund	ireds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet,	Eng feet.	_	Eng. feet.	-	Eng. feet.		Eng. feet.	
0	0.0	106.6	213.2	319.7	426.3	532.9	639.5	746.0	852.6	959.2
1000	1065.8	1172.3	1278.9		1	1598.6	1705.2	1	1	2025.0
2000	2131.5	2238.1	2344.7	2451.3	(2664.4	2771.0		2984.1	3090.7
3000	3197.3	1	3410.4	3517.0	3623.6	3730.2	3836.S		4049.9	4156.5
4000	4263.1	4369.6	4476.2	4582.8	4689.4	4795.9	4902.5	5009.1	5115.7	5222.3
5000	5328.8	5435.4	5542.0	5648.6	5755.1	5861.7	5968.3	6074.9	6181.4	6288.0
6000	6394.6	6501.2	6607.7	6714.3	6820.9	6927.5	7034.1	7140.6	7247.2	7353.8
7000	7460.4	7566.9	7673.5	7780.1	7886.7	7993.2	8099.8	8206.4	8313.0	8419.5
8000	8526.1	8632.7	8739.3	8845.9	8952.4	9059.0	9165.6	9272.2	9378.7	9485.3
9000	9591.9	9698.5	9805.0	9911.6	10018.2	10124.8	10231.3	10337.9	10444.5	10551.
10000	10657.7	10764.2	10870.8	10977.4	11084.0	11190.5	11297.1	11403.7	11510.3	11616.8
11000	11723.4	11830.0	11936.6	12043.1	12149.7	12256.3	12362.9	12469.5	12576.0	12682.6
12000	H	12895.S	13002.3	1	13215.5					
13000	13855.0	13961.5	14068.1	14174.7				1	14707.6	
14000	1	15027.3		1	15347.0					
15000	15986.5	16093.1	16199.6	16306.2	16412.8	16519.4	16625.9	16732.5	16839.1	16945.
16000	ł			f	17478.6			1		
17000		18224.6			18544.3					
18000	1	19290.4	1		19610.1					
19000		20356.1			20675.8				21102.2	•
20000	21315.3	21421.9	21528.5	21635.0	21741.6	21848.2	22054.8	22161.3	22167.9	22274.5
21000	1			1	22807.4				23233.7	
22000	1		1	1	23873.1				24299.5	
23000	i			1	24938.9				25365.2	
24000	li .				26004.7					
25000	26644.1	26750.7	26857.3	26963.9	27070.4	27177.0	27283.6	27390.2	27496.7	27603.3
26900					28136.2					
27000	II.				29202.0			l.		
1					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. feet.	Eng feet	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng feet	Eng feet.	Eng feet
0	0.000	1.066	2.132	3.197	4.263	5.329	6.395	7.460	8.526	9.592
10	10.658	11.723	12.789	13.855	14.921	15.986	17.052	18.118	19.184	20.250
20	21.315	22.381	23.147	24.513	25.578	26.644	27.710	28.776	29.841	30.907
30	31.973	33.039	34.104	35.170	36.236	37.302	38.368	39.433	40.499	41.565
40	42.631	43.696	44.762	45.828	46.894	47.959	49.025	50.091	51.157	52.225
50	53.288	54.354	55,420	56.486	57.551	58.617	59.683	60.749	61.814	62.880
60	63.946	65.012	66.077	67.143	68.209		70.341	71.406	72.472	73.538
70	74.604	75.669	76.735	77.801	78.867	79.932	80.998	82.064	83.130	1
80	85.261	86.327	87.393	83.459	89.524		91.656)	93.787	94.85
90	95.919			99.116		101.248		[
		1 0 0 0 0 0	1 *************************************							

1 French Foot = 1.0657034 American Foot.

rench Feet.					Hur	dreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Am. Feet	Am.Feet	Am. Feet.	1		Am. Feet.	Am. Feet	Am. Feet.	i	Am.Fe
0	0.0	106.6	213.1	319.7			639.4	1	i	i
1000	1065.7	1172.3	1	1	1	l .	1	1811.7		1
2000	2131.4	2238.0			1	2664.3	1	2577.4		
3000	3197.1	3303.7	3410.3	1	1	3730.0	1	3943.1	4049.7	Į.
4000	4262.8	4369.4	4476.0	4582.5	4689.1	4795.7	4902.2	5008.8	5115.4	5221
5000	5328.5	5435.1	5541.7	5648.2	5754.8	5861.4	5967.9	6074.5	6181.1	6287
6000	6394.2	6500.S	6607.4	6713.9	6820.5	6927.1	7033.6	7140.2	7246.8	7353
7000	7459.9	7566.5	7673.1	7779.6	7886.2	7992.8	8099.3	8205.9	8312.5	8419
8000	8525.6	8632.2	8738.8	8845.3	8951.9	9058.5	9165.1	9271.6	9378.2	9484
9000	9591.3	9697.9	9804.5	9911.0	10017.6	10124.2	10230.8	10337.3	10443.9	10550
10000	10657.0	10763.6	10870.2	10976.7	11083.3	11189.9	11296.5	11403.0	11509.6	11616
11000	11722.7	l	1		12149.0	1	12362.2	1	1	
12000	12788.4	l .	1	1	ł	13321.3	13427.9		13641.0	1
13000			14067.3			i	14493.6	Į.	14706.7	1
14000		1	15133.0	1		15452.7	15559.3			1
15000	15985.6	16092.1	16198.7	16305.3	16411.8	16518.4	16625.0	16731.5	16838.1	1694
16000		1	17264.4		1	17584.1		17797.2		1
17000		18223.5			18543.2			18863.0		
18000			,	l .		19715.5		19928.7		1
19000			1			20781.2	1	20994.4		1
20000	2121 (1	21 120 6	91597 9	21622 2	21740 4	21846.9	91059 5	22060.1	22166 6	22273
21000			į.	1		22912.6		23125.8		
22000			1	i .		23978.3			1	
23000	24511.2		1	ł)	25044.0		i		
24000	1			1	1	26109.7	1		ı	1
25000	266126	26740.2	96955 7	20002 2	27069 0	27175.4	อชอออ ก	94988 6	27105 2	27601
26000						28241.1				1
27000	- 1				1	29306.8				l
28000						30372.6)
					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	Am. Feet. 0.00	Am. Feet. 1.07	Am Feet 2.13	Am.Feet.	Am Feet 4.26	Am Feet. 5.33	Am.Feet. 6.39	7.16	Am Feet 8.53	Am Fe 9.5
10	10.66	11.72	12.79	13.85	14.92	15.99	17.05	18.12	19.18	20.2
20	21.31	22.38	23.45	24.51	25.58	26.64	27.71	28.77	29.84	30.9
30	31.97	33.04	34.10	35.17	36.23	37.30	38.37	39.43	40.50	41.5
40	42.63	43.69	44.76	45.83	46.89	47.96	49.02	50.09	51.15	52.2
50	53.29	51.35	55.42	56.48	57.55	58.61	59.68	60.75	61.81	62.8
60	63.94	65.01	66.07	67.14	68.21	69.27	70.34	71.40	72.47	73.5
76	74.60	75.66	76.73	77.80	78.86	79.93	80.99	82.06	83.12	84.1
80	85.26	86.32	87.39	88.45	89.52	90.58	91.65	92.72	93.78	94.8
~~	J-7-12-0	00.04	01.00	00.40	00.02	20.00	01.00	U	00000	1 2 1 4 0 1

ENGLISH YARDS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XIV. CONVERSION OF ENGLISH YARDS INTO FRENCH TOISES.

1 English Yard = 0.4691465 Toise.

English Yards					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises,	Toises.	Toises.	Toises,	Toises.	Toises	Toises.	Toises.	Toises.
0	0.00	46.91	93.83	140.74	187.66	234.57	281.49	328.40	375.32	422.23
1000	469.15	516.06	562.98	609.89	656.80	703.72	750.63	797.55	844.46	891.38
2000	938.29	985.21	1032.12	1079.04	1125.95	1172.87	1219.78	1266.70	1313.61	1360.52
3000	1407.44	1454.35	1501.27	1548.18	1595.10	1642.01	1688.93	1735.84	1782.76	1829.67
4000	1876.59	1923.50	1970.41	2017.33	2064.24	2111.16	2158.07	2204.99	2251.90	2298.82
5000	2345.73	2392.65	2439.56	2486.48	2533.39	2580.31	2627.22	2674.13	2721.05	2767.96
6000	2814.88	2861.79	2908.71	2955.62	3002.54	3049.45	3096.37	3143.28	3190.20	3237.11
7000	3284.02	3330.94	3377.85	3424.77	3471.68	3518.60	3565.51	3612.43	3659.34	3706.26
8000	3753.17	3800.09	3847.00	3893.92	3940.83	3987.74	4034.66	4081.57	4128.49	4175.40
9000	4222.32	4269.23	4316.15	4363.06	4409.98	4456.89	4503.81	4550.72	4597.63	4644.55

XV. CONVERSION OF ENGLISH YARDS INTO METRES.

1 English Yard = 0.91438348 Metre.

English Yards,					Hund	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	91.44	182.88	274.32	365.75	457.19	548.63	640.07	731.51	822.95
1000	914.38	1005.82	1097.26	1188.70	1280-14	1371.58	1463.01	1554.45	1645.89	1737.33
2000	1828.77	1920.21	2011.64	2103.08	2194.52	2285.96	2377.40	2468.84	2560.27	2651.71
3000	2743.15	2834.59	2926.03	3017.47	3108.90	3200.34	3291.78	3383.22	3474.66	3566.10
4000	3657.53	3748.97	3840.41	3931.85	4023.29	4114.73	4206.16	4297.60	4389.04	4480.48
5000	4571.92	4663.36	4754.79	4846.23	4937.67	5029.11	5120.55	5211.99	5303.42	5394.86
6000	5486.30	5577.74	5669.18	5760.62	5852.05	5943.49	6034.93	6126.37	6217.81	6309.25
7000	6400.68	6492.12	6583.56	6675.00	6766.44	6857.88	6949.31	7040.75	7132.19	7223.63
8000	7315.07	7406.51	7497.94	7589.38	7680.82	7772.26	7863.70	7955.14	8046.57	8138.01
9000	8229.45	8320.89	8412.33	8503.77	8595.20	8686.64	8778.08	8869.52	8960.96	9052.40

1 English Foot = 0.30479449 Metre.

English Feet.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	000.000	30.4794	60.9589	91.4383	121.918	152.397	182.877	213.356	243.836	274.31
1000	304.794	335.274	365.763	396.233	426.712	457.192	487.671	518.151	548.630	579.11
2000	609.589	640.068	670.548	701.027	731.507	761.986	792.466	822.945	853.425	883.90
3000	914.383	944.863	975.342	1005.82	1036.30	1066.78	1097.26	1127.74	1158.22	1188.7
4000	1219.18	1249.66	1280.14	1310.62	1341.10	1371.58	1402.05	1432.53	1463.01	1493.4
5000	1523.97	1554.45	1584.93	1615.41	1645.89	1676.37	1706.85	1737.33	1767.81	1798.2
6000	1828.77	1859.25	1889.73	1920.21	1950.68	1981.16	2011.64	2042.12	2072.60	2103.0
7000	2133.56	2164.04	2194.52	2225.00	2255.48	2285.96	2316.44	2346.92	2377.40	2407.8
8000	2438.36	2468.84	2499.31	2529.79	2560.27	2590.75	2621.23	2651.71	2682.19	2712.6
9000	2743.15	2773.63	2804.11	2834.59	2865.07	2895.55	2926.03	2956.51	2986.99	3017.4
10000	3047.94	3078.42	3108.90	3139.38	3169.86	3200.34	3230.82	3261.30	3291.78	3322.2
11000	3352.74	3383.22	3413.70	3444.18	3474.66	3505.14	3535.62	3566.10	3596.57	3627.0
12000	3657.53	3688.01	3718.49	3748.97	3779.45	3809.93	3840.41	3870.89	3901.37	3931.8
13000	3962.33	3992.81	4023.29	4053.77	4084.25	4114.73	4145.21	4175.68	4206.16	4236.6
14000	4267.12	4297.60	4228.08	4358.56	4389.04	4419.52	4450.00	4480.48	4510.96	4541.4
15000	4571.92	4602.40	4632.88	4663.36	4693.84	4724.31	4754.79	4785.27	4815.75	4846.2
16000	4876.71	4907.19	4937.67	4968.15	4998.63	5029.11	5059.59	5090.07	5120.55	5151.0
17000	5181.51	5211.99	5242.47	5272.94	5303.42	5333.90	5364.38	5394.86	5425.34	5455.8
18000	5486.30	5516.78	5547.26	5577.74	5608.22	5638.70	5669.18	5699.66	5730.14	5760.6
19000	5791.10	5821.57	5852.05	5882.53	5913.01	5943.49	5973.97	6004.45	6034.93	6065
20000	6095.89	6126.37	6156.85	6187.33	6217.81	6248.29	6278.77	6309.25	6339.73	6370.2
21000	6400.68	6431.16	6461.64	6492.12	6522.60	6553.08	6583.56	6614.04	6644.52	6675.
22000	6705.48	6735.96	6766.44	6796.92	6827.40	6857.88	6888.36	6918.83	6949.31	6979.
23000	7010.27	7040.75	7071.23	7101.71	7132.19	7162.67	7193.15	7223.63	7254.11	7284.
24000	7315.07	7345.55	7376.03	7406.51	7436.99	7467.47	7497.94	7528.42	7558.90	7589.
25000	7619.86	7650.34	7680.82	7711.30	7741.78	7772.26	7802.74	7833.22	7863.70	7894.
26000	7924.66	7955.14	7985.62	8016.10	8046.57	8077.05	8107.53	8138.01	8168.49	8198.9
27000	8229.45	8259.93	8290.41	8320.89	8351.37	8381.85	8412.33	8442.81	8473.29	8503.7
28000	8534.25	8564.73	8595.20	8625.68	8656.16	8686.64	8717.12	8747.60	8778.08	8808.
					Un	it s.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	1	0.30479	l .	I	1.21918		1.82877		2.43836	
10					4.26712					
20	6.09589	6.40068	6.70548	7.01027	7.31507	7.61986	7.92466	8.22945	8.53425	8.8390
30	9.14383	9.44863	9.75342	10.0582	10.3630	10.6678	10.9726	11.2774	11.5822	11.887
40					13.4110					
50	15. 2 397	15.5445	15.8493	16.1541	16.4589	16.7637	17.0685	17.3733	17.6781	17.982
60					19.5068					
70					22.5548					
80					25.6027					
					28.6507					

1 English Foot = 0.9382929 Paris Foot.

English Feet.					Hund	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet	Par. Feet.
0	0.000	93.8	187.7	281.5	375.3	469.1	563.0	656.8	750.6	844.5
1000	938.3	1032.1	1126.0	1219.8	1313.6	1407.4	1501.3	1595.1	1688.9	1782.8
2000	1876.6	1970.4	2064.2	2158.1	2251.9	2345.7	2439.6	2533.4	2627.2	2721.0
3000	2814.9	2908.7	3002.5	3096.4	3190.2	3284.0	3377.9	3471.7	3565.5	3659.3
4000	3753.2	3847.0	3940.8	4034.7	4128.5	4222.3	4316.1	4410.0	4503.8	4597.6
5000	4691.5	4785.3	4879.1	4973.0	5066.8	5160.6	5254.4	5348.3	5442.1	5535.9
6000	5629.8	5723.6	5817.4	5911.2	6005.1	6098.9	6192.7	6286.6	6380.4	6474.2
7000	6568.0	6661.9	6755.7	6849.5	6943.4	7037.2	7131.0	7224.9	7318.7	7412.5
8000	7506.3	7600.2	7694.0	7787.8	7881.7	7975.5	8069.3	8163.1	8257.0	8350.8
9000	8444.6	8538.5	8632.3	8726.1	8820.0	8913.8	9007.6	9101.4	9195.3	9289.1
10000	9382.9	9476.8	9570.6	9664.4	9758.2	9852.1	9945.9	10039.7	10133.6	10227.4
11000	J	10415.0		1	10696.5	I			11071.9	l .
12000	i .	11353.3	11447.2	1	11634.8		1		12010.1	1
13000		12291.6			12573.1		i	i .	12948.4	
14000	13136.1	13229.9	13323.8			Į.		1	13886.7	
15000	11071 1	14168.2	1 1262 0	1 (255 0	14449.7	1 15 12 5	11627 1	14721 9	1.1895.0	11018 0
16000	1	15106.5	ł]	15388.0		1			1
17000	1	16044.8	1	16232.5	1			!	16701.6	
18000		16983.1			17264.6	l.	l .		17639.9	
19000		17921.4	ı	ı	18202.9		1		18578.2	1
20000	10505 0	10050 #	10050 5	10047 0	101410	10007.0	10000 0	10 400 *	10516.5	10010.0
20000		18859.7	l .	l .	19141.2		1		1	
21000	1	19798.0		i	20079.5	1	1			1
22000	1		i		21017.8		i		1	ı
23000	21580.7				21956.0				22331.4	l .
24000	22319.0	22612.9	22706.7	22800.5	22894.3	22988.2	23082.0	23175.5	23269.7	25505.5
. 25000	1				23832.6					
26000	24395.6				24770.9		1		ŀ	i
27000	1				25709.2		1			
28000	26272.2	26366.0	26459.9	26553.7	26647.5	26741.3	26835.2	26929.0	27022.8	27116.7
_					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par. Feet.	Par. Feet.	Par Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par. Feet.	Par, Feet.	Par. Feet.
0	0.00	0.94	1.88	2.81	3.75	4.69	5.63	6.57	7.51	8.44
10	9.38	10.32	11.26	12.20	13.14	14.07	15.01	15.95	16.89	17.83
20	18.77	19.70	20.64	21.58	22.52	23.46	24.40	25.33	26.27	27.21
30	28.15	29.09	30.03	30.96	31.90	32.84	33.78	34.72	35.66	36.59
40	37.53	38.47	39.41	40.35	41.28	42.22	43.16	44.10	45.04	45.98
50	46.91	47.85	48.79	49.73	50.67	51.61	52.54	53.48	54.42	55.36
60	56.30	57.24	58.17	59.11	60.05	60.99	61.93	62.87	63.80	64.74
70	65.68	66.62	67.56	68.50	69.43	70.37	71.31	72.25	73.19	74.13
	, ,			- 1						
80	75.06	76.00	76.94	77.88	78.82	79.75	80.69	81.63	82.57	83.51

135

D

1 English Foot = 0.99994197 American Foot.

					Hund	lreds.				
Eng. Feet. Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Am Feet	Am. Feet.	Am. Feet.	Am Feet	Am.Feet.	Am Feet	Am Feet.	Am. Feet.	Am Feet.	Am. Feet
0	0.00	99.99	199.99	299.98	399.98	499.97	599.97	699.96	799.95	899.95
1000	999.94	1099.94	1199.93	1299.92	1399.92	1499.91	1599.91	1699.90	1799.90	1899.89
2000	1999.88	2099.88	2199.87	2299.87	2399.86	2499.85	2599.85	2699.84	2799.84	2899.83
3000	2999.83	3099.82	3199.81	3299.81	3399.80	3499.80	3599.79	3699.79	3799.78	3899.77
4000	3999.77	4099.76	4199.76	4299.75	4399.74	4499.74	4599.73	4699.73	4799.72	4899.72
5000	4999.71	5099.70	5199.70	5299.69	5399.69	5499.68	5599.68	5699.67	5799.66	5899.66
6000	5999.65	6099.65	6199.64	6299.63	6399.63	6499.62	6599.62	6699.61	6799.61	6899.60
7000	6999.59	7099.59	7199.58	7299.58	7399.57	7499.56	7599.56	7699.55	7799.55	7899.54
8000	7999.54	8099.53	8199.52	8299.52	8399.51	8499.51	8599.50	8699.50	8799.49	8899.48
9000	8999.48	9099.47	9199.47	9299.46	9399.45	9499.45	9599.44	9699.44	9799.43	9899.43
10000	9999.42	10099.1	10199.4	10299.4	10399.4	10499.4	10599.4	10699.4	10799.4	10899.4
11000	10999.4	11099.4	11199.4	11299.3	11399.3	11499.3	11599.3	11699.3	11799.3	11899.3
12000	11999.3	12099.3	12199.3	12299.3	12399.3	12499.3	12599.3	12699.3	12799.3	12899.2
13000	12999.2	13099.2	13199.2	13299.2	13399.2	13499.2	13599.2	13699.2	13799.2	13899.2
14000	13999.2	14099.2	14199.2	14299.2	14399.2	14499.2	14599.2	14699.1	14799.1	14899.1
15000	14999.1	15099.1	15199.1	15299.1	15399.1	15499.1	15599.1	15699.1	15799.1	15899.1

The following Table of Differences between English and American Feet, for every hundred feet, will make it easy to convert English into American Feet, or American into English Feet, by adding to, or subtracting from, the number of feet to be converted, which is contained in the first column, the numbers found in the other columns.

XIX. DIFFERENCES BETWEEN ENGLISH AND AMERICAN FEET.

To obtain English Feet add. To obtain American Feet subtract.

10000 American Feet = 10000.5803 English Feet.

Number of Feet.			Hundreds	١.		Number of Feet.			Hundreds		
Thou- sands.	0.	200.	400.	600.	800.	Thou- sands.	0.	200.	400.	600.	800.
	Diff feet	Diff.feet	Diff feet	Diff.feet.	Diff feet		Diff.feet.	Diff.feet	Diff.feet	Diff feet.	Diff.feet
0	+0.000	+0.012	+0.023	+0.035	± 0.046	15000	±0.870	±0.882	±0.894	± 0.905	± 0.917
1000	0.058	0.070	0.082	0.093	0.105	16000	0.928	0.940	0.952	0.963	0.975
2000	0.116	0.128	0.139	0.151	0.162	17000	0.987	0.998	1.010	1.021	1.033
3000	0.174	0.186	0.197	0.209	0.221	18000	1.045	1.056	1.068	1.079	1.091
4000	0.232	0.244	0.255	0.267	0.279	19000	1.103	1.114	1.126	1.137	1.149
5000	0.290	0.302	0.313	0.325	0.337	20000	1.161	1.172	1.184	1.195	1.207
6000	0.348	0.360		0.383	0.395	21000	1.219	1.230	1.242	1.253	1.265
7000	0.406	0.418	0.429	0.441	0.453	22000	1.277	1.288	1.300	1.311	1.323
8000	0.464	0.476	0.487	0.499	0.511	23000	1.335	1.346	1.358	1.370	1.381
9000	0.522	0.534	0.546	0.557	0.569	24000	1.393	1.404	1.416	1.428	1.439
10000	0.580	0.592	0.604	0.615	0.627	25000	1.451	1.462	1.474	1.486	1.497
11000	0.638	0.650	0.662	0.673	0.685	26000	1.509	1.520	1.532	1.544	1.555
12000	0.696	0.708	0.720	0.731	0.743	27000	1.567	1.578	1.590	1.602	1.613
13000	0.754	0.766	0.778	0.789	0.801	28000	1.625	1.636	1.648	1.660	1.671
14000	0.812	0.824	0.836	0.847	0.859	29000	1.683	1.694	1.606	1.718	1.729

AMERICAN YARDS AND FEET

INTO DIFFERENT MEASURES OF LENGTH

XX. CONVERSION OF AMERICAN YARDS INTO FRENCH TOISES.

1 American Yard = 0.4691737 Toise.

American Yards					Hune	lreds.				
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Torses.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.	"oises.
0	0.20	45.92	93.83	140.75	187.67	234.59	281.50	328.42	375.34	422.26
1000	469.17	516.09	563.01	609.93	656.84	703.76	750.68	797.60	844.51	891.43
2000	938.35	985.26	1032.18	1079.10	1126.02	1172.93	1219.85	1266.77	1313.69	1360.60
3000	1407.52	1454.44	1501.36	1548.27	1595.19	1642.11	1689.02	1735.94	1782.86	1829.78
4000	1876.69	1923.61	1970.53	2017.45	2064.36	2111.28	2158.20	2205.12	2252.03	2298.95
5000	2345.87	2392.79	2439.70	2486.62	2533.54	2580.45	2627.37	2674.29	2721.21	2768.12
6000	2815.04	2861.96	2908.88	2955.79	3002.71	3049.63	3096.55	3143.46	3190.38	3237.30
7000	3284.22	3331.13	3378.05	3424.97	3471.88	3518.80	3565.72	3612.64	3659.55	3706.47
8000	3753.39	3800.31	3847.22	3894.14	3941.06	3987.98	4034.89	4081.81	4128.73	4175.65
9000	4222.56	4269.48	4316.40	4363.31	4410.23	4457.15	4504.07	4550.98	4597.90	4644.82

XXI. CONVERSION OF AMERICAN YARDS INTO METRES.

1 American Yard = 0.91443655 Metre.

American Yards.					Hune	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	91.44	182.89	274.33	365.77	457.22	548.66	640.11	731.55	822.99
1000	914.44	1005.88	1097.32	1188.77	1280.21	1371.65	1463.10	1554.54	1645.99	1737.43
2000	1828.87	1920.32	2011.76	2103.20	2194.65	2286.09	2377.54	2468.98	2560.42	2651.87
3000	2743.31	2834.75	2926.20	3017.64	3109.08	3 2 00.53	3291.97	3383.42	3474.86	3566.30
4000	3657.75	3749.19	3840.63	3932.08	4023.52	4114.96	4206.41	4297.85	4389.30	4480.74
5000	4572.18	4663.63	4755.07	4846.51	4937.96	5029.40	5120.84	5212.29	5303.73	5395.18
6000	5486.62	5578.06	5669.51	5760.95	5852.39	5943.84	6035.28	6126.72	6218.17	6309.61
7000	6401.06	6492.50	6583.94	6675.39	6766.83	6858.27	6949.72	7041.16	7132.61	7224.05
8000	7315.49	7406.94	7498.38	7589.82	7681.27	7772.71	7864.15	7955.60	8047.04	8138.49
9000	8229 93	8321.37	8412.82	8504.26	8595.70	8687.15	8778.59	8870.03	8961.48	9052.92

XXII. CONVERSION OF AMERICAN FEET INTO METRES.

1 American Foot = 0.30481218 Metre.

Amer. Feet.					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.00	1			1	152.41		ł	1	1
1000	304.81	335.29		1	1	457.22		1	1	
2000	609.62	1		1		,	1			
3000	914.44		1	1		!	1097.32	-	1	
4000	1219.25	1249.73	1280.21	1310.69	1341.17	1371.65	1402.14	1432.62	1463.10	1493.5
5000	1524.06	1554.54	1585.02	1615.50	1645.99	1676.47	1706.95	1737.43	1767.91	1798.3
6000	1828.87	1859.35	1889.84	1910.32	1940.80	1971.28	2001.76	2032.24	2062.72	2093.2
7000	2123.69	2154.17	2184.65	2225.13	2255.61	2286.09	2316.57	2347.05	2377.54	2408.0
8000	2438.50	2468.98	2499.46	2529.94	2560.42	2590.90	2621.38	2651.87	2682.35	2712.8
9000	2743.31	2773.79			2865.23	ı	2926.20	1		
10000	3048.12	3078.60	3109.08	3139.57	3170.05	3200.53	3231.01	3261.49	3291.97	3322.4
11000	1				3474.86		3535.S2			1
12000	11	3688.23	1	3749.19	l .	3810.15		3871.11	1	1
13000	H	3993.04		4054.00			4145.45			1
14000	4267.37			4358.81	4389.30	4419.78		1	4511.22	1
11000	1207.51	1201100	1920.99	1000.01	1005.00	4415.10	4450.20	1100.11	4311.22	4041.1
15000	4572.18	4602.66	4633.15	4663.63	4694.11	4724.59	4755.07	4785.55	4816.03	4846.5
16000	4876.99	4907.48	4937.96	4968.44	4998.92	5029.40	5059.88	5090.36	5120.84	5151.3
17000	5181.81	5212.29	5242.77	5273.25	5303.73	5334.21	5364.69	5395.18	5425.66	5456.1
18000	5486.62	5517.10	5547.58	5578.06	5608.54	5639.03	5669.51	5699.99	5730.47	5760.9
19000	5791.43	5821.91	5852.39	5882.88	5913.36	5943.84	5974.32	6004.80	6035.28	6065.7
20000	6096.24	6126.72	6157.21	6187.69	6218.17	6248.65	6279.13	6309.61	6340.09	6370.5
21000	6401.06	6431.54	6462.02	6492.50	6522.98	6553.46	6583.94	6614.42	6644.91	6675.3
22000	6705.87	6736.35	6766.83	6797.31	6827.79	6858.27	6888.76	6919.24	6949.72	6980.2
23000		7041.16		7102.12	ì	7163.09	1		7254.53	
24000				7406.94		7467.90			7559.34	
25000	7620 30	7650 79	7681.97	7711 75	7742.23	7772.71	7809 10	7833 67	7864.15	78016
26000					8047.04		8108.00			1
27000					8351.85					
28000	1				8656.67				Í	
1	1			0020110		· -				
Tens.					Un	its.				
	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.0000	0.3048	0.6096	0.9144	1.2192	1.5241	1.8289	2.1337	2.4385	2.743
10	3.0481	3.3529	3.6577	3.9626	4.2674	4.5722	4.8770	5.1818	5.4866	5.791
20	6.0962	6.4011	6.7059	7.0107	7.3155	7.6203	7.9251	8.2299	8.5347	8.839
30	9.1444	9.4492	9.7540	10.0588	10.3636	10.6684	10.9732	11.2781	11.5829	11.887
40				13.1069		13.7165				
50	15,2406	15.5454	15.8509	16.1550	16.4599	16.7647	17,0695	17.3743	17.6791	17.983
60					19.4080					
70					22.5561					
• • •										
80	24.3850	24.6898	21.9916	25,2994	25.6042	25,9090	26.2138	26.5187	26.8235	27.128

 $1 \ \, American \ \, Foot=0.93834737 \ \, Paris \, \, Foot.$

Amer. Feet.					Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Par.Feet.	1	Par. Feet.	Par. Feet.	Par. Feet.	Par.Feet.	Par. Feet.	Par. Feet.	i	Par. Feet.
0	0.0	93.8	187.7	281.5	375.3	469.2	563.0	656.8	750.7	844.5
1000	938.3		1126.0		1313.7	1407.5	1501.4	1595.2		1782.9
2000	1876.7	1970.5	2064.4	2158.2	2252.0	2345.9	2439.7	2533.5	2627.4	2721.2
3000	2815.0	2908.9	3002.7	3096.5	3190.4	3284.2	3378.1	3471.9	3565.7	3659.6
4000	3753.4	3847.2	3941.1	4034.9	4128.7	4222.6	4316.4	4410.2	4504.1	4597.9
5000	4691.7	4785.6	4879.4	4973.2	5067.1	5160.9	5254.7	5348.6	5442.4	5536.2
6000	5630.1	5723.9	5817.8	5911.6	6005.4	6099.3	6193.1	6286.9	6380.8	647,1.6
7000	6568.4	6662.3	6756.1	6849.9	6943.8	7037.6	7131.4	7225.3	7319.1	7412.9
8000	7506.8	7600.6	7694.4	77 88.3	7882.1		8069.8	8163.6	8257.5	8351.3
9000	8445.1	8539.0	8632.8	8726.6	8820.5	8914.3	9003.1	9102.0	9195.8	9289.6
10000	9383.5	9477.3	9571.1	9665.0	9758.S	9852.6	9946.5	10040.3	10134.2	10228.0
11000	10321.8	10415.7	10509.5	10603.3	10697.2	10791.0	10884.8	10978.7	11072.5	11166.3
12000	11260.2	11354.0	11447.8	11541.7	11635.5	11729.3	11823.2	11917.0	12010.8	12104.7
13000	12198.5	12292.3	12386.2	12480.0	12573.9	12667.7	12761.5	12855.4	12949.2	13043.0
14000	13136.9	13230.7	13324.5	13418.4	13512.2	13606.0	13699.9	13793.7	13887.5	13981.4
15000	14075.2	14169.0	14262.9	14356.7	14450.5	14544.4	14638.2	14732.1	14825.9	14919.7
16000	1			ì		15482.7			1	l
17000	1			ì		16421.1				
18000		16984.1	1	1	1	17359.4			1	
19000		1		1		18297.8				
20000	19766 0	19960 9	180516	10018 1	101 (9.9	19236.1	10220 0	10499 8	10517 6	10611 5
21000				1		20174.5				
22000	I	1	1	1		21112.8				
23000	l		1	ı		22051.2				
24000	i		1	ı		22989.5				
24000	22020.0	22014.2	22700.0	22001.0	22033.1	22900.0	45005.5	20111.2	25271.0	20004.0
25000						23927.9				
26000						24866.2				
27000	ı	1				25804.5		4		1
28000	26273.7	26367.6	26461.4	26555.2	26649.1	26742.9	26836.7	26930.6	27024.4	27118.2
					$\mathbf{U}\mathbf{n}$	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Par Feet.	Par Feet.	Par. Feet.	Par. Feet.	Par.Feet.	Par Feet.	Par.Feet.	Par. Feet	Par Feet	Par. Feet
0	0.00	0.94	1.88	2.82	3.75	4.69	5.63	6.57	7.51	8.45
10	9.38	10.32	11.26	12.20	13.14	14.08	15.01	15.95	16.89	17.83
20	18.77	19.71	20.64	21.58	22.52	23.46	24.40	25.34	26.27	27.21
30	28.15	29.09	30.03	30.97	31.90	32.84	33.78	34.72	35.66	36.60
40	37.53	38.47	39.41	40.35	41.29	42.23	43.16	44.10	45.04	45.98
50	46.92	47.86	48.79	49.73	50.67	51.61	52.55	53.49	54.42	55.36
60	56.30	57.24	58.18	59.12	60.05	60.99	61.93	62.87	63.81	64.75
70	65.68	66.62	67.56	68.50	69.44	70.38	71.31	72.25	73.19	74.13
80	75.07	76.01	76.94	77.88	78.82	79.76	80.70	81.64	82.57	83.51
90	84.45	85.39	86.33	87.27	88.20	89.14	90.08	91.02	91.96	92.90

KLAFTER AND FEET OF VIENNA

INTO DIFFERENT MEASURES OF LENGTH.

1 KLAFTER OF VIENNA = 6 FEET OF VIENNA = 0.9730317 Toise DU PÉROU.

From this value are derived the equations used in computing the following tables.

XXIV. CONVERSION OF KLAFTER OF VIENNA INTO FRENCH TOISES. $1 \; {\rm Klafter} = 0.9730317 \; {\rm Toise}.$

Klafter of Vienna.					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises	Toises.	Toises.
0	0.00	97.30	194.61	291.91	389.21	486.52	583.82	681.12	778.43	875.7
1000	973.03	1070.33	1167.64	1264.94	1362.24	1459.55	1556.85	1654.15	1751.46	1848.7
2000	1946.06	2043.37	2140.67	2237.97	2335.28	2432.58	2529.88	2627.19	2724.49	2821.7
3000	2919.10	3016.40	3113.70	3211.00	3308.31	3405.61	3502.91	3600.22	3697.52	3794.8
4000	3592.13	3989.43	4086.73	4184.04	4281.34	4378.64	4475.95	4573.25	4670.55	4767.8
5000	4865.16	4962.46	5059.76	5157.07	5254.37	5351.67	5448.98	5546.28	5643.58	5740.8
Klafter.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.	Toises.
0	0.000	0.973	1.946	2.919	3.892	4.865	5.838	6.811	7.784	8.757
10	9.730	10.703	11.676	12.649	13.622	14.595	15.569	16.542	17.515	18.488
20	19.461	20.434	21.407	22.380	23.353	24.326	25.299	26.272	27.245	28.218
30	29.191	30.164	31.137	32.110	33.083	34.056	35.029	36.002	36.975	37.948
40	38.921	39.894	40.867	41.840	42.813	43.786	44.759	45.732	46.706	47.679
50	48.652	49.625	50.598	51.571	52.544	53.517	54.490	55.463	56.436	57.409
60										
70	58.382	59.355	60.328	61.301	62.274	63.247	64.220	65.193	66.166	67.139
	68.112	69.055	70.058	71.031	72.004	72.977	73.950	74.923	75.896	76.870
80	77.813	78.816	79.789	80.762	81.735	82.708	83.681	81.654	85.627	86.600
90	87.573	88.546	89.519	90.492	91.465	92.438	93.411	94.384	95.357	96.330

1 Klafter = 1.8964741 Metres.

Klafter of Vienna.					Hun	dreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	. Metres.	Metres.	Metre
0	0.00	189.65	379.29	568.94	758.59	948.24	1137.88	1327.53	1517.18	1706.8
1000	1896.47	2086.12	2275.77	2465.42	2655.06	2844.71	3034.36	3224.01	3413.65	3603.5
2000	3792.95	3982.60	4172.24	4361.89	4551.54	4741.19	4930.83	5120.48	5310.13	5499.7
3000	5689.42	5879.07	6068.72	6258.36	6448.01	6637.66	6827.31	7016.95	7206.60	7396.2
4000	7585.90	7775.54	7965.19	8154.84	8344.49	8534.13	8723.78	8913.43	9103.08	9292.7
Klafter.					Un	its.				
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres
0	0.000	1.896	3.793	5.689	7.586	9.482	11.379	13.275	15.172	17.06
10	18.965	20.861	22.758	24.654	26.551	28.447	30.344	32.240	34.136	36.03
20	37.929	39.826	41.722	43.619	45.515	47.412	49.308	51.205	53.101	54.99
30	56.891	58.791	60.687	62.584	64.480	66.377	68.273	70.170	72.066	73.96
40	75.859	77.755	79.652	81.548	83.445	85.341	£7.238	89.134	91.031	92.92
50	94.824	96.720	98.617	100.513	102.409	104.306	106.203	108 099	109 995	111 80
60			117.581				125.167			
70	li i		136.546				144.132	1		1
80	li l	1 1	155.511		1	ı	163.097	1		ľ
			100.011	101.401	100.001	101.500	100.007	104.000	100.050	100.10
90 XXVI.	170.683	172.579	F KLAF	TER OF	VIENN	180.165 A INTO	PARIS	,		
90 XXVI.	170.683	172.579	F KLAF	TER OF	VIENN	A INTO	PARIS	,		
90	170.683	172.579	F KLAF	TER OF	VIENN	A INTO	PARIS	,		EET.
XXVI.	170.683	172.579 SION O	F KLAF 1 Klafter 200.	TER OF = 5.83819	VIENN 02 Paris o Hund	IA INTO r French F	PARIS eet.	OR FR	800.	900
XXVI.	170.683	172.579 sion o	F KLAF 1 Klafter	TER OF = 5.83819 300. Par.Feet.	VIENN 002 Paris of Hund 400. Par.Feet.	A INTO r French F lreds. 500. Par.Feet.	PARIS eet. 600. Par.Feet.	700.	SOO.	900 Par.Fee
XXVI. Klafter of Vienna. Thousands.	170.683 CONVER Par.Feet. 0.00	172.579 ssion o Par.Feet. 583.82	F KLAF 1 Klafter 200. Par.Feet.	TER OF = 5.83819 300. Par. Feet. 1751.46	VIENN 002 Paris o Hund 400. Par.Feet. 2335.28	A INTO r French F dreds. 500. Par.Feet. 2919.10	PARIS deet. 600. Par.Feet. 3502.91	700. Par.Feet. 4086.73	800. Par.Feet.	900 Par.Fee 5254.3
90 XXVI. Klafter of Vienna. Thousands.	0.00 Dar.Feet. 0.00 5838.19	172.579 SION O Par.Feet. 583.82 6422.01	F KLAF 1 Klafter 200. Par.Feet. 1167.61	300. Par. Feet. 1751.46 7589.65	VIENN 002 Paris o Hund 400. Par.Feet. 2335.28 8173.47	A INTO r French F dreds. 500. Par.Feet. 2919.10 8757.29	PARIS eet. 600. Par.Feet.	700. Par.Feet. 4086.73 9924.92	800. Par.Feet. 4670.55	900 Par.Fee 5254.3
90 XXVI. Klafter of Vienna. Thousands. 0 1000	0.00 5838.19 11676.4	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2	F KLAF 1 Klafter 200. Par.Feet. 1167.61 7005.83	TER OF = 5.83819 300. Par.Feet. 1751.46 7589.65 13427.8	VIENN 002 Paris of Hund 200. Par.Feet. 2335.28 8173.47 14011.7	A INTO r French F dreds. 500. Par.Feet. 2919.10 8757.29 14595.5	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3	700. Par.Feet. 4086.73 9924.92 15763.1	800. Par.Feet. 4670.55 10508.7 16346.9	900 Par.Fee 5254.3 11092. 16930.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000	0. Par, Feet. 0.00 5838.19 11676.4 17514.6	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.61 7005.83 12844.0 18682.2	300. Par. Feet. 1751.46 7589.65 13427.8 19266.0	VIENN 002 Paris o Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8	A INTO r French F dreds. 500. Par.Feet. 2919.10 8757.29 14595.5	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900 Par.Fee 5254.3 11092. 16930. 22768.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000	0. Par, Feet. 0.00 5838.19 11676.4 17514.6	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.61 7005.83 12844.0 18682.2	300. Par. Feet. 1751.46 7589.65 13427.8 19266.0	VIENN 002 Paris o Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8	A INTO r French F lreds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900 Par.Fee 5254.3 11092. 16930. 22768.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000	0. Par, Feet. 0.00 5838.19 11676.4 17514.6	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4	Par.Feet. 1167.61 7005.83 12844.0 18682.2	300. Par. Feet. 1751.46 7589.65 13427.8 19266.0	VIENN 002 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0	A INTO r French F lreds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1	900 Par.Fee 5254.3 11092. 16930. 22768.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter.	0. Par.Feet. 0.00 5338.19 17514.6 23352.8	172.579 SION O Par.Feet. 583.82 6422.01 218098.4 23936.6	Par.Feet. 1167-61 7005-83 128-41.0 18682.2 24520.4	300. Par. Feet. 1751.46 13427.8 19266.0 25101.2	VIENN 102 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0	A INTO r French F lreds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 its.	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3	900 Par.Fee 5254.3 11092. 16930. 22768. 28607.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter.	0. Par.Feet. 0.00 5338.19 17514.6 23352.8	172.579 SION O Par.Feet. 583.82 6422.01 218098.4 23936.6	Par.Feet. 1167.61 7005.83 12844.0 18682.2 24520.4	300. Par. Feet. 1751.46 13427.8 19266.0 25101.2	VIENN 002 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni	A INTO r French F lreds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 its.	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par. Feet. 4670.55 10508.7 16346.9 22185.1 28023.3	900 Par.Fee 5254.3 11092. 16930. 22768. 28607.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens.	0. Par. Feet. 0.00 5838.19 117514.6 23352.8 0. Par. Feet.	172.579 SION O Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	Par.Feet. 1 Klafter 200. Par.Feet. 1167.61 7005.83 12844.0 18682.2 24520.4	TER OF = 5.83818 300. Par.Feet. 1751.46 7589.65 13427.8 19266.0 25101.2	VIENN 002 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par. Feet.	A INTO r French F lreds. 500. Par. Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 lts.	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3	Par.Fee 52.5. Par.Fee 52.5.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens.	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8 0. Par.Feet. 0.00	172.579 SION O Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	F KLAF 1 Klafter 200. Par.Feet. 1167.61 7005.83 12844.0 18682.2 24520.4 2. Par.Feet. 11.68	TER OF = 5.83818 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2	VIENN 002 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par. Feet. 23.35	A INTO r French F lreds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 its. 5. Par.Feet. 29.19	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 7. Par.Feet. 40.87	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 8. Par.Feet. 46.71 105.09	Par.Fee 5254.3 11092. 16930. 22768. 28607. Par.Fee 52.5.110.9:
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens.	0. Par.Feet. 0.00 5833.19 11676.4 17514.6 23352.8 Par.Feet. 0.00 58.38 116.76 175.15	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	Par.Feet. 11.68 70.06	TER OF = 5.83818 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2 3. Par. Feet. 17.51 75.90	VIENN 002 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par. Feet. 23.35 81.73	A INTO r French F lireds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 its. 5. Par.Feet. 29.19 87.57	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 35.03 93.41	700. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 Par.Feet. 40.87 99.25	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 8. Par.Feet. 46.71 105.09	Par.Fee 52.5. Par.Fee 52.5. 110.92. 169.30.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20	0. Par. Feet. 0.00 5838.19 11656.4 17514.6 23352.8 Par. Feet. 0.00 58.38 116.76	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6	Par.Feet. 1168 70.06 128.44	TER OF = 5.83819 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2 3. Par. Feet. 17.51 75.90 134.28	VIENN 002 Paris o Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par. Feet. 23.35 81.73 140.12	A INTO r French F lireds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 its. 5. Par.Feet. 29.19 87.57 145.95	PARIS eet. 600. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7 6. Par.Feet. 35.03 93.41 151.79	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 Par.Feet. 40.87 99.25 157.63	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47	Par.Fee 52.5. Par.Fee 52.5. 110.92. 169.30. 227.68. 28607.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40	0. Par.Feet. 0.00 5838.19 117514.6 23352.8 Par.Feet. 0.00 58.38 116.76 175.15 233.53	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6 Par.Feet. 5.84 64.22 122.60 180.98 239.37	Par.Feet. 1167-61 7005-83 12844.0 18682.2 24520.4 Par.Feet. 11.68 70.06 128.44 186.82 245.20	TER OF = 5.83819 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2 3. Par. Feet. 17.51 75.90 134.28 192.66 251.04	VIENN 002 Paris of Hund 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par. Feet. 23.35 81.73 140.12 198.50 256.88	Far. Feet. 2919.10 8757.29 14595.5 2043.7 26271.9 87.57 145.95 204.34 262.72	PARIS eet. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7 G. Par.Feet. 35.03 93.41 151.79 210.17 268.56	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 Par.Feet. 40.87 99.25 157.63 216.01 274.39	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23	Par.Fee 52.5. Par.Fee 52.5. 110.92. 169.30. 227.68. 28607.
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40 40 50	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8 Par.Feet. 0.00 58.38 116.76 175.15 233.53	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6 Par.Feet. 5.84 64.22 122.60 180.98 239.37 297.75	Par.Feet. 1167-61 7005-83 12844.0 18682.2 24520.4 Par.Feet. 11.66 70.06 128.44 186.82 245.20 303.59	TER OF = 5.83819 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2 3. Par. Feet. 175.90 134.28 192.66 251.04 309.42	VIENN 02 Paris o Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par.Feet. 23.35 81.73 140.12 198.50 256.88 315.26	Far. Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 87.57 145.95 204.34 262.72 321.10	PARIS eet. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7 G. Par.Feet. 35.03 93.41 151.79 210.17 268.56 326.94	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 Par.Feet. 40.87 99.25 157.63 216.01 274.39 332.78	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62	Par.Fee 52.5. 110.92. 169.30. 22768. 28607. Par.Fee 52.5. 110.93. 227.63. 227.63. 344.44
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40 40 50 60	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8 0.00 58.38 16.76 175.15 233.53 291.91 350.29	172.579 SION O Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6 Par.Feet. 5.84 64.22 122.60 180.98 239.37 297.75 356.13	Par.Feet. 1167-61 17005.83 12844.0 18682.2 24520.4 Par.Feet. 11.68 70.06 128.44 186.82 245.20 303.59 361.97	TER OF = 5-83816 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2 3. Par. Feet. 17.51 75.90 134.28 192.66 251.04 309.42 367.81	VIENN 1002 Paris of 11 Muno. 400. Par. Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni. Par. Feet. 23.35 81.73 140.12 198.50 256.88 315.26 373.64	A INTO r French F lreds. 500. Par.Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 its. Par.Feet. 29.19 87.57 145.95 204.34 262.72 321.10 379.48	PARIS eet. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7 Par.Feet. 35.03 93.41 151.79 210.17 268.56 326.94 385.32	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 Par.Feet. 40.87 99.25 157.63 216.01 274.39 332.78 391.16	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62 397.00	Par.Fee 5254.3 11092. 22768. 28607. Par.Fee 52.5 110.9: 169.3 227.66 286.0 344.4 402.8
90 XXVI. Klafter of Vienna. Thousands. 0 1000 2000 3000 4000 Klafter. Tens. 0 10 20 30 40 40 50	0. Par.Feet. 0.00 5838.19 11676.4 17514.6 23352.8 Par.Feet. 0.00 58.38 116.76 175.15 233.53	172.579 SION 0 Par.Feet. 583.82 6422.01 12260.2 18098.4 23936.6 Par.Feet. 5.84 64.22 122.60 180.98 239.37 297.75	Par.Feet. 1167-61 7005-83 12844.0 18682.2 24520.4 Par.Feet. 11.66 70.06 128.44 186.82 245.20 303.59	TER OF = 5.83819 300. Par. Feet. 1751.46 7589.65 13427.8 19266.0 25101.2 3. Par. Feet. 175.90 134.28 192.66 251.04 309.42	VIENN 02 Paris o Hund 400. Par.Feet. 2335.28 8173.47 14011.7 19849.8 25688.0 Uni 4. Par.Feet. 23.35 81.73 140.12 198.50 256.88 315.26	Far. Feet. 2919.10 8757.29 14595.5 20433.7 26271.9 87.57 145.95 204.34 262.72 321.10	PARIS eet. Par.Feet. 3502.91 9341.10 15179.3 21017.5 26855.7 G. Par.Feet. 35.03 93.41 151.79 210.17 268.56 326.94	760. Par.Feet. 4086.73 9924.92 15763.1 21601.3 27439.5 Par.Feet. 40.87 99.25 157.63 216.01 274.39 332.78	800. Par.Feet. 4670.55 10508.7 16346.9 22185.1 28023.3 Par.Feet. 46.71 105.09 163.47 221.85 280.23 338.62	Par.Fee 52.5. 110.92. 169.30. 22768. 28607. Par.Fee 52.5. 110.93. 227.63. 227.63. 344.44

1 Klafter = 6.2221403 English Feet.

Klafter of Vienna.					Huno	lreds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng fee
0	0.00	622.21	1244.43	1866.64	$\boldsymbol{2488.86}$	3111.07	3733.28	4355.50	4977.71	5599.9
1000	6222.14	6844.35	7466.57	8088.78	8711.00	9333.21	9955.42	10577.6	11199.9	11822.
2000	12444.3	13066.5	13688.7	14310.9	14933.1	15555.4	16177.6	16799.8	17422.0	18044
3000	18666.4	19288.6	19910.8	20533.1	21155.3	21777.5	22399.7	23021.9	23644.1	24266
4000	24888.6	25510.8	26133.0	26755.2	27377.4	27999.6	28621.8	29244.1	29866.3	30488
Klafter.					Un	its.				
Tens.	o.	ı.	2.	3.	4.	5.	6.	7.	8.	9.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. fcet.	Eng. feet.	Eng. feet,	Eng. fee
0	0.00	6.22	12.44	18.67	24.89	31.11	37.33	43.55	49.78	56.0
10	62.22	68.44	74.67	80.89	87.11	93.33	99.55	105.78	112.00	118.2
20	124.44	130.66	136.89	143.11	149.33	155.55	161.78	168.00	174.22	180.4
30	186.66	192.89	199.11	205.33	211.55	217.77	224.00	230.22	236.44	242.6
40	248.89	255.11	261.33	267.55	273.77	280.00	286.22	292.44	298.66	304.8
50	311.11	317.33	323.55	329.77	336.00	342.22	348.44	354.66	360.88	367.1
60	373.33	379.55	385.77	391.99	398.22	404.41	410.66	416.88	423.11	429.3
70	435.55	441.77	447.99	454.22	460.44	466.66	472.88	479.10	485.33	491.5
80	497.77	503.99	510.22	516.44	522.66	528.88	535.10	541.33	547.55	553.7
00										

XXVIII. CONVERSION OF FEET OF VIENNA INTO METRES.

1 Foot of Vienna = 0.3160790 Metre.

Feet of					Hune	dreds.				
Vienna. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	900.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	31.61	63.22	94.82	126.43	158.04	189.65	221.26	252.86	284.47
1000	316.08	347.69	379.29	410.90	442.51	474.12	505.73	537.33	568.94	600.55
2000	632.16	663.77	695.37	726.98	758.59	790.20	821.81	853.41	885.02	916.63
3000	948.24	979.84	1011.45	1043.06	1074.67	1106.28	1137.88	1169.49	1201.10	1232.71
4000	1264.32	1295.92	1327.53	1359.14	1390.75	1422.36	1453.96	1485.57	1517.18	1548.79
5000	1580.40	1612.00	1643.61	1675.22	1706.83	1738.43	1770.04	1801.65	1833.26	1864.87
6000	1896.47	1928.08	1959.69	1991.30	2022.91	2054.51	2086.12	2117.73	2149.34	2180.95
7000	2212.55	2244.16	2275.77	2307.3S	2338.98	2370.59	2402.20	2433.81	2465.42	2497.0
8000	2528.63	2560.24	2591.85	2623.46	2655.06	2686.67	2718.28	2749.89	2781.50	2813.10
9000	2844.71	2876.32	2907.93	2939.53	2971.14	3002.75	3034.36	3065.97	3097.57	3129.19
10000	3160.79	3192.40	3224.01	3255.61	3287.02	3318.83	$\begin{vmatrix} 3350.44 \end{vmatrix}$	3382.05	3413.65	3445.20
11000	3 176.87	3508.48	3540.05	3571.69	3603.30	3634.91	3666.52	3698.12	3729.73	3761.3
12000	3792.95	3824.56	3856.16	3887.77	3919.38	3950.99	3982.60	4014.20	4045.81	4077.4
13000	4109.03	1140.64	4172.24	4203.85	4235.46	4267.07	4298.67	4330.28	4361.89	4393.50
14000	4425.11	4456.71	4488.32	4519.93	4551.54	4583.15	4614.75	4646.34	4677.97	4709.5
15000	4741.19	4772.79	4804.40	4836.01	4867.62	4899.22	4930.83	4962.44	4994.05	5025.6

1 Foot of Vienna = 0.9730317 Paris Foot.

Feet of					Hund	reds.				
Vienna. Fhousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900
	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. feet.	Par. fee
0	0.0	97.30	19.46	29.19	38.92	48.65	58.38	68.11	77.84	87.
1000	973.0	1070.3	1167.6	1264.9	1362.2	1459.5	1556.9	1654.2	1251.5	1848
2000	1946.1	2043.4	2140.7	3238.0	2335.3	2432.6	2530.0	2627.2	2724 5	2821
3000	2919.1	3016.4	3113.7	3211.0	3308.3	3405.6	3502.9	3600.2	3697.5	3794
4000	3892.1	3989.4	4086.7	4184.0	4281.3	4378.6	4475.9	4573.2	4670.6	4767
5000	4865.2	4962.5	5059.8	5157.1	5254.4	5351.7	5449.0	5546.3	5643.6	5740
6000	5838.2	5935.5	6032.8	6130.1	6227.4	6324.7	6422.0	6519.3	6616.6	6713
7000	6811.2	6903.5	7005.8	7103.1	7200.4	7297.7	7395.0	7492.3	7589.6	7687
8000	7784.3	7881.6	7978.9	8076.2	8173.5	8270.8	8368.1	8465.4	8562.7	8660
9000	8757.3	8854.6	8951.9	9049.2	9146.5	9243.8	9341.1	9438.4	9535.7	9633
10000	9730.3	9827.6	9924.9	10022.2	10119.5	10216.8	10314.1	10411.4	10508.7	10606
11000	10703.3	10300.7	10898.0	10995.3	11092.6	11189.9	11287.2	11384.5	11481.S	11579
12000	11676.4	11773.7	11871.0	11968.3	12065.6	12162.9	12260.2	12357.5	12454.8	12552
13000	12649.4	12746.7	12844.0	12941.3	13038.6	13135.9	13233.2	13330.5	13427.8	13525
14000	13622.4	13719.7	13817.1	13914.3	14011.7	14109.0	14206.3	14303.6	14400.9	14498
15000	14595.5	14692.8	14790.1	14887.4	14984.7	15082.0	15179.3	15276.6	15373.9	15471
16000	15568.5	15665.8	15763.1	15860.4	15957.7	16055.0	16152.3	16249.6	16346.9	16414

XXX. CONVERSION OF FEET OF VIENNA INTO ENGLISH FEET AND DECIMALS.

1 Foot of Vienna = 1.0370234 English Foot.

Feet of Vienna,					Hund	reds.				
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. fee
0	0.0	103.7	207.4	311.1	414.8	518.5				933.
1000	1037.0	1140.7	1244.4	1348.1	1451.8	1555.5	1659.2	1762.9	1866.6	1970.
2000	2074.0	2177.7	2281.5	2385.2	2488.9	2592.6	2696.3	2800.0	2903.7	3007.
3000	3111.1	3214.8	3318.5	3422.2	3525.9	3629.6	3733.3	3837.0	3940.7	4044.
4000	4148.1	4251.8	4355.5	4459.2	4562.9	4666.6	4770.3	4874.0	4977.7	5081.
5000	5185.1	5288.8	5292.5	5496.2	5599.9	5703.6	5807.3	5911.0	6014.7	6118.
6000	6222.1	6325.8	6429.5	6533.2	6636.9	6740.7	6844.4	6948.1	7051.S	7155.
7000	7259.2	7362.9	7466.6	7570.3	7674.0	7777.7	7881.4	7985.1	8088.8	8192.
8000	8296.2	8399.9	8503.6	8607.3	8711.0	8814.7	8918.4	9022.1	9125.8	9229.
9000	9333.2	9436.9	9540.6	9644.3	9748.0	9851.7	9955.4	10059.1	10162.8	10266
10000	10370.2	10473.9	10577.6	10681.3	10785.0	10888.7	10992.4	11096.2	11199.9	11303.
11000	11407.3	 11511.0	 11614.7	11718.4	11822.1	11925.8	12029.5	12133.2	12236.9	12340.
12000					12859.1				13273.9	
13000	13481.3	13585.0	13688.7	13792.4	13896.1				14310.9	
14000	14518.3	14622.0	14725.7	14829.4	14933.1				15347.9	
15000	15555.4	15659.1	15762.8	15866.5	15970.2				16385.0	
16000	16592.4	16696.1	16799.8	16903.5	17007.2	17110.9				

RHINE OR PRUSSIAN FEET

INTO DIFFERENT MEASURES OF LENGTH.

The Rhine Foot is used in Physical Geography, though not so extensively as the French or Paris Foot, in the northwestern part of Germany, Denmark, and Holland. Its legal value in the Prussian system of weights and measures is 139.13 French or Paris Lines, from which are derived the equations used in computing the following tables.

XXXI. CONVERSION OF RHINE OR PRUSSIAN FEET INTO FRENCH TOISES.

1 Rhine Foot = 0.1610301 Toise.

Rhine Feet					Hun	dreds.				
l'housands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Toises.	Toises.	Toises.	Toises.	Toises.	Tolses	Toises.	Toises.	Toises.	Toises.
0	0.00	16.10	32.21	48.31	64.41	80.52	96.62	112.72	128.82	144.9
1000	161.03	177.13	193.24	209.34	225.44	241.55	257.65	273.75	289.85	305.9
2000	322.06	338.16	354.27	370.37	386.47	402.58	418.68	434.78	450.88	466.9
3000	483.09	499.19	515.30	531.40	547.50	563.61	579.71	595.81	611.91	628.0
4000	634.12	650.22	666.33	692.43	608.53	724.64	740.74	756.84	772.94	789.0
5000	805.15	821.25	837.36	853.46	869.56	885.67	901.77	917.87	933.97	950.0
6000	966.18	982.28	998.39	1014.49	1030.59	1046.70	1062.80	1078.90	1095.00	1111.1
7000	1127.21	1143.31	1159.42	1175.52	1191.62	1207.73	1223.83	1239.93	1256.03	1272.1
8000	1288.24	1304.34	1320.45	1336.55	1352.65	1368.76	1384.86	1400.96	1417.06	1433.1
9000	1449.27					1529.79			1	

1 Rhine Foot = 0.31385350 Metre.

Rhine Feet.				RI	nine Feet.	Hundreds	3.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.
0	0.00	31.39	62.77	94.16	125.54	156.93	188.31	219.70	251.08	282.47
1000	313.85	345.24	376.62	408.01	439.39	470.78	502.17	533.55	564.94	596.32
2000	627.71	659.09	690.48	721.86	753.25	784.63	816.02	847.40	878.79	910.18
3000	941.56	972.95	1004.33	1035.72	1067.10	1098.49	1129.87	1161.26	1192.64	1224.03
4000	1255.41	1286.80	1318.18	1349.57	1380.96	1412.34	1443.73	1475.11	1506.50	1537.88
5000	1569.27	1600.65	1632.04	1663.42	1694.81	1726.19	1757.58	1788.97	1820.35	1851.74
6000	1883.12	1914.51	1945.89	1977.28	2008.66	2040.05	2071.43	2102.82	2134.20	2165.59
7000	2196.97	2228.36	2259.75	2291.13	2322.52	2353.90	2385.29	2416.67	2448.06	2479.44
8000	2510.83	2542.21	2573.60	2604.98	2636.37	2667.76	2699.14	2730.53	2761.91	2793.30
9000	2824.68	2856.07	2887.45	2918.84	2950.22	2981.61	3012.99	3044.38	3075.76	3107.15

XXXIII. OF RHINE OR PRUSSIAN FEET INTO FRENCH FEET AND DECIMALS. $1 \ {\rm Rhine} \ {\rm Foot} = 0 \ 96618056 \ {\rm French} \ {\rm Foot}$

Rhine Feet.				R	hine Feet.	Hundred	s.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Fr Feet	Fr Feet.	Fr Feet	Fr Feet.	Fr. Feet	Fr Feet.	Fr.Feet.	Fr.Feet.	Fr Feet.	Fr. Feet.
0	0.00	96.62	193.24	289.85	386.47	483.09	579.71	676.33	772.94	869.56
1000	966.18	1062.80	1159.42	1256.03	1352.65	1449.27	1545.89	1642.51	1739.13	1835.74
2000	1932.36	2028.98	2125.60	2222.22	2318.83	2415.45	2512.07	2608.69	2705.31	2801.92
3000	2898.54	2995.16	3091.78	3188.40	3285.01	3381.63	3478.25	3574.87	3671.49	3768.10
4000	3864.72	3961.34	4057.96	4154.58	4251.19	4347.81	4444.43	4541.05	4637.67	4734.28
5000	4830.90	4927.52	5024.14	5120.76	5217.38	5313.99	5410.61	5507.23	5603.85	5700.47
6000	5797.08	5893.70	5990.32	6086.94	6183.56	6280.17	6376.79	6473.41	6570.03	6666.65
7000	6763.26	6859.88	6956.50	7053.12	7149.74	7246.35	7342.97	7439.59	7536.21	7632.83
8000	7729.44	7826.06	7922.68	8019.30	8115.92	8212.53	8309.15	8405.77	8502.39	8599.01
9000	8695.63	8792.24	8888.86	8985.48	9082.10	9178.72	9275.33	9371.95	9468.57	9565.19

XXXIV. OF RHINE OR PRUSSIAN FEET INTO ENGLISH FEET AND DECIMALS. 1 Rhine Foot = 10297217 English Foot.

Dhine Feet				P	thine Feet.	Hundre	ls.			
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.
	Eng feet	Eng. feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng feet
0	0.00	102.97	205.94	308.92	411.89	514.86	617.83	720.81	823.78	926.75
1000	1029.72	1132.69	1235.67	1338.64	1441.61	1544.58	1647.55	1750.53	1853.50	1956.47
2000	2059.44	2162.42	2265.39	2368.36	2471.33	2574.30	2677.28	2780.25	2883.22	2986.19
3000	3089.17	3192.14	3295.11	3398.08	3501.05	3604.03	3707.00	3809.97	3912.94	4015.92
4000	4118.89	4221.86	4324.83	4427.80	4530.78	4633.75	4736.72	4839.69	4942.66	5045.64
5000	5148.61	5251.58	5354.55	5457.53	5560.50	5663.47	5766.44	5869.41	5972.39	6075.36
6000	6178.33	6281.30	6384.28	6487.25	6590.22	6693.19	6796.16	6899.14	7002.11	7105.08
7000	7208.05	7311.02	7414.00	7516.97	7619.94	7722.91	7825.89	7928.86	8031.83	8134.80
8000	8237.77	8340.75	8443.72	8546.69	8649.66	8752.64	8855.61	8958.58	9061.55	9164.52
9000	9267.50	9370.47	9473.44	9576.41	9679.38	9782.36	9885.33	9988.30	10091.3	10194.2

SPANISH OR MEXICAN VARAS AND FEET

INTO DIFFERENT MEASURES OF LENGTH.

XXXV. CONVERSION OF SPANISH OR MEXICAN VARAS INTO METRES.

1 Vara = 0.847965 Metre.

Varas.		$\operatorname{Hundreds}.$													
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.					
	Metres.	Metres.	Metres	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.	Metres.					
0	0.00	84.80	169.59	254.39	339.19	423.98	508.78	593.58	678.37	763.1					
1000	847.96	932.76	1017.56	1102.35	1187.15	1271.95	1356.74	1441.54	1526.34	1611.1					
2000	1695.93	1780.73	1865.52	1950.32	2035.12	2119.91	2204.71	2289.51	2374.30	2459.10					
3000	2543.89	2628.69	2713.49	2798.28	2883.08	2967.88	3052.67	3137.47	3222.27	3307.0					
4000	3391.86	3476.66	3561.45	3646.25	3731.05	3815.84	3900.64	3985.44	4070.23	4155.0					
5000	4239.82	4324.62	4409.42	4494.21	4579.01	4663.81	4748.60	4833.40	4918.20	5002.9					
6000	5087.79	5172.59	5257.38	5342.18	5426.98	5511.77	5596.57	5681.37	5766.16	5850.9					
7000	5935.75	6020.55	6105.35	6190.14	6274.94	6359.74	6444.53	6529.33	6614.13	6698.9					
8000	6783.72	6868.52	6953.31	7038.11	7122.91	7207.70	7292.50	7377.30	7462.09	7546.8					
9000	7631.68	7716.48	7801.28	7886.07	7970.87	8055.67	8140.46	8225.26	8310.06	8391.8					

XXXVI. OF SPANISH OR MEXICAN VARAS INTO ENGLISH FEET AND DECIMALS.

1 Vara = 2.78209 English Feet.

Varas.		Hundreds.														
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.						
	Eng. feet.	Eng. feet	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet.	Eng. feet,	Eng. feet.						
0	0.0		556.4		_		1669.3	1947.5	2225.7	2503.9						
1000	2782.1	3060.3	3338.5	3616.7	3894.9	4173.1	4451.3	4729.6	5007.8	5286.0						
2000	5564.2	5842.4	6120.6	6398.8	6677.0	6955.2	7233.4	7511.6	7789.9	8068.1						
3000	8346 3	8624.5	8902.7	9180.9	9459.1	9737.3	10015.5	10293.7	10571.9	10850.2						
4000	11128.4	11406.6	11684.8	11963.0	12241.2	12519.4	12797.6	13075.8	13354.0	13632.2						
5000	13910.4	14188.7	14466.9	14745.1	15023.3	15301.5	15579.7	15857.9	16136.1	16414.3						
6000	16692.5	16970.7	17249.0	17527.2	17805.4	18083.6	18361.S	18640.0	18918.2	19196.4						
7000	19474.6	19752.8	20031.0	20309.3	20587.5	20865.7	21143.9	21422.1	21700.3	21978.5						
8000	22256.7	22534.9	22813.1	23091.3	23369.6	23647.8	23926.0	24204.2	24482.4	24760.6						
9000	25038.8	25317.0	25595.2	25873.4	26151.6	26429.9	26708.1	26986.3	27164.5	27442.7						

XXXVII. CONVERSION OF CASTILIAN FEET INTO METRES.

1 Castilian Foot = 0.282655 Metre.

Castilian	Hundreds.												
Feet. Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.			
	Metres.	Metres.	Metres.	Metres.	Metres.	Metres,	Metres.	Metres.	Metres.	Metres.			
0	0.00	28.27	56.53	84.80	113.06	141.33	169.59		226.12	254.39			
1000	282.65	310.92	339.19	367.45	395.72	423.98	452.25	480.51	508.78	537.04			
2000	565.31	593.58	621.84	650.11	678.37	706.64	734.90	763.17	791.43	819.70			
3000	847.96	876.23	904.50	932.76	961.03	989.29	1017.56	1045.82	1074.09	1102.35			
4000	1130.62	1158.89	1187.15	1215.42	1243.68	1271.95	1300.21	1328.48	1356.74	1385.01			
5000	1413.27	1441.54	1469.81	1498.07	1526.34	1554.60	1582.87	1611.13	1639.40	1667.66			
6000	1695.93	1724.20	1752.46	1780.73	1808.99	1837.26	1865.52	1893.79	1922.05	1950.32			
7000	1978.58	2006.85	2035.12	2063.38	2091.65	2119.91	2148.18	2176.44	2204.71	2232.97			
8000	2261.24	2289.51	2317.77	2346.04	2374.30	2402.57	2430.83	2459.10	2487.36	2515.63			
9000	2543.89	2572.16	2600.43	2628.69	2656.96	2685.22	2713.49	2741.75	2770.02	2798.28			

XXXVIII. CONVERSION OF CASTILIAN FEET 1NTO PARIS OR FRENCH FEET. 1 Castilian Foot = 0 870138 Paris Foot.

Castilian Feet.	Hundreds.											
Thousands.	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.		
	Par. Feet.	Par. Feet	Par Feet.	Par Feet.	Par Feet.	Par. Feet.	Par. Feet.	Par Feet.	Par.Feet.	Par.Feet.		
0	0.00	87.01	174.03	261.04	348.06	435.07	522.08	609.10	696.11	783.12		
1000	870.14	957.15	1044.17	1131.18	1218.19	1305.21	1392.22	1479.23	1566.25	1653.26		
2000	1740.28	1827.29	1914.30	2001.32	2088.33	2175.35	2262.36	2349.37	2436.39	2523.40		
3000	2610.41	2697.43	2784.44	2871.46	2958.47	3045.48	3132.50	3219.51	3306.52	3393.54		
4000	3480.55	3567.57	3654.58	3741.59	3828.61	3915.62	4002.64	4089.65	4176.66	4263.68		
5000	4350.69	4437.70	4524.72	4611.73	4698.75	4785.76	4872.77	4959.79	5046.80	5133.S2		
6000	5220.83	5307.84	5394.86	5481.87	5568.88	5655.90	5742.91	5829.93	5916.94	6003.95		
7000	6090.97	6177.98	6265.00	6352.01	6439.02	6526.04	6613.05	6700.06	6787.08	6874.09		
8000	6961.11	7048.12	7135.13	7222.15	7309.16	7396.17	7483.19	7570.20	7657.22	7744.23		
9000	7831.24	7918.26	8005.27	8092.29	8179.30	8266.31	8353.33	8440.34	8527.35	8614.37		

XXXIX. CONVERSION OF CASTILIAN FEET INTO AMERICAN FEET. 1 Castilian Foot = 0.927309 American Foot.

Castilian Feet.		Hundreds.												
Thousands	0.	100.	200.	300.	400.	500.	600.	700.	800.	900.				
	Am Feet	Am Feet	Am. Feet.	Am Feet.	Am. Feet.	Am Feet.	Am.Feet	Am Feet	Am Feet	Am. Feet				
0 1	0.00	92.73	185.46	278.19	370.92	463.65	556.39	649.12	741.85	834.58				
1000	927.31	1020.04	1112.77	1205.50	1298.23	1390.96	1483.69	1576.43	1669.16	1761.89				
2000	1854.62	1947.35	2040.08	2132.81	2225.54	2318.27	2411.00	2503.74	2596.47	2689.20				
3000	2781.93	2874.66	2967.39	3060.12	3152.85	3245.58	3338.31	3431.04	3523.78	3616.51				
4000	3709.24	3801.97	3894.70	3987.43	4080.16	4172.89	4265.62	4358.35	4451.08	4543.82				
5000	4636.55	4729.28	4822.01	4914.74	5007.47	5100.20	5192.93	5285.66	5378.39	5471.12				
6000	5563.86	5656.59	5749.32	5842.05	5934.78	6027.51	6120.24	6212.97	6305.70	6398.43				
7000	6491.17	6583.90	6676.63	6769.36	6862.09	6954.82	7047.55	7140.28	7233.01	7325.74				
8000	7418.47	7511.21	7603.94	7696.67	7789.40	7882.13	7974.86	8067.59	8160.32	8253.05				
9000	8345.78	8438.51	\$531.25	8623.98	8716.71	8809.44	8902.17	8994.90	9087.63	9180.36				

The length of the Spanish Vara, and of the Spanish or Castilian foot, used in the late Spanish Colonies of Mexico and South America, owing, no doubt, to the imperfection of the local standards, shows considerable variations from the value on which the preceding tables are based.

A careful comparison of the standard Vara, brought from Mexico by Major Turnbull, and deposited in the United States Office of Weights and Measures, (see above p. 113,) gave for its length 32.9682 American inches = 2.7473333 American feet = 2.7474928 English feet = 0.8374206 metre.

From a series of altitudes published in Mexico, by Cortina, in Castilian feet, and by Orbegozo in metres and Castilian feet, Jul. Schmidt derives the following value of the Vara and of the Castilian foot, used by these authors (see Petermann's *Mittheil*. 1857, p. 371): One Vara = 2.573296 Paris feet = 0.8358065 metre; and one Castilian foot = 0.857764 Paris foot = 0.91417 English foot.

According to Colonel J. Ondarza, one of the authors of the new official Map of Bolivia, the Bolivian government has declared the legal value of the Spanish Vara to be in the ratio of 100 metres = 118 Varas = 354 Spanish feet, which value has been adopted by him in publishing his measured altitudes.

XXXVIII' MEXICO. — CONVERSION OF CASTILIAN FEET INTO METRES, PARIS AND ENGLISH FEET.

Mexican or	Accordin	ng to Turnbull's	Standara.	According to Schmidt, from Cortina.					
Castilian Feet.	Metres.	Paris Feet.	English Feet.	Metres.	Paris Feet.	English Feet			
1000	279.14	859.30	915.83	278.64	857.76	914.17			
2000	558.28	1718.60	1831.66	557.27	1715.53	1828.34			
3000	837.42	2577.89	2747.49	\$35.91	2573.29	2742.51			
4000	1116.56	3437.19	3663.32	1114.54	3431.06	3656.68			
5000	1395.70	4296.49	4579.15	1393.18	4288.82	4570.85			
6000	1674.84	5155.79	5494.99	1671.81	5146.58	5485.02			
7000	1953.98	6015.08	6410.82	1950.45	6004.35	6399.19			
8000	2233.12	6874.38	7326.65	2229.08	6862.11	7313.36			
9000	2512.26	7733.68	8242.48	2507.72	7719.88	8227.53			

XXXIX'. BOLIVIA. — CONVERSION OF SPANISH VARA AND SPANISH FEET-1 Spanish foot = 0 2824859 metre = 0.8696171 Paris foot, = 0.9268078 English foot.

Bolivian or banish Feet.	Metres.	Paris Feet.	English Feet.	Metres.	Spanish Varas.	Spanish Feet.
1000	282.49	869.62	926.81	1000	1180	. 3540
2000	564.97	1739.23	1853.61	2000	2360	7080
3000	847.46	2608.85	2780.42	3000	3540	10620
4000	1129.94	3478.47	3707.23	4000	4720	14160
5000	1412.43	4348.09	4634.04	5000	5900	17700
6000	1694.92	5217.70	5560.85	6000	7080	21240
7000	1977.40	6087.32	6487.65	7000	8260	24780
8000	2259.89	6956.94	7414.46	8000	9440	28320
9000	2542.37	7826.55	8341.27	9000	10620	31860

FRACTIONAL PARTS OF A TOISE AND OF A FOOT

INTO EACH OTHER.

XL. CONVERSION OF INCHES INTO DUODECIMAL LINES.

I Inch = 12 Lines.

Inches.		Inches. Units.												
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.	Lines.				
0	0	12	24	36	48	60	72	84	96	108				
10	120	132	144	156	168	180	192	204	216	228				
20	240	252	264	276	288	300	312	324	336	348				
30	360	372	384	396	408	420	432	444	456	468				
40	480	492	504	516	528	540	552	564	576	588				
50	600	612	624	636	648	660	672	684	696	708				
60	720	732	744	756	768	780	792	804	816	828				
70	840	852	864	876	888	900	912	924	936	948				
80	960	972	984	996	1008	1020	1032	1044	1056	1068				
90	1080	1092	1104	1116	1128	1140	1152	1164	1176	1188				
100	1200	1212	1224	1236	1248	1260	1272	1284	1296	1308				

XLI. CONVERSION OF DECIMALS OF A TOISE INTO FEET AND INCHES.

1 Toise = 6 Feet = 72 Inches = 864 Lines.

Toises.	Hundredths of a Toise.												
Tens.	0.	1.	2.	3. 4.	5.	6.	7.	8. 9.					
	ft in lin	ft. in. lin.	ft. in. lin ft. in	lin. ft. in lin.	ft. in. lin.	ft. in. lin. ft.	in. lin. ft. in	. lin. ft. in, lin					
0.0	0.0.0,00	0. 0. 8,64	0. 1. 5,28 0. 2.	1,92 0. 2.10,56	0. 3.7,20	0. 4. 3,84 0.	5. 0,48 0.5	. 9,12 0. 6. 5,76					
0.1	0.7.2,40	0. 7.11,04	0. 8. 7,68 0. 9.	4,32 0.10. 0,96	0.10.9,60	0.11. 6,24 1.	0. 2,88 1. 0	.11,52 1. 1. 8,16					
0.2	1.2.4,80	1. 3. 1,44	1. 3.10,08 1. 4.	6,72 1. 5. 3,36	1. 6.0,00	1. 6. 8,64 1.	7. 5,28 1. 8	. 1,92 1. 8.10,56					
0.3	1.9.7,20	1.10. 3,84	1.11. 0,48 1.11.	9,12 2. 0. 5,76	2. 1.2,40	2. 1.11,04 2.	2. 7,68 2. 3	. 4,32 2. 4. 0,96					
0.4								6,72 2.11. 3,36					
0.5								. 9,12 3. 6. 5,76					
0.6								.11,52 4. 1. 8,16					
0.7	4.2.4,80	4. 3. 1,44	4. 3.10,08 4. 4.	6,72 4. 5. 3,36	4. 6.0,00	4. 6. 8,64 4.	7. 5,28 4. 8	. 1,92 4. 8.10,56					
0.8								. 4,32 5. 4. 0,96					
0.9								. 6,72 5.11. 3,36					

Feet.		Hundredths of a Foot.												
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches				
0.0	0.00	0.12	0.24	0.36	0.48	0.60	0.72	0.84	0.96	1.08				
0.1	1.20	1.32	1.44	1.56	1.68	1.80	1.92	2.04	2.16	2.28				
0.2	2.40	2.52	2.64	2.76	2.88	3.00	3.12	3.24	3.36	3.48				
0.3	3.60	3.72	3.84	3.96	4.08	4.20	4.32	4.44	4.56	4.68				
0.4	4.80	4.92	5.04	5.16	5.28	5.40	5.52	5.64	5.76	5.88				
0.5	6.00	6.12	6.24	6.36	6.48	6.60	6.72	6.84	6.96	7.08				
0.6	7.20	7.32	7.44	7.56	7.68	7.80	7.92	8.04	8.16	8.28				
0.7	8.40	8.52	8.64	8.76	8.88	9.00	9.12	9.24	9.36	9.48				
0.8	9.60	9.72	9.84	9.96	10.08	10.20	10.32	10.44	10.56	10.68				
0.9	10.80	10.92	11.04	11.16	11.28	11.40	11.52	11.64	11.76	11.88				

XLIII. CONVERSION OF DECIMALS OF A FOOT INTO INCHES AND DUODECIMAL LINES.

Feet.		Hundredths of a Foot.													
Tens.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.					
	In. Line.	In. Line.	In. Line.	In. Line.	In. Line.	In Line	In. Line	In. Line.	In. Line	In. Line.					
0.0	0.0,00	0. 1,44	0. 2,88	0. 4,32	0. 5,76	0.7,20	0. 8,64	0.10,08	0.11,52	1. 0,96					
0.1	1.2,40	1. 3,84	1. 5,28	1. 6,72	1. 8,16	1.9,60	1.11,04	2. 0,48	2. 1,92	2. 3,36					
0.2	2.4,80	2. 6,24	2. 7,68	2. 9,12	2.10,56	3.0,00	3. 1,44	3. 2,88	3. 4,32	3. 5,76					
0.3	3.7,20	3. 8,64	3.10,08	3.11,52	4. 0,96	4.2,40	4. 3,84	4. 5,28	4. 6,72	4. 8,16					
0.4	4 9,60	4.11,04	5. 0,48	5. 1,92	5. 3,36	5.4,80	5. 6,24	5. 7,68	5. 9,12	5.10,56					
0.5	6.0,00	6. 1,44	6. 2,88	6. 4,32	6. 5,76	6.7,20	6. 8,64	6.10,08	6.11,52	7. 0,96					
0.6	7.2,40	7. 3,84	7. 5,28	7. 6,72	7. 8,16	7.9,60	7.11,04	8. 0,48	8. 1,92	8. 3,36					
0.7	8.4,80	8. 6,24	8. 7,68	8. 9,12	8.10,56	9.0,00	9. 1,44	9. 2,88	9. 4,32	9. 5,76					
0.8	9.7,20	9. 8,64	9.10,08	9.11,52	10. 0,96	10.2,40	10. 3,84	10. 5,28	10. 6,72	10. 8,16					
0.9	10.9,60	10.11,04	11. 0,48	11. 1,92	11. 3,36	11.4,80	11. 6,24	11. 7,68	11. 9,12	11.10,56					

XLIV. CONVERSION OF INCHES AND DUODECIMAL LINES INTO DECIMALS OF A FOOT.

1 Inch = 0.08333 of a Foot. 1 Line = 0.006944 of a Foot.

	Lines.											
Inches.	0.	1.	2.	3.	4.	5.	6.	7.	8.	9.	10.	11.
	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot.	Foot	Foot.
0	0.0000	0.0069	0.0139	0.0208	0.0278	0.0347	0.0417	0.0486	0.0556	0.0625	0.0694	0.0764
1	0.0833	0.0903	0.0972	0.1042	0.1111	0.1181	0.1250	0.1319	0.1389	0.1458	0.1528	0.1597
2	0.1667	0.1736	0.1806	0.1875	0.1944	0.2014	0.2083	0.2153	0.2222	0.2292	0.2361	0.2431
3	0.2500	0.2569	0.2639	0.2708	0.2778	0.2847	0.2917	0.2986	0.3056	0.3125	0.3194	0.3264
-4	0.3333	0.3403	0.3472	0.3542	0.3611	0.3681	0.3750	0.3819	0.3889	0.3958	0.4028	0.4097
5	0.4167	0.4236	0.4306	0.4375	0.4444	0.4514	0.4583	0.4653	0.4722	0.4792	0.4861	0.4931
6	0.5000	0.5069	0.5139	0.5208	0.5278	0.5347	0.5417	0.5486	0.5556	0.5625	0.5694	0.5764
7	0.5833	0.5903	0.5972	0.6042	0.6111	0.6181	0.6250	0.6319	0.6389	0.6458	0.6528	0.6597
8	0.6667	0.6736	0.6806	0.6875	0.6944	0.7014	0.7083	0.7153	0.7222	0.7292	0.7361	0.7431
9	0.7500	0.7569	0.7639	0.7708	0.7778	0.7847	0.7917	0.7986	0.8056	0.8125	0.8194	0.8264
10	0.8333	0.8403	0.8472	0.8542	0.8611	0.8681	0.8750	0.8819	0.8889	0.8958	0.9028	0.9097
11	0.9167	0.9236	0.9306	0.9375	0.9444	0.9514	0.9583	0.9653	0.9722	0.9792	0.9861	0.9931

METEOROLOGICAL TABLES.

V.

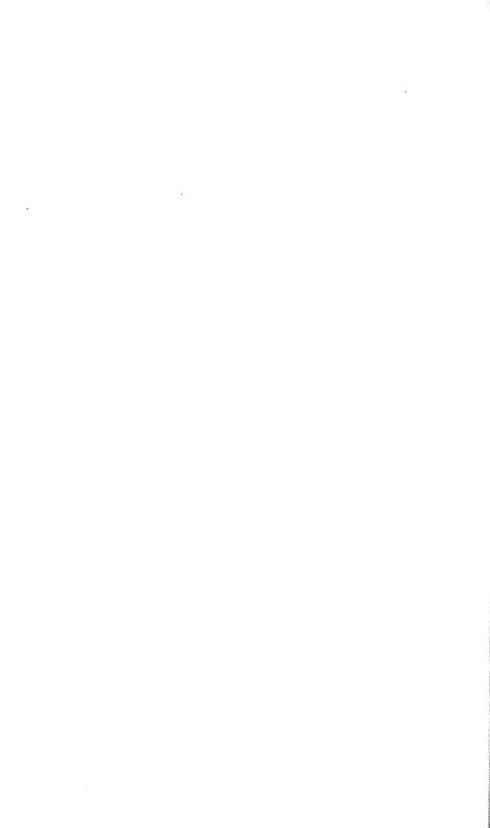
METEOROLOGICAL CORRECTIONS,

OR

TABLES

FOR CORRECTING SERIES OF OBSERVATIONS FOR THE PERIODIC AND NON-PERIODIC VARIATIONS.

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CONTENTS.

[The figures refer to the folio at the bottom of the page.—The letters near them mean, D. = calculated by Dove; Gl. = Glaisher; G. = Guyot; L. = Lefroy. For the letters before the latitudes, see page 12.]

Temperature.

Hourly Corrections for Periodic Variations.

NORTH AMERICA.

	Station.		Latitude.	Scale.	1	Page.			
TABLE I.	Washington, District Columbia,	B 1.	38 54 N.	Reau.	D.	15			
" II.	Philadelphia, Girard College,	A/3.	39 58 N.	Reau.	D.	15			
" III.	Philadelphia, Girard College,	A'3.	39 58 N.	Fahr.	G.	16			
" IV.	Frankfort Arsenal, Penn.,	C.	39 57 N.	Reau.	D.	17			
« V.	Frankfort Arsenal, Penn.,	C.	39 57 N.	Fahr.	D.	18			
" VI.	Toronto, Canada West,	В.	43 40 N.	Fahr.	D.	19			
" VII.	Toronto, Canada West,	В.	43 40 N.	Reau.	D.	20			
" VIII.	Toronto, Canada West,	A'6.	43 40 N.	Fahr.	L.	21			
" IX.	Toronto, Canada West,	A'6.	43 40 N.	Reau.	D.	22			
" X.	Montreal, Canada East,	A'1.	45 30 N.	Fahr.	G.	22			
" XI.	Sitka, Russian America,	A'5.	57 3 N.	Reau.	D.	23			
" XII.	Boothia Felix, Arctic America,	A.	69 59 N.	Reau.	D.	24			
" XIII.	Lake Athabasca, Arctic America,	C.	59 N.	Fahr.	L.	25			
" XIV.	Melville Island, Arctic America,	C.	74 47 N.	Reau.	D.	25			
" XV.	Hecla Cove, Spitzbergen,	C.	79 55 N.	Reau.	D.	25			
	Appendix.								
· · V'.	Amherst College, Mass.,	A'1.	42 22 N.	Fahr.	D.	28			
SOUTH AMERICA.									
" XVI.	Rio Janeiro, Brazil,	C.	22 54 S.	Fahr.	D.	26			
" XVII.	Rio Janeiro, Brazil,	C.	22 54 S.	Reau.	D.	27			

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	ASIA.		Latitude.	Scale.	1	Page.
Table XVIII.	Trevandrum, India,	Α.	8 31 N.	Fahr.	D.	31
" XIX.	Trevandrum, India,	Α.	8 31 N.	Reau.	D.	32
, XX.	Madras, India,	A.	13 4 N.	Fahr.	D.	33
" XXI.	Madras, India,	A.	13 4 N.	Reau.	D.	34
" XXII.	Bombay, India,	A.	18 56 N.	Fahr.	D.	35
" XXIII.	Bombay, India,	A.	18 56 N.	Reau.	D.	36
" XXIV.	Madras, India,	A'5.	13 4 N.	Reau.	D.	37
" XXV.	Bombay, India,	A'4.	18 56 N.	Reau.	D.	37
" XXVI.	Calcutta, India,	A'2.	22 33 N.	Reau.	D.	38
" XXVII.	Tiflis, Georgia,	A'4.	41 41 N.	Reau.	D.	39
" XXVIII.	Peking, China,	A'4.	39 54 N.	Reau.	D.	39
" XXIX.	Nertchinsk, Siberia,	A'6.	51 18 N.	Reau.	D.	40
" XXX.	Nertchinsk, Siberia,	A.	51 18 N.	Reau.	D.	41
" XXXI.	Barnaul, Siberia,	A.	53 20 N.	Fahr.	D.	42
" XXXII.	Barnaul, Siberia,	A.	53 20 N.	Reau.	D.	43
" XXXIII.	Barnaul, Siberia,	A'6.	53 20 N.	Reau.	D.	44
	EUROPE.					
		~		-	-	
" XXXIV.	Rome, Italy,	C.	41 54 N.	Reau.	D.	47
" XXXV.	Padua, Italy,	C.	45 24 N.	Reau.	D.	48
" XXXVI.	Geneva, Switzerland,		46 12 N.	Reau.	D.	49
" XXXVII.	Geneva, Switzerland,	C'4.	46 12 N.	Reau.	D.	49
" XXXVIII.	St. Bernard, Switzerland,		45 52 N.	Reau.	D.	50
" XXXIX.	St. Bernard, Switzerland,	C'4.	45 52 N.	Reau.	D.	50
" XL.	Kremsmünster, Austria,	C.	48 3 N.	Reau.	D.	51
" XLI.	Salzburg, Austria,	A'6.	47 48 N.	Reau.	D.	52
" XLII.	Munich, Bavaria,	A'6.	48 9 N.	Reau.	D.	52
" XLIII.	Prague, Bohemia,	A'10.		Reau.	D.	53
" XLIV.	Prague, Bohemia,	A.	50 5 N.	Reau.	D.	54
" XLV.	Plymouth, England,	C.	50 22 N.	Fahr.	D.	55 56
ADVI.	Plymouth, England,	C.	50 22 N. 50 51 N.	Reau. Reau.	D. D.	57
MB v III.	Brussels, Belgium,	В. В'.	50 51 N.	Reau.	D. D.	58
2X 12 V 1111.	Brussels, Belgium,	B'3.	50 51 N. 53 36 N.	Reau.	р. D.	58
" XLIX.	Schwerin, Germany,	Б з. С.	51 13 N.	Reau.	D.	59
" L. " LI.	Mühlhausen, Prussia, Utrecht, Holland,	A'2.	51 15 N. 52 5 N.	Reau.	D.	60
" LII.	Greenwich, England,	B'7.	51 29 N.	Reau.	D.	60
" LIII.	Greenwich, England,	В.	51 29 N.	Reau.	D.	61
" LIV.	Greenwich, England,	В.	51 29 N.	Fahr.	Gl.	62
" LV.	_	C.	51 30 N.	Reau.	D.	63
" LVI.		С.	51 32 N.	Reau.	D.	64
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		Station.		Latitude.	Scale.		Page.
TABLE	LVII.	Berlin, Prussia,	A.	52 30 N.	Reau.	D.	65
"	LVIII.	Salzuflen, Germany,	A.	52 5 N.	Reau.	D.	66
"	LIX.	Stettin, Germany,	A′.	53 25 N.	Reau.	D.	67
"	LX.	Apenrade, Sleswick,	C.	55 3 N.	Reau.	D.	68
"	LXI.	Leith, Scotland,	A.	55 59 N.	Fahr.	D.	69
"	· LXII.	Leith, Scotland,	A.	55 59 N.	Reau.	D.	70
"	LXIII.	Makerstoun, Scotland,	A′3.	55 36 N.	Reau.	D.	71
66	LXIV.	Dublin, Ireland,	B/4.	53 23 N.	Reau.	D.	71
"	LXV.	Catharinenburg, Russia,	A.	56 50 N.	Reau.	D.	72
"	LXVI.	Catharinenburg, Russia,	A'6.	56 50 N.	Reau.	D.	73
"	LXVII.	St. Petersburg, Russia,	A'10.	59 56 N.	Reau.	D.	73
"	LXVIII.	Helsingfors, Finland,	A/3.	60 10 N.	Reau.	D.	74
"	LXIX.	St. Petersburg, Russia,	A.	59 56 N.	Reau.	D.	75
"	LXX.	Helsingfors, Finland,	C.	60 10 N.	Reau.	D.	76
"	LXXI.	Christiania, Norway,	C.	59 55 N.	Reau.	D.	77
"	LXXII.	Drontheim, Norway,	C.	63 26 N.	Reau.	D.	78
"	LXXIII.	Strait of Kara, Russia,	A	70 37 N.	Reau.	D.	79
"	LXXIV.	Matoschkin Schar, Novaia Zemlia,	Α.	73 N.	Reau.	D.	80
"	LXXV.	Bossekop, Norway,	C.	69 58 N.	Reau.	D.	81
"	LXXV'.	Bossekop, Norway,	C.	69 58 N.	Centig.	G.	81
		AFRICA AND AUSTRA	LIA.				
"	LXXVI.	St. Helena, Africa,	A'5.	15 55 S.	Reau.	D.	85
66	LXXVII.	Cape of Good Hope, Africa,	A'5.	33 56 S.	Reau.	D.	85
"	LXXVIII.	Hobarton, Tasmania,	A's.	42 53 S.	Reau.	D.	86
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		Monthly Corrections for Non-period	odic V	ariations.			
		Station.		Latitude.	Scale.		Page.
TABL	E LXXIX.	Madras, India,		13 4 N.	Reau.	D.	90
44	LXXX.	Palermo, Sicily,		38 7 N.	Reau.	D.	91
"	LXXXI.	Milan, Italy,		45 28 N.	Reau.	D.	92
"	LXXXII.	Geneva, Switzerland,		46 12 N.	Reau.	D.	94
"	LXXXIII.	Vienna, South Germany,		48 13 N.	Reau.	D.	96
66	LXXXIV.	Ratisbon, South Germany,		49 1 N.	Reau.	D.	97
"	LXXXV.	Stuttgard, South Germany,		48 46 N.	Reau.	D.	99
"	LXXXVI.	Carlsruhe, South Germany		49 1 N.	Reau.	D.	100
"	LXXXVII.	Berlin, North Germany,		52 30 N.	Reau.	D.	102
" I	ZXXXVIII.	Copenhagen, Denmark,		55 41 N.	Reau.	D.	105
"	LXXXIX.	Paris, France,		48 50 N.	Reau.	D.	107
"	XC.	Zwanenburg, Holland,		52 23 N.	Reau.	D.	108
44	XCI.	London, England,		51 30 N.	Reau.	D.	110
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		Station.	Latitude.	Scale.		Page.
TABL	E XCII.	Kinfauns Castle, Scotland,	56 24 N.	Reau.	D.	112
"	XCIII.	Torneå, Finland,	65 50 N.	Reau.	D.	112
"	XCIV.	Albany, N. Y., North America,	42 39 N.	Reau.	D.	113
"	XCV.	Salem, Mass., North America,	42 31 N.	Reau.	D.	114
"	XCVI.	Reikiavik, Iceland,	64 8 N.	Reau.	D.	115
"	XCVII.	Godthaab, Greenland,	64 10 N.	Reau.	D.	115
		Force of Vapor and Relative	Humidity.			
		Hourly Corrections for Periodic	Variations.			

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" XCVIII. Greenwich, England, Force of Vapor, by Glaisher,

XCIX. Greenwich, England, Relative Humidity, by Glaisher,

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METEOROLOGICAL CORRECTIONS.

ONE of the prominent objects of a prolonged series of meteorological observations is to determine the mean condition of the atmosphere, during a given interval of time, such as a day, a month, or a year, as to its temperature, moisture, and barometric pressure. In order to furnish the true means of these elements, free from the periodic changes which depend upon the daily course of the sun and upon the seasons, the observations ought to be made at equal intervals of time, and be so often repeated as actually to represent the sum of the variations which took place during the stated time. It is generally admitted that observations taken at every one of the twenty-four hours of the day give means which do not sensibly differ from the means which would be obtained from a still larger number of observations during the same time; so that means derived from hourly observations may be considered as the true daily, monthly, and annual means of the year in which the observations were taken.

However, as the means of a given month, or year, will generally be found somewhat to differ from those of another year, at the same place, from causes which are not of a periodic nature, it is obvious that the absolute means can only be derived from the means of a series of years, in which the differences arising from these non-periodic variations may be considered as sufficiently balancing each other.

Hourly observations can be expected only from a very few stations, favored with peculiar arrangements for the purpose. By far the larger number of observers must necessarily confine themselves to three or four observations a day. The means, therefore, deduced from such a set of observations, generally differ from the true means which would be given by hourly observations, by a quantity which varies with the hours selected for the observations. If that quantity, however, is known by having been previously determined for every hour, or set of hours, by a long series

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METEOROLOGICAL CORRECTIONS.

of hourly observations taken at some station in a similar climatic situation, it is evident that, whatever be the hours at which observations are taken, the means derived from them can always be reduced to the true means by correcting them for that difference.

The following tables furnish such corrections, both for periodic and non-periodic variations of temperature, and for stations situated in various latitudes. They give the quantities which must be added to, or subtracted from, the hourly means, in order to obtain the true means of the day, of the month, and of the year.

Two tables of the same description, for moisture, which may be considered as specimens of the kind, close the set.

Two other tables, for correcting the mean barometric pressures, are found at the end of the Hypsometrical Tables, pp. 92, 93.

CORRECTIONS FOR TEMPERATURE.

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY, OF THE DAY, OF THE MONTH, AND OF THE YEAR.



HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

CORRECTIONS TO BE APPLIED TO THE MEANS OF THE HOURS OF OBSERVATION, OR SETS OF HOURS, IN ORDER TO OBTAIN THE TRUE MEAN TEMPERATURES

OF THE RESPECTIVE DAYS, MONTHS, AND OF THE YEAR.

The following set contains all the tables for correcting the means of observations on atmospheric temperature for the effect of diurnal variation which have been published by Dove, together with a few others of the same description. Dove's tables are found in two papers, published in the Memoirs of the Royal Academy of Berlin for 1846 and for 1856, and in the first Report on the Observations of the Meteorological Institute of Prussia, Berlin, 1851.

In the first paper are twenty-nine tables, in Reaumur's scale, nine of which have been republished, in Fahrenheit's scale, in the *Proceedings of the British Association* for 1847, and will also be found below. In that series the corrections have been formed by finding first the differences between the hourly and the true means, and then computing the observations by Bessel's formula, in order to eliminate the accidental irregularities due to the shortness of the period during which the observations were taken. Calling x the horary angle reckoned from noon, Bessel's formula is

$$tx = u + u' \sin(x + U') + u'' \sin(2x + U'') + u''' \sin(3x + U''').$$

The stations at which hourly observations were made are Trevandrum, Madras, Bombay, Salzufien, Prague, St. Petersburg, Catharinenburg, Barnaul, Nertchinsk, Matoschkin-Schar, Strait of Kara, and Boothia Felix. Bi-hourly observations were taken at Brussels, Greenwich, and Toronto; in all others the night observations are wanting, and were obtained by interpolation. Moreover, in several stations the number of observations was small, at Madras even only thirty-six days. The tables of that series may be readily distinguished from those belonging to the same stations in the second, by their containing the corrections for several sets of hours, which are not found in the tables of the other.

In Dove's second series, and in all other tables, the corrections given are simply the differences, with reverse signs, between the hourly and the true means, excepting, however, the stations of Toronto, in which the corrections were computed, by Bessel's formula, by Colonel Sabine; of Prague, by Jelineck; of Salzburg, and those of Geneva and St. Bernard, by Plantamour.

The observations from which these tables are derived were made hourly at Hobarton during 8 years; at the Cape of Good Hope, for $5\frac{1}{4}$ years; St. Helena, 5 years; Madras, 5 years; Bombay, 4 years; Calcutta, $1\frac{1}{2}$ years; Toronto, 6 years; Philadelphia, 3 years; Makerstoun, 3 years; Utrecht, $1\frac{2}{4}$ years; Prague, $10\frac{1}{2}$ years; Munich, 7 years; Salzburg, 6 years; St. Petersburg, 10 years; Catherinenburg, 6 years; Barnaul, 5 years; Tiflis, 4 years; Nertchinsk, 6 years; Peking, 4 years; Sitka, 5 years. In the following stations the observations were bi-hourly:— Washington, for $1\frac{1}{2}$ years; Greenwich, 7 years; Dublin, 4 years; Brussels, 9 years; Geneva and St. Bernard, 4 years; Schwerin, 3 years.

The observations made in England, and in her colonies, are found in the various government publications. Those of the Russian stations are taken from the Annuaire Météorologique et Magnétique des Ingénieurs des Mines, and in the Annales de

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l'Observatoire Physique Central de Russie. The observations made at Prague, Munich, Geneva, with those at St. Bernard, Makerstoun, Greenwich, Brussels, and Washington, were published by their respective Observatories; those of Utrecht, by Buys-Ballot; of Dublin, by Lloyd, in his Notes on the Meteorology of Ireland; those of Schwerin were communicated in manuscript by Dippe; the observations at Melville Island are published in No. 42 of the Parliamentary papers for 1854; and those at Bossekop, by Martins and Bravais, in the Voyage de la Commission Scientifique du Nord.

The tables of this second series being mostly deduced from longer series of observations than those in the first, when the same station is found in both, the table in the

second is generally to be preferred.

Glaisher's table for Greenwich has been taken from the Greenwich Observations. Captain Lefroy kindly furnished the tables for Toronto and Lake Athabasca. To him the author is also indebted for the observations made at Montreal by Mr. McCord, from which Table X. was computed. Table III., for Philadelphia, was deduced by the writer from the observations made at Girard College under the direction of Prof. A. D. Bache.

In order to facilitate the selection of the tables, they are marked in the table of

contents with capitals, which have the following signification: -

A and B mean that the tables have been derived from hourly and bi-hourly observations, and have been computed by Bessel's formula; C, that the tables contain values obtained by interpolation.

A', B', and C' indicate the tables based respectively on hourly and bi-hourly or partly interpolated observations, which give simply the differences between the hourly

and the true means.

The figures added to the letters indicate the number of years during which the observations used in forming the table were carried on. The stations are arranged, in each continent, in the order of their latitude.

Use of the Tables.

In order to reduce meteorological means obtained from any set of hours to the true means, the table best suited to the purpose must first be selected. The diurnal variation changing with the seasons, the latitude, the altitude, and the distance from the sea-shore, the station which comes nearest, in all these respects, to the station the observations of which are to be corrected, must be adopted.

Suppose the thermometer has been observed at Baltimore, during the month of January, at 7 A. M., 1 P. M., and 7 P. M., and the monthly means of these hours to be respectively 27°, 35°, and 31° Fahrenheit. We take Table III., Philadelphia, it being the nearest in latitude and elimatic situation. We find the correction for the

hours 7, 1, and 7, and we have

For 7 A. M.
$$27^{\circ}$$
 $+3^{\circ}.63$ $= 30^{\circ}.63$
For 1 P. M. 35° $-3^{\circ}.87$ $= 31^{\circ}.13$
For 7 P. M. 31° $-1^{\circ}.13$ $= 29^{\circ}.87$
Sums, 93° $-1^{\circ}.37$ $= 91^{\circ}.63$
Means, 31° $-0^{\circ}.46$ $= 30^{\circ}.54$ True Mean for January.

It is obvious that the corrections can be applied, either separately to each hour, as is done above, or collectively, in taking the mean of the three hourly corrections and applying it to the mean of the three observations, as in the last line, which is the more convenient method. Therefore, in order to find the correction for any set of hours, it suffices to take the mean of the corrections given in the table for the hours composing the set. The true daily means can be found in the same way, and the true yearly means can be derived from the corrected monthly means, or by applying the corrections given in the last column.

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HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

NORTH AMERICA. — SOUTH AMERICA.



North America. — Washington. Lat. 38° 54' N. Long. 77° 3' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M. 0 12'	1.15	1.26	1.60	1.95	2.33	2.87	2.94	2.31	2.39	1.73	0.85	0.96	1.80
2 12'	1.28	1.86	2.14	2.40	3.15	3.21	3.25	3.07	2.75	2.27	1.34	1.12	2.3
4 12'	1.45	2.18	2.67	2.75	3.56	3.64	3.83	3.49	3.15	2.89	1.92	1.54	2.7
6 12'	1.88	2.32	2.76	2.59	2.20	2.23	2.12	2.81	3.02	3.19	2.18	1.81	2.4
8 12'	1.48	1.76	1.68	1.05	0.32	-0.16	0.09	0.28	1.04	1.69	1.88	1.68	1.0
10 12'	-0.18	-0.58	-0.88	-0.76	-1.24	-1.82	-1.3 2	-1.81	-1.31	-1.25	-0.17	-0.15	-0.9
P.M. 0 12'	-1.47	-2.05	-2.36	-2.39	-2.64	-2.69	-2.55	-2.97	-2.92	-2.89	-1.90	-1.57	-2.3
2 12'	-2.60	-3.15	-3.35	-3.41	-3.57	-3.84	-3.49	-3.83	-3.74	-3.64	-2.44	-2.50	-3.3
$4 \ 12'$	-2.32	-3.05	-3.20	-3.51	-3.66	-4.29	-4.16	-3.59	-3.65	-3.29	-2.08	-2.19	-3.2
6 12'	-0.76	-1.25	-1.73	-2.18	-2.44	-1.60	-2.24	-1.74	-1.88	-1.84	-1.59	-1.01	-1.6
8 12'	-0.23	0.02	-0.05	0.06	0.27	0.44	-0.21	-0.26	-0.23	0.18	-0.22	-0.26	-0.0
10 12'	0.33	0.69	0.76	1.42	1.67	2.04	1.26	1.79	1.41	0.98	0.23	0.43	1.0
Means.	1.32	1.52	6.26	9.02	12.64	18.34	19.29	17.78	16.04	7.47	5.20	1.63	

II.

N. AMERICA. — PHILADELPHIA. Lat. 39° 58' N. Long. 75° 11' W. Gr. — Dove. Degrees of Reaumur.

							Troudin.						
Hour.	Jan.	Feb_	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.64	1.27	1.33	1,81	2.06	2.34	2.10	1.94	2.12	1.70	1.31	0.62	1.60
1	0.94	1.48	1.61	2.20	2.32	2.63	2.45	2.19	2.04	1.87	1.22	0.81	1.81
2	1.00	1.67	1.85	2.58	2.64	2.86	2.69	2.41	2.22	2.18	1.43	0.98	2.04
3	1.13	1.95	2.00	2.76	2.96	3.20	2.88	2.44	2.43	2.36	1.50	1.12	2.23
4	1.24	2.05	2.08	2.97	3.27	3.40	3.04	2.74	2.56	2.58	1.74	1.28	2.41
5	1.36	2.13	2.50	3.06	3.32	3.28	3.11	2.89	2.68	2.78	1.83	1.38	2.53
6	1.50	2.24	2.44	2.84	2.63	2.54	2.56	2.64	2.65	2.95	1.89	1.44	2.36
7	1.60	2.28	2.24	2.15	1.68	1.45	1.53	1.84	1.92	2.40	1.88	1.36	1.86
\mathbf{s}	1.40	1.46	1.26	1.17	0.65	0.40	0.54	0.67	0.78	1.08	1.21	1.14	0.98
9	0.78	0.57	0.35	0.23	-0.39	-0.52	-0.36	-0.20	-0.18	-0.15	0.26	0.52	0.08
10	0.02	-0.39	-0.46	-0.71	-1.06	-1.23	-1.00	-1.05	-1.08	-1.17	-0.56	-0.22	-0.74
11	-0.68	-1.20	-1.38	-1.54	-1.74	-1.93	-1.74	-1.84	-1.90	-1.96	-1.27	-0.92	-1.50
Noon.	-1.21	-1.77	-1.97	-2.16	-2.24	-2.51	-2.26	-2.34	-2.45	-2.61	-1.77	-1.28	-2.05
1	-1.73	-2.36	-2.45	-2.86	-2.71	-3.06	-2.66	-2.67	-2.88	-3.14	-2.26	-1.63	-2.53
2	-2.04	-2.66	-2.74	-3.29	-3.11	-3.32	-2.97	-3.01	-3.22	-3.45	-2.52	-1.84	-2.85
3	-2.10	-2.82	-3.07	-3.42	-3.36	-3.40	-3.15	-3.11	-3.26	-3.45	-2.48	-1.85	-2.96
4	-1.98	-2.69	-2.99	-3.44	-3.46	-3.44	-3.06	-2.98	-3.17	-3.33	-2.24	-1.63	-2.87
5	-1.30	-2.18	-2.52	-3.14	-3.26	-3.05	-2.94	-2.70	-2.77	-2.46	-1.46	-1.10	-2.41
6	-0.91	-1.37	-1.60	-2.49	-2.46	-2.47	-2.30	-2.03	-1.77	-1.33	-0.82	-0.64	-1.68
7	-0.51	-0.80	-0.88	-1.23	-1.28	-1.38	-1.44	-1.02	-0.76	-0.52	-0.33	-0.31	-0.87
8	-0.20	-0.21	-0.20	-0.29	-0.06	0.06	0.03	0.01	0.28	0.18	-0.14	-0.04	-0.05
9	0.07	0.11	0.90	0.35	0.65	0.82	0.57	0.60	0.81	0.65	0.29	0.09	0.49
10	0.33	0.48	0.77	0.93	1.24	1.37	1.08	1.09	1.33	1.24	0.45	0.27	0.88
11	0.56	0.75	0.96	1.44	1.74	1.91	1.55	1.44	1.64	1.63	0.79	0.40	1.23
Mean.	0.30	1.12	5.18	8.75	12.18	16.22	18.19	17.52	14.66	8.72	3.67	0.58	

NORTH AMERICA. — PHILADELPHIA. Lat. 39° 58 N. Long. 75° 11' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — GUYOT.

Degrees of Fahrenheit.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight	1.47	2.90	2.90	4.13	4.68	5.28	4.70	4.37	4.47	3.80	2.70	1.40	3.57
1	2.13	3.37	3.6 3	4.88	5.25	5.93	5.57	4.93	4.60	4.17	2.73	1.83	4.08
2	2.20	3.57	4.17	5.88	5.95	6.45	6.10	5.43	5.00	4.87	3.20	2.20	4.59
3	2.57	4.43	4.50	6.28	6.68	7.23	6.53	5.50	5.47	5.27	3.37	2.53	5 63
4	2.80	4.67	4.70	6.75	7.38	7.68	6.90	6.17	5.77	5.77	3.90	2.87	5.45
5	3.07	4.83	5.63	6.95	7.48	7.40	7.03	6.50	6.03	6.23	4.10	3.10	5.70
6	3.40	5.10	1	6.45	5.93	5.73	5.80	5.93	5.97	6.60	4.23	3.23	5.32
7	3.63	5.17	5.03	4.90	3.80	3.28	3.50	4.13	4.33	5.37	4.20	3.07	4.20
8	3.17	3.33	2.80	2.50	1.48	0.90	1.27	1.50	1.93	2.40	2.70	2.57	2.16
9	1.77	1.33					-0.77						0.19
10	0.07	-0.83	-1.03	-1.53	-2.38	-2.75	-2.20	-2.37	-2.43	-2.67	-1.27	-0.50	-1.66
11	-1.40	-2.63	-3.10	-3.40	-3.90	-4.33	-3.87	-4.13	-4.27	-4.43	-2.87	-2.07	-3.37
Noon.	-2.70	-3.93	-4.43	-4.72	-5.03	-5.63	-5.03	-5.27	-5.50	-5.90	-4.00	-2.87	-4.58
1	-3.87	-5.27	-5.50	-6.38	-6.08	-6.88	-5.93	-6.00	-6.47	-7.10	-5.10	-3.67	-5.69
2	-4.57	-5.97	-6.17	-7.12	-6.98	-7.45	-6.63	-6.83	-7.20	-7.80	-5.67	-4.13	-6.40
3	-4.70	-6.30	-6.90	-7.63	-7. 55	-7.63	-7.0 3	-7.00	-7.33	-7. 80	-5.60	-4.17	-6.64
4	-4.43	-6. 00	-6.73	-7.65	-7.7 8	-7.7 3	-6.83	-6.70	-7. 13	-7.5 3	-5.07	-3.67	-6.44
5	-2.90	-4.87	-5.67	-7.00	-7.33	-6.85	-6.57	-6.07	-6.23	-5.57	-3.30	-2.47	-5.40
6	-2.03	-3.03	-3.60	-5.55	-5.53	-5.55	-5.13	-4.57	-3.97	-3.03	-1.87	-1.43	-3.77
7	-1.13	-1.77	-1.97	-2.70	-2.88	-3.10	-3.20	-2.30	-1.70	-1.20	-0.77	-0.70	-1.95
8	-0.43	-0.43	-0.43	-0.60	-0.13	0.15	0.08	0.03	0.63	0.37	0.15	-0.10	-0.11
9	0.17	0.30	0.73	0.85	1.48	1.85	1.33	1.37	1.83	1.43	0.63	0.20	1.01
10	0.77	1.13	1.73	2.15	2.80	3.10	2.47	2.47	3.00	2.77	1.00	0.60	2.00
11	1.27	1.73	2.17	3.30	3.93	4.30	3.53	3.23	3.70	3.63	1.77	0.90	2.78
6, 6	0.69	1.04	0.95	0.45	0.20	0.09	0.34	0.68	1.00	1.79	1.18	0.90	0.78
7, 7	1.2	1.70	1	1	l	l	0.15	0.92	1.32		1	1.19	1.13
8, 8	1.37	1.45	1		0.68	1		0.77	1.01	1	1	1.24	1.04
9, 9	0.97	0.82	1		0.32		0.28	0.47	0.72	1	1	0.69	0.66
10, 10	0.42	0.15	0.35	0.31	0.21	0.18	0.14	0.05	0.29	0.05	-0.13	0.05	0.17
7, 2, 9				-0.53									-0.39
6, 2, 8	-0.53			-0.42									
6, 2, 10	-0.13	1	0.53	1	1	I		1)		-0.15	1	0.4
6, 2, 6	_1.07	_0.79	_1 .19	-2.07	_2 10	-2.12	-1.43	-1.82	-1.73	 -1.41	-1.10	-0.78	-1.4
7, 2				-1.11									
8, 2				-2.31									
8, 1				-1.94									
7, 1	_0 19	-0.03	_0.21	-0.74	_1 14	_1.80	 _1.99	-0.94	-1.07	-0.87	 -0.45	-0.30	-0.7!
			-2.45										

N. America. — Frankfort Arsenal. Lat. 39° 57′ N. Long. 75° 8′ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur. Hours. Jan. Feb. March, April. May. June. July. Aug. Sept. Oct. Nov. Dec. Mean. Morn. 1 1.34 1.46 1.75 1.87 2.60 3.41 3.07 2.69 2.63 2.40 1.18 1.34 2.15 2 1.51 1.73 2.13 2.33 3.05 3.73 2.67 1.27 3.51 3.04 3.05 1.50 2.46 3 1.82 1.98 2.56 2.88 3.43 3.92 3.83 3.32 3.49 2.94 1.41 1.66 2.77 4 2.13 2.23 2.90 3.293.57 3.84 3.84 3.36 3.73 3.13 1.51 1.80 2.94 5 2.31 2.46 2.95 3.31 3.32 3.36 3.40 2.99 3.54 3.12 1.73 1.87 2.86 2.25 2.35 6 2.62 2.83 2.65 2.46 2.21 2.84 2.82 1.38 2.52 1.80 2.39 1.88 2.01 7 1.91 1.94 1.66 1.26 1.34 1.15 1.71 2.19 1.06 1.52 1.64 1.22 1.33 0.85 0.57 - 0.030 36 1.26 8 0.94 0.08 0.01 0.58 0.97 0.68 9 0.30[-0.07]-0.20[-0.45]-1.20[-1.06]-1.00[-0.96]0.12 | -0.02-0.62[-0.72[-1.00]-1.05[-1.29]-2.11[-1.96[-1.78]-2.06]-1.13[-0.70]-0.76[-1.27]10 $-1.54 \left| -1.77 \right| -1.76 \left| -1.69 \right| -1.97 \left| -2.74 \right| -2.64 \left| -2.34 \right| -2.89 \left| -2.33 \right| -1.12 \left| -1.70 \right| -2.04$ 11 Noon. . . -2.30 $\left|-2.60\right|$ -2.32 $\left|-2.22\right|$ -2.35 $\left|-3.17\right|$ -3.16 $\left|-2.78\right|$ -3.47 $\left|-3.35\right|$ -1.96 $\left|-2.45\right|$ -2.68 $-2.85 \begin{vmatrix} -3.01 \end{vmatrix} - 2.74 \begin{vmatrix} -2.72 \end{vmatrix} - 3.07 \begin{vmatrix} -3.51 \end{vmatrix} - 3.58 \begin{vmatrix} -3.16 \end{vmatrix} - 3.86 \begin{vmatrix} -4.05 \end{vmatrix} - 2.38 \begin{vmatrix} -2.87 \end{vmatrix} - 3.15$ 1 2 -3.02 |-3.18 |-3.01 |-3.19 |-3.52 |-3.77 |-3.87 |-3.48 |-4.07 |-4.36 |-2.54 |-2.89 |-3.413 -2.92 |-2.93 |-3.10 |-3.53 |-3.78 |-3.89 |-3.94 |-3.61 |-4.02 |-4.22 |-2.40 |-2.54 |-3.41-2.53[-2.44[-2.95[-3.55[-3.70]-3.75[-3.67]-3.42[-3.63]-3.66[-1.96[-1.94[-3.10]-3.42[-3.63]-3.66]]4 5 -1.90 -1.87 -2.50 -3.11 -3.20 -3.23 -3.00 -2.81 -2.84 -2.75 -1.52-1.14 | -1.11 | -1.78 | -2.23 | -2.31 | -2.33 | -2.00 | -1.83 | -1.72 | -1.65 ||-0.56| -0.55| -1.606 -0.37 -0.46 -0.92 -1.09 -1.19 -1.16-0.83-0.67 -0.48 -0.540.14 0.01 -0.63 7 0.12 - 0.068 0.290.02[-0.10]0.07 0.28 0.43 0.66 0.69 0.42 0.27 0.76 0.66 0.61 0.85 0.80 1.17 1.17 1.29 1.49 1.02 0.71 9 1.17 0.98 1.32 10 1.02 0.93 1.05 1.43 2.02 1.79 1.84 1.96 1.66 1.15 0.90 1.42 11 1.13 1.18 1.31 1.50 1.85 2.61 2.24 2.15 2.18 1.96 0.91 1.06 1.67 1.36 3.04 1.19 1.48 1.62 2.01 2.63 2.40 2.35 2.18 1.15 1.20 1.88 Midn. . . 0.17 0.56 0.62 0.42 0.300.07 0.26 0.19 0.56 0.58 0.41 0.62 6. 6 0.40 7. 7 0.76 0.78 0.50 0.42 0.24 0.05 0.26 0.240.62 0.83 0.60 0.76 0.51 0.24 0.02 0.22 8. 8 0.76 0.72 0.440.430.18 0.510.85 0.630.70 0.489. 9 0.55 0.48 0.27 0.33 0.18 - 0.020.06 0.14 0.26 0.64 0.50 0.44 0.32 10.10 0.20 0.11 0.03 0.13 0.07 | -0.05-0.080.03 -0.050.26 0.230.07 0.08 7. 2. 9 $-0.13 \left| -0.17 \left| -0.16 \left| -0.13 \right| -0.35 \left| -0.45 \left| -0.45 \left| -0.35 \left| -0.29 \right| -0.33 \left| -0.15 \left| -0.22 \left| -0.27 \right| -0.22 \right| -0.27 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.22 \left| -0.27 \right| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -0.20 \right| -0.20 \left| -$ 6. 2. 8 $-0.16 \left| -0.24 \right| -0.15 \left| -0.11 \right| -0.32 \left| -0.41 \right| -0.36 \left| -0.28 \right| -0.19 \left| -0.37 \right| -0.16 \left| -0.22 \right| -0.25$ 6. 2.10 0.32 0.19 0.24 0.15 0.19 0.24 0.00 -0.06 0.14 0.08 0.03 0.22 0.04 6. 2. 6 -0.64 - 0.65 - 0.72 - 0.86 - 1.06 - 1.21 - 1.12 - 1.03 - 0.98 - 1.06 - 0.57 - 0.55 - 0.87-0.57 -0.59 -0.55 -0.63 -0.93 -1.26 -1.27 -1.17 -1.18 -1.09 -0.74 -0.69 -0.897. 2 -0.90 [-0.93] [-1.04] [-1.17] [-1.48] [-1.90] [-1.74] [-1.86] [-1.55] [-0.98] [-0.96] [-1.37]8. 2 $-0.82 \\ \left[-0.84 \\ \left[-0.90 \\ \left[-0.94 \\ \left[-1.25 \\ \left[-1.77 \\ \left[-1.75 \\ \left[-1.58 \\ \left[-1.75 \\ \left[-1.40 \\ \left[-0.90 \\ \left[-0.95 \\ \left[-0.95 \right] \right] -1.24 \right] \right] \right] \right] \\$ S. 1 $-0.49 \Big| -0.50 \Big| -0.42 \Big| -0.39 \Big| -0.71 \Big| -1.13 \Big| -1.12 \Big| -1.10 \Big| -1.08 \Big| -0.93 \Big| -0.66 \Big| -0.68 \Big| -0.76 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.76 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -0.68 \Big| -$ 7. 1 9.12.3.9 $-1.03 \left[-1.14 \left[-1.22 \left[-1.28 \left[-1.45 \left[-1.77 \left[-1.75 \left[-1.53 \left[-1.74 \left[-1.57 \left]-0.84 \left[-1.03 \left[-1.36 \left[-1.57 \left[-1.5$ 7. 2.2(9) 0.10 0.04 - 0.030.11 | -0.07 | -0.01 | -0.05 |0.06 0.16 0.04 0.14 -0.36 [-0.36 [-0.08 [-0.12] [-0.11] [0.02 [-0.05] [-0.13] [-0.17] [-0.62 [-0.41] [-0.51] [-0.24]Dail. ext.

N. America. — Frankfort Arsenal. Lat. 39° 57′ N. Long. 75° 8′ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degree	s of Fah	теппен						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
36 3	9 09	2 20	201		- 0=	7 07	6.01	6.02	5 00	= 10	9.66	2.00	
Morn. 1	3.02	3.29	3.94	4.21	5.85	7.67	6.91	6.05	5.92	5.40	I	1	4.84
2	3.40	3.89	4.79	5.24	6.86	8.39	7.90	6.84	6.86	6.01	2.86	3.38	5.54
3	4.10	4.46	5.7 6	6.48	7.72	8.82	8.62	7.47	7.85	6.62	3.17	3.74	6.23
4	4.79	5.02	6.53	7.40	8.03	8.64	8.64	7.56	8.39	7.04	3.40	4.05	6.62
5	5.20	5.54	6.64	7.45	7.74	7.56	7.65	6.73	7.97	7.02	3.89	4.21	6.44
6	5.06	5.29	5.90	6.37	5.96	5.54	5.67	4.97	6.39	6.35	3.11	4.05	5.38
7	4.23	4.52	4.30	4.37	3.74	2.84	3.02	2.59	3.85	4.93	2.39	3.42	3.69
8	2.75	2.99	2.12	1.91	1.28	-0.07	0.18	0.02	0.81	2.84	1.31	2.18	1.53
9	0.77	0.68	-0.16	-0.45	-1.01	-2.70	-2.39	-2.25	-2.16	0.27	-0.05	0.41	-0.77
10	!								1	-2.54	l l	l .	-2.86
11									1	-5.24	1	l .	-4.59
Noon	1						i .	1		-7.54	i		-6.03
1										-9.11			
2	4									-9.81		ı	l i
3										-9.50			-7.67
4	-5.69	-5.49	-6.64	-7. 99	-8.33	-8.44	-8.26	-7.70	-S.17	-8.24	-4.41	-4.37	-6.98
5	-4.28	-4.21	-5.63	-7.00	-7.2 0	-7.27	-6.75	-6.32	-6.39	-6.19	-3.42	-2.77	-5.63
6	-2.57	-2.50	-4.01	-5.02	-5.20	-5.24	-4.50	-4.12	-3.87	-3.71	-1.26	-1.24	-3.60
7	-0.83	-1.04	-2.07	-2.45	-2.68	-2.61	-1.87	-1.51	-1.08	-1.22	0.32	0.02	-1.42
s	0.65	0.27	-0.14	0.05	-0.23	0.16	0.63	0.97	1.49	0.97	1 55	0.95	0.61
9	1.71	1.48	1.37	1.91	1.80	2.63	2.63	2.90	3.35	2.63	2.30	1.60	2.21
10	2.30	2.09	2.36	1.97	3.22	4.55	4.03	4.14	4.41	3.74	2.59	2.03	3.20
10	2.54	2.66	$\frac{2.30}{2.95}$	3.38	4.16	5.87	5.04	4.84	4.91	4.41	2.05	2.39	3.76
t t	2.68	3.06	3.33	3.65	4.10	6.84	5.92	5.40	5.29	4.91	2.59	2.39	4.23
Midn	2.00	5.00	9.99	5.03	4.92	0.04	0.02	9.40	3.23	4.31	2.99	2.10	4.20
0.0	1.00	1 40	0.05	0.00	0.00	0.10	0.50	0.13	1.00	1 91	0.00	1 40	0.90
6. 6	1.26	1.40	0.95	0.68	0.38	0.16	0.59	0.43	1.26	1.31	0.92	1.40	1
7. 7	1.71	1.76	1.13	0.95	0.54	$\begin{array}{c} 0.11 \\ 0.05 \end{array}$	0.59 0.41	$0.54 \\ 0.50$	1.40 1.15	1.87	1.35	1.71	1.15 1.08
3.8	1.71	1.62	0.99	0.97	0.54		0.14	0.30	0.59	1.91	1.42	1.58	0.72
9. 9	1.24	1.08	0.61	0.74	0.41	-0.05 -0.11	-0.18		-0.11	0.59	1.13	0.99	0.12
10.10	0.45	0.25	0.07	0.29	0.10	-0.11	-0.13	0.07	-0.11	0.59	0.52	0.16	0.15
7. 2. 9	-0.29	-0.38	-0.36	-0.29	-0.79	-1.01	-1.01	-0.79	-0.65	-0.74	-0.34	-0.50	-0.61
6. 2. 8		-0.54						1	-0.43			-0.50	1
6. 2.10	0.18	0.07	0.50	0.72	0.43	0.54	0.34	0.43	0.54	0.09	0.00	-0.14	0.32
6. 2. 6	-1.44	-1.46	-1.62	-1.94	-2.39	-2.72	-2.52	-2.32	-2.21	-2.39	-1.28	-1.24	-1.96
7. 2	-1.28	_1 32	-190	_1.49	2 00	-2.84	-2.86	-2.63	-2.66	-2.45	-1.67	-1.55	-2.00
8. 2										-3.49			
8. 1										-3.75			
7. 2				1				ı		-2.09	1		1 1
9.12.3.9		-2.57								-3. 53			
7. 2.2(9)	0.23	0.09	0.07	0.25	-0.16	-0.09	-0.11	0.14	0.36	0.09	0.32	0.02	0.09
Dail.ext.	-0.81	-0.81	-0.18	-0.27	-0.25	0.04	-0.11	-0.29	-0.38	-1.39	-0.92	-1.15	-0.51

N. America. — Toronto. Lat. 43° 39′ 35″ N. Long. 79° 21′ 30″ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

	,				Degree	es of Fa	TI CHITCE	·.					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.87	0.92	3.04	4,43	5.90	5.94	6.30	5.06	5.74	4.16	1.91	1.04	3.87
2	2.16	1.33	3.56	5.11	6.64	6.62	7.13	5.68	6.68	4.68	2.14	1.13	4.41
3	2.10	1.91	1	!		7.29	8.01	6.82	7.63	5.04	2.14	1.40	5.02
		1	4.19	5.76	7.36	1	1						}
4	2.68	2.66	4.75	6.17	7.65	7.56	8.44	7.61	8.19	5.20	2.61	1.78	5.45
5	3.02	3.40	4.95	5.94	7.07	6.98	7.88	7.49	7.94	5.02	2.68	2.16	5.38
6	3.29	3.92	4.61	4.97	5.49	5.38	6.14	6.14	6.71	4.48	2.52	2.39	4.68
7	3.26	3.98	3.65	3.38	3.17	3.04	3.49	3.67	4.52	3.44	2.05	2.27	3.33
8	2.72	3.40	2.12	1.42	0.68	0.43	0.52	0.68	1.78	1.91	1.15	1.71	1.55
9	1.58	2.33	0.29	-0.50	-1.51	-1.85	-2.12	-2.09	-1.06	-0.05	-0.07	0.79	-0.36
10	0.00	0.61	-1.60	-2.07	-3.08	-3.47	-4.01	-4.14	-3.62	-2.25	-1.46	-0.34	-2.12
11	-1.71	-1.15	-3.26	-3.26	-4.14	-4.46	-5.15	-5.33	-5.72	-4.39	-2.79	-1.44	-3.58
Noon	-3.11			1	l .	-5.18	l .		i		-3.78	-2.30	-4.66
1	-3.89	-3.67	-5.36	-5.00	-5.90	-5.94	-6.59	-6.50	-8.33	-7.11	-1.28	-2.77	-5 45
2	-3.98		-5.72			-6.89			-8.89	l		-2.86	
3	-3.53		-5.60		-8.15		-8.28		-8.87	ĺ	1		
4	-2.84	-3.38	1		-8.51		-8.55		ı	l	l	ł	ľ
*	-2.04	-9.90	-5.02	-010	-0.31	0.00	-0.00	1.01	0.12	3.10	2.02	2.29	0.12
5	-2.14	-2.63	-4.03	-5.94	-7.76	-7.4 3	-7.83	-6.95	-6.59	-3.53	-1.44	-1.71	-4.84
6	-1.62	-1.89	-2.75	-4.66	-5.83	-5.65	-5.94	-5.00	-4.43	-1.91	-0.45	-1.13	-3.44
7	-1.24	-1.24	-1.31	-2.81	-3.08	-3.04	-3.17	-2.25	-1.94	-0.50	0.32	-0.54	-1.73
8	-0.88	-0.68	0.05	-0.77	-0.16	-0.18	-0.18	0.65	0.43	0.65	0.86	0.02	-0.02
9	-0.43	-0.25	1.15	1.06	2.30	2.30	2.39	2.97	2.30	1.53	1.17	0.47	1.42
10	0.16	0.11	1.89	2.41	3.94	3.98	4.14	4.32	3.58	2.25	1.37	0.81	2.41
11	0.83	0.38	2.34	3.26	4.82	4.93	5.11	4.77	4.37	2.90	1.53	0.97	3.02
Midn	1.42	0.63	2.66	3.85	5.33	5.45	5.64	4.84	5.00	3.56	1.71	1.01	3.42
6. 6	0.83	1.01	0.95	0.16	-0.18	0.14	0.11	0.56	1.13	1.28	1.04	0.63	0.61
7. 7	1.01	1.27	1.17	0.29	-0.05	0.00	0.16	0.72	1.28	1.49	1.19	0.86	0.81
8. 8	0.92	1.37	1.08	0.34	0.27	0.14	0.16	0.68	1.10	1.28	1.01	0.86	0.77
9. 9	0.59	0.99	0.72	0.29	0.41	0.23	0.14	0.45	0.63	0.74	0.56	0.63	0.54
10.10	0.07	0.36	0.14	0.16	0.43	0.27	0.07	0.09	-0.02	0.00	-0.05	0.23	0.14
7. 2. 9	-0.38	-0.11	-0.32	-0.45	-0.56	-0.52	-0.54	-0.16	-0.70	-0.77	-0.32	-0.05	-0.41
6. 2. 8	-0.52		-0.32				ı	-0.11			1	-0.16	-0.43
6. 2.10	-0.18	-0.27 -0.02	0.27	0.54	0.77	0.83	0.95	1.13		-0.18	i .	0.11	0.38
6. 2. 6			-1.28			-2. 39	!	1 .		-1.55	1		-1.58
	0.00	0.01			2.00		0.00		0.70	7.0-		0.20	107
7. 2			-1.04										
8. 2	-0.63		-1.80										
8. 1	-0.59		-1.62										
7. 1	-0.32	0.16	-0.86	-0.81	-1.42	-1.46	-1.55	-1.42	-1.91	-1.85	-1.13	-0.25	-1.06
9.12.3.9	-1.37	-1.15	-2.18	-2.50	-3.08	-3.13	-3.49	-3.20	-3.71	-2.79	-1.55	-0.92	-2.43
7. 2.2(9)	-0.41	-0.16	0.07	-0.07	0.16	0.18	0.20	0.63	0.07	-0.18	0.07	0.09	0.05
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VII.

N. America. — Toronto. Lat. 43° 39′ 35″ N. Long. 79° 21′ 30″ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						s of Ke							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.83	0.41	1.35	1.97	2.62	2.64	2.80	2.25	2.55	1.85	0.85	0.46	1.72
2	0.96	0.59	1.58	2.27	2.95	2.94	3.17	2.57	2.97	2.08	0.95	0.50	1.96
3	1.06	0.85	1.86	2.56	3.27	3.24	3.56	3.03	3.39	2.24	1.06	0.62	2.23
4	1.19	1.18	2.11	2.74	3.40	3.36	3.75	3 38	3.64	2.31	1.16	0.79	2.42
5	1.34	1.51	2.20	2.64	3.14	3.10	3.50	3.3 3	3.53	2.23	1.19	0.96	2.39
6	1.46	1.74	2.05	2.21	2.44	2.39	2.73	2.73	2.98	1.99	1.12	1.06	2.08
7	1.45	1.77	1.62	1.50	1.41	1.35	1.55	1.63	2.01	1.53	0.91	1.01	1.48
8	1.21	1.51	0.94	0.63	0.30	0.19	0.23	0.30	0.79	0.85	0.51	0.76	0.69
	1.41	1.01	0.04	0.00	0.00	0.10	0.20	0.00	0	0.00	0.01	0.10	0.00
9	0.70	0.99	0.13	-0.22	-0.67	-0.82	-0.94	-0.93	-0.47	-0.02	-0.03	0.35	-0.16
10	-0.00	0.27	-0.71	-0.92	-1.37	-1.54	-1.78	-1.84	-1.61	-1.00	-0.65	-0.15	-0.94
11	-0.76	-0.51	-1.45	-1.45	-1.84	-1.98	-2.29	-2.37	-2.54	-1.95	-1.24	-0.64	-1.59
Noon	-1.38	-1.18	-2.02	-1.86	-2.22	-2.30	-2.62	-2.65	-3.22	-2.72	-1.68	-1.02	-2.07
		1.00	0.00	0.00	0.00	9.61	9.09	9.60	2.70	9.16	-1.90	1 00	0.40
1	1	1	-2.38	2.22	-2.00	2.04	2.93	-2.00	2 05				
2	1	-1.81	1	-2.56									
3	-1.57			-2.82					-3.94				
4	-1.26	-1.50	-2.23	-2.88	-3.18	-3.59	-3.50	-3.47	-3.01	-2.50	-1.12	-0.99	-2.54
5	-0.95	-1.17	-1.79	-2.64	-3.45	-3.30	-3.48	-3.09	-2.93	-1.57	-0.64	-0.76	-2.15
6	-0.72			-2.07							-0.20	-0.50	-1.53
7	-0.55	-0.55		-1.25					-0.86		0.14	-0.24	-0.77
8	1	-0.30		-0.34					0.19	0.29	0.38	0.01	-0.01
					1.00	1.00	1.00	1.00	1.00	0.00	0.52	0.07	0.00
9	-0.19	l .	0.51	0.47	1.02	1.02	1.06	1.32	1.02	0.68		0.21	0.63
10	0.07	0.05	0.84	1.07	1.75	1.77	1.84	1.92	1.59	1.00	0.61	0.36	1.07
11	0.37	i .	1.04	1.45	2.14	2.19	1	2.12	1.94	1.29	0.68	0.43	
Midn	0.63	0.28	1.18	1.71	2.37	2.42	2.53	2.15	2.22	1.58	0.76	0.45	1.52
6. 6	0.37	0.45	0.42	0.07	-0.08	-0.06	0.05	0.25	0.50	0.57	0.46	0.28	0.27
7. 7	0.45	1	0.52	0.13	0.02	l	1	0.32	0.57	0.66	0.53	0.38	0.36
8.8	0.41		0.48	l .	0.12	1	0.07	0.30	0.49	0.57	0.45	0.38	0.34
9. 9	0.26		0.32	0.13	0.18	0.10	0.06	0.20	0.28	0.33	0.25	0.28	0.24
10.10	0.03	0.16	0.06	0.07	0.19	0.12	0.03	0.04	-0.01	0.00	-0.02	0.10	0.06
													0.70
7. 2. 9	-0.17	1	1		-0.25	1	1	1	-0.31				
6. 2. 8	П	-0.12	1	-0.23		l .	-0.22	1	-0.26		1	1	!
6. 2.10	 -0.0 8				1	1	1		1	1	-0.04	1	1
6. 2. 6	-0.34	-0.30	-0.57	-0.81	-1.11	-1.06	-1.08	-0.88	-0.98	-0.69	-0.31	-0.24	-0.70
7. 2	_0.16	-0.02	-0.46	-0.53	-0.89	-0.86	-0.89	-0.77	-0.97	-0.85	-0.47	-0.13	-0.58
8. 2	$\begin{bmatrix} -0.10 \\ -0.28 \end{bmatrix}$	-0.15	-0.80	-0.97	-1.44	-1.44	-1.55	-1.43	-1.58	-1.19	-0.67	-0.26	-0.98
8. 1	-0.26	-0.06	[-0.72]	-0.80	-1.18	-1.23	-1.35	-1.30	-1.46	-1.16	-0.70	-0.24	-0.87
7. 1	-0.14	0.07	-0.38	-0.36	-0.63	-0.65	-0.69	-0.63	-0.85	-0.82	-0.50	-0.11	-0.47
		1									1		
9.12.3.9			-0.97				1	1		-1.24		1	1
7. 2.2(9)	-0.18	-0.07	0.03	-0.03	0.07	0.08	0.09	0.28	0.03	-0.08	0.03	0.04	0.02
Dail and	_0.16	-0.0	_0.15	-0.07	_0 10	_0.19	_0.03	-0.0	-0.16	-0.46	-0.36	-0.11	-0.14
Dail. ext.	1-0.16	,-0.02	-0.17	1-0.07	0.19	-0.12	1 0.00	1 0.00	3.10	0.40	1 370	1 3.11	

VIII.

NORTH AMERICA. — TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Lefrox.

Degrees of Fahrenheit.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year.
Midnight.	1.47	1.73	2.63	3.22	5.02	5.15	6.37	5.33	5.96	3.22	1.80	0.90	3.57
1	1.95	2.09	3.11	3.79	5.93	6.00	7.13	6.06	4.57	3.80	2.10		4.00
2	2.05	2.46	3.47	4.48	6.77	6.70	7.68	6.69	5.17	4.13	2.36	1.85	4.48
3	2.20	2.82	3.76	5.08	7.45	7.50	8.41	7.29	5.59	4.31	2.66	1.96	4.92
4	2.28	3.20	4.07	5.38	7.93	8.06	9.03	7.63	6.18	4.64	2.85	2.04	5.27
5	2.46	3.62	4.35	5.75	7.83	7.58	9.02	7.89	6.77	4.77	2.76	2.07	5.43
6	1.83	4.23	4.75	5.48	5.40	5.21	5.92	6.57	6.17	4.71	2.52	2.39	4.60
7	1.94	4.34	3.93	3.22	2.43	2.41	2.38	3.28	3.68	3.94	2.52	2.55	3.05
8	1.66	3.29	1.89	1.09	0.06	0.10	-0.31	0.21	1.02	1.66	1.53	2.12	1.25
9	0.63	1)		-2.11		-2.39	-2.26	-1.52	1	0.01	0.92	-0.82
10	-0.59			l	-3.81	1	-3.98	-4.18	-3.47	-2.93	-1.41	-0.53	-2.47
11	-1.70	-2.44	-3.14	-3.85	-4.92	-4.77	-5.49	-5.57	[1	-2.44	i	-3.77
Noon.	-2.48	-3.56	-4.15	-4.86	-5.87	-5. 88	-6.7 2	-6.39	-5.95	-5.36	-3.34	-2.52	-4.76
1	-2.92	-4.49	-4.79	-5.72	-6.83	-6.59	-7. 58		-6.58			-3.06	-5.43
2					-7.13		-8.26		!	-6.04	-3.82	!	-5.81
3	-3.16	-4.90	-5.15	-6.16	-7.20			-7.9 8		1	í		-5.82
4	-2.63	-4.47	-4.65	-5.81	-7.17	-7.60	-8.2 5	-7.79	-6.75	-5.17	-2.83	-2.47	-5.47
5								-7.20					-4.61
6					-5.05		-6.57			-1.37			-3.12
7	-0.40	-0.98	-0.91	-0.94	-2.19	-2.99	-3.28	-1.64	-0.43	-0.25	-0.15	-0.47	-1.22
8	-0.12	-0.13	0.03	0.66	0.43	0.33	0.68	1.23	0.81	0.48	0.19	-0.12	0.38
9	0.07	0.52	1.00	1.78	2.31	2.44	2.99	2.70	1.90	1.25	0.44	0.18	1.46
10	0.44	1.06	1.63	2.59	3.29	3.80	4.24	3.73	2.94	1.97	0.78	0.47	2.24
11	0.77	1.60	2.01	3.07	4.20	4.76	5.21	4.54	3.61	2.68	1.13	0.59	2.85
2 2	0.40		7.00	- 00	0.7-	0.00							
6, 6	0.46	1.18	1.20 1.51	1.03		$-0.26 \\ -0.29$	-0.32	0.59	1.50	1.67	1.38	0.78	0.74
7, 7 8, 8	0.77	1.67 1.58	0.96	1.14 0.87	$0.12 \\ 0.24$	$0.29 \\ 0.21$	-0.45 0.18	$0.82 \\ 0.72$	$\begin{array}{c} 1.62 \\ 0.91 \end{array}$	1.84 1.45	1.18 0.98	1.04	$0.91 \\ 0.82$
9, 9	0.35	0.77	0.37	0.38	0.10	0.21	0.13	0.72	0.31	0.10	0.38	0.55	0.82
-0 -0	0.0=	0.0=			0.00	0.25							
10, 10	-0.07		-0.14			0.25			-0.26				-0.11
6, 2, 10	-0.31 -0.40	0.14	0.36	0.64	0.52	0.66	0.63	0.89	0.72		-0.17	1	0.34
7, 2, 9 $12, 3, 9$	-0.40 -1.23		-0.09 -2.01		-0.80 -3.22	-0.73 -3.16	-0.96 -3.61	-0.55 -3.48	-0.46 -3.14	-0.28			-0.43 -2.48
Mean.	25.82	23.70	29.79	41.99	52.92	60.67	66.39	65.86	57.55	44.14	36.18	27.40	44.37

NORTH AMERICA. - TORONTO. Lat. 43° 40' N. Long. 79° 21' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.68	0.81	1.10	1.45	2.24	2.36	2.91	2.43	1.76	1.44	0.81	0.40	1.53
1	0.88	0.93	1.31	0.78	2.62	2.67	3.29	2.72	2.03	1.71	0.94	0.66	1.80
2	0.92	1.13	1.48	2.08	2.99	2.98	3.54	3.02	2.29	1.85	1.06	0.83	2.01
3	0.99	1.32	1.61	2.17	3.31	3.32	3.86	3.32	2.49	1.92	1.20	0.38	2.20
4	1.03	1.45	1.78	2.36	3.52	3.58	4.14	3.48	2.76	2.06	1.28	0.90	2.36
5	1.11	1.61	2.01	2.52	3.49	3.49	4.16	3.57	3.04	2.13	1.23	0.91	2.44
6	0.79	1.86	2.13	2.47	2.40	2.32	2.74	2.92	2.74	2.04	1.11	1.09	2.05
7	0.83	1.92	1.75	1.45	1.08	1.07	1.11	1.60	1.60	1.70	1.11	1.16	1.36
8	0.73	1.47	0.87	0.45	0.09	0.03	-0.05	0.15	0.38	0.70	0.64	0.97	0.56
9	0.30	0.44	-0.10	-0.43	-0.94	-0.81	-1.03	-0.96	-0.69	-0.49	-0.04	0.45	-0.36
10	-0.25	-0.45	-0.87	-1.11	-1.69	-1.55	-1.78	-1.84	-1.57	-1.35	-0.68	-0.20	-1.11
11	-0.77	-1.16	-1.41	-1.72	-2.20	-2.12	-2.47	-2.48	-2.20	-1.96	-1.13	-0.75	-1.70
Noon,	-1.12	-1.69	-1.87	-2.18	-2.62	-2.61	-3.05	-3.04	-2.64	-2.36	-1.48	-1.11	-2.15
1	-1.34	-2.07	-2.16	-2.60	-3.03	-2.93	-3.46	-3.25	-2.90	-2.55	-1.66	-1.42	-2.45
2	-1.46	-2.25	-2.41	-2.76	-3.18	-3.12	-3.84	-3.51	-3.08	-2.70	-1.69	-1.49	-2.62
3	-1.44	-2.24	-2.32	-2.80	-3.21	-3.29	-3.92	-3.66	-3.09	-2.60	-1.62	-1.38	-2.63
4	-1.21	-2.00	-2.11	-2.62	-3.19	-3.40	-3.93	-3.60	-3.00	-2.28	-1.22	-1.09	-2.47
5	-0.77	-1.47	-1.78	-2.30	-3.02	-3.13	-3.72	-3.35	-2.57	-1.50	-0.68	-0.67	-2.0 S
6	-0.40	-0.82	-1.03	-1.50	-2.24	-2.55	-3.08	-2.51	-1.38	-0.59	-0.32	-0.36	-1.40
7	-0.17	-0.38	-0.38	-0.37	-0.96	-1.33	-1.54	-0.74	-0.18	-0.10	-0.06	-0.21	-0.53
8	-0.03	0.00	0.05	0.33	0.24	0.13	0.33	0.56	0.39	0.23	0.08	-0.04	0.19
9	0.06	0.28	0.50	0.81	1.02	1.09	1.38	1.26	0.85	0.57	0.20	0.07	0.67
10	0.23	0.53	0.79	1.16	1.45	1.69	1.93	1.72	1.32	0.90	0.36	0.20	1.02
11	0.37	0.76	1.08	1.38	1.86	2.12	2.45	2.07	1.60	1.20	0.52	0.25	1.31
Mean.	-2.97	-3.88	-0.98	4.72	9.29	12.75	15.11	15.00	11.37	5.42	1.88	-2.03	

X.

North America. — Montreal. Lat. 45° 30' N. Long. 73° 22' E. Gr.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oet.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year.
Midn.	4.00	3.89	2.83	1.36	1.68	1.10	1.28	1.31	2.52	4.55	5.25	4.39	2.85
2	5.39	4.34	4.01	1.59	1.00	2.36	2.69	2.88	4.37	6.95	7.42	7.17	4.20
4	6.34	5.60	4.84	1.81	1.38	2.88	3.36	5.56	7.09	6.95	7.18	7.57	4.96
6	5.99	4.59	4.83	1.36	1.32	3.54	3.90	5.22	5.56	6.61	5.55	5.46	4.50
8	2.79	2.19	2.52	0.78	0.92	3.10	3.22	3.30	3.44	3.06	0.88	0.60	2.24
10	-1.74	-1.48	-0.99	-0.41	0.21	-0.21	-0.81	-0.03	-0.79	-0.97	-1.75	-2.85	-0.93
Noon.	-5.63	-5.43	-4.22	-1.87	-1.22	-2.82	-3.50	-4.23	-5.01	-7.10	-5.17	-5.46	-4.30
2	1							l				-7.36	
4	-7.72	-6.70	-5.62	-2.52	-3.22	-3.88	-3.60	-5.96	-5.79	-8.35	-7.00	-7.51	-5.65
6	-5.63	-2.80	-2.79	-1.04	-1.30	-1.77	-1.50	-3.43	-3.88	-3.87	-5.02	-5.40	-3.20
8	-0.70	0.10	-0.25	0.03	0.02	-0.90	-0.59	-1.23	-0.81	-1.61	-1.10	-0.67	-0.65
10	1.99	2.39	1.42	1.18	0.89	0.17	0.22	-0.30	0.64	-1.87	2.47	2.64	1.30
Mean.	66.40	57.70	48.31	30.39	23.42	8.10	20.84	27.31	42.27	56.61	64.38	70.39	43.01

NORTH AMERICA. - MONTREAL, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.

Degrees of Fahrenheit.

Hour.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	March.	April.	May.	June.	July.	Year
A.M.1	5.03	4.92	2.53	1.16	0.88	1.43	1.61	4.38	3.12	4.85	4.55	5.07	3.30
3	5.99	5.20	3.61	1.58	1.79	1.30	2.72	5.18	5.14	6.51	5.10	6.80	4.25
5	6.44	5.43	4.45	2.08	2.21	1.87	3.95	6.84	6.54	6.56	6.30	7.76	5.05
7	2.10	3.47	3.61	2.01	2.08	1.98	5.22	7.07	3.84	3.56	4.72	3.04	3.56
9	-0.58	0.73	0.77	0.63	1.14	1.16	3.99	2.96	0.71	0.50	-0.02	0.22	1.02
11	-3.61	-2.20	-2.73	-1.35	-0.49	-1.08	-0.17	-2.51	-2.48	-2.79	-3.42	-3.21	-2.17
P.M.1	-6.61	-5.12	-5.41	-3.17	-2.38	-1.49	-4.80	-7.41	-4.93	-5.78	-5 97	-6.08	-4.95
3	-7.34	-6.65	-5.80	-3.22	-2.78	-2.36	-6.08	-9.03	-6.33	-6.46	-6.93	-S.01	-5.91
5	-5.47	-5.83	-3.15	-1.19	-1.44	-0.63	-4.12	-6.48	-5.63	-6.62	-6.18	-6.53	-1.43
7	-1.45	-0.62	-1.00	-0.44	-0.70	-0.60	-1.23	-2.40	-2.93	-3.50	-3.17	-2.88	-1.74
9	1.58	1.32	0.32	0.13	-0.71	-0.66	-0.96	-0.75	0.44	0.61	1.58	1.17	0.34
11	3.10	3.02	2.47	1.48	0.22	0.61	0.24	1.78	2.06	2.52	3.55	3.39	2.02
Mean.	69.69	57.53	41.70	32.76	15.91	18.96	14.52	22.50	34.47	51.33	65.08	67.42	41.24

XI.

NORTH AMERICA.—SITKA. Lat. 57° 3′ N. Long. 135° 18′ W. Gr.—Dove.

Degrees of Reaumur.

Hour, Jan. Feb. March. April. May. June. July. Aug. Sept. Oct. Nov. Dec Year.													
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Year.
Midn.	0.33	0.58	0.97	1.51	1.80	1.81	1.68	1.34	1.07	1.19	0.41	0.28	1.08
1	0.34	0.66	1.09	1.68	2.04	2.06	1.88	1.53	1.18	1.11	0.46	0.33	1.20
2	0.35	0.72	1.17	1.51	2.20	2.25	2.04	1.66	1.33	1.18	0.49	0.33	1.29
3	0.51	0.78	1.36	1.89	2.43	2.49	2.16	1.77	1.24	0.64	0.48	0.18	1.3
4	0.45	0.86	1.47	2.02	2.55	2.57	2.20	1.82	1.29	0.68	0.49	0.18	1.38
5	0.45	0.83	1.57	2.07	2.39	2.47	2.95	1.89	1.33	0.70	0.49	0.14	1.5
6	0.45	0.84	1.56	1.89	1.76	1.77	1.67	1.62	1.33	0.78	0.46	0.18	1.2
7	0.52	0.82	1.37	1.13	0.96	1.08	0.96	1.09	1.05	0.58	0.40	0.17	0.8
S	0.48	0.76	0.75	0.31	0.00	0.26	0.26	0.40	0.47	0.53	0.33	0.12	0.3
9	0.39	0.49	-0.08	-0.63	-0.82	-0.52	-0.58	-0.26	-0.17	0.12	0.23	0.10	-0.1
10	0.16	-0.03	-0.69	-1.12	-1.35	-1.28	-1.27	-0.95	-0.73	-0.28	0.00	-0.11	-0 6
11	-0.19	-0.60	-1.29	-1.68	-1.75	-1.70	-1.97	-1.57	-1.28	-0.75	-0.35	-0.11	-1.1
Noon.	-0.57	-1.05	-1.71	-2.13	-2.17	-2.11	-2.11	-2.04	-1.65	-1.14	-0.72	-0.32	-1.4
1	-0.83	-1.36	-1.74	-2.33	-2.35	-2.35	-2.25	-2.33	-1.56	-1.38	-0.84	-0.46	-1.6
2	-0.95	-1.44	-1.99	-2.28	-2.40	-2.42	-2.31	-2.16	-1.86	-1.42	-1.00	-0.50	-1.73
3	-0.95	-1.47	-1.94	-2.10	-2.28	-2.31	-2.13	-2.00	-1.72	-1.37	-0.94	-0.44	-1.6
4	-0.78	-1.20	-1.67	-1.91	-2.04	-2.09	-1.94	-1.76	-1.56	-1.13	-0.75	-0.32	-1.43
5	-0.50	-0.85	-1.17	-1.63	-1.73	-1.76	-1.65	-1.43	-1.24	-0.88	-0.45	-0.20	-1.15
6	-0.25	-0.45	-0.82	-1.13	-1.37	-1.48	-1.26	-1.02	-0.64	-0.50	-0.21	-0.10	-0.7
7	-0.15	-0.10	-0.29	-0.48	-0.76	-1.00	-0.81	-0.49	-0.28	-0.16	-0.04	-0.03	-0.33
8	-0.01	0.11	0.13	0.15	-0.23	-0.41	-0.22	0.12	0.19	0.06	0.07	0.01	0.00
9	0.15	0.30	0.44	0.70	0.48	0.27	0.33	0.66	0.52	0.21	0.22	0.12	0.3
10	0.23	0.37	0.64	1.07	1.02	0.97	0.99	0.96	0.76	0.30	0.29	0.19	0.63
11	0.31	0.48	0.84	1.28	1.57	1.46	1.38	1.19	0.90	0.95	0.43	0.22	0.9
lean.	-1.39	-1.07	0.55	3.51	6.21	9.10	10.24	10.28	7.96	5.26	2.52	1.73	

Arctic America. — Boothia Felix. Lat. 69° 59' N. Long. 92° 1' W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
								ļ					
Morn. 1	0.08		1.61	2.17	2.64	2.38	1		1		l .	0.12	1.12
2	0.10	0.28	1.85	2.25	2.75	1	1	1		l .	i	0.13	
3	0.11	0.25	2.10	1	2.61	2.45	1	1	0.66	1	1	0.10	l
4	0.11	0.21	2.30	2.26	2.23	2.05	1.35	1.02	0.66	0.34	0.31	0.06	1.02
5	0.10	0.22	2.38	2.02	1.76	1.39	0.99	0.86	0.56	0.32	0.24	0.02	0.87
6	0.10		2.23	1.53	l .	1	1	1	1	į.		ļ.	0.64
7	0.09	0.29	1.77	0.81	0.35	1	1	ř	0.27	0.17	l .	-0.07	0.37
8	0.08	0.22	0.98	-0.06		1	1	1	0.05	0.01	0.01	-0.10	0.04
											,		
9	0.06			1	l	l .		-0.10	l .	1	-0.04	l	ı
10		-0.26	l	i	l .		į.	-0.49		l .	1	l	ĺ
11	l l	-0.58		1	{	1	1	-0.86		l .		l .	-1.05
Noon	-0.05	-0.87	-3.05	-2.86	-2.46	-2.02	-1.43	-1.16	-0.82	-0.69	-0.32	-0.12	-1.32
1	-0.11	-1.02	-3.38	-3.03	-2.66	-2.33	-1.70	-1.34	-0.93	-0.68	-0.30	-0.14	-1.47
2	1	-0.98		ì	-2.65		1	-1.38	l .	Į.	1	f	-1.46
3	1	-0.78		l	l .			i .	l .			1	-1.31
4	ł			l .	l			-1.18	1		0.06		-1.03
								}					
5	-0.11	-0.14		1	-1.45	1	Į.	-1.01		0.01	0.24		-0.69
6	-0.09		-0.57	l	1	1	l	-0.7 8		0.14	0.31	ľ	-0.34
7	-0.06	0.32	0.01	0.06	-0.34	-0.01	-0.34	1	0.08	0.22	0.36	Į.	-0.01
8	-0.05	0.43	0.44	0.78	0.20	0.51	0.07	-0.16	0.26	0.25	0.38	0.11	0.27
9	-0.03	0.50	0.76	1.35	0.74	0.92	0.50	0.24	0.38	0.26	0.38	0.10	0.51
10	-0.02	0.51	0.99	1.74	1.28	1.26	0.90	l .	0.44	0.26		0.10	0.71
11	0.02	0.52	1.19	1.95	1.82	1.63	1.20	1.01	0.48	0.26	0.28	0.09	0.87
Midn	0.05	0.49	1.38	2.08	2.30	2.04	1.59	1.25	0.51	0.28	0.15	0.12	1.02
								İ					
6. 6	0.01	0.20	0.83	0.40			-0.09	J	0.15	0.21	0.09	0.02	0.15
7. 7	0.02	0.31	0.89	0.44			-0.04	1	0.18	0.20	0.17	0.02	0.18
8.8	0.02	0.33	0.71	0.36		-0.04	0.02	0.04	0.16	0.13	0.20	0.01	0.16
9. 9	0.02	0.28	0.35	0.19		-0.04	0.07	0.07	0.13	0.03	0.17	-0.00	0.10
10.10	-0.00	0.13	-0.12	-0.04	-0.13	-0.04	0.10	0.09	0.01	-0.08	0.11	-0.00	0.00
7. 2. 9	-0.03	-0.06	-0.24	-0.27	-0.52	-0.53	-0.37	-0.21	-0.10	-0.05	0.06	-0.03	-0.20
6. 2. 8	1 1	-0.10	- 1									-0.02	
6. 2.10	1 1	-0.07	1		-0.12				-0.01			-0.02	
6. 2. 6	1	-0.20										-0.03	
7. 2		-0.35		- 1					1				
8. 2	1 1	-0.38											
8. 1	1 1	-0.40	,	- 1				-0.55			1		1
7. 1	-0.01	-0.37	-0.81	-1.11	-1.16	-1.19	-0.72	-0.42	-0.33	-0.26	-0.16	-0.11	-0.55
9.12.3.9	-0.04	-0.28	-1.28	-1.29	-1.27	-1.12	-0.77	-0.59	-0.37	-0.25	-0.01	-0.06	-0.61
7. 2.2(9)	-0.03	0.08	0.01				-0.15		0.02	0.03		-0.00	1
` '			1			1							
Dail.ext.	-0.02	-0.25	-0.50	-0.37	0.05	0.04	-0.04	-0.02	-0.14	-0.18	0.03	-0.01	-0.16

N. AMERICA. — LAKE ATHABASCA. Lat. 59° N. Long. 111° W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Lefroy.

The corrections for April and May are derived from observations made at Fort Simpson, Lat. 62° N.

Degrees of Fahrenheit.

Hour.	April.	May.	October.	November.	December.	January.	February.
daily ext.	1.58	1.71	0.33	0.25	-0.17	0.77	1.19
6, 6	1.15	0.51	1.07	0.59	0.27	0.84	1.19
7, 7	1.50	0.16	0.76	0.54	0.30	0.58	1.31
8,8	1.72	0.18	0.69	0.55	0.62	0.95	1.27
9, 9	0.54	0.30	0.37	0.32	0.84	0.80	0.78
10, 10	-0.43	-0.08	-0.32	-0.06	0.34	0.12	0.31
11, 11	-1.68	-1.20	-0.57	-0.37	0.10	-0.62	-0.23
6, 2, 10	0.47	0.46	-0.31	-0.21	-0.22	-0.17	-0.05
7, 3, 11	0.46	0.59	-0.40	-0.16	0 17	0.06	-0.26
Mean.	32.48	44.56	21.44	9.76	0.40	-23.00	4.79

XIV.

Arctic America. — Melville Island. Lat. 74° 47′ N. Long. 110° 48′ W. Gr. — Dove.

Degrees of Reaumur.

Hour.	January.	February.	March.	October.	Hour.	November.	December.
A.M. 1	0.12	0.10	1.04	0.04	A.M. 2	-0.12	-0.09
3	0.18	0.05	1.22	0.12	4	-0.02	-0.06
5	0.07	0.25	0 90	0.24	6	0.00	0.11
7	0.11	0.29	0.57	0.20	8	-0.22	0.07
9	-0.13	-0.24	0.29	-0.15	10	-0.38	0.11
11	-0.35	-0.43	-1.33	-0.46	12	-0.41	0.24
P.M. 1	-0.22	-0.65	-1.72	-0.43	P.M. 2	-0.27	0.14
3	-0.25	-0.52	-1.00	0.22	4	0.16	0.00
5	0.04	0.01	-0.43	-0.24	6	0.27	-0.12
7	0.04	0.24	0.06	-0.10	8	0.38	-0.26
9	0.11	0.35	0.33	0.11	10	0.36	-0.12
11	0.40	0.49	0.66	0.43	12	0.25	0.00
Mean.	-29.75	-27.58	-22.73	-14 32	Mean.	-18.65	-25.75

XV.

Spitzbergen. — Hecla Cove. Lat. 79° 55' N. Long. 16° 49' E. Gr. — Dove.

Hour.	June.	July.	August.	Hour.	June.	July.	August.
A.M. 1	0.63	0.62	0.42	P.M. 1	-0.67	-0.67	-0.63
3	0.43	0.84	0.54	3	-0.58	-0.42	-0.58
5	0.26	0.51	0.53	5	-0.27	-0.14	-0.32
7	-0.12	-0.02	0.25	7	0.26	-0.17	-0.06
9	-0.29	-0.09	-0.09	9	0.21	0.06	0.14
11	-0.47	-0.49	-0.45	11	0.61	0.26	0.24
				Mean.	1.71	3.63	2.84

S. AMERICA. — RIO JANEIRO. Lat. 22° 54′ S. Long. 43° 16′ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

								,					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.74	1.51	1.80	0.90	1.13	0.56	1.85	1.31	1.04	0.97	1.76	1.31	1.24
2	1.64	2.41	2.48	1.64	2.12	1.53	2.75	2.00	1.69	1.64	2.32	2.05	2.03
3	2.50	3.11	3.02	2.32	2.93	2.43	3.47	2.66	2.27	2.21	2.75	2.66	2.70
4	3.08	3.90	3.24	2.79	3.38	3.04	3.87	3.04	2.59	2.50	2.93	2.99	3.06
5	3.22	3.29	3.15	2.90	3.40	3.29	3.83	3.08	2.66	2.52	2 79	2.99	3.08
6	2.93	2.84	2.75	2.75	3.06	3.20	3.47	2.79	2.41	2.27	2.32	2.68	2.79
7	2.30	2.21	2.14	2.30	2.48	2.84	2.70	2.25	2.00	1.82	1.67	2.12	2.23
8	1.49	1.49	1.40	1.71	1.85	2.39	1.96	1.60	1.46	1.28	0.90	1.40	1.58
9	0.68	0.72	0.59	1.04	1.15	1.82	1.15	0.90	0.86	0.68	0.14	0.59	0.86
10	-0.07	-0.05	-0.23	0.32	0.50	1.13	0.32	0.23	0.18	0.05	-0.56	-0.23	-0.14
11	-0.77	-0.86	-1.01	-0.45	-0.23	0.32	-0.50	-0.50	-0.54	-0.59	-1.22	-1.04	-0.61
Noon. · ·	-1.40	-1.64	-1.71	-1.22	-0.99	-0.65	-1.31	-1.19	-1.26	-1.22	-1.80	-1.82	-1.35
1	-2.00	-2.30	-2.30	-1.94	-1.71	-1.67	-2.16	-1.91	-1.89	-1.78	-2.32	-2.43	-2.03
2	-2.41	-2.75	-2.66	-2.41	-2.30	-2.48	-2.88	-2.48	-2 34	-2.16	-2.66	-2.81	-2.52
3	-2.59	-2.88	-2.84	-2.66	-2.66	-2.99				-2.27		-2.86	-2.77
4	-2.45	-2.70	-2.77	-2.57	-2.75	-3.04	-3.60	-2.93	-2.36	-2.12	-2.66	-2.59	-2.70
5	-2 05	-2.30	-2.50	-2.21	-2.54	-2.75	-3.47	-2.68	-2.00	-1.78	-2.25	-2.09	-2.39
6	-1.51	-1.82	-2.12	-1.76	-2.21	-2.23	-3.04	-2.23	-1.55	-1.37	-1.67	-1.49	-1.91
7	-1.04	-1.40	-1.67	-1.28	-1.89	-1.76	-2.39	-1.67	-1.13	-1.04	-1.08	-0.99	-1.44
8	-0.72	-1.13	-1.22	-0.95	-1.67	-1.42	-1.85	-1.13	-0.83	-0.77	-0.59	-0.61	-1.08
9	-0.59	-0.92	-0.77	-0.72	-1.44	-1.26	-1.22	-0.70	-0.61	-0.61	-0.14	-0.38	-0.79
0	-0.56	-0.63	-0.25	-0.52	-1.13	-1.13	-0.59	-0.32	-0.41	-0.45	0.23	-0.16	-0.50
11	-0.41	-0.14	0.36	-0.25	-0.63	-0.86	0.09	0.09	-0.09	-0.16	0.65	0.14	0.09
Midn	0.00	0.59	1.06	0.23	0.14	-0.29	0.92	0.61	0.38	0.32	1.15	0.65	0.47
c c	0.72	0.70	0.00	0.50	0.40	0.50	0.30	0.00	0.49	0.45	0.34	0.61	0.45
6. 6 7. 7	0.72	0.52	0.32	$0.50 \\ 0.52$	0.43	$0.50 \\ 0.54$	0.30	$0.29 \\ 0.29$	$0.43 \\ 0.45$	0.45	0.34	0.56	0.45
8. 8	0.03	0.41	$0.25 \\ 0.09$	0.38	0.29	0.50	0.16	0.25	0.45	0.41	0.25	0.30	0.25
9. 9	0.05	-0.11	-0.09		0.09 -0.16	0.30	-0.05	0.23	0.14	0.05	0.00	0.11	0.05
10.10	-0.35	-0.34	_0.95	_0.11	_0.99	0.00	-0.14	-0.05	-0.11	-0.20	-0.18	-0.20	-0.18
7. 2. 9		-0.50		1				-0.32				-0.36)
6. 2. 8	I .	-0.34		ĺ			-0.43		-0.32			-0.25	1
6. 2.10		-0.18		-0.07		-0.14	0.00	F	-0.11			-0.09	i
6. 2. 6	-0.34	-0.59	-0.68	-0.47	-0.47	-0.50	-0.81	-0.63	-0.50	-0.43	-0.68	-0.54	-0.56
7. 2	-0.07		-0.27	-0.07	0.09		-0.09	-0.11				-0.36	1
8. 2		-0.63	-0.63	-0.36	-0.23		-0.47		-0.45		-0.88	-0.72	i
8. 1	-0.27		-0.45		0.07			-0.16	i			-0.52	ł
7. 1	0.16	-0.05	-0.09	0.18	0.38	0 59	-0.27	0.18	0.07	0.02	-0.34	-0.16	-0.11
9.12.3.9	1	-1.19			-0.99		-1.19	-0.97	-0 88	-0.86			-1.01
7. 2.2(9)		-0.61			-0.68	-0.54		-0.41		-0.38	-0.32	-0.36	

XVII.

S. America. - Rio Janeiro. Lat. 22° 54' S. Long. 43° 16' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
7.5	Δ 99	0.67	0.00	0.40	0.50	0.05	0.00	A	0.46	0.49	0.50	0.50	0.55
Morn. 1	0.33	0.67	0.80	0.40	0.50	0.25	0.82	i	0.46	0.43	1		0.55
2	0.73	1.07	1.10	0.73	0.94	0.68	1.22	1	0.75	0.73	1		0.90
3	1.11	1.38	1.34	1.03	1.30	1.08	1.54	1	1	0.98		1	1.20
4	1.37	1.51	1.44	1.24	1.50	1.35	1.72	1.35	1.15	1.11	1.30	1.33	1.36
5	1.43	1.46	1.40	1.29	1.51	1.46	1.70	1.37	1.18	1.12	1.24	1.33	1.37
6	1.30	1.26	1.22	1.22	1.36	1.42	1.54	1.24	1.07	1.01	1.03	1.19	1.24
7	1.02	0.98	0.95	1.02	1.10	1.26	1.20	1.00	0.89	0.81	0.74	0.94	0.99
8	0.66	0.66	0.62	0.76	0.82	1.06	0.87	0.71	0.65	0.57	0.40	0.62	0.70
9	0.30	0.32	0.26	0.46	0.51	0.81	0.51	0.40	0.38	0.30	0.06	0.26	0.38
10	-0.03	-0.02	-0.10	0.14	0.22	0.50	0.14	0.10	0.08	0.02	-0.25	-0.10	0.06
11	-0.34	-0.38	-0.45	-0.20	-0.10	0.14	-0.22	-0.22	-0.24	-0.26	-0.54	-0.46	-0.27
Noon	-0.62	-0.73	-0.76	-0.54		-0.29	i	1	-0.56		-0.80	-0.81	-0.60
1	-0.89	-1.02	-1.02	-0.86	-0.76	-0.74	-0.96	-0.85	-0.84	-0.79	-1.03	-1.08	-0.90
2	11			-1.07			ì	•	1		l	1	
3				-1.18			ı	1	l .		1	1	
	1			-1.14			l .	1	l .	1	1	1	1 1
1 4	-1.03	-1.20	-1.23	-1.14	-1.22	-1.00	-1.00	-1.50	-1.03	-0.94	-1.10	-1.15	-1.20
5	-0.91	-1.02	-1.11	-0.98	-1.13	-1.22	-1.54	-1.19	-0.89	-0.79	-1.00	-0.93	-1.06
6	-0.67	-0.81	-0.94	-0.78	-0.98	-0.99	-1.35	-0.99	-0.69	-0.61	-0.74	-0.66	-0.85
7	-0.46	-0.62	-0.74	-0.57	-0.84	-0.78	-1.06	-0.74	-0.50	-0.46	-0.48	-0.44	-0.64
8	-0.32	-0.50	-0.54	-0.42	-0.74	-0.63	-0.82	-0.50	-0.37	-0.34	-0.26	-0.27	-0.48
9	-0.26	-0.41	-0.34	-0.32	-0.64	-0.56	-0.54	-0.31	-0.27	-0.27	-0.06	-0.17	-0.35
10				-0.23			l				l .	-0.07	1 1
11		-0.06		-0.11			0.04				0.29	i	1
Midn	0.00	0.26	0.47	0.10		-0.13	0.41	0.27	0.17	0.14	0.51	0.29	0.21
Midit	0.00	0.20	0.47	0.10	0.00	-0.13	0.41	0.27	0.17	0.14	0.51	0.23	0.21
6. 6	0.32	0.23	0.14	0.22	0.19	0.22	0.10	0.13	0.19	0.20	0.15	0 27	0.20
7. 7	0.32	0.18	0.11	0.23	0.13	0.24	0.07	0.13	0.13	0.18	0.13	0.25	0.18
8. 8	0.17	0.18	0.04	0.23	0.13		0.03	0.13	0.20	0.13	0.13	0.23	0.13
()						0.22						ļ.	1
9. 9	0.02	-0.05	-0.04	0.07	-0.07	0.13	-0.02	0.05	0.06		-0.00	0.05	0.02
10.10	-0.14	-0.15	-0.11	-0.05	-0.14	-0.00	-0.06	-0.02	-0.05	-0.09	-0.08	-0.09	-0.08
7. 2. 9	-0.10	-0.22	-0.19	-0.12	-0.19	-0.13	-0.21	-0.14	-0.14	-0.14	-0.17	-0.16	-0.16
6. 2. 8	1			-0.09								1	-0.12
6. 2.10	-0.01	-0.08	-0.02	-0.03	-0.05	-0.06	-0.00	-0.00	-0.05	-0.05	-0.02	-0.04	-0.03
6. 2. 6	-0.15	-0.26	-0.30	-0.21	-0.21	-0.22	-0.36	-0.28	-0.22	-0.19	-0.30	-0.24	-0.25
7. 2	-0.03	-0.12	-0.12	-0.03	0.04	0.08	-0.04	-0.05	-0.08	-0.08	-0.22	-0.16	-0.07
8. 2	-0.21	-0.2 S	-0.28	-0.16	-0.10	-0.02	-0.21	-0 20	-0.20	-0.20	-0.39	-0.32	-0.21
8. 1			-0.20		0.03	0.16			1			-0.23	
7. 1		-0.02		0 08	0.17	0.26	0.12			1	-0.15		0.05
9.12.3.9				-0.40 -0.17								-0.50	-0.45
7. 2.2(9)	-0.14	-0.27	-0.23	-0.17	~0.30	-0.24	-0.29	-0.18	-0.17	-0.17	-0.14	-0.16	-0.21
Dail.ext.	0.14	0.12	0.09	0.06	0.15	0.06	0.06	0.04	0.04	0.06	0.03	0.03	0.07

N. America. — Amherst College. — Lat. 42° 22' N. Long. 72° 30' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dewey.

Degrees of Fahrenheit.

Degrees of Panremert.													
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Morn. 1	3.90	2.78	4.73	6.23	5.51	6.64	6.39	5.14	5.36	4.87	2.34	1.63	4.63
2	4.24	3.03	4.81	6.69	6.48	7.28	6.83	5.66	6.12	5.65	2.99	2.20	5.16
3	4.13	3.20	5.36	7.42	7.41	7.92	7.28	6.03	6.92	6.46	3.49	2.55	5.68
4	4.50	3.94	5.69	7.85	7.88	8.04	7.42	6.29	6.56	7.09	3.72	2.70	6.06
5	4.72	4.20	6.04	8.12	8.18	7.80	7.54	6.66	7.88	7.72	4.03	3.32	6.35
6	4.68	4.78	6.12	7.77	6.77	5.96	6.02	5.81	7.44	7.65	4.34	3.78	5.93
7	4.75	4.78	4.62	5.97	4.22	4.20	3.80	4.48	5.32	6.87	4.28	3.97	4.77
8	3.83	3.78	2.08	3.04	1.62	1.40	1.09	1.96	2.52	4.31	2.68	4.13	2.70
			1		l				1		1		
9	1.46	1.45	-0.46	0.08	-0.60	-0. SS	-0.87	-0.93	-0.56	0.83	0.34	2.40	0.19
10	-1.26	-0.85	-2.57	- 2.69	-1.12	-3.12	-3.80	-3.04	-3.32	-2.24	-1.43	-0.55	-2.34
11	-4.10	-2.72	-4.77	- 5.65	-5.12	-5.68	-6.43	-5.45	-6.04	-5.02	-3.01	-2.76	-4.73
Noon.	-6.32	-4.26	-6.38	- 7.9 2	-6.75	-8.08	-8.50	-6.86	-8.16	-7.06	-5.01	-4.30	-6.63
	,									1			
1	-7.46	-5.35	-7.6 5	- 9.46	5	-9.36	-8.83	-8.23		-8.24	-6.12	-6.14	-7.84
2	-7.SO		-8.34	-10.42	1	-9.00	-9.50	-7. 86	1	1	-5.97	-6.30	-8.26
3	-7. 32	-5.80	-8.11	- 9.81	-8.27	-8.60	-7.50	-7.67	-9.20	-9.24	-5.28	-5.60	II.
4	-5.84	-4.89	-7. 23	- 8.61	-7.86	-7.84	-7.17	-6.23	-8.40	-8.24	-3.85	-3.76	-6.66
_	0.00						.				2.00	0.00	
5	-3.32	-3.10	-5.65	- 7.04	l	-6.00	-5.83	-5.26	-6.44	-5.65	-2.28	-2.03	-4.88
6	-2.06	-1.18	-3.46	- 4.50	l	-4.20	-4.17	-2.82	-3.52	-3.50	-0.85	-0.68	-2.92
7	0.24	-1.05	0.17	- 1.69	-2.38	-1.92	-1.54	-1.44	-1.47	-1.24	-0.64	-0.31	-1.11
8	0.64	-0.43	0.93	0.27	-0.19	0.04	0.98	0.33	0.11	0.13	0.08	0.20	0.26
9	1.50	0.28	1.89	1.77	1.66	1.96	3.05	1.59	1.99	1.16	0.80	0.69	1.53
10	2.01	0.57	3.29	3.31	2.73	3.20	3.79	3.02	3.53	1.90	1.16	1.20	2.48
11	2.42	1.19	4.29	4.23	3.99	4.20	4.24	3.79	4.61	3.24	1.96	1.58	3.31
Midnight.	2.50	1.70	4.85	4.92	4.75	5.48	5.31	4.52	5.34	4.09	2.40	1.98	3.99
		1	1.00	1.02	1.,,	0.10	0.01	1.02	0.01	1.00	2.10	1.00	0.00
3, 9, 3, 9	-0.05	-0.22	-0.08	- 0.13	0.05	0.10	0.49	0.26	-0.21	-0.20	-0.16	-0.01	-0.01
9,9	1.48	0.87	0.72	0.93	0.53	0.54	1.09	0.33	0.72	1.00	0.57	1.55	0.86
10, 10	0.38	-0.14	0.36	0.31	0.81	0.04	0.00	-0.51	0.11	-0.17	-0.13	0.33	0.12
7, 2, 9	-0.48	-0.33	-0.61	- 0.89	-0.96	-0.95	-0.88	-0.60	-0.83	-0.42	-0.29	-0.55	-0.65
												l	
6, 2, 10	-0.37	-0.24	0.36	- 0.24	0.25	0.05	0.10	0.32	0.39	0.09	-0.16	-0.44	0.01
7, 2, 10	-0.35	-0.04	-0.14	- 0.38	-0.60	-0.53	-0.64	-0.12	-0.32	-0.17	-0.18	-0.38	-0.32
7, 2, 11	-0.21	-0.03	0.19	- 0.07	-0.18	-0.20	-0.49	0.14	0.04	0.28	0.09	-0.25	-0.07
6, 8, 2 4, } 10, 12 }	-0.09	0.02	0.13	0.00	-0.12	-0.13	-0.08	0.20	0.11	0.07	0.13	0.17	0.03
7,2,2,(9)	-0.01	-0.18	0.01	- 0.23	-0.30	-0.22	0.10	-0.05	-0.12	-0.02	-0.02	-0.24	-0.11
76			2 . 2										
Mean.	22.94	28.57	34.81	48.54	56.92	61.60	71.61	67.44	59.80	50.46	34.80	29.28	47.23

The numbers without sign must be added; those with the sign - must be subtracted.

The above Table has been derived from one year of hourly observations made at Amherst College, Massachusetts, in 1839, under the direction of Professor Snell, and communicated by Professor Chester Dewey. It gives the simple differences of the monthly means of each hour from the monthly means of the twenty-four hours which are found in the last line.

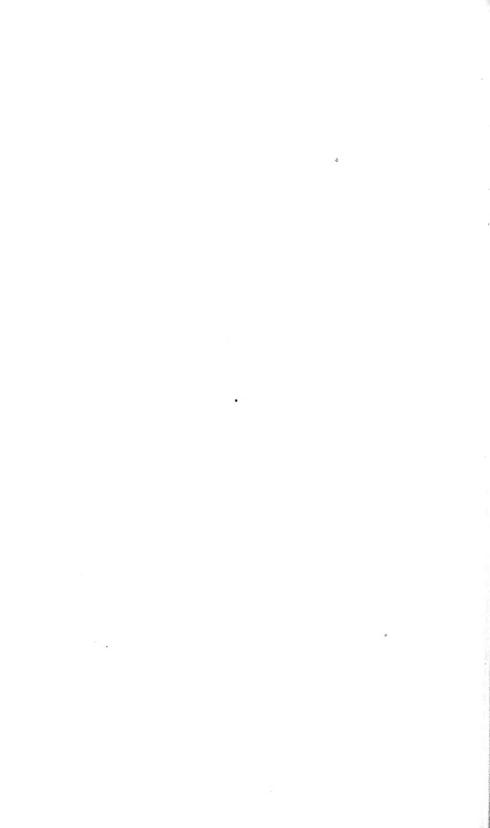
HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

ASIA.

 \mathbf{E}



XVIII.

India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

Degrees of Fahrenheit.													
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	4.41	4.03	3.80	3.85	3.26	2.66	2.41	2.88	2.99	3.06	3.33	4.25	3.42
2	5.13	4.95	4.64	4.46	3.80	3.02	2.75	3.24	3.44	3.44	3.83	4.86	3.96
3	6.03	6.12	5.67	5.15	4.39	3.47	3.17	3.74	3.98	3.92	4.46	5.67	4.66
4	6.95	7.31	6.64	5.74	4.82	3.80	3.58	4.21	4.48	4.34	5.04	6.50	5.29
5	7.56	8.15	7.13	5.81	4.82	3.83	3.76	4.41	4.61	4.46	5.22	6.93	5.56
6	7.34	8.01	6.73	5.11	4.14	3.35	3.49	4.07	4.14	4.01	4.73	6.57	5.15
7	6.01	6.59	5.20	3.53	2.81	2.34	2.68	3.06	3.02	2.88	3.40	5.11	3.89
8	3.56	3.92	2.66	1.22	0.95	0.90	1.35	1.49	1.26	1.13	1.40	2.70	1.87
	0.50	0.02	2.00	1.22	0.55	0.50	1.00	1.43	1.20	1.10	1.40		1.01
9	0.41	0.50	-0.47	-1.42	-1.13	-0.74	-0.27	-0.45	-0.81	-0.99	-0.92	-0.29	-0.54
10	-2.84	-2.97	-3.53	-3.89	-3.04	-2.30	-1.91	-2.41	-2.86	-3.06	-3.11	-3 24	-2.93
11	-5.51	-5.85	-5.94	-5.76	-4.48	-3.53	-3.33	-4.05	-4.50	-4.73		-5.58	-4.84
11	ì	-7.5 8		-6.82				-5.1S				-7.00	-6.01
												ŀ	
1	-7.92	-S.17	-7.72	-7.04	-5.60	-4.68	-4.79	-5.69	-5.87	-5.94	-5.90	-7.49	-6.41
2 -	-7.76	-7. 83	-7.22	-6.59	-5.38	-4.61	-4.77	-5.60	-5.60	-5.54	-5.60	-7.25	-6.14
3 -	-7.09	-6.98	-6.26			: 1	1	-5.04		1	1		-5.45
4 -	-6.17	-5.99	-5.06			-3.47				-3.53	1	1	-4.48
					,								
5 -	-5.15	-4.88	-3.83	-3.11	-2.88	-2.52	-2.52	-2.90	-2.59	-2.32	-3.15	-4.61	-8.38
6 -	-3.92	-3.74	-2.57	-1.71	-1.69	-1.42	-1.40	-1.58	-1.31	-1.10	-2 03	-3.35	-2.16
7 -	-2.50	-2.45	-1.31	-0.34	-0.50	-0.32	-0.29	-0.27	-0.11	0.00	-C-S1	-1.89	-0.90
8 -	-0.92	-1.04	-0.07	0.92	0.63	0.70	0.68	0.90	0.92	0.97	0.38	-0.32	0.32
9	0.68	0.38	1.06	1.91	1.53	1.46	1.40	1.76	1.69	1.71	1.42	1.19	1.35
10	2.05	1.64	1.96	2.61	2.16	1.96	1.85	2.30	2.18	2.25	2.21	2.43	2.14
11	3.08	2.57	2.63	3.06	2.57	2.23	2.09	2.54	2.48	2.57	2.68	3.26	2.66
Midn	3.83	3.31	3.17	3.42	2.88	2.41	2.23	2.68	2.70	2.81	2.99	3.80	3.02
6. 6	1.71	2.14	2.09	1.71	1.24	0.97	1.04	1.24	1.42	1.46	1.35	1.60	1.51
7. 7	1.76	$\frac{2.14}{2.07}$	1.96	1.60	1.17	1.01	1.19	1.40	1.44	1.44	1.28	1.62	1.49
11	- 1	1		i 1				1 1	1.08	1.06	0.88	1.19	1.10
8. 8	1.33	1.44	1.31	1.06	0.79	0.79	1.01	1.19				1	
9. 9	0.54	0.43	0.29	0.25	0.20	0.36	0.56	0.65	0.43	0.36	0.25	0.45	0.41
10.10	-0.41	-0.65	-0.79	-0.63	-0.45	-0.18	-0.02	-0.07	-0.34	-0.41	-0.45	-0.40	-0.41
7. 2. 9	-0.36	-0.29	-0.32	-0.38	-0.34	-0.27	-0.23	-0.27	-0.29	-0.32	-0.27	-0.32	-0.32
	-0.45	-0.29	-0.18	-0.18	-0.20	1 1	-0.20		-0.18		-0.16	1	-0.23
6. 2.10	0.54	0.61	0.50	0.38	0.32	0.23	0.18	0.25	0.25	0.25	0.45	0.59	0.38
11	1	-1.19	-1.01			1	-0.90	1		-0.88	-0.97	l .	-1.06
7. 2	-0.88	-0.63	-1.01	-1.53	-1.28	-1.15	-1.06	-1.28	-1.31	-1.33	-1.10	-1.08	-1.13
	-2.12					-1.87				-2.21			-2.14
8. 1	-2.18	-2.14	-2.54	-2.93	-2.34	-1.89	-1.73	-2.12	-2.32	-2.41	-2.25	-2.41	-2.27
7. 1	-0.97							-1.33				-1.19	-1.26
0.10.00	0.07	0.40	0.00	0.00	0.40	1 00	1.00	0.00	0.00	0.4-	0	9.1*	9 00
الدما	-3.31	-3.42	-3.26		-2.43			-2.23			}	-3.17	-2.66
7. 2.2(9)	-0.11	-0.11	0.02	0.20	0.14	0.16	0.18	0.25	0.20	0.20	0.16	0.07	0.11

XIX.

India. — Trevandrum. Lat. 8° 31' N. Long. 74° 50' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.													
Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	1.96	1.79	1.69	1.71	1.45	1.18	1.07	1.28	1.33	1.36	1.48	1.89	1.52
III .	2.28	1	1	1	1	1	1	1	1	1		i	1
2	11		1		1			1	1		1	1	1
3	2.68	1	1	1		1	1.41	1.66	1		1	1	j .
4	3.09	3.25	2.95	2.55	2.14	1.69	1.59	1.87	1.90	1.93	2.24	2.89	2.35
5	3.36	3.62	3.17	1	1	1.70	1.67	1.96	2.05	1.98	2.32	3.08	2.47
6	3.26	3.56	2.99	2.27	1.85	1.49	1.55	1.81	1.84	1.78	2.10	2.92	2.29
7	2.67	2.93	2.31	1.57	1.25	1.04	1.19	1.36	1.34	1.28	1.51	2.27	1.73
8	1.58	1.74	1.18	0.54	0.42	0.40	0.60	0.66	0.56	0.50	0.62	1.20	0.83
9	0.18	0.22	-0.21	-0.63	-0.50	-0.33	-0.12	-0.20	-0.36	-0.44	-0.41	-0 13	-0.24
10	-1.26	-1.32	-1.57	-1.73	-1.35	-1.02	-0.85	-1.07	-1.27	-1.36	-1.38	-1.44	-1.30
11	-2.45	-2.60	-2.64	-2.56	-1.99	-1.57	-1.48	-1.80	-2.00	-2.10	-2.11	-2.48	-2.15
Noon	11	-3.37			-2.37				1		-2.52		-2.67
		0.00				2.00	2.0		2 02				
1	-3.52			6	-2.49	i			1	1	1	-3.33	
2		-3.48											
3		-3.10	1	4		1	l .	1	1	1	1		1 1
4	-2.74	-2.66	-2.25	-1.98	-1.75	-1. 54	-1 56	-1.82	-1.69	-1.57	-1.83	-2.52 	-1.99
5	-2.28	-2.17	-1.70	-1.38	-1.28	-1.12	-1.12	-1.29	-1.15	-1.03	-1.40	-2.05	-1.50
6	-1.74	-1.66	-1.14	-0.76	-0.75	-0.63	-0.62	-0.70	-0.58	-0.49	-0.90	-1.49	-0.96
7	-1.11	-1.09	-0.58	-0.15	-0.22	-0.14	-0.13	-0.12	-0.05	0.00	-0.36	-0.84	-0.40
8	-0.41	-0.46	-0.03	0.41	0.28	0.31	0.30	0.40	0.41	0.43	0.17	-0.14	0.14
9	0.30	0.17	0.47	0.85	0.68	0.65	0.62	0.78	0.75	0.76	0.63	0.53	0.60
10	0.91	0.73	0.87	1.16	0.96	0.87	0.82	1.02	0.97	1.00	0.98	1.08	0.95
11	1.37	1.14	1.17	1.36	1.14	0.99	0.93	1.13	1.10	1.14	1.19	1.45	1.18
Midn	1.70	1.47	1.41	1.52	1.28	1.07	0.99	1.19	1.20	1.25	1.33	1.69	1.34
Midn	1.70	1.41	1.41	1.02	1.20	1.07	0.55	1.13	1.20	1.20	1.00	1.03	1.01
6. 6	0.76	0.95	0.93	0.76	0.55	0.43	0.46	0.55	0.63	0.65	0.60	0.71	0.67
7. 7	0.78	0.55	0.33	0.70	0.52	0.45	0.53	0.62	0.64	0.64	0.57	0.72	0.66
8. 8	0.59	0 64	0.58	0.47	0.35	0.35	0.45	0.53	0.48	0.47	0.39	0.53	0.49
9. 9	0.24	0.19	0.13	0.11	0.09	0.16	0.25	0.29	0.19	0.16	0.11	0.20	0.18
10.10	-0.18	-0.29	-0.35	-0.28		-0.08	-0.01	-0.03		-0.18			-0.18
		ļ											İ
7. 2. 9	-0.16				-0.15						-0.12		i
6. 2. 8	-0.20	-0.13	-0.08	-0.08	-0.09	-0.08	-0.09	-0.09	-0.08	-0.08	-0.07	-0.15	-0.10
6. 2.10	0 24	0.27	0.22	0.17	0.14	0.10	0.08	0.11	0.11	0.11	0.20	0.26	0.17
6. 2. 6	-0.64	-0.53	-0.45	-0.47	-0.43	-0.40	-0.40	-0.46	-0.41	-0.39	-0.43	-0.60	-0.47
7. 2	-0.39	-0.28	-0.45	-0.68	-0.57	-0.51	-0.47	-0.57	-0.58	-0.59	-0.49	-0.48	-0.50
8. 2		-0.87											13
8. 1	-0.97			- 1	-1.04		1	- 1			- 1		, ,
7. 1		-0.35	1	- 1		1				1	- 1		11
0.70.5.5													,
9.12.3.9	-1.47		-1.45		-1.08	- 1	4	- 1			-1.13 0.07	0.03	-1.18 \parallel 0.05 \parallel
7. 2.2(9)	-0.05	-0.03	0.01	0.09	0.06	0.07	0.08	0.11	0.09	0.09	0.07	0.03	0.00
Dail. ext.	-0.08	-0.01	-0.13	-0.28	-0.18	-0.19	-0.23	-0.29	-0.28	-0.33	-0.15	-0.13	-0.19

India. - Madras. Lat. 13° 4′ N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

						es of F							
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	2.05	2.54	2.25	3.65	2.74	3.03	2.90	2.86	2.34	1.84	2.05	1.89	2.50
1	2.54	3.26	2.90	3.08	3.31	3.50	3.10	3.01	2.70	2.27	2.54	2.25	2.87
2	2.96	3.95	3.60	3.57	3.72	3.86	3.55	3.39	3.10	2.79	3.03	2.63	3 35
3	3.33	4.52	4.25	4.07	4.07	4.27	3.93	3.69	3.55	3.12	3.50	2.96	3.77
4	3.62	5.06	4.79	4.40	4.45	4.68	4.31	3.98	3.95	3.46	3.91	3.19	4.15
5	3.81	5.49	5.24	4.45	4.68	4.95	4.66	4.34	4.23	3.71	4.23	3.60	4.45
6	4.05	5.64	5.11	3.78	3.86	4.21	4.31	4.07	3.82	3.28	4.05	3.73	4.16
7	2.43	3.33	2.54	1.78	2.07	2.51	2.92	2.79	2.43	1.80	2.00	2.38	2.41
s	-0.04	0.29	0.16	-0.18	-0.11	0.38	1.06	0.99	0.72	0.13	-0.56	0.00	0.23
9	-2.02	-1.93	-1.89	-2.11	-2.43	-1.73	-0.76	-0.90	-1.12	-1.26	-2.49	-1.73	-1.72
10	-3.26	-3.60	-3.67	-4.14	-4.68	-3.67	-2.67	-2.74	-2.96		-3.53	-3.05	-3 36
11	-4.02	-4.81	-4.81	-4.83	-5.75	-5.02	-4.25	-4.16	-4.54	-3.17	-4.09	-2.62	-4.42
Noon.	-4.43	-5.06	-5.35	-5.66	-5.87	-5.S5	-5.51	-5.28	-5.04	-3.76	-4.31	-3.93	-5.01
1		-5.35	1				4	-5.75		-3.73			
2		-5.30					1	-5.40	ì	-3.55		-3.60	
3	-3.46	-4.85	-4.27	-4.07	-4.00	-4.61	-4.92	-4.59	-3.73	-3.03	-3.05	-2.88	-3.95
4		-3.64						1	-2.56		-1.98	-2.04	-2.83
5		-2.27			-1.01	-1.91	-2.18	-1.84	-1.44	-1.26	-0.88	-1.01	-1.47
6	-0. 38	-1.10	-0.52	0.20	0.11	-0.58	-0.81	-0.70	-0.52	-0.63	-0.25	-0.38	-0.46
7	0.09	-0.36	0.17	0.83	0.76	0.36	0.16	0.13	0.07	-0.18	0.09	0.00	0.18
8	0.54	0.27	0.58	0.99	1.19	0.97	0.83	0.74	0.47	0.16	0.47	0.34	0.63
9	0.94	0.81	0.97	1.57	1.57	1.42	1.35	1.17	0.99	0.49	0.74	0.67	1.06
10	1.39	1.33	1.39	1.89	1.96	2.11	1.87	1.64	1.39	0.90	1.08	1.03	1.50
11	1.84	1.87	1.84	2.25	2.34	2.41	2.29	2.14	1.89	1.28	1.46	1.44	1.92
6 6	1.83	2.27	2.29	1.99	1.98	1.81	1.75	1.65	1.65	1.32	1.90	1.67	1.84
6, 6 7, 7	1.26	1.48	1.35	1.30	1.41	1.43	1.54	1.46	1.05	0.81	1.04	1.07	1.29
7, 7 8, 8	0.25	0.28	0.37	0.40	0.54	0.67	0.94	0.81	0.59	0.31	-0.04	0.17	0.43
9, 9	-0.54	1 1	-0.46		-0.43	-0.15	0.29	0.13	-0.06		-0.87	-0.53	-0.33
10, 10	-0.93	-1.13	-1.14	-1.12	-1.36	-0.78	-0.40	-0.55	-0.78	-0.70	-1.22	-1.01	-0.93
7, 1		-1.01			- 1		-1.57		-1.30			-0.74	-1.33
7, 2, 9		-0.39		-0.53		1	-0.58		-0.41			-0.18	-0.43
6, 2, 10	0.43	0.56	0.50	0.24	0.28	0.21	0.05	0.10	0.18	0.21	0.47	0.39	0.30
Mean.	76.77	78.25	82.24	85.73	87.10	87.01	86.22	84.51	83.50	81.18	78.53	76.75	

XXI.

India. — Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hours.	Jan.	E.L	Degrees of Reaumur.													
		Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.			
		- 00														
Morn. 1	1.41	1.22	1.32	1.06	1.26	1.15	0.93			1		1.38	1.17			
2	1.79	1.64	1.42	1.36	1.59	1.42	1.09	Į.		1.46			1.46			
3	2.14	2.10	1.50	1.76	1.94	1.70	1.26		1.67	1	1	1	ĺ			
4	2.38	2.42	1.58	2.10	2.17	1.90	1.42	1.66	1.70	1.88	1.90	1.93	1.92			
5	2.42	2.43	1.61	2.20	2.18	1.95	1.42	1.45	1.62	1.88	2.02	2.17	1.95			
6	2.22	2.05	1.48	1.91	1.86	1.77	1.33	1.10	1.39	1.64	1.81	2.25	1.73			
7	1.76	1.30	1.14	1.24	1.19	1.30	1.12	0.75	1.02	1.14	1.27	2.00	1.27			
8	1.05	0.36	0.54	0.30	0.27	0.70	0.78	0.46	0.47	0.40	0.50	1.32	0.60			
9	0.15	-0.59	-0.23	-0.71	-0.75	-0.06	0.35	0.16	-0.23	-0.46	-0.35	0.27	-0.20			
10 -	-0.82	-1.38	-1.04	-1.56				-0.18	ł)	-1.00			
	i i						i	-0.62	l	l	ì					
11								-1.12			-2.12)	-2.14			
1 -	2.00	9.94	2.10	0.24	0.40	9.90	0.70	-1.57	0.47	0.15	0.0-	0.00	-2.33			
11 11			-2.10 -1.88		- 1						i					
11 11			1					-1.82					, ,			
11	- 1		-1.52	1				-1.77								
4 -	-2.14	-1.S1	-1.14	-1.40	-1.11	-1.74	-2.12	-1.43	-1.12	-1.08	-1.61	-1.65	-1.55			
5 -	-1.47	-1.34	-0.83	-1.00	-0.65	-1.28	-1.44	-0.94	-0.50	-0.70	-1.10	-1.13	-1.03			
6 -	-0.81	-0.78	-0.58	-0.48	-0.27	-0.78	-0.65	-0.46	-0.06	-0.38	-0.58	-0.72	-0.55			
7 -	-0.26	-0.18	-0.35	0.04	0.02	-0.30	0.08	-0.14	0.18	-0.14	-0.14	-0.39	-0.13			
8	0.13	0.30	-0.0s	0.49	0.26	0.12	0.62	-0.04	0.27	0.06	0.36	-0.06	0.20			
9	0.38	0.62	0.42	0.71	0.45	0.42	0.86	-0.06	0.33	0.26	0.64	0.30	0.44			
10	0.58	0.77	0.60	0.90	0.61	0.63	0.91	1	0.44	0.46	0.81	0.66	0.61			
11	0.79	0.84	0.91	0.91	0.78	0.79	0.87	0.11	0.66	0.67	0.83	0.99	0.76			
Midn	1.06	0.96	1.16	0.92	0.98	0.94	0.84	0.47	0.95	0.91	0.89	1.22	0.94			
Minn	1.00	0.50	1.10	0.02	0.50	0.51	0.04	0.11	0.00	0.01	0.00	1.22	0.01			
6. 6	0.71	0.64	0.45	0.72	0.80	0.50	0.34	0.32	0.67	0.63	0 62	0.77	0.60			
7. 7	0.75	0.56	0.40	0.64	0.61	0.50	0.60	0.31	0.60	0.50	0.57	0.81	0.57			
8.8	0.59	0.33	0.23	0.40	0.27	0.41	0.70	0.21	0.37	0.23	0.43	0.63	0 40			
9. 9	0.27	0.02	0.10	-0.00	-0.15	0.18	0.61	0.05	0.05	-0.10	0.15	0.29	0.12			
10.10	-0.12	-0.31	-0.22	-0.33	-0.53	-0.10	-0.35	-0.12	-0.29	-0.40	-0.15	-0.14	-0.20			
7. 2. 9	-0.28	-0.13	-0.11	-0.06	-0.16	-0.17	-0.16	-0.38	-0.31	-0.17	-0.09	-0.15	-0.18			
	-0.21	1	-0.16	0.09				-0.25			-0.01					
	-0.06	0.17	0.07	0.22	0.11	0.05	-0.08	-0.26		0.06	0.15	0.05	0.03			
11		1	-0.33		- 1	1		-0.39			-0.32	-0.41	-0.36			
7. 2	-0.61	_0.50	-0.27	-0.15	-0.17	_0 47	_0 60	-0.54	-0.69	-0.20	-0.16	-0.38	-0.50			
11 11				- 1	1			-0.68								
11			1					-0.56					-0.87			
1à II								-0.30 -0.41	- 1							
	1		- 1					ł								
1				1			1	-0.70								
7. 2.2(9)	-0.11	0.06	0.03	0.13	-0.01	-0.03	0 09	-0.30	-0.15	-0.06	0.09	-0.04	-0.03			
Dail.ext.	-0.28	0.05	-0.25	-0.08	-0.20	-0.15	-0.53	-0.08	-0.39	-0.15	-0.12	-0.37	-0.19			

XXII.

India. — Bombay. Lat. 18° 56′ N. Long. 72° 54′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degree	s of Fal	T CHILCIC						
Hours.	Jan.	Feb.	March.	April.	Мау.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
		7 40	0.00		7 40		0.50	0.05	0.86	1.49	2.03	1.55	1.26
Morn. 1	1.49	1.40	0.99	1.13	1.42	1.15	0.79	0.97			2.18	1.87	1.53
2	1.80	1.69	1.33	1.51	1.78	1.40	0.88	1.13	0.97	1.87			1.91
3	2.27	2.21	1.91	2.05	2.14	1.69	0.90	1.24	1.24	2.32	2.45	2.41	
4	2.86	2.84	2.59	2.48	2.32	1.91	0.90	1.31	1.53	2.75	2.81	3.11	2.27
5	3.47	3.40	3.04	2.61	2.23	1.96	0.86	1.31	1.71	2.95	3.11	3.78	2.54
4	3.83	3.62	3.06	2.34	1.80	1.80	0.79	1.24	1.67	2.79	3.15	4.16	2.52
7	3.69	3.33	2.54	1.67	1.15	1.42	0.65	1.04	1.22	2.21	2.79	4.01	2.14
8	2.97	2.48	1.58	0.77	0.36	0.88	0.38	0.74	0.79	1.28	1.91	3.24	1.44
9	1.69	1.22	0.38	-0.14	-0.41	0.23	0.00	0.32	0.09	0.16	0.63	1.87	0.50
10	0.07	-0.23	-0.77	-0.90	-1.06	-0.43	-0.52	-0.20	-0.65	-0.95	-0.83	0.16	-0.52
11	-1.55		-1.67				-6.08			-1.91	-2.21	-1.60	-1.49
Noon	-2.86	-2.61	-2.30	-1.91	-1.94	-1.64	-1.55	-1.35	-1.80	-2.59	-3.29	-3.08	-2.25
1	-3.69	-3.29	-2.66	-2.25	-2.21	-2.12	-1.82	-1.78	-2.12	-2.99	-3.92	-4.1 0	-2.75
2							-1.78			-3.13		-4.59	
3	-3.85		-2.86							-2.99	-3.85	-4.55	-2.90
4	-3.42	i					-0.92						
_									7.00	0.14	0.61	0.00	0.05
5							-0.38			l .	-2.61	1	ı
6	-2.18	1	1		l .	l .	0.09	-0.72		1	-1.78	į.	ì
7	-1.49	1	1	-0.54	i	ì	0.38	-0.23	ì	l	1	-1.46	l .
8	-0.79	-0.56	-0.07	0.23	0.18	0.14	0.50	0.16	0.47	-0.02	0.00 	-0.52	-0.02
9	-0.11	0.23	0.56	0.72	0 59	0.54	0.54	1.43	0.86	0.52	0.77	0.29	0.50
10	0.47	0.81	0 90	0.92	0.83	0.79	0.54	0.59	0.99	0.88	1.35	0.86	0.83
11	0.92	1.10	0.97	0.92	0.99	0.96	0.61	0.72	0.97	1.08	1.71	1.19	1.01
Midn	1.24	1.26	0 92	0.95	1.15	0.99	0.70	0.83	0.88	1.26	1.91	1.37	1.13
6.6	0.01	0.00	0.00	0.50	0.00	0.04	0.48	0.05	0.15	0.68	0.70	0.86	0.56
6. 6	0.81	$0.68 \\ 0.95$	1	i	I .	$0.34 \\ 0.47$		0.25	$0.45 \\ 0.63$	0.08	1	1.28	1
8. 8	1	1	1	1	1	1	1	l .	1	į.	1		1
9. 9	1.08	1	1	1	1	0.50	1	0.45		0.83	1	1	1
10.10	0.79	$0.72 \\ 0.29$		0.29	1	0.38	1	$0.36 \\ 0.20$	0.47	1	1	0.52	i
10.10	0.27	0.29	0.07	0.00	-0.11	0.18	0.02	0.20	0.18	-0.03	. 0.25	0.52	0.10
7. 2. 9	-0.14	-0.02	0.09	-0.05	-0.20	-0.16	-0.20	-0.18	-0.07	-0.14	-0.18	-0.09	-0.11
6. 2. 8	-0.32	-0.18	0.05	0.02	-0.11		-0.16					-0.32	
6. 2.10	0.11	0.27	0.38	1			-0.16					0.14	0.14
6. 2. 6	-0.79	-0.74	1	-0.52	1	1	-0.29	l .	-0.45	-0.61	-0.90	-0.97	-0.61
7. 2	-0.16	-0.14	-0.16	-0.43	-0.61	-0.50	-0.56	-0.50	-0.52	-0.47	-0.65	-0.29	-0.41
8. 2							-0.70						
8. 1							-0.72						
7. 1	0.00						-0.59						
9.12.3.9	-1.28	-1.22	-1.06	-0.99	-1.01	-0.83	-0.61	-0.65	-0.77	-1.24	-1.44	-1.37	-1.04
7. 2.2(9)	-0.14	0.05	0.20	0.16	1	1	-0.02	1	1	1	1	1	0.05
	<u></u>	<u> </u>		1	1		1	<u> </u>	1	1	1	<u></u>	<u></u>

XXIII.

India. — Bombay. Lat. 18° 56' N. Long. 72° 54' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of R	eaumur	•					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.00	0.60	0.44	0.50	0.00	0.51	0.05	0.40	0.00	0.00	0.00	0.00	0.50
Morn. 1	0.66	0.62	0.44	0.50	0.63	1	0.35	1	1	0.66	\$	i	0.56
2	0.80	0.75	0.59	0.67	0.79	0.62	1				1	0.83	0.68
3	1.01	0.98	0.85	0.91	0.95	0.75		1	1	1	1	1.07	0.85
4	1.27	1.26	1.15	1.10	1.03	0.85	0.40	0.58	0.68	1.22	1.25	1.38	1.01
5	1.54	1.51	1.35	1.16	0.99	0.87	0.38	0.58	0.76	1.31	1.38	1.68	1.13
6	1.70	1.61	1.36	1.04	0.80	0.80	0.35	0.55	0.74	1.24	1.40	1.85	1.12
7	1.64	1.48	1.13	0.74	0.51	0.63	0.29	0.46	0.54	0.98	1.24	1.78	0.95
8	1.32	1.10	0.70	0.34	0.16	0.39	0.17	0.33	0.35	0.57	0.85	1.44	0.64
9	0.75	0.54	0.17	-0.06	-0.18	0.10	-0.	0.14	0.04	0.07	0.28	0.83	0.22
10		-0.10	-0.34	ı		1		1	-0.29	1	-0.37	0.07	-0.23
11	-0.69	-0.69	-0.74	-0.66	-0.69	-0.48	-0.48	-0.35	-0.57	-0.85	-0.98	-0.71	-0 66
Noon	-1.27	-1.16	-1.02	-0.85	-0.86	-0.73	-0.69	-0.60	-0.80	-1.15	-1.46	-1.37	-1.00
1	1.00	-1.46	1 10	_1.00	0.00	0.04	_0.01	0.70	-0 94	1 22	_1 74	-1.82	-1.22
2		-1.40 -1.60			i	1		1	1	Į.	į.	l	1
3		-1.62										-202	-1.29
4		-1.52											
*	1.02	1		1.11	0.00	1.00	0.11	0.10	0.00	1.10	1.10	1.00	1.10
5	-1.26	-1.31	-1.04	-0 .92	-0.7 3	-0.79	-0.17	-0.55	-0.61	-0.95	-1.16	-1.50	-0.92
6	-0.97	-1.01		-0.61	-0.46	-0.51	0.04	-0.32	-0.33	-0.65	l l	1	-0.62
7		-0.64	-0.39		-0.17	!	0.17	-0.10	0.02	-0.32	l .	-0.65	-0.30
\mathbf{s}	-0.35	-0.25	0.03	0.10	0.08	0.06	0.22	0.07	0.21	-0.01	0.	-0.23	-0 01
9	-0.05	0.10	0.25	0.32	0.26	0.24	0.24	0.19	0.38	0.23	0.34	0.13	0.22
10	0.21	0.36	0.40	0 41	0.37	0.35	0.24	0.20	0.44	0.39	0 60	0.38	0.37
11	0.41	0.49	0.43	0.41	0.44	0.40	0.27	0.32	0.43	0.48	0.76	0.53	0.45
Midn	0.55	0.56	0.41	0.42	0.51	0.44	0.31	0.37	0.39	0.56	0.85	0.61	0.50
6. 6	0.36	0.30	0.30	0.22	0.17	0.15	0.19	0.11	0.20	0.30	0.31	0 38	0.25
7. 7	0.49	0.42	0.37	0.25	0.17	0.21	0.23	0.18	0.28	0.33	0.42	0 57	0.33
8. 8	0.48	0.43	0.34	0.22	0.12	0.22	0.20	0.20	0 28	0.28	0.42	0.60	0.32
9 9	0.35	0 32	0.21	0.13	0.04	0.17	0.12	0.16	0.21	0.15	0.31	0.48	0.22
10.10	0.12	0.13	0.03	0.00	-0.05	0.08	0.01	0.09	0.08	-0.02	0.11	0.23	0.07
~ 0 0	-0.06	0.01	001	0.00	0.00	0.0*	0.00	0.00	0.09	0.06	-0.08	-0.04	-0.05
7. 2. 9 6. 2. 8	1 1	-0.08	$\begin{array}{c} 0.04 \\ 0.02 \end{array}$		-0.09 -0.05			-0.08 -0.09				-0.04	-0.05
6. 2.10	0.14	0.12	0.02	0.01	0.04			-0.03	0.06	0.03	0.06	0.06	0.06
6. 2 6	-0.35	-0.33	1					-0.22		-0.27	-0.40	-0.43	-0.27
	0.00	0.00	0.22	0.20	0.20	0.20	0.10	0.22		0.2.			
7. 2	-0.07	-0.06						-0.22				-0.13	-0.18
8. 2		-0.25						-0.28					
8. 1	-0.16	-0.18						-0 23					
7. 1	0.00	0.01	-0.03	-0.13	-0.24	-0.16	-0.26	-0.17	-0.20	-0.18	-0.25	-0.02	-0.14
9.12.2.9	-0.57	-0.54	-0.47	-0.44	-0.45	-0.37	-0.27	-0.29	-0.34	-0.55	-0.64	-0.61	-0.46
7. 2.2(9)	-0.06	0.02	0.09	0.07	0.00		-0.01	-0.01	0.08	0.01	0.03	0 00	0.02
Dail.ext.	-0.04	-0.01	0.05	0.01	0.00	-0.11	-0.21	-0.16	-0.12	-0.04	-0.21	-0.10	-0.09
Zimin CAL		0.01	0.00	0.01	0.00	0.11	0.51	0.10	0.12	3.01	5.21	55.0	

XXIV.

India. — Madras. Lat. 13° 4' N. Long. 80° 19' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.91	1.13	1.00	1.62	1.22	1.35	1.19	1.27	1.04	0.82	0.91	0.84	1.11
1	1.13	1.45	1.29	1.37	1.47	1.56	1.38	1.34	1.20	1.01	1.13	1.00	1.28
2	1.32	1.76	1.60	1.59	1.65	1.72	1.58	1.51	1.38	1.24	1.35	1.17	1.49
3	1.48	2.01	1.88	1.81	1.81	1.90	1.75	1.64	1.58	1.39	1.56	1.32	1.68
4	1.61	2.25	2.13	1.96	1.98	2.08	1.92	1.77	1.76	1.54	1.74	1.42	1.85
5	1.74	2.44	2.33	1.98	2.08	2.20	2.07	1.93	1.88	1.65	1.88	1.60	1.98
6	1.80	2.51	2.27	1.68	1.72	1.87	1.92	1.81	1.70	1.46	1.80	1.66	1.85
7	1.08	1.48	1.13	0.79	0.92	1.12	1.30	1.24	1.08	0.80	1.89	1.06	1.07
8	-0.02	0.13	0.07	-0.08	-0.05	0.17	0.47	0.44	0.32	0.06	-0.25	0.00	0.10
9	-0.90	-0. 86	-0.84	-1.07	-1.08	-0.77	-0.34	-0.40	-0.50	-0.56	-1.11	-0.77	-0.77
10	-1.45	-1.60	-1.63	-1.84	-2.08	-1.63	-1.19	-1.22	-1.32	-1.04	-1.57	-1.36	-1.49
11	-1.79	-2.14	-2.14	-2.15	-2.56	-2.23	-1.89	-1.85	-2.02	-1.41	-1.82	-1.61	-1.47
Noou.	-1.97	-2.25	-2.38	-2.52	-2.61	-2.60	-2.45	-2.35	-2.24	-1.67	-1.92	-1.75	-2.23
1	-1.96	-2.38	-2.41	-2.46	-2.51	-2.69	-2.70	-2.56	-2.24	-1.66	-1.89	-1.72	-2.26
2	-1.84	-2.36	-2.22	-2.20	-2.22	-2.53	-2.67	-2.40	-2.07	-1.58	-1.66	-1.60	-2.11
3	-1.54	-2.16	-1.90	-1.81	-1.78	-2.05	-2.19	-2.04	-1.66	-1.35	-1.36	-1.28	-1.76
4	13	1	1		1			-1.53	!		-0. SS	1	-1.26
5	-0.53	-1.01	-0.74	-0.46	-0.45	-0.85	-0.97	-0.82	-0.64	-0.56	-0.39	-0.45	-0.66
6	-0.17	-0.49	-).23	0.09	0.05	-0.26	-0.36	-0.31	-0.23	-0.28	-0.11	-0.17	-0.21
7	0.04	-0.16	6.07	0.37	0.34	0.16	0.07	0.06	0.03	-0.08	0.04	0.00	0.08
8	0.24	0.12	026	0.44	0.53	0.43	0.37	0.33	0.21	0.07	0.21	0.15	0.28
9	0.42	0.36	0.3	0.70	0.70	0.63	0.60	0.52	0.44	0.22	0.33	0.30	0.47
10	0.62	0.59	0.61	0.84	0.87	0.94	0.83	0.73	0.62	0.40	0.48	0.46	0.67
11	0.82	0.83	0.82	1.00	1.04	1.07	1.02	0.95	0.84	0.57	0.65	0.64	0.85
Mean.	19.90	20.56	22.33	23.88	24.49	24.45	24.10	23.34	22.89	21.86	20.68	19.89	

XXV.

India. — Bombay. Ltt. 18° 56′ N. Long. 72° 54′ E. Greenw. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.76	1.68	1.43	1.40	١٠30	0.80	0.57	0.59	0.92	1.36	1.74	1.93	1.29
1	1.91	1.88	1.65	1.54	140	0.89	0.65	0.64	0.98	1.52	1.80	2.00	1.40
2	2.04	2.04	1.80	1.75	154	0.88	0.63	1.16	1.09	1.62	1.97	2.18	1.56
3	2.18	2.22	1.90	1.92	1.9	0.94	0.65	0.81	1.18	1.74	2.11	2.28	1.63
4	2.39	2.44	2.26	2.02	1.8.	1.04	0.76	0.82	1.25	1.89	2.23	2.41	1.78
5	2.65	2.68	2.42	2.26	1.92	1.09	0.83	0.90	1.25	1.96	2.40	2.62	1.92
				2 22	3.05						2	2 00	
6	2.88	2.88	2.60	2.20		1.03	0.84	0.84	1.21	2.00	2.55	2.66	1.94
7	2.53	2.37	1.61	0.76	0.44	√60	0.55	0.51	0.61	1.02	1.47	2.08	1.21
8	0.72	0.48	-1.04	-0.62	-0.51	-0)1	0.02	0.08	-0.20	-0.31	-0.12	0.20	-0.11
9	-1.01	-1.05	-1.49	-1.53	-1.30	-0.6	-0.46	-0.45	-0.84	-1.53	-1.40	-1.00	-1.05
10	-2.40	-2.29	-2.28	-2.00	-1.73	-0.7	-0.74	-0.76	-1.32	-2.17	-2.38	-2.14	-1.75
11	-3.08	-2.98	-2.54	-2.20	-2.08	-1.18	-1.07	-1.12	-1.51	-2.38	-3.18	-2.94	-2.19

XXV.

India. - Bombay, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Pec.	Year.
Noon.	-3.40	-3.29	-2.52	-2.44	-2.32	-1.40	-1.09	-1.34	-1.72	-2.39	-3.26	-3.32	-2.37
1	-3.02	-3.12	-2.67	-2.53	-2.28	-1.50	-1.12	-1.35	-1.77	-2.22	-2.96	-3.35	-2.32
2	-2.78	-2.89	-2.56	-2.32	-2.14	-1.52	-0.97	-1.35	-1.55	-2.09	-2.55	-2.97	-2.14
3	-2. 38	-2.54	-2.25	-2.05	-1.85	-1.31	-0.85	-1.09	-1.37	-1.79	-2.22	-2.59	-1.86
4	-1.96	-2.07	-1.72	-1.49	-1.36	-0.89	-0.63	-0.76	-0.95	-1.38	-1.55	-2.03	-1.40
5	-1.30	-1.41	-1.08	-0.96	-0.53	-0.49	-0.36	-0.34	-0.36	-0.61	-0.67	-1.09	-0.79
6	-0.61	-0.44	-0.16	0.00	0.09	-0.02	0.03	0.13	0.14	0.01	-0.14	-0.52	-0.13
7	-0.28	-0.07	0.19	0.43	0.63	0.22	0.21	0.26	0.28	0.30	0.09	-0.23	0.17
8	0.00	0.23	0.48	0.66	0.87	0.39	0.28	0.34	0.44	0.53	0.36	0.10	0.39
9	0.58	0.63	0.80	0.83	0.92	0.44	0.36	0.41	0.58	0.76	0.85	0.75	0.66
10	1.16	1.15	1.04	1.09	0.95	0.52	0.41	0.52	0.78	0.96	7.32	1.35	0.94
11	1.47	1.48	1.20	1.24	1.17	0.71	0.48	0.56	0.89	1.18	1.58	1.65	1.13
Mean.	18.38	19.30	21.00	22.50	23.43	22.35	21.67	21.45	21.42	22.08	:1.28	19.54	

XXVI.

India. — Calcutta. Lat. 22° 33′ 5″ N. Long. 88° 19′ 2″ E. Greenw. — Dove. Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct	Nov.	Dec.	Year.
Àidn.	1.86	1.69	2.06	1.60	1.90	1.12	0.69	0.69	0.71	1.00	1.24	1.51	1.3
1	2.24	2.00	2.37	1.96	2.06	1.12	0.80	0.78	0.76	.17	1.47	1.77	1.5
2	2.53	2.22	2.62	2.18	2.21	1.16	0.91	0.85	0.84	1.26	1.69	2.00	1.7
3	2.80	2.44	2.84	2.27	2.32	1.29	1.02	0.92	0.93	1.26	1.82	2.31	1.8
4	3.06	2.71	3.08	2.40	2.41	1.29	1.11	0.96	1.04	1.46	2.00	2.40	1.9
5	3.33	2.89	3.25	2.47	2.50	1.34	1.24	1.07	1.16	1.53	2.22	2.66	2.1
6	3.53	3.11	3.42	2.53	2.41	1.34	1.24	1.12	1.6	1.62	2.36	2.80	2.2
7	3.71	3.24	3.42	2.22	1.90	1.03	0.96	0.89	033	0.86	2.31	2.93	2.0
8	2.73	2.20	1.97	1.18	0.81	0.45	0.42	0.32	6.27	0.31	0.93	1.68	1.1
9	0.91	0.71	. 0.46	0.11	-0.34	-0.13	-0.16	-0.22	-∂.24	-0.47	-0.13	0.35	0.0
10	-0.78	-0.62	-0.98	-0.44	-1.39	-0.66	-0.69	-0.33	-0.73	-0.58	-1.02	-0.76	-0.7
11	-2.09	-1.64	-2.14	-1.82	-2.14	-1.15	-1.13	-1.08	-1.16	-1.60	-1.91	-1.87	-1.6
Noon.	-3.31	-2.62	-3.16	-2.67	-2.76	-1.60	-1.51	-1.5	-1.40	-1.94	-2.44	-2.80	-2.3
1	-4.14	-3.28	-3.87	-3.09	-3.12	-1.68	-1.58	-1.5	-1.44	-2.05	-2.80	-3.29	-2.6
2	-4.52	-3.64	-4.25	-3.47	-3.32	-1.73	-1.29	-130	-1.63	-2.12	-3.07	-3.69	-2.8
3	-4.65	-3.87	-4.40	-3.62	-3.43	-1.92	-1.24	20	-1.27	-1.83	-2.98	-3.69	-2.8
4	-3.78	-3.69	-4.23	-3.40	-3.10	-1.53	-0.96	- J.95	-0.91	-1.49	-2.18	-2.76	-2.4
5	-3.07	-3.13	-3.36	-2.73	-2.43	-1.20	-0.64	-0.68	-0.56	-0.92	-1.60	-2.18	-1.8
6	-1.87	-1.91	-1.96	-1.42	-1.23	-0.57	-0.31	-0.31	-0.16	-0.25	-0.76	-1.34	-1.0
7	-0.96	-0.93	-0.78	-0.31	-0.14	-0.11	-0.0	-0.09	0.04	0.13	-0.22	-0.63	-0.3
8	-0.20	-0.22	0.00	0.40	0.68	0.20	0.0	0.25	0.22	0.42	0.27	-0.05	0.1
9	0.42	0.38	0.73	0.89	1.08	0.49	022	0.45	0.33	0.60	0.62	0.44	0.5
10	0.95	0.80	1.22	1.20	1.46	0.63	.36	0.56	0.47	0.75	1.07	0.93	0.8
11	1.37	1.20	1.66	1.54	1.64	0.74	0.49	0.65	0.60	0.88	1.16	1.20	1.0
Mean.	15.49	17.57	21.19	22.51	24.01	23 20	22,68	22.86	22.42	21.73	18.88	16.36	

XXVII.

Asia. — Tiflis. Lat. 41° 41′ N. Long. 45° 17′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept	Oct.	Nov.	Dec.	Year.
Midn.	0.87	1.01	1.54	1.81	1.95	2.38	2.43	2.22	1.60	1.38	0.99	0.80	1.58
1	1.02	1.15	1.80	2.10	2.28	2.67	2.79	2.52	1.81	1.64	1.16	0.94	1.82
2	1.17	1.33	2.02	2.40	2.58	2.94	3.13	2.82	2.08	1.88	1.37	1.04	2.06
3	1.32	1.47	2.23	2.64	2.84	3.22	3.49	3.13	2.29	2.11	1.59	1.14	2.28
4	1.46	1.57	2.39	2.94	3.14	3.43	3.73	3.44	2.59	2.39	1.73	1.25	2.51
5	1.60	1.69	2.58	3.12	3.09	3.09	3.55	3.59	2.74	2.62	1.85	1.35	2.57
6	1.76	1.75	2.63	2.89	2.39	2.35	2.77	3.06	2.63	2.77	1.99	1.40	2.37
7	1.87	1.75	2.14	2.19	1.53	1.28	1.50	2.16	1.99	2.38	1.85	1.42	1.8
8	1.40	1.23	1.23	0.99	0.53	0.35	0.70	1.05	1.07	1.52	1.44	1.19	1.06
9	0.05	0.50	0.16	-0.22	-0.51	-0.65	-0.32	-0.21	-0.03	0.30	0.54	0.49	0.01
10	-0.41	-0.46	-0.94	-1.20	-1.41	-1.66	-1.35	-1.32	-1.15	-0.47	-0.46	-0.19	-0.9:
11	-1.17	-1.33	-1.85	-2.06	-2.19	-2.40	-2.27	-2.20	-2.01	-1.77	-1.31	-1.11	-1.81
Noon.	-1.91	-1.94	-2.64	-2.77	-2.89	-2.42	-2.99	-2.89	-2.67	-2.53	-2.07	-1.76	-2.46
I	-2.37	-2.45	-3.12	-3.29	-3.21	-3.42	-3.53	-3.60	-3.17	-3.07	-2.50	-2.21	-3.00
2	-2.59	-2.65	-3.25	-3.37	-3.34	-3.50	-3.68	-3.85	-3.41	-3.56	-2.81	-2.38	-3.20
3	-2.33	-2.58	-3.21	-3.41	-3.25	-3.51	-3.82	-3.98	-3.37	-3.41	-2.55	-2.08	-3.15
4	-1.78	-2.07	-2.78	-3.20	-2.97	-3.39	-3.82	-3.72	-2.95	-2.81	-1.87	-1.43	-2.73
5	-0.99	-1.24	-2.08	-2.46	-2.65	-2.86	-3.47	-3.20	-1.53	-1.85	-1.27	-0.90	-2.0
6	-0.57	-0.60	-1.11	-1.56	-1.47	-1.81	-2.36	-2.01	-1.18	-1.17	-0.73	-0.49	-1.26
7	-0.17	-0.19	-0.48	-0.69	-0.45	-0.63	-0.86	-0.85	-0.46	-0.50	-0.35	-0.13	-0.4
8	0.15	0.19	0.12	-0.02	0.26	0.23	0.13	-0.02	0.18	0.11	-0.02	0.19	0.13
9	0.33	0.44	0.51	0.64	0.83	0.92	0.87	0.72	0.61	0.50	0.24	0.36	0.58
10	0.55	0.65	0.91	1.05	1.28	1.51	1.44	1.33	1.00	0.81	0.48	0.53	0.96
11	0.69	0.89	1.25	1.45	1.63	1.95	1.96	1.80	1.32	1.10	0.76	0.68	1.29
Mean.	-0.20	3.00	5.64	9.99	13.54	16.10	19.01	19.43	15.03	11.40	5.07	2.45	ı

XXVIII.

China. — Peking. Lat. 39° 54′ N. Long. 116° 26′ E. Greenw. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June	July.	Aug	Sept.	Oct.	Nov	Dec	Year
Midn.	1.16	1.70	1.83	1.75	2.19	2.24	1.61	1.49	1.69	1.64	1.19	1.25	1.64
1	1.47	2.07	2.19	2.26	2.76	2.73	1.89	1.80	2.04	2.05	1.47	1.39	2.01
2	1.66	2.35	2.78	2.67	3.20	3.12	2.23	2.04	2.32	2.37	1.68	1.65	2.34
3	1.93	2.55	2.93	3.18	3.72	3.47	2.50	2.31	2.55	2.62	1.88	1.83	2.62
4	2.13	2.81	3.27	3.57	4.13	3.82	2.74	2.54	2.97	2.92	2.01	2.46	2.95
5	2.41	2.91	3.57	3.89	4.30	3.88	2.78	2.71	3.10	3.19	2.20	2.10	3.09
6	2.58	3.15	3.65	3.81	3.37	2.86	2.10	2.46	2.96	3.43	2.32	2.18	2.91
7	2.63	3.21	3.19	2.91	2.30	1.95	1.34	1.65	2.10	2.98	2.30	2.29	2.40
8	2.23	2.37	1.84	1.65	1.19	1.07	0.52	0.76	0.87	1.68	1.39	1.73	1.44
9	0.77	0.70	0.49	0.34	0.00	0.03	-0.12	-0.20	-0.24	0.15	0.19	0.31	0.20
10	-0.57	-0.65	-0.81	-0.79	-1.20	-1.06	-0.97	-1.09	-1.36	-1.05	-0.84	-0.97	-0.95
11	-1.35	-1.90	-1.93	-2.03	-1.24	-2.17	-1.71	-1.67	-2.17	-2.18	-1.74	-1.96	-1.84

XXVIII.

CHINA. — PEKING, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur

Hour.	Jan.	Feb.	March.	April.	May.	June.	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.83	-2.80	-2.95	-2.92	-3.05	-2.92	-2.24	-2.02	-2.77	-3.03	-2.39	-2.64	-2.71
1	-3.01	-3.54	-3.54	-3.59	-3.74	-3.55	-2.65	-2.64	-3.10	-3.65	-2.87	-3.18	-3.25
2	-3.37	-3.84	-4.03	-3.98	-4.08	-3.97	-2.88	-2.90	-3.38	-3.96	-3.07	-3.41	-3.57
3	-3.40	-3.94	-4.12	-4.06	-4.24	-4.00	-2.85	-2.94	-3.44	-3.97	-2.88	-2.74	-3.55
4	-2.88	-3.65	-3.92	-3.86	-4.03	-3.74	-2.74	-2.79	-3.06	-2.43	-2.23	-2.50	-3.15
5	-1.79	-2.83	-3.21	-3.24	-3.65	-3.31	-2.36	-2.20	-2.34	-2.34	-1.18	-1.34	-2.48
6	-0.97	-1.79	-2.20	-2.34	-3.04	-2.44	-1.76	-1.45	-1.18	-1.12	-0.59	-0.64	-1.63
7	-0.48	-0.15	-1.05	-1.13	-1.18	-1.21	-0.72	-0.45	-0.50	-0.54	-0.48	-0.26	-0.68
8	-0.02	-0.27	-0.30	-0.33	-0.19	-0.11	0.12	0.08	0.09	-0.02	0.01	0.18	-0.06
9	0.30	0.26	0.26	0.24	0.59	0.59	0.63	0.51	0.57	0.42	0.30	0.54	0.43
10	0.57	0.73	0.83	0.84	1.15	1.14	1.04	0.83	0.97	0.86	0.59	0.77	0.86
11	0.90	1.20	1.30	1.28	1.67	1.65	1.35	1.18	1.32	1.00	0.81	1.01	1.22
Mean.	-3.57	-2.04	3.42	9.66	15.83	19.61	21.27	19.30	15.68	9.61	1.79	-2.44	

XXIX.

Siberia. — Nertchinsk. Lat. 51° 18′ N. Long. 117° 20′ E. Gr. — Dove.

	Degrees of Reaumur. Hour. Jan. Feb. March. April. May. June. July. Aug. Sept. Oct. Nov. Dec. Year.												
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.78	1.38	1.92	2.53	3.10	3.13	2.63	2.51	2.12	1.66	0.96	0.75	1.96
1	1.06	1.61	2.25	2.95	3.71	3.55	3.00	2.87	2.58	1.98	1.22	0.94	2.31
2	1.24	1.84	2.65	3.36	4.20	3.98	3.34	3.25	2.93	2.27	1.42	1.16	2.64
3	1.45	2.15	3.02	3.75	4.78	4.32	3.64	3.57	3.28	2.57	1.70	1.33	2.96
4	1.70	2.40	3.38	4.09	5.04	4.29	3.86	3.79	3.62	2.80	1.91	1.45	3.19
5	1.93	2.72	3.70	4.15	3.97	3.27	3.17	3.68	3.97	3.00	2.06	1.63	3.10
6	2.08	2.94	3.89	2.96	2.31	2.03	1.99	2.61	3.63	3.16	2.15	1.76	2.63
7	2.26	3.00	2.88	1.43	0.82	0.74	1.01	1.31	2.07	2.46	2.35	1.95	1.86
8	2.20	1.82	1.36	0.19	-0.53	-0.45	-1.28	0.11	0.66	0.84	1.61	1.98	0.71
9	0.56	-0.20	-0.12	-1.32	-1.77	-1.59	-1.25	-1.08	-0.72	-0.69	-0.03	0.62	-0.63
10	-0.96	-1.27	-1.71	-2.35	-2.73	-2.52	-2.13	-2.10	-1.99	-1.52	-1.17	-0.89	-1.80
11	-1.90	-2.34	-2.61	-3.08	-3.34	-3.17	-2.79	-2.91	-2.94	-2.78	-2.12	-1.85	-2.65
Noon,	-2.70	-3.16	-3.43	-3.70	-3.82	-3.62	-3.28	-3.49	-3.71	-3.41	-2.84	-2.58	-3.31
1	-3.06	-3.75	-3.96	-4.01	-4.08	-3.80	-3.58	-3.76	-4.09	-3.75	-3.09	-2.85	-3.65
2	-3.00	-3.80	-4.23	-4.0S	-4.10	-3.73	-3.66	-3.92	-4.20	-3.66	-2.97	-2.52	-3.66
3	-2.50	-3.47	-4.03	-3.84	-3.99	-3.59	-3.48	-3.79	-3.86	-3.26	-2.27	-1.87	-3.33
-1	~1.54	-2.73	-3.53	-3.48	-3.55	-3.24	-3.02	-3.21	-3.34	-2.43	-1.34	-0.96	-2.70
5	-0.71	-1.61	-2.75	-2.85	-3.02	-3.73	-2.38	-2.56	-2.48	-1.42	-0.87	-0.43	-1.98
6	-0.28	-0.63	-1.71	-1.97	-2.27	-2.06	-1.73	-1.68	-1.22	-0.50	-0.10	-0.17	-1.20
7	0.02	0.01	-0.34	-0.34	-0.93	-0.93	-0.82	-0.66	-0.49	-0.24	-0.17	-0.70	-0.47
8	0.13	0.39	0.24	0.61	0.27	0.97	0.37	0.41	0.34	0.30	0.06	0.08	0.29
9	0.27	0.63	0.66	1.19	1.34	1.32	1.24	1.30	0.89	0.64	0.34	0.22	0.84
10	0.43	0.86	1.06	1.72	1.92	2.02	1.78	1.70	1.30	1.01	0.54	0.43	1.23
11	0.57	1.16	1.47	2.17	2.63	2.63	2.29	2.14	1.71	1.31	0.75	0.56	1.62
Mean.	-21.94	-17.84	-8.35	0.04	7.51	1.78	13.91	11.91	6.55	-1.80	-13.44	-21.36	

XXX.

Siberia. - Nertchinsk. Lat. 51° 18' N. Long. 119° 21' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						3 01 10							
Hours.	Jan.	Feb.	March	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.91	1.42	2.07	2.69	4.07	4.29	3.07	3.00	2.16	2.31	0.76	0.66	2.28
2	1.00	1.68	2.57	3.29	4.69	4.71	3.46	3.48	2.96	1	0.96	1	2.69
3	1.15	2.08	3.16	3.78	5.08	4.90	3.75	3.89	3.27	3.26	1.26	0.84	3.04
4	1.42	2.52	3.63	3.97	4.98	4.70	3.76	4.04	3.81	3.61	1.66	1	3.26
	1.12	1.02	0.00	""	1.00	10,0	0.10	1.01	0.01	0.01	1.00	1.0.	0.20
5	1.78	2.84	3.73	3.69	4.24	3.96	3.37	3.72	3.94	3.66	2.06	1.41	3.20
6	2.07	2.80	3.28	2.88	2.86	2.67	2.54	2.89	3.15	3.30	2.30	1.75	2.71
7	2.06	2.28	2.31	1.63	1.07	0.99	1.37	1.62	2.38	2.47	2.18	1.87	1.85
8	1.60	1.28	0.99	0.16	-0.78	-0.79	0.06	0.15	0.87	1.24	1.58	1.59	0.66
9	0.65	-0.05	-0.41	-1.26	-2.33	-2.34	-1.19	-1.25	-0.70	-0.23	0.55	0.87	-0.64
10	-0.59	-1.43	-1.67	-2.42	-3.40	-3.41	-1.98	-2.38	-1.74	-1.70	-0.69	-0.17	-1.80
11	-1.79	-2.58	-2.64	-3.22	-3.98	-3.97	-2.92	-3.15	-2.99	-2.96	-1.84	-1.23	-2.77
Noon	-2.61	-3.29	-3.25	-3.64	-4.19	-4.12	-3.38	-3.61	-3.49	-3.84	-2.60	-2.01	-3.34
1	-2.57	-3.49	-3.61	-3.76	-4.22	-4.05	-3.64	-3.83	-3.69	-4.25	-2.81	-2.30	-3.54
2	-2.56	-3.27	-3.74	-3.65	-4.18	-3.92	-3.72	-3.88	-4.00	-4.20	-2.50	-2.08	-3.48
3	-1.89	-2.76	-3.65	-3.33	-4.03	-3.77	-3.62	-3.75	-3.54	-3.77	-1.87	-1.54	-3.13
4	-1.14	-2.12	-3.31	-2.84	-3.69	-3.54	-3.29	-3.40	-3.24	-3.08	-1.17	-0.92	-2.65
5		-1.45											
6		-0.81											-1.31
7		-0.21	-0.77	-0.56	-0.92)		ì			-0.60
8	-0.04	0.31	0.18	0.20	0.26	0.00	0.20	0.24	0.17	0.17	-0.25	-0.24	0.12
9	0.09	0.74	0.90	0.82	1.29	1.21	1.06	1.11	0.97	0.74	0.05	-0.17	0.73
10	0.03	1.02				$\frac{1.21}{2.25}$	1.51	1.74	1.17	1.18	0.00		1.18
11	0.57		1.34	1.29	2.11	3.09		2.19	1.73	1.16	0.20		1.61
	1	1.19	1.56	1.71	2.78		2.23	2.19	1.73		0.58	0.23	1.94
Midn	0.78	1.29	1.76	2.15	3.41	3.75	2.65	2.37	1.50	1.90	0.55	0.52	1.34
6. 6	0.92	1.00	0.75	0.75	0.39	0.19	0.36	0.52	0.80	0.97	1.01	0.75	0.70
7. 7	0.98	1.04	0.77	0.53	0.07	-0.12	0.28	0.41	0.76	0.97	1.03	0.82	0.63
8. 8	0.78	0.80	0.58	0.18	-0.26	-0.39	0.13	0.20	0.52	0.71	0.77	0.67	0.39
9. 9	0.37	0.34	0.24	-0.22	-0.52	-0.56	-0.06	-0.07	0.13	0.26	0.30	0.35	0.05
10.10	-0.14	l	1		-0.65			-0.32	-0.29	-0.26	-0.25	-0.07	-0.31
			, ,										
7. 2. 9	-0.14	-0.08	-0.18	-0.40	-0.61								
6. 2. 8	-0.18	-0.05	-0.09	-0.19	-0.35	-0.42	-0.33	-0.25	-0.23	-0.24	-0. 08	-0.19	-0.22
6. 2.10	-0.06		0.29		0.26	0.33		0.25		0.09		-0.01	0.14
6. 2. 6	-0.24	-0.43	-0.75	-0.72	-1.13	-1.18	-1.00	-0.95	-0.80	-0.75	-0.16	-0.19	-0.69
									0.00	0.00	0.00	0.25	000
7. 2		-0.61											
8. 2		-1.34											
8. 1		-1.11											
7. 1	-0.25	-0.50	-0.72	-1.01	-1.56	-1.47	-1.18	-1.13	-0.81	-0.87	-0.16	-0.11	-0.81
9.12.3.9	_0.40	-1.00	 -1.90	_1 ~	_9 40	_9 96	_1 69	_1 0~	_1 5*	-1 10	-0.46	-0.25	_1 11
$\begin{bmatrix} 9.12.3.9 \\ 7. \ 2.2(9) \end{bmatrix}$	-0.48	1		1	-2.43 -0.13							-0.23	
1. 2.2(9)	-0.05	0.12	0.09	-0.09	-0.13	-0.13	-0.00	-0.01	0.00	0.04	0.00	0.14	0.04
Dail.ext.	-0.40	-0.33	-0.01	-0.11	0.43	0.39	0.02	0.08	-0.03	-0.30	-0.26	-0.22	-0.14
Zan. Cxt.	0.10	1 0	0.01	0.11	0.10			1 0.00					

XXXI.

Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

		_			Degre	es of Fa	nrennei	τ.					
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec	Mean.
Morn. 1	2.54	1.85	4.70	5.49	8.82	7.83	8.37	7.11	5.45	3.06	2.48	1.82	4 95
2	2.81	2.14	5.47	6.30	10.19	8.87	9.77	8.35	6.50	3.78	2.97	2.00	5.76
3	2.70	2.48	6.28	7.07	10.96	9.59	10.69	9.52	7.65	4.52	3.35	2.07	6.41
4	2.39	2.81	7.02	7.45	10.76	9.14	10.67	10.15	8.48	5.15	3.71	2.18	6.66
5	2.07	3.13	* 40	* 00	0.00		0.50	0.55	0.00		4.01	0.45	0.05
1 1			7.43	7.09	9.32	7.58	9.50	9.77	8.60	5.47	4.01	2.45	6.37
6	1.96	3.33	9.38	5.87	6.68	5.45	7.18	8.12	5.58	i	4.16	2.79	5.65
7	2.00	3.20	5.90	3.87	3.38	2.50	4.05	5.36	2.70	1		2.99	3.94
8	1.93	2.59	3.71	1.37	-0.11	-0.18	0.70	1.96		2.97	3.15	2.70	1.96
9	1.53	1.37	0.86	-1.28	-3.02	-2.48	-2.32	-1.44	-0.56	0.99	1.64	1.73	-0.25
10	0.45	-0.36	-2.18	-3.74	-5.06	-4.61	-4.68	-4 32	- 3.67	-1.22	-0.41	0.11	-2.48
11	-1.22	-2.30	-4.91			-5.99		l	-6.21	1	·	-1.76	
Noon		-4 03				-7.31		1	l	ı		-3.42	4
1	4	-5.13							1	1	l	l .	l .
2	1	-5.38				-8.78			1	1	l.	-4.48	-7.47
3	-4.93		-7.76			-S 91		-9.88	l		}	-3.78	-7.27
4	-3.78	-3.56	-6.84	-7.34	-9.50	-8.01	-9.36	-9.50	-7.81	-5.22	-3.85	-2.68	-6.46
5	-2.25	-2.14	-5.65	-5.58	-8.66	-6.32	-8.35	-8.28	-6.26	-4.05	-2.57	-1.60	5.15
6	-0.90			1		-4.39		l :		1	1	-0.83	
7	0.02	1	-2.61			-1.94			1	-1.49	1	-0.43	1
8	0.47		-0.97		-1.31	0.11				-0.36	-0.41	-0.23	
	0.47	0.00	0.57	1.04	-1.51	0.11	-1.51	0.03	0.02	-0.50	-0.41	-0.20	0.25
9	0.70	0.92	0.63	2.61	1.46	1.80	1.24	1.80	1.76	0.54	0.00	0.00	1.13
10	0.95	1.10	2.00	3.62	3.78	3.49	3.38	3.67	2.99	1.28	0.52	0.38	2.27
11	1.42	1.28	3.13	4.25	5.69	4.75	5.20	4.97	3.85	1.87	1.15	0.92	3.22
Midn	2.03	1.55	3.98	4.82	7.36	6.26	6.82	6.03	4.59	2.45	1.85	1.44	4.10
6. 6	0.54	1.24	1.46	1.26	-0.07	0.54	0.34	0.97	1.69	1.28	1.31	0 99	0.97
7. 7	1.01	1.64	1.64		-0.41	0.27	0.02	0.92	1.76	1.49	1.55	1 28	1.06
8. 8	1.24	1.62	1.37		-0.72	-0.05	-0.29	0.65	1.35	1.31	1.37	1.24	0.86
9. 9	1.10	1.15	0.74		-0.79	-0.34	-0.54	0.18	0.59	0.77	0.83	0.86	0.43
10.10	0.70	0.38	-0.09			-0.56		1 1	-0.34	0.05	0.07	0.25	-0.11
7. 2. 9		-0.43						1 1		-0.47			
6. 2. 8	-0.95	-0.47	0.07	-0.61	-1.13	-1.08	-1.1 0	-0.72	-0.52	-0.50	-0.65	-0.63	-0.70
6. 2.10	-0.79	-0.32	1.06	0.27	0.56	0 05	0.47	0.72	0.47	0.07	-0.34	-0.43	0.16
6. 2. 6	-1.10	-0.97	-1.76	-2.07	-2.97	-2.57	-2.S1	-2.57	-1.94	-1.28	-1.04	0 83	-1.85
7. 2	_1 64	1.00	1.10	9.40	9.70	9 1 4	9.50	_0.14	1 00	_0.0~	_0.99	_0.75	_1 77
8. 2		-1.09				-3.14					1		
8. 2		-1.40	į.					,	1	l .	1	-0.89	
1 !		-1.27	!		1	,			l .	l .	1	-0.85	
7. 1	-1.30	-0.97	-1.04	-2.24	-z 33 	-2.95	-2.19	-1.80	-1.09	-0.80	-0.51	-0.70	-1.57
9 12.3 9	-1.45	-1.62	-3.29	-3.60	-4,55	-4.23	-4.55	-4.37	-3 92	-2.39	-1.96	-1.37	-3.11
7. 2.2(9)	1	-0.09	1		1	-0.68				1	l		
										l			
Dail. ext.	-1.24	-1.04	0.59	-0.63	0.74	0.34	0.56	0.14	-0 32	-0.47	-0 79	-0.74	-0.41
<u>'</u>	<u> </u>		1	<u> </u>	1					<u>'</u>	!		

XXXII.

Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
				-									
Morn. 1	1.13	0.82	2.09	2.44	3.92	3.48	3.72	3.16	2.42	1.36	ŀ	0.81	2.20
2	1.25	0.95	2.43	2.80	4.53	3.94	4.34	3.71	2.89	1.68	1.32	0.89	2.56
3	1.20	1.10	2.79	3.14	4.87	4.26	4.73	4.23	3.40	2.01	1.49	0.92	2.85
4	1.06	1.25	3.12	3.31	4.78	4.06	4.74	4.51	3.77	2.29	1.65	0.97	2.96
5	0.92	1.39	3.30	3.15	4.14	3.37	4.22	4.34	3.82	2.43	1.78	1.09	2.83
6	0.87	1.48	4.17	2.61	2.97	2.42	3.19	3.61	3.40	2.35	1.85	1.24	2.51
7	0.89	1.42	2.62	1.72	1.50	1.11	1.80	2.38	2.48	1.98	1.76	1.33	1.75
8	0.88	1.15	1.65	0.61	-0.05	-0.08	0.31	0.87	1.20	1.32	1.40	1.20	0.87
9	0.68	0.61	0.38	-0.57	-1 3.1	-1 10	-1.03	-0.64	-0.25	0.44	0.73	0.77	-0.11
10		-0.16					ļ	4)	i e	1	l	-1.10
11		-1.02					ł	l		t	Į.	1	i 1
Noon	l .	-1.79					t .				-1.99	ı	ł I
	20.							2.00		2 00	2 10		
1		-2.28						-3.98	l		1		1 1
2		-2.39						-4.28	ł				1 6
3 4		-2.12	i					-4.39	1	4			, ,
4	-1.05	-1.58	-3.04	-5.20	-4.22	-3.50	-4.10	-4.22	-3.47	-2.52	-1.71	-1.19	-2.87
5	-1.00	-0.95	-2.51	-2.48	-3.85	-2.81	-3.71	-3.68	-2.78	-1.80	-1.14	-0.71	-2.29
6	-0.40	-0.37	-2.87	-1.49	-3.03	-1.95	-2.88	-2.75	-1.89	-1.22	-0.69	-0.37	-1.66
7	0.01	0.04	-1.16	-0.46	-1.85	-0.86	-1.78	-1.56	-0.92	-0.66	-0.38	-0.19	-0.81
8	0.21	0.28	-0.43	0.46	-0.58	0.05	-0.58	-0.30	0.01	-0.16	-0.18	-0.10	-0.11
9	0.31	0.41	0.28	1.16	0.65	0.80	0.55	0.80	0.78	0.24	0.00	0.00	0.50
10	0.42	0.49	0.89	1.61	1.68	1.55	1.50	1.63	1.33	0.57	0.23	0.17	1.01
11	0.63	0.57	1.39	1.89	2.53	2.11	2.31	2.21	1.71	0.83	0.51	0.41	1.43
Midn	0.90	0.69	1.77	2.14	3.27	2.78	3.03	2.68	2.04	1.09	0.82	0.64	1.82
			0.05	0.50	0.00	0.01	0.15	0.40	0	0	0.50	0.44	0.40
6. 6	0.24	0.55	$0.65 \\ 0.73$		-0.03 -0.18	0.24	$0.15 \\ 0.01$	$0.43 \\ 0.41$	0.75	$0.57 \\ 0.66$	0.58 0.69	$0.44 \\ 0.57$	0.43
7. 7	0.45	$0.73 \\ 0.72$	0.73			$0.12 \\ -0.02$		0.41	0.78	0.58	0.69	0.57	0.47
8. 8 9. 9	0.55	0.72	0.33		-0.32 -0.35	-0.02 -0.15		0.29	$0.60 \\ 0.26$	0.33	0.37	0.38	0.38
10.10	0.31	0.17	-0.04	-0.03		-0.25		-0.15	-0.15	0.02	0.03	0.11	-0.05
10.10	0.01	0.11	0.01	0.00	0.20	0.20	0.20	0.10	0.10	0.02	0.05	0.11	0.00
7. 2. 9	-0.38	-0.19	-0.25	-0.33	-0.58	-0.66	-0.57	-0.37	-0.28	-0.21	-0.26	-0.22	-0.36
6. 2. 8	-0.42	-0.21	0.03	-0.27	-0.50	-0.48	-0.49	-0.32	-0.23	-0.22	-0.29	-0.28	-0.31
6. 2.10		-0.14	0.47	0.12	0.25	0.02	0.21	0.32	0.21	l 1	-0.15		0.07
6. 2. 6	-0.62	-0.43	-0.78	-0.92	-1.32	-1.14	-1.25	-1.14	-0.86	-0.57	-0.46	-0.37	-0.82
7. 2	-0.73	-0.49	-0.52	-1.80	-1.20	-1.40	-1.14	-0.95	-0.81	-0.43	-0.39	-0.33	-0.79
8. 2	1	-0.62								1			
8. 1	1	-0.57											
7. 1		-0.43											
0.10.00	0.01	0.50	7.40	1 00	0.00	, 00	0.00	7.04	3.00	1.00	0.0*	0.03	1.00
9.12.3.9 7. 2.2(9)		-0.72 -0.04						-1.94 -0.08					
1. 2.2(3)	-0.21	-0.04	0.14	0.04	0.23	0.50	-0.29	-0.05	0.02	-0.10	0.20	-0.17	-0.15
Dail.ext.	-0.55	-0.46	0.26	-0.28	0.33	0.15	0.25	0.06	-0.14	-0.21	-0.35	-0.33	-0.18

XXXIII.

Siberia. — Barnaul. Lat. 53° 20' N. Long. 83° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — DOVE.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.99	1.98	2.43	2.65	3.70	3.75	3.48	3.10	2.80	1.99	1.06	0.77	2.3
1	1.15	2.21	2.77	3.03	4.11	4.30	4.07	3.50	3.20	2.24	1.22	0.86	2.7
2	1.26	2.36	3.13	3.24	4.47	4.83	4.49	3.90	3.63	2.50	1.39	0.95	3.0
3	1.41	2.47	3.34	3.49	4.72	4.95	4.77	4.29	3.92	2.69	1.46	1.01	3.2
4	1.56	2.56	3.61	3.59	4.20	4.41	4.40	4.23	4.11	2.89	1.51	1.07	3.1
5	1.55	2.68	3.70	2.78	2.85	3.12	3.34	3.60	3.90	2.91	1.57	1.10	2.7
6	1.61	2.69	2.90	1.58	1.44	1.75	1.88	2.29	3.06	2.68	1.59	1.09	2.0
7	1.53	2.30	1.63	0.46	0.28	0.49	0.50	0.85	1.54	1.84	1.50	1.18	1.1
8	0.94	1.15	0.13	-0.69	-0.80	-0.65	-0.54	-0.51	-0.08	0.87	0.95	0.93	0.1
9	0.27	-0.47	-1.35	-1.80	-1.94	-1.78	-1.81	-1.79	-1.62	-0.73	-0.03	0.11	-1.0
10	-0.79	-1.90	-2.36	-2.68	-2.71	-2.75	-2.70	-2.50	-2.84	-1.96	-1.12	-0.83	-2.1
11	-1.69	-2.95	-3.31	-3.27	-3.39	-3.39	-3.44	-3.41	-3.75	-2.81	-1.93	-1.62	-2.9
Noon.	-2.35	-3.89	-3.78	-3.66	-3.73	-3.98	-3.90	-3.81	-4.19	-3.48	-2.42	-2.04	-3.4
1	-2.61	-4.25	-4.11	-3.68	-4.04	-4.19	-4.09	-4.11	-4.41	-3.72	-2.57	-2.12	-3.6
2	-2.39	-4.23	-4.07	-3.65	-4.13	-4.34	-4.21	-4.10	-4.34	-3.64	-2.39	-1.70	-3.6
3	-1.88	-3.62	-3.69	-3.39	-4.09	-4.19	-3.89	-3.91	-4.11	-3.17	-1.66	-1.09	-3.2
4	-1.19	-2.30	-2.67	-2.62	-3.51	-3.57	-3.65	-3.68	-3.21	-2.53	-1.05	-0.76	-2.5
5	-0.81	-1.30	-1.69	-1.82	-3.09	-3.04	-3.07	-2.78	-2.29	-1.49	-0.71	-0.53	-1.8
6	-0.41	-0.56	-0.84	-0.62	-1.92	-2.19	-2.09	-1.54	-1.05	-0.72	-0.33	-0.28	-1.0
7	-0.20	0.09	0.35	0.27	-0.46	-0.84	-0.69	-0.20	-0.17	-0.08	-0.03	-0.02	-0.1
8	0.12	0.69	0.39	0.99	0.77	0.51	0.52	0.67	0.60	0.31	0.23	0.19	0.5
9	0.32	1.08	0.88	1.50	1.64	1.48	1.42	1.46	1.26	0.82	0.42	0.39	1.0
10	0.73	1.47	1.46	2.02	2.42	2.31	2.22	2.04	1.85	1.29	0.58	0.58	1.5
11	0.78	1.76	1.92	2.35	3.11	3.05	2.88	2.58	2.36	1.68	0.83	0.75	2.0
Mean.	-14.71	-13.47	-5.47	1.77	7.78	13.62	14.98	12.76	7.53	1.58	-8.36	-13.07	4.9

The numbers without sign must be added; those with the sign — must be subtracted.

HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

EUROPE.



XXXIV.

Italy. - Rome. Lat. 41° 54′ N. Long. 12° 25′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Rea	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.90	1.08	1.22	1.55	1.88	2.44	2.17	2.20	1.63	1.50	1.15	0.93	1.55
2	0.99	1.26	1.50	1.84	2.10	2.59	2.41	2.49	1.91	1.75	1.29	1.02	1.76
3	1.14	1.58	1.96	2.31	2.56	3.02	2.99	3.00	2.38	2.12	1.53	1.19	2.15
4	1.36	1.99	2.46	2.80	3.06	3.51	3.68	3.54	2.91	2.58	1.87	1.43	2.60
5	1.60	2.36	2.80	3.07	3 30	3.71	4.06	3.79	3.25	2.96	2.22	1.70	2.90
6	1.77	2.52	2.76	2.92	3.04	3.36	3.81	3.53	3.17	3.10	2.42	1.87	2.86
7	1.74	2.33	2.24	2.25	2.19	2.38	2.82	2.62	2.58	2.82	2.33	1.83	2.34
8	1.40	1.73	1.29	1.15	0.93	0.98	1.27	1.22	1.51	2.05	1.82	1.47	1.40
9	0.72	0.78			-0.47				0.15	0.86	0.93	0.78	0 20
10	-0.24	-0.38	-1.08										
11	-1.27			-2.36					-2.41	-2.00	1	-1.14	1
Noon	-2.15	-2.49	-2.71	-2.9 8	-3.01	-3.08	-3.38	-3.49	-3.24	-3.14	-2.39	-1.99	-2.84
1			-3.02									-2.52	
2	-2.78	-3.25	-3.04	-3.28	-3.31	-3.70	-3.76	-3.92	-3.80	-3.99	-3.16	-2.66	-3.39
3			-2.84									-2.44	
4	-1.83	-2.51	-2.45	-2.72	-3.14	-4.05	-3.88	-3.62	-3.11	-3.04	-2.41	-1.95	-2.89
5	-1.11	-1.81	-1.89	-2.15	-2.70	-3.70	-3.53	-3.05	-2.38	-2.21		-1.35	1
6	-0.45	-1.05	-1.20	-1.39	-1.91	-2.79	-2.67	-2.18	-1.48	I	1	-0.75	1
7	0.05	-0.34	-0.14	-0.53	-0.84	-1.42	l .		-0.51	-0.50	1	i	i
8	0.39	0.25	0.26	0.30	0.29	0.13	0.08	0.21	0.38	0.19	0.05	0.17	0.23
9	0.59	0.67	0.78	0.94	1.22	1.46	1.33	1.22	1.05	0.71	0.46	0.46	0.9
10	0 71	0.90	1.07	1.31	1.76	2 29	2.10	1.86	1.43	1.05	0.76		1
11	0.78	0.99	1.15	1.44	1.93	2.57	2.33	2.11	1.54	1.24	0.95	0.79	1.49
Midn	0.84	1.02	1.15	1.46	1.88	2.51	2.24	2.14	1.55	1.36	1.06	0.86	1.51
	0.00			0.70	0.55	0.00	0.57	0.68	0.85	0.89	0.67	0.56	0.67
6. 6 7. 7	0.66	0.74	0.78 0.90	$0.76 \\ 0.86$	1	$0.28 \\ 0.48$	0.57	0.80	ı	1.16	0.92	0.50	0.83
8. 8	$0.90 \\ 0.89$	$\begin{bmatrix} 1.00 \\ 0.99 \end{bmatrix}$	0.30	0.72	0.68	0.55	0.67	0.71	0.95	1.12	0.94	l	0.81
9. 9	0.65	0.72	0.44	0.12	0.37	0.48	0.45	0.43	i	0.78	0.70	0.62	0.53
10.10	0.24	0.26	1	!	0.04	0.27	0.10	0.04	l .	0.23	1	0.26	0.1
7. 2. 9	-0.15	-0.08	-0.01	-0.03	0.03	0.05	0.13	-0.03	-0.06	-0.15	-0.12	-0.12	-0.0
6. 2. 8	l .	i .	-0.01	l .		-0.07	1	-0.06				-0.21	-0.10
6. 2.10	-0.10	1		l	0.50	0.65	l .	0.49		0.05		-0.04	0.2
6. 2. 6	1	1	-0.49	1	-0.73	-1.04	-0.87	-0.86	-0.70	-0.74	-0.61	-0.51	-0.68
7. 2	-0.52	-0.46	-0.40	-0.52	-0.56	-0.66	-0.47	-0.65	-0.61	-0.59	-0.42	-0.42	-0.5
-8. 2	-0.69	-0.76	-0.88	-1.07	-1.19	-1.36	-1.25	-1.35	-1.15	-0.97	-0.67	-0.60	-1.00
8. 1	-0.65	-0.67	-0.87	-1.06	-1.15	-1.21	-1.17	-1.30	-1.10	-0.89]-0.59	-0.53	-0.93
7. 1	-0.48	-0.37	-0.39	-0.51	-0.52	-0.51	-0.40	-0.60	-0.56	-0.50	-0.34	-0.35	-0.46
9.12.3.9	_0 89	_1 02	-1.17	-1.32	-1.39	-1.53	-1.60	-1.62	-1.41	-1.32	-0.98	-0.80	-1.2
7. 2.2(9)	0.04		1	0.21	0.33					0.06	}	1	1

XXXV.

ITALY. — PADUA. Lat. 45° 24' N. Long. 11° 52' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

							aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.58	0.57	0.89	1.23	2.43	2.21	2.86	2.27	1.50	0.00	1.04	0.00	1
	ll .	i	1	1	1	1		(1	1	1	i	
2	0.58	0.81	1.20	l .	2.70		3.20	i .	1	1	1		1
3	0.76	0.97	1.42	1.66	3.00	1	1	1	1	1	J.	0.98	
4	0.79	1.13	1.68	1.97	3.14	2.71	3.78	3.44	2.34	1.39	1.35	1.05	2.06
5	1.06	1.31	1.89	2.26	2.97	2.39	3.34	3.44	2.66	1.58	1.42	1.12	2.12
6	1.13	1.46	2.06	2.22	1.96	1.22	2.07	2.93	2.54	1 54	1.49	1.16	1.82
7	1.25	1.58	1.86	1.82	0.66	0.08	0.56	1.82	1.78	1.37	1.58	1.23	1.30
8	1.07	1.42	0.66	1.03	-0.23	-0.65	-0.25	0.58	0.79	0.81	0.97	1.00	0.60
9	0.70	0.82	0.61	0.18	-1.07	-1.24	-1.63	-1.65	-0.58	0.18	0.02	0.33	-0.28
10	0.10	-0.08	-0.83					-1.90			-0.81	-0.26	-0.95
11	-0.58	-0.62						-2.38				1	í
Noon	-0.98	-1.24	-1.32			1	1	-2.97	į.			-1.50	ľ
1	-1.38	-1.45	-1.54	-1.68	-2.88	-2.61	-3.53	-3.34	-2 51	-171	_2.12	_1 90	-2 25
								-3.73					
3								-3.81					
4													
4	-1.15	-1.54	-1.71	-2.10	-2.07	-2.20	-2.52	-3.23	-2.38	-1.94	-1.53	-1.14	-2.02
5	-0.87	-0.98	-1.39	-1.98	-2.08	-1.60	-2.44	-2.49	-1.60	-1.05	-0.73	-0.74	-1.50
6		-0.79						-1.34				-0.33	-0.89
7							-0.46	-0.32	-0.18	-0.14	0.12	-0.15	-0.36
8		-0.42				0.38	1.01	1	-0.10	0.05	0.33	0.04	0.06
9	0.05	-0.14	-0.10	-0.11	1.11	1.38	1.54	1.01	0.23	0.26	0.49	0.26	0.50
10	0.18	0.09	0.24	0.27	1.44	1.72	1.67		0.58	0.52	0.72	0.46	0.77
11	0.29	0.31	0.48	0.60	1.75	1.86	2.14	1.78	0.84	0.68	0.86	0.59	1.02
Midn	0.37	0.49	0.72	0.85	2.02	2.10	2.43	2.23	1.36	0.78	0.94	0.70	1.25
	0.0.		0	0.00	2.02	2.10	2.10		1.50	0.18	0.54	0.,0	1.20
6. 6	0.27	0.34	0.52	0.36	0.38	0.11	0.33	0.80	0.86	0.50	0.67	0.42	0.46
7. 7	0.47	0.48	0.57	0.35	0.20	-0.02	0.05	0.75	0.80	0.62	0.55	0.54	0.47
8.8	0.50	0.50	0.12	0.28	-0.19	-0.14	0.38	0.54	0.35	0.43	0.65	0.52	0.33
9. 9	0.38	0.34	0.26	0.04	0.02	0.07	-0.05	-0.32		0.22	0.26	0.30	0.11
10.10	0.14	0.01	1	-0.08	-0.13	1	-0.31	1 1	- 1	0.01	-0.05		-0.09
7. 2. 9	-0.07	-0.06	0.01	-0.07	-0.39	-0.39	-0.55	-0.30	-0.28	-0.13	-0.16	-0.19	-0.21
6. 2. 8	-0.15		-0.04		I			-0.10					
6. 2.10	-0.07	- 1	0.19	0.19	0.15	,	-0.00		0.09		-0.11		0.05
6. 2. 6	-0.32			- 1				-0.71			- 1	- 1	-0.51
7 9	0.10	0.00	0.00										0.52
11 11	-0.13							-0 96					
8. 2						1		-1.58					
8. 1 7. 1	-0.16 -0.07	$\begin{bmatrix} -0.02 \\ 0.07 \end{bmatrix}$	0.14					-1.38 -0.76					- 11
								1		ļ	1		
9.12.3.9 7. 2.2(9)	-0.42	- 1						-1.86					
1. 2.2(9)	-0.04	-0.0s	-0.02	-0.08	-0.02	0.06	-0.03	0.03	-0.15	-0.03	-0.00	-0.05	-0.04
Dail.ext.	-0.13	-0.04	0.08	0.06	0.10	0.05	0.02	-0.19	-0.11	-0.23	-0.49	-0.42	-0.16

XXXVI.

Switzerland. — Geneva. Lat. 46° 12′ N. Long. 6° 9′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.50	0.68	1.38	1.68	2.16	2.77	2.54	2.38	1.86	1.44	0.80	0.48	1.56
1	0.62	0.83	1.88	2.14	2.72	3.32	3.19	3.08	2.41	1.71	0.97	0.54	1.95
2	0.74	1.01	2.34	2.53	3.16	3.68	3.70	3.68	2.93	1.95	1.14	0.61	2.29
3	0.83	1.22	2.70	2.76	3.40	3.74	3.89	4.03	3.34	2.14	1.30	0.70	2.50
4	0.92	1.46	2.89	2.78	3.34	3.50	3.80	4.00	3.49	2.22	1.43	0.81	2.55
5	0.98	1.66	2.83	2.54	2.93	2.88	3.26	3.52	3.30	2.14	1.51	0.91	2.37
6	1.02	1.75	2.49	2.03	2.22	2.03	2.39	2.65	2.72	1.85	1.48	0.97	1.97
7	0.97	1.66	1.90	1.33	1.28	1.05	1.38	1.54	1.84	1.34	1.26	0.92	1.37
s	0.78	1.33	1.09	0.50	0.27	0.08	0.26	0.37	0.78	0.65	0.84	0.70	0.64
9	0.46	0.74	0.17	-0.34	-0.69	-0.82	-0.71	-0.70	-0.30	-0.15	0.23	0.34	-0.16
10	-0.02	-0.01	-0.77	-1.10	-1.51	-1.57	-1.53	-1.58	-1.26	-0.98	-0.47	-9.16	-0.91
11	-0.57	-0.80	-1.61	-1.75	-2.17	-2.18	-2.24	-2.29	-2.06	-1.70	-1.14	-0.67	-1.60
Noon.	-1.06	-1.49	-2.26	-2.23	-2.66	-2.70	-2.74	-2.85	-2.66	-2.22	-1.66	-1.10	-2.14
1 .	-1.40	-1.98	-2.70	-2.55	-2.98	-3.10	-3.18	-3.29	-3.08	-2.53	-1.94	-1.37	-2.51
2	-1.50	-2.18	-2.87	-2.67	-3.12	-3.35	-3.48	-3.5 8	-3.29	-2. 58	-1.94	-1.41	-2.66
3	-1.41	-2.10	-2.81	-2.61	-3.07	-3.42	-3.51	-3.65	-3.28	-2.41	-1.74	-1.26	-2.61
4	-1.14	-1.82	-2.54	-2.37	-2.80	-3.25	-3.37	-3.43	-3.04	-2.06	-1.38	-0.97	-2.35
5	-0.79	-1.37	-2.10	-1.97	-2.32	-2.78	-2.90	-2.92	-2.57	-1.59	-0.99	-0.64	-1.91
6	-0.46	-0.94	-1.59	-1.46	-1.70	-2.11	-2.22	-2.18	-1.91	-1.06	-0.62	-0.32	-1.38
7	-0.20	-0.51	-1.06	-0.90	-1.00	-1.29	-1.40	-1.31	-1.16	-0.53	-0.30	-0.07	-0.81
8	-0.01	-0.14	-0.54	-0.34	-0.29	-0.42	-0.49	-0.46	-0.42	-0.02	-0.03	0.11	-0.26
9	0.12	0.14	0.05	0.20	0.38	0.47	0.34	0.32	0.26	0.42	0.20	0.24	0.26
10	0.25	0.37	0.42	0.70	0.91	1.30	1.10	1.02	0.83	0.82	0.42	0.34	0.71
11	0.37	0.54	0.90	1.20	1.51	2.07	1.87	1.70	1.35	1.15	0.62	0.41	1.14
Mean	-0.53	1.24	3.41	6.77	10.37	13.31	14.30	13.58	11.46	7.48	3.76	0.58	

XXXVII.

SWITZERLAND. — GENEVA. Lat. 46° 12' N. Long. 6° 9' E. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.45	0.69	1.26	1.44	1.54	1.98	2.12	1.63	1.44	0.94	0.50	0.59	1.21
2	0.70	0.96	2.21	2.62	2.60	3.20	3.18	2.83	2.72	1.46	0.73	0.66	1.99
4	1.01	1.33	2.91	3.36	3.11	3.55	3.82	3.51	3.26	1.90	1.02	0.80	2.46
6	1.19	1.49	2.70	2.87	2.26	2.38	2.47	2.82	2.79	1.74	1.13	0.97	2.07
8	1.22	1.22	1.42	0.74	0.27	0.13	0.22	0.49	0.72	0.94	0.90	0.95	0.77
10	-0.02	-0.25	-0.68	-1.70	-1.30	-1.34	-1.25	-1.01	-1.10	-0.73	-0.26	-0.14	-0.73
Noon.	-0.13	-1.30	-1.97	-2.14	-2.42	-2.54	-2.50	-2.34	-2.38	-1.86	-1.18	-1.22	-1.91
2	-1.69	-1.70	-2.82	-2.94	-2.97	-3.09	-3.11	-3.17	-3.03	-2.35	-1.55	-1.46	-2.49
4	-1.30	-1.61	-2.70	-2.94	-2.46	-2.87	-2.89	-3.04	-2.86	-1.53	-1.19	-1.05	-2.20
6	-0.54	-0.90	-1.79	-2.06	-1.40	-1.89	-2.24	-2.01	-1.74	-0.88	-0.45	-0.43	-1.36
8	-0.09	-0.21	-0.89	-0.70	-0.10	-0.25	-0.58	-0.33	-0.38	-0.08	0.03	0.10	-0.29
10	0.20	0.28	0.34	0.40	0.86	0.78	0.78	0.69	0.57	0.47	0.29	0.18	0.49
	l												
Mean	1.20	0.47	2.28	6.81	9.48	12.82	14.43	13.74	10.66	7.73	3.30	0.12	

XXXVIII.

SWITZERLAND. - St. BERNARD. Lat. 45° 52' N. Long. 9° 22' E. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.48	0.81	1.34	1.96	2.10	1.72	1.62	1.30	0.76	1.02	0.59	0.31	1.1
1	0.63	0.91	1.58	2.22	2.45	1.99	1.93	1.53	0.97	1.17	0.66	0.33	1.3
2	0.81	1.09	1.82	2.40	2.73	2.15	2.14	1.82	1.17	1.30	0.78	0.40	1.5
3	0.99	1.26	1.98	2.46	2.81	2.24	2.24	1.94	1.34	1.36	0.89	0.50	1.6
4	1.08	1.38	2.02	2.34	2.67	2.14	2.17	1.91	1.41	1.34	0.98	0.52	1.6
5	1.08	1.34	1.84	2.00	2.28	1.88	1.90	1.70	1.35	1.19	0.98	0.66	1.5
6	0.91	1.14	1.42	1.45	1.72	1.42	1.44	1.34	1.14	0.92	0.86	0.62	1.2
7	0.60	0.74	0.79	0.70	0.81	0.81	0.82	0.76	0.77	0.83	0.61	0.50	0.7
S	0.17	0.18	0.00	-0.16	-0.08	0.09	0.10	0.12	0.29	0.06	0.26	0.26	0.1
9	-0.31	-0.48	-0.85	-1.06	-1.10	-0.66	-0.66	-0.53	-0.26	-0.46	-0.22	-0.06	-0.5
10	-0.78	-1.13	-1.63	-1.86	-1.94	-1.36	-1.34	-1.13	-0.78	-0.94	-0.68	-0.41	-1.1
11	-1.14	-1.66	-2.23	-2.50	-2.58	-1.95	-1.90	-1.60	-1.22	-1.33	-1.09	-0.71	-1.6
Noon.	-1.34	-1.98	-2.58	-2.S7	-2.96	-2.34	-2.26	-1.90	-1.51	-1.58	-1.36	-0.94	$ _{-1.9}$
1	-1.38	-2.04	-2.62	-2.98	-3.06	-2.51	-2.40	-2.02	-1.62	-1.66	-1.47	-1.03	-2.0
2	-1.24	-1.86	-2.38	-2.78	-2.89	-2.44	-2.33	-1.94	-1.56	-1.59	-1.39	-0.99	-1.9
3	-0.98	-1.47	-1.92	-2.36	-2.51	-2.21	-2.08	-1.74	-1.35	-1.3 8	-1.16	-0.82	-1.6
4	-0.65	-0.97	-1.34	-1.79	-1.98	-1.80	-1.70	-1.42	-1.05	-1.07	-0.83	-0.57	-1.2
5	-0.32	-0.43	-0.73	-1.17	-1.40	-1.32	-1.26	-1.06	-0.70	-0.72	-0.46	-0.27	-0.8
6	-0.05	0.04	-0.19	-0.54	-0.81	-0.80	-0.80	-0.70	-0.38	-0.36	-0.10	0.00	-0.3
7	0.14	0.39	0.25	0.04	-0.25	-0.28	-0.34	-0.34	-0.11	-0.03	0.19	0.21	-0.0
8	0.25	0.60	0.56	0.54	0.27	0.20	0.09	0.00	0.10	0.24	0.38	0.34	0.3
9	0.30	0.69	0.78	0.96	0.76	0.63	0.50	0.32	0.27	0.47	0.49	0.38	0.5
10	0.34	0.72	0.96	1.33	1.22	1.02	0.89	0.64	0.42	0.67	0.53	0.38	0.7
11	0.38	0.74	1.14	1.66	1.68	1.40	1.26	0.97	0.58	0.85	0.55	0.33	0.9
Ican.	-8.26	-6.62	-5.72	-2.97	0.74	3.55	4.82	4.32	2.40	-0.91	-3.95	-5.86	

XXXIX.

Switzerland. — St. Bernard. Lat. 45° 52' N. Long. 9° 22' E. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.34	0.55	0.75	1.19	1.26	1.39	1.02	1.08	0.81	0.66	0.33	0.28	0.80
2	0.52	0.78	1.14	1.64	1.75	1.88	1.62	1.53	1.16	0.94	0.42	0.27	1.14
4	0.82	1.06	1.50	1.84	1.91	1.98	1.82	1.71	1.34	1.17	0.65	0.42	1.35
6	0.65	0.86	1.20	1.50	1.53	1.46	1.46	1.27	0.98	0.88	0.50	0.32	1.05
8	0.48	0.26	0.14	-0.08	-0.25	0.01	0.22	0.16	0.08	0.28	0.27	0.15	0.14
10	-0.35	-0.91	-1.06	-1.26	-1.39	-1.18	-1.11	-0.94	-0.86	-0.68	-0.54	-0.23	-0.88
Noon.	-1.40	-1.66	-1.74	-2.11	-2.15	-1.92	-1.81	-1.77	-1.58	-1.45	-1.26	-0.91	-1.65
2	-1.37	-1.55	-1.89	-2.12	-2.12	-2.23	-2.01	-1.97	-1.54	-1.52	-1.23	-1.22	-1.73
4	-0.42	-0.71	-1.14	-1.55	-1.47	-1.65	-1.49	-1.30	-0.88	-0.86	-0.37	-0.02	-0.99
6	0.09	0.17	0.09	-0.26	-0.35	-0.71	-0.57	-0.46	-0.26	-0.07	0.08	0.22	-0.17
8	0.25	0.44	0.49	0.49	0.50	0.35	0.30	0.26	0.26	0.22	0.70	0.30	0.38
10	0.37	0.55	0.55	0.71	0.76	0.64	0.56	0.43	0.46	0.43	0.40	0.40	0.52
Mean.	-6.08	-8.83	-6.66	-3.01	-0.42	2.71	4.82	4.70	2.07	-0.36	-5.46	-6.18	

XL.

Austria. — Kremsmünster. Lat. 48° 3′ N. Long. 14° 7′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	CB 01 110	eaumur.						
Hours.	Jan.	Feb.	March	April	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.50	0.00	1.05		0.00	0.55	1.00	1	1.50	1.00	0.01	0.40	
Morn. 1	0.58		i	1.14	1	1	1	1.94	1	1		1	
2	0.66		ı	1.36	1	3.08	2.16	2.26	1.94	1.58	0.72	0.42	1.60
3	0.71	1.07	1.57	1.63	ł	3.14	2.35	2.50	2.32	1.82	0.78	0.42	1.76
4	0.78	1.12	1.80	1.88	2.78	2.90	2.34	2.54	2.58	1.97	0.83	0.42	1.83
5	0.84	1.19	1.90	1.99	2.44	2.32	2.08	2.30	2.60	1.98	0.88	0.46	1.75
6	0.88	1.24	1.82	1.88	1.86	1.54	1.54	1.80	2.34	1.91	0.93	0.54	1.52
7	0.84	1.26	1.50	1.41	1.11	0.68	0.94	1.11	1.81	1.63	1	1	1.15
8	0.67	1.07	0.96	0.87	0.31	i		0.35			0.80	1	1 1
9	0.35	0.67	0.30	0.14	-0.45	-0.86	-0.42	-0.37	0.28	0.62	0.51	0.38	0.10
10	-0.10	i	-0.41	l .	1	1	-0.95		1			1	-0.56
11	-0.58		1				-1.39					1	1 1
[]	1												-1.08
Noon	-0.95	-1.37	-1.56	-1.65	-2.09	-2.17	-1.75	-1.86	-1.81	-1.68	-0.97	-0.78	-1.56
1	-1.22	-1.78	-1.89	-1.93	-2.42	-2.42	-2.05	-2.21	-2.28	-2.25	-1.30	-1.03	-1.90
2		-1.90											
3		-1.69											
4		-1.32											
									i				
5		-0.92											
6	-0.35	-0.57	-1.08	-1.18	-1.62	-1.66	-1.38	-1.49	-1.66	-1.14	-0.41		
7		-0.36										l	-0.62
8	-0.04	-0.19	-0.23	-0.17	-0.34	-0.35	-0.15	-0.24	-0.46	-0.26	-0.11	0.09	-0.20
9	0.07	-0.02	0.13	0.28	0.28	0.34	0.38	0.30	0.05	0.06	-0.02	0.12	0.16
10	0.20	0.18	0.42	0.61	0.84	1.02	0.82	0.76	0.46	0.34	0.11	0.18	0.49
11	0.34	0.46	0.63	0.82	1.36	1.68	1.19	1.15	0.80	0.63	0.27	0.25	0.80
Midn	0.47	0.70	0.83	0.97	1.85	2.27	1.52	1.53	1.14	0.94	0.46	0.34	1.08
6. 6	0.27	0.34	0.37	0.35	0.12	-0.06	0.08	0.16	0.34	0.39	0.26	0.22	0.24
7. 7	0.33	0.45	0.43	0.37	i	-0.18	0.09	0.13	0.38	0.48	0.35	0.29	0.27
8.8	0.32	0.44	0.37		-0.02		0.04	0.06	0.32	0.48	0.35	0.24	0.24
9. 9	0.21	0.33	0.22		-0.09			-0.04	0.17	0.34	0.25	0.25	0.13
10.10	0.05	0.10	0.01				-0.02		1 1	0.11	0.23	0.12	0.13
7. 2. 9		-0.22											
6. 2. 8	-0.14	-0.28	-0.14	-0.12	1		-0.29	-0.27	-0.23	-0.29	-0.19	-0.15	-0.24
6. 2.10	-0.06	-0.16	0.07	0.14	0.03	-0.01	0.03	0.06	0.08	-0.09	-0.12	-0.12	-0.01
6. 2. 6	-0.24	-0.41	-0.43	-0.45	-0.79	-0.90	-0.70	-0.69	-0.63	-0.94	-0.36	-0.15	-0.56
7. 2	-0.21	-0.32	-0.26	-0.33	-0.76	-0.95	-0.66	-0.63	-0.38	-0.45	-0.24	-0.25	-0.45
8. 2		-0.42											
8. 1		-0.36											
7. 1	-0.19	-0.26	-0.20	-0.26	-0.66	-0.87	-0.56	-0.55	-0.24	-0.31	-0.19	-0.22	-0.38
				1		- 1	1						
9.12.3.9		-0.60											
7. 2.2(9)	-0.07	-0.17	-0.07	-0.02	-0.24	-0.31	-0.15	-0.17	-0.14	-0.19	-0.13	-0.07	-0.14
Dail. ext.	-0.19	-0.32	-0.06	-0.04	0.09	0.36	0.01	0.04	-0.03	-0.2 8	-0.21	-0.25	-0.08

XLI.

Austria. - Salzburg. Lat. 47° 48' N. Long. 13° 1' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.54	0.70	1.06	1.31	2.03	2.07	1.87	1.57	1.21	1.02	0.48	0.42	1.19
1	0.59	0.79	1.29	1.58	2.37	2.27	2.13	1.81	1.45	1.15	0.65	0.50	1.38
2	0.72	0.97	0.51	1.79	2.64	2.56	2.36	2.05	1.61	1.27	0.81	0.59	1.49
3	0.82	1.08	1.75	2.04	2.90	2.73	2.64	2.24	1.87	1.41	0.88	0.70	1.75
4	0.96	1.09	1.89	2.21	3.10	2.82	2.62	2.23	2.01	1.52	0.91	0.69	1.84
5	1.03	1.28	2.01	2.37	3.10	2.75	2.59	2.24	2.14	1.72	1.03	0.81	1.92
6	1.06	1.34	2.14	2.28	2.76	2.45	2.31	2.26	2.18	1.77	1.03	0.87	1.87
7	1.09	1.36	2.06	1.86	1.89	1.53	1.61	1.74	1.94	1.74	1.06	0.94	1.57
s	1.12	1.24	1.58	1.06	0.84	0.63	0.67	0.89	1.15	1.26	1.07	1.00	1.04
9	0.91	0.75	0.76	0.14	-0.10	-0.25	0.20	0.04	0.33	0.48	0.64	0.74	0.39
10	0.38	0.04	-0.06	-0.67	-0.92	-1.10	-0.97	-0.76	-0.53	-0.35	0.06	0.21	-0.39
11	-0.26	-0.62	-0.96	-1.39	-1.80	-1.87	-1.63	-1.40	-1.25	-1.17	-0.62	-0.35	-1.11
Noon	-0.90	-1.19	-1.75	-1.99	-2.36	-2.90	-2.14	-2.13	-2.00	-1.84	-1.25	-0.93	-1.78
1	-1.47		-2.26				1	-2.59				-1.47	
2	-1.70	-1.96	-2.55	-2.74	-3.08		i	-2.73				-1.64	-2.44
3	-1.68	-2.04	-2.61	-2.74	-3.21		i	-2.75			1	-1.55	-2.45
4	-1.40	-1.80	-2.55	-2.60	-3.27	-3.00	-2.90	-2.85	-2.56	-2.21	-1.37	-1.19	-2.31
5	-1.00	-1.46	-2.26	-2.10	-2.97	-2.64	-2.64	-2.46	-2.09	-1.63	-0.85	-0.72	-1.90
6	-0.60	-0.76	_1 51	_1.50	_9 97	. 9.10	-2.05	-1.78	1 91	-0.83	-0.35	-0.42	_1.00
7	-0.31		-0.76	i		-1.21		-0.85	-0.48	-0.29	-0.10		-0.65
8	-0.25		-0.16			-0.13		0.06	0.15	0.16	0.11		-0.06
9	-0.04	0.20	0.17	0.51	0.48	0.71	0.67	0.70	0.15	0.48	0.24	0.04	0.40
10	0.12	0.43	0.46	0.81	1.03	1.41	1.22	1.09	0.78	0.76	0.34	0.33	0.73
11	0.28	0.53	0.76	1.08	1.50	1.70	1.56	1.38	0.76	1.03	0.52	0.41	0.96
Mean.	-2 71	1.14	2.49	6.90	10.42	13.22	13.93	13.66	10.39	7.37	1.52	1.63	

XLII.

Germany. — Munich. Lat. 48° 9′ N. Long. 11° 37′ E. Greenw. — Dove.

Hour	Jan.	Feb.	March.	April.	May.	June	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Year.
Midn	0.71	0.92	1.54	2.27	2.58	2.49	2.84	2.37	2.17	1.53	0.91	0.46	1.73
1	0.90	1.04	1.83	2.37	3.02	3.06	3.27	2.64	2.33	1.59	0.87	0.58	1.96
2	0.97	1.18	2.04	2.62	3.30	3.39	3.56	2.94	2.61	1.67	0.94	0.67	2.16
3	1.04	1.30	2.16	2.89	3.61	3.66	3.80	3.19	2.81	1.78	1.00	0.77	2.33
4	1.03	1.33	2.25	3.12	3.85	3.82	4.05	3.41	2.98	1.91	1.04	0.85	2.47
5	1.07	1.43	2.37	3.29	3.69	3.25	3.71	3.50	3.16	2.01	1.12	0.92	2.46
1			1					!				- 1	
6	1.14	1.52	2.56	2.93	2.61	2 11	2.41	2.79	3.08	2.14	1 13	0 99	2.12
7	1.17	1.55	2.17	1.80	1.21	0.77	0.93	1.48	2.22	1.84	1.13	0.97	1.44
8	1.10	1.14	1.14	0.36	-0.07	-0.35	-0.28	0.18	0.59	0.99	0.75	0.88	0.54
9	0.46	0.36	-0.11	-0.79	-1.00	-1.21	-1.25	-1.05	-0.74	-0.24	0.06	0.41	-0.42
10	-0.72	-0.61	-1.18	-1.80	-1.99	-1.96	-2.12	-1.88	-1.70	-1.34	-0.79	-0.42	-1.38
11	-1.06	-1.46	-2.04	-2.39	-2.59	-2.69	-2.66	-2.58	-2.61	-2.19	-1.49	-0.97	-2.06
				-									

XLII.

GERMANY. - MUNICH, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon	-1.70	-1.93	-2.67	-2.99	-3.28	-2.98	-3.14	-3.09	-3.18	-2.69	-1.94	-1.02	-2.55
1	-2.08	-2.31	-3.01	-3.27	-3.59	-3.41	-3.48	-3.55	-3.58	-3.08	-2.23	-1.83	-2.95
2	-2.15	-2.40	-3.24	-3.60	-3.77	-3.79	-3.75	-3.72	-3.74	-3.15	-2.05	-1.85	-3.10
3	-1.83	-2.15	-3.17	-3.45	-3.77	-3.54	-3.S3	-3.58	-3.56	-2.87	-1.75	-1.43	-2.91
4	-1.08	-1.67	-2.64	-3.18	-3.41	-3.34	-3.49	-3.30	-3.24	-2.27	-1.02	-0.76	-2.45
5	-0.46	-0.95	-1.93	-2.51	-2.87	-2.80	-3.07	-2.76	-2.56	-1.27	-0.43	-0.34	-1.83
													1
6	-0.16	-0.37	-0.94	-1.53	-2.05	-1.94	-2.32	-1.81	-1.29	-0.44	-0.12	-0.13	-1.09
7	0.04	-0.07	-0.20	-0.36	-0.74	-0.84	-2.99	-0.47	-0.30	0.08	0.20	0.06	-0.47
8	0.23	0.22	0.28	0.40	0.41	0.61	0.40	0.55	0.37	0.56	0.44	0.14	0.38
9	0.39	0.45	0.55	0.91	1.13	1.35	1.20	1.15	0.93	0.88	0.57	0.23	0.81
10	0.49	0.59	1.02	1.31	1.65	1.86	1.87	1.60	1.40	1.14	0.74	0.33	1.17
11	0.61	0.77	1.33	1.69	2.18	2.28	2.41	2.06	1.80	1.34	0.85	0.40	1.48
Mean.	-2.15	-0.12	0.75	5.57	9.29	12.74	13.65	12.93	9.45	6.28	1.55	-1.28	

XLIII.

Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 25′ E. Greenw. — Dove.

					D	egrees of	Reaum	ur.					
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug	Sept	Oct.	Nov.	Dec.	Year.
Midn	0.30	0.52	1.03	1.47	1.70	1.68	1.72	1.17	1.23	0.84	0.36	0.25	1.02
1	0.40	0.60	1.14	1.68	1.97	1.97	2.05	1.78	1.49	1.02	0.45	0.32	1.24
2	0.50	0.71	1.29	1.95	2.25	2.23	2.34	2.10	1.72	1.19	0.54	0.39	1.43
3	0.55	0.83	1.44	2.17	2.46	2.47	2 60	2.3 $^{\circ}$	1.96	1.31	0.61	0.50	1.61
4	0.65	0.89	1.60	2.39	2.75	2.71	2.91	2.63	2.19	1.49	0.70	0.56	1.79
5	0.71	0.99	1.72	2.64	2.96	2.86	3.07	2.88	2.43	1.65	0.77	0.65	1.94
6	0.77	1.00	1.31	2.75	2.96	2.71	2.92	2.93	2.61	1.73	0.82	0.72	1.98
7	0.68	0.99	1.53	2.32	2.11	1.88	2.13	2.34	2.29	1.65	0.79	0.73	1.62
8	0.73	0.88	1.28	1.29	0.98	0.82	1.02	1.30	1.62	1.29	0.66	0.70	1.05
9	0.62	0.57	0.63	0.32	0.06	-0.14	0.17	0.21	0.60	0.70	0.41	0.54	0.39
10	0.26	0.15	-0.11	-0.53	-0.91	-0.93	-0.95	-0.77	-0.51	-0.10	-0.12	0.17	-0.26
11	-0.16	-0.45	-0.77	-1.51	-1.60	-1.58	-1.62	-1.50	-1.46	-0.86	-0.46	-0.22	-1.02
Noou	-0.60	-0.92	-1.37	-2.09	-2.16	-2.08	-2.16	-2.18	-2.02	-1.53	-0.86	-0.65	-1.55
1	-0.93	-1.27	-1.83	-2.48	-2.56	-2.48	-2.59	-2.61	-2.56	-2.01	-1.13	-0.95	-1.95
2	-1.10	-1.50	-2.20	-2.74	-2.80	-2.73	-2.83	-2.89	-2.84	-2.31	-1.25	-1.07	-2.19
3	-1.11	-1.51	-2.29	-2.88	-2.90	-2.79	-2.93	-3.01	-2.96	-2.32	-1.28	-0.99	-2.25
4	-0.93	-1.05	-2.20	-2.76	-2.82	-2.71	-2.92	-2.85	-2.78	-2.10	-0.87	-0.79	-2.09
5	-0.63	-0.97	-1.83	-2.46	-2.53	-2.56	-2.83	-2.66	-2.35	-1.58	-0.62	-0.55	-1.80
6	-0.44	-0.61	-1.26	-1.91	-2.17	-2.10	-2.36	-2.11	-1.64	-1.01	-0.36	-0.37	-1.36
7	-0.31	-0.32	-0.70	-1.12	-1.49	-1.37	-1.59	-1.23	-0.87	-0.54	-0.19	-0.21	-0.83
8	-0.23	-0.06	-0.24	-0.33	-0.51	-0.39	-0.58	-0.34	-0.24	-0.10	0.01	-0.19	-0.27
9	0.01	0.12	0.09	0.20	0.27	0.30	0.22	0.20	0.27	0.23	0.16	0.06	0.18
10	0.10	0.26	0.40	0.72	0.80	0.91	0.90	0.81	0.74	0.51	0.29	0.16	0.55
11	0.19	0.39	0.66	1.12	1.24	1.28	1.32	1.20	1.08	0.85	0.43	0.25	0.83
Mean.	-1.69	0.61	2.20	7.27	11.27	14.47	15.66	15.01	11.52	7.94	3.02	-0.12	

XLIV.

Bohemia. — Prague. Lat. 50° 5′ N. Long. 14° 24′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	}												
Morn. 1	0.45	0.76	0.86	1.73	1.47	1.90	1.93	1.59	1.46	1.06	0.73	0.45	1.20
2	0.52	0.88	1.05	2.06	1.77	2.22	2.24	1.85	1.69	1.18	0.79	0.52	1.40
3	0.54	0.98	1.24	2 45	2.08	2.62	2.36	2.04	1.85	1.23	0.82	0.54	1.56
4	0.53	1.06	1.42	2.82	2.31	3.02	2.27	2.10	1.95	1.24	0.78	0.55	1.67
5	0.50	1.14	1.55	3.02	2.35	3.22	2.01	2.01	1.97	1.22	0.78	0.60	1.70
6	0.49		1.60	2.92	2.12	3.03	1.62	1.76	1.90	1	0.80	ĺ	1.61
7	0.47	1.09	1.51	2.43	1.62	2.40	1.16	1.36	1.69	1.10	0.77	0.80	1.37
8	0.42	0.91	1.24	1.59	0.92	1.40	0.66	0.83		0.90			0.97
	0.20			0.50		0.04			0.01		0.40	0.00	0.10
9	0.29	0.55	0.77	0.53	0.15	0.24	0.10	1		1	0.42	0.67	0.42
10	11	-1.01	1	-0.56		1	ì		1	-0.07			-0.31
11	1}	-1.19	ł	-1.52	l .	ł	1	1	1		1	-1.18	-0.95
Noon	-0.52	-1.10	-1.16	-2.25	-1.60	-2.23	-1.84	-1.86	-2.00	-1.47	-1.10	-0.70	-1.49
1	-0.76	-1.51	$ _{-1.63}$	-2.74	-1.91	-2.55	-2.37	-2.33	-2.63	-1.99	-1.47	-1.08	-1.91
2	11	1	i	1	1					1		-1.23	-2.13
3	II .	ł	1	i	ı						1	-1.13	1
4		1		1	l			1		ĺ	l .	-0.87	
4	-0.71	-1.55	1.75	-2.51	-2.20	-2.30	-2.50		291	-1.03	1.03	0.07	-1.00
5	-0.51	-1.05	-1.45	-2.65	-2.08	-2.86	-1.86	-1.75	-1.70	-1.14	-0.67	-0.56	-1.52
6	-0.31	-0.66	-1.10	-2.13	-1.71	-2.45	-1.28	-1.18	-1.07	-0.60	-0.31	-0.31	-1.09
7	-0.16	-0.34	-0.73	-1.42	-1.17	-1.75	-0.73	-0.62	-0.52	-0.17	-0.04	-0.17	-0.65
8	-0.06	-0.09	-0.40	-0.64	-0.56	-0.85	-0.24	-0.12	-0.08	0.13	0.10	-0.11	-0.24
	0.02		0.10	0.11	0.00	0.06	0.19	0.30	0.26	0.24	0.20	0.07	0.70
9	1			0.11	0.03				1]		0.12
10	0.11	1.35	0.18	0.71	0.52	0.81	0.61	0.65	0.57	0.51	0.32	0.01	0.53
11	0.22	1.10	0.42	1.15	0.89	1.32	1.05	0.97	0.87	0.70	0.44	0.14	0.77
Midn	0.34	0 61	0.65	1.46	1.18	1.64	1.51	1.28	1.17	0.89	0.61	0.31	0.97
									ļ				
6. 6	0.09	0.24	0.25	0.40	0.21	0.29	0.17	0.29	0.42	0.29	0.25	0.19	0.26
7. 7	0.15	0.38	0.39	0.50	0.22	0.33	0.22	0.37	0.59	0.47	0.37	0.32	0.36
8. 8	0.18	0.41	0.42	0.47	0.18	0.27	0.21	0.36	0.60	0.51	0.39	0.35	0.36
9. 9	0.16	0.33	0.34	0.32	0.90	0.15	0.15	0.25	0.45	0.42	0.31	0.30	0.27
10.10	0.09	0.17	0.17	1	-0.03	-0.02	0.04	0.07	0.18	0.22	0.15	0.16	0.11
7. 2. 9	-0.13	-0.17	-0.16	-0.15	-0.16	-0.10	-0.4.1	-0.30	-0.31	-0.26	-0.20	-0.17	-0.21
6. 2. 8		1		-0.13				1	1		1		-0.25
6. 2.10	-0.09	1	-0.23	0.21	0.15			1		-0.17		1	0.01
6. 2. 6		l		-0.74				1		l .	(-0.54
7. 2	1 1	1							1		i	-0.22	1 1
8. 2	4							1		1	1	-0.21	
8. 1				1				1	1	ł		-0.13	
7. 1	-0.15	-0.21	-0.06	-0.16	-0.15	-0.08	-0.61	-0.49	-0.47	-0.45	-0.35	-0.14	-0.28
9.12.3.9	-0.2*	-0 50	_0.60	_1 17	_0 09	_1 91	_1 0×	-0.05	_0 0~	-0.69	_0 19	-0.31	-0.76
7. 2.2(9)												-0.14	
		'							1				
Dail. ext.	-0.17	-0.18	-0.16	-0.03	0.05	0.12	-0.15	-0.24	-0.46	-0.49	-0.38	0.21	-0.22

XLV.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degrees	of Far	renheit.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean,
								4.70	3.24	2 00		0.05	2.95
Morn. 1	0.86	1.46	2 32	4.01	5.13	4.34	4.75	4.16	i	2.66	1.58	0.95	
2	0.90	1.67	2.63	4.43	5.94	4.82	5.38	4.79	3.60	2.79	1.69	0.86	3.29
3	0.99	1.87	3 02	4.91	6.62	5.13	5.69	5.45	4.03	3.02	1.80	0.74	3.60
4	1.15	2.12	3.31	5.13	6.75	5.00	5.58	5.76	4.34	3.31	1.96	0.81	3.76
5	1.37	2.36	3.40	4.91	6.03	4.57	4.82	5.42	4.25	3.51	2.09	1.04	3.65
6	1.53	2.48	3.08	3.98	4.37	2.79	3 35	4.21	3.62	3.38	2.14	1.31	3.02
7	1.46	2 30	2.25	2.39	2.00	0.95	1.92	2.25	2.32	2.66	1.89	1.40	1.94
8	1.10	1.67	0.97	0.29	-0.54	-1.01	-0.65	-0.11	0.50	1.26	1.24	1.13	0.50
9	0.36	0.59	_0.63	_1.01	-2.88	_9.70	_9 57	_2 39	-1.53	_0.65	0.16	0.41	-1.15
1 11	-0.61		-2.23		-4.57								1
10							,				ı	(1
11	-1.58		-3.56									l .	1
	-2.32	-3.33	-4.43	-6.17	-6.12	-4.93	-5.58	-5.87	-9.14	-5.40	-3.29	-2.43	-4.04
Noon. 1	-2.63			-6.37			-5.81						
2	-2.50	-3.69	-4.43	-5.99	-6.37	-4.91	-5.76	-5.72	-5.49	-4.84	-3.22	-2.45	-4.61
3			-3.74										
4	-1.26		1	1	-5.47			3	4	1	1		,
	2 - 2			2.50				0.44	0.10	1 00	0.77	0.41	0.10
5	-0.59				-4.32			1	1	1		L.	-2.12
6	-0.07	-0.38	1		-2.68		1	I	1				-1.06
7	0.29	0.09	0.14	1	-0.81	1	-0.3S	1	1	0.23			-0.05
8	0.50	0.36	0.86	1.26	0.99	0.74	1.10	1.06	1.37	0.79	0.25	0.52	0.81
9	0.63	0.56	1.35	2.25	2.36	2.21	2.27	2.23	2.12	1.33	0.47	0.72	1.55
10	0.72	0.77		2.93	3.29	2.93	3.11	2.97	2.59	1.85	0.77	0.88	2.05
11	0.79	0.99	1	1	3.89	3.44		1	2.84		1		2.39
Midn	0.83	1.26		3.67	1	3.87	1		2.99	l.	l		1
Midi	0.00	1.20	1.01	0.0.	1.10	0.01	11.21	0		2.1	1.5	1	
				7.00	0.00		0.00	0.00	1.00	, ,	0.05	0.00	0.99
6. 6	0.74	1.06				0.54			1	1	1	I.	1
7. 7	0.88	1		1	1	0.34		1	1				
8. 8	0.81			1	1	1	1	1	1		1)	[
9. 9	0.50	1	i	1		1		1	1	1		i	ł
10.10	0.07	-0.05	0.27	-0.52	-0.65	-0.47	-0.47	-0.63	-0.48	-0.43	-0.20	0.1	1-0.32
7. 2. 9	-0.14	-0.27	-0.27	-0.45	-0.68	-0.59	0.70	$ _{-0.41}$	-0.36	-0.29	-0.29	-0.11	-0.38
6. 2. 8	H	-0.29			-0.34								
6. 2.10	li .	-0.10	1	-				1	1		[-0.1]		
6. 2. 6	II .	1	1 -0.70		1	1	1				-0.4		1
7. 2													1-1.35
8. 2	11	1							1	1	1		-2.07
8. 1	H			1	1		1				1	1	9 -2.21
7. 1	-0.59	-0.79	9 -1.2	1 -2.00	-2.18	-2.0	[-2.2]	1 -1.87	7 -1.80	-1.4	1-0.8	3 -0.6	5 -1.46
9.12.3.9	-0.8	3 -1 2	1 -1.8	7 -2.7	7 -1.20) -2.5	2 -2.8	-2.8	1 -2.4	5 -2.1	2 -1.28	3 -0.79	$ _{-2.07}$
7. 2.2(9)	11	7 -0.0	1		i	1				1	1 -0.09	1	i i
11 " 2.2(3)	0.5	1 0.0		1 0.2.	1	3.1		1 0.1	1		- 0.0.	1	

XLVI.

England. — Plymouth. Lat. 50° 22' N. Long. 4° 7' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.38	0.65	1.03	1.78	2.28	1.93	2.11	1.85	1.44	1.18	0.70	0.42	1.31
Morn. 1	0.40	0.74	1.17	1.97	2.64	2.14	2.39	2.13	1.60	1.24	0.75	0.38	1.46
3	0.44	0.83	1.34	2.18	2.94	2.28	2.53	2.42	1.79	1.34	0.80	0.33	1.60
4	0.51	0.94	1.47	2.28	3.00	2.22	2.48	2.56	1.93	1.47	0.87	0.36	1.67
5	0.61	1.05	1.51	2.18	2.68	2.03	2.14	2.41	1.89	1.56	0.93	0.46	1.62
6	0.68	1.10	1.37	1.77	1.94	1.24	1.49	1.87	1.61	1.50	0.95	0.58	1.34
7	0.65	1.02	1.00	1.06	0.89	0.42	0.63	1.00	1.03	1.18	0.84	0.62	0.86
8	0.49	0.74	0.43	0.13	-0.24	-0.45	-0.29	-0.05	0.22	0.56	0.55	0.50	0.22
9	0.16	0.26	-0.28	-0.86	-1.2 8	-1.20	-1.14	-1.06	-0.68	-0.29	0.07	0.18	-0.51
10			-0.99					1	ı			ı	-1.19
11 ,	1	F	-1.58					1				-0.74) I
Noon	-1.03	-1.48	-1.97	-2.74	-2.72	-2.19	-2.4 8	-2.61	-2.55	-2.4 0	-1.46	-1.08	-2.06
1	-1.17	-1.71	-2.09	-2.83	-2.83	-2.23	-2.5 8	-2.65	-2.63	-2.45	-1.58	-1.20	-2.16
2	-1.11	-1.64	-1.97	-2.66	-2.83	-2.1 8	-2.56	-2.54	-2.44	-2.15	-1.43	-1.09	-2.05
3	-0.87	-1.34	-1.66	-2.32	-2.72	-2.06	-2.40	-2.34	-2.06	-1.65	-1.09	-0.82	-1.78
4	-0.56	-0.92	-1.25	-1.84	-2.43	-1.7 9	-2. 06	-2.01	-1.55	-1.09	-0.69	-0.49	-1.39
5	-0.26	-0.49	-0.78	-1.27	-1.92	-1.35	-1.54	-1.53	-0.97	-0.59	-0.34	-0.18	-0.94
6	-0.03	-0.17	-0. 33	-0.63	-1.19	-0.77	-0.89	-0.99	-0.39	-0.20	-0.10	0.02	-0.47
7	0.13	0.04	0.06	-0.00	-0. 36	-0.12	-0.17	-0.21	0.16	0.10	0.03	0.15	-0.02
8	0.22	0.16	0.38	0.56	0.44	0.33	0.49	0.47	0.61	0.35	0.11	0.23	0.36
9	0.28	0.25	0.60	1.00	1.05	0.98	1.01	0.99	0.94	0.59	0.21	0.32	0.69
10	0.32	0.34	0.75	1.30	1.46	1.30	1.38	1.32	1.15	0.82	0.34	0.39	0.91
11	0.35	0.44	0.84	1.49	1.73	1.53	1.63	1.51	1.26	0.99	0.48	0.45	1.06
Midn	0.37	0.56	0.92	1.63	1.98	1.72	1.87	1.65	1.33	1.10	0.61	0.46	1.18
	0.00		0.50	0	0.00	0.01	0.00			0.05	0.40	0.00	
6. 6	0.33	$0.47 \\ 0.53$	$0.52 \\ 0.53$	$0.57 \\ 0.53$	$0.38 \\ 0.27$	$0.24 \\ 0.15$	$0.30 \\ 0.23$	0.44	0.61	$0.65 \\ 0.64$	$0.43 \\ 0.44$	0.30 0.39	0.44
8.8	0.36	0.35	0.33	0.35		-0.06	0.23	0.40	0.42	0.46	0.33	0.37	0.42
9. 9	0.30	0.26	0.16	0.07		-0.11	-0.07	-0.04	0.13	0.15	0.14	0.25	0.09
10.10	0.03	Į.	1	-0.23		-0.21	-0.21	-0.28		5	-0.09	0.06	1
7. 2. 9	-0.06	-0.19	-0.12	-0.20	-0.30	-0.26	-0.31	-0.18	-0.16	-0.13	-0.13	-0.05	-0.17
6. 2. 8			-0.07					-0.07			-0.12		
6. 2.10		-0.07		0.14	0.19	0.12	0.10	1		i .	-0.05		1
6. 2. 6		1	-0.31			-0.57	1		-0.41	!	-0.19		1
7. 2	-0.23	-0.31	-0.42	-0.80	-0.97	-0.88	-0.97	-0.77	-0.71	-0.49	-0.30	-0.24	-0.60
8. 2			-0.77					1	i	1	1	1	1
8. 1		1	-0.83	l .	l .		1	i		1		1	
7. 1	11	1	-0.55				1	l .	1	1	1	1	1
9.12.3.9	_0.27	-0.50	-0.83	_1 22	-1.42	-1.12	-1.25	_1 20	-1.09	-0.04	-0.57	_0.35	-0.92
7. 2.2(9)	11	-0.03		0.10	0.04	Į.	0.02	1	1		-0.04	1	i
Dail.ext.	-0.25			_0.28	0.09	0.03	-0.03	-0.05	-0.35	-0.45	-0.32	-0.29	-0.25

XLVII.

Belgium. — Brussels. Lat. 50° 51′ N. Long. 4° 22′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Resumur.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.58	0.67	1.19	2.23	2.57	2.83	2.34	2.49	1.71	0.85	0.49	0.73	1.56
2	0.60	0.73	1.36	2.59	2.89	3.12	2.57	2.84	2.00	0.99	0.49	0.39	1.71
3	0.60	0.79	1.54	2.99	3.17	3.18	2.74	3.20	2.33	1.15	0.54	0.08	1.86
4	0.60	0.86	1.70	3.29	3.28	3.14	2.74	3.42	2.57	1.31	0.65	0.02	1.97
5	0.62	0.92	1.79	3.29	3.06	2.71	2.47	3.32	2.58	1.40	l	0.25	1.93
6	0.64	0.97	1.74	2.86	2.45	2.00	1.88	2.82	2.28	1.35	0.85	0.65	1.71
7	0.61	0.93	1.50	2.01	1.52	1.10	1.06	1.94	1.67	1.11	0.81	0.97	1.27
8	0.46	0.75	1.03	0.86	0.44	0.16	0.15	0.82	0.82	0.68	0.58	0.97	0.64
	0.70	0.00	0.00	0.05	0.50	0.01	0.00			0.00	0.10	0.50	0.00
9	0.18	0.39		-0.35		Į.	l	4	1	0.08	0.19		-0.08
10	-0.22			-1.42									
11		-0.71		-2.23		1	l	l .		1	l	-0.84	I I
Noon	-1.01	-1.23	-1.72	-2.77	-2.52	-2.27	-2.06	-2.81	-2.48	-1.71	-1.16	-1.29	-1.92
1	_1.90	-1.57	_9.19	-9 11	-2.89	_2 65	_2 20	_9 0**	-2.88	_1 06	_1 29	-1.33	_9 99
] [l	!	•	l .)		i I
2	-1.19			-3.29			-2.51		-3.05	i	l	l	, ,
3				-3.33								-0.59	1 !
4	-0.70	-1.14	-1.93	-3.18	-3.36	-3.16	-2.71	-3.53	-2.63	-1.31	-0.75	-0.20	-2.06
5	-0.39	-0.72	-1.51	-2.76	-2 97	-2.83	-2.47	-3.02	-2.05	-0.84	-0.45	-0.16	-1.68
6				-2.70		1	ł	ì	1	1		-0.25	
7	0.02			-1.13		1	-1.11	l	-0.49	l	l	-0.37	í I
8	0.02			1			l	-0.09		1	l .	-0.33	
	0.12	0.17	-0.10	-0.16	-0.12	-0.51	-0.20	-0.03	0.2.5	0.20	0.13	0.00	0.05
9	0.21	0.31	0.28	0.69	0.82	0.68	0.64	0.82	0.78	0.48	0.32	0.05	0.50
10	0.31	0.41	0.59	1.31	1.51	1.37	1.31	1.48	1.13	0.60	0.41	0.37	0.90
11	0.42	0.50	0.83	1.70	1.96	ı	1.77	1.89	1.33	0.68	0.47	0.75	1.19
Midn	0.52	0.59	1.02	1.96	2.28	2.44	2.08	2.19	1.49	0.75	0.49	0.89	1.39
Midi	0.02	0.00	1.02	1.00	2.20	2.11	2.00		1.10		0.20		
	1												
6. 6	0.25	0.32	0.35	0.41	0.12	-0.09	-0.01	0.31	0.49	0.48	0.33	0.20	0.26
7. 7	0.31	0.45	0.47	0.44	0.16	-0.09	-0.02	0.39	0.59	0.55	0.42	0.30	0.33
8.8	0.29	0.46	0.47	0.35	0.16	-0.07	-0.03	0.37	0.53	0.48	0.39	0.32	0.31
9. 9	0.20	0.35	0.34	0.17	0.12	0.04	-0.02	0.24	0.32	0.28	0.25	0.25	0.21
10.10	0.05	0.14	0.11	0.05	0.04	0.01	-0.01	0.05	0.03	0.00	0.05	0.12	0.05
<u> </u>													
7. 2. 9		-0.14	-0.17	-0.20	-0.29	-0.40	-0.27	-0.27	-0.20	-0.12	-0.05	-0.04	-0.19
6. 2. 8		-0.17		-0.20									
6. 2.10	}	-0.09	0.01	0.29	0.25		0.23	0.24	0.12		-0.00		0.09
6. 2. 6	-0.23	-0.34	-0.53	-0.83	-0.99	-1.05	-0.85	-0.98	-0.69	-0.33	-0.20	-0.21	-0.60
	0.00	0.00	0.40	0.0.	0.05	00.	0.50	0.00	0.60	-0.49	_0.99	-0.09	_0.59
7. 2	-0.29	-0.36	-0.40	-0.64	-0.85	-0.94	-0.73	1.00	-0 09	_0.42	_0.23	_0.03	_0.95
8. 2	-0.37	-0.45	-0.63	-1.22	-1.39	-1.41	-1.18	-1.38	1.02	-0.04	-0.50 -0.0*	_0.03	_0.50
8. 1	-0.37	-0.41	-0.55	-1.13	-1.23	-1.25	-1.07	-1.23	-1.03	-0.64	0.37	-0.18	-0.19
7. 1	-0.30	-0.32	-0.32	-0.55	-0.69	-0.78	-0.62	-0.67	-0.61	-0.43	-0.26	-0.18	-0.45
9.12.2.9	-0.10	-0.51	-0.89	-1.44	-1.49	-1 36	-1 20	-1.51	-1.21	-0.72	0.43	-0.34	$_{-0.95}$
11		-0.03				-0.13			0.05	0.03		-0.04	- 1
7. 2.2(9)	0.04	-0.03	-0.00	0.03	0.01	0.15	0.04	0.00	0.00	0.00	0.00	0.04	0.02
Dail.ext.	-0.28	-0.34	-0.25	-0.02	-0.06	-0.04	0.02	-0.14	-0.24	-0.28	-0.24	-0.18	-0.18
25.611.63.61	1 3.20	1 0.01	0.20										

XLVIII.

Belgium. - Brussels. Lat. 50° 51′ N. Long. 4° 22′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.30	0.60	1.09	1.72	2.27	2.46	2.20	1.88	1.52	0.92	0.51	0.30	1.3
2	0.56	0.82	1.39	2.19	3.00	2.82	2.77	2.44	2.03	1.20	0.77	0.47	1.70
4	0.64	0.97	1.66	2.64	3.32	3.53	3.14	2.76	2.38	1.44	0.83	0.62	1.9
6	0.66	1.03	1.83	2.43	2.44	2.27	2.30	2.44	2.47	1.56	0.93	0.63	1.7
8	0.67	0.84	1.02	0.76	0.49	0.41	0.32	0.68	1.03	0.96	0.79	0.63	0.7
9	0.36	0.33	0.21	-0.38	0.61	-0.61	-0.63	-0.39	-0.14	0.07	0.21	0.34	0.0
10	0.07	-0.09	-0.54	-1.18	-1.43	-1.32	-1.36	-1.26	-1.19	-0.78	-0.36	-0.08	-0.79
Noon.	-0.92	-1.27	-1.78	-2.42	-2.61	-2.47	-2.35	-2.47	-2.46	-1.87	-1.27	-0.83	-1.8
2	-1.15	-1.65	-2.30	-2.95	-3.22	-3.21	-2.92	-3.08	-3.04	-2.17	-1.42	-1.04	-2.3
4	-0.72	-1.19	-2.04	-2.63	-3.15	-3.18	-2.90	-2.93	-2.70	-1.61	-0.90	-0.65	-2.0
6	-0.21	-0.49	-0.94	-1.71	-2.44	-2.57	-2.38	-1.87	-1.21	-0.37	-0.28	-0.18	-1.2
8	-0.08	-0.05	-0.00	0.13	0.05	-0.16	-0.15	0.17	0.21	0.23	0.07	-0.03	0.0
9	0.13	0.17	0.31	0.63	0.76	0.80	0.79	0.76	0.64	0.43	0.24	0.07	0.4
10	0.20	0.30	0.58	1.04	1.25	1.45	1.39	1.27	1.01	0.54	0.38	0.14	0.8
Mean.	0.52	2.45	3.56	7 97	10 37	13 10	13.69	13.58	11.22	7.69	4.72	1.89	

XLIX.

Germany. — Schwerin. Lat. 53° 36' N. Long. 11° 30' E. Gr. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.05	0.49	0.92	1.66	1.97	2.10	2.12	1.92	1.70	0.87	0.21	0.16	1.18
2	0.08	0.69	1.20	2.17	2.44	2.69	2.72	2.41	2.19	1.14	0.24	0.34	1.53
4	0.27	0.83	1.43	2.53	2.96	2.97	2.96	2.62	2.54	1.51	0.42	0.48	1.79
6	0.35	0.86	1.62	2.67	2.07	1.80	1.94	2.13	2.70	1.67	0.62	0.48	1.55
8	0.59	1.19	1.24	0.98	0.56	0.25	0.12	0.32	0.95	1.21	0.70	0.63	0.73
10	0.17	0.18	-0.11	-0.97	-1.15	-1.20	-1.26	-1.17	-1.12	-0.34	0.01	0.13	-0.57
Noon.	-0.42	-0.97	-1.32	-2.34	-2.47	-2.36	-2.20	-2.29	-2.42	-1.80	-0.77	-0.43	-1.65
2	-0.61	-0.72	-2.21	-3.50	-3.38	-3.23	-3.26	-3.45	-3.58	-2.54	-0.91	-0.68	-2.42
4	-0.43	-1.22	-2.13	-2.86	-2.70	-2.62	-2.76	-2.76	-3.03	-1.85	-0.62	-0.62	-1.97
6	-0.02	-0.42	-0.95	-1.54	-1.62	-1.71	-1.70	-1.37	-1.32	-0.55	-0.23	-0.27	-0.98
8	-0.07	-0.07	-0.11	0.13	0.11	-0.02	0.08	0.34	0.26	0.16	0.02	-0.14	0.06
10	0.06	0.21	0.45	1.01	1.15	1.28	1.29	1.30	1.19	0.57	0.24	-0.02	0.73
Maan	_1.05	-2.00	1.18	5.26	9.15	12 10	12 50	13.02	10.42	7.48	1.49	-1. 38	

The numbers without sign must be added; those with the sign — must be subtracted.

L.

PRUSSIA. — MÜHLHAUSEN. Lat. 51° 13' N. Long. 10° 27' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
			_										
Morn. 1	0.71	1.28	1.10	1.84	2.40	3.56	2.91	2.49	1.95	1.39	0.47	0.58	1.72
2	0.75	1.30	1.28	2.19	2.80	3.97	3.30	2.80	2.20	1.65	0.53	0.59	1.95
3	0.77	1.33	1.46	2.40	3.06	4.16	3.50	3.06	3.29	1.85	0.60	0.60	2.17
4	0.82	1.40	1.60	2.74	3.06	3.98	3.42	3.14	2.70	1.99	0.66	0.62	2.18
5	0.86	1.47	1.62	2.61	2.67	3.40	3.00	2.98	2.73	2.05	0.68	0.66	2.06
6	0.91	1.50	1.46	2.25	2.06	2.49	2.22	2.51	2.46	1.93	0.63	0.67	1.76
7	0.86	1.36	1.11	1.41	1.15	1.32	1.20	1.73	1.03	1.50	0.46	0.59	1.14
8	0.62	0.98	0.55	0.58	0.16	0.11	0.09	0.86	0.87	0.84	0.16	0.46	0.52
9	0.21	0.33	-0.02	-0.38	-0.75	-1.02	-0.97	-0.36	-0.26	-0.03	-0.22	0.03	-0.29
10	-0.38	-0.50	-0.70	-1.16	-1.50	-1.98	-1.82	-1.38	-1.40	-0.99	-0.62	-0.54	-1.08
11	-0.93	-1.35	-1.30	-1.97	-2.06	-2.77	-2.46	-2.24	-2.42	-1.88	-0.92	-0.77	-1.76
Noon	-1.38	-2.02	-1.76	-2.42	-2.44	-3.39	-2.94	-2.89	-3.14	-2.53	-1.09	-1.06	-2.26
1	-1.58	-2.38	-2.02	-2.80	-2.71	-3.86	-3.26	-3.29	-3.52	-2.82	-1.08	-1.15	-2.54
2	-1.52	-2.38	-2.07	-2.94	-2.87	-4.14	-3.42	-3.46	-3.54	-2.99	-0.89	-1.10	-2.61
3	1	i	-1.90					1		1	l		
4	1	ľ	-1.58				1	-3.07	1	l .		l	l 1
5	-0.44	-1.02	-1.11	-1.95	-2.19	-3.06	-2.52	-2.51	-1.89	-1.21	-0.14	-0.23	-1.52
6	1	1	-0.62				i	-1.76		i	0.02	-0.02	1 1
7		-0.17	1	-0.47	1		-0.85	1	-0.24	ı	0.06	0.12	-0.38
8	0.18	0.13	0.16	0.09	-0.08	0.05		1	0.50	0.38	0.22	0.26	0.16
9	0.27	0.41	0.45	0.53	0.58	1.01	0.81	0.71	0.99	0.70	0.26	0.32	0.59
10	0.27	0.41	0.43	0.59	1.10	1.76	1.46	1.24	1.35	0.91	0.20	0.32	0.93
11	0.53	0.89	0.78	1.14	1.56	2.42	2.01	1.78	1.58	1.10	0.34	0.47	1.22
	0.64	1.08	0.73	1.58	1.98	3.05		1		1	0.30	1	l i
Midn	0.04	1.03	0.94	1.50	1.30	3.03	3.29	2.16	1.75	1.26	0.42	0.54	1.56
6. 6	0.36	0.48	0.42	0.53	0.24	0.20	0.23	0.38	0.70	0.68	0.33	0.33	0.41
7. 7	0.41	0.60	0.47	0.47	0.16	0.15	0.18	0.42	0.40	0.74	0.26	0.36	0.38
8.8	0.40	0.56	0.36	0.34	0.04	0.08	0.06	0.41	0.69	0.61	0.19	0.36	0.34
9. 9	0.24	0.37	0.22	0.08	-0.09	-0.01	-0.08	0.18	0.37	0.34	0.02	0.18	0.15
10.10	-0.01	0.08	-0.03	-0.14		-0.11	l .	1		5	1	-0.07	, ,
7. 2. 9	-0.13	-0.20	-0.17	-0.23	-0.38	-0.60	-0.47	-0.34	-0.51	-0.26	-0.06	-0.06	-0.29
6. 2. 8	[-0.25		ı				-0.33			1	!	
6. 2.10		-0.07	0.01	0.07	0.10		0.09	1	0.09		ı	-0.01	0.03
6. 2. 6		1	-0.41	í	,		1	1		1		1	1 1
7. 2	-0.33	-0.51	-0.48	-0.77	-0.86	-1.41	-1.11	-0.87	-1.26	-0.75	-0.22	-0.26	-0.74
8. 2	1	l .	-0.76	1	1		1	i	}	1		1	1 1
8. 1	1	l .	-0.74	į.	i		1		1	1	1		1
7. 1		}	-0.46		1		1	1				Į.	
0.10.00	0	0.0											
9.12.3.9 7. 2.2(9)			-0.81 -0.02									1	-1.10 -0.07
`		Ì					1			ł			-0.22
Dail.ext.	-0.34	-0.44	-0.23	-0.10	0.09	0.01	0.04	-0.10	-v.13	-0.47	-0.21	-U.24	-0.22

Holland. — Utrecht. Lat. 52° 5′ N. Long. 5° 8′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.36	0.62	1.13	1.71	2.56	2.74	2.64	1.87	1.91	1.07	0.76	0.11	1.44
1	0.37	0.74	1.18	1.87	2.86	3.29	2.67	1.91	2.10	1.11	0.70	0.19	1.58
2	0.46	0.82	1.24	2.00	3.00	3.21	2.82	2.02	2.21	1.18	0.78	0.32	1.67
3	0.51	0.87	1.27	2.10	3.02	3.25	2.97	2.07	2.34	1.25	0.82	0.42	1.74
4	0.57	0.90	1.31	2.16	2.70	2.84	2.76	2.06	2.45	1.31	0.82	0.44	1.69
5	0.61	0.97	1.26	1.92	1.80	1.82	1.86	1.80	2.42	1.42	0.90	0.50	1.44
6	0.66	0.98	1.02	1.30	0.67	0.44	0.33	1.05	1.87	1.22	0.91	0.46	0.91
7	0.64	0.84	0.62	0.37	-0.38	-0.70	-0.77	0.04	0.72	0.39	0.78	0.38	0.2
S	0.50	0.56	-0.01	-0.40	-1.17	-1.50	-1.28	-0.68	-0.39	0.12	0.29	0.31	-0.30
9	0.13	-0.07	-0.53	-1.20	-1.68	-2.02	-1.69	-1.33	-1.12	-0.50	-0.22	0.14	-0.84
10	-0.26	-0.49	-1.05	-1.71	-2.06	-2.42	-2.02	-1.65	-1.79	-1.12	-0.71	-0.14	-1.29
11	-0.62	-0.97	-1.50	-2.16	-2.46	-2.78	-2.27	-1.87	-2.34	-1.68	-1.15	-0.33	-1.68
Noon.	-0.85	-1.34	-1.77	-2.41	-2.78	-2.94	-2.53	-2.16	-2.83	-1.98	-1.49	-0.62	-1.9
1	-0.98	-1.58	-1.88	-2.42	-2.94	-3.00	-2.61	-2.40	-3.07	-2.11	-1.62	-0.75	-2.1
2	-1.02	-1.54	-1.82	-2.42	-2. SS	-2.94	-2.60	-2.30	-2.99	-1.99	-1.43	-0.66	-2.0
3	-0.81	-1.21	-1.54	-2.24	-2.58	-2.64	-1.58	-2.13	-2.68	-1.64	-1.08	-0.47	-1.73
4	-0.60	-0.89	-1.25	-1.82	-2.06	-2.20	-2.00	-1.79	-2.06	-1.10	-0.70	-0.23	-1.39
5	-0.35	-0. 48	-0.75	-1.23	-1.42	-1.53	-1.62	-1.30	-1.34	-0.52	-0.42	-0.17	-0.9
6	-0.19	-0.21	-0.24	-0.47	-0.76	-0.74	-0.76	-0.61	-0.52	-0.11	-0.18	-0.10	-0.4
7	-0.05	-0.03	0.14	0.20	0.07	0.17	0.02	0.14	0.10	0.22	-0.02	-0.03	0.0
8	0.05	0.12	0.48	0.72	0.85	1.01	0.82	0.86	0.62	0.53	0.18	0.02	0.5
9	0.22	0.23	0.74	1.13	1.51	1.77	1.50	1.24	1.17	0.84	0.40	0.06	0.9
10	0.36	0.40	0.94	1.41	1.92	2.25	1.96	1.52	1.51	1.01	0.58	0.04	1.10
11	0.36	0.67	1.02	1.58	2.16	2.53	2.17	1.70	1.76	1.14	1.06	0.02	1.3
lean	-2.83	4.18	3.20	7.14	10.55	12.95	13.75	12.90	10.87	6.88	4.65	0.76	

LII.

England. — Greenwich. Lat. 51° 28′ 38″ N. Long. 0° 0′. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.14	0.75	1.44	2.32	2.72	3.24	2.73	2.49	2.05	1.34	0.67	0.47	1.72
3	0.62	0.94	1.66	2.66	3.04	3.70	3.11	2.82	2.40	1.42	0.80	0.56	1.98
5	0.75	1.06	1.92	2.84	2.84	3.25	2.91	2.89	2.58	1.54	0.87	0.56	2.00
7	0.86	1.08	1.60	1.31	0.75	0.80	0.88	1.22	1.65	1.26	0.88	0.60	1.07
9	0.41	0.24	-0.22	-0.82	-1.30	-1.52	-1.14	-1.14	-0.76	-0.30	0.11	0.24	-0.50
11	-0.74	-1.03	-1.90	-2.48	-2.60	-2.91	-2.67	-2.64	-2.57	-1.88	-1.06	-0.73	-1.93
P.M. 1	-1.25	-1.73	-2.62	-3.31	-3.36	-3.75	-3.17	-3.40	-3.28	-2.40	-1.64	-1.20	-2.59
3	-1.10	-1.59	-2.43	-3.08	-3.02	-3.60	-3.09	-3.20	-2.94	-2.04	-1.26	-0.85	-2.35
5	-0.36	-0.63	-1.33	-2.04	-2.05	-2.51	-2.24	-2.11	-1.65	-0.73	-0.38	-0.24	-1.37
7	0.03	0.05	0.09	-0.16	-0.29	-0.58	-0.50	-0.11	0.04	0.11	0.09	0.00	-0.10
9	0.10	0.32	0.71	0.99	1.20	1.40	1.13	1.22	0.89	0.63	0.40	0.21	0.77
11	0.23	0.54	1.11	1.77	2.06	2.52	2.08	1.96	1.60	1.07	0.53	0.37	1.33
Mean.	2.48	2.53	4.53	6.71	9.62	12.47	13.08	12.98	11.12	7.71	5.47	3.09	

LIII.

England. — Greenwich. Lat. 51° 29' N. Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						s of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.38	0.68	1.29	2.21	2.72	3.13	2.61	2.61	1.89	1.28	0.60	0.40	1.65
2	0.63	0.82	1.44	2.31	2.85	3.30	2.71	2.68	2.06	1.45	0.75	0.52	1.79
3	0.83	0.95	1.62	2.44	2.91	3.41	2.74	2.78	2.22	1.56	0.88	0.59	1.91
4	0.93	1.02	1.82	2.54	2.85	3.40	2.71	2.86	2.34	1.60	0.95	0.62	1.97
				1							1		
5	0.93	1.03	1.95	2.46	2.60	3.14	2.53	2.81	2.35	1.56	0.95	0.62	1.91
6	0.84	0.97	1.93	2.17	2.08	2.52	2.11	2.48	2.15	1.42	0.89	0.60	1.68
7	0.71	0.84	1.66	1.56	1.25	1.53	1.38	1.77	1.67	1.15	0.75	0.57	1.24
8	0.53	1	1.11	0.66	0.20	0.28	0.40	0.72	0.88	0.71	0.52	0.48	0.59
	0,00	0.01	1	0.00	0.20	0.20	0.10	0112	0.00	0			0.00
9	0.30	0.26	0.30	-0.37	-0.92	-1.02	-0.71	-0.55	-0.13	0.09	0.19	0.28	-0.19
10	-0.01		-0.66	1			1		1	i			1
11	-0.39		-1.60					ì		i	-0.77	i .	1 1
11 1	1	1	-2.35								i		-2.27
Noon	-0.79	-1.27	-2.55	-2.01	-5.15	-0.25	2.94	.9.49	-2.94	2.07	1.23	0.57	-2.21
1	-1.12	-1 66	-2.79	-3.17	-3.26	-3.39	-3.04	-3.69	-3.28	-2.45	-1.59	-1.17	-2.55
2	1		-2.75 -2.85										
1	1							1		1	1		· .
3	1		-2.57							1	Į.		1 1
4	-0.95	-1.29	-2.05	-2.54	-2.54	-3.01	-2.38	-2.89	-2.28	-1.63	-1.10	-0.76	-1.95
_	0.50	0.00		1.0*	9.00	0.0*	0.00	0.00	1 00	1.01	0.50	0.00	1 45
5	-0.58	1	-1.40					l	l	1		-0.36	1
6	-0.22	t .	-0.75					ł	l	-0.43		-0.01	
7	0.03	0.14	-0.17					1		0.02	0.24)	-0.34
8	0.11	0.37	0.30	0.17	0.11	-0.24	-0.19	0.24	0.29	0.32	0.41	0.26	0.18
9	0.08	0.46	0.65	0.84	0.92	0.81	0.64	1.11	0.77	0.52	0.44	0.23	0.62
10	0.03	0.48	0.89	1.42	1.62	1.74	1.41	1.81	1.17	0.69	0.41	0.19	0.99
11	0.04	0.49	1.05	1.81	2.16	2.42	2.01	2.27	1.47	0.87	0.40	0.20	1.27
Midn	0.16	0.56	1.17	2.03	2.51	2.86	2.40	2.51	1.70	1.08	0.46	0.28	1.48
6. 6	0.31	0.36	0.59	0.42	0.31	0.21	0.27	0.46	0.62	0.50	0.39	0.30	0.40
7. 7	0.37	0.49	0.75	0.48	0.27	0.13	0.21	0.54	0.70	0.59	0.50	0.38	0.45
8.8	0.32	0.49	0.71	0.42	0.16	0.02	0.10	0.48	0.59	0.52	0.47	0.37	0.39
9. 9	0.19	0.36	0.48	0.24	0.00	-0.10	-0.04	0.28	0.32	0.31	0.31	0.25	0.22
10.10	0.01	0.14		-0.00		-0.19	-0.16	0.01	ł.	0.02	0.08	0.07	-0.01
									ì				
7. 2. 9	-0.16	-0.17	-0.18	-0.25	-0.33	-0.33	-0.30	-0.25	-0.26	-0.27	-0.17	[-0.15]	-0.24
6. 2. 8	1	1	-0.21							-0.25			-0.24
6. 2.10		-0.12		0.15	0.18		-0.20	l.		-0.12			0.04
6. 2. 6			-0.56							-0.50			-0.59
J. 2. 3	"	3,1	0.00	"	0.01	0.01	00	1				- · ·	
7. 2	-0.29	-0.49	-0.60	-0.79	-0.96	-0.91	-0.77	-0.93	-0.78	-0.67	-0.47	-0.34	-0.67
8. 2			-0.87										
8. 1			-0.84										
7. 1	-0.31	_0.11	-0.57	_0.81	-1.01	-0.05	-0.83	-0.96	-0.81	-0.65	-0.49	-0.30	-0.66
·· 1	0.21	0.41	-0.37	0.01	1.01	0.30	0.00	0.00	0.01	0.00	0.72	0.50	0.00
9.12.3.9	-0.41	-0.56	-0.99	-1.33	-1.51	-1.68	-1.42	-1.55	-1.29	-0.91	-0.53	-0.37	-1.05
7. 2.2(9)	1	-0.01	(-0.02					-0.07			
1. 2.2(3)	-0.10	-0.01	0.03	0.03	-0.02	0.03	-0.00	0.03	0.01	0.07	-0.02	0.00	-0.02
Dail.ext.	-0.18	-0.30	-0.45	-0.39	-0.18	0.01	-0.15	-0.49	-0.47	-0.44	-0.37	-0.32	-0.30
I/aii. CXt.	J.10		0.40	0402	0.10	U-11/1				J. 11	0.01	0.02	0.00

LIV. England. — Greenwich. Lat. 51° 29′ N. Long. 0° 0′.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.—GLAISHER.

Degrees of Fahrenheit.

Midn. 1.0						Degrees	or Tan	геппен.						
1	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
1														
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Midn	1.0	1.6	2.9	4.8	5.4	6.2	5.0	5.1	4.0	2.9	1.7	0.9	3.5
3		0.9	1.8	3.0	5.2	6.0	7.1	5.5	5.5	4.5	3.0	1.8	1.0	3.8
1.6	2	1.2	2.0	3.3	5.7	6.4	8.0	6.0	6.0	5.5	3.4	2.0	1.2	4.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	1.3	2.1	3.6	6.2	6.7	8.7	6.4	6.3	6.4	3.6	2.0	1.3	4.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	11 1	1											1.4	4.8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1												1.4	1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					6.0		6.4			5.3	,	1.9	1.4	3.9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	1.9	2.1	3.6	4.3	2.6	3.0	2.5	3.3	4.0	2.8	1.7	1.5	2.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						^ =			0.0		- 0	7.0		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		1	1					1					1 .
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1	ì									i	l .	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		1	l									1		1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	-1.3	-2.1	-3.5	-5.3	-5.5	-5.S	-5.4	-5.4	-5.0	-3.8	-2.0	-1.3	-3.9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Noon	_9 9	-2.2	-5.0	-6.8	-6 7	-73	-6.1	-6.5	-6.1	_5 1	_9 1	_9 1	_5 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	fi .		1						1				Į.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1													
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	i i	1									l .		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	-2.5	-5.0	-5.5	-1.1	-7.3	-0.4	-0.0	-7.0	-0.0	-3.7	-5.0	-1.5	-9.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	-1.9	-2.8	-4.5	-6.7	-6.1	-7.4	-5.8	-5.5	-5.5	-2.8	-2.1	-1.3	-4.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11 1			ł			1				1	l		1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 1		1	!			•				l	l .		1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			1	1								l .	l .	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.1	0.6	0.9	0.7	0.9	0.0	0.3	1.0	1.0	0.7	0.6	0.2	0.6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.4	1.0	1.7	2.0	2.3	1.8	1.9	2.4	1.8	1.3	1.0	0.4	1.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	0.6	1.3	2.3	3.2	3.5	3.6	3.3	3.3	2.7	1.9	1.3	0.5	2.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	0.7	1.5	2.6	4.1	4.5	5.0	4.2	4.3	3.4	2.4	1.5	0.8	2.9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$									1					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6.6	0.6	0.0	10	1.0		0.0	0.5	1 7	1.4	1 2	0.6	0.5	0.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	ll .	l .	1	l .	l .	1		1					1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		11	ł.	j .	l .	l	l .	1						1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8.8	0.8	1.1	1.7	1.0	0.7	0.0	0.1	0.9	1,	1.1	0.0	0.0	0.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.9	0.7	0.8	0.9	0.5	0.1	-0.3	-0.0	0.4	0.7	0.6	0.7	0.6	0.5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 .			í	l .		1	1	i	1		i		l I
$ \begin{bmatrix} 6. & 2. & 8 & & & & & & & & & & & & & & & & & $	11	1		1	1	1		l	l .			1	1	
$ \begin{bmatrix} 6 & 2.10 \\ 6 & 2. & 6 \end{bmatrix} $	1. 2. 3	"	"	0.2	3.3			3.3			1			
$ \begin{bmatrix} 6 & 2.10 \\ 6 & 2 & 6 \end{bmatrix} $	6. 2. 8	-0.3	-0.3	-0.3	-0.5	-0.7	-0.7	-0.6	-0.4	-0.3	-0.2	-0.4	-0.2	-0.4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	1!	i		l .	1	i	l .	0.3	0.3	0.2	-0.1	-0.1	0.1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Li	-		1	1		1	-1.9	-1.4	-1.4	-0.7	-0.7	-0.4	-1.3
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					1		1							
$ \begin{vmatrix} 8. & 1 \\ 7. & 1 \end{vmatrix} \begin{vmatrix} -0.7 \\ -0.5 \end{vmatrix} \begin{vmatrix} -1.1 \\ -0.9 \end{vmatrix} \begin{vmatrix} -1.6 \\ -1.1 \end{vmatrix} \begin{vmatrix} -2.9 \\ -1.1 \end{vmatrix} \begin{vmatrix} -3.5 \\ -2.4 \end{vmatrix} \begin{vmatrix} -4.0 \\ -2.6 \end{vmatrix} \begin{vmatrix} -3.4 \\ -2.1 \end{vmatrix} \begin{vmatrix} -3.3 \\ -2.1 \end{vmatrix} \begin{vmatrix} -2.5 \\ -1.5 \end{vmatrix} \begin{vmatrix} -1.9 \\ -1.4 \end{vmatrix} \begin{vmatrix} -1.3 \\ -0.9 \end{vmatrix} \begin{vmatrix} -0.5 \\ -0.4 \end{vmatrix} \begin{vmatrix} -2.2 \\ -1.5 \end{vmatrix} $	7. 2	-0.5	-0.9	-1.1	-1.9	-2.5	-2. 8	-2.1	-2.2	-1.5	-1.0	1	1	1
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	8. 2	-0.7	-1.1	-1.6	-3.1	-3.6	1	-3.3	l.	Ĭ .		1	1	
	8. 1	-0.7	-1.1	-1.6	-2.9	-3.5	-4.0	-3.4	-3.3	-2.5	-1.9	1	1	1
$ \begin{vmatrix} 9.12.3.9 & \begin{vmatrix} -0.8 & -1.3 & -2.1 & -3.3 & -3.4 & -4.1 & -3.2 & -3.2 & -2.9 & -1.9 & -1.2 & -0.7 & -2.4 \end{vmatrix} $	7. 1	-0.5	-0.9	-1.1	-1.8	-2.4	-2.6	-2.1	-2.1	-1.5	-1.4	-0.9	-0.4	-1.5
$ \parallel 9.12.3.9 \parallel -0.8 \parallel -1.3 \parallel -2.1 \parallel -3.3 \parallel -3.4 \parallel -4.1 \parallel -3.2 \parallel -3.2 \parallel -2.9 \parallel -1.9 \parallel -1.2 \parallel -0.7 \parallel -2.4 \parallel -1.2 \parallel $										2.0		1.0	0	0.4
	9.12.3.9	-0.8	-1.3	-2.1	-3.3	-3.4	-4.1	-3.2	-3.2	-2.9	-1.9	1-1.2	-0.7	-2.4

LV.

PRUSSIA. — HALLE. Lat. 51° 30' N. Long. 11° 57' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degre	es of Re	eaumur.						
Hours,	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
35	0.53	1.00	1.90	0.50	3.98	3.91	3.72	3.32	2.70	2.01	0.95	0.46	2.21
Morn. 1	ll .	1	1.36	2.52			1		1	4	1	1	
2	0.56	1.14	1.58	2.86	4.10	3.94	3.82	3.57	2.99	1	1	1	
3	0.60	1.26	1.74	3.00	3.78	3.62	3.56	3.56	3.12	2.37	1.01	0.50	2.34
4	0.66	1.34	1.82	2.94	3.10	2.95	2.97	3.27	3.02	2.41	1.03	0.54	2.17
5	0.72	1.36	1.72	2.62	2.18	2.09	2.14	2.64	2.62	2.25	1.00	0.55	1.82
6	0.72	1.30	1.42	1.98	1.30	1.18	1.24	1.90	1.97	1.90	0.92	0.58	1.37
7	0.65	1.10	0.94	1.07	0.32	0.25	0.23	0.84	0.98	1.32	0.74	0.55	0.75
8	0.36	0.53	0.20	0.03	-0.56	-0.58	-0.57	-0.20	0.12	0.33	0.30	0.28	0.02
9	0.05	-0.08	-0.66	-0.98	-1.34	-1.34	-1.30	-1.20	-1.14	-0.71	-0.31	-0.09	-0.76
10	-0.45	-0.76	-1.18	-1.86	-2.09	-2.01	-1.99	-2.10	-2.03	-1.66	-0.87	-0.54	-1.46
11	-0.82	-1.29	-1.73	-2.58	-2.66	-2.68	-2.65	-2.90	-2.72	-2.44	-1.35	-0.90	-2.06
Noon				ł .	i		1	-3.35	1	I	l .	1	
1	-1.17	-2.02	-2.22	-3.32	-3.33	-3.35	-3.46	-3.53	-3.30	-3.01	-1.73	-1.09	-2.63
2		-1.86					l .	-3.57		1	-1.52	1	1 1
3								-3.30		1	1	1	1
4								1	1	1			1
*	-0.55	-1.01	-1.42	-2.59	-2.74	-2.74	-2.70	-2.84	-2.90	-1.01	-0.75	-0.42	-1.05
5	-0.30	-0.59	-0.91	-1.78	-2.24	-2.22	-2.16	-1.97	-1.83	-1.20	-0.40	-0.20	-1.32
6	-0.13	-0.29	-0.52	-0.96	-1.58	-1.50	-1.39	-1.38	-1.12	-0.69	-0.14	-0.03	-0.81
7	-0.00	-0.09	-0.06	-0.34	-0.86	-0.73	-0.55	-0.59	-0.38	-0.21	0.04	0.09	-0.31
8	0.11	0.13	0.26	0.32	-0.10	0.07	0.26	0.15		0.25	0.21	0.22	-0.18
9	0.21	0.30	0.59	0.88	0.68	0.90	1.09	0.90	0.87	0.68	0.39	0.34	0.65
10	0.21	0.46	0.79	1.33	1.64	1.81	1.87	1.61	1.42	1.12	0.59	0.37	1.11
1 11	[l	1		
11	0.41	0.65	0.98	1.78	2.61	2.69	2.64	2.30	1.90	1.47	0.76	0.40	1.55
Midn	0.48	0.83	1.16	2.17	3.43	3.42	3.29	2.86	2.33	1.77	0.89	0.43	1.92
	0.07	0.00	0.41	0.49	0.00	0.00	0.03	0.04	0.40	0.50	0.00	0.10	0.00
6. 6	0.21	0.39	0.41		-0.03			0.34	0.40	0.53	0.30	0.18	0.26
7. 7	0.30	0.51	0.45		-0.14			0.26	0.43	0.61	0.39	0.28	0.28
8.8	0.33	0.51	0.44		-0.27			0.13	0.30	0.56	0.39	0.32	0.22
9. 9	0.24	0.33	0.23	0.18				-0.03	0.21	0.29	0.26	0.25	0.10
10.10	0.13	0.11	-0.04	-0.05	-0.33	-0.22	-0.11	-0.15	-0.14	-0.02	0.04	0.13	-0.05
7. 2. 9	-0.11	-0.20	-0.18	-0.34	-0.71	-0.70	-0.65	-0.49	-0.35	-0.29	-0.20	-0.10	-0.36
6. 2. 8	-0.15	-0.25	-0.19	-0.35	-0.67	-0.66	-0.62	-0.49	-0.35	-0.32	-0.23	-0.15	-0.37
6. 2.10	-0.08	-0.12	0.03	0.06	-0.16	-0.12	-0.08	-0.00	0.06	-0.03	-0.11	-0.07	-0.05
6. 2. 6	-0.25	-0.42	-0.47	-0.83	-1.13	-1.16	-1.16	-0.95	-0.84	-0.65	-0.38	-0.25	-0.71
7. 2	-0.23	-0.36	-0.40	-0.67	-1.02	-1.09	-1.11	-0.82	-0.67	-0.56	-0.41	-0.26	-0.63
8. 2								-1.35					
8. 1			ì			. 1		-1.26			-0.46	1	1
7. 1	1			1 4				-0.73			i 1		1
		0.00							ا ا				
9.12.3.9								-1.63					
7. 2.2(9)	-0.06	-0.12	-0.07	-0.18	-0.56	-0.51	-0.43	-0.33	-0.19	-0.15	-0.10	-0.02	-0.23
Dail.ext.	-0.23	-0.33	-0.20	-0.16	0.37	0.24	0.14	0.00	-0.09	-0.30	-0.35	-0.26	-0.14

LVI.

Hanover. — Göttingen. Lat. 51° 32' N. Long. 9° 56' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Morn. 1 0.90 1.13 1.58 2.24 3.31 3.43 3.56 3.35 2.31 1.58 0.69 0.60 2.06 2 0.92 1.14 1.77 2.49 3.70 3.71 3.82 3.70 2.68 1.75 0.74 0.59 2.25 3 0.94 1.16 2.01 2.79 3.93 3.73 3.92 3.92 3.23 1.94 0.82 0.58 2.41						Degre	es of Re	aumur.						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
3	Morn. 1	0.90	1.13	1.58	2.24	3.31	3.43	3.56	3.35	2.31	1.58	0.69	0.60	2.06
1	2	0.92	1.14	1.77	2.49	3.70	3.71	3.82	3.70	2.68	1.75	0.74	0.59	2.25
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	0.94	1.16	2.01	2.79	3.93	3.73	3.92	3.92	3.23	1.94	0.82	0.58	2.41
6 1.12 1.20 2.10 2.73 2.62 2.22 2.59 2.79 3.50 1.99 1.08 0.66 2.05 7 1.13 1.14 1.77 2.24 1.78 1.21 1.40 1.69 2.62 1.58 0.94 0.65 1.51 0.50 0	4	0.99	1.20	2.22	3.04	3.91	3.57	3.79	3.89	3.63	2.10	0.92	0.58	2.49
6 1.12 1.20 2.10 2.73 2.62 2.22 2.59 2.79 3.50 1.99 1.08 0.66 2.05 7 1.13 1.14 1.77 2.24 1.78 1.21 1.40 1.69 2.62 1.58 0.94 0.65 1.51 0.50 0		1.15	1 00	0.00	0.00		0.10	0.00	9.50	0.00	0.1-	1.00	0.00	2.00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1	1	l	į.	Į			l l		i		1	1	
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I I	1	ł	l			1		l .	i	1	1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	1.12	0.80	1.02	0.89	0.75	0.49	0.48	0.56	1.36	1.08	0.53	0.54	0.80
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.50	-0.08	-0.14	-0.16	-0.47	-0.55	-0.65	-0.68	-0.22	-0.21	0.10	0.30	-0.19
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	-0.37	-0.88	-1.09	-1.32	-1.53	-1.60	-2.22	-1.84	-1.45	-0.82	-0.42	1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1			l				1	1	j .	1	1	1	
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	-2.02	-2.32	-2. S1	-3.37	-3.82	-3.72	-3.78	-3.82	-3.80	-2.89	-1.58	-1.42	-2.95
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	-2.03	-2.23	-3.05	-3.56	-3.98	-4.03	-4.09	-4.15	-4.00	-2.98	-1.60	-1.28	-3.08
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	-1.74	-1.98	-2.88	-3.48	-3.95	-3.91	-4.00	-4.03	-4.03	-2.84	-1.32	-1.02	-2.93
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	-1.23	-1.35	-2.48	-3.24	-3.67	-3.65	-3.82	-3.71	-3.62	-2.40	-0.90	-0.66	-2.56
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	ا ا	0.70	0.50	_1 ~0	9.64	0.10	9.00	_9 10	_0.15	9.04	1 ~ (0.54	0.20	2.00
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 1							1				ı		1
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$. ,						1	ł	l .				1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.24	0.58	0.34	0.04	0.22	-0.15	0.03	0.13	0.05	0.24	0.17	0.20	0.14
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.40	0.82	0.78	0.77	0.88	0.79	1.09	1.05	0.78	0.71	0.30	0.30	0.72
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	0.57	0.94	1.05	1.30	1.59	1.73	1.87	1.62	1.28		0.42	0.40	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1								l				ı	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$									l				i	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Trium	0.00	1.0.	1.01	2.11		0.01	0.10	2.00		1.11	0.02	0.50	1.22
$\begin{array}{cccccccccccccccccccccccccccccccccccc$										0				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1			i 1			ł .		l	1			l .	3 1
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.10	0.10	0.03	-0.02	-0.01	0.03	0.07	-0.19	-0.11	-0.09	0.10	-0.00	0.19	0.01
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	7. 2. 9	-0.17	-0.09	-0.17	-0.18	-0.44	-0.68	-0.53	-0.47	-0.20	-0.23	-0.12	-0.11	-0.28
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				1 :				•	1				Į.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1	1						-		1		1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		ł	1	}	1		ì		i	1	ì			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1		ì				ı	î .				1		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1		l				Į.	ı		l 1	1	!		
		1	l .							1 1	1	ł		1 6
$\begin{vmatrix} 9.12.3.9 & -0.67 & -0.85 & -1.17 & -1.46 & -1.71 & -1.72 & -1.76 & -1.80 & -1.71 & -1.21 & -0.60 & -0.39 & -1.25 & -0.60 & -0.39 & -1.25 & -0.60 & -0.39 & -1.25 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & -0.60 & -0.39 & -0.67 & $	7. 1	-0.45	-0.59	-0.52	-0.57	-1.02	-1.26	-1.19	-1.07	-0.59	-0.66	-0.32	-0.39	-0.72
	9,12 3.0	-0.67	-0.85	-1.17	-1 46	_1 71	-1 79	-1 76	-1 80	-1 71	_1 91	-0.60	-0.39	-1.25
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1	l								1	1		
	` '													
Dail. ext. -0.44 -0.53 -0.38 -0.24 -0.03 -0.15 -0.09 -0.12 -0.20 -0.42 -0.26 -0.38 -0.30	Dail. ext.	-0.44	-0.53	-0.38	-0.24	-0.03	-0.15	-0.09	-0.12	-0.20	-0.42	-0.26	-0.38	-0.30

LVII.

PRUSSIA. — BERLIN. Lat. 52° 30' N. Long. 13° 24' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midnight.	0.34	0.59	0.90	1.78	2.21	2.15	1.78	1.52	1.50	0.95	0.44	0.34	1.2
1	0.43	0.78	1.13	2.22	3.23	2.80	2.52	2.53	1.99	1.48	0.59	0.37	1.6
2	0.49	0.97	1.38	2.56	3.83	3.38	3.06	3.05	2.41	1.95	0.68	0.43	2.0
3	0.54	1.09	1.64	2.41	4.00	3.46	3.28	3.15	2.76	2.31	0.73	0.46	2.1
4	0.58	1.25	1.85	3.03	3.77	3.18	3.12	3.40	2.94	2.45	0.79	0.52	2.2
5	0.65	1.37	1.97	3.05	3.16	2.59	2.67	3.16		2.32	0.84	0.56	2.1
6	0.73	1.39	1.92	2.69	3.23	1.73	1.92	2.57	2.56	1.52	0.84	0.71	1.7
7	0.75	1.18	1.62	2.01	1.43	0.94	1.18	1.83	2.03	1.15	0.65	0.63	1.2
s	0.62	0.89	1.14	0.94	0.42	0.41	0.44	0.75	1.03	0.62	0.56	0.60	0.7
9	0.41	0.49	0.44	-0.17	-0.65	-0.40	-0.35	-0.36	-0.09	-0.04	0.35	0.38	0.0
10	0.19	-0.09	-0.25	-1.08	-1.47	-1.14	-1.15	-1.27	-0.81	-0.81	-0.09	0.05	-0.6
11	-0.30	-0.66	-1.02	-1.78	-2.20	-1.72	-1.78	-2.07	-1.90	-1.46	-0.55	-0.36	-1.3
Noon.	-0.55	-1.16	-1.44	-2.37	-2.65	-2.17	-2.26	-2.64	-2.49	-1.87	-0.95	-0.69	-1.7
1									-2.96				-2.1
2									-3.16				-2.2
3	-1.03	-1.67	-2.28	-3.27	-3.34	-2.84	-2.82	-3.25	-3.19	-2.12	-1.20	-0.95	-2.3
4									-3.16				-2.1
5									-2.34				-1.7
6	11 1						1	3	-1.58			-0.25	-1.3
7	-0.22	-0.46	-0.64	-1.13	-1.55	-1.75	-1.44	-1.22	-0.82	-0.63	-0.11	-0.15	-0.8
8									-0.16	-0.30	0.05	-0.02	-0.2
9	0.06	0.03	0.05	0.40	0.13	0.31	0.38	0.84		-0.08	0.10	0.06	0.2
10	0.14	0.21	0.39	0.93	0.82	0.96	1.01	1.06	0.98		0.20	0.17	0.5
11	0.24	0.38	0.65	1.37	1.56	1.58	1.44	1.57	1.20	0.56	0.36	0.25	0.9
6, 6	0.17	0.32	0.40	0.32	-0.06	-0.31	-0.12	0.19	0.49	0.32	0.27	0.23	0.1
7, 7	0.27	0.36	0.49		-0.06		-0.13	0.30	0.60	0.26	0.27	0.24	0.2
s, s	0.25	0.35	0.44		-0.08		0.03	0.23	0.44	0.16	0.26	0.29	0.1
9, 9	0.24	0.26	0.30	0.12	0.21	-0.05	0.02	0.24	-0.23	-0.06	0.23	0.22	0.1
10, 10	0.17	0.06							-0.09		0.06	0.11	0.0
7, 1	,							i	-0.46				-0.4
7, 2, 9					1				-0.26				-0.2
5, 2, 10	-0.07	-0.04	0.04	0.21	-0.07	-0.01	0.06	0.15	0.13	-0.15	-0.08	-0.03	-0.0
aily ext.	-0.16	-0.17	-0.16	-0.11	0.33	0.31	0.23	0.08	-0.13	0.11	-0.22	-0.13	0.0

LVIII.

Germany. — Salzuflen. Lat. 52° 5′ N. Long. 8° 40′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Morn. 1 0.00 1.10 1.05 2.11 2.41 2.57 2.05 1.71 2.12 1.24 0.90 0.31 1.46 2 0.65 1.22 1.20 2.44 2.93 2.85 2.27 2.01 2.44 1.55 1.26 0.48 1.77 3 0.60 1.27 1.34 2.64 3.29 2.98 2.39 2.23 2.23 2.24 1.82 1.53 0.65 0.48 1.77 3 0.60 1.27 1.34 2.64 3.29 2.98 2.39 2.23 2.24 1.82 1.55 0.65 0.48 1.77 3 0.60 1.27 1.83 1.26 2.33 3.08 2.47 1.99 2.00 2.71 1.97 1.58 0.63 1.85 6 0.62 1.01 1.06 1.80 2.41 1.83 1.42 1.48 2.18 1.75 1.37 0.79 1.48 7 0.51 0.75 0.70 1.05 1.45 1.02 0.70 0.70 0.79 1.34 1.34 1.04 0.66 0.64 0.94 8 0.31 0.41 0.23 0.20 0.38 0.15 -0.06 0.08 0.30 0.75 0.62 0.33 0.31 0.41 0.23 0.20 0.38 0.15 -0.06 0.08 0.30 0.75 0.62 0.33 0.31 0.41 0.23 0.20 0.38 0.15 -0.06 0.08 0.30 0.75 0.62 0.33 0.31 0.41 0.23 0.20 0.38 0.15 -0.06 0.08 0.30 0.75 0.62 0.33 0.31 0.41 0.23 0.25 0.68 -1.36 -1.42 1.38 -1.15 1.02 1.47 -0.63 0.35 -0.24 0.88 111 0.74 1.02 1.06 1.93 1.96 1.19 1.102 1.17 -0.64 1.38 1.27 0.02 0.48 1.29 11 0.94 1.42 1.39 2.32 2.31 2.39 1.90 1.72 2.41 1.175 1.18 0.62 1.17 0.05 1.05 1.45 1.00 1.05 1.47 1.05 1.05 1.47 1.05 1.05 1.47 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05						Degree	es of Re	aumur.						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Mann 1	0.00	1 10	1.05	9 11	9 (1	9.57	2.05	1.71	9 19	190	0.00	0.21	1 16
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		ł	1	1	1	i	1		1				i .	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1)		1	1	1	1	1		1	1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		i .	1		i .	ı	1	1			1	i	1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	0.72	1.18	1.29	2.35	3.08	2.47	1.99	2.00	2.71	1.97	1.58	0.83	1.85
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	0.62	1.01	1.06	1.80	2.41	1.83	1.42	1.48	2.18	1.75	1.37	0.79	1.48
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I	1	0.75	0.70	1.05	1.45	1.02	0.70	0.79	1.34	1.34	1.04	0.64	0.94
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	0.31	0.41	0.25	0.20	0.38	0.15	-0.06	0.08	0.30	0.75	0.62	0.38	0.31
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		0.08	-0.03	-0.22	-0.63	-0.59	-0.67	-0.74	-0.54	-0.65	0.09	0.14	0.06	-0.31
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	I		1			ł .	l .	l .	I	1	l .			1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			1	1	ı			l .	1	*	1			1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Noon	-0.91	-1.42	-1.39	-2. 32	-2.31	-2.39	-1.90	-1.72	-2.41	-1.78	-1.18	-0.62	-1.70
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	-1.01	-1.68	-1.59	-2.54	-2.53	-2.72	-2.13	-2.03	-2.75	-2.09	-1.48	-0.64	-1.93
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2	-0.94	-1.74	-1.65	-2.60	-2.66	-2.91	-2.30	-2.30	-2.90	-2.18	-1.56	-0.58	-2.03
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3	-0.79	-1.58	-1.56	-2.49	-2.72	-2.92	-2.36	-2.42	-2.90	-2.06	-1.46	-0.50	-1.98
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	4	-0.50	-1.29	-1.33	-2.21	-2.65	-2.71	-2.24	-2.30	-2.70	-1.76	-1.22	-0.41	-1.78
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5	-0.20	-0.90	-0.98	-1.77	-2.39	-2.26	-1.89	-1.87	-2.25	-1.34	-0.92	-0. 35	-1.43
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6	-0.10	-0.51	-0.56	-1.22	-1.94	-1.62	-1.32	-1.22	-1.55	-0.90	-0.65	-0.32	-0.99
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7	0.01	-0.17	-0.15	-0.62	-1.34	-0.86	-0.62	0.47	-0.71	-0.47	-0.44	-0.30	-0.51
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	s	0.08	0.11	0.19	-0.04	-0.65	-0.09	0.09	0.21	0.12	-0.11	-0.31	-0.27	-0.06
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	0.14	0.34	0.45	0.48	0.04	0.62	0.70	0.71	0.81	0.18	-0.20	-0.21	0.34
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	ì	0.55	0.63	0.94	0.68	1.22	1.26	1.03	1.30	0.42	-0.06	-0.12	0.67
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11		1 1			1.27	1.74	1.52		1.61	0.66	0.18	0.01	0.94
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Midn	0.40	0.93	0.90	1.74	1.84	2.18	1.80	1.45	1.86	0.94	0.50	0.15	1.22
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	e e	0.26	0.95	0.95	0.20	0.01	0.11	0.05	0.19	0.90	0 (0	0.90	0.01	0.01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1		1 1		1				1	1				1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			l 1	- 1	1								1	i
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			1 1	i										
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2. 9	-0.10	-0.22	-0.17	-0.36	-0.39	-0.42	-0.30	-0.27	-0.25	-0.22	-0.24	-0.05	-0.25
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	The state of the s													
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11		1		- 1									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7)	1								
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7. 2	-0.22	-0.50	-0.48	-0.78	-0.61	-0.95	-0.80	-0.76	-0.78	-0.42	-0.26	0.03	-0.54
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8. 2	-0.32	1			I								
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	8. 1						- 1				1			
7. $2.2(9)$ $\begin{vmatrix} -0.04 & -0.08 & -0.01 & -0.15 & -0.28 & -0.16 & -0.05 & -0.02 & 0.02 & -0.12 & -0.23 & -0.09 & -0.10 & -0.12 & -0.12 & -0.23 & -0.09 & -0.10 & -0.12 &$	7. 1				,	- 1		1				- 1		
7. $2.2(9)$ $\begin{vmatrix} -0.04 & -0.08 & -0.01 & -0.15 & -0.28 & -0.16 & -0.05 & -0.02 & 0.02 & -0.12 & -0.23 & -0.09 & -0.10 & -0.12 & -0.12 & -0.23 & -0.09 & -0.10 & -0.12 &$	9.12.3.9	-0.37	-0.67	-0.68	-1.24	-1.40	-1.34	-1.08	-0.99	-1.29	-0.89	-0.68	-0.32	-0.91
D. 7													1	
Dail. ext. $ -0.15 -0.24 -0.14 $ 0.02 0.33 0.03 0.02 -0.08 -0.02 -0.10 0.04 0.10 -0.02	Dail.ext.	-0.15	-0.24	-0.14	0.02	0.33	0.03	0.02	-0.08	-0.02	-0.10	0.04	0.10	-0.02

PRUSSIA. — STETTIN. Lat. 53° 25' N. Long. 14° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

						es of R							
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midnight.	0.26	0.54	0.98	1.66	2.21	2.21	1.83	1.93	1.53	0.88	0.50	0.39	1.2
1	0.38		1.17	1.91	2.66	2.46	2.25	2.24	1.61	1.01	0.44	0.46	1.4
2	0.43	0.70	1.30	1	3.03	2.84	2.62	2.54	1.87	1.13	0.47	0.50	16
3	0.49	0.88	1.41	2.39	3.39	3.10	2.95	2.83	2.11	1.24	0.51	0.56	1.9
4	0.53	0.89	1.51	2.60	3.58	3.08	3.07	3.08	2.33	1.33	0.55	0.61	1.9
5	0.57	0.97	1.63	2.67	3.45	2.78	2.85	3.10	2.46	1.40	0.58	0.64	1.9
6	0.55	0.94	1.62	2.40	1	2.12	2.21	2.78	2.45	1.42	0.60	0.56	1.7
7	0.46	0.83	1.37	1.70	1.63	1.17	1.31	2.02	1.98	1.25	0.52	0.46	1.2
8	0.36	0.66	0.90	0.66	0.33	0.20	0.35	0.96	1.11	0.79	0.43	0.38	0.5
9	0.22	0.36			-0.88			1	1	0.16			-0.1
10	-0.01				-1.87					1	-0.22	í	i
11	-0.36				-2.62								
Noon.	-0.63	-0.93	-1.59	-2.50	-3.09	-2.59	-2.46	-2.93	-2.58	-1.68	-0.90	-0.64	-1.S
1					-3.36								
2					-3.50								
3	-0.78	-1.34	-2.06	-2.84	-3.35	-2.90	-2.80	-3.3S	-2.82	-1.88	-0.94	-0.86	-2.1
4					-2.99								
5	-0.41	-0.83	-1.43	-2.02	-2.46	-2.46	-2.15	-2.40	-1.85	-0.99	-0.39	-0.48	-1.4
6	-0.25	-0.46	-0.90	-1.32	-1.74	-1.74	-1.62	-1.68	-1.14	-0.46	-0.19	-0.30	-0.9
7	-0.11	-0.23	-0.40	-0.55	-0.89	-0.89	-0.93	-0.7 8	-0.52	-0.10	-0.00	-0.1S	-0.4
8	0.01	-0.01	-0.02	0.10	-0.14	-0.14	-0.17	0.02	0.06	0.17	0.18	-0.06	-0.0
9	0.08	0.16	0.32	0.68	0.73	0.73	0.48	0.74	0.60	0.39	0.30	0.07	0.3
10	0.20		0.61	1.10	1.30	1.30	1.03	1.20	1.00	0.58	0.43	0.22	0.7
11	0.25	0.42	0.79	1.42	1.76	1.76	1.47	1.60	1.31	0.74	0.50	0.32	1.0
6, 6	0.15	0.21	0.36	0.54	0.52	0.19	0.29	0.55	0.65	0.48	0.21	0.13	0.3
7, 7	0.17	0.30	0.48	0.57	0.37	0.14	0.19	0.62	0.73	0.57	0.26	0.14	0.3
8, 8	0.19	0.31	0.44	0.38	0.10	0.03	0.09	0.49	0.59	0.48	0.31	0.16	0.3
9, 9	0.15	0.26	0.28	0.13	-0.08	0.01	-0.03	0.21	0.28	0.28	0.22	0.15	0.1
10, 10	0.03	0.14	0.09	-0.13	-0.29	-0.12	-0.15	-0.10	-0.06	0.02	0.11	0.10	-0.0
7, 1	-0.17												,
7, 2, 9	-0.13												
, 2, 10	-0.05	-0.05	0.38	0.19	0.19	0.14	0.03	0.16	0.15	-0.02	-0.01	-0.05	0.0
aily ext.	-0.16	-0.21	-0.23	-0.14	10.0	0.06	0.04	-0.20	-0.27	-0.32	-0.23	-0.15	-0.1

 \mathbf{E}

Sleswick. — Apenrade. Lat. 55° 3' N. Long. 9° 25' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

			_		Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Mom 1	0.26	0.69	0.98	1.73	3.18	3.82	2.50	2.61	2.16	i.06	0.54	0.21	1 65
Morn. 1	0.20	0.03	1.14	1.73	3.17	3.90	2.38	$\frac{2.61}{2.66}$	2.10	1.19	1	0.31 0.35	1.65 1.72
3	0.38	0.79	1.14	1	3.02	3.82	2.13	2.66	1	1.19		$0.35 \\ 0.37$	1.74
4	0.33	0.75	1.34	2.10	2.71	3.50	1.78	$\frac{2.66}{2.64}$	2.62	1.37	0.66	0.38	1.69
-1	0.42	0.10	1.04	2.10	2.71	3.50	1.70	4.01	2.02	1.01	0.00	0.00	1.03
5	0.44	0.69	1.31	2.02	2.22	2.89	1.35	2.18	2.43	1.36	0.69	0.40	1.50
6	0.50	0.62	1.18	1.63	1.54	1.94	0.86	1.56	2.02	1.25	0.69	0.40	1.18
7	0.47	0.54	0.90	1.15	0.70	0.83	0.30	0.77	1.18	0.97	0.61	0.37	0.73
8	0.39	0.38	0.50	0.41	-0.23	-0.34	-0.29	-0.18	0.18	0.52	0.42	0.27	0.17
_													
9	0.23			-0.42	1	l	1			-0.10	1	0.10	
10		1		-1.22		i				l	l .	-0.15	-1.00
11	II.	į.		-1.90		1		l .	-2.38	l	-0.68	1	-1.41
Noon	-0.62	-1.19	-1.62	-2.42	-2.86	-2.9 8	-2.09	-2.74	-2.79	-1.94	-0.98	-0.66	-1.91
1	-0.78	-1.40	-1.90	-2.75	-3.08	-3.24	-2.23	-2.89	-3 03	-2.15	-1.10	-0.78	-2.11
2	1			-2.89				l	l				-2.14
3	II .	i	į.	-2.79				l	l .	-1.74	1	-0.59	
4	11			-2.43			1	I				l	-1.71
										1	1		
5	-0.16	-0.23	-0.92	-1.80	-2.40	-3.34	-1.70	-2. 02	-1.93	-0.71	-0.29	-0.15	-1.30
6	-0.03	0.05	-0.42	-0.99	-1.70	-2.57	-1.18	-1.23	-1.13	-0.25	-0.12	0.02	-0.80
7	0.01	0.18	0.02	-0.12	-0.79	-1.42	-0.57	-0.47	-0.26	0.10	0.02	0.10	-0.27
8	0.03	0.18	0.33	0.66	0.22	-0.07	0.18	0.40	0.56	0.34	0.03	0.14	0.25
9	0.01	0.17	0.54	1.25	1.22	1.25	0.97	1.21	1.21	0.51	0.09	0.15	0.71
10	0.01	0.17	0.66	1.57	2.05	2.33	1.63	1.72	1.61	0.65	0.03	0.13	1.07
11	0.07	0.33	0.76	1.69	2.66	3.10	2.14	2.25	1.83	0.85	0.30	0.10	1.35
Midn	0.15	0.52	0.86	1.70	3.02	3.57	2.43	1.68	1.97	0.92	0.42	0.26	1.46
2,2,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1	0.10	0.02	0.00	1	0.02	0.01	2.10	1.00	1.0.	0.02	0	0.20	2
6. 6	0.24	0.34	0.38		-0.08			0.17	0.45	0.50	0.29	0.21	0.19
7. 7	0.24	0.36	0.46		-0.05			0.15	0.46	0.54	0.30	0.24	0.23
8. 8	0.21	0.28	0.42	0.54				0.11	0.37	0.43	0.23	0.21	0.21
9. 9	0.11	0.14	0.26	0.42	0.04	-0.07	0.05	0.06	0.19	0.21	0.10	0.13	0.14
10.10	-0.02	-0.05	-0.00	0.18	0.08	0.09	0.12	-0.13	-0.05	-0.07	-0.06	0.02	0.01
7. 2. 9	_0.08	-0.21	-0.17	-0.16	-0.41	-0.47	-0.33	_0.31	0.93	-0.20	_0 11	-0.08	-0.23
6. 2. 8	ł.	-0.18	í	1	-0.47					-0.16	1	r .	-0.23
6. 2.10	1	-0.17	-0.04	0.10	0.14	0.26	0.07	0.13		-0.06			0.04
6. 2. 6	1	-0.22)	-1.11	-1.37		-0.86		-0.36			-0.58
	""	0.22	0.10			1.01	0.00	0.00	0	5.50			
7. 2	-0.11	-0.10	-0.53	-0.87	-1.23	-1.33	-0.99	-1.07	-0.95	-0.55	-0.21	-0.19	-0.70
8. 2	-0.15	-0.48	-0.73	-1.24	-1.70	-1.92	-1.2 8	-1.54	-1.45	-0.78	-0.30	-0.24	-0.98
8. 1	-0.20	-0.51		-1.17									-0.97
7. 1	-0.16	-0.43	-0.50	-0.80	-1.19	-1.21	-0.97	-1.06	-0.93	-0.59	-0.25	-0.21	-0.69
9.12.3.9	0.05	0.50	0.70	1.10	1 4~	1 -0	1 05	1.95	1 0 4	0.00		_0.95	-0.91
1	1	-0.50	(-1.70				-0.82 -0.02)	1	0.01
7. 2.2(9)	-0.06	-0.12	0.01	0.19	0.01	-0.04	-0.01	0.07	0.13	-0.02	-0.00	-0.02	0.01
Dail.ext.	-0.14	-0.31	-0.31	-0.40	0.01	0.11	0.12	-0.12	-0.23	-0.39	-0.21	-0.19	-0.20

LXI.

Scotland. — Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Fahrenheit.

					Degree	SOL Fai	renheit	•					
Hours,	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.38	0.86	1.76	3.02	3.04	3.29	4.10	2.95	2.54	1.10	1.26	0.72	2.09
2	0.61	0.77	1.98	3.92	3.47	3.62	4.28	3.20	2.77	1.19	1.53	0.65	2.33
3	0.68	0.77	2.41	4.57	3.96	3.74	4.66	3.49	3.29	1.31	1.40	0.61	2.57
4	0.95	0.95	2.59	5.31	4.41	3.98	5.11	3.71	3.65	1.33	1.46	0.70	2.84
5	1.06	1.17	2.75	5.49	4.28	3.94	4.59	3.65	3.78	1.62	1.37	0.77	2.87
6	1.06	1.31	2.79	5.36	3.51	3.04	3.56	3.26	3.51	2.03	1.28	0.59	2.61
7	0.97	1.24	2.48	3.47	2.66	2.25	2.39	2.25	2.75	1.62	1.06	0.68	1.98
8	0.88	1.26	1.80	2.18	1.40	1.10	1.15	1.08	1.46	0.97	1.04	0.54	1.24
											1.01	0.01	1.21
9	0.61	0.77	0.81		1 1			-0.50	1	1	0.56	0.32	0.18
10	0.16	-0.07										-0.02	-0.75
11		-0.97		-3.02			1		1	1		-0.86	
Noon	-1.04	-1.69	-2.61	-3.92	-2.75	-2.79	-3.58	-2.99	-3.13	-2.36	-1.96	-1.33	-2.51
1	-1.42	-2.25	-2.97	-4.37	-3.35	-3.15	-3.67	-3.44	-3.92	-2.79	-2.30	-1.51	-2.03
2												-1.55	
3												-1.13	
	1						Į.		1			1	1 1
4	-1.19	-1.75	-3.33	-4.79	-4.19	-3.94	-4.40	-3.87	-3.56	-1.96	-1.69	-0.83	-2.96
5	-0.68	-0.95	-2.84	-4.25	-4.03	-3.71	-4.57	-3.76	-3.56	-1.31	-1.04	-0.50	-2.60
6	-0.45	-0.47	-2.14	-3.83	-3.51	-3.29	-4.41	-3.47	-2.30	-0.59	-0.68	-0.27	-2.12
7	-0.09	-0.09	-1.17	-2.45	-2.61	-2.52	-3.58	-1.69	-0.97	1	-0.25		-1.27
8	0.14	0.32	-0.45	-0.81	-1.17	-0.79	-1.31	-0.41	-0.16	0.59	ì	l .	-0.31
	0.00	0.01	0.05	0.00	0.00	0.50	0.40	0.50		0 -0			
9	0.23	0.61	0.25	0.38	0.32	0.50	0.43	0.59	0.59	0.72	0.32	0.36	0.44
10	0.18	0.88	0.77	1.08	0.86	1.89	1.71	1.58	1.24	1.15	0.79	0.41	1.04
11	0.32	0.99	1.31	2.18	1.69	2.16	2.52	2.23	1.67	1.60	1.19	0.54	1.53
Midn	0.38	1.01	1.44	2.68	2.32	2.68	3.44	2.77	2.27	1.49	1.42	0.59	1.87
6. 6	0.32	0.43	0.34	0.77	0.00	0.14	-0.43	- 0.11	0.61	0.00	0.99	0.16	0.25
7. 7	0.32	0.43	0.65	0.77	0.00	-0.14	1	0.29	0.61	$0.72 \\ 0.83$	0.32 0.41	0.10	0.25
8.8	0.52	0.39	0.68	0.32	0.02	0.14	1	0.34	0.65	0.79	0.54	0.43	0.47
9. 9	0.32	0.70	0.54	0.07	0.11	0.16	0.11	0.05	0.03	0.79	0.45	0.34	0.32
10.10	0.18	0.41	0.34			0.10	0.11	0.03	0.23	0.16	0.43	0.20	0.15
10.10	0.10	0.41	0.47	-0.47	-0.11	0.25	0.10	0.10	0.07	0.10	0.20	0.20	0.15
7. 2. 9	-0.14	-0.14	-0.18	-0.29	-0.27	-0.36	-0.43	-0.27	-0.32	-0.16	-0.41	-0.18	-0.26
6. 2. 8	-0.14	-0.20	-0.32	-0.07	-0.47	-0.52	-0.61	-0.27	-0.32	-0.07	-0.41	-0.23	-0.30
6. 2.10	-0.11	-0.02	0.09	0.56	0.20	0.36	0.41	0.41	0.16	0.11	-0.16	-0.18	0.15
6. 2. 6	-0.32	-0.47	-0.88	-1.06	-1.26	-1.35	-1.64	-1.28	-1.01	-0.47	-0.65	-0.41	-0.90
7. 2	-0 30	_0.50	_0.41	_0.62	-0.56	_0.50	-0.86	-0.70	-0.77	-0.61	-0.77	-0.45	_0.61
8. 2												-0.45 -0.52	
8. 1							l .				1		
7. I			i		1				l		i	-0.50 -0.41	1
			1										
9.12.3.9	-0.45	-0.65	-1.21	-2.23	-1.55	-1.71	-1.94	-1.64	-1.71	-0.97	-0.92	-0.45	-1.29
7. 2.2(9)	-0.05			-0.14								-0.05	
Dail. ext.	-0.27	-0.49	-0.29	0.20	-0.11	-0.20	0.27	-0.09	-0.25	-0.40	-0.56	-0.40	-0.20

LXII.

Scotland. - Leith. Lat. 55° 59' N. Long. 3° 10' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Morn. 1	0.17	0.38	0.78	1.34	1.35	1.46	1.82	1.31	1.13	0.49	0.56	0.32	0.93
2	0.27	0.34	0.88	1.74	1.54	1.61	1.90	1.42	1.23	0.53	0.68	0.29	1.04
3	0.30	0.34	1.07	2.03	1.76	1.66	2.07	1.55	1.46	0.58	0.62	0.27	1.14
4	0.42	0.42	1.15	2.36	1.96	1.77	2.27	1.65	1.62	0.59	0.65	0.31	1.26
5	0.47	0.52	1.22	2.44	1.90	1.75	2.04	1.62	1.68	0.72	0.61	0.34	1.28
6	0.47	0.58	1.24	2.38	1.56	1.35	1.58	1.45	1.56	0.90	0.57	0.26	1.16
7	0.43	0.55	1.10	1.54	1.18	1.00	1.06	1.00	1.22	0.72	0.47	0.30	0.88
8	0.39	0.56	0.80	0.97	0.62	0.49	0.51	0.48	0.65	0.43	0.46	0.24	0.55
9	0.27	0.34	0.36	-0.12	0.05	-0.08	-0.10	-0.22	-0.06	0.14	0.25	0.14	0.08
10	0.07	-0.03	0.08	-0.89	-0.47	-0.58	-0.61	-0.56	-0.49	-0.37	-0.15	-0.01	-0.33
11	-0.15	-0.43	-0.54	-1.34	-0.89	-1.02	-1.00	-0.90	-0.98	-0.76	-0.59	-0.38	-0.75
Noon	-0.46	-0.75	-1.16	-1.74	-1.22	-1.24	-1.59	-1.33	-1.39	-1.05	-0.87	-0.59	-1.12
1	-0.63	-1.00	-1.32	-1.94	-1.49	-1.40	-1.63	-1.53	-1.74	-1.24	-1.02	-0.67	-1.30
2	1	1	l	l i			1	-1.62					
3							l	-1.62			1		
4	l .	1	1				1	-1.72		,			
5	1			ı		1		-1.67			1	l .	
6	l .		}	1				-1.54	1		1	l	-0.94
7	-0.04		i .	L				-0.75		i .	-0.11	t .	-0.56
s	0.06	0.14	-0.20	-0.36	-0.52	-0.35	-0.58	-0.18	-0.07	0.26	0.02	0.13	-0.14
9	0.10	0.27	0.11	0.17	0.14	0.22	0.19	0.26	0.26	0.32	0.14	0.16	0.20
10	0.08	0.39	0.34	0.48	0.38	0.84	0.76	0.70	0.55	0.51	0.35	0.18	0.46
11	0.14	0.44	0.58	0.97	0.75	0.96	1.12	0.99	0.74	0.71	0.53	0.24	0.68
Midn	0.17	0.45	0.64	1.19	1.03	1.19	1.53	1.23	1.01	0.66	0.63	0.26	0.83
6. 6	0.14	0.19	0.15	0.34	0.00	-0.06	-0.19	-0.05	0.27	0.32	0.14	0.07	0.11
7. 7	0.20		1	0.23	0.01	ĺ	-0.27	0.13	0.40	0.37	0.18	0.19	0.16
8. 8	0.23		0.30	0.31	0.05		-0.04	1	0.29	0.35	0.24	0.19	0.21
9. 9	0.19	1	0.24	0.03	0.10	ł	0.05	I	0.10	0.23	0.20	0.15	0.14
10.10	0.08	1	i		-0.05	0.13	ļ	1	0.03	ı	0.10	0.09	
7. 2. 9	l l	-0.06	I	1	1	1	1	-0.12	i	l .	l .	l .	1
6. 2. 8	Į.	-0.09		-0.03	1	ı	1	1	i	-0.03	1	l .	
6. 2.10		-0.01	0.04	0.25		1)		l .	1	-0.07	1	
6. 2. 6	-0.14	-0.21	-0.39	-0.47	-0.56	-0.60	-0.73	-0.57	-0.45	-0.21	-0.29	-0.18	-0.40
7. 2								-0.31					
8. 2								-0.57					
8. 1								-0.53					
7. 1	-0.10	-0.23	-0.11	-0.20	-0.16	-0.20	-0.29	-0.27	-0.26	-0.26	-0.28	-0.18	-0.21
9.12.3.9	$\ _{-0.20}$	-0.29	-0.55	-0.99	-0.69	-0.76	-0.86	-0.73	-0.76	-0.43	-0.41	-0.20	-0.57
7. 2.2(9)	-0.02							-0.03					-0.04
Dail. ext.	-0.12	-0.22	-0.13	0.09	0.05	-0.09	0.12	-0.04	-0.11	-0.18	$ _{-0.25}$	-0.18	-0.09
i					·		(

LXIII.

Scotland. — Makerstoun. Lat. 55° 36' N. Long. 2° 31' W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.67	0.88	1.24	2.30	2.00	2.25	2.10	1.98	1.95	0.88	0.46	0.24	1.4
1	0.76	0.92	1.37	2.52	2.04	2.43	2.44	2.24	2.15	0.88	0.46	0.16	1.5
2	0.78	1.08	1.37	2.70	2.33	2.54	2.57	2.38	2.26	1.06	0.60	0.18	1.6
3	0.76	1.06	1.48	2.79	2.55	2.65	2.79	2.56	2.35	1.57	0.60	0.29	1.7
4	0.67	1.01	1.66	2.96	2.51	2.43	2.70	2.56	2.48	1.20	0.68	0.40	1.7
5	0.78	0.92	1.77	2.88	2.06	1.96	2.21	2.44	2.46	1.40	0.60	0.44	1.6
6	0.60	0.85	1.73	2.25	1.31	1.12	1.35	1.78	2.22	1.31	0.66	0.51	1.5
7	0.51	0.99	1.26	1.43	0.48	0.32	0.46	0.91	1.24	1.26	0.66	0.44	0.8
8	0.53	0.79	0.46	0.36	-0.25	-0.51	-0.39	-0.09	0.00	0.62	0.66	0.40	0.5
9	0.33	0.08	-0.38	-0.79	-0.94	-1.11	-0.96	-1.02	-1.00	-0.16	0.08	0.22	-0.
10	-0.22	-0.72	-1.12	-1.86	-1.52	-1.68	-1.59	-1.78	-1.92	-0.96	-0.47	-0.20	-1.
11	-0.84	-1.21	-1.67	-2.55	-2.09	-2.26	-2.14	-2.33	-2.45	-1.63	-0.94	-0.62	-1.
Noon.	-1.36	-1.61	-2.09	-3.06	-2.34	-2.48	-2.45	-2.73	-2.67	-2.03	-1.34	-0.93	-2.
1	-1.71	-2.03	-2.27	-3.44	-2.69	-2.75	-2.48	-2.87	-3.03	-2.25	-1.56	-1.13	-2.
2	-1.67	-2.05	-2.36	-3.57	-2.65	-2.57	-2.52	-2.93	-3.12	-2.20	-1.47	-0.96	-2.
3	-1.29	-1.68	-2.32	-3.52	-2.65	-2.28	-2.54	-2.73	-2.85	-1.83	-0.96	-0.60	-2.
4	-0.71	-1.30	-1.80	-3.05	-2.27	-1.95	-2.28	-2.47	-2.29	-1.23	-0.45	-0.16	-1.
5	-0.13	-0.50	-1.20	-2.30	-1.76	-1.64	-1.81	-1.78	-1.49	-0.49	-0.07	-0.11	-1.
6	0.18	-0.08	-0.40	-1.39	-0.98	-0.95	-1.34	-1.07	-0.60	-0.09	0.13	0.18	-0.
7	0.29	0.15	0.08	-0.19	-0.18	-0.40	-0.59	-0.18	0.06	0.17	0.17	0.18	-0.
8	0.31	0.37	0.46	0.52	0.62	0.36	0.35	0.56	0.46	0.40	0.28	0.18	0.
9	0.29	0.52	0.73	1.21	1.15	1.00	0.95	1.09	0.95	0.64	0.37	0.24	0.
10	0.27	0.64	0.95	1.74	1.46	1.56	1.48	1.58	1.33	0.73	0.46	0.31	1.
11	0.22	0.79	1.06	2.08	1.77	1.94	1.70	1.89	1.51	0.73	0.40	0.36	1.
Mean.	1.53	0.35	2.06	5.96	6.86	10.25	10.12	10.00	8.51	6.64	4.60	1.16	

LXIV.

IRELAND. — DUBLIN. Lat. 53° 23' N. Long. 6° 20' W. Gr. — Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
A.M.1	0.58	0.53	1.56	2.18	2.53	2.76	2.18	2.22	1.64	1.16	0.53	0.36	1.52
3	0.80	0.71	1.64	2.40	2.89	3.11	2.53	2.40	1.87	1.42	0.67	0.49	1.74
5	0.93	0.98	1.64	2.49	2.31	2.18	2.18	2.53	1.87	1.73	0.76	0.58	1.68
7	0.84	0.93	1.38	0.58	-0.22	-0.89	-0.36	0.40	1.07	1.56	0.80	0.53	0.56
9	0.36	0.18	-0.31	-1.11	-1.24	-1.38	-1.10	-1.16	-0.76	-0.09	0.27	0.36	-0.50
11	-0.98	-0.07	-1.82	-2.40	-2.18	-2.09	-2.04	-2.27	-2.13	-1.91	-0.98	-0.71	-1.71
P.M.1	-1.60	-1.78	-2.67	-2.93	-2.62	-2.40	-2.27	-2.62	-2.67	-2.44	-1.56	-1.16	-2.23
3	1		,			(1	-2.49				1	-1.99
5	-0.44	0.44	-1.29	-1.82	-1.82	-1.87	-1.64	-1.73	-1.29	-0.84	-0.27	-0.18	-1.14
7	0.09	0.18	0.18	0.04	-0.27	-0.44	-0.27	-0.09	0.27	0.04	0.04	0.09	-0.01
9	0.22	0.31	0.76	1.20	1.29	1.24	1.20	1.16	0.93	0.58	0.36	0.18	0.79
11	0.36	0.40	1.07	1.73	1.96	2.04	1.87	1.64	1.42	0.84	0.44	0.22	1.17
Mean.	4.09	4.75	5.10	6.66	9.51	11.86	12.48	12.31	10.79	7.73	5.99	4.88	

LXV.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
					- 00								
Morn. 1	0.59	0.91	1.84	1.97	3.09	3.69	i	2.49	1.99	0.68	0.47	0.65	1.82
2	0.58	0.89	2.09	2.41	3.52	4.15	3.76	2.93	2.27	0.84	0.42	0.67	2.04
3	0.53	0.87	2.42	2.87	3.80	4.35	3.96	3.42	2.60	1.04	0.36	0.64	2.24
4	0.48	0.89	2.80	3.21	3.82	4.17	4.01	3.78	2.89	1.23	0.35	0.61	2.35
5	0.58	0.95	3.11	3.23	3.45	3.54	3.78	3.79	2.98	1.36	0.43	0.63	2.32
6	0.54	1.00	3.15	2.83	2.67	2.49	3.18	3.30	2.74	1.36	0.55	0.72	2.04
7	0.60	0.94	2.76	1.99	1.57	1.18	2.21	2.29	2.11	1.17	0.64	0.81	1.52
8	0.56	0.71	1.90	0.84	0.31	0.17	0.98	0.94	1.16	0.80	0.60	0.80	0.79
9	0.37	0.27	0.65	-0.41	-0.88	-1.35	-0.34	-0.48	0.05	0.28	0.37	0.61	-0.07
10	-0.01	-0.33	-0.75	-1.52	-1.85	-2.23	-1.61	-1.70	-1.03	-0.32	-0.02	0.21	-0.93
11	-0.60	-0.97	-2.03	-2.34	-2.53	-2.79	-2.72	-2.55	-1.93	-0.89	-0.49	-0.34	-1.68
Noon	i .	-1.47	1	-2.83		1	í	-3.03	l	ł	-0.89	l .	-2.23
1	-1.30	_1.75	-3.52	-3.04	-3.25	-3.35	-1.33	-3.25	-2.98	-1.62	-1.12	-1.32	-2.57
2	1	-1.77	1	-3.03		l .	}	i	}	-1.69		!	1
3	j	-1.55	l .			l	ł	1	1	-1.58	1		
4	1	l	1			l .	1	l		1			
4	-0.54	-1.19	-2.96	-2.60	-3.33	-3.40	-4.62	-3.27	-2.98	-1.31	-0.66	-1.10	-2.30
5	-0.34	-0.79	-2.40	-2.18	-2.95	-3.09	-3.90	-2.98	-2.57	-0.96	-0.37	-0.73	-1.94
6	-0.11	-0.42	-1.77	-1.61	-2.29	-2.43	-2.77	-2.39	-1.93	-0.58	-0.14	-0.39	-1.40
7	0.11	-0.10	-1.08	-0.92	-1.41	-1.52	-1.39	-1.53	-1.12	-0.23	0.01	-0.14	-0.78
8	0.22	0.17	0.36	-0.22	-0.42	-0.48	0.03	-0.53	-0.26	0.06	0.12	0.03	0.14
9	0.30	0.42	0.32	0.42	0.53	0.56	1.28	0.43	0.52	0.26	0.22	0.15	0.45
10	0.37	0.63		0.91	1.35	1.51	2.22	1.20	1.13	1	0.33	0.28	0.95
11	0.36	0.80	l .	1.29	2.03	2.35	2.84	1.74	1.52	0.48	0.42	0.43	1.30
Midn	0.55	0.89	l	1.61	2.59	3.07	3.23	2.12	1.77	0.56	0.48	0.57	1.59
Midi	0.55	0.00	1.02	1.01	2.00	0.07	0.20	2.12	1	0.50	0.40	0.51	1.00
6. 6	0.21	0.27	0.69	0.61	0.19	0.03	0.20	0.45	0.40	0.39	0.21	0.17	0.32
7. 7	0.35	0.42	1	0.53	l .	-0.17	0.41	0.38	0.49	1	0.33	0.33	0.37
8. 8	0.39	0.44	0.77	0.31	l .	-0.33	0.51	0.20	0.45	1	0.36	0.41	0.32
9. 9	0.33	0.34	0.49	0.01	-0.17	i	0.47	-0.03	1	0.43	0.30	0.38	0.19
10.10	0.33	0.15	1	1	-0.17 -0.25	l .	1	-0.25	0.25	0.04	0.15	0.35	0.00
7. 2. 9	-0.16	-0.14	-0.18	_0.91	-0.44	-0.59	_0.49	-0.21	-0.18	_0.00	-0.09	_0.19	-0.20
6. 2. 8	il .		i	1	1		1	-0.21	í	1	-0.15		-0.26
	II	i .	-0.28	1	l	i	į.	l .	1	l	ł	1	1
6. 2.10	11	-0.05		0.24	1	1	1	0.39	l .	1	1	-0.17	0.10
6. 2. 6	-0.31	-0.40	-0.75	-0.60	-0.01	-1.15	-1.46	-0.81	-0.78	-0.30	-0.24	-0.39	-0.68
7. 2			-0.43										
8. 2	i i	i	-0.86	1	ľ	i	1	1		1		1	1
8. 1	-0.37	-0.52	-0.81	-1.10	-1.47	-1.76	-1.68	-1.16	-0.91	-0.41	-0.26	[-0.26]	-0.89
7. 1	-0.35	-0.41	-0.38	-0.53	-0.84	-1.09	-1.06	-0.48	-0.44	-0.23	-0.24	-0.26	-0.53
9.12.3.9	-0.38	_0.59	-1.36	_1 49	_1 70	_1 97	_1 00	_1 61	-1.30	_0.60	-0.31	-0.30	-1.12
7. 2.2(9)	11		-0.06			1	1	1	1	1	-0.01	1	
Dail.ext.	-0 20	_0 20	_0.31	0.10	0.10	0.40	_0.15	0.99	0.17	_0.17	_0.95	-0.35	-0.17
Dan.ext.	(- 0.09	-0.08	-0.24	0.10	0.18	1 0.40	-0.49	0.44	0.17	-0.17	-0.20	0.00	0.17

LXVI.

Russia. — Catharinenburg. Lat. 56° 50' N. Long. 60° 34' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year
Midn.	0.42	1.07	1.70	2.12	2.64	3.06	2.93	2.16	1.96	0.89	0.47	0.47	1.6
1	0.52	1.19	2.00	2.40	3.11	3.51	3.41	2.49	2.31	1.08	0.51	0.50	1.9
2	0.52	1.25	2.23	2.82	3.49	3.90	3.86	2.76	2.58	0.99	0.54	0.52	2.1
3	0.55	1.41	2.53	3.05	3.73	4.15	4.11	3.03	2.83	1.47	0.58	0.54	2.3
4	0.63	1.52	2.75	3.26	3.74	3.92	4.28	3.22	3.06	1.61	0.68	0.58	2.4
5	0.68	1.67	2.85	3.24	3.27	3.35	3.66	3.14	3.22	1.67	0.71	0.61	2.3
6	0.73	1.76	3.06	2.24	2.27	1.99	2.47	2.45	3.04	1.69	0.82	0.64	1.9
7	0.81	1.76	2.59	1.61	0.89	0.61	1.02	1.37	2.27	1.53	0.85	0.65	1.3
8	0.88	1.51	1.46	0.34	-0.24	-0.53	-0.28	0.18	0.85	0.91	0.77	0.58	0.5
9	0.67	0.73	-0.06	-0.81	-1.09	-1.46	-1.45	-0.97	-0.57	-0.03	0.33	0.39	-0.3
10	0.13	-0.45	-1.45	-1.99	-1.94	-2.23	-2.35	-1.72	-1.68	-0.78	-0.22	-0.08	-1.2
11	-0.57	-1.44	-2.39	-2.62	-2.72	-2.93	-3.10	-2.54	-2.50	-1.46	-0.72	-0.71	-1.9
Noon.	-1.04	-2.13	-2.95	-3.09	-3.19	-3.38	-3.58	-2.99	-3.09	-1.73	-1.03	-1.19	-2.4
1	-1.39	-2.58	-3.27	-3.22	-3.28	-3.48	-3.57	-3.04	-3.32	-1.99	-1.25	-1.45	-2.6
2	-1.50	-2.74	-3.38	-3.26	-3.41	-3.59	-3.55	-3.02	-3.36	-2.02	-1.23	-1.39	-2.7
3	-1.28	-2.37	-3.18	-2.86	-3.14	-3.37	-3.40	-3.03	-3.48	-2.23	-1.11	-1.00	-2.5
4	-0.85	-1.97	-2.82	-2.65	-2.99	-3.05	-3.15	-2.83	-3.18	-1.61	-0.79	-0.61	-2.2
5	-0.50	-1.2 S	-2.20	-2.14	-2.60	-2.49	-2.67	-2.37	-2.48	-0.95	-0.47	-0.33	-1.7
6	-0.22	-0.74	-1.37	-1.46	-1.98	-1.98	-2.14	-1.66	-1.56	-0.56	-0.26	-0.11	-1.1
7	0.00	-0.25	-0.67	-0.59	-0.95	-1.17	-1.29	-0.79	-0.65	-0.22	-0.07	0.02	-0.5
8	0.10	0.08	-0.12	0.13	-0.04	-0.12	-0.16	0.11	0.07	0.06	0.06	0.11	0.0
9	0.17	0.40	0.44	0.65	0.85	0.96	0.83	0.84	0.67	0.36	0.16	0.26	0.5
10	0.24	0.65	0.94	1.13	1.53	1.88	1.67	1.39	1.25	0.53	0.27	0.39	0.9
11	0.34	0.86	1.34	1.58	2.13	2.51	2.36	1.81	1.65	0.74	0.40	0.56	1.3
Mean.	-10.76	-9.50	-5.83	0.47	6.31	12.08	14.53	10.61	6.32	1.41	-6.11	-11.68	

LXVII.

Russia.—St. Petersburg. Lat. 59° 56′ N. Long. 30° 18′ E. Gr.—Dove.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.14	0.38	0.73	1.44	2.08	1.99	1.77	1.68	1.17	0.52	0.15	0.17	1.02
1	0.21	0.44	0.99	1.68	2.43	2.29	2.05	2.02	1.38	0.60	0.17	0.21	1.21
2	0.25	0.46	1.22	1.91	2.70	2.56	2.24	2.24	1.58	0.65	0.15	0.27	1.35
3	0.30	0.52	1.38	2.11	2.91	2.73	2.43	2.48	1.75	0.73	0.25	0.34	1.49
4	0.38	0.63	1.56	2.24	2.86	2.44	2.32	2.59	1.87	0.78	0.30	0.36	1.53
5	0.43	0.72	1.71	2.28	2.38	1.97	1.92	2.40	1.96	0.84	0.34	0.34	1.44
6	0.45	0.76	1.75	1.95	1.72	1.33	1.33	1.96	1.90	0.90	0.37	0.30	1.23
7	0.41	0.78	1.57	1.32	0.93	0.63	0.64	1.19	1.47	0.82	0.37	0.29	0.87
8	0.42	0.60	1.07	0.65	0.14	-0.04	0.05	0.42	0.81	0.57	0.32	0.25	0.44
9	0.35	0.40	0.40	-0.05	-0.59	-0.69	-0.56	-0.40	0.00	0.20	0.17	0.17	-0.05
10	0.13	-0.05	-0.19	-0.78	-1.30	-1.21	-1.12	-1.07	-0.71	-0.22	0.00	0.04	-0.54
11	-0.20	-0.48	-0.86	-1.42	-1.92	-1.71	-1.58	-1.64	-1.27	-0.61	-0.20	-0.14	-1.00

LXVII.

Russia. - St. Petersburg, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-0.38	-0.90	-1.31	-1.93	-2.30	-1.99	-1.89	-2.10	-1.72	-0.94	-0.37	-0.30	-1.34
1	-0.63	-0.97	-1.62	-2.10	-2.41	-2.17	-2.03	-2.47	-2.26	-1.75	-0.64	-0.48	-1.63
2	-0.66	-1.04	-1.88	-2.36	-2.65	-2.32	-2.15	-2.60	-2.34	-1.29	-0.63	-0.58	-1.71
3	-0.55	-0.99	-1.94	-2.49	-2.90	-2.45	-2.29	-2.64	-2.31	-1.06	-0.46	-0.40	-1.71
4	-0.33	-0.83	-1.92	-2.65	-2.92	-2.60	-2.41	-2.80	-2.27	-0.86	-0.20	-0.31	-1.68
5	-0.25	-0.45	-1.53	-2.31	-2.48	-2.23	-2.06	-2.45	-1.76	-0.50	-0.16	-0.22	-1.37
6	-0.19	-0.26	-1.02	-1.43	-1.65	-1.41	-1.30	-1.41	-0.95	-0.25	-0.11	-0.14	-0.84
7	-0.18	-0.16	-0.55	-0.61	-0.74	-0.71	-0.63	-0 62	-0.35	-0.09	-0.05	-0.10	-0.40
8	-0.14	-0.03	-0.25	-0.03	0.06	-0.03	0.02	0.09	0.07	0.07	0.01	0.08	-0.01
9	-0.11	0.08	0.03	0.47	0.79	0.67	0.64	0.65	0.40	0.18	0.08	0.03	0.33
10	-0.03	0.17	0.24	0.84	1.22	1.25	1.18	1.05	0.66	0.33	0.08	0.02	0.58
11	0.06	0.30	0.50	1.17	1.76	1.65	1.45	1.40	0.91	0.45	0.11	0.11	0.82
Mean.	-7.41	-6.73	-3.56	1.10	7.01	11.33	13.39	13.58	8.43	3.61	-0 80	-3.75	

LXVIII.

Russia. — Helsingfors. Lat. 60° 10′ N. Long. 24° 57′ E. Gr. — Dove.

	Degrees of Reaumur.												
Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	0.06	0.47	1.28	1.61	1.61	2.01	1.65	1.36	0.83	0.37	0.18	0.20	0.9
1	0.13	0.49	1.48	1.87	1.94	2.44	1.90	1.68	1.03	0.45	0.15	0.21	1.1
2	0.16	0.52	1.64	2.07	2.21	2.84	2.17	1.98	1.21	0.55	0.18	0.18	1.3
3	0.23	0.67	1.84	2.21	2.58	3.04	2.45	2.23	1.35	0.65	0.23	0.15	1.4
4	0.35	0.64	1.91	2.37	2.68	2.77	2.42	2.49	1.48	0.62	0.28	0.23	1.5
5	0.38	0.77	1.98	2.34	2.28	2.21	2.05	2.41	1.63	0.67	0.33	0.10	1.4
6	0.38	0.92	2.01	1.74	1.31	1.31	1.33	1.81	1.63	0.75	0.33	0.03	1.1
7	0.41	0.99	1.78	1.14	0.58	0.51	0.55	1.11	1.28	0.73	0.36	0.01	0.7
8	0.43	0.99	1.04	0.17	-0.19	-0.36	-0.10	0.26	0.58	0.57	0.35	0.00	0.8
9	0.38	0.55	0.04	-9.73	-0.86	-0.83	-0.73	-0.56	-0.09	0.33	0.25	0.06	-0.1
10	0.08	-0.20	-0.89	-1.49	-1.39	-1.29	-1.23	-1.12	-0.65	-0.15	0.13	-0.07	-0.6
11	-0.19	-0.93	-1.19	-1.93	-1.76	-1.83	-1.65	-1.59	-1.05	-0.47	-0.19	-0.32	-1.0
Noon.	-0.72	-1.25	-2.36	-2.26	-1.82	-1.76	-1.80	-2.02	-1.67	-0.90	-0.59	-0.42	-1.4
1	-0.79	-1.50	-2.62	-2.46	-2.12	-2.06	-2.13	-2.26	-1.82	-1.08	-0.70	-0.45	-1.6
2	-0.74	-1.60	-2.62	-2.56	-2.19	-2.36	-2.28	-2.31	-1.85	-1.10	-0.64	-0.42	-1.7
3	-0.49	-1.33	-2.46	-2.37	-2.16	-2.49	-2.13	-2.17	-1.75	-0.95	-0.50	-0.22	-1.5
-1	-0.24	-0.90	-2.12	-1.89	-1.82	-2.16	-1.75	-1.84	-1.52	-0.77	-0.29	-0.02	-1.2
5	-0.12	-0.43	-1.56	-1.59	-1.49	-1.89	-1.48	-1.64	-1.20	-0.43	-0.17	0.03	-1.0
6	-0.04	-0.21	-0.79	-1.09	-1.09	-1.53	-1.15	-1.19	-0.72	-0.25	-0.09	-0.02	-0.6
7	0.03	0.07	-0.29	-0.49	-0.86	-0.96	-0.68	-0.64	-0.27	-0.13	-0.04	0.01	-0.3
8	0.08	0.20	0.01	0.14	-0.16	-0.36	-0.10	-0.14	0.05	-0.03	0.00	0.11	-0.0
9	0.10	0.25	0.44	0.64	0.44	0.37	0.55	0.28	0.23	0.05	0.06	0.13	0.2
10	0.08	0.35	0.74	1.04	0.94	1.04	1.02	0.71	0.43	0.13	0.10	0.18	0.5
11	0.01	0.42	1.01	1.37	1.34	1.54	1.37	1.06	0.63	0.27	0.18	0.15	0.7
Mean.	-5.02	-7.43	-3.89	-0.06	5.11	10.84	12.75	14.11	9.23	4.55	1.13	-3.42	

LXIX.

Russia. — Petersburg. Lat. 59° 56' N. Long. 30° 18' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees	of	Reaumur.

					Degre	es of Re	eaumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
25 1	0.00	0.90	0.00	1.50	0.50	9.40	1.00	2.00	1.00	0.70	0.14	0.15	1 01
Morn. 1 2	$0.20 \\ 0.23$	$0.38 \\ 0.37$	0.92 1.10	1	2.59 2.84	$2.40 \\ 2.69$			l	$0.72 \\ 0.77$	1	0.17	1.21 1.38
3	0.23	í	1.10	I	3.03	2.99	I		1.97	0.82	1	0.27	I
4	0.21	0.43	1.49		3.05	2.91	1	3.01	2.20	0.88		0.35	1.62
*	0.21	0.10	1.40	2.13	0.00	2.01		0.01	1.20		0.10	0.00	1.02
5	0.26	0.50	1.59	2.17	2.79	2.60	2.37	2.92	2.25	0.95	0.20	0.35	1.58
6	0.37	0.57	1.56	1.88	2.20	1.98	1.88	2.46	2.06	0.98	0.23	0.34	1.38
7	0.51	0.56	1.36	1.35	1.27	1.13	1.15	1.70	1.62	0.92	0.23	0.33	1.01
8	0.59	0.46	0.99	0.68	0.41	0.24	0.34	0.79	1.01	0.72	0.16	0.31	0.56
9	0.53	0.23	0.17	-0.02	-0.47	-0.53	_0.40	-0.10	0.31	0.36	0.03	0.27	0.06
10	11	-0.09		-0.65		1	1	ł	l .	1		į.	-0.43
11	11	-0.43	1	-1.18	l .	1	-1.37	1	l	1	1	4	-0.86
Noon	†	-0.73		,		J	1	-2.01			-0.49	1	-1.25
2.0011.	1												
1	-0.59	-0.92	-1.68	-2.01	-2.50	-2.20	-1.98	-2.53	-2.29	-1.27	-0.54	-0.32	-1.57
2	1	-0.95	i				1				l .		1
3	11	-0.86					i	l .		1			l
4	-0.45	-0.67	-1.75	-2.50	-3.36	-3.12	-2.68	-3.39	-2.65	-1.12	-0.18	-0.44	-1.86
5	-0.27	-0.44	-1.11	-2 10	-3 11	-2.89	-2.16	-3.02	-2 19	_0.88	-0.02	-0.36	-1.61
6	1	-0.22					1			l .	1	-0.26	
7		-0.02					l .	i .	l .	1	l	-0.19	i
8	-0.13			-0.10			ř.		-0.01	l .	l	-0.14	ı
9	-0.14	0.24	0.14	0.54	0.69	0.61	0.49	0.66	0.53	0.11	1	-0.12	0.33
10	-0.09	0.32	0.40	0.96	1.47	1.30	1.07	1.24	0.87	0.33	l .	-0.09	0.66
11	0.02	0.37	0.59	1.20	2.00	1.77	1.45	1.58	1.05	0.50	l .	-0.02	0.89
Midn	0.12	0.38	0.75	1.35	2.33	2.11	1.73	1.81	1.20	0.63	0.16	0.07	1.05
6. 6	0.11	0.18	0.26	0.14	-0.12	-0.14	-0.03	0.10	0.28	0.18	0.17	0.04	0.10
7. 7	0.20	0.27	0.38	1	-0.05			0.23	0.45	0.28	0.20	0.07	0.18
8. 8	0.23	0.29	0.40	0.29	- 1	-0.04	0.03	0.29	0.50	0.30	0.18	0.09	0.22
9. 9	0.20	0.24	0.31	0.26	0.11	0.04	0.04	0.28	0.42	0.24	0.11	0.08	0.19
10.10	0.12	0.12	0.13	0.15	0.16	0.11	0.05	0.19	0.22	0.12	0.01	0.05	0.12
7. 2. 9		-0.05		-0.15				-0.22		-0.11		-0.08	
6. 2. 8		-0.08	1	-0.18	1			-0.25					
6. 2.10 6. 2. 6	-0.13	-0.02 -0.20	0.02	$0.17 \\ -0.69$	0.25	0.22	0.21	0.23			-0.03 -0.05		0.08
0. 2. 0	-0.15	-0.20	-0.40	-0.03	-1.05	0.57	-0.75	-0.94	-0.70	-0.55	-0.05	-0.12	-0.54
7. 2	-0.09	-0.20	-0.27	-0.49	-0.82	-0.75	-0.58	-0.66	-0.53	-0.22	-0.13	-0.06	-0.40
8. 2	-0.05	-0.25	-0.45	-0.83	-1.25	-1.19	-0.99	-1.11	-0.83	-0.32	-0.17	-0.07	-0.63
8. 1		-0.23										-0.01	-0.51
7. 1	-0.04	-0.18	-0.16	-0.33	-0.62	-0.54	-0.42	-0.42	-0.34	-0.18	-0.16	0.01	-0.28
0.10.00	0.14	_0.00	0.05	0.01	1.00	_1.10	1.04	1 00	0.00		0.10	0.50	0.70
9.12.3.9	-0.14 -0.11	-0.28	-0.65 -0.06		-0.07			-1.20		1	-0.16		-0.70
7. 2.2(9)	-0.11	0.02	-0.00	0.03	-0.07	-0.07	-0.05	0.00	0.00	-0.06	0.03	-0.09	-0.04
Dail.ext.	-0.05	-0.19	-0.17	-0.17	-0.16	-0.11	-0.06	-0.19	-0.28	-0.19	-0.16	-0.07	-0.15
	4			1		1							

LXX.

Russia. — Helsingfors. Lat. 60° 10' N. Long. 24° 57' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						es of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
		0.07											
Morn. 1	0.47	0.85	1.40	2.10	2.49	3.37	3.16	2.58	1.60	1.06	0.64	0.34	1.67
2	0.79	1.25	1.86	3.18	2.82	3.78	3.48	2.96	2.09	1.45	0.99	0.68	2.11
3	0.99	1.55	2.28	2.79	2.89	3.74	3.45	3.11	2.48	1.70	1.22	0.91	2.26
4	1.13	1.71	2.52	2.77	2.62	3.22	3.02	2.92	2.61	1.74	1.26	0.97	2.21
	1.00	1.00	0.40	0.43	2.00	2.02	0.05	0.00	2.0				
5	1.06	1.66	2.49	2.41	2.06	2.32	2.25	2.39	1		1.09	Į.	1.87
6	0.86	1.43	2.16	1.76	1.30	1.24	1.23		1.84	1	0.76		1.32
7	0.58	1.07	1.57	0.92	0.49	0.20	0.17	0.64	1.06		0.38	0.31	0.67
8	0.28	0.60	0.79	0.05	-0.26	-0.65	-0.78	-0.28	0.21	0.08	0.02	0.07	0.01
9	0.01	0.10	-0.05	-0.74	-0.87	-1.26	-1.51	-1.07	-0.58	-0.38	$ _{-0.27}$	-0.10	-0.56
10	li .	-0.42)			1	1	ŧ.	I	1	1	ſ
11	II	-0.91						1	ł	1	1	1	1
Noon		-1.29											
110011	0.70	1.23	2.00	2.10	1.93	-2.10	2.04	2.40	2.04	1.50	0.76	0.40	1.09
1	-0.86	-1.54	-2.36	-2.30	-2.19	-2.36	-2.65	-2.61	-2.23	-1.42	-0.85	-0.54	-1.83
2	-0.92	-1.60											
3		-1.47											
4		-1.20)		}	1	1
- 1		1.20			2.11	22		1.20	1.02	1.00	0.00	0.40	1100
5	-0.52	-0.87	-1.56	-1.73	-1.77	-2.13	-1.85	-1.80	-1.48	-0.74	-0.48	-0.33	-1.27
6	-0.32	-0.57	-1.07	-1.25	-1.30	-1.71	-1.30	-1.24	-0.95	-0.44	-0.28	-0.18	-0.88
7	-0.19	-0.38	-0.60	-0.72	-0.78	-1.20	-0.68	-0.62	-0.42	-0.22	-0.16	-0.11	-0.51
8		-0.25			l i					l		ł	
9	-0.16	-0.18	0.10	0.26	0.29	0.07	0.61	0.52	0.31	-0.03	-0.12	-0.20	0.12
10	-0.16	-0.08	0.36	0.69	0.82	0.87	1.27	1.03	0.54	0.08	-0.10	-0.25	0.42
11	-0.06	0.12	0.63	1.13	1.40	1.75	1.95	1.54	0.79	0.29	0.02	-0.19	0.78
Midn	0.16	0.44	0.96	1.60	1.97	2.63	2.61	2.08	1.14	0.63	0.28	0.02	1.21
0.0	0.00	0.10			0.00	0.24	0.01			0.00	0.04	0.01	0.00
6. 6	0.27	0.43	0.55		-0.00			0.18	0.45	1		0.21	0.22
7. 7	0.20	0.35	0.49		-0.15				0.32	1		0.10	0.08
8.8	0.07	0.18			-0.25				0.11			-0.03	í
9. 9	-0.08							-0.28		-0.21			-0.22
10.10	-0.21	-0.25	-0.26	-0.33	-0.26	-0.39	-0.3 S	-0.33	-0.35	-0.35	-0.29	-0.24	-0.30
7. 2. 9	-0.17	-0.21	-0.26	-0.40	-0.51	-0.75	-0.63	_0.50	-0.31	-0.29	-0.21	-0.17	-0.37
6. 2. 8	1	-0.14								-0.14			
6. 2.10	-0.07				-0.42 -0.07					-0.14 -0.08			
1	1 1		0.02		1								
6. 2. 6	-0.13	-0.29	-0.45	-0.02	-0.77	-0.99	-0.91	-0.77	-0.47	-0.26	-0.15	-0.07	0.40
7. 2	-0.17	-0.27	-0.44	-0.73	-0.92	-1.16	-1.25	-1.01	-0.62	-0.42	-0.25	-0.15	-0.62
8. 2	-0.32	-0.50	1					1					
8. 1		-0.47								-0.67			
7. 1		-0.24											
						İ							
9.12.3.9										-0.75			
7. 2.2(9)	-0.17	-0.22	-0.17	-0.23	-0.31	-0.54	-0.32	-0.25	-0.16	-0.23	-0.19	-0.18	-0.25
Doil out	0.11	0.06	0.04	0.47	0.00	0.60	0.47	0.99	0.16	0.16	0.19	0.18	C.19
Dail.ext.	0.11	0.06	0.04	0.41	0.29	0.62	0.41	0.23	0.16	0.16	0.19	0.15	1.19

LXXI.

Norway. — Christiania. Lat. 59° 55′ N. Long. 10° 43′ E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					- 8	es of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.10	0.00	1.00	1.50		2.50	2 21		7.04		0.50		
Morn. 1	0.16	1	1	1.56		2.58		ì	1		1	1	1.35
2	0.21	0.94	1.30	1.88	2.85	3.15	2.53	2.23		0.82	0.50	0.21	1.54
3	0.27	1.17	1.51	2.03	3.23	3.28	2.64	2.41	2.03	0.94	0.49	0.28	1.69
4	0.32	1.49	1.67	2.12	3.21	3.05	2.62	2.60	2.07	1.06	0.55	0.30	1.84
5	0.38	1.60	1.82	2.23	2.55	2.39	2.09	2.44	2.14	1.16	0.51	0.22	1.63
6	0.47	1.54	1.69	1.81	1.63	1.31	1.37	1.98	2.10	1.16	0.60	0.11	1.31
7	0.51	1.67	1.71	1.28	0.71	0.43	0.58	1.00	1.50	1.13	0.46	0.19	0.93
8	0.54	1.42	1.29	0.56	0.07	-0.32	-0.22	0.10	0.62	0.75	0.38	0.15	0.44
9 .	0.48	1.11	0.36	-0.06	-0.52	-0.86	-0.78	-0.59	0.01	0.15	0.17	0.16	-0.03
10	0.24	1						-1.23					-0.59
11	-0.17							-1.67					
Noon	-0.67	1	1					-2.11	1				
	0.00					İ							
1								-2.35					
2								-2.50					
3								-2.50					
4	-0.62	-2.00	-1.99	-2.11	-2.53	-2.29	-2.00	-2.32	-2.35	-1.33	- 0.55 	-0.12	-1.68
5	-0.35	-1.42	-1.58	-1.80	-2.20	-2.14	-1.87	-1.97	-1.80	-0.90	-0.23	-0.06	-1.36
6	-0.12	-1.10	-1.10	-1.27	-1.82	-1.70	-1.48	-1.48	-1.21	-0.52	-0.02	-0.03	-0.99
7	-0.01	-0.60	-0.65	-0.70	-1.35	-0.98	-0.89	-0.78	-0.57	-0.24	0.11	-0.10	-0.58
8	0.12	-0.32	-0.20	-0.14	-0.44	-0.31	-0.30	-0.10	0.02	0.18	0.23	-0.13	-0.12
9	0.16	0.09	0.09	0.36	0.24	0.44	0.45	0.55	0.36	0.36	0.27	-0.05	0.28
10	0.27	0.34	0.36	0.70	0.93	1.20	1.06	1.08	0.81	0.58	0.33	l .	0.63
11	0.31	0.52	0.53	0.99	1.46	1.76	1.63	1.41	1.06	1	0.43	1	0.91
Midn	0.33	0.86	0.77	1.20	1.90	2.31	2.00	1.75	1.38	0.95	0.48		1.17
						_,,,		1110	1100	0.00		0.00	1111
6. 6	0.18	0.22	0.30	0.27	-0.10	-0.20	-0.06	0.25	0.45	0.32	0.29	0.04	0.16
7. 7	0.25	0.54	0.53		-0.32			0.11	0.47	0.45	0.29	0.05	0.18
8. 8	0.33	0.55	0.55		-0.19			0.00	0.32	0.47	0.31	0.01	0.16
9. 9	0.32	0.60	0.23		-0.14				0.19	0.26	0.22	0.06	0.12
10.10	0.26	0.31	0.01		-0.13				0.02	0.05	0.05	0.04	0.02
7. 2. 9	-0.12							-0.32		1			
6. 2. 8	-0.15		-0.15					-0.21		-0.11			
6. 2.10	-0.10	-0.11	0.03	0.06	0.03	0.04	0.08				-0.07		
6. 2. 6	-0.23	-0.59	-0.45	-0.59	-0.76	-0.67	-0.70	-0.67	-0.55	-0.34	-0.19	-0.11	-0.49
7. 2	-0.27	-0.28	-0.12	-0.52	-0.88	-0.99	-0.81	-0.75	-0.52	-0.27	-0.35	-0.08	-0.49
8. 2								-1.20					
8. 1								-1.13					
7. 1								-0.68					
9.12.3.9	_0.56	_0.60		_0 0.1	_1 95	_1 20	_1.1.1	-1.16	-1.04	-0.50	_0.39	_0.19	-0.82
7. 2.2(9)								-0.10			-0.35 -0.04		1
` '					1			0.05					
Dail.ext.	-0.25	-0.31	-0.17	-0.03	0.55	ບາວສ	0.24	0.00	-0.20	-0.20	-0.23	-0.00	-0.05

LXXII.

Lat. 63° 26' N. Long. 10° 25' E. Greenw. NORWAY. — DRONTHEIM.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	s of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
3.5	0.29	0.41	0.77	1.94	2.63	2.64	0.59	2.51	1.37	0.89	0.27	0.33	1.38
Morn. 1	0.29	0.41	0.77	$\frac{1.94}{2.09}$	$\frac{2.03}{2.97}$	$\frac{2.04}{2.76}$	$2.53 \\ 2.75$	2.68	1.48	0.89	0.27	0.31	1.50
3	0.23	0.64	1.11	$\frac{2.03}{2.19}$	3.13	2.82	$\frac{2.75}{2.77}$	2.91	1.59	0.97	0.23	0.42	1.58
4	0.20	0.71	1.27	2.32	3.03	2.82	2.65	2.77	1.55	1.07	0.28	0.34	1.58
5	0.13	0.75	1.37	2.05	2.76	2.52	2.35	2.58	1.59	0.86	0.30	0.42	1.47
6	0.11	0.82	1.42	1.67	2.30	1.96	1.86	2.13	1.49	0.71	0.14	0.43	1.25
7	0.04	0.58	1.35	1.36	1.68	1.39	1.17	1.58	1.07	0.42	0.00	0.36	0.92
s	0.08	0.23	1.17	0.94	0.83	0.61	0.40	1.02	0.57	0.06	-0.02	0.36	0.52
9	0.00	-0.08	0.41	-0.03	-0.28	-0.03	-0.14	0.22	-0.07	-0.29	-0.14	0.19	-0.02
10		1	-0.13					1	1				-0.65
11				-1.90							-0.33		
Noon		-1.08		-2.57		1		-3.21			-0.38		1
1100111 1 1													
1	-0.80	-1.22	-1.70	-2.66	-3.2 8	-3.25	-3.20	-3. 39	-2.12	-1.14	-0.44	-0.42	-1.97
2		i	-1.70			l	1	l .	1				l I
3	1		-1.54)	l .	1					
4	-0.36	-0.56	-1.37	-1.83	-2.90	-2.78	-2.41	-2.81	-1.43	-0.86	-0.16	-0.29	-1.48
5	_0.20	_0.26	-1.07	_1 20	_9 90	_9 15	_9 09	_9 99	_1 00	_0.50	_0.06	_0 22	-1.15
6		-0.30	1	-0.90		ì	l .	(ł.		l	-0.22	1 1
7	0.09	1	1 .	-0.57		-1.00		l .	-0.32		į.	-0.30	1
8	0.27	0.17				0.04	l	0.11	1	-0.02		-0.19	1 1
	"		0.2.	0.20	0.0.		0.02	0.11			****	0.20	0.02
9	0.45	0.37	0.00	0.16	0.50	0.41	0.66	0.51	0.43	0.22	0.05	-0.11	0.30
10	0.52	0.53	0.23	0.61	1.10	1.08	1.17	1.18	0.75	0.55	0.13	-0.06	0.65
11	0.47	0.50	0.43	0.90	1.61	1.63	1.48	1.67	1.02	0.74	0.11	0.02	0.88
Midn	0.45	0.49	0.63	1.27	1.92	2.07	1.88	2.13	1.28	1.14	0.19	0.02	1.12
		}											
6. 6	-0.03	0.36	0.34	0.39	0.30	0.06	0.36	0.43	0.35	0.10	0.11	0.10	0.24
7. 7	0.03	0.30	Į.	0.39	0.33			0.45	0.38	0.10	0.11	0.10	1 1
8. 8	0.07	0.20		0.37	0.33			0.43	0.30	1	0.03	0.09	0.24
9. 9	0.23	0.15	1	0.07	0.11	0.19	l	0.37	0.18		1	0.04	0.14
10.10	0.22	0.03	1		-0.10				1	1		1	0.00
7. 2. 9	-0.06	-0.07	1				5	1	1	1	-0.12		
6. 2. 8	ì	-0.05	-0.18	-0.33							-0.04		
6. 2.10	-0.02	i	1	-0.06	(1)	1	-0.01		-0.05)	1
6. 2. 6	-0.25	-0.62	-0.39	-0.56	-0.89	-1.06	-0.79	-0.83	-0.53	-0.30	-0.07	-0.09	-0.53
7. 2	-0.39	-0.20	-0.18	-0.55	_0.80	_0.07	-0.05	_0.80	-0.61	-0.34	-0.21	-0.06	-0.51
8. 2	-0.30	1	-0.13 -0.27	1		1	1	1		1	I .		1
8. 1	-0.36	1	-0.27	1	1	1		1	•		1		1
7. 1			-0.18	1	1	1		!	1	1	1	1	1
					1		1	1			İ		
9.12.3.9	-0.16		-0.62										
7. 2.2(9)	0.07	0.04	-0.09	-0.19	-0.15	-0.28	-0.15	-0.19	-0.09	-0.16	-0.02	-0.12	-0.11
D-11	-0.14	0.00	0.74	0.15	0.00	0.05	0.00	0.84	0.05	0.07	0.07	0.00	0.16
Dail. ext.	1-0.14	-0.20	y-0.14	J-0.17	-0.08	-0.25	J-0.22	J-0.24	-0.35	-0.07	-0.07	-0.02	-0.10

LXXIII.

Strait of Kara. Lat. 70° 37' N. Long. 57° 47' E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

						es of Re							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
M 1	0.27	0.38	1.66	9.59	2.26	1.86	1.97	0.00	0.00	0.00	0.00	0.55	0.00
Morn. 1			1	2.53	ł	1	1.37	0.62	0.33	0.00	ĺ		0.99
2	0.24	0.38	1.78	2.67	2.22	1.68	1.24	0.58	0.40	0.02	0.14	0.42	0.98
3	0.22	0.40	1.86	2.66	2.06	1.41	1.03	0.53	0.49	0.02	0.14	0.26	0.92
4	0.23	0.42	1.88	2.44	1.82	1.12	0.79	0.47	0.58	0.06	0.15	0.11	0.84
5	0.25	0.42	1.80	1.98	1.48	0.82	0.54	0.38	0.61	0.17	0.22	-0.00	0.72
6	0.27	0.33	1.55	1.30	1.01	0.49	0.25	0.26	0.58	0.29	0.36	-0.15	0.55
7	0.29	0.16	1.10	0.52	0.40	0.10	-0.05	0.10	0.42	0.35	0.52	-0.29	0.30
8	0.30	0.08	0.42	-0.27	-0.30	-0.33	-0.35	-0.07	0.27	0.32		-0.42	0.01
9	0.26	0.30	-0.43	-0.98	-1.01	-0.78	-0.66	-0.23	0.01	0.18	0.66	-0.54	-0.32
10			-1.32	ı	1				1	0.02		-0.61	
11	1	i	-2.07	l		1			1	Į.		-0.62	
Noon	1		-2.56					1	ı	1		-0.52	
1,001	0.12		1										
1	-0.31	-0.70	-2.70	-2.67	-2.26	-1.62	-1.03	-0.63	-0.81	-0.43	-0.13	-0.44	-1.14
2	-0.49	-0.64	-2.52	-2.81	-2.11	-1.54	-1.00	-0.71	-0.78	-0.36	-0.25	-0.31	-1.13
3	-0.60	-0.53	-2.10	-2.75	-1.88	-1.40	-0.95	-0.76	-0.66	-0.23	-0.30	-0.21	-1.03
4	-0.63	-0.38	-1.54	-2.46	-1.61	-1.25	-0.90	-0.69	-0.49	-0.10	-0.32	-0.11	-0.87
5	-0.58	-0.21	-0.98	-1.91	-1.30	-1.05	-0.78	-0.59	-0.30	0.02	-0.35	-0.04	-0.67
6	-0.46	-0.02	-0.47						-0.13	0.07	-0.41	0.06	-0.43
7	-0.26		-0.04	1				1	0.06		-0.48	1	-0.15
8	-0.06	0.32	0.34	0.42	0.20	0.18	0.11	0.22	0.11		-0.52	0.33	0.14
						0 =0	\ \ \						
9	0.11	0.12	0.67	1.08	0.83	0.78	0.54	0.46	0.17		-0.49		0.43
10	0.22	0.46	0.98	1.59	1.42	1.31	0.94	0.62	0.20		-0.38	0.61	0.67
11	0.28	0.44	1.25	1.98	1.88	1.71	1.23	0.68	0.23		-0.20	0.66	0.85
Midn	0.29	0.40	1.48	2.29	2.16	1.90	1.38	0.66	0.27	0.01	-0.03	0.64	0.95
6. 6	0.10	0.16	0.54	0.06	0.06	-0.14	-0.17	-0.06	0.23	0.18	-0.03	-0.05	0.06
7. 7	0.02	0.15	0.53	0.08	-0.00	-0.13	-0.17	0.01	0.24	0.22	0.02	-0.06	0.08
8. 8	0.12	0.12	0.38	0.08	-0.05	-0.08	-0.12	0.08	0.19	0.20	0.06	-0.05	0.08
9. 9	0.19	0.06	0.12	0.05	-0.09	-0.00	-0.06	0.12	0.09	0.12	0.09	-0.03	0.05
10.10	1	-0.02	-0.17		-0.11	0.06		1	-0.04	0.04	0.09	-0.00	0.02
7. 2. 9	-0.03	-0.09	-0.25	-0.40	_0.20	-0.22	-0.17	-0.05	-0.06	0.02	-0.07	-0.04	-0.1 3
6. 2. 8			-0.21										
6. 2.10	-0.00		-0.00		0.11	0.09				-0.00			0.03
6. 2. 6		-0.11		-0.90									0.34
	1												
7. 2	-0.10	-0.24	-0.71	-1.15	-0.86	-0.72	-0.53	-0.31	-0.18	-0.01		-0.30	
8. 2			-1.05									-0.37	
8. 1	-0.01	-0.39	-1.14	-1.47	-1.28	-0.98	-0.69	-0.35	-0.27	-0.06		-0.43	
7. 1	-0.01	-0.27	-0.80	-1.08	-0.93	-0.76	-0.54	-0.27	-0.20	-0.01	0.20	-0.37	-0.42
9.12.3.9	-0.09	-0.29	-1.11	-1 27	-1.08	-0.76	-0.53	-0.27	-0.30	-0.09	-0.01	-0.20	0.50
7. 2.2(9)	0.01		-0.02			0.03			-0.01		-0.18	0.09	0.01
` '	0.1-					0.14	0.15	_0.04	_0.10	_0.04	0.0~	0.00	^0
Dail. ext.	J-0.17	-0.12	-0.41	-0.07	-0.01	0.14	0.17	-0.04	-0.10	-0.01	0.07	0.02	-0.08

LXXIV.

NOVAIA ZEMLIA. — MATOSCHKIN SCHAR. Lat. 73° — N. Long. 57° 20' E. Gr. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

					Degree	es of Re	aumur.						
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	0.00	0.10	0.40	1.00	0.40	1.70	1.18	0.73	1.00	-0.49	0.14	0.11	0.70
Morn. 1	-0.22 -0.30		0.46 0.70	1.63 1.34	2.42 2.28	1.70	1.18	1	1	-0.49 -0.47	i	i .	0.70
3	-0.31	0.03	0.70	1.15	1.89	1.26	1.11	0.80	1	-0.22		1	0.61
4	-0.26	1	1.02	1.09	1.41	0.93	0.94		0.46	i	-0.00		0.54
-													
5	1	-0.09	0.99	0.81	0.85	0.61	0.73	1	0.46	0.20	0.10		0.45
6		-0.09	0.86	0.63	0.26	0.30	0.47	1	0.56	0.26	0.20	1	0.34
7	1	-0.07	0.62	0.09	-0.38	1	0.18	Į.	0.58	0.18	0.26		0.16
8	0.10	-0.05	0.34	-0.50	-1.03	-0.3 S	-0.13	-0.30	0.38	0.06	0.26	0.46	-0.07
9	0.10	-0.05	0.02	-1.14	-1.65	-0.78	-0.46	-0.58	-0.00	-0.06	0.24	0.43	-0.33
10	!	-0.06		-1.78		l	i		ı	1	0.18	1	-0.61
11	0.05	-0.10		-2.02	1	ŀ	-0.97	1	-1.24		0.15	I.	-0.79
Noon	0.05	-0.13	-0.78	-2.09	-2.67	-1.58	-1.08	-0.93	-1.46	-0.12	0.11	0.18	-0.88
1	1	-0.14		1	1				I	[0.08	i .	-0.85
2		-0.14										1	-0.74
3 4		-0.11 -0.07						-0.32 -0.32				-0.11 -0.20	
4	0.10	-0.07	-0.71	-0.50	-1.50	0.70	-0.00	-0.52	-0.07	-0.02	-0.10	-0.20	-0.41
5	0.10	-0.03	-0.50	-0.54	-0.72	-0.57	-0.54	-0.14	-0.02	0.10	-0.18	-0.26	-0.28
6	0.10	0.02	-0.30	-0.26	-0.14	-0.38	-0.43	-0.00	-0.17	0.26	-0.20	-0.36	-0.16
7	0.10	0.06	-0.16	0.30	0.46	-0.16	-0.30	0.12	-0.35	0.40	-0.18	-0.43	-0.01
8	0.12	0.10	-0.09	0.70	1.04	0.15	-0.11	0.21	-0.36	0.46	-0.14	-0.48	0.13
9	0.12	0.15	-0.06	7.04	1.50	0.56	0.14	0.30	-0.12	0.20	0.10	0.40	0.91
10	0.12		-0.06	1.24 1.50	$\frac{1.59}{2.06}$	1.02	0.14	ļ	0.33		-0.10 -0.08		$0.31 \\ 0.47$
11	-0.00	0.13	0.09	1.75	2.40	1.42	0.78	0.50	0.33		-0.08	l .	0.47
Midn	-0.11	0.20	0.23	1.73	2.55	1.66	1.03	0.62	1.06		-0.11	l .	0.69
Direction	0.11		0.20	1	2.00			0.02	2.00				0.00
6. 6	0.04	0.04	0.28	0.19		-0.04	0.02	0.15	0.20	0.26	0.00	0.03	0.10
7. 7	0.08	0.01	0.23	0.20			-0.06		0.12	0.29	0.04	0.01	0.08
8.8	0.11	0.03	0.13	0.10	1	-0.12			0.01	0.26		-0.01	0.03
9. 9 10.10	0.11		-0.02 -0.15	0.05 -0.14		-0.11	-0.16 -0.15		-0.06	$0.15 \\ -0.01$	0.07	-0.03 -0.04	-0.01 -0.07
10.10	0.00	0.07	-0.15	-0.14	-0.00	0.07	-0.13	-0.20	-0.13	-0.01	0.05	-0.04	-0.01
7. 2. 9	0.09	-0.02	-0.13	-0.10	-0.36	-0.26	-0.21	-0.13	-0.14	0.15	0.06	-0.02	-0.09
6. 2. 8	0.06	-0.04	-0.06	-0.10	-0.33	-0.29	-0.20	-0.06	-0.23	0.21	0.03	-0.03	-0.09
6. 2.10		-0.01		0.17				-0.00		0.12		-0.02	0.03
6. 2. 6	0.05	-0.07	-0.13	-0.42	-0.72	-0.47	-0.31	-0.13	-0.17	0.14	0.01	0.01	-0.18
7. 2	0.06	-0.11	_0.1~	_0 ~~	_1 29	_0.67	-0 30	_0.25	_0.16	0.05	0.14	0.22	-0.29
8. 2		-0.11 -0.10								-0.03	0.14	0.22	-0.29 -0.40
8. 1		-0.10								-0.02	0.17	0.28	-0.46
7. 1	1	-0.11						1 :		0.04	0.17		-0.34
9.12.3.9	0.09		-0.43	-0.81		-0.71		-0.43	i i	0.03		-0.00	-0.37
7. 2.2(9)	0.10	0.02	-0.12	0.24	0.13	-0.06	-0.13	-0.02	-0.14	0.20	0.02	-0.14	0.01
Dail.ext.	-0.10	0.04	0.03	-0.17	-0.06	0.06	0.06	-0.07	-0.19	-0.02	0.03	-0.02	-0.09
Dan CAL	0.10	0.04	0.00	-0.17	0.00	0.00	0.00	0.07	0.13	0.04	0.00	0.02	0.00

LXXV.

Norway. — Bossekop. Lat. 69° 58' N. Long. 22° E. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

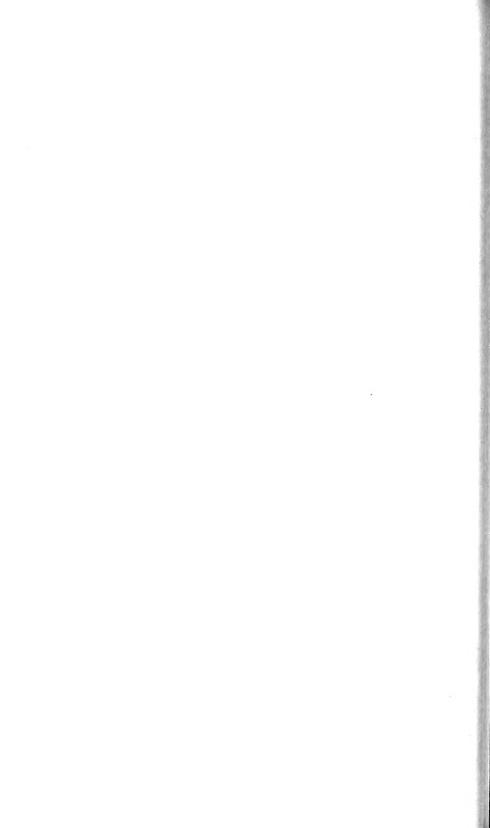
Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.26	0.36	1.37		1.20	0.66	0.04	0.35	0.04
4	-0.11	0.30	1.78		1.01	0.53	-0.03	0.42	0.10
6	0.00	0.50	1.90		1.22	0.73	0.04	0.28	0.08
8	0.09	0.26	1.18	0.36	0.62	0.41	0.07	0.10	0.02
10	-0.13	-0.19	-1.09	-0.85	-1.01	-0.29	-0.15	-0.14	-0.19
Noon.	0.18 0.20	-0.79 -1.02	$\begin{vmatrix} -2.39 \\ -2.85 \end{vmatrix}$	-1.29 -1.22	-1.66 -1.69	-1.05 -1.02	-0.13 -0.09	-0.09 -0.34	-0.03 -0.10
4	0.30	-0.11	-2.38	-0.82	-1.54	-0.50	0.09	-0.38	0.06
6	0.18	0.06	-0.57	-0.10	-0.27	-0.17	0.18	-0.23	0.09
8	0.12	0.16	0.46	0.70	0.39	0.09	0.14	-0.26	0.02
10	-0.34	0.21	1.19	1.44	0.79	0.13	-0.03	0.14	-0.10
12	-0.27	0.22	1.39	1.83	0.89	0.49	-0.13	0.17	-0.10
Mean.	-7.67	-6.39	-7.55	-0.77	5.91	-1.62	-6.55	-5.66	-7.66

LXXV'.

NORWAY. — BOSSEKOP. Lat. 69° 58′ N. Long. 22° E. Greenw. Centigrade Degrees.

Hour.	Jan.	Feb.	March.	April.	Sept.	Oct.	Nov.	Dec.	80 Days without Sun.
A.M. 2	-0.32	0.45	1.71		1.50	0.82	0.05	0.44	0.05
4	-0.14	0.37	2.22		1.26	0.66	-0.04	0.52	0.12
6	0.00	0.62	2.37		1.52	0.91	0.05	0.35	0.10
8	0.11	0.32	1.47	0.45	0.77	0.51	0.09	0.12	0.02
10	-0.16	-0.24	-1.36	-1.06	-1.26	-0.36	-0.19	-0.17	-0.24
Noon.	0.22	-0.99	-2.98	-1.62	-2.07	-1.31	-0.16	-0.11	-0.04
2	0.25	-1.27	-3.56	-1.52	-2.11	-1.27	-0.11	-0.42	-0.12
4	0.37	-0.14	-2.97	-1.02	-1.92	-0.62	0.11	-0.47	0.07
6	0.22	0.07	-0.71	-0.12	-0.34	-0.21	0.22	-0.29	0.11
8	0.15	0.20	0.57	0.87	0.49	0.11	0.17	-0.32	0.02
10	-0.42	0.26	1.48	1.80	0.99	0.16	-0.01	0.17	-0.12
12	-0.34	0.27	1.73	2.29	1.11	0.61	-0.16	0.21	-0.12
Mean.	-9.59	-7.99	-9.44	-0.96	7.39	-2.02	-8.19	-7.07	-9.57



HOURLY CORRECTIONS

FOR

PERIODIC VARIATIONS.

AFRICA. — AUSTRALIA.



LXXVI.

Africa. — St. Helena. Lat. 15° 55' S. Long. 5° 43' W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oet.	Nov.	Dec.	Year.
Midn.	0.76	0.70	0.63	0.58	0.52	0.43	0.48	0.43	0.52	0.62	0.71	0.73	0.59
1	0.85	0.76	0.71	0.66	0.61	0.48	0.53	0.48	0.56	0.71	0.78	0.81	0.66
2	0.93	0.84	0.77	0.70	0.66	0.54	0.56	0.53	0.62	0.78	0.86	0.90	0.72
3	1.03	0.92	0.86	0.76	0.73	0.59	0.62	0.63	0.69	0.86	0.95	0.98	0.80
4	1.06	1.00	0.92	0.81	0.80	0.65	0.66	0.66	0.76	0.91	0.99	1.02	0.85
5	1.11	1.04	0.93	0.86	0.83	0.67	0.69	0.73	0.79	0.94	1.02	1.08	0.89
6	1.15	1.07	0.98	0.93	0.83	0.68	0.72	0.74	0.83	0.99	1.07	1.09	0.92
7	1.16	1.08	0.97	0.94	0.89	0.71	0.75	0.79	0.81	0.96	1.03	1.06	0.93
8	0.95	0.99	0.78	0.85	0.88	0.69	0.72	0.72	0.72	0.77	0.80	0.98	0.82
9	0.53	0.63	0.52	0.49	0.46	0.42	0.41	0.43	0.42	0.38	0.40	0.48	0.46
10	-0.05	0.06	-0.07	-0.04	-0.08	-0.04	-0.04	-0.02	-0.05	-0.17	-0.16	-0.09	-0.06
11	-0.62	-0.55	-0.49	-0.51	-0.47	-0.40	-0.40	-0.40	-0.55	-0.66	-0.67	-0.56	-0.52
Noon.	-1.14	-1.06	-0.95	-1.00	-0.96	-0.73	-0.76	-0.80	-0.92	-1.11	-1.12	-1.08	-0.97
1	-1.64	-1.46	-1.28	-1.31	-1.20	-1.04	-1.06	-1.12	-1.25	-1.45	-1.60	-1.52	-1.33
2	-1.81	-1.67	-1.48	-1.46	-1.32	-1.20	-1.26	-1.25	-1.42	-1.67	-1.80	-1.80	-1.51
3	-1.76	-1.78	-1.62	-1.50	-1.35	-1.18	-1.24	-1.31	-1.38	-1.64	-1.84	-1.82	-1.54
4	-1.69	-1.66	-1.54	-1.35	-1.24	-1.03	-1.12	-1.13	-1.20	-1.37	-1.64	-1.76	-1.39
5	-1.48	-1.38	-1.27	-1.06	-0.94	-0.78	-0.84	-0.86	-0.91	-0.99	-1.24	-1.38	-1.09
6	-0.92	-0.91	-0.S3	-0.61	-0.47	-0.40	-0.44	-0.42	-0.43	-0.48	-0.66	-0.82	-0.62
7	-0.27	-0.33	-0.28	-0.11	-0.23	-0.03	-0.07	-0.03	0.01	0.02	-0.04	-0.18	-0.13
8	0.26	0.21	0.18	0.20	-0.12	0.17	0.13	0.15	0.23	0.29	0.32	0.30	0.19
9	0.47	0.44	0.34	0.34	0.14	0.26	0.23	0.25	0.32	0.26	0.48	0.48	0.33
10	0.60	0.55	0.48	0.44	0.41	0.32	0.33	0.32	0.38	0.49	0.56	0.58	0.46
11	0.69	0.64	0.55	0.51	0.45	0.39	0.38	0.38	0.46	0.55	0.64	0.67	0.53
Mean.	14.21	15.04	15.22	14.93	13.80	12.48	11.55	11.19	11.14	11.66	12.37	13.23	

LXXVII.

 $\textbf{Africa.--Cape of Good Hope.} \quad \textit{Lat. } \textbf{33° 56' S.} \quad \textit{Long. } \textbf{19° 39' E. } \textit{Gr.--Dove.}$

Hour	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	1.69	1.50	1.51	1.37	1.00	0.88	1.04	0.85	1.07	1.45	1.62	1.85	1.32
1	2.80	1.64	1.64	1.49	1.07	1.01	1.20	1.03	1.25	1.62	1.79	2.01	1.55
2	1.89	1.74	1.81	1.61	1.14	1.09	1.33	1.14	1.39	1.72	1.98	2.16	1.58
3	2.01	1.92	1.92	1.70	1.24	1.16	1.43	1.23	1.54	1.82	2.12	2.30	1.70
4	2.10	2.00	2.05	1.88	1.34	1.30	1.53	1.37	1.63	1.92	2.21	2.42	1.81
5	1.96	2.13	2.13	1.93	1.46	1.42	1.59	1.53	1.59	1.93	1.92	2.01	1.80
6	1.06	1.53	1.97	1.98	1.59	1.48	1.73	1.55	1.62	1.26	0.85	0.86	1.46
7	0.15	0.70	1.21	1.39	1.41	1.47	1.57	1.22	0.81	0.39	-0.02	-0.20	0.84
8	-0.53	-0.01	0.16	0.36	0.53	0.86	0.77	0.64	-0.06	-0.46	-0.67	-0.81	0.06
9	-1.10	-0.80	-0.76	-0.68	-0.39	-0.12	-0.21	-0.42	-0.82	-1.24	-1.25	-1.36	-0.77
10												-1.90	-1.47
11	-2.23	-2.31	-2.37	-2.10	-1.64	-1.46	-1.72	-1.63	-1.85	-2.25	-2.24	-2.25	-2.00

LXXVII.

AFRICA. - CAPE OF GOOD HOPE, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. — Dove.

Degrees of Reaumur.

Hour.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Noon.	-2.48	-2.72	-2.66	-2.56	-2.09	-1.92	-2.11	-1.88	-2.15	-2.45	-2.46	-2.52	-2.33
1								l				-2.61	i
2	-2.42	-2.54	-2.86	-2.79	-2.14	-2.06	-2.33	-1.97	-2.18	-2.44	-2.30	-2.44	-2.37
3	-2.16	-2.20	-2.51	-2.42	-1.84	-1.86	-2.13	-1.77	-1.82	-2.0S	-2.01	-2.16	-2.08
4	-1.75	-1.70	-1.78	-1.75	-1.28	-1.28	-1.49	-1.32	-1.28	-1.52	-1.66	-1.90	-1.56
5	-1.21	-1.09	-1.03	-0.71	-0.61	-0.64	-0.76	-0.57	-0.56	-0.71	-1.05	-1.28	-0.sa
6	-0.16	-0.13	-0.10	-0.03	-0.21	-0.29	-0.33	-0.17	0.00	0.20	-0.01	-0.15	-0.13
7	0.65	0.54	0.35	0.22	0.09	-0.05	-0.03	0 12	0.30	0.57	0.60	0.63	0.3
8	0.95	0.79	0.61	0.48	0.36	0.19	0.26	0.32	0.51	0.86	0.92	0.96	0.60
9	1.14	1.00	0.92	0.73	0.54	0.40	0.48	0.46	0.69	1.09	1.10	1.20	0.8
10	1.30	1.14	1.14	1.00	0.78	0.61	0.69	0.65	0.97	1.26	1.31	1.46	1.0
11	1.55	1.32	1.29	1.22	0.95	0.81	0.91	0.76	1.02	1.44	1.48	1.67	1.20
Mean	15.81	15.96	15.00	12.61	11.99	0.01	0.06	10.06	11.01	10 (9	19.51	14.00	

LXXVIII.

Australia. — Hobarton. Lat. 42° 53′ S. Long. 147° 21′ E. Gr. — Dove.

					176	grees of	Reaum	ur.					
Hour.	Jan	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
Midn.	2.31	1.95	1.78	1.31	0.88	0.66	0.72	1.10	1.51	1.99	2.44	2.45	1.59
1	2.59	2.17	1.99	1.41	1.03	0.76	0.86	1.36	1.71	2.19	2.67	2.76	1.79
2	2.89	2.32	2.19	1.62	1.11	0.88	1.01	1.43	1.93	2.45	2.77	2.95	1.96
3	3.09	2.53	2.39	1.75	1.23	0.97	1.16	1.58	2.06	2.68	2.98	3.24	2.1
4	3.20	2.68	2.49	1.85	1.31	1.15	1.28	1.69	2.20	2.80	3.11	3.38	2.20
5	3.33	2.82	2.54	1.99	1.44	1.15	1.40	1.82	2.32	2.85	2.99	3.13	2.3
6	2.62	2.59	2.64	2.11	1.55	1.29	1.50	1.91	2.34	2.60	2.24	2.24	2.1
7	1.48	1.75	2.10	2.00	1.60	1.37	1.50	1.90	1.84	1.61	1.16	1.03	1.6
8	0.27	0.68	1.08	1.30	1.27	1.26	1.31	1.32	0.93	0.41	0.01	-0.24	0.80
9	-0.88	-0.56	-0.17	0.24	0.45	0.60	0.60	0.44	-0.21	-0.70	-1.13	-1.27	-0.23
10	-1.92	-1.61	-1.28	-0.85	-0.46	-0.18	-0.21	-0.52	-1.21	-1.68	-2.10	-2.16	-1.18
11	-2.75	-2.31	-2.24	-1.78	-1.29	-0.96	-1.01	-1.53	-2.09	-2.54	-2.89	-2.85	-2.0
Noon.	-3.51	-3.22	-3.03	-2.58	-2.00	-1.67	-1.67	-2.28	-2.70	-3.10	-3.43	-3.36	-2.7
1	-3.82	-3.52	-3.48	-2.95	-2.42	-2.08	-2.17	-2.73	-3.14	-3.48	-3.72	-3.67	-3.1
2	-3.91	-3.54	-3.63	-3.11	-2.53	-2.22	-2.38	-2.91	-3.25	-3.48	-3.67	-3.56	-3.13
3	-3.60	-3.36	-3.43	-2.87	-2.32	-2.02	-2.23	-2.71	-3.10	-3.32	-3.33	-3.45	-2.9
4	-3.20	-2.94	-2.92	-2.23	-1.69	-1.43	-1.73	-2.20	-2.53	-3.04	-3.12	-3.12	-2.5
5	-2.57	-2.22	-2.02	-1.35	-0.92	-0.73	-1.01	-1.37	-1.59	-2.02	-2.30	-2.56	-1.7
6	-1.38	-1.04	-0 84	-0.56	-0.36	-0.25	-0.48	-0.64	-0.65	-0.80	-1.01	-1.38	-1.7
7	-0.13	-0.20	-0.04	-0.05	0.01	0.00	0.12	-0.13	0.01	0.05	0.20	-0.09	-0.0
8	0.82	0.68	0.45	0.32	0.27	0.24	0.14	0.21	0.46	0.55	0.90	0.89	0.4
9	1.31	1.13	0.82	0.57	0.42	0.24	0.34	0.57	0.79	1.00	1.41	1.51	0.8
10	1.71	1.47	1.19	0.84	0.62	0.40	0.50	0.79	1.08	1.34	1.75	1.91	1.13
11	2.05	1.77	1.47	1.06	0.77	0.54	0.64	0.93	1.31	1.63	2.05	2.25	1.3
Mean.	13.38	13.96	11.96	9.41	7.69	5.93	5.21	6.24	7.97	9.39	11.38	12.95	

CORRECTIONS FOR TEMPERATURE.

MONTHLY AND YEARLY

CORRECTIONS FOR NON-PERIODIC VARIATIONS,

OR

TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS

TO THE MEANS DERIVED FROM A SERIES OF YEARS.



TABLES

FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS TO THE
MEANS DERIVED FROM A SERIES OF YEARS.

Observation shows that the monthly and annual mean temperature of a place somewhat varies from year to year. No law, however, has been as yet discovered as to the course of these oscillations. It follows that the means derived from observations carried on during a single year are but approximations to the true means. These last must be obtained from observations made for a series of years, during which these irregular variations become insensible by compensating each other; and it is obvious that their accuracy increases with the number of years which compose the series.

Professor Dove, having proved by his researches that these abnormal temperatures above and below the average of a whole month, or of a year, are apt to be felt simultaneously on extensive tracts of country, concluded that the means of a single year could be made available for obtaining the true means of the place, by being corrected for the non-periodic variations by means of normal stations in the same meteorological region, in which those elements had been more accurately determined by the observations of a long series of years. Comparing, namely, the means of a given year with the means derived from the whole series, we find a difference in + or -, which, applied, with reverse signs, to the means of the same year in the neighboring station to be corrected, will reduce, with a good degree of probability, the means of that particular year to the means which would have been obtained from a long series of years similar to that of the normal station.

The following tables, LXXIX. to XCVII., have been selected from those given by Dove in his five papers on the non-periodic variations of the atmospheric temperature, to be found in the *Memoirs of the Academy of Sciences of Berlin* for the years 1838, 1839, 1842, 1848, and 1853, to which we must refer for further details. They furnish normal stations for various latitudes; the columns contain the corrections for every month, viz. the differences, with *reverse* signs, between the monthly means in the year indicated in the first and last columns, and the means derived from the whole series, which are contained in the line at the bottom.

E

LXXIX.

Region of the Monsoons. — Madras.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

-						5	Reaum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	c	0	0	0	0	0	
1796	0.00	0.24	0.00	0.36	-0.10	-1.48	-1.16	1	-0.31	-0.28	1	-0.51	1796
1797			0.66	0.53	0.39	0.56	0.09	0.85	1	-0.33			1797
1798	-0.13	1.12	0.40	• •		0.39	0.53	-0.31	0.27	0.56)	0.20	1798
1799	-0.13	-0.08	0.62	0.36	0.26	-0.06	-1.20	0.00	1	0.38		0.25	1799
1800	0.40	0.41	0.57	1.20	-0.23	-0.50	-1.02	-0.40	-0.58	0.20	0.47	-0.60	1800
1801	0.44	0.01	1.77	• •		-0.59	-0.67	0.63	1	-0.02	1	0.25	1801
1802	0.11	0.86	1.77	1.02	-0.36	0.65	0.58	-0.04	1.60	0.43		-0.28	1802
1803	0.22	0.24	0.80	0.53	-0.32	0.08	0.18	0.80	t	0.38		0.65	1803
1804	1.64	1.48	0.75	1.38	0.70	0.70	1.24	0.00	1	0.38	0.91	0.29	1804
1805	0.27	0.41	0.66	-0.36	0.61	0.52	-0.76	-0.22	-0.27	-0.33	0.69	0.65	1805
1806	0.00	-0.39	-0.09	0.09	-0.41	-1.61	0.00	-0.13	1.07	0.47	0.96	0.12	1806
1807	0.22	-1.54	-3.20	-5.47	-1.79	0.48	1.20	-0.17	-0.09	-0.64	-0.20	0.78	1807
1813	0.80	0.37	0.13	0.96	1.12	-0.32	0.44	-0.22	1	0.25	1	1	1813
1814	-0.36	-0.39	-0.58	0.04	-2.99	1.10	1.38	0.29	1	1	-0.20	1	1814
1815	-0.98	0.32	-0.67	2.00	1.55	-1.39	-0.98	0.27	0.31	-0.73	-0.91	-0.82	1815
1816	-1.09	-1.76	-1.56	-0.93	0.44	0.39	-0.44	-0.71	-0.67	-0.20	0.33	-0.51	1816
1817	-0.58	-0.70	-0.67	-0.62	0.12	-0.19	0.67	0.29	-0.71	-0.55	-0.96	0.52	1817
1818	0.22	0.32	-0.80	-0.04	1.41	0.65	-1.33	-2.00	-0.18	-0.55	-0.56	-0.37	1818
1819	-1.78	-1.28	-0.76	-0.13	0.48	0.88	0.44	0.98	-0.31	0.03	0.78	0.16	1819
1820	-0.67	-0.30	-0.85	0.58	-1.16	-0.32	0.18	0.23	-0.09	0.47	0.69	0.47	1820
1821	1.02	0.64	1.06	-1.51	0.26	0.08	0.58	0.94	-0.04	-0.02	0.20	0.20	1821
Means.	19.19	20.07	21.30	22.41	24.41	24.96	23.84	23.43	23.03	22.16	20.74	19.48	Means.
1822	-0.36	0.37	0.41	-0.28	0.07	-0.95	-0.76	0.72	-0.37	-0.70	-0.35	-0.19	1822
1823	0.31	0.37	-0.21	0.30	0.15	0.29	0.22	0.17	-0.60	0.72	0.27	0.97	1823
1824	0.71	0.59	0.27	0.52	-0.02	0.60	1.55	0.88	1.36	-0.93	0.14	0.26	1824
1825	-0.09	0.37	-0.21	0.12	0.24	-0.29	0.04	-0.36	0.03	0.32	0.59	-0.59	1825
1826	0.80	0.24	0.45	0.92	0.78	-1.17	0.04	-0.36	0.25	0.81	0.36	0.30	1826
1827	-0.09	-0.29	-0.17	0.17	-1.27	-0.46	-0.01	-0.09	-0.15	-0.13	0.54	0.08	1827
1828	1.07	0.51	-0.57	-0.59	-0.42		-0.23	0.04	1	-0.17	0.81	0.21	1828
1829	0.09	-0.69	-0.35	0.08	-0.11	0.16	-0.89	-0.01	0.16	0.54	0.23	0.12	1829
1830	-0.27	-0.74	0.01	-0.32	-2.73	-0.15	-0.36	-0.23	0.25	1.12	0.68	0.53	1830
1831	0.31	1.49	1.66	0.48	1.89	1.36	0.04	0.67	0.70	0.41	0.41	0.53	1831
1832	-0.49	-0.29	1.26	1.73	2.51	2.65	1.64	2.40	0.34	-0.25	0.46		1832
1833	0.36	0.91	-0.19	0.97	0.83	0.83	1.33	0.40	0.16	0.41	0.19	1.06	1833
1834	0.18	0.60	0.55	-0.58	1.31	0.12	-0.98	-0.18	-0.15	-0.03	0.01	-0.01	1834
1835	-0.66	-0.73	-0.57	-1.07	-0.24	-0.86	-0.67	-0.45	-0.46	-0.74	-0.48	-0.94	1835
1836	-0.75	-0.73	-1.41	-0.72	0.60	0.12	-0.58	-1.29	-0.24	0.15	-0.92	-1.03	1836
1837	-0.31	-0.02	0.06	-0.63	-1.17	-0.41	-0.40	-0.05	0.03	-0.34		1	1837
1838	-1.24	-0.69		0.04	-0.33	-0.24	0.75	-0.05	0.65	ı	-0.57	1 1	1838
1839		-0.11		-0.45	-0.15	-0.41	-0.49	-0.93			-0.83	0.71	1839
1840		-0.42		0.17	0.29	0.25	-0.45	0.27	i		-1.14	-0.32	1840
1841		-0.16		-0.58	-1.17	l .	0.35	-0.71	!	1	-0.34	1	1841
1842		-0.51	1	-0.49	0.47	0.07	0.00	0.09		-0.30		1 (1842
1843	0.23	-0.02	-0.03	0.22	-1. 53	-1.04	-0.22	0.44	0.16	-0. 52	0.23	-0.32	1843
Means.	20.53	21.31	22.92	24.27	25.62	25.35	24.31	23.73	23.70	22.92	21.32	20.67	Means.

LXXX.

SICILY. — PALERMO.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						grees of							
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1801	0	0	0	0	0	0	0 70	0 07	0 07	° -0.36	0	0.00	1791
1791	1 10	0.51	0.00	0.10	-0.44						1.73	1 11	1791
1792	1.18	0.51	0.09		-0.48		-1.01				-0.83		1792
1793	1	-0.38					-1.28	-1.14	0.86		-0.25 -0.29	0.44	1793
1794	1 1	-0.69	-0.51	0.59					-0.14			-0.47	
1795	-1.62	1.27	0.78	-0.10	0.12	-0.59	-1.12	-0.34	-0.72	• •	-0.23	0.18	1795
1796	0.78	0.58	-0.84	-1.56	-0.19	-0.59	-0.39	-0.01	0.40	1.11	0.00	0.98	1796
1797	-0.24	-0.29	1	-0.19		l	-0.56	0.39	0.15	0.13)	0.16	1797
1798	0.03	0.20	E .	-0.90		l	0.72	-0.41	0.00	-1.00		0.31	1798
1799	-1.75	1.38	0.52	0.64	t i	0.08	0.37	0.75	0.48	l	-0.32	0.40	1799
1800	2.27	2.96	0.69	2.46	0.63	1		-0.41	-0.58	l	-0.18	0.09	1500
1801	-0.11	0.76	1.45	0.24	-0.10	-0.16	1.26	-0.56	-0.07	1.04	1.04	1.64	1801
1802	0.09			-1.01		2.50	0.17	0.72	0.42	0.77	1.51	1.40	1802
1803	1.67		1	1	-1.08	0.66	0.04	0.52	0.31	-0.65	1.42	0.42	1803
1804	4.63	-0.82	0.16	0.21	0.14	1.30	1.12	1	-0.14	0.31	1.22	1.40	1804
1805	0.80	0.69		-1.59	-1.59	1.21	-0.65			0.06		-1.02	1805
1													
1806	-1.15	0.64	-0.04	-0.50	0.41	0.10	-0.14	-0.85	-1.16	-0.43	-0.14	0.40	1806
1807	-1.06	0.16	0.34	1	0.74	0.90	1.37	0.92	2.80	1.26		-0.07	1807
1808	-0.24	-1.22	1	l	-0.48	-0.43	0.88	0.04	2.42	-1.92	ł	-2.31	1808
1809	0.57	1	0.23	ì	-0.48	0.86	1.46		l	1		-0.95	1809
1810	0.01		2.49	0.28	0.50		1	-0.19	1		0.06	-0.91	1810
1811	-0.15	0.69	-0.91	0.24	0.43	1.46	0.97	0.26	0.04	0.95	0.00	-0.76	1811
1812	-1.51	0.40	0.00	-0.39	-0.61	0.15		-0.21	-0.69	-0.16	0.35	-0.18	1812
1813	-1.51		-0.80	1	0.79	1	1	-1.25	1	1.31	0.04	-1.18	1813
1814	0.54	-3.04	-0.88	0.04	-1.46	-0.59	-0.96	-0.56	-2.03	-0.49	-0.52	-0.42	1814
1815	-0.46	0.07	0.29	0.90	0.61	-0.63	1	-2.01	-0.78	0.22	0.08	-0.78	1815
										1			
1816	-0.40	-0.31	-0.71	-0.54	0.05	-1.94	-0.65	-0.48	-0.80	-1.09	-0.63	-1.24	1816
1817	-0.11	-0.09	-0.15			0.32	-0.39	0.46	-0.34	0.11	-0.47	-0.02	1817
1818	-0.66	0.87		1.21	0.19	-1.10	-0.25	-0.45	0.24	-0.78	0.33	0.62	1818
1819	-1.02	0.18	0.72	0.97	-0.12	-0.21	-0.28	-0.34	-0.32	0.82	1.11	0.82	1819
1820	1.89	-0.11	-0.97	0.37	2.03	0.68	0.48				-0.65	0.29	1820
1821	1.92	-0.76	0.49	0.50	0.85	-0.74	-0.30	-0.21	0.51	-0.74	-0.72	0.69	1821
1822	-1.28	-1.11	-0.53		0.68	2.97	1.48	1.46	1.88	1.51	0.06	0.18	1822
1823	0.52	1.78	-0.80	0.28	0.99	0.30	-0.36	0.35	-0.34	-0.76	-1.63	-0.53	1823
1824	-0.91	1	-1.04	-1.01	1.25	-0.25	-0.70	1.86	0.13	1.51	0.64	0.51	1824
1825	-1.04	-1.02	-0.17	0.12	0.30	-0.45	-0.10	0.46	0.55	-1.00	-0.05	1.67	1825
1826	-0.88	0.56	-0.29	-0.59	-1.08	-0.74	0.39	0.52	1.35	0.46	-0.87	-0.24	1826
1827	0.07	0.83	0.82	-0.51	0.18	-1.30	0.80	1.33	-0.73	0.50	-1.76	-0.04	1827
1828	-0.16	0.20	0.23	0.29	1.99	1.28	2.48	1.10	0.74	-0.34	0.06	-0.37	1828
1829	0.79	-1.90	1.12	2.49	-0.09	-0.47	0.16	-0.12	0.41	-0.38	-0.35	-0.16	1829
36								-					Magne
Means.	8.35	8.27	9.40	11.52	14.35	17.12	19.25	19.48	17.60	14.78	11.69	9.44	Means.

LXXXI.

NORTH ITALY. - MILAN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1763	$^{\circ}_{-1.32}$	0 1.58	° -0.60	0.27	° -2.28	-0.79	0.68	° 1.11	° -1.11	-1.69	° -0.56	0 1.02	1763
1764	1.68	1.98	l		1.32		-0.12	1	-1.21	-1.19		1	1764
1765	3.88	-0.92	0.60		-1.08	0.11	-2.62		-0.11	0.11	0.24	1	1765
1766	-3.42	-1.52	-0.40	0.57	0.02	1.31	-1.32	-0.19	1	-0.49	1	-0.68	1766
1767	-4.22	0.38	1	-0.93		-1.19		-0.69				-0.88	1767
1768	-0.82	-1.22	-1.50	0.37	-0.58	-2.19	0.68	0.51			0.64	-0.78	1768
1769	1.88	-0.42	-0.50	-1.63	-0.48	1.01	-0.52	1.51		-2.19	1.24	0.62	1769
1770	-0.52	0.98	-0.60	-0.33	-0.58	0.81	-0.72	0.01	1.99	0.51	1.04	-0.68	1770
1771	1.78	-0.52	-0.60	-1.43	1.02	-0.19	0.68	1.51	0.49	-0.69	-1.06	2.32	1771
1772	1.58	2.48	2.50	0.57	-0.58	1.61	1.38	0.41	0.29	2.01	1.94	2.02	1772
1773	1.58	-0.42	_0.so	_0.02	-0.48		-1.72	-1.29	0.69	1.61	0.34	1.82	1773
1774	0.48	0.08	0.70	l.	-0.28	0.51	-0.12	1.31	l	l .	-0.96	1	1773
1775	0.38	2.08	1.60	1	-0.58	0.71	0.78	-0.09		-1.79		-0.88	1775
1776	-0.32	-0.02	1.30		-1.28	0.11	0.48		-0.71	0.11		-1.18	1776
1777	-1.52	-1.42	1.30	-0.23		-0.79	-1.22	0.51	0.19	0.41	l	-1.98	1777
1	1.02	1	1.00	0.20	1.00	0	1.22	0.01	0.10	0.41	1.24	1.50	1
1778	0.38	0.08	-1.90	1.47	0.62	-0.29	0.98	0.81	-0.81	-0.09	0.64	1.72	1778
1779	-3.52	1.98	0.00	1.07	1.72	-1.39	0.18	-0.19	1.59	1.81	-0.16	1.82	1779
1780	-0.62	-1.92	2.70	-0.43	1.72	1.51	0.78	0.11	-0.51	1.81	-0.16	-1.08	1780
1781	-0.12	0.38	1.90	1.47	0.22	0.01	1.78	0.41	0.39	-0.89	0.04	1.42	1781
1782	2.18	-2.42	-0.70	-1.03	-1.08	1.21	2.08	0.91	-0.31	-1.79	-2.46	-0.58	1782
1783	0.98		-0.60	0.97	0.42	-0.99	1.08	-0.29		1.51	l .	-1.88	1783
1784	0.48			-2.03	2.62	2.11	1.38	0.61	1.49	-1.49	-0.46		1784
1785	0.58	1	-3.80		0.72	1.21	0.68	0.61	2.69	0.41	0.74	2.02	1785
1786	0.18	0.68	-0.90	0.87	0.72	0.81	-0.52	-0.89	1.09	-1.89	-0.36	-0.48	1786
1787	-0.32	0.08	0.90	-0.03	-1.9 S	1.71	-0.02	1.61	0.09	0.81	0.84	1.72	1787
1788	2.78	1.08	2.30	1.37	-0.18	1.51	2.78	-0.39	0.99	0.21	-0.86	-2.88	1788
1789	-1.72	0.98	-1.70	1.37	2.22	-0.79	0.28	0.11	0.29	0.31	-1.26	-2.38	1789
1790	-0.12	1.48	-0.20	-1.73	1.62	0.71	-0.72	1.21	0.19	2.21	1.21	0.02	1790
1791	2.48	1.08	1.20	1.87	-0.18	-0.49	0.58	1.51	0.09	-0.29	-0.46	1.92	1791
1792	0.98	-0.12	1.30	1.87	-0.1 S	0.21	0.08	0.11	-0.41	0.71	0.54	-0.08	1792
1793	-1.22	-0.02	0.40	-1.43	-0.88	0.01	1.78	-0.29	9 (0	1 91	1	2.22	1793
1793	2.28	$\frac{-0.02}{3.08}$	2.00	$\frac{-1.45}{2.37}$		0.01	1.78	0.29	2.49 -1.11	1.31 -0.49	1.44	-0.38	1793
1794	-3.72		-0.20	1.37			-1.42	0.21	$\begin{bmatrix} -1.11 \\ 0.49 \end{bmatrix}$	1.71	-0.16	1.52	1794
1796	$\frac{-3.72}{2.48}$		-0.20	-0.13		-0.79	-0.12	0.51	1.39	0.41	1.24	1	1796
1797	0.78		-1.40	0.67		-0.23 -1.59	1.18	2.51	1.09	-0.59	0.94	1.32	1797
1.31	".,"	0.10	1.70	0.07	1.22	1.00	1.10	2.01	1.0.7	0.93	0.04	1.02	1,5,
1798	1.78	2.08	0.20	0.27	0.72	-0.09	0.48	0.51	0.29	-0.39	-0.86	-2.08	1798
1799	-3.22	0.88	0.60	-1.23	-0.98	-1.49	-0.62	0.41	1.39	0.51	-0.96	-1.18	1799
1800	1.78	4.58	-1.10	2.67	1.32	-1.5 9	0.38	-0.09	0.49	0.01	1.24	-0.08	1800
1901	1.90	1.00	1.50	0.77	0.90	_0.90	_0.00	0.00	0 (0	0.07	0.04	0.00	1901
1801 1802	1.38 0.18	1.08	1.50	0.77	0.32	-0.39	-0.62	-0.79	0.49	0.61	0.04	0.02	1801
1802		1.18 -3.82	$0.70 \\ 0.30$	0.87	-0.08	1.71	0.28	2.21	1.09	2.81	0.51	$\begin{array}{c} 1.52 \\ 0.22 \end{array}$	1802 1803
1009	4.05	-0.82	0.30	1.47	-0.88	1.11	0.78	1.11	-0.91	-0.49	0.54	0.22	1003

LXXXI.

NORTH ITALY. - MILAN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						51000 01	Reaum	· · · · · · · · · · · · · · · · · · ·					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1804	3.98	0	-0.60	0 00	0	° 2.11	0	0 20	° 0.49	° 0.71	-0.36	° -0.18	1804
1 1		1	i	ı	1.32		J	-0.39		}	1	1 1	1805
1805			-0.10		-0.78	0.21	1	-0.29		-1.19	l	-1.58	
1806	0.18	1.68	l	-1.53	0.32	1.01	1			-0.19	1.34		1806
1807	0.58	0.28	l .	-1.33	1.32	0.21	1.18	l	0.19	1.71	1.34	1 1	1807
1808	-1.02	-1.62	-3.80	-1.23	1.62	-0.49	1.98	-0.69	0.39	-2.39	0.24	-2.08	1808
1809	0.48	1.98	-1.40	-2.63	1.02	0.51	-0.52	0.21	-0.51	-0.19	-0.96	0.22	1809
1810	0.08		1	-0.23	0.22	Į.	-2.12		1	1.11	0.34	1.82	1810
1811	-0.72	1.48	1.70		l	-0.29	1	-0.49		2.21)		1811
1812	-3.32	-0.32	-0.40		0.92	l .	i		l .	0.11	l	1	1812
1813	-0.12	1.08	0.50	l	!	1	-2.12		i	0.21	1	1 1	1813
1010	0.12	1.00	0.50	1.01	1.02	-0.55	2.12	1.03	1	3.21	0.00	1.02	1010
1814	-0.19	-4.42	-1.40	0.77	-1 98	_1 09	-0.12	_1.09	-1.91	-0.69	1.01	1.82	1814
1815		-0.32	1.90	1		1	-1.22			0.81	1		1815
1816	I	-2.92	-1.20	1		1	-2.22	1		0.41	1	-1.88	1816
1817	-2.52	2.08	0.30	l .	-1.28		-3.52	ł.	1	-1.89	0.44	1 1	1817
1818	0.48	3.34	0.30	0.37				-0.79	1	0.48	i .	1 1	1818
1010	0.40	0.04	0.70	0.57	3.00	0.20	0.55	0.73	0.25	0.40	1.13	0.00	1010
1819	0.00	0.73	1.48	1.35	-0.02	-0.53	0.32	-0.50	0.48	0.46	0.93	0.30	1819
1820	-0.79	0.58	-0.56	1.60	1.03	-0.48	-0.48	1.76	-0.09	-0.30	-0.72	-0.03	1820
1821	0.80	-0.18	-0.52	0.59	0.10	-2.20	-1.46	0.43	1.01	-0.29	0.78	0.35	1821
1822	1.81	1.28	2.10	0.99	1.05	3.31	0.53	0.26	0.78	0.66	1.38	-0.48	1822
1823	-1.92	-0.25	-0.37	-0.55	0.93	-0.78	-0.60	0.53	1.18	0.11	-1.37	0.01	1823
1								}					
1824	1.01	1.49	-0.40	-0.85	-0.16	-1.57	1.33	0.90	0.71	0.23	1.25	2.07	1824
1825	1.39	0.62	-2.38	1.21	-0.17	0.32	0.05	0.53	0.86	-0.81	0.82	3.92	1825
1826	-2.18	0.44	0.76	-0.72	-1.23	-0.09	0.18	1.55	0.71	1.48	-0.56	1.16	1826
1827	0.36	-1.72	1.12	0.73	0.46	-1.26	1.20	-0.60	-1.06	1.37	-1.46	0.25	1827
1828	1.38	-0.36	1.49	0.64	0.45	1.27	1.38	0.19	0.47	0.38	-0.81	0.60	1828
		0.00	0.05	0.05	0.00	2.00	0.00		0.00	0.40	1.00	1.00	1000
1829		-2.79	0.05	ì	-0.03		l .		-0.89		-1.68	1	1829
1830		-3.45	1.66			-0.33	1.71		-0.79	-0.81	0.99		1830
1831		-0.51	0.73	0.19		-0.56	0.12		-1.08	1.77	0.24		1831
1832	0.41	0.52	-0.21	-0.68		-1.27	0.03		-1.15	-0.47	-0.41	-1.71	1832
1833	-0.47	1.18	-0.59	-1.23	2.00	0.37	-2.28	-2.77	-3.20	-1.36	0.14	1.37	1833
1834	0.17			-1.97			-0.23	1	l		-0.23	1 1	1834
1835	1.03	0.76	-0.44	-0.88	-1.01	-1.47	-2.59	-2.35	-2.01	-2.24	-3.27	-2.69	1835
1836	-2.51	-2.08	-0.05	-1.07	-3.41	-0.49	-0.97				ı	1 1	1836
1837	-0.83	-4.75	-3.12	-2.41	-3.58	0.64	-1.29	0.37	-2.40	-1.93	-1.76	-0.36	1837
1838	-2.16	-2.39	-0.7 2	-2.74	-0.98	-0.75	-0.78	-1.55	-1.58	-1.74	0.08	-0.80	1838
Means.	0.52	2.82	6.40	10.03	14.08	17.09	18.92	18.39	15.31	10.79	5.76	2.08	Means.

LXXXII.

SWITZERLAND. - GENEVA.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						grees of	Ittauin	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	o	0	0	0	0	0	
1768	-0.86	-0.01	-2.3 8	-0.14	Į.	-1.71	-0.92	1	1	0.99	0.77	0.08	1768
1769	0.92	0.16			-0.71		l	-1.43		ŀ	1.62	0.61	1769
1770	-1.25	-1.30	-1.72		-1.20		-2.97	l	0.49		0.35	0.42	1770
1771	0.53	-0.67	0.17	-2.6 8	0.34			-1.45	\$	-0.17	-1.80	1.66	1771
1772	0.61	2.57	1.76	-0.41	-2.23	0.35	-0.72	-0.47	0.52	1.34	1.29	1.16	1772
1773	1.47	-1.84	-1.18	-1 16	-1.64	-0.87	-2.03	-1 70	-0.12	-0.35	-0.12	1.01	1773
1774	1.22	0.91	2.38		-0.94		-1.27	1	-1.08	-1.45	ŀ	-2.03	1774
1775	0.89	1.89	0.99		-1.90	0.54	-0.84	ļ.	-0.02	-0.24	0.33		1775
1776	-1.78	1.92	1.85		-1.96	0.09	0.20	1	-1.50	0.26	ľ	-0.09	1776
1777	-0.41	-0.76	2.46	-1.23	-1.51	-0.38	-1.12	0.45	1	1.27	0.21	-1.72	1777
1	0011	0.10	2.10	1.20	1.01	0.00		0.10				1112	
1778	0.03	-0.93	0.86	0.78	-0.09	-0.76	1.59	0.68	-1.85	0.32	0.76	1.85	1778
1779	-3.43	-0.28	-0.14	1.70	0.97	-1.22	-0.61	-0.45	0.48	1.77	0.57	2.70	1779
1780	-1.48	-1.63	2.35	-0.86	0.97	1.14	0.95	1.16	0.14	0.51	-1.02	-1.25	1780
1781	0.96	1.09	0.37	2.15	1.78	0.28	-1.17	0.30	* 0.76	-0.47	1.69	2.97	1781
1782	2.22	-3.74	-0.53	-0.95	-1.76	0.18	-1.10	-0.72	-0.97	-1.06	-1.83	-2.04	1782
1783	2.01	1.68		-0.71	-0.06	-1.13		-0.94	0.17	0.93	0.81	1.03	1783
1784		-2.03			1.73	1.69		-1.62	1.40	-1.87		-3.38	1784
1785	0.58	-3.26				0.30		-1.75	0.94	-0.40	0.11	0.42	1785
1786	0.41	0.08	-1.62	0.69	-0.25	1.92	-0.99		-0.59	-1.71	-0.69	0.19	1786
1787	-1.99	-1.15	1.76	-0.30	-1.98	0.79	-0.70	0.21	-0.27	0.41	0.72	2.83	1787
1788	1.01	2.06	2.19	1.04	1.13	1.04	1.61	-0.45	0.71	-0.83	-2.15	-4.48	1788
1789	-1.17	1.12	-1.97	1.19	1.71	-1.25	-0.80				-1.59	-0.17	1789
1790	0.36	0.75	0.99	-0.73	1.52	0.94	-1.10	0.63	1	1.95	1.13	0.78	1790
1791	2.40	0.04	-0.02	2.86	0.61	1.04	0.98	2.30	0.98	0.72	-1.37	1.30	1791
1792	1.22		2.11	1.81	-0.12	1.14	1.03	0.83	-0.09	1.37	0.86	0.45	1792
1.52	1,	0.20		1.01	0112		1.00		"""	1.07	0.00	0110	1.02
1793	-0.52	1.05	1.77	0.08	-0.05	0.20	3.12	2.49	-0.12	1.24	0.61	1.19	1793
1794	0.14	2.21	1.91	3.26	0.76	1.10	2.11	0.39	-0.74	-0.28	0.86	-1.75	1794
1795	-4.85	0.37	0.26	1.76	1.32	1.34	-0.73	1.34	1.54	1.92	-0.96	1.11	1795
1796	1.25	0.72	-2.15	-0.06	0.60	0.60	0.37	0.80	1.61	0.41	-0.14	-1.92	1796
1797	0.11	-1.41	-1.08	1.49	2.14	-1.28	2.21	1.28	0.71	-0.08	0.71	1.61	1797
1798	0.53	-1.17	-1.02	0.83	1.00		0.45	0.81	0.48	-0.29	0.44	-0.96	1798
1799	-1.57	1.71	-0.16	-1.73	l	-1.16	-0.13	0.67	0.21	-0.40	-0.54	-2.59	1799
1800	1.61	0.06	-1.66	2.43	2.40	-0.83	1.48	0.82	0.96	-1.55	0.63	-0.27	1800
Means.	-0.43	0.75	3.08	7.19	11.21	14.03	15.44	14.85	11.49	7.32	3.34	0.57	Means.
1796	2.27	0.07	-2.14	-0.25	-0.91	-0.64	-1.10	0.16	0.70	0.08	-0.68	-1.70	1796
1797	1	-0.85	-0.66	0.97		-2.03	1.27	0.71	-0.48	-0.26	0.47	1.58	1797
1798	1	-0.25	-0.40	0.96		0.32	-0.64	-0.14	0.12	1	-0.76	1	1798
1799	-1.44	1.93		-1.60			-0.46	0.33	0.19	-0.26	-1.24	-3.30	1799
1800	2.06	0.03	-1.53	2.88	1.66	-0.97	1.62	0.70	0.41	-1.16	0.67	-0.32	1800
1801	1.81	0.13	1.43	0.74	0.43	-0.26	0.42	0.15	0.90	0.84	0.67	0.95	1801
1802	1	-0.38	0.94	1.18	0.43	1.66	-0.12	2.68	1.72	2.51	0.63	0.58	1802
1803		-2.58	0.34	2.05	-1.42	0.89	2.20	2.25	-0.79	-0.57	1.04	1.88	1803
1804	1	-1.58		0.30	1.50	2.02	0.04	0.47	0.59	0.22	1	-0.59	1804
1.01	4.00	1 1	.,,13	0,0	1.50	2.02	0.04	0.41	0.00	0.52	1	00	

LXXXII.

SWITZERLAND. — GENEVA (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Keaumu	ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1805	-0.41	-0.23	-0.41	-1.35	-1.22	-0.49	-0.41	-0.73	0.18	-1.45	-2.19	-1.64	1805
1806	3.23	1.83	0.12	-1.80	1.33	1.66	0.08	-0.39	0.11	1.10	1.34	2.42	1806
1807	-1.10	0.24	-2.65	-1.47	1.42	0.43	2.66	3.03	-0.58	1.42	0.39	-2.48	1807
1808	-0.49	-3.14	-2.58	-1.87	1.14	-1.33	0.70	0.59	-0.14	-2.40	-0.28	-2.99	1808
1809	2.23	1.95	0.19	-3.68	-0.06	0.12	-0.43	-0.32	-1.00	-1.05	-1.76	0.70	1809
				i									
1810	-3.14	-3.34	3.08	-0.28	0.29	-0.45	-1.01	-0.70	1.37	1.26	1.05	1.19	1810
1811	-2.22	1.98	1.46	1.34	1.23	1.82	1.53	-0.14	0.70	2.21	0.71	-0.85	1811
1812	-3.92	1.40	-0.02	-1.54	0.27	0.02	-0.37	-0.69	-0.43	0.13	-1. S0	-2.74	1812
1813	-1.74	1.51	-0.69	0.53	0.54	-0.84	-2.10	-1.02	-1.14	0.78	-0.49	0.32	1813
1814	-1.32	-3.92	-1.44	0.96	-1.74	-0.26	0.37	-0.66	-1.74	-0.87	0.95	2.34	1814
1815	-2.24	1.43	2.17	1.06	0.82	0.08		-0.59	0.54	1.43	-1.57	-0.39	1815
1816	-0.13	-1.33	2.54	-0.48	-0.54	-1.41		-2.14	-0.47	0.59		-0.02	1816
1817	2.50	2.38	0.29	-2.11	-1.34	1.35	-0.25	-0.71	2.16	-1.58		-0.45	1817
1818	0.54	0.69	0.13	-0.08	-1.26	0.66	1.41	-0.41	-0.89	-0.29	1.60	-0.26	1818
1819	1.86	0.98	0.82	1.00	-0.21	-0.19	0.07	-0.34	0.42	0.07	-0.40	0.95	1819
1820	0.10	0.54	-1.24	2.07	0.39	-0.59	-0.65	0.84	-1.93	-0.31	-2.16	0.02	1820
II I						1		0.62	0.26	0.27	$\frac{-2.10}{2.34}$	3.36	1821
1821	1.98	-1.31	0.94	0.71	-1.19	-1.54	-1.17	-0.85	ł		1.60	1	1822
1822	0.20	1.27	3.06	0.47	1.32	3.85	0.27	ļ	Į.	0.69	-1.97	1.04	1823
1823	-1.17	1.46	-0.29	-0.42	0.17	-1.62	-1.54	l .	1	1			1824
1824	-0.78	-0.30	-1.84	-2.05	-1.50	-2.05	0.17	1		1	0.03	1.30	1825
1525	-0.07	-0.55	-1.09	1.69	-0.63	0.26	-0.40	-0.11	0.88	0.30	0.54	2.76	1020
Means.	-0.42	1.87	4.70	8.79	13.45	15.81	17.67	17.66	14.70	9.73	5.23	1.27	Means.
1826	-3.23	1.12	1.47	0.34	-1.04	-0.06	0.90	2.57	1.22	0.95	-1.19	0.03	1826
1827	1.49	-2.15	1.02	1.29	1	-0.07	1.95				-2.02	1	1827
1828	2.82	1.06	0.70	0.81	1.22	ı	0.59	1			1	1 1	1828
1829	-0.85	-0.63	0.10	0.25	-0.06		1	-0.89		-1.52	1	1	1829
1830	-4.14	-1.74	1.20		0.57	1	0.53	1	-0.94			1 1	1830
1030	4.1.1	_1.,4	1.20	2.10	0.51	0.43			1				
1831	-1.10	0.46	1.67	1.54	0.53	-0.11	-0.02	T.		1			1831
1832	0.10	0.36		0.45	-0.40		0.81	2.29	1	1			1832
1833	-0.06	3.36	-0.50	-0.68	2.67	1	1	Ĭ .	1	1	1	1	1833
1834	5.06	1.47	0.35	-0.70	2.28	1.53	1.94	1				1 1	1834
1835	1.15	1.40	-0.44	-0.06	0.56	0.15	1.69	0.40	0.22	-1.34	-2.27	-2.66	1835
1836	0.48	-0.04	1.82	-0.95	-2.14	0.17	0.57	0.28	-0.62	0.14	-0.02	0.50	1836
1837	0.37	0.52	-2.94	-1.89	-2.18	1.21	-0.58	1.41	-1.16	-0.39	-1.06	-0.46	1837
1838	-3.64	-0.91	0.25	-1.75	-0.11	-0.71	-0.56	-1.23	-0.58	-0.61	1.18	-0.57	1838
1839	0.55	-0.07	-0.42	-1.55	-0.97	1.14	0.24	-1.73	-0.58	1.11	1.43	2.81	1839
1840	2.60	0.02	-3.22	0.71	-0.10	-0.37	-2.32	-0.01	-0.56	-1.74	1.43	3.14	1840
1841	0.45					-1.71	-1.98	-1.37	0.09	0.90	0.26	0.89	1841
1842	-5.18	1	1		1	l l	-0.19	1	1	-2.18		1 i	1842
1843	1.50		1	1	1			1	1	-0.24		1	1843
1844	II .	2.22		0.21	1.00		2.50	0.7.	0.00			0.00	1844
1845	1.70		1	1				1					1845
Means.	-0.72	·	-	-	-	13.61	·	·	·	·	3.98		Means.

LXXXIII.

South Germany. - Vienna.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	egrees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1775	-1.43	1.86	1.21	-2.35	-2.77	1.32	l	1.29	1	0.26	0.29	-1.09	1775
1776	-4.30	0.57	0.70		-2.30	-0.42	-0.24	.0.25	-1.42	-1.53	-1.32	-2.19	1776
1777	-1.79	-1.24	0.32	-2.93	-0.22	-0.10	-1.17	0.57	-1.38	-0.53	0.35	-1.00	1777
1778	1.92	-1.04	0.18	1.89	0.04	-0.43	1.18	0.95	-0.89	-0.54	0.87	3.61	1778
1779	-1.75	3.15	2.27	3.05	1.24	-1.32	-1.35	-0.07	0.65	1.00	0.43	3.01	1779
1780	-1.68	3.04	2.73	-1.38	-0.18	-0.92	-0.70	-0.48	-1.08	0.51	0.19	-1.99	1780
1781	-0.87	0.05	0.77	0.86	0.25	1.44	-0.06	2.31	1.40	-0.45	1.84	0.34	1781
1782	2.72	-2.63	0.60	-0.06	0.54	1.82	2.74	0.85	0.86			0.62	1782
1783	3.59	4.12	-0.08	0.65	1.81	1.94	1.66	1.81	2.12	1.59	0.58	1 1	1783
1784	-3.51	-1.87	-0.42	-1.36	1.69	0.86	0.47	0.49	1.98	-2.56	1	0.03	1784
l l	.												1.04
1785	-0.73	-0.93	-5.63	-3.04		-1.47	-0.83	-0.86	2.11	-0.55	0.41	0.17	1785
1786	0.52	0.16	-0.04	1.84		0.25	-1.54	-1.85	-0.92	-2.11	-2.12	0.60	1786
1787	-0.39	1.47	0.65	-1.46	-2.11	1.11	-0.40	0.35	-0.78	1.10	0.93	2.82	1787
1788	2.22	0.17	0.81	0.05	-0.36	1.18	2.28	-1.72	1.00	-0.29	-1.39	-6.79	1788
1789	-0.49	2.00	-2.43	1.19	2.15	-0.49	0.40	-0.60	0.37	0.77	0.73	0.21	1789
1790	0.86	2.87	0.31	-1.11	1.20	1.56	-1.10	0.31	-0.83	-0.76	-0.43	2.09	1790
1791	4.29	1.01	1.63	1.33	-0.44	~0.33	-0.37	0.67	-0.84	-0.40		0.89	1791
1792	0.56	-1.24	0.47	0.38	-0.96	0.62	0.38		-0.93	-1.11	-0.24	0.56	1792
1793	-1.55	1.27	-1.00	-2.40	-1.23	-1.08	1.81		-0.07	1.13	0.64	1.99	1793
1794	2.24	2.99	1.95	3.74	1.35	1.55	2.92	-0.75	i e	-0.19	0.33	1 1	1794
}}		7 00		1 01	0.05		7.05	0.02	0.15	0 ***	1.00		
1795	-4.94	-1.29	0.23	1.81	-0.05	1.44	-1.95	0.31	-0.17	2.75	1	1 (1795
1796	5.23	1.32	-2.73	-1.52	0.48	-0.04	0.14	0.58	1.96	0.84	-0.14	1 }	1796
1797	1.58	1.02	-0.71	2.10	2.94	0.68	1.95	2.17	2.01	1.23	0.54	1.11	1797
1798	1.96	2.83	1.40	0.65	0.26	0.84	0.14	1.29	1.62	-0.47	-0.68		1798
1799	-5.34	-2.08	-0.83	-0.43	-0.45	-1.16	-0.58	1.00	-0.50	0.45	0.58	-2.94	1799
1800	0.74	-0.19	-3.31	5.57	1.90	-1.45	-0.44	1.49	0.27	~0.40	1.57	0.10	1800
1801	1.85	-0.21	2.47	0.80	1.83	-0.85	-1.18	-1.32	1.37	1.94	1.71	0.99	1801
1802	-0.43	-1.34	0.89	0.73	-1.14	1.33	1.02	1.65	0.38	2.10	1.84	1.40	1802
1803	-2.68	-3.46	-0.50	2.49	-1.59	-0.75	0.23	0.08	-2.12	-0.45	1.24	0.27	1803
1804	3.42	-0.59	-2.44	0.05	0.29	-0.10	0.25	-0.51	0.80	0.48	-2.47	-2.40	1804
1805	-0.48	-1.18	-1.28	-2.16	-1.85	-0.79	-1.26	-1.61	-0.04	-2.89	-2.19	0.24	1805
1806	4.04	$\frac{-1.15}{2.12}$	$\frac{-1.28}{1.07}$	-2.10 -2.07			-0.16	-0.62	0.56	-0.80	1.60	3.48	1806
- 11	i 1	1.96	-1.54			-0.02	$\frac{-0.16}{1.25}$	4.74	0.30	1.37	1.96	0.46	1807
1807	1.08	-0.51	1 1	-1.18 -1.20	1.42	-0.34	1.30	1.80	1.13	-0.97	-0.32	-3.68	1807
1808	$1.20 \\ -0.08$	1.54	-4.99 -1.13	-1.20 -2.51	0.89	0.15	0.23	0.79	0.11	-1.31	-0.32 -0.75	1.67	1809
1809	-0.08	1.94							ļ			1 1	i i
1810	-0.71	-0.03	2.03		0.50	-1.65	0.82	0.15	2.26	-0.18	1	2.01	1810
1811	-3.58	-0.91	2.08	0.75	3.12	4.62	2.56	0.99	0.42	3.63	1.20	0.19	1811
1812	-2.13	0.53	0.67	-2.67	0.65	0.35	-0.87	-0.52	-1.32	2.04	-0.84	-3.96	1812
1813	-1.84	2.07	-0.76	1.56	0.36	-1.82	-1.34	-1.80		-0.37	-0.24	0.68	1813
1814	-0.34	-4.37	-0.55	1.54	-2.19	-1.76	0.66	-0.21	-2.45	-0.73	0.32	2.19	1814
1815	-1.03	2.39	2.06	0.10	0.52	0.28	-1.51	-1.29	-1.20	0.06	-1.07	-2.87	1815
1816	1.84	-0.80	-0.19	0.09		-0.73	-1.58		-0.95	-0.73	-0.39		1816
1817	3.24	3.78	0.51	-4.08	0.53	2.18	-0.08		0.56	-2.29	1.09	0.16	1817
1818	2.77	0.78	1.84	2.01	-0.11	0.55	0.13		0.41	0.84	0.60	1	1818
1819	1.22	2.04	1.94		-0.75	1.01		-0.35		-0.12	0.51		1819
1_1010	1.22		1 2.04		3								

LXXXIII.

South Germany. - Vienna (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						51005 02	Reaum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1820	$^{\circ}_{-2.47}$	o 0.36	° -0.86	° 1.78	0	° -1.18	0 00	0	0 71	° 0.16	0 26	° -1.49	1820
l i		i	1 1					2.36	-0.71		-0.36	1 1	1
1821	2.22	-1.56	-0.72	1.57	-0.81	-3.08		-0.76	0.51	-0.12	1.93	}	1821
1822	2.85	1.63	3.44	1.05	1.21	1.50	1.16	-0.27	0.06	2.12	0.44	-0.27	1822
1823	-4.55	0.68	0.80	-0.29	0.42	-0.68		0.15	0.36	1.13	0.29	1.35	1823
1824	1.77	2.31	0.09	-0.72	-0.74	-0.60	-0.22	-0.53	1.36	0.60	1.56	4.00	1824
1825	3.15	0.50	-1.59		-0.14	-0.31	-0.72	-0.47	-0.62	-1.71	1.74	3.11	1825
1826	-3.65	-2.12	0.91		-2.42	-0.38	1.34	2.06	0.69	0.89	-0.32	1.78	1826
1827	0.69	-2.92	1.61	1.65	1.33	1.19	1.67		-0.57	0.82	-3.48	0.83	1827
1828	0.19		0.88		-0.16	0.21	0.63	-1.49	-0.70	-0.82	, 0.48	1.57	1828
1829	-1.66	-3.79	-1.87	-0.23	-2.26	-2.69	-0.32	-2.62	-0.31	-2.12	-3.62	-6.11	1829
1830	-5.31	-3.23	-0.44	0.94	-0.39	0.33	0.02	-0.04	-1.81	-1.68	0.76	1.13	1830
1831	-1.42	0.26	0.43	2.23	-0.90	-1.86	0.33	-1.01	-1.96	2.02	-0.16	-0.04	1831
1832	0.55	0.61	0.04	-0.16	-1.90	-1.46	-1.29	0.32	-0.86	0.04	-1.57	-1.36	1832
1833	-3.35	2.33	0.24	-1.40	2.57	1.20	-2.26	-2.80	-1.22	-0.55	0.23	4.03	1833
1834	4.67	0.32	-0.29	-1.17	2.24	1.65	2.61	1.26	2.85	-0.08	-0.89	1.25	1834
1835	1.71	1.46	0.46	-1.10	0.27	-0.07	0.92	0.19	0.09	-0.76	-3.77	-1.39	1835
1836	-0.08	0.29	3.84	0.00	-2.95	0.30		-0.78	i .	0.91	1	1	1836
1837	0.20	-2.39	-1.96		-2.57	-1.38	-2.96	0.84	-2.22	-0.82	-0.74	1 1	1837
1838	-5.10	-4.14	-0.50		-0.76	-0.74	-1.39	-2.29	-0.03	-1.75	-0.65		1838
1839	1.12	0.73	-2.31	-3.85	-2.04	1.06	0.36	-2.23	0.23	1.05	1.55		1839
1840	1.03	-0.88	-3.76	-0.55	-1.59	-1.05	-1.56	-1.94	-0.11	-2.03	2.09		1840
1841	0.33	-3.24	0.65	0.93	2.19	-1.02	0.55	-1.10	0.24	2.04	0.28		1841
											ļ		
Means.	-1.22	0.63	3.85	8.66	13.31	15.72	17.14	16.77	13.25	8.51	3.67	0.39	Means.
			LXX	XIV.	Sou	тн С	ERMAI	NY. —	RATI	SBON.			
1773	3.00	-0.28	-0.01	-0.28	0.25	0.34	-1.23	-0.60	0.47	1.20	1.06	2.35	1773
1774	1.63	0.85	2.17	1.97	-0.10	-0.17	-1.11	0.16	-1.29	-0.63	-2.98	-2.32	1774
1775	0.67	2.87	1.13	-2.41	-3.42	-0.51	-1.91		-0.73	-2.19	-0.14	-0.64	1775
1776	-3.04	1.19			• •								1776
1777	-1.47	-0.68	2.37	-1.29	-0.16	0.28	-1.02	1.24	0.01	1.07	1.31	-1.17	1777
1778	1.88	0.21	0.89	1.98	1.76	0.81	3.20	2.38	-1.3 3	-0.36	1.36	3.06	1778
1779	-2.51	1.43	2.27	2.89	1.88	-0.34	-0.38	0.95	1.40	2.18	1.47	3.74	1779
1780	-0.83	-1.52	2.87	-0.92	0.87	1.30	0.64	1.65	1.32	1.25	0.25	-0.75	1780
1781			1.52	1.88	0.82	1.52	0.48	2.36	2.45	-1.03	0.53	0.56	1781
1782	2.46	-2.93	3.32	3.15	3.74	1.92	2.02	-0.28	0.80	-1.67	-2.72	-0.32	1782
1783	3.48	2.22	-0.95	0.26	0.93	0.92	1.73	0.45	0.13	1.00	-0.34	-2.38	1783
1784	-4.07	-3.45	-1.69	-2.76	1.67	0.60	0.23	0.34	2.21	-2.46	0.36	-1.21	1784
1785	-1.20	-2.85	-6.49	-4.37	-1.08	-0.83	-1.42	-1.91	2.05	-0.77	0.28	0.10	1785
1786	0.66	0.04	-2.05	1.32	-1.54	1.28	-2.31	-1.85	-1.30	-1.93	-2.68	-0.18	1786
1787	-1.03	4.29	0.75	-1.53	-2.51	0.92	-1.31	0.36	0.07	1.78	0.89	2.06	1787
1788	1.86	-0.61	-0.30	-0.59	-0.35	0.88	1.66	-1.53	1.44	-0.20	-2.14	-8.30	1788
1789	-1.93	1.41	-2.90	0.64	1.62	-1.30	-0.29	-0.28	-0.53	0.27	0.25	0.64	1789
1790	1.99	1.73	1	-1.21	1.20	1.42	1	-0.08	-0.87	-0.37	-0.26	0.89	1790
1791	3.24	0.14	1.00	l	1	-0.35	l	1.14	-0.15	0.50	-2.43	0.84	1791
	11 1	1 1	1	1	,	1						1	

LXXXIV.

South Germany. — Ratisbon (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

							Keaum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1792	-0.57	-0.21	° 1.41	。 1.17	° -1.12	$\overset{\circ}{0.87}$	0.66	0.88	° -1.01	0.05	° 0.17	° 0.89	1792
1793	-1.17	1.26	0.53			-0.76	1.56		-0.47	1.87	0.95	1.26	1793
1794	2.30	3.01	3.05	3.04	1.19	1.69	2.85		-1.00	1.24	0.67	-0.78	1794
1795	-5.05	-0.89	-0.10	1.96	-0.82	1.39	-2.22	0.29	1.08	3.11	-0.98	2.26	1795
i li		1.59	-1.63	1	-0.25	0.05		0.29	ł	0.28		-2.04	1796
1796	4.26	1.55	-1.03	-0.77	-0.23	0.05	0.47	0.93	2.24	0.28	-0.55	-2.04	1730
1797	1.46	1.52	-0.17	2.09	2.60	-0.72	2.14	1.73	0.75	0.06	1.00	1.59	1797
1798	1.88	1.94	0.18	1.02	0.66	1.65	0.50	1.26	1.08	-0.73	-0.68	-2.69	1798
1799	-5.61	0.14	-0.29	-1.87	-1.37	-0.83	-0.91	-2.86	-0.60	-0.23	-0.35	-3.81	1799
1800	1.15	-0.63	-2.62	4.66	1.80	-1.42	0.32	1.53	0.43	1	1.30	4	1800
1801	2.72	0.10	1.82	0.76	2.45			0.13	1.15	1.60	1.45	0.81	1801
									1		-		
1802	-3.20	-0.90	0.29	0.62	0.16	1.66		2.80	0.73	2.40	0.63	0.71	1802
1803		-2.05	-0.06	2.70	-1.78	-0.31	1.70	1.31	1	1	0.29	0.93	1803
1804	3.84	-0.86	-1.18	-0.49	1.17	0.88	0.29	-0.14	1.27	1.09	-0.71	-1.68	1804
1805	-1.41	-1.00		-1.27	-1.76	-0.88	-0.88	-1.60	0.74	-2.03	-1.81	-0.21	1805
1806	4.22	2.45	0.40	-2.24	2.47	0.16	-0.49	0.15	0.86	0.04	1.94	3.58	1806
1807	1.19	1.18	_1 17	-1.32	1.24	0.46	2.87	4.63	-0.94	1.58	1.03	1.54	1807
1808	1.08	-0.7 3	i .	-1.93	2.02		1.61	1.19	0.33	-1.97	-0.23	-5.46	1808
11			1	1		-0.45		1	1	-0.76	1	1 1	1
1809	0.33	2.19		-2.92	0.71		0.02	0.23	ł			0.93	1809
1810	-1.72	-2.39		-0.63	-0.05	-1.00	-0.41	0.17	2.72	0.52	0.04	1.89	1810
1811	-2.93	-0.16	2.09	1.48	2.23	2.85	1.75	0.24	0.43	2.24	1.43	-0.25	1811
1812	-1.33	1.05	0.28	-2.87	0.13	-1.15	-2.18	-1.44	-1.39	0.60	-1.99	-4.72	1812
	-3.03	0.99	-1.15	0.46	1	-1.86			}			1 1	1813
	-1.37	-4.71	-2.93	0.49					-2.45	1	0.65	1.77	1814
1815	-1.30	1.05	1.18	-0.37		-0.74			Į.	1	-1.37	!	1815
1816	1.36	-1.83	-1.23	-0.93	-2.69		-2.42		-2.04	-0.93	-1.49	1	1816
i li									1		ŀ		
1817	2.51	2.42	-1.14	-5.01	-1.93	i .	-1.79	-1.89	0.56	-3.22	0.63	-0.70	1817
1818	2.08	0.29	-0.16	0.27	-1.72	-0.02	-0.48	-2.27	-1.09	-0.71	0.41	-2.08	1818
1819	1.49	0.60	0.64	-0.09	-0.76	0.15	-0.05	-0.35	-0.28	-0.78	-0.99	-1.34	1819
1820	-2.43	-0.35	-2.26	0.38	-0.47	-2.89	-1.66	0.93	-2.28	-1.22	-1.63	-1.66	1820
1821	1.17	-3.06	-1.51	0.99	-2.48	-3.01	-2.77	-1.18	-0.06	-0.99	1.51	2.53	1821
1000	9 91	0.69	1.00	0.26	0.53	2.43	0.49	-0.87	-0.56	0.79	0.48	-2.29	1000
1822	2.21	0.63	1.92		0.33	i	-1.05	0.43		$\begin{array}{c c} 0.73 \\ 0.02 \end{array}$	1	1.05	1822
1823	-4.17	0.86	0.11	-1.72	l .	l .	1	i	1			t e	1823
1824	0.92	0.38		-2.10	1	l	-0.14	-0.51	0.97	-0.26	2.00	3.93	1824
1825	2.80	0.39	-1.05	2.12	0.93	0.56	0.51	0.32	1.31	0.21	3.09	4.15	1825
1826	-3.57	-0.34	1.39	0.17	-1.04	1.05	1.99	3.61	1.61	1.38	-0.28	0.92	1826
1827	0.09	-4.95	1.00	1.31	1.20	1.05	2.06	-0.57	0.93	1.35	-1.30	2.93	1827
1828	2.12	0.27	0.51	0.31		0.39	0.85	-2.47	ł	-0.20	0.61	2.28	1828
1829	-0.85	}	-1.38	0.20		-1.11		-2.37	i	-1.41	-3.79	-5.79	1829
1830	-5.98	1	1.17	0.77			0.50	1	-1.05	-0.88	1.14	-0.58	1830
1831	1	-0.82	0.70	3.60	1	-1.36		-0.12	1	2.40	2.27	0.26	1831
1832	0.77	1.28	0.09	0.21	-2.45	-0.87	-1.18	0.59	-0.98	0.16	-0.71	0.25	1832
1833	-3.05	3.32	0.21	-1.45	2.29	1.06	-1.70	1	1	-0.90	2.78	3.95	1833
1834	1	-0.43	l		0.99	0.44	4.89	2.48	Į.	0.50	0.74	1.36	1834
Means.	_9.19	-0.09	3.09	7.55	11 0	13.72	1.1 88	14.69	11 60	7.11	2 22	-0.71	Means.
	-2.42	-0.09	5.09	1.35	11.94	15.72	14.00	14.02	11.09	1.11	4.42	-0.71	

LXXXV.

SOUTH GERMANY. - STUTTGARD.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees of	Reaumi	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1792	0.64	-1.23	1.78		-1.12		1.04	1	-0.70	1.30	l	l 1	1792
1793	-1.41	1.64	0.37	-1. 36		-0.31	2.52		-0.84	1.71	0.66	2.10	1793
1794	2.02	3.72	2.76	3.26	0.41	1.30	2.75	0.12	-1.34	0.32	0.85	-1.72	1794
1795	-4.88	0.36	0.65	2.81	0.64	1.43		1.33	1.93		-0.49	3.76	1795
1796	6.17	1.90	-2.51	-0.67	-0.32	0.10	-0.36	0.23	2.34	0.13	-0.87	-2.18	1796
1797	2.46	0.08	-0.27	1.88	1.16	-1.30	2.86	1.01	1.04	0.36	1.82	3.02	1797
1798	0.65	1.44	0.69	1.16	0.66	1.21	0.14	0.66	1.36	0.53	0.33	()	1798
1799	-3.46	1.77	-0.78	-1.30	-0.89	-0.75	-0.98	0.32	-0.04	-0.15	0.42	-4.70	1799
1800	3.03	-0.92	-2.04	4.56	2.03	-1.81	0.00	0.79	0.84	-0.37	1.61	-0.18	1800
1801	3.95	0.97	1.98	0.24	0.94	-0.54	0.91	1.42	2.32	2.89	1.30	1.46	1801
1000	0.55	0.00	0.00	0.10	0.00	1.50	0.04	0.00	0.00	2.00	0.01		1000
1802	11	-0.02	0.80	2.13	0.23		-0.24	2.22	0.62	2.08	0.81	1.41	1802
1803	-0.81	-1.90	1	1.49	-2.28	0.05	1.21	1.28		-0.90	0.46	1.36	1803
1804	4.61	-0.98		-0.22	0.78		-0.35	-0.66	2.88	0.74	0.56	-1.56	1804
1805	-1.03	-0.28		-1.38	-2.16	-1.35	-1.28	-1.44	0.38	-2.73	-2.47	0.06	1805
1806	-2.78	2.77	1.10	-1.99	1.37	-0.27	-0.62	-0.59	-0.27	0.03	1.67	4.85	1806
	!												
1807	0.76	1.58	-2.43	-1.14	-1.02	-0.21	2.15	3.23	-0.74	1.71	1.37	-0.94	1807
1808	1.95	-1.23	-3.55	-1.35	1	-0.98	0.54	ļ.	-0.34		-0.17		1808
1809	1.56	3.64	0.69	-2.58	0.84	-0.65	-0.36	0.16	0.30	-1.05	-1.65	2.12	1809
1810	-1.56	-2.45	2.11	-4.12	-0.25	-0.95	-0.26	-0.48	2.08	0.09	1.44	0.97	1810
1811	-3.01	0.49	2.31	0.97	1.41	1.41	0.75	-0.38	-0.04	3.02	1.28	-0.04	1811
			1										
1610	-2.36	1.96	-0.23	9.1*	0.64	0.27	-1.85	1 17		0.01	-2.28	4.01	1010
1812	l l		ı	1	1	-1.45						1	1812
1813	-2.25		-0.42	0.53			1				-1.15	1	1813
1814 1815	-1.90	-3.96 1.26	-3.67 2.15	1.09 0.39	0.71	-1.52	-1.95		-1.56 -0.48		$0.69 \\ -2.30$		1814
1816	0.69	-2.37	l	-0.68		-0.42 -2.63		!	}		-2.30 -2.45		1815
1510	0.09	-2.57	-0.00	-0.03	_2.22	-2.03	-2.49	_≂.94	-0.00	-0.17	-2.45	-0.82	1816
1817	3.31	1.47	-0.71	-3.71	-1.78	0.92	-1.54	-0.97	1.08	-3.25	1.01	-0.49	1817
1818	2.67	0.40	0.41	1.33	-0.82	1.06	0.15	-0.91	-0.70	-0.91	1.62	-2.04	1818
1819	-0.61	1.54	0.89	1.21	0.29	0.36	1.02	0.36	-0.92	-0.02	-0.95	1.16	1819
1820	-1.64	-0.06	-2.16	1.31	-0.05	-1.91	-1.37	1.10	-1.84	-1.11	-2.81	-0.66	1820
1821	2.13	-2.72	0.19	1.52	-1.98	-2.26	-1.97	0.15	0.77	-0.62	2.42	3.25	1821
1822	2.11	1.58	2.61	0.51	1.43	2.90	0.08	-0.85	-0.48	1.33	1.82	-3.09	1822
1823	-2.76	1.25	-0.05	-0.77	0.92	-1.42	-1.19	0.25	-0.38	-1.03		1.70	1823
1824	0.79	0.79	1	-1.61	1	-0.98		-0.39	0.68	0.44	2.52	3.81	1824
1825	1.92	-0.37	-1.36	1.85	0.27	0.26	0.19	0.02	-0.61	-0.64	1.27	2.74	1825
1826	-4.81	1.06	1.16	0.19		0.54	1.70	1.78	1.51		-1.07	0.54	1826
1827	_0 10	-5.36	1.47	1.22	1.60	0.23	1 10	-0.45	0.08	0.67	-2.41	2.98	1827
1828	H	-0.35	0.61	0.54	0.43	0.23		-0.45 -1.10		-0.61		1.19	1827
1828	11	-0.55 -3.10	1		-0.36				-1.50	i .		-5.91	1829
1529	72.40	-5.10	-0.95	0.40	-0.50	-0.01	0.40	-1.13	-1.50	-1.00	-4.88	-5.91	1029

LXXXV.

South Germany. - Stuttgard (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
										1			
1830	-6.40	-3.47	$\stackrel{\circ}{1.62}$	2.06	0.90	-0.38	0 1.05	0.00	0 -1.43	-0.S9	0.90	-0.74	1830
1831	-0.73	1.25	1.68		-0.11	ł	1	-0.10	1	1	1	1.26	1831
1832			-0.64		-0.93	1				-0.78	1	0.05	1832
1833	-2.56		-0.99	1	f	}	1	-2.81	ì		}		1833
1834	5.05		-0.60	1	-	1		}		-0.06		-0.27	1834
1001													1001
!													
1835	1.53		-0.15	-0.90	-0.53			-0.21		1	i	-2.85	1835
1836	0.45	-1.27	3.18	-0.90	-2.14	0.64	0.22	1	-1.21		-0.01	1.04	1836
1837	0.90	0.24	-2.68	-2.84	-2.23	1.16	-1.19	1.17	-1.94	-0.60	-0.40	0.04	1837
1838	-4.43	-2.0 8	0.21	-2.32	-0.45	-0.03	-0.36	-0.90	0.64	-0.36	1.03	-1.34	1838
1839	0.78	-0.03	-1.31	-2.71	-1.07	2.30	0.58	-1.55	0.64	0.84	1.07	1.95	1839
1840	1.82	0.15	-2.90	1.36	0.29	0.16	-1.42	-0.23	-0.26	-2.39	1.10	-5.61	1840
1841	0.89	-1.98	2.09	0.53	3.42	-1.55	-1.83	-0.69	1.65	1.24	1.22	2.85	1841
1842	-1.50	-1.05	1.36	-0.47	1.35	1.74	0.35	2.64	0.07	-2.47	-1.82	-0.20	1842
1843	2.07	1.54	0.15		-1.06	-1.48	-0.68	0.20	-0.15	0.02	0.67	0.23	1843
1844	0.31	-0.91	-0.30		-1.01			-2.17	0.56	0.39	0.91	-3.18	1844
Means.	-0.80	1.64	3.97	7. S0	11.87	14.03	15.48	15.02	12.05	8.05	4.11	1.25	Means.

LXXXVI. South Germany - Carlsruhe.

1779	-3.98	1.18	1.26	2.19	1.14	-0.64	0.80	1.72	2.40	2.75	1.71	2.94	1779
1780	-2.23	-2.20	3.27	-1.17	0.52	0.41	0.27	1.39	0.18	0.83	0.00	-1.32	1780
1781	0.45	1.82	0.99	2.26	0.87	1.63	0.63	1.20	1.11	-0.94	-0.38	1.09	1781
1782	3.13	-3.95	-0.67	-1.10	-1.44	0.93	1.00	-1.62	-1.69	-2.08	-3.90	-1.07	1782
1783	3.33	1.35	-1.60	0.05	-0.14	0.47	1.69	-0.38	-0.71	-0.35	-1.04	-3.26	1783
						}							
1784	_4 05	_9 17	_1 67	_9 79	0 19	_0 19	_0.19	_1 07	-0 es	_2 71	-0.71	-2.14	1784
1785	1					l	-0.46		-0.05			-0.60	1785
1786	1	-3.00	-3.49	l	-1.35	1	-1.77					-0.18	1786
1788				0.70	1.55	1.20	1			1.5.	0.15	-8.65	1788
1789	-0.91	1	-3.15	1		-1.49		-0.14	1			0.91	1789
1100	0.51	1.17	0.10	٠.	2.13	1.40	0.54	0.14	1	••		0.01	11.00
			}										
1798							0.20	0.39	0.59	0.55	0.14	-1.90	1798
1799	-3.09	0.92	-0.59	-1.15	-1.43	-0.70	-0.60	0.20	0.01	0.12	-0.12	-4.22	1799
1800	2.53	-1.60	-2.25	3.40		i	-0.26	l		-0.43	1.15	0.21	1800
1801	3.13	0.68	1.95	0.32	0.98	-0.98	-0.15	-0.49	0.76	0.98	1.17	2.21	1801
1802	-2.69	0.64	0.83	1.08	-0.60	1.37	-0.97	2.33	0.23	1.38	-0.38	0.53	1802
	11												
1803	-1.27	-2.92	_1.30	1.11	-2.75	-0.71	0.63	0.54	-2.37	-0.90	0.52	1.99	1803
1804	ti .			1	i .	l	-0.56	1	l	1		-2.05	1804
1805	II .	1		1	ł .	l	-1.21	ı	1	į ·	i	-0.39	1805
1806	4.11		l	1	i	l	0.03	1	l	1	1	4.71	1806
1000			1 0.00				3.00	*****	100			لتنتيا	

LXXXVI.

South Germany. — Carlsruhe (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					De	grees or	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1807	0.02	1.11	-2.83	-1.34	1.19	-0.28	2.34	3.15	-1.57	1.30	1.21	-0.53	1807
1808	1.38	-1.25	-3.54	-1.63	2.40	-0.41	1.94	0.96	-0.54	-1.28	-0.24	-3.75	1808
1809	1.24	3.25	0.52	-3.16	0.41	-1.22	-0.61	-0.33	-0.80	-1.36	-1.90	1.60	1809
1810	-3.19	-2.78	1.26	-0.17	-0.60	-0.62	-0.65	-0.46	1.58	-0.05	0.84	1.69	1810
1811	-2.40	1.17	2.79	1.65	2.32	1.55	0.78	-0.29	0.53	2.92	1.21	0.48	1811
1812	-2.09	1.47	-0.16	-2.96	0.83	-0.50	-1.53	-0.27	-0.24	1.33	-1.42	-3.80	1812
1813	-0.84	2.15	0.57	1.50	0.12	-1.01	-1.75	-1.78	-1.15	0.27	-0.11	-0.89	1813
1814	-1.51	-3.24	-1.56	1.82	-1.68	-1.66	0.07	-1.12	-1.07	-0.68	0.82	2.67	1814
1815	-2.35	2.31	2.67	0.75	1.10	-0.57	-1.75	-1.03	0.09	0.62	-1.99	-1.02	1815
1816	1.38	-2.00	-0.27	0.27	-2.23	-2.48	-2.61	-2.16	-0.89	-0.33	-2.14	0.17	1816
1817	3.56	2.16	-0.36	_9 1.1	-1.63	0.87	-1.47	-1 40	1.60	-2.82	1.78	0.13	1817
1818	2.91	1.12	0.59	1.53	-1.44	1.00		-1.01	l	-0.63	1.49	-2.11	1818
1818	1.85	1.12	0.39	1.42	0.49	0.15	0.42	0.64		-0.15		0.31	1819
1820	-1.09	0.55	-1.35	2.19	0.22	-2.16	-0.96	0.66		-0.61	-1.80	0.00	1820
1821	2.31	-1.59	0.73	1.78	-1.87		-2.03	0.14	0.17	1	2.72	3.52	1821
1021	2.51	-1.55	0.75	1.70	1.07	2.01	2.00	0.14	0.17	0.00	2.,2	3.52	1021
1822	2.52	2.96	4.04	1.75	2.11	3.77	0.56	-0.14	0.46	1.19	2.66	-1.31	1822
1823	-2.23	2.20	1.05	-0.09	1.23	-1.02	-1.14	0.87	0.24	-0.27	-0.11	2.95	1823
1824	1.39	1.98	-0.10	-0.89	-1.13	-0.65	0.32	-0.22	1.04	0.66	2.68	4.09	1824
1825	1.92	0.28	-0.76	1.43	-0.15	-0.41	0.85	0.49	1.15	0.15	1.51	3.05	1825
1826	-3.48	1.35	1.13	0.20	-1.25	1.06	2.12	2.86	1.75	1.94	-0.21	0.93	1826
	ii .												
1827	-0.55	-5.10	1.19	1.50	1.25	1.01	2.06	0.00	1.15	1.34	-2.01	2.85	1827
1828	3.18	0.41	1.17	0.82	0.74	1.19	0.91	-1.22	0.48	0.28	-0.33	1.85	1828
1829	-2.12	-2.33	-0.05	0.72	-0.04	0.21	0.50	-1.17	-0.88	-0.60	i .	-4.97	1829
1830	-5.83	-2.98	2.14	2.21	0.81	-0.22	0.86	-0.13	-1.01	-0.17	1.31	-0.32	1830
1831	-0.98	0.96	1.68	1.83	-0.50	-0.61	0.38	0.40	-0.81	3.26	0.30	1.64	1831
1832	0.10	-0.27	0.23	0.96	-0.88	-0.49	-0.01	1.09	-0.59	0.18	-0.68	0.95	1832
1833	-2.63	3.41		-0.78	2.94	1.45	ı		-1.08	-0.17	0.51	4.43	1833
1834	5.74	0.29	i	-1.12	1.87	1.12	l	1.35	1.82	0.53	0.79	0.29	1834
1835	1.77	1.74		-0.90		0.13	1.46	-0.17		-0.83	-2.92	-2.23	1835
1836	0.43	-0.85	1	-0.66		0.17	0.21	0.17	1.67	0.82	0.66	1.56	1836
1000			J.21			"	"-"				5.00	1.00	1.500
1837	1.30	0.80	-1.86	-2.33	-2.05	1.26	-0.86	1.24	-1.66	0.28	0.46	0.72	1837
1838	-4.35	-2.13		-2.36		-0.21	-0.36	-1.20	0.44	-0.02	1.10	i i	1838
1839	0.88	0.67	-0.73		l	2.28	0.16	-0.47	0.09	1.20	1.49	2.20	1839
1840	1.37	-0.69	-2.82	ı	-0.51	0.23	1	0.34		-2.04	1.81	-5.32	1840
Means.	0.35	100	4.50		10.40	14.40	15.00	15 43	10.00	0.00	430	1.05	Means.
means.	-0.17	1.95	4.39	8.31	12.40	14.43	15.80	15.41	12.60	8.30	4.16	1.35	Means.
[t	1										<u> </u>	!!	1

LXXXVII.

NORTH GERMANY. - BERLIN.

Yor Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					1)6	grees or	Reaum	ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	С	0	0	
1719	2.44	0.21	1.50	0.69	1.45	2.38	3.13	1.86	0.08	0.66	2.09	1 1	1719
1720	2.27	0.40	1	0.70	1.34	0.94	2.01	0.31	0.10	1.62	-0.03	1.47	1720
1721	2.38	-1.80	-1.53	2.23	-0.91	1.21	-0.67	-0.17	0.54	0.40	1.69	0.07	1721
1728	1.50	-2.28	2.39	0.65	1.24	0.26	-0.38	-1.36	-0.10	0.66	-0.5S	-1.51	1728
1729	-3.18	-1.46	-3.57	-2.11	• •	• •	• •	• •	• •	• •	• •	• • •	1729
1730	1.64	0.20	0.29	0.70	0.00	0.12	-0.62	-0.03	-0.69	-2.55	1.99	-0.48	1730
1731	-2.00	-1.78	-0.67	-1.67	-1.33	-0.89				1.85	0.67	0.26	1731
1732	-1.50	1.34	1.05	1.34	0.29		-1.95			1.14	-0.78	-3.99	1732
1733	2.69	2.54	0.56	1.59	-1.77		-0.38			-0.53	0.21	2.46	1733
1734	0.40	2.51	1.86	0.55	-0.54		-0.62	-0.93	l .	0.65	-2.85		1734
	0,,0		1.00	0.00	0.0.	1.20	0.02	0.00		0.05	2.00	1.00	2.01
1735	1.79	0.30	1.81	1.49	-0.87	-0.33	-1.38	-0.84	0.91	-1.01	-1.07	-0.17	1735
1736	-0.08	-0.92	-0.73	0.85	-0.88		-0.24	0.64	1		-0.09	1 1	1736
1737	1.83	0.55	1.57	-1.36	0.77		-0.77		-0.10	-0.39	-0.83	-0.05	1737
1738	-0.55	0.55	1.11	1.54	-0.08	-0.42	-0.79	-0.38	-0.05	0.88	-2.21	0.90	1738
1739	-0.17	2.06	1.11	-1.65	0.64	-0.96	0.99	-1.23	0.91	-2.62	-5.35	-0.01	1739
1740	-6.61	-6.54	-3.28	-3.45	-3.49	-1.70	-0.96	-0.62	1.62	-3.12	-2.35	-0.18	1740
1741	-0.93	1.88	-0.71	-1.38	-1.90	-1.59	0.17	-0.54	-0.20	1.22	1.77	-0.16	1741
1742	-1.23	1.08	-0.99	-2.16	-1.83	-0.72	-0.66	-1.26	-1.78	0.19	0.70	-3.22	1742
1743	1.32	0.99	-0.53	-1.94	0.28	1.05	-1.46	0.32	-0.50	-1.44	2.77	0.84	1743
1744	-1.98	-2.42	-0.09	2.33	0.10	-1.47	0.25	-0.60	0.94	2.10	1.25	-0.39	1644
1745	-1.92		-0.10	0.20	0.73	1.01	0.01	0.17	0.10	1.15	2.17		1745
1746	0.12	0.03	l .	-0.39	0.43	-0.72	1.41	-0.43	0.44	-1.06	1		1746
1747	-0.17		-2.09	0.70	-0.67	2.34	-0.33	0.18	1.43	0.43	0.21		1747
1748	-1.17	1	-2.29	0.22	1.53	2.11	0.56	2.85	-0.14	0.00	1.79		1748
1749	2.28	0.47	-1.52	-0.14	1.58	0.21	0.39	1.64	0.33	0.05	-0.63		1749
1750	1.19	3.22	3.87	1.26	0.30	1.06	1.97	1.56	0.26	-0.55	• •	-0.06	1750
1751	-0.45	-1.70	2.79	-0.86	3.59	2.39	1.78	3.12	0.42	-0.04	• •		1751
Means.	-0.19	0.69	2.65	6.51	10.63	12.82	14.02	13.14	11.06	6.53	3.15	1.24	Means.
1755	-4.56	-6.47		0.54				-0.25				2.14	1755
1756	4.13	2.63	1.85	1.77	0.37	2.55	1	-0.35	1	1.62	ļ		1756
1757	1.17	2.37	1.71		-0.39	1.47	3.25	0.22	l .	-2.88	1.21		1757
1758	-2.57	-0.17	0.13	-0.21	1.08	0.18	-0.86	0.55		-0.97	0.16	1	1758
1759	3.26	1.79	1.18	l	-1.45	0.87	1.15	0.60		1.09			1759
								,					
1760	-0.56	-1.48	1	0.34	0.33	0.57	l	0.03	0.87	0.98			1760
1761	0.97	1.65	2.51	-0.01	1.55	1.95	-0.62	1.88	2.30	1	-0.12		1761
1762	2.11	-0.01	-1.88	1.88	0.42	0.27	-0.19	-1.45	0.23		-0.32		1762
1763	-2.25	3.02		l .	-0.34	0.17	0.92	1.32	1		-0.25		1763
1764	2.91	2.88	-0.10	-0.30	1.71	-1.94	1.43	-0.60	-1.70	-0.63	-1.32	-1.54	1764
1765	1.64	-2.90	1.70	0.78	-2.50	-0.88	-1.92	1.12	-1.16	1.20	0.15	0.03	1765
1766	-0.10	1	1	2.07	1.17	1		-0.25	0.73	-0.43	0.48	1 1	1766
1767	-5.54	i .	1	1	-1.03		i	0.88	1	0.95		-1.75	1767
	1		, 5.01	1			1 3.20	,					

LXXXVII.

NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						grees of	Treatain						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1768	-3.52	-0.98	-1.28	° -0.11	-0.68	-0.06	° 0.28	-0.0s	-1.03	-0.48	0.54	0.47	1768
1769		-0.74	0.75	0.14	-1.01	-1.01		-1.07	0.58	-2.26	0.26	0.84	1769
1770		-0.21	-3.16		-0.11	-1.20		-0.08	0.62	0.81	0.16	1.92	1770
1771	-1.24	-3.28	-3.40	1	i	-0.21		-2.12	-0.46	0.76	1	0.95	1771
1772	0.66	1.20	0.86	1	l .	-0.10		-0.41	0.60	1.62	1.89	1.38	1772
1773	2.50		-0.61	0.49		-1.22	-0.85	0.06	l	1	-0.92	2.21	1773
Means.	-0.13	1.64	3.87	7.71	11.94	15.23	16.18	15.34	12.12	7.73	4.38	1.85	Means.
1774	1.50	2.26	2.29	1.56	-0.05	0.69	-1.56	-1.92	-1.61	0.71	-3.70	-0.75	1774
1775	0.95	3.20	2.53	-0.65	-0.72	3.26	1.88	1.61	2.00	1.23	-0.84	2.16	1775
1776	-5.55	2.42	2.10	-0.13	-2.11	1.19	1.21	0.32	0.12	-0.47	0.70	0.54	1776
1777	0.04	-1.67	0.67	-1.12	0.52	0.04	-0.60	-0.01	-1.71	0.23	2.23	0.75	1777
1778	-0.58	-1.72	1.09	1.98	0.67	0.30	1.02	0.66	-0.67	-1.69	1.44	3.84	1778
1779	0.33	3.82	2.99	2.39	0.61	-0.30	0.74	1.71	1.59	1.95	0.90		1779
1780	-1.06	-2.02	3.37	-1.27	0.72	0.24	0.45	0.99	-0.03	1.46	1	1 1	1780
1781	-0.44	0.53	2.05	1.85	1.19	1.97	2.02	2.56	1.60	-0.39	0.80	1	1781
1782	3.15	-2.86	-0.39	-0.87	0.33	1.78	1.52	0.21	1.75	-0.30	-1.13	0.78	1782
1783	3.19	3.67	-0.58	0.86	1.38	2.71	1.45	0.71	0.36	0.34	0.50	-1.51	1783
1784	-3.97	-3.54	-1.68	-2.30	0.58	0.20	-0.75	-1.35	0.02	-2.21	1.29	-0.94	1784
1785	0.47		-5.74		-1.48	ł	-0.70	1	l	-0.34	ł	-1.42	1785
1786	1.81	-0.93		1.60	l .	0.54		-1.26	1	ł	-3.64	l l	1786
1787	-0.29	1.38	2.05	-1.31		0.99	ł	-0.59	1	1.32	0.69		1787
1788	2.46	-1.26	-1.47	0.10	0.45	1.64	1.64	-1.21	1.20	-0.35	-0.79	-8.64	1788
											0.00		
1789	-1.93	l .	-4.45	0.01	1.85	0.14	0.11	0.36	1.85	0.64	0.89	3.55	1789
1790	3.05	2.82	2.19	1	1.70	0.58		-0.54		-0.44		1.92	1790
1791	3.91	1.52	1.47	1.74	}	0.19	0.78	1.08	l		-0.89	1.35	1791
1792	0.53	-1.89	0.80	1	-0.81	0.83	1.59	l .	-0.98		-0.01	1.14	1792
1793	-0.70	2.14	0.61	-0.68	-0.58	-1.34	1.68	0.22	-0.83	1.99	0.99	2.05	1793
1794	1.18	2.56	3.66	3.12	0.18	1.77	2.79	-0.59	-1.62	0.37	1.53	-2.14	1794
1795	-5.23	-0.36	-0.84	2.88	-1.78	2.10	-0.92	-0.37	1.27	3.36		1 1	1795
1796	6.51	0.68	-1.70	-0.34	-0.46	0.38	0.48	1.33	1.74	0.07	-0.60	-1.82	1796
1797	1.60	1.89	0.66	1.09	1.41	-0.23	1.55	1.26	2.02	0.55	-0.80	1.81	1797
1798	1.79	1.57	-0.07	1.29	0.76	1.20	0.38	0.92	1.24	-0.17	-0.45	-3.54	1798
1799	-2.97	-4.47	-1.65	-2.12	-2.27	-1.53	-1.05	-0.32	-0.65	-0.70	0.48	-4.41	1799
1800	-1.12	-3.61	-4.09	4.43	2.33	-3.06	-1.99	0.22	0.67	-0.41	1.47	0.00	1800
1801	1.88	-1.02	1.84	0.05	3.00	-1.37	-0.61	-0.68	1.01	1.40	0.93	0.84	1801
1802	-1.00	0.50	1.65	0.45	-2.37	-1.01	-1.54	1.54	-0.08	3.04	0.78	1.81	1802
1803	-5.33	2.02	-0.16	2.84	-1.36	-1.46	2.03	1.80	-1.82	-0.45	0.68	-0.39	1803
1804	1.51	-1 19	-3.11	-1 06	1.04	-0.54	0.10	-0.73	1.17	-0.02	-2.40	-3.92	1804
1805	1	-1.46	t t	-1.58	1	-1.53		{	0.55	1	-2.58	1.24	1805
1806	3.02	0.94	i .	-2.82	1	$\begin{bmatrix} -1.33 \\ -2.26 \end{bmatrix}$)	0.33	-0.12	1.47	4.14	1806
1807	1.62	1	-1.97	j .	1	1	1	L	-2.15	0.08	1.11	1.53	1807
1007	1.02	0.18	-1.97	-1.45	-0.42	-1.50	0.42	0.12	2.19	0.08	1.11	1.99	1007

LXXXVII.

NORTH GERMANY. - BERLIN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

T					De	grees of	Keaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1808	0.83		-3.39			-0.42	1.19	0.69		-1.56	1		1808
1809	-3.31	1.64		-3.34		-0.89	-0.48	0.36	j.	-0.99	0.02	2.23	1809
1810	-0.99	-1.66	l	-1.41		-1.93		-0.47	1.16	-1.33	0.09	1.22	1810
1811	-2.93	-0.72	2.01	-0.15	3.07	2.67	0.94	-0.59	[-0.72]	2.21	0.35	1.50	1811
1812	-1.14	-0.27	-1.05	-3.98	-1.20	-0.68	-2.37	-0.78	-1.81	1.14	-1.57	-5.52	1812
1019	-1.20	2.38	0.24	1.00	0.72	-1.23	1 07		-0.82	-1.30	0.05	1.02	1019
1813 1814	-2.12		-2.78		-2.92		1		-2.23	-1.30 -1.21	0.55	1.02	1813 1814
1814	-2.12 -2.81	1.14	1.56	1	-0.15	0.61	ł	-1.54 -1.57		0.42	1		1
11	li .		l	1	1	!	l	1	f .	Į.			1815
1816	0.95	-2.27	-0.68			-1.54	l	-2.59	1	-1.23		1 1	1816
1817	2.58	1.79	-0.19	-3.86	-0.49	1.04	-1.57	-0.55	1.43	-2.57	2.37	-0.14	1817
1818	2.54	0.19	1.56	0.53	0.22	0.95	0.72	-1.41	0.14	-0.58	-0.60	-0.89	1818
1819	2.51	1.57	1.59	0.85	1.00	2.28	1.42	1.60	0.81	-0.41	-0.66	-2.61	1819
1820	-3.08	0.34	-0.02	1.52	0.91	-2.38	-2.08	1.23	-0.75	0.99	-1.57	-1.88	1820
1821	1.52	-1.05	0.14	3.28	-0.48	-2.17	-1.51	-0.78	0.91	1.33	3.27	3.44	1821
Means.	-1.59	0.30	2.28	6.89	11.36	13.73	15.16	15.00	11.83	7.16	2.61	-0.32	Means.
4													
1822	3.39	3.67	3.22	1.55	0.59	0.58	l	-0.19	l	1.36	1.58	1	1822
1823	-7. 56	-0.25	0.41	1	-0.26	l	-1.76	1	-0.34	0.66	1	1.12	1823
1824	3.67	2.45	0.29	1	-1.04	l	-0.56		1.27	0.56	1.96	2.69	1824
1825	3.92	0.92	-2.26	1	-0.15	-1.10	-0.47	0.05	0.54	-0.12	1.30	1 1	1825
1826	-3.44	1.98	1.15	-0.19	-0.24	1.20	3.03	3.00	0.35	0.71	-0.33	0.49	1826
1827	0.25	-4.90	1.25	2.29	1.98	1.33	0.80	-0.04	1.09	0.83	-2.24	1.16	1827
1828	-0.26	-0.55	0.67	1.22	0.33	0.30	1.17	-0.71	-0.15	-0.28	0.17	0.47	1828
1829	-2.87	-2.67	-1.23	0.41	-0.29	0.12	0.41	-0.56	-0.16	-1.62	-2.54	-8.25	1829
1830	-4.21	-2.70	1.09	1.53	0.30	0.07	0.35	-0.26	-0.57	-0.69	1.47	-1.79	1830
1831	-1.81	0.75	0.40	2,21	-0.94	-1.34	0.36	0.20	-1.22	1.77	-0.54	0.11	1831
1832	0.76	1.12	0.42	0.32	-1.43	-0.33	-2.40	0.22	-1.22	-0.35	-0.63	-0.24	1832
1833	-0.86	3.16		-1.82	3.46	1.33	-0.45	-3.12		l	0.14	2.48	1833
1834	4.73	1.31	1	-0.68	1.82	1.23	3.65	2.34	0.74	-0.33 -0.28	0.14	0.36	1834
1835	2.81	2.37	0.57	-0.91	-0.86	0.13	0.21	-0.59	1.22	-0.23	-2.71	-1.77	1835
1836	1.37	1.11	3.42	0.07	-2.55	0.13	-1.08	-1.49	-1.06	ı	-1.10	0.26	1836
1000	1.57	1.11	3.42	0.07	_2.00	0.20	-1.00	1.45	-1.00	1.00	-1.10	0.20	1050
1837	1.91	0.38	-1.98	-1.68	-1.42	-0.69	-1.11	1.20	-0.92	0.37	0.72	-0.87	1837
1838	-6.30	-3.63	0.42	-1.42	-0.24	0.35	-0.22	-1.78	1.27	-0.89	-1.14	-0.33	1838
1839	0.79	1.50	-1.98	-2.54	0.58	0.95	0.77	-0.44	1.10	0.15	1.10	-1.49	1839
1840	-0.09	0.65	0.23	-0.07	-0.03	0.16	0.27	-0.07	-0.05	0.09	-0.05	-0.33	1840
1841	-0.01	-4.03	0.91	1.01	2.51	-0. SS	-1.10	-0.01	0.58	1.29	0.75	1.62	1841
1842	-1.34	0.39	0.93	-1.52	0.75	-0.54	-0.84	3.13	0.42	-1.55	-2.82	0.71	1842
1843	2.40	2.45		0.44	-2.01	-1.00		1.17		-0.66	1.42	1.96	1843
1844	H	-0.96	-1.50	0.48	0.56			-1.60		-0.24	0.56	2.41	1844
1845	1.65	-4.55	-6.24	0.28	-1.48	0.49		-0.94	-0.93	-0.18	1.26	0.33	1845
Means.	-1.90	-0.15	2.74	6.88	10.92	13.94	15.04	14.43	11.75	7.97	3.25	1.32	Means.

LXXXVIII.

DENMARK. — COPENHAGEN.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

7						5.000	f Reaum						
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
1767	-3.89	0.34	0.52	0	° -1.83	0	0	-0.47	0.22	-0.75	° 1.58	-0.29	1767
1768	-0.67	-0.14	1	0.11	1	4	1	-0.59	ł.	4	0.57	ļ.	11
1769	1.74	0.79	I	0.30		I	ì	1	1	-0.49 -1.92	1	1.66 0.37	1768
1770	0.19	1		-0.77	-0.70 -0.32		1		1	1.38	i	l .	1769
1771	-1.20		1	-3.14	0.32	1.50	i .		1	i	-0.48 -1.11	0.69 1.10	1770
1771	-1.20	-2.10	-3.30	-3.14	0.27	1.50	-0.55 	2.04	-0.90	0.05	-1.11	1.10	1771
1772	-0.88	-1.71	-2.53	-1.72	-1.94	-0.51	-0.56	-0.59	0.83	1.49	2.39	1.33	1772
1773	1.78	-0.46	0.35	0.33	0.83	-0.54	0.50	1	0.45	1.73	i	0.94	1773
1774	-2.37	0.34	0.87	0.83	}	0.37	0.04		-1.07	-0.31		-2.55	1774
1775	-0.51	1.79	1.72		-0.09	2.13	1.39	1.72	2.60			0.71	1775
1776	-5.22	1.18	1.49		-0.87	1.61	2.30	1	0.59	0.67	0.77	0.69	1776
													1
1782	2.38	-0.61	-0.99	-0.62	-0.63	3.43	0.12	0.32	0.99	-1.09	-1.42	0.07	1782
1783	0.81	2.57	-0.38	2.01	1.97	2.36	3.05	1.56	1.67	1.91	-0.06	-0.87	1783
1784	-2.02	-0.59	-2.41	-1.51	0.24	0.07	-0.31	-0.21	0.18	-0.78	1.16	-0.76	1784
1785	0.53	-2.27	-2.96	-1.04	-1.52	0.78	-0.33	-0.46	0.10	-0.05	1.55	-0.20	1785
1786	0.13	0.06	-2.69	0.83	-1.08	1.48	-0.35	-0.41	-0.74	-1.21	-2.91	-0.04	1786
			1										
1787	0.94	2.21	2.09	-0.20	0.07	0.01		-0.31	0.58			0.26	1787
1788	2.02	0.63	-1.14	0.95	1.00	1.28		0.38	1.71	-0.31	1	-6.92	1788
1798	1.15	2.27	1.31	2.48	2.71	2.06	2.00	2.15	1.09	1.01	0.01	-2.29	1798
1799	-0.71	-4.50	-1.94	-1.59	-2.12	-0.44	-0.18	-0.43	0.21	0.56	1.27	-2.55	1799
1800	-0.96	-2.07	-3.57	2.60	1.77	-1.69	-0.89	0.42	0.21	1.19	1.78	1.20	1800
1801	1.28	0.75	2.82	1.44	9 02	-0.10	1.30	0.58	0.69	2.17	1.97	0.46	1801
1802	-0.56	1.04	1.90	1.74	I	-2.26		-0.56	-0.87	0.98	0.45	0.32	1802
1802	1	-1.58	-0.39			-2.02		-0.14	1	-0.90	1	-1.36	1802
1804	1	-1.35 -1.47	-1.82	-0.58	1	-0.57		0.12	1.23		-0.51 -1.74	- 11	1804
1805	-1.79			-1.03				-1.03	0.77		-0.56	0.77	1805
1000	-1.75	-2.02	0.20	1.03	-2.14	9.40	-1.40	-1.03	0.77	-2.55	-0.50	0.77	1809
	ĺ		.					1	ĺ				
1806	1.90	1.63	-0.49	-1.59	0.03	-2.28	-1.79	-0.08	1.32	0.35	1.27	2.54	1806
1807	1.75		-0.55	1		-1.60	- 1	2.54	-2.22	0.02	0.19	0.77	1807
1808	1.04	1	-1.30	l l	0.19	0.02	1.26	1.34		1	,	-2.42	1808
1809	-2.64	1	-0.42	i	- 1	ł	-0.89	0.47	- 1		-0.55 -0.23	1.65	1809
1810		-0.28		-1.19			- 1	-0.29			-0.23 -0.22	0.10	1810
1010	0.00	0.23	0.00	-1.13	-2.03	1.01	0.07	-0.29	0.01	0.19	-0.22	0.10	1010
1811	-0.65	0.23	2.46	-0.71	1.75	0.96	2.07	-0.32	-0.26	1.28	1.12	1.07	1811
1812	0.40	1.21	I	-2.62	,	I	- 1	-0.61	- 1			-3.56	1812
1813	0.23	2.66	1.50	- 1	-1.01	-1.00		-0.89		-2.01	0.20	0.97	1813
1814	-3.81	-4.01	-2.15		-2.99	-1.97		-0.87		-0.58	1.22	0.85	1814
1815	-0.67	1.47	1.82	- 1	- 1	- 1		-0.81		0.59		$_{-0.66}^{-0.65}$	1815
1019	0.07	1.41	1.02	00	0.20	1.20	1.00	0.01	1.11	0.00	0.20	0.00	1019
												- 1	
1816	0.72	-1.56	-0.05	-0.49^{1}	-2.69	-1.87	-0.49	-1.86	-0.89	-0.72^{1}	-0.95	$_{-0.31}$	1816
	1				1							31112	

LXXXVIII.

DENMARK. - COPENHAGEN (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Jan. 0 2.79 1.99 3.46	Feb. 0 2.98 1.73	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Voca
2.79 1.99 3.46	2.98								000.	2101.	200.	Year.
1.99 3.46			0 .	0	0	0	0	0 00	c	0	0	
3.46		1 1	-1.10			-1.53		0.62		1.41		1817
	1	2.40	-1.05		0.97	1.29	-0.24	0.69	0.87	1.48	0.20	1818
	2.30	2.39	1.56	1.25	1.69	1.58	3.28	1.46	-0.79		-1.26	1819
-1.67	0.51	0.52	1.55	0.25		-0.36		-0.60	-0.64	-0.56	-0.87	1820
0.36	0.16	0.24	2.24	-0.43	-1.77	-1.81	-0.86	0.67	1.62	1.68	2.47	1821
2.56	3.82	3.64	2.28	1.59	0.87	0.24	-0.17	-0.64	1.52	2.63	0.56	1822
-2.60	-0.08	0.70	-0.04	0.51	0.15	-0.94	0.41	0.47	1.02	1.88	1.74	1823
3.65	2.36	0.97	0.91	0.14	1.22	-0.61	-0.48	1.62	0.09	1.20	2.18	1824
				4.30	5.91	7.76	6.63				2.04	1826
0.16	-2. 30	0.59	2.14	1.44	1.93	0.09	-0.29	1.48	1.16	-1.20	2.30	1827
0.05	0.40	1.00	0.70	1 01	1.04	1.00	0.00	0.41	0.40	0.01	0.50	1000
11			1				1					1828
							1					1829
ll l	1	1 1	1	1			4				[]	1830
					i .						1 11	1831
1.52	1.73	1.55	1.84	-0.23	1.29	-0.94	-0.06	-0.98	0.60	-0.47	0.58	1832
0.05	1.50	-0.45	-0.72	2.32	0.72	0.79	-2.27	0.08	0.63	0.77	1.32	1833
2.26	1.71	2.23	0.90	1.98	0.72	3.60	3.26	0.11	-0.05	0.22	0.59	1834
ll l				-0.92		1.03	-0.57				-0.88	1835
li l	0.63	1 1	i I		1		1	1			0.09	1836
0.17			,		ł		}					1837
2.09		0.50	0.00	0.0=	0.70	0.00	0.05		7.00	0.01	0.05	1000
!!		1	1		l)					1 1:	1838
ři.	1		l			!						1839
1.1			l		1			i			1 1	1840
11	1)	ł				ı	!			1	1841
-0.26	1.43	2.05	0.61	1.78	-0.11	-0.99	2.73	0.31	-0.88	-1.57	2.36	1842
1.82	0.79	-0.33	0.46	-0.96	-0.25	-0.67	1.03	-0.20	-1.23	0.86	2.99	1843
0.07	-2.48	-1.50	0.74	1.49	-1.12	-2.17	-1.42	-0.62	-0.29	0.46	-1.43	1844
H	l		0.54	-1.01	0.20	0.22	-0.86	-1.26	-1.04	1.28	0.59	1845
-1.16	-0.80	0.55	4.45	8.98	12.45	13.81	13.50	10.86	7.05	3.12	0.68	Means.
	2.56 -2.60 3.65 0.16 -0.07 -1.14 -2.26 -1.60 1.52 0.05 2.26 1.87 0.29 0.17 -2.83 -0.17 -0.63 -1.14 -0.26 1.82 0.07 1.24	2.56 3.82 -2.60 -0.08 3.65 2.36 0.16 -2.30 -0.07 0.43 -1.14 -3.06 -2.26 -2.85 -1.60 0.61 1.52 1.73 0.05 1.50 2.26 1.71 1.87 2.16 0.29 0.63 0.17 0.54 -2.83 -4.85 -0.17 -0.38 -0.63 -0.39 -1.14 -2.52 -0.26 1.43 1.82 0.79 0.07 -2.48 1.24 -4.16	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$

LXXXIX.

France. — Paris.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Year. Jan. Feb. March. April. May. June. July. Aug. Sept. Oct. Nov. Dec.	Year.
1000 9.95 1.90 0.90 1.54 9.04 0.44 0.00 0.50 0.00 - 00 0.00	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1806
1807 0.34 1.39 -2.74 -0.63 1.28 -0.52 1.94 2.34 -2.08 1.15 -0.74 -1.75	1807
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1808
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1809
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1810
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1811
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1812
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1813
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1814
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1815
1816 0.54 -1.69 -0.71 0.10 -1.40 -1.83 -2.53 -2.37 -1.26 0.29 -2.24 0.07	1816
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1817
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1818
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1819
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1820
1821 1.02 -2.58 0.54 1.34 -1.95 -2.05 -1.39 1.20 0.85 -0.14 2.70 3.10	1821
1822 1.96 1.52 2.62 1.01 1.72 3.26 0.09 0.42 0.18 1.72 1.82 -3.42 1.23	1822
1823 -1.79 0.88 -0.14 -0.62 0.50 -1.69 -1.23 0.46 0.00 -0.58 -0.84 1.58	1823
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1824
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1825
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1826
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1827
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1828
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1829
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1830
1.550 5.15 2.55 2.55 5.15	1000
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1831
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1832
1833 -1.73 2.34 -1.82 -0.38 2.54 1.06 -0.24 -1.65 -1.53 0.57 -0.61 3.46	1833
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1834
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1835
$oxed{1}{1836} oxed{1}{0.55} oxed{-1.03} oxed{1.62} oxed{-1.02} oxed{-1.67} oxed{1.06} oxed{0.56} oxed{0.30} oxed{-1.24} oxed{-0.04} oxed{0.66} oxed{0.36}$	1836
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1836
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1837
$ \begin{vmatrix} 1638 & -3.21 & -3.03 & 0.20 & -2.32 & -0.63 & -0.52 & -0.42 & -0.12 & -0.04 & 0.74 & -1.45 \\ 1839 & 0.75 & 0.73 & -0.62 & -1.70 & -0.71 & 1.62 & -0.04 & -0.86 & 0.00 & -0.56 & 1.10 & 1.60 \\ \end{vmatrix} $	1838
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1840
100 000 000 100 000 4110	1040
1841 0.47 -1.35 1.94 0.42 2.25 -1.26 -1.68 -0.50 2.28 0.12 0.02 1.48	1841
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1842
1843 2.07 -0.39 1.06 0.50 -0.31 -0.86 -0.48 0.70 0.96 0.12 0.54 0.60	1843
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1844
Means. 1.53 3.35 5.33 7.90 11.59 13.66 14.96 14.82 12.52 9.00 5.41 2.92	Means.
Means. 1.53 3.35 5.33 7.90 11.59 13.66 14.96 14.82 12.52 9.00 5.41 2.92	means,

XC.

Holland. — Zwanenburg.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	ear. 743
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	4.4
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	745
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	47
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	748
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	749
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	750
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	751
$oxed{1754} oxed{0.64} -1.14 -2.23 -1.40 oxed{0.41} -0.49 -1.33 -0.16 -0.44 oxed{0.61} 0.05 -0.36 oxed{17}$	752
$oxed{1754} oxed{0.64} -1.14 -2.23 -1.40 oxed{0.41} -0.49 -1.33 -0.16 -0.44 oxed{0.61} 0.05 -0.36 oxed{17}$	
	753
	754
	755
	756
$oxed{1}{1757} oxed{0.22} -0.59 0.00 1.00 -1.01 -0.11 2.37 0.36 -0.21 -1.09 1.43 -0.09 1.43 $	757
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	758
	759
	760
	761
	762
1102 2.10 0.00 1.20 2.01 0.00 0.01 0.01	
7700 400 070 094 094 104 099 099 076 099 076 179 74	***
	763
	764
	765
	766
$oxed{1767} egin{array}{ c c c c c c c c c c c c c c c c c c c$	767
$oxed{1}{1768} oxed{1}{-1.94} oxed{0.93} oxed{-0.07} oxed{-0.09} oxed{-0.02} oxed{0.54} oxed{0.65} oxed{0.65} oxed{0.33} oxed{-1.27} oxed{-0.37} oxed{0.70} oxed{0.72} oxed{1}^{17}$	768
	769
	770
	771
	772
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	773
	774
	775
	776
	777
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	778
1779 -0.28 2.55 1.79 1.21 0.61 -0.77 0.60 1.51 1.27 1.61 0.19 0.53 1°	779
1780 -1.54 -0.56 2.68 -0.78 1.07 -0.51 -0.25 2.04 1.08 1.03 -0.07 -1.09 1	

XC.

Holland. — Zwanenburg (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

						egrees of	Reaum	ur.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1781	-0.97	1.18	1.18	1.23	1	2.47	1.04	1.56	0.91	0.75	0.36	-0.39	1781
1782	2.88	-1.88	-0.56	-1.11	-1.09	0.77	0.34	-0.54	0.50	-0.93	-2.43	-0.89	1782
1783	2.39	2.13	-1.31	1.24	-0.05	0.92	2.75	0.93	0.44	0.73	0.48	-2.74	1783
1784	-3.26	-3.01	-2.04	-2.16	1.23	0.15	-0.37	-0.80	0.94	-2.30	0.80	-1.60	1784
1785	-0.06	-2.34	-3.32	-1.54	-0.96	-0.46	-0.01	-0.59	1.14	0.40	0.41	-1.70	1785
		1	ł		l			1				1	
1786	0.35	-0.0s	-3.19	0.44	-0.59	0.72	-1.80	-0.75	-1.55	-1.49	-3.59	-0.23	1786
1787	-0.23	1.24	1.82	-0.90	-1.11		-0.82	l .	1.00			0.20	1787
1788	2.20	-0.42		0.24	0.58	1.05	0.87	ł.			-0.73	-6.23	1788
1789	-2.66	0.98	j .	-1.64	0.56		l	1	-0.40			1.84	1789
1790	2.20	2.51	1.53	i	0.89	1	-1.76		f	-0.86		0.89	1790
1.00	2.20	2.01	1.00		0.00	02	10	1.20	1	0.00	1	0.00	1100
1791	2.74	1.29	1.23		-1.21							-0.53	1791
1792	1.06	-0.38	0.03		-1.11		-0.07	0.27			-0.14	1.05	1792
1793	0.52	1.59	0.03		-1.61		0.67		-1.68	0.98	-0.17	1.60	1793
1794	-0.21	2.09	2.58		-0.76		1.52	-0.87	-1.14	-0.54	0.41	-2.08	1794
1795	-4.52	-1.53	-0.92	0.85	-1.88	-0.18	-2.29	-0.08	1.51	2.39	0.37	2.87	1795
1796	4.72	1.76	-0.99	1.00	-0.63	-0.50	-0.91	0.02	0.64	-0.80	-0.46	-2.07	1796
1797	0.84	1	-0.18	0.81		-1.18	1.38	0.01	-0.78	-0.60	0.32	1.59	1797
1798	1.45	1.73		1.22	0.11	1	-0.05	0.36	0.19	0.68	-0.17	1 1	1798
1799	-2.11	-2.00		-2.19		-1.83		-1.08	-0.72	-0.63	0.59	-3.54	1799
1800	-0.65	1		2.08		-2.10		0.04	0.50	0.02	1.12		1800
				0.00	0.00			0.00	۰				
1801	1	1	1.61	0.26		-1.43		0.32	0.45	1.16	0.53	0.47	1801
1802	-0.75	0.24	0.56	0.55				1.08	0.03	1.15	0.54	1.19	1802
1803	-3.04	-2.29	0.00		-1.55	-0.92	1.43	0.75	-1.11	0.06	0.29	0.43	1803
1804	3.30		-0.92	-0.84	1.35	0.26	0.03	-0.20	1.57	0.62	-1.7 9	-2.84	1804
1805	-1.22	-0.36	-0.07	-0.56	-2.16	-1.97	-1.18	0.05	1.47	-2.00	-1.69	0.94	1805
1806	3.14	1.58	0.25	-1.95	1.79	-0.52	0.13	0.67	1.41	0.23	2.52	4.12	1806
1807	2.36	1.74	-1.32	-0.37	1.09	-0.17	1.64	2.53	-1.40	1.63	-0.15	0.84	1807
1808	1.19	0.07	-1.71	-2.02	2.07	-0.46	2.62	1.64	0.24	-1.35	-0.05	-1.50	1808
1809				-2.53	1.30	-1.03	-0.47	0.09	-0.27	-1.32	-0.99	0.68	1809
1810	-1.94	-1.39	-0.36	-0.41	-1.76	-0.96	0.05	-0.07	0.99	-0.63	-0.03	1.06	1810
1811	-2.75	0.55	1.41	1.16	2.75	1.53	0.4~	-0.30		9 40	1.80	1.05	1011
1812	0.81	1.20	-1.21	-2.48						2.40		-4.00	1811
1813	-0.84	1.53	0.16	-2.48 0.04		-0.08	-1.28	-0.91		-1.32	-2.11 -0.76		1812 1813
1814	-3.33	-4.20	-2. S9	1.27	1	-0.32 -1.86		-0.66		-1.32 -1.44	-0.76 -0.17	0.17	1814
1814	-3.33 -2.69	0.96	2.39 2.23	0.59	1	1	-1.63				-0.17 -0.97	-1.90	1814
1019	2.09	0.00	2.20	0.09	0.00	0.00	1.00	-0.77	-0.94	0.07	-0.87	-1.90	1019
1816	0.52	-1.64	-0.78	-0.28	-1.48	-2.28	-1.31	-1.85	-1.14	-0.12	-2.06	-0.45	1816
1817	2.36	2.31		-2.12	1		-0.83	- 1		-3.16	1.83	-0.67	1817
1818	1.96	-0.40	0.40	-0.21	-0.56	1.69	0.99	-0.64	-0.36	-0.34	0.74	-1.22	1818

XC.

HOLLAND. - ZWANENBURG (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0		0	0	-0	0	0	0		-		0	
1819	1.47	1.04		0.84	0.91					-0.79			1819
1820	-2.89	-1.49	-1.21	0.72	0.12	-1.71	-1.06	-0.11	-0.93	-0.81	-1.84	-1.59	1820
1821	-0.67	-1.32	-0.16	1.66	-1.24	-1.91	-1.81	-0.14	0.72	0.20	1.72	2.08	1821
1822	2.64	1.93	2.26	0.40	1.53	1.65	0.24	-0.19	-0.88	0.74	1.99	-2.95	1822
1823	-6.29	-0.94	0.11	-1.19	0.44	-1.88	-0.89	0.12	-0.37	-0.66	0.90	1.65	1823
1824	2.30		-0.22			ì	1	i	1	1	1	1 1	1824
1825	2.63		-1.42		0.12		-0.04	1				1.70	1825
1826	-2.57	0.97	0.87	0.17	i		2.12	l	0.30	1.95	ĺ	1.99	1826
1827	il .	-3.83	1	0.93	,	-0.24	1	-0.55	i	0.88	1	2.79	1827
1828	0.75	-0.75	1.05	0.43	0.49	0.70	0.79	-0.64	0.43	0.24	-0.18	1.96	1828
								ļ					
1829	-3.35	-2.47	-1.43	-0.45	0.10	$ _{-0.37}$	-0.42	-1.35	-1.52	-0.43	-1.61	-5.77	1829
1830	1	-4.01	0.50			-1.45	1	1	-1.45		i	-1.80	1830
1831	-1.07	0.04			-0.10	1		í	-0.14	1	ł	1 1	1831
1832	-0.77		-0.43	}	-1.49	1		1		_	-1.37	0.72	1832
1833	-2.12		-1.62	1	l	1	-0.48	ł	1	0.11	ì		1833
1000		1.00	1.02	""		0.02		1	0.00		"	0.0.	1000
											-		
1834	4.21	0.40	1	-0.87							-0.31		1834
1835	1.21	1.81	0.47	-0.76	-1.09	0.92	0.47	0.07	-0.22	-0.77	-1.44	-0.44	1835
													1
Means.	0.99	3.14	3.86	6.80	10.12	12.45	13.97	14.13	12.30	8.61	4.84	2.16	Means.

XCI. ENGLAND. - LONDON.

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1794	-0.96	2.72	1.23	1.64	-0.99	-0.43	1.83	-0.38	-1.35	-0.61	0.36	-1.10	1794
1795	-5.04	-2.08	-1.26	-0.23	-0.46	-1.98	-0.04	0.11	1.76	1.61	-0.88	2.46	1795
1796	4.42	0.50	-1.00	1.10	-1.26	-1.00	-1.28	-0.51	1.23	-1.45	-0.97	-3.76	1796
1797	-0.01	-1.44	-1.51	-0.45	-0.70	-1.56	0.62	-0.82	-0.97	-1.34	-0.44	0.93	1797
1798	-3.44	-0.28	-0.12	1.41	0.44	1.31	-0.10	0.88	-0.11	0.09	-1.24	-2.39	1798
li l						ŀ							
1799	-1.00	-1.05	-1.74	-1.94	-1.39	-1.34	-0.79	-1.40	-1.19	-1.02	0.13	-2.79	1799
1800	0.59	-2.04	-1.70	1.14	0.66	-1.37	0.66	1.23	0.42	-0.86	-0.15	-0.24	1800
1801	1.64	-0.08	1.26	-0.35	-0.10	-0.09	-0.48	0.76	0.88	0.33	-1.08	-1.37	1801
1802	-1.21	0.11	-0.04	1.14	-1.50	-0.66	-2.20	1.74	0.49	0.23	-0.89	-0.56	1802
1803	-0.92	-1.03	0.51	0.88	-1.12	-0.89	0.97	0.41	-1.77	-0.40	-0.31	0.98	1803
							ĺ						
li i	1	ļ							ł		1		Į.
1804	3.39	-0.73	0.00	-0.95	1.80	1.07	-0.57	-0.20	1.16	0.66	0.68	-1.52	1804
1805	-0.52	0.04	0.34	-0.20	-1.38	-1.49	-0.89	0.60	1.15	-1.06	-1.17	0.08	1805
1806	2.27	1.27	-0.23	-1.21	1.00	0.64	-0.06	0.38	0.16	0.54	2.11	3.64	1806
1807	0.64	0.54	-1.80	-0.14	1.05	-0.34	1.07	1.36	-1.61	1.44	-1.60	-1.19	1807
1808	0.64	-1.01	-1.80	-1.43	1.99	0.02	1.87	0.82	-0.55	-1.76	0.58	-1.32	1808
1809	-0.11	2.36	0.65	-2.05	1.23	-0.38	-0.75	-1.09	-0.24	-0.08	-1.33	0.72	1809
<u> </u>	·	`	-	'		<u>'</u>			'		·		

XCI.

England. — London (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

					Deg	grees of	Reaumu	ır.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1810	-0.47	0.01	0.38	0.12	-1.44	i .		-0.16	1.32	0.95		-0.03	1810
1811	-1.09	0.85	1.54	1.64	2.03	0.51	0.36	-0.51	0.83	2.50	1.29	-0.16	1811
1812	0.42	1.43	-0.68	-1.56	-0.19	-1.09	-1.24	-1.89	-0.64	-1.10	-0.75	0.90	1812
1813	-0.51	1.34	0.87	-0.81	0.12	-0.96	-0.97	-1.00	-0.99	-1.05	-0.84	-1.01	1813
1814	-3.80	-2.21	-2.55	1.06	-1.66	-2.03	-0.04	-0.91	-0.72	-1.10	-0.75	0.90	1814
1815	-1.49	1.34	1.94	0.44	1.19	0.24	-0.53	-0.07	2.48	0.55	-1.42	-0.83	1815
1816	0.64	-0.70	-0.64	-0.50	-0.99	-1.27	-2.35	-1.18	0.96	0.28	-1.24	-0.48	1816
1817	1.84	2.05	0.25	-0.63	-1.75	0.77	-1.46	-2.60	-0.81	-1.76	2.14	-0.70	1817
1818	1.67	-1.32	0.03	0.04	-0.06	2.24	2.40	1.98	2.30	2.06	3.20	-0.08	1818
1819	2.29	0.85	1.36	1.37		-0.69	0.36	1.58	0.70	3.08	-0.75	-0.74	1819
1820	-1.44	_0 gg	0.25	1.68	-0.01	_0.71	_0.71	_1 19	-0.99	-0.96	-0.22	0.59	1820
1521	1.04		0.23	2.08	-1.26	l .	1	0.47	1.28	0.32	2.32	2.32	1821
1822	$\frac{1.04}{2.16}$	$\frac{-0.57}{2.19}$	2.78	0.48	1.45	1.57	0.36	0.29		1.04	2.36	-1.14	1822
i ii		0.19	1	-0.10	2.16	0.33	0.30	0.23	0.39	-0.56	0.54	0.55	1823
1823	-1.40			-0.10 -0.94		-1.40	0.00		0.39	-0.03	1.38	1.08	1
1824	0.78	2.41	-0.73	-0.94	-1.48	-1.40	0.00	-0.29	0.48	_0.05 	1.55	1.05	1824
1825	1.31	-0.21	-1.17	1.28	0.08	-0.03	1.47	0.38	1.63	0.32	-0.84	0.59	1825
1826	-1.49	1.61		1.46	1.16	1.97	1.69	1.67	0.30	1.28	-1.11	1.19	1826
1827	-0.96	-3.19	0.74	0.39	-0.08	-0.40	0.74	-0.73	0.21	0.84	-0.28	1.99	1827
1828	1.73	0.54	1.00	0.28	0.70	0.88	0.36	-0.62	0.52	-0.16	0.65	2.37	1828
1829	-1.76	-0.24	-1.08	-0.85	0.50	0.35	-0.48	-1.22	-1.41	-1.16	-1.60	-3.14	1829
1830	-2.31	-2.17	1.98	1.15	_1 20	-1.09	0.65	-1.09	_1 27	0.32	0.69	-2.12	1830
1831	$\begin{bmatrix} -2.31 \\ -0.73 \end{bmatrix}$	1.01	1.16	1.13	1	0.55	1.49	į.	-0.04	2.39	-0.08	1.21	1831
1832	0.13	1	-0.42	0.35	ı	0.57	-0.20	1	-0.04	0.52	0.47	1.08	1832
1833	-0.64	1.45	-0.42 -1.68	-0.10	2.72	0.66	-0.20	1	-1.41	0.32	0.16	2.21	1833
1834	3.73	0.48		-0.48	1	1.20	i		ł	0.10	0.10	0.35	1834
1994	3.75	0.40	1.10	-0.40	1.55	1.20	1.29	0.70	0.70	0.10	0.49	0.35	1094
1001		0.01	0.00	0.00	0.10	0	000	1 00	0.01		0.05		3005
1835	0.82	0.81		i	-0.12	0.71	0.87	1	1	-0.90	1	1 1	1835
1836	0.80	ł	l	-1.12	1	0.48	1	-1.11		1	1	0.28	1836
1837	0.73	0.74		-2.79	1	0.04		-0.16		1	-0.57	1.17	1837
1838	-2.93	-2.57	l .	-1.50		0.02		1	-0.92	ì	-0.68		1838
1839	0.73	0.14	-1.08	-2.48	-1.24	0.66	-0.35	-0.73	-1.06	-0.52	0.67	-0.21	1839
1840	1		-1.97	1	0.14	1	-0.77	1		-1.32	1	-2.41	1840
1841		-1.41	2.58	0.61	2.08	2.17	1		1	-0.01	0.40	1 1	1841
1842	-1.02	0.81	1.47	-0.43	0.59	2.84	0.18	2.11	0.19	-1.70	0.36	2.50	1842
Means.	2.38	3.81	5.00	7.30	10.46	12.92	14.26	14.07	12.06	8.88	5.51	3.81	Means.
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XCII.

SCOTLAND. - KINFAUNS CASTLE.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	(814) (815) (816) (817) (818) (819) (820) (821)
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1815 1816 1817 1818 1819 1820
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1816 1817 1818 1819 1820
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1817 1818 1819 1820
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	818 819 820
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	819 820
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	820
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	
1822 1.85 1.28 1.08 0.79 0.97 2.04 0.50 0.26 -0.81 0.48 1.38 -0.61 1	821
1823 1-0 91-1.69-0 16-0 60 0 63-1 01-0 92-0 85-0 15-0 56 9 92-0 91 3	822
1 100 0.10 0.00 0.00 -1.01 -0.00 -0.00 -0.01 -0.00 2.02 -0.01	823
$\parallel \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	824
$\parallel \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	825
$\parallel \ \ 1827 \ \parallel \ \ 0.68 \ -0.77 \ \mid \ \ 0.02 \ \mid \ \ 0.73 \ \mid \ \ 0.51 \ \mid \ \ 0.38 \ \mid \ \ 0.16 \ \mid \ \ 0.37 \ \mid \ \ 1.48 \ \mid \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	827
$\parallel \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	828
1829 -0.38 0.96 0.42 -0.48 0.87 1.00 -0.12 -0.44 -1.02 0.34 -0.19 0.02 1	829
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	830
$\parallel \ \ 1832 \ \parallel \ \ 1.91 \ \mid \ 1.27 \ \mid \ 0.92 \ \mid \ \ 1.22 \ \mid \ -0.19 \ \mid \ 0.50 \ \mid \ 0.24 \ \mid \ 0.93 \ \mid \ 1.35 \ \mid \ 1.53 \ \mid \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	832
	833
	.834
	835
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	836
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	837
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	838
$\parallel 1839 \parallel -0.90 \mid -0.79 \mid -1.56 \mid -1.24 \mid -1.18 \mid -0.45 \mid -0.34 \mid -0.79 \mid -0.64 \mid -0.17 \mid 0.11 \mid -0.35 \mid 1.00 \mid -0.00$	839
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	840
$\parallel 1841 \parallel -2.19 \mid -0.09 \mid 2.25 \mid -0.28 \mid 0.51 \mid -1.07 \mid -0.83 \mid -0.20 \mid 0.51 \mid -1.52 \mid -1.94 \mid -0.49 \mid 1$	841
	842
Means. 1.77 2.74 3.87 5.71 8.13 10.58 11.76 11.28 9.52 6.72 4.35 2.96 M	eans.
1111 2111 0.01 0.11 0.10 10.00 11.10 11.20 0.02 0.12 4.00 2.00	
XCIII. FINLAND. — TORNEA.	
1801 -0.01 -1.67 1	801
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	802
	803
$\parallel 1804 \parallel -2.50 \mid -4.82 \mid -2.34 \mid 1.99 \mid 1.50 \mid -0.97 \mid 0.78 \mid -0.70 \mid -0.21 \mid 1.19 \mid 1.46 \mid -4.01 \mid 1$	804
	805
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	806
	807
	808
	809
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	810
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	811
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	812

XCIII.

FINLAND. — TORNEÅ (continued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees	of	Reaumur.	
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					De	grees or	Reaumu	11.					
Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
										с		-	
1814	-7.01	$\overset{\circ}{2.71}$	$^{\circ}_{-1.85}$	$\stackrel{\circ}{0.92}$	-0.59	$^{\circ}_{2.44}$	4.65	$\overset{\circ}{4.46}$	$\overset{\circ}{2.60}$		-0.15		1814
1815	1.22	3.16	0.66	5.27	3.22	5.58	4.70	5.03	4.02	3.38	4.30	4.82	1815
1816	2.27		-4.25	0.50		-0.12		-0.41	1.97	0.16	1.17	2.29	1816
1817	3.54		-2.78	0.19		-1.14	i	-1.34	-0.36	-1.14	-0.07	-2.85	1817
1818	3.46	-3.34	-1.07	-2.61			l .	-2.55	0.09	1.08	2.89	5.83	1818
1010		0 7 7	0.50	2.0=	0.00		2 00	0.00			0.00	9.75	1010
1819	4.47		-0.50	1 -			2.90		-		-3.62		1819
1820	-5.74		-0.63					-0.17			-1.94		1820
1821	-2.18	1.12		l			-2.44	l	}		-1.52	-4.13	1821
1822	0.13	6.44	5.68	4.22	1.67	-1.39	-0.89	1.75	-0.14	0.47	-2.05	4.46	1822
1823	-4.01	-1.08	4.15	0.66	0.87	-0.43	-0.09	-0.73	-0.86	2.06	-1.38	1.26	1823
1824	0.71	4.20	1.75	-0.22	-0.40	0.29	-0.89	-0.73	1.25	-2.18	-1.01	-0.96	1824
1825	3.99	1.42	1.83	1.78	-0.29	-0.43	-1.53	-0.17	6.34	2.14	2.35	3.20	1825
1826	1.99	4.70	4.99	0.50	2.65	1.56	2.28	1.70	-0.70	2.67	3.23	3.74	1826
1827	0.03	0.00	0.59	-2.13	2.39	1.79	-2.00	-1.64	1.21	-1.53	-0.56	5.68	1827
1828	-0.50	-0.84	-1.77	-0.66	2.84	0.18	-1.73	-0.73	-2.86	1.18	0.50	1.69	1828
1829	1.26	-1.27	-2.69	-2.53	1.26	-0.31	0.30	-1.82	0.38	 -1.78	-0.53	2.86	1829
1830	0.99					1	-0.89	1	1	i	1		1830
1831	-3.98	-0.07			0.98				-0.54	i		1 1	1831
1832	5.26				0.10	1	1	1	-3.67	l .			1832
													7.5
Means.	-12.55	-10.76	-7.19	-1.62	4.01	10.59	13.05	10.81	6.22	0.26	-6.27	-10.32	Mean

XCIV. NORTH AMERICA. - ALBANY, N. Y.

Degrees of Reaumur.

					De	grees of	Reaum	ur.					
1826	1.92	2.44	1.65	-1.02	3.23	1.07	0.72	1.09	1.57	1.46	0.81	0.35	1826
1827	-2.91	1.07	1.15	1.62	-0.02	0.05	0.55	0.08	0.43	1.14	-1.72	0.77	1827
1828	2.80	4.52	2.10	-0.88	0.76	2.66	-0.41	1.33	0.35	-0.31	0.76	3.17	1828
1829	-0.21	-2.27	-0.87	0.12	2.09	0.03	-1.54	-0.42	-1.93	0.92	0.50	3.63	1829
1830	0.28	-0.11	1.41	3.64	-0.21	-0.92	0.81	0.27	0.19	1.42	3.83	4.71	1830
1831	-1.30	-1.03	2.77	1.89	1.07	2.11	0.32	1.01	1.00	1.52	0.63	-4.94	1831
1832		-0.87		-1.29	1			-0.31				ł 1	1832
1833	2.34	-1.34	-1.15	1.75	1.55	-2.35	-1.06	-1.47	-0.55	-0.55	-0.61	0.18	1833
1834	-1.18	3.73	0.67	0.68	-0.05	-1.12	1.59	-0.03	0.27	-1.31	-0.36	-1.13	1834
1835	-1.06	-1.50	-0.98	-1.59	-0.57	-0.34	-0.43	-0.90	-2.14	1.45	0.31	-3.06	1835
1836	 -0.35	-3.89	-3.48	-2.27	-0.95	-1.30	0.20	-2.39	-0.39	-3.06	-0.62	-0.92	1836
1837		-0.72	1					-0.98			1	-0.49	
1838	ll .	-4.01	l		-1.26	l .	1				1	-2.11	1838
1839	-0.25		f	1	-0.79		0.15	-0.14				-0.19	1839
1840	-3.32	3.14				-0.14	l	l		1	l	-1.26	1
1841	1.05	-0.72	1 10	_9 59	_1 19	1.90	0.	1.23	0.66	_1.79	-0.49	0.86	1841
1841	2.03				-1.13 -1.96			l .				-1.69	
1843		-3.06			1	l			ł	ľ	-1.00 -1.11	! !	1843
1844	13	-0.15	1		1	l	ì	-0.19	ľ	ł	-0.20	1	1844
1044	3.74	-0.13	0.27	2.91	0.47	-0.23		-0.13	0.72	0.02	0.20	0.47	1044
Means.	-3.58	-3.08	1.28	7.04	12.33	16.02	17.80	16.86	13.06	7.64	2.70	-1.65	Mea ns .

XCV.

NORTH AMERICA. - SALEM, MASS.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Tear Jam Feb March April May June July Aug Sept Oct Nov. Dec. Year	T						5,000 0	Reaum						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$											-			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	11	l	1		1		ł	1	1	l		1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ì	1	1		1	1	i	(l .	1	1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	l i		-	1	1	l	1	1	Į.			1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	11					ł.		1	i	l	1	1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1791	0.17	-1.48	0.90	0.64	1.50	1.16	-0.08	0.16	-0.69	-2.23	-0.42	0.07	1791
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1792	-2.94	-0.37	1.79	0.87	1.61	-0.84	-0.64	-0.28	-1.80	0.77	$ _{0.92}$	-1.15	1792
1794	1793	1.03	0.70	1.42	1.51	1	2.07	0.59	0.75	0.37	1	0.07	1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1794	0.95	-0.25	1.91	1.19	1.16	0.11	0.52	0.58	0.75	-1.26	-0.16	4.35	1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1795	0.20	-0.50	0.54	0.21	0.39	0.12	-0.31	1.85	1.04	1.24	0.36	1.51	1795
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1796	1.18	0.12	-0.37	1.17	-0.11	0.40	0.39	0.80	-0.06	-0.55	-1.26	-3.02	1796
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				l										
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$!!	1			í	l .		1	į.		1	1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1			l 1	1	l		i			ł	l	I .	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	11	1				i		}			i	l .		1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1		1		1		l					1	1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1801	0.40	0.46	1.51	0.21	1.69	0.08	0.35	0.49	1.41	0.96	0.17	0.30	1801
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1802	3.79	-0.16	0.76	0.31	-1.34	0.13	0.13	0.88	1.19	1.87	1.23	1.19	1802
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1)		1									1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1	ļ)					1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		1				l '			i .			i	1	t
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1806	0.48	1.60	-1.83		-0.44			1					1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$														
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	i (1 1										1 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1			!!!									1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1			1 1					1 1				1 1	!
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						i i							1 1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1811	0.30	0.14	1.69	-0.01	0.65	0.43	0.16	0.14	0.58	1.74	0.67	-0.34	1811
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1812	-1.51	-1.16	-2.68	-1.05	-3.22	-2.04	-2.13	-1.64	-2.07	-0.30	-0.90	-0.73	1812
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	}	-1.09	-0.34		1									
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1814	-0.73	0.80	-0.51					1				1 1	1 -
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1815	-0.93	-1.98	0.28	-1.47	-1.49	-0.16	1.12	-1.82	-0.50	-0.69	1.07	-0.45	1815
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1816	-0.16	0.07	-2.14	-0.44	-1.36	-2.36	-2.49	-1.31	-1.77	0.17	1.79	0.31	1816
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	101*	0 *1	9.40	_1 40	0.70	ابیا	1.05	0.50	0.00	0.30	0 -0	0.00	0.00	10.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						i i				- 1				f I
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1			1						- 1) 1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	1		l 1					1		1		1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1									- 1				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1021	J	1.50	0.00	0.91	-0.07	0.00	-1.03	0.53	-0.11	-0.03	0.42	1.91	1021
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	l 1		-0.50	1.64	-0.87	1.77	0.09	0.44	0.06	1.84	0.75	0.96	0.12	1822
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1			1			-0.42	-0.19	0.35	-1.63	-0.58	-1.72	0.52	1823
1826 0.96 1.11 0.10 -1.05 2.95 0.04 1.56 -0.13 0.78 0.23 0.19 0.55 1826 1827 -1.49 0.52 0.64 1.56 -0.03 -0.60 -0.35 -0.82 -0.28 1.13 -2.74 0.01 1827 1828 2.42 4.05 1.10 -0.97 -0.68 1.06 0.36 0.96 0.37 -0.19 1.17 2.04 1828	1 1	1 1		-0.11	0.62	-0.84	-0.59	-0.14	-1.08	0.12	0.21	-0.61	1.43	1824
1827 1828	1			1		1	- 1		j.					1 1
1828 2.42 4.05 1.10 -0.97 -0.68 1.06 0.36 0.96 0.37 -0.19 1.17 2.04 1828	1826	0.96	1.11	0.10	-1.05	2.95	0.04	1.56	-0.13	0.78	0.23	0.19	0.55	1826
1828 2.42 4.05 1.10 -0.97 -0.68 1.06 0.36 0.96 0.37 -0.19 1.17 2.04 1828	1827	-1.49	0.52	18.0	1.56	-0.03	-0.60	-0.35	-0.82	-0.28	1.12	-2.7.1	0.01	1827
	1			i	i i									
\mid Means. \mid \mid $-2.84' - 1.85' - 1.54 \mid -6.36' 11.05' 15.61 \mid 17.97 \mid 17.17 \mid 13.80 \mid -8.56 \mid -3.53 \mid -0.63 \mid $ Means. \mid														
	Means.	-2.84	-1.85	1.54	6.36	11.05	15.61	17.97	17.17	13.80	8.56	3.53	-0.63	Means.

XCVI.

ICELAND. — REIKIAVIK.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

Year.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Year.
	0	0	0	0	0	0	0	0	0	0	0	0	
1823	1.80	-0.56	0.40	2.09	-0.60	0.06	2.44	1.76	0.84	-1.50	0.18	-0.86	1823
1824	-0.32	0.61	-0.05	2.16	2.95	4.63	3.12	1.53	-0.73	-2.37	-3.64	-3.99	1824
1825	-1.07	-0.40	3.04	0.98	0.50	0.33	1.70	0.66	2.34	1.68	-0.81	-0.92	1825
1826	-0.19	2.84	2.15	-0.79	1.58	-1.10	-0.75	-0.18	1.24	1.12	0.36	1.17	1826
1827	-0.72	1.93	-3.80	-0.86	0.67	0.86	0.14	1.73	0.64	2.29	2.26	0.88	1827
1828	1.98	2.48	1.54	1.29	2.37	0.53	3.15	3.98	3.07	3.26	0.94	2.77	1828
1829	1.02	-0.09	0.20	0.56	0.79	0.26	1.21	2.21	-0.20	-1.16	0.03	1.86	1829
1830	1.89	-0.58	-1.22	-0.72	2.44	0.52	-0.80	0.68	0.85	2.09	-0.35	-2.60	1830
1831	0.28	-0.95	2.58	1.39	-1.76	1.44	-1.89	-1.85	-0.37	0.95	-0.76	1.45	1831
1832	0.71	-0.48	-1.77	0.17	-2.20	-1.87	-2.50	-2.94	-2.59	-0.42	1.22	-0.29	
													1832
1833	1.41	-0.1 3	1.93	-0.21	-0.57	-0.40	-1.96	-2.14	-1.22	-0.79	0.31	-1.64	1833
1834	-0.43		}	1	l	-1.99	l	1	i	l	1		1834
1835	11		-1.55	ł .	l	l	l .	ļ	1	l			1835
1836	11	ł	-2.00		l	l	i	1	ŀ	l .		1 1	1836
1837	-0.42	(-2.23		l	i	ı		1.00				1837
1001		0.40					0.40						
Means.	-1.00	-1.60	-1.07	1.84	5.54	8.67	10.78	9.27	6.42	2.19	-0.60	-1.15	Means.
	"		·		·								

XCVII. GREENLAND. — GODTHAAB.

Degrees of Reaumur.

1796										-2.52	1.51	2.19	1796
1797	0.91	-2.08	-0.73	-1.96	1.14	0.27	1.40	1.31	0.77	1.02	2.22	0.87	1797
1798	-1.30	0.53	3.98	0.08	0.37	-0.39	0.39	0.07	-0.37	-0.67	0.83	-0.08	1798
1799	-0.40	3.08	-1.87	0.47	0.37	-0.71	-0.47	-0.72	0.62	-0.43	-0.91	4.72	1799
1800	2.75	0.22	2.32	-0.68	1.52	1.05	0.35	0.88	-0.42	0.48	0.05	0.07	1800
1801	-0.86	2.63	0.00	-1.00	-2.86	-1.61	0.89	0.92	-0.39	0.19	0.22	1.94	1801
1802			-3.76										1802
1816		1								ľ	-0.01		1816
1817			-4.17		l					l	1	-1.73	1817
1818			-4.00				0.52		l .	l	-1.82		1818
10.0			2.00										
		001	0.05	0.00	0.03		0 -0	2 20	0.00	3.50		9.15	1010
1819	-2.74		-0.35		i .		-3.7S		l			1 1	1819
1820	4.16	l	l	-2.15	l	l .	-0.96	-1.57	-0.72	-0.06		1 1	1820
1821	0.04	0.42	1.30	1.00	-0.07	0.68	• •	• •		1	• •	• •	1821
1841									0.45		-0.27	0.23	1841
1842	1.13	-1.15	-1.12	1.56	2.03	0.37	0.89	0.34	1.39	1.95	-0.37	-1.37	1842
,		}				1					1		
1843	0.11	4.74	4.65	2.18	1.18	1.16	1.52	0.72	1.57	1.66	-2.89	-3.93	1843
1844	-0.13	0.40	-0.51	l .	1	Į	l .	l .		0.19	-1.08	0.01	1844
1845	1.54		1		1	0.32						1	1845
Means.	-8.72	-8.64	-7.29	-4.44	0.07	3.15	4.41	3.93	1.62	-0.96	-4.47	-6.45	Means.

CORRECTIONS

FOR

FORCE OF VAPOR AND RELATIVE HUMIDITY.

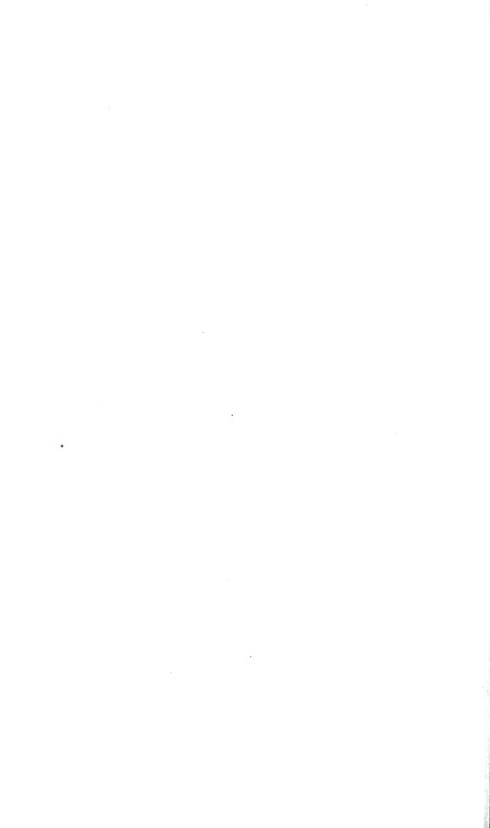
HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

OR

TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN FORCE OF VAPOR AND RELATIVE HUMIDITY OF THE DAY, OF THE MONTH, AND OF THE YEAR.

 \mathbf{E}



XCVIII.

England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Force of Vapor for the respective Months. (GLAISHER.)

English Inches.

Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
	Inch.	Inch	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
Midn	.006	.006	.008	.017	.026	.031	.028	.025	.024	.018	.010	.009	.017
1	.011	.008	.010	.021	.028	.037	.031	.031	.030	.020	.012	.010	.021
2	.015	.010	.011	.024	.031	.043	.036	.035	.035	.021	.015	.010	.024
3	.015	.011	.013	.027	.032	.048	.038	.039	.037	.023	.017	.011	.026
4	.015	.013	.015	.029	.031	.047	.037	.040	.040	.025	.019	.011	.027
5	.015	.014	.016	.029	.027	.037	.031	.038	.040	.023	.021	.011	.025
6	.014	.015	.016	.025	.019	.022	.019	.029	.033	.021	.021	.010	.020
7	.013	.014	.014	.016	.007	.008	.007	.014	.022	.018	.018	.009	.013
8	.010	.010	.010	.005	005	004	004	.000	.010	.011	.012	.007	.005
9	.007	.006	.005	.005	016	015	014	012	005	.005	.005	.005	002
10	.002	.000	003	013	024	027	019	021	019	005	004	.001	010
11	004	005	007	020	028	036	025	027	027	009	010	004	017
Noon		009		026								007	
1	008	013	013	027									
2	007	015						 034					
3	007	012	012	025	026	039	033	031	027	014	016	0 08	021
4	007	010	010	020						009	010	007	017
5	004	006	006	014	015	025	021	020	017	006	005	005	012
6	002	004	002	006	010	017	016	015	010	004		 003	1
7	001	001	.002	.001	004	007	007	006	003	.003	.004	001	002
8	.000	.001	.004	.005	.005	.005	.004	.004	.004	.005	.006	.001	.004
9	.000	.003	.005	.007	.013	.015	.010	.010	.008	.008	.008	.004	.007
10	.001	.004	.007	.010	.017	.023	.017	.015	.013		.009	.005	.011
11	.002	.005	.008	.014	.022	.029	.024	.020	.018	.014	.010	.006	.014
		į		ŀ									
						000			0.0	000	0.70	00.	000
6. 6	.006	.005	.007	.009	.005	.003	.001	•007	.012	.008	.010	.004	.006
7. 7	.006	.006	.008	.009	.001	.000	.000	.004	.009	.011	.011	.004	.005
8. 8	.005	.005	.007	.005	.000	.000	.000	.002	.007	.008	.009	.004	.005
			00=	000	000	000	000	001	000	000	00*	.004	.003
9. 9	.003	.004	.005		002	1	002		.002 003	.006	.007	.003	.000
10.10	.001	.002		002	003		001 006	1	.000	.003	.002	.003	(
7. 2. 9	.002	.001	.002	001	003	007	000	003	.000	.003	.002	.002	.001
6. 2. 8	.002	.000	.002	.001	 001	- 005	004	 000	.003	.003	.002	.001	.000
i I	ll .	.000	.002		.002	.001	.001	.003	.006	.005	.002	.002	.003
6. 2.10 6. 2. 6	.003	001	.003	ł		i	010		l .	.000	.000	000	1
0. 2. 0	.002	001	.000	003	000	019	010	.507	002	.500	.500	.550	
7. 2	000	000	.000	005	011	017	01.1	010	003	.000	001	.000	005
8. 2	.003	1		011							1	l .	009
8. 1	.001	001		011								l .	009
7. 1	.001	.000	1	005		1	1	(1			1	005
	.002	.500											
9.12.3.9	002	003	003	010	015	020	016	016	013	004	005	001	009
						1			1	1	<u> </u>		

XCIX.

England. — Greenwich. Lat. 51° 29' N.; Long. 0° 0'.

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours to obtain the true Mean *Humidity* for the respective Months. (Glaisher.)

Thousandths.

						housand							
Hours.	Jan.	Feb.	March.	April.	May.	June.	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Mean.
Midn	013	021	063	095	087	105	091	096	080	053	018	011	061
1	.002	021	065	106	100	114	095		080	!	009	012	064
2	.004	026	066	116	108	125	107	11 3	085	066	011	017	069
3	003	033	067	123	113	132	116	117	091	070	020	019	075
4	 013	036	068	126	114	138	120	123	097	075	030	024	080
5	019	035		125	106		120		098				080
6	021	034	063	112	085	107	097	107	097	071	033	026	071
7	020	030	055	080	059	065	055	061	080	058	031	025	052
8	020	020	025	065	024	015	005	020	047	037	021	018	027
9	020 017	020	0 03	ı	.018	.035	.041	.030	.000	1	00S	007	.003
10	004	.009	.031	l	.051	.035	.080	.030	.042	.025	l .	.008	.032
11	.011	.028	.060	1	.083	.100	.104	.102	.082	.060	l .	.022	.052
**		•040				.100	•104	1102	1302	.550			
Noon	.031	.045	.084	.070	.110	.123	.114	.127	.115	.088	.040	.033	.082
1	.054	.058	.100	.132	.126	.137	.119	.142	.131	.109	.050	.046	.100
2	.059	.065	.106		.125	.135	.123	.145	.132	.113	.054	.048	.105
3	.048	.065	.104	.147	.118	.123	.121	.138	.126	.108	.047	.036	.098
4	.036	.053	.087	.128	.108	.113	.111	.120	.103	.089	.032	.024	.084
5	.021	.032	.063	.110	.091	.099	.095	.100	.071	.055	.018	.013	.064
6	.007	.009	.038	.088	.074	.078	.062	.071	.044	.030	.005	.004	.042
7	005	010	.010	.059	.052	.049	.025	.036	.009	.007	005	003	.019
8	014	023	010	.020	.022	010	015	000	015	- 011	_ 019	 005	004
9		029		1 !		l .	019 040		040	}		1	
10	019	030		058	050		068	067		039			
11	018	036		080		ı	080	1	071	l .	020		
6. 6	007	019	010	012	_ 005	- 015	017	- 019	_ 027	_ 020	_ 014	_ 011	- 015
7. 7	012	020		012 010		008	1		1				017
8. 8	! !	021						010					016
9. 9	016	,	1	032	.000	.005	.000		020		012	007	1 1
10.10	011	010	1	037	.000	.009	.006	•001	008	007	006	.000	
7. 2. 9	.008	.002	.006	.014	.016	.015	.009	.015	.004	.010	.002	.005	.009
6. 2. 8	.008	.003	.011	.019	.021	.013	.004	.013	.016	.010	.003	.006	.010
6. 2.10	006	.000	002	006	003	010	014	009	008	.001	.000	.005	003
6. 2. 6	.015	.013	.027	.042	.038	.035	.029	.036	.026	.024	.009	.009	.025
7. 2	.019	.017	.026	.036	.033	.035	.034	.042	.026	.027	.012	.011	.026
8. 2	.019	.022	.036	.043	.050	.060	.059	.062	.042	.038	.016	.015	.039
8. 1	.017	.019	.032	.034	.051	.061	.057	.061	.042	.036	.014	.014	.037
7. 1	.017	.014	.023	.026	.033	.036	.032	.041	.025	.026	.009	.010	.024
9.12.3.9	.011	0 18	.038	.038	.032	.064	.059	.064	.050	.040	.016	.014	.037

METEOROLOGICAL TABLES.

VI.

MISCELLANEOUS TABLES,

USEFUL IN

TERRESTRIAL PHYSICS AND METEOROLOGY.



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1.

POSITIONS OF THE PRINCIPAL OBSERVATORIES.

[From the American Nautical Almanac.]

(North Latitudes and West Longitudes are considered as positive.)

Place.	Latitude.	Longitude from Washington in Time.	Longitude from Washington in Arc.	Longitude from Greenwich in Arc.
Åbo,	+60 26 56.8	h. m. s. - 6 37 20.0	260 40 0.6	337 42 48.6
Altona,	53 32 45.3	5 47 57.4	273 0 39.8	350 3 27.8
Athens,	37 58 20	6 43 6.4	259 13 24.2	336 16 12.2
Berlin,	52 30 16.7	6 1 46.1	269 33 28.1	346 36 16.1
Bilk,	51 12 25	5 35 16.1	276 10 58.1	353 13 46.1
Bonn,	$50\ 43\ 45.0$	5 36 35.7	275 51 5.1	352 53 53.1
Breslau,	51 6 56.0	6 16 21.2	$265 \ 54 \ 42.0$	342 57 30.0
Brussels,	50 51 10.7	5 25 38.8	278 35 18.0	355 38 6.0
Cambridge (Eng.),	52 12 51.8	5 8 34.7	282 51 18.9	359 54 6.9
Cambridge (Mass.),	+42 22 48.6	0 23 41.5	354 4 36.9	71 7 24.9
Cape of Good Hope,	-33 56 3	6 22 7.2	264 28 12.3	341 31 0.3
Christiania,	+59 54 43.7	- 5 51 6.0	272 13 30.6	349 16 18.6
,			7 26 42.8	
Cincinnati,		+ 0 29 46.9		84 29 30.8
Copenhagen,	55 40 53.0	- 5 58 30.5	270 22 22.5	347 25 10.5
Cracow,	50 3 50.0	6 28 2.4	262 59 23.4	340 2 11.4
Dorpat,	58 22 47.1	6 55 5.8	256 13 33.6	333 16 21.6
Dublin,	53 23 13	4 42 49.2	289 17 42.0	6 20 30.0
Durham,	54 46 6.4	5 1 53.2	284 31 42.0	1 34 30.0
Edinburgh,	55 57 23.2	4 55 28.2	286 7 57.0	3 10 45.0
Florence,	43 46 40.8	5 53 12.9	271 41 47.1	348 44 35.1
Geneva,	46 11 58.8	- 5 32 48.9	276 47 46.S	353 50 34.8
Georgetown,	38 54 26.1	+ 0 0 6.2	0 1 33.0	77 4 21.0
Göttingen,	51 31 47.9	- 5 47 57.3	273 0 40.5	350 3 28.5
Gotha,	$50 \ 56 \ 5.2$	5 51 6.9	272 13 17.1	349 16 5.1
Greenwich,	51 28 38.2	5 8 11.2	282 57 12.0	0 0 0
Hambuna	53 33 7	- 5 48 4.8	272 58 48.6	350 1 36.6
Hamburg,		+ 0 17 32.1	4 23 0.9	81 25 48.9
Hudson,		- 8 24 43.1	233 49 13.1	310 52 1.1
Kasan,				339 29 54.6
Königsberg,	54 42 50.4			345 51 38.7
Kremsmünster,	48 3 23.8	6 4 44.6	268 48 50.7	940 91 95.7
Leipsic,	51 20 20.7	5 57 39.7	270 35 4.5	347 37 52.5
Leyden,	52 9 28.2	5 26 8.6	278 27 50.6	355 30 38.6
Liverpool,	53 24 47.7	4 56 11.1	285 57 13.7	3 0 1.7
London,	51 31 29.8	5 7 34.1	283 6 28.5	0 9 16.5
Madras,	+13 4 9.2	-10 29 8.2	202 42 57.0	279 45 45.0

Place.	Latitude.	Longitude from Washington in Time.	Longitude from Washington in Arc.	Longitude from Greenwich in Arc.
Mannheim,	+49 29 12.9	h. m. s. -5 42 2.7	274 29 19.5	351 32 7.5
Markree,			291 24 18.0	
Marseilles,	54 10 31.7		277 34 57.2	8 27 6.0
Milan,	43 17 49			354 37 45.2
Modena,	45 28 0.7			350 48 20.4
Modena,	44 38 52.8	5 51 55.2	272 1 12.5	349 4 0.5
Moscow,	55 45 19.8	7 38 28.5	245 22 52.7	322 25 40.7
Munich,	48 8 45	5 54 37.6	271 20 35.4	348 23 23.4
Naples,	40 51 46.6	6 5 12.1	268 41 58.1	345 44 46.1
Olmiitz,	49 35 40.0	6 17 11.3	265 42 10.5	342 44 58.5
Oxford,	51 45 36.0	5 3 8.6	284 12 51.0	1 15 39.0
Padua,	45 24 2.5	5 55 40.2	271 4 56.6	348 7 44.6
Palermo,	+38 6 44	-6 1 36.7	269 35 50.1	346 38 38.1
Paramatta,	-33 48 49.8	+8 47 42.6	131 55 38.3	208 58 26.3
Paris,	+48 50 13.2	-5 17 32.7	280 36 50.1	357 39 38.1
St. Petersburg,	59 56 29.7	7 9 24.7	252 38 49.8	329 41 37.8
Philadelphia,	39 57 7.5	0 7 33.6	358 6 35.4	75 9 23.4
Prague,	50 5 18.5	6 5 53.2	268 31 42.6	345 34 30.6
Pulkowa,	59 46 18.7	7 9 29.9	252 37 31.9	329 40 19.9
Rome,	41 53 54	5 58 5.9	270 28 31.5	347 31 19.5
San Fernando,	+36 · 27 45	4 43 22.1	289 9 29.1	6 12 17.1
Santiago,	-33 26 24.8	0 25 52.3	353 31 55.5	70 34 43.5
Senftenberg,	+50 5 10.1	6 14 1.1	266 29 43.1	343 82 31.1
Vienna,	48 12 35.5	6 13 43.7	266 34 4.1	313 36 52.1
Washington,	38 53 39.3	0 0 0	0 0 0	77 2 48.0
Wilna,	+54 40 59.1	-6 49 23.0	257 39 15.5	334 42 3.5
	1			

II. TO CONVERT PARTS OF THE EQUATOR IN ARC INTO SIDIREAL TIME, OR TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

					D	EGREES.					
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.
1	0 4	41	2 44	81	5 24	121	8 4	161	10 44	201	13 24
2	0 8	42	2 48	82	5 28	122	8 8	162	10 48	202	13 28
3 4	0 12 0 16	43 44	$\begin{array}{cccc} 2 & 52 \\ 2 & 56 \end{array}$	83 84	5 32 5 36	123 124	8 12 8 16	163 164	10 52 10 56	203 204	13 32
5	0 20	45	3 0	85	5 40	125	8 20	165	11 0	204	13 36 13 40
	0 20	4.0	5 0		3 40	120	0 20	103	11 0	200	15 40
6	0 24	46	3 4	86	5 44	126	8 24	166	11 4	206	13 44
7	0 28	47	3 8	87	5 48	127	8 28	167	11 8	207	13 48
8	0 32	48	3 12	88	5 52	128	8 32	168	11 12	208	13 52
9	0 36	49	3 16	89	5 56	129	8 36	169	11 16	209	13 56
10	0 40	50	3 20	90	6 0	130	8 40	170	11 20	210	14 υ
11	0 44	51	3 24	91	6 4	131	8 44	171	11 24	211	14 4
12	0 48	52	3 28	92	6 8	132	8 48	172	11 28	212	14 8
13	0 52	53	3 32	93	6 12	133	8 52	173	11 32	213	14 12
14	0 56 1 0	54	3 36 3 40	94	6 16 6 20	134 135	8 56 9 0	174 175	11 36	214 215	14 16
15	1 0	55	3 40	99	0 20	199	9 0	175	11 40	219	14 20
16	1 4	56	3 44	96	6 24	136	9 4	176	11 44	216	14 24
17	1 8	57	3 48	97	6 28	137	9 8	177	11 48	217	14 28
18	1 12	58	3 52	98	6 32	138	9 12	178	11 52	218	14 32
19 20	$\begin{array}{c c} 1 & 16 \\ 1 & 20 \end{array}$	59 60	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	99 100	6 36 6 40	139 140	$\begin{array}{c c} 9 & 16 \\ 9 & 20 \\ \end{array}$	179 180	$11 ext{ } 56$ $12 ext{ } 0$	219 220	14 36 14 40
20	1 20		4 0	100	0 40	140	3 20	100	12 0	120	14 40
21	1 24	61	4 4	101	6 44	141	9 24	181	12 4	221	14 44
22	1 28	62	4 8	102	6 48	142	9 28	182	12 8	222	14 48
23	1 32	63	4 12	103	6 52	143	9 32	183	12 12	223	14 52
24	1 36	64	4 16	104	6 56	144	9 36	184	12 16	224	14 56
25	1 40	65	4 20	105	7 0	145	9 40	185	12 20	225	15 0
26	1 44	66	4 24	106	7 4	146	9 44	186	12 24	226	15 4
27	1 48	67	4 28	107	7 8	147	9 48	187	12 28	227	15 8
28	1 52	68	4 32	108	7 12	148	9 52	188	12 32	228	15 12
29	1 56	69	4 36	109	7 16	149	9 56	189	12 36	229	15 16
30	$\begin{bmatrix} 2 & 0 \end{bmatrix}$	70	4 40	110	7 20	150	10 0	190	12 40	230	15 20
31	2 4	71	4 44	111	7 24	151	10 4	191	12 44	231	15 24
32	2 8	72	4 48	112	7 28	152	10 8	192	12 48	232	15 28
33	2 12	73	4 52	113	7 32	153	10 12	193	12 52	233	15 32
34	2 16	74	4 56	114	7 36	154	10 16	194	12 56	234	15 36
35	2 20	75	5 0	115	7 40	155	10 20	195	13 0	235	15 40
36	2 24	76	5 4	116	7 44	156	10 24	196	13 4	236	15 44
37	2 28	77	5 8	117	7 48	157	10 28	197	13 8	237	15 48
38	2 32	78	5 12	118	7 52	158	10 32	198	13 12	238	15 52
39	2 36 2 40	79 80	5 16	119	7 56 8 0	159	10 36	199	13 16	239	15 56 16 0
40 F	2 40	30	5 20	120	0 0	160	10 40	200	13 20	240	10 0

to convert parts of the equator in arc into sidereal time, or 2 TO CONVERT TERRESTRIAL LONGITUDE IN ARC INTO TIME.

			· · · · · · · · · · · · · · · · · · ·	-	Degr	tees,	, .				
Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.
0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.	0	h. m.
241	16 4	261	17 24	281	18 44	301	20 4	321	21 24	341	22 44
242	16 8	262	17 28	282	18 48	302	20 8	322	21 28	342	22 48
243	16 12	263	17 32	283	18 52	303	20 12	323	21 32	343	22 52
244	16 16	264	17 36	284	18 56	304	20 16	324	21 36	344	22 56
245	16 20	265	17 40	285	19 0	305	20 20	325	21 40	345	23 0
246	16 24	266	17 44	286	19 4	306	20 24	326	21 44	346	23 - 4
247	16 28	267	17 48	287	19 8	307	20 28	327	21 48	347	23 8
248	16 32	268	17 52	288	19 12	308	20 32	328	21 52	348	23 12
249	16 36	269	17 56	289	19 16	309	20 36	329	21 56	349	23 16
250	16 40	270	18 0	290	19 20	310	20 40	330	22 0	350	23 20
251	16 44	271	18 4	291	19 24	311	20 44	331	22 4	351	23 24
252	16 48	272	18 8	292	19 28	312	20 48	332	22 8	352	23 28
253	16 52	273	18 12	293	19 32	313	20 52	333	22 12	353	23 32
254	16 56	274	.18 16	294	19 36	314	20 56	334	22 16	354	23 36
255	17 0	275	18 20	295	19 40	315	21 0	335	22 20	355	23 40
256	17 4	276	18 24	296	19 44	316	21 4	336	22 24	356	23 44
257	17 8	277	18 28	297	19 48	317	21 8	337	22 28	357	23 48
258	17 12	278	18 32	298	19 52	318	21 12	338	22 32	358	23 52
259	17 16	279	18 36	299	19 56	319	21 16	339	22 36	359	23 56
260	17 20	280	18 40	300	20 0	320	21 20	340	22 40	360	24 0
					Min	UTES.					
í	m. s. 0 4	11	m. s. 0 44	21	m. s. 1 24	31	m. s. 2 4	41	m. s. 2 44	, 51	m. s. 3 24
2	0 8	12	0 48	22	1 28	32	2 8	42	2 48	52	3 28
3	0 12	13	0 52	23	1 32	33	2 12	43	2 52	53	3 32
4	0 16	14	0 56	24	1 36	34	2 16	44	2 56	54	3 36
5	0 20	15	1 0	25	1 40	35	2 20	45	3 0	55	3 40
6	0 24	16	1 4	26	1 44	36	2 24	46	3 4	56	3 44
7	0 28	17	1 8	27	1 48	37	2 28	47	3 8	57	3 48
8	0 32	18	1 12	28	1 52	38	2 32	48	3 12	58	3 52
9	0 36	19	1 16	29	1 56	39	2 36	49	3 16	59	3 56
10	0 40	20	1 20	30	2 0	40	2 40	50	3 20	60	4 0
					Sec	onds.					
"	s.	"	s.	"	s.	91	s.	//	S.	// 51	s.
1 2	0.067	11 12	0.733 0.800	21	1.400	31 32	$\begin{bmatrix} 2.067 \\ 2.133 \end{bmatrix}$	41	2.733 2.800	51 52	3.400 3.467
3	0.133	12	0.867	$\frac{22}{23}$	1.467 1.533	33	2.133 2.200	43	2.860 2.867	53	3.533
4	0.267	11	0.867	$\frac{23}{24}$	1.600	34	2.267	44	$\frac{2.507}{2.933}$	54	3.600
5	0.333	14 15	1.000	25	1.667	35	2.333	45	3.000	55	3.667
				1	i		1				
6	0.400	16	1.067	26	1.733	36	2.400	46	3.067	56	3.733
7	0.467	17	1.133	27	1.800	37	2.467	47	3.133	57	3.800
8 9	0.533	18 19	1.200	28 29	1.867 1.933	38	2.533	48	3.200	58	3.867
10	0.667	20	1.267 1.333	30	2.000	39	2.600	49 50	3.267	59 60	3.933 4.000
10	0.007	11 20	1.555	au	4.000	40	2.667	90	3.333	60	4.000

III. TO CONVERT SIDEREAL TIME INTO PARTS OF THE EQUATOR IN ARC, OR TO CONVERT TIME INTO TERRESTRIAL LONGITUDE IN ARC.

					Hot	RS.					
Time.	Arc.	Time.	Arc	Time.	Arc.	Time.	Arc.	Time.	Arc.	Time.	Arc.
h.	0	h.	0	h.	0	h.	0	h.	0	h.	0
1	15	5	75	9	135	13	195	17	255	21	315
2	30	6	90	10	150	14	210	18	270	22	330
3	45	7	105	11	165	15	225	19	285	23	345
4	60	8	120	12	180	16	240	20	300	24	360
	,				Min	UTES.					
m. 1	0 15	11 I	$\stackrel{\circ}{2}$ $\stackrel{\prime}{45}$	m. 21	5 15	m. 31	° ' 7 45	m. 41	$\stackrel{\circ}{10}$ $\stackrel{\prime}{15}$	m. 51	$^{\circ}_{12}$ $^{\prime}_{45}$
2	0 30	12	3 0	22	5 30	32	8 0	42	10 30	52	13 0
3	0 45	13	3 15	23	5 45	33	8 15	43	10 45	53	13 15
4	1 0	14	3 30	24	6 0	34	8 30	44	11 0	54	13 30
5	1 15	15	3 45	25	6 15	35	8 45	45	11 15	55	13 45
6	1 30	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8	2 0	18	4 30	28	7 0	38	9 30	48	12 0	58	14 30
9	2 15	19	4 45	29	7 15	39	9 45	49	12 15	59	14 45
10	2 30	20	5 0	30	7 30	40	10 0	50	12 30	60	15 0
					Sec	onds.					
s.	, ,,	s.	, ,,	s.	, ,,	s.	, ,,	s.	, ,,	s.	, ,,
1	0 15	11	2 45	21	5 15	31	7 45	41	10 15	51	12 45
2	0 30	12	3 0	22	5 30	32	8 0	42	10 30	52	13 0
3	0 45	13	3 15	23	5 45	33	8 15	43	10 45	53	13 15
4	1 0	14	3 30	24	6 0	34	8 30	44	11 0	54	13 30
5	1 15	15	3 45	25	6 15	35	8 45	45	11 15	55	13 45
6	1 30	16	4 0	26	6 30	36	9 0	46	11 30	56	14 0
7	1 45	17	4 15	27	6 45	37	9 15	47	11 45	57	14 15
8	2 0	18	4 30	28	7 0	38	9 30	48	12 0	58	14 30
9	2 15	19	4 45	29	7 15	39	9 45	49	12 15	59	14 45
10	2 30	20	5 0	30	7 30	40	10 0	50	12 30	60	15 0
	,	71	,		TENTHS O	,	DS.	0		П	,
s. 0.01	0.15	0.18	2.70	s. 0.35	5.25	s. 0.52	7.80	s. 0.69	10.35	s. 0.86	12.90
0.01	0.13	0.19	2.85	0.36	5.40	0.53	7.95	0.70	10.50	0.87	13.05
0.03	0.45	0.20	3.00	0.37	5.55	0.54	8.10	0.71	10.65	0.88	13.20
0.04	0.60	0.21	3.15	0.38	5.70	0.55	8.25	0.72	10.80	0.89	13.35
0.05	0.75	0.22	3.30	0.39	5.85	0.56	8.40	0.73	10.95	0.90	13.50
0.06	0.90	0.23	3.45	0.40	6.00	0.57	8.55	0.74	11.10	0.91	13.65
0.07	1.05	0.24	3.60	0.41	6.15	0.58	8.70	0.75	11.25	0.92	13.80
0.08	1.20	0.25	3.75	0.42	6.30	0.59	8.85	0.76	11.40	0.93	13.95
0.09	1.35	0.26	3.90	0.43	6.45	0.60	9.00	0.77	11.55	0.94	14.10
0.10	1.50	0.27	4.05	0.44	6.60	0.61	9.15	0.78	11.70	0.95	14.25
0.11	1.65	0.28	4.20	0.45	6.75	0.62	9.30	0.79	11.85	0.96	14.40
0.12	1.80	0.29	4.35	0.46	6.90	0.63	9.45	0.80	12.00	0.97	14.55
0.13	1.95	0.30	4.50	0.47	7.05	0.64	9.60	0.81	12.15	0.98	14.70
0.14	2.10	0.31	4.65	0.48	7.20	0.65	9.75	$\begin{vmatrix} 0.82 \\ 0.83 \end{vmatrix}$	12.30 12.45	0.99 1.00	14.85 15.00
$0.15 \\ 0.16$	2.25 2.40	$0.32 \\ 0.33$	4.80	0.49	7.35	$\begin{vmatrix} 0.66 \\ 0.67 \end{vmatrix}$	9.90	0.83	12.45	1.00	15.00
0.17	2.40	0.34	4.95	0.50	7.50 7.65	0.67	10.03	0.85	12.75	1	
0.17	2.00	1 0.04	5.10	U 0.91	1.00	11 0.00	10.20	11 0.00	12.10	<u> </u>	<u> </u>

F

IV. FOR CONVERTING SIDEREAL TIME INTO MEAN SOLAR TIME, AND MEAN TIME INTO SIDEREAL TIME.

	Hours				MINU	JTES.				SECO	NDS.	
Hours	Mean Time.	Sidereal Time.	Min- utes.	Mean Time.	Sidereal Time.		Mean Time.	Sidereal Time.	Sec- onds.	Mean or Sidereal Time.	Sec- onds.	Mean or Sidereal Time
	m s.	m. s.		s.	s.		s.	s		8.	-	S.
1	0 9.83	0 9.86	1	0.16	0.16	31	5.08	5.09	1	0.00	31	0.09
2	0 19.66	0 19.71	2	0.33	0.33	32	5.24	5.26	2	0.01	32	0.09
3	0 29.49	0 29.57	3	0.49	0.49	33	5.41	5.42	3	0.01	33	0.09
4	0 39.32	0 39.43	4	0.66	0.66	34	5.57	5.59	4	0.01	34	0.09
5	0 49.15	0 49.28	5	0.82	0.82	35	5.75	5.75	5	0.01	35	0.10
6	0 58.98	0 59.14	6	0.98	0.99	36	5.90	5.91	6	0.02	36	0.10
7	1 8.81	1 9.00	7	1.15	1.15	37	6.06	6.08	7	0.02	37	0.10
8	1 18.64	1 18.85	8	1.31	1.31	38	6.23	6.24	8	0.02	38	0.10
9	1 28.47	1 28.71	9	1.47	1.48	39	6.39	6.41	9	0.03	39	0.11
10	1 38.30	1 38.57	10	1.64	1.64	40	6.55	6.57	10	0.03	40	0.11
11	1 48.13	1 48.42	11	1.80	1.81	41	6.72	6.74	11	0.03	41	0.11
12	1 57.96	1 58.28	12	1.97	1.97	42	6.88	6.90	12	0.03	42	0 12
13	2 7.78	2 8.13	13	2 13	2.14	43	7.05	7.06	13	0.04	43	0.12
14	2 17.61	2 17.99	14	2.29	2.30	44	7.21	7.23	14	0.04	14	0.12
15	2 27.44	2 27.85	15	2.46	2.46	45	7.37	7.39	15	0.04	45	0.12
16	2 37.27	2 37.70	16	2.62	2.63	46	7.54	7.56	16	0.04	46	0.13
17	2 47.10	2 47.56	17	2.79	2.79	47	7.70	7.72	17	0 05	47	0.13
18	2 56.93	2 57.42	18	2.95	2.96	48	7.86	7.89	18	0.05	48	0.13
19	3 6.76	3 7.27	19	3.11	3.12	49	8.03	8 05	19	0.05	49	0.13
20	3 16.59	3 17.13	20	3.28	3.29	50	8.19	8.21	20	0.06	50	0.14
21	3 26.42	3 26.99	21	3.44	3.45	51	8.36	8.38	21	0.06	51	0.14
22	3 36.25	3 36.84	22	3.60	3.61	52	8.52	8.54	22	0.06	52	0.14
23	3 46.08	3 46.70	23	3.77	3.79	53	8.68	8.71	23	0.06	53	0.15
24	3 55.91	3 56.56	24	3.93	3.94	51	8.85	8.87	24	0.07	54	0.15
25	4 5.74	4 6.41	25	4.10	4.11	55	9.01	9.04	25	0.07	55	0.15
26	4 15.57	4 16.27	26	4.26	4.27	56	9.17	9.20	26	0.07	56	0.15
27	4 25.40	4 26.13	27	4.42	4.43	57	9.34	9.36	27	0.07	57	0.16
28	4 35.23	4 35.98	28	4.59	4.60	58	9.50	9.53	28	0.08	58	0.16
29	4 45.06	4 45.84	29	4.75	4.76	59	9.67	9.69	29	0.08	59	0.16
30	4 54.89	4 55.69	30	4.92	4.93	60	9.83	9.86	30	0.08	60	0.16
	1	1	1)	1	1	<u> </u>			 	 	<u> </u>	

V.

CORRECTION OF THE TIME OBTAINED BY OBSERVATION OF THE SUN, IN ORDER TO HAVE THE TRUE TIME OF THE CLOCK.

							i			1						
	Jan.	Feb.	Mar.	Apr.	Apr.	May.	June.	June	July.	Aug.	Sept.	Oct.	Nov.	Dec.	Dec.	
Day of	Jan.	T CD.	1,101.	11/11	2171.	1.14.	o une.	June	Jan,		- ope.	000.	11011	200.	200.	Day of
Month.													i		_	Month.
Intoller	Add.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Add.	Add.	Add.	Subt.	Subt.	Subt.	Subt.	Add.	
										}			1			
	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	Min.	
1	4	14	13	4		3	3		3	6	0	10	16	11		1
2	4	14	12	4		3	2	• •	4	6	0	11	16	10		2
3	5	14	12	3		3	2	• •	4	6	1	11	16	10		3
4	5	14	12	3		3	2		4	6	1	11	16	10		4
5	6	14	12	3		4	2	• •	4	6	1	12	16	9		5
6	6	14	12	2		4	2	• •	4	6	2	12	16	9		6
7	7	14	11	2		4	2	. •	4	5	2	12	16	8	• •	7
8	7	15	11	2		4	1	• •	5	5	2	12	16	8		8
9	8	15	11	2		4	1		5	5	3	13	16	7	• •	9
10	8	15	11	1		-1	1	• •	5	5	3	13	16	7		10
11	9	15	10	1	• •	4	1	$ \cdot\cdot $	5	5	3	13	16	6	• •	11
12	9	15	10	1		4	1	$ \cdot\cdot $	5	5	4	13	16	6	• •	12
13	9	15	10	1	• •	-4	0	• •	5	5	4	14	16	5	• •	13
14	10	14	9	0		4	0	• • •	5	4	5	14	15	5	• •	14
15	10	14	9	0		4	0	• •	6	4	5	14	15	4	• •	15
16	10	14	9	0		4	0	• •	6	4	5	14	15	4	• •	16
17	11	14	9	0	٠.	4	0	• •	6	4	6	15	15	3	• •	17
18	11	14	8	• •	1	4		1	6	4	6	15	15	3	• •	18
19	11	14	8		1	4		1	6	3	6	15	14	2	• •	19
20	11	14	8		1	4	• •	1	6	3	7	15	14	2	• •	20
21	12	14	7		1	4	• •	1	6	3	7	15	14	1	• •	21
22	12	14	7	• •	2	4	$ \cdot \cdot $	2	6	3	7	15	14	1	• •	22
23	12	14	7		2	4	• •	2	6	2	8	16	13	0	• •	23
24	12	13	6	• •	2	3	• •	2	6	2	8	16 16	13	0	• •	24
25	13	13	6		2	3		2	6	2	8	16	13 12	0		$\begin{array}{c c} 25 \\ 26 \end{array}$
26	13	13	6	• •	$\frac{2}{2}$	3	•••	2	6	2	ļ	16	12 12	٠.	1 1	20 27
27	13	13	5			3		3	6	1	9	16	12	• •	2	28
28	13	13	5		3	3		3	6	- 1	10	16	11	• •	2	28
29	14	13	5	• •	3	3		3	1	1 0	10	16	11	• •	3	30
30	14	• •	4	• •		-			6			16		• •	3	31
31	14	• •	4		• •	3		• • •	6	0	• •	10	• • •	• •	9	31
T)									!							

F

TABLE FOR COMPUTING TERRESTRIAL SURFACES.

The tables under No. VI. were published by Delcros in the Annuaire Météoro-logique de la France pour 1850, p. 65 et seq.

The formula from which they have been computed reads as follows: —

$$S = \frac{ab\pi}{90} \begin{cases} \sin\frac{1}{2}\phi\cos\left(L + \frac{1}{2}\phi\right) \\ -\frac{1}{3}\left[2\cdot\left(\frac{a-b}{a+b}\right) + \left(\frac{a-b}{a+b}\right)^{2}\right]\sin\left(\phi + \frac{1}{2}\phi\right)\cos\left[3L + (\phi + \frac{1}{2}\phi)\right] \\ +\frac{1}{5}\left[3\cdot\left(\frac{a-b}{a+b}\right)^{2} + \left(\frac{a-b}{a+b}\right)^{3}\right]\sin\left(2\phi + \frac{1}{2}\phi\right)\cos\left[5L + (2\phi + \frac{1}{2}\phi)\right] \\ -\text{etc.}; \end{cases}$$

in which $a=\frac{1}{2}$ great axis of the globe; $b=\frac{1}{2}$ small axis; L= the latitude of the lower limit of a quadrilateral surface; L'= the latitude of the upper limit of the same; $\phi=L'-L$; S= the area of a quadrilateral surface of one degree in longitude; $\pi=$ the ratio of the circumference to the diameter.

Substituting the numerical values, the quarter of the meridian being = 10,000,724 legal metres; the $\frac{1}{2}$ great axis, or a, = 6,376,989 metres; the $\frac{1}{2}$ small axis, or b, = 6,356,323 metres; the ratio of the axis $\frac{1}{308.61}$; and making ϕ = 1° nonagesimal, the formula becomes,

$$S = \begin{cases} 224.996360 \cos \left(\begin{array}{c} L + 0^{\circ} 30' \right) \\ -0.730851 \cos \left(3 L + 1^{\circ} 30' \right) \\ +0.001784 \cos \left(5 L + 2^{\circ} 30' \right) \\ -0.000004 \cos \left(7 L + 3^{\circ} 30' \right) \\ + \text{etc.} \end{cases}$$

The first three terms of the formula give the results with sufficient accuracy.

In order to avoid too large a number of figures, the results are given in square miles, the linear base of which is a mile equal to $\frac{1}{15}$ of the mean degree of the meridian. That mile is thus $=\left(\frac{10000724}{90\times15}\right)=7407.942$ metres. In order to convert the results into new geographical miles, of which $60=1^\circ$, multiply by 16, $\log=1.2041200$; into common French leagues, $25=1^\circ$, multiply by 2.777778, $\log=0.4436975$; into nautical leagues, $20=1^\circ$, multiply by 1.777778, $\log=0.2498775$; into English statute miles, $69.163=1^\circ$, by 21.711034, $\log=1.3366868$.

Use of the Tables.

Table I., which gives the number of square miles contained in the quadrilateral surfaces of one degree in latitude and longitude, successively from the equator to the pole, will be more frequently used. Table II. has been computed for maps on a smaller scale; and Tables III. and IV. for maps of very small scale, covering large areas, in which surfaces of one degree could not be estimated with sufficient accuracy. If the scale is large enough to have the minutes traced on, then Table V. is to be used.

For computing a surface by Table I., which may serve as an example for all the others, find first the lowest parallel circle which crosses, on the map, the surface to be estimated; suppose it is 40° lat. N., and the zone within 40° and 41° lat. N. contains four integral degrees of longitude, that is, four surfaces of one degree each way; then in the first column of the table, on the line beginning with latitude 40°, and in the vertical column headed 4, take the value of these four surfaces, viz. 685.88. Then take likewise the value of the number of surfaces between 41° and 42° lat. N., and so on. The fractional parts left outside of the integral degrees are best estimated, with the compass, in decimals, the values of which can be found in the columns of the multiples, by properly moving the decimal point to the left. Having taken them in that way, and summing them up with all the integral surfaces, we obtain the total surface required.

TABLE I. QUADRILATERAL SURFACES OF I DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Lim	iting	1				IAL ELLI		11-511		··· ····
LATIT	udes.			Multiples	of these Qu	adrilateral S	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	1	224.259	448.52	672.78	897.04	1121.29	1345.55	1569.81	1794.07	2018.3
1	2	224.192	448.38	672.58	896.77	1120.96	1345.15	1569.35	1793.54	2017.7
2	3	224.059	448.12	672.18	896.24	1120.30	1344.36	1568.42	1792.47	2016.5
3	4	223.860	447.72	671.58	895.44	1119.30	1343.16	1567.02	1790.88	2014.7
-1	5	223.594	447.19	670.78	894.37	1117.97	1341.56	1565.16	1788.75	2012.3
5	6	223.261	446.52	669.78	893.05	1116.31	1339.57	1562.83	1786.09	2009.3
6	7	222.863	445.73	668.59	891.45	1114.31	1337.18	1560.04	1782.90	2005.7
7	8	222.398	444.80	667.19	889.59	1111.99	1334.39	1556.78	1779.18	2001.5
8	9	221.867	443.73	665.60	887.47	1109.33	1331.20	1553.07	1774.93	1996.8
9	10	221.270	442.54	663.81	885.08	1106.35	1327.62	1548.89	1770.16	1991.4
10	11	220.607	441.21	661.82	882.43	1103.03	1323.64	1544.25	1764.85	1985.4
11	12	219.878	439.76	659.63	879.51	1099.39	1319.27	1539.15	1759.02	1978.9
12	13	219.084	433.17	657.25	876.34	1095.42	1314.50	1533.59	1752.67	1971.7
13	14	218.225	436.45	654.67	872.90	1091.12	1309.35	1527.57	1745.80	1964.0
14	15	217.300	434.60	651.90	869.20	1086.50	1303.80	1521.10	1738.40	1955.7
15	16	216.311	432.62	648.93	865.24	1081.55	1297.86	1514.17	1730.48	1946.8
16	17	215.257	430.51	645.77	861.03	1076.28	1291.54	1506.80	1722.05	1937.3
17	18	214.138	428.28	642.41	856.55	1070.69	1284.83	1498.97	1713.10	1927.2
18	19	212.955	425.91	638.87	851.82	1064.78	1277.73	1490.69	1703.64	1916.6
19	20	211.709	423.42	636.13	846.84	1058.54	1270.25	1481.96	1693.67	1905.3
20	21	210.399	420.80	631.20	841.59	1051.99	1262.39	1472.79	1683.19	1893.3
21	22	209.025	418.05	627.08	836.10	1045.13	1254.15	1463.18	1672.20	1881.2
22	23	207.589	415.18	622.77	830.36	1037.95	1245.54	1453.12	1660.71	1868.3
23	24	206.090	412.18	618.27	824.36	1030.45	1236.54	1442.63	1648.72	1854.8
24	25	204.529	409.06	613.59	818.12	1022.65	1227.18	1431.71	1636.24	1840.7
25	26	202.907	405.81	608.72	811.63	1014.53	1217.44	1420.35	1623.25	1826.1
26	27	201.223	402.45	603.67	804.89	1006.11	1207.34	1408.56	1609.78	1811.0
27	28	199.477	398.95	598.43	797.91	997.39	1196.86	1396.34	1595.82	1795.3
28	29	197.672	395.34	593.02	790.69	988.36	1186.03	1383.70	1581.38	1779.0
29	30	195.806	391.61	587.42	783.23	979.03	1174.84	1370.64	1566.45	1762.2
30	31	193.881	387.76	581.64	775.52	969.40	1163.29	1357.17	1551.05	1744.9
31	32	191.897	383.79	575.69	767.59	959.48	1151.38	1343.28	1535.17	1727.0
32	33	189.854	379.71	569.56	759.41	949.27	1139.12	1328.98	1518.83	1708.6
33	34	187.753	375.51	563.26	750.01	938.76	1126.52	1314.27	1502.02	1689.7
34	35	185.594	371.19	556.78	742.38	927.97	1113.57	1299.16	1484.75	1670.
35	36	183.379	366.76	550.14	733.52	916.89	1100.27	1283.65	1467.03	1650.
36	37	181.107	362.21	543.32	724.43	905.53	1086.64	1267.75	1448.86	1629.9
37	38	178.780	357.56	536.34	715.12	893.90	1072.68	1251.46	1430.24	1609.0
38	39	176.397	352.79	529.19	705.59	881.98	1058.38	1234.78	1411.18	1587.5
39	40	173.960	347.92	521.88	695.84	869.80	1043.76	1217.72	1391.68	1565.6
40	41	171.469	342.94	514.41	685.88	857.34	1028.81	1200.28	1371.75	1543.2
41	42	168.925	337.85	506.77	675.70	844.62	1013.55	1182.47	1351.40	1520.2
42	43	166.328	332.66	498.98	665.31	831.64	997.97	1164.30	1330.62	1496.9
43	44	163.680	327.36	491.04	654.72	818.40	982.08	1145.76	1309.44	1473.1
44	45	160.980	321.96	482.94	643.92	804.90	965.88	1126.86	1287.84	1448.8

TABLE I. (Continued.) QUADRILATERAL SURFACES OF 1 DEGREE IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi ATIT	iting UDES.			Multiples	of these Qu	adrilateral S	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
45	46	158.231	316.46	474.69	632.92	791.15	949.39	1107.62	1265.85	1424.08
46	47	155.432	310.86	466.30	621.73	777.16	932.59	1088.02	1243.46	1398.89
47	48	152.584	305.17	457.75	610.34	762.92	915.51	1068.09	1220.67	1373.20
48	49	149.689	299.38	449.07	598.75	748.44	899.13	1047.82	1197.51	1347.2
49	50	146.746	293.49	440.24	586.98	733.73	880.48	1027.22	1173.97	1320.7
50	51	143.757	287.51	431.27	575.03	718.78	862.54	1006.30	1150.06	1293.8
51	52	140.723	281.45	422.17	562.89	703.61	844.34	985.06	1125.78	1266.5
52	53	137.644	275.29	412.93	550.58	688.22	825.86	963.51	1101.15	1238.8
53	54	134.522	269.04	403.57	538.09	672.61	807.13	941.65	1076.17	1210.7
54	55	131.357	262.71	394.07	525.43	656.78	788.14	919.50	1050.86	1182.2
55	56	128.150	256.30	384.45	512.60	640.75	768.90	897.05	1025.20	1153.3
56	57	124.903	249.81	374.71	499.61	624.51	749.42	874.32	999.22	1124.1
57	58	121.616	243.23	364.85	486.46	608.08	729.69	851.31	972.92	1094.5
58	59	118.289	236.58	354.87	473.16	591.45	709.74	828.03	946.32	1064.6
59	60	114.926	229.85	344.78	459.70	574.63	689.55	804.48	919.41	1034.3
60	61	111.525	223.05	334.58	446.10	557.63	669.15	780.68	892.20	1003.7
61	62	108.089	216.18	324.27	432.35	540.44	648.53	756.62	864.71	972.8
62	63	104.618	209.24	313.85	418.47	523.09	627.71	732.32	836.94	941.5
63	64	101.113	202.23	303.34.	404.45	505.56	606.68	707.79	808.90	910.0
64	65	97.575	195.15	292.73	390.30	487.88	585.45	683.03	780.60	878.1
65	66	94.007	188.01	282.02	376.03	470.03	564.04	658.05	752.05	846.0
66	67	90.408	180.82	271.22	361.63	452.04	542.45	632.85	723.26	813.6
67	68	86.779	173.56	260.34	347.12	433.90	520.68	607.46	694.23	781.0
68	69	83.123	166.25	249.37	332.49	415.61	498.74	581.86	664.98	748.1
69	70	79.439	158.88	238.32	317.76	397.20	476.64	556.08	635.52	714.9
70	71	75.730	151.46	227.19	302.92	378.65	454.38	530.11	605.84	681.5
71	72	71.996	143.99	215.99	287.99	359.98	431.98	503.98	575.97	647.9
72	73	68.239	136.48	204.72	272.96	341.20	409.44	477.68	545.91	614.1
73	74	64.460	128.92	193.38	257.84	322.30	386.76	451.22	515.68	580.1
74	75	60.659	121.32	181.98	242.64	303.30	363.96	424.62	485.28	545.9
75	76	56.839	113.68	170.52	227.36	284.20	341.04	397.88	454.72	511.5
76	77	53.001	106.00	159.00	212.00	265.00	318.00	371.00	424.00	477.0
77	78	49.145	98.29	147.43	196.58	245.72	294.87	344.01	393.16	442.3
78	79	45.272	90.54	135.82	181.09	226.36	271.63	316.91	362.18	407
79	80	41.386	82.77	124.16	165.54	206.93	248.31	289.70	331.08	372.
80	81	37.485	74.97	112.46	149.91	187.43	224.91	262.40	299.88	337.3
81	82	33.572	67.14	100.72	134.29	167.86	201.43	235.01	268.58	302.1
82	83	29.649	59.30	88.95	118.59	148.24	177.89	207.54	237.19	266.8
83	84	25.715	51.43	77.15	102.86	128.58	154.29	180.01	205.72	231.
84	85	21.773	43.55	65.32	87.09	108.87	130.64	152.41	174.19	195.9
85	86	17.824	35.65	53.17	71.30	89.12	106.95	124.77	142.59	 160.4
86	87	13.869	27.74	41.61	55.48	69.35	83.22	97.09	110.96	124.8
87	ss	9.910	19.82	29.73	39.61	49.55	59.46	69.37	79.28	89.1
88	89	5.947	11.89	17.84	23.79	29.74	35.68	41.63	47.58	53.5
89	90	1.983	3.97	5.95	7.93	9.91	11.90	13.88	15.86	17.5

TABLE II. QUADRILATERAL SURFACES OF 2 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	iting UDES.			Multiples	of these Qu	adrilateral	Surfaces fro	m 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	2	896.903	1793.S1	2690.71	3587.61	4484.51	5381.42	6278.32	7175.22	8072.13
2	4	895.838	1791.68	2687.51	3583.35	4479.19	5375.03	6270.87	7166.71	8062.54
4	6	893.710	1787.42	2681.13	3574.84	4468.55	5362.26	6255.97	7149.68	8043.39
6	8	890.520	1781.04	2671.56	3562.08	4452.60	5343.12	6233.64	7124.16	8014.68
8	10	886.272	1772.54	2658.82	3545.09	4431.36	5317.63	6203.91	7090.18	7976.45
10	12	880.969	1761.94	2642.91	3523.88	4404.85	5285.82	6166.79	7047.76	7928.72
12	14	874.617	1749.23	2623.85	3498.47	4373.09	5247.70	6122.32	6996.94	7871.55
14	16	867.221	1734.44	2601.66	3468.88	4336.11	5203.33	6070.55	6937.77	7804.99
16	18	858.789	1717.5S	2576.37	3435.16	4293.95	5152.74	6011.52	6870.31	7729.10
18	20	849.328	1698.66	2547.98	3397.31	4246.64	5095.97	5945.30	6794.63	7643.95
20	22	838.848	1677.70	2516.54	3355.39	4194.24	5033.09	5871.94	6710.78	7549.63
22	24	827.359	1654.72	2482.08	3309.44	4136.80	4964.16	5791.51	6618.87	7446.23
24	26	814.872	1629.74	2444.62	3259.49	4074.36	4889.23	5704.11	6518.98	7333.85
26	28	811.400	1602.80	2404.20	3205.60	4007.00	4808.40	5609.80	6411.20	7212.60
28	30	786.956	1573.91	2360.87	3147.83	3934.78	4721.74	5508.69	6295.65	7082.61
30	32	771.555	1543.11	2314.67	3086.22	3857.78	4629.33	5400.89	6172.44	6944.00
32	34	755.213	1510.43	2265.64	3020.85	3776.06	4531.28	5286.49	6041.70	6796.92
34	36	737.946	1475.89	2213.84	2951.78	3689.73	4427.68	5165.62	5903.57	6641.51
36	38	719.773	1439.55	2159.32	2879.09	3598.87	4318.64	5038.41	5758.19	6477.96
38	40	700.713	1401.43	2102.14	2802.85	3503.57	4204.28	4904.99	5605.71	6306.42
40	42	680.787	1361.57	2042.36	2723.15	3403.93	4084.72	4765.51	5446.29	6127.08
42	44	660.016	1320.03	1980.05	2640.06	3300.08	3960.09	4620.11	5280.13	5940.14
44	46	638.423	1276.85	1915.27	2553.69	3192.11	3830.54	4468.96	5107.38	5745.81
46	48	616.032	1232.06	1848.10	2464.13	3080.16	3696.19	4312.23	4928.26	5544.29
48	50	592.869	1185.74	1778.61	2371.48	2964.34	3557.21	4150.08	4742.95	5335.82
50	52	568.960	1137.92	1706.88	2275.84	2844.80	3413.76	3982.72	4551.68	5120.64
52	54	544.332	1088.66	1632.99	2177.33	2721.66	3265.99	3810.32	4354.65	4898.99
54	56	519.014	1038.03	1557.04	2076.06	2595.07	3114.09	3633.10	4152.11	4671.13
56	58	493.037	986.07	1479.11	1972.15	2465.18	2958.22	3451.26	3944.29	4437.33
58	60	466.430	932.86	1399.29	1865.72	2332.15	2798.58	3265.01	3731.44	4197.87
60	62	439.228	878.46	1317.68	1756.91	2196.14	2635.37	3074.59	3513.82	3953.05
62	64	411.461	822.92	1234.38	1645.84	2057.30	2468.76	2880.23	3291.69	3703.15
64	66	383.164	766.33	1149.49	1532.66	1915.82	2298.99	2682.15	3065.32	3448.48
66	68	354.374	708.75	1063.12	1417.50	1771.87	2126.24	2480.62	2834.99	3189.36
68	70	325.124	650.25	975.37	1300.50	1625.62	1950.75	2275.87	2601.00	2926.12
70	72	295.453	590.91	886.36	1181.81	1477.27	1772.72	2068.17	2363.63	2659.08
72	74	265.398	530.80	796.20	1061.59	1326.99	1592.39	1857.79	2123.19	2388.59
74	76	234.998	469.99	704.99	939.99	1174.99	1409.99	1644.98	1879.98	2114.98
76	78	204.290	408.58	612.87	817.16	1021.45	1225.74	1430.03	1634.32	1838.61
78	80	173.316	346.63	519.95	693.26	866.58	1039.90	1213.21	1386.53	1559.85
80	82	142.115	284.23	426.34	568.46	710.57	852.69	994.80	1136.92	1279.03
82	84	110.728	221.46	332.18	442.91	553.64	664.37	775.09	885.82	996.55
84	86	79.195	168.39	237.59	316.78	395.98	475.17	554.37	633.56	712.76
86	88	47.559	95.12	142.68	190.24	237.79	285.35	332.91	380.47	428.03
88	90	15.860	31.72	47.58	63.44	79.30	95.16	111.02	126.88	142.74

TABLE III. QUADRILATERAL SURFACES OF 5 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT	ting UDES.			Multiple	es of these	Quadrilateral	Surfaces fro	om 1 to 9.		
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.
0	5	5599.821	11199.64	16799.46	22399.29	27999.11	33598.93	39198.75	44798.57	50398.39
5	10	5558.288	11116.58	16674.87	22233.15	27791.44	33349.73	38908.02	44466.31	50024.60
10	15	5475.466	10950.93	16426.40	21901.87	27377.33	32852.80	38328.27	43803.73	49279.20
15	20	5351.846	10703.69	16055.54	21407.39	26759.23	32111.08	37462.93	42814.77	48166.62
20	25	5188.165	10376.33	15564.49	20752.66	25940.82	31128.99	36317.15	41505.32	46693.48
25	30	4985,425	9970.85	14956 27	19941 70	24927.12	29912.55	34897.97	39883.40	44868.82
30	35	4744.891				23724.46	28469.35	33214.24	37959.13	42704.02
35	40	4468.110				22340.55	26808.66	31276.77	35744.88	40212.99
40	45	4156.909				20784.54	24941.45	29098.36	33255.27	37412.18
45	50	3813.408				19067.04	22880.45	26693.86	30507.26	34320.67
50	55	3440.013				17200.06	20640.08	24080.09	27520.10	30960.12
55	60	3039.419	6078.84	_		15197.09	18236.51	21275.93	24315.35	27354.77
60	65	2614.598	5229.20		1	13072.99	15687.59	18302.19	20916.79	23531.39
65	70	2168.779	4337.56	-		10843.89	13012.67	15181.45	17350.23	19519.01
70	75	1705.427	3410.85	5116.28	6821.71	8527.13	10232.56	11937.99	13643.42	15348-84
75	80	1228.213	2456.43	3684.64	4912.85	6141.07	7369.28	8597.49	9825.71	11053.92
80	85	740.973	1481.95	2222.92	2963.89	3704.86	4445.84	5186.81	5927.78	6668.76
85	90	247.668	495.34	743.00	990.67	1238.34	1486.01	1733.68	1981.34	2229.01

TABLE IV. QUADRILATERAL SURFACES OF 10 DEGREES IN LATITUDE AND IN LONGITUDE ON THE TERRESTRIAL ELLIPSOID.

Limi LATIT			Multiples of these Quadrilateral Surfaces from 1 to 9.											
Inf.	Sup.	1.	2.	3.	4.	5.	6.	7.	8.	9.				
0	10	22316.220	44632.44	66948.66	S9264.88	111581.10	133897.32	156213.54	178529.76	200845.98				
10	20	21654.626	43309.25	64963.88	86618.50	108273.13	129927.76	151582.38	173237.01	194891.63				
20	30	20347.180	40694.36	61041.54	81388.72	101735.90	122083.08	142430.26	162777.44	183124.62				
30	40	18426.004	36852.01	55278 . 01	73704.02	92130.02	110556.02	128982.03	147408.03	165834.04				
40	50	15940.634	31881.27	47821.90	63762.54	79703.17	95643.80	111584.14	127525.07	143465.71				
50	60	12958-864	25917.7 3	38876.59	51835.46	64794.32	77753.18	90712.05	103670.91	116629.78				
60	70	9566.755	19133.51	28700.26	38267.02	47833.77	57400.53	6696 7.2 8	76534.04	86100.79				
70	80	5867.281	11734.56	17601.84	23469.12	29336.40	35203.69	41070.97	46938.25	52805.53				
80	90	1977.282	3954.56	5931.85	7909.13	9886.41	11863.69	13840.97	15818.26	17795.54				

TABLE V. Mean Quadrilateral Surfaces of 1, 10, 20, and 30 Minutes in Latituda and in Longitude deduced from each Quadrilateral of 1 Degree in Table I.

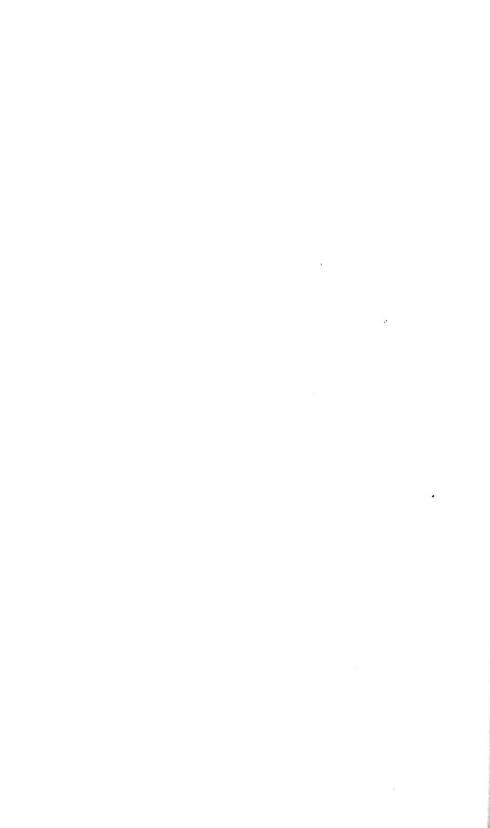
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	Sup. 1	0.0623 0.0623 0.0622 0.0622 0.0622 0.0621 0.0620 0.0619 0.0616 0.0615 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0595 0.0592	6.229 6.228 6.224 6.218 6.211 6.202 6.191 6.178 6.163 6.146 6.128 6.008 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.918 24.910 24.895 24.873 24.844 24.807 24.763 24.711 24.652 24.586 24.512 24.431 24.247 24.144 24.035 23.917 23.793 23.662 23.523	30'. 56.065 56.048 56.015 55.965 55.898 55.815 55.716 55.599 55.467 55.317 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239 52.927	1nf. 45 46 47 48 49 50 51 52 53 54 55 66 67 68 69 60 61 62 63 64	Sup. 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64	1/. 0.0440 0.0432 0.0424 0.0416 0.0408 0.0399 0.0391 0.0382 0.0374 0.0365 0.0356 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291 0.0281	4.395 4.318 4.238 4.158 4.076 3.993 3.909 3.823 3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906 2.809	20'. 17.581 17.270 16.954 16.632 16.305 15.973 15.636 15.294 14.947 14.595 14.239 13.878 13.513 12.770 12.392 12.010 11.624	30'. 39.558 38.858 38.146 37.422 36.686 35.939 35.181 34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.0623 0.0622 0.0622 0.0621 0.0620 0.0619 0.0616 0.0615 0.0613 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0595 0.0592	6.228 6.224 6.218 6.211 6.202 6.191 6.178 6.163 6.146 6.128 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.910 24.895 24.873 24.844 24.807 24.763 24.711 24.652 24.586 24.512 24.431 24.247 24.144 24.035 23.917 23.793 23.662	56.048 56.015 55.965 55.898 55.716 55.599 55.467 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.334 53.239	46 47 48 49 50 51 52 53 54 55 56 57 58 60 61 62 63	47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63	0.0432 0.0424 0.0416 0.0408 0.0399 0.0391 0.0382 0.0374 0.0365 0.0356 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	4.318 4.238 4.158 4.076 3.993 3.909 3.823 3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	17.270 16.954 16.632 16.305 15.973 15.636 15.294 14.947 14.595 13.878 13.513 12.770 12.392 12.010 11.624	38.858 38.146 37.422 36.686 35.939 35.181 34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.0622 0.0622 0.0621 0.0620 0.0619 0.0618 0.0615 0.0613 0.0611 0.0609 0.0606 0.0604 0.0598 0.0595 0.0595 0.0592	6.224 6.218 6.211 6.202 6.191 6.178 6.163 6.146 6.128 6.086 6.062 6.036 6.090 5.979 5.948 5.915 5.881	24.895 24.873 24.844 24.807 24.763 24.711 24.652 24.586 24.512 24.431 24.247 24.144 24.035 23.917 23.793 23.662	56.015 55.965 55.898 55.815 55.716 55.599 55.467 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63	48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63	0.0424 0.0416 0.0408 0.0399 0.0391 0.0382 0.0374 0.0365 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	4.238 4.158 4.076 3.993 3.909 3.823 3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	16.954 16.632 16.305 15.973 15.636 15.294 14.947 14.595 14.239 13.878 13.513 12.770 12.392 12.010 11.624	38.146 37.422 36.686 35.939 35.181 34.411 33.630 32.839 31.226 30.404 29.572 28.731 27.881 27.022 26.154
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.0622 0.0621 0.0620 0.0619 0.0618 0.0615 0.0613 0.0611 0.0609 0.0606 0.0604 0.0598 0.0595 0.0595 0.0592	6.218 6.202 6.191 6.178 6.163 6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.873 24.844 24.807 24.763 24.711 24.652 24.586 24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.965 55.898 55.815 55.716 55.599 55.467 55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63	50 51 52 53 54 55 56 57 58 59 60 61 62 63	0.0416 0.0408 0.0399 0.0391 0.0382 0.0374 0.0365 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	4.158 4.076 3.993 3.909 3.823 3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	16.632 16.305 15.973 15.636 15.294 14.947 14.595 14.239 13.878 13.513 13.143 12.770 12.392 12.010 11.624	37.422 36.686 35.939 35.181 34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.0621 0.0620 0.0619 0.0618 0.0616 0.0613 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.211 6.202 6.191 6.178 6.163 6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.844 24.807 24.763 24.711 24.652 24.586 24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.898 55.815 55.716 55.599 55.467 55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	49 50 51 52 53 54 55 56 57 58 59 60 61 62 63	50 51 52 53 54 55 56 57 58 59 60 61 62 63	0.0408 0.0399 0.0391 0.0382 0.0374 0.0365 0.0347 0.0338 0.0329 0.0310 0.0300 0.0291	4.076 3.993 3.909 3.823 3.737 3.649 3.560 3.470 3.378 5.286 3.192 3.098 3.002 2.906	16.305 15.973 15.636 15.294 14.947 14.595 14.239 13.878 13.513 12.770 12.392 12.010 11.624	36.686 35.939 35.181 34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.0620 0.0619 0.0618 0.0616 0.0615 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.202 6.191 6.178 6.163 6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.807 24.763 24.711 24.652 24.586 24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.815 55.716 55.599 55.467 55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	50 51 52 53 54 55 56 57 58 59 60 61 62 63	51 52 53 54 55 56 57 58 59 60 61 62 63	0.0399 0.0391 0.0382 0.0374 0.0365 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.993 3.909 3.823 3.737 3.649 3.560 3.470 3.378 5.286 3.192 3.098 3.002 2.906	15.973 15.636 15.294 14.947 14.595 14.239 13.878 13.513 12.770 12.392 12.010 11.624	35.939 35.181 34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	7 8 9 10 11 12 13 14 15 16 17 18 19 20	0.0619 0.0618 0.0616 0.0615 0.0613 0.0611 0.0609 0.0606 0.0604 0.0598 0.0595 0.0595 0.0592	6.191 6.178 6.163 6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.763 24.711 24.652 24.586 24.512 24.431 24.247 24.144 24.035 23.917 23.793 23.662	55.716 55.599 55.467 55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	51 52 53 54 55 56 57 58 59 60 61 62 63	52 53 54 55 56 57 58 59 60 61 62 63	0.0391 0.0382 0.0374 0.0365 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.909 3.823 3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	15.636 15.294 14.947 14.595 13.878 13.513 13.143 12.770 12.392 12.010 11.624	35.181 34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	8 9 10 11 12 13 14 15 16 17 18 19 20	0.0618 0.0616 0.0615 0.0613 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.178 6.163 6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.711 24.652 24.586 24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.599 55.467 55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	52 53 54 55 56 57 58 59 60 61 62 63	53 54 55 56 57 58 59 60 61 62 63	0.0382 0.0374 0.0365 0.0356 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.823 3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	15.294 14.947 14.595 14.239 13.878 13.513 13.143 12.770 12.392 12.010 11.624	34.411 33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	9 10 11 12 13 14 15 16 17 18 19 20	0.0616 0.0613 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.163 6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.652 24.586 24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.467 55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	53 54 55 56 57 58 59 60 61 62 63	54 55 56 57 58 59 60 61 62 63	0.0374 0.0365 0.0356 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.737 3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	14.947 14.595 14.239 13.878 13.513 13.143 12.770 12.392 12.010 11.624	33.630 32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	10 11 12 13 14 15 16 17 18 19 20	0.0615 0.0613 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.146 6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.586 24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.317 55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	54 55 56 57 58 59 60 61 62 63	55 56 57 58 59 60 61 62 63	0.0365 0.0356 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.649 3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	14.595 14.239 13.878 13.513 13.143 12.770 12.392 12.010 11.624	32.839 32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	11 12 13 14 15 16 17 18 19 20	0.0613 0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.128 6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.512 24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	55.152 54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	55 56 57 58 59 60 61 62 63	56 57 58 59 60 61 62 63	0.0356 0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.560 3.470 3.378 3.286 3.192 3.098 3.002 2.906	14.239 13.878 13.513 13.143 12.770 12.392 12.010 11.624	32.038 31.226 30.404 29.572 28.731 27.881 27.022 26.154
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	12 13 14 15 16 17 18 19 20	0.0611 0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.108 6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.431 24.343 24.247 24.144 24.035 23.917 23.793 23.662	54.970 54.771 54.556 54.325 54.078 53.814 53.534 53.239	56 57 58 59 60 61 62 63	57 58 59 60 61 62 63	0.0347 0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.470 3.378 3.286 3.192 3.098 3.002 2.906	13.878 13.513 13.143 12.770 12.392 12.010 11.624	31.226 30.404 29.572 28.731 27.881 27.022 26.154
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	13 14 15 16 17 18 19 20	0.0609 0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.086 6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.343 24.247 24.144 24.035 23.917 23.793 23.662	54.771 54.556 54.325 54.078 53.814 53.534 53.239	57 58 59 60 61 62 63	58 59 60 61 62 63	0.0338 0.0329 0.0319 0.0310 0.0300 0.0291	3.378 3.286 3.192 3.098 3.002 2.906	13.513 13.143 12.770 12.392 12.010 11.624	30.404 29.572 28.731 27.881 27.022 26.154
13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	14 15 16 17 18 19 20	0.0606 0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.062 6.036 6.009 5.979 5.948 5.915 5.881	24.247 24.144 24.035 23.917 23.793 23.662	54.556 54.325 54.078 53.814 53.534 53.239	58 59 60 61 62 63	59 60 61 62 63	0.0329 0.0319 0.0310 0.0300 0.0291	3.286 3.192 3.098 3.002 2.906	13.143 12.770 12.392 12.010 11.624	29.572 28.731 27.881 27.022 26.154
14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	15 16 17 18 19 20	0.0604 0.0601 0.0598 0.0595 0.0592 0.0588	6.036 6.009 5.979 5.948 5.915 5.881	24.144 24.035 23.917 23.793 23.662	54.325 54.078 53.814 53.534 53.239	59 60 61 62 63	60 61 62 63	0.0319 0.0310 0.0300 0.0291	3.192 3.098 3.002 2.906	12.770 12.392 12.010 11.624	28.731 27.881 27.022 26.154
15 16 17 18 19 20 21 22 23 24 25 26 27 28	16 17 18 19 20	0.0601 0.0598 0.0595 0.0592 0.0588	6.009 5.979 5.948 5.915 5.881	24.035 23.917 23.793 23.662	54.078 53.814 53.534 53.239	60 61 62 63	61 62 63	0.0310 0.0300 0.0291	3.098 3.002 2.906	12.392 12.010 11.624	27.881 27.022 26.154
16 17 18 19 20 21 22 23 24 25 26 27 28	17 18 19 20	0.0598 0.0595 0.0592 0.0588	5.979 5.948 5.915 5.881	23.917 23.793 23.662	53.814 53.534 53.239	61 62 63	62 63	0.0300 0.0291	3.002 2.906	12.010 11.624	27.022 26.154
17 18 19 20 21 22 23 24 25 26 27 28	18 19 20	0.0595 0.0592 0.0588	5.948 5.915 5.881	23.793 23.662	53.534 53.239	62 63	63	0.0291	2.906	11.624	26.154
17 18 19 20 21 22 23 24 25 26 27 28	19 20	0.0595 0.0592 0.0588	5.915 5.881	23.662	53.239	63	t I				
18 19 20 21 22 23 24 25 26 27 28	19 20	0.0592 0.0588	5.915 5.881	23.662	53.239	1	t I		9 800		
19 20 21 22 23 24 25 26 27 28	20	0.0588	5.881	1		l e i	- 1		1 4.000	11.235	25.278
21 22 23 24 25 26 27 28	21	0.0584	- 0			04	65	0.0271	2.710	10.842	24.394
21 22 23 24 25 26 27 28			5.844	23.378	52.600	65	66	0.0261	2.611	10.445	23.502
22 23 24 25 26 27 28	22	0.0581	5,806	23.225	52.256	66	67	0.0251	2.511	10.045	22.602
23 24 25 26 27 28	23	0.0577	5.766	23.065	51.897	67	68	0.0241	2.411	9.642	21.695
24 25 26 27 28	24	0.0572	5.725	22.899	51.523	68	69	0.0231	2.309	9.236	20.781
26 27 28	25	0.0568	5.681	22.725	51.132	69	70	0.0221	2.207	8.827	19.860
26 27 28	26	0.0564	5.636	22.545	50.727	70	71	0.0210	2.104	8.414	18.933
27 28	27	0.0559	5.590	22.358	50.306	71	72	0.0200	2.000	8.000	17.999
28	28	0.0554	5.541	22.164	49.869	72	73	0.0190	1.896	7.582	17.060
	29	0.0549	5.491	21.964	49.418	73	74	0.0179	1.791	7.162	16.113
	30	0.0544	5.439	21.756	48.952	74	75	0.0168	1.685	6.740	15.165
30	31	0.0539	5.386	21.542	48.470	75	76	0.0158	1.579	6.315	14.210
31	32	0.0533	5.330	21.322	47.974	76	77	0.0147	1.472	5.889	13.250
32	33	0.0527	5.274	21.095	47.463	77	78	0.0137	1.365	5.461	12.286
33	34	0.0522	5.215	20.861	46.938	78	79	0.0126	1.258	5.030	11.318
34	35	0.0516	5.155	20.622	46.399	79	80	0.0115	1.150	4.598	10.340
35	36	0.0509	5.094	20.375	45.845	80	81	0.0104	1.041	4.165	9.37
36	37	0.0503	5.031	20.123	45.277	81	82	0.0093	0.933	3.730	8.39
37	38	0.0303	4.966	19.864	44.695	82	83	0.0033	0.824	3.294	7.415
38	39	0.0490	4.900	19.600	44.099	83	84	0.0071	0.714	2.857	6.429
39	40	0.0483	4.832	19.329	43.490	84	85	0.0060	0.605	2.419	5.44
40	41	0.0476	4.763	19.052	42.867	85	86	0.0049	0.495	1.980	4.450
41	42	0.0469	4.692	18.769	42.231	86	87	0.0039	0.385	1.541	3.46
42	43	0.0462	4.620	18.481	41.582	87	88	0.0038	0.355	1.101	2.47
42	40	0.0462	4.547	18.187	40.920	88	89	0.0023	0.275	0.661	1.48
44	41	0.0133	4.472	17.887	40.920	89	90	0.0006	0.055	0.220	0.49

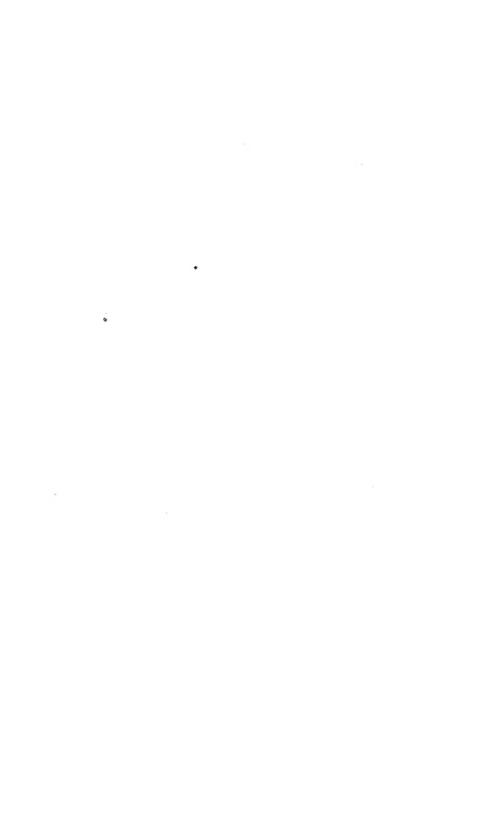
ERRATA IN THE FIRST EDITION.

- A, page 7, line below the title, instead of $(32 + \frac{4}{5}x^{\circ})$ read $(32 + \frac{9}{5}x^{\circ})$.
- A, " 21, on the line beginning with 30, in the last four columns, instead of 100.75 100.97 101.20 101.42 read 100.85 101.07 101.30 101.52.
- B, "7, on the line beginning with 23°, second column, instead of 20.410, read 20.888.
- B, "23, on the line beginning with 12°, third column, instead of 5 87, read 5.37.
- B, "30-32, at the head of each first column, Temperature of the Air, add "in Centigrade degrees."
- B, "40, Table II., first part, on the line beginning with 60, column headed 7, instead of 24.11,01, read 24.9,01.
- B, " Table II., first part, on the line beginning with 70, column headed 5, instead of 27.4,47, read 27.8,47; and column headed 8, instead of 28.11,77, read 28.9,77.
- B, " Table II., second part, on the line beginning with 70, column headed 5, instead of 328.47, read 332.47.
- B, "41, Table III., line beginning with 20, the five last columns, instead of 63.54 66.08 68 62 71.16 73.70, read 63.50 66.04 68.58 71.12 73.66.
- B, " Table III, line beginning with 200, column headed 3, instead of 515.11, read 515.61.
- B, "42, Table V., line beginning with 180, column headed 7, instead of 516.21, read 506.21.
- B, "43, Table VI., first part, on line beginning with 70, column headed 2, instead of 76.635, read 76.735.
- В, Table VI., second part, on line beginning with 7, the last eight columns, instead of 0.6483 0.65720 6661 0 6750 0.68390.69270.7016 0.7105, 0.63950.64830.65720 6661 0.6750 0.68390.6927 0.7016.
- B, "43, Table VI., second part, on line beginning with 12, column headed 5, instead of 1.1018, read 1.1102.
- C, "11, on line beginning with 26.5 inches, column headed 6, instead of 674.41, read 674.61.
- C, " on line of 27.1 inches, column headed 1, instead of 688 38, read 688.58.
- C, "12, on line of 30.5 inches, column headed 2, instead of 778.20, read 775.19.
- C, " 39 and 41, at the head of table, instead of "Tenths of Degrees," read "English Inches."
- D, "28, 29, and 30, head of page, instead of "Tenths of a Degree," read "Hundredths of a Degree."
- D, " 35, note at the bottom, instead of "Geology," read "Geodesy."
- D, " 36, on line beginning with 160, columns headed 8 and 9, instead of 550.19 and 553.47, read 551.19 and 554.47.
- D, " 36, on line beginning with 260, columns headed 2, 3, 5, and 6,

instead of	860.59	863.87	879.43	882.72,
read	859.60	862.88	869.44	872.72.

- D, " 37, on line beginning with 620, column headed 4, instead of 2048.28, read 2047.28.
- D, " " " " " 770, " 0, " 2526.39, " 2526.29.
- D, "38, " " 880, " 5, " 2903.69, " 2903 60.
- D, " " " 890. " 6, " 2939.79, " 2939.69.
- D, " " " " 930, " 5, " 3069.64, " 3067.64.
- D, """"""""3261.71, "3261.21.
- D, " " " " " 990, " 5, " 3264.59, " 3264.49.
- D, " 39, on line beginning with 1380, columns headed 3, 4, 5, 6, 7, 8,
- D, "40, on line beginning with 1610, column headed 5, instead of 5292.65, read 5298.65.
- D, "44, Table X., on line beginning with 3, column headed 6, instead of 21.0205, read 23 0205.
- D, "45, Table XII., on line beginning with column 0, column headed 5, instead of 0.83333, read 0.08333.





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