


## SMITIISONIAN

## IIISCLLLALEOLS COLLECTIONS.

## YOL. XXVIII.


"ETERY MAS IS AVALUABLE MEMBER OF SOCIETY WHO BY HIS OBRERYATIONF, REAEARCYES AND EXPERIMENTB PROCURES KNOWLEDGE FUR MEN,"-SMITHSON.

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PUBLISHED BY THE SMITHEONIAN INSTITUTION.
1887.

## ADTERTISEMENT.

The present scries, entitled "Smithsonian Miscellaneous Collections," is intended to embrace all the publications issued directly by the Smithsonian lustitution in octavo form ; those in quarto constituting the "Smithsonian Contributions to Knowledge." The quarto series inclutes memoirs embracing the records of extended original investigations and researches resulting in what are believed to be new truths, and constituting positive additions to the sum of human knowledge. The octavo series is desigued to contain reports on the present state of our knowledge of particular branches of science: instructions for collecting and digesting facts and materials for research : lists and synopses of species of the organic and inorganic world: museum catalogues: reports of explorations: aids to bibliographical investigations, etc., generally prepared at the expressed request of the Iustitution, and at its expense.

The position of a work in one or the other of the two series will sometimes depend upon whether the required illustrations can be presented more conveniently in the quarto or the octavo form.

In the Smithsonian Contributions to Knowledge, as well as in the present series, each article is separately paged and indexed, and the actual date of its publication is that given on its special title-page, and not that of the volume in which it is placed. In many cases, works have been published, and largely distributed, years before their combinations into volumes.

SPENCER F. BAIRD,

Secretary S. I.

## Smithsonian $\mathfrak{f l t s c e l l a n f o u s ~} \mathfrak{C o l l e c t i o n s . ~}$

## TABLES,

## meteorological and Physical,

BY
ARNOLD GUYOT, P.D., LL.D., PROFESSOR OF GEOLOGY AND PHYSICAL GEOGRAPHY, COLLEGE OF NEW JERSEY.

FOURTH EDITION, REVISED AND ENLARGED.

Edited by WILLiAM LIBBEY, Jr., PROFESSOR OF PHYSICAL GEOGRAPHY, COLLEGE OF NEW JERSEY.


WASIIINGTON:
SMITHSONIAN INSTITUTION.

## ADVERTISEMENT.

A quarter of a century has now elapsed since the publication of the last (the third) edition of Dr. Guyot's Meteorological and Physical Tables. This forms the first of an early projected series of "Tables of Constants" to which the Smithsonian Institution is gradually making important contributions. None has been in more general demand than this collection, and to its improvement and extension Prof. Guyot gratuitously devoted a large amount of time and laborions attention.
'The first edition, published in 1852 , comprised 212 pages. Five years later (in 1857) a second edition was published, with careful revision by the author; and the various series of Tables were so enlarged as to extend the work to over 600 pages. A third edition was published in 1859, with further amendments.

To this, the author, with untiring industry, has been making constant additions; and the present issue projected by him in 1879-from various delays occasioned by pressing professional occupations, as well as by illness and death in his family-has been about forn vears in passing through the press. The result is at last submitted in this fourth edition, which extends to about 750 pages.

Just before completing the last few tahles, the estimable and distinguished author departed this life, Feloruary 8, 1884, in the seventyseventh year of his age. Dr. Guyot had for thirty years been the honored Professor of Geology and Physlal Geograply in Princeton College.

The completion of the work has been entruster to his able assistant, Prof. William Libbey, Jr., who has conscientionsly and judiciously execnted his duties as the final editor. In the Preface to this edition he has indicated the character of the additions and re-arrangements adopted.

> SPENCER F. BAIRD, Secretary S. $I$.

Washington, September, 1884.

## PREFACE

TO THE FIRST EDITION.

## To PROF. JOSEPII HENRY,

 Secretary of the Smithsonian Institution. Sir, -In compliance with your instructions, I have prepared the collection of Meteorological Tables contained in the following pages. I have endeavored to render it useful, not only to the observers engaged in the system of Meteorological Observations now in operation ander the direction of the Smithsonian Institution, for whom it was immediately desigued, but also to any Meteorologist who may desire to compare and to work out portions of the vast amount of Meteorological Observations already accumulated in the stores of science.

The reduction of the observations and the extensive comparisons, without which Meteorology can do but little, require an amount of mechanical labor which renders it impossible for most observers to deduce for themselves the results of their own observations. The difficulty is still further increased by the diversity of the thermometrical and barometrical scales which Meteorologists, faithful to old habits rather than to science and to reason, choose to retain, notwithstanding the additional labor they thus gratuitously assume to themselves. 'To relieve the Meteorologist of a great portion of this labor, by means of tables sufficiently extensive to render calculations and even interpolations unnecessary, is to save his time and his forces in favor of science itself, and thus materially contribute to its advancement. But most of the tables useful in Meteorology being scattered through many volumes, which are often not of easy access, this collection will be, it is hoped, acceptable to the friends of Meteorology, ant will supply a want very much felt in this department of the physical sciences.

In the selection of the matter, I have been gnided by the idea that the tables which I sought for my own use might aiso be those most likely to be wanted by others. But I wish the following to be considered as a first collection, containing only the tables most appropriate to the present purpose. They are, therefore, arranged in different and independent series, with distinct paging, but constituting together a frame-work into which any tables may be readily inserted when wanted, either to make the collection more complete, or to present a choice of tables calculated from somewhat different elements, or adapted to various methods of calculation.
'The measurement of heights by means of the barometer being incimately comnected with Meteorology, it was thought not inappropriate to admit into this collection Hypsometrical 'Tables, destined to render this kind of calculations more easy and more rapid, and thus to increase the taste for a method so useful in physical geography. I have preferred the tables of Delcros, as uniting in the greatest degree simplicity and accuracy. 'Those of Gauss, Bessel, and Baily may be given afterwards.

Every table contains directions for its use, when necessary; moreover, the indication of the clements used in its calculation, and of the source from which it has been taken. When no remark is made as to this last point, the table has been expressly calculated for this volune.

Very respectfuliy,
Your obedient servant,
A. GUYOT.

Casmridge, Mass., December 15th. 1851.

## PREFACE

## TO THE SECOND EDITION.

## To PROF. JOSEPII IIENRY,

Secretary of the Smithsonian Institution.

## Sir, -

In sending to you the Meteorological Tables composing the first edition of this volume, published in 1852 , I expressed the desire that they be considered as a first collection, containing the talbles most needed at the time by the meteorological observers engaged in the system carried on under the supervision of the Smithsonian Institution, but destined to be increased. It was in that expectation, I remarked, that the tables had been arranged in independent series, as a kind of framework, into which a larger number could readily be inserted. It seemed, indeed, lighly desirahle to offer to the Meteorologist and Physical Geographer, not only the tables they daily need for working out the results of their observations, but also such a variety of tables, computed from different elements, or by different methods, or adapted to different measures, as to enable every one to choose among them those that he most approves, and at the same time properly to compare and to appreciate the results obtained by others.

Thanks to the congenial spirit with which the elerated views of the founder of the Smithsonian Institution are carried out, that character of general usefulness is not wanting in the present volume. With your agreement, the present edition contains more than three times as much matter as the first ; and a rapid indication of the additions will suffice to justify them, and to show that, in selecting or calculating the new tables, the object just mentioned was constantly kept in view

As to the tables in the first edition, I must remark that, several of them having been printed in my absence, the copy prepared for the printer, in which decimals had to be left out, failed to give always the nearest value. Though these errors are too small to have any importance whatsoever in Meteorology, a careful revision of all the tahles on the original computations was made, and they were corrected in the present edition The few actual misprints which were discovered are indicated in a table of errate to the first edition.

In the Thermometrical series six small tables have been added; they were prepared for converting into each other differential results given in degrees of any one of the three thermometrical scales, irrespective of their zero point.

The Hygrometrical series has been entirely reorganized. It only contained five tables, all in French measures, and the Appendix. It is now composed of twenty-seven, arranged in three divisions. In the first are found ten tables, hased on Regnanlt's hygrometrical eonstants, both in French and in English measures, in two corresponding sets, for the use of the prychrometer, the dew-point instruments, and for computing the weight of vaper in the air. The whole set in English measures, and Table V. in French measures, have been prepared for this edition. Being based on the best elements we now possess, they are given here for ordinary use. The second division contains the seren most important tables published in the Greemurirh Obsfrutious, and Glaisher's extensive Psychrometrical Table. These tables being much used in England, and the results obtained by them exhibiting no inconsiderable differences from those derived from the preceding ones, they are indispensable for comparing these results. The third division, composed of ten miscellancous tables, furnishes the means of comparing the different values of the force and the weight of vapor, especially those which have frequently been used in Germany, and also of reducing the indications of saussure's Hair-Hygrometer to the ordinary seale of moistmre. The Appendix has remained as in the first edition, but all the tables have been revised and corrected.

The Barometrical series, now in four divisions, has been increased from twelve to twentr-eight tables. Excepting three small tahles for capillary action, all the new ones have been comphted for this edition. The comparison, now so much needed, of the Russian barometer with the other seales, appears here for the first time.

The Hypsometrical series is almost entirely new. It contained only Delcros's table for barometric and Regnault's table for thermometric measurements, hesides two anxiliary tables and the thirteen small tables of the Appendix. It now offers twenty-three tables for harometrical measurement of heights, in which all the principal formula and scales are represented ; three for the measurement of heights by the thermometer, in French and in English measures; and a rich Apmendix of forty-four tables, more extensive and convenient than those in the old set, which afford the means of readily converting into each other all the measures usually employed for indicating altitudes.

The series of Meteorological Corrections for periodic and non-periodie variations, for all parts of the world, mostly due to the untiring industry of Professor Dove, is an addition which will surely be appreciated by those who know how difficult access to the original tables is for most Meteorol-
ogists. A few tables have been added to Dove's collection, computed by Glaisher, Captain Lefroy, and by myself. Most of the tahles refer to temperature, only two to moisture. 'Two tables of Barometrical Corrections have been placed in the Hypsometrical series, where they were needed, until they can be joined by others to make a set in this series, which still awaits new contributions, especially for these last two departments.

The Hiscellaneous series is but begun. I have prepared a list of useful tables, which would be no doubt welcome to the lover's of 'Terrestrial Physics, and which may be published at some future occasion, if you should then find it expedient.

The present collection being designed, not for the scientific only, but for the observers at large, the propriety of the explieit and popular form of the explanations which accompany the tables, and of the directions for using them, will readily be understood.

I close by the remark, that, in every instance, the works from which the tables were taken have been carefully noted, and due eredit given to their authors. For all the tables without author's names, I am myself responsible.

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\begin{aligned}
& \text { I remain, Sir, } \\
& \qquad \text { Very respectfully, yours, }
\end{aligned}
$$

A. GUYOT.

Princeton, N. J., December, 18.57.

## PREIACE

## TO THE TIIIRD EDITION.

A new series of Itygrometrical Tables, based on Regnault's Table of Elastic Forces of Vapor, has been published ly Mr. Glaisher, in London, 1850. As, however, the Psychrometrical Table has not been computed from Regnault's formula, but by means of empirical factors, the results differ from those contained in Table VII. B. A table containing Glaisher's empirical factors, therefore, has been added, and will be found on page 144 B .

Table XVIIl. of the Barometrical set, C, page 72, of the Second Edition, for redueing to the freezing point the Barometers with glass or wooden seales, copied from the Instructions of the Royal Society of London, and which is reprinted in most of the English works on Metcorology, haring been found erroneous, a new table has been computed and substituted for it. As a large mumber of observers still use barometers with wooden scales, it was found alvisable to enable them to make the needed interpolations at sight, by giving the corrections for every degree of the thermometer, from $0^{\circ}$ to $100^{\circ}$ Fahr., and for barometric heights ranging between 26 and 31 inches.

The small Table VI. D, page 48, of the Hypsometrical Tables by the writer, having been found useful for rapid computation of approximate results, a larger one of the same description, which allows to make at sight every interpolation, has been added, on page 92, as Table XIX'. The scientific traveller, wishing to determine, when asconding a monntain, the elevation of the physical or geological phenomena that he meets with, such as the stations of remarkable plants, limits of zones of vegetation, - the geologist who uses the ancroid barometer for geological sections, - the engineer who wishes to know, on the ground, approximately, his results, - will find it convenient to obtain the relative heights indicated by their instrument by a simple multiplication. The use of the table is explained page D 90 .

Some of the decimals in the smaller Tahle VI. D, page 48, above mentioned, have been slightly altered in order to make both tables agree.

In set E of Meteorological Corrections, a talle of corrections derived by Professor C. Dewey from the hourly observations of Professor Snell, at Amherst College, has been added, which will be of service especially to the numerons observers in New England and in the neighboring States.

The errata indicated in the Second Edition, and a few unimportant ones found since, have been corrected. No other changes have been made in this edition.
A. GUYOT.

Princeton, N. J., April, 1859.

## PREFACE

## TO THE FOURTHEDITION.

## To PROF. SPENCER F. BAIRD, Secretary of the Smithsonian Institution. <br> $$
\mathrm{Str},-
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I take pleasure in transmitting herewith the completed fourth edition of Guyot's Smithsonian Meteorological and Physical Tables.

A new arrangement of the tables composing the thitr edition of this book has allowed the insertion of quite a large number of new and useful tables:-

Series I., containing the Thermometrical Tables, has remained unchanged.

Series II., containing the Hygrometrical Tables, has been enlarged by an addition to Table vir. The Psychrometrical Tables of Dr. Guyot (pp. 108, 109) are based upon Regnault's modification of the formula of August ; which have been extended so as to include differences of $29^{\circ} .5$ in temperature between the wet and dry bulb thermometers.

Series III., containing the Barometrical Tables, has remained unchanged.

Series IV., containing the Hypsometrical Tables, is now limited to the first twenty-six tables of the same series in the former edition, and as a new section remains unchanged.

Series V. is partly new and partly old, seventeen of the remaining forty-four tables of the old series IV. having been retained as they were. Of the remainder, some have been discarded as of no further valueothers have been re-calculated from more recent data; and others are entirely new. The series now contains three sets of tables of Geographical Measures, as follows:-
a. For containing the most important measures of length used for indicating altitude; containing forty-mine tables.
b. For comparing the most important Gengraphical Distances ; containing ten tables.
c. For enmparing the most important measures of Geographical Surfaces; containing ten tables.

Series V., containing the Meteorological Tables, now becomes Series VI., with the same name, and remains unchanged.

Series VI., containing the Miscellaneous Tables, now becomes Series VII., and has heen considerably modified.

Table i., which formerly contained but about 60 names of ohservatories, now gives the names and loeations of over 150 , and, in addition to the data formerly given, the time west of Greenwich has been deemed of sufficient importance to be placed in the table.

Tables in., iII., iv., and v. remain the same as they were.
Table vi. is now a new table, giving the length of a degree of both the meridian and of the parallel in the various gengraphical measures. These have been calculated from Clarke's formula for the spheroid of revolution, of 1866.

Table vin. now contains tables for computing terrestrial surfaces, which are new and are also based upon Clarke's formula.

Table viri. is a new table, giving a comparison of the Standards of Length, of England, France, Belgium, Prussia, Russia, India, and Australia, made by Capt. A. R. Clarke, at the English Ordnance Survey Office, under the direction of Col. Sir Henry James, Director of the Ordnance Survey.

Table in. is a new table, giving the length of Insolation for any latitude, and for any day of the year.

All the corrections which have been found or which have been reported, have been made, and the book is now comparatively free from typographical errors; but it is hoped that the same kind courtesy which has prompted the friends, who have aided to make the book more perfect, will be continued in the future; and that all errors observed will be reported as soon as found, so that they may be corrected at some future time.

A general Index has been prepared for the whole Volume, which will greatly facilitate the use of the book, while the old plan of dividing it according to Series has also been retained.

I wish to acknowledge in this place my great indebtedness to you; and also to Mr. M. McNeill of the Princeton Observatory, for valuable assistance in computation and in proof-reading.

> I am,

> Yours most respectfully,
> WILLIAM LIBBEY, JR.

Princeton, N. J., July, 1884.

## CONTENTS.

Tue Tables contained in this collection are divided into seven series, as follows:-
I. Thermometrical Tables, marked A.
II. Hygrometrical Tables, " B.
III. Barometrical Tables, "، C.
IV. Hypsometrical Tables, " D.
V. Geographical Measures, " E.
VI. Meteorological Corrections, " F.

V II. Miscellaneous Tables, " G.
Each series has an independent paging ruming through all the tables that it contains.

The letters A, B, C, D, E, F, G, at the bottom of each page, indicate the series, and the figure the folio of the series to which the page belongs.

The figure at the top of the page indicates the page number referred to in the index.

At the head of each series is found a detailed table of its contents.

## GENERAL INDEX.

(The figures refer to the page number at the top of the page.)
PA㒾现
1
I. THERMOMETRICAL TABLES
Table I. Comparison of Fahreulheit's scale with Centigrade and Reaumur's, full degrees, from $+212^{\circ}$ to $-39^{\circ}$ ..... 8
" II. Comparison of the Centigrade scale with Reaumur's and Fahren- heit's, full degrees, from $+100^{\circ}$ to $+50^{\circ}$ ..... 10
". III. Comparison of Reammur's scale with Fahrenheit's and the Centi- grade, full degrees, from $+80^{\circ}$ to $+40^{\circ}$ ..... 10
" IV. Conversion of degrees of Fahrenheit into Centigrade degrees, for every tenth of a degree, from $+122^{\circ}$ to $-76^{\circ} \mathrm{F}$. ..... 13
" V. Conversion of degrees of Fahrenheit into degrees of Reaumur, for every tenth of a degree, from $+122^{\circ}$ to $-38^{\circ} \mathrm{F}$. ..... 18
" VI. Conversion of Centigrade degrees into degrees of Falurenheit, for every tenth of a degree, from $+50^{\circ}$ to $-54^{\circ}$, and from $+100^{\circ}$ to $+89^{\circ}$ C. . ..... 25
" VII. Conversion of Centigrade degrees into degrees of Reaumur, for every tenth of a degree, from $+40^{\circ}$ to $-40^{\circ} \mathrm{C}$. ..... 28
" VIII. Conversion of degrees of Reaumur into degrees of Fahrenheit, for every tenth of a degree, from $+40^{\circ}$ to $-40^{\circ} \mathrm{R}$. ..... 30
" IX. Conversion of degrees of Reaumur into Centigrade, degrees for every tenth of a degree, from $+40^{\circ}$ to $-40^{\circ} \mathrm{R}$. ..... 32
" X. Value of any number of degrees of Fahrenheit, expressed by a cor- responding number of Centigrade degrees ..... 34
" XI. Value of any number of degrees of Fahrenheit, expressed by a cor- responding number of degrees of Reaumur ..... 34
" XII. Value of any number of Centigrade degrees, expressed by a cor- responding number of degrees of Reaumur ..... 34
" XIII. Value of any number of Centigrade degrees, expressed by a cor- responding number of degrees of Fabrenheit ..... 35
" XIV. Value of any number of degrees of Reaumur, expressed by a cor- responding number of Centigrade degrees ..... 35
" XV. Value of any number of degrees of Reanmur, expressed by a cor- responding number of degrees of Fahrenheit ..... 35
(XV)II. HYGROMETRICAI TABLES
Tables based on Regranlt's constants. a. In French measures.37
Table I. Elastic Force of Aqueous Vipor, by Regnanlt ..... 46
-. II. Psychrometrical Tables, by Ilaeghens ..... 48
.- III. For detucing the relative humidity from the Indications of Dew- point lnstruments, by Hacghens ..... 66
-. IV. Factor $\frac{100}{F}$ for computing Relative Humidity ..... 72
-. V. Weight of Vapor contained in a Cubic Metre of air ..... 74
b. In English measures.
.. VI. Elastic Force of vapor, reduced from Regnault's table ..... 78
.. Vil. Psychrometrical tables, by A. Guyot ..... 82
.. VIII. For deducing the Relative Humidity from the Indications of Dew-point Iustroments, by A. Guyot ..... 111
$\because \quad$ IN. Factor $\frac{100}{F}$ tor computing Reative Humidity ..... 126
.. X. Weight of Vapor in a Cubic Foot of saturated air ..... 130
Tables based on the constants used in the Greenacich obsprrations.

- SI. Elastic Force of Aqucous Vapor ..... 137
-. XII. Psychrometrical Tables, by Glaisher ..... 140
- X111. Factors for computing the Force of Vapor from Psychrometrical observations, by $A_{\text {pjohn's formula }}$ ..... 176
" XIV. Factors for finding the Temperature of the Dew-pmint from the Readings of the Psychrometer ..... 178
" XIV'. Factors for finding the 'Temperature of the Dew-point from the Readings of the Psychrometer ..... 182
" XV . Weight of Vapor contained in a Cubie Foot of saturated air ..... 179
" XV1. Factors for deducing the Weight of Vapor from the Indications of Dew-point Instruments ..... 179
" XVII. For comparing the Weight of a Cubic Foot of dry and of satniated Air ..... 180
Miscellaneous Tables.
" XVIII. Elastic Force of Vapor expressed in Millimetres by August ..... 186
" XIX. Elastic Force of Vapor expressed in Millimetres by Kaemtz ..... 188
" XX. Elastic Force of Vapor expressed in Millimetres by Magnus ..... 188
". XXI. Elastic Force of Vapor in English Inches from the Royal So- ciety's Report ..... 189
-" XXII. For showing the differences in the values of the Elastic Force of Vapor adopted by different authorities ..... 190
" XXIII. Weight of Vapor in Grammes contained in a Cubic Metre of saturated air by Pouillet ..... 192
" XXIV. Wright of Vapor in Grammes contained in a Cubic Metre of air, by Kaemtz ..... 192
Table XXV. Force of Vapor and Relative Humidity corresponding to the degrees of Saussure's Hair Hygrometer, by Gay-hassac ..... 198
" XXVI. For deducing the Relative Mumidity from the Indications of Saussure's Hair Hygrometer, by Haeghens ..... 194
"XXVII. Relative Humidity corresponding to the degrees of Satussure's Hygrometer, by Kaemtz ..... $1!. i$
Comparison of Quantities of Rain Water in different measnres.
Table I. Conversion of Centimetres into English Inches ..... 200
، II. Conversion of Centimetres into French Inches and Lines ..... 2010
" III. Conversion of English Inches into Centimetres ..... 201
" IV. Conversion of English Inches into French Inches and Lines ..... $\because 11$
* V. Conversion of French Inches and Lines into Centimetres ..... $2(1)$
". VI. Conversion of French Inches and Lines into English Inches ..... 203
III. BAROMETRICAL TABLES ..... 20.5
Comparison of the different Barometrical Scales.
Table I. Comparison of the English and the Metrical Barometers ..... 215
" II. Comparison of the English and the old French Barometers ..... 219 ..... 219
" III. Comparison of the Metrical and the English Barometers ..... 205
" IV. Comparison of the Metrical and the old French Barometers ..... 231
" V. Comparison of the old French and the English Barometers ..... 238
" VI. Comparison of the old French and the Metrical Barometers ..... 243
"VII. Comparison of the Russian and the Metrical Barometers ..... $\because 47$
" VIII. Comparison of the Russian and the old French Barometers ..... 2.5
Comparison of Barometrical differences.
" IX. Conversion of English Inches into Millimetres ..... $2 \% 3$
" X. Conversion of English Inches into French or Paris Lines ..... 2.94
" XI. Conversion of Millimetres into English Inches ..... 2.is
، XII. Conversion of Millimetres into French or Paris Lines ..... 2.9
" XIII. Conversion of French or Paris Lines into Millimetres ..... $2(0)$
". XIV. Conversion of French or Paris Lines into English Ineher ..... $2(6)$
". XV. Conversion of Russian Half-Lines into Millimetres ..... $2(6)$
". XVI. Conversion of Russian Half-Lines into Paris Lines . ..... 261
Reduction of Barometrical observations to the Freezing Point.
" XVII. Reduction of English Barometers with Brass scales ..... 269
" XVIII. Reduction of English Barometers with Glass or Wooden Scales ..... 276
" XIX. Reduction of the Metrical Barometer, by Delcros ..... 2 s
" XX. Reduction of the Metrical Barometar, by Haeghens ..... $\geq 87$
" XXI. Reduction of the old Fremeh Barometer, by Kaemaz ..... 380
Correction of Barometrical observations for Capillary action.
Table XXII. Correction to be applied to English Barometers for Capilary action ..... 337
.. XXIII. Normal Height of Meniseus in millimetres, by Delcros ..... 337
-. XXIV. Correction to be applied to Metrical Barometers for Capilary action, by Delcros ..... 308
.. XXV. Depression of the Barometrical Column due to Capillary action -Pouillet ..... $8: 39$
-. XXVI. Depression of the Barometrical Column due to Capillary action —Gehlers Wörterbuch ..... 3:3!
.- XXVII. Depression of the Barometrical Column due to Capillary action reduced from Deleros' Tables ..... 310
" XXVIII. Depression of the Barometrical Column due to Capillary action —Baily ..... 340
IV. IIYPsOAIETRICAL TABLES ..... 341
Tubles based on Laplace's Constants.
Table I. Delcror' Tables, in Metrical measures ..... 319
" II. Guyot's Tables, in English measures ..... $: 37$
357
357
.. IV. Gans' Tables, modified by Dippe, old French measures ..... $3!7$
.- V. Dippe's Tables, for reducing Barometrical observations to another Level, and for compuing Heights, old French measures ..... 398
.- VI. Babinct's Modification of Laplace's Formula ..... 406
". VII. Baily's Tables, in English measmes ..... 407
Tubles based on Bessel's Formula.
*V VII. Plantamou's Tables, in Metrical measures ..... 410
Miscellaneons Tables.
- IX. Correction for the Hour of the Day at which the Observations lave been taken, Coefficients, by Berghans ..... 418
" X. Correction for the Ifour of the Day, old Frencla measures ..... 419
* XI. Correction to be applied to the Half-sums of the Temperatures olserved at Geneva and St. Bernard, and its Value in Metres at all Ifours and Seasons of the Year, by Plantamour . ..... 420
.- XII. Mean Ineight of the Barometer at the Level of the Sea in vari- ous Latitudes ..... 423
- XIII. Mean Iteight of the Barometer in all months of the year ..... 424
" XIV. Mean Height of the Barometer at all hours of the day ..... 424
- SV. Tropic IIours of Daily Variation at Halle ..... 425
" $\mathrm{XV}^{+\prime}$. Amplitade of Daily Variations in various Latiturles ..... 425
Reducing the Barometer to the Level of the Sea ..... 426
Table XVI. Height. in English Feet of a column of air corresponining to a Tenth of an Inch in the Barometer ..... $4: 3$
.. XVII. Height, in French Feet of a column of air comerpunding to a Paris Line in the Barometer ..... $4: 7$
- NVII. Height, in Metres of a column of air correponding to a Milli- metre in the Barometer ..... $4 \div 7$
.. XIX. Height. in Metres of a colmmof air corresponding to a Milli- metre in the Barometer at different Temperatures and Elera- tions ..... 4こ:." NIX'. Height, in English Fett of a column of air corresponding to atenth of an incl in the Barometer, at different Temperaturesand Elevations$4: 3$
* XX. Correction to be applied to the means of the Hours of Olmerva- tion to obtain the True Mean Barometrical Pressurr. Phila- lelphia ..... $4: \% 1$
-. SXI. Correction to be applied to the means of the Hours of Oherera- tion to obtain the True Mean Barometrical Presure, Green- wich ..... $4 \because 2$
-. NXII. For reducing Minutes into Decimals of an Hour ..... $4: 3$

2. XXIII. Correction for currature and retraction ..... $4: 1$
Thermometrical Mensurement of Heights.
.. XXIV. Regnault's Barometric Presures corresponding to the Tempera- ture of Boiling Water ..... 435
.. XXV. Regnault's Barometric Pressures corresponding to the Tempera- ture of Boiling Water, revised by Moritz, in metrical mea- sures ..... 412
.. XXVI. Regnault's Barometric Presures corresponding to the Tempura- ture of Boiling Water, revised by Moritz, in English meatures ..... 44
V. GEOGRAPHICAL MEASURES ..... 4.5
a.) Comparison of the measures of Length most generally used for indicating altitudes ..... 119
Table I. Conversion of French Toises into Metres ..... 4:11
" II. Conversion of French Toises into Paris Fept ..... thin

* III. Conversion of French Toises into English Fert ..... 461
.. iV. Conversion of French Toise into Rhine Feet ..... $4 h_{1}$
.. V. Conversion of Metres into Toises ..... 462
6 VI. Conversion of Metres into Paris Feet ..... 463
.- VII. Conversion of Metres into English Feet ..... 4 4ri
.. VIII. Conrersion of Metres into Rhine. or Prussian Fert ..... 47
- IX. Conversion of Metres into Ftet of Vienna ..... 4. 1
X. Conversion of Paris Feet into Toises ..... 47.Table XI. Conversion of Paris Feet into Metres . . . 476able
SII. Conversion of Paris Feet into English Feet ..... 477
6 . 6 III. Conversion of Paris Feet into Rhine Feet ..... 478
. $\quad$ XIV. Conversion of Paris Feet into Feet of Vienna ..... 479
* $\quad$. Conversion of English Iards into French 'Ioises ..... 480
6 XVI. Conversion of English Iards into Metres ..... 480
6 XVII. Conversion of English Feet into Metres ..... 481
6 XVIII. Conversion of Finglish Feet into Paris Feet ..... $45^{\circ}$
6 SIX. Conversion of English Feet into Rhine Feet ..... 483
66 XX. Conversion of English Feet into Feet of Vienna ..... 484
". XXI. Conversion of IVlafter of Vienna monto Metres ..... 485
. $\quad$ XXII. Conversion of Klafter of Vienna into Paris Feet ..... 486

6. XXIII. Conversion of Klafter of Vienna into English Feet ..... 486
. XXIV. Conversion of Feet of Vienna into Metres . ..... 487
7. $\underset{\text {. Conversion of Feet of Viennainto Paris Feet }}{ }$ ..... 488
. KXVI. Conversion of Feet of Vienna into English Feet ..... 489
-6 XXVII. Conversion of Feet of Vienna into Rhine Feet ..... 490
.. XXVIII. Conversion of Rhine Feet into French 'Ioises ..... 491
" XXIX. Conversion of Rhine Feet into Metres ..... 491.

* $\quad$ S. Conversion of Rhine Feet into Paris Heet ..... 492
. 6 XXI. Conversion of Rline Feet into Englisti feet ..... 492
. XXXII. Conversion of Riline Feet into Feet of Vienna ..... 493
" XXIII. Conversion of Bavarian Feet into Netres ..... 493
6 $X X$ IV. Conversion of Dld Spanish or Castilian Varas into Netres ..... 494
" $x$ KXV. Conversion of Old Spanish Feet into Metres ..... 494
* XXXVI. Conversion of Mexican Vilias into Metres ..... 495

6. CXXII Conversion of Mexicun Feet into Metres ..... 495

* XXXIII. Conversion of Mexican Feet into Finglish Feet ..... 49\%
 ..... 196;
. . Conversion of Bolivian Feet into Metres ..... 496
" "hi. Conversion of Bolivian Feet into Enolish Feet ..... 496
.6 VJII. Conversion of Inclues into Duodecimal Itines ..... 497
66 SlII. Conversion of Decimals of a Toise into Tert and Incins ..... 417
6 Nuv. Conversion of Decimals of a Foot into Inclus innd I)no-decimal Lines498
↔ KI, VI. Conversion of Inches and Duodecinal Lines into IDecimals ot \& Toot ..... 498
6 $\quad$. TLID. Tablefor Comparing the nost important measures of tanoth ..... $49!$

6. KINIII. Conversion of Fanglish Fathoms into Metres ..... 51)()
NDIX. Convelsion of Meties into finglish Fathoms ..... 5) $0(1$
b.) Compurison of the most imporiant measures of Geographical Distances ..... 501
Table I. Conversion ot Kilonetres into Anstrian Miles-TMasian MilesCerman Miles_Nintieal Jfagues_- French Leaguts_(teoglaphical Miles-Knglish Statute Miles-Rnssian Wersts$5(1.5$
Table Il. Conversion of Anstrian Miles into Kilometres-Prussian Miles _German Miles-Nautical Leagues-Frrench Leagues-Geo- graphical Miles_English Statute Miles-Russian Wersts ..... 508

- III. Conversion of Prussian Miles into Kilometres-Austrian Miles- German Miles-Nantical Leagues-French Leagues_Geo- graphical Miles-English Statute Miles-Russian Wersts ..... 511
.. IV. Conversion of German Miles into Kilometres-Austrian Miles -Prussian Miles - Nautical Leagnes - Freuch Leagues- Geographical Miles-English Statute Miles-Linssian Wersts ..... 514
.. V. Conversion of Nautical Leagues into Kilometres-AustrianMiles_Prussian Miles—German Miles_French Leagues_Geographical Miles-English statute Miles-Russian Wersts517
". VI. Couversion of French Leagues into Kilometres-Austrian Miles—Prussian Miles_German Miles—Nautical Leagues_Geo-graphical Miles-English statute Miles-Russian Wersts520
". VII. Conversion of Geographical Miles into Kilometres-AustrianMiles-Prussian Miles-German Miles-Nautical Leagues-French Leagues-English Statute Miles_Russian Wersts523
.- VII. Conversion of English Statute Miles into Kilometres-Austrian Miles_Prussian Miles-German Miles—Namtical Leagues- French Leagues-Geographical Miles-Russian Wersts ..... 526
- 1X. Conversion of Russian Wersts into Kilometres-Austrian Miles-l'russian Miles - German Miles - Nantical Leagues-French Leagues-Geographical Miles-English Statute Miles 52.9
". X. Table for Comparing the most Important Itinerary Measures ..... 532
c.) Comparisen of the most important measures of Geographical Surfaces ..... 533
'table l. Conversion of' Square Kilometres into Austrian Square Miles- Prussian Square Miles_German Square Miles - Nantical Square Leagnes - French Square Leagues - Geographical Square Miles_English Square Statute Miles-Russian Square Wersts ..... 537
II. Conversion of Anstrian Square Miles into Square Kilometres- Prussian Square Miles-German Square Miles-Nautical Square Leagues - French Square Leagues - Geographical Square Miles_English Square Statute Miles_Russian Square Wersts ..... 540" III. Conversion of Prussian Square Miles into Square Kilometres-Austrian Square Miles-German Square Miles-NauticalSquare Leagnes - French Square Leagues - GeographicalSquare Miles - English Square Statute Miles - RussianSquare Wersts543
" IV. Conversion of German Square Miles into Square Kilometres-Austrian Square Miles-Prussian Square Miles-NauticalSquare Leagues - French Square Leagues - GeographicalSquare Miles - English Square Statute Miles - RussianSquare Wersts546
Table V. Conversion of Nautical Square Leagues into Square Kilometres -Austrian Square Miles-Prussian Square Miles-German Square Miles_French Square Leagues-Geographical Square Miles_English Square Statute Miles_Russian Square Wersts ..... 549
" VI. Conversion of French Square Leagues into Square Kilometres -Austrian Square Miles-Prussian Square Miles—German Square Miles - Nautical Square Leagues - Geographical Square Miles_English Square Statute Miles_Russian Square Wersts ..... 55.3
" VII. Conversion of Geographical Square Miles into Square Kilo- metres-Austrian Square Miles - Prussian Square Miles- German Square Miles - Nautical Square Leagues-French Syuare Leagues - English Square Statute Miles - Russian Square Wersts ..... 555
" VIII. Conversion of English Square Statute Miles into Square Kilo- metres-Austrian Square Miles - Prussian Square Miles_ German Square Miles-Nantical Square Leagues - French Square Leagues—Geographical Square Miles_Russian Square Wersts ..... 558
" IX. Conversion of Russian Square Wersts into Square Kilometres -Austrian Square Miles_Prussian Square Miles_German Square Miles - Nautical Square Leagues - French Square Leagues_Geographical Square Miles_English Square Statute Miles ..... 561
" X. Table for comparing the most important Measures of Surface ..... 564
VI. METEOROLOGICAL TABLES FOR CORRECTING SERIES OF OBSERVATIONS FOR THE PERIODIC AND NON- PERIODIC VARIATIONS ..... 56.5
Temperature.-Hourly Corrections for Periodic Variations.NORTIf AMERICA.
Table I. Washington, D. C. ..... 579
، II. Philadelphia, Girard College ..... 579
" III. ..... 580
" IV. Frankfort Arsenal, Pa. ..... 581
، $\quad \mathrm{V}$. ..... 582
.، VI. Toronto, Canada West ..... 583
." VII. ..... 584
". VIII. ..... 585
" IX. ..... 586
" X. Montreal, Canada East ..... 586
" XI. Sitka, Alaska ..... 587
Table XII. Boothia Felix, Arctic America ..... 588
XIII. Lake Athabasca, ..... 589
" XIV. Melville Island, ..... 589
XV. Hecla Cove, Spitzbergen ..... 589
APPENDIX.
$\mathbf{V}^{\prime}$. Amherst College, Mass. ..... 592
SOUTII AMERICA.
XVI. Rio Janeiro, Brazil ..... 590
XVII ..... 591
ASIA.
XVIII. Trivandrum, India ..... 595
XIX. ..... 596
XX. Madras, ..... 597
XXI. " ..... 598
XXII. Bombay, ..... 599
XXIII. ،6 ..... 600
XXIV. Madras, ..... 601
XXV. Bombay, ..... 601
XXVI. Calcutta, ..... 602
XXVII. 'Tiflis, Georgia ..... 603
XXVIII. Pekin, China ..... 603
XXIX. Nertchinsk, Siberia ..... 604
XXX. ..... 605
XXXI. Bernaul, ..... G06
XXXII. " ..... 607
XXXIII. ..... 608
EdROPE
XXXIV. Rome, Italy ..... 611
XXXY. Padua, ..... 612
XXXYI. Geneva, Switzerland ..... 613
XXXVII. " ..... 613
XXXVII. St. Bernard, ..... 614
XXXIX. ..... 614
XL. Kremsmïnster, Austria . ..... 615
NLI. Salzburg, ..... 616
XLII. Municl, Bavaria ..... 616
XLIII. Prague, Bohemia ..... 617
XLIV. ..... 618
XLV. Plymouth, England ..... 61!
XLVI. ..... 620
Table XLYII. Brussels, Belginm ..... 621
SLVII. ..... $6 \div 2$
NLIX. Schwerin, Germany ..... $62:$
L. Mühllansen, Prussia ..... 623
LI. Utrecht, Hollam! ..... 624
LII. Greenwich, England ..... 624
" LIII. ..... 625624
.. LT. Halle, Prussia ..... 627
LVI. Göttingen, IIanover ..... 628
LVII. Berlin, Prussia ..... 629
" LVII. Salzuflen, Germany ..... 630
" LYIX. Stettin, ..... 631
" LX. Apremade, Sleswick ..... 632
LXI. Leith, Scotland ..... 633
LXII. " ..... 634
" LXlII. Makerstown, Scotland ..... 635
" LXIV. Dablin, Ireland ..... 635
.. LNV. Catherinenburg, Russia ..... 636
-• LNTI. ..... 637
" LXVII. St. Petersburg, ..... 637
" LAVIII. IIelsingfors, Finland ..... 638
.. LXIX. St. Petersburg, Russia ..... 639
.- LXX. Helsingsfors, Finland ..... 640
". LXXI. Christiania, Norway ..... 641
.. LXXII. Drontheim, ..... 642
، LXXIII. Strait of Kara, Russia ..... 643
.. LXXIV. Matoschkin Schar, Novaia Zemblia ..... 644
.- LXAT. Bosekop, Norway ..... 645
.. LXXV'. ..... 645
AFRICA AND AUSTRALIA.
LXXVI. St. Helena ..... 649
، LXXVII. Cape of Good Hope, Africa ..... 649
" LXXVIII. Hobarton, 'Tasmania ..... 650
Monthly Corrections for Non-Periodic Variations.
" LXXIX. Madras, India ..... 654
" LXXX. Palermo, Sicily ..... 655
" LXXXI. Milan, Italy ..... 656
". LXXXII. Geneva, Switzerland ..... 658
" LXXXIII. Viemna, Austria ..... 660
-- LXXXIV. Ratisbon, Austria ..... 661
" LXXXV. Stuttgart, South Germany ..... 663page
Table LXXXVI. Carlsruhe, South Germany ..... 664
" LNXXVII. Berlin, Prussia ..... $66 \%$
"LXXXVIII. Copenhagen, Denmark ..... 669
" LXXXIX. Paris, France ..... 671
" XC. Zwamenburg, Holland ..... 67 2
". XCI. London, England ..... 674
" XCII. Kinfams Castle, Scotland ..... 676
.- XCIII. Tornei, Finland ..... 676
." XCIV. Albany, N. Y. ..... 677
" XCV. Salem, Mass. ..... 67s
" XCVI. Reikiarik, Ieeland ..... 679
". XCVII. Godthat, Greenland ..... 679
Force of Vapor and Relatice Humidity.
" XCYIII. Greenwich, England, Force of Vapor, by Glaisher ..... 68:;
" XCIX. Greenwich, England, Relative Humidity, by Glaisher ..... 684
VII. MISCELLANEOCS ME'TEOROLOGICAL TABLES ..... $68 \%$
Table I. Positions of the Principal Observatories ..... 689
" II. To convert parts of the Equator in Are into Sidereal Time, or to convert Terrestrial Longitude in Are into Time ..... $69:$
" III. To convert Sidereal Time into parts of the Equator in Arc, or to convert Time into Terrestrial Longitude in Are ..... 695
" IV. For converting Sidereal Time into Mean Solar Time, and Mean Solar Time into Sidereal Time ..... 696
" V. Correction of the Time obtained by observation of the Sun in order to have the True Time of the Clock ..... 697
" VI. Tables giving the Length of a Degree of the Meridian and of the Parallel . ..... 698
" VII. Tables for computing Terrestrial Surfares ..... 703
" VIII. Comparison of the Standards of Length of England, France, Belgium, Prussia, Russia, India, and Australia ..... 709
" IX. Table for giving the Length of Insolation for any given Latitude ..... 711


# METEOROLOGICAL TABLES. 

SERIES I.
'I H ERMOMETRICAL TABLES.

## CONTENTS.

## COMPARISON OF THE THERMOMETRICAL SCALES.

(The figures refer to the folio at the hottom of the page.)
Table 1. Comparison of Fahrenheit's Scale with the Centigrade and Reau-
mur's, full degrees, from $+212^{\circ}$ to $-39^{\circ}$, . . . 8
" Il Comparison of the Centigrade Scale with Reaumur's and Fahrenheit's, full degrees, from $+100^{\circ}$ to $+50^{\circ}$, . . . . . 10
" III. Comparison of Reaumur's Scale with Fahrenheit's and the Centi-
grade, full degrees, from $+80^{\circ}$ to $+40^{\circ}$, . . . . 10
" IV. Conversion of Degrees of Fahrenheit into Centigrade Degrees, for every tenth of a degree, from $+122^{\circ}$ to $-76^{\circ}$ F., . . . 13
". V. Conversion of Degrees of Fahrenheit into Degrees of Reaumur, for $\quad$ every tenth of a degree, from $+122^{\circ}$ to $-38^{\circ} \mathrm{F}$., . . . 18
" VI. Conversion of Centigrade Degrees into Degrees of Fahrenheit, for every tenth of a degree, from $+50^{\circ}$ to $-54^{\circ}$, and from $+100^{\circ}$ to $+89^{\circ}$ C., . . . . . . . . . . 25
" VII. Conversion of Centigrade Degrees into Degrees of Reaumur, for every
tenth of a degree, from $+40^{\circ}$ to $-40^{\circ} \mathrm{C}$. . . . . 28
" VIII. Conversion of Degrees of Reaumur into Degrees of Fahrenheit, for every tenth of a degree, from $+40^{\circ}$ to $-40^{\circ}$ R., . . . 30
" IX. Conversion of Degrees of Reaumur into Centigrade Degrees for every $\begin{gathered}\text { tenth of a degree, from }+40^{\circ} \text { to }-40^{\circ} \text { R., . . . . } 32\end{gathered}$
" X. Value of any number of Degrees of Fahrenheit, expressed by a cor-
" XI. Value of any number of Degrees of Fahrenheit, expressed by a cor- $\quad 31$
'6 XII. Value of any number of Centigrade Degrees, expressed by a cor-
'6 XIII. Value of any number of Centigrade Degrees, expressed by a corresponding number of Degrees of Fabrenheit, . . . . 35
"XIV. Value of any number of Degrees of Reaumur, expressed by a cor-
responding number of Centigrade Degrees, . . . . . 35
" XV. Value of any number of Degrees of Reaumur expressed by a cor-
responding number of Degrees of Fahrenheit, . . . . 35 A

# I. - III. <br> GENERAL COMPARISON 

${ }^{0}$

# THE THERMOMETRICAL SCALES, 

OR

TABLES

showing the corresponding values of eacil full degree of failreniieit's, Centigrade, and reaumur's thermoneters, from $+212^{\circ}$ то $-39^{\circ}$ FAHRENHEIT.

## ©OMPARISON OF THE THERMOME'TRICAL SCALES.

The first three tables of this set give a simultaneous comparison of the three scales mostly used at present in Meteorology, and espeeially of the portion of the seales not comprised in the more extensive tables which follow them. They form thus a complement to these last tables; but as most' of the temperatures contained in them do not occur in Meteorology, the comparison of the full degrees was found sufficient.

These three tables have been taken from E. L. Schubarth's Collection of Physical Tables.' Berlin, 1836.

Tables IV. to IX. being more useful to the Meteorologist, the calculation has been carried out for every tenth of a degree. Tables VII. and IX. are from the Annuaire Météorologique de France; the others have been calculated.

A comparison of the Centigrade and Fahrenheit degrees near the boiling point, for every tenth of a degree, for the sake of the comparison of standard thermometers, will be found at the end of Table VI.

Tables X. to XV. will be found useful for comparing differential results, such as ranges of temperature, and any relative amount expressed in degrees of different acales, without reference to their respective zeros.

## I COMPARISON OF FAHRENHEIT'S THERMOMETRICAL SCALE WITH THE

## CENTIGRADE AND REAUMUR'S.

$x^{\circ}$ Fahr. $=\left(x^{\circ}-32^{\circ}\right) \frac{5}{9}$ Centig. $=\left(x^{\circ}-32^{\circ}\right) \frac{4}{9}$ Reaum.

| Fahren. | Centigrade. | Reaumur. | Fahren. | Centigrade. | Reaumur. | Fahren. | Centigrade. | Reaumur. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +212 | +100.00 | +80.00 | $+172$ | +77.78 | +62.22 | $+132$ | $+55.56$ | +44.44 |
| 211 | 99.44 | 79.56 | 171 | 77.22 | 61.78 | 131 | 55.00 | . 4.00 |
| 210 | 98.89 | 79.11 | 170 | 76.67 | 61.33 | 130 | 54.44 | 43.56 |
| 209 | 93.33 | 78.67 | 169 | 76.11 | 60.89 | 129 | 53.89 | 43.11 |
| 208 | 97.78 | 78.22 | 168 | 75.56 | 60.44 | 128 | 53.33 | 42.67 |
| 207 | 97.22 | 77.78 | 167 | 75.00 | 60.00 | 127 | 52.78 | 42.22 |
| 206 | 96.67 | 77.33 | 166 | 74.44 | 59.56 | 126 | 52.22 | 41.78 |
| 205 | 96.11 | 76.59 | 165 | 73.59 | 59.11 | 125 | 51.67 | 41.33 |
| 204 | 95.56 | 76.44 | 164 | 73.83 | 58.67 | 124 | 51.11 | 40.89 |
| 203 | 95.00 | 76.00 | 163 | 72.78 | 58.22 | 123 | 50.56 | 40.44 |
| 202 | 94.44 | 75.56 | 162 | 72.22 | 57.78 | 122 | 50.00 | 40.00 |
| 201 | 93.89 | 75.11 | 161 | 71.67 | 57.33 | 121 | 49.44 | 39.56 |
| 200 | 93.33 | 74.67 | 160 | 71.11 | 56.89 | 120 | 48.89 | 39.11 |
| 199 | 92.78 | 74.22 | 159 | 70.56 | 56.44 | 119 | 48.33 | 38.67 |
| 198 | 92.22 | 73.78 | 158 | 70.00 | 56.00 | 118 | 47.78 | 38.22 |
| 197 | 91.67 | 73.33 | 157 | 69.44 | 55.56 | 117 | 47.22 | 37.78 |
| 196 | 91.11 | 72.89 | 156 | 68.89 | 55.11 | 116 | 46.67 | 37.33 |
| 195 | 90.56 | 72.44 | 155 | 68.33 | 54.67 | 115 | 46.11 | 36.89 |
| 194 | 90.00 | 72.00 | 154 | 67.78 | 54.22 | 114 | 45.56 | 36.44 |
| 193 | S9.44 | 71.56 | 153 | 67.22 | 53.78 | 113 | 45.00 | 36.00 |
| 192 | 88.89 | 71.11 | 152 | 66.67 | 53.33 | 112 | 44.44 | 35.56 |
| 191 | 58.33 | 70.67 | 151 | 66.11 | 52.89 | 111 | 43.89 | 35.11 |
| 190 | 87.78 | 70.22 | 150 | 65.56 | 52.44 | 110 | 43.33 | 34.67 |
| 189 | 87.22 | 69.78 | 149 | 65.00 | 52.00 | 109 | 4278 | 34.22 |
| 158 | S6.67 | 69.33 | 148 | 64.44 | 51.56 | 108 | 42.22 | 33.78 |
| 187 | 86.11 | 68.89 | 147 | 63.89 | 51.11 | 107 | 41.67 | 33.33 |
| 186 | 85.56 | 68.44 | 146 | 63.33 | 50.67 | 106 | 41.11 | 32.89 |
| 185 | 85.00 | 68.00 | 145 | 62.78 | 50.22 | 105 | 40.56 | 32.44 |
| 184 | 84.44 | 67.56 | 144 | 62.22 | 49.78 | 104 | 40.00 | 32.00 |
| 183 | 83.59 | 67.11 | 143 | 61.67 | 49.33 | 103 | 39.44 | 31.56 |
| 152 | 83.33 | 66.67 | 142 | 61.11 | 48.89 | 102 | 38.89 | 31.11 |
| 181 | 82.78 | 66.22 | 141 | 60.56 | 48.44 | 101 | 38.33 | 30.67 |
| 180 | 82.22 | 65.78 | 140 | 60.00 | 48.00 | 100 | 37.78 | 30.22 |
| 179 | 81.67 | 65.33 | 139 | 59.44 | 47.56 | 99 | 37.22 | 29.78 |
| 178 | 81.11 | 64.89 | 138 | 58.89 | 47.11 | 98 | 36.67 | 29.33 |
| 177 | 80.56 | 64.44 | 137 | 58.33 | 46.67 | 97 | 36.11 | 28.89 |
| 176 | 80.00 | 64.00 | 136 | 57.78 | 46.22 | 96 | 35.56 | 28.44 |
| 175 | 79.44 | 63.56 | 135 | 57.22 | 45.78 | 95 | $35 . \mathrm{rr}$ | 28.00 |
| 174 | 78.59 | 63.11 | 134 | 56.67 | 45.33 | 94 | 34.44 | 27.56 |
| 173 | 78.33 | 62.67 | 133 | 56.11 | 44.89 | 93 | 33.89 | 27.11 |

$x^{\circ}$ Fahr. $=\left(x^{\circ}-32^{\circ}\right){ }_{9}^{5}$ Centig. $=\left(x^{\circ}-32^{\circ}\right)_{4}^{4}$ Reaum.

| Fahren. | Centigrade. | Reaumur. | Fahren. | Centigrade. | Reaumur. | Fahren. | Centigrade. | Reiumur. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +92 | +33.33 | +26.67 | +48 | + 8.89 | $+7.11$ | $+4$ | -15.56 | -12.44 |
| 91 | 32.78 | 26.22 | 47 | 8.33 | 6.67 | 3 | -16.11 | -12.89 |
| 90 | 32.22 | 25.78 | 46 | 7.78 | 6.22 | 2 | -16.67 | -13.33 |
| 89 | 31.67 | 25.33 | 45 | 7.22 | 5.78 | 1 | -17.22 | -13.78 |
| S8 | 31.11 | 24.89 | 44 | 6.67 | 5.33 | 0 | -17.78 | -14.22 |
| 87 | 30.56 | 24.44 | 43 | 6.11 | 4.89 | - 1 | -18.33 | -14.67 |
| 86 | 30.00 | 24.00 | 42 | 5.56 | 4.44 | -2 | -18.89 | -15.11 |
| 85 | 29.44 | 23.56 | 41 | 5.00 | 4.00 | - 3 | -19.44 | -15.56 |
| 84. | 28.89 | 23.11 | 40 | 4.44 | 3.56 | - 4 | -20.00 | -16.00 |
| 83 | 25.33 | 22.67 | 39 | 3.89 | 3.11 | - 5 | -20.56 | -16.44 |
| 82 | 27.78 | 22.22 | 38 | 3.33 | 2.67 | - 6 | -21.11 | -16.89 |
| S1 | 27.22 | 21.78 | 37 | 2.75 | 2.22 | $-7$ | -21.67 | -17.33 |
| 80 | 26.67 | 21.33 | 36 | 2.22 | 1.78 | -8 | -22.22 | -17.78 |
| 79 | 26.11 . | 20.89 | 35 | 1.67 | 1.38 | - 9 | -22.78 | -18.22 |
| 78 | 25.56 | 20.44 | 34 | 1.11 | 0.59 | -10 | -23.33 | -18.67 |
| 77 | 25.00 | 20.00 | 33 | 0.56 | 0.44 | -11 | -23.89 | -19.11 |
| 76 | 24.44 | 19.56 | 32 | 0.00 | 0.00 | -12 | -24.44 | -19.56 |
| 75 | 23.89 | 19.11 | 31 | $-0.56$ | -0.44 | -13 | -25.00 | -20.00 |
| 74 | 23.33 | 18.67 | 30 | - 1.11 | -0.s9 | -14 | -25.56 | -20.41 |
| 73 | 22.78 | 18.22 | 29 | - 1.67 | - 1.33 | -15 | --26.11 | -20.89 |
| 72 | 22.22 | 17.78 | 28 | - 2.22 | - 1.78 | -16 | -26.67 | -21.33 |
| 71 | 21.67 | 17.33 | 27 | - 2.78 | - 2.22 | -17 | -27.22 | -21.7S |
| 70 | 21.11 | 16.89 | 26 | - 3.33 | - 2.67 | -18 | -27.78 | -22.22 |
| 69 | 20.56 | . 16.44 | 25 | - 3.89 | - 3.11 | -19 | -28.33 | -22.67 |
| 68 | 20.00 | 16.00 | 24 | - 4.44 | - 3.56 | -20 | -25.89 | -23.11 |
| 67 | 19.44 | 15.56 | 23 | - 5.00 | $-4.00$ | -21 | -29.44 | -23.56 |
| 66 | 18.89 | 15.11 | 22 | $-5.56$ | - 4.44 | -22 | $-30.00$ | -24.00 |
| 65 | 18.33 | 14.67 | 21 | $-6.11$ | - 4.89 | -23 | -30.56 | -24.44 |
| 64 | 17.78 | 14.22 | 20 | - 6.67 | - 5.33 | -24 | -31.11 | -24.89 |
| 63 | 17.22 | 13.78 | 19 | - 7.22 | - 578 | -25 | -31.67 | -2.5.33 |
| 62 | 16.67 | 13.33 | 18 | - 7.78 | -6.22 | -26 | -32.22 | -25.78 |
| 61 | 16.11 | 12.89 | 17 | - 5.33 | -6.67 | -27 | -32.78 | -26.22 |
| 60 | 15.56 | 12.44 | 16 | - 8.59 | $-7.11$ | -28 | -33.33 | -26.67 |
| 59 | 15.00 | 12.00 | 15 | - 9.44 | - 7.56 | -29 | -33.89 | -27.11 |
| 58 | 14.44 | 11.56 | 14 | -10.00 | - 8.00 | -30 | -34.44 | $-27.56$ |
| 57 | 13.59 | 11.11 | 13 | -10.56 | -8.44 | -:31 | -35.00 | -28.00 |
| 56 | 13.33 | 10.67 | 12 | $-11.11$ | - 8.59 | -32 | -35.56 | -28.44 |
| 55 | 12.78 | 10.22 | 11 | -11.67 | -9.33 | -33 | -36.11 | -28.89 |
| 54 | 12.22 | 9.78 | 10 | $-12.22$ | -9.78 | -34 | -36.67 | -29.33 |
| 53 | 11.67 | 9.33 | 9 | -12.78 | -10.22 | -35 | -37.22 | -29.78 |
| 52 | 11.11 | 8.89 | 8 | -13.33 | -10.67 | -36 | -37.75 | -30.22 |
| 51 | 10.56 | 8.44 | 7 | -13.89 | -11.11 | -37 | $-38.33$ | -30.67 |
| 50 | 10.00 | 8.00 | 6 | -14.44 | -11.56 | -38 | -38.89 | -31.11 |
| 49 | 9.44 | 7.56 | 5 | $-15.00$ | -12.00 | -39 | -39.44 | -31.56 |
|  |  |  |  |  |  |  |  |  |
| For the Continuation see Table IV. and V. |  |  |  |  |  |  |  |  |

A
II. COMPARISON OF THE CENTIGRADE THERMOMETER WITH REAUMUR'S AND FAHRENIIEIT'S.
$x^{\circ}$ Centig. $=\left(32+\frac{9}{5} x^{0}\right)$ Fahr. $=\frac{4}{5} x^{0}$ Reaum.

| Centig. | Reaumur. | Fahrenheit. | Centig. | Reaumur. | Fahrenheit. | Centig. | Reaumur. | Fahrenheit. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $+100$ | +80.0 | $+212.0$ | +83 | +66.4 | +181.4 | $+66$ | +52.8 | +150.8 |
| 99 | 79.2 | 210.2 | 82 | 6.56 | 179.6 | 6.5 | 52.0 | 149.0 |
| 98 | 78.4 | 208.4 | 81 | 64.8 | 177.8 | 64 | 51.2 | 147.2 |
| 97 | 77.6 | 206.6 | So | 64.0 | 176.0 | 63 | 50.4 | 145.4 |
| 96 | 76.8 | 204.8 | 79 | 63.2 | 174.2 | 62 | 49.6 | 143.6 |
| 95 | 76.0 | 203.0 | 78 | 62.4 | 172.4 | 61 | 48.8 | 141.8 |
| 94 | 75.2 | 201.2 | 77 | 61.6 | 170.6 | 60 | 48.0 | 140.0 |
| 93 | 74.4 | 199.4 | 76 | 60.8 | 168.8 | 59 | 47.2 | 138.2 |
| 92 | 736 | 197.6 | 75 | 60.0 | 167.0 | 58 | 46.4 | 136.4 |
| 91 | 72.8 | 19.5 .8 | 74 | 59.2 | 16.). 2 | 57 | 45.6 | 134.6 |
| 90 | 72.0 | 194.0 | 73 | 58.4 | 163.4 | 56 | 4.8 | 132.8 |
| 89 | 71.2 | 192.2 | 72 | 57.6 | 161.6 | 55 | 44.0 | 131.0 |
| 88 | 70.4 | 190.4 | 71 | . 26.3 | 1.59 .8 | 54 | 43.2 | 129.2 |
| 87 | 69.6 | 188.6 | 70 | 560 | 1.58 .0 | 53 | 42.4 | 127.4 |
| 86 | 68.8 | 186.8 | 69 | 5.52 | 156.2 | 52 | 41.6 | 125.6 |
| 85 | 68.0 | 185.0 | 68 | 54.4 | 154.4 | 51 | 40.8 | 123.8 |
| 84 |  | 183.2 | 67 | 53.6 | 152.6 | 50 | 40.0 | 122.0 |
| For the Contmuation see Tables V. and VI. |  |  |  |  |  |  |  |  |
| III. COMPARISON OF REAUMUR'S THERMOMETER WITH FAHRENIIEIT'S AND TILE CENTIGRADE. <br> $x^{\circ}$ Reaum. $=\left(32^{2}+\frac{9}{4} r^{\infty}\right)$ Fahr. $=\frac{5}{4} x^{2}$ Centig. |  |  |  |  |  |  |  |  |
| Reaumur. | Fahrenheit. | Centigrade. | Reaumur. | Fahrenleit. | Centigrade. | Reaumur. | Fahrenheit. | Centigrade. |
| $+80$ | $+212.00$ | $+100.00$ | $+66$ | $+180.50$ | +82.50 | $+52$ | +149.00 | $+65.00$ |
| 79 | 209.7. | 98.75 | 65 | 17ヶ.2.5 | 81.25 | 51 | 146.75 | 63.75 |
| 78 | 207.50 | 97.50 | 64 | 176.00 | 80.00 | 50 | 14.4 .50 | 62.50 |
| 77 | 20.5 .2 .5 | 962.5 | 63 | 173.75 | 78.75 | 49 | 142.25 | 61.25 |
| 76 | 203.00 | 9.5 .00 | 62 | 171.50 | 77.50 | 48 | 140.00 | 60.00 |
| 75 | 200.75 | 93.75 | 61 | 169.2.5 | 76.25 | 47 | 137.75 | 58.75 |
| 74 | 198.50 | 92.50 | 60 | 167.00 | 75.00 | 46 | 135.50 | 57.50 |
| 73 | 196.25 | 91.25 | 59 | 164.7.5 | 73.75 | 45 | 183.25 | 56.25 |
| 72 | 194.00 | 90.00 | 58 | 162.50 | 72.50 | 44 | 131.00 | 5.5 00 |
| 71 | 191.75 | 88.75 | 57 | 160.25 | 71.25 | 43 | 128.75 | 63.75 |
| 70 | 189.50 | 87.50 | 56 | 158.00 | 70.00 | 42 | 126.50 | 52.50 |
| 69 | 187.25 | 86.25 | 55 | 155.75 | 68.75 | 41 | 124.25 | 51.25 |
| 68 | 185.00 | 85.00 | 54 | 153.50 | 67.50 | 40 | 122.00 | 50.00 |
| 67 | 182.75 | 83.75 | 53 | 151.25 | 66.25 | 39 | 119.75 | 4875 |
|  |  |  |  |  |  |  |  |  |
| For the Continuation see Tables VIII. and IX. |  |  |  |  |  |  |  |  |

## A

IV. - V.

COMPARISON
of

## FAIIRENHEIT'S THERIIOMETER

WITH

THE CENTIGRADE AND WITH THAT OF REAUMLR,
or

TABLES
for converting the degrees of fahrenheit into centigrade degrees and into megrees of reaumur ;
giving the corresponding values for each tenth of a degree, Fron $+122^{\circ}$ ro - $76^{\circ}$ Fallrenheit.
A

| Degrees of Fahrenheit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| +122 | $\begin{array}{r} \text { Centig. } \\ +50.00 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.06 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.11 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.17 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.22 \end{array}$ | $\begin{array}{r} \text { Centig: } \\ +50.28 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.33 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.39 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +50.44 \end{array}$ | $\begin{gathered} \text { Centig. } . \\ +50.50 \end{gathered}$ |
| 121 | 49.44 | 49.50 | 49.56 | 49.61 | 49.67 | 49.72 | 49.78 | 49.83 | 49.89 | 49.94 |
| 120 | 48.89 | 49.94 | 49.00 | 49.06 | 49.11 | 49.17 | 49.22 | 49.25 | 49.33 | 49.39 |
| 119 | 48.33 | 48.39 | 48.44 | 48.50 | 48.56 | 48.61 | 48.67 | 48.72 | 48.78 | 48.83 |
| 118 | 47.78 | 47.83 | 47.89 | 47.94 | 48.00 | 48.06 | 48.11 | 48.17 | 48.22 | 48.28 |
| 117 | 47.22 | 47.28 | 47.33 | 47.39 | 47.44 | 47.50 | 47.56 | 47.61 | 47.67 | 47.72 |
| 116 | 46.67 | 46.72 | 46.78 | 46.83 | 46.89 | 46.94 | 47.00 | 47.06 | 47.11 | 47.17 |
| 115 | 46.11 | 46.17 | 46.22 | 46.28 | 46.33 | 46.39 | 46.44 | 46.50 | 46.56 | 46.61 |
| 114 | 45.56 | 45.61 | 45.67 | 45.72 | 45.78 | 45.83 | 45.59 | 45.94 | 46.00 | 46.06 |
| 113 | 45.00 | 45.06 | 45.11 | 45.17 | 45.22 | 45.28 | 45.33 | 45.39 | 45.44 | 45.50 |
| 112 | 44.44 | 44.50 | 44.56 | 44.61 | 44.67 | 44.72 | 44.78 | 44.83 | 44.89 | 44.94 |
| 111 | 43.59 | 43.94 | 44.00 | 44.06 | 44.11 | 44.17 | 44.22 | 44.28 | 44.33 | 44.39 |
| 110 | 43.33 | 43.39 | 43.44 | 43.50 | 43.56 | 43.61 | 43.67 | 43.72 | 43.78 | 43.83 |
| 109 | 42.78 | 42.83 | 42.89 | 42.94 | 43.00 | 43.06 | 43.11 | 43.17 | 43.22 | 43.28 |
| 108 | 42.22 | 42.28 | 42.33 | 42.39 | 42.44 | 42.50 | 42.56 | 42.61 | 42.67 | 42.72 |
| 107 | 41.67 | 41.72 | 41.78 | 41.83 | 41.89 | 41.94 | 42.00 | 42.06 | 42.11 | 42.17 |
| 106 | 41.11 | 41.17 | 41.22 | 41.28 | 41.33 | 41.39 | 41.44 | 41.50 | 41.56 | 41.61 |
| 105 | 40.56 | 40.61 | 40.67 | 40.72 | 40.78 | 40.83 | 40.89 | 40.9 .4 | 41.00 | 41.06 |
| 104 | 40.00 | 40.06 | 40.11 | 40.17 | 40.22 | 40.28 | 40.33 | 40.39 | 40.44 | 40.50 |
| 103 | 39.44 | 39.50 | 39.56 | 39.61 | 39.67 | 39.72 | 39.78 | 39.83 | 39.59 | 39.94 |
| 102 | 38.89 | 38.94 | 39.00 | 39.06 | 39.11 | 39.17 | 39.22 | 39.28 | 39.33 | 39.39 |
| 101 | 38.33 | 38.39 | 38.44 | 38.50 | 35.56 | 38.61 | 38.67 | 38.72 | 38.78 | 38.83 |
| 100 | 37.78 | 37.83 | 37.59 | 37.94 | 38.00 | 38.06 | 38.11 | 38.17 | 38.22 | 38.25 |
| 99 | 37.22 | 37.28 | 37.33 | 37.39 | 37.44 | 37.50 | 37.56 | 37.61 | 37.67 | 37.72 |
| 98 | 36.67 | 36.72 | 36.78 | 36.53 | 36.89 | 36.94 | 37.00 | 37.06 | 37.11 | 37.17 |
| 97 | 36.11 | 36.17 | 36.22 | 36.28 | 36.33 | 36.39 | 36.44 | 36.50 | 36.56 | 36.61 |
| 96 | 35.56 | 35.61 | 35.67 | 35.72 | 35.78 | 35.83 | 35.89 | 35.94 | 36.00 | 36.06 |
| 95 | 35.00 | 35.06 | 35.11 | 35.17 | 35.22 | 35.28 | 35.33 | 35.39 | 35.44 | 35.50 |
| 94 | 34.44 | 34.50 | 34.56 | 34.61 | 34.67 | 34.72 | 34.78 | 34.83 | 34.89 | 34.94 |
| 93 | 33.89 | 33.94 | 34.00 | 34.06 | 34.11 | 34.17 | 34.22 | 34.28 | 34.33 | 34.39 |
| 92 | 33.33 | 33.39 | 33.44 | 33.50 | 33.56 | 33.61 | 33.67 | 33.72 | 33.78 | 33.83 |
| 91 | 32.78 | 32.83 | 32.89 | 32.94 | 33.00 | 33.06 | 33.11 | 33.17 | 33.22 | 33.28 |
| 90 | 32.22 | 32.28 | 32.33 | 32.39 | 32.44 | 32.50 | 32.56 | 32.61 | 32.67 | 32.72 |
| 89 | 31.67 | 31.72 | 31.75 | 31.83 | 31.89 | 31.94 | 32.00 | 32.06 | 32.11 | 33.17 |
| 88 | 31.11 | 31.17 | 31.22 | 31.28 | 31.33 | 31.39 | 31.44 | 31.50 | 31.56 | 31.61 |
| 87 | 30.56 | 30.61 | 30.67 | 30.72 | 30.78 | 30.83 | 30.89 | 30.94 | 31.00 | 31.06 |
| 86 | 30.00 | 30.06 | 30.11 | 30.17 | 30.22 | 30.28 | 30.33 | 30.39 | 30.44 | 30.50 |
| 85 | 29.44 | 29.50 | 29.56 | 29.61 | 29.67 | 29.72 | 29.78 | 29.83 | 29.59 | 29.94 |
| 84 | 25.89 | 28.94 | 29.00 | 29.06 | 29.11 | 29.17 | 29.22 | 29.28 | 29.33 | 29.39 |
| 83 | 28.33 | 28.39 | 28.44 | 28.50 | 28.56 | 28.61 | 28.67 | 28.72 | 28.78 | 28.83 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

If conversion of degrees of fahrenheit into centigrade degrees.

| Degrees of Fahren. heit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| +82 | $\begin{array}{r} \text { Centig. } \\ +27.78 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +27.83 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +27.89 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +27.94 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +28.00 \end{array}$ | $\begin{gathered} \text { Centig. } \\ +28.06 \end{gathered}$ | $\begin{array}{r} \text { Centig. } \\ +28.11 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +28.17 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +28.22 \end{array}$ | $\begin{array}{r} \text { Centig. } \\ +28.28 \end{array}$ |
| 81 | 27.22 | 27.28 | 27.33 | 27.39 | 27.44 | 27.50 | 27.56 | 27.61 | 27.67 | 27.72 |
| 80 | 26.67 | 26.72 | 26.78 | 26.83 | 26.59 | 26.94 | 27.00 | 27.06 | 27.11 | 27.17 |
| 79 | 26.11 | 26.17 | 26.22 | 26.28 | 26.33 | 26.39 | 26.44 | 26.50 | 26.56 | 26.61 |
| 78 | 25.56 | 25.61 | '25.67 | 25.72 | 25.78 | 25.83 | 25.59 | 25.94 | 26.00 | 26.06 |
| 77 | 25.00 | 25.06 | 25.11 | 25.17 | 25.22 | 2.9 .28 | 25.33 | 25.39 | 25.44 | 25.50 |
| 76 | 24.44 | 24.50 | 24.56 | 24.61 | 24.67 | 24.72 | 24.78 | 24.83 | 24.59 | 24.94 |
| 75 | 23.59 | 23.94 | 24.00 | 24.06 | 24.11 | 24.17 | 24.22 | 24.28 | 24.33 | 24.39 |
| 74 | 23.33 | 23.39 | 23.44 | 23.50 | 23.56 | 23.61 | 23.67 | 23.72 | 23.78 | 23.83 |
| 73 | 22.78 | $2: 3.53$ | 22.59 | 22.94 | 23.00 | 23.06 | 23.11 | 23.17 | 23.22 | 23.28 |
| 72 | 22.22 | 22.28 | 22.33 | 22.39 | 22.44 | 22.50 | 22.56 | 22.61 | 22.67 | 22.72 |
| 71 | 21.67 | 21.72 | 21.78 | 21.53 | 21.89 | 21.94 | 22.00 | 22.06 | 22.11 | 22.17 |
| 70 | 21.11 | 21.17 | 21.22 | 21.28 | 21.33 | 21.39 | 21.44 | 21.50 | 21.56 | 21.61 |
| 69 | 20.56 | 20.61 | 20.67 | 20.72 | 20.78 | 20.83 | 20.89 | 2094 | 21.00 | 21.06 |
| 68 | 20.00 | 20.06 | 20.11 | 20.17 | 20.22 | 20.28 | 20.33 | 20.39 | 20.44 | 20.50 |
| 67 | 19.44 | 19.50 | 19.56 | 19.61 | 19.67 | 19.72 | 19.78 | 19.83 | 19.89 | 19.94 |
| 66 | 18.59 | 18.94 | 19.00 | 19.06 | 19.11 | 19.17 | 19.22 | 19.28 | 19.33 | 19.39 |
| 65 | 18.33 | 18.39 | 18.44 | 18.50 | 18.56 | 18.61 | 18.67 | 18.72 | 18.78 | 18.83 |
| 6.4 | 17.78 | 17.83 | 17.59 | 17.94 | 19.00 | 18.06 | 18.11 | 18.17 | 18.22 | 18.28 |
| 63 | 17.22 | 17.28 | 17.33 | 17.39 | 17.44 | 17.50 | 17.56 | 17.61 | 17.67 | 17.72 |
| 62 | 16.67 | 16.72 | 16.75 | 16.83 | 16.59 | 16.94 | 17.00 | 17.06 | 17.11 | 17.17 |
| 61 | 16.11 | 16.17 | 16.22 | 16.28 | 16.33 | 16.39 | 16.44 | 16.50 | 16.56 | 16.61 |
| 60 | 15.56 | 15.61 | 15.67 | 15.72 | 15.78 | 15.53 | 15.89 | 15.94 | 16.00 | 16.06 |
| 59 | 15.00 | 15.06 | 15.11 | 15.17 | 15.2. | 15.25 | 1.5 .33 | 15.39 | 15.44 | 15.50 |
| 59 | 14.44 | 14.50 | 14.56 | 14.61 | 14.67 | 14.72 | 14.75 | 14.83 | 14.89 | 14.94 |
| 57 | 13.59 | 13.94 | 14.00 | 14.06 | 11.11 | 14.17 | 14.22 | 14.28 | 14.33 | 14.39 |
| 56 | 13.33 | 13.39 | 13.44 | 13.50 | 13.56 | 13.61 | 13.67 | 13.72 | 13.78 | 13.83 |
| . 53 | 12.78 | 12.83 | 12.59 | 12.94 | 13.00 | 13.06 | 13.11 | 13.17 | 13.22 | 13.28 |
| 54 | 12.22 | 12.28 | 12.33 | 12.39 | 12.44 | 12.50 | 12.56 | 12.61 | 12.67 | 12.72 |
| 53 | 11.67 | 11.72 | 11.78 | 11.83 | 11.59 | 11.94 | 12.00 | 12.06 | 12.11 | 12.17 |
| 52 | 11.11 | 11.17 | 11.22 | 11.28 | 11.33 | 11.39 | 11.44 | 11.50 | 11.56 | 11.61 |
| 51 | 10.56 | 10.61 | 10.67 | 10.72 | 10.78 | 10.83 | 10.89 | 10.94 | 11.00 | 11.06 |
| 50 | 10.00 | 10.06 | 10.11 | 10.17 | 10.22 | 10.25 | 10.33 | 10.39 | 10.44 | 10.50 |
| 49 | 9.44 | 9.50 | 9.56 | 9.61 | 9.67 | 9.72 | 9.78 | 9.83 | 9.89 | 9.94 |
| 48 | S.89 | S. 94 | 9.00 | 9.06 | 9.11 | 9.17 | 9.22 | 9.28 | 9.33 | 9.39 |
| 47 | 8.33 | 8.39 | 8.44 | 8.50 | 8.56 | 8.61 | 8.67 | 8.72 | 8.78 | 8.83 |
| 46 | 7.78 | 7.83 | 7.89 | 7.94 | 8.00 | 8.06 | 8.11 | 8.17 | 8.22 | 8.28 |
| 45 | 7.22 | 7.28 | 7.33 | 7.39 | 7.44 | 7.50 | 756 | 7.61 | 7.67 | 7.72 |
| 44 | 6.67 | 6.72 | 6.78 | 6.83 | 6.59 | 6.94 | 7.00 | 7.06 | 7.11 | 7.17 |
| 43 | 6.11 | 6.17 | 6.22 | 6.28 | 6.33 | 6.39 | 6.44 | 6.50 | 6.56 | 6.61 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |




| Degrees of Fahrenheit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 \% | 8. | 9. |
|  | Centig. | Centig. | Centig. | Centig. | Cer | Centig. | Centig. | ig. | Centig. | g. |
| -37 | -38.33 | --38.39 | -38.44 | -38.50 | -38.56 | -35.61 | -38.67 | -38.72 | $-38.78$ | -38.83 |
| -38 | -38.89 | -38.94 | -39.00 | -39.06 | -39.11 | -39.17 | -39.22 | -39.28 | -39.33 | -39.39 |
| -39 | -39.44 | -39.50 | -39.56 | -39.61 | -39.67 | -39.72 | -39.78 | -39.83 | -39.89 | -39.94 |
| -40 | -40.00 | -40.06 | -40.11 | -40.17 | $-40.22$ | -40.28 | -40.33 | $-40.39$ | $-40.44$ | -40.50 |
| -41 | -40.56 | -40.61 | -40.67 | -40.72 | $-40.78$ | -40.83 | $-40.59$ | $-40.94$ | $-41.00$ | $-41.06$ |
| -42 | $-41.11$ | -41.17 | -41.22 | -41.28 | -41.33 | -41.39 | -41.44 | $-41.50$ | $-41.56$ | -41.61 |
| -43 | -41.67 | -41.72 | -41.78 | -41.83 | -41.89 | -41.94 | $-42.00$ | -42.06 | -42.11 | -42.17 |
| -44 | -42.22 | -42.28 | -42.33 | -42.39 | -42.44 | $-42.50$ | -42.56 | $-42.61$ | $-42.67$ | -42.72 |
| -45 | -42.78 | -42.93 | -42.59 | -42.94 | -43.00 | -43.06 | -43.11 | -43.17 | -43.22 | -43.28 |
| $-46$ | -.13.33 | -43.39 | -43.44 | -43.50 | $-43.56$ | -43.61 | -43.67 | -43.72 | $-43.78$ | -43.83 |
| -47 | -43.89 | -43.94 | -14.00 | -44.06 | -44.11 | -44.17 | -44.22 | -44.28 | -44.33 | -44.39 |
| -48 | -44.44 | $-44.50$ | -44.56 | -44.61 | -44.67 | -44.72 | -44.78 | $-44.83$ | $-44.89$ | -44.94 |
| -49 | -45.00 | -4.5.06 | - 45.11 | $-45.17$ | -4.5.22 | -45.28 | -45.33 | $-45.39$ | $-45.44$ | $-45.50$ |
| -50 | -45.56 | -45.61 | -45.67 | -45.72 | -45.78 | $-45.83$ | -45.89 | $-4.5 .94$ | $-16.00$ | $-46.06$ |
| -51 | -46.11 | -46.17 | -46.22 | -46.28 | $-46.33$ | $-46.39$ | -46.44 | $-46.50$ | $-46.56$ | -46.61 |
| -52 | -46.67 | -46.72 | -46.78 | -46.83 | $-46.89$ | -46.94 | -47.00 | $-47.06$ | -47.11 | -47.17 |
| -58 | -47.22 | -47.28 | $-47.33$ | -47.39 | -47.44 | -47.50 | -47.56 | -47.61 | -47.67 | $-47.72$ |
| -54 | -47.78 | -47.83 | -47.59 | -47.94 | $-48.00$ | -48.06 | -48.11 | $-48.17$ | $-48.22$ | -48.28 |
| -55 | -48.33 | -48.39 | -48.44 | -48.50 | -48.56 | -48.61 | -48.67 | $-48.72$ | -48.78 | -48.83 |
| $-56$ | -43.59 | -48.94 | -49.00 | -49.06 | $-49.11$ | -49.17 | -49.22 | $-49.2 \mathrm{~S}$ | $-49.33$ | -49.39 |
| -57 | -49.44 | -49.50 | -49.56 | -49.61 | -49.67 | -49.72 | -49.78 | -49.53 | -49.89 | -49.94 |
| -58 | -50.00 | -50.06 | -50.11 | -50.17 | $-50.22$ | -50.28 | -50.33 | -50.39 | -50.44 | -50.50 |
| -59 | -50.56 | -50.61 | -50.67 | $-50.72$ | -50.78 | -50.53 | -50.59 | -50.94 | $-51.00$ | -51.06 |
| -60 | -51.11 | -51.17 | -51.22 | $-51.28$ | -51.33 | -51.39 | -51.44 | -51.50 | $-51.56$ | -51.61 |
| $-61$ | -51.67 | -51.72 | $-51.78$ | -51.83 | $-51.89$ | -51.94 | $-52.00$ | $-52.06$ | -52.11 | -52.17 |
| -62 | -52.22 | -52.29 | $-52.33$ | -52.39 | -52.44 | -52.50 | -52.56 | -32.61 | -52.67 | -52.72 |
| -63 | -52.78 | -52.83 | -52.59 | -52.91 | $-53.00$ | -53.06 | -53.11 | $-53.17$ | $-53.22$ | -53.28 |
| -64 | -53.33 | -53.39 | -53.44 | -53.50 | $-53.56$ | -53.61 | -53.67 | $-53.72$ | -53.75 | -53.83 |
| -65 | -53.89 | -53.94 | $-54.00$ | -54.06 | -54.11 | -54.17 | -54.22 | -54.2S | $-54.33$ | -54.39 |
| -66 | -54.44 | -54.50 | $-54.56$ | -54.61 | -54.67 | $-.54 .72$ | $-54.75$ | -54.83 | $-54.89$ | -54.94 |
| -67 | -5.5.00 | -55.06 | -5.5. 11 | -55.17 | -55.22 | -5.5.29 | -55.33 | -55.39 | -55.44 | -55.50 |
| -6S | -5.5.56 | -55.61 | -5.5.67 | -55.72 | -5.5.78 | -.55.83 | -55.59 | -5.5.94 | $-56.00$ | $-56.06$ |
| -69 | -.56.11 | -56.17 | $-56.22$ | -. 6.28 | -56.39 | $-56.39$ | -56.44 | -56.50 | -56.56 | $-56.61$ |
| -70 | -56.67 | -56.72 | -56.78 | -56.83 | -56.89 | -56.94 | $-57.00$ | -57.06 | $-57.11$ | -57.17 |
| -71 | -57.22 | -57.28 | $-57.33$ | -57.39 | -57.44 | $-.57 .50$ | -57.56 | -57.61 | $-57.67$ | $-57.12$ |
| -72 | -57.78 | -57. 53 | -57. 39 | -57.94 | $-58.00$ | -58.06 | -58.11 | -58.16 | -58.22 | -58.28 |
| -73 | -58.33 | -58.39 | -58.44 | -58.50 | -58.56 | -58.61 | -58.67 | -58.72 | -.58.78 | -58.83 |
| -74 | -58.39 | -58.94 | -59.00 | -59.06 | -59.11 | -59.17 | -59.22 | -59.28 | -59.33 | -.59.39 |
| -75 | -59.44 | -59.50 | -59.56 | -59.61 | -59.87 | -59.72 | -59.78 | -59.83 | -59.59 | -59.94 |
| -76 | -60.00 | -60.06 | -60.11 | -60.17 | -60.22 | -60.28 | -60.33 | -60.39 | -60.44 | -60.50 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

A

| Degrees of Fahtenheit. | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Reaumur. | Reaumur | Reammar | Reammur. | Reammur | Reaumur. | Reaumur. | Reaumar. | Reaumur. | Reammur. |
| +122 | +40.00 | + +40.04 | +40.09 | +40.13 | +10.18 | +40.22 | $+40.27$ | $+10.31$ | +40.36 | +40.40 |
| 121 | 39.56 | 39.60 | 39.64 | 39.69 | 39.73 | 39.75 | 39.82 | 39.57 | 39.91 | 39.96 |
| 120 | 39.11 | 39.16 | 39.20 | 39.24 | 39.29 | 39.33 | 39.38 | 39.42. | 39.47 | 39.51 |
| 119 | 38.67 | 38.71 | 38.76 | 38.50 | 35.84 | 38.89 | 38.93 | 35.95 | 39.02 | 39.07 |
| 119 | 38.22 | 38.27 | 35.31 | 35.36 | 38.40 | 38.41 | 38.49 | 35.53 | 38.58 | 38.62 |
| 117 | 37.78 | 3782 | 37.87 | 37.91 | 37.96 | 38.00 | 38.01 | 38.09 | 38.13 | 35.18 |
| 116 | 37.3; | 37.35 | 37.42 | 37.47 | 37.51 | 3756 | 37.60 | 37.64 | 37.69 | 37.73 |
| 11.5 | 36.89 | 36.93 | 36.95 | 37.02 | 37.07 | 37.11 | 37.16 | 37.20 | 37.24 | 37.29 |
| 114 | 36.41 | 36.49 | 36.53 | 36.55 | 36.62 | 36.67 | 36.71 | 36.76 | 36.80 | 36.54 |
| 113 | 36.00 | 36.01 | 36.09 | 36.13 | 36.18 | 36.22 | 36.27 | 36.31 | 36.36 | 36.40 |
| 112 | 3.5.56 | 95.60 | 35.64 | 3569 | 35.73 | 3.5 .78 | 3.5.82 | 3.5 .87 | 35.91 | 35.96 |
| 111 | 3.5.11 | 35.16 | 3.5 .20 | 35.24 | 35.29 | 3.5 .33 | 3.5.35 | 3.5 .42 | 35.47 | 35.51 |
| 110 | 31.67 | 34.71 | 31.76 | 34.80 | 34.84 | 34.59 | 31.93 | 31.98 | 35.02 | 3.5 .07 |
| 109 | 34.22 | 34.27 | 31.31 | 34.36 | 34.40 | 34.44 | 34.49 | 34.53 | 34.58 | 34.62 |
| 108 | 33.78 | 33.82 | 33.87 | 33.91 | 33.96 | 34.00 | 34.01 | 31.09 | 34.13 | 34.18 |
| 107 | 33.33 | 33.38 | 33.42 | 33.47 | 33.51 | 33.56 | 33.60 | 33.64 | 33.69 | 33.73 |
| 106 | 32.59 | 32.93 | 32.95 | 33.02 | 33.07 | 33.11 | 33.16 | 33.20 | 33.24 | 33.29 |
| 10.5 | 32.44 | 32.49 | 32.53 | 32.58 | 32.62 | 32.67 | 32.71 | 32.76 | 32.50 | 32.84 |
| 104 | 32.00 | 32.04 | 32.09 | 32.13 | 3215 | 32.22 | 32.27 | 32.31 | 32.36 | 32.40 |
| 103 | 31.56 | 31.60 | 31.64 | 31.69 | 31.73 | 31.75 | 31.82 | 31.57 | 31.91 | 31.96 |
| 102 | 31.11 | 31.16 | 31.20 | 31.24 | 31.29 | 31.33 | 31.38 | 31.42 | 31.47 | 31.51 |
| 101 | 30.67 | 30.71 | 30.76 | 30.50 | 30.84 | 30.59 | 30.93 | 30.98 | 31.02 | 31.07 |
| 100 | 30.22 | 30.27 | 30.31 | 30.36 | 30.40 | 30.44 | 30.49 | 30.53 | 30.58 | 30.62 |
| 99 | 29.78 | 29.82 | 29.87 | 29.91 | 29.96 | 30.00 | 30.04 | 30.09 | 30.13 | 30.18 |
| 98 | 29.33 | 29.38 | 29.42 | 29.47 | 29.51 | 29.56 | 29.60 | 29.64 | 29.69 | 29.73 |
| 97 | 28.89 | 29.93 | 28.98 | 29.02 | 29.07 | 29.11 | 29.16 | 29.20 | 29.24 | 29.29 |
| 96 | 28.44 | 25.49 | 28.53 | 28.58 | 28.62 | 25.67 | 28.71 | 23.76 | 28.50 | 28.84 |
| 95 | 28.00 | 28.01 | 28.09 | 28.13 | 28.18 | 28.22 | 28.27 | 28.31 | 28.36 | 28.40 |
| 94 | 27.56 | 27.60 | 27.64 | 27.69 | 27.73 | 27.75 | 27.82 | 27.87 | 27.91 | 27.96 |
| 93 | 27.11 | 27.16 | 27.20 | 27.24 | 27.29 | 27.33 | 27.38 | 27.12 | 27.47 | 27.51 |
| 92 | 26.67 | 26.71 | 26.76 | 26.80 | 26.54 | 26.59 | 26.93 | 26.98 | 27.02 | 27.07 |
| 91 | 26.22 | 26.27 | 26.31 | 26.36 | 26.40 | 26.41 | 26.49 | 26.53 | 26.58 | 26.62 |
| 90 | 2.5.75 | 2.5. 8. | 25.57 | 2.5.91 | 2.5 .96 | 26.00 | 26.01 | 26.09 | 26.13 | 26.18 |
| S9 | 2.5.33 | 2.5 .39 | 25.42 | 25.47 | 25.51 | 2.5.56 | 25.60 | 25.61 | 25.69 | 25.73 |
| 88 | 24.59 | 24.93 | 21.98 | 25.02 | 25.07 | 25.11 | 25.16 | 25.20 | 25.24 | 2.5 .29 |
| 87 | 24.44 | 24.49 | 2453 | 21.58 | 24.62 | 24.67 | 24.71 | 24.76 | 24.80 | 24.84 |
| 86 | 24.00 | 24.04 | 24.09 | 24.1:3 | 2418 | 24.22 | 21.27 | 24.31 | 24.36 | 24.40 |
| 8.5 | 23.56 | 23.60 | 23.64 | 2369 | 23.73 | 23.75 | 23.82 | 23.87 | 2391 | 23.96 |
| 84 | 23.11 | 23.16 | 23.20 | 23.24 | 23.29 | 2333 | 23.38 | 23.42 | 23.47 | 23.51 |
| 83 | 22.67 | 22.71 | 22.76 | 22.80 | 22.54 | 22.59 | 22.93 | 22.95 | 23.02 | 23.07 |
| 82 | 22.22 | 22.27 | 22.34 | 22.36 | 22.40 | 22.44 | 22.49 | 22.53 | 22.58 | 22.62 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | O. |


| Derrees of Fahreuheit. | Tentis of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | む. | 6. | 8. | 8. | 9. |
|  | Reaumur P | Reaumur | Reanmur | Reaumur. | Reaumur. | Reaumur. | Reaumur | Reanmur. | Reaumui. B | Reatumur. |
| +81 | +21.75 | $+21.82$ | +21.57 | +21.91 | $+21.96$ | $+22.00$ | $+2.24$ | $+2 \cdot .09$ | 3 | +22.15 |
| 80 | 21.33 | 21.35 | 21.42 | 21.47 | 21.51 | 21.56 | 21.60 | 21.64 | 21.69 | 21.73 |
| 79 | 20.59 | 20.93 | 20.98 | 21.02 | 21.07 | 21.11 | 21.16 | 21.20 | 21.24 | 21.29 |
| 78 | 20.44 | 20.49 | 20.53 | 20.55 | 20.62 | 20.67 | 20.71 | 20.76 | 20.80 | 20.84 |
| 77 | 20.00 | 20.04 | 20.09 | 20.13 | 20.18 | 20.23 | 20.27 | 20.31 | 20.36 | 20.40 |
| 76 | 19.66 | 19.60 | 19.64 | 19.69 | 19.73 | 19.78 | 19.82 | 19.57 | 19.91 | 19.96 |
| 75 | 19.11 | 19.16 | 19.20 | 19.24 | 19.29 | 19.33 | 19.38 | 19.42 | 19.47 | 19.51 |
| 74 | 18.67 | 18.71 | 18.76 | 18.50 | 1584 | 18.89 | 18.93 | 13.98 | 19.02 | 19.07 |
| 73 | 18.22 | 15.27 | 18.31 | 18.36 | 18.40 | 18.44 | 18.49 | 18.53 | 18.58 | 18.62 |
| 72 | 17.78 | 17.52 | 17.87 | 17.91 | 17.96 | 18.00 | 18.04 | 18.09 | 15.13 | 18.18 |
| 71 | 17.33 | 17.38 | 17.42 | 17.47 | 17.51 | 17.56 | 17.60 | 17.64 | 17.69 | 17.73 |
| 70 | 16.89 | 16.93 | 16.98 | 17.02 | 17.07 | 17.11 | 17.16 | 17.20 | 17.24 | 17.29 |
| 69 | 16.44 | 16.49 | 16.53 | 16.55 | 16.62 | 16.67 | 16.71 | 16.76 | 16.50 | 16.54 |
| 68 | 16.00 | 16.04 | 16.09 | 16.13 | 16.18 | 16.22 | 16.27 | 16.31 | 16.36 | 16.40 |
| 67 | 15.56 | 15.60 | 15.64 | 15.69 | 15.73 | 15.78 | 15.82 | 15.87 | 15.91 | 15.96 |
| 66 | 15.11 | 15.16 | 15.20 | 15.24 | 15.29 | 15.33 | 15.38 | 15.42 | 15.47 | 15.51 |
| 65 | 11.67 | 14.71 | 14.76 | 14.80 | 14.84 | 14.89 | 14.98 | 14.98 | 15.02 | 15.07 |
| 64 | 14.22 | 14.27 | 14.31 | 14.36 | 14.40 | 14.44 | 14.49 | 14.53 | 14.55 | 14.62 |
| 63 | 13.78 | 13.82 | 13.87 | 13.91 | 1396 | 14.00 | 14.04 | 14.09 | 14.13 | 14.18 |
| 63 | 13.33 | 13.35 | 13.42 | 13.47 | 13.51 | 13.56 | 13.60 | 13.64 | 13.69 | 13.73 |
| 61 | 12.89 | 12.93 | 12.98 | 13.02 | 13.07 | 13.11 | 13.16 | 13.20 | 13.24 | 13.29 |
| 60 | 12.44 | 12.49 | 12.53 | 12.58 | 12.62 | 12.67 | 12.71 | 12.76 | 12.80 | 12.84 |
|  | 12.00 | 12.04 | 12.09 | 12.13 | 12.18 | 12.22 | 12.27 | 12.31 | 12.36 | 12.40 |
| 59 | 12.00 |  |  |  | 11.73 | 11.78 | 11.82 | 11.87 | 11.91 | 11.96 |
| 58 | 11.56 | 11.60 | 11.64 11.20 | 11.69 11.24 | 11.73 11.29 | 11.73 11.33 | 11.38 | 11.42 | 11.47 | 11.51 |
| 57 | 11.11 | 11.16 | 11.20 | 11.24 | 11.29 | 11.33 | 11.05 | 11.42 |  |  |
| 56 | 10.67 | 10.71 | 10.76 | 10.80 | 10.84 | 10.89 | 10.93 | 10.98 | 11.02 | 11.07 |
| 55 | 10.22 | 10.27 | 10.31 | 10.36 | 10.40 | 10.44 | 10.49 | 10.53 | 10.58 | 10.62 |
| 5. | 9.78 | 9.82 | 9.87 | 9.91 | 9.96 | 10.00 | 10.04 | 10.09 | 10.13 | 10.18 |
| 54 | 9.78 9.3 .3 | 9.82 9.38 | 9.42 | 9.47 | 9.51 | 9.56 | 9.60 | 9.64 | 9.69 | 9.73 |
| 53 | 9.33 8.59 | 9.35 8.93 | 9.42 8.93 | 9.47 9.02 | 9.51 9.07 | 9.11 | 9.16 | 9.20 | 9.24 | 9.29 |
| 52 | S. 89 | 8.93 | 8.95 | 9.02 | 9.07 | 9.11 | 9.16 |  |  |  |
| 51 | 8.14 | 8.49 | 8.53 | 8.58 | 8.62 | 8.67 | 8.71 | 8.76 | 8.80 | 8.84 |
| 50 | 8.00 | S.04 | 8.09 | 8.13 | 8.18 | 8.22 | 8.27 | 8.31 | 8.36 | 8.40 |
|  | 7. | 7.60 | 7.64 | 7.69 | 7.73 | 7.78 | 7.82 | 7.87 | 7.91 | 7.96 |
| 15 | 7. | 7.16 | 7.20 | 7.24 | 7.29 | 7.33 | 7.38 | 7.42 | 7.47 | 7.51 |
| 47 | 6.67 | 6.71 | 6.76 | 6.80 | 6.84 | 6.89 | 6.93 | 6.98 | 7.02 | 7.07 |
| 46 | 6.22 | 6.27 | 6.31 | 6.36 | 6.40 | 6.44 | 6.49 | 6.53 | 3.58 | - 6.62 |
| 45 | 5.78 | 5.82 | 5.87 | 75.91 | 5.96 | 6.00 | 6.04 | 6.09 | - 6.13 | 6.15 |
| 45 |  |  |  |  | 5.51 | 5.56 | 5.60 | 5.64 | 45.69 | 5.73 |
| 44 | 533 | 5.35 | 5.42 | - 5.47 | 5.51 | 5.56 | 5.60 5.16 | 5.20 | 0 5.24 | 45.29 |
| 43 | 4.89 | - 4.93 | 4.98 | 3.02 | 5.07 | 5.11 | 5.16 | 5.20 | - 3.24 | - 5.29 |
| 42 | 4.44 | 4.49 | 4.53 | 4.58 | 4.62 | 4.67 | 4.71 | 4.76 | $3 \quad 4.80$ | ) 4.54 |
| $4:$ | 4.00 | - 4.04 | 4.4 .09 | 9 4.13 | 4.18 | 4.22 | 4.27 | 4.31 | 14.36 | $6 \quad .1 .40$ |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 78 | 8. | 9. |

A

| Degrees of Fahrelheit. | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Reaumur | Re:mume | Reammur. | Reammur. | Reaumur | Reaumur. | Reaumur. | Reaumur | Reaumur | Reaumur. |
| +40 | + 3.56 | + 3.60 | + 3.64 | + 3.69 | + 3.73 | 3.78 | + 3.82 | $+3.57$ | +3.91 | $+3.96$ |
| 39 | 3.11 | 3.16 | 3.20 | 3.24 | 3.29 | 3.33 | 3.38 | 3.12 | 3.47 | 3.51 |
| 38 | 2.67 | 2.71 | 2.76 | 2.80 | 2.84 | 2.89 | 2.93 | 2.95 | 3.02 | 3.07 |
| 37 | 2.22 | 2.27 | 2.31 | 2.36 | 2.40 | 2.44 | 2.49 | 2.53 | 2.58 | 2.62 |
| 36 | 1.78 | 1.82 | 1.87 | 1.91 | 1.96 | 2.00 | 2.04 | 2.09 | 2.13 | 2.18 |
| 35 | 1.83 | 1.38 | 1.42 | 1.17 | 1.51 | 1.56 | 1.60 | 1.64 | 1.69 | 1.73 |
| 34 | 0.89 | 0.93 | 0.98 | 1.02 | 1.07 | 1.11 | 1.16 | 1.20 | 1.24 | 1.29 |
| 83 | 0.14 | 0.19 | 0.53 | 0.58 | 0.62 | 0.67 | 0.71 | 0.76 | 0.80 | 0.84 |
| 32 | 0.00 | 0.04 | 0.09 | 0.13 | 0.18 | 0.22 | 0.27 | 0.31 | 0.36 | 0.40 |
| 81 | - 0.44 | $-0.10$ | $-0.36$ | $-0.31$ | - 0.27 | -0.22 | $-0.15$ | $-0.13$ | $-0.09$ | - 0.04 |
| 30 | - 0.89 | -0.54 | - 0.80 | - 0.76 | - 0.71 | - 0.67 | -0.62 | - 0.58 | - 0.53 | - 0.49 |
| 29 | - 1.33) | - 1.29 | - 1.24 | - 1.20 | - 1.16 | $-1.11$ | - 1.07 | $-1.02$ | - 0.98 | -0.93 |
| 28 | - 1.78 | - 1.73 | - 1.69 | - 1.61 | $-1.60$ | $-1.56$ | - 1.51 | - 1.17 | - 1.12 | - 1.38 |
| 27 | - 2.22 | - 2.15 | $-2.13$ | - 2.09 | - 2.04 | - 2.00 | - 1.96 | - 1.91 | - 1.87 | - 1.82 |
| 26 | - 2.67 | - 2.62 | - 2.58 | - 2.53 | - 2.49 | - 2.44 | - 2.40 | $-2.36$ | - 2.31 | - 2.27 |
| 2.5 | - 3.11 | - 3.07 | - 3.02 | - 2.98 | - 2.93 | -2.89 | - 2.84 | - 2.80 | - 2.76 | - 2.71 |
| 24 | - 3.56 | - 3.51 | $-3.47$ | - 3.42 | - 3.35 | - 3.33 | - 3.29 | -3.24 | - 3.20 | $-3.16$ |
| 23 | - 4.00 | - 3.96 | - 3.91 | $-3.87$ | - 3.82 | $-3.78$ | - 3.73 | -3.69 | -3.64 | - 3.60 |
| 22 | - 4.44 | $-4.10$ | - 4.36 | $-4.31$ | - 4.27 | - 4.22 | - 4.18 | - 4.13 | - 4.09 | - 4.04 |
| 21 | - 4.39 | $-4.54$ | - 4.80 | $-4.76$ | - 4.71 | $-4.67$ | $-4.62$ | - 4.58 | $-4.53$ | $-4.49$ |
| 20 | - 5.33 | - 5.29 | - 5.24 | - 5.20 | - 5.16 | - 5.11 | $-5.07$ | - 5.02 | - 4.98 | - 4.93 |
| 19 | - 5.78 | $-5.73$ | - 5.69 | - 5.64 | - 5.60 | $-5.56$ | - 5.51 | - 5.47 | - 5.42 | - 5.38 |
| 18 | - 6.22 | - 6.18 | - 6.13 | - 6.09 | - 6.04 | - 6.00 | - 5.96 | - 5.91 | - 5.87 | - 5.82 |
| 17 | - 6.68 | - 6.62 | - 6.58 | - 6.53 | - 6.49 | - 6.14 | - 6.10 | - 6.36 | - 6.3 .31 | - 6.27 |
| 16 | - 7.11 | - 7.07 | - 7.02 | - 6.98 | - 6.93 | -6.89 | -6.54 | - 6.80 | -6.76 | -6.71 |
| 15 | - 7.56 | - 7.51 | - 7.17 | $-7.42$ | - 7.38 | $-7.33$ | - 7.29 | - 7.24 | - 7.20 | -7.16 |
| 14 | $1-8.00$ | - 7.96 | - 7.91 | - 7.57 | - 7.82 | - 7.78 | - 7.73 | - 7.69 | - 7.64 | - 7.60 |
| 13 | -8.11 | - 5.40 | - 8.36 | - 8.31 | - 8.27 | - 8.22 | - 8.18 | - 8.13 | - 8.09 | -8.04 |
| 12 | - 8.59 | -8.81 | $-5.80$ | - 8.76 | $-8.71$ | - 8.67 | - 8.62 | -8.58 | - 8.53 | - 8.49 |
| 11 | - 9.33 | - 9.29 | - 9.24 | - 9.20 | - 9.16 | - 9.11 | - 9.07 | - 9.02 | - 8.98 | - 8.93 |
| 10 | - 9.73 | - 9.73 | - 9.69 | - 9.64 | - 9.60 | - 9.56 | - 9.51 | - 9.47 | - 9.42 | - 9.38 |
| 9 | -10 22 | -10.18 | -10.13 | -10.09 | -10.04 | -10.00 | - 9.96 | - 9.91 | - 9.87 | -9.82 |
| 8 | -10.67 | -10.62 | -10.58 | -10.53 | -10.49 | -10.44 | $-10.10$ | $-10.36$ | -10.31 | -10.27 |
| 7 | -11.11 | -11.07 | -11.02 | -10.93 | -10.93 | -10.89 | -10.5.1 | -10.80 | $-10.76$ | -10.71 |
| 6 | -11.56 | -11.51 | -11.47 | -11.42 | -11.33 | -11.33 | -11.29 | -11.24 | $-11.20$ | -11.16 |
| 5 | -12.00 | -11.96 | -11.91 | -11.87 | -11.82 | -11.78 | -11.73 | -11.69 | -11.64 | -11.60 |
| 4 | -12.44 | -12.4t, | $-12.36$ | -12.31 | -12.27 | -12.22. | $-12.18$ | $-12.13$ | --12.09 | -12.04 |
| 3 | -12.89 | -12.84 | -12.80 | -12.76 | -12.71 | -12.67 | -12.62 | -12.58 | -12.53 | -12.19 |
| 2 | -13.33 | -13.29 | -13.21 | -13.20 | $-13.16$ | -13.11 | -13.07 | $-12.02$ | -12.98 | $-12.93$ |
| 1 | -13.78 | -13.73 | -13.69 | -13.64 | -13.60 | -13.56 | -13.51 | -13.47 | -13.42 | -13.35 |
| $+0$ | -14.22 | -14.18 | -14.13 | -11.09 | -14.04 | -14.00 | $-13.96$ | -13.91 | -13.87 | -13.52 |
|  | (1. | 1. | 2. | 3. | 4. |  | 6. | 7. | 8. | 9. |
| A |  |  |  |  | 20 |  |  |  |  |  |


| Degrees of Fahrenheit. | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Reaumur. | Reaumur. | Reaumur. | Reaumur. | Reaumur | Reaumur. | Reaunur | Reaumur. | Reaumur. |  |
| - 0 | -14.22 | -14.27 | -14.31 | -14.36 | -14.40 | -14.44 | -14.49 | -14.53 | -14.58 | -14.62 |
| - | -14.67 | -14.71 | -14.76 | -14.80 | -14.84 | -14.89 | -14.93 | -14.98 | -15.02 | -15.07 |
| 2 | -15.11 | -15.16 | -15.20 | -15.24 | -15.29 | -15 33 | -15.38 | -15.42 | -15.47 | -15.51 |
| - 3 | -15.56 | -15.60 | -15.64 | -15.69 | -15.73 | -15.78 | -15.82 | -15.87 | -15.91 | -15.96 |
| -4 | -16.00 | -16.04 | -16.09 | -16.13 | -16.18 | -16.22 | -16.27 | -16.31 | -16.36 | -16.40 |
| - 5 | -16.44 | -16.49 | -16.53 | -16.58 | -16.62 | -16.67 | -16.71 | -16.76 | -16.80 | -16.84 |
| 6 | -16.59 | -17.93 | -16.98 | $-17.02$ | -17.07 | -17.11 | -17.16 | -17.20 | -17.24 | $-17.29$ |
| - 7 | -17.33 | -17.38 | -17.42 | -17.47 | -17.51 | -17.56 | $-17.60$ | -17.64 | -17.69 | $-17.73$ |
| - 8 | -17.78 | -18.52 | $-17.57$ | $-17.91$ | -17.96 | -18.00 | -18.04 | -18.09 | -18.13 | -18.13 |
| -9 | -18.22 | $-18.27$ | -18.31 | -18.36 | $-18.40$ | -18.44 | -18.19 | -18.53 | $-18.58$ | -18.62 |
| -10 | -18.67 | -18.71 | -18.76 | -18.80 | -18.84 | -18.59 | -18.93 | -18.98 | -19.02 | -19.07 |
| -11 | -19.11 | -19.16 | -19.20 | -19.24 | -19.29 | -19.33 | -19.38 | -19.42 | -19.47 | -19.51 |
| -12 | -1956 | -19.60 | -19.64 | -19.69 | -19.73 | -19.78 | -19.52 | -19.87 | -19.91 | -19.96 |
| -13 | -20.00 | -20.04 | -20.09 | -20.13 | -20.18 | -20.22 | -20.27 | -20.31 | -20.36 | -20.40 |
| -14 | -20.44 | -20.49 | -20.53 | $-20.58$ | $-20.62$ | -20.67 | -20.71 | -20.76 | -20.80 | $-20.84$ |
| -15 | -20.59 | -20.93 | -20.98 | -21.02 | $-21.07$ | -21.11 | $-21.16$ | $-21.20$ | -21.24 | -21.29 |
| -16 | $-21.33$ | -21.38 | -21.42 | $-21.47$ | -21.51 | -21.56 | -21.60 | -21.64 | -21.69 | -21.73 |
| -17 | -21.78 | -21.82 | -21.57 | -21.91 | -21.96 | -22.00 | -22.04 | -22.09 | $-2.213$ | -22.18 |
| -18 | -22.22 | -2.2.27 | -22.31 | -22.36 | -22.40 | $-2.44$ | -23.49 | $-22.53$ | -2.2.58 | -22.62 |
| -19 | $-2.67$ | $-22.71$ | -22.76 | $-22.80$ | -22.84 | -22.89 | $-22.93$ | -22.98 | -23.02 | -23.07 |
| -20 | -23.11 | -23.16 | -23.20 | -23.24 | -23.29 | -23.33 | -23.38 | -23.42 | -23.47 | -23 51 |
| -21 | -23.56 | -23.60 | -23.64 | -23.69 | -23.73 | -23.78 | -23.82 | -23.87 | -23.91 | -23.96 |
| -22 | -24.00 | -24.04 | -24.09 | -24.13 | -2.1.18 | -2 4.22 | -24.27 | $-24.31$ | -24.36 | -24.40 |
| -23 | -24.44 | -24.49 | -24.53 | -24.58 | -24.62 | -24.67 | -24.71 | -24.76 | $-24.50$ | -24.84 |
| -24 | -24.59 | -24.93 | -24.98 | $-2.5 .02$ | -25.07 | -25.11 | -25.16 | -25.20 | -25.24 | -25.29 |
| -2: | -25.33 | -25.35 | -25.42 | -2.5.47 | -25.51 | -25.56 | -25.60 | -2.5.64 | -25.69 | -25 73 |
| -26 | -25.78 | -2.5.82 | -25.87 | -25.91 | -25.96 | -26.00 | -26.04 | -26.09 | -26.13 | -26.18 |
| -27 | -26.22 | -26.27 | -26.31 | -26.36 | -26.40 | -26.44 | -26.49 | -26.53 | -26.58 | -26.62 |
| -23 | -26.67 | -26.71 | $-26.76$ | -26.80 | -26.84 | -26.69 | -26.93 | $-26.98$ | -27.02 | -27.07 |
| -29 | -27.11 | -27.16 | $-27.20$ | $-27.24$ | $-27.29$ | $-27.33$ | $-27.38$ | $-27.42$ | $-27.47$ | $-27.51$ |
| -30 | -27.56 | -27.60 | -27.64 | -27.69 | -27.73 | -27.78 | -27.82 | -27.87 | -27.91 | -27.96 |
| -31 | -28.00 | $-28.04$ | -28.09 | -28.13 | -25.18 | -28.22 | -28.27 | -28.31 | -28.36 | -28.40 |
| -32 | -23 44 | -28.49 | $-28.53$ | -28.55 | -28.62 | $-28.67$ | -28.71 | -28.76 | -28.50 | -28.84 |
| -33 | -28.89 | -28.93 | -23.98 | -29.02 | -29.07 | -29.11 | -29.16 | -29 20 | -29.24 | -29.29 |
| -34 | -29.33 | -29.33 | -29.42 | -29.47 | $-29.51$ | -29.56 | -29.60 | -29.64 | -29.69 | $-29.73$ |
| -35 | -29.78 | -29.82 | -29.87 | -29.91 | -29.96 | $-30.00$ | -30.04 | -30.09 | -30.13 | $-30 \cdot 18$ |
| -36 | -30.22 | -30.27 | -30.31 | -30.36 | -30.40 | -30.44 | -30.49 | -30.53 | $-30.58$ | -30.62 |
| -37 | -30.67 | -30.71 | -30.76 | -30.50 | -30.84 | -30.89 | -30.93 | -30.98 | -31.02 | -31.07 |
| -35 | -31.11 | --31.16 | -31.20 | -31.24 | $-31.29$ | $-31.33$ | -31.38 | -31.42 | $-31.47$ | -31.51 |
| -39 | -31.56 | -31.60 | $-31.64$ | -31.69 | -31.73 | -31.78 | -31.82 | -31.57 | $-31.91$ | -31.96 |
| -40 | -32.00 | $-30.04$ | -30.09 | -30.13 | -30.18 | -30.22 | -30.27 | -30.31 | -30.36 | $-30.40$ |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

A

## VI.-VII.

## C0MPARIS0N

of

# THE CENTIGRADE THERMOMETER 

WITH

TIIE THERMOMETERS OF FAHRENIIEIT AND OF REAUMUR, or

TABLES

FOR CONVERTING CENTIGRADE DEGREES INTO DEGREES OF FAHRENHEIT AND OF REAUMUR;
giving the corresponding values for eacif tenth of a degree, FROM + $50^{\circ}$ TO - $54^{\circ}$ CENTIGRADE.
A

| Centigrade Derrees. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | $\%$ \% | 8. | 9. |
| $+50$ | $\begin{gathered} \text { Fahren. } \\ +122.00 \end{gathered}$ | Fahren. $+122.18$ | $\begin{aligned} & \text { Fahren. } \\ & +122.36 \end{aligned}$ | $\begin{array}{\|} \text { Fahren. } \\ +122.54 \end{array}$ | $\begin{array}{\|c\|} \text { Fahren. } \\ +122.72 \end{array}$ | $\left\|\begin{array}{c} \text { Fahren. } \\ +122.90 \end{array}\right\|$ | $\begin{array}{r} \text { Fahren. } \\ +123.08 \end{array}$ | $\begin{aligned} & \text { Fahren. } \\ & +123.26 \end{aligned}$ | $\begin{gathered} \text { Fahren. } \\ +123.44 \end{gathered}$ | Fahren. $+123.62$ |
| 49 | 120.20 | 120.38 | 120.56 | 120.74 | 120.92 | 121.10 | 121.28 | 121.46 | 121.64 | 121.82 |
| 48 | 118.40 | 118.58 | 118.76 | 118.9 .11 | 119.12 | 119.30 | 119.48 | 119.66 | 119.84 | 120.02 |
| 47 | 116.60 | 116.75 | 116.96 | 117.14 | 117.32 | 117.50 | 117.68 | 117.86 | 118.04 | 118.22 |
| 46 | 114.50 | 114.98 | 115.16 | 115.34 | 115.52 | 115.70 | 115.88 | 116.06 | 116.24 | 116.42 |
| 45 | 113.00 | 113.18 | 113.36 | 113.54 | 113.72 | 113.90 | 114.08 | 114.26 | 114.44 | 114.62 |
| 44 | 111.20 | 111.38 | 111.56 | 111.74 | 111.92 | 112.10 | 112.28 | 112.46 | 112.64 | 112.82 |
| 43 | 109.40 | 109.58 | 109.76 | 109.94 | 110.12 | 110.30 | 110.48 | 110.66 | 110.8.t | 111.02 |
| 42 | 107.60 | 107.75 | 107.96 | 105.14 | 108.52 | 105.50 | 105.68 | 108.86 | 109.04 | 109.22 |
| 41 | 105.80 | 105.98 | 106.16 | 106.34 | 106.52 | 106.70 | 106.58 | 107.06 | 107.24 | 107.42 |
| 40 | 104.00 | 104.18 | 104.36 | 104.5t | 104.72 | 104.90 | 10.5 .08 | 105.26 | 105.44 | 105.62 |
| 39 | 102.20 | 102.38 | 102.56 | 102.74 | 102.92 | 103.10 | 103.28 | 103.46 | 103.64 | 103.52 |
| 38 | 100.40 | 100.58 | 100.76 | 100.94 | 101.12 | 101.30 | 101.48 | 101.66 | 101.84 | 102.02 |
| 37 | 98.60 | 98.78 | 98.96 | 99.14 | 99.32 | 99.50 | 99.68 | 99.86 | 100.04 | 100.22 |
| 36 | 96.50 | 96.95 | 97.16 | 97.34 | 97.52 | 97.70 | 97.88 | 98.06 | 98.24 | 98.42 |
| 35 | 95.00 | 95.18 | 95.36 | 95.54 | 95.72 | 95.90 | 96.08 | 96.26 | 96.44 | 96.62 |
| 34 | 93.20 | 93.38 | 93.56 | 93.74 | 93.92 | 94.10 | 94.28 | 94.46 | 94.64 | 94.82 |
| 33 | 91.40 | 91.58 | 91.76 | 91.94 | 92.12 | 92.30 | 92.48 | 92.66 | 92.84 | 93.02 |
| 32 | 89.60 | 89.78 | 89.96 | 90.14 | 90.32 | 90.50 | 90.68 | 90.86 | 91.04 | 91.22 |
| 31 | 87.50 | 87.98 | 88.16 | 88.34 | 88.52 | 88.70 | 85.38 | 89.06 | 89.24 | 89.42 |
|  |  |  |  |  |  |  |  |  |  | - |
| 30 | 86.00 | 86.18 | 86.36 | 86.54 | 86.72 | 86.90 | 87.08 | 87.26 | 87.44 | 87.62 |
| 29 | 84.20 | 84.38 | 84.56 | 84.74 | S4.92 | 55.10 | 85.28 | 85.46 | 85.64 | 85.82 |
| 28 | 82.40 | 82.58 | 82.76 | 82.94 | 83.12 | 83.30 | 83.48 | 83.66 | 83.84 | 84.02 |
| 27 | 80.60 | 80.78 | 80.96 | 81.14 | 81.32 | 81.50 | 81.68 | 81.86 | 82.04 | 82.22 |
| 26 | 78.80 | 78.98 | 79.16 | 79.34 | 79.52 | 79.70 | 79.58 | 80.06 | 80.24 | 80.42 |
| 25 | 77.00 | 77.18 | 77.36 | 77.54 | 77.72 | 77.90 | 78.08 | 78.26 | 78.44 | $78.62{ }^{\text {² }}$ |
| 24 | 75.20 | 75.83 | 75.56 | 75.74 | 75.92 | 76.10 | 76.28 | 76.46 | 76.64 | 76.82 |
| 23 | 73.40 | 73.58 | 73.76 | 73.94 | 74.12 | 74.30 | 74.48 | 74.66 | 74.84 | 75.02 |
| 22 | 71.60 | 71.78 | 71.96 | 72.14 | 72.32 | 72.50 | 72.65 | 72.86 | 73.04 | 73.22 |
| 21 | 69.50 | 69.98 | 70.16 | 70.34 | 70.52 | 70.70 | 70.58 | 71.06 | 71.24 | 71.42 |
| 20 | 68.00 | 68.15 | 68.36 | 65.54 | 68.72 | 68.90 | 69.08 | 69.26 | 69.44 | 69.62 |
| 19 | 66.20 | 66.35 | 66.56 | 66.74 | 66.92 | 67.10 | 67.28 | 67.16 | 67.64 | 67.82 |
| 18 | 64.40 | 64.58 | 64.76 | 64.94 | 65.12 | 65.30 | 65.48 | 65.66 | 65.84 | 66.02 |
| 17 | 62.60 | 62.75 | 62.96 | 63.14 | 63.32 | 63.50 | 63.68 | 63.56 | 64.04 | 64.22 |
| 16 | 60.50 | 60.98 | 61.16 | 61.34 | 61.52 | 61.70 | 61.58 | 62.06 | 62.24 | 62.42 |
| 15 | 59.00 | 59.18 | 59.36 | 59.54 | 59.72 | 59.90 | 60.08 | 60.26 | 60.44 | 60.62 |
| 14 | 57.20 | 57.38 | 57.56 | 57.74 | 57.92 | 58.10 | 55.28 | 55.46 | 58.64 | 58.82 |
| 13 | 55.40 | 55.58 | 5.5 .76 | 55.94 | 56.12 | 56.30 | 56.48 | 56.66 | 56.8 .1 | 57.02 |
| 12 | 53.60 | 53.78 | 53.96 | 54.14 | 54.32 | 54.50 | 54.68 | 54.86 | 55.04 | 55.22 |
| 11 | 51.80 | 51.98 | 52.16 | 52.34 | 52.52 | 52.70 | 52.88 | 53.06 | 53.24 | 53.42 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| CentigradeDegrees. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | ¢. | 6. | $\%$ \% | 8. | 9. |
| +10 | 0.00 | Falren. | $\begin{aligned} & \text { Fahren. } \\ & \text { +50.30 } \end{aligned}$ | Fahren. | Fahren. | Fahren. $+50.90$ | Fahren $+51.08$ | $\begin{aligned} & \text { Fahren. } \\ & \text { +5l. } \end{aligned}$ | $\begin{aligned} & \text { Fahren. } \\ & +51.44 \end{aligned}$ | Fahren. |
| 9 | 48.20 | 48.38 | 48.56 | 48.74 | 48.92 | 49.10 | 49.25 | 49.46 | 49.64 | 49.82 |
| S | 46.40 | 46.58 | 46.76 | 46.94 | 17.12 | 47.30 | 47.48 | 47.66 | 47.84 | 45.02 |
| 7 | 44.60 | 44.78 | 44.96 | 45.14 | 43.32 | 45.50 | 45.68 | 45.86 | 46.04 | 46.22 |
| 6 | 42.50 | 42.98 | 43.16 | 43.34 | 43.52 | 43.70 | 43.58 | 44.06 | 44.24 | 44.42 |
| 5 | 41.00 | 41.18 | 41.36 | 41.54 | 41.72 | 41.90 | 42.08 | 42.26 | 42.44 | 42.62 |
| 4 | 39.20 | 39.38 | 39.56 | 39.74 | 39.92 | 40.10 | 40.28 | 40.46 | 40.64 | 40.82 |
| 3 | 37.40 | 37.58 | 37.76 | 37.94 | 38.12 | 38.30 | 38.48 | 38.66 | 38.84 | 39.02 |
| 2 | 35.60 | 33.78 | 35.96 | 36.14 | 36.32 | 36.50 | 36.68 | 36.86 | 37.04 | 37.22 |
| 1 | 33.50 | 33.98 | 34,16 | 34.34 | 34.52 | 34.70 | 34.58 | 35.06 | 35.24 | 35.42 |
| 0 | 32.00 | 32.18 | 32.36 | 32.54 | 32.72 | 32.90 | 33.08 | 33.26 | 33.44 | 33.62 |
| - 0 | 32.00 | 31.82 | 31.64 | 31.46 | 31.25 | 31.10 | 30.92 | 30.71 | 30.56 | 30.38 |
| -1 | 30.20 | 0.02 | 29.84 | 29.66 | 29.48 | 29.30 | 29.12 | 25.91 | 25.76 | 28.58 |
| 2 | 28.40 | 23.22 | 28.04 | 27.56 | 27.68 | 27.50 | 27.32 | 27.14 | 26.96 | 26.78 |
| - 3 | 26.60 | 26.42 | 26.24 | 26.06 | 25.88 | 25.70 | 2.5 .52 | 2.5 .34 | 25.16 | 24.98 |
| - | 24.50 | 24.62 | 24.44 | 24.26 | 24.08 | 23.90 | 23.72 | 23.54 | 23.36 | 23.18 |
| - 5 | 23.00 | 22.82 | 22.64 | 22.46 | 22.28 | 22.10 | 21.92 | 21.74 | 21.56 | 21.38 |
| - 6 | 21.20 | . 02 | 20.84 | 20.66 | 20.48 | 20.30 | 20.12 | 19.94 | 19.76 | 19.58 |
| - 7 | 19.40 | 19.22 | 19.04 | 18.86 | 18.65 | 18.50 | 18.32 | 18.14 | 17.96 | 17.78 |
| 8 | 17.60 | 17.42 | 17.24 | 17.06 | 16.58 | 16.70 | 16.52 | 16.34 | 16.16 | 15.98 |
| - 9 | 15.80 | 15.62 | 15.44 | 15.26 | 15.08 | 14.90 | 14.72 | 14.54 | 14.36 | 14.18 |
| -10 | 14.00 | 13.82 | 13.64 | 13.46 | 13.28 | 13.10 | 12.92 | 12.74 | 12.56 | 12.38 |
| $-11$ | 12.20 | 12.02 | 11.84 | 11.66 | 11.48 | 11.30 | 11.12 | 10.94 | 10.76 | 10.58 |
| -12 | 10.40 | 10.22 | 10.04 | 9.56 | 9.68 | 9.50 | 9.32 | 9.14 | 8.90 | 8.78 |
| -13 | 8. 60 | 8.12 | 8.24 | S.06 | 7.85 | 7.70 | 7.52 | 7.34 | 7.16 | 6.98 |
| -14. | 6.80 | 6.62 | 6.44 | 6.26 | 6.08 | 5.90 | 5.72 | 5.54 | 5.36 | 5.18 |
| -15 | 5.00 | 4.82 | 4.64 | 4.46 | 4.28 | 4.10 | 3.92 | 3.74 | 3.56 | 3.38 |
| -16 | 3.20 | 3.02 | 2.84 | 2.66 | 2.48 | 2.30 | 2.12 | 1.94 | 1.76 | 1.58 |
| -17 | 1.40 | 22 | 1.04 | 0.86 | 0.68 | 0.50 | 0.32 | 0.14 | -0.04 | -0.22 |
| -18 | - 0.40 | -0.5s | -0.76 | -0.94 | - 1.12 | - 1.30 | - 1.48 | - 1.66 | - 1.84 | - 2.02 |
| -19 | $-2.20$ | - 2.38 | - 2.56 | - 2.74 | - 2.92 | - 3.10 | -3.28 | -3.46 | -3.64 | -3.82 |
| -20 | -4.00 | - 4.18 | - 4.36 | $-4.54$ | - 4.72 | - 4.90 | - 5.08 | -5.26 | - 5.4.4 | - 5.62 |
| -21 | - 5.80 | - 5.98 | -6.16 | -6.34 | -6.52 | - 6.70 | - 6.38 | - 7.06 | - 724 | - 7.42 |
| -22 | - 7.60 | - 7.78 | - 7.96 | - 8.14 | - 8.33 | - 8.50 | - 8.68 | -8.56 | -9.04 | -9.22 |
| -23 | - 9.40 | $-9.58$ | 9.76 | - 9.94 | -10.12 | -10.30 | -10.48 | -10.66 | -10.84 | -11.02 |
| -24 | -11.20 | -11.38 | -11.56 | -11.74 | -11.92 | -12.10 | -12.28 | -12.46 | -12.64 | -12.82 |
| -25 | -13.00 | -13.15 | -13.36 | -13.54 | -13.72 | -13.90 | -14.08 | -14.26 | -14.44 | -14.62 |
| -26 | -14.50 | -14.98 | -15.16 | -15.34 | $-15.52$ | $-15.70$ | -15. 88 | -16.06 | -16.24 | -16.42 |
| -27 | -16.60 | -16.78 | -16.96 | -17.14 | $-17.32$ | -17.50 | -17.68 | -17.86 | -18.04 | -18.22 |
| -28 | -18.40 | -18.58 | -18.76 | -18.91 | -19.12 | -19.30 | -19.48 | -19.66 | -19.84 | -20.02 |
| -29 | -20.20 | -20.35 | $-20.56$ | $-20.74$ | -20.92 | -21.10 | -21.29 | -21.46 | -21.64 | -21.82 |
|  | o. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigrade Degrees. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. |
| -30 | -22.00 | -22.18 | -22.36 | -2.2.54 | -22.72 | -22.90 | $-23.08$ | -23.26 | -23.44 | -23.62 |
| -31 | -23.80 | -23.98 | -24.16 | $-24.34$ | $-24.52$ | $-24.70$ | -24.88 | -2.5. 06 | -25.24 | -25.12 |
| -32 | -25.60 | -25.78 | -25.96 | -26.14 | -26.32 | $-26.50$ | -26.65 | $-26.86$ | -27.04 | -27.22 |
| -83 | $-27.40$ | $-27.58$ | $-27.76$ | $-27.94$ | -28.12 | $-28.30$ | $-28.45$ | -28.66 | -28.84 | $-29.02$ |
| -34 | $-29.20$ | -29.38 | $-29.56$ | $-29.74$ | $-29.92$ | $-30.10$ | $-30.28$ | $-30.46$ | -30.64 | $-30.82$ |
| -35 | -31.00 | -31.18 | -31.36 | -31.54 | $-31.72$ | -31.90 | $-32.08$ | -32.26 | -32.44 | -32.62 |
| -36 | -32.80 | $-32.98$ | -33.16 | $-33.34$ | $-33.52$ | $-33.70$ | -33.58 | $-34.06$ | -34.24 | -34.42 |
| -37 | -34.60 | $-34.78$ | -34.96 | -35.14 | -35.32 | $-35.50$ | -35.68 | -35. 86 | -36.04 | -36.29 |
| -38 | -36.40 | $-36.58$ | -36.76 | -36.94 | -37.12 | -37.30 | $-37.48$ | -37.66 | -37.84 | -38.02 |
| -39 | -38.20 | $-38.38$ | -38.56 | -38.74 | $-35.92$ | $-39.10$ | -39.2S | -39.46 | -39.64 | -39.82 |
| -40 | $-40.00$ | $-40.18$ | $-40.36$ | $-40.54$ | $-40.72$ | $-40.90$ | $-41.05$ | -41.26 | $-41.44$ | -41.62 |
| -41 | $-41.80$ | $-41.98$ | $-42.16$ | $-42.34$ | $-42.52$ | $-42.70$ | $-42.88$ | $-43.06$ | $-43.24$ | $-43.42$ |
| $-42$ | -43.60 | $-43.78$ | $-43.96$ | $-44.14$ | $-44.32$ | $-4.1 .50$ | $-44.68$ | -44.86 | $-45.04$ | $-45.22$ |
| $-43$ | $-45.40$ | $-45.58$ | $-45.76$ | $-45.94$ | $-16.12$ | $-46.30$ | $-46.45$ | $-46.66$ | -46.84 | -47.02 |
| -44 | $-47.20$ | $-47.38$ | $-47.56$ | $-47.74$ | $-47.92$ | $-48.10$ | $-48.28$ | $-48.46$ | $-48.64$ | $-48.82$ |
| -45 | $-49.00$ | $-49.18$ | $-49.36$ | $-49.54$ | $-49.72$ | $-49.90$ | -50.08 | -50.26 | $-50.44$ | $-50.62$ |
| -46 | $-50.80$ | $-50.98$ | $-51.16$ | $-51.34$ | -51.53 | -51.70 | -51.88 | -52.06 | $-52.24$ | $-52.42$ |
| $-47$ | $-52.60$ | $-52.78$ | $-52.96$ | -53.14 | $-53.32$ | -53.50 | -53.65 | $-53.86$ | -.54.04 | -54.22 |
| -48 | $-54.40$ | $-54.58$ | $-54.76$ | $-54.94$ | $-55.12$ | $-55.30$ | $-5.5 .48$ | $-5.5 .66$ | $-5.5 .54$ | -56.02 |
| -49 | $-56.20$ | $-56.38$ | $-56.56$ | $-56.74$ | $-56.92$ | $-57.10$ | $-57.28$ | $-57.46$ | $-57.64$ | $-57.82$ |
| -50 | -58.00 | -58.18 | -58.36 | $-58.54$ | $-55.72$ | -58.90 | -59.08 | $-59.26$ | -59.44 | $-59.62$ |
| -51 | -59.80 | $-59.98$ | $-60.16$ | -60.34 | $-60.52$ | $-60.70$ | -60.s8 | -61.06 | -61.24 | $-61.42$ |
| -52 | -61.60 | $-61.78$ | -61.96 | $-62.14$ | $-6.932$ | $-62.50$ | $-62.63$ | $-62.86$ | $-63.04$ | $-63.22$ |
| -53 | $-63.40$ | $-63.58$ | $-63.76$ | $-63.94$ | $-64.12$ | $-64.30$ | $-64.18$ | -6i1.66 | $-64.84$ | -6.5.02 |
| -54 | $-65.20$ | $-6.5 .38$ | $-6.9 .56$ | $-6.9 .74$ | $-6.3 .92$ | $-66.10$ | $-66.25$ | -66.46 | -66.64 | -66.82 |

TABLE FOR COMPARING THE CENTIGRADE AND FAIIRENIEIT'S TIIERMOMETERS NEAR THE BOILING POINT.

| Centigrade Degrees. | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fahren. | Fiahren. | Fahren. | Fahren. | Fahren. |
| 100 | 212.00 | 212.18 | 212.36 | 212.54 | 212.72 | 212.90 | 213.08 | 213.26 | 213.44 | 213.62 |
| 99 | 210.20 | 210.38 | 210.56 | 210.74 | 210.92 | 211.10 | 211.28 | 211.46 | 211.64 | 211.82 |
| 98 | 203.40 | 208.58 | 205.76 | 208.94 | 209.12 | 209.30 | 209.48 | 209.66 | 209.84 | 210.02 |
| 97 | 206.60 | 206.78 | 206.96 | 207.14 | 207.32 | 207.50 | 207.65 | 207.86 | 20s.04 | 208.22 |
| 96 | 204.80 | 204.98 | 205.16 | 205.34 | 20.5.52 | 20.570 | 20.5.58 | 206.06 | 206.24 | 206.42 |
| 95 | 203.00 | 203.18 | 203.36 | 203.54 | 203.72 | 203.90 | 204.08 | 204.26 | 204.44 | 204.62 |
| 94 | 201.20 | 201.38 | 201.56 | 201.74 | 201.92 | 202.10 | 202.28 | 202.46 | 20264 | 202.82 |
| 93 | 199.40 | 199.58 | 199.76 | 199.94 | 200.12 | 200.30 | 200.48 | 20066 | 200.54 | 201.02 |
| 92 | 197.60 | 197.78 | 197.96 | 198.14 | 195.32 | 198.50 | 198.68 | 199.86 | 199.04 | 199.22 |
| 91 | 195.80 | 195.98 | 196.16 | 196.34 | 196.52 | 196.70 | 196.88 | 197.06 | 197.24 | 197.42 |
| 90 | 194.00 | 194.18 | 194.36 | 194.54 | 194.72 | 194.90 | 195.08 | 195.26 | 195.44 | 195.62 |
| 89 | 192.20 | 192.38 | 192.56 | 192.74 | 192.92 | 193.10 | 193.28 | 193.46 | 193.64 | 193.82 |

A
VII. CONVERSION OF CENTIGRADE DEGREES INTO DEGREES OF REAUMUR.

| Centıgrade Degrees. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
|  | Rearm. | Reatum | Reaum. | $\begin{array}{r} \text { Resum. } \\ +\because \cdot \omega \cdot 1 \end{array}$ | Reaun. | Reaum. | Reaum. | Reaum. | $\begin{aligned} & \text { Reaum. } \\ & +\boldsymbol{9 9 . 6 . 1} \end{aligned}$ | $\begin{aligned} & \text { Reaum. } \\ & +32.72 \end{aligned}$ |
| $\pm 40$ | $\pm 32.00$ | $\pm 32.08$ | $\pm 32.16$ | $\pm: 32.24$ | $\pm 32.32$ | $\pm 32.40$ | $\pm 32.48$ | $\pm 32.56$ | $\pm 32.64$ | $\pm 32.72$ |
| 39 | 31.20 | 31.28 | 31.36 | 31.44 | 31.52 | 31.60 | 31.65 | 31.76 | 31.84 | 31.92 |
| 38 | 30.40 | 30.48 | 30.56 | 30.64 | 30.72 | 30.50 | 30.58 | 30.96 | 31.04 | 31.12 |
| 37 | 29.60 | 29.68 | 29.76 | 29.84 | 29.92 | 30.00 | 30.08 | 30.16 | 30.24 | 30.32 |
| 36 | 28.80 | 28.88 | 28.96 | 29.04 | 29.12 | 29.20 | 29.28 | 29.36 | 29.44 | 29.52 |
| 35 | 28.00 | 28.08 | 28.16 | 28.24 | 28.32 | 28.40 | 28.48 | 25.56 | 28.64 | 28.72 |
| 34 | 27.20 | 27.28 | 27.36 | 27.44 | 27.52 | 27.60 | 27.68 | 27.76 | 27.84 | 27.92 |
| 33 | 26.40 | 26.48 | 26.56 | 26.64 | 26.72 | 26.80 | 26.88 | 26.96 | 27.04 | 27.12 |
| - 32 | 25.60 | 25.65 | 25.76 | 25.84 | 25.92 | 26.00 | 26.08 | 26.16 | 26.2-4 | 26.32 |
| 31 | 24.80 | 24.88 | 24.96 | 25.04 | 25.12 | 25.20 | 25.28 | 25.36 | 25.44 | 25.52 |
| 30 | 24.00 | 24.08 | 24.16 | 24.24 | 25.32 | 24.40 | 24.48 | 24.56 | 24.64 | 24.72 |
| 29 | 23.20 | 23.28 | 23.36 | 23.44 | 23.52 | 23.60 | 23.68 | 23.76 | 23.54 | 23.92 |
| 28 | 22.40 | 22.48 | 22.56 | 22.64 | 22.72 | 22.50 | 22.58 | 22.96 | 23.04 | 23.12 |
| 27 | 21.60 | 21.68 | 21.76 | 21.84. | 21.92 | 22.00 | 22.08 | 22.16 | 22.24 | 22.32 |
| 26 | 20.50 | 20.88 | 20.96 | 21.04 | 21.12 | 21.20 | 21.28 | 21.36 | 21.44 | 21.52 |
| $2{ }^{*}$ | 20.00 | 20.08 | 20.16 | 20.24 | 20.32 | 20.40 | 20.48 | 20.56 | 20.64 | 20.72 |
| 24 | 19.20 | 19.28 | 19.36 | 19.44 | 19.52 | 19.60 | 19.68 | 19.76 | 19.84 | 19.92 |
| 23 | 18.40 | 18.48 | 18.56 | 18.64 | 18.72 | 18.80 | 18.88 | 18.96 | 1904 | 19.12 |
| 22 | 17.60 | 17.68 | 17.76 | 17.84 | 17.92 | 18.00 | 18.08 | 18.16 | 18.24 | 18.32 |
| 21 | 16.80 | 16.88 | 16.96 | 17.04 | 17.12 | 17.20 | 17.28 | 17.36 | 17.44 | 17.52 |
| 20 | 16.00 | 16.08 | 16.16 | 16.24 | 16.32 | 16.40 | 16.48 | 16.56 | 16.64 | 16.72 |
| 19 | 15.20 | 15.28 | 15.36 | 15.44 | 15.52 | 15.60 | 15.68 | 15.76 | 15.84 | 15.92 |
| 18 | 14.40 | 14.48 | 14.56 | 14.64 | 14.72 | 14.50 | 14.88 | 14.96 | 15.04 | 15.12 |
| 17 | 13.60 | 13.68 | 13.76 | 13.84 | 13.92 | 14.00 | 14.08 | 14.16 | 14.24 | 14.32 |
| 16 | 12.80 | 12.88 | 12.96 | 13.04 | 13.12 | 13.20 | 13.28 | 13.36 | 13.44 | 13.52 |
| 15 | 12.00 | 12.08 | 12.16 | 12.24 | 12.32 | 12.40 | 12.48 | 12.56 | 12.64 | 12.72 |
| 14 | 11.20 | 11.25 | 11.36 | 11.44 | 11.52 | 11.60 | 11.68 | 11.76 | 11.54 | 11.92 |
| 13 | 10.40 | 10.48 | 10.56 | 10.61 | 10.72 | 10.50 | 10.58 | 10.96 | 11.04 | 11.12 |
| 12 | 9.60 | 9.69 | 9.76 | 9.84 | 9.92 | 10.00 | 10.08 | 10.16 | 10.24 | 10.32 |
| 11 | 8.80 | 8.58 | 8.96 | 9.04 | 9.12 | 9.20 | 9.28 | 9.36 | 9.44 | 9.52 |
| 10 | 8.00 | 8.08 | 8.16 | 8.2 .1 | 8.32 | 8.40 | 8.48 | 8.56 | 8.64 | 8.72 |
| 9 | 7.20 | 7.28 | 7.36 | 7.44 | 7.52 | 7.60 | 7.68 | 7.76 | 7.84 | 7.92 |
| 8 | 6.40 | 6.48 | 6.56 | 6.64 | 6.72 | 6.80 | 6.85 | 6.96 | 7.04 | 7.12 |
| 7 | 5.60 | 5.68 | 5.76 | 5.84 | 5.92 | 6.00 | 6.08 | 6.16 | 6.24 | 6.32 |
| 6 | 4.50 | 4.88 | 4.96 | 5.04 | 5.12 | 5.20 | 5.25 | 5.36 | 5.44 | 5.52 |
| 5 | 4.00 | 4.08 | 4.16 | 4.24 | 4.32 | 4.40 | 4.48 | 4.56 | 4.64 | 4.72 |
| 4 | 3.20 | 3.25 | 3.36 | 3.44 | 3.52 | 3.60 | 3.68 | 3.76 | 3.84 | 3.9\% |
| 3 | 2.40 | 2.48 | 2.56 | 2.64 | 2.72 | 2.80 | 2.88 | 2.96 | 3.04 | 3.12 |
| 2 | 1.60 | 1.68 | 1.76 | 1.54 | 1.92 | 2.00 | 2.08 | 2.16 | 2.24 | 2.32 |
| 1 | 0.80 | 0.88 | 0.96 | 1.04 | 1.12 | 1.20 | 1.28 | 1.36 | 1.44 | 1.52 |
| O | 0. | 0, | . |  | - | , | , | - | $\bigcirc$ | $\bigcirc$ |
| 0 | 0.00 | 0.08 | 0.16 | 0.24 | 0.32 | 0.40 | 0.48 | 0.56 | 0.6 .4 | 0.72 |
|  | ©. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |

## VIII. -IX.

COMPARISON<br>of

## REAUMUR'S TIIERMOMETER

WITH

# TIIE TIIERMOMETER OF FAHRENHEIT AND THE CENTIGRADE TILERMOMETER, 

OR

## T A B L E S

FOR CONVERTING DEGREES of REAUMLR into DEGREES OF FAHRENiLEIT AND INTO CENTIfRADE DEGREES;
giving the corresponding values for eacil tentil of a degree, from $+40^{\circ}$ to - $40^{\circ}$ reaumur.
vill. conversion of degrees of reaumur into degrees of fahrenheit.

| Degrees of Reaumur. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 4.40 | $\begin{gathered} \text { Fahren. } \\ +122.00 \end{gathered}$ | $\begin{gathered} \text { Fahren. } \\ +122.22 \end{gathered}$ | $\begin{aligned} & \text { Fahren. } \\ & +122.45 \end{aligned}$ | $\begin{aligned} & \text { Fahren. } \\ & +122.67 \end{aligned}$ | $\begin{gathered} \text { Fahren. } \\ +122.90 \end{gathered}$ | $\begin{gathered} \text { Fahren. } \\ +123.12 \end{gathered}$ | $\begin{aligned} & \text { Fathren. } \\ & +123.3 . \end{aligned}$ | $\begin{gathered} \text { Futren. } \\ +123.57 \end{gathered}$ | $\begin{aligned} & \text { Fahren. } \\ & +123.50 \end{aligned}$ | $\begin{gathered} \text { Fahren. } \\ +124.02 \end{gathered}$ |
| 39 | 119.75 | 119.97 | 120.20 | 120.42 | 120.65 | 120.57 | 121.10 | 121.32 | 121.55 | 121.77 |
| 39 | 117.50 | 117.72 | 117.95 | 118.17 | 118.40 | 118.62 | 118.55 | 119.07 | 119.30 | 119.52 |
| 37 | 115.25 | 115.47 | 115.80 | 115.92 | 116.15 | 116.37 | 116.60 | 116.82 | 117.05 | 117.27 |
| 36 | 113.00 | 113.22 | 113.45 | 113.67 | 113.90 | 114.12 | 114.35 | 114.57 | 114.80 | 115.02 |
| 35 | 110.75 | 110.97 | 111.20 | 111.42 | 111.65 | 111.87 | 112.10 | 112.32 | 112.55 | 112.77 |
| 31 | 108.50 | 105.72 | 105.9.5 | 109.17 | 109.40 | 109.62 | 109.55 | 110.07 | 110.30 | 110.52 |
| 33 | 106.25 | 106.47 | 106.70 | 106.92 | 107.15 | 107.37 | 107.60 | 107.82 | 108.05 | 108.27 |
| 32 | 104.00 | 104.22 | 104.45 | 104.67 | 104.90 | 105.12 | 105.3.5 | 105.57 | 105.50 | 106.02 |
| 31 | 101.75 | 101.97 | 102.20 | 102.42 | 102.6. | 102.57 | 103.10 | 103.32 | 103.55 | 103.77 |
| 30 | 99.50 | 99.72 | 99.95 | 100.17 | 100.40 | 100.62 | 100.85 | 101.07 | 101.30 | 101.52 |
| 29 | 97.25 | 97.17 | 97.70 | 97.92 | 98.15 | 98.37 | 98.60 | 95.82 | 99.05 | 99.27 |
| 29 | 95.00 | 9.3 .22 | 95.45 | 95.67 | 95.90 | 96.12 | 96.35 | 96.57 | 96.30 | 97.02 |
| 27 | 92.75 | 92.97 | 93.20 | 93.42 | 93.65 | 93.57 | 94.10 | 94.32 | 94.55 | 94.77 |
| 26 | 90.50 | 90.72 | 90.95 | 91.17 | 91.40 | 91.62 | 91.55 | 92.07 | 92.30 | 92.52 |
| 25 | 88.2.5 | 88.47 | 88.70 | 88.92 | 89.15 | 89.37 | 89.60 | 89.92 | 90.05 | 90.27 |
| 24 | 86.00 | 86.22 | 86.45 | 6.67 | 6.90 | \% 12 | 87.35 | 57.57 | ) | 85.02 |
| 23 | 83.75 | 83.97 | 84.20 | 81.42 | 84.6.5 | S4.57 | 85.10 | 85.32 | 85.55 | 8.3.77 |
| 22 | 81.50 | 81.72 | 81.95 | 82.17 | 82.40 | 82.62 | 82.95 | 83.07 | 83.30 | 83.52 |
| 21 | 79.25 | 79.17 | 79.70 | 79.92 | 80.15 | 80.37 | 80.60 | 80.82 | 81.05 | 81.27 |
| 20 | 77.00 | 77.22 | 77.45 | 77.67 | 77.90 | 78.12 | 78.35 | 78.57 | 78.80 | 79.02 |
| 19 | 74.75 | 74.97 | 75.20 | 75.42 | 75.6 .4 | 75.87 | 76.10 | 76.32 | 76.55 | 76.77 |
| 18 | 72.50 | 72.72 | 72.9.5 | 73.17 | 73.40 | 73.62 | 73.85 | 74.07 | 74.30 | 74.52 |
| 17 | 70.25 | 70.47 | 70.70 | 70.92 | 71.15 | 71.37 | 71.60 | 71.82 | 72.05 | 72.27 |
| 16 | 68.00 | 65.22 | 68.45 | 65.67 | 68.90 | 69.12 | 69.35 | 69.57 | 69.50 | 70.02 |
| 15 | 6.5 .75 | 6.5 .97 | 66.20 | 66.42 | 66.65 | 66.57 | 67.10 | 67.32 | 67.55 | 67.77 |
| 14 | 63.50 | 63.72 | 63.9.5 | 64.17 | 64.40 | 64.62 | 64.85 | 6.9 .07 | 65.30 | 65.52 |
| 13 | 61.2 .5 | 61.17 | 61.70 | 61.92 | 62.15 | 62.37 | 62.60 | 62.52 | 63.05 | 63.27 |
| 12 | 59.00 | 59.22 | 59.45 | 59.67 | 59.90 | 60.12 | 60.3 .5 | 60.57 | 60.80 | 61.02 |
| 11 | 56.75 | 56.97 | 57.20 | 57.42 | 57.65 | 57.87 | 58.10 | 58.32 | 58.55 | 58.77 |
| 10 | 54.50 | 51.72 | 54.9.5 | 55.17 | 55.40 | 55.62 | 5.7.85 | 56.07 | 56.30 | 56.52 |
| 9 | 52.25 | 52.17 | 52.70 | 52.92 | 53.15 | 53.37 | 53.60 | 53.82 | 54.05 | 54.27 |
| 8 | 50.00 | 50.22 | 50.45 | 50.67 | 50.90 | 51.12 | 51.35 | 51.57 | 51.80 | 52.02 |
| 7 | 47.75 | 47.97 | 48.20 | 48.42 | 48.65 | 48.87 | 49.10 | 49.32 | 49.55 | 49.77 |
| 6 | 45.50 | 45.72 | 45.9.5 | 46.17 | 46.40 | 46.62 | 46.55 | 47.07 | 47.30 | 47.5? |
| 5 | 43.25 | 43.17 | 43.70 | 43.92 | 44.15 | 44.37 | 44.60 | 44.52 | 45.05 | 15.27 |
| 4 | 41.00 | 41.22 | 41.45 | 41.67 | 41.90 | 42.12 | 42.35 | 42.57 | 42.80 | 43.02 |
| 3 | 38.75 | 38.97 | 39.20 | 39.42 | 39.65 | 39.57 | 40.10 | 10.32 | 40.55 | 10.77 |
| 2 | 36.50 | 36.72 | 36.95 | 37.17 | 37.40 | 37.62 | 37.85 | 38.07 | 38.30 | 38.52 |
| 1 | 34.2.5 | 34.17 | 34.70 | 34.92 | 35.15 | 35.37 | 35.60 | 35.82 | 36.05 | 36.27 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Degrees of Reaumur. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| $+0$ | $\begin{gathered} \text { Fahren. } \\ +32.00 \end{gathered}$ | $\begin{aligned} & \text { Fahren. } \\ & +32.22 \end{aligned}$ | $\begin{aligned} & \text { Fahren. } \\ & +3.45 \end{aligned}$ | Fahren. $+32.67$ | Fahren. $\div 32.90$ | Fahren. $+33.12$ | $\begin{aligned} & \text { Fahren. } \\ & +33.35 \end{aligned}$ | Fahren. $+33.57$ | Fahren. $+33.80$ | Fahren. $+34.02$ |
| -0 | 32.00 | 31.77 | 31.55 | 31.32 | 31.10 | 30.87 | 30.65 | 30.42 | 30.20 | 29.97 |
| $-1$ | 29.75 | 29.52 | 29.30 | 29.07 | 28.53 | 28.62 | 28.10 | 25.17 | 27.95 | 27.72 |
| -2 | 27.50 | 27.27 | 27.05 | 26.82 | 26.60 | 26.37 | 26.15 | 25.92 | 2.5.70 | 25. 47 |
| $-3$ | 25.25 | 2.5.02 | 24.90 | 24.57 | 24.35 | 21.12 | 23.90 | 23.67 | 23.45 | 23.22 |
| $-4$ | 23.00 | 22.77 | 22.55 | 22.32 | 22.10 | 21.87 | 21.65 | 21.42 | 21.20 | 20.97 |
| - 5 | 20.75 | 20.52 | 20:30 | 20.07 | 19.85 | 19.62 | 19.40 | 19.17 | 18.9.5 | 18.72 |
| -6 | 18.50 | 18.27 | 18.05 | 17.82 | 17.60 | 17.37 | 17.15 | 16.92 | 16.70 | 16.47 |
| -7 | 16.25 | 16.02 | 15.80 | 15.57 | 15.35 | 15.12 | 14.90 | 14.67 | 14.4 .5 | 14.22 |
| - 8 | 14.00 | 13.77 | 13.55 | 13.32 | 13.10 | 12.57 | 12.65 | 12.42 | 12.20 | 11.97 |
| -9 | 11.75 | 11.52 | 11.30 | 11.07 | 10.85 | 10.62 | 10.40 | 10.17 | 9.95 | 9.72 |
| -10 | 9.50 | 9.27 | 9.05 | 8.82 | 8.60 | 8.37 | 8.15 | 7.92 | 7.70 | 7.47 |
| -11 | 7.25 | 7.02 | 6.50 | 6.57 | 6.35 | 6.12 | 5.90 | 5.67 | 5.45 | 5.22 |
| -12 | 5.00 | 4.77 | 4.55 | 4.32 | 4.10 | 3.87 | 3.65 | 3.42 | 3.20 | 2.97 |
| -13 | 2.75 | 2.52 | 2.30 | 2.07 | 1.85 | 1.62 | 1.40 | 1.17 | 0.95 | 0.72 |
| -14 | 0.50 | 0.27 | 0.05 | - 0.17 | - 0.40 | - 0.62 | -0.85 | - 1.07 | - 1.30 | $-1.52$ |
| -15 | - 1.75 | - 1.97 | - 2.20 | - 2.42 | - 2.65 | - 2.87 | - 3.10 | - 3.32 | - 3.55 | - 3.77 |
| -16 | - 4.00 | - 4.22 | - 4.45 | - 4.67 | - 4.90 | - 5.12 | - 5.35 | $-5.57$ | - 5.80 | -6.02 |
| -17 | - 6.25 | - 6.47 | - 6.70 | - 6.92 | - 7.15 | - 7.37 | - 7.60 | - 7.82 | - 8.05 | - 8.27 |
| -18 | - 8.50 | - 8.72 | - 8.9 .5 | - 9.17 | - 9.40 | - 9.62 | - 9.85 | -10.07 | -10.30 | -10.52 |
| -19 | -10.75 | -10.97 | -11.20 | -11.42 | -11.65 | -11.87 | -12.10 | -12.32 | $-12.55$ | -12.77 |
| -20 | -13.00 | -13.22 | -13.45 | -13.67 | -13.90 | -14.12 | -14.35 | -14.57 | $-14.80$ | -15.02 |
| -21 | -15.25 | -15.47 | $-15.70$ | -15.92 | -16.15 | -16.37 | -16.60 | -16.82 | -17.0. | $-17.27$ |
| -22 | -17.50 | $-17.72$ | -17.9. | -18.17 | -18.40 | -18.62 | -18.85 | -19.07 | -19.30 | -19.52 |
| -23 | -19.75 | -19.97 | -20.20 | -20.42 | -20.65 | -20.87 | -21.10 | $-21.32$ | -21.5.5 | -21.77 |
| -24 | -22.00 | -22.22 | $-22.45$ | -22.67 | -22.90 | -23.12 | -23.35 | $-23.57$ | -23.80 | $-24.02$ |
| -25 | -24.25 | -24.47 | $-24.70$ | -24.92 | -25.15 | -25.37 | -25.60 | -25.82 | -26.05 | -26.27 |
| -26 | -26.50 | -26.72 | -26.95 | -27.17 | -27.40 | -27.62 | -27.5.5 | -29.07 | -28.30 | -2 5.52 |
| -27 | -28.75 | -28.97 | -29.20 | -29.42 | -29.65 | -29.87 | -30.10 | -30.32 | -30.55 | -30.77 |
| -28 | -31.00 | -31.22 | -31.45 | -81.67 | -31.90 | -32.12 | -32.35 | -32.57 | -32.80 | -33.02 |
| -29 | -33.25 | -33.47 | $-33.70$ | -33.92 | -34.15 | -34.37 | -34.60 | $-34.82$ | -35.05 | -35.27 |
| -30 | -35.50 | -35.72 | -35.9.5 | -36.17 | -36.40 | -36.62 | -36.85 | -37.07 | -37.30 | -37.52 |
| -31 | -37.75 | -37.97 | -38.20 | -35.42 | -38.65 | -38.57 | -39.10 | -39.82 | -39.55 | -39.77 |
| -32 | -40.00 | -40.22 | -40.45 | -40.67 | -40.90 | -41.12 | -41.35 | -41.57 | -41.80 | -42.02 |
| -33 | -42.25 | -42.47 | -42.70 | $-42.92$ | -43.15 | -43.37 | -43.60 | -43.82 | -44.0.5 | -44.27 |
| -34 | -44.50 | $-44.72$ | $-44.95$ | -45.17 | $-45.40$ | -45.62 | -45.85 | -46.07 | -46.30 | -46.52 |
| -35 | -46.75 | -46.97 | $-47.20$ | -47.42 | -47.65 | $-47.87$ | -4S.10 | -48.32 | -48.55 | -48.77 |
| -36 | -49.00 | -49.22 | -49.45 | -49.67 | -49.90 | -50.12 | -50.35 | -50.57 | -50.80 | -51.02 |
| -37 | -51.25 | -51.47 | -51.70 | -51.92 | -52.15 | -52.37 | -52.60 | -52.82 | -53.05 | $-53.27$ |
| -38 | -53.50 | $-53.72$ | -53.95 | -54.17 | $-54.40$ | $-54.62$ | -54.85 | -55.07 | $-55.30$ | -55.52 |
| -39 | -55.75 | $-5.5 .97$ | -56.20 | -56.42 | -56.65 | -56.87 | -57.10 | -57.32 | -57.55 | -57.77 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 3. | 8. | 9. |

A
18. CONVERSION OF DEGREES OF REAUMUR INTO CENTIGKADE DEGREES.

| Degrees of Reaumur. | 'Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. |
| $\pm 40$ | $\pm 50.00$ | $\pm 50.13$ | $\pm 50.25$ | $\pm 50.38$ | $\pm 50.50$ | ${ }_{-}+50.63$ | $\pm 50.75$ | $\pm 50.88$ | $\pm 51.00$ | $\pm 51.13$ |
| 39 | 48.75 | 48.88 | 49.00 | 49.13 | 49.25 | 49.38 | 49.50 | 49.63 | 49.75 | 49.88 |
| 35 | 47.50 | 47.63 | 47.75 | 47.88 | 48.00 | 48.13 | 48.25 | 48.38 | 48.50 | 48.63 |
| 37 | 46.25 | 46.38 | 46.50 | 46.63 | 46.75 | 46.88 | 47.00 | 47.13 | 47.25 | 47.38 |
| 36 | 45.00 | 45.13 | 45.25 | 45.38 | 45.50 | 45.63 | 45.75 | 45.58 | 46.00 | 46.13 |
| 35 | 43.75 | 43.88 | 44.00 | 44.13 | 44.25 | 44.35 | 44.50 | 44.63 | 44.75 | 44.88 |
| 34 | 42.50 | 42.63 | 42.75 | 42.58 | 43.00 | 43.13 | 43.25 | 43.38 | 43.50 | 43.63 |
| 33 | 41.25 | 41.38 | 41.50 | 41.63 | 41.75 | 41.88 | 42.00 | 42.13 | 42.25 | 42.38 |
| 32 | 40.00 | 40.13 | 40.25 | 40.38 | 40.50 | 40.63 | 40.75 | 40.88 | 41.00 | 41.13 |
| 31 | 38.75 | 38.58 | 39.00 | 39.13 | 39.25 | 39.38 | 39.50 | 39.63 | 39.7 | 39.88 |
| 30 | 37.50 | 37.63 | 37.75 | 37.88 | 38.00 | 38.13 | 38.25 | 38.38 | 38.50 | 38.63 |
| 29 | 36.25 | 36.38 | 36.50 | 36.63 | 36.75 | 36.85 | 37.00 | 37.13 | 37.25 | 37.38 |
| 28 | 3.3 .00 | 35.13 | 35.25 | 35.38 | 35.50 | 35.63 | 35.75 | 35.88 | 36.00 | 36.13 |
| 27 | 33.75 | 33.58 | 34.00 | 34.13 | 34.25 | 34.38 | 34.50 | 34.63 | 34.75 | 34.88 |
| 26 | 32.50 | 32.63 | 32.75 | 32.88 | 33.00 | 33.13 | 33.25 | 33.38 | 33.50 | 33.63 |
| 25 | 31.25 | 31.38 | 31.50 | 31.63 | 31.75 | 31.85 | 32.00 | 32.13 | 32.25 | 32.38 |
| 24 | 30.00 | 30.13 | 30.25 | 30.38 | 30.50 | 30.63 | 30.75 | 30.88 | 31.00 | 31.13 |
| 23 | 28.75 | 28.88 | 29.00 | 29.13 | 29.25 | 29.38 | 29.50 | 29.63 | 29.75 | 29.88 |
| 22 | 27.50 | 27.63 | 27.75 | 27.88 | 28.00 | 28.13 | 28.25 | 28.38 | 28.50 | 2863 |
| 21 | 26.25 | 26.38 | 26.50 | 26.63 | 26.75 | 26.88 | 27.00 | 27.13 | 27.25 | 27.38 |
| 20 | 2.5 .00 | 25.13 | 25.25 | 25.38 | 25.50 | 25.63 | 25.75 | 2.5.88 | 26.00 | 20.13 |
| 19 | 23.75 | 23.88 | 24.00 | 24.13 | 24.25 | 24.38 | 24.50 | 24.63 | 24.75 | 24.88 |
| 18 | 22.50 | 22.63 | 22.75 | 22.88 | 23.00 | 23.13 | 23.25 | 23.38 | 23.50 | 23.63 |
| 17 | 21.25 | 21.38 | 21.50 | 21.63 | 21.75 | 21.85 | 22.00 | 22.13 | 22.25 | 22.38 |
| 16 | 20.00 | 20.13 | 20.25 | 20.38 | 20.50 | 20.63 | 20.75 | 20.88 | 21.00 | 21.13 |
| 15 | 18.75 | 18.88 | 19.00 | 19.13 | 19.25 | 19.38 | 19.50 | 19.63 | 19.75 | 19.88 |
| 14 | 17.50 | 17.63 | 17.75 | 17.88 | 18.00 | 18.13 | 18.25 | 18.38 | 18.50 | 18.63 |
| 13 | 16.2 .5 | 16.38 | 16.50 | 16.63 | 16.75 | 16.88 | 17.00 | 17.13 | 17.25 | 17.38 |
| 12 | 15.00 | 15.13 | 15.25 | 15.38 | 15.50 | 15.63 | 15.7.) | 15.88 | 16.00 | 16.13 |
| 11 | 13.75 | 13.88 | 14.00 | 14.13 | 14.25 | 14.38 | 14.50 | 14.63 | 14.75 | 14.88 |
| 10 | 12.50 | 12.63 | 12.75 | 12.88 | 13.00 | 13.13 | 13.25 | 13.38 | 13.50 | 13.63 |
| 9 | 11.2.) | 11.38 | 11.50 | 11.63 | 11.75 | 11.85 | 12.00 | 12.13 | 12.25 | 12.38 |
| 8 | 10.00 | 10.13 | 10.25 | 10.38 | 10.50 | 10.63 | 10.75 | 10.88 | 11.00 | 11.13 |
| 7 | 8.75 | 8.85 | 9.00 | 9.13 | 9.25 | 9.38 | 9.50 | 9.63 | 9.75 | 9.88 |
| 6 | 7.50 | 7.63 | 7.75 | 7.88 | 8.00 | 8.13 | 8.25 | 8.38 | 8.50 | 8.63 |
| 5 | 6.25 | 6.38 | 6.50 | 6.63 | 6.75 | 6.88 | 7.00 | 7.13 | 7.25 | 7.38 |
| 4 | 5.00 | 5.13 | 5.25 | 5.38 | 5.50 | 5.63 | 5.75 | 5.88 | 6.00 | 613 |
| 3 | 3.75 | 3.88 | 4.00 | 4.13 | 4.25 | 4.38 | 4.50 | 4.63 | 4.75 | 4.88 |
| 2 | 2.50 | 2.63 | 2.75 | 2.88 | 3.00 | 3.13 | 3.25 | 3.38 | 3.50 | 3.63 |
| 1 | 1.25 | 1.38 | 1.50 | 1.63 | 1.75 | 1.88 | 2.00 | 2.13 | 2.25 | 2.38 |
| 0 | 0.00 | 0.13 | 0.25 | 0.38 | 0.50 | 0.63 | 0.75 | 0.88 | 1.00 | 1.13 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

X. - XV.

## TABLES

## FOR

## COMPARING THERMOMETRICAL DIFFERENCES

EXPRESSED IN DEGREES OF DIFFERENT SCALES,

IRRESPECTIVE OF THEIR ZERO POINT.
x. Number of degrees of fahrenheit = number of centigrade degrees.
$4^{\circ}$ Reaumur $=5^{3}$ Centigrale $=9^{\circ}$ Fahrenheit.

| $\begin{aligned} & \text { Degrees } \\ & \text { of } \\ & \text { Fahren- } \\ & \text { heit. } \end{aligned}$ | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Cemig. | Centig. | Centig. | Centig. | Centig | Centig. | Centig. | Ceatig. | Centig. | Ceatig. |
| 0 | 0.00 | 0.06 | 0.11 | 0.17 | 0.22 | 0.25 | 0.33 | 0.39 | 0.44 | 0.50 |
| 1 | 0.56 | 0.61 | 0.67 | 0.72 | 0.75 | 0.83 | 0.89 | 0.94 | 1.00 | 1.06 |
| 2 | 1.11 | 1.17 | 1.22 | 1.28 | 1.33 | 1.39 | 1.44 | 1.50 | 1.56 | 1.61 |
| 3 | 1.67 | 1.72 | 1.78 | 1.83 | 1.89 | 1.94 | 2.00 | 2.06 | 2.11 | 2.17 |
| 4 | 2.22 | 2.28 | 2.33 | 2.39 | 2.41 | 2.50 | 2.56 | 2.61 | 2.67 | 2.72 |
| 5 | 2.78 | 2.83 | 2.89 | 2.94 | 3.00 | 3.06 | 3.11 | 3.17 | 3.22 | 3.28 |
| 6 | 3.33 | 3.39 | 3.44 | 3.50 | 3.56 | 3.61 | 3.67 | 4.72 | 3.78 | 3.83 |
| 7 | 3.59 | 3.94 | 4.00 | 4.06 | 4.11 | 4.17 | 4.22 | 4.28 | 1.33 | 4.39 |
| 8 | 4.41 | 4.50 | 4.56 | 4.61 | 4.67 | 4.72 | 4.75 | 4.83 | 4.59 | 4.94 |
| 9 | 5.00 | 5.06 | 5.11 | 5.17 | 5.22 | 5.28 | 5.33 | 5.39 | 5.14 | 5.50 |

XI. Number of degrees of fahrenheit = number of degrees of reaumur.

| $\begin{aligned} & \text { Degrees } \\ & \text { of } \\ & \text { Fahren. } \\ & \text { heit. } \end{aligned}$ | Temths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Reanmur. | f.eanmur. | Reaumur | Retumur | Remmur | Reammur | Reanmur. | Reaumur. | Reammur | Rexumu: |
| 0 | 0.00 | 0.04 | 0.09 | 0.13 | 0.15 | 0.22 | 0.27 | 0.31 | 0.36 | 0 40 |
| 1 | 0.14 | 0.19 | 0.53 | 0.58 | 0.62 | 0.67 | 0.71 | 0.76 | 0.50 | 0.84 |
| 2 | 0.89 | 0.93 | 0.98 | 1.02 | 1.07 | 1.11 | 1.16 | 1.20 | 1.24 | 1.29 |
| 3 | 1.33 | 1.35 | 1.42 | 1.47 | 1.51 | 1.56 | 1.60 | 1.64 | 1.69 | 1.73 |
| 4 | 1.78 | 1.82 | 1.87 | 1.91 | 1.96 | 2.00 | 2.04 | 2.09 | 2.13 | 2.18 |
| 5 | 2.22 | 2.27 | 2.31 | 2.36 | 2.40 | 2.44 | 2.49 | 2.53 | 2.58 | 2.62 |
| 6 | 2.67 | 2.71 | 2.76 | 2.50 | 2.8 .4 | 2.59 | 2.93 | 2.98 | 3.02 | 3.07 |
| 7 | 3.11 | 3.16 | 3.20 | 3.21 | 3.29 | 3.33 | 3.35 | 312 | 3.17 | 3.51 |
| 8 | 3.56 | 3.60 | 3.64 | 3.69 | 3.73 | 3.79 | 3.82 | 3.57 | :3.91 | 8.96 |
| 9 | 4.00 | 4.04 | 4.09 | 4.13 | 1.18 | 4.22 | 4.27 | 4.31 | 4.36 | 4.10 |

xif. NuMber of Centigrade degrees = Number of degrees of reaunur.

| Centig. Degrees | Teuths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Rean'mar | R.pamur | Reaumur. | Reaumur. | Remunur | Reaumur | Rearmur. | Reabmur | Reaurmir | Reammur. |
| 0 | 0.00 | 0.08 | 0.16 | 0.24 | 0.32 | 0.40 | 0.48 | 0.56 | 0.61 | 0.72 |
| 1 | $0 . \infty 0$ | 0.58 | 0.98 | 1.04 | 1.12 | 1.20 | 1.28 | 1.36 | 1.4 | 1.52 |
| 2 | 1.60 | 1.65 | 1.76 | 1.84 | 1.92 | 2.00 | 2.08 | 2.16 | 2.21 | 2.32 |
| 3 | 2.10 | 2.49 | 2.96 | 2.64 | 2.72 | 2.80 | 2.88 | 2.96 | 3.04 | 3.12 |
| 4 | 3.20 | 3.28 | 3.36 | 3.44 | 3.52 | 3.60 | 3.65 | 3.76 | 3.34 | 3.92 |
| 5 | 4.00 | 4.03 | 4.16 | 4.24 | 4.32 | 4.10 | 4.48 | 4.56 | 4.64 | 4.72 |
| 6 | 4.80 | 4.98 | 4.96 | 5.04 | 5.12 | 5.20 | 5.28 | 5.36 | 5.14 | 5.92 |
| 7 | 5.60 | 5.69 | 5.76 | 5.84 | 5.92 | 6.00 | 6.03 | 6.16 | 6.24 | 6.32 |
| 8 | 6.40 | 6.45 | 6.56 | 6.64 | 6.72 | 6. 80 | 6.88 | 6.96 | 7.04 | 7.12 |
| 9 | 7.20 | 7.28 | ${ }^{*} .36$ | 7.44 | 7.52 | 7.60 | 7.68 | 7.76 | 7.54 | 7.92 |

xill. NUMBER OF CENTIGRADE DEGREES = NUMbER of DEGREES of FAHRENHEIT.
$4^{\circ}$ Reaumur $=5^{\prime}$ Centigrade $=9^{\prime}$ Fahrenheit.

| Centig. Degrees | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fahr. | Fahr. | Fahr. | Fahr | Fahr. | Fahr. | Fahr. | Fahr. | Fatr. | Fahr. |
| 0 | 0.00 | 0.18 | 0.36 | 0.54 | 0.72 | 0.90 | 1.08 | 1.26 | 1.44 | 1.62 |
| 1 | 1.80 | 1.98 | 2.16 | 2.34 | 2.52 | 2.70 | 2.88 | 3.06 | 3.24 | 3.42 |
| 2 | 3.60 | 3.78 | 3.96 | 4.14 | 4.32 | 4.50 | 4.68 | 4.86 | 5.04 | 5.22 |
| 3 | 5.40 | 5.58 | 5.76 | 5.9 . 4 | 6.12 | 6.30 | 6.48 | 6.66 | 6.8 .1 | 7.02 |
| 4 | 7.20 | 7.38 | 7.56 | 7.74 | 7.92 | 8.10 | 8.28 | 8.46 | 8.64 | 8.82 |
| 5 | 9.00 | 9.18 | 9.36 | 9.54 | 9.72 | 9.90 | 10.08 | 10.26 | 10.44 | 10.62 |
| 6 | 10.50 | 10.98 | 11.16 | 11.34 | 11.52 | 11.70 | 11.88 | 12.06 | 12.24 | 12.42 |
| 7 | 12.60 | 12.75 | 12.96 | 13.14 | 13.32 | 13.50 | 13.68 | 13.86 | 14.04 | 14.22 |
| 8 | 14.40 | 14.58 | 14.76 | 14.94 | 15.12 | 15.30 | 15.48 | 15.66 | 15.84 | 16.02 |
| 9 | 16.20 | 16.38 | 1656 | 16.74 | 16.92 | 17.10 | 17.28 | 1:.46 | 17.64 | 17.82 |

xiv. Number of degrees of reaumur = number of centigrade degrees.

| $\begin{gathered} \text { Degrees } \\ \text { of } \\ \text { Reaum. } \end{gathered}$ | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | $\%$ \% | 8. | 9. |
|  | Centig. | Centig. | Centig | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. | Centig. |
| 0 | 0.00 | 0.12 | 0.25 | 0.37 | 0.50 | 0.62 | 0.75 | 0.87 | 1.00 | 1.12 |
| 1 | 1.25 | 1.37 | 1.50 | 1.62 | 1.75 | 1.87 | 2.00 | 2.12 | 2.25 | 2.37 |
| 2 | 2.50 | 2.62 | 2.75 | 2.57 | 3.00 | 3.12 | 3.25 | 3.37 | 3.50 | 2.62 |
| 3 | 3.75 | 3.87 | 4.00 | 4.12 | 4.25 | 4.37 | 4.50 | 4.62 | 4.75 | 4.87 |
| 4 | 5.00 | 5.12 | 5.25 | 5.37 | 5.50 | 5.62 | 5.75 | 5.87 | 6.00 | 3.12 |
| 5 | 6.25 | 6.37 | 6.50 | 6.62 | 6.75 | 6.57 | 7.00 | 7.12 | 7.25 | 7.37 |
| 6 | 7.50 | 7.62 | 7.75 | 7.87 | 8.00 | 8.12 | 8.25 | 8.37 | 8.50 | 8.62 |
| 7 | 8.75 | 8.87 | 9.00 | 9.12 | 9.25 | 9.37 | 9.50 | 9.62 | 9.75 | 9.87 |
| 8 | 10.00 | 10.12 | 10.25 | 10.37 | 10.50 | 10.62 | 10.75 | 10.57 | 11.00 | 11.12 |
| 9 | 11.25 | 11.37 | 11.50 | 11.62 | 11.75 | 11.87 | 12.00 | 12.12 | 12.25 | 12.37 |

xv. Number of degrees of reaumur = number of degrees of fahrenheit.

| Degrees of Reaum. | Tenths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fahr. | Fahr. | Fahr. | Fahr. | Fahr. | Fahr. | Fahr. | Fahr. | Fahr. | Fithr. |
| 0 | 0.00 | 0.22 | 0.45 | 0.67 | 0.90 | 1.12 | 1.35 | 1.57 | 1.80 | 2.02 |
| 1 | 2.25 | 2.17 | 2.70 | 2.92 | 3.15 | 3.37 | 3.60 | 3.82 | 4.05 | 4.27 |
| 2 | 4.50 | 4.72 | 4.95 | 5.17 | 5.10 | 5.62 | 5.85 | 6.07 | 6.30 | 6.52 |
| 3 | 6.75 | 6.97 | 7.20 | 7.42 | 7.65 | 7.87 | 8.10 | 8.32 | 8.55 | 8.77 |
| 4 | 9.00 | 9.22 | 9.45 | 9.67 | 9.90 | 10.12 | 10.35 | 10.57 | 10.80 | 11.02 |
| 5 | 11.25 | 11.47 | 11.70 | 11.92 | 12.15 | 12.37 | 12.60 | 12.82 | 13.05 | 13.27 |
| 6 | 13.50 | 13.72 | 13.95 | 14.17 | 11.40 | 14.62 | 14.85 | 15.07 | 15.30 | 15.52 |
| 7 | 15.75 | 15.97 | 16.20 | 16.42 | 16.65 | 16.87 | 17.10 | 17.32 | 17.55 | 17.77 |
| 8 | 18.00 | 18.22 | 18.45 | 18.67 | 18.90 | 19.12 | 19.35 | 19.57 | 19.80 | 20.02 |
| 9 | 20.25 | 20.47 | 20.70 | 20.92 | 21.15 | 21.37 | 21.60 | 21.82 | 22.05 | 22.27 |

[^0]
# METEOROLOGICAL TABLES 

SERIES II.

HYGROMETRICAL TABLES.

## C 0 N TENTS.

(The figures refer to the folio at the bottom of the page.)
Practical Tables based on Regnault's Mygrometrical Constants.
a. In French Measures.
Page
Page
Table I. Elastic Force of Aqueous Vapor, by Regnault
Table I. Elastic Force of Aqueous Vapor, by Regnault ..... 9 ..... 9
" II. Psychrometrical Tables, by Hacghens
" II. Psychrometrical Tables, by Hacghens ..... 12 ..... 12
" III. For deducing the Relative Humidity from the Indications of Dew-
" III. For deducing the Relative Humidity from the Indications of Dew- Point Instruments, by Hacghens Point Instruments, by Hacghens ..... 30 ..... 30
" IV. Factor $\frac{100}{\mathrm{~F}^{-}}$for computing Relative Humidity
" IV. Factor $\frac{100}{\mathrm{~F}^{-}}$for computing Relative Humidity ..... 36 ..... 36
" V. Weight of Vapor contained in a Cubic Metre of Air
" V. Weight of Vapor contained in a Cubic Metre of Air ..... 38 ..... 38
b. In English Measures.
b. In English Measures.
" VI. Elastic Force of Vapor, reduced from Reguault's Table
" VI. Elastic Force of Vapor, reduced from Reguault's Table ..... 43 ..... 43
" VII. Psychrometrical Tables, by A. Guyot
" VII. Psychrometrical Tables, by A. Guyot ..... 46 ..... 46
" VIII. For deducing the Relative Humidity from the Indications of Dew-
" VIII. For deducing the Relative Humidity from the Indications of Dew- Point Instruments, by A. Guyot Point Instruments, by A. Guyot ..... 75 ..... 75
" IX. Factor $\frac{100}{\mathrm{~F}}$, for computing Relative Humidity
" IX. Factor $\frac{100}{\mathrm{~F}}$, for computing Relative Humidity ..... 90 ..... 90
" X. Weight of Vapor in a Cubic Foot of Saturated Air
" X. Weight of Vapor in a Cubic Foot of Saturated Air ..... 94 ..... 94
Practical Tables based on the Hygrometrical Constants adopted in the
Practical Tables based on the Hygrometrical Constants adopted in the Greenwich Observations. Greenwich Observations.
Table XI. Elastic Force of Aqueous Vapor
Table XI. Elastic Force of Aqueous Vapor ..... 101 ..... 101
" XII. Psychrometrical Tables, by Glaisher
" XII. Psychrometrical Tables, by Glaisher ..... 104 ..... 104
" XIII. Factors for computing the Force of Vapor from Psychrometrical
" XIII. Factors for computing the Force of Vapor from Psychrometrical Observations, by Apjohn's Formula Observations, by Apjohn's Formula ..... 140 ..... 140
" XIV. Factors for finding the Temperature of the Dew-Point from the
" XIV. Factors for finding the Temperature of the Dew-Point from the Readings of the Psychrometer Readings of the Psychrometer ..... 142 ..... 142
" XV. Weight of Vapor contained in a Cubic Foot of Saturated Air
" XV. Weight of Vapor contained in a Cubic Foot of Saturated Air ..... 143 ..... 143
" XVI. Factors for deducing the Weight of Vapor from the Indications of
" XVI. Factors for deducing the Weight of Vapor from the Indications of Dew-Point Instruments . Dew-Point Instruments . ..... 143 ..... 143
" XVII. For comparing the Weight of a Cubic Foot of Dry and of Satu-
" XVII. For comparing the Weight of a Cubic Foot of Dry and of Satu- rated Air rated Air ..... 144 ..... 144
" XIV'. Factors for finding the Temperature of the Dew-Point from the
" XIV'. Factors for finding the Temperature of the Dew-Point from the Readings of the Psychrometer Readings of the Psychrometer ..... 146 ..... 146
B
B

## Miscellaneous Tables for Comparison.

Page
Table XVIII. Elastic Force of Vapor, expressed in Millimetres, by August ..... 150
" XIX. Elastic Force of Vapor, expressed in Millimetres, by Kaemtz ..... 152
" XX. Elastic Force of Vapor, expressed in Millimetres, by Magnus ..... 152
" XXI. Elastic Force of Vapor, in English Inches, from the Royal Society's Report ..... 153
" XXII. For showing the Differences in the Values of the Elastic Force of Vapor adopted by different Authorities ..... 154
" XXIII. Weight of Vapor, in Grammes, contained in a Cubic Metre of Saturated Air, by Pouillet ..... 156
" XXIV. Weight of Vapor, in Grammes, contained in a Cubic Metre of Air, by Kaemtz ..... 156
" XXV. Force of Vapor and Relative Humidity corresponding to the Degrees of Saussure's Hair-Hygrometer, by Gay-Lussae ..... 157
" XXVI. For deducing the Relative Humidity from the Indications of Saussure's Hair-Hygrometer, by Haeghens ..... 158
" XXVII. Relative Humidity corresponding to the Degrees of Saussure's Hygrometer, by Kaemtz . ..... 159
APPENDIX.
For comparing Quantities of Rain-water given in Different Measures.
Table 1. Conversion of Centimetres into English Inches ..... 164
" II. Conversion of Centimetres into French Inches and Lines ..... 164
" III. Conversion of English Inches into Centimetres ..... 165
" IV. Conversion of English Inches into French Inches and Lines ..... 165
" V. Conversion of French Inches and Lines into Centimetres ..... 166
" VI. Conversion of French Inches and Lines into English Inehes ..... 167

## HYGROMETRICAL TABLES.

Hygrometers, or instruments used for determining the amount of aqueous vapor present in the air, are of three classes. In the first, we find the hygrometers based on the absorption of moisture by hygroscopic substances, the best of which is Saussure's Hair-Hygrometcr; in the second class, the Psychrometer, or wet-bulb thermometer, which gives the temperature of evaporation ; in the third, the various instruments designed for ascertaining the temperature of the dew-point. From the data furnished by each of these instruments, and a table of the elastic forces of vapor at different temperatures, the humidity of the air can be deduced with more or less accuracy.

The use of the hygroscopic substances as hygrometers having been nearly given up on account of the inaccuracy of the results, the variability of the instruments, and the difficulty, if not impossibility, of making them comparable, the psychrometer and the dew-point instruments represent the two methods now usually employed in Meteorology. The following set, therefore, contains extensive tables, in Frencis and English measures, for deducing the hygrometrical condition of the atmosphere from the indications of the Psychrometer and of the dew-point instruments, to which have been added tables of the weight of vapor, in a given space, at different temperatures, - an element often needed in Meteorology.

As, however, the results deduced from the same data furnished by the observations may considerably differ, according to the values of the elastic force of vapor, and the formule used in the computation, the tables have been arranged in two series.

The first series contains Regnault's table of the elastic forces of vapor, with tables of the three kinds above mentioned, together with a corresponding set in English measures. Tables V. to X. have bcen computed for this volume.

The second series gives the table of elastic forces of vapor deduced from Dalton's experiments, and adopted in the Greenwich Observations, together with the various tables based on it.

A third series of miscellaneous tables furnishes the means of comparing the different values of the elastic force and weight of vapor determined by various physicists, as well as the results of Saussure's Hair-Hygrometer, with those obtained by other methods.

An Appendix, containing tables for comparing the quantity of rain-water indicated in different measures, closes the set.

Though the first series of tables, based on Regnault's table of tensions, is recommended for ordinary use, as being derived from the determinations which seem to deserve the greatest degree of confidence, it was thought expedient to give also the Greenwich tables, which have been, and still are, so extensively used in England, in order to enable meteorologists to judge of the differences which exist between the results obtained by them and those dednced from the constants of Regnault and others.

# PRACTICALTABLES, 

IN

## FRENCH MEASURES,

based on regnallt's hygronetrical constants.

TABLE


#### Abstract

of

THE ELASTIC FORCE OF AQUEOUS VAPOR,


expressed in millimetres of mercury for centigrade temperatures, BY REGNAULT.

This table contains the elastic forces of vapor corresponding to every tenth of a degree of temperature between $-35^{\circ}$ and $+40^{\circ}$ Centigrade, as determined by the experiments of V. Regnault, made by order of the French government, for the purpose of establishing the numerical value of the elements which enter into the computations concerning the steam-engine. These results are generally considered as the most accurate science possesses at present. They are published in the Mémoires de l'lnstitut, Tom. XXI.; and more correctly in Regnault's Etudes sur l'Hygrométrie, in the Amnales de Chimie et de Physique. In Vol. XV. Regnault gives the table of elastic forces for every tenth of a degrec from $-10^{\circ}$ to $+35^{\circ}$ Centigrade, which is reprinted in Table I. The numbers below - $10^{\circ}$ and above $+35^{\circ}$, in the same table, have been taken from another table for every full degree, previously published in Vol. XI. p. 333 of the same periodical, and in the same volume of the Mémoires de l'Institut, extending from $-32^{\circ}$ to $+230^{\circ}$.

It should be remarked, however, that the numbers below zero, in the two tables just mentioned, having been computed from different formulas of interpolation, slightly disagree. In order to establish a continuity, therefore, the numbers in Table I. corresponding to full degrees from $-10^{\circ}$ to $-35^{\circ}$ have been formed by starting from the value due to $-10^{\circ}$ in the larger table of Regnault, and subtracting from it the difference between $-10^{\circ}$ and $-11^{\circ}$ in the other table, in order to find the value of - $11^{\circ}$, and so on, by subtracting successively the corresponding differences to $-35^{\circ}$. For the fractions of degrees below $-10^{\circ}$, the mean values have been adopted as sufficiently accurate for meteoroiogical purposes.

## I. ELASTIC FORCE OF AQUEGUS VAPOR,

expressed in millimetres of mercury for centig bade temperatures.

By regnadlt.

| $\begin{aligned} & \text { Tempera- } \\ & \text { ture } \\ & \text { Centigrade } \end{aligned}$ | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| $\bigcirc$ | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. |
| -3.3 | 0.221 | 0.219 | 0.216 | 0.214 | 0.211 | 0.209 | 0.267 | 0.204 | 0.202 | 0.199 |
| -:31 | 0.217 | 0.244 | 0.242 | 0.219 | 0.237 | 0.234 | 0.231 | 0.299 | 0.226 | 0.2.4 |
| -33 | 0.275 | 0.272 | 0.269 | 0.267 | 0.264 | 0.261 | 0.2 .58 | 0.255 | 0.253 | 0.250 |
| -32 | 0.305 | 0.302 | 0.299 | 0.296 | 0.293 | 0.290 | 0.257 | 0.284 | 0.281 | 0.278 |
| -31 | 0.337 | 0.331 | 0.331 | 0.327 | 0.324 | 0.321 | 0.318 | 0.315 | 0.311 | 0.30s |
| -30 | 0.371 | 0.368 | 0.364 | 0.361 | 0.3 .97 | 0.3.54 | 0.351 | 0.347 | 0.344 | 0.340 |
| -29 | 0.409 | 0.405 | 0.401 | 0.398 | 0.391 | 0.390 | $0.3 \times 6$ | 0.382 | 0.379 | 0.375 |
| -28 | 0.449 | 0.445 | 0.441 | 0.437 | 0.433 | 0.129 | 0.42 .5 | 0.421 | 0.417 | 0.113 |
| -27 | 0.493 | 0.459 | 0.484 | 0.450 | 0.475 | 0.471 | 0.167 | 0.162 | 0.458 | 0.453 |
| -26 | 0.540 | 0.535 | 0.531 | 0.526 | 0.521 | 0.516 | 0.512 | 0.507 | 0.502 | 0.498 |
| -25 | 0.590 | 0.585 | 0.580 | 0.575 | 0.570 | 0.565 | 0.560 | 0.5 .55 | 0.550 | 0.545 |
| -24 | 0.645 | 0.639 | 0.634 | 0.623 | 0.623 | 0.617 | 0.612 | 0.606 | 0.601 | 0.59. |
| -23 | 0.704 | 0.698 | 0.692 | 0.686 | 0.650 | 0.674 | 0.669 | 0.663 | 0.6 .57 | 0.651 |
| -22 | 0.768 | 0.762 | 0.755 | 0.749 | 0.742 | 0.736 | 0.730 | 0.723 | 0.717 | 0.710 |
| -21 | 0.838 | 0.531 | 0.524 | 0.817 | 0.810 | 0.503 | 0.796 | 0.789 | 0.782 | 0.755 |
| -20 | 0.912 | 0.905 | 0.897 | 0.890 | 0.882 | 0.575 | 0.868 | 0.660 | 0.853 | 0.845 |
| -19 | 0.993 | 0.985 | 0.977 | 0.969 | 0.961 | 0.9 .22 | 0.941 | 0.936 | 0.923 | 0.920 |
| -15 | 1.050 | 1.071 | 1.063 | 1.0.54 | 1.06 | 1.036 | 1.028 | 1.019 | 1.010 | 1.062 |
| -17 | 1.174 | 1.165 | 1.155 | 1.116 | 1.136 | 1.127 | 1.118 | 1.108 | 1.099 | 1.089 |
| -16 | 1.275 | 1.265 | 1.255 | 1.245 | 1.235 | 1.224 | 1.214 | 1.204 | 1.194 | 1.184 |
| -15 | 1.38 .3 | 1.374 | 1.363 | 1.352 | 1.311 | 1.330 | 1.319 | 1.308 | 1.297 | 1.2 s 6 |
| -14 | 1.503 | 1.191 | 1.179 | 1. 468 | 1.4 .96 | 1.444 | 1.432 | 1.120 | 1.109 | 1.397 |
| -13 | 1.63 I | 1.618 | 1.605 | 1.593 | 1.580 | 1.567 | 1.5 .51 | 1.541 | 1.529 | 1.516 |
| -12 | 1.769 | 1.754 | $1.7+1$ | 1.727 | 1.713 | 1.699 | 1.656 | 1.672 | 1.6 .75 | 1.65 |
| -11 | 1.918 | 1.903 | 1.888 | 1.873 | 1.853 | 1.813 | 1.823 | 1.513 | 1.798 | 1.753 |
| -10 | 2.078 | 2.062 | 2.046 | 2.030 | 2.014 | 1.993 | 1.982 | 1.966 | 19.50 | 1.934 |
| $-9$ | 2.261 | 2.242 | 2.223 | 2.204 | 2.186 | 2.168 | 2.150 | 2.132 | 2.114 | 2.096 |
| -8 | 2.456 | 2.136 | 2.116 | 2.396 | 2.376 | 2.356 | 2.337 | 2.318 | 2.299 | 2.280 |
| - 7 | 2.666 | 2.645 | 2.624 | 2.603 | 2.582 | 2.561 | 2.540 | 2.519 | 2.498 | 2.177 |
| $-6$ | 2.890 | 2.567 | 2.844 | 2.521 | 2.798 | 2.776 | 2.754 | 2.732 | 2.710 | 2.688 |
| - 5 | 3.131 | 3.106 | 3.082 | 3.0.58 | 3.0:3 | 3.010 | 2.946 | 2.962 | 2.938 | 2.914 |
| - 4 | 3.357 | 3.361 | 3.335 | 3.369 | 3.253 | 3.257 | 3.231 | 3.206 | 3.181 | 3.156 |
| -3 | 3.662 | 3.634 | 3.606 | 3.578 | 3.550 | 3.522 | 3.495 | 3.468 | 3.441 | 3.411 |
| $-2$ | 3.955 | 3.925 | 3.595 | 3.865 | 3.636 | 3.807 | 3.778 | 3.749 | 3.720 | 3.691 |
| -1 | 4.267 | 4.235 | 1.203 | $4 . .71$ | 4.140 | 4.109 | 4.078 | 4.047 | 4.016 | 3.985 |
| - 0 | 1.600 | 4.565 | 4.531 | 4.497 | 1463 | 4.430 | 4.397 | 4.364 | 4.331 | 4.299 |
| , | O. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |


| Centigrade Degrees. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\bigcirc$ | Millim. | Millim. | Millim. | Millim. | Mıllim. | Millim. | Mullim. | Mıllim. | Millim. | Millim. |
| 0 | 4.600 | 4.633 | 4.667 | 4.700 | 4.733 | 4.767 | 4.801 | 4.836 | 4.871 | 4.90 .5 |
| 1 | 4.940 | 4.975 | 5.011 | 5.047 | 5.082 | 5.118 | 5.155 | 5.191 | 5.228 | 5.265 |
| 2 | 5.302 | 5.340 | 5.378 | 5.416 | 5.4.5 | 5.191 | 5.530 | 5.569 | 5.608 | 5.647 |
| 3 | 5.687 | 5.727 | 5.767 | 5.507 | 5.848 | 5.889 | 5.930 | 5.972 | 6.014 | 6.055 |
| 4 | 6.097 | 6.140 | 6.183 | 6.226 | 6.270 | 6.313 | 6.3 .57 | 6.401 | 6.44 .5 | 6.490 |
| 5 | 6.534 | 6.580 | 6.625 | 6.671 | 6.717 | 6.763 | 6.810 | 6.857 | 6.90 .1 | 6.951 |
| 6 | 6.998 | 7.047 | 7.095 | 7.144 | 7.193 | 7.242 | 7.292 | 7.342 | 7.392 | 7.412 |
| 7 | 7.492 | 7.514 | 7.59 .5 | 7.647 | 7.699 | 7.751 | 7.804 | 7.8 .57 | 7.910 | 7.961 |
| 8 | 8.017 | 8.072 | 8.126 | 8.181 | 8.236 | 8.291 | 8.347 | 8.404 | 8.161 | 8.517 |
| 9 | 8.571 | 8.632 | 8.690 | 8.718 | 8.807 | 8.865 | 8.925 | 8.98 .3 | 9.045 | 9.103 |
| 10 | 9.165 | 9.227 | 9.288 | 9.350 | 9.412 | 9.174 | 9.537 | 9.601 | 9.665 | 9.728 |
| 11 | 9.792 | 9.857 | 9.923 | 9.959 | 10.054 | 10.120 | 10.187 | 10.25.5 | 10.322 | 10.889 |
| 12 | 10.457 | 10.526 | 10.596 | 10.665 | 10.734 | 10.804 | 10.875 | 10.947 | 11.019 | 11.090 |
| 13 | 11.162 | 11.235 | 11.309 | 11.383 | 11.456 | 11.530 | 11.605 | 11.681 | 11.757 | 11.532 |
| 14 | 11.903 | 11.986 | 12.064 | 12.142 | 12.220 | 12.298 | 12.378 | 12.458 | 12.5388 | 12.619 |
| 15 | 12.699 | 12.781 | 12.864 | 12.947 | 13.029 | 13.112 | 13.197 | 13.281 | 13.366 | 13.451 |
| 16 | 13.586 | 13.623 | 13.710 | 13.797 | 13.855 | 13.972 | 14.062 | 14.151 | 14.241 | 14.331 |
| 17 | 11.421 | 14.513 | 14.605 | 14.697 | 14.790 | 14.582 | 14.977 | 15.072 | 15.167 | 1.5 .262 |
| 18 | 15.3.57 | 15.454 | 15.5.52 | 15.6.50 | 15.747 | 15.845 | 15.945 | 16.015 | 16.14.5 | 16.246 |
| 19 | 16316 | 16.449 | 16.592 | 16.6.5. | 16.7 .58 | 16.861 | 16.967 | 17.073 | 17.179 | 1728.5 |
| 20 | 17.391 | 17.500 | 17.605 | 17.717 | 17.826 | 17.935 | 18.047 | 15.159 | 18.271 | 18.353 |
| 21 | 15.19.7 | 18.610 | 18.724 | 18.839 | 18.954 | 19.069 | 19.187 | 19.305 | 19.423 | 19.511 |
| 22 | 19.6 .99 | 19.780 | 19.901 | 20.022 | 20.143 | 20.265 | 20.389 | 20.514 | $\underline{20.639}$ | 20.763 |
| 2:3 | 20.885 | 21.016 | 21.14 | 21.272 | 21.400 | 21.528 | 21.659 | 21.790 | 21.921 | 22.0.33 |
| 24 | 22.184 | 2.2319 | 22.453 | 2.2585 | 2.2.723 | 22.558 | 22.996 | 2313.5 | 23.273 | 23.111 |
| 25 | 23.550 | 23.692 | 23.534 | 23.976 | 24.119 | 24.261 | 24.406 | 24.552 | 24.697 | 24.812 |
| 23 | 21.988 | 2.5.139 | 25.289 | 25.138 | 25.588 | 25.738 | 25.691 | 26.045 | 26.193 | 26.351 |
| 27 | 26.50 .5 | 26.663 | 26.820 | 26.978 | 27.136 | 27.294 | 27.455 | 27.617 | 27.778 | 27.989 |
| - | 29.101 | 28.267 | 25.433 | 29.599 | 28.765 | 28.931 | 29.101 | 29.271 | 29.141 | 29.612 |
| 23 | 29.782 | 29.956 | 30.131 | 30.30 .5 | 30.179 | 30.654 | 30.833 | 31.011 | 31.190 | 31.369 |
| 30 | 31.548 | 31.729 | 31.911 | 32.094 | 32.278 | 32.163 | 32.650 | 32.837 | 33.026 | 33.215 |
| :1 | 33.406 | 33.596 | 33.787 | 33.980 | 34.174 | 34.368 | 34.564 | 34.761 | 34.959 | 35.1.59 |
| 3 ? | 35359 | 3.5.5.59 | 3.5 .760 | 35.962 | 36.16 .5 | 36.370 | 36.576 | 36.78.3 | 36.991 | 37.200 |
| :3; | 37.410 | 37.621 | 37.833 | 38.045 | 38.258 | 38.173 | 38.689 | 38.906 | 39.124 | 39.311 |
| $\therefore 1$ | 39.565 | 39.786 | 40.007 | 10.230 | 40.4.5 | 40.680 | 40.307 | 41.135 | 41.364 | 41.59 .5 |
| : ${ }^{\text {l }}$ | 41.227 | 12.059 | 42.293 | 42.527 | 42.763 | 43.000 | 43.235 | 43.177 | 43.717 | 43.959 |
| $\because 6$ | 14.201 | 11.44 .5 | 4.690 | 4.936 | 45.183 | 4.5 .131 | 45.681 | 15.932 | 46.184 | +6.137 |
| 37 | 16.6.\%1 | 46.917 | 17.20:3 | 47.462 | 17.721 | 47.9×1 | 18.213 | 48.506 | 48.770 | 49.0835 |
| 沓 | 19.31) | 49.570 | 49.8:39 | 50.110 | 50.3-2 | 50.655 | 50.929 | 51.205 | 51.481 | 51.759 |
| 31 | 52.03. | -2.320 | 52.602 | 52.585 | 53.170 | 53.4.6 | 53.743 | 54.032 | 51.822 | 51.613 |
| 49 | 5 5.406 | 5200 | 57.196 | 5.7.793 | 56.091 | 56.391 | 56.692 | 56.991 | 57.293 | 57.603 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6 | 8. | 8. | 9. |

# PSYCHROMETRICAL TABLES. <br> giving mmediately the force of aqueous vapor and the relative humidiy FROM THE INDICATIONS OF THE PSYCHROMETER. 

Calculated by M. T. Haeghens.

In his Etudes sur l'Hygrométrie,* M. V. Regnault discusses the theoretical bases of the formula of the Psychrometer, given by M. August, which was,

$$
x=f^{\prime}-\frac{0.565\left(t-t^{\prime}\right)}{610-t^{\prime}} h
$$

in which $h$ represents the height of the barometer; $t$ the temperature of the air given by the dry-bulb thermometer; $t^{\prime}$ the temperature of the wet-bulb thermometer; $f^{\prime}$ the force of aqueous vapor in the saturated air at a temperature equal to $t^{\prime} ; x$ the elastic force of aqueous vapor which exists in the air at the time of the observation.

After having modified some of the numerical values, which form the coefficients, M. Regnault adopted this formula,

$$
x=f^{\prime}-\frac{0.429\left(t-t^{\prime}\right)}{610-t^{\prime}} h .
$$

But comparative experiments, made by himself, showed that by substituting the coefficient 0.480 for that of 0.429 , the calculated results, and those obtained by direct observation, agree perfectly in the fractions of saturation, which are greater than 0.40 . This formula thus modified, or

$$
x=f^{\prime}-\frac{0.450\left(t-t^{\prime}\right)}{610-t^{\prime}} h
$$

has been used for calculating the following tables. In that part of the tables which supposes the wet-bulb to be covered with a film of ice, or below the freezing point, the value $610-t^{\prime}$, which represents the latent heat of aqueous vapor, has been changed into this: $610+79-t^{\prime}=689-t^{\prime}$.

The only hypothesis made, is that of a mean barometric pressure $h$, equal to 755 millimetres. If we take into account the causes of errors inherent to the psychrometer, and to the tables of the force of vapor, by means of which the absolute force of vapor is calculated, as well as to the differences of these tensions, taken at temperatures differing only by one tenth of a degree, it will be obvious that the correction due to the variations of barometric pressure can almost always be neglected. Nevertheless, a separate table has been calculated, giving the correction to be applied to the numbers in the Psychrometrical Tables for the heights of the barometer between 650 and 800 millimetres. It will be found at the end of the tables.

The disposition of the tables is the following :-
The temperatures are noted in centigrade degrees; the elastic force of vapor in the arr, or its pressure on the barometer, is expressed in millimetres of mercury; the rel-

[^1]ative humidity is indicated in per cent. of the full saturation of the air at the corresponding temperature of the dry-bulb thermometer $t$.

The first vertical column contains the indications of the wet-bulb thermometer $t^{\prime}$, begimning with the temperatures below the freezing point, when the bulb is coverer with ice, from $-35^{\circ}$, and continuing from the freezing point up to $+35^{\circ}$ centigrade, the bulb being simply wet.

The second column gives the differences of the force of vapor for each tenth $\left(0^{\circ} .1\right)$ of a degree, between each full degree of the first column. It enables the observer to find out the correction for any fraction of a degree of the wet-bulb thermometer.

The following double columns give immediately the force of vapor and the relative humidity, corresponding to each degree of the wet-bulb, placed in the first column, on the same horizontal line, and to differences of the two thermoneters, or to $t-t^{\prime}$, taken at every two tenths of a degree.

The horizontal column at the bottom indicates the mean difference, for each tenth of a degree, of the force of vapor contained in the same horizontal line. It gives the correction for the intermediate differences of the thermometers; $0.1,0.3,0.5,0.7$, $0.9, \& c ., \& c$.

To meet the wants arising from the extreme climate of North America, the tables of Mr. Haeghens have been extended from $-15^{\circ}$ to $-35^{\circ}$ centigrade, and from $+30^{\circ}$ to $+35^{\circ}$ of temperature of the wet bulb, and to $+40^{\circ}$ of temperature of the dry-bulb thermometer. The forces of aqueous vapor of Regnault, as given in 'Table I., have been used for the calculations.

## Use of the Tables.

Enter the tables with the difference of the two thermometers, or $t-t^{\prime}$, and with the temperature of the wet-bulb thermometer $t^{\prime}$, taking the first three pages, when the temperature of the wet-bulb is below the freezing point; and the following ones when it is above the freezing point.

Seek first the column at the head of which you find the difference of the thermometers; go down as far as the horizontal line, at the beginning of which you see the temperature of the wct-bulb thermometer; there you find the force of vapor, and the relative humidity corresponding to your observation.

Two corrections for fractions may be required for a complete caleulation of the force of vapor; one for the fractions of degrecs of the wet-bulb thermometer ; another for the intermediate differences of the two thermometers, viz. for $0.1,0.3,0.5$, 0.7 , \&c.

The first correction for fractions of degrees of the wet-bulb thermometer is found by multiplying the decimal fraction by the number placed in the second vertical column next to the whole degree, which number is the value of a tenth of a degree. The product must be added to the value of the full degree given in the table, when the temperature of the wet-bulb is above the freezing point: it must be subtracted when the temperatire is below the freezing point, and receives the sign -. This correction is too important to be neglected.

The second correction, less inportant, for the intermediate differences of the therB
mometers, which are greater by one tenth than those indicated in the tables, is given in the horizontal column at the bottom of the page. It is constant and always sub tractive.

## Examples of Calculation.

Difference of thermometers, or $t-t^{\prime}=0^{\circ} .8$.
Temperature of the wet-bulb thermometer, $t^{\prime}=11^{\circ} .0$.
We find, page 18 , for $t-t^{\prime}$, fifth double column ; and for $t^{\prime}$, first column, The force of vapor in the air $=9^{\mathrm{mm}} .31$. Relative humidity, $=90$.

Difference of thermometers, or $t-t^{\prime}=7^{\circ} . .$.
Wet-bulb thermometer, or $t^{\prime}$, $\quad=17^{\circ} .9$.
We find, page 24 , for $t-t^{\prime},=7^{\circ} .2$, and $t^{\prime}=17^{\circ} .0$, force of vapor $10^{\mathrm{mm}} .02$.
Additive correction for fraction $0^{\circ} .9$, or $9 \times 0.09=0 \quad .81$.
Force of vapor in the air $=10 \quad .83$
Relative humidity, 46

$$
\begin{aligned}
& \text { Difference of thermometers, } t-t^{\prime}=6^{\circ} .5 \\
& \text { Wet-bulb thermometer, } t^{\prime} \\
& =23^{\circ} .6 .
\end{aligned}
$$

We find, page 23 , for $t^{\prime}=23^{\circ} .0$, and $t-t^{\prime}$, or difference, $=6^{\circ} .4$, force of vapor $1 t^{\text {nut }} .94$; applying immediately the correction found at the bottom of the page for one if nth more difference, or $6^{\circ} .4+0.1=6^{\circ} .5$, we have,
Force of vapor $=16^{\mathrm{mm}} .94-006$, or $\quad 16^{\mathrm{mm}} .88$.

Additive correction for fraction 0.6 of the wet-bulb, $6 \times 0.13=0 \quad .78$.

$$
\begin{aligned}
& \text { Force of vapor in the air }=17 . .66 . \\
& \text { Relative humidity, }
\end{aligned}
$$

The wet-bulb thermometer covered with ice.

$$
\text { Difference of thermometers, } t-t^{\prime}=2^{\circ} .8 \text {. }
$$

$$
\text { Wet-bulb thermometer (ice), } t^{\prime}=-8^{\circ} .5 \text {. }
$$

Page 17 gives for $t-t^{\prime}=\mathfrak{Z}^{\circ} .8$, and $t^{\prime}=-8^{\circ} .0$, foree of vapor $=1^{m m} .0$.
Subtractive correction for fraction 0.5 of wet-bulb, $5 \times 0.019=-0 \quad .1$.
Force of vapor in the air $=\mathbf{0} \quad \mathbf{. 9 .}$
Relative humidity, $\quad 30$.

Below the Freezing-Point; the Bulb covered with a Film of Ice


B

Below the Freexing-Point ; the Bulb covered with a Film of Ice.


Nean IIorizontal Difference of Force of Vapor for each $0^{\circ} .1=0.05 \mathrm{~mm}$.

Below the Freezing-Point ; the Bulb covered with a Film of Ice.

|  | Mean Vertical Ditlerence for exch $0^{\circ} .1$ | t-1', Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 20.4 |  | 20.6 |  | $2 \times .8$ |  | $8 \bigcirc 0$ |  | $3^{\circ} \cdot \mathbf{2}$ |  | $3{ }^{\circ} .4$ |  |
|  |  | Force of Vapor. | Relative Hu-midity. | Force of Vapor | Relative Hu-midity. | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Itu- } \\ & \text { midi- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative Hu-midity. | Ence or Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ |
| $\begin{gathered} \circ \\ -15 \\ -14 \\ -13 \\ -12 \\ -11 \end{gathered}$ | Nillim. | Millim $0.15$ | 9 | Millim. | 3 | Millim. |  | Millim. |  | Millim. |  | Millim. |  |
|  | $\begin{aligned} & 0.011 \\ & 0.013 \\ & 0.013 \\ & 0.015 \end{aligned}$ | 0.27 | 15 | 0.16 | 9 | 0.06 | 4 |  |  |  |  |  |  |
|  |  | 0.39 | 20 | 0.29 | 14 | 0.19 | 9 | 0.08 | 4 |  |  |  |  |
|  |  | 0.53 | 25 | 0.42 | 19 | 0.32 | 14 | $0.2 \%$ | 10 | 0.11 | 5 |  |  |
|  |  | 0.68 | 29 | 0.57 | 24 | 0.47 | 19 | 0.36 | 15 | 0.26 | 10 | 0.16 | 6 |
| -10-9 | 0.016 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $0.018$ | 0.83 | 33 | 0.73 | 28 | 0.63 | 24 | 0.52 | 20 | 0.42 | 16 | 0.32 | 12 |
|  |  | 1.02 | 37 | 0.91 | 33 | 0.81 | 28 | 0.70 | 2.4 | 0.60 | 20 | 0.50 | 17 |
| -9 -8 | 0.019 | 1.21 | 40 | 1.10 | 36 | 1.00 | 32 | 0.90 | 28 | 6.79 | 25 | 0.69 | 21 |
| $\begin{aligned} & -7 \\ & -6 \end{aligned}$ | $\begin{aligned} & 0.021 \\ & 0.022 \end{aligned}$ | 1.42 | 44 | 1.31 | 40 | 1.21 | 36 | 1.11 | 32 | 1.00 | 29 | 0.90 | 26 |
|  |  | 1.64 | 47 | 1.54 | 43 | 1.43 | 40 | 1.33 | 36 | 1.22 | 33 | 1.12 | 30 |
| $-5$ | 0.024 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.025 | 1.88 | 50 | 1.77 | 46 | 1.67 | 43 | 1.57 | 40 | 1.46 | 36 | 1.36 | 33 |
| - 4 |  | 2.13 | 52 | 2.03 | 49 | 1.92 | 46 | 1.82 | 43 | 1.71 | 40 | 1.61 | 37 |
| - 3 | 0.027 | 2.40 | 55 | 2.30 | 52 | 2.19 | 48 | 2.09 | 45 | 1.99 | 43 | 1.88 | 40 |
| $\begin{aligned} & -2 \\ & -1 \end{aligned}$ | $\begin{aligned} & 0.029 \\ & 0.031 \end{aligned}$ | 2.70 | 57 | 2.59 | 54 | 2.49 | 51 | 2.38 | 48 | 2.25 | 46 | 2.17 | 43 |
|  |  | 3.01 | 59 | 2.90 | 56 | 2.80 | 54 | 2.69 | 51 | 2.59 | 48 | 2.48 | 46 |
|  |  | $3 \bigcirc .6$ |  | $3 \bigcirc .8$ |  | 40.0 |  | 40.2 |  | 4.4 |  | 40.6 |  |
|  |  | Millim. |  | Millim. |  | Millim. |  | Nillim. |  | Millim. |  | Nillim. |  |
| -15 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -14 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -13 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -12 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $-11$ | 0.016 | 0.05 | 2 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -10 | 0.018 | 0.21 | 8 | 0.11 | 4 |  |  |  |  |  |  |  |  |
| $-9$ | 0.019 | 0.39 | 13 | 0.29 | 9 | 0.19 | 6 | 0.08 | 3 |  |  |  |  |
| -8 |  | 0.55 | 18 | 0.18 | 14 | 0.38 | 11 | 0.27 | 8 | 0.17 | 5 | 0.06 | 2 |
| $\begin{aligned} & -7 \\ & -6 \end{aligned}$ | 0.021 | 0.79 | 22 | 0.69 | 19 | 0.59 | 16 | 0.48 | 13 | 0.38 | 10 | 0.27 | 7 |
|  | 0.022 | 1.91 | 26 | 0.91 | 23 | 0.81 | 20 | 0.70 | 17 | 0.60 | 15 | 0.49 | 12 |
| $-5$ | 0.024 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.025 | 1.25 | 30 | 1.15 | 27 | 1.04 | 24 | 0.94 | 22 | 0.83 | 19 | 0.73 | 16 |
| $-4$ |  | 1.50 | 34 | 1.40 | 31 | 1.30 | 28 | 1.19 | 26 | 1.09 | 23 | 0.98 | 20 |
| $-3$ | 0.027 | 1.78 | 37 | 1.67 | 34 | 1.57 | 32 | 1.46 | 29 | 1.36 | 27 | 1.25 | 24 |
| -2 | 0.0290.031 | 2.07 | 40 | 1.96 | 37 | 1.86 | 35 | 1.75 | 33 | 1.65 | 30 | 1.54 | 28 |
| -1 |  | 2.38 | 43 | 2.27 | 40 | 2.17 | 38 | 2.06 | 36 | 1.96 | 34 | 1.85 | 31 |

Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.05 \mathrm{~mm}$.

| Wet-ButbThermo-meter.$t^{\prime}$Centi-gradeDegrees. | Mean Vertical Difference for each $0^{\circ} .1$. | $\mathbf{t}-\mathbf{t}^{\prime}$, Difference of Wet and Dry-Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0^{\circ} .0$ |  | $0^{\circ} .2$ |  | $0^{\circ} .4$ |  | $0^{\circ} .6$ |  | $0^{\circ} .8$ |  | 10.0 |  |
|  |  | Force of Vapor. | Relative Humid ity. | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hul- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { helve } \\ & \text { Hur } \\ & \text { Heit- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Rela- <br> itive <br> Hu- <br> nid- <br> ity. |
| $\bigcirc$ | Millim. | Millim. | 100 | Millim. | 96 | Millim |  | Millim. |  | Millim. |  | Millim. |  |
| 1 | 0.03 . | 4.60 4.94 | 100 | 4.82 | 96 | 4.70 | 93 | 4.58 | 89 | 4.46 | 85 | 4.35 | 82 |
| 2 | 004 | 5.30 | 100 | 5.18 | 96 | 5.06 | 93 | 4.94 | 89 | 4.83 | 86 | 4.71 |  |
| 3 | 0.040.04 | 5.69 | 100 | 5.57 | 97 | 5.45 | 93 | 5.33 | 90 | 5.21 | 87 | 5.09 | 83 |
| 4 |  | $\begin{aligned} & 6.10 \\ & 6.53 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 5.98 \\ & 6.41 \end{aligned}$ | $\begin{aligned} & 97 \\ & 97 \end{aligned}$ | $\begin{aligned} & 5.86 \\ & 6.29 \end{aligned}$ | $\begin{aligned} & 93 \\ & 94 \end{aligned}$ | 5.746.17 | $\begin{aligned} & 90 \\ & 91 \end{aligned}$ | $\begin{aligned} & 5.62 \\ & 6.05 \end{aligned}$ | 87 | 5.50 |  |
| 5 | 0.04 |  |  |  |  |  |  |  |  |  | 88 | 5.94 | 85 |
|  | 0.05 |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 0.05 | 7.00 | 100 | 6.88 | 97 | 6.76 | 94 | 6.64 | 91 | 6.52 | 88 | 6.40 |  |
| 7 |  | 7.49 | 100 | 7.37 | 97 | 7.25 | 94 | 7.13 | 91 | 7.01 | 89 | 6.89 |  |
| 8 | $0.05$ | S. 02 | 100 | 7.90 | 97 | 7.788.33 | 94 | 7.66 | 9292 | 7.548.09 | 89 | 7.42 |  |
| 9 | $\begin{aligned} & 0.06 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 8.57 \\ & 9.17 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 8.45 \\ & 9.04 \end{aligned}$ | $\begin{aligned} & 97 \\ & 97 \end{aligned}$ |  |  | $\begin{aligned} & 8.21 \\ & 8.80 \end{aligned}$ |  |  | 8990 |  |  |
| 10 |  |  |  |  |  | $\begin{aligned} & 8.33 \\ & 8.92 \end{aligned}$ | $\begin{aligned} & 95 \\ & 95 \end{aligned}$ |  | $\begin{aligned} & 92 \\ & 93 \end{aligned}$ | $\begin{aligned} & 8.09 \\ & 8.68 \end{aligned}$ |  | 7.97 86 <br> 8.56 87 | 6 |
|  | 0.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 0.07 | 9.79 | 100 | 9.67 | 97 | 9.55 | 95 | 9.43 | 93 | 9.31 | 90 | 9.19 | 88 |
| 12 |  | 10.46 | 100 | 10.34 | 98 | 10.21 | 95 | 10.09 | 93 | 9.97 | 90 | 9.85 | 88 |
| 13 | 0.07 | $\begin{aligned} & 11.16 \\ & 11.91 \end{aligned}$ | 100 | 11.04 | 98 | 10.92 | 95 | 10.50 | 93 | 10.68 | 91 | 10.56 | 89 |
| 14 | 0.07 0.08 |  | 100 | 11.79 | 98 | 11.66 | 95 | 11.54 | 93 | 11.42 | 91 | 11.30 | 89 |
| 15 | 0.08 | 12.70 | 100 | 12.58 | 98 | 12.46 | 96 | 12.33 | 93 | 12.21 | 91 | 12.09 | 89 |
|  | 0.08 |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 0.09 | 13.54 | 100 | 13.41 | 98 | 13.29 | 96 | 13.17 | 94 | 13.05 | 92 | 12.93 | 90 |
| 17 | 0.09 | 14.42 | 100 | 14.30 | 98 | 14.18 | 96 | 14.05 | 9.4 | 13.93 | 92 | 13.81 | 90 |
| 18 |  | 15.36 | 100 | 15.23 | 98 | 15.11 | 96 | 14.99 | 94 | 14.87 | 92 | 14.75 | 90 |
| 19 | 0.10 | 16.35 | 100 | 16.22 | 98 | 16.10 | 96 | 15.98 | 94 | 15.86 | 92 | 15.73 | 91 |
| 20 | 0.10 | 17.39 | 100 | 17.27 | 98 | 17.15 | 96 | 17.02 | 94 | 16.90 | 92 | 16.78 | 91 |
|  | 0.11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 |  | 18.50 | 100 | 18.37 | 98 | 18.25 | 96 | 18.13 | 94 | 18.00 | 92 | 17.88 | 91 |
| 22 |  | 19.66 | 100 | 19.54 | 98 | 1941 | 96 | 19.29 | 95 | 19.17 | 93 | 19.04 | 91 |
| 23 |  | 20.59 | 100 | 20.76 | 98 | 20.64 | 96 | 20.52 | 95 | 20.39 | 93 | 20.27 | 91 |
| 24 |  | 22.18 | 100 | 22.06 | 98 | 21.94 | 97 | 21.81 | 95 | 21.69 | 93 | 21.57 | 92 |
| 25 | 14 | 23.55 | 100 | 23.43 | 95 | 23.30 | 97 | 23.18 | 95 | 23.05 | 93 | 22.93 | 92 |
|  | 0.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 |  | 24.99 | 100 | 24.86 | 98 | 24.74 | 97 | 24.62 | 95 | 24.49 | 93 | 24.37 | 92 |
| 27 |  | 26.51 | 100 | 26.38 | 98 | 26.26 | 97 | 26.13 | 95 | 26.01 | 93 | 25.88 | 92 |
| 28 |  | 28.10 | 100 | 27.98 | $98^{\circ}$ | 27.85 | 97 | 27.73 | 95 | 27.60 | 93 | 27.48 | 92 |
| 29 |  | 29.78 | 100 | 29.66 | 98 | 29.53 | 97 | 29.41 | 95 | 29.28 | 94 | 29.16 | 92 |
| 30 | 0.15 | 31.55 | 100 | 31.42 | 98 | 31.30 | 97 | 31.17 | 95 | 30.05 | 94 | 30.92 | 93 |
|  | 0.19 |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | 0.20 | 33.40 | 100 | 33.28 | 95 | 33.15 | 97 | 33.03 | 96 | 32.90 | 94 | 32.78 | 93 |
| 32 | 0.20 | 35.36 | 100 | 35.23 | 99 | 35.11 | 97 | 34.98 | 96 | 34.66 | 94 | 34.73 | 93 |
| 33 | 0.21 | 37.41 | 100 | 37.28 | 99 | 37.16 | 98 | 37.03 | 96 | 36.91 | 94 | 36.78 | 93 |
| 34 | 0.23 | 39.56 | 100 | 39.43 | 99 | 39.31 | 98 | 39.18 | 96 | 39.06 | 94 | 38.93 | 93 |
| 35 |  | 41.83 | 109 | 41.70 | 99 | 41.58 | 98 | 41.45 | 96 | 41.33 | 95 | 41.20 | 93 |

Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.06 \mathrm{~mm}$.

| Wet-BulbThermometer.t $t^{\prime}$Centi-gradeDegrees | Mean Vertical Differ. ence for each $0^{\circ} .1$. | $\mathbf{t}$ - $\mathbf{t}$, Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1{ }^{\circ} .2$ |  | 10.4 |  | 10.6 |  | $1{ }^{\circ} .8$ |  | $2 \cdot 0$ |  | $2{ }^{\circ} \mathbf{2}$ |  |
|  |  | Force of Vapor. | $\begin{gathered} \text { Relative } \\ \text { Humid } \\ \text { ity. } \end{gathered}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mit- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Reld- } \\ & \text { tuve } \\ & \text { Hu- } \\ & \text { mid } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Rela. tive $\mathrm{Ha}-$ mid. ity. | Force of Vapor. | Relative H H. mid ity. | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ |
| 0 | Millim. | Millim. | 78 | Mialim. | 74 | Millim. | 71 | $\begin{array}{\|c} \text { Millim. } \\ \mathbf{3 . 5 3} \end{array}$ | 67 | $\begin{array}{\|c} \text { Millim. } \\ 3.4 \mathrm{I} \end{array}$ | 64 | $\begin{array}{r} \text { Millim. } \\ 3.29 \end{array}$ | 61 |
|  | $0.03$ | 3.89 |  | 3.77 |  | 3.65 |  |  |  |  |  |  |  |
| 1 |  | 4.23 | 79 | 4.11 | 75 | 3.99 | 72 | 3.87 | 69 | 3.75 | 66 | 3.63 | 63 |
| 2 | $0.04$ | 4.59 | 80 | 4.47 | 76 | 4.35 | 73 | 4.23 | 70 | 4.11 | 67 | 3.99 65 |  |
| 3 |  | 4.97 | 80 | 4.85 | 77 | 4.73 | 74 | 4.615.02 | 71 | 4.494.90 | 69 | 4.3766 |  |
| 4 | $0.04$ | $\begin{aligned} & 5.38 \\ & 5.82 \end{aligned}$ | $\begin{aligned} & 81 \\ & 82 \end{aligned}$ | $\begin{aligned} & 5.26 \\ & 5.70 \end{aligned}$ | $\begin{aligned} & 78 \\ & 79 \end{aligned}$ | $\begin{aligned} & 5.14 \\ & 5.58 \end{aligned}$ | $\begin{aligned} & 75 \\ & 77 \end{aligned}$ |  | $\begin{aligned} & 73 \\ & 74 \end{aligned}$ |  | 70 | 4.7867 |  |
| 5 |  |  |  |  |  |  |  | $\begin{aligned} & 5.02 \\ & 5.46 \end{aligned}$ |  | $\begin{array}{r} 4.90 \\ 5.34 \end{array}$ | 71 | 5.22 69 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 0.05 | 6.28 | 83 | 6.16 | S0 | 6.04 | 77 | 5.92 | 75 | 5.50 | 72 | 5.68 | 70 |
| 7 |  | 6.77 | 83 | 6.65 | 81 | 6.53 | 78 | 6.41 | 76 | 6.29 | 73 | 6.17 |  |
| 8 | 0.05 | 7.29 | 84 | 7.17 | 81 | 7.05 | 79 | 6.93 | 76 | 6.81 | 74 | 6.69 |  |
| 9 | $\begin{aligned} & 0.06 \\ & 0.06 \end{aligned}$ | $\begin{aligned} & 7.8 .5 \\ & 8.44 \end{aligned}$ | $\begin{aligned} & 84 \\ & 85 \end{aligned}$ | $\begin{aligned} & 7.73 \\ & 8.32 \end{aligned}$ | $\begin{aligned} & 82 \\ & 83 \end{aligned}$ | $\begin{aligned} & 7.61 \\ & 8.20 \end{aligned}$ | $\begin{aligned} & 80 \\ & 80 \end{aligned}$ | $\begin{aligned} & 7.49 \\ & 8.08 \end{aligned}$ | $\begin{aligned} & 77 \\ & 78 \end{aligned}$ | $\begin{aligned} & 7.37 \\ & 7.96 \end{aligned}$ | 75 | 7.2587 |  |
| 10 |  |  |  |  |  |  |  |  |  |  | 76 | 7.84 | 3 |
|  | 0.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 0.07 | 9.07 | 86 | 8.95 | 83 | 8.82 | 81 | 8.709.37 | 79 | 8.58 | 77 | 8.46 | 75 |
| 12 |  | 9.73 | 86 | 9.61 | 84 | 9.49 | 82 |  | 80 | 9.25 | 78 | 9.12 76 |  |
| 13 | $\begin{aligned} & 0.07 \\ & 0.08 \end{aligned}$ | $\begin{aligned} & 10.43 \\ & 11.18 \end{aligned}$ | 86 | 10.3111.06 | 84 | 10.19 | 82 | 9.37 10.07 | 80 | 9.9.5 | 78 | 9.83 | 76 |
| 14 |  |  | 87 |  | 85 | 10.9 ¢ | 83 | 10.81 | 81 | 10.69 | 79 | 10.57 | 77 |
| 15 |  | 11.97 | 87 | 11.85 | 85 | 11.73 | 83 | 11.60 | 81 | 11.48 | so | 11.36 | 78 |
|  | 0.08 |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 0.09 | 12.80 | 88 | 12.68 | 86 | 12.56 | 84 | 12.44 | 82 | 12.32 | S0 | 12.19 | 75 |
| 17 |  | 13.69 | 88 | 13.57 | 86 | 13.44 | 84 | 13.32 | 83 | 13.20 | 81 | 13.08 | 79 |
| 18 | 0.0 | 14.62 | 88 | 14.50 | 87 | 14.38 | 85 | 14.26 | 83 | 14.13 | 81 | 14.01 | 80 |
| 19 |  | 15.61 | 89 | 15.49 | 87 | 15.37 | 85 | 15.24 | 83 | 15.12 | 82 | 15.00 | 80 |
| 20 | 0.11 | 16.65 | 89 | 16.53 | 87 | 16.41 | 86 | 16.29 | 84 | 16.16 | 82 | 16.04 | 81 |
|  | 0.11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 |  | 17.76 | 59 | 17.63 | 58 | 17.51 | 86 | 17.39 | 84 | 17.27 | 83 | 17.14 | 81 |
| 22 |  | 18.92 | 90 | 18.80 | 88 | 18.67 | 86 | 18.55 | 85 | 18.43 | 83 | 18.30 | 82 |
| 23 |  | 20.15 | 90 | 20.02 | 58 | 19.90 | 87 | 19.78 | 85 | 19.65 | 83 | 19.53 | 82 |
| 24 | 0. | 21.44 | 90 | 21.32 | 88 | 21.20 | 87 | 21.07 | 85 | 20.95 | 84 | 20.82 | 82 |
| 25 | 0.14 | 2.2 .81 | 90 | 22.68 | 89 | 22.56 | 87 | 22.44 | 86 | 22.31 | 84 | 22.19 | 83 |
|  | 0.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 |  | 24.24 | 90 | 24.12 | 89 | 23.99 | 87 | 23.87 | 86 | 23.75 | 85 | 23.62 | 83 |
| 27 |  | 25.76 | 91 | 25.63 | S9 | 2.5 .51 | 88 | 25.39 | 86 | 2.5.26 | 85 | 2.5 .14 | 83 |
| 28 |  | 27.35 | 91 | 27.23 | 89 | 27.10 | 88 | 26.98 | 87 | 26.86 | 85 | 26.73 | 84 |
| 29 | 18 | 29.03 | 91 | 28.91 | 90 | 28.78 | 88 | 28.66 | 87 | 28.53 | 85 | 28.41 | 84 |
| 30 | 0.15 | 30.80 | 91 | 30.67 | 90 | 30.55 | 89 | 30.42 | 87 | 30.30 | 86 | 30.17 | 84 |
|  | 0.19 |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 |  | 32.65 | 91 | 32.53 | 90 | 32.40 | 89 | 32.28 | 87 | 32.15 | 86 | 32.03 | 8.5 |
| 32 | 0.21 | 34.61 | 91 | 34.48 | 90 | 34.36 | 89 | 34.23 | 88 | 34.11 | 86 | 33.98 | 85 |
| 33 | 0.21 | 36.66 | 92 | 36.53 | 90 | 36.41 | 89 | 36.28 | 88 | 36.16 | 86 | 36.03 | 8.5 |
| 34 |  | 38.81 | 92 | 38.68 | 90 | 35.56 | 89 | 38.43 | 88 | 38.31 | 87 | 38.18 | 85 |
| 35 | 0.23 | 41.07 | 92 | 40.94 | 91 | 40.82 | 89 | 40.69 | 88 | 40.57 | 87 | 40.44 | 86 |
|  |  | Mean | Horizont | al Differe | ce of | Force of | Vapor | each | $1=$ | 06 mm . |  |  |  |




| Wet-BulbThermo-meter.t $^{\prime}$Centi-gradeDegrees. | Mean Vertical Difference for each $0^{\circ} .1$. | $\mathbf{t}-\mathbf{t}^{\prime}$, Difflerence of Wet and Dry-Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $4{ }^{3} .8$ |  | $5^{\circ} .0$ |  | 5.2 |  | $5{ }^{\circ} .4$ |  | $5^{\circ} .6$ |  | $5^{\circ} .8$ |  |
|  |  | Force of Vapor. | Relative Humid ity. | Force of Vapar. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{array}{\|l\|l} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { Hui- } \\ \text { mity- } \end{array}$ | Force of Vapor. | Rela tive He- mid- ity. | Force of Vapor. | Rela <br> tive <br> Hu- <br> mid <br> ity. | Force of Vapor. | Rela- live Hu- midl- ity. it |
| $\bigcirc$ | Millim. | Millim. |  | Millim. |  | Millim. |  | Millim. |  | Millim. |  | Millim. |  |
| 0 | 0.03 | 1.75 | 27 | 1.63 | 25 | 1.51 | 23 | 1.39 | 21 | 1.27 | 19 | 1.15 | 17 |
| 1 | 0.04 | 2.08 | 30 | 1.97 | 28 | 1.85 | 26 | 1.73 | 2.4 | 1.61 | 22 | 1.49 | 20 |
| 2 |  | 2.44 | 33 | 2.32 | 31 | 2.20 | 29 | 2.08 | 27 | 1.96 | 25 | 1.85 | 23 |
| 3 | 0.04 | 2.82 | 36 | 2.70 | 34 | 2.55 | 32 | 2.46 | 30 | 2.34 | 28 | 2.22 | 26 |
| 4 | $\begin{aligned} & 0.04 \\ & 0.04 \end{aligned}$ | 3.23 | 38 | 3.11 | 36 | 2.99 | 34 | 2.87 | 33 | 2.75 | 31 | 2.63 | 29 |
| 5 |  | 3.66 | 40 | 3.54 | 39 | 3.42 | 37 | 3.30 | 35 | 3.18 | 33 | 3.06 | 32 |
|  | 0.05 |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 0.05 | 4.12 | 43 | 4.00 | 41 | 3.85 | 39 | 3.76 | 37 | 3.64 | 36 | 3.52 | 34 |
| 7 |  | 4.61 | 45 | $4 \cdot 49$ | 43 | 4.37 | 41 | 4.25 | 40 | 4.13 | 38 | 4.01 | 36 |
|  | 0.05 | 5.13 | 47 | 5.01 | 45 | 4.89 | 43 | 4.77 | 42 | 4.65 | 40 | 4.53 | 39 |
| 910 | 0.06 | 5.65 | 48 | 5.56 | 47 | 5.44 | 45 | 5.32 | 44 | 5.20 | 42 | 5.08 | 41 |
|  | 0.66 | 6.27 | 50 | 6.15 | 48 | 6.02 | 47 | 5.90 | 45 | 5.78 | 44 | 5.66 | 42 |
|  | 0.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 0.07 | 6.89 | 52 | 6.77 | 50 | 6.65 | 49 | 6.53 | 17 | 6.10 | 46 | 6.25 | 44 |
| 12 |  | 7.55 | 53 | 7.43 | 52 | 7.31 | 50 | 7.15 | 49 | 7.06 | 47 | 6.94 | 46 |
| 13 | 0.07 | 8.25 | 55 | 8.13 | 53 | 8.01 | 52 | 7.88 | 50 | 7.76 | 49 | 7.64 | 47 |
| 14 |  | 8.99 | 56 | 8.87 | 54 | 8.75 | 53 | 8.62 | 51 | 8.50 | 50 | 8.38 | 49 |
|  | $0.08$ | 9.78 | 57 | 9.65 | 55 | 9.53 | 54 | 9.41 | 53 | 9.29 | 51 | 9.17 | 50 |
| 16 | 0.08 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.09 | 10.61 | 58 | 10.49 | 57 | 10.36 | 55 | 10.24 | 54 | 10.12 | 53 | 10.00 | 51 |
| 17 | 0.09 | 11.49 | 59 | 11.37 | 58 | 11.24 | 56 | 11.12 | 55 | 11.00 | 54 | 10.88 | 53 |
| 18 |  | 12.42 | 60 | 12.30 | 59 | 12.17 | 58 | 12.05 | 56 | 11.93 | 55 | 11.81 | 54 |
| 19 | 0.10 | 13.40 | 61 | 13.28 | 60 | 13.16 | 59 | 13.04 | 57 | 12.91 | 56 | 12.79 | 55 |
| 20 | 0.11 | 14.44 | 62 | 14.32 | 61 | 14.20 | 60 | 14.08 | 58 | 13.95 | 57 | 13.83 | 56 |
| 21 | 0.11 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.12 | 15.54 | 63 | 15.42 | 62 | 15.30 | 60 | 15.17 | 59 | 15.05 | 58 | 14.93 | 57 |
| 22 | 0.12 | 16.70 | 64 | 16.58 | 63 | 16.46 | 61 | 16.33 | 60 | 16.21 | 59 | 16.09 | 58 |
| 23 |  | 17.93 | 65 | 17.80 | 63 | 17.68 | 62 | 17.56 | 61 | 17.43 | 60 | 17.31 | 59 |
| 24 | 0.13 | 19.22 | 65 | 19.09 | 64 | 18.97 | 63 | 15.85 | 62 | 18.72 | 61 | 18.60 | 60 |
|  | 0.14 | 20.58 | 66 | 20.46 | 65 | 20.33 | 64 | 20.21 | 63 | 20.08. | 62 | 19.96 | 60 |
|  | 0.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 | 0.15 | 22.01 | 67 | 21.58 | 6.5 | 21.76 | 64 | 21.63 | 63 | 21.51 | 62 | 21.39 | 61 |
| 27 | 0.16 | 23.52 | 67 | 23.40 | 66 | 23.27 | 65 | 23.15 | 64 | 23.02 | 63 | 22.90 | 62 |
| 28 |  | 25.11 | 68 | 24.99 | 67 | 24.86 | 66 | 24.74 | 65 | 24.61 | 64 | 24.49 | 63 |
| 2930 | 0.17 | 26.79 | 68 | 26.66 | 67 | 26.54 | 66 | 26.41 | 65 | 26.29 | 64 | 26.16 | 63 |
|  | 0.18 | 28.55 | 69 | 28.42 | 68 | 28.30 | 67 | 25.17 | 66 | 28.05 | 65 | 27.92 | $6 i$ |
| 31 | 0.19 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.20 | 30.40 | 70 | 30.28 | 69 | 30.15 | 68 | 30.03 | 67 | 29.90 | 66 | 29.78 | 65 |
| 32 | 0.21 | 32.35 | 70 | 32.22 | 69 | 32.10 | 68 | 31.97 | 67 | 31.85 | 66 | 31.72 | 65 |
| 33 |  | 34.40 | 71 | 34.27 | 70 | 34.15 | 69 | 34.02 | 68 | 33.90 | 67 | 33.77 | 66 |
| 34 | 0.22 | 36.5 .5 | 71 | 36.42 | 70 | 36.30 | 69 | 36.17 | 68 | 36.05 | 67 | 35.92 | 66 |
| 35 |  | 38.80 | 71 | 38.68 | 70 |  |  |  |  |  |  |  |  |

Mean Horizontal Difference of Force of Vapor for each $0^{\top} .1=0.06 \mathrm{~mm}$.

| Wet-BulbThermometer.$\mathbf{t}^{\prime}$Centi-gradeDegrees | Mean Vertical Difference for each $0^{\circ} .1$. | t- $\mathbf{t}^{\prime}$, Difference of Wet and Dry-Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $6^{\circ} \cdot 0$ |  | $6^{\circ} .2$ |  | $6^{\circ} .4$ |  | $6^{\circ} .6$ |  | $6^{\circ} .8$ |  | $7{ }^{\circ} \cdot 0$ |  |
|  |  | Force of Vapor. | Relative Humid. ity. | Force of Vapor. | $\begin{aligned} & \text { Hela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { Huid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tue } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Rela tive Hu. midity. | Force of Vapor. | Rela tive Hu- mid. ity. | Furce of Vapor. | Rela- tive Hu- mud- ity. |
| $\bigcirc$ | Millim. | Millim. $1.04$ | 15 | $\begin{array}{\|r} \text { Millim. } \\ 0.92 \end{array}$ | 13 | $\begin{array}{r} \text { Millim. } \\ 0.80 \end{array}$ | 11 | $\begin{array}{\|r} \hline \text { Millinı. } \\ 0.6 \mathrm{~S} \end{array}$ | 9 | $\begin{array}{r} \text { Millim. } \\ 0.56 \end{array}$ | 8 | $\begin{array}{\|r} \hline \text { Millim. } \\ 0.44 \end{array}$ | 6 |
| 1 | $\begin{aligned} & 0.03 \\ & 0.04 \end{aligned}$ | 1.37 | 18 | 1.25 | 16 | 1.13 | 15 | 1.01 | 13 | 0.89 | 11 | 0.78 | 30 |
| 2 |  | 1.73 | 22 | 1.61 | 20 | 1.49 | 18 | 1.37 | 16 | 1.25 | 1.5 | 1.13 | 13 |
| 3 | 0.04 | 2.11 | 25 | 1.99 | 23 | 1.57 | 21 | 1.75 | 19 | 1.63 | 18 | 1.51 |  |
| 4 | 0.04 |  | 28 | 2.39 | 26 | 2.27 | 2427 | 2.15 | 23 | 2.03 | 21 | 1.91 |  |
| 5 | 0.04 | $\begin{aligned} & 2.51 \\ & 2.94 \end{aligned}$ | 30 | 2.82 | 25 |  |  | 2.58 | 25 | 2.46 | 24 | 1.91 19 <br> 2.34 22 |  |
|  | 0.05 |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 0.05 | 3.40 | 33 | 3.28 | 31 | 3.16 | 29 | 3.04 | 28 | 2.92 | 26 | 2.80 | 25 |
| 7 |  | 3.59 | 35 | 3.77 | 33 | 3.65 | 32 | 3.53 | 30 | 3.413.92 | 29 | 3.2925 |  |
| 8 | 0.05 | 4.414.96 | 37 | 4.25 | 35 | 4.16 | 34 | 4.04 | 33 |  | 3.9231 | 3.80 30 |  |
| 9 | $\begin{aligned} & 0.06 \\ & 0.06 \end{aligned}$ |  | 39 | $\begin{aligned} & 4.8 .4 \\ & 5.42 \end{aligned}$ | $\begin{aligned} & 38 \\ & 40 \end{aligned}$ | $\begin{aligned} & 4.71 \\ & 5.30 \end{aligned}$ | $\begin{aligned} & 36 \\ & 38 \end{aligned}$ |  | $\begin{aligned} & 35 \\ & 37 \end{aligned}$ | $\begin{aligned} & 4.47 \\ & 5.06 \end{aligned}$ | $\begin{aligned} & 33 \\ & 35 \end{aligned}$ | 4.35 |  |
| 10 |  | $\begin{aligned} & 4.96 \\ & 5.54 \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & 4.59 \\ & 5.18 \end{aligned}$ |  |  |  | 4.94 | 34 |
|  | 0.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 0.07 | 6.16 | 43 | 6.04 | 41 | 5.92 | 40 | 5.80 | 39 | 5.68 | 37 | $5.56$ | 36 |
| 12 |  | 6.82 | 44 | 6.70 | 43 | 6.58 | 42 | 6.46 | 41 | 6.34 | 39 |  | 35 |
| 13 | 0.07 | $\begin{aligned} & 7.52 \\ & 8.26 \\ & 9.05 \end{aligned}$ | 46 | 7.40 | 45 | 7.28 | 43 | 7.16 | 42 | 7.03 | 41 | 6.91 40 |  |
| 14 | $\begin{aligned} & 0.07 \\ & 0.08 \end{aligned}$ |  | $\begin{aligned} & 47 \\ & 49 \end{aligned}$ | $\begin{aligned} & 8.14 \\ & 8.92 \end{aligned}$ | $\begin{aligned} & 46 \\ & 48 \end{aligned}$ | $\begin{aligned} & 5.02 \\ & 8.80 \end{aligned}$ | $\begin{aligned} & 45 \\ & 46 \end{aligned}$ | $\begin{aligned} & 7.90 \\ & 8.68 \end{aligned}$ | 44 | 7.77 | 43 | 7.65 | 41 |
| 15 |  |  |  |  |  |  |  |  | 45 | 8.56 | 44 | 8.44 | 43 |
|  | 0.08 |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 0.09 | 9.88 | 50 | 9.75 | 49 | 9.63 | 48 | 9.51 | 47 | 9.39 | 45 | 9.27 | 44 |
| 17 | 0.09 | 10.76 | 52 | 10.63 | 50 | 10.51 | 49 | 10.39 | 48 | 10.27 | 47 | 10.14 | 46 |
| 18 |  | 11.69 | 53 | 11.56 | 51 | 11.44 | 50 | 11.32 | 49 | 11.20 | 48 | 11.07 | 47 |
| 19 | 0.10 | 12.67 | 54 | 12.55 | 53 | 12.42 | 51 | 12.30 | 50 | 12.18 | 49 | 12.06 | 48 |
| 20 | 0.11 | 13.71 | 55 | 13.58 | 54 | 13.46 | 53 | 13.34 | 52 | 13.22 | 50 | 13.09 | 49 |
|  | 0.11 |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 |  | 14.81 | 56 | 14.68 | 55 | 14.56 | 54 | 14.44 | 53 | 14.31 | 52 | 14.19 | 51 |
| 22 |  | 15.96 | 57 | 15.34 | 56 | 15.72 | 55 | 15.59 | 54 | 15.47 | 53 | 15.3.5 | 52 |
| 23 | 0.12 0.13 | 17.19 | 58 | 17.06 | 57 | 16.94 | 56 | 16.82 | 55 | 16.69 | 54 | 16.57 | 53 |
| 24 |  | 18.48 | 59 | 18.35 | 58 | 18.23 | 56 | 18.11 | 35 | 17.98 | 54 | 17.86 | 53 |
| 25 | 0.14 | 19.84 | 59 | 19.71 | 58 | 19.59 | 57 | 19.46 | 56 | 19.34 | 55 | 19.22 | 54 |
|  | 0.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 |  | 21.26 | 60 | 21.14 | 59 | 21.01 | 58 | 20.89 | 57 | 20.77 | 56 | 20.64 | 55 |
| 27 | 0.15 | 22.77 | 61 | 22.65 | 60 | 22.52 | 59 | 22.40 | 58 | 22.28 | 57 | 22.15 | 56 |
| 28 | 0.16 | 24.36 | 62 | 24.24 | 61 | 24.11 | 60 | 23.99 | 59 | 23.86 | 58 | 23.74 | 57 |
| 29 | 0.17 | 26.04 | 62 | 2.5.91 | 61 | 2.5 .79 | 60 | 25.66 | 59 | 25.54 | 58 | 2.5 .41 | 57 |
| 30 | 0.15 | 27.80 | 63 | 27.67 | 62 | 27.55 | 61 | 27.42 | 60 | 27.30 | 59 | 27.17 | 58 |
|  | 0.19 |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 |  | 29.65 | 64 | 29.53 | 63 | 29.40 | 62 | 29.28 | 61 | 29.15 | 60 | 29.03 | 59 |
| 32 |  | 31.59 | 64 | 31.47 | 63 | 31.34 | 62 | 31.22 | 61 | 31.09 | 60 | 30.97 | 59 |
| 33 |  | 33.64 | 65 | 33.51 | 64 | 33.39 | 63 | 33.26 | 62 | 33.14 | 61 | 33.01 | 60 |
| 34 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 35 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Mean | Horizont | al Differen | nce of | Force of | Vapo | reach | $1=$ | 0.06 mm . |  |  |  |



Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.06 \mathrm{~mm}$.




Mean Horizonta! Difference of Force of Vapor for each $0^{\circ} .1=0.06 \mathrm{~mm}$.


Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=006 \mathrm{~mm}$.

Correc ion for the Barometrical Height.


## III.

T A B L E<br>GIVING AT SIGHT THE RELATIVE HUMIDITY DEDUCED FROM THE INDIGA. TIONS OF THE DEW POINT INSTRUMENTS.<br>By M. T. Haeghens.

This table, whici has been published in the Amuaire Météorologique de Fi ance for 1850 , page 86 , and following, has been calculated by Mr. Haeghens, using Regnault's Tables of Elastic Forces of Vapor. It gives directly the relative humidity when the hygrometrical observations bave been made by means of dew point instruments like those of Daniell, Regnault, Bache, and others.

These hygrometers are destined to find out the temperature of the dew point, that is the temperature to which it would be necessary to lower the temperature of the air, in order that this air be completely saturated by the aqueous vapor which it contained at the time of the observation.

The force of vapor contained in the air, or its absolute humidity, is thus the maximum of force of vapor which corresponds to the temperature of the dew point; it is given directly in the Table I. of the Elastic Forces of Vapor, by Reguault.

The ratio of that maximum of force of vapor at the temperature of the dew point to the force of vapor which corresponds, in the same table, to the temperature of the suromuling air at the time of the observation, is the relative humidity. This ratio is given in hundredths in the following table, which relieves the observer of the trouble of calculating it.

Let $t=$ temperature of the air surrounding the instrument.
$t^{\prime}=$ temperature of the dew point.
$t-t^{\prime}=$ the difference between these two temperatures.
The first column, on the left, contains the temperature of the air $t$, in centigrade degrces. The following ones, headed with the differences, $t-t^{\prime}$, between the temperatures of the air and of the dew point, give the relative humidity corresponding to the two elements.

$$
\begin{array}{ccccc} 
& \text { Tenp. of the } A \text { ir }=t . & \text { Dew point }=t^{t} . & \text { Difference } t-t^{t} . & \text { Relative Humidity } \\
\text { Example : } & 10^{\circ} .0 & 4^{\circ} .4 & 5^{\circ} .6 & 68
\end{array}
$$

Should the temperature of the air $t^{\prime}$, or the difference $t-t^{\prime}$, fall between the numbers found in the columns, it is obvious, by glancing at the table, that an interpolation at sight will always be easy.

| 1emper |  | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatares of the Dew Point and of the Air. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| the wr | $10^{\circ} .0$ | $0^{\circ} .2$ | $0^{\circ} .4$ | $10^{\circ} .16$ | $0^{\circ} \cdot \mathrm{s}$ | $1{ }^{\circ} .0$ | $11^{\circ} .2$ | $1{ }^{\circ} .1$ | $1^{\circ} .6$ | $1^{\circ} .8$ | $3^{\circ} .11$ | $2{ }^{\circ} .13$ | $9^{\circ} .4$ | $2^{\circ} .6$ | $2{ }^{\circ} .8$ |
| Cellig. | 100 | 98 | 97 | 95 | 9 | 92 | 90 | 89 | 88 | 86 | 85 | 83 | 82 | S0 | 79 |
| -7 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 89 | 88 | 86 | 85 | 83 | 82 | 81 | 79 |
| -1 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 89 | 88 | s7 | 85 | 84 | 82 | 81 | S0 |
| -5 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 89 | 88 | 87 | 85 | 84 | 82 | 81 | so |
| -4 | 100 | 98 | 97 | 93 | 94 | 92 | 91 | 89 | 88 | 87 | 85 | 84 | 83 | 81 | 80 |
| --3 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 90 | 88 | 87 | 85 | 84 | 83 | 81 | s0 |
| $\cdots$ | 100 | 98 | 97 | 95 | 94 | 93 | 91 | 90 | S8 | S7 | 86 | 84 | 83 | 82 | s0 |
| -1 | 100 | 98 | 97 | 95 | 94 | 93 | 91 | 90 | 89 | 87 | 86 | 85 | 83 | 82 | 81 |
| 0 | 100 | 98 | 97 | 96 | 94 | 93 | 91 | 90 | S9 | 87 | 86 | 85 | 83 | 82 | 81 |
| $t 1$ | 100 | 99 | 97 | 96 | 9.5 | 93 | 92 | 90 | 59 | 88 | 86 | 85 | 84 | 83 | 81 |
| 2 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 89 | 88 | 87 | 85 | 84 | 83 | 82 |
| 3 | 100 | 99 | 97 | 96 | 9.3 | 93 | 92 | 91 | 89 | 88 | 87 | 86 | 84 | 83 | 82 |
| 4 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 89 | 58 | 87 | 86 | 85 | 83 | 82 |
| 5 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 90 | 88 | 87 | 86 | 8.5 | 83 | 82 |
| 6 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 90 | 88 | 87 | 86 | 85 | 84 | 82 |
| 7 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 90 | 89 | 87 | 86 | 85 | 84 | 83 |
| 8 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 90 | 89 | 87 | 86 | 85 | 84 | 83 |
| 9 | 100 | 99 | 97 | 96 | 95 | 94 | 92 | 91 | 90 | 59 | 87 | 86 | 85 | 84 | 53 |
| 10 | 100 | 99 | 97 | 96 | 95 | 94 | 92 | 91 | 90 | 89 | S7 | 86 | 85 | 84 | 83 |
| 11 | 100 | 99 | 97 | 96 | 9.) | 94 | 92 | 91 | 90 | 89 | 87 | 86 | 85 | 84 | 83 |
| 12 | 100 | 99 | 97 | 96 | 93 | 94 | 92 | 91 | 90 | 89 | 88 | 87 | 85 | 84 | 83 |
| 13 | 100 | 99 | 97 | 96 | 95 | 94 | 92 | 91 | 90 | 59 | 88 | 87 | 85 | 84 | 83 |
| 14 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 91 | 90 | 89 | 88 | 87 | 86 | 84 | 83 |
| 15 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 91 | 90 | s9 | 88 | 87 | 86 | 84 | 83 |
| 16 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 91 | 90 | 89 | 88 | 87 | 86 | 85 | 84 |
| 17 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 91 | 90 | S9 | 88 | 87 | 86 | 85 | 84 |
| 18 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 92 | 90 | S9 | 88 | S7 | 86 | 85 | 84 |
| 19 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 92 | 91 | 89 | 88 | 87 | 86 | 85 | 84 |
| 20 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 92 | 91 | 89 | 88 | 87 | 86 | 8.5 | 84 |
| 21 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 92 | 91 | 90 | 88 | 87 | 86 | 85 | 84 |
| 22 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 92 | 91 | 90 | 89 | 87 | 86 | 85 | 84 |
| 23 | 100 | 99 | 98 | 96 | 95 | 94 | 93 | 92 | 91 | 90 | 89 | S8 | 86 | 83 | 84 |
| 24 | 100 | 99 | 98 | 97 | 95 | 94 | 93 | 92 | 91 | 90 | S9 | S8 | 87 | 85 | S4 |
| 2.5 | 100 | 99 | 98 | 97 | 95 | 94 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | 86 | 85 |
| 26 | 100 | 99 | 98 | 97 | 95 | 94 | 93 | 92 | 91 | 90 | 89 | S8 | 87 | 86 | 8.5 |
| 27 | 100 | 99 | 98 | 97 | 9.5 | 94 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | S6 | 8.5 |
| 28 | 100 | 99 | 98 | 97 | 95 | 94 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | 86 | 8.5 |
| 29 | 100 | 99 | 98 | 97 | 96 | 94 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | 86 | 8.) |
| 30 | 100 | 99 | 98 | 97 | 96 | 94 | 93 | 92 | 91 | 90 | S9 | 88 | 87 | 86 | 85 |
| 31 | 100 | 99 | 98 | 97 | 96 | 94 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | 86 | 85 |
| 32 | 100 | 99 | 98 | 97 | 96 | 94 | 93 | 92 | 91 | 90 | S9 | 88 | 87 | 86 | 85 |
| 33 | 100 | 99 | 98 | 97 | 96 | 94 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | 86 | 85 |
| 34 | 100 | 99 | 98 | 97 | 96 | 95 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | S6 | 85 |
| 3.5 | 100 | 99 | 98 | 97 | 96 | 95 | 93 | 92 | 91 | 90 | 89 | 88 | 87 | 86 | 85 |


| Temper ature of $t=$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $3{ }^{\circ} .0$ | 30. 2 | 3.4 | 30.6 | 30.8 | $4^{\circ} .0$ | $4^{\circ} .2$ | $4^{\circ} .4$ | $4^{\circ} .6$ | $4^{\circ} .8$ | $5^{\circ} .0$ | $5^{\circ} .2$ | $5{ }^{\circ} .4$ | $5^{\circ} .6$ | $5^{\circ} .8$ |
| Centig. | 78 | 77 | 75 | 74 | 73 | 72 | 71 | 69 | 68 | 67 | 66 | 65 | 64 | 63 | 62 |
| -7 | 78 | 77 | 75 | 74 | 73 | 72 | 71 | 69 | 68 | 67 | 66 | 65 | 64 | 63 | 62 |
| -6 | 78 | 77 | 76 | 74 | 73 | 72 | 71 | 69 | 68 | 67 | 66 | 65 | 64 | 63 | 62 |
| -5 | 79 | 77 | 76 | 75 | 73 | 72 | 71 | 70 | 68 | 67 | 66 | 65 | 64 | 63 | 62 |
| -4 | 79 | 77 | 76 | 75 | 74 | 73 | 71 | 70 | 69 | 68 | 67 | 66 | 64 | 63 | 62 |
| -3 | 79 | 77 | 76 | 75 | 74 | 73 | 72 | 70 | 69 | 68 | 67 | 66 | 65 | 64 | 63 |
| -2 | 79 | 78 | 77 | 76 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 66 | 65 | 64 | 63 |
| -1 | 79 | 78 | 77 | 76 | 75 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 | 64 |
| 0 | 80 | 78 | 77 | 76 | 75 | 74 | 73 | 71 | 70 | 69 | 68 | 67 | 66 | 65 | 6. |
| +1 | 80 | 79 | 78 | 77 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 66 | 65 | 64 |
| 2 | 81 | 79 | 78 | 77 | 76 | 75 | 74 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 |
| 3 | 81 | 80 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 66 | 65 |
| 4 | 81 | 80 | 79 | 78 | 77 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 |
| 5 | S1 | 80 | 79 | 78 | 77 | 76 | 75 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 |
| 6 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 |
| 7 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 |
|  | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 |
| 8 | 82 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 |
| 10 | 82 | 81 | 80 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 |
| 11 | 82 | 81 | 80 | 79 | 78 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 70 | 69 | 68 |
| 12 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 |
| 13 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 |
| 14 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 |
| 15 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 |
| 16 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 71 | 70 | 69 |
| 17 | 83 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 73 | 72 | 71 | 70 | 69 |
| 18 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 |
| 19 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 |
| 20 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 |
| 21 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 70 |
| 22 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 73 | 72 | 71 | 70 |
| 23 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 74 | 73 | 72 | 71 | 70 |
| 24 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 |
| 25 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 |
| 26 | 84 | 83 | 82 | 81 | 50 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 |
| 27 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 |
| 28 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 |
| 29 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 75 | 74 | 73 | 72 | 71 |
| 30 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 76 | 75 | 74 | 73 | 72 | 71 |
| 31 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 77 | 76 | 75 | 74 | 73 | 72 | 71 |
| 32 | 84 | 83 | 82 | 81 | 80 | 79 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 72 |
| 33 | 84 | 83 | 82 | 81 | 80 | so | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 72 |
| 34 | 85 | 84 | 83 | 52 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 74 | 74 | 73 | 72 |
| 35 | 85 | 84 | 83 | 82 | 81 | 80 | 79 | 78 | 77 | 76 | 75 | 75 | 74 | 73 | 72 |


| Teniper-ature ofthe air.$\mathbf{t}=-$ | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Dew Point and of the Air. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $6^{\circ} 0$ | $6^{\circ} .2$ | $6^{\circ} .4$ | $0^{\circ} .6$ | $6^{\circ} .8$ | $7{ }^{\circ} .0$ | $7{ }^{\circ} .2$ | $7^{\circ} .4$ | $7^{\circ} .6$ | $7^{\circ} .8$ | $8^{\circ} .0$ | $8^{\circ} .2$ | $8^{\circ} .4$ | $8^{\circ} .6$ | $8^{\circ} .8$ |
| Centig. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -6 | 61 | 60 | 59 | 58 | 57 | 56 |  |  |  |  |  |  |  |  |  |
| -5 | 61 | 60 | 59 | 58 | 58 | 57 | 56 | 55 | 54 | 53 | 52 |  |  |  |  |
| -4 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 53 | 52 |  |  |  |  |
| -3 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 53 | 53 | 52 | 51 | 50 | 49 |
| -2 | 62 | 61 | 60 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 53 | 52 | 51 | 50 | 49 |
| -1 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 53 | 52 | 51 | 50 | 49 |
| 0 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 53 | 53 | 52 | 51 | 50 |
| +1 | 63 | 62 | 61 | 61 | 60 | 58 | 58 | 57 | 56 | 55 | 54 | 53 | 52 | 51 | 51 |
| 2 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 55 | 55 | 54 | 53 | 52 | 51 |
| 3 | 64 | 63 | 62 | 62 | 60 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 53 | 53 | 52 |
| 4 | 65 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 56 | 55 | 54 | 53 | 52 |
| 5 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 55 | 54 | 54 | 53 |
| 6 | 66 | 65 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 57 | 56 | 55 | 54 | 53 |
| 7 | 66 | 65 | 64 | 63 | 62 | 61 | 60 | 60 | 59 | 58 | 57 | 56 | 55 | 55 | 54 |
| 8 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 | 58 | 57 | 56 | 56 | 55 | 54 |
| 9 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 58 | 57 | 56 | 55 | 54 |
| 10 | 67 | 66 | 65 | 64 | 63 | 62 | 61 | 60 | 59 | 59 | 58 | 57 | 56 | 55 | 55 |
| 11 | 67 | 66 | 65 | 64 | 63 | 62 | 61 | 61 | 60 | 59 | 58 | 57 | 56 | 56 | 55 |
| 12 | 67 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 | 58 | 57 | 57 | 56 | 55 |
| 13 | 67 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 60 | 59 | 59 | 58 | 57 | 56 | 55 |
| 14 | 67 | 66 | 66 | 65 | 64 | 63 | 62 | 61 | 60 | 60 | 59 | 58 | 57 | 56 | 56 |
| 15 | 67 | 67 | 66 | 65 | 64 | 63 | 62 | 61 | 61 | 60 | 59 | 58 | 57 | 57 | 56 |
| 16 | 68 | 67 | 66 | 65 | 64 | 63 | 63 | 62 | 61 | 60 | 59 | 58 | 58 | 57 | 56 |
| 17 | 68 | 67 | 66 | 65 | 64 | 6. | 63 | 62 | 61 | 60 | 59 | 59 | 58 | 57 | 56 |
| 18 | 68 | 67 | 66 | 65 | 65 | 64 | 63 | 62 | 61 | 60 | 60 | 59 | 58 | 57 | 57 |
| 19 | 68 | 67 | 67 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 | 58 | 58 | 57 |
| 20 | 68 | 68 | 67 | 66 | 65 | 64 | 63 | 63 | 62 | 61 | 60 | 59 | 59 | 58 | 57 |
| 21 | 69 | 68 | 67 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 60 | 60 | 59 | 58 | 57 |
| 22 | 69 | 68 | 67 | 66 | 65 | 65 | 64 | 63 | 62 | 61 | 61 | 60 | 59 | 58 | 58 |
| 23 | 69 | 68 | 67 | 67 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 | 59 | 58 |
| 24 | 69 | 68 | 68 | 67 | 66 | 65 | 64 | 63 | 63 | 62 | 61 | 60 | 60 | 59 | 58 |
| 23 | 69 | 69 | 68 | 67 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 61 | 60 | 59 | 58 |
| 26 | 70 | 69 | 68 | 67 | 66 | 65 | 65 | 64 | 63 | 62 | 61 | 61 | 60 | 59 | 58 |
| 27 | 70 | 69 | 68 | 67 | 66 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 | 59 |
| 28 | 70 | 69 | 68 | 67 | 67 | 66 | 65 | 6. | 63 | 63 | 62 | 61 | 60 | 60 | 59 |
| 29 | 70 | 69 | 69 | 68 | 67 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 61 | 60 | 59 |
| 30 | 70 | 69 | 69 | 68 | 67 | 66 | 65 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 59 |
| 31 | 70 | 70 | 69 | 68 | 67 | 66 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 | 60 |
| 32 | 71 | 70 | 69 | 68 | 67 | 67 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 61 | 60 |
| 33 | 71 | 70 | 69 | 68 | 68 | 67 | 66 | 65 | 64 | 64 | 63 | 62 | 61 | 61 | 60 |
| 34 | 71 | 70 | 69 | 69 | 68 | 67 | 66 | 66 | 65 | 64 | 63 | 62 | 62 | 61 | 60 |
| 35 | 71 | 70 | 70 | 69 | 68 | 67 | 66 | 66 | 65 | 64 | 63 | 63 | 62 | 61 | 60 |


| 「emper athre of the alt. $\mathbf{t}=$ | ference of Cemperatures of the Dew P |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $9{ }^{\circ} .0$ | $9^{\circ} .9$ | $9^{\circ} .4$ | $9^{\circ}, 6$ | $9 \times .8$ | $10^{\circ} .0$ | $10^{\circ} .2$ | $10^{\circ} .4$ | $10^{\circ} .6$ | $10^{\circ} .8$ | $11^{\circ} .0$ | $11^{\circ} .2$ | $11^{\circ} .4$ | $11^{\circ} .6$ | $11^{c} .8$ |
| Centig. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $-7$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -. 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| +1 | 50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | 50 | 19 | 49 | 48 | 47 | 46 |  |  |  |  |  |  |  |  |  |
| 3 | 51 | 50 | 49 | 48 | 48 | 47 | 46 | 45 | 45 | 44 | 43 |  |  |  |  |
| 4 | 51 | 51 | 50 | 49 | 48 | 47 | 47 | 46 | 45 | 44 | 44 | 43 | 42 | 42 | 41 |
| 5 | 52 | 51 | 50 | 49 | 49 | 48 | 47 | 46 | 46 | 45 | 44 | 13 | 43 | 42 | 41 |
| 6 | 52 | 52 | 51 | 50 | 49 | 48 | 48 | 47 | 46 | 45 | 45 | 44 | 43 | 43 | 42 |
| 7 | 53 | 52 | 51 | 51 | 50 | 49 | 48 | 47 | 47 | 46 | 45 | 45 | 44 | 43 | 42 |
| S | 53 | 52 | 52 | 51 | 50 | 49 | 49 | 48 | 47 | 46 | 46 | 45 | 44 | 44 | 43 |
| 9 | 54 | 53 | 52 | 51 | 50 | 50 | 49 | 48 | 48 | 47 | 46 | 45 | 45 | 44 | 43 |
| 10 | 54 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 47 | 47 | 46 | 45 | 44 | 44 |
| 11 | 54 | 53 | 53 | 52 | 51 | 50 | 50 | 49 | 48 | 48 | 47 | 46 | 46 | 45 | 44 |
| 12 | 54 | 54 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 47 | 47 | 46 | 45 | 45 |
| 13 | 55 | 54 | 53 | 52 | 52 | 51 | 50 | 50 | 49 | 48 | 47 | 47 | 46 | 46 | 45 |
| 14 | 55 | 54 | 53 | 53 | 52 | 51 | 50 | 50 | 49 | 45 | 48 | 47 | 46 | 46 | 45 |
| 15 | 55 | 54 | 54 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 47 | 47 | 46 | 45 |
| 16 | 55 | 55 | 54 | 53 | 52 | 52 | 51 | 50 | 50 | 49 | 48 | 48 | 47 | 46 | 46 |
| 17 | 56 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 47 | 47 | 46 |
| 18 | 56 | 5.5 | 54 | 54 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 47 | 47 | 46 |
| 19 | 56 | 55 | 55 | 54 | 53 | 52 | 52 | 51 | 50 | 50 | 49 | 48 | 48 | 47 | 47 |
| 20 | 56 | 56 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 47 | 47 |
| 21 | 57 | 56 | 55 | 54 | 54 | 53 | 52 | 52 | . 51 | 50 | 50 | 49 | 48 | 48 | 47 |
| 22 | 57 | 56 | 55 | 55 | 54 | 53 | 53 | 52 | 51 | 50 | 50 | 49 | 49 | 48 | 47 |
| 23 | 57 | 56 | 56 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 | 48 |
| 2.1 | 57 | 57 | 56 | 5.5 | 54 | 5.4 | 53 | 52 | 52 | 51 | 50 | 50 | 49 | 48 | 48 |
| 25 | 58 | 57 | 56 | 55 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 49 | 49 | 48 |
| 26 | 58 | 57 | 56 | 56 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 50 | 49 | 48 |
| 27 | 58 | 57 | 56 | 56 | 55 | 54 | 54 | 53 | 52 | 52 | 51 | 50 | 50 | 49 | 48 |
| 28 | 58 | 57 | 57 | 56 | 55 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 49 | 49 |
| 29 | 58 | 58 | 57 | 56 | 56 | 35 | 54 | 5:3 | 53 | 52 | 52 | 51 | 50 | 50 | 49 |
| 30 | 59 | 58 | 57 | 57 | 56 | 55 | 54 | 54 | 53 | 52 | 52 | 51 | 51 | 50 | 49 |
| 31 | 59 | 58 | 57 | 57 | 56 | 55 | 55 | 54 | 53 | 53 | 52 | 51 | 51 | 50 | 49 |
| 32 | 59 | 58 | 58 | 57 | 56 | 56 | 55 | 54 | 54 | 53 | 52 | 52 | 51 | 50 | 50 |
| 33 | 59 | 59 | 58 | 57 | 56 | 56 | 55 | 54 | 54 | 53 | 52 | 52 | 51 | 51 | 50 |
| 34 | 60 | 59 | 58 | 57 | 57 | 56 | 55 | 55 | 54 | 53 | 53 | 52 | 52 | 51 | 50 |
| 35 | 60 | 59 | 58 | 58 | 57 | 56 | 56 | 55 | 54 | 54 | 53 | 52 | 52 | 51 | 50 |



## TABLE IV.

```
FACTOR ['00, FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE. OF THE AIR FROM ITS ABSOLUTE HUMIDITY, GIVEN IN MILLIMETRES.
```

By HAEGIIENS.
The Relative Humidity, or the degree of moisture of the air, is the ratio of the quantity of vapor contained in the air to the quantity it could contain at the tem. perature observed, if fully saturated.

If we call
The force of vapor contained in the air $=f$,
The maximum of the force of vapor at the temperature of the air $=\mathrm{F}$,
The point of saturation $=100$,
we have the proportion,
Relative Humidity : $100:: f: \mathrm{F}$,
and

$$
\underset{\mathbf{F}}{f \times 100}=\text { Relative Humidity in Hundredths. }
$$

But as $\underset{F}{f \times 100}=f \times \underset{F}{100}$, it is obvious that the operation indicated by the former expression, viz. $\stackrel{f \times{ }_{F} 100}{ }$, would be reduced to a simple multiplication, if we had a table of the factors ${ }_{F}^{100}$. Such a table is obtained by dividing the constant number 100 by each number in the Table of Elastic Forees of Vapor, and substituting the quotients to the tensions.

The following Table, taken from the Annuaire Météorologique de la France, for 1850, p. 79, gives the factor ${ }_{F}^{100}$ for every tenth of a degree from - 10 to $+35^{\circ}$ Centigrade, corresponding to the Forces of Vapor in Table I.

## Use of the Table.

The force of vapor contained in the air being given in millimetres, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation ; the result will be the Relative Humidity in Hundredths.

## Examples.

1. Suppose the temperature of the air to be $=24^{\circ}$ Centigrade.
" " force of vapor in the air to be $=\mathbf{1 0 . 7 6}$ millimetres.
Opposite $24^{\circ}$ is found in the table the factor 4.51 .
Then $\quad 10.76 \times 4.51=48.5$, Relative Humidity in Hundredths.
2. Suppose the temperature of the air to be $=16.7$.
" " force of vapor in the air to be $=1 \longleftrightarrow .07$.
Table gives for 16.7 the factor 7.07 .
Then $\quad 1: .07 \times 7.07=85.3$, Relative Humidity.
B

| $\mathbf{t}=$ <br> Temp. of Air, Centig. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | s. | 9. |
| $\begin{array}{r} 0 \\ -10 \end{array}$ | 48.1 | 48.5 | 48.9 | 49.3 | 49.7 | 50.1 | 50.5 | 50.9 | 51.4 | 51.8 |
| 9 | 44.2 | 44.6 | 45.0 | 45.4 | 45.7 | 46.1 | 46.5 | 46.9 | 47.3 | 47.7 |
| 8 | 40.7 | 41.1 | 41.4 | 41.7 | 42.1 | +2.4 | 42.8 | 43.1 | 43.5 | 43.9 |
| 7 | 37.5 | 37.8 | 38.1 | 38.4 | 38.7 | 39.0 | 39.4 | 39.7 | 40.0 | 40.4 |
| 6 | 34.6 | 34.9 | 35.2 | 35.4 | 35.7 | 36.0 | 36.3 | 36.6 | 36.9 | 37.2 |
| 5 | 31.9 | 32.2 | 32.4 | 32.7 | 33.0 | 33.2 | 33.5 | 33.8 | 34.0 | 31.3 |
| 4 | 29.5 | 29.8 | 30.0 | 30.2 | 30.5 | 30.7 | 31.0 | 31.2 | 31.4 | 31.7 |
| 3 | 27.3 | 27.5 | 27.7 | 27.9 | 28.2 | 28.4 | 28.6 | 28.8 | 29.1 | 29.3 |
| 2 | 2.5 .3 | 25.5 | 25.7 | 2.7 .9 | 26.1 | 26.3 | 26.5 | 26.7 | 26.9 | 27.1 |
| 1 | 23.4 | 23.6 | 23.8 | 24.2 | 24.0 | 24.3 | 24.5 | 24.7 | 24.9 | 25.1 |
| -0 | 21.7 | 21.9 | 22.1 | 22.2 | 22.4 | 22.6 | 22.8 | 22.9 | 23.1 | 23.3 |
| +0 | 21.7 | 21.6 | 21.4 | 21.3 | 21.1 | 21.0 | 20.8 | 20.7 | 20.5 | 20.4 |
| 1 | 20.2 | 20.1 | 20.0 | 19.8 | 19.7 | 19.5 | 19.4 | 19.3 | 19.1 | 19.0 |
| 2 | 18.9 | 18.7 | 18.6 | 18.5 | 18.3 | 18.2 | 18.1 | 18.0 | 17.8 | 17.7 |
| 3 | 17.6 | 17.5 | 17.3 | 17.2 | 17.1 | 17.0 | 16.9 | 16.7 | 16.6 | 16.5 |
| 4 | 16.4 | 16.3 | 16.2 | 16.1 | 15.9 | 15.8 | 15.7 | 15.6 | 15.5 | 15.4 |
| 5 | 15.3 | 15.2 | 15.1 | 1.9 .0 | 14.9 | 14.8 | 14.7 | 14.6 | 14.5 | 14.4 |
| 6 | 14.3 | 14.2 | 14.1 | 14.0 | 13.9 | 13.8 | 13.7 | 13.6 | 13.5 | 13.4 |
| 7 | 13.4 | 13.3 | 13.2 | 13.1 | 13.0 | 13.9 | 12.8 | 12.7 | 12.6 | 12.6 |
| 8 | 12.5 | 12.4 | 12.3 | 12.2 | 12.1 | 12.1 | 12.0 | 11.9 | 11.8 | 11.7 |
| 9 | 11.7 | 11.6 | 11.5 | 11.4 | 11.4 | 11.3 | 11.2 | 11.1 | 11.1 | 11.0 |
| 10 | 10.9 | 10.8 | 10.8 | 10.7 | 10.6 | 10.6 | 10.5 | 10.4 | 10.3 | 10.3 |
| 11 | 10.2 | 10.1 | 10.1 | 10.0 | 9.95 | 9.88 | 9.82 | 9.75 | 9.69 | 9.63 |
| 12 | 9.56 | 9.50 | 9.44 | 9.38 | 9.32 | 9.26 | 9.20 | 9.13 | 9.08 | 9.02 |
| 13 | 8.96 | 8.90 | 8.84 | 8.79 | 8.73 | 8.67 | 8.62 | 8.56 | 8.51 | 8.45 |
| 14 | 8.40 | 8.34 | 8.29 | 8.24 | 8.18 | 8.15 | 8.08 | 8.03 | 7.98 | 7.92 |
| 15 | 7.87 | 7.82 | 7.77 | 7.72 | 7.63 | 7.63 | 7.58 | 7.53 | 7.18 | 7.43 |
| 16 | 7.39 | 7.34 | 7.29 | 7.25 | 7.20 | 7.16 | 7.11 | 7.07 | 7.02 | 6.98 |
| 17 | 6.93 | 6.89 | 6.85 | 6.80 | 6.76 | 6.72 | 6.68 | 6.63 | 6.59 | 6.55 |
| 18 | 6.51 | 6.47 | 6.43 | 6.39 | 6.35 | 6.31 | 6.27 | 6.23 | 6.19 | 6.16 |
| 19 | 6.12 | 6.03 | 6.04 | 6.00 | 5.97 | 5.93 | 5.89 | 5.86 | 5.82 | 5.79 |
| 20 | 5.75 | 5.71 | 5.68 | 5.64 | 5.61 | 5.58 | 5.54 | 5.51 | 5.47 | 5.44 |
| 21 | 5.41 | 5.37 | 5.34 | 5.31 | 5.27 | 5.24 | 5.21 | 5.18 | 5.15 | 5.12 |
| 22 | 5.09 | 5.06 | 5.02 | 4.99 | 4.96 | 4.93 | 4.90 | 4.87 | 4.85 | 4.82 |
| 23 | 4.79 | 4.76 | 4.73 | 4.70 | 4.67 | 4.65 | 4.62 | 4.59 | 4.56 | 4.53 |
| 24 | 4.51 | 4.48 | 4.45 | 4.43 | 4.40 | 4.37 | 4.35 | 4.32 | 4.30 | 4.27 |
| 25 | 4.25 | 4.22 | 4.20 | 4.17 | 4.15 | 4.12 | 4.10 | 4.07 | 4.05 | 4.03 |
| 26 | 4.00 | 3.98 | 3.9 .5 | 3.93 | 3.91 | 3.89 | 3.86 | 3.84 | 3.82 | 3.79 |
| 27 | 3.77 | 3.75 | 3.73 | 3.71 | 3.69 | 3.66 | 3.64 | 3.62 | 3.60 | 3.58 |
| 28 | 3.56 | 3.54 | 3.52 | $3 . \% 0$ | 3.18 | 3.46 | 3.44 | 3.12 | 3.40 | 3.38 |
| 29 | 3.36 | 3.34 | 3.32 | 3.30 | 3.28 | 3.26 | 3.24 | 3.22 | 3.21 | 3.19 |
| 30 | 3.17 | 3.15 | 3.13 | 3.12 | 3.10 | 3.08 | 3.06 | 3.05 | 3.03 | 3.01 |
| 31 | 2.99 | 2.98 | 2.96 | 2.94 | 2.93 | 2.91 | 2.89 | 2.88 | 2.86 | 2.84 |
| 32 | 2.83 | 2.81 | 2.80 | 2.78 | 2.77 | 2.75 | 2.73 | 2.72 | 2.70 | 2.69 |
| 33 | 2.67 | 2.66 | 2.64 | 2.63 | 2.61 | 2.60 | 2.58 | 2.57 | 2.56 | 2.54 |
| 34 | 2.53 | 2.51 | 2.50 | 2.49 | 2.47 | 2.16 | 2.44 | 2.43 | 2.42 | 2.40 |
| 35 | 2.39 | 2.39 | 2.36 | 2.35 | 2.34 | 2.33 | 2.31 | 2.30 | 2.29 | 2.28 |

TABLE V.

WEIGHT OF VAPOR, IN GRAMMES,

CONTAINED IN A CUBIC METRE OF SATCRATED AIR UNDER A BAROMETRIC PRESSURE OF 760 MILLIMETRES, AND AT TEMPERATURES BETWEEN - $20^{\circ}$ AND $+40^{\circ}$ CENTIGRADE.

The theoretic density of aqueous vapor is very nearly 0.622 , or $\frac{5}{8}$, of the density of the air at the same temperature and pressure. Regnault's experiments gatve similar results. From this ratio the weight of the vapor contained in a given volume of air, the temperature and humidity of which are known, can be computed.

If we call
$t=$ the temperature of the air;
$f=$ the elastic force of the vapor contained in the air at the time of the observation; $F=$ the maximum elastic force of vapor due to the temperature $t$, as given in the table;
$p=$ the weight of the vapor contained in a litre of air at the temperature $t$, and with a force of vapor $f$;
$P=$ the weight of vapor in a litre of air at the temperature $t$, and at full saturation, or $F$.

Then,

$$
p=0.622 \underset{1+0.0036 \bar{z} t}{1+29323 \mathrm{gr}} \cdot \stackrel{f}{1+60^{\mathrm{mmu}} \cdot}
$$

In which 1.293223 grammes is the weight of a litre of dry air, at the temperature of zero Centigrade, and under a barometric pressure of 760 millimetres, according to the determination of Regnault ; 0.00367 , the coefficient of the expansion of the air as foum by the same; 760 millimetres, the assumed normal burometric pressure.

The weight of a litre of air given by Reguault in the Mémoires de l'Institut, Tom. XXI. p. 157 , is 1.293187 grammes; but by correcting a slight error of computation (sce E. Ritter, Mémoires de la Société Physique de Genève, Tom. XIII. p. 361), it becomes, as given above, 1.293293 grammes.

In order to obtain the weight of vapor in a cubic metre, or 1000 litres, of saturated air, the formula becomes,

$$
P=0.622 \frac{1293.223^{3 r}}{1+0.00367 t} \cdot \frac{F}{760^{\text {min. }}} .
$$

From this formula Table V. has been computed. The tensions due to the temperatures in the first column are placed opposite the weights of vapor; they are taken from Table 1. It will be seen that, thronghout the table, the number of grammes of vapor nearly corresponds to the number of millimetres of pressure expressing the temsion.

The table of the weights of vapor given in Pouillet's Eléments des Physique, Tom. II. p. 707 , being based on older values, gives results somewhat different. In that published by Becquerel, Eléments de Physique Terrestre, p. 354, Regnault's tensions and coefficient of expansion of the air have been used, but the value of the weight of vapor in a litre of air formerly determined by Biot and Arago, viz. 1.29954 grammes, has been retained.
V. WEIGHT OF VAPOR, IN GRAMMES,

Contained in a cubic metre of saturated air,

At Temperatures between $-2^{\prime} \mathrm{JO}$ and +400 Centigrade.

| $\begin{gathered} \text { Temperature } \\ \text { of } \\ \text { Dew-Point. } \end{gathered}$ | Force of Vapor. | Weight ot Vapor. | Difference. | Temperature of Dew-Point. | Force of Vapor. | Weight ot Vapor. | Difference. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Centigrade. | Millimetres. | Grammes. | Grammes. | Centigrade. | Millimetres. | Grammes. | Grammes. |
| $-20^{\circ}$ | 0.912 | 1.042 | 0.088 | $+10^{\circ}$ | 9.165 | 9.357 |  |
| $-19$ | 0.993 | 1.130 | 0.088 | 11 | 9.792 | $9.96{ }^{\circ}$ | 0.603 |
| -18 | 1.050 | 1.224 | 0.094 | 12 | 10.457 | 10.601 | 0.639 |
| -17 | 1.174 | 1.325 | 0.101 | 13 | 11.162 | 11.276 | 0.625 |
| -16 | 1.275 | 1.434 | 0.109 | 14 | 11.908 | 11.988 | 0.712 |
| -15 | 1.385 | 1.551 | 0.118 | 15 | 12.699 | 12.739 | 0.751 |
|  |  | 1.551 | 0.127 |  |  | 12.789 | 0.793 |
| -14 | 1.503 | 1.678 | 0.134 | 16 | 13.536 | 13.532 | 0.835 |
| -13 | 1.631 | 1.813 | 0.134 | 17 | 14.421 | 14.367 | 0.805 |
| -12 | 1.768 | 1.957 | 0.145 | 18 | 15.357 | 15.247 | . 880 |
| -11 | 1.918 | 2.114 | 0.157 | 19 | 16.316 | 16.173 | 0.926 |
| -10 | 2.078 | 2.283 | 0.169 | 20 | 17.391 | 17.148 | 0.975 |
| $-9$ | 2.261 | 2.475 | 0.192 | 21 | 18.495 | 18.171 | 1.026 |
|  |  |  | 0.203 |  |  | 18.171 | 1.078 |
| -8 | 2.456 | 2.678 | 0.218 | 22 | 19.6 .59 | 19.253 | 1.134 |
| $-7$ | 2.666 | 2.896 | 0.218 | 23 | 20.888 | 20.387 | 1.134 |
| $-6$ | 2.890 | 3.128 | 0.232 | 24 | 22.184 | 21.579 | 1.192 |
| $-5$ | 3.131 | 3.376 | 0.248 | 25 | 23.550 | 22.831 | 1.252 |
|  | 3.387 |  | 0.262 | 26 |  |  | 1.313 |
| -4 | 3.387 | 3.638 | 0.281 | 26 | 24.988 | 24.144 | 1.380 |
| $-3$ | 3.662 | 3.919 | 0.281 | 27 | 26.505 | 25.524 | 1.380 |
| $-2$ | 3.955 | 4.217 | 0.298 | 28 | 28.101 | 26.971 | 1.447 |
| $-1$ | 4.267 | 4.534 | 0.317 | 29 | 29.752 | 28.489 | 1.019 |
| 0 | 4.600 | 4.869 | 0.334 | 30 |  |  | 1.589 |
| +1 |  |  | 0.341 |  |  |  | 1.666 |
| +1 | 4.940 | 5.209 | 0.361 | 31 | 33.405 | 31.744 | $1.74{ }^{\circ}$ |
| 2 | 5.302 | 5.571 | 0.361 | 32 | 35.359 | 33.491 | 1.74 |
| 3 | 5.687 | 5.953 | 0.383 | 33 | 37.410 | 35.317 | 1.827 |
| 4 | 6.097 | 6.360 | 0.406 | 34 | 39.565 | 37.230 | 1.913 |
| 5 | 6.534 | 6.791 | 0.431 | 35 | 41.827 | 39.231 | 2.001 |
| 6 | 6.998 | 7.247 | 0.456 | 36 |  | 11.393 | 2.092 |
| 6 | 6.958 | 7.247 | 0.484 |  | 4.201 | 41.323 | 2.187 |
| 7 | 7.492 | 7.731 | 0.484 | 37 | 46.691 | 43.510 | 2.184 |
| 8 | 8.017 | 8.243 | 0.512 | 38 | 49.302 | 45.795 | 2.285 |
| 9 | 8.574 | 8.785 | 0.54 | 39 | 52.039 | 48.182 | 2.387 |
| $+10$ | 9.165 | 9.357 | 0.572 | $+40$ | 54.906 | 50.674 | 2.492 |

# PRACTICALTABLES, 

IN

ENGLISH MEASURES,

BASED ON REGNAULT'S HYGROMETRICAL CONSTANTS.

## V I.

## TABLE OF THE ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, REDUCED FROM REGNAULT'S TABLE.

The values of the elastic force of vapor furnished by V. Regnault, which are found in Table I. of this Hygrometrical set, are derived from a series of experiments conducted, during several years, with great care, consummate skill, and all the means of prectsion which are at the disposal of modern science. The methods of investigation, and all the steps in each experiment, were minntely described and submitted to the judgment of the scientific, successively in separate papers in several volumes of the Annales de Chimie et de Physique, and collectively in his final Report to the Minister of Public Works, (see above, p. 9,) which fills Volume XXI. of the Mémoires de l'Institut de France. The confidence which has been deservedly granted to these determinations by nearly all scientific men, is increased by the fact that one of the best physicists and experimenters in Germany, Professor Maguus, came, about the same time, to results so little different, that both tables, for most purposes, may be cousitered identical. (Compare below, Table XXII.) It seems, therefore, that these values ought to be used in our hygrometrical tables, as has been done in France, in preference to the older and less reliable determinations on which they are baserl.

Though Regnault's table of the elastic force of vapor is considered, even, it is believed, by a majority of scientific men in Englant, as the most reliable which seience now porsesses, the author is not aware that any extensive reduction of it to English measures, such as is wanted for meteorological purposes, has been as yet published; still less a series of tables based on these values. Such a set of hygrometrical tables in English measures, corresponding to the preceding one in French measures, is offered here, which, it is hoped, supplies a real want felt by a large number of meteorologists.

Tible VI. is Regnault's Table of the Elastic Force of Vapor as given in Table I., rednced to English measures, in which the fourth decimal is given in order to secure the third, and otherwise to facilitate the computations. From these values Tables VII. to X. have been computed.
VI. ELASTIC FORCE OF AQUEOUS VAPOR,

Expressed in English Inches of Mercury for Temperatcres of Falirenheit.

Reduced from Regnault's Table.


Expressed in English Inches of Mercury for Temperatures of Fiahenheit.

| Temperature of Fahrenheit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| - | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng In. | Eng. In. | Eng. In. |
| 32 | 0.1811 | 0.1818 | 0.1825 | 0.1833 | 0.1840 | 0.1847 | 0.1854 | 0.1861 | 0.1569 | 0.1876 |
| 33 | 0.1883 | 0.1591 | 0.1898 | 0.1906 | 0.1913 | 0.1921 | 0.1928 | 0.1936 | 0.1944 | 0.1951 |
| 34 | 0.1959 | 0.1967 | 0.1974 | 0.1982 | 0.1990 | 0.1998 | 0.2006 | 0.2013 | 0.2021 | 0.2029 |
| 35 | 0.2037 | 0.2045 | 0.2053 | 0.2061 | 0.2070 | 0.2077 | 0.2086 | 0.2094 | 0.2102 | 0.2111 |
| 36 | 0.2119 | 0.2127 | 0.2135 | 0.2144 | 0.2152 | 0.2161 | 0.2169 | 0.2178 | 0.2186 | 0.2195 |
| 37 | 0.2204 | 0.2212 | 0.2221 | 0.2230 | 0.2238 | 0.2247 | 0.2256 | 0.2265 | 0.2273 | 0.2282 |
| 38 | 0.2291 | 0.2300 | 0.2309 | 0.2318 | 0.2327 | 0.2336 | 0.2345 | 0.2354 | 0.2364 | 0.2373 |
| 39 | 0.2382 | 0.2391 | 0.2400 | 0.2410 | 0.2419 | 0.2428 | 0.2438 | 0.2447 | 0.2457 | 0.2466 |
| 40 | 0.2476 | 0.2485 | 0.2495 | 0.2504 | 0.2514 | 0.2524 | 0.2533 | 0.2543 | 0.2553 | 0.2563 |
| 41 | 0.2572 | 0.2582 | 0.2592 | 0.2602 | 0.2612 | 0.2622 | 0.2632 | 0.2642 | 0.2652 | 0.2662 |
| 42 | 0.2672 | 0.2682 | 0.2692 | 0.2702 | 0.2713 | 0.2723 | 0.2733 | 0.2744 | 0.2754 | 0.2764 |
| 43 | 0.2775 | 0.2785 | 0.2796 | 0.2807 | 0.2817 | 0.2828 | 0.2839 | 0.2850 | 0.2860 | 0.2571 |
| 44 | 0.2882 | 0.2893 | 0.2904 | 0.2915 | 0.2926 | 0.2937 | 0.2948 | 0.2960 | 0.2971 | 0.2982 |
| 45 | 0.2993 | 0.3005 | 0.3016 | 0.3028 | 0.3039 | 0.3050 | 0.3062 | 0.3074 | 0.3085 | 0.3097 |
| 46 | 0.3108 | 0.3120 | 0.3132 | 0.3144 | 0.3156 | 0.3168 | 0.3179 | 0.3191 | 0.3203 | 0.3215 |
| 47 | 0.3228 | 0.3240 | 0.3252 | 0.3264 | 0.3276 | 0.3289 | 0.3301 | 0.3313 | 0.3326 | 0.3338 |
| 48 | 0.3351 | 0.3363 | 0.3376 | 0.3388 | 0.3401 | 0.3414 | 0.3426 | 0.3439 | 0.3452 | 0.3465 |
| 49 | 0.3477 | 0.3490 | 0.3503 | 0.3516 | 0.3529 | 0.3542 | 0.3556 | 0.3569 | 0.3582 | 0.3595 |
| 50 | 0.3608 | 0.3622 | 0.3635 | 0.3648 | 0.3661 | 0.3675 | 0.3688 | 0.3702 | 0.3715 | 0.3729 |
| 51 | 0.3743 | 0.3756 | 0.3770 | 0.3784 | 0.3798 | 0.3812 | 0.3826 | 0.3840 | 0.3854 | 0.3868 |
| 52 | 0.3882 | 0.3896 | 0.3911 | 0.3925 | 0.3939 | 0.3954 | 0.3968 | 0.3983 | 0.3997 | 0.4012 |
| 53 | 0.4027 | 0.4041 | 0.4056 | 0.4071 | 0.4086 | 0.4101 | 0.4116 | 0.4131 | 0.4146 | 0.4161 |
| 54 | 0.4176 | 0.1191 | 0.4207 | 0.422: | 0.4237 | 0.4253 | 0.4268 | 0.4284 | 0.4299 | 0.4315 |
| 55 | 0.4331 | 0.4346 | 0.4362 | 0.4378 | 0.4394 | 0.4410 | 0.4426 | 0.4442 | 0.4458 | 0.4474 |
| 56 | 0.4490 | 0.4507 | 0.4523 | 0.4539 | 0.4556 | 0.4572 | 0.4589 | 0.4605 | 0.4622 | 0.4638 |
| 57 | 0.4655 | 0.4672 | 0.4689 | 0.4705 | 0.4722 | 0.4739 | 0.4756 | 0.4773 | 04791 | 0.4808 |
| 58 | 0.4825 | 0.1842 | 0.4859 | 0.1876 | 0.4894 | 0.4912 | 0.4929 | 0.4947 | 0.4964 | 0.4982 |
| 5 S | 0.5000 | 0.5017 | 0.5035 | 0.5053 | 0.5071 | 0.5089 | 0.5107 | 0.5125 | 0.5143 | 0.5161 |
| 60 | 0.5179 | 0.5198 | 0.5216 | 0.5234 | 0.5253 | 0.5271 | 0.5290 | 0.5301 | 0.5328 | 0.5546 |
| 61 | 0.5365 | 0.5384 | 0.5403 | 0.5422 | 0.5441 | 0.5461 | 0.5480 | 0.5499 | 0.5519 | 0.5538 |
| 62 | 0.5558 | 0.5577 | 0.5597 | 0.50 .17 | 0.5636 | 0.5656 | 0.5676 | 0.5696 | 0.5716 | 0.5736 |
| 63 | 0.5756 | 0.5777 | 0.5797 | 0.5817 | 0.5838 | 0.5858 | 0.5879 | 0.5899 | 0.5920 | 0.5941 |
| 64 | 0.5962 | 0.5983 | 0.6004 | 0.6025 | 0.6046 | 0.6067 | 0.6088 | 0.6109 | 0.6131 | 0.6152 |
| 65 | 0.6173 | 0.6195 | 0.6217 | 0.6238 | 0.6260 | 0.6282 | 0.6304 | 0.6325 | 0.6347 | 0.6369 |
| 66 | 0.6392 | 0.6414 | 0.6436 | 0.6458 | 0.6481 | 0.6503 | 0.6525 | 0.6548 | 06571 | 0.6593 |
| 67 | 0.6616 | 0.6639 | 0.6662 | 0.6685 | 0.6708 | 0.6731 | 0.6754 | 0.6777 | 0.6800 | 0.6824 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

Expressed in English Inches of Mercury for Temperatures of Fairenineit.

| Temperature of Fahrenheit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\bigcirc$ | Eng. In. | Eng. In. | Eug. In. | Eug. In. | E, ig. ln . | Eng. In. | Eng. In. | Eng In. | Eng. In | Eng. In. |
| 63 | 0.6547 | 0.6570 | 0.6594 | 0.6917 | 0.6911 | 0.6965 | 0.6959 | 0.701 ${ }^{\text {a }}$ | ${ }^{6} .7036$ | 0.7060 |
| 69 | 0.7054 | 0.7108 | 0.7133 | 0.7157 | 0.7181 | 0.7206 | 0.7230 | 0.725 .5 | 0.7290 | 0.7305 |
| 70 | 0.7329 | 0.73 .54 | 0.7379 | 0.740 .5 | 0.7430 | 0.7455 | 0.7480 | 0.7506 | 0.7531 | 0.7.9.7 |
| 71 | 0.7.583 | 0.7609 | 0.7631 | 0.7660 | 0.7636 | 0.7712 | 0.7539 | 0.7765 | 0.7791 | 0.7818 |
| 72 | 0.7844 | 0.7571 | 0.7597 | 0.7921 | 0.79.51 | 0.7978 | 0.5005 | 0.3032 | 0.8059 | 0.5056 |
| 73 | 0.8113 | 0.8141 | 0.8163 | 0.8196 | 0.8223 | 0.8251 | 0.9279 | 0.8307 | 0.8385 | 0.8363 |
| 71 | 0.8391 | 0.8419 | 0.8447 | 0.8476 | 0.5504 | 0.8533 | 0.8561 | 0.5590 | 0.5619 | 0.86 15 |
| 75 | 0.8676 | 0.870.5 | 0.873. | 0.8764 | 0.5793 | 0.952. | 0.5852 | 0.8881 | 0.5911 | 0.5940 |
| 76 | 0.5970 | 0.9000 | 0.9030 | 0.9060 | 0.9090 | 0.9120 | 0.9150 | 0.9180 | 0.9211 | 0.92 ll |
| 77 | 0.9272 | 0.9302 | 0.9333 | 0.936 t | 0.9395 | 0.9426 | 0.9457 | 0.9488 | 0.9519 | 0.9550 |
| 78 | 0.9582 | 0.9613 | 0.9645 | 0.9677 | 0.9709 | 0.9710 | 0.9773 | 0.9805 | 0.98 .37 | 0.9869 |
| 79 | 0.9902 | 0.9934 | 0.9967 | 1.0000 | 1.0033 | 1.0065 | 1.0099 | 1.0132 | 1.0163 | 1.0198 |
| S0 | 1.02:32 | 1.0265 | 1.0299 | 1.0332 | 1.0366 | 1.0400 | 1.0134 | 1.0163 | 1.0503 | 1.0537 |
| 81 | 1.0572 | 1.0606 | $1.06+1$ | 1.0675 | 1.0710 | 1.0745 | 1.0790 | 1.081 .5 | 1.0551 | 1.0886 |
| 82 | 1.0922 | 1.0957 | 1.0993 | 1.1028 | 1.1064 | 1.1100 | 1.1136 | 1.1172 | 1.1209 | 1.1245 |
| 83 | 1.1281 | 1.1818 | 1.185. | 1.1391 | 1.1428 | 1.1465 | 1.1502 | 1.1539 | 1.1576 | 1.1614 |
| 84 | 1.16 .51 | 1.1659 | 1.1726 | 1.1764 | 1.1502 | 1.1840 | 1.1875 | 1.1916 | 1.19 .94 | 1.1993 |
| 85 | 1.20 .11 | 1.2070 | 1.2103 | 1.2147 | 1.2186 | 1.2225 | 1.2264 | 1.2303 | 1.2342 | 1.2351 |
| 86 | 1.2421 | 1.2160 | 1.2500 | 1.2510 | 1.2 .580 | 1.2620 | 1.2660 | 1.2700 | 1.2740 | 1.2781 |
| 87 | 1.28 .1 | 1.2862 | 1.2403 | 1.2944 | 1.2985 | 1.3026 | 1.3068 | 1.3109 | 1.3151 | 1.3192 |
| 85 | 1.3234 | 1.3276 | 1.3318 | 1.3361 | 1.3403 | 1.3.445 | 1.3188 | 1.3531 | 1.3573 | 1.3616 |
| 89 | 1.3659 | 1.3703 | 1.3746 | 1.3789 | 1.3833 | 1.3877 | 1.3920 | 1.3964 | 1.4003 | 1.4053 |
| 90 | 1.4097 | 1.4141 | 1.1186 | 1.4230 | 1.4275 | 1.4320 | 1.4365 | 1.4410 | 1.1456 | 1.4501 |
| 41 | 1.4 .546 | 1.1592 | 1.4639 | 1.465 .1 | 1.1730 | 1.7756 | 1.1922 | 1.4869 | 1.491 .5 | 1.4962 |
| 92 | 1.5005 | 1.5055 | 1.5102 | 1.5149 | 1.5197 | 1.5244 | 1.5291 | 1.5339 | 1.5357 | 1.5435 |
| 93 | 1.5482 | 1.5531 | 1.5579 | 1.5627 | 1.5676 | 1.5724 | 1.5773 | $1.582 \%$ | 1.5871 | 1.5920 |
| 94 | 1.5969 | 1.6018 | 1.6068 | 1.6117 | 1.6167 | 1.6217 | 1.6267 | 1.6317 | 1.6367 | 1.6417 |
| 95 | 1.6463 | 1.6518 | 1.6569 | 1.6620 | 1.6671 | 1.6722 | 1.6773 | 1.682 .5 | 1.6876 | 1.6928 |
| 96 | 1.6980 | 1.7032 | 1.7084 | 1.7137 | 1.7189 | 1.7242 | 1.7295 | 1.7348 | 1.7401 | 1.7454 |
| 97 | 1.7505 | 1.7561 | 1.7615 | 1.7669 | 1.7723 | 1.7777 | 1.7831 | 1.7886 | 1.7940 | 1.7995 |
| 93 | 1.5050 | 1.8105 | 1.8160 | 1.8215 | 1.8271 | 1.8327 | 1.8382 | 1.8488 | 1.8494 | 1.8551 |
| 93 | 1.8607 | 1.8664 | 1.5720 | 1.8777 | 1.8834 | 1.8891 | 1.8949 | 1.9006 | 1.9064 | 1.9121 |
| 100 | 1.9179 | 1.9237 | 1.929.5 | 1.93.54 | 1.9412 | 1.9.171 | 1.9530 | 1.9789 | 1.9618 | 1.9707 |
| 101 | 1.9766 | 1.9826 | 1.9885 | 1.9945 | 2.0005 | 2.0065 | 2.0126 | 2.0186 | 2.0247 | 2.0307 |
| 102 | 2.0368 | 2.0129 | 2.0190 | 2.0.53 | 2.0613 | 2.0675 | 2.0737 | 2.0798 | 2.0861 | 2.0923 |
| 10:3 | 2.0935 | 2.1018 | 2.1110 | 2.1173 | 2.1236 | 2.1299 | 2.1362 | 2.1426 | 2.1489 | 2.1553 |
| 101 | 2.1617 | 2.1631 | 2.1745 | 2.1810 | 2.1874 | 2.1939 | 2.2004 | 2.2069 | 2.2135 | 2.2200 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

## VII.

## PSYCHROMETRICAL TAELES,

## GIVING, IN ENGLISH INEHES OF MEREURY, THE ELASTIC FORCE OF VAPOR CONTAINED

 IN THE AIR, AND ITS RELATIVE HUMIDITY IN HUNDREDTHS;DERIVED FROM TIE INDICATIONS OF THE WET AND DRY BULB THERMOMETERS, IN DEGREES OF FAHRENIIEJT.

By A. Guyot.*

M. V. Regnault, in his Etudes sur l'Hygrométrie Annales de Chimie et de Physique, $3^{\text {me }}$ série, Tom. XV. p. 199, after having discussed the theoretical bases of the psychrometric formula given by August, and modified the numerical values of some of its coefficients, adopts the formula

$$
x=f-\frac{0.480\left(t-t^{\prime}\right)}{610-t^{\prime}} h
$$

for temperatures above the freezing-point; and when the temperature of the wet thermometer is below the freezing-point, the bulb being covered with a film of ice,

$$
x=f-\frac{0.480\left(t-t^{\prime}\right)}{689-t^{\prime}} h
$$

[^2]in which
$x$ represents the force of vapor in the air at the time of the observation;
$t$, the temperature of the air in Centigrade degrees, indicated by the dry thermometer;
$t^{\prime}$, the temperature of evaporation given by the wet thermometer;
$f$, the force of vapor in a saturated air at the temperature $t^{\prime}$;
$h$, the height of the barometer.

Substituting the Fahrenheit scale for the Centigrade, the formula, for temperatures above the freezing-point, reads

$$
x=f-\frac{0.480 \times \frac{5}{9}\left(t-t^{\prime}\right)}{610-\frac{5}{9}\left(t^{\prime}-32^{\circ}\right)} h=f-\frac{0.480\left(t-t^{\prime}\right)}{1130-t^{\prime}} h ;
$$

and below the freezing-point,

$$
x=f-\frac{0.480 \times \frac{5}{9}\left(t-t^{\prime}\right)}{689-\frac{5}{9}\left(t^{\prime}-32^{\circ}\right)} h=f-\frac{0.480\left(t-t^{\prime}\right)}{1272.2-t^{\prime}} h .
$$

Making, further, $h=$ 29.7 English inches, these formulæ become

$$
x=f-\frac{0.480\left(t-t^{\prime}\right)}{1130-t^{\prime}} 29.7=f-\frac{14.256\left(t-t^{\prime}\right)}{1130-t^{\prime}},
$$

and

$$
x=f-\frac{0.480\left(t-t^{\prime}\right)}{1272.2-t^{\prime}} 29.7=f-\frac{14.256\left(t-t^{\prime}\right)}{1272.2-t^{\prime}}
$$

The mean barometric pressure for which the table has been computed, viz. 29.7 inches, is, within a small fraction, the same as that adopted in Haeghens's Tables, No. II., which is 755 millimetres $=29.725$ Eng. inches. As that slight difference in the barometric pressure cannot cause, in the most extreme cases, a difference exceeding two thousandths of an inch in the elastic forces, the results in the two tables may be considered identical.

That barometric pressure, corresponding, in our latitudes, to a mean altitude of 250 to 300 feet above the sea, is likely to suit, without requiring a correction, the largest number of meteorological stations. Should the mean height of the barometer, in consequence of the elevation of the station, much differ from that adopted in the table, a constant correction can be determined, to be applied to the numbers in the table. At the end, page 72 , will be found a table which furnishes that correction for barometric heights between 20 and 31 inches, and for values of $t-t^{\prime}$ between $2^{\circ}$ and $26^{\circ}$ Fahrenheit.

The effect of the irregular variations of the barometer at the same station can, in most cases, be neglected; for the error due to that cause will scarcely ever exceed those which may arise from the uncertainty of the very elements on which the tables are based.

## Arrangement of the Tables.

The same arrangement as is found in the Psychrometrical for the Centigrade scale has been adopted.

The first column at the left contains the indications of the wet-bulb thermometer, from - $31^{\circ}$ to $105^{\circ}$ Fahrenheit.

The second column gives the differences of the force of vapor for each tenth of a degree, between each two consecutive full degrees in the first column. It enables the observer easily to find the values for the fractions of degrees of the wet themometer.

The following double columns furnish the forces of vapor and the relative humidity corresponding to eath full degree of the wet-bulb thermometer given in the first column in the same horizontal line, and to the diflerence of the two thermometers, or $t$ - $t^{\prime}$, found at the head of each column, for every half-degree from $0^{\circ}$ to $26^{\circ} .5$. The relative bumidity, or the fraction of saturation, is given in bundredths, which is near enough for meteorological purposes ; but one decimal more has been added, though separated by a point, in order to facilitate the interpolations.

At the bottom of each page is found the mean difference, for each tenth of a degree, between the forces of vapor on the same line. It gives the means of finding the values for the intermediate differences of $t-t^{\prime}$, not found in the tables.

## Use of the Tables.

Enter the tables with the difference of the two thermometers, or $t-t$, and the temperature of the wet-bulb thermometer, given by observation.

In the column healed by the observed difference of the thermometer, $t-t$, and on the horizontal line beaded by the observed temperature of the wet thermometer, $t^{\prime}$, are found the force of vapor, and the relative bumidity corresponding to these temperatures.

For the fractions of degrees of the wet thermometer, multiply the decimal fraction by the number placed in the second column between the full degree and the next, and add the product if the temperature is above, and subtract it if it is below zero Falrenbeit.

The intermediate values of $t-t^{\prime}$ not given in the table are found by subtracting the number in the line at the bottom of the page, multiplied by the number of additional tenths, from the value given in the table. This correction, being always very small, can usually be neglected.

For the relative humidity, interpolations at sight will generally suffice.

## Examples.

1. 

$$
\begin{aligned}
& \text { Dry thermometer, } \quad t=50^{\circ} \mathrm{F} . \\
& \text { Wet thermometer, } \quad t^{\prime}=43^{\circ} \mathrm{F} . \\
& \text { Difference, or } t-t^{\prime}=7^{\circ} \mathrm{F} .
\end{aligned}
$$

Page 58, we find for $t-t^{\prime}=7^{\circ}$ in the third double column, and for $t^{\prime}=43^{\circ}$ in the first column

$$
\begin{aligned}
& \text { Force of vapor in the air }=0.186 \text { inch. } \\
& \text { Relative humidity in hundredths }=51
\end{aligned}
$$

2. 

Dry thermometer, $t=88^{\circ} .5 \mathrm{~F}$.
Wet thermometer, $t^{\prime}=76^{\circ} .3 \mathrm{~F}$.
Difference, $t-t^{\prime}=1 \gtrsim^{\circ} .2 \mathrm{~F}$.
Page 63, Table gives for $t-t^{\prime}=12$ and $t^{\prime}=76^{\circ}=0.735$ inch.
Add for fraction of $t^{\prime}=0.3, \quad 0.003 \times 3=0.009$
Subtract for fraction of $t-t^{\prime}=0^{\circ} .2, \quad .0013 \times 2=-0.003$
Force of vapor in the air $=0.741$
Relative humidity $=55$
$\qquad$
3.

Dry thermometer, $t=-4^{\circ} .5 \mathrm{~F}$.
Wet thermometer, $t^{\prime}=6^{\circ} .0 \mathrm{~F}$.
Difference, $t-t^{\prime}=1^{\circ} .5 \mathrm{~F}$.
Page 50, Table gives for $t-t^{\prime}=1^{\circ} .5$ and $t^{\prime}=-6^{\circ}=0.016$ inch.
Subtract for fraction of $t^{\prime}=0.5, \quad 0.0002 \times 5=-0.001$ Force of vapor in the air $=0.015$
Relative lamidity $=45$

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Kumidity in Hundredths.


Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative IIumidity in IIundredths.


Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0012$.

Temperature, Fahrenheit - Force of Vapor in English lnches.- Relative Humidity in Ilundredths.


Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0012$.

Temperature, Fahrenheit. - Force of Vapor in English Inches - Relative Humidity in IIundredths.


Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0012$.

Temperature, Fahrenheit - Force of Vapor in English Inches. - Relative Humidity in Hundredths

| WetBulb meter $\mathrm{Pahr}_{\mathrm{L}}^{\mathrm{t}} \mathrm{n}$ heit. |  | t-t, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0^{\circ} \cdot 0$ |  | 0.5 |  | 10.0 |  | 10.5 |  | $2{ }^{\circ} \mathrm{O}$ |  | 20.5 |  |
|  |  | Force of Valor. | Relative Hu-midity |  Rela- <br> tive <br> Force of <br> tive <br> Vapor. <br> Inid- <br> mid- <br> ity <br>   |  |  |  | Force of Vapor. | Relative Ifu-midity. | Force of rapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Huu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ |  |  |
| 。 |  | Eng. In. |  | Eng. In. |  | Eng In. |  | Eng In. |  | Eng. In. |  | Eng. In. |  |
| 32 | 2.0007 | 0.151 | 100 | 0.175 | 9 1.5 | 0.165 | 59.3 | 0.162 | 84.1 | \| 0.155 | 79.2 | 0.149 | 74.4 |
| 83 |  | 0.188 | 100 | 10.182 | 94.7 | 0.175 | 59.5 | 0.169 | 84.5 | 0.162 | 79.7 | 0.156 | 75.0 |
| 34 |  | 0.196 | 100 | 0.189 | 94.5 | 0.183 | 89.8 | 0.176 | 84.9 | 0.170 | 80.2 | 0.163 | 75.6 |
| 35 |  | 0.204 | 100 | 0.197 | 94.9 | 0.191 | 90.0 | 0.154 | 85.3 | 0.178 | 50.7 | $0.1 \% 1$ | 76.2 |
| 36 |  | 0.212 | 100 | 0.205 | 95.0 | 0.199 | 90.3 | 0.192 | 85.6 | 0.156 | 81.1 | 0.179 | 76.8 |
|  | . 0009 |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 | -(009 | 0.220 | 100 | 0.214 | 9.5 .2 | 0.207 | 90.5 | 0.201 | 86.0 | 0.194 | 81.6 | 0.188 | 77.3 |
| 35 |  | 0.229 | 100 | 0.223 | 9.5.3 | 0.216 | 90.7 | 0.210 | 86.3 | 0.203 | 82.0 | 0.196 | 77.9 |
| 39 |  | 0.238 | 100 | 0.232 | 9.9 .4 | 0.225 | 91.0 | 0.219 | 86.6 | 0.212 | 82.4 | 0.206 | 78.4 |
| 40 |  | 0.245 | 100 | 0.241 | 9.5 .5 | 0.235 | 91.2 | 0.223 | 86.9 | 0.221 | 82.9 | 0.215 | 78.9 |
| 41 |  | 0.257 | 100 | 0.251 | 95.6 | 0.214 | 91.4 | 0.238 | 87.3 | 0.231 | 83.3 | 0.2.24 | 79.4 |
| 12 |  | 0.267 | 100 | 0.260 | 95.7 | 0.254 | 91.6 | 0.247 | 87.5 | 0.241 | 83.6 | 0.234 | 79.8 |
| 43 |  | 0.275 | 100 | 0.271 | 9.5 .8 | 0.264 | 91.8 | 0.258 | 87.8 | 0.251 | 84.0 | 0.245 | 80.3 |
| 4 |  | 0.298 | 100 | 0.282 | 95.9 | 0.275 | 92.0 | 0.268 | 88.1 | 0.262 | 84.3 | 0.255 | 80.7 |
| 45 |  | 0.299 | 100 | 0.293 | 96.0 | $0.2 \leq 6$ | 92.1 | 0.280 | 88.3 | 0.273 | 84.7 | 0.266 | 81.1 |
| 46 |  | 0.311 | 100 | 0.304 | 96.1 | 0.297 | 92.3 | 0.291 | 88.6 | 0.254 | 85.0 | 0.278 | 81.5 |
|  | . 0012 |  |  |  |  |  |  |  |  |  |  |  |  |
| 47 |  | 0.323 | 100 | 0.316 | 96.2 | 0.310 | 92.5 | 0.303 | 88.8 | 0.297 | 85.3 | 0.290 | 81.9 |
| 43 |  | 0.335 | 100 | 0.329 | 96.2 | 0.322 | 92.6 | 0.315 | 89.0 | 0.309 | 85.6 | 0.302 | 82.2 |
| 49 | . 0013 | 0.315 | 100 | 0.341 | 96.3 | 0.33 .5 | 92.7 | 0.325 | 89.3 | 0.321 | 85.9 | 0.315 | 22.6 |
| 50 | . 0013 | 0.361 | 100 | 0.354 | 96.4 | 0.345 | 92.9 | 0.341 | 89.5 | 0.334 | 86.1 | 0.32 6 | 82.9 |
| 51 |  | 0.374 | 100 | 0.368 | 96.5 | 0.361 | 93.0 | 0.354 | 89.7 | 0.348 | 86.4 | 0.341 | 83.2 |
|  | . 0014 |  | 100 | 0.389 | 96.5 | 0.375 | 93.9 | 0.362 | 89.9 | 0.362 | 86.7 | 0.355 | 83.6 |
| 3 3 | . 0014 | 0.403 | 100 | 0.396 | 46.6 | 0.389 | 93.3 | 0.35 | 90.1 | 0.376 | 86.9 | 0.370 | 83.9 |
| 54 | . 0015 | 0.413 | 100 | 0.411 | 96.7 | 0.104 | 93.4 | 0.:398 | 90.2 | 0.391 | 87.2 | 0.385 | 84.2 |
| 55 |  | 0.433 | 100 | 0.426 | 96.7 | 0.420 | 93.5 | 0.413 | 90.4 | 0.407 | 87.4 | 0.400 | 84.4 |
| 56 | .0016 | 0.449 | 160 | 0.442 | 96.8 | 0.436 | 93.6 | 0.429 | 90.6 | 0.422 | 87.6 | 0.416 | 84.7 |
|  | . 0016 |  |  |  |  |  |  |  |  |  |  |  |  |
| 57 |  | 0.466 | 100 | 0.459 | 96.8 | 0.152 | 93.7 | 0.446 | 90.7 | 0.439 | 87.5 | 0.432 | 85.0 |
| 53 | .0017 | 0.452 | 100 | 0.476 | 96.9 | 0.169 | 93.9 | 0.463 | 90.9 | 0.456 | 88.0 | 0.449 | 85.2 |
| 59 | 017 | 0.500 | 100 | 0.493 | 96.9 | 0.157 | 94.0 | 0.480 | 91.0 | 0.473 | 88.2 | 0.467 | 8.5 .5 |
| 60 | 018 | 0.515 | 100 | 0.511 | 97.0 | 0.50 .5 | 94.1 | 0.498 | 91.2 | 0.491 | S8.4 | 0.485 | 85.7 |
| 61 | . 0019 | 0.537 | 100 | 0.530 | 97.0 | 0.523 | 94.2 | 0.517 | 91.3 | 0.510 | 88.6 | 0.503 | 85.9 |
| 62 | . 0013 | 0.5 .56 | 100 | 0.549 | 97.1 | 0.512 | 9 ¢.2 | 0.536 | 91.5 | 0.529 | 88.8 | 0.522 | 86.2 |
| (i3) | . 0120 | 0.576 | 100 | 0.569 | 97.1 | 0.562 | 94.3 | 0.556 | 91.6 | 0.549 | 89.0 | 0.542 | 86.4 |
| 61 | . 00 | 0.596 | 100 | 0.559 | 97.2 | 0.553 | 94.4 | 0.576 | 91.7 | 0.569 | 89.1 | 0.563 | 86.6 |
| 6.5 | . 002 | 0.617 | 100 | 0.611 | 97.2 | 0.604 | 94.5 | 0.597 | 91.9 | 0.591 | 89.3 | 0.584 | 86-8 |
| 66 | .002 | 0.639 | 100 | 0.633 | 97.3 | 0.626 | 91.6 | 0.619 | 92.0 | 0.612 | 89..) | 0.606 | 87.0 |
| 67 | . 0023 | 0.662 | 100 | 0.655 | 97.3 | 0.648 | 94.7 | 0.642 | 92.1 | 0.635 | 89.6 | 0.62 S | 87.2 |
| Mean Horizontal Difference of Force of Vapor for each 00.1 $=0.0018$. |  |  |  |  |  |  |  |  |  |  |  |  |  |

Temperature, Fahrenheit. - Force of Vapor in English Inches - Relative IIumidivy in Hundredths.

| Wet-BulbThermo-metert'Fahren-heit. | Mcan <br> Vertical Dífference of Force of Vapor for each 00.1. | $\mathbf{t - t}$, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0.0 |  | 0.05 |  | 10.0 |  | 10.5 |  | 20.0 |  | 2.5 |  |
|  |  | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | Relative IIu-midity. | Force of Vapor. | Rclative Hu-midity. | Force of Vapor. | Rela. tive Hu-midity. | Force of Vapor. | Relative Hu-midity |  Rela- <br> Force of tive <br> Vapor. Iud- <br>  mid. <br>  ity. |  |
| 63 | 0.0023 | Eng. In. |  |  | 97.3 |  | 94.7 | $\begin{gathered} \text { Eng. In. } \\ 0.665 \end{gathered}$ |  | $\begin{gathered} \text { Eng In. } \\ 0.658 \end{gathered}$ | S9.8 | Eng In. |  |
| 65 |  | 0.685 | 100 | 0.675 |  | 0.671 |  |  |  |  |  | 0.651 | 87.3 |
| 69 | . 0024 | 0.708 | 100 | 0.702 | 97.4 | 0.695 | 94.8 | 0.653 | 92.3 | 0.682 | 89.9 | 0.675 | 87.5 |
| 70 |  | 0.733 | 100 | 0.726 | 97.4 | 0.720 | 94.9 | 0.713 | 92.4 | 0.706 | 90.0 | 0.649 | 87.7 |
| 71 |  | 0.759 | 100 | 0.752 | 97.5 | 0.745 | 95.0 | 0.735 | 92.5 | 0.731 | 90.2 | 0.725 | 87.9 |
| 72 | .0026 | 0.754 | 100 | 0.778 | 97.5 | 0.771 | 95.0 | 0.764 | 92.7 | 0.757 | 90.3 | 0.751 | 88.0 |
| .00:27 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | . 0028 | 0.811 | 100 | 0.805 | 97.5 | 0.798 | 9.5 .1 | 0.791 | 92.7 | 0.754 | 90.4 | 0.778 | 88.2 |
| 74 |  | 0.539 | 100 | 0.832 | 976 | 0.826 | 95.2 | 0.319 | 92.5 | 0.512 | 90.6 | 0.805 | 88.3 |
| 75 | . 0028 | 0.568 | 100 | 0.861 | 97.6 | 0.554 | 95.2 | 0.847 | 92.9 | 0.841 | 90.7 | 0.834 | 88.5 |
| 76 | $\begin{aligned} & .0029 \\ & .0030 \end{aligned}$ | 0.897 | 100 | 0.590 | 97.6 | 0.883 | 95.3 | 0.877 | 93.0 | 0.870 | 90.8 | 0.563 | 85.6 |
| 77 |  | 0.927 | 100 | 0.920 | 97.7 | 0.914 | 95.4 | 0.907 | 93.1 | 0.900 | 90.9 | 0.893 | 88.8 |
|  | . 0031 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | $\begin{array}{r} .0032 \\ .033 \end{array}$ | 0.958 | 100 | 0.9 .71 | 97.7 | 0.945 | 95.4 | 0.938 | 93.2 | 0.931 | 91.0 | 0.924 | 88.9 |
| 79 |  | 0.990 | 100 | 0.983 | 97.7 | 0.977 | 95.5 | 0.970 | 93.3 | 0.963 | 91.1 | 0.956 | 89.0 |
| 80 |  | 1.023 | 100 | 1.016 | 97.7 | 1.010 | 95.5 | 1.003 | 93.4 | 0.996 | 91.2 | 0.959 | 89.2 |
| 81 | $\begin{aligned} & .0634 \\ & .0035 \end{aligned}$ | 1.057 | 100 | 1.050 | 97.8 | 1.044 | 95.6 | 1.037 | 93.4 | 1.030 | 91.3 | 1.023 | 89.3 |
| 82 |  | 1.092 | 100 | 1.085 | 97.8 | 1.079 | 95.6 | 1.072 | 93.5 | 1.065 | 91.4 | 1.058 | 89.4 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | . 0037 | 1.128 | 100 | 1.121 | 97.8 | 1.115 | 95.7 | 1.108 | 93.6 | 1.101 | 91.5 | 1.094 | 89.5 |
| 84 |  | 1.165 | 100 | 1.153 | 97.8 | 1.152 | 95.7 | 1.14. | 93.6 | 1.138 | 91.6 | 1.1:31 | 59.6 |
| 85 | . 0038 | 1.203 | 100 | 1.196 | 97.9 | 1.189 | 95.8 | 1.183 | 93.7 | 1.176 | 91.7 | 1.169 | 89.7 |
| 86 | $\begin{aligned} & .0039 \\ & .0040 \end{aligned}$ | 1.242 | 100 | 1.235 | 97.9 | 1.228 | 95.8 | 1.222 | 93.8 | 1.215 | 91.5 | 1.208 | 89.8 |
| 87 |  | 1.282 | 100 | 1.275 | 97.9 | 1.268 | 95.9 | 1.263 | 93.8 | 1.256 | 91.9 | 1.249 | 90.0 |
|  | .0041 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 | . 0042 | 1.323 | 100 | 1.317 | 97.9 | 1.310 | 95.9 | 1.303 | 93.9 | 1.296 | 92.0 | 1.259 | 90.1 |
| 89 |  | 1.366 | 100 | 1.359 | 97.9 | 1.352 | 95.9 | 1.345 | 94.0 | 1.339 | 92.0 | 1.332 | 90.2 |
| 90 | . 0044 | 1.410 | 100 | 1.403 | 98.0 | 1.396 | 96.0 | 1.389 | 94.0 | 1.382 | 92.1 | 1.375 | 90.3 |
| 91 | . 0045 | 1.455 | 100 | 1.448 | 98.0 | 1.441 | 96.0 | 1.434 | 94.1 | 1.427 | 92.2 | 1.420 | 90.3 |
| 92 | . 0046 | 1.501 | 100 | 1.494 | 98.0 | 1.487 | 96.1 | 1.480 | 94.1 | 1.473 | 92.3 | 1.466 | 90.4 |
|  | . 0048 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 | . 0049 | 1.548 | 100 | 1.541 | 98.0 | 1.53 .5 | 96.1 | 1.528 | 94.2 | 1.521 | 92.4 | 1.514 | 90.5 |
| 94 |  | 1.597 | 100 | 1.590 | 98.1 | 1.583 | 96.1 | 1.576 | 94.3 | 1.569 | 92.4 | 1.562 | 90.6 |
| 95 | . 0050 | 1.647 | 100 | 1.640 | 98.1 | 1.633 | 96.2 | 1.626 | 94.3 | 1.619 | 92.5 | 1.612 | 90.7 |
| 96 | . 0051 | 1.698 | 100 | 1.691 | 98.1 | 1.684 | 96.2 | 1.677 | 9 +.4 | 1.670 | 92.6 | 1.664 | 90.8 |
| 97 | . 0053 | 1.751 | 100 | 1.744 | 95.1 | 1.739 | 96.2 | 1.730 | 94.4 | 1.723 | 92.6 | 1.716 | 90.9 |
| 93 | . 0054 | 1.505 | 100 | 1.798 | 98.1 | 1.791 | 96.3 | 1.784 | 94.5 | 1.777 | 92.7 | 1.770 | 90.9 |
|  | . 0056 |  |  |  |  |  |  |  |  |  |  |  |  |
| 99 |  | 1.861 | 100 | 1.854 | 98.1 | 1.847 | 96.3 | 1.840 | 94.5 | 1.833 | 92.8 | 1. $\mathrm{S}^{2} 6$ | 91.0 |
| 100 | .0057 | 1.918 | 100 | 1.911 | 98.2 | 1.904 | 96.3 | 1.597 | 94.6 | 1.890 | 92.8 | 1.853 | 91.1 |
| 101 | . 0059 | 1.977 | 100 | 1.970 | 98.2 | 1.963 | 96.4 | 1.9 .56 | 94.6 | 1.949 | 92.9 | 1.942 | 91.2 |
| 102 | . 0060 | 2.037 | 100 | 2.030 | 98.2 | 2.023 | 96.4 | 2.016 | 94.7 | 2.009 | 92.9 | 2.002 | 91.2 |
| 103 | . 0062 | 2.098 | 100 | 2.092 | 98.2 | 2.055 | 96.4 | 2.078 | 94.7 | 2.071 | 93.0 | 2.064 | 91.3 |
| 104 | . 0063 | 2.162 | 100 | 2.155 | 98.2 | 2.148 | 96.5 | 2.141 | 94.7 | 2.134 | 93.1 | 2.127 | 91.4 |
| Mean Horizontal Difference of Force of Vapor for each $00.1=0.0013$. |  |  |  |  |  |  |  |  |  |  |  |  |  |

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative IIumidity in Iundredths.

| WetBulb Thermo meter 1 Fahrenheit. | Mean <br> Vertical Diflerence of Force of Vapor for ench 0.1. | $\mathbf{t}$ - $\mathbf{t}^{\prime}$, or Difference of Wet and Dry Bulb Thermometers |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 3.0 |  | 30.5 |  | 40.0 |  | $4 \times .5$ |  | 5.0 |  | 5.5 |  |
|  |  | Force of Vapor. | Relative IIt-millity | Foree of Vapor. | Relative Itu-midity. | Force of Vapor. | Relative Ill-mility. | Force of Vapor | Relative Ifu-midity. | Force of <br> Vapor. | Rela tive IIu midity. | Force of <br> Vapor. | Rela tive Hu-nidity |
| $\begin{gathered} 0 \\ 32 \\ 3 . \\ 34 \\ 35 \\ 36 \end{gathered}$ | 0.0007 | Eng. In. |  | Eng. In. |  | Eug. In. |  | Eng. In. |  | Eng In. |  | Eng. In. |  |
|  |  | 142 | 69.8 | .136 | 65.3 | 0.129 | 61.0 | 0.123 | 56.8 | 116 | 52.7 | 0.110 | 15.8 |
|  | . 0007 | 0.149 | 70.5 | 0.143 | 66.1 | 0.136 | 61.9 | 0.130 | 57.7 | 0.123 | 53.7 | 0.117 | 50.0 |
|  | .000s | 0.157 | 71.2 | 0.150 | 66.9 | 0.144 | 62.5 | 0.137 | 58.6 | 0.131 | 51.7 | 0.12! | 51.2 |
|  | . 0008 | 0.16 .5 | 71.9 | 0.158 | 67.7 | 0.152 | 63.6 | 0.145 | 59.5 | 0.139 | 5.5 .7 | 0.132 | 52.3 |
|  |  | 0.173 | 72.6 | 0.166 | 63.5 | 0.160 | 64.5 | 0.153 | 60.5 | 0.147 | 56.7 | 0.140 | 53.4 |
| .0008 |  | 0.181 | 73.2 | 0.17 .5 | 69.2 | 0.162 | 65.3 | 0.162 | 61.4 | 0.155 | 57.7 | 0.119 | 54.5 |
| 29 .0009 |  | 0.190 | 73.5 | 0.183 | 69.9 | 0.177 | 66.1 | 0.170 | 62.3 | 0.164 | 55.7 | 0.157 | 55.5 |
| . 1010 |  | 0.149 | 71.1 | 0.192 | 70.6 | 0.156 | 66.9 | 0.179 | 63.2 | 0.173 | 59.7 | 0.166 | 56.5 |
| 4011 |  | 0.208 | 75.0 | 0.902 | 71.3 | 0.19 .5 | 67.7 | 0.189 | 64.1 | 0.182 | 60.7 | 0.176 | 57.5 |
|  |  | 0.218 | 75.6 | 0.211 | 72.0 | 0.205 | 68.4 | 0.198 | 65.0 | 0.192 | 61.7 | 0.185 | 35.5 |
| . 0010 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 42 | . 0010 | 0.225 | 76.2 | 0.221 | 72.6 | 0.215 | 69.1 | 0.208 | 65.7 | 0.202 | 62.1 | 0.195 | 59.4 |
| 43 |  | 0.235 | 76.7 | 0.232 | 73.2 | 0.225 | 69.8 | 0.219 | 66.3 | 0.212 | 63.1 | 0.20 .5 | 60.2 |
| 44 | . 0041 | $0.2+9$ | 77.2 | 0.212 | 73.7 | 0.236 | 70.4 | 0.229 | 67.0 | $0.2 \cdot 3$ | 63.8 | 0.216 | (61.1 |
| 45 | . 0011 | 0.260 | $7 \% .7$ | 0.253 | 74.3 | 0.247 | 71.0 | 0.210 | 67.6 | 0.231 | 164.6 | 0.227 | 61.8 |
| 46 | . 0011 | 0.271 | 75.1 | $0.26 \%$ | 74.8 | 0.258 | 71.6 | 0.252 | 68.3 | 0.245 | 65.3 | 0235 | 62.6 |
| 46 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 47 | .001:3 | 0.283 | 78.6 | 0.277 | 75.3 | 0.270 | 72.2 | 0.264 | 68.9 | 0.257 | 66.0 | $0.2 \% 0$ | 63.3 |
| 48 |  | 0.296 | 79.0 | 0.259 | 7.5 .8 | 0.282 | 72.7 | 0.276 | 69.6 | 0.269 | 66.7 | 0.263 | 61.0 |
| 49 | . 0013 | 0.308 | 79.1 | 0.302 | 76.3 | 0.295 | 73.3 | 0.258 | 70.2 | 0.2-2 | 67.4 | 0.275 | 64.7 |
| 50 | . 0013 | 0.321 | 79.8 | 0.315 | 76.7 | 0.305 | 73.8 | 0.301 | 70.9 | 0.295 | 6-.1 | 0.288 | 65.4 |
| 51 | . 0013 | 0.335 | 80.2 | 0.328 | 77.2 | 0.321 | 74.3 | 0.315 | 71.4 | 0.308 | 65.7 | 0.302 | 66.0 |
| 5.$) .0014$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.349 | 80.5 | 0.312 | 77.6 | 0.335 | 74.7 | 0.329 | 71.9 | 0.322 | 69.2 | 0.315 | 66.6 |
| 53 | . 0014 | 0.36\%3 | 80.9 | 0.356 | 75.0 | 0.350 | 75.2 | $0.34: 3$ | 72.5 | 0.336 | 69.8 | 0.330 | 67.2 |
| 54 | . 0015 | 0.378 | 81.2 | 0.371 | 7-.4 | 0.365 | 75.6 | 0.358 | 72.9 | 0.3 J 1 | 70.3 | 0.345 | 67.8 |
| 5.5 | . 0015 | 0.393 | 81.6 | 0.357 | 78.8 | $0.3>0$ | 76.1 | 0.373 | 73.4 | 0.367 | 70.8 | 0.360 |  |
| 56 | . 0016 | 0.409 | S1.9 | 0.403 | 79.1 | 0.396 | 76.5 | 0.389 | 73.9 | 0.883 | 71.3 | 0.376 | 65.9 |
| 57 ${ }^{\text {\% }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.426 | 8.2 .2 | 0.419 | 79.5 | 0.412 | 76.9 | 0.406 | 74.3 | 0.399 | 71.8 | 0.392 | 69.4 |
| 58 | . 0017 | 0.41: | 82.5 | 0.436 | 79.8 | 0.12!) | 77.2 | 0.423 | 74.8 | 0.116 | 72.3 | 0.109 | 69.9 |
| 59 | . 0017 | 0.160 | 82.8 | 0.153 | 80.2 | 0.417 | 77.6 | 0.440 | 75.1 | 0.433 | 72.7 | 0.127 | 70.3 |
| 60 | $\begin{aligned} & .0018 \\ & .0019 \end{aligned}$ | 0.478 | ¢3.1 | 0.17 I | 80.5 | 0.16 .5 | 78.0 | 0.4 .58 | 75.5 | 0.451 | 73.1 | 0.445 | 70.8 |
| 61 |  | 0.497 | S3.3 | 0.490 | 80.8 | 0.183 | 75.3 | 0.177 | 75.9 | 0.470 | 73.5 | 0.463 | 71.3 |
| $6 . \quad .0019$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 0.516 | 83.6 | 0.509 | 81.1 | 0.502 | 78.6 | 0.196 | 76.3 | 0.489 | 74.0 | 0.182 | 71.7 |
| 63 | .00:30 | 0.536 | 83.8 | 0.529 | 81.4 | 0.522 | 79.0 | 0.516 | 76.6 | 0.509 | 74.8 | 0.502 | 72.1 |
| 64 | .0020 | 0.556 | 84.1 | 0.519 | 81.7 | 0.543 | 79.3 | 0.536 | 77.0 | 0.529 | 74.7 | 0.523 | 72.5 |
| 6.5 | $\begin{aligned} & .0021 \\ & .0022 \\ & .0023 \end{aligned}$ | 0.577 | 84.3 | 0.570 | 81.9 | 0.561 | 79.6 | 0.5 .57 | 77.3 | 0.5 .50 | 75.1 | 0.544 | 72.9 |
| 66 |  | 0.599 | 84.6 | 0.592 | 82.2 | 0.506 | 79.9 | 0.579 | 77.6 | 0.572 | 7.5 .1 | 0.566 | 73.3 |
| 67 |  | 0.622 | 84.8 | 0.615 | 82.4 | 0.605 | 80.2 | 0.601 | 75.0 | 0.595 | 75.8 | 0.588 | 73.7 |
| Mean Ilorizontal Difference of Force of Vapor for each $0^{\circ} 1=0.0013$. |  |  |  |  |  |  |  |  |  |  |  |  |  |

Temp srature, Fahrenheit. - Force of Vapor in English Inches. - Relative Humidity in Hundredtha.

| Wet-BulbThermo-meter$t^{1}$Fabren-beit | MeanVerticalDiferenceof Forceof Vaporfor each0.1. | $\mathbf{t}$ - $\mathbf{t}^{\prime}$, or Difference of Wet and Dry Buib Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $3{ }^{\circ} .9$ |  | 30.5 |  | 4.0 |  | $4{ }^{10} .5$ |  | $5{ }^{\circ} .0$ |  | 50.5 |  |
|  |  | $\begin{aligned} & \text { Force of } \\ & \text { Vapor. } \end{aligned}$ | Rela- <br> tive <br> Lu- <br> mid- <br> ity <br> in | Force of Yapor. | Relative 11u-midity. | Force of Vapor. | Relative 1Fu-midity. | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { 11u- } \\ & \text { midu- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor | $\begin{aligned} & \text { Rela } \\ & \text { tive } \\ & \text { Ilu } \\ & \text { mini- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative Hu* midity. |
|  | 0.0024.0024.0025.0026.0027 | Eng. In |  | Eng. 1n. |  | Eng. 1n. |  | Eng. In. |  | Eng ln. |  | Eng. In. |  |
| 63 |  | 0.644 85.0 |  | 0.633 | 82.7 | 0.631 | 80.4 | 0.624 | 78.3 | . 6 | 76.1 | 0.611 | 74.0 |
| 69 |  | 0.665 | 85.2 | 0.661 | 82.9 | 0.655 | 80.7 | 0.648 | 78.6 | 0.641 | 76.4 | 0.635 | 74.4 |
| 70 |  | 0.693 | 85.4 | 0.686 | 83.2 | 0.679 | 81.0 | 0.672 | 78.8 | 0.666 | 76.8 | 0.659 | 74.7 |
| 71 |  | $0.715$ | 85.6 | 0.714 | 83.1 | 0.704 | 81.2 | 0.693 | 79.1 | 0.691 | 77.1 | 0.654 | 75.1 |
| 72 |  | $0.74$ | 85.8 | 0.737 | 83.6 | 0.731 | 81.5 | 0.724 | 79.4 | 0.718 | 77.4 | 0.710 | 75.4 |
|  |  | 0.771 |  |  |  |  |  |  |  |  |  |  |  |
| 73 | .0028 |  | 56.0 | 0.764 | 83.8 | 0.757 | 81.7 | 0.751 | 79.7 | 0.744 | 77.6 | 0.737 | 75.7 |
| 74 |  | $\begin{aligned} & 0.771 \\ & 0.799 \end{aligned}$ | 56.2 | 0.792 | S4.0 | 0.785 | 81.9 | 0.778 | 79.9 | 0.772 | 77.9 | 0.765 | 76.0 |
| 75 |  | 0.527 | S6.3 | 0.820 | 84.2 | 0.814 | 82.2 | 0.807 | 80.2 | 0.500 | 78.2 | 0.79:3 | 76.3 |
| 76 | . 0030 | $\begin{aligned} & 0.856 \\ & 0.857 \end{aligned}$ | 86.5 | 0.550 | 84.4 | 0.843 | 82.4 | 0.536 | S0.t | 0.829 | 78.4 | 0.523 | 76.6 |
| 77 |  |  | 86.7 | 0.880 | 84.6 | 0.573 | 82.6 | 0.566 | 50.6 | 0.560 | 78.7 | 0.553 | 76.8 |
|  | . 0031 | 0.918 |  |  |  |  |  |  |  |  |  |  |  |
|  | .0032 | 0.919 |  |  |  |  |  |  |  |  |  |  |  |
| 79 | . 0033 |  |  |  |  | 0. | 83.0 | 0.929 | 1.1 | 0.922 | 79.2 | 0.916 | 77.4 |
| 80 |  | 0.982 | 87.1 | 0.976 | 85.1 | 0.969 | 83.2 | 0.962 | 81.3 | 0.955 | 79.4 | 0.919 | 77.6 |
| 81 | . 0035 | $\begin{aligned} & 1.016 \\ & 1.051 \end{aligned}$ | 87.3 | 1.010 | 85.3 | 1.003 | 83.4 | 0.996 | 81.5 | 0.989 | 79.7 | 0.952 | 77.9 |
| 82 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 84 |  | 1.124 | 87 | 1.117 | 85.8 | 1.111 | 83.9 | 1.104 | 82.1 | 1.096 | . 3 | 090 |  |
| 85 |  | 1.162 | 87.8 | 1.155 | 85.9 | 1.148 | 84.1 | 1.142 | 82.3 | 1.135 | 80.5 | 1.128 | 78.8 |
| 86 |  |  | 87.9 | 1.194 | 86.1 | 1.187 | 84.2 | 1.181 | 82.4 | 1.174 | 80.7 | 1.167 | 79.0 |
| S7 |  | $\begin{aligned} & 1.201 \\ & 1.242 \end{aligned}$ | 88.1 | 1.235 | S6.2 | 1.228 | 84.4 | 1.222 | 82.6 | 1.215 | 80.9 | 1.208 | 79.2 |
| 88 | . 0041 | $1.282$ | 85.2 | 1.276 | 86.3 | 1.269 | 84.6 | 1.262 | 82.8 | 1.2.5. | 81. | 1 | 9. |
| 89 |  | 1.32 .5 | 88.3 | 1.318 | 86.5 | 1.311 | 84.7 | 1.304 | 83.0 | 1.297 | 81.3 | 1.291 | 79.6 |
| 90 | .0044 | 1.369 | 88.4 | 1.362 | 86.6 | 1.355 | 84.9 | 1.348 | 83.1 | 1.341 | 81.4 | 1.33 | 9.8 |
| 91 | .0045 | $\begin{array}{\|l\|l} 1.369 \\ 1.413 \\ 1.460 \end{array}$ | 88.5 | 1.407 | 86.7 | 1.400 | 85.0 | 1.393 | 83.3 | 1.386 | 81.6 | 1.379 | 0.0 |
| 92 |  |  | 85.6 | 1.453 | 86.9 | 1.446 | 85.1 | 1.439 | 83.4 | 1.132 | 81.5 | 1.425 | 80.2 |
|  | . 0047 | $1.507$ |  |  |  |  |  |  |  |  |  |  |  |
| 94 | . 0049 | $1 \begin{aligned} & 1.507 \\ & 1.556\end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |
| 95 | .0050 | 1.606 | 85.9 | 1.599 |  | 92 |  | 1.585 |  |  |  |  |  |
| 96 | . 0051 | 1.657 | 89.0 | 1.650 | 87.3 | 1.643 | 85.7 | 1.636 | 84.0 | 1.629 | 8.4 | 1.620 | s0.9 |
| 97 | . 0 | 1.709 | 89.1 | 1.702 | 87.5 | 1.696 | 85.8 | 1.688 | 84.2 | 1.682 | 82.6 | 1.675 | 81.0 |
| 98 | . 0054 | 1.764 | 89.2 | 1.757 | 87.6 | 1.750 | 85.9 | 1.743 | 84.3 | 1.736 | 82.7 | 1.729 | 81.2 |
|  | . 0055 | 1.819 |  |  |  |  |  |  |  |  |  |  |  |
| 99 |  |  | 89.3 | 1.812 | 87.7 | 1.505 | 86.0 | 1.798 | 84.4 | 1.792 | 82.9 | 1.785 | 81.3 |
| 100 | 57 | 1.576 | 89.4 | 1.869 | 87.8 | 1.863 | 86.2 | 1.856 | 84.6 | 1.849 | -3.0 | 1.8.12 | 81.5 |
| 101 | .005s | 1.935 | 89.5 | 1.923 | 87.9 | 1.921 | 86.3 | 1.914 | 84.7 | 1.907 | 83.2 | J. 900 | 81.6 |
| 102 | .0060 | 1.99.) | 89.6 | 1.988 | 88.0 | 1.981 | 86.4 | 1.974 | 84.9 | 1.967 | 83.3 | 1.961 | 81.3 |
| 103 |  | 2.057 | 89.7 | 2.050 | 88.1 | 2.043 | 86.5 | 2.036 | 81.9 | 2.029 | 83.4 | 2.022 | 81.9 |
| 104 | .0063 | $\left\|\begin{array}{l}2.057 \\ 2.120\end{array}\right\|$ | 59.8 | 2.113 | 88.2 | 2.106 | 866 | 2.099 | 85.1 | 2.092 | 83.5 | 2.085 | 82.1 |

Mean IIorizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0013$.

Temperature, Fahrenheit - Force of Vapor in English Inches. - Relative IIumidity in Ilundredths


Temperature, Fahrenheit. - Force of Vapor in English Inches - Relative Humidity in Hundredthe

| Wet-BuIbThermo-metertFahren-heit. | MeanVerticalDiferenceof Forceof Vaporfor each$0^{\circ} .1$. | $\mathbf{t}$ - $\mathbf{t}$, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $6^{\circ} .0$ |  | $6^{\circ} .5$ |  | $7 \bigcirc 0$ |  | 70.5 |  | 80.0 |  | $88^{\text {c. }} 5$ |  |
|  |  | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | Relative 14. midity. | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | Relative Hu-midity | Force of Vapor. | Relative Humid. ity. |
| 68 | 0.0024 | Eng. In. |  | Eng. In. |  | Eng. In. | $68.1$ | Eng. In. | $66.2$ | $\begin{gathered} \text { Eng In. } \\ 0.577 \end{gathered}$ | $\left.64.4\right\|_{0.571} ^{\text {Eng In. }}$ |  | 62.6 |
| 68 |  | 0.604 | $72.0$ | 0.597 |  |  |  | 0.584 |  |  |  |  |  |
| 69 | .0124 | 0.628 | 72.1 | 0.621 | 70.4 | 0.614 | 68.5 | 0.605 | 66.6 | 0.601 | 64.8 | 0.594 | 63.0 |
| 70 | . 0025 | 0.652 | 72.7 | 0.646 | 70.8 | 0.639 | 68.9 | 0.632 | 67.1 | 0.625 | 65.3 | 0.619 | 63.3 |
| 71 | . 0026 | 0.678 | 73.1 | 0.671 | 71.2 | 0.664 | 69.3 | 0.657 | 67.5 | 0.651 | 65.7 | 0.644 | 64.0 |
| 72 |  | 0.704 | 73.4 | 0.697 | 71.5 | 0.690 | 69.7 | 0.683 | 67.9 | 0.677 | 66.1 | 0.670 | 64.4 |
|  | . 0027 |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | .002s | 0.730 | 73.8 | 0.724 | 71.9 | 0.717 | 70.1 | 0.710 | 68.3 | 0.703 | 66.5 | 0.697 | 64.8 |
| 74 |  | 0.758 | 74.1 | 0.751 | 72.2 | 0.745 | 70.4 | 0.738 | 68.7 | 0.731 | 66.9 | 0.724 | 65.3 |
| 75 | . $0 \cap \geq 9$ | 0.787 | 74.1 | 0.750 | 72.6 | 0.773 | 70.8 | 0.766 | 69.0 | 0.760 | 67.3 | 0.753 | 65.7 |
| 76 | . 0030 | 0.916 | 74.7 | 0.809 | 72.9 | 0.502 | 71.1 | 0.796 | 69.4 | 0.789 | 67.7 | 0.782 | 66.1 |
| 77 | .0030 | 0.816 | 75.0 | 0.839 | 73.2 | 0.832 | 71.4 | 0.826 | 69.7 | 0.819 | 65.1 | 0.812 | 66.4 |
|  | . 0031 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | .0032 | 0.877 | 75.3 | 0.870 | 73.5 | 0.863 | 71.8 | 0.857 | 70.1 | 0.850 | 68.4 | 0.843 | 66.8 |
| 79 |  | 0.909 | 75.6 | 0.902 | 73.8 | 0.895 | 72.1 | 0.888 | 70.4 | 0.882 | 68.8 | 0.875 | 67.2 |
| 80 | .0033 | 0.942 | 75.8 | 0.935 | 74.1 | 0.928 | 72.4 | 0.921 | 70.7 | 0.915 | 69.1 | 0.908 | 67.5 |
| 81 | $\begin{aligned} & .0034 \\ & .0035 \end{aligned}$ | 0.976 | 76.1 | 0.969 | 74.4 | 0.962 | 72.7 | 0.955 | 71.0 | 0.918 | 69.4 | 0.942 | 67.9 |
| 82 |  | 1.011 | 76.4 | 1.004 | 74.6 | 0.997 | 73.0 | 0.990 | 71.3 | 0.983 | 69.8 | 0.977 | 68.2 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | . 0037 | 1.046 | 76.6 | 1.010 | 74.9 | 1.033 | 73.3 | 1.026 | 71.6 | 1.019 | 70.1 | 1.012 | 68.5 |
| 84 |  | 1.083 | 76.8 | 1.077 | 75.2 | 1.070 | 73.5 | 1.063 | 71.9 | 1.056 | 70.4 | 1.049 | 68.8 |
| 85 | .003s | 1.121 | 77.1 | 1.114 | 75.4 | 1.108 | 73.8 | 1.101 | 72.2 | 1.094 | 70.7 | 1.087 | 69.1 |
| 86 | .1038 <br> . 0439 | 1.160 | 77.3 | 1.153 | 75.7 | 1.147 | 74.1 | 1.140 | 72.5 | 1.133 | 70.9 | 1.126 | 69.4 |
| 87 |  | 1.201 | 77.5 | 1.194 | 75.9 | 1.187 | 7.1.3 | 1.181 | 72.7 | 1.174 | 71.2 | 1.167 | 69.7 |
|  | . 0040 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 | . 0042 | 1.241 | 77.7 | 1.235 | 76.1 | 1.228 | 74.6 | 1.221 | 73.0 | 1.214 | 71.5 | 1.207 | 70.0 |
| 89 |  | 1.284 | 78.0 | 1.277 | 76.4 | 1.270 | 74.8 | 1.263 | 73.3 | 1.256 | 71.8 | 1.250 | 70.3 |
| 90 | .0044 | 1.327 | 78.2 | 1.321 | 76.6 | 1.314 | 75.0 | 1.307 | 73.5 | 1.300 | 72.0 | 1.293 | 70.6 |
| 91 | . 0045 | 1.372 | 78.4 | 1.365 | 76.8 | 1.359 | 75.3 | 1.352 | 73.7 | 1.345 | 72.3 | 1.33s | 70.8 |
| 92 | . 0046 | 1.418 | 78.6 | 1.412 | 77.0 | 1.405 | 75.5 | 1.398 | 74.0 | 1.391 | 72.5 | 1.384 | 71.1 |
|  | . 0047 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 | . 0049 | 1.466 | 78.8 | 1.459 | 77.2 | 1.452 | 75.7 | 1.445 | 74.2 | 1.438 | 72.8 | 1.431 | 71.3 |
| 94 | . 0050 | 1.514 | 79.0 | 1.507 | 77.4 | 1.501 | 75.9 | 1.49-4 | 74.4 | 1.457 | 73.0 | 1.480 | 71.6 |
| 95 |  | 1.564 | 79.1 | 1.557 | 77.6 | 1.5 .50 | 76.1 | 1.544 | 74.7 | 1.537 | 73.2 | 1.530 | 71.8 |
| 96 | . 0051 | 1.615 | 79.3 | 1.608 | 77.8 | 1.602 | 76.3 | 1.595 | 74.9 | 1.588 | 73.4 | 1.581 | 72.1 |
| 97 | . 0052 | 1.668 | 79.5 | 1.661 | 78.0 | 1.654 | 76.5 | 1.647 | 75.1 | 1.640 | 73.7 | 1.633 | 72.3 |
| 98 | . 0054 | 1.722 | 79.7 | 1.715 | 78.2 | 1.708 | 76.7 | 1.701 | 75.3 | 1.694 | 73.9 | 1.688 | 72.5 |
|  | . 0056 |  |  |  |  |  |  |  |  |  |  |  |  |
| 99 | . 0057 | 1.778 | 79.8 | 1.771 | 78.4 | 1.764 | 76.9 | 1.757 | 75.5 | 1.750 | 74.1 | 1.743 | 72.7 |
| 100 |  | 1.83 .5 | 80.0 | 1.828 | 78.5 | 1.821 | 77.1 | 1.814 | 75.7 | 1.807 | 74.3 | 1.800 | 72.9 |
| 101 | .0059 | 1.893 | 80.2 | 1.887 | 78.7 | 1.880 | 77.3 | 1.873 | 75.9 | 1.566 | 74.5 | 1.859 | 73.2 |
| 102 | . 0060 | 1.954 | 80.3 | 1.947 | 78.9 | 1.940 | 77.4 | 1.933 | 76.1 | 1.926 | 74.7 | 1.919 | 73.4 |
| 103 | $\begin{aligned} & .0061 \\ & .0063 \end{aligned}$ | 2.015 | 80.5 | 2.008 | 79.0 | 2.001 | 77.6 | 1.994 | 76.2 | 1.987 | 74.9 | 1.980 | 73.6 |
| 104 |  | 2.078 | 50.6 | 2.071 | 79.2 | 2.064 | 77.8 | 2.057 | 76.4 | 2.051 | 75.1 | 2.044 | 73.8 |

Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0013$.

Temperature, Fahrenheit. - Force of Vapor in English Inches - Relative IIumidity in IIundredths.

| Wet-BubThermo-metertFahren-heit | MeanVerticalDifereareof Forceif Vaporfir euch$v^{\circ} .1$. | t- $\mathbf{t}^{\prime}$, or Difference of Wet and Dry Bulb Thermometers |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 9.0 |  | $9 \bigcirc .5$ |  | $10^{\circ} .0$ |  | 10.5 |  | 110.0 |  | 110.5 |  |
|  |  | $\begin{aligned} & \text { 'orce of } \\ & \text { Vapor. } \end{aligned}$ | Relative Hu-midity | Force of Vapor | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mill- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative Jua-niddity. | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { IIu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { tiru- } \\ & \text { nuid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{array}{\|c\|c\|c\|} \text { Rela- } \\ \text { tise } \\ \text { Iuu- } \\ \text { mid- } \\ \text { ity. } \end{array}$ |
| $\bigcirc$ | 00007 | Eny. 14 | 25.0 | Eng. 1n | 22.0 | Eug. In. | 19.2 | $\begin{aligned} & \text { Eng. In } \\ & 0.045 \end{aligned}$ | 16.4 | $\begin{gathered} \text { Eug. In. } \\ 0.035 \end{gathered}$ | 13.8 |  |  |
| 32 |  | 0.061 |  | 0.053 |  | 0.051 |  |  |  |  |  | $0.032$ | 11.2 |
| 33 | $\cdots 07$ | 0.071 | 26.7 | 0.065 | 23.8 | 0.058 | 21.0 | 0.052 | 18.3 | 0.045 | 15.7 | 0.039 | 13.2 |
| 34 |  | 0.079 | 28.3 | 0.072 | 2.5.5 | 0.066 | 22.7 | 0.059 | 20.1 | 0.053 | 17.5 | 0.046 | 15.1 |
| 35 | . 0008 | 0.057 | 29.9 | 0.080 | 27.1 | 0.07 .1 | 24.4 | 0.067 | 21.8 | 0.061 | 19.3 | 0.054 | 16.9 |
| 36 | .000s | 0.09 .5 | 31.4 | 0.058 | 28.7 | 0.082 | 26.0 | 0.075 | 23.5 | 0.069 | 21.1 | 0.062 | 18.7 |
|  | . 0008 |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 | .0009 | 0.103 | 33.0 | 0.096 | 30.3 | 0.090 | 27.6 | 0.083 | 25.2 | 0.077 | 22.8 | 0.070 | 20.1 |
| 38 |  | 0.112 | 34.4 | 0.105 | 31.8 | 0.099 | 29.2 | 0.092 | 26.8 | 0.086 | 24.4 | 0.079 | 22.1 |
| 39 | . 0009 | 0.121 | 35.9 | 0.114 | 33.3 | 0.108 | 30.7 | 0.101 | 28.4 | 0.094 | 26.1 | 0.088 | 23.8 |
| 40 | $\begin{aligned} & .0009 \\ & .0010 \end{aligned}$ | 0.130 | 37. | 0.123 | 31.5 | 0.117 | 32.2 | 0.110 | 29.9 | 0.104 | $\because 7.6$ | 0.097 | 25.4 |
| 41 |  | 0.139 | 35.6 | 0.133 | 36.2 | 0.126 | 33.7 | 0.120 | 31.4 | 0.113 | 29.2 | 0.107 | 27.0 |
|  | . 0010 |  |  |  |  |  |  |  |  |  |  |  |  |
| 42 | . 0010 | 0.149 | 39.9 | 0.143 | 37.5 | 0.136 | 35.0 | 0.130 | 32.8 | 0.123 | 30.6 | 0.116 | 28.4 |
| 43 |  | 0.160 | 41.1 | 0.153 | 38.7 | 0.146 | 36.3 | 0.110 | 34.1 | 0.133 | 32.0 | 0.127 | 29.8 |
| 44 | . 0010 | 0.170 | 42.3 | 0.163 | 39.3 | 0.157 | 37.6 | 0.150 | 35.4 | 0.144 | 33.3 | 0.137 | 31.2 |
| 45 | $\begin{aligned} & .0011 \\ & .0011 \end{aligned}$ | 0.181 | 43.4 | 0.175 | 41.1 | 0.168 | 38.9 | 0.161 | 36.7 | 0.155 | 34.6 | 0.148 | 32.5 |
| 46 |  | 0.192 | 4.5 | 0.186 | 42.2 | 0.179 | 39.9 | 0.173 | 37.9 | 0.166 | 35.8 | 0.160 | 33.8 |
|  | . 0012 |  |  |  |  |  |  |  |  |  |  |  |  |
| 47 | . 0012 | 0.204 | 45.5 | 0.195 | 43.3 | 0.191 | 41.1 | 0.185 | 39.0 | 0.178 | 37.0 | 0.171 | 350 |
| 48 |  | 0.217 | 46.5 | 0.210 | 44.3 | 0.203 | 42.1 | 0.197 | 40.1 | 0.190 | 35.1 | 0.184 | 36.1 |
| 49 | .0012 | 0.229 | 47.5 | 0.222 | 45.3 | 0.216 | 43.2 | 0.209 | 41.2 | 0.203 | 39.2 | 0.196 | 37.2 |
| 50 | . 0013 | 0.242 | 48.4 | 0.235 | 46.3 | 0.22! | 4.2 | 0.222 | 42.2 | 0.216 | 40.2 | 0.209 | 33.3 |
| 51 | . 0013 | 0.255 | 49.3 | 0.219 | 47.2 | 0.242 | 45.2 | 0.236 | 43.2 | 0.229 | 41.2 | 0.222 | 39.3 |
|  | . 0014 |  |  |  |  |  |  |  |  |  |  | 0.236 |  |
| 52 | . 0015 | 0.269 | 50.2 | 0.263 | 48.1 | 0.256 | 46.1 | 0.249 | 4.1 | 0.243 | 42.2 | 0.236 | 40.3 |
| 53 |  | 0.254 | 51.1 | 0.277 | 19.0 | 0.270 | 47.0 | 0.264 | 45.1 | 0.2 .57 | 13.2 | 0.250 | 41.3 |
| 54 | . 0015 | 0.298 | 51.9 | 0.292 | 49.8 | 0.255 | 47.9 | 0.279 | 46.0 | 0.272 | 4.4 | 0.265 | 42.3 |
| 55 | . 0015 | 0.314 | 52.7 | 0.307 | 50.7 | 0.300 | 48.7 | 0.294 | 46.8 | 0.287 | 45.0 | 0.281 | 43.2 |
| 56 | . 0016 | 0.330 | 53.5 | 0.323 | 51.4 | 0.316 | 49.5 | 0.310 | 47.7 | 0.303 | 45.9 | 0.296 | 44.1 |
|  | . 0016 |  |  |  |  |  |  |  |  |  |  |  |  |
| 57 | . 0017 | 0.316 | 54.3 | 0.339 | 52.2 | 0.333 | 50.3 | 0.326 | 48.5 | 0.319 | 46.7 | 0.313 | 44.9 |
| 58 |  | 0.363 | 55.0 | 0.356 | 52.9 | 0.350 | 51.1 | 0.343 | 49.2 | 0.336 | 47.5 | 0.330 | 4.5 .7 |
| 59 | . 0017 | 0.350 | 55.7 | 0.373 | 53.6 | 0.367 | 51.8 | 0.360 | 50.0 | 0.354 | 48.2 | 0.317 | 46.5 |
| 60 | $\begin{aligned} & .0018 \\ & .0018 \end{aligned}$ | 0.393 | 56.4 | 0.391 | 54.3 | 0.385 | 52.5 | 0.379 | 50.7 | 0.371 | 49.0 | 0.365 | 47.3 |
| 61 |  | 0.416 | 57.0 | 0.410 | 55.0 | 0.403 | 53.2 | 0.396 | 51.4 | 0.390 | 49.7 | 0.383 | 48.1 |
|  | . 0019 |  |  |  |  |  |  |  |  |  |  |  |  |
| 62 | .00:2 | 0. 436 | 57.6 | 0.429 | 55.6 | 0.422 | 53.9 | 0.116 | 52.1 | 0.409 | 50.4 | 0.102 | 48.8 |
| 63 |  | 0.455 | 58.2 | 0.449 | 56.3 | 0.442 | 54.5 | 0.135 | . 52.8 | 0.429 | 51.1 | 0.422 | 495 |
| 64 | . 0021 | 0.476 | 58.8 | 0.469 | 56.9 | 0.462 | 55.1 | 0.456 | 53.4 | 0.449 | 51.8 | 0.442 | 50.2 |
| 65 | $\begin{array}{r} .0021 \\ 0022 \\ 0023 \end{array}$ | 0.197 | 59.3 | 0.490 | 57.5 | 0.483 | 55.8 | 0.177 | 54.1 | 0.470 | 52.4 | 0.463 | 50.8 |
| 66 |  | 0.519 | 59.9 | 0.512 | 58.0 | 0.505 | 56.3 | 0.498 | 54.7 | 0.492 | 53.1 | 0.485 | 51.5 |
| 67 |  | 0.512 | 60.3 | 0.531 | 58.6 | 0.527 | 569 | 0.52 I | 5.5 .3 | 0.514 | 53.7 | 0.507 | 52.1 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0013$.

Tcmperature, Fabreuheit. -- Force of Vapor in Enylish Inches. - Relative Humidity in IIundredths.

| $\begin{gathered} \text { Wet- } \\ \text { Bulb } \\ \text { Thermo- } \\ \text { meter } \\ \mathbf{t}^{\prime} \\ \text { Fahren- } \\ \text { heit. } \end{gathered}$ | $\underset{\text { Mertical }}{\substack{\text { Mcan } \\ \hline}}$ bilference of Force of rapor $0 \cdot 1$. | $\mathbf{t}$ - $\mathbf{t}^{\prime}$, or Difference of Wet and Dry Beib Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $9{ }^{\circ} .0$ |  | 90.5 |  | $10^{\circ} 0$ |  | $10^{\circ} .5$ |  | 110.0 |  | 110.5 |  |
|  |  | Force of Vapor | $\begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { nitid- } \\ \text { ity. } \end{gathered}$ | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | Relative Hu-midity. | $\begin{aligned} & \text { Force of } \\ & \text { Vapor. } \end{aligned}$ | Relative Hu-midity. | Force of Vapor. | Relative IIu midity. | Force of Vapor. | Rela. tive 11u-midity |
| - |  | Eng. In. |  | Fing. In. |  | Eng. In. |  | Eng. In. |  | Eng. In. |  | $\overline{\text { Cog. } 1 \mathrm{n}}$ |  |
| 63 |  |  | 60.8 | 0.55 | 59.1 | . 550 | 57.4 | $0.5+4$ | 55.8 | 0.53 | 54.2 | 0.530 | 52.7 |
| 69 | .0025 | 0.588 | 61.3 | 0.551 | 59.6 | 0.574 | 58.0 | 0.567 | 56.4 | 0.561 | 51.8 | 0.554 | 53.3 |
| 70 |  | 0.612 | 61.8 | 0.605 | 60.1 | 0.598 | 58.5 | 0.592 | 56.9 | 0.585 | 55.1 | 0.575 | 53.8 |
| 71 | .0025 <br> .00:2 | 0.637 | 62.3 | 0.630 | 60.6 | 0.624 | 59.0 | 0.617 | 57.4 | 0.610 | 55.9 | 0.603 | 54.4 |
| 72 |  | 0.663 | 62.7 | 0.656 | 61.1 | 0.650 | 59.5 | 0.643 | 58.0 | 0.636 | 56.4 | 0.629 | 54.9 |
|  | . 0027 |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | .00:27 | 0.390 | 63.2 | 0.683 | 61.6 | 0.677 | 60.0 | 0.670 | 58.4 | 0.663 | 56.9 | 0.656 | 55.5 |
| 74 |  | 0.718 | 63.6 | 0.711 | 62.0 | 0.704 | 60.5 | 0.697 | 5-.9 | 0.691 | 57.4 | 0.684 | 56.0 |
| 75 | . 0023 | 0.746 | 64.0 | 0.739 | 62.5 | 0.733 | 60.9 | 0.726 | 59.4 | 0.719 | 57.9 | 0.712 | 56.5 |
| 76 | $.0029$$.0030$ | 0.775 | 64.4 | 0.769 | 62.9 | 0.762 | 61.3 | 0.755 | 59.8 | 0.748 | 58.4 | 0.741 | 56.9 |
| 77 |  | 0.805 | 64.5 | 0.799 | 63.3 | 0.792 | 61.8 | 0.785 | 60.3 | 0.778 | 58.5 | 0.772 | 57.4 |
|  | . 0031 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | .0032 | 0.836 | 65.2 | 0.829 | 63.7 | 0.523 | 62.2 | 0.816 | 60.7 | 0.509 | 59.2 | 0.802 | 57.8 |
| 79 |  | 0.868 | 65.6 | 0.861 | 64.1 | 0.555 | 62.6 | 0.818 | 61.1 | 0.541 | 59.7 | 0.534 | 58.3 |
| 80 | . 0033 | 0.901 | 66.0 | 0.894 | 64.5 | 0.597 | (63.0 | 0.581 | 61.5 | 0.574 | 60.1 | 0.567 | 58.7 |
| 81 | $\begin{aligned} & .0034 \\ & .0035 \end{aligned}$ | 0.935 | 66.3 | 0.928 | 64.8 | 0.921 | 63.4 | 0.914 | 61.9 | 0.908 | 60.5 | 0.901 | 59.1 |
| 82 |  | 0.970 | 66.7 | 0.963 | 65.2 | 0.956 | 63.7 | 0.949 | 62.3 | 0.943 | 60.9 | 0.936 | 59.5 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | . 0037 | 1.006 | 67.0 | 0.999 | 65.5 | 0.992 | 64.1 | 0.985 | 62.7 | 0.97S | 61.3 | 0.972 | 59.9 |
| 84 |  | 1.042 | 67.3 | 1.036 | 65.9 | 1.029 | 64.4 | 1.022 | 63.0 | 1.015 | 61.7 | 1.005 | 60.3 |
| 85 | .003s | 1.050 | 67.7 | 1.073 | 66.2 | 1.067 | 64.5 | 1.060 | 63.4 | 1.053 | 62.0 | 1.016 | 60.7 |
| 86 | $.0039$ | 1.119 | 65.0 | 1.112 | 66.5 | 1.106 | 65.1 | 1.099 | 63.7 | 1.092 | 62.4 | 1.08:5 | 61.0 |
| 87 | . 0010 | 1.160 | 68.3 | 1.153 | 66.8 | 1.146 | 65.4 | 1.140 | 64.1 | 1.133 | 62.7 | 1.126 | 61.4 |
|  | . 0041 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 |  | 1.200 | 68.6 | $1.19+$ | 67.1 | 1.187 | 65.8 | 1.180 | 64.4 | 1.173 | 63.1 | 1.166 | 61.7 |
| 89 | .0042 | 1.243 | 65.9 | 1.236 | 67.4 | 1.229 | 66.1 | 1.222 | 64.7 | 1.215 | 63. 4 | 1.208 | 62.1 |
| 90 | . 0044 | 1.256 | 69.1 | 1.279 | 67.7 | 1.273 | 66.4 | 1.266 | 65.0 | 1.259 | 63.7 | 1.252 | 62.4 |
| 91 | . 0045 | 1.331 | 69.4 | 1.324 | 63.0 | 1.317 | 66.7 | 1.311 | 65.3 | 1.304 | 64.0 | 1.297 | 62.7 |
| 92 | . 0046 | 1.377 | 69.7 | 1.370 | 68.3 | 1.363 | 67.0 | 1.357 | 65.6 | 1.850 | 64.3 | 1.343 | 63.1 |
|  | . 0047 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 | . 0048 | 1.425 | 69.9 | 1.418 | 68.6 | 1.411 | 67.2 | 1.404 | 6.3. 9 | 1.397 | 64.6 | 1.390 | 63.4 |
| 94 |  | 1.473 | 70.2 | 1.466 | 65.5 | 1.459 | 67.5 | 1.452 | 66.2 | 1.446 | 64.9 | 1.439 | 63.7 |
| 9.5 | . 0050 | 1.523 | 70.4 | 1.516 | 69.1 | 1.509 | 67.8 | 1.502 | 66.5 | 1.495 | 65.2 | 1.488 | 64.0 |
| 96 | . 0051 | 1.574 | 70.7 | 1.567 | 69.4 | 1.560 | 68.0 | 1.553 | 66.7 | 1.546 | 65.5 | 1.539 | 64.2 |
| 97 | .0053 | 1.627 | 70.9 | 1.620 | 69.6 | 1.613 | 68.3 | 1.606 | 67.0 | 1.599 | 65.8 | 1.592 | 64.5 |
| 98 | .0054 | 1.681 | 71.2 | 1.674 | 69.8 | 1.667 | 68.5 | 1.660 | 67.3 | 1.653 | 66.0 | 1.646 | 64.8 |
|  | . 0056 |  |  |  |  |  |  |  |  |  |  |  |  |
| 99 | . 0057 | 1.736 | 71.4 | 1.729 | 70.1 | 1.722 | 68.8 | 1.716 | 67.5 | 1.709 | 66.3 | 1.702 | 65.1 |
| 100 |  | 1.793 | 71.6 | 1.786 | 70.3 | 1.780 | 69.0 | 1.773 | 67.8 | 1.766 | 66.5 | 1.759 | 65.3 |
| 101 | . 0058 | 1.852 | 71.8 | 1.845 | 70.5 | 1.838 | 69.3 | 1.831 | 68.0 | 1.824 | 66.8 | 1.817 | 65.6 |
| 102 | . 0060 | 1.912 | 72.0 | 1.905 | 70.8 | 1.898 | 69.5 | 1.891 | 68.2 | 1.884 | 67.0 | 1.877 | 65.5 |
| 103 | .0062.0063 | 1.974 | 72.3 | 1.967 | 71.0 | 1.960 | 69.7 | 1.953 | 68.5 | 1.946 | 67.3 | 1.939 | 66.1 |
| 104 |  | 2.037 | 72.5 | 2.030 | 71.2 | 2.023 | 69.9 | 2.016 | 68.7 | 2.009 | 67.5 | 2.002 | 66.3 |

Mean IIorizontal Difference of Foree of Vapor for each $0^{\circ} .1=0.0013$.

Temperature, Falirenheit. - Force of Vapor in English Inches. - Relatire Humidity in Hundredths.

| $\begin{gathered} \text { Wet- } \\ \text { Bulb } \\ \text { Therino- } \\ \text { metter } \\ \text { t } \\ \text { Falirenn- } \\ \text { heit. } \end{gathered}$ | $\left\lvert\, \begin{gathered} \text { Mean } \\ \text { Yertical } \\ \text { Dinfferene } \\ \text { of Force } \\ \text { of Viper } \\ \text { for each } \\ 0^{\circ} .1 . \end{gathered}\right.$ | $\mathbf{t}$ - $\mathbf{t}$, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1200 |  | 120.5 |  | $13^{\circ}$. 0 |  | $13^{\circ} .5$ |  | 140.0 |  | 140.5 |  |
|  |  | $\begin{gathered} \text { Force of } \\ \text { Vapor: } \end{gathered}$ | $\left\lvert\, \begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Ilu- } \\ \text { mid- } \\ \text { ity } \end{gathered}\right.$ | $\begin{aligned} & \text { Force of } \\ & \text { Vapor. } \end{aligned}$ | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { llu- } \\ & \text { mill- } \\ & \text { ity } \end{aligned}$ | $\begin{aligned} & \text { Force of } \\ & \text { Vapor. } \end{aligned}$ | $\left\lvert\, \begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { 11u- } \\ \text { mid- } \\ \text { ity } \end{gathered}\right.$ | $\begin{gathered} \text { Force of } \\ \text { Vapor. } \end{gathered}$ | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Ilu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | $\left\lvert\, \begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { Mud } \\ \text { mity. } \end{gathered}\right.$ |
| $\bigcirc$ | 3.0007 | Eug. In. | 8.8 | Eng. In. |  | Eng In. |  | Eng In. |  | Eng. In. |  | Eng. In. |  |
| 32 |  | $10.025$ |  |  |  | 0.012 | 4.1 |  |  |  |  |  |  |
| 33 | . 0007 | 0.0:3 | 10.5 | 0.026 | 8.4 | 0.019 | 6.2 | 0.013 | 4.0 |  |  |  |  |
| 31 |  | 0.040 | 12.7 | 0.033: | 10.1 | 0.027 | 8.2 | 0.020 | 6.0 | 0.014 | . 1 |  |  |
| 35 | .0107 | 0.048 | 14.6 | 0.041 | 12.3 | 0.0344 | 10.1 | 0.02 b | 8.0 | 0.021 | 6.1 | 0.015 | 4.2 |
| 36 | .000s | 0.056 | 16.4 | 0.049 | 14.2 | 0.042 | 12.0 | 0.036 | 10.0 | 0.029 | 8.1 | 0.023 | 6.2 |
|  | .0008 |  |  |  |  |  |  |  |  |  |  |  |  |
| 37 | .0009 | 0.064 | 18.2 | 0.0.37 | 16.0 | 0.051 | 13.9 | 0.014 | 11.9 | 0.038 | 10.0 | 0.031 | 8.2 |
| 38 |  | 0.072 | 19.9 | 0.066 | 17.4 | 0.059 | 1.5 .7 | 0.053 | 13.7 | 0.046 | 11.9 | 0.040 | 10.1 |
| 39 | $.0009$ | 0.081 | 21.6 | 0.075 | 19.5 | 0.068 | 17.5 | 0.062 | 15.5 | 0.055 | 13.7 | 0.049 | 11.9 |
| 40 | $\begin{aligned} & .0009 \\ & .0010 \end{aligned}$ | 0.091 | 23.3 | 0.054 | 21.2 | 0.078 | 19.2 | 0.071 | 17.2 | 0.064 | 15.4 | 0.058 | 13.6 |
| 41 |  | 0.100 | 24.9 | 0.094 | 22.5 | 0.087 | 20.8 | 0.081 | 18.9 | 0.074 | 17.1 | 0.067 | 15.3 |
| 42 | . 0010 |  |  |  |  |  |  |  |  |  |  |  |  |
| 43 | . 0010 | 0.120 | 27.8 | 0.114 | 2.5.5 | 0.107 | 23.9 | 0.100 | 22.0 | 0.095 | 20.1 | 0.087 | 18.3 |
| 44 | . 0011 | 0.131 | 29.2 | 0.124 | 27.2 | 0.118 | 2.). 3 | 0.111 | 23.5 | 0.104 | 21.5 | 0.098 | 19.8 |
| 45 | .0011 | 0.112 | 30.5 | 0.135 | 25.6 | 0.129 | 26.7 | 0.122 | 24.9 | 0.115 | 22.9 | 0.109 | 21.2 |
| 46 | . 0011 | 0.153 | 31.8 | 0.146 | 30.0 | 0.140 | 25.1 | 0.133 | 26.3 | 0.127 | 24.3 | 0.119 | 22.7 |
| 47 | . 0012 | 0.16 .5 | 33.0 | 0.158 | 31.2 | 0.152 | 29.3 | 0.145 | 6 | 138 | 257 | 0.132 | 0 |
| 48 | . 0012 | 0.177 | 34.2 | 0.170 | 32.4 | 0.164 | 30.6 | 0.157 | 28.8 | 0.151 | 27.0 | 0.144 | 25.4 |
| 49 | . 0013 | 0.190 | 33.3 | 0.183 | 3:3.5 | 0.176 | 31.7 | 0.170 | 30.0 | 0.163 | 25.3 | 0.157 | 26.7 |
| 50 | . 1013 | 0.202 | 36.4 | 0.196 | 34.6 | 0.189 | 32.9 | 0.183 | 31.2 | 0.176 | 29.5 | 0.169 | 27.9 |
| 51 | . 0014 | 0.216 | 37.5 | 0.209 | 35.7 | 0.202 | 31.0 | 0.196 | 32.3 | 0.189 | 30.7 | 0.183 | 29.1 |
| 52 | . 0014 | 0.229 | 32.5 | 0.223 | 36.8 | 0.216 | 3.7. 1 | 0.210 | 33.4 | 0.203 | 31.8 | 0.196 | 30.2 |
| 53 | . 0014 | 0.244 | 39.5 | 0.237 | 37.8 | 0.2:31 | 36.1 | 0.224 | 34.5 | 0.217 | 32.9 | 0.211 | 31.4 |
| 5.4 | . 0015 | 0.259 | 40.5 | 0.252 | 35.5 | 0.24.) | 37.1 | 0.239 | 35.5 | 0.232 | 34.0 | 0.226 | 32.4 |
| 55 | . 0015 | 0.274 | 11.5) | 0.267 | 39.8 | 0.261 | 38.1 | 0.254 | 36.5 | 0.247 | 35.0 | 0.241 | 33.5 |
| 56 | . 0016 | 0.290 | 12.4 | 0.283 | 40.7 | 0.276 | 39.1 | 0.270 | 37.5 | 0.263 | 35.9 | 0.257 | 34.4 |
| 57 | . 0016 | 0.306 | 43.2 | 0.299 | 41.6 | 0.293 | 400 | 0.296 | 38.4 | 0.250 | 36.9 | 0.273 | 35.4 |
| 58 | . 0017 | 0.323 | 44.1 | 0.316 | 42.4 | 0.310 | 40.8 | 0.303 | 39.3 | 0.296 | 37.8 | 0.290 | 36.3 |
| 59 | . 0017 | 0.310 | 4.9 | 0.334 | 43.3 | 0.327 | 41.7 | 0.320 | 40.1 | 0.314 | 38.7 | 0.307 | 37.2 |
| 60 | . 0018 | 0.358 | 45.7 | 0.351 | 44.1 | 0.345 | 42.5 | 0.338 | 41.0 | 0.331 | 39.5 | 0.325 | 38.1 |
| 61 | .0018 | 0.376 | 46.4 | 0.370 | 4.4.9 | 0.363 | 43.3 | 0.3 .54 | 41.8 | 0.3 .50 | 40.3 | 0.343 | 35.9 |
| 62 | . 0019 | 0.396 | 47.2 | 0.389 | 45.6 | 0.392 | 44.1 | 0.376 | 42.6 | 0.369 | 11.2 | 0.362 | 39.8 |
| 63 | . 0020 | 0.415 | 47.7 | 0.409 | 46.4 | 0.402 | 41.5 | 0.395 | 43.4 | 0.389 | +1.9 | 0.382 | 40.6 |
| 64 | .0021 | 0.436 | 48.6 | 0.429 | 47.1 | 0.422 | 45.6 | 0.416 | 44.1 | 0.409 | 42.7 | 0.402 | 41.3 |
| 65 | .0021 | 0.457 | 49.3 | 0.450 | 47.8 | 0.44: | 46.3 | 0.437 | 4.8 | 0.431 | 43.4 | 0.423 | 42.1 |
| 66 | $\begin{aligned} & .024 \\ & .0023 \end{aligned}$ | 0.478 | 49.9 | 0.472 | 48.4 | 0.465 | 47.0 | 0.4 .58 | 45.5 | 0.452 | 4.1 | 0.445 | 42.8 |
| 67 |  | 0.501 | 50.6 | 0.494 | 49.1 | 0.457 | 47.6 | 0.481 | 46.2 | 0.474 | 4.8 | 0.467 | 43.5 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0013$. |  |  |  |  |  |  |  |  |  |  |  |  |  |

Temferature, Fahrenheit. - Force of Vapor in English Inches - Relative Humidity in Hundredths.

| $\begin{gathered} \text { Wet- } \\ \text { Mulb } \\ \text { Thermo- } \\ \text { meter } \\ \mathbf{t}^{\prime} \\ \text { Fahren- } \\ \text { heit. } \end{gathered}$ | $\begin{array}{\|c\|} \text { Mean } \\ \text { Vertical } \\ \text { Difference } \\ \text { of Force } \\ \text { of Vapor } \\ \text { for each } \\ 0.1 . \end{array}$ | $\mathbf{t - \mathbf { t } ^ { \prime }}$, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 120.0 |  | $12^{\circ} .5$ |  | $13^{\circ} 0$ |  | $13 \bigcirc .5$ |  | 140.0 |  | 140.5 |  |
|  |  | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { IIn- } \\ & \text { muid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { mid- } \\ \text { ity. } \end{gathered}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { 11u- } \\ & \text { 1nid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { IIu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { llu- } \\ & \text { mid- } \\ & \text { ity } \end{aligned}$ | Force of Vajor. | Relative Humid. ty. |
| $\bigcirc$ |  | Eng. In. |  | Eng. In. |  | Eng. In. |  | Eng. In. |  | g. In. |  | Eng In. |  |
| 68 | 0.0024 | 0.524 | 51.2 | 0.517 | 49.7 | 0.510 | 48.3 | 0.503 | 46.9 | 0.497 | 45.5 | 0.490 | 44.1 |
| 69 | . 002 | 0.547 | 51.8 | 0.541 | 50.3 | 0.534 | 48.9 | 0.527 | 47.5 | 0.520 | 46.1 | 0.514 | 44.8 |
| 70 | . 002 | 0.572 | 52.4 | 0.565 | 50.9 | 0.558 | 49.5 | 0.551 | 48.1 | 0.545 | 46.8 | 0.539 | 45.5 |
| 71 | . 0026 | 0.597 | 52.9 | 0.590 | 51.5 | 0.553 | 50.1 | 0.577 | 18.7 | 0.570 | 47.4 | 0.563 | 46.1 |
| 72 | .0020 | 0.623 | 53.5 | 0.616 | 22.1 | 0.609 | 50.7 | 0.603 | 49.3 | 0.596 | 48.0 | 0.589 | 46.7 |
|  | . 0026 |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 |  | 0.650 | 54.0 | 0.643 | 52.6 | 0.636 | 51.3 | 0.629 | 49.9 | 0.623 | 18.6 | 0.616 | 47.3 |
| 74 |  | 0.677 | 54.5 | 0.670 | 53.2 | 0.664 | 51.8 | 0.657 | 50.5 | 0.650 | 49.2 | 0.643 | 47.9 |
| 75 |  | 0.705 | 55.0 | 0.699 | 53.7 | 0.622 | 52.3 | 0.685 | 51.0 | 0.678 | 49.7 | 0.672 | 48.4 |
| 76 |  | 0.735 | 55.5 | 0.728 | 54.2 | 0.721 | 52.9 | 0.714 | 51.5 | 0.708 | 50.3 | 0.701 | 48.9 |
| 77 |  | 0.765 | 56.0 | 0.759 | 54.7 | 0.752 | 53.4 | 0.745 | 52.1 | 0.739 | 50.8 | 0.731 | 49.5 |
|  | . 0031 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 |  | 0.796 | 56.5 | 0.782 | 55.2 | 0.752 | 53.8 | 0.775 | 52.5 | 0.768 | 51.3 | 0.762 | 50.0 |
| 79 |  | 0.827 | 56.9 | 0.821 | 55.6 | 0.814 | 54.3 | 0.507 | 53.0 | 0.800 | 51.8 | 0.794 | 50.5 |
| 80 |  | 0.860 | 57.3 | 0.853 | 56.1 | 0.817 | 54.5 | 0.840 | 53.5 | 0.833 | 52.2 | 0.826 | 51.0 |
| 81 |  | 0.394 | 57.8 | 0.887 | 56.5 | 0.880 | 55.2 | 0.574 | 53.9 | 0.867 | 52.7 | 0.560 | 51.4 |
| 82 | .0035 | 0.929 | 58.2 | 0.922 | 56.9 | 0.915 | 55.6 | 0.909 | 54.4 | 0.902 | 53.2 | 0.895 | 51.9 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 |  | 0.965 | 58.6 | 0.958 | 57.3 | 0.951 | 56.1 | 0.944 | 54.8 | 0.937 | 53.6 | 0.931 | 52.4 |
| 84 |  | 1.002 | 59.0 | 0.995 | 57.7 | 0.988 | 56.5 | 0.981 | 55.2 | 0.974 | 54.0 | 0.968 | 52.8 |
| 85 |  | 1.039 | 59.4 | 1.033 | 58.1 | 1.026 | 56.8 | 1.019 | ธ5. 6 | 1.012 | 54.1 | 1.005 | 53.2 |
| 86 |  | 1.075 | 59.7 | 1.071 | 58.5 | 1.06 .5 | 57.2 | 1.058 | 56.0 | 1.051 | 54.8 | 1.044 | 53.6 |
| 87 |  | 1.119 | 60.1 | 1.112 | 58.5 | 1.105 | 57.6 | 1.099 | 56.4 | 1.092 | 55.2 | 1.085 | 54.0 |
|  | . 0041 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 |  | 1.159 | 5 | 1.152 | 2 | 1. | 58.0 | 1. | 56.8 | 1. | 5. | 1.125 | 54.4 |
| <9 |  | 1.202 | 60.9 | 1.19J | 59.6 | 1.188 | 58.3 | 1.181 | 57.1 | 1.174 | 56.0 | 1.167 | 54.8 |
| 90 |  | 1.245 | 61.3 | 1.238 | 59.9 | 1.251 | 58.7 | 1.225 | 57.5 | 1.218 | 56.3 | 1.211 | 55.2 |
| 91 |  | 1.290 | 61.6 | 1.283 | 60.2 | 1.276 | 59.0 | 1.269 | 57.9 | 1.263 | 66.7 | 1.256 | 55.6 |
| 92 |  | 1.336 | 61.9 | 1.329 | 60.6 | 1.322 | 59.4 | 1.315 | 55.2 | 1.309 | 57.0 | 1.302 | 55.9 |
|  | . 0047 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 |  | 1.383 | 62.2 | 1.376 | 60.9 | 1.370 | 59.7 | 1.363 | 58.5 | 1.356 | 57.4 | 1.349 | 56.3 |
| 94 |  | 1.432 | 62.5 | 1.425 | 61.2 | 1.418 | 60.0 | 1.411 | 58.9 | 1.404 | 57.7 | 1.897 | 56.6 |
| 95 | . 0050 | 1.482 | 62.7 | 1.475 | 61.5 | 1.468 | 60.4 | 1.461 | 59.2 | 1.454 | 55.1 | 1.447 | 57.0 |
| 96 | .00.31 | 1.533 | 63.0 | 1.526 | 61.8 | 1.519 | 60.7 | 1.512 | 59.5 | 1.505 | 58.4 | 1.498 | 57.3 |
| 97 | . 0052 | 1.585 | 63.3 | 1.578 | 62.1 | 1.571 | 61.0 | 1.564 | 59.5 | 1.558 | 58.7 | 1.551 | 57.6 |
| 98 | . 0054 | 1.639 | 63.6 | 1.632 | 62.4 | 1.625 | 61.3 | 1.618 | 60.1 | 1.612 | 59.0 | 1.605 | 57.9 |
| 99 | . 0056 | 1.695 | 63.9 | 1.688 | 62.7 | 1.681 | 61.6 | 1.674 | 60.4 | 1.667 | 59.3 | 1.660 | 58.2 |
| 100 | . 0057 | 1.752 | 64.2 | 1.745 | 63.0 | 1.735 | 62.0 | 1.731 | 60.7 | 1.724 | 59.6 | 1.717 | 55.5 |
| 101 | . 0059 | 1.810 | 64.4 | 1.803 | 63.2 | 1.797 | 62.3 | 1.790 | 61.0 | 1.783 | 59.9 | 1.776 | 58.8 |
| 102 | . 0060 | 1.870 | 64.7 | 1.863 | 63.5 | 1.857 | 62.6 | 1.850 | 61.3 | 1.543 | 60.2 | 1.836 | 59.1 |
| 103 | . 0062 | 1.932 | 64.9 | 1.925 | 63.8 | 1.918 | 62.9 | 1.911 | 61.5 | 1.90 .4 | 60.4 | 1.897 | 59.4 |
| 104 | . 0063 | 1.995 | 65.2 | 1.988 | 64.0 | 1.981 | 63.2 | 1.97\& | 61.8 | 1.967 | 60.7 | 1.960 | 59.6 |

[^3]Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Humidíty in Hundredths.


Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0013$.

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Mumidity in Hundredths.

| Wet-BulbThermo-metert $^{\prime}$Fahren-heit. | Mean Vertical Difference of Force of Vapor for each 0.1 . | $\mathbf{t}$ - $\mathbf{t}^{\prime}$, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 150.0 |  | $15^{\circ} .5$ |  | $16^{\circ} 0$ |  | $16^{\circ} .5$ |  | 180.0 |  | $17^{\circ} .5$ |  |
|  |  | Force of Vapor. | Relative Hu-midity | Force of Yapor. | Relative Hu-midity. | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | Relative Hu-midity. | Force of <br> Vapor | Relative Hu-midity. | Force of Vapor. | Rela. tive Ilu-midity |
| $\begin{gathered} 0 \\ 68 \\ 69 \\ 70 \\ 71 \\ 72 \end{gathered}$ | 0.0024 |  | 42 | Eng. In. $0.47 \%$ |  | Eng. In. $0.470$ |  | Eng. In. <br> 0.463 | 39. | Eng. In. <br> 0.456 | 37.9 | $\begin{gathered} \text { Eng. In. } \\ 0.450 \end{gathered}$ | 36.8 |
|  |  |  |  |  | 41. |  | 40.8 |  | 39. |  |  |  |  |
|  | .0024 | 0.507 | 43.5 | 0.500 | 42.3 | 0.594 | 41.0 | 0.487 | 39.8 | 0.480 | 38.7 | 0.473 | 37.5 |
|  |  | 0.531 | 44.2 | 0.524 | 42.9 | 0.518 | 41.7 | 0.511 | 40.5 | 0.504 | 39.3 | 0.495 | 38.2 |
|  | $\begin{aligned} & .0025 \\ & .0026 \end{aligned}$ | 0.556 | 44.8 | 0.5 .50 | 43.6 | 0.543 | 42.4 | 0.536 | 41.2 | 0.529 | 40.0 | 0.523 | 38.9 |
|  |  | 0.582 | 45.4 | 0.576 | 44.2 | 0.569 | 43.0 | 0.562 | 41.3 | 0.55 .5 | 40.7 | 0.549 | 39.5 |
|  | . 0027 |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | . 0028 | 0.609 | 46.0 | 0.602 | 44.8 | 0.596 | 43.6 | 0.589 | 42.4 | 0.582 | 41.3 | 0.575 | 40.2 |
| 74 |  | 0.637 | 46.6 | 0.630 | 45.4 | 0.623 | 44.2 | 0.616 | 43.0 | 0.610 | 41.9 | 0.603 | 40.8 |
| 75 | . 0028 | 0.665 | 47.2 | 0.655 | 46.0 | 0.6 .51 | 44.8 | 0.645 | 43.6 | 0.638 | 42.5 | 0.631 | 41.4 |
| 76 | .0029 | 0.694 | 47.7 | 0.687 | 46.5 | 0.651 | 45.4 | 0.674 | 44.2 | 0.667 | 43.1 | 0.660 | 42.0 |
| 77 | . 0030 | 0.721 | 48.2 | 0.717 | 47.1 | 0.711 | 45.9 | 0.704 | 44.8 | 0.697 | 43.6 | 0.690 | 42.6 |
| .0031 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | . 0032 | 0.755 | 48.8 | 0.748 | 47.6 | 0.741 | 46.4 | 0.735 | 45.3 | 0.728 | 44.2 | 0.721 | 43.1 |
| 79 |  | 0.787 | 49.3 | 0.780 | 48.1 | 0.773 | 47.0 | 0.766 | 45.8 | 0.760 | 44.7 | 0.753 | 43.7 |
| 80 | . 0033 | 0.820 | 49.8 | 0.813 | 48.6 | 0.806 | 47.5 | 0.799 | 46.4 | 0.792 | 45.3 | 0.786 | 44.2 |
| 81 | . 0034 | 0.853 | 50.3 | 0.517 | 49.1 | 0.840 | 48.0 | 0.833 | 46.9 | 0.526 | 45.8 | 0.519 | 44.6 |
| 82 | . 0035 | 0.858 | 50.7 | 0.831 | 49.6 | 0.875 | 48.5 | 0.863 | 47.4 | 0.861 | 46.3 | 0.854 | 45.1 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | . 0037 | 0.924 | 51.2 | 0.917 | 50.0 | 0.910 | 48.9 | 0.903 | 47.5 | 0.597 | 46.8 | 0.890 | 15.6 |
| 84 |  | 0.961 | 51.6 | 0.9 .54 | 50.5 | 0.947 | 19.4 | 0.940 | 48.3 | 0.933 | 47.2 | 0.927 | 46.2 |
| 85 | . 1038 | 0.998 | 52.1 | 0.992 | 50.9 | 0.985 | 49.8 | 0.973 | 48.7 | 0.971 | 47.7 | 0.96 .1 | 46.6 |
| 86 | . 0039 | 1.037 | 52.5 | 1.030 | 51.3 | 1.024 | 50.3 | 1.017 | 49.2 | 1.010 | 48.1 | 1.003 | 47.1 |
| 87 | . 0040 | 1.078 | 52.9 | 1.071 | 51.8 | 1.064 | 50.7 | 1.058 | 49.6 | 1.051 | 4 S .6 | 1.044 | 47.5 |
|  | . 0041 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 |  | 1.118 | 53.3 | 1.111 | 52.3 | 1.105 | 51.1 | 1.098 | 50.0 | 1.091 | 49.0 | 1.084 | 48.0 |
| 89 | . 0042 | 1.161 | 53.7 | 1.154 | 52.6 | 1.147 | 51.5 | 1.140 | 50.4 | 1.13: | 49.4 | 1.126 | 48.4 |
| 90 | . 0044 | 1.204 | 54.1 | 1.197 | 53.0 | 1.190 | 51.9 | 1.183 | 50.9 | 1.177 | 49.8 | 1.170 | 48.8 |
| 91 | . 0045 | 1.249 | 54.5 | 1.242 | 53.4 | 1.235 | 52.3 | 1.228 | 51.2 | 1.221 | 50.2 | 1.215 | 49.2 |
| 92 | . 0046 | 1.295 | 54.8 | 1.288 | 53.7 | 1.281 | 52.7 | 1.274 | 51.6 | 1.267 | 50.6 | 1.260 | 49.6 |
|  | . 0048 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 |  | 1.342 | 55.2 | 1.335 | 54.1 | 1.328 | 53.0 | 1.321 | 52.0 | 1.315 | 51.0 | 1.308 | 50.0 |
| 94 | . 0049 | 1.390 | 55.5 | 1.384 | 54.4 | 1.377 | 53.1 | 1.370 | 52.4 | 1.363 | 51.4 | 1.356 | 50.4 |
| 95 | . 00.50 | 1.440 | 55.9 | 1.433 | 54.8 | 1.126 | 53.7 | 1.420 | 52.7 | 1.413 | 51.7 | 1.406 | 50.7 |
| 96 | .0051 | 1.491 | 56.2 | 1.484 | 55.1 | 1.477 | jı. 1 | 1.471 | 53.1 | 1.464 | 52.1 | 1.457 | 51.1 |
| 97 | .0053 | 1.544 | 56.5 | 1.537 | 55.5 | 1.530 | 54.4 | 1.523 | $5: 3$ | 1.516 | 52.4 | 1.509 | 51.5 |
| 98 | . 0054 | 1.598 | 56.8 | 1.591 | 55.8 | 1.554 | 54.8 | 1.577 | 533. 6 | 1.570 | 52.8 | 1.563 | 51.8 |
|  | . 0056 |  |  |  |  |  |  |  |  |  |  |  |  |
| 99 |  | 1.6 .33 | 57.2 | 1.646 | 56.1 | 1.639 | 55.1 | 1.6:33 | 54.1 | 1.626 | 53.1 | 1.619 | 52.1 |
| 100 | . 0057 | 1.710 | 57.5 | 1.703 | 36.4 | 1.696 | 55.4 | 1.690 | 54.4 | 1.683 | 53.1 | 1.676 | 52.5 |
| 101 | . 0059 | 1.769 | 57.8 | 1.762 | 56.7 | 1.75.7 | 5.9 .7 | 1.743 | 54.7 | 1.74 I | 53.7 | 1.734 | 52.8 |
| 102 | . 0060 | 1.829 | 58.0 | 1.423 | 57.0 | 1.815 | . 6.0 | 1.809 | 55.0 | 1.802 | 54.0 | 1.794 | 53.1 |
| 103 | . 0062 | 1.890 | 58.3 | 1.883 | 57.3 | 1.576 | 56.7 | 1.869 | 55.3 | 1.863 | 51.3 | 1.856 | 53.4 |
| 104 | $.0063$ | 1.953 | 58.6 | 1.946 | 57.6 | 1.939 | 56.6 | 1.932 | 55.6 | 1.92.5 | 54.6 | 1.919 | 53.7 |

Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0913$.

Temptrature. Fabrenheit. - Foree of Tapor in English Inches. - Relative Humidity in Hundredths.


Temnerature, Fahrenheit. - Force of Vapor in English Inches - Relative Humidity in Hundredtha.

| Wet-BulbThermo-meter$t^{\prime}$Fehren-heit. | $\begin{gathered} \text { Mean } \\ \text { Yertical } \\ \text { Difference } \\ \text { of Force } \\ \text { of Vapor } \\ \text { for each } \\ 0^{\circ} .1 . \end{gathered}$ | $\mathbf{t - t ^ { \prime }}$, or Difference of Wet and Dry Buib Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 18.0 |  | 180.5 |  | $19^{\circ} .0$ |  | $19^{\circ} .5$ |  | $20^{\circ} .0$ |  | 20.5 |  |
|  |  | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { liu- } \\ & \text { mill- } \\ & \text { ity. } \end{aligned}$ | Force of Yapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Ifu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Fielative Hu midity. | Force of Vapor. | Relative Hu-midity. | Force of Vapor. | $\begin{aligned} & \text { Rola- } \\ & \text { tive } \\ & \text { IIu- } \\ & \text { mid- } \\ & \text { ity } \end{aligned}$ | Force of Vapor | Rela tive Ifumil. ity. |
| $\bigcirc$ |  | Eng. In. |  | Eng. In. |  | Eng. In. | $33.5$ | $\begin{aligned} & \overline{\text { Eng. In. }} \\ & 0 .+23 \end{aligned}$ |  | $\begin{gathered} \text { Eng ln. } \\ 0.416 \end{gathered}$ | $31.4$ | $\begin{array}{cc} \begin{array}{cc} \text { Eng In. } \\ 0.409 & 30.4 \end{array} \end{array}$ |  |
| 68 |  | 0.44:3 | 35.7 | 0.436 | 34.6 |  |  |  |  |  |  |  |  |
| 69 | 125 | 0.467 | 36.4 | 0.460 | 35. | 0.453 | 34.2 | 0.446 | 33.2 | 0.440 | 32.2 | 0.433 | 31.2 |
| 70 | . 0023 | 0.491 | 37.1 | 0.484 | 36.0 | 0.477 | 35.0 | 0.471 | 33.9 | 0.464 | 32.9 | 0.457 | 31.9 |
| 71 |  | 0.516 | 37.8 | 0.509 | 36.7 | 0.502 | 35.7 | 0.496 | 34.6 | 0.489 | 33.6 | 0.482 | 32.7 |
| 72 | . 0026 | 0.542 | 38.5 | 0.535 | 37.4 | 0.528 | 36.3 | 0.522 | 35.3 | 0.515 | 34.3 | 0.508 | 33.4 |
|  | . 0026 |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | . 0027 | 0.569 | 39.1 | 0.562 | 32.0 | 0.555 | 37.0 | 0.548 | 36.0 | 0.542 | 35.0 | 0.535 | 34.0 |
| 74 |  | 0.596 | 39.7 | 0.559 | 38.7 | 0.583 | 37.7 | 0.576 | 36.6 | 0.569 | 35.7 | 0.562 | 34.7 |
| 75 | . 0028 | 0.624 | 40.3 | 0.618 | 39.3 | 0.611 | 3s. 3 | 0.604 | 37.3 | 0.597 | 36.3 | 0.591 | 35.3 |
| 76 | $\begin{aligned} & .0029 \\ & .0030 \end{aligned}$ | 0.654 | 40.9 | 0.647 | 39.9 | 0.640 | 3 3.9 | 0.633 | 37.9 | 0.627 | 36.9 | 0.620 | 35.9 |
| 77 | . 0031 | 0.683 | 41.5 | 0.677 | 40.5 | 0.670 | 39.5 | 0.663 | 3-.5 | 0.656 | 37.5 | 0.650 | 36.5 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | .0032 | 0.714 | 42.1 | 0.707 | 41.0 | 0.701 | 40.0 | 0.694 | 39.0 | 0.657 | 38.1 | 0.680 | 37.1 |
| 79 |  | 0.746 | 42.6 | 0.739 | 11.6 | 0.732 | 40.6 | 0.726 | 39.6 | 0.719 | 38.6 | 0.712 | 37.7 |
| so | . 0033 | 0.779 | 43.2 | 0.752 | 42.1 | 0.765 | 41.1 | 0.758 | 40.2 | 0.752 | 39.2 | 0.745 | 35.3 |
| 81 | .n034 | 0.513 | 43.7 | 0.506 | 42.7 | 0.799 | 41.7 | 0.792 | 40.7 | 0.755 | 39.7 | 0.779 | 38.5 |
| 82 | . $003 \overline{5}$ | 0.547 | 44.2 | 0.840 | 43.2 | 0.834 | 42.2 | $0 . .27$ | 41.2 | 0.820 | 40.2 | 0.813 | 39.4 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | . 0036 | 0.853 | 4.7 | 0.876 | 43.7 | 0.869 | 42.7 | 0.663 | 41.7 | 0.656 | 40.7 | 0.549 | 39.9 |
| 84 |  | 0.920 | 45.2 | 0.918 | 4.2 | 0.906 | 13.2 | 0.899 | 42.2 | 0.593 | 41.3 | 0.856 | 40.4 |
| 85 | . 0038 | 0.958 | 45.6 | 0.9 .51 | +1.6 | 0.914 | 43.7 | 0.937 | 42.7 | 0.930 | 11.5 | 0.923 | 40.9 |
| 86 | .0639 | 0.996 | 16.1 | 0.989 | 45.1 | 0.983 | 4.1 | 0.976 | 43.2 | 0.969 | 42.3 | 0.962 | 41.3 |
| 87 | . 0040 . | 1.037 | 46.5 | 1.030 | 45.6 | 1.023 | 4.6 | 1.017 | 43.6 | 1.010 | 42.7 | 1.003 | 41.5 |
|  | -104 4 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 | . 0042 | 1.077 | 47.0 | 1.070 | 46.0 | 1.064 | 45.0 | 1.0 .57 | 44.1 | 1.050 | 43.2 | 1.043 | 42.3 |
| 89 |  | 1.119 | 17.4 | 1.113 | 46.4 | 1.106 | 45.5 | 1.099 | 44.5 | 1.092 | 43.6 | 1.055 | 42.7 |
| 90 | .0n 43 | 1.163 | 47.8 | 1.156 | 46.9 | 1.149 | 45.9 | 1.142 | 45.0 | 1.136 | 14.1 | 1.129 | 43.2 |
| 91 | $\begin{aligned} & .0045 \\ & .0047 \end{aligned}$ | 1.208 | 48.2 | 1.201 | 47.3 | 1.194 | 46.3 | 1.157 | 45.4 | 1.180 | 44.5 | 1.173 | 43.6 |
| 92 |  | 1.254 | 48.6 | 1.247 | 47.7 | 1.240 | 46.7 | 1.233 | 45.8 | 1.226 | +4.9 | 1.219 | 4.0 |
|  | . 0043 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 | . 0049 | 1.301 | 49.0 | 1.294 | 45.1 | 1.237 | 47.1 | 1.250 | 46.2 | 1.273 | 45.3 | 1.266 | 4.4 |
| 94 |  | 1.319 | 49.4 | $1.34{ }^{2}$ | 48.4 | 1.335 | 47.5 | 1.329 | 46.6 | 1.322 | 45.7 | 1.315 | 44.8 |
| 95 | .0050 | 1.399 | 49.8 | 1.392 | 48.5 | 1.385 | 47.9 | 1.375 | 47.0 | 1.371 | 46.1 | 1.364 | 45.2 |
| 96 | . 0051 | 1.450 | 50.1 | 1.443 | 49.2 | 1.436 | 45.3 | 1.429 | 47.3 | $1.4 \geq 2$ | 46.5 | 1.415 | 45.6 |
| 97 | . 0053 | 1.502 | 50.5 | 1.495 | 49.5 | 1.459 | 48.6 | 1.482 | 47.7 | 1.475 | 46.8 | 1.468 | 46.0 |
| 98 | .005 4 | 1.556 | 50.8 | 1.549 | 49.9 | 1.543 | 49.0 | 1.536 | 48.1 | 1.529 | 47.2 | 1.522 | 46.3 |
|  | . 0055 |  |  |  |  |  |  |  |  | 1.584 | 47 | 1.577 | 46.7 |
| 100 | . 0057 | 1.669 | 51.5 | 1.662 | 50.6 | 1.655 | 49.7 | 1.648 | 45.8 | 1.641 | 47.9 | 1.634 | 47.0 |
| 101 | . 0038 | 1.727 | 51.8 | 1.720 | 50.9 | 1.713 | 50.0 | 1.706 | 49.1 | 1.700 | 45.2 | 1.693 | 47.4 |
| 102 | . 0060 | 1.757 | 52.2 | 1.750 | 51.2 | 1.773 | 50.3 | 1.766 | 49.4 | 1.759 | 48.6 | 1.753 | 47.7 |
| 103 | .0062.0063 | 1.849 | 52.5 | 1.542 | 51.5 | 1.635 | 50.7 | 1.828 | 49.5 | 1.521 | 48.9 | 1.814 | 48.9 |
| 104 |  | 1.912 | 52.8 | 1.905 | 51.9 | 1.698 | 31.0 | 1.891 | 50.1 | 1.584 | 49.2 | 1.877 | 48.4 |

Mean Horizontal Difference of Force of Vapor for each $0^{\circ} .1=0.0013$.

Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Lumidity in Ifundrelths.


Temperature, Fahrenheit. - Force of Vapor in English Inches. - Relative Humidity in Hundredths.

| Wet-BulbThermo-metertFahren-heit. |  | $\mathbf{t}$ - $\mathbf{t}^{\prime}$, or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 210.0 |  | 210.5 |  | 240.0 |  | 220.5 |  | $\mathbf{2} \mathbf{3}^{\circ} \mathbf{0}$ |  | $23^{\circ} .5$ |  |
|  |  | $\begin{aligned} & \text { Force of } \\ & \text { Vapor. } \end{aligned}$ | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { IIn- } \\ & \text { mid- } \\ & \text { ity } \end{aligned}$ | $\begin{aligned} & \text { Force of } \\ & \text { Vapor. } \end{aligned}$ | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mini- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative Hu-midit $y$. | Force of Vapor. | Relative IIu. midity. | $\left\lvert\, \begin{aligned} & \text { Force of } \\ & \text { Vapor } \end{aligned}\right.$ | Relative Hu-midity. |
| - | 0.0024 |  |  | Eng. In. |  | Eng. In. |  | Eng. In. |  | Eng In. |  | Eug. In: |  |
| 68 |  | 0.403 | 29.5 |  | 28.5 | $0.3 \sim 9$ | 27.6 | 0.383 | 26.7 | 0.376 | 25.8 | 0.369 | 2.5 .0 |
| 69 | .0024 | 0.426 | 30.2 | 0.420 | 29.3 | 0.413 | 28.4 | 0.406 | 27.5 | 0.399 | 26.6 | 0.393 | 25.8 |
| 70 |  | 0.451 | 31.0 | 0.444 | 30.1 | 0.437 | 29.1 | 0.430 | 28.2 | 0.424 | 27.4 | 0.417 | 26.5 |
| 71 | . 0025 | 0.476 | 31.7 | 0.469 | 30.8 | 0.462 | 29.9 | 0.455 | 29.0 | 0.449 | 28.1 | 0.442 | . 27.3 |
| 72 | .0026 | 0.501 | 32.4 | 0.495 | 31.5 | 0.458 | 30.6 | 0.481 | 29.7 | 0.475 | 28.8 | 0.468 . | 28.0 |
|  | . 0027 |  |  | 0.501 |  | 0.515 | 31.3 | 0.508 | 30.1 | 501 | 29.5 | 1 | 28.7 |
| 7 | . 0023 | 0 | 3.8 .1 | 0.521 | 32.2 | 0.515 | 31.8 | 0.508 | 30.4 | 0.501 | 30.5 | 0.494 | 28.7 |
| 75 | . 0022 | 0.556 | 31.4 | 0.577 | 33.5 | 0.542 | 32.6 | 0.535 | 31.7 | 0.5.59 | 30.9 | 0.522 | 30.0 |
| 76 | $\begin{aligned} & .00 \cdot 9 \\ & .0030 \end{aligned}$ | 0.613 | 35.0 | 0.606 | 34.1 | 0.599 | 33.2 | 0.593 | 32.3 | 0.556 | 31.5 | 0.579 | 30.7 |
| 77 |  | 0.643 | 35.6 | 0.636 | 34.7 | 0.629 | 33.5 | 0.623 | 33.0 | 0.616 | 32.1 | 0.609 | 31.3 |
|  | . 0031 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | . 0032 | 0.674 | 36.2 | 0.667 | 35.3 | 0.660 | 34.4 | 0.653 | 33.6 | 0.647 | 32.7 | 0.640 | 31.9 |
| 79 |  | 0.705 | 36.5 | 0.699 | 35.9 | 0.692 | 35.0 | 0.685 | 34.2 | 0.678 | 33.3 | 0.671 | 32.5 |
| 80 | . 0033 | 0.738 | 37.4 | 0.731 | 36.5 | 0.724 | 3.9. 6 | 0.718 | 34.7 | 0.711 | 33.9 | 0.704 | 33.1 |
| 81 | .0034 | 0.752 | 37.9 | 0.765 | 37.0 | 0.758 | 36.1 | 0.751 | 35.3 | 0.745 | 34.5 | 0.738 | 33.5 |
| 82 | . 0035 | 0.806 | 38.4 | 0.500 | 37.6 | 0.793 | 36.7 | 0.756 | 35.8 | 0.779 | 35.0 | 0.772 | 34.2 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | .0037 | 0.842 | 39.0 | 0.535 | 38.1 | 0.829 | 37.2 | 0.822 | 36.4 | 0.815 | 35.5 | 0.808 | 34.7 |
| 84 |  | 0.579 | 39.5 | 0.572 | 35.6 | 0.865 | 37.7 | 0.858 | 36.9 | 0.552 | 36.1 | 0.845 | 35.2 |
| 85 | . 0038 | 0.917 | 40.0 | 0.910 | 39.1 | 0.903 | 38.2 | 0.896 | 37.4 | 0.589 | 36.6 | 0.882 | 35.8 |
| 86 | $\begin{aligned} & .0039 \\ & .0040 \end{aligned}$ | 0.955 | 40.4 | 0.445 | 39.6 | 0.942 | 38.7 | 0.935 | 37.9 | 0.923 | 37.1 | 0.921 | 36.3 |
| 87 |  | 0.995 | 40.9 | 0.988 | 40.1 | 0.981 | 39.2 | 0.975 | 38.4 | 0.968 | 37.5 | 0.961 | 36.7 |
|  | . 0041 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 | . 0042 | 1.036 | 41.4 | 1.029 | 40.5 | 1.022 | 39.7 | 1.016 | 38.8 | 1.009 | 38.0 | 1.002 | 37.2 |
| 89 |  | 1.078 | 41.8 | 1.071 | 41.0 | 1.065 | 40.1 | 1.058 | 39.3 | 1.051 | 38.5 | 1.044 | 37.7 |
| 90 | . 0044 | 1.122 | 4.3 | 1.115 | 41.1 | 1.108 | 40.6 | 1.101 | 39.7 | 1.094 | 38.9 | 1.085 | 38.1 |
| 91 | .0045 | 1.166 | 42.7 | 1.160 | 41.9 | 1.153 | 41.0 | 1.116 | 40.2 | 1.139 | 39.4 | 1.132 | 35.6 |
| 92 | . 0046 | 1.212 | 43.1 | 1.206 | 42.3 | 1.199 | 41.4 | 1.192 | 40.6 | 1.155 | 39.8 | 1.178 | 39.0 |
|  | . 0048 |  |  |  |  |  |  |  |  |  |  |  |  |
| 93 |  | 1.260 | 43.5 | 1.253 | 42.7 | 1.216 | 41.9 | 1.239 | 41.0 | 1.232 | 40.2 | 1.225 | 39.4 |
| 94 | . 0049 | 1.308 | 43.9 | 1.301 | 43.1 | 1.291 | 42.3 | 1.287 | 41.4 | 1.250 | 40.6 | 1.274 | 39.9 |
| 95 | .0050 | 1.353 | 41.3 | 1.351 | 43.5 | 1.344 | 42.7 | 1.337 | 41.8 | 1.330 | 41.0 | 1.323 | 40.3 |
| 96 | .0051 | 1.408 | 4.7 | 1.402 | 43.9 | 1.395 | 13.0 | 1.858 | 42.2 | 1.351 | 41.4 | 1.374 | 40.7 |
| 97 | $\begin{aligned} & .0053 \\ & .0054 \end{aligned}$ | 1.461 | +5. 1 | 1.454 | 44.3 | 1.447 | 43.4 | 1.440 | 12.6 | 1.133 | 41.8 | 1.426 | 41.1 |
| 98 |  | 1.515 | 45.5 | 1.508 | 44.6 | 1.501 | 43.5 | 1.494 | 43.0 | 1.487 | 42.2 | 1.480 | 41.4 |
|  | . 0056 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | . 0057 |  |  | 1.620 |  | 5 | 4.2 | 1.530 | 4.3 |  | 13.0 |  |  |
|  | . 0059 | 1.627 | 46.2 | 1.620 | 45.4 | 1.613 | 14.5 | 1.607 | 43.7 | 1.600 | 43.0 | 1.593 | 42.2 |
| 101 |  | 1.686 | 46.5 | 1.679 | 4.5 .7 | 1.672 | 44.9 | 166.5 | 44.1 | 1.6 .78 | 43.3 | 1.651 | 12.5 |
| 102 | . 0060 | 1.716 | 46.8 | 1.739 | 46.0 | 1.782 | 45.2 | 1.725 | 44.4 | 1.718 | 43.7 | 1.711 | 12.9 |
| 10:3 | .0062 | 1.807 | 47.2 | 1.400 | 46.4 | 1.793 | 45.6 | 1.786 | 4.8 | 1.779 | 44.0 | 1.772 | 43.2 |
| 104 | . 0063 | 1.870 | 47.5 | 1.863 | 46.7 | 1.856 | 45.9 | 1.849 | 45.1 | 1.542 | 4.3 | 1.435 | 43.6 |
|  |  |  | Hor | ntal 1 | ference | of Force | of Vapo | or for ea | $0^{\circ} .1=$ | $=0.0013$. |  |  |  |

Temperature, Fahrenheit. - Force of Vapor iu Euglish Inches. - Relative Humidity in Hundredths.


Temperature. Fahrenheit. - Foree of Vapor in English Inches. - Relative Mumidity in IIundredths.

| $\left\lvert\, \begin{gathered} \text { Wet- } \\ \text { Bulb } \\ \text { Themmo } \\ \text { meter } \\ \text { } \left.\begin{array}{c} \text { t } \\ \text { Faren- } \\ \text { heit. } \end{array} \right\rvert\, \end{gathered}\right.$ | MeanVerticalDiflerenceof Foreeof Vaporfor cach$0^{\circ} .1$. | t-t', or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 210.0 |  | 210.5 |  | 250.0 |  | $25^{\circ} .5$ |  | 126.0 |  | $26^{\circ} .5$ |  |
|  |  | $\left\lvert\, \begin{gathered} \text { Force of } \\ \text { Yapor. } \end{gathered}\right.$ | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Ifu- } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Int } \\ & \text { mid- } \\ & \text { ity. } \end{aligned}$ | Force of Vapor. | Relative ILu-midity. | Force of Vapor. | Relative In midity. | Force of Vapor. | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hu- } \\ & \text { mid- } \\ & \text { ity } \end{aligned}$ | Force of Vapor | Rela tive Hu* mid. ity. |
| $\stackrel{\circ}{68}$ | 0.0024 | $\left\lvert\, \begin{gathered} \text { Eng. In. } \\ 0.363 \end{gathered}\right.$ | 24.2 | Eng. In. <br> 0.356 |  | $\left\lvert\, \begin{gathered} \text { Eng. In. } \\ 0.349 \end{gathered}\right.$ | 22.5 | $\begin{aligned} & \text { Eng. In. } \\ & 0.342 \end{aligned}$ | 21.8 | Eng In. <br> 0.336 | 21.8 | $\begin{gathered} \text { Eng In. } \\ 0.329 \end{gathered}$ |  |
| 65 |  |  | 24.2 | 0.550 | 23.3 |  | 22.5 |  | 21.8 |  | 21.5 |  | 20.3 |
| 69 | . 0024 | 0.356 | 24.9 | 0.379 | 2.1 .1 | 0.373 | 23.3 | 0.366 | 22.6 | 0.359 | 21.8 | 0.352 | 21.1 |
| 70 |  | 0.410 | 25.7 | 0.403 | 24.9 | 0.397 | 24.1 | 0.390 | 23.3 | $0.3>3$ | 22.6 | 0.377 | 21.9 |
| 71 | $\begin{aligned} & .0025 \\ & .0026 \end{aligned}$ | 0.435 | 26.4 | 0.425 | 25.6 | 0.422 | 24.9 | 0.415 | 24.1 | 0.408 | 23.3 | 0.402 | 22.6 |
| 72 |  | 0.461 | 27.2 | 0.454 | 26.4 | 0.448 | 25.6 | 0.441 | 24.8 | 0.434 | 24.1 | 0.427 | 23.3 |
|  | .0027 |  |  |  |  |  |  |  |  |  |  |  |  |
| 73 | . 0028 | 0.188 | 27.9 | 0.481 | 27.1 | 0.474 | 26.3 | 0.467 | 25.5 | 0.461 | 24.8 | 0.454 | 24.0 |
| 74 |  | 0.515 | 25.5 | 0.505 | 27.7 | 0.502 | 27.0 | 0.495 | 26.2 | 0.488 | 25.5 | 0.481 | 24.7 |
| 75 | $.0028$ | 0.513 | 29.2 | 0.537 | 28.4 | 0.530 | 27.6 | 0.523 | 26.5 | 0.516 | 26.1 | 0.510 | 25.4 |
| 76 | .0029.0030 | 0.572 | 29.5 | 0.566 | 29.1 | 0.559 | 25.3 | 0.552 | 27.1 | 0.545 | 26.8 | 0.539 | 26.1 |
| 77 |  | 0.602 | 30.5 | 0.595 | 29.7 | 0.589 | 28.9 | 0.582 | 25.0 | 0.575 | 27.4 | 0.568 | 26.7 |
|  | . 0031 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78 | .0032 | 0.633 | 31.1 | 0.626 | 30.3 | 0.619 | 29.5 | 0.613 | 28.7 | 0.606 | 28.0 | 0.599 | 27.3 |
| 76 |  | 0.665 | 31.7 | 0.6 5̄ | 30.9 | 0.651 | 30.1 | 0.644 | 29.3 | 0.635 | 28.6 | 0.631 | 27.9 |
| 80 | $\begin{aligned} & .0033 \\ & .0034 \end{aligned}$ | 0.697 | 32.3 | 0.691 | 31.5 | 0.684 | 30.7 | 0.677 | 29.9 | 0.670 | 29.2 | 0.663 | 28.5 |
| 81 |  | 0.731 | 32.8 | 0.724 | 32.1 | 0.717 | 31.3 | 0.711 | 30.5 | 0.704 | 29.8 | 0.697 | 29.1 |
| 82 | . 0035 | 0.766 | 33.4 | 0.759 | 32.6 | 0.752 | 31.8 | 0.745 | 31.0 | 0.735 | 30.4 | 0.732 | 29.7 |
|  | . 0036 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83 | . 0037 | 0.501 | 33.9 | 0.795 | 33.2 | 0.788 | 32.4 | 0.781 | 31.6 | 0.774 | 30.9 | 0.767 | 30.2 |
| 84 |  | 0.538 | 34.5 | 0.831 | 33.7 | 0.824 | 32.9 | 0.818 | 32.1 | 0.511 | 31.5 | 0.804 | 30.7 |
| 85 | . 0038 | 0.876 | 35.0 | 0.869 | 34.2 | 0.862 | 33.4 | 0.85. | 32.7 | 0.848 | 32.0 | 0.842 | 31.3 |
| 86 | $\begin{aligned} & .0639 \\ & .00+0 \end{aligned}$ | 0.914 | 35.5 | 0.908 | 34.7 | 0.901 | 33.9 | 0.594 | 33.2 | 0.887 | 32.5 | 0.880 | 31.8 |
| 87 |  | 0.951 | 36.0 | 0.947 | 35.2 | 0.940 | 34.4 | 0.934 | 33.7 | 0.927 | 33.0 | 0.920 | 32.3 |
|  | . 0041 |  |  |  |  |  |  |  |  |  |  |  |  |
| 58 | .004.2 | 0.995 | 36.4 | 0.985 | 35.7 | 0.981 | 34.9 | 0.975 | 34.2 | 0.965 | 33.5 | 0.961 | 32.5 |
| 89 |  | 1.037 | 36.9 | 1.030 | 36.1 | 1.024 | 35.4 | 1.017 | 34.7 | 1.010 | 33.9 | 1.003 | 33.2 |
| 90 | . 0044 | 1.051 | 37.4 | 1.074 | 36.6 | 1.067 | 35.8 | 1.060 | 35.1 | 1.053 | 34.4 | 1.046 | 33.7 |
| 91 | . 0045 | 1.125 | 37.8 | 1.118 | 37.1 | 1.112 | 36.3 | 1.105 | 35.6 | 1.098 | 34.9 | 1.091 | 34.2 |
| 92 | . 0046 | 1.171 | 38.2 | 1.161 | 37.5 | 1.157 | 36.7 | 1.151 | 36.0 | 1.144 | 35.3 | 1.137 | 34.6 |
| 93 | . 0048 | 1.218 | 38.7 | 1.211 | 37.9 | 1.205 | 37.1 | 1.195 | 36.5 | 1.191 | 35.7 | 1.184 | 35.0 |
| 94 | . 0049 | 1.267 | 39.1 | 1.260 | 38.3 | 1.253 | 37.5 | 1.216 | 36.9 | 1.239 | 36.2 | 1.232 | 35.5 |
| 95 | .0050 | 1.316 | 39.5 | 1.309 | 38.7 | 1.302 | 37.9 | 1.296 | 37.3 | 1.289 | 36.6 | 1.282 | 35.9 |
| 96 | . 0051 | 1.367 | 39.9 | 1.360 | 39.1 | 1.353 | 38.3 | 1.346 | 37.7 | 1.340 | 37.0 | 1.333 | 36.3 |
| 97 | . 0053 | 1.420 | 40.3 | 1.413 | 39.5 | 1. 406 | 38.7 | 1.399 | 38.1 | 1.392 | 37.4 | 1.355 | 36.7 |
| 98 | . 0054 | 1.473 | 40.7 | 1.467 | 39.9 | 1.460 | 39.1 | 1.453 | 38.5 | 1.446 | 37.8 | 1.439 | 37.1 |
| 99 | . 0056 | 1.529 | 41.1 | 1.522 | 40.3 | 1.515 | 39.5 | 1.508 | 38.9 | 1.501 | 38.2 | 1.494 | 37.5 |
| 100 | .0657 | 1.586 | 41.4 | 1.579 | 40.7 | 1.572 | 39.9 | 1.565 | 39.2 | 1.558 | 38.5 | 1.551 | 37.9 |
| 101 | $.0059$ | 1.644 | 41.8 | 1.637 | 41.0 | 1.630 | 40.3 | 1.623 | 39.6 | 1.616 | 38.9 | 1.609 | 38.2 |
| 102 | . 0060 | 1.704 | 42.2 | 1.697 | 41.4 | 1.690 | 40.7 | 1.683 | 40.0 | 1.676 | 39.3 | 1.669 | 35.6 |
| 103 |  | 1.765 | 42.5 | 1.758 | 41.8 | 1.75 | 41.0 | 1.745 | 40.3 | 1.738 | 39.6 | 1.731 | 38.9 |
| 104 | . 0063 | 1.829 | 42.8 | 1.821 | 42.1 | 1.811 | 41.4 | 1.807 | 40.7 | 1.500 | 40.0 | 1.793 | 39.3 |
| Mean Horizontal Difference of Force of Vapor for eash $0^{\circ} .1=0.0013$. |  |  |  |  |  |  |  |  |  |  |  |  |  |

Temperature, Fahreuh it. - Force of Vapor in English Inches.-Relative Humidity in Inndredths.


Temperature, Fahrenheit.-Force of Vapor in English Inches.-Relative In midity in Hundredths,

| $\begin{gathered} \text { Wet- } \\ \text { Bulb } \\ \text { Thermin } \\ \text { meter } \\ t^{\prime} \\ \text { Faliren- } \\ \text { heit. } \end{gathered}$ | MeanVericalDitier-ence ofForee otHaporfor each$0^{\circ} .1$. | t-t', or Difference of Wet and Dry Bulb Thermometers. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 280.0 |  | 28.5 |  | 25.0 |  | 250.5 |  | 29.0 |  | 290.5 |  |
|  |  | $\begin{aligned} & \text { Force } \\ & \text { of } \\ & \text { of } \end{aligned}$ | $\left\lvert\, \begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { IIu- } \\ \text { midid- } \\ \text { ity. } \end{gathered}\right.$ | Force of Vapor. | $\begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hur } \\ \text { tuid- } \\ \text { ity. } \end{gathered}$ | Force ot Vapor. | $\begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { mid- } \\ \text { ity. } \end{gathered}$ | $\begin{aligned} & \text { Force } \\ & \text { of } \\ & \text { Vapor. } \end{aligned}$ | $\begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { Hitd- } \\ \text { ity. } \end{gathered}$ | $\begin{aligned} & \text { Force } \\ & \text { of } \\ & \text { fapor. } \end{aligned}$ | $\begin{gathered} \text { Rela- } \\ \text { tive } \\ \text { Hu- } \\ \text { mid- } \\ \text { ity. } \end{gathered}$ | $\begin{aligned} & \text { Force } \\ & \text { of } \\ & \text { Vapor. } \end{aligned}$ | $\begin{aligned} & \text { Rela- } \\ & \text { tive } \\ & \text { Hui- } \\ & \text { mind- } \\ & \text { ity. } \end{aligned}$ |
| $\bigcirc$ |  |  |  |  |  |  |  | Eng.In. |  |  |  | 5 |  |
| 68 |  | 0.302 | 19.5 | . 31 | 18.8 | . 309 | 18.2 | 302 | 17.5 | 0.295 | 16.9 | 9 | 6.2 |
| 69 |  | 0.34 | 20.3 | 0.339 | 19.6 | 0.332 | 19.0 | 0.325 | 18.3 | 0.319 | 17.7 | 0.312 | 7.0 |
| 70 | 0.002 | 0.37 | 21.1 | 0.363 | 20.4 | 0.356 | 19.7 | 0.350 | 19.1 | 0.343 | 18.4 | 0.336 | 17.8 |
| 71 | 0.0 | 0.39 | 21.9 | 0.388 | 21.2 | 0.381 | 20.5 | 0.375 | 19.8 | 0.368 | 19.2 | 0.361 | 18.5 |
| 72 | 0.0 | $0.4 * 1$ | 22.6 | 0.414 | 21.9 | 0.407 | 21.2 | 0.400 | 20.6 | 0.394 | 19.9 | 0.387 | 19.3 |
|  | 0.0027 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.0 |  |  |  |  |  |  |  |  |  |  |  | . 0 |
|  | 0.0 |  |  |  |  |  |  |  |  |  | 21.3 | 0.441 | 20.7 |
| 75 |  | 0.5 | 24.7 | 0.496 | 24.0 | 0.489 | 23.3 | 0.48 | 2.2 .6 | 0.476 | 22.0 | 1.469 | 21.4 |
| 76 |  | 0.532 | 25.3 | 0.525 | 24.6 | 0.518 | 24.0 | 0.511 | 23.3 | 0.505 | 22.7 | 0.498 | 22.0 |
| 77 |  | 0.562 | 26.0 | 0.555 | 25.3 | 0.548 | 24.6 | 0.541 | 23.9 | 0.535 | 23.3 | 0.528 | 22.7 |
| 78 | 0.0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 79 |  | 0.624 | 27.2 | 0.617 | 26.5 | 0.610 | . 8 | 0. | 25.2 | 0.597 | -4 | O... | 23.9 |
| 80 |  | 0.65 | 27.8 | 0.650 | 27.1 | 0.6i43 | 20.4 | 0.636 | 25.8 | 0.629 | 25.1 | 0.623 | 2.5 |
| 81 |  | 0.690 | 28.4 | 0.683 | 27.7 | 0.677 | 27.0 | 0.670 | 26.3 | 0.603 | 25.7 | 0.656 | 25.1 |
| 82 |  | 0.725 | 29.0 | 0.718 | 28.3 | 0.711 | 27.6 | 0.705 | 26.9 | 0.698 | 26.3 | 0.691 | 25.7 |
|  | 0.0036 |  |  | 0.754 | 28 |  |  |  |  |  |  |  |  |
| 84 | 0.0037 | 0.797 | 30.0 | 0.790 | 29.3 | 0.783 | 28.7 | 0.777 | 28.0 | 0. | 27.4 | 0.763 | 6. 5 |
| 85 | 0.0039 | 0.835 | 30.6 | 0.828 | 29.9 | 0.821 | 29.2 | 0.814 | 28.5 | 0.808 | 27.9 | 0.801 | 27.3 |
| 86 | 0.11 | 0.87 | 31.1 | 0.867 | 30.4 | 0.860 | 29.7 | 0.853 | 29.1 | 0.846 | 28.4 | 0.839 | 27.6 |
| 87 |  | 0.913 | 31.6 | 0.906 | 30.9 | 0.899 | 30.2 | 0.893 | 29.6 | 0.886 | 28.9 | 0.879 | 8.3 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 88 |  | 0.95 | 32.1 | 0.947 | 31.4 | 0.940 | 30.7 | 0.933 | 30.1 | 0.927 | 29.4 | 0.920 | 8.8 |
| 89 |  | 0.996 | 32.5 | 0.989 | 31.9 | 0.983 | 31.2 | 0.976 | 30.6 | 0.969 | 29.9 | 0.962 | 9.3 |
| 90 |  | 1.040 | 33.0 | 1.033 | 3ミ.3 | 1.026 | 31.7 | 1.019 | 31.0 | 1.012 | 30. | 1.005 | 29.8 |
| 91 |  | 1.084 | 33.5 | 1.077 | 32.8 | 1.070 | 32.1 | 1.064 | 31.5 | 1.057 | 30.9 | 1.050 | 30.3 |
| 92 |  | 1. | 33.9 | 1.123 | 33.2 | 1.116 | 32.6 | 1.109 | 31.9 | 1.103 | 31.3 | 1.096 | 30.7 |
|  | 0.0 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 1.218 |  |  |  |  |  |  |  |  | 31.2 |
|  | 0.00.50 |  |  | , |  |  |  |  |  |  |  | 1.191 | 31.6 |
|  | 0.0051 |  |  |  |  |  |  | 1. |  | 1.2 | 32.6 | 1.241 | 32.0 |
| 96 |  | 1.326 | 35.6 | 1.319 | 34.9 | 1.312 | 34.3 | 1.305 | 33.6 | 1.29 | 33.0 | 1.291 | 32.4 |
| 9 | 0.0054 | 1.378 | 36.0 | 1.371 | 35.3 | 1.364 | 347 | 1.357 | 34.0 | 1.351 | 33.4 | 1.344 | 32.8 |
| 98 | 0.005 | 1.432 | 36.4 | 1.425 | 35.7 | 1.418 | 35.1 | 1.411 | 34.4 | 1.404 | 33.5 | 1.398 | 33.2 |
|  | 0.005. |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 0.0057 |  |  | 1.480 | . 1 | 1.473 | 35.5 | 1.467 | 34.8 | 1.460 | 34.2 | 1.453 | 3.6 |
| 100 |  | 1.544 | 37.2 | 1.537 | 36.5 | 1.530 | 35.9 | 1.523 | 35.2 | 1.516 | 34.6 | 1.510 | 34.0 |
| 101 |  | 1.603 | 37.6 | 1.596 | 36.9 | 1.589 | 30.2 | 1.582 | 35.6 | 1.575 | 35.1 | 1.568 | 4. |
| 102 |  | 1.662 | 37.9 | 1.655 | 37.3 | 1.648 | 36.6 | 1.642 | 36.0 | 1.635 | 35.3 | 1.628 | 34.7 |
| 103 |  | 1.724 | 38.3 | 1.717 | 37.6 | 1.710 | 37.0 | 1.703 | 36.3 | 1.696 | 35.7 | 1.689 | 35.1 |
| 104 | 0.0063 | 1.787 | 38.6 | 1.779 | 38.0 | 1.773 | 37.3 | 1.766 | 36.7 | 1.759 | 36.1 | 1.752 | 35.5 |

Mean. Horizontal Difference of Force of Vapor for each $0^{0} .1=0.0013$.

Correction for Barometrical Height above or below the Normal Meight of 29.7 Inches.


## TABLE VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR FROM THE INDICATIONS, IN ENGLISH MEASURES, OF THE DEW-POINT INSTRUMENTS.

The object of every Dew-Point instrument is to ascertain, by causing a part of the apparatus to cool, the temperature at which the vapor contained in the air begins to condense, in the shape of light dew, on the cooled portion of the instrument. It is obvious that this is the temperature at which the atmosphere itself, if cooled likewise, would be fully saturated by the amount of vapor present in the air at the time of the observation.

The temperature of the dew-point being known, all the hygrometrical conditions of the air can be easily deduced from it.

The Absolute Humidity, or the total amount of vapor in the atmosphere, is expressed by the number, in the Tables of Elastic Forces of Vapor, due to that temperature.

The Relative Humidity, or the degree of moisture, being the ratio of the quantity of vapor actually contained in the air to the quantity it could contain if fully saturated, is expressed by the proportion

Relative Humidity : $1:$ : Force of Vapor at Dew-Point : Maximum Force of Vapor. Calling the

Force of Vapor at the Temperature of the Dew-Point, $f$;
Force of Vapor at the Temperature of the Air, F;
then

$$
\text { Relative Humidity }=\frac{f}{\mathrm{~F}}
$$

It is thus found by dividing the force of vapor due, in the Table of Elastic Forces, to the temperature of the dew-point, by the maximum of the force of vapor duc, in the same table, to the temperature of the air at the time of the observation. F being always greater than $f$, when the air is not saturated, the Relative Humidity is expressed by a fraction, which is termed the fraction of saturation. Making the point of saturation $=100$, in order to obtain this fraction in hundredths, we have

$$
\text { Relative Humidity }=\frac{f \times \mathbf{1 0 0}}{\mathcal{F}^{\prime}} \text {. }
$$

## Example.

Suppose the

| Temperature of the Air, or $\mathbf{t}$, to be | $=43^{\circ} \mathrm{F}$. |
| :--- | :--- |
| Temperature of the Dew-Point, or $\mathbf{t}^{\prime}$, to be | $=35^{\circ} \mathrm{F}$. |
| Difference between the two, or $\mathbf{t}-\mathbf{t}^{\prime}$, to be | $=8^{\circ} \mathrm{F}$. |

Taking in Table VI. the Elastic Forces due to $t$ and $\mathbf{t}^{\prime}$, we have
$\underset{\text { Force of Sapor at at } \mathbf{t}^{\prime}}{\begin{array}{l}\text { fare }\end{array}}=\frac{.2037 \times 100}{2750}=73.4$, Relative Humidity in Hundredths.
The following 'Table VIII. gives, in hundredths, the fraction of saturation, or Relative Humidity, corresponding to each degree of $t^{\prime}$, or of the temperature of the air, from $0^{\circ}$ to $104^{\circ}$; and for every half degree of $t-t^{\prime}$, or of the difference between the temperature of the air and of the dew-point, from $0 .{ }^{\circ} 5$ to $21 .{ }^{\circ} 5$. Regnault's Table of Elastic Forces of Vapor, reduced to English measures, has been used in the computation.

Though the fraction of saturation expressed in hundredths indicates the Relative Humidity with sufficient accuracy, the thousandths have been added to fucilitate, as remarked above in the preface to the Psychrometrical Tables, the interpolations for any number falling between those given in the table.

## Use of the Table. <br> Example.

| Temperature of Air, or $\mathbf{t}$, being | $=69^{\circ} \mathrm{F}$. |
| :--- | :--- |
| Temperature of the Dew-Point, or $\mathbf{t}^{\prime}$, | $=53^{\circ} \mathrm{F}$. |
| Difference, or $t-\mathbf{t}^{\prime}$, | $=9^{\circ} \mathrm{F}$. |

Find out the Relative Humidity.
In the column of temperatures, the first on the left, find $62^{\circ}$; on the same horizontal line, in the column headed $9^{\circ}$, is found $7 \times .4$, which is the Relative Humidity required.

Should it seem desirable to compute the Relative Humidity for values of $\mathbf{t}-\mathbf{t}^{\prime}$. not contained in the table, the factors given below in Table IX. may be used. It may be seen, however, that an interpolation at sight will always suffice for meteorological purposes.

## VIII.

FOR DEDUCING THE RELATIVE HUMIDITY OF THE AIR,

## FRON THE INDICATIONS OF DEW•POINT INSTRUMENTS.

Relative IIumidity expressed in IIundredths, full Saturation being $=100$.

| Temperature of Air, Fahreubeit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 |
| $0^{\circ}$ | 100. | 97.7 | 95.4 | 93.2 | 91.0 | 88.9 | 86.8 | 84.8 | 82.8 | と0.9 |
| 1 | 100. | 97.7 | 95.5 | 93.3 | 91.1 | 89.0 | 86.9 | 84.9 | 82.9 | 81.0 |
| 2 | 100. | 97.7 | 95.5 | 93.3 | 91.2 | 89.1 | 87.0 | 85.0 | \&3.0 | 81.1 |
| 3 | 100. | 97.8 | 95.5 | 93.4 | 91.2 | 89.2 | 87.1 | 85.1 | \&3.1 | 81.2 |
| 4 | 100. | 97.8 | 95.6 | 93.4 | 91.3 | 89.2 | 87.2 | 85.2 | 83.2 | 81.3 |
| 5 | 100. | 97.8 | 9.5 .6 | 93.5 | 91.4 | 89.3 | 87.3 | 85.3 | 83.3 | 81.4 |
| 6 | 100. | 97.8 | 9.5 .6 | 93.5 | 91.4 | 89.3 | 87.3 | と5.3 | 83.3 | 81.5 |
| 7 | 100. | 97.8 | 95.6 | 93.5 | 91.4 | 89.3 | 87.3 | 85.3 | 83. 4 | 81.5 |
| 8 | 100. | 97.8 | 95.6 | 93.5 | 91.3 | 89.3 | 87.3 | 85.3 | 83.4 | 81.5 |
| 9 | 100. | 97.8 | 95.6 | 93.5 | 91.3 | 89.3 | 87.3 | 85.3 | 83.4 | 81.5 |
| 10 | 100. | 97.8 | 95.6 | 93.1 | 91.3 | 89.3 | 87.3 | 85.3 | 83.4 | 81.5 |
| 11 | 100. | 97.8 | 95.6 | 93.4 | 91.3 | 89.3 | 87.3 | 85.3 | 83.4 | 81.6 |
| 12 | 100. | 97.8 | 95.5 | 93.4 | 91.3 | 89.3 | 87.3 | 85.4 | 83.4 | 81.6 |
| 13 | 100. | 97.8 | 95.5 | 93.4 | 91.3 | 89.3 | 57.3 | 85.4 | 83.5 | 81.6 |
| 14 | 100. | 97.7 | 95.5 | 93.4 | 91.3 | 89.3 | 87.3 | 85.4 | 83.5 | 81.7 |
| 15 | 100. | 97.7 | 9.5 .5 | 93.4 | 91.3 | 89.4 | 87.4 | 85.5 | 83.5 | 81.7 |
| 16 | 100. | 97.7 | 95.5 | 93.4 | 91.3 | 89.3 | 87.3 | 85.4 | 83.5 | 81.6 |
| 17 | 100. | 97.7 | 95.5 | 93.4 | 91.3 | 89.3 | 87.3 | 85.3 | 83.4 | 81.6 |
| 18 | 100. | 97.7 | 95.5 | 93.4 | 91.3 | 89.3 | 87.3 | 85.3 | 83.4 | 81.5 |
| 19 | 100. | 97.8 | 95.5 | 93.1 | 91.3 | 89.3 | 87.2 | 85.2 | 83.3 | 81.4 |
|  | 0.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 |


| Temperature of Air, Fahrenheit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5.0 | 5.5 | 6.0 | 6.5 | 7.0 | 7.5 | 8.0 | 8.5 | 9.0 | 9.5 |
| $0^{\circ}$ | 79.0 | 77.2 | 75.4 | 73.6 | 71.9 | 70.1 | 68.5 | 66.9 | 65.3 | 63.7 |
| 1 | 79.1 | 77.3 | 75.5 | 73.7 | 72.0 | 70.2 | 68.6 | 67.0 | 65.4 | 63.8 |
| 2 | 79.2 | 77.4 | 75.6 | 73.8 | 72.1 | 70.3 | 68.7 | 67.1 | 65.5 | 64.0 |
| 3 | 79.3 | 77.5 | 75.7 | 73.9 | 72.2 | 70.5 | 68.8 | 67.2 | 65.6 | 64.1 |
| 4 | 79.4 | 77.6 | 75.8 | 74.0 | 72.3 | 70.6 | 68.9 | 67.3 | 65.7 | 64.2 |
| 5 | 79.5 | 77.7 | 75.9 | 74.1 | 72.4 | 70.7 | 69.1 | 67.4 | 65.8 | 64.4 |
| 6 | 79.6 | 77.8 | 76.0 | 71.2 | 72.5 | 70.8 | 69.2 | 67.6 | 66.0 | 64.5 |
| 7 | 79.6 | 77.8 | 76.0 | 74.3 | 72.6 | 70.9 | 69.3 | 67.7 | 66.1 | 64.6 |
| S | 79.6 | 77.9 | 76.1 | 74.4 | 72.7 | 71.0 | 69.4 | 67.8 | 66.2 | 64.7 |
| 9 | 79.7 | 77.9 | 76.1 | 74.4 | 72.7 | 71.1 | 69.5 | 67.9 | 66.3 | 64.8 |
| 10 | 79.7 | 77.9 | 76.2 | 74.5 | 72.8 | 71.2 | 69.6 | 68.0 | 66.4 | 64.9 |
| 11 | 79.7 | 78.0 | 76.2 | 74.5 | 72.8 | 71.2 | 69.6 | 68.0 | 66.5 | 64.9 |
| 12 | 79.8 | 78.0 | 76.2 | 74.5 | 72.9 | 71.2 | 69.6 | 68.0 | 66.5 | 65.0 |
| 13 | 79.8 | 75.0 | 76.3 | 74.6 | 72.9 | 71.3 | 69.6 | 68.1 | 66.5 | 65.0 |
| 14 | 79.8 | 78.1 | 76.3 | 74.6 | 72.9 | 71.3 | 69.6 | 68.1 | 66.5 | 65.1 |
| 15 | 79.8 | 78.1 | 76.3 | 74.6 | 72.9 | 71.3 | 69.7 | 68.1 | 66.6 | 65.1 |
| 16 | 79.5 | 78.0 | 76.2 | 74.5 | 72.9 | 71.2 | 69.6 | 68.1 | 66.5 | 65.1 |
| 17 | 79.7 | 77.9 | 76.1 | 74.5 | 72.8 | 71.2 | 69.6 | 68.0 | 66.5 | 65.0 |
| 18 | 79.6 | 77.8 | 76.1 | 74.4 | 72.7 | 71.1 | 69.5 | 68.0 | 66.5 | 65.0 |
| 19 | 79.6 | 77.8 | 76.0 | 74.3 | 72.7 | 71.1 | 69.5 | 68.0 | 66.4 | 65.0 |
|  | 10.0 | 10.7 | 11.0 | 11.5 | 12.0 | 12.5 | 13.0 | 13.7 | 14.0 | 14.5 |
| $0^{\circ}$ | 62.1 | 60.7 | 59.2 | 57.7 | 56.3 | 54.9 | 53.6 | 52.3 | 51.0 | 49.8 |
| 1 | 62.3 | 60.8 | 59.3 | 57.9 | 56.5 | 55.1 | 53.7 | 52.5 | 51.2 | 50.0 |
| 2 | 62.4 | 61.0 | 59.5 | 58.1 | 56.6 | 55.3 | 53.9 | 52.7 | 51.4 | 50.1 |
| 3 | 62.6 | 61.1 | 59.6 | 58.2 | 56.8 | 5.5 .5 | 54.1 | 52.8 | 51.5 | 50.3 |
| 4 | 62.7 | 61.3 | 59.8 | 58.4 | 57.0 | 55.7 | 54.3 | 53.0 | 51.7 | 50.5 |
| 5 | 62.9 | 61.4 | 60.0 | 59.6 | 57.2 | 55.8 | 54.5 | 53.2 | 51.9 | 50.7 |
| 6 | 63.0 | 61.5 | 60.1 | 58.7 | 57.3 | 55.9 | 54.6 | 53.3 | 52.0 | 50.8 |
| 7 | 63.1 | 61.7 | 60.2 | 58.8 | 57.4 | 56.0 | 54.7 | 53.4 | 52.1 | 50.9 |
| 8 | 63.2 | 61.5 | 60.3 | 58.9 | 57.5 | 56.2 | 54.8 | 53.5 | 52.3 | 51.0 |
| 9 | 63.3 | 61.9 | 60.4 | 59.0 | 57.6 | 56.3 | 54.9 | 53.6 | 52.4 | 51.2 |
| 10 | 63.4 | 62.1 | 60.5 | 59.1 | 57.7 | 56.4 | 5.5 .0 | 53.8 | 52.5 | 51.3 |
| 11 | 63.5 | 62.1 | 60.6 | 59.2 | 57.8 | 56.5 | 55.1 | 53.9 | 52.6 | 51.4 |
| 12 | 63.5 | 62.1 | 60.6 | 59.3 | 57.9 | 56.6 | 55.2 | 54.0 | 52.7 | 51.5 |
| 13 | 63.5 | 622 | 60.7 | 59.3 | 58.0 | 56.6 | 55.3 | 54.1 | 52.8 | 51.6 |
| 11 | 63.6 | 62.3 | 60.8 | 59.4 | 58.1 | 56.7 | 55.4 | 54.2 | 52.9 | 51.7 |
| 15 | 63.6 | 62.3 | 60.8 | 59.5 | 58.1 | 56.8 | 55.5 | 54.3 | 53.0 | 51.8 |
| 16 | 63.6 | 62.3 | 60.8 | 59.5 | 55.1 | 56.3 | 55.5 | 54.3 | 53.0 | 51.8 |
| 17 | 63.6 | 6.2 | 60.8 | 59.4 | 58.1 | 56.7 | 55.5 | 54.2 | 53.0 | 51.8 |
| 18 | 63.5 | 62.2 | 60.7 | 59.4 | 58.0 | 56.7 | 55.1 | 54.2 | 53.0 | 51.8 |
| 19 | 63.5 | 62.1 | 60.7 | 59.3 | 58.0 | 56.6 | 55.4 | 54.2 | 52.9 | 51.8 |



| Temperature of Air, Fahrenheit. | $\mathbf{t} \mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 |
| $20^{\circ}$ | 100. | 97.8 | 95.6 | 93.4 | 91.3 | 89.2 | 87.2 | 85.2 | 83.2 | 81.3 |
| 21 | 100. | 97.8 | 95.6 | 93.4 | 91.3 | 89.3 | 87.3 | 85.3 | 83.3 | 81.5 |
| 22 | 100. | 97.8 | 95.6 | 93.5 | 91.4 | 89.3 | 87.3 | 85.4 | 83.4 | 81.6 |
| 23 | 100. | 97.8 | 95.6 | 93.5 | 91.4 | 89.4 | 87.4 | 8.5.5 | 83.5 | 81.7 |
| 24 | 100. | 97.8 | 95.7 | 93.5 | 91.5 | 89.5 | 87.5 | 85.5 | 83.6 | 81.8 |
| 25 | 100. | 97.8 | 95.7 | 93.6 | 91.5 | 89.5 | 87.6 | 85.6 | 83.7 | 81.9 |
| 26 | 100. | 97.8 | 95.7 | 93.6 | 91.6 | 89.6 | 87.7 | 85.7 | 83.8 | 82.0 |
| 27 | 100. | 97.9 | 95.8 | 93.7 | 91.7 | 89.7 | \$7.8 | 85.9 | 84.0 | 82.1 |
| 28 | 100. | 97.9 | 9.5 .8 | 93.8 | 91.8 | 89.8 | 87.9 | 86.0 | 84.1 | 82.3 |
| 29 | 100. | 97.9 | 95.9 | 93.8 | 91.8 | 89.9 | 88.0 | 86.1 | 84.2 | 82.4 |
| 30 | 100. | 97.9 | 95.9 | 93.9 | 91.9 | 90.0 | 88.1 | 86.2 | 84.3 | 82.5 |
| 31 | 100. | 98.0 | 96.0 | 94.0 | 92.0 | 90.1 | 88.2 | 86.4 | 84.5 | 82.7 |
| 32 | 100. | 98.0 | 96.0 | 94.0 | 92.1 | 90.2 | 88.4 | 86.6 | 84.7 | 83.0 |
| 33 | 100. | 98.0 | 96.1 | 94.1 | 92.2 | 90.4 | 88.6 | 86.7 | 84.9 | 83.2 |
| 34 | 100. | 98.0 | 96.1 | 94.2 | 92.3 | 90.5 | S8.7 | 86.9 | 85.1 | 83.4 |
| 35 | 100. | 98.0 | 96.1 | 94.3 | 92.4 | 90.6 | 88.9 | 87.1 | 85.3 | 83.6 |
| 36 | 100. | 98.1 | 96.2 | 94.3 | 92.5 | 90.7 | 85.9 | 87.1 | 85.4 | 83.7 |
| 37 | 100. | 98.1 | 96.2 | 94.3 | 92.5 | 90.7 | 88.9 | 87.2 | 85.4 | 83.7 |
| 39 | 100. | 98.1 | 96.2 | 94.3 | 92.5 | 90.7 | 89.0 | 87.2 | 85.5 | 83.8 |
| 39 | 100. | 98.1 | 96.2 | 94.3 | 92.5 | 90.7 | 89.0 | 87.2 | 85.5 | 83.9 |
| 40 | 100. | 98.1 | 96.2 | 94.4 | 92.5 | 90.8 | 89.0 | 87.3 | 85.6 | 83.9 |
| 41 | 100. | 98.1 | 96.2 | 9.4 .4 | 92.6 | 90.8 | 89.1 | 87.3 | 85.7 | 84.0 |
| 42 | 100. | 98.1 | 96.2 | 94.4 | 92.6 | 90.8 | 89.1 | 87.4 | 85.7 | 84.1 |
| 43 | 100. | 98.1 | 96.3 | 94.4 | 92.6 | 90.9 | 89.2 | 87.5 | 85.8 | 84.2 |
| 44 | 100. | $9 \mathrm{S}$. | 96.3 | 94.5 | 92.7 | 90.9 | 89.2 | 87.5 | 85.9 | 84.2 |
| 45 | 100. | 98.1 | 96.3 | 94.5 | 92.7 | 91.0 | 89.3 | 87.6 | 85.9 | 84.3 |
| 46 | 100. | 98.1 | 96.3 | 94.5 | 92.7 | 91.0 | 89.3 | 87.6 | 86.0 | 84.4 |
| 47 | 100. | 95.1 | 96.3 | 94.5 | 92.8 | 91.0 | 89.3 | 87.7 | 86.0 | 84.4 |
| 48 | 100. | 98.2 | 96.3 | 94.6 | 92.8 | 91.1 | 89.4 | 87.7 | 86.1 | 84.4 |
| 49 | 100. | 98.2 | 96.4 | 94.6 | 92.8 | 91.1 | 89.4 | 87.7 | 86.1 | 84.5 |
| 50 | 100. | 98.2 | 96.4 | 94.6 | 92.9 | 91.1 | 89.4 | 87.3 | 86.2 | 84.5 |
| 51 | 100. | 98.2 | 96.4 | 94.6 | 92.9 | 91.2 | 89.5 | 87.8 | 86.2 | S.4.6 |
| 52 | 100. | 98.2 | 96.4 | 94.6 | 92.9 | 91.2 | 89.5 | 87.9 | 86.3 | 84.7 |
| 53 | 100. | 98.2 | 96.4 | $9+.7$ | 92.9 | 91.2 | 89.6 | 87.9 | 86.3 | 84.7 |
| 54 | 100. | 98.2 | 96.4 | 94.7 | 93.0 | 91.3 | 89.6 | 88.0 | 86.4 | 84.8 |
| 55 | 100. | 98.2 | 96.5 | 94.7 | 93.0 | 91.3 | 89.7 | 88.0 | 86.4 | 81.8 |
| 56 | 100. | 98.2 | 96.5 | 94.7 | 93.0 | 91.4 | 89.7 | 88.1 | 86.5 | 84.9 |
| 57 | 100. | 98.2 | 96.5 | 94.8 | 93.1 | 91.4 | 89.7 | 88.1 | 86.5 | 85.0 |
| 55 | 100. | 93.2 | 96.5 | 9.4 .8 | 93.1 | 91.4 | 89.8 | 88.2 | 86.6 | 85.0 |
| 59 | 100. | 98.2 | 96.5 | 94.8 | 93.1 | 91.5 | 89.8 | 83.2 | 86.6 | 8.5 .1 |
| 60 | 100. | 98.2 | 96.5 | 94.8 | 93.2 | 91.5 | 89.9 | 88.3 | 86.7 | 8.5 .1 |
| 61 | 100. | 98.3 | 96.5 | 94.9 | 93.2 | 91.5 | 89.9 | 88.3 | 86.7 | 85.2 |
| 62 | 100. | 98.3 | 96.6 | 94.9 | 93.2 | 91.6 | 90.0 | 88.4 | 86.8 | 8.5 .3 |
|  | 0.0 | 0.5 | 1.6 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 |


| Temperature of Air, Fahren. heit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 0.5 | 1.0 | 1.5 | 2.1 | 2.5 | 3.0 | 3.5 | 4.9 | 4.5 |
| $62^{\circ}$ | 100. | 93.3 | 96.6 | 94.9 | 93.2 | 91.6 | 90.0 | 88.4 | 86.8 | 85.3 |
| 63 | 100. | 98.3 | 96.6 | 94.9 | 93.2 | 91.6 | 90.0 | 88.4 | 86.8 | 85.3 |
| 6.4 | 100. | 98.3 | 96.6 | 94.9 | 93.3 | 91.6 | 90.0 | 88.5 | 86.9 | 85.3 |
| 65 | 100. | 93.3 | 96.6 | 94.9 | 93.3 | 91.7 | 90.1 | 88.5 | 86.9 | 85.4 |
| 68 | 100. | 93.3 | 96.6 | 94.9 | 93.3 | 91.7 | 90.1 | 88.5 | 87.0 | 85.4 |
| 67 | 100. | 95.3 | 96.6 | 95.0 | 93.3 | 91.7 | 90.1 | 88.6 | 87.0 | 55.5 |
| 63 | 100. | 98.3 | 96.6 | 95.0 | 9:3.4 | 91.8 | 90.2 | 88.6 | 87.1 | 85.5 |
| 69 | 100. | 98.3 | 96.6 | 95.0 | 93.4 | 91.8 | 90.2 | 88.7 | 87.2 | 85.6 |
| 70 | 100. | 98.3 | 96.7 | 95.0 | 93.4 | 91.8 | 90.3 | 88.7 | 87.2 | 85.7 |
| 71 | 100. | 98.3 | 96.7 | 95.0 | 93.4 | 91.9 | 90.3 | 88.8 | 87.2 | 85.8 |
| 72 | 100. | 98.3 | 96.7 | 9.5 .1 | 93.5 | 91.9 | 90.3 | 88.8 | 87.3 | 85.8 |
| 73 | 100. | 98.3 | 96.7 | 9.5 | 93.5 | 91.9 | 90.4 | 88.8 | 87.3 | 85.9 |
| 74 | 100. | 98.3 | 96.7 | 9.9 .1 | 93.5 | 91.9 | 90.4 | 88.9 | 87.4 | 85.9 |
| 75 | 100. | 98.3 | 96.7 | 95.1 | 93.5 | 92.0 | 90.4 | 88.9 | 87.4 | 86.0 |
| 76 | 100. | 98.3 | 96.7 | 95.1 | 93.6 | 92.0 | 90.5 | S9.0 | 87.5 | 86.0 |
| 77 | 100. | 98.4 | 96.7 | 95.2 | 93.6 | 92.0 | 90.5 | 89.0 | 87.5 | 86.1 |
| 78 | 100. | 98.4 | 96.7 | 95.2 | 93.6 | 92.1 | 90.5 | 89.1 | S7.6 | 86.1 |
| 79 | 100. | 93.4 | 96.5 | 95.2 | 93.6 | 92.1 | 90.6 | 89.1 | 87.6 | 86.2 |
| s0 | 100. | 98.4 | 96.8 | 95.2 | 93.6 | 92.1 | 90.6 | 89.1 | 87.7 | 86.2 |
| 81 | 100. | 98.4 | 96.8 | 95.2 | 93.7 | 92.1 | 90.6 | 89.2 | 87.7 | 86.3 |
| 82 | 100. | 95.4 | 96.8 | 95.2 | 93.7 | 92.2 | 90.7 | 89.2 | 87.8 | 86.3 |
| 83 | 100. | 95.4 | 96.8 | 9.5 .3 | 93.7 | 92.2 | 90.7 | 89.3 | 87.8 | 86.4 |
| 84 | 100. | 95.1 | 96.8 | 95.3 | 93.7 | 92.2 | 90.8 | 89.3 | 87.8 | 86.4 |
| 85 | 100. | 98.4 | 96.8 | 95.3 | 93.8 | 9.3 | 90.8 | 89.3 | 57.9 | 86.5 |
| 86 | 100. | 98.4 | 96.8 | 95.3 | 93.8 | 92.3 | 90.8 | 89.4 | 87.9 | 86.5 |
| 87 | 100. | 95.4 | 96.9 | 95.3 | 93.8 | 92.3 | 90.9 | 89.4 | 88.0 | 86.6 |
| 88 | 100. | 98.4 | 96.9 | 95.3 | 93.8 | 92.3 | 90.9 | 89.4 | 88.0 | 86.6 |
| 89 | 100. | 98.4 | 96.9 | 95.4 | 93.9 | 92.4 | 90.9 | 89.5 | 88.1 | 86.7 |
| 90 | 100. | 98.4 | 96.9 | 95.4 | 93.9 | 92.4 | 91.0 | 89.5 | 88.1 | 86.7 |
| 91 | 100. | 98.4 | 96.9 | 95.4 | 93.9 | 92.4 | 91.0 | 89.6 | 88.2 | 86.8 |
| 92 | 100. | 98.5 | 96.9 | 95.4 | 93.9 | 92.5 | 91.0 | 89.6 | 88.2 | 86.8 |
| 93 | 100. | 98.5 | 96.9 | 95.4 | 93.9 | 92.5 | 91.1 | 89.6 | 88.2 | 86.9 |
| 94 | 100. | 98.5 | 96.9 | 95.4 | 94.0 | 92.5 | 91.1 | 89.7 | 88.3 | 86.9 |
| 95 | 100. | 95.5 | 97.0 | 95.5 | 94.0 | 92.5 | 91.1 | 89.7 | 88.3 | S7.0 |
| 96 | 100. | 95.5 | 97.0 | 95.5 | 9.4 .0 | 92.6 | 91.2 | 89.7 | 88.4 | 87.0 |
| 97 | 100. | 98.5 | 97.0 | 95.5 | 94.0 | 92.6 | 91.2 | 89.8 | 88.4 | 87.0 |
| 98 | 100. | 98.5 | 97.0 | 95.5 | 94.1 | 92.6 | 91.2 | 89.8 | 88.4 | 87.1 |
| 99 | 100. | 98.5 | 97.0 | 95.5 | 94.1 | 92.7 | 91.3 | 89.9 | 88.5 | S7.1 |
| 100 | 100. | 98.5 | 97.0 | 95.6 | 94.1 | 92.7 | 913 | 89.9 | S-. 5 | 87.2 |
| 101 | 100. | 98.5 | 97.0 | 95.6 | 94.1 | 92.7 | 91.3 | 89.9 | 88.6 | 87.2 |
| 102 | 100. | 98.5 | 97.0 | 95.6 | 94.2 | 92.7 | 91.4 | 90.0 | $8 \bigcirc .6$ | 87.3 |
| 103 | 100. | 98.5 | 97.0 | 95.6 | 94.2 | 92.5 | 91.1 | 90.0 | 88.7 | 87.3 |
| 104 | 100. | 95.5 | 97.0 | 95.6 | 94.2 | 92.5 | 91.4 | 90.0 | 88.7 | 87.4 |
|  | 0.0 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 |
| B |  |  |  |  | 81 |  |  |  |  |  |


| Temperature of Air, Fahrenheit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5.0 | 5.5 | 6.0 | 6.5 | 8.0 | 7.5 | 8.0 | 8.5 | 9.0 | 9.5 |
| $20^{\circ}$ | 79.3 | 77.7 | 75.9 | 74.2 | 72.6 | 71.0 | 69.4 | 67.9 | 66.4 | 64.9 |
| 21 | 79.6 | 77.8 | 76.0 | 74.3 | 72.7 | 71.1 | 69.5 | 68.0 | 66.4 | 65.0 |
| 2. | 79.7 | 77.9 | 76.1 | 74.4 | 72.8 | 71.2 | 69.6 | 68.0 | 66.5 | 65.0 |
| 23 | 79.8 | 78.0 | 76.2 | 74.6 | 72.9 | 71.3 | 69.6 | 68.1 | 66.5 | 65.0 |
| 21 | 79.9 | 73.1 | 76.4 | 74.7 | 73.0 | 71.4 | 69.7 | 68.1 | 66.6 | 65.1 |
| 25 | 80.0 | 78.2 | 76.5 | 74.5 | 73.1 | 71.5 | 69.8 | 68.2 | 66.6 | 65.1 |
| 26 | 80.2 | 78.4 | 76.6 | 74.9 | 73.2 | 71.7 | 70.0 | 68.4 | 66.8 | 65.3 |
| 27 | 80.3 | 78.5 | 76.5 | 75.1 | 78.4 | 71.8 | 70.1 | 68.6 | 67.0 | 65.5 |
| 28 | 80.5 | 78.7 | 76.9 | 75.2 | 73.6 | 72.0 | 70.3 | 68.8 | 67.2 | 65.7 |
| 29 | 80.6 | 75.8 | 77.1 | 75.4 | 73.7 | 72.1 | 70.5 | 68.9 | 67.4 | 65.9 |
| 30 | 80.7 | 78.9 | 77.2 | 75.6 | 73.9 | 72.3 | 70.7 | 69.1 | 67.6 | 66.1 |
| 31 | 81.0 | 79.2 | 77.5 | 75.8 | 74.2 | 72.6 | 71.0 | 69.4 | 67.9 | 66.4 |
| 32 | 81.2 | 79.4 | 77.7 | 76.1 | 74.4 | 72.8 | 71.3 | 69.7 | 68.2 | 66.7 |
| 33 | 81.4 | 79.7 | 75.0 | 76.4 | 74.7 | 73.1 | 71.5 | 70.0 | 68.5 | 67.0 |
| 31 | 81.7 | 79.9 | 78.3 | 76.6 | 75.0 | 73.4 | 71.8 | 70.3 | 68.8 | 67.3 |
| 35 | 81.9 | 80.2 | 78.5 | 76.9 | 75.3 | 73.7 | 72.1 | 70.6 | 69.1 | 67.6 |
| 36 | 82.0 | 80.3 | 78.6 | 77.0 | 7.9 .4 | 73.9 | 72.3 | 70.8 | 69.3 | 67.8 |
| 37 | 8.2 | 80.4 | 78.8 | 77.2 | 7.7 .6 | 74.0 | 72.5 | 71.0 | 69.5 | 68.1 |
| 35 | 82.1 | 80.5 | 78.9 | 77.3 | 75.8 | 74.2 | 72.7 | 71.2 | 69.8 | 68.3 |
| 39 | 82.2 | S0.6 | 79.0 | 77.4 | 75.9 | 74.4 | 72.9 | 71.5 | 70.0 | 68.6 |
| 40 | 82.3 | 80.7 | 79.1 | 77.6 | 76.1 | 74.6 | 73.2 | 71.7 | 70.2 | 68.8 |
| 41 | 82.4 | 80.8 | 79.2 | 77.7 | 76.2 | 74.7 | 73.2 | 71.8 | 70.3 | 68.9 |
| 42 | 82.5 | 80.9 | 79.3 | 77.8 | 76.3 | 74.8 | 73.3 | 71.9 | 70.5 | 69.0 |
| 43 | 82.5 | 80.9 | 79.4 | 77.9 | 76.4 | 74.9 | 73.4 | 72.0 | 70.6 | 69.2 |
| 44 | 82.6 | 81.0 | 79.5 | 78.0 | 76.5 | 75.0 | 73.5 | 72.1 | 70.7 | 69.3 |
| 45 | 82.7 | 81.1 | 79.6 | 78.0 | 76.5 | 75.1 | 73.6 | 72.2 | 70.8 | 69.1 |
| 46 | 82.8 | 81.2 | 79.6 | 78.1 | 76.6 | 7.5 .1 | 73.7 | 72.3 | 70.9 | 69.5 |
| 47 | 8.2 .9 | 81.2 | 79.7 | 78.2 | 76.7 | 7.3 .2 | 73.9 | 72.4 | 71.0 | 69.6 |
| 48 | 82.9 | 81.3 | 79.8 | 78.2 | 76.8 | 75.3 | 73.9 | 72.5 | 71.1 | 69.7 |
| 49 | 82.9 | 81.3 | 79.8 | 78.3 | 76.8 | 7.5 .1 | 74.0 | 72.6 | 71.2 | 69.8 |
| 50 | 83.0 | 81.4 | 79.9 | 78.4 | 76.9 | 75.5 | 74.0 | 72.7 | 71.3 | 69.9 |
| 51 | 83.0 | 81.5 | S0.0 | 78.5 | 77.0 | 75.5 | 74.1 | 72.8 | 71.4 | 70.0 |
| 52 | 83.1 | 81.5 | 80.0 | 78.5 | 77.1 | 7.9 .6 | 74.2 | 72.8 | 71.5 | 70.1 |
| 53 | 83.2 | 81.6 | 80.1 | 78.6 | 77.2 | 7.7 | 74.3 | 72.9 | 71.6 | 70.2 |
| 54 | 83.2 | S 1.7 | 80.2 | 78.7 | 77.2 | 7.5 .8 | 74.4 | 73.0 | 71.7 | 70.3 |
| 55 | 53.3 | 81.5 | 80.3 | 78.8 | 77.3 | 75.9 | 74.5 | 73.1 | 71.8 | 70.4 |
| 56 | 83.4 | 81.8 | 80.3 | 78.9 | 77.4 | 76.0 | 74.6 | 73.2 | 71.9 | 70.5 |
| 57 | 83.4 | 81.9 | 80.4 | 78.9 | 77.5 | 76.1 | 74.7 | 73.3 | 72.0 | 70.6 |
| 59 | $8: 3.5$ | 82.0 | 80.5 | 79.0 | 77.6 | 76.2 | 74.8 | 73.4 | 72.1 | 70.7 |
| 59 | 83.6 | 8.3 .0 | S0.6 | 79.1 | 77.7 | 76.2 | 71.9 | 73.5 | 72.2 | 70.9 |
| 60 | 83.6 | 82.1 | 80.6 | 79.2 | 77.7 | 76.3 | 75.0 | 73.6 | 72.3 | 71.0 |
| 61 | 83.7 | 82.2 | 80.7 | 79.2 | 77.8 | 76.4 | 75.0 | 73.7 | 72.4 | 71.0 |
| 62 | 83.7 | 8.2 .2 | 80.8 | 79.3 | 77.9 | 76.3 | 75.1 | 73.8 | 72.4 | 71.1 |
|  | 5.0 | 5.5 | 6.0 | 6. 5 | 7.0 | 7.5 | 8.0 | 8.5 | 3.0 | 9.5 |


| Temperature <br> of Air, <br> Fahrenheit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5.0 | 5.5 | 6.0 | 6.5 | 7.0 | 7.5 | 8.0 | 8.5 | 9.0 | 9.5 |
| $62^{\circ}$ | 83.7 | 8.2.2 | 50.8 | 79.3 | 77.9 | 76.5 | 75.1 | 73.8 | 72.4 | 71.1 |
| 63 | 83.8 | 82.3 | 80.8 | 79.4 | 78.0 | 76.6 | 75.2 | 73.9 | 72.5 | 71.2 |
| 64 | 83.9 | 82.4 | 80.9 | 79.5 | 78.1 | 76.7 | 75.3 | 74.0 | 72.6 | 71.3 |
| 65 | 83.9 | 82.4 | 81.0 | 79.6 | 78.1 | 76.8 | 75.4 | 74.0 | 72.7 | 71.4 |
| 66 | 84.0 | 82.5 | 81.1 | 79.6 | 78.2 | 76.8 | 75.5 | 74.1 | 72.8 | 71.5 |
| 67 | 84.0 | 82.6 | 81.1 | 79.7 | 78.3 | 76.9 | 75.6 | 74.2 | 72.9 | 71.6 |
| 63 | 84.1 | 82.6 | 81.2 | 79.8 | 78.4 | 77.0 | 75.7 | 74.3 | 73.0 | 71.7 |
| 69 | 84.2 | 82.7 | 81.3 | 79.9 | 78.5 | 77.1 | 75.7 | 74.4 | 73.1 | 71.8 |
| 70 | 84.2 | 82.8 | 81.3 | 79.9 | 78.5 | 77.2 | 75.8 | 74.5 | 73.2 | 71.9 |
| 71 | 84.3 | 82.8 | 81.4 | 80.0 | 78.6 | 77.3 | 75.9 | 74.6 | 73.3 | 72.0 |
| 72 | 84.3 | 82.9 | 81.5 | 80.1 | 78.7 | 77.3 | 76.0 | 74.7 | 73.4 | 72.1 |
| 73 | 84.4 | 83.0 | 81.5 | 80.1 | 78.7 | 77.4 | 76.1 | 74.8 | 73.5 | 72.2 |
| 74 | 84.5 | 83.0 | 81.6 | 80.2 | 78.8 | 77.5 | 76.2 | 74.9 | 73.6 | 72.3 |
| 75 | 84.5 | 83.1 | 81.7 | 80.3 | 78.9 | 77.6 | 76.2 | 74.9 | 73.7 | 72.4 |
| 76 | 84.6 | 83.1 | 81.7 | 80.4 | 75.9 | 77.7 | 76.3 | 75.0 | 73.7 | 72.5 |
| 77 | 84.6 | 83.2 | 81.8 | S0.4 | 79.0 | 77.7 | 76.4 | 75.1 | 73.8 | 72.6 |
| 79 | 84.7 | 83.3 | 81.9 | 80.5 | 79.1 | 77.8 | 76.5 | 75.2 | 73.9 | 72.7 |
| 79 | 84.7 | 83.3 | 81.9 | 80.6 | 79.1 | 77.9 | 76.6 | 75.3 | 74.0 | 72.8 |
| 80 | 84.8 | 83.4 | 82.0 | 80.6 | 79.2 | 78.0 | 76.7 | 75.4 | 74.1 | 72.9 |
| 81 | 84.9 | 83.5 | 82.1 | 80.7 | 79.3 | 73.0 | 76.7 | 75.5 | 74.2 | 73.0 |
| 82 | 84.9 | 83.5 | 82.1 | 80.8 | 79.4 | 78.1 | 76.8 | 75.5 | 74.3 | 73.0 |
| 83 | 85.0 | 83.6 | 82.2 | 80.8 | 79.4 | 78.2 | 76.9 | 75.6 | 74.4 | 73.1 |
| S4 | 85.0 | 83.6 | 82.3 | 80.9 | 79.5 | 78.3 | 77.0 | 75.7 | 74.5 | 73.2 |
| 85 | 8.5 .1 | 83.7 | 82.3 | 81.0 | 79.6 | 78.4 | 77.1 | 75.8 | 74.6 | 73.3 |
| 86 | 85.1 | 83.7 | 82.4 | 81.1 | 79.7 | 78.4 | 77.1 | 75.9 | 74.6 | 73.4 |
| 87 | 85.2 | 83.8 | 82.) | 81.1 | 79.8 | 78.5 | 77.2 | 76.0 | 74.7 | 73.5 |
| 88 | 8.5 .2 | 83.9 | 82.) | 81.2 | 79.9 | 78.6 | 77.3 | 76.1 | 74.8 | 73.6 |
| 89 | 85.3 | 83.9 | 82.6 | 81.3 | 79.9 | $7 \times .7$ | 77.4 | 76.1 | 74.9 | 73.7 |
| 90 | 85.3 | 84.0 | 82.6 | 81.3 | 80.0 | 78.7 | 77.5 | 76.2 | 75.0 | 73.8 |
| 91 | 85.4 | 84.0 | 82.7 | 81.1 | 80.1 | 78.5 | 77.5 | 76.3 | 75.1 | 73.9 |
| 92 | 85.4 | 84.1 | 82.8 | 81.5 | 80.2 | 78.9 | 77.6 | 76.4 | 75.2 | 74.0 |
| 93 | 85.5 | 84.2 | 82.8 | 81.5 | 80.2 | 79.0 | 77.7 | 76.5 | 75.2 | 74.0 |
| 94 | 8.5. 6 | 84.2 | 82.9 | 81.6 | 80.3 | 79.0 | 77.8 | 76.6 | 75.3 | 74.1 |
| 95 | 85.6 | 84.3 | 83.0 | 81.7 | 80.4 | 79.1 | 77.9 | 76.6 | 75.4 | 74.2 |
| 96 | 85.7 | 84.3 | 83.0 | 81.7 | 80.4 | 79.2 | 77.9 | 76.7 | 75.5 | 74.3 |
| 97 | 85.7 | 84.4 | 83.1 | 81.8 | 80.5 | 79.3 | 78.0 | 76.8 | 75.6 | 74.4 |
| 93 | 85.8 | 84.4 | 83.1 | 81.9 | 80.6 | 79.3 | 78.1 | 76.9 | 75.7 | 74.5 |
| 99 | 85.8 | 84.5 | 83.2 | 81.9 | 80.7 | 79.4 | 78.2 | 77.0 | 75.8 | 74.6 |
| 100 | 85.9 | 84.6 | 83.3 | 82.0 | 80.7 | 79.5 | 78.3 | 77.0 | 75.8 | 74.7 |
| 101 | 85.9 | 84.6 | 83.3 | 82.0 | 80.8 | 79.6 | 78.3 | 77.1 | 75.9 | 74.8 |
| 102 | 86.0 | 84.7 | 83.4 | 82.1 | 80.9 | 79.6 | 75.4 | 77.2 | 76.0 | 74.9 |
| 103 | 86.0 | 84.7 | 83.4 | 82.2 | 80.9 | 79.7 | 75.5 | 77.3 | 76.1 | 74.9 |
| 104 | 86.1 | 84.3 | 83.5 | 82.2 | 81.0 | 79.8 | 78.6 | 77.4 | 76.2 | 75.0 |
|  | 5.0 | 5.5 | 6.0 | 6.5 | 7.0 | 7.5 | 8.0 | 8.5 | 9.0 | 9.5 |


| $\begin{aligned} & \text { Temper- } \\ & \text { ature } \\ & \text { of Air, } \\ & \text { Fahr n- } \\ & \text { heit. } \end{aligned}$ | $\mathbf{t} \mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point.-Fabrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 10.5 | 11.0 | 11.5 | 12.0 | 1-2.5 | 13.0 | 13.5 | 14.0 | 14.5 |
| $20^{\circ}$ | 63..5 | 62.1 | 60.6 | 59.3 | 58.0 | 56.6 | 55.1 | 54.1 | 52.9 | 51.7 |
| 21 | 63.5 | 62.1 | 60.7 | 59.3 | 55.0 | 56.6 | 55.4 | 54.2 | 53.0 | 51.8 |
| 22 | 63.5 | 62.1 | 60.7 | 59.4 | 58.0 | 56.7 | 55.5 | 54.2 | 53.0 | 51.8 |
| 23 | 63.6 | 62.1 | 60.7 | 59.4 | 58.0 | 56.7 | 5.3.5 | 54.3 | 53.0 | 51.9 |
| 21 | 63.6 | 62.1 | 60.7 | 59.4 | 58.1 | 56.8 | 55.5 | 54.3 | 53.1 | 51.9 |
| 2.5 | 63.6 | 62.1 | 60.7 | 59.4 | 58.1 | 56.9 | 55.6 | 54.4 | 53.1 | 52.0 |
| 26 | 63.8 | 62.3 | 60.9 | 59.6 | 58.3 | 57.0 |  | 54.5 | 53.3 | 52.1 |
| 27 | 61.0 | 62.5 | 61.1 | 59.8 | 58.5 | 57.2 | 55.9 | 54.6 | 53.4 | 52.2 |
| 25 | 64.2 | 62.7 | 61.3 | 60.0 | 58.6 | 57.3 | 56.0 | 54.8 | 53.5 | 52.3 |
| 29 | 64.4 | 63.0 | 61.5 | 60.2 | 58.8 | 57.5 | 56.2 | 54.9 | 53.7 | 52.4 |
| 30 | 64.6 | 63.2 | 61.8 | 60.4 | 59.0 | 57.7 | 56.3 | 55.1 | 53.8 | 52.6 |
| 31 | 64.9 | 63.5 | 62.1 | 60.7 | 59.3 | 58.0 | 56.6 | 55.4 | 54.1 | 52.9 |
| 32 | 65.2 | 63.8 | 62.4 | 61.0 | 59.6 | 58.3 | 57.0 | 55.7 | 54.4 | 53.2 |
| 33 | 6.5 .5 | 64.1 | 62.7 | 61.3 | 59.9 | 58.6 | 57.3 | 56.0 | 54.7 | 53.5 |
| 34 | 65.8 | 64.4 | 63.0 | 61.6 | 60.2 | 55.9 | 57.6 | 56.3 | 55.0 | 53.8 |
| 3.5 | 66.1 | 64.7 | 63.3 | 61.9 | 60.5 | 59.2 | 57.9 | 56.6 | 55.4 | 54.1 |
| 36 | 66.4 | 64.9 | 63.5 | 62.1 | 60.8 | 59.5 | 58.2 | 56.9 | 55.6 | 51.4 |
| 37 | 66.6 | 6.9 .2 | 63.8 | 62.4 | 61.1 | 59.8 | 58.5 | 57.2 | 55.9 | 54.7 |
| 35 | 66.9 | 65.5) | 64.1 | 62.7 | 61.4 | 60.1 | $5 \times .8$ | 57.5 | 56.2 | 55.0 |
| 39 | 67.1 | 65.7 | 64.4 | 63.0 | 61.7 | 60.3 | 59.1 | 57.8 | 56.5 | 55.3 |
| 40 | 67.4 | 66.0 | 64.6 | 63.3 | 62.0 | 60.6 | 59.4 | 58.1 | 56.8 | 55.6 |
| 41 | 67.5 | 66.1 | 64.8 | 63.5 | 62.1 | 60.9 | 59.6 | 58.3 | 57.1 | 55.9 |
| 42 | 67.7 | 66.3 | 65.0 | 63.6 | 62.3 | 61.1 | 59.8 | 58.6 | 57.3 | 56.1 |
| 43 | 67.8 | 66.4 | 65.1 | 63.8 | 62.5 | 61.3 | 60.0 | 58.8 | 57.6 | 56.4 |
| 44 | 67.9 | 66.6 | 65.3 | 64.0 | 62.7 | 61.5 | 60.3 | 59.0 | 57.8 | 56.6 |
| 45 | 68.1 | 66.7 | 65.4 | 64.2 | 62.9 | 61.7 | 60.5 | 59.3 | 58.1 | 56.9 |
| 46 | 63.2 | 669 | 6.3 .6 | 64.3 | 63.0 | 61.8 | 60.6 | 59.4 | 58.2 | 57.0 |
| 47 | 65.3 | 67.0 | 65.7 | 64.4 | 63.2 | 61.9 | 60.7 | 59.5 | 58.3 | 57.2 |
| 48 | 68.4 | 67.1 | 65.5 | 64.5 | 633.3 | 62.0 | 60.8 | 59.6 | 58.5 | 57.3 |
| 49 | 68.5 | 67.2 | 67.9 | 61.6 | 63.4 | 62.1 | 61.0 | 59.8 | 58.6 | 57.4 |
| 50 | 63.6 | 67.3 | 66.0 | 64.7 | 63.5 | 62.2 | 61.1 | 59.9 | 58.7 | 57.6 |
| 51 | 68.7 | 67.4 | 66.1 | 64.9 | 63.6 | 62.4 | 61.2 | 60.0 | 58.9 | 57.7 |
| 52 | 65.5 | 67.5 | 66.2 | 65.0 | 63.7 | 62.5 | 61.3 | 60.1 | 59.0 | 57.5 |
| 53 | 68.9 | 67.6 | 66.4 | 65.1 | 63.9 | 62.6 | 61.4 | 60.3 | 59.1 | 58.0 |
| 54 | 69.0 | 67.7 | 66.5 | 65.2 | 64.0 | 62.7 | 61.6 | 60.4 | 59.2 | 58.1 |
| 55 | 69.1 | 67.5 | 66.6 | 65.3 | 64.1 | 62.9 | 61.7 | 60.5 | 59.4 | 58.2 |
| 56 | 69.2 | 67.9 | 66.7 | 65.4 | 64.2 | 63.0 | 61.8 | 60.6 | 59.5 | 58.4 |
| 57 | 69.3 | 69.1 | 66.8 | 65.6 | 64.3 | 63.1 | 61.9 | 60.8 | 59.6 | 58.5 |
| 59 | 69.5 | 68.2 | 66.9 | 65.7 | 61.4 | 63.2 | 62.1 | 60.9 | 59.8 | 58.6 |
| 59 | 69.6 | 68.3 | 67.0 | 65.8 | 64.6 | 63.4 | 62.2 | 61.0 | 59.9 | $588$ |
| 60 | 69.7 | 68.4 | 67.1 | 67.9 | 64.7 | 63.5 | 62.3 | 61.2 | 60.0 | 58.9 |
| 61 | 69.8 | 68.5 | 67.2 | 66.0 | 64.8 | 63.6 | 62.4 | 61.3 | 60.1 | 59.0 |
| 62 | 69.9 | 62.6 | 67.4 | 66.1 | 64.9 | 6:3.7 | 62.6 | 61.4 | 60.3 | 59.1 |
|  | 10.0 | 10.5 | 11.0 | 11.5 | 1 BO | 10.3.7 | 13.0 | 13.5 | 18.0 | 14.5 |
| B |  |  |  |  | 64 |  |  |  |  |  |


| Temperature of Air, Fahrenheit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10.0 | 10.5 | 11.0 | 11.5 | 12.0 | 12.5 | 13.0 | 13.5 | 14.0 | 14.5 |
| $62^{\circ}$ | 69.9 | 68.6 | 67.4 | 66.1 | 64.9 | 63.7 | 62.6 | 61.4 | 60.3 | 59.1 |
| 63 | 70.0 | 68.7 | 67.5 | 66.2 | 65.0 | 63.8 | 62.7 | 61.5 | 60.4 | 59.3 |
| 64 | 70.1 | 68.8 | 67.6 | 66.3 | 65.1 | 64.0 | 62.8 | 61.6 | 60.5 | 59.4 |
| 65 | 70.2 | 63.9 | 67.7 | 66.5 | 65.3 | 64.1 | 62.9 | 61.8 | 60.6 | 59.5 |
| 66 | 70.3 | 69.0 | 67.8 | 66.6 | 65.4 | 64.2 | 63.0 | 61.9 | 60.8 | 59.7 |
| 67 | 70.4 | 69.1 | 67.9 | 66.7 | 65.5 | 64.3 | 63.2 | 62.0 | 60.9 | 59.8 |
| 65 | 70.5 | 69.2 | 68.0 | 66.8 | 65.6 | 64.4 | 63.3 | 62.1 | 61.0 | 59.9 |
| 69 | 70.6 | 69.3 | 63.1 | 66.9 | 6.7.7 | 64.5 | 63.4 | 62.3 | 61.1 | 60.0 |
| 70 | 70.7 | 69.4 | 68.2 | 67.0 | 65.8 | 64.7 | 63.5 | 62.4 | 61.3 | 60.2 |
| 71 | 70.9 | 69.5 | 68.3 | 67.1 | 65.9 | 64.8 | 63.6 | 62.5 | 61.4 | 60.3 |
| 72 | 70.9 | 69.6 | 68.4 | 67.2 | 66.0 | 64.9 | 63.7 | 62.6 | 61.5 | 60.4 |
| 73 | 71.0 | 69.7 | 68.5 | 67.3 | 66.2 | 6.5 .0 | 6:3.9 | 62.7 | 61.6 | 60.5 |
| 74 | 71.1 | 69.8 | 68.6 | 67.4 | 66.3 | 6.9 .1 | 64.0 | 62.8 | 61.7 | 60.7 |
| 75 | 71.1 | 69.9 | 68.7 | 67.5 | 66.4 | 6.5 .2 | 64.1 | 63.0 | 61.9 | 60.8 |
| 76 | 71.2 | 70.0 | 68.8 | 67.6 | 66.5 | 65.3 | 64.2 | 63.1 | 62.0 | 60.9 |
| 77 | 71.3 | 70.1 | 68.9 | 67.8 | 66.6 | 65.5 | 64.3 | 63.2 | 62.1 | 61.0 |
| 78 | 71.4 | 70.2 | 69.0 | 67.9 | 66.7 | 65.6 | 64.4 | 63.3 | 62.2 | 61.1 |
| 79 | 71.5 | 70.3 | 69.1 | 68.0 | 66.8 | 6.7 .7 | 64.5 | 63.4 | 62.3 | 61.3 |
| 80 | 71.6 | 70.4 | 69.2 | 68.1 | 66.9 | 6.5 .8 | 64.7 | 63.6 | 62.5 | 61.4 |
| 81 | 71.7 | 70.5 | 69.3 | 68.2 | 67.0 | 65.9 | 64.8 | 63.7 | 62.6 | 61.5 |
| 82 | 71.8 | 70.6 | 69.4 | 68.3 | 67.1 | 66.0 | 64.9 | 63.8 | 62.7 | 61.6 |
| 83 | 71.9 | 70.7 | 69.) | 68.4 | 67.2 | 66.1 | 65.0 | 63.9 | 62.8 | 61.8 |
| St | 72.0 | 70.9 | 69.6 | 6.9.5 | 67.3 | 66.2 | 65.1 | 64.0 | 62.9 | 61.9 |
| 85 | 72.1 | 70.9 | 69.7 | 69.6 | 67.4 | 66.3 | 65.2 | 64.1 | 63.0 | 62.0 |
| 86 | 72.2 | 71.0 | 69.8 | 68.7 | 67.5 | 66.4 | 65.3 | 64.2 | 63.2 | 62.1 |
| 87 | 72.3 | 71.1 | 69.9 | 68.8 | 67.7 | 66.5 | 6.5 .4 | 64.4 | 63.3 | 62.2 |
| 88 | 72.4 | 71.2 | 70.0 | $6 \checkmark .9$ | 67.8 | 66.6 | 65.5 | 64.5 | 63.4 | 62.3 |
| 89 | 72.5 | 71.3 | 70.1 | 69.0 | 67.9 | 66.8 | 65.7 | 64.6 | 63.5 | 62.5 |
| 90 | 72.6 | 71.4 | 70.2 | 69.1 | 68.0 | 66.9 | 65.5 | 64.7 | 63.6 | 62.6 |
| 91 | 72.7 | 71.4 | 70.3 | 69.2 | 68.1 | 67.0 | 65.9 | 64.8 | 63.7 | 62.7 |
| 92 | 72.8 | 71.5 | 70.4 | 69.3 | 68.2 | 67.1 | 66.0 | 64.9 | 63.9 | 62.8 |
| 93 | 72.9 | 71.6 | 70.5 | 69.4 | 68.3 | 67.2 | 66.1 | 65.0 | 64.0 | 62.9 |
| 94 | 72.9 | 71.7 | 70.6 | 69.5 | 68.4 | 67.3 | 66.2 | 65.1 | 64.1 | 63.0 |
| 95 | 73.0 | 71.8 | 70.7 | 69.6 | 63.5 | 67.4 | 66.3 | 65.2 | 64.2 | 63.2 |
| 96 | 73.1 | 71.9 | 70.8 | 69.7 | 68.6 | 67.5 | 66.4 | 65.4 | 64.3 | 63.3 |
| 97 | 73.2 | 72.0 | 70.9 | 69.5 | 68.7 | 67.6 | 66.5 | 6.5 .5 | 64.4 | 63.4 |
| 93 | 73.3 | 72.1 | 71.0 | 69.9 | 68.5 | 67.7 | 66.6 | 65.6 | 64.5 | 63.5 |
| 99 | 73.4 | 72.3 | 71.1 | 70.0 | 68.9 | 67.8 | 66.7 | 6.5 .7 | 64.6 | 63.6 |
| 100 | 73.5 | 72.4 | 71.2 | 70.1 | 69.0 | 67.9 | 66.8 | 6.5 .8 | 64.8 | 6:3.7 |
| 101 | 73.6 | 72.5 | 71.3 | 70.2 | 69.1 | 68.0 | 67.0 | 6.5 .9 | 64.9 | 63.9 |
| 102 | 73.7 | 72.6 | 71.4 | 70.3 | 69.2 | 68.1 | 67.1 | 66.0 | 65.0 | 64.0 |
| 103 | 73.8 | 72.7 | 71.5 | 70.4 | 69.3 | 68.2 | 67.2 | 66.1 | 65.1 | 64.1 |
| 104 | 73.9 | 72.8 | 71.6 | 70.5 | 69.4 | 68.3 | 67.3 | 66.2 | 6.5 .2 | 64.2 |
|  | 10.0 | 10.5 | 11.0 | 1.1 .3 | 12.0 | 19.5 | 13.6 | 13.5 | 1. 1.0 | 14.3.5 |


| Temperature of Air , Fahrenheit. | $\mathbf{t}$ - $\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenbeit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15.0 | 15.5 | 16.0 | 16.5 | 18.0 | 17.5 | 18.0 | 18.5 | 19.0 | 18.5. |
| $20^{\circ}$ | 50.6 | 49.5 | 43.4 | 47.3 | 46.2 | 45.1 | 44.1 | 43.1 | 42.1 | 41.2 |
| 21 | 50.6 | 49.5 | 48.4 | +7.3 | 46.2 | 45.1 | 44.2 | 43.2 | 42.2 | 41.2 |
| 22 | 50.7 | 49.5 | 18.4 | 47.4 | 46.3 | 4.5 .2 | 44.2 | 43.2 | 42.2 | 41.3 |
| 23 | 50.7 | 49.6 | 48.5 | 47.4 | 46.3 | 45.2 | 44.2 | 43.3 | 42.3 | 41.3 |
| 24 | 50.7 | 49.6 | 48.5 | 17.4 | 46.4 | 45.3 | 44.3 | 43.3 | 42.3 | 41.4 |
| 2.5 | 50.8 | 49.7 | 18.5 | 47.5 | 46.4 | 45.4 | 44.3 | 43.3 | 42.4 | 41.4 |
| 26 | 50.9 | 49.9 | 48.6 | 47.6 | 46.5 | 45.4 | 44.4 | 43.4 | 42.4 | 41.5 |
| 27 | 51.0 | 49.9 | 48.7 | 47.7 | 46.6 | 4.5 .5 | 44.5 | 43.5 | 42.5 | 41.6 |
| 23 | 51.1 | 50.0 | 43.8 | 47.7 | 46.7 | 45.6 | 44.6 | 43.6 | 42.6 | 41.6 |
| 29 | 51.2 | 50.1 | 48.9 | 47.8 | 46.8 | 45.7 | 44.7 | 43.7 | 42.7 | 41.7 |
| 30 | 51.4 | 50.2 | 49.0 | 47.9 | 46.8 | 45.8 | 44.7 | 43.7 | 42.7 | 41.8 |
| 31 | 51.7 | 50.5 | 49.4 | 43.2 | 47.1 | 46.1 | 45.0 | 44.0 | 43.0 | 42.0 |
| 32 | 52.0 | 50.8 | 49.7 | 48.5 | 47.4 | 46.4 | 45.3 | 44.3 | 43.3 | 42.3 |
| 33 | 52.3 | 51.1 | 50.0 | 48.8 | 47.7 | 46.6 | 45.6 | 44.5 | 43.5 | 42.5 |
| 34 | 52.6 | 51.4 | 50.3 | 49.1 | 48.0 | 46.9 | 45.9 | 44.8 | 43.8 | 42.8 |
| 3.5 | 52.9 | 51.7 | 50.6 | 49.4 | 48.3 | 47.2 | 46.1 | 45.1 | 44.1 | 43.0 |
| 36 | 53.2 | 52.0 | 50.9 | 49.7 | 48.6 | 47.5 | 46.4 | 45.4 | 14.4 | 43.3 |
| 37 | 53.5 | 52.3 | 51.2 | 50.0 | 48.9 | 47.8 | 46.7 | 45.7 | 44.7 | 43.6 |
| 38 | 53.8 | 52.6 | 51.5 | 50.3 | 49.2 | 48.1 | 47.0 | 46.0 | 45.0 | 43.9 |
| 39 | 54.1 | 52.9 | 51.3 | 50.6 | 49.5 | 48.4 | 47.3 | 46.3 | 45.3 | 4.4 .2 |
| 40 | 54.4 | 53.2 | 52.1 | 50.9 | 49.8 | 48.7 | 47.6 | 46.6 | 4.7 .6 | 44.5 |
| 41 | 54.7 | 53.5 | 52.3 | 51.2 | 50.1 | 49.0 | 47.9 | 46.9 | 45.8 | 44.8 |
| 42 | 51.9 | 53.8 | 52.6 | 51.5 | 50.4 | 49.3 | 48.2 | 47.2 | 46.1 | 45.1 |
| 43 | 5.5 .2 | 54.0 | 52.9 | 51.8 | 50.7 | 49.6 | 48.5 | 47.5 | 46.4 | 45.4 |
| 44 | 55.5 | 54.3 | 53.2 | 52.1 | 50.9 | 49.9 | 48.8 | 47.7 | 46.7 | 45.7 |
| 45 | 53.7 | 54.6 | 53.4 | 52.3 | 51.2 | 50.2 | 49.1 | 48.0 | 47.0 | 46.0 |
| 46 | 5.5 .9 | $5+7$ | 53.6 | 52.5 | 51.4 | 50.4 | 49.3 | 48.3 | 47.2 | 46.2 |
| 47 | 56.0 | 54.9 | 53.8 | 52.7 | 51.6 | 50.6 | 49.5 | 48.5 | 47.5 | 46.5 |
| 18 | 56.2 | 55.0 | 54.0 | 52.9 | 51.8 | 50.8 | 49.8 | 48.7 | 47.7 | 46.7 |
| 49 | 56.3 | 55.2 | 51.1 | 53.1 | 52.0 | 51.0 | 50.0 | 49.0 | 47.9 | 47.0 |
| 50 | 56.5 | 55.1 | 51.3 | 53.2 | 52.2 | 51.2 | 50.2 | 49.2 | 48.2 | 47.2 |
| 51 | 56.6 | 5.5 .5 | 51.4 | 53.4 | 52.3 | 51.3 | 50.3 | 49.3 | 48.3 | 47.4 |
| 52 | 56.7 | 5.5 .6 | 54.6 | 53.5 | 52.5 | 51.5 | 50.5 | 49.5 | 48.5 | 47.5 |
| 53 | 58.9 | 5.5 .8 | 54.7 | 53.6 | 52.6 | 51.6 | 50.6 | 49.6 | 48.6 | 47.7 |
| 54 | 57.0 | 55.9 | 54.8 | 53.8 | 52.7 | 51.7 | 50.7 | 49.8 | 48.8 | 47.8 |
| 55 | 57.1 | 56.0 | 5.5 .0 | 53.9 | 52.9 | 51.9 | 50.9 | 49.9 | 48.9 | 48.0 |
| 56 | 57.3 | 56.2 | 55.1 | 54.1 | 53.0 | 52.0 | 51.0 | 50.0 | 49.1 | 48.1 |
| 57 | 57.4 | 56.3 | 55.2 | 54.2 | 53.2 | 52.2 | 51.2 | 50.2 | 49.2 | 48.3 |
| 53 | 57.5 | 56.4 | 5.5 .4 | 54.3 | 53.3 | 52.3 | 51.3 | 50.3 | 49.4 | 48.4 |
| 59 | 57.7 | 56.6 | 5.5 .5 | 54.5 | 53.4 | 52.4 | 51.4 | 50.5 | 49.5 | 486 |
| 60 | 57.8 | 56.7 | 55.6 | 54.6 | 53.6 | 52.6 | 51.6 | 50.6 | 49.7 | 48.7 |
| 61 | 57.9 | 56.8 | 5.5 .8 | 54.7 | 53.7 | 52.7 | 51.7 | 50.8 | 49.8 | 48.9 |
| 62 | 58.0 | 57.0 | 5.5 .9 | 54.9 | 53.8 | 52.8 | 51.9 | 50.9 | 49.9 | 49.0 |
|  | 1.5.0 | 15.5 | 16.0 | 16.5 | 17.0 | 17.5 | 18.0 | 18.5 | 19.0 | 19.5 |


| Temperature of Air, Fahrenheit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of 'Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 15.0 | 15.5 | 16.0 | 16.5 | 17.0 | 17.5 | 18.0 | 18.5 | 19.0 | 19.5 |
| $62^{\circ}$ | 58.0 | 57.0 | 55.9 | 54.9 | 53.8 | 52.8 | 51.9 | 50.9 | 49.9 | 49.0 |
| 63 | 58.2 | 57.1 | 56.0 | 55.0 | 54.0 | 53.0 | 52.0 | 51.0 | 50.1 | 49.1 |
| 64 | 58.3 | 57.2 | 56.2 | 55.1 | 54.1 | 53.1 | 52.1 | 51.2 | 50.2 | 49.3 |
| 65 | 58.4 | 57.4 | 56.3 | 55.3 | 54.3 | 53.3 | 52.3 | 51.3 | 50.4 | 49.4 |
| 66 | 58.6 | 57.5 | 56.4 | 55.4 | 54.4 | 53.4 | 52.4 | 51.5 | 50.5 | 49.6 |
| 67 | 58.7 | 57.6 | 56.6 | 55.5 | 54.5 | 53.5 | 52.6 | 51.6 | 50.6 | 49.7 |
| 68 | 58.8 | 57.8 | 56.7 | 55.7 | 54.7 | 53.7 | 52.7 | 51.7 | 50.8 | 49.9 |
| 69 | 59.0 | 57.9 | 56.8 | 55.8 | 54.8 | 53.8 | 52.8 | 51.9 | 50.9 | 50.0 |
| 70 | 59.1 | 58.0 | 57.0 | 55.9 | 54.9 | 53.9 | 53.0 | 52.0 | 51.1 | 50.1 |
| 71 | 59.2 | 58.2 | 57.1 | 56.1 | 55.1 | 54.1 | 53.1 | 52.1 | 51.2 | 50.3 |
| 72 | 59.3 | 58.3 | 57.2 | 56.2 | 55.2 | 54.2 | 53.2 | 52.3 | 51.3 | 50.4 |
| 73 | 59.5 | 58.4 | 57.4 | 56.3 | 55.3 | 54.3 | 53.4 | 52.4 | 51.5 | 50.6 |
| 74 | 59.6 | 58.5 | 57.5 | 56.5 | 55.5 | 54.5 | 53.5 | 52.6 | 51.6 | 50.7 |
| 75 | 59.7 | 55.7 | 57.6 | 56.6 | 55.6 | 54.6 | 53.6 | 52.7 | 51.7 | 50.8 |
| 76 | 59.8 | 58.8 | 57.8 | 56.7 | 55.7 | 54.7 | 53.8 | 52.8 | 51.9 | 51.0 |
| 77 | 60.0 | 58.9 | 57.9 | 56.9 | 55.9 | 54.9 | 53.9 | 530 | 52.0 | 51.1 |
| 78 | 60.1 | 59.1 | 58.0 | 57.0 | 56.0 | 55.0 | 54.0 | 53.1 | 52.2 | 51.2 |
| 79 | 60.2 | 59.2 | 58.1 | 57.1 | 56.1 | 55.1 | 54.2 | 53.2 | 52.3 | 51.4 |
| 80 | 60.3 | 59.3 | 58.3 | 57.3 | 56.3 | 55.3 | 54.3 | 53.4 | 52.4 | 51.5 |
| 81 | 60.5 | 59.4 | 58.4 | 57.4 | 56.4 | 55.4 | 54.5 | 53.5 | 52.6 | 51.7 |
| 82 | 60.6 | 59.6 | 58.5 | 57.5 | 56.5 | 55.5 | 54.6 | 53.6 | 52.7 | 51.8 |
| 83 | 60.7 | 59.7 | 58.6 | 57.6 | 56.6 | 55.7 | 54.7 | 53.8 | 52.8 | 51.9 |
| 84 | 60.8 | 59.8 | 58.8 | 57.8 | 56.8 | 55.8 | 54.8 | 53.9 | 53.0 | 52.1 |
| 85 | 60.9 | 59.9 | 58.9 | 57.9 | 56.9 | 55.9 | 55.0 | 54.0 | 53.1 | 52.2 |
| 86 | 61.1 | 60.0 | 59.0 | 58.0 | 57.0 | 56.1 | 55.1 | 54.2 | 53.2 | 52.3 |
| 87 | 61.2 | 60.2 | 59.1 | 58.1 | 57.2 | 56.2 | 55.2 | 54.3 | 53.4 | 52.5 |
| 88 | 61.3 | 60.3 | 59.3 | 58.3 | 57.3 | 56.3 | 55.4 | 54.4 | 53.5 | 52.6 |
| 89 | 61.4 | 60.4 | 59.4 | 58.4 | 57.4 | 56.5 | 55.5 | 54.6 | 53.7 | 52.7 |
| 90 | 61.6 | 60.5 | 59.5 | 58.5 | 57.6 | 56.6 | 55.6 | 54.7 | 53.5 | 52.9 |
| 91 | 61.7 | 60.7 | 59.6 | 58.7 | 57.7 | 56.7 | 55.8 | 54.8 | 53.9 | 53.0 |
| 92 | 61.8 | 60.8 | 59.8 | 58.8 | 57.8 | 56.9 | 55.9 | 55.0 | 54.1 | 53.2 |
| 93 | 61.9 | 60.9 | 59.9 | 58.9 | 57.9 | 57.0 | 56.0 | 55.1 | 54.2 | 53.3 |
| 94 | 62.0 | 61.0 | 60.0 | 59.0 | 58.1 | 57.1 | 56.2 | 55.2 | 54.3 | 53.4 |
| 95 | 62.1 | 61.1 | 60.1 | 59.2 | 58.2 | 57.2 | 56.3 | 55.4 | 54.5 | 53.6 |
| 96 | 62.3 | 61.3 | 60.3 | 59.3 | 58.3 | 57.4 | 56.4 | 55.5 | 54.6 | 53.7 |
| 97 | 62.4 | 61.4 | 60.4 | 59.4 | 58.4 | 57.5 | 56.5 | 55.6 | 54.7 | 53.8 |
| 98 | 62.5 | 61.5 | 60.5 | 59.5 | 58.6 | 57.6 | 56.7 | 55.8 | 54.9 | 54.0 |
| 99 | 62.6 | 61.6 | 60.6 | 59.6 | 58.7 | 57.7 | 56.9 | 55.9 | 55.0 | 54.1 |
| 100 | 62.7 | 61.7 | 60.7 | 59.8 | 58.8 | 57.9 | 56.9 | 56.0 | 55.1 | 54.2 |
| 101 | 62.8 | 61.9 | 60.9 | 59.9 | 58.9 | 58.0 | 57.1 | 56.2 | 55.3 | 54.4 |
| 102 | 63.0 | 62.0 | 61.0 | 60.0 | 59.1 | 58.1 | 57.2 | 56.3 | 55.4 | 54.5 |
| 103 | 63.1 | 62.1 | 61.1 | 60.1 | 59.2 | 58.3 | 57.3 | 56.4 | 55.5 | 54.6 |
| 104 | 63.2 | 62.2 | 61.2 | 60.3 | 59.3 | 58.4 | 57.5 | 56.6 | 55.7 | 54.8 |
|  | 15.0 | 15.5 | 16.0 | 16.5 | 17.0 | 17.5 | 18.0 | 18.5 | 19.0 | 19.5 |

B

| Temperature of Air , Fahr uheit. | $\mathbf{t}-\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point.-Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 | 24.0 | 28.5 |
| $20^{\circ}$ | 40.2 | 39.3 | 38.4 | 37.5 | 36.6 | 35.8 | 34.9 | 34.1 | 33.3 | 32.5 |
| 21 | 40.3 | 39.4 | 38.4 | 37.6 | 36.7 | 35.8 | 35.0 | 34.2 | 33.1 | 33.6 |
| 22 | 40.3 | 39.4 | 38.5 | 37.6 | 36.8 | 3.5.9 | 35.1 | 34.3 | 33.5 | 32.7 |
| 23 | 40.4 | 39.5 | 35.6 | 37.7 | 36.8 | 36.0 | 35.2 | 34.4 | 33.6 | 32.8 |
| 24 | 40.1 | 39.6 | 38.6 | 37.8 | 36.9 | 36.1 | 35.2 | 34.4 | 33.6 | 32.9 |
| 2.5 | 40.5 | 39.6 | 38.7 | 37.8 | 37.0 | 36.2 | 3.5 .3 | 34.5 | 33.7 | 33.0 |
| 26 | 40.5 | 39.7 | 38.8 | 37.9 | 37.0 | 36.2 | 35.4 | 34.6 | 33.8 | 83.1 |
| 27 | 40.6 | 39.7 | 38.8 | 38.0 | 37.1 | 36.3 | 35.5 | 34.7 | 33.9 | 33.1 |
| 28 | 40.7 | 39.8 | 38.9 | 38.0 | 37.2 | 36.3 | 35.5 | 34.7 | 34.0 | 33.2 |
| 29 | 40.8 | 39.9 | 38.9 | 38.1 | 37.2 | 36.4 | 35.6 | 34.5 | 3 +. 0 | 33.3 |
| 30 | 40.8 | 39.9 | 39.0 | 38.1 | 37.3 | 36.5 | 35.7 | 34.9 | 34.1 | 33.4 |
| 31 | 41.1 | 40.2 | 39.2 | 38.4 | 37.5 | 36.7 | 35.9 | 35.1 | 34.3 | 33.6 |
| 32 | 41.3 | 40.4 | 39.5 | 38.6 | 37.7 | 37.0 | 36.1 | 35.3 | 34.5 | 83.8 |
| 33 | 41.6 | 40.6 | 39.7 | 38.8 | 38.0 | 37.2 | 36.3 | 35.5 | 34.7 | 84.0 |
| 34 | 41.8 | 40.9 | 39.9 | 39.1 | 38.2 | 37.4 | 36.5 | 35.7 | 34.9 | 31.2 |
| 3.5 | f2.1 | 41.1 | 40.2 | 39.3 | 38.4 | 37.7 | 36.7 | 35.9 | 35.1 | 34.4 |
| 36 | 42.3 | 41.4 | 40.4 | 39.6 | $\cdot 38.7$ | 37.9 | 37.0 | 36.2 | 35.4 | 34.6 |
| 37 | 42.6 | 41.7 | 40.7 | 39.8 | 38.9 | 38.2 | 37.2 | 36.4 | 35.6 | 34.8 |
| 35 | 42.8 | 42.0 | 41.0 | 40.1 | 39.2 | 38.4 | 37.5 | 36.6 | 35.8 | 35.0 |
| 39 | 43.1 | 42.3 | 41.3 | 40.4 | 39.5 | 38.6 | 37.7 | 36.9 | 36.0 | 35.2 |
| 40 | 43.3 | 42.6 | 41.6 | 40.7 | 39.8 | 38.9 | 38.0 | 37.1 | 36.3 | 35.4 |
| 41 | 43.7 | 42.9 | 41.9 | 41.0 | 40.0 | 39.1 | 38.3 | 37.4 | 36.5 | 35.7 |
| 42 | 4.0 | 43.2 | 42.2 | 41.2 | 40.3 | 39.4 | 38.5 | 37.7 | 36.8 | 36.0 |
| 43 | 44.3 | 43.4 | 42.5 | 41.5 | 40.6 | 39.7 | 38.8 | 38.0 | 37.1 | 36.3 |
| 44 | 44.7 | 43.7 | 42.8 | 41.8 | 40.9 | 40.0 | 39.1 | 38.2 | 37.4 | 36.6 |
| 45 | 45.0 | 440 | 43.1 | 42.1 | 41.2 | 40.3 | 39.4 | 38.5 | 37.7 | 36.8 |
| 46 | 45.2 | 44.3 | 43.3 | 42.4 | 41.4 | 40.5 | 39.7 | 38.8 | 37.9 | 37.1 |
| 47 | 45.5 | 44.5 | 43.6 | 42.6 | 41.7 | 40.8 | 39.9 | 39.1 | 38.2 | 87.4 |
| 48 | 4.5 .7 | 44.5 | 43.9 | 42.9 | 42.0 | 41.1 | 40.2 | 39.3 | 38.5 | 87.6 |
| 49 | 46.0 | 45.0 | 44.1 | 43.2 | 42.2 | 41.3 | 40.5 | 39.6 | 38.7 | 37.9 |
| 50 | 46.2 | 45.3 | 4.3 | 43.4 | 42.5 | 41.6 | 40.7 | 39.9 | 39.0 | 37.2 |
| 51 | 46.4 | 4.). 4 | 44.5 | 43.6 | 42.7 | 41.8 | 40.9 | 40.1 | 39.2 | 38.4 |
| 52 | 46.6 | 45.5 | 44.7 | 43.8 | 42.9 | 42.0 | 41.2 | 40.3 | 39.5 | 38.6 |
| 53 | 46.7 | 45.8 | 4.9 | 44.0 | 43.1 | 42.2 | 41.4 | 40.5 | 39.7 | 38.9 |
| 54 | 46.9 | 46.0 | 45.1 | 44.2 | 43.3 | 42.4 | 41.6 | 40.8 | 39.9 | 39.1 |
| 55 | 47.0 | 46.1 | 45.2 | 44.4 | 43.5 | 42.6 | 41.8 | 41.0 | 40.1 | 39.3 |
| 56 | 47.2 | 46.3 | 45.4 | 44.5 | 43.6 | 42.8 | 42.0 | 41.1 | 40.3 | 39.5 |
| 57 | 47.3 | 46.4 | 45.5 | 4.4 | 43.8 | 42.9 | 42.1 | 41.3 | 40.5 | 39.6 |
| 58 | 47.5 | 46.6 | 4.78 | 44.8 | 43.9 . | 43.1 | 42.3 | 41.4 | 40.6 | 39.8 |
| 59 | 47.6 | 46.7 | 45.8 | 45.0 | 44.1 | 43.2 | 42.4 | 41.6 | 40.8 | 40.0 |
| 60 | 47.8 | 46.9 | 46.0 | 45.1 | 44.2 | 43.4 | 42.5 | 41.7 | 40.9 | 40.1 |
| 61 | 47.9 | 47.0 | 46.1 | 45.3 | 44.4 | 43.5 | 42.7 | 41.9 | 41.1 | 40.3 |
| 62 | 48.1 | 47.2 | 46.3 | 45.4 | 44.5 | 43.7 | 42.8 | 42.0 | 41.2 | 40.4 |
|  | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 | 24.0 | 24.5 |


| Temperature of $\operatorname{Air}$, Fahrenheit. | $\mathbf{t}$ - $\mathbf{t}^{\prime}=$ Difference of Temperatures of the Air and of the Dew-Point. - Fahrenheit. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20.0 | 20.5 | 21.1 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 | 24.0 | 94.5 |
| $62^{\circ}$ | 48.1 | 47.2 | 46.3 | 45.4 | 44.5 | 43.7 | 42.8 | 42.0 | 41.2 | 40.4 |
| 63 | 48.2 | 47.3 | 46.4 | 45.5 | 44.7 | 43.8 | 43.0 | 42.2 | 41.4 | 40.6 |
| 64 | 48.4 | 47.5 | 46.6 | 4.5 | 44.8 | 4.0 | 43.1 | 42.3 | 41.5 | 40.7 |
| 65 | 48.6 | 47.6 | 46.7 | 45.8 | 45.0 | 44.1 | 43.3 | 42.5 | 41.7 | 40.9 |
| 66 | 48.7 | 47.8 | 46.9 | 46.0 | 45.1 | 44.3 | 43.4 | 42.6 | 41.8 | 41.0 |
| 67 | 48.8 | 47.9 | 47.0 | 46.1 | 45.3 | 44.4 | 43.6 | 42.8 | 42.0 | 41.2 |
| 68 | 48.9 | 45.0 | 47.2 | 46.3 | 45.4 | 44.6 | 43.7 | 42.9 | 42.1 | 41.3 |
| 69 | 49.1 | 48.2 | 47.3 | 46.4 | 45.6 | 44.7 | 43.9 | 43.1 | 42.3 | 41.5 |
| 70 | 49.2 | 48.3 | 47.4 | 46.6 | 45.7 | 44.9 | 44.0 | 43.2 | 4-.4 | +1.6 |
| 71 | 49.4 | 48.5 | 47.6 | 46.7 | 45.9 | 45.0 | 44.2 | 43.4 | 42.6 | 41.8 |
| 72 | 49.5 | 48.6 | 47.7 | 46.9 | 46.0 | 45.2 | 44.3 | 43.5 | 42.7 | 41.9 |
| 73 | 49.6 | 48.8 | 47.9 | 47.0 | 46.1 | 45.3 | 44.5 | 43.7 | 42.9 | 42.1 |
| 74 | 49.8 | 48.9 | 48.0 | 47.1 | 46.3 | 45.4 | 44.6 | 43.8 | 43.0 | 42.2 |
| 75 | 49.9 | 49.0 | 48.2 | 47.3 | 46.4 | 45.6 | 44.8 | 44.0 | 43.1 | 42.4 |
| 76 | 50.1 | 49.2 | 48.3 | 47.4 | 46.6 | 45.7 | 44.9 | 4.1 | 43.3 | 42.5 |
| 77 | 50.2 | 49.3 | 48.5 | 47.6 | 46.7 | 45.9 | 45.1 | 4.2 | 43.4 | 42.6 |
| 78 | 50.3 | 49.5 | 48.6 | 47.7 | 46.9 | 46.0 | 45.2 | 44.4 | 43.6 | 42.8 |
| 79 | 50.5 | 49.6 | 49.7 | 47.8 | 47.0 | 46.2 | 45.3 | 44.5 | 43.7 | 43.0 |
| 80 | 50.6 | 49.7 | 49.9 | 48.0 | 47.2 | 46.3 | 45.5 | 44.7 | 43.9 | 43.1 |
| 81 | 50.8 | 49.9 | 49.0 | 48.1 | 47.3 | 46.5 | 45.6 | 44.8 | 44.0 | 43.2 |
| 82 | 50.9 | 50.0 | 49.2 | 48.3 | 47.4 | 46.6 | 45.8 | 45.0 | 44.2 | 43.4 |
| 83 | 51.0 | 50.1 | 49.3 | 48.4 | 47.6 | 46.8 | 45.9 | 45.1 | 44.3 | 43.5 |
| 84 | 51.2 | 50.3 | 49.1 | 48.6 | 47.7 | 46.9 | 46.1 | 45.3 | 44.5 | 43.7 |
| 85 | 51.3 | 50.4 | 49.6 | 48.7 | 47.9 | 47.0 | 46.2 | 45.4 | 44.6 | 43.5 |
| S6 | 51.4 | 50.6 | 49.7 | 48.8 | 48.0 | 47.2 | 46.4 | 45.6 | 44.8 | 44.0 |
| 87 | 51.6 | 50.7 | 49.8 | 49.0 | 48.1 | 47.3 | 46.5 | 45.7 | 44.9 | 4.1 |
| 88 | 51.7 | 50.8 | 50.0 | 49.1 | 48.3 | 47.5 | 46.6 | 45.8 | 45.0 | 44.3 |
| 89 | 51.9 | 51.0 | 50.1 | 49.3 | 48.4 | 47.6 | 46.8 | 46.0 | 45.2 | 44.4 |
| 90 | 52.0 | 51.1 | 50.3 | 49.4 | 48.6 | 47.7 | 46.9 | 46.1 | 45.3 | 44.6 |
| 91 | 52.1 | 51.3 | 50.4 | 49.5 | 48.7 | 47.9 | 47.1 | 46.3 | 45.5 | 44.7 |
| 92 | 52.3 | 51.4 | 50.5 | 49.7 | 48.3 | 48.0 | 47.2 | 46.4 | 45.6 | 4.8 |
| 93 | 52.4 | 51.5 | 50.7 | 49.8 | 49.0 | 48.2 | 47.4 | 46.6 | 15.8 | 45.0 |
| 94 | 52.5 | 51.7 | 50.8 | 50.0 | 49.1 | 48.3 | 47.5 | 46.7 | 45.9 | 45.1 |
| 9.5 | 52.7 | 51.8 | 50.9 | 50.1 | 49.3 | 45.4 | 47.6 | 46.8 | 46.1 | 453 |
| 96 | 52.8 | 51.9 | 51.1 | 50.2 | 49.1 | 48.6 | 47.8 | 47.0 | 46.2 | 45.4 |
| 97 | 52.9 | 52.1 | 51.2 | 50.1 | 49.5 | 48.7 | 47.9 | 47.1 | 46.3 | 45.6 |
| 98 | 53.1 | 52.2 | 51.4 | 50.5 | 49.7 | 48.9 | 48.1 | 47.3 | 46.5 | 45.7 |
| 99 | 53.2 | 52.3 | 51.5 | 50.6 | 49.8 | 49.0 | 48.2 | 47.4 | 46.6 | 45.9 |
| 100 | 53.4 | 52.5 | 51.6 | 50.8 | 50.0 | 49.1 | 48.3 | 47.5 | 46.8 | 46.0 |
| 101 | 53.5 | 52.6 | 51.8 | 50.9 | 50.1 | -19.3 | 48.5 | 47.7 | 46.9 | 46.2 |
| 102 | 53.6 | 52.8 | 51.9 | 51.1 | 50.2 | 49.4 | 48.6 | 47.8 | 47.1 | 46.3 |
| 103 | 53.8 | 52.9 | 52.0 | 51.2 | 50.4 | 49.6 | 48.8 | 48.0 | 47.2 | 46.4 |
| 104 | 53.9 | 53.0 | 52.2 | 51.3 | 50.5 | 49.7 | 48.9 | 48.1 | 47.3 | 46.6 |
|  | 20.0 | 20.5 | 21.0 | \$11.5 | 22.0 | 29.5 | $\mathbf{2 3 . 0}$ | 23.5 | 21.0 | 24.5 |
| B |  |  |  |  | ऽЭ |  |  |  |  |  |

## TABLE IX.

```
FACTOR }\mp@subsup{}{F}{100},\mp@code{FOR COMPUTING THE RELATIVE HUMIDITY, OR THE DEGREE OF MOISTURE
        OF THE AIR, EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE
                        HUMIDITY GIVEN IN ENGLISH MEASURES.
```

The Relative Humidity, or the degree of moisture of the air, is, as explained above, the ratio of the quantity of vapor contained in the air to the quantity it could contain at the temperature observed, if fully saturated.

If we call
The force of vapor contained in the air $=f$,
The maximum of the force of vapor at the temperature of the air $=\mathrm{F}$,
The point of saturation $=100$,
we have the proportion,

$$
\text { Relative Humidity : } 100:: f: \mathrm{F} \text {, }
$$

and

$$
{ }_{F}^{f \times 100}=\text { Relative Humidity in Hundredths. }
$$

But as $\frac{f \times{ }_{\mathbf{F}}^{100}}{{ }^{10}}=f \times{ }_{\mathbf{F}}^{\mathbf{1 0 0}}$, it is obvious that the operation indicated by the former expression, viz. $\frac{f \times{ }_{\mathbf{F}}{ }^{100} \text {, would be reduced to a simple muttiplication, if we had a }}{}$ table of the factors ${ }_{F}^{100}$. Such a table is obtained by dividing the constant number 100 by each number in the 'Table of Elastic Forces of Vapor, and substituting the quotients for the tensions, or forees of vapor.

The following Table gives the factor ${ }_{F}^{100}$ for every tenth of a degree from $0^{\circ}$ to $104^{\circ}$ Fahrenheit, corresponding to the Forces of Vapor in Table VI., or Reguault's table reduced to English measures.

## Use of the Table.

The force of vapor contained in the air, or its absolute humidity, being given in English measures, multiply the number expressing it by the factor in the table corresponding to the temperature of the air at the time of the observation; the result will be the Relatice Humidity in Hundredths.

## Examples.

1. Suppose the temperature of the air to be $=60^{\circ}$ Fahrenheit.
" " foree of vapor in the air to be $=.388$ English inch.
Opposite $60^{\circ}$ is found in the table the factor 193.1.
Then $\quad 0.388 \times 193.1=74.9$, Relative Humidity in Hundredths.
2. Suppose the temperature of the air to be $=74^{\circ} .5$ Fahrenheit.
" " force of vapor in the air to be $=.650$ English inch.
Table gives for $74^{\circ} .5$ the factor 117.2 .
Then $\quad 0.650 \times 117.2=76.2$, Relative Humidity required.
B
Ix. factor $\frac{100}{F}$, for COMPUTing the Relative humidity, or the degree of moisture of the Air,

EXPRESSED IN HUNDREDTHS, FROM ITS ABSOLUTE HUMIDITY
GIVEN IN ENGLISH INCHES.

| Temperature of Air, Fahrenheit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $0^{\circ}$ | 2306 | 2295 | 2285 | 2275 | 2264 | 2254 | 2.43 | 22:33 | 2222 | 22.1 |
| 1 | 2201 | 2191 | 2181 | 2171 | 2162 | 2152 | 2142 | 2132 | 2122 | 2111 |
| 2 | 2101 | 2092 | $\underline{2083}$ | 2074 | 2064 | 2055 | 2045 | 2036 | 2026 | 2017 |
| 3 | 2007 | 1998 | 1990 | 1981 | 1972 | 1963 | 19.54 | 1945 | 1936 | 1927 |
| 4 | 1918 | 1910 | 1901 | 1893 | 1885 | 1876 | 1868 | 1859 | 1851 | 1842 |
| 5 | 1834 | 1826 | 1818 | 1810 | 1802 | 1794 | 1786 | 1777 | 1769 | 1761 |
| 6 | 1753 | 1745 | 1733 | 1730 | 1722 | 1714 | 1707 | 1699 | 1691 | 1683 |
| 7 | 1675 | 1668 | 1660 | 1653 | 1616 | 1638 | 1631 | 1623 | 1616 | 1608 |
| 8 | 1600 | 1594 | 1557 | 1580 | 1572 | 1565 | 15.58 | 1551 | 1544 | 1537 |
| 9 | 1529 | 1523 | 1516 | 1509 | 1503 | 1496 | 1489 | 1482 | 1475 | 1469 |
| 10 | 1462 | 1455 | 1449 | 1443 | 1436 | 1430 | 1423 | 1417 | 1410 | 1404 |
| 11 | 1397 | 1391 | 1355 | 1379 | 1373 | 1367 | 1361 | 1355 | 1348 | 1342 |
| 12 | 1336 | 1330 | 1324 | 1319 | 1313 | 1307 | 1301 | 1295 | 1289 | 1284 |
| 13 | 1278 | 1272 | 1267 | 1261 | 1255 | 1250 | 1244 | 1239 | 1233 | 1228 |
| 14 | $1 \because 22$ | 1217 | 1211 | 1206 | 1200 | 1195 | 1189 | 1184 | 1178 | 1173 |
| 15 | 1167 | 1162 | 1157 | 1151 | 1146 | 1141 | 1136 | 1130 | 1125 | 1120 |
| 16 | 1114 | 1109 | 1104 | 1099 | 1094 | 1089 | 1084 | 1079 | 1074 | 1069 |
| 17 | 1064 | 1059 | 1053 | 1050 | 1045 | 1040 | 1035 | 1031 | 1026 | 1021 |
| 18 | 1016 | 1012 | 1007 | 1003 | 998.2 | 993.6 | 989.1 | 984.5 | 979.9 | 975.3 |
| 19 | 970.6 | 966.4 | 962.2 | 957.9 | 953.7 | 949.4 | 945.0 | 940.7 | 936.3 | 931.9 |
| 20 | 927.5 | 923.5 | 919.5 | 915.5 | 911.4 | 907.4 | 903.3 | S99.1 | 895.0 | 890.8 |
| 21 | 886.7 | 882.9 | 879.1 | 875.3 | 871.4 | 867.6 | 863.7 | 859.8 | 855.8 | 851.9 |
| 22 | 817.9 | 844.3 | 840.7 | 837.1 | 833.4 | 829.8 | 826.1 | 82.2 .4 | 818.7 | 815.0 |
| 23 | SI1.2 | 807.8 | S04.3 | 800.8 | 797.3 | 793.8 | 790.2 | 786.7 | 783.1 | 779.5 |
| 24 | 775.9 | 772.6 | 769.3 | 766.0 | 762.7 | 759.3 | 756.0 | 752.6 | 749.2 | 745.8 |
| 2.5 | 742.4 | 739.3 | 736.2 | 733.0 | 729.9 | 726.7 | 723.5 | 720.3 | 717.1 | 713.9 |
| 26 | 710.6 | 707.7 | 704.7 | 701.8 | 693.8 | 695.8 | 692.8 | 689.7 | 686.7 | 683.6 |
| 27 | 650.5 | 677.8 | 675.0 | 672.1 | 669.3 | 666.5 | 663.6 | 660.7 | 657.8 | 654.9 |
| 28 | 652.0 | 649.4 | 646.7 | 644.1 | 641.4 | 638.7 | 636.0 | 633.3 | 630.5 | 627.5 |
| 29 | 625.0 | 622.5 | 620.0 | 617.5 | 614.9 | 612.4 | 609.5 | 607.2 | 604.6 | 602.0 |
| 30 | 599.4 | 597.1 | 594.7 | 592.3 | 589.9 | 587.4 | 585.0 | 582.6 | 580.1 | 577.6 |
| 31 | 575.1 | 572.9 | 570.7 | 568.4 | 566.2 | 563.9 | 561.6 | 559.2 | 556.9 | 554.5 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

B

| Temperature of Air, Fahrenheit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $32^{\circ}$ | 552.2 | 550.0 | 547.8 | 545.7 | 543.6 | 541.4 | 539.3 | 537.2 | 5:5.1 | 533.0 |
| 33 | 530.9 | 528.8 | 526.8 | 524.7 | 522.7 | 520.6 | 518.6 | 516.5 | 514.5 | 512.5 |
| 34 | 510.5 | 508.5 | 506.5 | 504.5 | 502.5 | 500.5 | 498.6 | 496.6 | 494.7 | 492.7 |
| 35 | 490.8 | 488.9 | 487.0 | 485.1 | 483.2 | 481.3 | 479.4 | 477.5 | 475.6 | 473.8 |
| 36 | 471.9 | 470.1 | 468.2 | 466.4 | 464.6 | 462.8 | 461.0 | 459.2 | 457.4 | 455.6 |
| 37 | 453.8 | 452.0 | 450.3 | 448.5 | 446.8 | 445.0 | 443.3 | 441.6 | 439.9 | 438.1 |
| 38 | 436.4 | 434.7 | 433.1 | 431.4 | 429.7 | 428.0 | 426.4 | 424.7 | 423.1 | 421.4 |
| 39 | 419.8 | 418.2 | 416.6 | 415.0 | 413.4 | 411.8 | 410.2 | 408.6 | 407.0 | 405.5 |
| 40 | 403.9 | 402.4 | 400.8 | 399.3 | 397.8 | 396.2 | 394.7 | 393.2 | 391.7 | 290.2 |
| 41 | 388.7 | 387.2 | 385.8 | 384.3 | 382.9 | 381.4 | 350.0 | 378.5 | 377.1 | 375.7 |
| 42 | 374.3 | 372.9 | 371.5 | 370.0 | 368.6 | 367.3 | 365.9 | 364.5 | 363.1 | 361.7 |
| 43 | 360.4 | 3.59 .0 | 357.6 | 356.3 | 354.9 | 353.6 | 352.3 | 350.9 | 349.6 | 348.3 |
| 44 | 347.0 | 345.6 | 3 4.3 | 343.0 | 341.7 | 340.4 | 339.2 | 337.9 | 336.6 | 335.3 |
| 45 | 334.1 | 332.8 | 331.6 | 330.3 | 328.1 | 327.8 | 326.6 | 325.4 | 324.1 | 322.9 |
| 46 | 321.7 | 320.5 | 319.3 | 318.1 | 316.9 | 315.7 | 314.5 | 313.3 | 312.2 | 311.0 |
| 47 | 309.8 | 308.7 | 307.5 | 306.4 | 305.2 | 304.1 | 302.9 | 301.8 | 300.7 | 299.6 |
| 43 | 295.5 | 297.3 | 296.2 | 293.1 | 294.0 | 292.9 | 291.9 | 290.8 | 259.7 | $2 \times 8.6$ |
| 49 | 2~7.6 | 286.5 | 283.4 | 281.4 | 283.3 | 282.3 | 281.3 | 280.2 | 279.2 | 278.2 |
| 50 | 277.1 | 276.1 | 275.1 | 274.1 | 273.1 | 272.1 | 271.1 | 270.1 | 269.1 | 268.2 |
| 51 | 267.2 | 266.2 | 265.2 | 264.3 | 263.3 | 262.3 | 261.4 | 260.4 | 259.5 | 258.5 |
| 52 | 2.57 .6 | 2.56 .6 | 255.7 | 2.54 .8 | 253.8 | 252.9 | 252.0 | 251.1 | 250.2 | 249.3 |
| 53 | 218.3 | 217.1 | 216.5 | 24.5 .6 | 24.7 | 243.9 | 243.0 | 242.1 | 241.2 | 240.3 |
| 54 | 239.5 | 238.6 | 237.7 | 236.9 | 236.0 | 23.5 .1 | 234.3 | 233.4 | 232.6 | 231.7 |
| 55 | 2:30.9 | 230.1 | 229.2 | 228.4 | 227.6 | 226.8 | 225.9 | 225.1 | $22+.3$ | 223.5 |
| 50 | 22.7 | 221.9 | 221.1 | 220.3 | 219.5 | 218.7 | 217.9 | 217.1 | 216.4 | 215.6 |
| 57 | 214.8 | 214.0 | 213.3 | 212.5 | 211.8 | 211.0 | 210.2 | 209.5 | 208.7 | 208.0 |
| 58 | 207.3 | 206.5 | 205.8 | 20.5 .0 | 204.3 | 203.6 | 202.9 | 202.2 | 201.4 | 200.7 |
| 59 | 200.0 | 199.3 | 19 ¢. 6 | 197.9 | 197.2 | 196.5 | 195.8 | 19.5. 1 | 194.4 | 193.8 |
| 60 | 193.1 | 192.4 | 191.7 | 191.0 | 190.1 | 189.7 | 189.0 | 188.4 | 187.7 | 187.0 |
| 61 | 186.4 | 185.7 | 185.1 | 184.4 | 183.8 | 183.1 | 182.5 | 181.8 | 181.2 | 180.6 |
| 62 | 179.9 | 179.3 | 178.7 | 178.0 | 177.4 | 176.8 | 176.2 | 175.6 | 174.9 | 174.3 |
| 63 | 173.7 | 173.1 | 172.5 | 171.9 | 171.3 | 170.7 | 170.1 | 169.5 | 168.9 | 168.3 |
| 64 | 167.7 | 167.1 | 16 t.6 | 166.0 | 165.4 | 164.3 | 164.3 | 163.7 | 163.1 | 162.5 |
| 65 | 162.0 | 1614 | 160.9 | 160.3 | 159.7 | 159.2 | 158.6 | 158.1 | 157.5 | 157.0 |
| 66 | 156.5 | 15.5 .9 | 155.4 | 154.8 | 154.3 | 153.8 | 153.2 | 152.7 | 152.2 | 151.7 |
| 67 | 1.51 .1 | 150.6 | 150.1 | 149.6 | 149.1 | 145.6 | 148.1 | 147.6 | 147.1 | 146.6 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Temperature of Air. Fahrenbeit. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 | 8. | 9. |
| -68 ${ }^{\circ}$ | 146.0 | 145.6 | 145.1 | 144.6 | 14.1 | 143.6 | 143.1 | 142.6 | 142.1 | 141.6 |
| 69 | 141.2 | 140.7 | 140.2 | 139.7 | 139.2 | 138.8 | 138.3 | 137.8 | 137.4 | 136.9 |
| 70 | 136.4 | 136.0 | 135.5 | 135.1 | 134.6 | 134.1 | 133.7 | 133.2 | 132.8 | 132.3 |
| 71 | 131.9 | 131.4 | 131.0 | 130.5 | 130.1 | 129.7 | 129.2 | 128.8 | 128.3 | 127.9 |
| 72 | 127.5 | 127.1 | 126.6 | 126.2 | 125.8 | 125.3 | 124.9 | 124.5 | 124.1 | 123.7 |
| 73 | 123.3 | 122.8 | 122.4 | 122.0 | 121.6 | 121.2 | 120.8 | 120.4 | 120.0 | 119.6 |
| 74 | 119.2 | 118.8 | 118.4 | 118.0 | 117.6 | 117.2 | 116.8 | 116.4 | 116.0 | 115.6 |
| 75 | 115.3 | 114.9 | 114.5 | 114.1 | 113.7 | 113.3 | 113.0 | 112.6 | 112.2 | 111.9 |
| 76 | 111.5 | 111.1 | 110.7 | 110.4 | 110.0 | 109.6 | 109.3 | 108.9 | 108.6 | 108.2 |
| 77 | 107.9 | 107.5 | 107.1 | 106.8 | 106.4 | 106.1 | 105.7 | 105.4 | 105.1 | 104.7 |
| 78 | 104.4 | 104.0 | 103.7 | 103.3 | 103.0 | 102.7 | 102.3 | 102.0 | 101.7 | 101.3 |
| 79 | 101.0 | 100.7 | 100.3 | 100.0 | 99.68 | 99.35 | 99.02 | 98.70 | 98.38 | 98.06 |
| 80 | 97.73 | 97.42 | 97.10 | 96.78 | 96.47 | 96.15 | 95.84 | 95.52 | 95.21 | 94.90 |
| 81 | 94.59 | 94.29 | 93.98 | 93.67 | 93.37 | 93.06 | 92.76 | 92.46 | 92.16 | 91.86 |
| 82 | 91.56 | 91.26 | 90.97 | 90.67 | 90.38 | 90.09 | 89.80 | 89.51 | 89.22 | 88.93 |
| 83 | 88.64 | 88.36 | 88.07 | 87.79 | 87.50 | 87.22 | 86.94 | 86.66 | 86.38 | 86.10 |
| 84 | 85.83 | 85.55 | 85.27 | 85.00 | 84.73 | 84.46 | 84.19 | 83.92 | 83.65 | 8:3.3 |
| 85 | 83.12 | 82.85 | 82.59 | 82.32 | 82.06 | 81.80 | 81.54 | 81.28 | 81.02 | 80.75 |
| 86 | 80.51 | 80.25 | 80.00 | 79.71 | 79.49 | 79.24 | 78.99 | 78.74 | 78.49 | 78.24 |
| 87 | 77.99 | 77.75 | 77.50 | 77.26 | 77.01 | 76.77 | 76.52 | 76.28 | 76.04 | 75.80 |
| 88 | 75.56 | 75.32 | 75.08 | 74.85 | 74.61 | 74.37 | 74.14 | 73.91 | 73.67 | 73.44 |
| 89 | 73.21 | 72.98 | 72.75 | 72.52 | 72.29 | 72.06 | 71.81 | 71.61 | 71.39 | 71.16 |
| 90 | 70.94 | 70.72 | 70.49 | 70.27 | 70.05 | 69.83 | 69.61 | 69.39 | 69.18 | 68.96 |
| 91 | 68.74 | 65.53 | 68.32 | 68.10 | 67.89 | 67.68 | 67.47 | 67.26 | 67.05 | 66.81 |
| 92 | 66.63 | 66.42 | 66.22 | 66.01 | 65.81 | 65.60 | 65.40 | 65.19 | 64.99 | 64.79 |
| 93 | 64.59 | 64.39 | 64.19 | 63.99 | 63.79 | 63.59 | 63.40 | 63.20 | 63.01 | 62.81 |
| 94 | 62.62 | 62.43 | 62.24 | 62.04 | 61.85 | 61.66 | 61.47 | 61.29 | 61.10 | 60.91 |
| 95 | 60.72 | 60.54 | 60.35 | 60.17 | 59.98 | 59.80 | 59.62 | 5943 | 59.25 | 59.07 |
| 96 | 58.89 | 58.71 | 58.53 | 58.35 | 58.17 | 58.00 | 57.82 | 57.64 | 57.47 | 57.29 |
| 97 | 57.12 | 56.94 | 56.77 | 56.60 | 56.42 | 56.25 | 56.08 | 55.91 | 5.5 .74 | 55.57 |
| 98 | 55.40 | 55.23 | 55.06 | 54.90 | 54.73 | 54.56 | 54.40 | 54.23 | 51.07 | 53.91 |
| 99 | 53.74 | 5358 | 53.42 | 53.26 | 53.09 | 52.93 | 52.77 | 52.61 | 52.45 | 52.30 |
| 100 | 52.14 | 51.98 | 51.82 | 51.67 | 51.51 | 51.36 | 51.20 | 51.05 | 50.90 | 50.74 |
| 101 | 50.59 | 50.44 | 50.29 | 50.14 | 49.99 | 49.84 | 49.69 | 49.54 | 49.39 | 49.24 |
| 102 | 49.10 | 48.95 | 48.80 | 48.66 | 48.51 | 48.37 | 48.22 | 48.08 | 47.94 | 47.79 |
| 103 | 47.65 | 47.51 | 47.37 | 47.23 | 47.09 | 46.95 | 46.81 | 46.67 | 46.53 | 46.40 |
| 104 | 46.26 | 46.12 | 45.99 | 45.85 | 45.72 | 45.58 | 45.45 | 45.31 | 45.18 | 45.04 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 | 8. | 9. |

## TABLE X.

WEIGIIT OF VAPOR, IN GRAINS TROY,

CONTAINED IN A CUBIC FOOT OF SATURATED AIR, UNDER A BAROMETRIC PRESSURE OF 30 ENGLISH INCHES, AT TEMPERATURES BETWEEN $0^{\circ}$ AND $105^{\circ}$ FAHRENHEIT.

The weight of a litre of dry air at the temperature of zero Centigrade, or $32^{\circ}$ Fahrenheit, and under a barometric pressure of 760 millimetres, as determined by the experiments of Regnault (Mémoires de l'Institut, Tom. XXI. p. 157), and corrected for a slight error of computation (see above, p. 38), is 1.293223 grammes. The coefficient of expansion of the air, according to the same physicist, is 0.00367 for $1^{\circ}$ Centigrade ; and the theoretic density of vapor is nearly 0.622 , or $\frac{5}{8}$, of that of the air at the same temperature and pressure. From these elements the weight of the vapor contained in a determined volume of air, the temperature and humidity of which are known, can be deduced.

Reducing these values to English measures, 1 litre being $=61.02705$ cubic inches, and I gramme $=15.43208$ grains Troy, we have

$$
1.293223 \text { grammes }=19.9571208 \text { grains, }
$$

and
61.027051 cubic inches : 19.9571208 grains : : 1 cubic inch : 0.32702 grain.

Therefore, the weight of a cubic foot of dry air, at $3 \mathfrak{Z}^{\circ}$ Fahreuheit, under a pressure of 760 millimetres, or 29.922 English inches, is $=0.32702$ grain $\times 1728=565.0923$ grains Troy. Under a barometric pressure of 30 inches, it becomes

$$
\frac{30}{29922} \times 565.0923=566.5654 \text { grains. }
$$

The cocfficient for the expansion of the air becomes 0.0020361 of its bulk for $1^{\circ}$ Fithenheit.

Now, if we call
$t=$ the temperature of the air;
$W=$ the weight of vapor in a saturated air at the temperature $t$;
$\mathrm{F}=$ the maximum of the force of vapor due to the temperature $t$, as given in the tables;
then the weight of the vapor contained in a cubic foot of saturated air is given by the formula

$$
\mathrm{W}=0.622 \frac{566.5654 \text { grains }}{1+0.002036 \times\left(t-32^{\circ}\right)} \cdot \frac{\mathrm{F}}{30}
$$

from which the values in Table $X$. have been computed. The forces of vapor due to the temperatures in the first column are those of Regnault, as given in Table VI.

It is evident, that, in order to find the weight of the vapor contained in the air at any state of humidity and pressure, it suffices to substitute for the normal values of $\frac{\mathrm{F}}{30}$ the force of vapor and the barometric pressure given by the observation.

## x. Weight of vapor, in grains troy,

CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES
BETWEEN $0^{\circ}$ AND $105^{\circ}$ FAHRENHEIT.

| Temperature of Air, Fahren. | Force of Vapor in Eug. Iuches. | Weight of Vapor in Grains. | Difference. | Temperature of Air, Fahren. | Force of Vapor in Eng. Inches. | Weight of Vapor in Grains. | Difference. | Temperature of Air, Fahren | Force of Vapor in Eng. Inches. | Weight of Vapor in Grains. | Differeuce. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 0.04:3 | 0.545 |  | $35^{\circ}$ | 0.204 | 2.379 |  | $70^{\circ}$ | 0.733 | 7.992 |  |
| 1 | 0.045 | 0.569 | 0.0 | 36 | 0.212 | 2.469 |  | 71 | 0.758 | 8.252 | 0.261 |
| 2 | 0.018 | 0.595 |  | 37 | 0.220 | 2.563 | 0.093 | 72 | 0.784 | 8.521 | 0.268 |
| 3 | 0.0 .50 | 0.621 | 0.027 | 38 | 0.229 | 2.659 | 0.0 | 73 | 0.811 | 8.797 | 0.276 |
| 4 | 0.052 | 0.649 | 0.028 | 39 | 0.238 | 2.759 | 0.100 | 74 | 0.839 | 9.051 | 0.284 |
|  |  |  | 0.0:9 |  |  |  | 0.103 |  |  |  | 0.291 |
| 5 | 0.055 | 0.678 |  | 40 | 0.248 | 2.862 |  | 75 | 0.865 | 9.372 |  |
| 6 | 0.0 .57 | 0.708 | 0.030 | 41 | 0.257 | 2.967 | 0.106 | 76 | 0.697 | 9.670 | 0.298 |
| 7 | 0.060 | 0.739 |  | 42 | 0.267 | 3.076 | 0.109 | 77 | 0.927 | 9.977 | 0.307 |
| 8 | 0.062 | 0.772 |  | 43 | 0.277 | 3.189 | 0.113 | 78 | 0.958 | 10.292 | 0.315 |
| 9 | 0.065 | 0.506 | 0.034 | 44 | 0.288 | 3.306 | 0.116 | 79 | 0.940 | 10.616 | 0.324 |
|  |  |  | 0.035 |  |  |  | 0.120 |  |  |  | 0.332 |
| 10 | 0.068 | 0.841 |  | 45 | 0.299 | 3.426 |  | 80 | 1.023 | 10.9 .49 |  |
| 11 | 0.072 | 0.878 | 0.037 | 46 | 0.311 | 3.5 .50 | 0.124 | 81 | 1.057 | 11.291 | 0.342 |
| 12 | 0.075 | 0.916 | 0. | , 47 | $0 .: 323$ | 3.679 | 0.129 | 82 | 1.092 | 11.643 | 0.352 |
| 13 | 0.078 | 0.957 | 0.040 | 48 | 0.335 | 3.511 | 0.133 | 83 | 1.128 | . 0 | 0.361 |
| 14 | 0.052 | 0.949 | 0.042 | 49 | 0.348 | 3.948 | 0.137 | S4 | 1.165 | 12.376 | 0.371 |
|  |  |  | 0.044 |  |  |  | 0.141 |  |  | 12.376 | 0.380 |
| 15 | 0.086 | 1.013 |  | 50 | 0.361 | 4.089 |  | 85 | 1.203 | 12.756 |  |
| 16 | 0.090 | 1.090 | 0.046 | 51 | 0.374 | 4.234 | 0.145 | 86 | 1.212 | 13.146 | 0.390 |
| 17 | 0.034 | $1.13{ }^{\text {P }}$ | 0.049 | 52 | 0.388 | 4.38:3 | 0.149 | 87 | 1.282 | 13.546 | 0.400 |
| 18 | 0.098 | 1.190 | 0.051 | 53 | 0.403 | 4.537 | 0.154 | 88 | 3 |  | 0.411 |
| 19 |  |  | 0.053 | 5 |  |  | 0.159 |  | 1.38 |  | 0.421 |
| 19 | 0.103 |  | 0.055 | 54 | 4 | 4.696 | 0.163 | 89 | 6 | 14.375 | 0.432 |
| 20 | 0.109 | 1.299 |  | 55 | 0.133 | 4.860 |  | 90 | 1.410 | 14.810 |  |
| 21 | 0.113 | 1.3 .55 | 0.057 | 56 | 0.449 | 5.028 | 0.168 | 91 | 1.455 | 15.254 | 0.143 |
| 22 | 0.118 | 1.415 | 0.059 | 57 | 0.166 | 5.202 | 0.174 | 92 | 1.501 | 15.709 | 0.855 |
| 23 | 0.123 | 1.47 | 0.062 | 58 | 0.48 | 5.381 | 0.179 |  | 1.548 |  | 0.467 |
| 24 | 0.129 | 1.54 | 0.064 | 59 | 500 | 5.566 | 0.185 | 94 | 597 |  | 0.479 |
|  |  | 1.5 | 0.066 | 5 | 0.50 | 5.566 | 0.190 | 94 | 1.597 | 16.654 | 0.491 |
| 25 | 0.135 | 1.606 |  | 60 | 0.518 | 5.756 |  | 95 | 1.647 | 17.145 |  |
| 26 | 0.141 | $1.67 \pm$ | 0.068 | 61 | 0.337 | 5.952 | 0.196 | 96 | 1.698 | 17.648 | 0.503 |
| 27 |  | 1.745 | 0.070 | $6 \cdot$ | 0.55 |  | 0.202 |  | 1.71 |  | 0.516 |
| 8 |  | 1.745 | 0.073 | 6 |  | 6. | 0.208 | 9 | 1.8 | 18.164 | 0.529 |
| 28 | 0.153 | 1.817 |  | 63 | 0.576 | 6.361 |  | 98 | 1.805 | 18.693 | 0.5.12 |
| 29 | 0.160 | 1.892 | $0.077$ | 64 | 0.596 | 6.575 | 0.220 | 99 | 1.861 | 19.235 | 0.545 |
| 30 | 0.167 | 1.969 |  | 65 | 0.617 | 6.795 |  | 100 | 1.918 | 19.790 |  |
| 31 | 0.174 | 2.046 | 0.077 | 66 | 0.639 | 7.021 | 0.226 | 101 | 1.977 | 20.357 | 0.567 |
|  |  |  | 0.080 |  |  |  | 0.232 |  |  |  | 0.582 |
| 32 | 0.181 | 2.126 | 082 | 67 | 0.662 | 7.253 | 0.239 | 102 | 2.037 | 20.935 | 0.596 |
| 33 | 0.188 | 2.208 |  | 68 | 0.685 | 7.493 | 0.289 | 103 | 2.099 | 21.535 | 0.596 |
| 31 | 0.196 | 2.292 | 0.084 | 69 | 0.703 | 7.739 | 0.246 | 104 | 2.162 | 22.146 | 0.611 |
| 35 | 0.204 | 2.379 | 0.057 | 70 | 0.733 | 7.992 | 0.253 | 105 | 2.227 | 22.771 | 0.625 |

B
95

# PRACTICAL TABLES, 

ENGLISH MEASURES,

BASED ON THE HYGROMETRICAL CONSTANTA ADOPTED IN THE GREENWICH OBSERVATIONS.

TABLE

OF

THE ELASTIC FORCES OF AQUEOUS VAPOR,

UNDER A PRESSURE OF 30 INCHES, EXPRESSED IN ENGLISH INCHES OF MERCURY FOR TEMPERATURES OF FAHRENHEIT, ADOPTED IN THE GREENWICH OBSERVATIONS.

This table contains the values of the elastic force of vapor for temperatures from $0^{\circ}$ to $90^{\circ}$ Fahrenheit, derived from Dalton's experiments by Biot's formula, by Anderson, and published in Edinburgh Encyclopadia, Art. Hygrometry. It is republished, without the last decimal, in the volumes of the Greenwich Magnetic and Meteorological Obserrations, and on it are based the various hygrometrical tables published by Mr. Glaisher, either in the Greenwich volumes, or separately, most of which will be found below, Tables XII. to XVII.

Since Dalton published his experiments, numerous attempts have been made by various skilful physicists to determine with greater accuracy the elastic foree of vapor. Dr. Ure in England, Regnault in France, and Magnus in Germany, deserve in this respect a special notice.

The last two experimenters having arrived simultaneonsly at results nearly identical, and then experiments having been conducted with all the care that modern science requires, and the means that it can secure, their determinations seem to command an especial confidence, and to deserve the preference over all others. It is, therefore, much to be regretted that the usefuhess of the following otherwise so vahtiable tables, the formation of which involved so much labor, is in a measure impaired by the fact that they were computed from elements which cannot be regarded as the most reliable we now possess.
XI.

T A B L. E

OF TIIE

ELASTIC FORCE OF AQUEOUS VAPOR,
mNDER A barometric pressure of 30 inches, EXPressed in english anchet op mercury for temperatures of fahrenheit.

From the Greenwicil Observations.


From the Greenwich Observations.

| Temperature Fabren heit | Teaths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| - | Eng. In. | Eng. In | Eug. In | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 21 | 0.134 | 0.135 | 0.135 | 0.136 | 0.136 | 0.1:7 | 0.1 .7 | 0.138 | 0.135 | 0.139 |
| 22 | 0.139 | 0.140 | 0.140 | 0.141 | $0.1+1$ | 0.142 | 0.142 | 0.143 | 0.143 | 0.144 |
| 23 | 0.14 | 0.145 | 0.119 | 0.146 | 0.146 | 0.117 | 0.147 | 0.148 | 0.148 | 0.149 |
| 24 | 0.150 | 0.150 | 0.1 .1 | 0.152 | 0.152 | 0.1.52 | 0.153 | 0.153 | 0.154 | 0.155 |
| 25 | 0.155 | 0.156 | 0.156 | 0.157 | 0.157 | 0.150 | 0.158 | 0.159 | 0.160 | 0.160 |
| 26 | 0.161 | 0.161 | 0.162 | 0.163 | 0.163 | 0.164 | 0.161 | 0.165 | 0.165 | 0.166 |
| 27 | 0.167 | 0.167 | 0.165 | 0.168 | 0.169 | 0.170 | 0.170 | 0.171 | 0.172 | 0.172 |
| 28 | 0.173 | 0.173 | 0.174 | 0.175 | 0.175 | 0.176 | 0.177 | 0.177 | 0.178 | 9.178 |
| 29 | 0.179 | 0.150 | 0.180 | 0.181 | 0.182 | 0.152 | 0.153 | 0.184 | 0.184 | 0.185 |
| 30 | $0.1 \times 6$ | 0.186 | 0.187 | 0.158 | 0.158 | 0.189 | 0.190 | 0.190 | 0.191 | 0.192 |
| 31 | 0.192 | 0.193 | 0.194 | 0.194 | 0.195 | 0.196 | 0.197 | 0.197 | 0.198 | 0.198 |
| 32 | 0.199 | 0.200 | 0.201 | 0.201 | 0.202 | 0.203 | 0.204 | 0.204 | 0.205 | 0.206 |
| 33 | 0.207 | 0.207 | 0.208 | 0.209 | 0.210 | 0.210 | 0.211 | 0.212 | 0.213 | 0.213 |
| 34 | 0.211 | 0.215 | 0.216 | 0.216 | 0.217 | 0.218 | 0.219 | 0.219 | 0.2\%0 | 0.221 |
| 3.5 | 0.222 | 0.223 | 0.223 | 0.224 | 0.225 | 0.226 | 0.227 | 0.227 | 0.228 | 0.229 |
| 36 | 0.230 | 0.231 | 0.231 | 0.232 | 0.233 | 0.234 | 0.235 | 0.235 | 0.236 | 0.237 |
| 37 | 0.2:3 | 0.2:39 | 0.240 | 0.240 | 0.241 | 0.242 | 0.243 | 0.244 | 0.245 | 0.246 |
| 38 | 0.246 | 0.247 | 0.245 | 0.219 | 0.250 | 0.251 | 0.252 | 0.253 | 0.253 | 0.254 |
| 39 | 0.2 .55 | 0.256 | 0.257 | 0.258 | 0.259 | 0.260 | 0.261 | 0.262 | 0.263 | 0.263 |
| 40 | 0.264 | 0.265 | 0.266 | 0.267 | 0.268 | 0.269 | 0.270 | 0.271 | 0.272 | 0.273 |
| 41 | 0.274 | 0.275 | 0.276 | 0.277 | 0.278 | 0.279 | 0.280 | 0.281 | 0.282 | 0282 |
| 42 | 0.283 | 0.284 | 0.255 | 0.286 | 0.257 | 0.2ss | 0.289 | 0.290 | 0.291 | 0.292 |
| 13 | 0.293 | 0.295 | 0.296 | 0.297 | 0.298 | 0.299 | 0.300 | 0.301 | 0.302 | 0.303 |
| 4 | 0.304 | 0.30 .5 | 0.306 | 0.307 | 0.308 | 0.309 | 0310 . | 0.311 | 0.312 | 0.313 |
| 45 | 0.315 | 0.316 | 0.317 | 0.313 | 0.319 | 0.320 | 0.321 | 0.322 | 0.323 | 0.324 |
| 46 | 0.326 | 0.327 | 0.323 | 0.329 | 0.330 | 0.331 | 0.332 | 0.333 | 0.335 | 0.336 |
| 16 | 0.337 | 0.338 | 0.339 | 0.340 | 0.342 | 0.343 | 0.344 | 0.345 | 0.346 | 0.318 |
| 4 | 0.819 | 0.350 | 0.351 | 0.352 | 0.354 | 0.355 | 0.356 | 0.357 | 0.358 | 0.360 |
| 49 | 0.361 | 0.362 | 0.363 | 0.365 | 0.366 | 0.367 | 0.368 | 0.370 | 0.371 | 0.372 |
| 50 | 6.373 | 0.375 | 0.376 | 0.377 | 0.379 | 0.380 | 0.381 | 0.382 | 0.383 | 0.385 |
| 51 | 0.386 | 0.388 | 0.359 | 0.390 | 0.392 | 0.393 | 0.394 | 0.396 | 0.397 | 0.398 |
| 52 | 0.400 | 0.401 | 0.402 | 0.404 | 0.40 .5 | 0.407 | 0.408 | 0.109 | 0.411 | 0.412 |
| 53 | 0.414 | 0.415 | 0.416 | 0.418 | 0.419 | 0.421 | 0.422 | 0.423 | 0.425 | 0.426 |
| 51 | 0.428 | 0.429 | 0.431 | 0.432 | 0.434 | 0.435 | 0.437 | 0.438 | 0.440 | 0.441 |
| 55 | 0.442 | 0.444 | 0.445 | 0.447 | 0.449 | 0.450 | 0.452 | 0.453 | 0.455 | 0456 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

From the Greenwich Observations.


## XII.

## PSYCHROMETRICAL TABLE,

GIVING THE TEMPERATURE OF THE DEW-POINT, THE FOREE AND THE WEIGHT OF VAPOR JN THE ATMOSPHERE, AND ITS RELATIVE JUMIDITY, DEDUCED FROM THE INDICATIONS OF THE PSYCHROMETER, OR DRY AND WET BULB THERMOMETERS.

By James Glaisher.

'This elaborate table, first published in London, in 1847, in pamphlet form, by J. Glaisher, of the Royal Observatory at Greenwich, is based on the tables of elastic forces of vapor deduced from Dalton's experiments, and given above, Table XI.

The weight of a cubic foot of dry air at $32^{\circ}$ Fahrenheit, and under the barometric pressure of 30 inches, which has been adopted by Glaisher, and from which the weight of vapor in a cubic foot of air is derived, is the mean of the determinations obtained by Shuckburgh and by Biot and Arago, which is 563.2154 grains Troy; 563 being the number actually used in the calculations. See Preface to the Table, p. 13, and also the Greenwich Meteorologieal Obsercations for 1842, p. xlvi.

The coefficient of the expansion of air which has been employed is that determined by the experiments of Gay-Lussac, according to which the air expands $\mathbf{0 . 0 0 3 7 5}$ of its bulk for $1^{\circ}$ Centigrade, or $\frac{1}{480}$ for $1^{\circ}$ Fahrenbeit.

All these values, as may be seen by comparing Tables VI. and XI. of the elastic forces, and also page $9 \bullet$, materially differ from those more recently determined with great care by Regnault, and on which are based the Psychrometrical Tables given above, page 50 et seq. This will account for the no inconsiderable differences often found between the results in the two tables derived from the same data. A few examples, taken from various parts of the tables, may be given here, in order to enable the meteorologist to judge of the amount of the diserepancies which may occur in the results when computed from different hygrometrical constants.

1. Suppose the temperature of the air indicated by the dry thermome$\begin{aligned} \text { ter to be } & =10^{\circ} \mathrm{F} . \\ & =\frac{9^{\circ} \mathrm{F} .}{1^{\circ} \mathrm{F} .}\end{aligned}$
Then, Glaisher's table gives, The Force of Vapor $\quad=0.065$ inch. 'The Relative Ilumidity $=0.730$
Guyot's table gives,
The Force of Vapor $\quad=0.054$ inch.
The Relative Humidity $=0.791$
B
2. By observation we have,

$$
\begin{aligned}
\text { Dry Thermometer } & =50^{\circ} \mathrm{F} . \\
\text { Wet Thermometer } & =40^{\circ} \mathrm{F} \\
\text { Difference } & =10^{\circ} \mathrm{F} .
\end{aligned}
$$

Then, by Glaisher's table, we find,
Force of Vapor $\quad=0.186$ inch.
Relative Humidity $=0.495$
And by Guyot's table, we find,
Force of Vapor $\quad=0.117$ inch.
Relative Humidity $=0.322$
3. The reading of the

$$
\begin{aligned}
\text { Dry Thermometer is } & =90^{\circ} \mathrm{F} . \\
\text { Wet Thermometer is } & =70^{\circ} \mathrm{F} . \\
\text { Difference } & =20^{\circ} \mathrm{F} .
\end{aligned}
$$

By Glaisher's table we have,

| Force of Vapor | $=0.523$ inch. |
| :--- | :--- |
| Relative Humidity | $=0.381$ |

And by Guyot's table,
Force of Vapor $\quad=0.464$ inch.
Relative Humidity $=0.329$
The temperatures of the Dew-Point, given in Glaisher's tables, have been computed by means of the empirical factors given below, page 140 , and in the manner there described. See Preface to the Table, page 11.

## Arrangement of the Table.

In the first two columns, at the left, are found the indications, in degrees of Fahrenheit, of the dry and wet bulb thermometers. In the following columns, in their order, and opposite to each of the temperatures of the wet thermometer, are given the temperature of the dew-point ; the force of vapor, in English inches; the weight of vapor, in grains, contained in a cubic foot of air ; the amount of the same required for saturation ; and the relative bumidity in thousandths, corresponding to the difference of temperature between the two thermometers. The second half of the page, at the right, furnishes, in seven columns, the weight, in grains, of a cubic foot of air, under various barometric pressures from 28 to 31 inches, and in the different hygrometric conditions indicated by the differences of the two thermometers. These numbers have been computed in the manner described below, page $\mathbf{1 4 2}$.

The range of the table extends from $10^{\circ}$ to $90^{\circ}$ of the dry thermometer, or of the temperature of the air. From $10^{\circ}$ to $34^{\circ}$ Fahrenheit the results are calculated for every second, third, and fifth of a degree of the wet thermometer, and for extreme differeaces of the temperature of evaporation ranging from $2^{\circ}$ to $5^{\circ}$ below the temperature of the air. From $34^{\circ}$ to $90^{\circ}$ the results are given only for every full deg'ce of the wet thermometer, and for extreme differences gradually increasing
from $5^{\circ}$ to $27^{\circ}$. This range falls short of the wauts of the extreme ctimate of North America, where temperatures above $90^{\circ}$ and far below $10^{\circ}$ are of usual occurrence over a great portion of the continent. The same may be said of the range of the differences between the two thermometers in the first part of the table. The double interpolation for the fractions of degrees of both thermometers being rather too large to be neglected, its application becomes inconvenient.

## Use of the Table.

Enter the table with the observed temperatures of the dry and wet bulb thermometers. On the same line as the last, and in their appropriate columns, the results deduced from these data will be found.

## Example.

The observation has given,
Temperature of the air by the dry thermometer $\quad=62^{\circ} \mathrm{F}$.
Temperature of evaporation by the wet-bulb thermometer $=53^{\circ} \mathrm{F}$.
Page 1:39, find in the first column, headed Reading of the Dry Thermometer, the temperature of $62^{\circ}$, and in the second, that of the wet, $53^{\circ}$. On the line beginning with $53^{\circ}$ are found, in their respective columns, the results deduced from these data, viz.:-

The temperature of the Dew-point
The force of vapor in the air The weight of vapor in a eubic foot of air
The amount of vapor required for saturation
The relative humidity in thousandths

$$
\begin{aligned}
& =46^{\circ} .7 \mathrm{~F} . \\
& =0.333 \text { inch. } \\
& =3.72 \text { grains. } \\
& =2.53 \text { grains. } \\
& =0.595
\end{aligned}
$$

| Reading of Thermometer, Fahr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | Force of Vapor in English Inches. | Weight of Vapor |  | Humidity, Satura1000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { Requ. } \\ & \text { for } \end{aligned}$ | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Foot of Air. | of aCn bic Ft. |  | $\operatorname{ing.}_{28.0}$ | in. | $\begin{array}{\|c\|} \operatorname{ing} .0 \\ \mathbf{9 . 0} \\ \hline \end{array}$ | $\operatorname{in.}_{29.5}$ | $\operatorname{in.}_{\mathbf{3 0 . 0}}$ | $\operatorname{in}_{\mathbf{3 0} .5}$ |  |
| $10^{\circ}$ |  |  |  | in. | gr. |  | gr |  | gr. | gr. | r. | gr. | gr. | r. | gr. |
|  | 10.0 | 10.0 | 0.089 | 1.11 | 0.00 | 1.000 | 550.1 | 560.0 | 569.8 | 579.6 | 559.4 | 599.2 | 609.0 |
|  | 9.8 | 8.3 | 0.084 | 1.05 | 0.06 | 0.946 | 550.2 | 560.1 | 569.9 | 579.7 | 589.5 | 599.3 | 609.1 |
|  | 9.6 | 6.6 | 0.079 | 0.98 | 0.13 | 0.883 | 550.2 | 560.1 | 569.9 | 579.7 | 589.5 | 599.3 | 609.1 |
|  | 9.4 | 4.9 | 0.074 | 0.92 | 0.19 | 0.829 | 550.2 | 560.1 | 569.9 | 579.7 | 559.5 | 599.3 | 609.1 |
|  | 9. | 3.2 | 0.069 | 0.86 | 0.25 | 0.775 | 550.3 | 560.2 | 570.0 | 579.8 | 589.6 | 599.4 | 609.2 |
|  | 9.0 | 1.5 | 0.065 | 0.81 | 0.30 | 0.730 | 550.3 | 560.3 | 570.0 | 579.8 | 589.6 | 599.4 | 609.3 |
| 11 | 11.0 | 11.0 | 0.093 | 1.15 | 0.00 | 1.000 | 548.9 | 558.7 | 565.5 | 578.3 | 589.1 | 597.9 | 607.7 |
|  | 10.8 | 9.3 | 0.087 | 1.08 | 0.07 | 0.939 | 548.9 | 558.7 | 568.5 | 578.3 | 588.1 | 597.9 | 607.7 |
|  | 10.6 | 7.6 | 0.082 | 1.02 | 0.13 | 0.887 | 549.0 | 558.8 | 568.6 | 578.4 | 588.2 | 598.0 | 607.5 |
|  | 10.4 | 5.9 | 0.077 | 0.96 | 0.19 | 0.835 | 549.0 | 558.8 | 568.6 | 578.4 | 588.2 | 598.0 | 607.8 |
|  | 10.2 | 4.2 | 0.072 | 0.90 | 0.25 | 0.783 | 549.0 | 558.8 | 568.6 | 578.4 | 588.2 | 598.0 | 607.8 |
|  | 10.0 | 2.5 | 0.067 | 0.84 | 0.31 | 0.731 | 549.1 | 558.9 | 568.7 | 5786 | 585.3 | 595.1 | 607.9 |
|  | 9. | 0.8 | 0.063 | 0.78 | 0.37 | 0.679 | 549.1 | 558.9 | 568.7 | 578.6 | 588.3 | 598.1 | 607.9 |
| 12 | 12.0 | 12.0 | 0.096 | 1.19 | 0.00 | 1.000 | 547.7 | 557.5 | 567.2 | 577.0 | 586.8 | 596.6 | 606.4 |
|  | 11.8 | 10.3 | 0.090 | 1.12 | 0.07 | 0.942 | 547.7 | 557.5 | 567.2 | 577.0 | 586.8 | 596.6 | 606.4 |
|  | 11.6 | 8.6 | 0.085 | 1.05 | 0.14 | 0.883 | 547.8 | 557.6 | 567.3 | 577.1 | 586.9 | 596.7 | 606.5 |
|  | 11.4 | 6.9 | 0.080 | 0.99 | 0.20 | 0.832 | 547.8 | 557.6 | 567.3 | 577.1 | 586.9 | 596.7 | 606.5 |
|  | 11.2 | 5.2 | 0.075 | 0.93 | 0.26 | 0.782 | 547.8 | 557.6 | 567.3 | 577.1 | 586.9 | 596.7 | 606.5 |
|  | 11.0 | 3.5 | 0.070 | 0.87 | 0.32 | 0.731 | 547.9 | 557.7 | 567.4 | 577.2 | 587.0 | 596.5 | 606.6 |
|  | 10.8 | 1.8 | 0.066 | 0.81 | 0.38 | 0.681 | 547.9 | 557.7 | 567.4 | 577.2 | 587.0 | 596.8 | 606.6 |
|  | 10.6 | 0.1 | 0.061 | 0.76 | 0.43 | 0.639 | 547.9 | 557.7 | 567.4 | 577.2 | 587.0 | 596.8 | 606.6 |
| 13 | 13.0 | 13.0 | 0.100 | 1.24 | 0.00 | 1.000 | 546.5 | 556.3 | 566.0 | 575.8 | 585.5 | 595.3 | 605.0 |
|  | 12.8 | 11.3 | 0.094 | 1.16 | 0.08 | 0.936 | 546.5 | 556.3 | 566.0 | 575.8 | 585.5 | 595.3 | 605.0 |
|  | 12.6 | 9.6 | 0.088 | 1.08 | 0.16 | 0.871 | 546.6 | 556.4 | 566.1 | 575.9 | 585.6 | 595.4 | 605.1 |
|  | 12.4 | 7.9 | 0.083 | 1.02 | 0.22 | 0.823 | 546.7 | 556.5 | 566.2 | 576.0 | 585.7 | 595.5 | 605.2 |
|  | 12.2 | 6.2 | 0.077 | 0.97 | 0.27 | 0.783 | 546.7 | 556.5 | 566.2 | 576.0 | 585.7 | 595.5 | 605.2 |
|  | 12.0 | 4.5 | 0.073 | 0.91 | 0.33 | 0.734 | 546.7 | 556.5 | 566.2 | 576.0 | 585.7 | 595.5 | 605.2 |
|  | 11.8 | 2.8 | 0.068 | 0.84 | 0.40 | 0.678 | 546.8 | 556.6 | 566.3 | 576.1 | 585.8 | 595.6 | 605.3 |
|  | 11.6 | 1.1 | 0.064 | 0.79 | 0.45 | 0.637 | 546.8 | 556.6 | 566.3 | 576.1 | 585.8 | 595.6 | 605.3 |
| 14 | 14.0 | 14.0 | 0.104 | 1.28 | 0.00 | 1.000 | 545.3 | 555.0 | 564.7 | 574.4 | 584.2 | 594.0 | 603.7 |
|  | 13.8 | 12.3 | 0.097 | 1.20 | 0.08 | 0.938 | 545.3 | 555.0 | 564.7 | 574.4 | 584.2 | 594.0 | 603.7 |
|  | 13.6 | 10.6 | 0.091 | 1.12 | 0.16 | 0.875 | 545.4 | 555.1 | 564.8 | 574.5 | 584.3 | 594.1 | 603.8 |
|  | 13.4 | 8.9 | 0.086 | 1.06 | 0.22 | 0.828 | 545.4 | 555.1 | 564.8 | 574.5 | 584.3 | 594.1 | 603.8 |
|  | 13.2 | 7.2 | 0.080 | 1.00 | 0.28 | 0.782 | 545.4 | 555.1 | 564.8 | 574.5 | 584.3 | 594.1 | 603.8 |
|  | 13.0 | 5.5 | 0.075 | 0.93 | 0.35 | 0.727 | 545.5 | 555.2 | 564.9 | 574.6 | 584.4 | 594.2 | 603.9 |
|  | 12.8 | 3.8 | 0.071 | 0.87 | 0.41 | 0.650 | 545.5 | 555.2 | 564.9 | 574.6 | 584.4 | 594.2 | 603.9 |
|  | 12.6 | 2.1 | 0.066 | 0.82 | 0.46 | 0.641 | 545.6 | 555.3 | 565.0 | 574.7 | 584.5 | 594.2 | 603.9 |
| 15 | 15.0 | 15.0 | 0.108 | 1.32 | 0.00 | 1.000 | 544.0 | 553.8 | 563.5 | 573.2 | 582.9 | 592.6 | 602.3 |
|  | 14.8 | 13.3 | 0.101 | 1.24 | 0.08 | 0.940 | 544.0 | 553.8 | 563.5 | 573.2 | 582.9 | 592.6 | 602.3 |
|  | 14.6 | 11.6 | 0.095 | 1.16 | 0.16 | 0.879 | 544.1 | 553.9 | 563.6 | 573.3 | 583.0 | 592.7 | 602.4 |
|  | 14.4 | 9.9 | 0.089 | 1.10 | 0.22 | 0.833 | 544.1 | 553.9 | 563.6 | 573.3 | 583.0 | 592.7 | 602.4 |
|  | 14.2 | 8.2 | 0.083 | 1.04 | 0.28 | 0.788 | 544.2 | 554.0 | 563.7 | 573.4 | 583.1 | 592.8 | 602.5 |
|  | 14.0 | 6.5 | 0.078 | 0.97 | 0.35 | 0.735 | 544.2 | 554.0 | 563.7 | 573.4 | 583.1 | 592.8 | 602.5 |
|  | 13.8 | 4.8 | 0.073 | 0.90 | 0.42 | 0.682 | 544.2 | 554.0 | 563.7 | 573.4 | 583.1 | 592.8 | 602.5 |
|  | 13.6 | 3.1 | 0.069 | 0.85 | 0.47 | 0.644 | 544.3 | 554.1 | 563.8 | 573.5 | 583.2 | 592.9 | 602.6 |



| Reading of Thermometer, Fahr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | Force of Vapor English lnches. | Weight of Vapor |  | Humidity, Saturation $=$ 1000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { In a } \\ & \text { Cubic } \\ & \text { Foot of } \\ & \text { Air. } \end{aligned}$ |  | Reqd. for Sat'n. of aCn bic Ft . of Air. | Height of the Barometer in English Inches. |  |  |  |  |  |  |
|  |  |  |  |  | ${ }_{28.0}^{i n .}$ |  | in. | $\operatorname{in}_{\mathbf{2 9 . 0}}$ | ${ }_{29.5}^{\text {in. }}$ | in. | $\operatorname{in.}_{\mathbf{3 0 . 5}}$ | $\sin ^{\text {in }}$ |
| Dry. | Wet. |  |  |  |  |  |  |  |  |  |  |  |
| $21^{\circ}$ | $\bigcirc$ | $\bigcirc$ | in. | gr. | gr |  |  | gr. | gr. | gr. | r. | gr. | gr. | r. |
|  | 21.0 | 21.0 | 0.134 | 1.63 | 0.00 | 1.000 | 537.0 | 546.6 | 556.1 | 565.7 | 575.3 | 584.9 | 594.5 |
|  | 20.8 | 19.3 | 0.126 | 1.53 | 0.10 | 0.939 | 537.0 | 546.6 | 556.1 | 565.7 | 575.3 | 384.9 | 594.5 |
|  | 20.6 | 17.6 | 0.118 | 1.44 | 0.19 | 0.954 | 537.1 | 546.7 | 556.2 | 565.8 | 575.4 | 585.0 | 594.6 |
|  | 20.4 | 15.9 | 0.111 | 1.36 | 0.27 | 0.835 | 537.1 | 546.7 | 556.2 | 565.8 | 575.4 | 585.0 | 594.6 |
|  | 20.2 | 14.2 | 0.104 | 1.28 | 0.35 | 0.785 | 537.2 | 546.8 | 556.3 | 565.9 | 575.5 | 585.1 | 594.7 |
|  | 20.0 | 12.5 | 0.098 | 1.20 | 0.13 | 0.736 | 537.2 | 546.8 | 556.3 | 565.9 | 575.5 | 585.1 | 594.7 |
|  | 19.8 | 10.8 | 0.092 | 1.12 | 0.51 | 0.687 | 537.3 | 546.9 | 556.4 | 566.0 | 575.6 | 585.2 | 594.8 |
|  | 19.6 | 9.1 | 0.086 | 1.05 | 0.58 | 0.644 | 537.3 | 546.9 | 556.4 | 566.0 | 575.6 | 585.2 | 594.8 |
|  | 19.4 | 7.4 | 0.051 | 0.99 | 0.64 | 0.607 | 537.3 | 546.9 | 556.4 | 566.0 | 575.6 | 585.2 | 594.8 |
| 22 | 22.0 | 22.0 | 0.139 | 1.69 | 0.00 | 1.000 | 535.7 | 545.3 | 554.9 | 564.5 | 574.0 | 583.6 | 593.1 |
|  | 21.8 | 20.3 | 0.131 | 1.59 | 0.10 | 0.941 | 535.8 | 545.4 | 555.0 | 564.6 | 574.1 | 583.7 | 593.2 |
|  | 21.6 | 18.6 | 0.123 | 1.49 | 0.20 | 0.882 | 535.8 | 54.5 .4 | 555.0 | 564.6 | 574.1 | 583.7 | 593.2 |
|  | 21.4 | 16.9 | 0.115 | 1. 40 | 0.29 | 0.825 | 535.9 | 545.5 | 555.1 | 564.7 | 574.2 | 583.8 | 593.3 |
|  | 21.2 | 15.2 | 0.108 | 1.31 | 0.38 | 0.775 | 535.9 | 545.5 | 555.1 | 564.7 | 574.2 | 583.8 | 593.3 |
|  | 21.0 | 13.5 | 0.102 | 1.23 | 0.46 | 0.728 | 536.0 | 545.6 | 555.2 | 564.8 | 574.3 | 583.9 | 593.4 |
|  | 20.8 | 11.8 | 0.096 | 1.16 | 0.53 | 0.686 | 536.0 | 545.6 | 555.2 | 564.8 | 574.3 | 583.9 | 593.4 |
|  | 20.6 | 10.1 | 0.090 | 1.09 | 0.60 | 0.645 | 536.1 | 545.7 | 555.3 | 564.9 | 574.4 | 584.0 | 593.5 |
|  | 20.4 | 8.4 | 0.084 | 1.02 | 0.67 | 0.604 | 536.1 | 545.7 | 555.3 | 564.9 | 574.4 | 584.0 | 593.5 |
|  | 20.2 | 6.7 | 0.079 | 0.96 | 0.73 | 0.568 | 536.1 | 545.7 | 555.3 | 564.9 | 574.4 | 584.0 | 593.5 |
| 23 | 23.0 | 23.0 | 0.144 | 1.75 | 0.00 | 1.000 | 534.6 | 544.2 | 553.7 | 563.3 | 572.8 | 582.4 | 591.9 |
|  | 22.8 | 21.3 | 0.136 | 1.65 | 0.10 | 0.943 | 534.6 | 544.2 | 553.7 | 563.3 | 572.8 | 582.4 | 591.9 |
|  | 22.6 | 19.6 | 0.127 | 1.55 | 0.20 | 0.856 | 534.7 | 544.3 | 553.8 | 563.4 | 572.9 | 582.5 | 592.0 |
|  | 22.4 | 17.9 | 0.120 | 1.45 | 0.30 | 0.829 | 534.7 | 544.3 | 553.8 | 563.1 | 572.9 | 582.5 | 592.0 |
|  | 22.2 | 16.2 | 0.112 | 1.36 | 0.39 | 0.777 | 534.8 | 544.4 | 553.9 | 563.5 | 573.0 | 582.6 | 592.1 |
|  | 22.0 | 14.5 | 0.106 | 1.25 | 0.47 | 0.731 | 534.8 | 544.4 | 553.9 | 563.5 | 573.0 | 582.6 | 592.1 |
|  | 21.8 | 12.8 | 0.099 | 1.21 | 0.54 | 0.691 | 534.9 | 544.5 | 554.0 | 563.6 | 573.1 | 582.7 | 592.2 |
|  | 21.6 | 11.1 | 0.093 | 1.13 | 0.62 | 0.646 | 534.9 | 544.5 | 554.0 | 563.6 | 573.1 | 582.7 | 592.2 |
|  | 21.4 | 9.4 | 0.057 | 1.06 | 0.69 | 0.606 | 535.0 | 544.6 | 554.1 | 563.7 | 573.2 | 582.8 | 592.3 |
|  | 21.2 | 7.7 | 0.082 | 1.00 | 0.75 | 0.571 | 535.0 | 544.6 | 554.1 | 563.7 | 573.2 | 552.8 | 592.3 |
| 24 | 24.0 | 24.0 | 0.150 | 1.81 | 0.00 | 1.000 | 533.4 | 542.9 | 552.4 | 562.0 | 571.5 | 581.1 | 590.6 |
|  | 23.8 | 22.5 | 0.142 | 1.72 | 0.09 | 0.951 | 533.5 | 543.0 | 552.5 | 562.1 | 571.6 | 581.2 | 590.7 |
|  | 23.6 | 21.1 | 0.135 | 1.63 | 0.18 | 0.901 | 533.5 | 543.1 | 552.5 | 562.1 | 571.6 | 581.2 | 590.7 |
|  | 23.4 | 19.6 | 0.127 | 1.55 | 0.26 | 0.856 | 533.6 | 543.2 | 552.6 | 562.2 | 571.7 | 581.3 | 590.8 |
|  | 23.2 | 18.2 | 0.121 | 1.46 | 0.35 | 0.807 | 533.6 | 543.2 | 552.6 | 562.2 | 571.7 | 581.3 | 590.8 |
|  | 23.0 | 16.7 | 0.115 | 1.38 | 0.43 | 0.762 | 533.7 | 543.3 | 552.7 | 562.3 | 571.8 | 581.4 | 590.9 |
|  | 22.8 | 15.2 | 0.105 | 1.31 | 0.50 | 0.724 | 533.7 | 543.3 | 552.7 | 562.3 | 571.8 | 581.4 | 590.9 |
|  | 22.6 | 13.8 | 0.103 | 1.24 | 0.57 | 0.685 | 533.7 | 543.3 | 552.7 | 562.3 | 571.8 | 581.4 | 590.9 |
|  | 22.4 | 12.3 | 0.097 | 1.18 | 0.63 | 0.652 | 533.8 | 543.4 | 552.8 | 562.4 | 571.9 | 581.0 | 591.0 |
|  | 22.2 | 10.8 | - 0.091 | 1.12 | - 0.69 | 0.634 | 533.8 | 543.4 | 552.8 | 562.4 | 571.9 | 581.5 | 591.0 |
| 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Keading of Thermoueter, Fithr. |  | Temp of DewPoint, Fahr. | Force of <br> Fapor in <br> English <br> Inches. | {f4a8444b8-6dc6-4900-b01d-e4533305a469} Wei  <br>  of  V}$\substack{\text { In a } \\ \text { Cubic }}$ | ght <br> apos <br> Reqd. <br> for <br> Sat'n. | $\begin{gathered} \text { Hu- } \\ \text { midity, } \\ \text { Satura- } \\ \text { tion }= \\ 1000 . \end{gathered}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dry. | Wet. |  |  | Air. | bic Ft. of Air. |  | $\operatorname{in}_{\mathbf{i n}}^{\$ .0}$ | $\operatorname{in.}_{28.5}$ | $\operatorname{in.}_{\mathbf{2 9 . 0}}$ | $\operatorname{in.}_{\mathbf{2 9 . 5}}$ | $\operatorname{ing}^{\text {in.0 }}$ | $\frac{\operatorname{in}}{80.5}$ | $\begin{gathered} \text { in } \\ 31.0 \end{gathered}$ |
| $25^{\circ}$ | $\bigcirc$ | $\bigcirc$ | in. | gr | gr |  | gr. | gr. | gr. | gr. | gr. | gr . | gr. |
|  | 25.0 | 2.5 .0 | 0.15 .5 | 1.57 | 0.00 | 1.000 | 532.3 | 541.8 | 551.3 | 560.8 | 570.3 | 579.8 | 559.3 |
|  | 24.8 | 23. 7 | 0.148 | 1.78 | 0.09 | 0.9.52 | 532.3 | 541.5 | 551.3 | 560.8 | 570.3 | 579.8 | 5.9 .3 |
|  | 24.6 | 2.2 .1 | 0.141 | 1.70 | 0.17 | 0.909 | 532.4 | 541.9 | 551.4 | 560.9 | 570.4 | 579.9 | 589.4 |
|  | 24.4 | 21.2 | 0.135 | 1.62 | 0.25 | 0.867 | 532.4 | 541.9 | 551.4 | 560.9 | 570.4 | 579.9 | 559.1 |
|  | 24.2 | 19.9 | 0.129 | 1.55 | 0.32 | 0.829 | 532.4 | 541.9 | 55i.4 | 560.9 | 570.4 | 579.9 | 559.4 |
|  | 24.0 | 18.6 | 0.123 | 1.48 | 0.49 | 0.791 | 532.5 | 542.0 | 551.5 | 561.0 | 570.5 | 580.0 | 589.5 |
|  | 23.8 | 17.3 | 0.117 | 1.41 | 0.46 | 0.754 | 532.5 | 542.0 | 551.5 | 561.0 | 570.5 | 580.0 | 589.5 |
|  | 23.6 | 16.0 | 0.112 | 1.34 | 0.53 | 0.717 | 532.6 | 542.1 | 551.6 | 561.1 | 570.6 | 580.1 | 589.6 |
|  | 23.4 | 14.8 | 0.107 | 1.28 | 0.59 | 0.685 | 532.6 | 542.1 | 551.6 | 56 I .1 | 570.6 | 580.1 | 559.6 |
|  | 23.2 | 13.5 | 0.102 | 1.22 | 0.65 | 0.653 | 532.6 | 542.1 | 551.6 | 561.1 | 570.6 | 580.1 | 589.6 |
| 26 | 26.0 | 26.0 | 0.161 | 1.93 | 0.00 | 1.000 | 531.1 | 540.6 | 550.0 | 559.5 | 569.0 | 578.5 | 588.0 |
|  | 25.8 | 24.8 | 0.154 | 1.85 | 0.08 | 0.959 | 531.2 | $5 \cdot 10.7$ | 550.1 | 559.6 | 569.1 | 578.6 | 588.1 |
|  | 25.6 | 23.6 | 0.147 | 1.78 | 0.15 | 0.923 | 531.2 | 540.7 | 550.1 | 559.6 | 569.1 | 575.6 | 585.1 |
|  | 25.4 | 23.3 | 0.111 | 1.70 | 0.23 | 0.881 | 531.2 | 540.7 | 550.1 | 559.6 | 569.1 | 578.6 | 588.1 |
|  | 25.2 | 21.2 | 0.135 | 1.62 | 0.31 | 0.539 | 531.3 | 540.8 | 550.2 | 559.7 | 569.2 | 578.7 | 588.2 |
|  | 25.0 | 19.9 | 0.129 | 1.55 | 0.38 | 0.804 | 531.3 | 5408 | 550.2 | 559.7 | 569.2 | 578.7 | 588.2 |
|  | 2 2. 8 | 18.7 | 0.123 | 1.48 | 0.45 | 0.767 | 531.4 | 540.9 | 550.3 | 559.8 | 569.3 | 578.8 | 588.3 |
|  | 24.6 | 17.5 | 0.118 | 1.41 | 0.52 | 0.731 | 531.4 | 510.9 | 550.3 | 559.8 | 569.3 | 578.8 | 588.3 |
|  | 24.4 | 16.2 | 0.112 | 1.35 | 0.58 | 0.700 | 531.4 | 540.9 | 550.3 | 559.8 | 569.3 | 578.8 | 58.3 |
|  | 24.2 | 15.0 | 0.108 | 1.29 | 0.64 | 0.668 | 531.5 | 541.0 | 550.4 | 559.9 | 569.4 | 578.9 | 58..4 |
| 27 | 27.0 | 27.0 | 0.167 | 2.00 | 0.00 | 1.000 | 529.9 | 539.4 | 548.9 | 558.4 | 567.8 | 577.3 | 586.7 |
|  | 26.7 | 25.2 | 0.156 | 1.88 | 0.12 | 0.940 | 529.9 | 539.4 | 548.9 | 558.4 | 567.8 | 577.4 | 586.8 |
|  | 26.4 | $2: 3.3$ | 0.146 | 1.76 | 0.24 | 0.880 | 530.0 | 589.5 | 549.0 | 5.58 .5 | 567.9 | 577.5 | 586.9 |
|  | 26.1 | 21.5 | 0.137 | 1.64 | 0.36 | 0.820 | 530.1 | 539.6 | 549.1 | 558.6 | 568.0 | 577.6 | 587.0 |
|  | 25.8 | 19.7 | 0.128 | 1.53 | 0.47 | 0.765 | 530.1 | 539.6 | 549.1 | 558.6 | 568.0 | 577.6 | 557.0 |
|  | 2.5 .5 | 17.8 | 0.119 | 1.43 | 0.57 | 0.715 | 530.2 | 539.7 | 549.2 | 558.7 | 568.1 | 577.7 | 587.1 |
|  | 25.2 | 16.0 | 0.112 | 1.34 | 0.66 | 0.670 | 530.3 | 539.8 | 549.3 | 5.58 .8 | 568.2 | 577.8 | 557.2 |
|  | 24.9 | 14.2 | 0.104 | 1.26 | 0.74 | 0.630 | 530.3 | 539.8 | 549.3 | 558.8 | 568.2 | 577.8 | 587.2 |
|  | 24.6 | 12.4 | 0.098 | 1.17 | 0.83 | 0.585 | 530.4 | 539.9 | 549.4 | 558.9 | 568.3 | 577.9 | 557.3 |
|  | 24.3 | 10.5 | 0.091 | 1.09 | 0.91 | 0.545 | 530.5 | 540.0 | 549.5 | 559.0 | 568.3 | 577.9 | 557.3 |
| 28 | 28.0 | 28.0 | 0.173 | 2.07 | 0.00 | 1.000 | 528.7 | 538.1 | 547.6 | 557.0 | 566.5 | 575.9 | 58.3 .4 |
|  | 27.7 | 26.3 | 0.163 | 1.95 | 0.12 | 0.942 | 528.8 | 538.2 | 547.7 | 557.1 | 566.6 | 576.0 | 585.. |
|  | 27.1 | 24.6 | 0.153 | 1.84 | 0.23 | 0.889 | $52 \mathrm{S.9}$ | 538.3 | 547.8 | 5.75 | 566.7 | 576.1 | 585.6 |
|  | 27.1 | 22.9 | 0.141 | 1.73 | 0.34 | 0.836 | 528.9 | 5:38.3 | 547.8 | 557.2 | 566.7 | 576.1 | 58.5 .6 |
|  | 26.8 | 21.2 | 0.135 | $1.6 \%$ | 0.45 | 0.783 | 529.0 | 535.4 | 547.9 | 557.3 | 566.8 | 576.2 | 555.7 |
|  | 26.5 | 19.4 | 0.126 | 1.52 | 0.55 | 0.734 | 529.1 | 538.5 | 548.0 | 557.4 | 566.9 | 576.3 | 585.8 |
|  | 26.2 | 17.7 | 0.119 | 1.42 | 0.65 | 0.686 | 529.1 | 538.5 | 548.0 | 557.4 | 566.9 | 576.3 | 585.5 |
|  | 25.9 | 16.0 | 0.112 | 1.34 | 0.73 | 0.648 | 529.2 | 538.6 | 548.1 | 557.5 | 567.0 | 576.4 | . 88.5 .9 |
|  | 25.6 | 14.3 | 0.105 | 1.26 | 0.82 | 0.604 | 529.2 | 538.6 | 548.1 | 557.5 | 567.0 | 576.4 | 585.9 |
| 1 | 25.3 | 12.6 | 0.098 | 1.18 | 0.59 | 0.571 | 529.2 | 538.6 | 548.1 | 557.5 | 567.0 | 576.4 | 555.9 |


| Reading of Thermometer, Fahr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | $\begin{array}{\|c\|} \text { Force } \\ \text { of } \\ \text { Vapor } \\ \text { in } \\ \text { Euglish } \\ \text { lnches. } \end{array}$ | Weight of Vapor |  | IIumidity, Saturation $=$ 1 Ou0. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a Cubic Foot of Air. |  | Reqd <br> Sat'n. of aCubic Ft. of Air. | Ileight of the Barometer in English Inches. |  |  |  |  |  |  |
|  |  |  |  |  | $\operatorname{in}_{28.0}$ |  | $\begin{gathered} \text { in. } \\ 28.5 \end{gathered}$ | $\underset{\mathbf{2 9 . 0}}{\text { in. }}$ | $\operatorname{in}_{\mathbf{2 9} .5}$ | $\sin _{30.0}$ | $\operatorname{in.}_{\mathbf{3 0 . 5}}$ | $\mathbf{3 n}^{\text {in.0 }}$ |
| Dry. | Wet. |  |  |  |  |  |  |  |  |  |  |  |
| $29^{\circ}$ | - | $\bigcirc$ | in. | gr. | gr |  |  | gr. | gr. | gr. | gr. | gr | gr. | gr. |
|  | 29.0 | 29.0 | 0.179 | 2.14 | 0.00 | 1.000 | 527.6 | 537.0 | 5465 | 555.9 | 565.3 | 574.7 | 5S4.1 |
|  | 28.7 | 27.5 | 0.170 | 2.03 | 0.11 | 0.949 | 527.7 | 537.1 | 546.6 | 556.0 | 565.4 | 574.8 | 584.2 |
|  | 28.4 | 26.0 | 0.161 | 1.92 | 0.22 | 0.898 | 527.7 | 537.1 | 546.6 | 556.0 | 56.5.4 | 574.8 | 584.2 |
|  | 28.1 | 24.5 | 0.152 | 1.82 | 0.32 | 0.851 | 527.8 | 537.2 | 546.7 | 556.1 | 265.5 | 574.9 | 584.3 |
|  | 27.8 | 23.0 | 0.144 | 1.73 | 0.41 | 0.809 | 527.8 | 537.2 | 546.7 | 556.1 | 565.5 | 574.9 | 584.3 |
|  | 27.5 | 21.5 | 0.137 | 1.64 | 0.50 | 0.766 | 527.9 | 537.3 | 546.7 | 556.2 | 565.6 | 575.0 | 584.5 |
|  | 27.2 | 20.0 | 0.129 | 1.55 | 0.59 | 0.725 | 528.0 | 537.4 | 5468 | 556.2 | 565.7 | 575.1 | 584.6 |
|  | 26.9 | 18.5 | 0.122 | 1.47 | 0.67 | 0.687 | 528.0 | 537.4 | 546.8 | 556.3 | 565.7 | 575.2 | 584.6 |
|  | 26.6 | 17.0 | 0.116 | 1.38 | 0.76 | 0.645 | 528.1 | 537.5 | 546.9 | 556.4 | 565.8 | 575.3 | 584.7 |
|  | 26.3 | 15.5 | 0.110 | 1.30 | 0.84 | 0.617 | 528.1 | 537.5 | 546.9 | 556.4 | 565.8 | 575.3 | 58.1.7 |
| 30 | 30.0 | 30.0 | 0.186 | 2.21 | 0.00 | 1.000 | 526.5 | 535.9 | 515.3 | 554.7 | 564.1 | 573.5 | 582.9 |
|  | 29.7 | 28.6 | 0.177 | 2.10 | 0.11 | 0.951 | 526.5 | 535.9 | 545.3 | 554.7 | 564.1 | 573.5 | 582.9 |
|  | 29.4 | 27.2 | 0.168 | 2.00 | 0.21 | 0.905 | 526.6 | 536.0 | 545.4 | 554.8 | 564.2 | 573.6 | 583.0 |
|  | 29.1 | 25.9 | 0.160 | 1.91 | 0.130 | 0.864 | 526.7 | 536.1 | 545.5 | 554.9 | 564.3 | 573.7 | 583.1 |
|  | 28.8 | 24.5 | 0.152 | 1.82 | 0.39 | 0.824 | 526.7 | 536.1 | 545.5 | 554.9 | 564.3 | 573.7 | 583.1 |
|  | 28.5 | 23.1 | 0.145 | 1.73 | 0.48 | 0.783 | 526.8 | 536.2 | 545.6 | 555.0 | 564.4 | 573.8 | 583.2 |
|  | 28.2 | 21.7 | 0.138 | 1.64 | 0.57 | 0.742 | 526.8 | 536.2 | 545.6 | 555.0 | 564.4 | 573.8 | 583.2 |
|  | 27.9 | 20.3 | 0.131 | 1.56 | 0.6.5 | 0.706 | 526.9 | 536.3 | 545.7 | 555.1 | 564.5 | 573.9 | 583.3 |
|  | 27.6 | 19.0 | 0.12. | 1.49 | 0.72 | 0.674 | 526.9 | 536.3 | 545.7 | 555.1 | 564.5 | 573.9 | 583.3 |
|  | 27.3 | 17.6 | 0.118 | 1.42 | 0.79 | 0.643 | 527.0 | 536.4 | 545.8 | 555.2 | 564.6 | 574.0 | 583.4 |
| 31 | 31.0 | 31.0 | 0.192 | 2.29 | 0.00 | 1.000 | 525.4 | 534.7 | 544.1 | 553.5 | 562.9 | 572.3 | 581.7 |
|  | 30.7 | 29.9 | 0.185 | 2.20 | 0.09 | 0.961 | 525. 4 | 534.7 | 544.1 | 553.5 | 562.9 | 572.3 | 581.7 |
|  | 30.4 | 28.8 | 0.178 | 2.12 | 0.17 | 0.926 | 525.5 | 534.8 | 544.2 | 553.6 | 563.0 | 572.4 | 581.8 |
|  | 30.1 | 27.7 | 0.171 | 2.04 | 0.2.5 | 0.891 | 525.5 | 534.8 | 54.2 | 553.6 | 563.0 | 572.4 | 581.8 |
|  | 29.8 | 26.6 | 0.164 | 1.95 | 0.34 | 0.852 | 525.6 | 534.9 | 544.3 | 553.7 | 563.1 | 572.5 | 581.9 |
|  | 29.5 | 2.5 | 0.158 | 1.87 | 0.42 | 0.817 | 525.6 | 534.9 | 544.3 | 553.7 | 563.1 | 572.5 | 581.9 |
|  | 29.2 | 24.4 | 0.152 | 1.80 | 0.49 | 0.786 | 525.6 | 534.9 | 544.3 | 553.7 | 563.1 | 572.5 | 581.9 |
|  | 28.9 | 23.4 | 0.146 | 1.73 | 0.56 | 0.756 | 525.7 | 535.0 | 544.4 | 553.8 | 563.2 | 572.6 | 582.0 |
|  | 28.6 | 22.3 | 0.141 | 1.67 | 0.62 | 0.729 | 525.7 | 535.0 | 544.4 | 553.8 | 563.2 | 572.6 | 582.0 |
|  | 25.3 | 21.2 | 0.135 | 1.60 | 0.69 | 0.699 | 525.7 | 535.0 | 544.4 | 553.8 | 563.2 | 572.6 | 582.0 |
| 32 | 32.0 | 32.0 | 0.199 | 2.37 | 0.00 | 1.000 | 524.2 | 533.5 | 542.9 | 552.3 | 561.6 | 570.9 | 580.3 |
|  | 31.6 | 30.8 | 0.191 | 2.27 | 0.10 | 0.958 | 524.3 | 533.6 | 543.0 | 552.4 | 561.7 | 571.0 | 580.4 |
|  | 31.2 | 29.5 | 0.182 | 2.17 | 0.20 | 0.916 | 524.4 | 533.7 | 543.1 | 552.5 | 561.8 | 571.1 | 580.5 |
|  | 30.8 | 28.3 | 0.175 | 2.07 | 0.30 | 0.874 | 524.4 | 533.7 | 543.1 | 552.5 | 561.8 | 571.1 | 580.6 |
|  | 30.4 | 27.0 | 0.167 | 1.98 | 0.39 | 0.836 | 524.5 | 533.8 | 543.2 | 552.6 | 561.9 | 571.2 | 550.6 |
|  | 30.0 | 25.8 | 0.160 | 1.90 | 0.47 | 0.802 | 524.5 | 533.8 | 543.2 | 552.6 | 561.9 | 571.2 | 580.6 |
|  | 29.6 | 24.6 | 0.153 | 1.82 | 0.55 | 0.768 | 524.6 | 533.9 | 543.3 | 552.7 | 562.0 | 571.3 | 580.7 |
|  | 29.2 | 23.3 | 0.146 | 1.74 | 0.63 | 0.735 | 524.6 | 533.9 | 543.3 | 552.7 | 562.0 | 571.3 | 580.7 |
|  | 28.8 | 22.1 | 0.140 | 1.67 | 0.70 | 0.705 | 524.6 | 533.9 | 543.3 | 552.7 | 562.0 | 571.3 | 580.7 |
|  | 28.4 | 20.8 | 0.133 | 1.60 | 0.77 | 0.675 | 524.7 | 534.0 | 543.4 | 552.8 | 562.1 | 571.4 | 580.8 |


| Reading of Thernometer, Fahr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | Force of <br> Vapor in <br> English Inches. | Weight of Vapor |  | $\begin{aligned} & \text { IIu- } \\ & \text { midity, } \\ & \text { Satura- } \\ & \text { tiou }= \\ & 1000 . \end{aligned}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { Reqd. } \\ & \text { for } \end{aligned}$ | Height of the Barometer in Euglish Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | bie Ft. of Air. |  | in. | $\operatorname{in.}_{28.5}$ | $\operatorname{in.}_{\mathbf{2 9 . 0}}$ | $\begin{gathered} \text { in. } \\ 29.5 \end{gathered}$ | $\begin{array}{\|c\|} \operatorname{in} . \\ \mathbf{3 0 . 0} \end{array}$ | $\frac{\operatorname{in}}{\mathbf{3 0 . 5}}$ | $\begin{gathered} \operatorname{in} \\ \mathbf{3 1 . 0} \end{gathered}$ |
| $33^{\circ}$ | $\stackrel{0}{33.0}$ |  | 33.0 | in. 0.207 | gr. 2.45 |  | gr 0.00 | 1.000 | $\begin{aligned} & \text { gr. } \\ & 23.0 \end{aligned}$ | gr. | gr. 5.11 .7 | gr. | gr. | $\begin{gathered} \text { gr. } \\ 569.7 \end{gathered}$ | $\begin{gathered} \mathrm{gr} . \\ 579.1 \end{gathered}$ |
|  |  |  | 0.19 | 2.33 | 0.12 | 0.951 | , |  |  |  | 50.5 | 69.8 | 79.3 |
|  |  | 0. | 0 | 2.22 | 0.2 : | 0.906 | 5 |  |  | 3 | 560.6 | 569.9 | 79.3 |
|  | 31.5 | 28.8 | 0.178 | 2.11 | 0.34 | 0.562 | 523.3 | 532.7 | 542.0 | 551.4 | 560.7 | 570.0 | 579.4 |
|  | 31.0 | 27.4 | 0.169 | 2.01 | 0.44 | 0.821 | 523.3 | 532.7 | 542.0 | 551.4 | 560.7 | 570.0 | 579.4 |
|  | 30.5 | 26.0 | 0.161 | 1.91 | 0.54 | 0.780 | 523.4 | 532.8 | 542.1 | 551.5 | 560.8 | 570.1 | 579.5 |
|  | 30.0 | 24.6 | $0.15 \%$ | 1.82 | 0.63 | 0.743 | 523.4 | 532.8 | 542.1 | 551.5 | 560.8 | 570.1 | 579.5 |
|  | 29.5 | 23.2 | 0.145 | 1.74 | 0.71 | 0.711 | 523.5 | 532.9 | 542.2 | 551.6 | 560.9 | 570.2 | 579.6 |
|  | 29.0 | 21.8 | 0.138 | 1.65 | 0.80 | 0.674 | 523.5 | 532.9 | 542.2 | 551.6 | 560.9 | 570.2 | 579.6 |
|  | 28.5 | 20.4 | 0.131 | 1.57 | 0.88 | 0.641 | 523.6 | 533.0 | 542.3 | 551.7 | 561.0 | 570.3 | 579.7 |
| 34 | 34.0 | 34.0 | 0.214 | 2.53 | 0.00 | 1.000 | 521.9 | 531.2 | 540.6 | 549.9 | 559.2 | 568.5 | 577.8 |
|  | 33.5 | 32.7 | 0.204 | 2.42 | 0.11 | 0.957 | 522.0 | 531.4 | 540.7 | 550.0 | 559.3 | 568.6 | 577.9 |
|  | 33.0 | 31.4 | 0.195 | 2.31 | 0.22 | 0.913 | 522.0 | 531.4 | 540.7 | 550.0 | 559.3 | 568.6 | 577.9 |
|  | 32.5 | 30.1 | 0.186 | 2.21 | 0.32 | 0.574 | 522.1 | 531.5 | 540.8 | 550.1 | 559.4 | 568.7 | 578.0 |
|  | 32.0 | 28.8 | 0.175 | 2.11 | 0.12 | 0.834 | 522.1 | 531.5 | 540.8 | 550.1 | 559.4 | 568.7 | 575.0 |
| 35 | 31.5 | 27.5 | 0.170 | 2.01 | 0.52 | 0.795 | 522.2 | 531.6 | 540.9 | 550.2 | 559.5 | 568.8 | 578.1 |
|  | 31.0 | 26.2 | 0.162 | 1.91 | 0.62 | 0.755 | 522.3 | 531.7 | 541.0 | 550.3 | 559.6 | 568.9 | 578.2 |
|  | 30.5 | 24.9 | 0.153 | 1.83 | 0.70 | 0.724 | 522.3 | 531.7 | 541.0 | 550.3 | 559.6 | 568.9 | 578.2 |
|  | 30.0 | 23.6 | 0.147 | 1.75 | 0.78 | 0.692 | 522.4 | 531.5 | 541.1 | 550.4 | 559.7 | 569.0 | 578.3 |
|  | 29.5 | 22.3 | 0.141 | 1.67 | 0.86 | 0.660 | 522.4 | 531.8 | 541.1 | 550.4 | 559.7 | 569.0 | 578.3 |
|  | 29.0 | 21.0 | 0.134 | 1.59 | 0.94 | 0.629 | 522.5 | 531.9 | 541.2 | 550.5 | 559.8 | 569.1 | 578.4 |
|  | 35 | 35.0 | 0.222 | 2.62 | 0.00 | 1.000 | 520.8 | 530.1 | 539.4 | 548.7 | 558.0 | 567.3 | 576.6 |
|  | 34 | 32.5 | 0.203 | 2.40 | 0.22 | 0.916 | 520.9 | 530.2 | 539.5 | 548.8 | 558.1 | 567.4 | 576.7 |
|  | 33 | 30.0 | 0.186 | 2.19 | 0.43 | 0.836 | 521.0 | 530.3 | 539.6 | 548.9 | 558.3 | 567.5 | 576.8 |
|  | 32 | 27.5 | 0.170 | 2.00 | 0.62 | 0.764 | 521.1 | 530.4 | 539.7 | 549.0 | 558.4 | 567.6 | 576.9 |
|  | 31 | 25.0 | 0.155 | 1.53 | 0.79 | 0.698 | 521.2 | 530.5 | 539.8 | 549.1 | 558.5 | 567.7 | 577.0 |
| 36 | 30 | 22.5 | 0.142 | 1.68 | 0.94 | 0.641 | 521.3 | 530.6 | 539.9 | 549.2 | 558.6 | 567.8 | 577.1 |
|  | 29 | 20.0 | 0.129 | 1.53 | 1.09 | 0.584 | 521.3 | 530.7 | 540.0 | 549.8 | 558.6 | 567.9 | 577.2 |
|  | 28 | 17.5 | 0.117 | 1.39 | 1.23 | 0.531 | 521.4 | 530.8 | 540.1 | 549.4 | 558.7 | 568.0 | 577.3 |
|  | 27 | 15.0 | 0.103 | 1.27 | 1.35 | 0.485 | 521.5 | 530.9 | 540.2 | 549.5 | 558.7 | 568.1 | 577.4 |
|  | 36 | 36.0 | 0.230 | 2.71 | 0.00 | 1.000 | 519.7 | 529.0 | 538.3 | 547.5 | 5.56 .9 | 566.1 | 575.4 |
|  | 35 | 33.5 | 0.210 | 2.48 | 0.23 | 0.915 | 519.8 | 529.1 | 538.4 | 547.6 | 556.9 | 566.2 | 575.5 |
|  | 34 | 31.0 | 0.192 | 2.27 | 0.44 | 0.838 | 519.9 | 529.2 | 538.5 | 547.7 | 557.0 | 566.3 | 575.6 |
|  | 33 | 28.5 | 0.176 | 2.07 | 0.64 | 0.764 | 520.0 | 529.3 | 538.6 | 547.8 | 557.1 | 566.4 | 575.7 |
|  | 32 | 26.0 | 0.161 | 1.89 | 0.82 | 0.698 | 520.1 | 529.4 | 538.7 | 547.9 | 557.2 | 566.5 | 575.8 |
|  | 31 | 23.5 | 0.147 | 1.74 | 0.97 | 0.642 | 520.2 | 529.5 | 538.8 | 548.0 | 557.3 | 566.6 | 575.9 |
|  | 30 | 21.0 | 0.134 | 1.58 | 1.13 | 0.583 | 520.3 | 529.6 | 535.9 | 518.1 | 557.4 | 566.7 | 576.0 |
|  | 29 | 18.5 | 0.122 | 1.45 | 1.26 | 0.5:35 | 520.4 | 529.7 | 539.0 | 548.2 | 557.5 | 566.8 | 576.1 |
|  | 28 | 16.0 | 0.112 | 1.32 | 1.39 | 0.487 | 520.5 | 529.8 | 539.1 | 548.3 | 557.6 | 566.9 | 576.2 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |



| Reading of Thermometer, Filir. |  | Temp. of JewPoint, Fahr. | Force of <br> Vapor in <br> English <br> Incues. | $\begin{array}{r} \text { Weit } \\ \text { of } \mathrm{V} \\ \ln \mathrm{a} \end{array}$ | ight <br> apor <br> Reqd. <br> for | $\begin{aligned} & \text { Hu- } \\ & \text { midity, } \\ & \text { Sarura- } \\ & \text { tion }= \\ & 1.000 . \end{aligned}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dry. | We |  |  | Font of Air. | bic Ft. of Air . |  | $\operatorname{in.}_{28.0}$ | $\operatorname{in.}_{2 \% .5}$ | $\operatorname{in.~}_{29.0}$ | $\operatorname{in.}_{\mathbf{i n} .5}$ | $\operatorname{in}_{\mathrm{in} .}^{\mathbf{3} .0}$ | ${ }_{\mathbf{3 0} .5}^{\text {in. }}$ | $\mathbf{i n .}$ |
| $\bigcirc$ | - | $\bigcirc$ | in. | gr | gr |  | gr. | gr. | gr | gr. | gr | gr. | gr. |
| 41 | 41 | 41.0 | 0.274 | 3.19 | 0.00 | 1.000 | 514.1 | 52:3.3 | 532.5 | 541.6 | 550.8 | 560.0 | 569.2 |
|  | 40 | 38.8 | 0.253 | 2.96 | 0.23 | 0.928 | 514.2 | 523.4 | 532.6 | 541.7 | 550.9 | 5601 | 509.3 |
|  | 39 | 36.6 | 0.235 | 2.74 | 0.45 | 0.659 | 51.1 .3 | 523.5 | 5327 | 541.8 | 551.0 | 560.2 | 569.4 |
|  | 38 | 34.4 | 0.217 | 2.54 | 0.6 .5 | 0.796 | 514.4 | 523.6 | 532.8 | 541.9 | 551.1 | 560.3 | 569.5 |
|  | 37 | 32.2 | 0.201 | 2.35 | 0.84 | 0.737 | 514.5 | 523.7 | 532.9 | 54.0 | 551.2 | 560.1 | 54.96 |
|  | 36 | 30.0 | 0.186 | 2.16 | 1.03 | 0.677 | 514.6 | 523.8 | 533.0 | 542.1 | 551.3 | 560.5 | 569.7 |
|  | 35 | 27.8 | 0.172 | 2.01 | 1.18 | 0.630 | 514.7 | 523.9 | 5331 | 542.2 | 551.4 | 560.6 | 569.8 |
|  | 34 | 2.5 .6 | 0.158 | 1.85 | 1.34 | 0580 | 514.8 | 524.0 | 533.2 | 542.3 | 551.5 | 560.7 | 563.9 .9 |
|  | 33 | 23.4 | 0.146 | 1.71 | 1.18 | 0.5336 | 514.9 | 524.1 | 5333.3 | 542.4 | 551.6 | 560.8 | 570.0 |
|  | 32 | 21.2 | 0.135 | 1.58 | 1.61 | 0.495 | 514.9 | 524.1 | 533.3 | 542.5 | 551.7 | 560.9 | 570.1 |
|  | 31 | 19.0 | 0.125 | 1.46 | 1.73 | 0.458 | 515.0 | 524.2 | 533.4 | 542.6 | 551.8 | 561.0 | 570.2 |
| 42 | 42 | 42.0 | 0.283 | 3.30 | 0.00 | 1.000 | 513.0 | 522.2 | 531.3 | 540.5 | 549.6 | 558.8 | 5679 |
|  | 41 | 39.8 | 0.263 | 3.06 | 0.24 | 0.927 | 513.1 | 522.3 | 531.4 | 540.6 | 549.7 | 558.9 | 568.0 |
|  | 40 | 37.6 | 0.243 | 2.83 | 0.47 | 0.8 .38 | 513.2 | 522.4 | 531.5 | 540.7 | 549.9 | 559.0 | 568.1 |
|  | 39 | 3.5 .4 | 0.225 | 2.63 | 0.67 | 0.797 | 513.3 | 52.3.5 | 531.6 | 540.8 | 550.0 | 559.1 | 568.2 |
|  | 38 | 33.2 | 0.208 | 2.43 | 0.87 | 0.736 | 51:3.4 | 522.6 | 531.7 | 540.9 | 5.50 .1 | 559.2 | 568.3 |
|  | 37 | 31.0 | 0.192 | 2.24 | 1.06 | 0.679 | 513.5 | 522.7 | 531.8 | 541.0 | 5.50 .2 | 599.3 | 568.4 |
|  | 36 | 28.8 | 0.178 | 2.08 | 1.22 | 0.631 | 513.6 | 52.2 .6 | 531.9 | 541.1 | 550.3 | 5.59 .4 | 568.5 |
|  | 85 | 26.6 | 0.164 | 1.91 | 1.39 | 0.579 | 513.7 | 522.9 | $5: 32.0$ | 541.2 | 550.4 | 5.59 .5 | 56s. 6 |
|  | 34 | 24.1 | 0.152 | 1.77 | 1.58 | 0.536 | 513.8 | 52:3.0 | $5: 32.1$ | $5+1.3$ | 550.5 | 559.6 | 568.7 |
|  | 33 | 22.2 | 0.140 | 1.6:3 | 1.67 | 0.494 | 513.9 | 523.1 | $5: 32.2$ | 541.4 | 5.50 .6 | 559.7 | 568.8 |
|  | 32 | 20.0 | 0.129 | 1.51 | 1.79 | 0.6 .58 | 513.9 | 523.1 | 532.3 | 541.5 | 5.50 .6 | 559.8 | 569.0 |
| 43 | 43 | 43.0 | 0.293 | 3.11 | 0.00 | 1.000 | 511.8 | 520.9 | 530.1 | 539.3 | 548.4 | 5.37.5 | 5667 |
|  | 42 | 40.8 | 0.272 | 3.16 | 0.2 .5 | 0.927 | 511.9 | 521.0 | 530.2 | 589.4 | 518.6 | 557.7 | 566.9 |
|  | 41 | 38.6 | 0.252 | 2.93 | 0.18 | 0.8 .59 | 512.0 | 521.1 | 5:30.3 | $5: 39.5$ | 548.7 | 557.8 | 567.0 |
|  | 40 | 36.1 | 0.283 | 2.71 | 0.70 | 0.795 | 512.1 | 521.2 | 5:30.4 | 539.6 | 548.8 | 557.9 | 567.1 |
|  | 39 | 34.2 | 0.216 | 2.51 | 0.90 | 0.736 | 512.2 | 521.3 | $5: 30.5$ | 5:19.7 | 548.9 | 558.0 | 567.2 |
|  | 38 | 32.0 | 0.199 | 2.32 | 1.09 | 0.650 | 512.3 | 521.4 | 530.7 | 539.8 | 549.0 | 558.1 | 567.8 |
|  | 37 | 29.8 | 0.184 | 2.15 | 1.26 | 0.630 | 512.4 | 521.5 | 530.8 | 539.9 | 549.1 | 558.2 | $56 \% .4$ |
|  | 36 | 27.6 | 0.170 | 1.98 | 1.18 | 0.581 | 512.5 | $5 \because 1.6$ | 530.9 | 510.0 | 549.2 | 558.8 | 567.5 |
|  | 3.3 | 2.5 .1 | 0.1 .97 | 1.82 | 1.59 | 0.534 | 512.6 | 521.7 | 531.0 | 540.1 | 549.3 | 558.4 | 567.6 |
|  | 34 | 23.2 | 0.115 | 1.69 | 1.72 | 0.49 .5 | 512.7 | 521.8 | 5:31.1 | 510.3 | 5.49 .4 | 555.5 | 567.7 |
|  | 33 | 21.0 | 0.134 | 1.56 | 1.85 | 0.458 | 512.9 | 52.3 .0 | 581.2 | 540.3 | 549.5 | 555.6 | 567.8 |
| 44 | 44 | 44.0 | 0.304 | 3 52 | 0.00 | 1000 | 510.8 | 519.9 | 529.0 | 538.1 | 547.3 | 556.4 | 56.5 .5 |
|  | 43 | 41.8 | 0.252 | 3.27 | 0.2 .5 | 0.929 | 510.9 | 520.0 | 529.1 | 538.2 | 547.5 | 556.5 | 565.7 |
|  | 42 | 39.6 | 0.261 | 3.02 | 0.50 | 0.858 | 511.0 | 520.1 | 5292 | 538.3 | 547.6 | 556.6 | 565.8 |
|  | 41 | 37.1 | 0.241 | 2.80 | 0.72 | 0.796 | 511.1 | 520.2 | 529.3 | 538.4 | 547.7 | 556.7 | 56.5 .9 |
|  | 40 | 3.5 .2 | $0.2 \cdot 3$ | 2.60 | 0.92 | 0.739 | 511.2 | 520.3 | 529.4 | 538.5 | 547.8 | 556.8 | 566.0 |
|  | 39 | 33.0 | 0.207 | 2.10 | 1.12 | 0.682 | 511.3 | 520.4 | 529.5 | 538.6 | 547.9 | 556.9 | 566.1 |
|  | 38 | 30.8 | 0.191 | 2.23 | 1.30 | 0.631 | 511.4 | 520.5 | 529.6 | 538.7 | 548.0 | 557.0 | 566.2 |
|  | 37 | 28.6 | 0.177 | 2.0 .5 | 1.47 | 0.582 | 511.5 | 520.6 | 529.7 | 538.8 | 548.1 | 557.1 | 566.3 |
|  | 36 | 26.4 | 0.16:3 | 1.89 | 1.63 | 0.537 | 511.6 | 520.7 | 529.8 | 538.9 | 548.2 | 557.2 | 566.4 |
|  | 35 | 21.2 | 0.1 .51 | 1.75 | 1.77 | 0.497 | 511.7 | 520.8 | 529.9 | 539.0 | 548.3 | 557.3 | 566.5 |
|  | 34 | 22.0 | 0.139 | 1.62 | 1.90 | 0.160 | 511.7 | 520.8 | 530.0 | 589.1 | 548.3 | 5.57 .1 | 566.6 |


| Reading of 'Thermoneter, Fialur. |  | $\begin{aligned} & \text { Temp. } \\ & \text { of } \\ & \text { ofew- } \\ & \text { Poont, } \\ & \text { Fuhr. } \end{aligned}$ | $\begin{gathered} \text { Force } \\ \text { of } \\ \text { Vinpor } \\ \text { int } \\ \text { English } \\ \text { lnches. } \end{gathered}$ | Weight of Viapor |  | Humidity, Satura$1011=$1.000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a |  |  | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air | of actu- bic F't. of Air. |  | $\stackrel{i n}{28.0}$ | $\operatorname{in.}_{28.5}^{2}$ | $\mathrm{in}_{\mathbf{2 9 . 0}}$ | $\cos _{29.5}$ | $\begin{gathered} \text { in. } \\ \mathbf{3 0 . 0} \end{gathered}$ | $\operatorname{sin.~}_{\mathbf{3 @} \mathbf{5}}$ | 31. |
| 45 |  |  | $\bigcirc$ | in. | gr |  | gr. |  | 09.7 | 18. | -7 | - | 16 | gr. | 4 |
|  | 4.5 | 4.5 .0 | 0.31 .5 | 3.64 | 0.00 | 1.000 | 509.7 | 518.8 | 527.9 | 537.0 | 546.1 | 555.2 | 564.3 |
|  | 41 | +2.9 | 0.292 | 3.39 | 0.25 | 0.931 | 509.8 | 518.9 | 525.0 | 537.1 | 546.3 | 5553 | 564.5 |
|  | 43 | 40.8 | 0.272 | 3.14 | 0.50 | 0.863 | 509.9 | 519.0 | 5251 | 537.2 | 546.4 | 555.4 | 564.6 |
|  | 12 | 38.7 | 0.253 | 2.92 | 0.72 | 0.802 | 510.0 | 519.1 | 525.2 | 537.3 | 546.5 | 555.5 | 564.7 |
|  | 41 | 36.6 | 0.23.5 | 2.70 | 0.91 | 0.742 | 510.1 | 519.2 | 528.3 | 537.4 | 546.6 | 555.6 | 5648 |
|  | 40 | 34.5 | 0.218 | 2.52 | 1.12 | 0.692 | 510.2 | 519.3 | 528.4 | 537.5 | 546.7 | 5.55 .7 | 564.9 |
|  | 39 | 32.4 | 0.203 | 2.34 | 1.30 | 0.643 | 510.3 | 519.4 | 5285 | 537.6 | 546.8 | 555.8 | 565.0 |
|  | 38 | 30.3 | 0.188 | 2.16 | 1.45 | 0593 | 510.4 | 519.5 | 528.6 | 537.7 | 546.9 | 5.55.9 | 565.1 |
|  | 37 | 28.2 | 0.174 | 2.01 | 1.63 | 0.552 | 510.5 | 519.6 | 528.7 | 537.8 | 547.0 | 556.0 | 56.5 .2 |
|  | 36 | 26.1 | 0.161 | 1.57 | 1.77 | 0.514 | 510.6 | 519.7 | 528.8 | 537.9 | 547.1 | 556.1 | 565.3 |
|  | 35 | 24.0 | 0.1 .50 | 1.73 | 1.91 | 0.475 | 510.7 | 519.8 | 525.9 | 538.0 | 547.2 | 556.3 | 565.4 |
| 46 | 46 | 46.0 | 0.326 | 3.76 | 0.00 | 1.000 | 508.6 | 517.7 | 526.7 | 335.8 | 544.9 | 554.0 | 563.1 |
|  | 45 | 43.9 | 0.3')3 | 3.50 | 0.26 | 0.931 | 508.7 | 517.8 | 526.8 | 535.9 | 545.0 | 554.1 | 563.2 |
|  | 44 | 41.8 | 0.232 | 3.25 | 0.51 | 0.864 | 505.8 | 517.9 | 526.9 | 5:36.0 | 545.1 | 554.2 | 563.3 |
|  | 43 | 39.7 | 0.262 | 3.02 | 0.74 | 0.803 | 508.9 | 518.0 | 527.0 | 536.1 | 545.2 | 554.3 | 563.4 |
|  | 42 | 37.6 | 0.243 | 2.90 | 0.96 | 0.74. 5 | 509.0 | 518.1 | 527.2 | 536.3 | 545.4 | 554.5 | 563.6 |
|  | 41 | 3.5.5 | 0.226 | 2.61 | 1.15 | 0.694 | 509.1 | 518.2 | 527.3 | 536.4 | 545.5 | 554.6 | 563.7 |
|  | 40 | 33.4 | 0.210 | 2.42 | 1.34 | 0.643 | 509.2 | 518.3 | 527.1 | 536.5 | 5.55 .6 | 554.7 | 563.8 |
|  | 39 | 31.3 | 0.114 | $\underline{2.24}$ | 1.52 | 0.596 | 509.3 | 518.4 | 527.5 | 536.6 | 545.7 | 554.8 | 563.9 |
|  | 38 | 29.2 | 0.180 | 2.08 | 1.68 | 0.553 | 509.4 | 518.5 | 527.6 | 536.7 | 545.8 | 554.9 | 564.0 |
|  | 37 | 27.1 | 0.167 | 1.93 | 1.83 | 0.514 | 509.5 | 518.6 | 527.7 | 5:36.8 | 515.9 | 555.0 | 564.1 |
|  | 36 | 25.0 | 0.15.5 | 1.79 | 1.97 | 0.476 | 509.5 | 518.6 | 527.7 | 536.8 | 545.9 | 555.0 | 564.1 |
| 47 | 47 | 7.0 | 0.337 | 3.88 | 0.00 | 1.000 | 507.5 | 516.5 | 525.6 | 534.7 | 543.8 | 552.8 | 561.9 |
|  | 46 | 44.9 | 0.:313 | 3.62 | 0.26 | 0.933: | 507.6 | 516.6 | 32.5 .7 | 534.8 | 543.9 | 552.9 | 562.0 |
|  | 4.5 | 42.5 | 0.291 | 3.36 | 0.52 | 0.866 | 507.8 | 516.7 | 525.9 | 5355.0 | 544.1 | 553.1 | 562.2 |
|  | 4 | 40.7 | 0.271 | 3.12 | 0.76 | 0.604 | 507.9 | 516.8 | 526.0 | 535.1 | 544.2 | 5.33 .2 | 562.3 |
|  | 43 | 38.6 | 0.2 .52 | 2.90 | 0.98 | 0.717 | 508.0 | 516.9 | 526.1 | 535.2 | 544.3 | 553.3 | 562.4 |
|  | 42 | 36.5 | 0.234 | 2.70 | 1.18 | 0.696 | 50ヶ. 1 | 517.0 | 526.3 | 53.5.3 | 544.4 | 55\%.4 | 562.5 |
|  | 41 | 34.1 | 0.217 | 2.51 | 1.37 | 0.647 | 508.2 | 517.1 | 526.3 | 53.5.4 | 544.5 | 553.5 | 562.6 |
|  | 40 | 32.3 | 0.201 | 2.32 | 1.36 | 0.998 | 508.3 | 517.2 | 526.4 | 5:35.5 | 541.6 | 553.6 | 562.7 |
|  | 39 | 30.2 | 0.187 | 2.16 | 1.72 | 0.5 .57 | 508.4 | 517.3 | 526.5 | 53.3.6 | 544.7 | 553.7 | 562.8 |
|  | 38 | 29.1 | 0.173 | 2.00 | 1.88 | 0.515 | 508.5 | 517.1 | 5266 | 533.7 | 544.8 | 553.6 | 562.9 |
|  | 37 | 26.0 | 0.161 | 185 | 2.03 | 0.177 | 508.5 | 517.6 | 526.7 | 535.6 | 544.9 | 554.0 | 563.1 |
| 48 | . 18 | 48.0 | 0.349 | 4.01 | 0.00 | 1.000 | 506.1 | 515.4 | 524.5 | 533.5 | 512.6 | 551.6 | 560.7 |
|  | 47 | 45.9 | 0.321 | 3.73 | 0.28 | 0.930 | 506.5 | 515.5 | 524.6 | 533.7 | 542.8 | 551.8 | 560.9 |
|  | 46 | 43.2 | 0.302 | 3.47 | 0.51 | 086.5 | 506.6 | 515.6 | 5247 | 533.8 | 54.9 | 551.9 | 561.0 |
|  | 4.5 | 41.7 | 0.281 | 3.23 | 0.78 | 0.50 .5 | 5067 | 51.5 .7 | 524.8 | 5:3:.9 | 543.0 | 552.0 | 561.1 |
|  | 4 | 39.6 | 0.361 | 3.00 | 1.01 | 0.748 | 506.8 | 515.8 | 524.9 | $53+.0$ | 543.1 | 5.22 .1 | 561.2 |
|  | 43 | 87.5 | 0.212 | 2.79 | 1.22 | 0.696 | 506.9 | 51.5.9 | 52.5.0 | 534.1 | 543.2 | 552.2 | 561.3 |
|  | 42 | 35.4 | 0.225 | 2.60 | 1.41 | 0.648 | 507.0 | 516.0 | 52.5.1 | 534.2 | 543.3 | 552.3 | 561.4 |
|  | $4^{1}$ | 33.3 | 0.209 | 2.40 | 1.61 | 0.995 | 507.1 | 516.1 | 525.2 | 5:3.4 | 543.5 | 552.5 | 561.5 |
|  | 40 | 31.2 | 0.191 | 2.21 | 1.77 | 0.5 .58 | 507.2 | 516.2 | 525.3 | 531.5 | 543.5 | $55: 2.5$ | 561.6 |
|  | 39 | 29.1 | 0.180 | 2.07 | 1.91 | 0.316 | 507.3 | 516.3 | 52.5 .4 | 584.6 | 543.6 | 552.6 | 561.6 |
|  | 39 | 27.0 | 0.167 | 1.92 | 2.09 | 0.479 | 507.4 | 516.4 | 52.5 .5 | 531.7 | $5+3.6$ | 552.7 | 561.7 |
|  | 37 | 24.9 | 0.1.35 | 1.77 | 2.21 | 0.441 | 507.4 | 516.4 | 525.6 | 534.7 | 513.7 | 552.8 | 561.8 |


| Reading of Thermometer, Fahr. |  | Temp of DewPoint, Fahr. | Force of Vapor in English Inches. | Weight of Vapor |  | $\begin{aligned} & \text { IIu- } \\ & \text { midity, } \\ & \text { Satura- } \\ & \text { tion }= \\ & 1000 . \end{aligned}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Reqd. |  |  |  |  |  |  |  |  |
|  |  |  |  |  | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | bic F t. of Air. |  | $\operatorname{in}_{28.0}$ | $\operatorname{ing}_{28.5}$ | $\operatorname{in.}_{\mathbf{2 9} .0}$ | $\operatorname{in.}_{29.5}$ | $\operatorname{ing}_{\mathbf{3 0} .0}$ | $\operatorname{ing}_{\mathbf{3 0} .5}$ | $\operatorname{in}^{\text {in }}$ |
| $\begin{array}{r} \circ \\ 49 \end{array}$ | $\bigcirc$ |  | $\bigcirc$ | in. | gr. |  | gr |  | gr. | gr. | gr . | gr. | gr. | gr. | r. |
|  | 49 |  | 49.0 | 0.361 | 4.14 | 0.00 | 1.000 | 505.3 | 514.3 | 523.3 | 53.3 .3 | 541.4 | 550.4 | 559.4 |
|  | 48 | 46.9 | 0.336 | 3.55 | 0.29 | 0.930 | 505.4 | 514.4 | 523.4 | 532.4 | 541.5 | 550.5 | 559.5 |
|  | 47 | 44.8 | 0.312 | 3.59 | 0.55 | 0.567 | 505.6 | 514.6 | 523.6 | 532.6 | 541.7 | 550.7 | 559.7 |
|  | 46 | 42.7 | 0.290 | 3.34 | 0.80 | 0.807 | 505.7 | 514.7 | 523.7 | 532.7 | 541.8 | 550.6 | 559.8 |
|  | 45 | 40.6 | 0.270 | 3.10 | 1.04 | 0.749 | 505.9 | 514.9 | 523.8 | 532.9 | 542.0 | 551.0 | 560.0 |
|  | 44 | 38.5 | 0.251 | 2.88 | 1.26 | 0.696 | 506.0 | 515.0 | 523.9 | 533.0 | 542.1 | 551.1 | 560.1 |
|  | 43 | 36.4 | 0.233 | 2.68 | 1.46 | 0.647 | 506.1 | 515.1 | 524.0 | 533.1 | 542.2 | 551.2 | 560.2 |
|  | 42 | 34.3 | 0.216 | 2.49 | 1.65 | 0.601 | 506.2 | 515.2 | 524.1 | 533.2 | 542.3 | 551.3 | 560.3 |
|  | 41 | 32.2 | 0.201 | 2.32 | 1.82 | 0.560 | 506.3 | 515.3 | 524.2 | 5333.3 | 542.4 | 5.51 .4 | 560.4 |
|  | 40 | 30.1 | 0.186 | 2.14 | 2.00 | 0.517 | 506.3 | 515.3 | 5243 | 533.4 | 542.5 | 551.5 | 560.5 |
|  | 39 | 28.0 | 0.173 | 1.99 | 2.15 | 0.481 | 506.4 | 515.4 | 524.4 | 533.5 | 542.6 | 551.6 | 560.6 |
|  | 38 | 25.9 | 0.160 | 1.84 | 2.30 | 0.444 | 506.4 | 51.5 .4 | 524.4 | 533.5 | 542.6 | 551.6 | 560.6 |
| 50 | 50 | 50.0 | 0.373 | 4.28 | 0.00 | 1.000 | 504.1 | 513.1 | 522.1 | 531.1 | 540.2 | 549.2 | 558.2 |
|  | 49 | 45.0 | 0.349 | 3.99 | 0.29 | 0.932 | 504.2 | 513.2 | 522.2 | 531.2 | 540.3 | 519.3 | 558.3 |
|  | 48 | 46.0 | 0.326 | 3.73 | 0.55 | 0.571 | 504.4 | 513.4 | 522.4 | 531.4 | 540.5 | 549.5 | 558.5 |
|  | 47 | 44.0 | 0.304 | 3.48 | 0.80 | 0.813 | 504.5 | 513.5 | 524.5 | 531.5 | 540.6 | 549.6 | 558.6 |
|  | 46 | 42.0 | 0.283 | 3.25 | 1.03 | 0.759 | 504.6 | 513.6 | 522.6 | 531.6 | 540.7 | 5.49 .7 | 558.7 |
|  | 45 | 40.0 | 0.264 | 3.03 | 1.25 | 0.708 | 504.5 | 513.8 | 522.8 | 531.8 | 540.9 | 549.9 | 558.9 |
|  | 44 | 38.0 | 0.246 | 2.82 | 1.46 | 0.659 | 504.9 | 513.9 | 522.9 | 532.0 | 541.0 | 550.0 | 559.0 |
|  | 43 | 36.0 | 0.230 | 2.63 | 1.65 | 0.614 | 505.1 | 514.1 | 523.1 | 5:92.1 | 541.2 | 550.2 | 559.2 |
|  | 42 | 34.0 | 0.214 | 2.45 | 1.83 | 0.572 | 505.2 | 514.2 | 523.2 | 532.2 | 541.3 | 550.3 | 559.3 |
|  | 41 | 32.0 | 0.199 | 2.28 | 2.00 | 0.533 | 50.5 .3 | 514.3 | 523.3 | 532.3 | 541.4 | 550.4 | 559.4 |
|  | 40 | 30.0 | 0.186 | 2.12 | 2.16 | 0.49 .5 | 505.4 | 514.4 | 523.4 | 532.4 | 541.5 | 550.5 | 559.5 |
|  | 39 | 28.0 | 0.173 | 1.97 | 2.31 | 0.460 | 505.5 | 514.5 | 523.5 | 5332.5 | 541.6 | 550.6 | 559.6 |
| 51 | 51 | 51.0 | 0.38 | 4.42 | 0.00 | 1.000 | 503.1 | 512.1 | 521.1 | 530.0 | 539.0 | 548.0 | 557.0 |
|  | 50 | 49.0 | 0.361 | 4.12 | 0.30 | 0.932 | 503.2 | 512.2 | 521.2 | 530.1 | 539.1 | 548.1 | $55 \% .1$ |
|  | 49 | 47.0 | 0.337 | 3.85 | 0.57 | 0.871 | 503.3 | 512.3 | 521.3 | 530.3 | 539.3 | 548.3 | 557.3 |
|  | 48 | 45.0 | 0.315 | 3.60 | 0.82 | 0.514 | 503.4 | 512.4 | 521.4 | 530.4 | 539.-1 | 548.4 | 557.4 |
|  | 47 | 43.0 | 0.293 | 3.36 | 1.06 | 0.760 | 503.5 | 512.5 | 521.5 | 530.5 | 539.5 | 548.5 | 557.5 |
|  | 46 | 41.0 | 0.274 | 3.13 | 1.29 | 0.708 | 503.7 | 512.7 | 521.7 | 5:30.7 | 539.7 | 548.7 | 557.7 |
|  | 45 | 39.0 | 0.255 | 2.92 | 1.50 | 0.661 | 503.8 | 512.8 | 521.5 | 530.8 | 539.8 | 548.8 | 557.8 |
|  | 44 | 37.0 | 0.235 | 2.72 | 1.70 | 0.615 | 503.9 | 512.9 | 521.9 | 5:30.9 | 539.9 | 548.9 | 557.9 |
|  | 43 | 3.5 .0 | 0.222 | 2.54 | 1.85 | 0.575 | 504.0 | 513.0 | 522.0 | 531.0 | 540.0 | 5.19 .0 | 555.0 |
|  | 42 | 33.0 | 0.207 | 2.36 | 2.06 | 0.534 | 504.1 | 513.1 | 5221 | 531.1 | 540.1 | 549.1 | 5.58 .1 |
|  | 41 | 31.0 | 0.192 | 2.20 | 2.22 | 0.498 | 504.2 | 513.2 | 522.2 | 531.2 | 540.3 | 549.3 | 558.3 |
|  | 40 | 29.0 | 0.179 | 2.05 | 2.37 | 0.464 | 504.3 | 513.3 | 523.3 | 5:31.3 | 540.4 | 549.4 | 559.4 |
| 52 | 52 | 52.0 | 0.400 | 4.56 | 0.00 | 1.000 | 502.1 | 511.0 | 520.0 | 528.9 | 537.9 | $5-16.8$ | 55.5.5 |
|  | 51 | 50.0 | 0.373 | 4.26 | 0.30 | 0.9:34 | 502.2 | 511.1 | 520.1 | 529.0 | 538.0 | 546.9 | 55.5.9 |
|  | 50 | 48.0 | 0.349 | 3.98 | 0.58 | 0.873 | 502.4 | 511.3 | 520.3 | 529.2 | 538.2 | 547.1 | 5.56 .1 |
|  | 49 | 46.0 | 0.326 | 3.72 | 0.84 | 0.816 | 502.5 | 511.4 | 520.4 | 529.3 | 5:36.3 | 5.47 .2 | 556.2 |
|  | 48 | 44.0 | 0.304 | 3.47 | 1.09 | 0.761 | 502.6 | 511.5 | 520.5 | 529.4 | 538.4 | 5.47 .3 | 556.3 |
|  | 47 | 42.0 | 0.283 | 3.23 | 1.33 | 0.709 | 502.8 | 511.7 | 520.7 | 529.6 | 538.6 | 547.5 | 556.5 |
|  | 16 | 40.0 | 0.264 | 3.02 | 1.54 | 0.662 | 502.9 | 511.5 | 520.8 | 529.7 | 538.7 | 547.6 | 556.6 |
|  | 45 | 38.0 | 0.246 | 2.81 | 1.75 | 0.616 | 502.9 | 511.9 | 520.9 | 529.8 | 538.8 | 547.8 | 556.8 |
|  | 44 | 36.0 | 0.230 | 2.63 | 1.93 | 0.577 | 503.1 | 512.0 | 521.0 | 529.9 | 539.0 | 548.0 | 557.0 |
|  | 43 | 34.0 | 0.214 | 2.44 | 2.12 | 0.535 | 50.3 .2 | 512.1 | 521.1 | 530.0 | 539.1 | 548.1 | 557.1 |
|  | 42 | 32.0 | 0.199 | 2.28 | 2.28 | 0.500 | 50.3 .3 | 512.3 | 521.3 | 530.2 | 5399.2 | 548.2 | $55 \% .2$ |
|  | 41 | $\left.\right\|_{1} 30.0$ | 0.156 | 2.13 | 2.43 | 0.467 | 503.4 | 512.4 | 521.4 | 530.3 | 539.3 | 548.3 | 557.3 |


| Reading of Thermometer, Fahr. |  | $\begin{aligned} & \text { Temp. } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | $\begin{aligned} & \text { Force } \\ & \text { of } \\ & \text { Vapor } \\ & \text { in } \\ & \text { English } \\ & \text { Inches. } \end{aligned}$ | Weight of Vapor |  | $\begin{aligned} & \text { Hu- } \\ & \text { midity, } \\ & \text { Satura- } \\ & \text { tion }= \\ & 1.000 . \end{aligned}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a |  |  | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Foot of Air. | of aCu tic Ft. of Air. |  | ${ }_{28.0}^{\text {in. }}$ | $\operatorname{in.}_{28.5}$ | $\begin{array}{r} \text { in. } \\ \mathbf{2 9 . 0} \end{array}$ | $\operatorname{in.}_{\mathbf{2 9 . 5}}$ | $\begin{aligned} & \text { in. } \\ & \mathbf{0 . 0} \\ & \hline \end{aligned}$ | $\operatorname{in.}_{\mathbf{3 0 . 5}}$ | $3 \mathrm{in} .0$ |
| 53 |  |  | - | in. | gr |  | gr. |  | gr. | gr. | gr. | $\mathrm{gr}_{\text {gr }}$ | gr. | ${ }_{\text {gr }}$ | 6 |
|  | 53 | 53.0 | 0.414 | 4.71 | 0.00 | 1.000 | 500.9 | 509.8 | 518.8 | 527.7 | 536.7 | 545.6 | 554.6 |
|  | 52 | 51.0 | 0.386 | 4.40 | 0.31 | 0.934 | 501.1 | 510.0 | 519.0 | 527.9 | 536.9 | 5458 | 55.4 .8 |
|  | 51 | 49.0 | 0.361 | 4.11 | 0.60 | 0.873 | 501.2 | 510.1 | 5191 | 528.0 | 537.0 | 545.9 | 554.9 |
|  | 50 | 47.0 | 0.337 | 3.84 | 0.87 | 0.815 | 501.4 | 510.3 | 519.3 | 528.2 | 537.2 | 546.1 | 555.1 |
|  | 49 | 45.0 | 0.315 | 3.58 | 1.13 | 0.760 | 501.5 | 510.4 | 519.4 | 528.3 | 537.3 | 546.2 | 555.2 |
|  | 48 | 43.0 | 0.293 | 3.34 | 1.37 | 0.709 | 501.6 | 510.5 | 519.5 | 528.4 | 537.4 | 546.3 | 555.3 |
|  | 47 | 41.0 | 0.274 | 3.12 | 1.59 | 0.662 | 501.7 | 510.6 | 5196 | 528.5 | 537.5 | 546.4 | 555.4 |
|  | 46 | 39.0 | 0.255 | 2.91 | 1.80 | 0.618 | 501.5 | 510.7 | 519.7 | 528.6 | 537.6 | 546.5 | 555.5 |
|  | 45 | 37.0 | 0.238 | 2.71 | 2.00 | 0.575 | 502.0 | 510.9 | 519.9 | 528.8 | 537.8 | 546.7 | 555.7 |
|  | 44 | 35.0 | 0.222 | 2.53 | 2.18 | 0.537 | 502.1 | 511.0 | 520.0 | 528.9 | 537.9 | 546.8 | 555.8 |
|  | 43 | 330 | 0.207 | 2.35 | 2.36 | 0.499 | 502.1 | 511.0 | 520.0 | 528.9 | 238.0 | 546.9 | 55.5.9 |
|  | 42 | 31.0 | 0.192 | 2.18 | 2.53 | 0.463 | 502.2 | 511.1 | 520.1 | 529.0 | 538.1 | 547.0 | 556.0 |
| 54 | 54 | 54.0 | 0.428 | 4.86 | 0.00 | 1.000 | 499.9 | 505.8 | 517.8 | 526.7 | 535.6 | 544.5 | 553.5 |
|  | 53 | 52.0 | 0.400 | 4.54 | 0.32 | 0.934 | 500.0 | 508.9 | 517.9 | 526.8 | 535.7 | 54.6 | 553.6 |
|  | 52 | 50.0 | 0.373 | 4.25 | 0.61 | 0.875 | 500.2 | 509.1 | 518.1 | 527.0 | 535.9 | 544.5 | 553.8 |
|  | 51 | 48.0 | 0.349 | 3.96 | 0.90 | 0.815 | 500.3 | 509.2 | 518.2 | 527.1 | 536.0 | 544.9 | 553.9 |
|  | 50 | 46.0 | 0.326 | 3.70 | 1.16 | 0.761 | 500.4 | 509.3 | 518.3 | 527.2 | 536.1 | 545.0 | 554.0 |
|  | 49 | 4.0 | 0.304 | 3.45 | 1.41 | 0.709 | 500.6 | 509.5 | 518.5 | 527.4 | 536.3 | 545.2 | 554.2 |
|  | 48 | 42.0 | 0.283 | 3.23 | 1.63 | 0.665 | 500.7 | 509.6 | 518.6 | 527.5 | 536.4 | 545.3 | 554.3 |
|  | 47 | 40.0 | 0.264 | 3.01 | 1.85 | 0.619 | 500.8 | 509.7 | 518.7 | 527.6 | 536.5 | 545.4 | 554.4 |
|  | 46 | 38.0 | 0.246 | 2.80 | 2.06 | 0.576 | 500.9 | 509.8 | 518.8 | 527.7 | 536.7 | 545.6 | 554.6 |
|  | 45 | 36.0 | 0.230 | 2.61 | 2.25 | 0.537 | 501.0 | 509.9 | 518.9 | 527.8 | 536.8 | 545.7 | 554.7 |
|  | 4 | 34.0 | 0.214 | 2.43 | 2.43 | 0.500 | 501.1 | 510.0 | 519.0 | 527.9 | 536.9 | 545.8 | 55.48 |
|  | 43 | 32.0 | 0.199 | 2.27 | 2.59 | 0.467 | 501.2 | 510.1 | 519.1 | 528.0 | 537.0 | 545.9 | 554.9 |
|  | 42 | 30.0 | 0.186 | 2.10 | 2.76 | 0.432 | 501.3 | 510.2 | 519.2 | 528.1 | 537.1 | 546.0 | 555.0 |
|  | 41 | 28.0 | 0.173 | 1.96 | 2.90 | 0.403 | 501.1 | 510.3 | 519.3 | 528.2 | 537.2 | 546.1 | 555.1 |
|  | 40 | 26.0 | 0.161 | 1.82 | 3.04 | 0.375 | 501.5 | 510.4 | 519.4 | 528.3 | 537.3 | 546.2 | 555.2 |
| 55 | 55 | 55.0 | 0.442 | 5.02 | 0.00 | 1.000 | 498.8 | 507.7 | 516.6 | 525.5 | 53.4 | 543.3 | 552.2 |
|  | 54 | 53.3 | 0.418 | 4.74 | 0.23 | 0.944 | 499.0 | 507.9 | 516.8 | 525.7 | 53.1 .6 | 543.5 | 5.52 .4 |
|  | 53 | 51.6 | 0.394 | 4.46 | 0.56 | 0.888 | 499.1 | 508.0 | 516.9 | 525.8 | 534.7 | 543.6 | 552.5 |
|  | 52 | 49.9 | 0.372 | 4.23 | 0.79 | 0.843 | 499.3 | 508.2 | 517.1 | 526.0 | 534.9 | 543.8 | 552.7 |
|  | 51 | 48.2 | 0.3 .51 | 3.98 | 1.04 | 0.793 | 499.4 | 508.3 | 517.2 | 526.1 | 535.0 | 543.9 | 552.8 |
|  | 50 | 46.5 | 0.331 | 376 | 1.26 | 0.749 | 499.5 | 508.4 | 517.3 | 526.2 | 535.1 | 544.0 | 552.9 |
|  | 49 | 4.8 | 0.312 | 3.55 | 1.47 | 0.707 | 499.7 | 508.6 | 517.5 | 526.3 | 535,3 | 544.2 | 553.1 |
|  | 48 | 43.1 | 0.295 | 3.34 | 1.68 | 0.665 | 499.8 | 508.7 | 517.6 | 526.5 | 535.4 | 544.3 | 553.3 |
|  | 47 | 41.4 | 0.278 | 3.14 | 1.88 | 0626 | 499.8 | 508.7 | 517.6 | 526.6 | 535.5 | 544.4 | 5.53 .4 |
|  | 46 | 39.7 | 0.262 | 2.97 | 2.05 | 0.591 | 499.9 | 505.8 | 517.7 | 526.7 | 535.6 | 544.5 | 5.53.5 |
|  | 45 | 38.0 | 0.246 | 2.79 | 2.23 | 0.5 .56 | 500.0 | 508.9 | 517.9 | 526.8 | 535.7 | 54.6 | 553.6 |
|  | 4 | 36.3 | 0.232 | 2.64 | 2.38 | 0.526 | 500.1 | 509.0 | 518.0 | 526.9 | 535.8 | 544.7 | 558.7 |
|  | 43 | 34.6 | 0.219 | 2.17 | 2.55 | 0.492 | 500.2 | 509.1 | 518.1 | 527.0 | 535.9 | 544.8 | 553.8 |
|  | 42 | 32.9 | 0.206 | 2.32 | 2.70 | 0.462 | 500.3 | 509.2 | 518.2 | 527.1 | 536.0 | 544.9 | 553.9 |
|  | 41 | 31.2 | 0.194 | 2.20 | 2.82 | 0.438 | 500.4 | 509.3 | 518.3 | 527.1 | 5:6.0 | 54+.9 | 554.0 |
|  | 40 | 29.5 | 0.182 | 2.07 | 2.95 | 0.412 | 500.5 | 509.3 | 518.4 | 527.2 | 536.1 | 545.0 | 554.1 |
|  | 39 | 27.8 | 0.172 | 1.95 | 3.07 | 0.388 | 500.6 | 509.1 | 518.5 | 527.3 | 536.2 | 545.1 | 5.4 .2 |
|  | 38 | 26.1 | 0.161 | 1.83 | 3.19 | 0.365 | 500.7 | 509.5 | 518.6 | 527.4 | 536.2 | 545.1 | 551.2 |







| Reading of Thermometer, Faur. |  | Temp. of DewPoint, Fahr. | Force of <br> Vapor in <br> English <br> Inches. | Weight of Vajor |  | Ifumidity, Saturation $=$ 1.000. | Weight in Grains of a Cubic Foot of Air |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | a |  | Requd. for | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry |  |  |  | Air. | bic Ft. of Air. |  | $\operatorname{in.}_{28.0}$ | $\mathrm{in}_{2}^{28.5}$ | $\begin{array}{\|c\|} \text { in. } \\ 28.0 \end{array}$ | $\operatorname{in.}_{2(9.5)}$ | $\begin{gathered} \mathrm{in}_{3} \\ \mathbf{3 0 . 0} \end{gathered}$ | $\frac{\mathrm{in} .}{36.5}$ | $\begin{aligned} & i n . \\ & 31.0 \end{aligned}$ |
|  |  |  | $\bigcirc$ | in. | gr |  | gr. |  | gr | gr. | gr . | gr. | gr. | r. | gr. |
| 66 | 66 | 66.0 | 0.638 | 7.08 | 0.00 | 1.000 | 187.0 | 495.7 | 504.4 | 513.1 | 521.8 | 520.5 | 539.2 |
|  | 65 | 6.4 .4 | 0.605 | 6.72 | 0.36 | 0.949 | 487.2 | 495.9 | 504.6 | 51:.3 | 522.0 | 53817 | 539.1 |
|  | 64 | 62.8 | 0.574 | 6.35 | 0.73 | 0.597 | 457.3 | 196.0 | 5047 | 513.4 | 522.1 | 330.8 | 589.5 |
|  | 63 | 61.2 | 0.544 | 6.04 | 1.04 | 0.5 .53 | 187.5 | 496.2 | 504.9 | 513.6 | 522.3 | 5:31.0 | 539.7 |
|  | 62 | 59.6 | 0.516 | 5.72 | 1.36 | $0.80{ }^{\circ}$ | 157.7 | 496.4 | 50.3 .1 | 513.8 | 52.2 .5 | 531.2 | $5: 399$ |
|  | 61 | 58.0 | 0.489 | 5.42 | 1.66 | 0.766 | 487.9 | 496.6 | 505.3 | 514.0 | 522.7 | $5: 31.4$ | 540.1 |
|  | 60 | 56.1 | 0.464 | 5.14 | 1.94 | 0.726 | 488.0 | 496.7 | 50.54 | 514.1 | 522.5 | 533.5 | 510.2 |
|  | 59 | 54.8 | 0.440 | 4.85 | 2.20 | 0.689 | 458.1 | 496.8 | 50.5 .5 | $51+.2$ | 523.0 | 531.7 | 510.4 |
|  | 53 | 53.2 | 0.416 | 4.62 | 2.46 | 0.652 | 488.2 | 496.9 | 505.6 | 514.3 | 523.1 | 531.8 | 540.5 |
|  | 57 | 51.6 | 0.394 | 4.37 | 2.71 | 0.619 | 488.4 | 497.1 | 505.5 | 514.5 | 52:3.3 | 5:32.0 | 540.7 |
|  | 56 | 50.0 | 0.373 | 4.15 | 2.93 | 0.586 | 488.5 | 497.2 | 505.9 | 514.6 | 52:3.4 | 533.2 .1 | 510.8 |
|  | 55 | 48.1 | 0.354 | 3.92 | 3.16 | 0.553 | 188.6 | 497.3 | 506.1 | 514.8 | 523.5 | 5:32.2 | $5+1.0$ |
|  | 51 | 46.8 | 0.335 | 3.72 | 3.36 | 0.525 | 488.8 | 497.5 | 506.3 | 51.5 .0 | 523.7 | 532.4 | 5.11 .2 |
|  | 53 | 45.2 | 0.317 | 3.51 | 3.57 | 0.496 | 488.9 | 497.6 | 506.4 | 515.1 | 523.8 | 532.5 | $5+1.3$ |
|  | 52 | 43.6 | 0.300 | 3.33 | 3.75 | 0.470 | 489.0 | 497.7 | 506.5 | 515.2 | 523.9 | 5:32.6 | 541.1 |
|  | 51 | 42.0 | 0.233 | 3.14 | 3.94 | 0.443 | 459.1 | 497.8 | 506.6 | 515.3 | 524.0 | 532.7 | 541.5 |
|  | 50 | 10.1 | 0.263 | 2.97 | 4.11 | 0.419 | 489.2 | 497.9 | 506.7 | 515.4 | 524.1 | 533.8 | 541.6 |
|  | 49 | 35.8 | 0.25:3 | 2.81 | 4.27 | 0.397 | 489.3 | 493.0 | 506.8 | 515.5 | 524.2 | 532.9 | 541.7 |
|  | 45 | 37.2 | 0.240 | 2.66 | 4.42 | 0.376 | 489.4 | 498.1 | 506.9 | 515.6 | 524.3 | 533.0 | 541.8 |
|  | 47 | 35.6 | 0.227 | 2.51 | 4.57 | 0.35 .5 | 489.4 | 498.1 | 506.9 | 515.6 | 524.3 | 533.0 | 5-41.8 |
|  | 46 | 34.0 | 0.214 | 2.37 | 4.71 | 0.335 | 489.5 | 498.2 | 507.0 | 515.7 | 52.4 .4 | 5833.1 | 541.9 |
|  | 45 | 32.4 | 0.202 | 221 | 4.84 | 0.316 | 489.6 | 498.3 | 507.1 | 515.8 | 524.5 | 5:33.2 | 542.0 |
|  | 44 | 30.8 | 0.191 | 2.12 | 4.96 | 0.999 | 489.7 | 498.4 | 507.2 | 515.9 | 524.6 | 533.3 | 42.1 |
|  | 43 | 29.2 | 0.180 | 2.00 | 5.0 s | 0.2 si | 489.7 | $19 \mathrm{S.4}$ | 507.2 | 515.9 | 524.6 | 533.3 | 542.1 |
| 67 | 67 | 67.0 | 0.659 | 7.30 | 0.00 | 1.000 | 485.9 | 494.6 | 503.3 | 512.0 | 520.6 | 529.3 | 538.0 |
|  | 66 | 6.5 .4 | 0.626 | 6.98; | $0 .: 37$ | 0.919 | 486.1 | 491.8 | 503.5 | 512.2 | 520.8 | 529.5 | 538.2 |
|  | 6.5 | 63.8 | 0.593 | 6.5 .5 | 0.75 | 0.597 | 486.3 | 49.5.0 | 503.7 | 512.4 | 521.0 | 529.7 | 588.4 |
|  | 64 | 62.2 | 0.56:3 | 6.23 | 1.07 | 0.853 | 486.5 | 49.5.2 | 503.9 | 512.6 | 521.2 | 529.9 | .338.6 |
|  | 63 | 60.6 | 0.534 | 5.931 | 1.39 | 0.810 | 186.7 | 49.5 .4 | 501.1 | 512.8 | 521.4 | 530.1 | 53.8 |
|  | 62 | 59.0 | 0.506 | 5.60 | 1.70 | 0.767 | 486.8 | 495.5 | 501.2 | 512.9 | 521.6 | 530.3 | 589.0 |
|  | 61 | 57.4 | 0.480 | 5.81 | 1.99 | 0.725 | 486.9 | 49.5 .6 | 504.3 | 513.0 | 521.7 | 530.4 | 589.1 |
|  | 60 | 55.5 | 0.455 | 5.04 | 2.26 | 0.691 | 487.1 | 49.5 .8 | 501.5 | 513.2 | 521.9 | 530.6 | 539.3 |
|  | 59 | 54.2 | . 0.481 | 1.77 | 2.53 | 0.65:3 | 487.2 | 49.\%.9 | 504.6 | 513.3 | 522.0 | 530.7 | 589.4 |
|  | 53 | 52.6 | 0.405 | 4.52 | 2.78 | 0.619 | 487.3 | 496.0 | 504.7 | 513.4 | 52.21 | 530.8 | 539.5 |
|  | 57 | 51.0 | 0.336 | 4.25 | 3.02 | 0.586 | 487.5 | 496.2 | 504.9 | 513.6 | $52 \cdot 2.3$ | 531.0 | 539.7 |
|  | 56 | 49.1 | 0.366 | 4.0 .5 | 3.25 | 0.555 | 487.6 | 496.3 | 50.5 .0 | 513.7 | 522.4 | 531.1 | 539.5 |
|  | 5.) | 17.8 | 0.316 | 3.8:3 | 3.47 | 0.524 | 487.9 | 496.5 | 50.5 .1 | 513.8 | 52.2 .6 | 531.2 | 549.9 |
|  | 54 | 46.2 | 0.328 | 3.62 | 365 | 0.49 j | 457.9 | 196.6 | 50.5 .2 | 513.9 | 522.7 | 531.3 | 540.0 |
|  | 53 | 4.6 | 0.310 | 3.43 | 3.87 | 0.470 | 488.0 | 496.7 | 50.5 .3 | 514.0 | 52.2 .8 | 531.4 | 540.1 |
|  | 52 | 43.0 | 0.393 | 3.25 | 4.05 | 0.445 | 488.1 | 496.8 | 504.4 | 514.1 | 522.9 | 531.5 | 540.2 |
|  | 51 | 41.4 | 0.278 | 3.08 | 1.22 | 0.422 | 488.2 | 496.9 | 50.5 .5 | 514.2 | 523.0 | 531.6 | 540.3 |
|  | 50 | 39.5 | 0.263 | 2.91 | 4.39 | 0.399 | 483.4 | 497.1 | 50.5 .7 | 514.4 | 523.1 | 531.8 | 540.5 |
|  | 49 | 39.2 | $0.2+8$ | 2.75 | 4.55 | 0.377 | 488.5 | 497.2 | 50.5 .8 | 514.5 | 523.2 | 531.9 | 540.6 |


| Reading of Thermometer, Fuhr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | Force of Vapor in Euglish Inches. | Weight of Vapor |  | Humidity, Saturation $=$ I 000 . | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Reqd. | Height of the Barometer in English Inches. |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | bic $\mathbf{F}^{\prime} \mathrm{t}$. of Air. |  | in. | $\operatorname{ing}_{28.5}$ | $\operatorname{in}_{\mathbf{2 0}}$ | $\operatorname{in.}_{29.5}$ | $\operatorname{in.}_{\mathbf{3 0 . 0}}$ | $\operatorname{in}_{\mathbf{3 0} .5}$ | $\sin ^{\text {in. }}$ |
| $67$ | $\bigcirc$ |  | $\bigcirc$ | in. | gr |  | gr |  | gr. | gr. | gr | gr. | gr. | gr. | r. |
|  | 49 |  | 35.2 | 0.248 | 2.75 | 4.55 | 0.377 | 488.5 | 497.2 | 505.8 | 514.5 | 523.2 | 531.9 | 540.6 |
|  | 48 | 36.6 | 0.235 | 2.60 | 4.70 | 0.356 | 488.6 | 497.3 | 505.9 | 514.6 | 523.3 | 532.0 | 540.7 |
|  | 47 | 35.0 | 0.222 | 2.46 | 4.84 | 0.337 | 488.7 | 497.4 | 505.9 | 514.7 | 52:3.4 | 532.1 | 540.8 |
|  | 46 | 33.4 | 0.210 | 2.32 | 4.98 | 0.318 | 488.7 | 497.4 | 506.0 | 514.7 | 523.4 | 532.1 | 540.8 |
|  | 45 | 31.8 | 0.198 | 2.19 | 5.11 | 0.301 | 488.8 | 497.5 | 506.1 | 514.8 | 523.5 | 532.2 | 540.9 |
|  | 44 | 30.2 | 0.187 | 2.07 | 5.23 | 0.254 | 488.9 | 497.6 | 506.2 | 514.9 | 523.6 | 532.3 | 541.0 |
| 68 | 68 | 68.0 | 0.681 | 7.53 | 0.00 | 1.000 | 484.9 | 493.5 | 502.2 | 510.8 | 519.5 | 528.1 | 536.8 |
|  | 67 | 66.4 | 0.6 .46 | 7.15 | 0.38 | 0.949 | 48.5 .1 | 493.8 | 502.5 | 511.1 | 519.7 | 528.4 | 537.1 |
|  | 66 | 64.8 | 0.613 | 6.77 | 0.76 | 0.899 | 485.3 | 494.0 | 502.6 | 511.2 | 519.9 | 525.6 | 537.3 |
|  | 65 | 63.2 | 0.552 | 6.43 | 1.10 | 0.854 | 485.5 | 494.2 | 5028 | 511.4 | 520.1 | 528.8 | $53 \% .5$ |
|  | 64 | 61.6 | $0.55:$ | 6.10 | 1.43 | 0.810 | 485.7 | 494.4 | 503.0 | 511.6 | 520.3 | 529.0 | 537.7 |
|  | 63 | 60.0 | 0.523 | 5.78 | 1.75 | 0.765 | 485.8 | 49.4 .5 | 503.1 | 511.8 | 520.5 | 529.2 | 537.9 |
|  | 62 | 58.4 | 0.496 | 5.47 | 2.06 | 0.726 | 485.9 | 494.6 | 503.3 | 512.0 | 520.7 | 529.4 | 535.1 |
|  | 61 | 56.8 | 0.470 | 5.20 | 2.33 | 0.691 | 486.0 | 494.7 | 503.4 | 512.1 | 520.8 | 529.5 | 538.3 |
|  | 60 | 5.5.2 | 0.445 | 4.93 | 2.60 | 0.655 | 486.2 | 494.9 | 503.6 | 512.3 | 521.0 | 529.7 | 538.5 |
|  | 59 | 5:3.6 | 0.422 | 4.67 | 2.86 | 0.620 | 486.3 | 495.0 | 503.7 | 512.4 | 521.1 | 529.3 | 535.6 |
|  | 58 | 52.0 | 0.100 | 4.42 | 3.11 | 0.557 | 486.4 | 495.1 | 503.8 | 512.5 | 521.2 | 529.9 | 538.6 |
|  | 57 | 50.4 | 0.379 | 4.19 | 3.34 | 0.556 | 486.6 | 495.3 | 504.0 | 512.7 | 521.4 | 530.1 | 598.8 |
|  | 56 | 48.8 | 0.358 | 3.96 | 3.57 | 0.526 | 486.7 | 495.4 | 504.1 | 512.8 | 521.5 | 530.2 | 535.9 |
|  | 55 | 47.2 | 0.339 | 3.75 | 3.75 | 0.495 | 486.8 | 495.5 | 504.2 | 512.9 | 521.6 | 530.3 | 539.0 |
|  | 54 | 45.6 | 0.321 | 3.54 | 3.99 | 0.470 | 456.9 | 495.6 | 504.3 | 513.0 | 521.7 | 530.4 | 539.1 |
|  | 53 | 44.0 | 0.304 | 3.35 | 4.18 | 0.445 | 487.0 | 495.7 | 504.4 | 513.1 | 521.8 | 530.5 | 539.2 |
|  | 5 | 42.4 | 0.257 | 3.17 | 4.36 | 0.421 | 487.1 | 495.8 | 504.5 | 513.2 | 521.9 | 530.6 | 539.3 |
|  | 51 | 40.8 | 0.272 | 8.00 | 4.53 | 0.399 | 187.2 | 495.9 | 504.6 | 513.3 | 522.0 | 530.7 | 539.4 |
|  | 50 | 39.2 | 0.257 | 2.84 | 4.69 | 0.377 | 487.3 | 496.0 | 504.7 | 513.4 | 522.1 | 530.8 | 539.5 |
|  | 49 | 37.6 | 0.243 | 2.68 | 4.85 | 0.356 | 457.4 | 496.1 | 504.8 | 513.5 | 522.2 | 530.9 | 539.6 |
|  | 48 | 36.0 | 0.230 | 2.54 | 4.99 | 0.337 | 487.5 | 496.2 | 504.9 | 513.6 | 522.3 | 531.0 | 539.7 |
|  | 47 | 34.4 | 0.217 | 2.10 | 5.13 | 0.319 | 487.6 | 496.3 | 505.0 | 513.7 | 5.22 .4 | 531.1 | 539.8 |
|  | 46 | 32.5 | 0.20 .5 | 2.27 | 5.26 | 0.302 | 487.6 | 496.3 | 50.5 .0 | 513.7 | 522.1 | 531.1 | 539.8 |
|  | 45 | 31.2 | 0.194 | 2.15 | 5.35 | 0.286 | 487.7 | 496.4 | 50.5 .1 | 513.8 | 522.5 | 531.2 | 539.9 |
|  | 41 | 29.6 | 0.153 | 2.04 | 5.49 | 0.371 | 487.8 | 496.5 | 505.2 | 513.9 | 522.6 | 531.3 | 540.0 |
| 69 | 69 | 69.0 | 0.704 | 7.76 | 0.00 | 1.000 | 483.8 | 492.4 | 501.1 | 509.7 | 518.3 | 527.0 | 535.6 |
|  | 68 | 67.4 | 0.665 | 7.37 | 0.39 | 0.950 | 484.0 | 492.6 | 501.3 | 509.9 | 518.5 | 527.2 | 53.5 .8 |
|  | 67 | 65.8 | 0.634 | 7.00 | 0.76 | 0.902 | 484.2 | 492.8 | 5015 | 510.1 | 518.7 | 527.4 | 536.0 |
|  | 66 | 61.2 | 0.601 | 6.63 | 1.13 | 0.854 | 484.4 | 493.0 | 501.7 | 510.3 | 518.9 | 527.6 | 5:36.2 |
|  | 6.5 | 62.6 | 0.570 | 6.29 | 1.47 | 0.810 | 484.6 | 493.2 | 501.9 | 510.5 | 519.1 | 527.8 | 536.4 |
|  | 6.4 | 61.0 | 0.541 | 5.97 | 1.79 | 0.769 | 484.8 | 493.4 | 502.1 | 510.7 | 519.3 | 528.0 | 536.6 |
|  | 63 | 59.4 | 0.513 | 5.65 | 2.11 | 0.728 | 485.0 | 493.6 | 502.3 | 510.9 | 519.5 | 528.2 | 536.8 |
|  | 62 | 57.8 | 0.186 | 5.37 | 2.39 | 0.693 | 485.1 | 493.7 | 502.4 | 511.0 | 519.6 | 528.3 | $5: 36.9$ |
|  | 61 | 56.2 | 0.161 | 5.09 | 2.67 | 0.657 | 485.1 | 493.7 | 502.6 | 511.2 | 319.8 | 528.5 | 537.1 |
|  | 60 | 54.6 | 0.137 | 4.82 | 2.94 | 0.621 | 485.2 | 493.9 | 502.7 | 511.3 | 519.9 | $52 \mathrm{S.6}$ | 537.3 |
|  | 59 | 53.0 | 0.114 | 4.57 | 3.19 | 0.589 | 185.4 | 494.1 | 502.8 | 511.5 | 520.1 | 528.8 | 537.5 |
|  | 58 | 51.4 | 0.392 | 4.33 | 3.48 | 0.558 | 485.5 | 49 4.2 | 502.9 | 511.6 | 520.2 | 528.9 | 537.6 |


| Rewding of Thermometer, Fahr. |  | Temp of DewPoint, Fahr. | Force of <br> Vapor in English Inches. | Weight of Vapor |  | Humidity, Saturation $=$ 1000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a for Cubic sat'n. Foot of of aCu- <br> Air. Die Ft. of Air. |  | Height of the Barometer in English Inches. |  |  |  |  |  |  |
|  |  |  |  |  |  |  | in. | in. | n. | in. |
| Dry. | Wet. |  |  |  | $28.0{ }^{6}$ |  | 2 \%.3 | 29.0 |  |  |  |  |
| $\begin{array}{r} \circ \\ 69 \end{array}$ | $\bigcirc$ |  |  |  |  |  | in. | gr. | gr |  | gr. | gr. | gr. | gr. | gr. | gr. | gr. |
|  | 58 | 51.40 | 0.392 | 4.33 3 | 3.430 | 0.55 S | 485.54 | 191.25 | 502.9 5 | 511.65 | 520.2 | 9 | 537.6 |
|  | 57 | 49.80 | 0.371 | 4.09 3 | 3.670 | 0.5274 | 485.7 4 | 494.45 | 503.15 | 511.85 | 520.45 | 529.1 5 | 537.8 |
|  | 56 | 48.20 | 0.351 | 3.87 3 | 3.890 | 0.499 | 485.84 | 494.55 | 503.25 | 511.95 | 520.5 5 | $529.2{ }^{5}$ | 537.9 |
|  | 55 | 46.60 | 0.332 | 3.664 | 4.100 | 0.472 | 485.94 | 494.65 | 503.3 | 512.0 | 520.6 | 529.3 5 | 538.0 |
|  | 54 | 45.0 | 0.315 | 3.47 4 | 4.290 | 0.447 | 486.0 | 494.75 | 503.4 | 512.15 | 520.7 | 529.45 | 5:38.1 |
|  | 53 | 43.4 | 0.298 | 3.29 4 | 4.470 | 0.424 | 456.1 | 494.8 | 503.5 | 512.25 | 520.8 | 529.5 | 535.2 |
|  | 52 | 41.5 | 0.282 | 3.11 t | 4.650 | 0.401 | 486.24 | 494.9 | 503.6 | 512.35 | 520.9 | 529.6 | 538.3 |
| 70 |  |  |  |  |  |  |  |  | 83.7 | 512.4 | 521.0 | 529.7 | 5:38.4 |
|  | 51 | 40.2 | 0.266 | 2.94 | 4.520 |  |  | 495.0 | 0.. 7 | 51.5 | 5.21.1 | 529.8 | 538.5 |
|  | 50 | 38.6 | 0.252 | 2.78 | 4.950 | 0.358 | 486.4 | 495.1 | 503.8 | 512.5 | 521.1 | 529.8 |  |
|  | 49 | 37.0 | 0.238 | 2.635 | 5.130 | 0.339 | 486.5 | 495.2 | 503.9 | 512.6 | 521.2 | 529.9 | 535.6 |
|  | 48 | 35.4 | 0.225 | 2.49 | 5.27 0, | 0.321 | 456.6 | 495.3 | 504.0 | 512.7 | 521.3 | 530.0 | 535.7 |
|  | 47 | 33.8 | 0.213 | 2.34 | 5.420 | 0.30:2 | 456.7 | 49.5 .4 | 504.1 | 512.8 | 521.4 | 530.1 | 535.5 |
|  | 46 | 32.2 | 0.201 | 2.20 | 5.56 | 0.284 | 486.8 | 495.5 | 504.2 | 512.9 | 521.5 | 530.2 | 538.9 |
|  | 45 | 30.6 | 0.190 | 2.06 | 5.70 | 0.266 | 486.8 | 495.5 | 504.2 | 512.9 | 521.5 | 530.2 | 535.9 |
|  | 70 | 70.0 | 0.727 | 8.00 | 0.00 | 1.000 | 482.8 | 491.4 | 500.0 | 508.6 | 517.2 | 525.8 | 534.4 |
|  | 69 | 68.5 | 0.692 | 7.62 | 0.38 | 0.953 | 483.0 | 491.6 | 500.2 | 505.8 | 517.4 | 526.0 | 534.6 |
|  | 68 | 67.0 | 0.659 | 7.26 | 0.74 | 0.907 | 483.2 | 491.5 | 500.4 | 509.0 | 517.6 | 526.2 | 534.5 |
|  | 67 | 65.5 | 0.62 S | 6.91 | 1.09 | 0.865 | 483.3 | 491.9 | 500.5 | 509.1 | 517.7 | 526.3 | 534.9 |
|  | 66 | 64.0 | 0.597 | 6.57 | 1.43 | 0.522 | 483.5 | 492.1 | 500.7 | 509.3 | 517.9 | 526.5 | 535.1 |
|  | 65 | 62.5 | 0.568 | 6.25 | 1.75 | 0.781 | 483.7 | 492.3 | 500.9 | 509.5 | 518.1 | 526.7 | 535.3 |
|  | 64 | 61.0 | 0.541 | 5.95 | 2.05 | 0.744 | 453.8 | 492.4 | 501.0 | 509.6 | 518.3 | 526.9 | 535.5 |
|  | 63 | 59.5 | 0.515 | 5.66 | 2.34 | 0.708 | 484.0 | 492.6 | 501.2 | 509.8 | 518.5 | 527.1 | 535.7 |
|  | 62 | 58.0 | 0.489 | 5.38 | 2.62 | 0.672 | 454.2 | 492.8 | 501.4 | 510.0 | 518.7 | 527.3 | 535.9 |
|  | 61 | 56.5 | 0.465 | 5.12 | 2.53 | 0.640 | 484.3 | 492.9 | 501.5 | 510.1 | 518.8 | 527.4 | 536.0 |
|  |  |  | 0.442 | 4.87 | 3.13 | 0.609 | 454.4 | 493.0 | 501.6 | 510.2 | 518.9 | 527.5 | 536.1 |
|  |  |  | 0.421 | 14.62 | 3.38 | 0.578 | 454.6 | 493.2 | 501.8 | 510.4 | 519.1 | 527.7 | 536.3 |
|  |  | 52.0 | 0.400 | 4.40 | 3.60 | 0.550 | 454.7 | 493.3 | 501.9 | 510.5 | 519.2 | 527.8 | 536.4 |
|  | 58 57 | 52.0 50.5 | 0.400 0.380 | ( 4.18 | 3.60 | 0.522 | 484.8 | 493.4 | 502.0 | 510.6 | 519.3 | 527.9 | 536.5 |
|  | 57 | 50.5 | 0.350 | 4.15 |  |  |  |  |  |  |  |  |  |
|  |  |  | 0.361 | 13.96 | 4.04 | 0.495 | 484.9 | 493.5 | 502.1 | 510.7 | 519.4 | 528.0 | ) 536.6 |
|  | 56 | 49.0 | 0.361 0.343 | 13.96  <br> 3 3.76 | 4.04 4.24 | 0.470 | 485.1 | 493.7 | 502.8 | 510.9 | 519.6 | 528.2 | 536.8 |
|  | 55 | 47.5 | 0.34 .3 | 3.76 |  |  |  | 493.5 | 502.4 | 511.0 | 519.7 | 528.3 | 536.9 |
|  | 54 | 46.0 | 0.326 | $6 \quad 3.57$ | 4.43 | 0.446 | 485.2 | 493.5 <br> 19.3 | 502.4 | 511.0 | 519.8 | 528.4 | 4537.0 |
|  | 53 | 44.5 | 0.309 | 9 3.40 | 4.60 | 0.425 | 485.3 | 493.9 | 502.5 | 511.1 | 519.8 | 528.4 | 5 537.1 |
|  | 52 | 43.0 | 0.292 | 23.23 | 4.77 | 0.404 | 485.4 | $449+0$ | 502.6 | - 511.2 | 519.9 | 528.5 | 5537.1 |
|  | 51 | 41.5 | 50.279 | 9 3.07 | 4.93 | 0.384 | 48.5 .5 | 5494.1 | 5027 | 7511.3 | 520.0 | - 228.6 | 6537.2 |
|  | 50 | 40.0 | 0.264 | 42.81 | 5.19 | 0.351 | 485.5 | 5494.1 | 502. 7 | 7 511.3 | 520.0 | 528.6 | 6 537.2 |
|  |  |  |  |  |  |  |  |  | $50 \cdot 8$ | 511.4 | + 520.1 | 1528.7 | 7 537. |
|  | 49 | 38.5 | 50.251 | 51 2.76 | 6.24 | 40.345 | 5485.6 | 6 494.2 | 502.8 | 8511.4 | 4520.1 | 528.7 | - 53.ロ |
|  | 45 | -37.0 | 0.238 | 882.63 | 5.37 | 70.329 | 485.7 | 7494.3 | -502.9 | ) 511.5 | 5520.2 | 258.8 | 8 537. |
|  | 47 | 735.5 | 50.226 | $26 \quad 2.50$ | 5.50 | 0.313 | 455.5 | S 494.4 | 4503.0 | ( 511.6 | 6520.3 | 3528.9 | 9537.5 |
|  | 46 | 6 34.0 | 0.214 | 142.37 | 75.63 | 30.296 | 6 485.8 | 8 494.4 | 4503.0 | 0511.6 | 6 520.3 | 3528.9 | 9537.5 |
|  | 45 | 534.0 <br> 32.5 | 50.203 | 032.24 | 45.76 | 60.280 | 0483.9 | 9494.5 | 5503.1 | 1511.7 | 7 520.4 | 4529.0 | 0537.6 |
|  |  |  | 0 0.192 | 922.12 | 2.5 .58 | 80.265 | $5 \quad 486.0$ | $0 \quad 494.6$ | 6503.2 | 2511.8 | 3520.5 | $5 \quad 529.1$ | 1537.7 |
|  |  | 31.0 | $5{ }^{5}$ | 822.01 | 15.94 | 1 0.251 | 1 186.1 | 1494.7 | \% 503.3 |  | 9 520.6 | 6 529.2 | 2 537. |
|  | 4 | \| 29.5 | 5 - 0.152 | - 2.01 | - 5.95 |  |  |  |  |  |  |  |  |




| Reading of Ther-mometer, Fathr. |  | $\begin{aligned} & \text { Temp. } \\ & \text { of } \\ & \text { oew- } \\ & \text { Pount, } \\ & \text { Fahr. } \end{aligned}$ | $\begin{gathered} \text { Force } \\ \text { of } \\ \text { Vapor } \\ \text { in } \\ \text { Enylish } \\ \text { Inches. } \end{gathered}$ | Weight of Vapor |  | $\begin{gathered} \text { Hu- } \\ \text { midity, } \\ \text { Satura- } \\ \text { tion }= \\ 1.0000 . \end{gathered}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ina |  | $\begin{aligned} & \text { Reqd. } \\ & \text { for } \end{aligned}$ | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | of acuof Air. |  | $\operatorname{ing}_{28.0}$ | $\operatorname{in.~}_{23.5}$ | $\begin{array}{c\|c\|} \hline 9.0 \\ \hline 9.0 \end{array}$ | $\operatorname{in}_{\mathbf{i n} .5}$ | $\operatorname{in}_{3 \oplus .0}$ | 30.5 | $3 \text { in. } 0$ |
|  | $\bigcirc$ |  |  | in. | gr |  | gr. |  |  |  |  |  | gr |  | gr. |
| 74 | 74 | 74.0 | 0.827 | 9.04 | 0.00 | 1.000 | 475.4 | 486.9 | 495.5 | 504.0 | 512.6 | 521.1 | 529.7 |
|  | 73 | 72.5 | 0.787 | 8.60 | 0.44 | 0.951 | 478.6 | 487.1 | 495.7 | 504.2 | 512.8 | 521.3 | 529.9 |
|  | 72 | 71.0 | 0.751 | 5.20 | 0.84 | 0.907 | 478.8 | 487.3 | 4959 | 504.4 | 513.0 | 521.5 | 530.1 |
|  | 71 | 69.5 | 0.715 | 7.81 | 1.23 | 0.864 | 479.0 | 487.5 | 496.1 | 504.6 | 513.2 | 521.7 | 530.3 |
|  | 70 | 68.0 | 0.681 | 7.44 | 1.60 | 0.823 | 479.2 | 487.7 | 496.3 | 504.8 | 513.4 | 521.9 | 530.5 |
|  | 69 | 66.5 | 0.618 | 7.05 | 1.96 | 0.783 | 479.4 | 487.9 | 496.5 | 505.0 | 513.6 | 522.1 | 530.7 |
|  | 68 | 65.0 | 0.617 | 6.75 | 2.29 | 0.747 | 479.6 | 488.1 | 4967 | 505.2 | 513.8 | 52.2 .3 | 530.9 |
|  | 67 | 63.5 | 0.588 | 6.41 | 2.63 | 0.709 | 479.8 | 488.3 | 496.9 | 505.4 | 514.0 | 522.5 | 531.1 |
|  | 66 | 62.0 | 0.559 | 6.10 | 2.94 | 0.675 | 480.0 | 188.5 | 497.1 | 505.6 | 514.2 | 522.7 | 531.3 |
|  | 65 | 60.5 | 0.532 | 5.81 | 3.23 | 0.643 | 480.1 | 488.7 | 497.3 | 505.9 | 514.4 | 522.9 | 531.5 |
|  | 64 | 59.0 | 0.506 | 5.52 | 3.52 | 0.611 | 480.3 | 455.9 | 497.5 | 506.1 | 314.6 | 523.2 | 531.8 |
|  | 63 | 57.5 | 0.481 | 5.24 | 3.50 | 0.550 | 480.5 | 489.1 | 497.7 | 506.3 | 514.8 | 523.4 | 532.0 |
|  | 62 | 56.0 | 0.458 | 4.99 | 4.05 | 0.552 | 450.6 | 489.2 | 497.8 | 506.4 | 514.9 | 523.5 | 532.1 |
|  | 61 | 54.5 | 0.435 | 4.75 | 4.29 | 0.525 | 480.7 | 489.3 | 497.9 | 506.5 | 515.0 | 523.6 | 532.2 |
|  | 60 | 53.0 | 0.414 | 4.52 | 4.52 | 0.500 | 480.9 | 489.5 | 498.1 | 506.7 | 515.2 | 523.5 | 532.4 |
|  | 59 | 51.5 | 0.393 | 4.29 | 4.75 | 0.475 | 481.0 | 489.6 | 498.2 | 506.8 | 515.3 | 523.9 | 532.5 |
|  | 58 | 50.0 | 0.373 | 4.08 | 4.96 | 0.451 | 481.1 | 489.7 | 498.3 | 506.9 | 515.4 | 524.0 | 532.6 |
|  | 57 | 18.5 | 0.355 | 3.86 | 5.18 | 0.427 | 481.2 | 189.8 | 498.4 | 507.0 | 515.5 | 524.1 | 532.7 |
|  | 56 | 47.0 | 0.337 | 3.66 | 5.38 | 0.405 | 181.3 | 189.9 | 498.5 | 507.1 | 515.6 | 524.2 | 532.5 |
|  | 55 | 45.5 | 0.320 | 3.48 | 5.56 | 0.385 | 481.4 | 490.0 | 498.6 | 507.2 | 515.7 | 524.3 | 532.9 |
|  | 54 | 44.0 | 0.304 | 3.32 | 5.72 | 0.367 | 481.5 | 490.1 | 498.7 | 507.3 | 515.8 | 524.4 | 533.0 |
|  | 53 | 42.5 | 0.288 | 3.15 | 5.59 | 0.348 | 481.6 | 490.2 | 498.6 | 507.4 | 515.9 | 524.5 | 533.1 |
|  | 52 | 11.0 | 0.274 | 2.99 | 6.05 | 0.331 | 481.7 | 490.3 | 498.9 | 507.5 | 516.0 | 524.6 | 533.2 |
|  | 51 | 39.5 | 0.260 | 2.83 | 6.21 | 0.313 | 481.5 | 490.4 | 499.0 | 507.6 | 516.1 | 524.7 | 533.3 |
|  | 50 | 38.0 | 0.246 | 2.69 | 6.35 | 0.298 | 481.9 | 490.5 | 499.1 | 507.7 | 516.2 | 524.8 | 533.4 |
|  | 49 | 36.5 | 0.234 | 2.55 | 6.49 | 0.282 | 481.9 | 490.5 | 499.1 | 507.7 | 516.2 | 524.8 | 533.4 |
|  | 48 | 3.5 .0 | 0.222 | 2.42 | 6.62 | 0.268 | 482.0 | 490.6 | 499.2 | 507.8 | 516.3 | 524.9 | 533.5 |
|  | 47 | 33.5 | 0.210 | 2.30 | 6.74 | 0.254 | 482.1 | 490.7 | 499.2 | 507.9 | 516.4 | 525.0 | 533.6 |
| 75 | 75 | 75.0 | 0.8 .54 | 9.31 | 0.00 | 1.000 | 477.4 | 485.9 | 494.4 | 502.9 | 511.5 | 520.0 | 528.5 |
|  | 74 | 73.5 | 0.514 | 8.87 | 0.44 | 0.9 .33 | 177.6 | 486.1 | 194.6 | 503.1 | 511.7 | 520.2 | 528.7 |
|  | 73 | 72.0 | 0.776 | 8.4 .5 | 0.56 | 0.908 | 477.8 | 446.3 | 49 -. 3 | 503.3 | 511.9 | 520.4 | 528.9 |
|  | 72 | 70.5 | 0.7:39 | 8.0 .5 | 1.26 | 0.865 | 178.0 | 486.5 | 495.0 | 503.5 | 512.] | 520.6 | 529.1 |
|  | 71 | 69.0 | 0.704 | 7.67 | 1.61 | 0.824 | 475.2 | 4 $\times 6.7$ | 19.5 .2 | 503.7 | 512.3 | 520.8 | 529.3 |
|  | 70 | 67.5 | 0.670 | 7.30 | 2.01 | 0.784 | 478.3 | 486.5 | 19.5 .3 | 503.8 | 512.5 | 521.0 | 529.5 |
|  | 69 | 66.0 | 0.638 | 6.95 | 2.36 | 0.746 | 478.5 | 4.7 .0 | 49.5 .5 | 504.0 | 512.7 | 521.2 | 529.7 |
|  | 68 | 64.5 | 0.607 | 6.62 | 2.69 | 0.711 | 478.7 | 157.2 | 19.5 .7 | 304.2 | 512.9 | 521.4 | 529.9 |
|  | 67 | 63.0 | 0.578 | 6.30 | 3.01 | 0.677 | 478.9 | 157.1 | 49.5 .9 | 504.4 | 513.1 | 521.6 | 530.1 |
|  | 66 | 61.5 | 0.5 .50 | 5.99 | 3.32 | 0.643 | 479.1 | 157.6 | 496.1 | 504.6 | 513.3 | 521.8 | 530.3 |
|  | 65 | 60.0 | 0.52.3 | 5.69 | 3.62 | 0.611 | 479.3 | 457.8 | 196.4 | 504.9 | 513.5 | 522.0 | 530.6 |
|  | 64 | 58.5 | 0.498 | 5.42 | 3.59 | 0.582 | 479.5 | 48 B .0 | 496.6 | 50.5.1 | 513.7 | -22.2 | 530.8 |
|  | 63 | 57.0 | 0.173 | 5.1.5 | 4.16 | 0.553 | 479.6 | 485.1 | 196.7 | 505.2 | 513.8 | 52:23 | 530.9 |
|  | 62 | 5.5.5 | 0.450 | 1.90 | 4.41 | 0.526 | 479.7 | 4, 1.2 | 496.5 | 50.5 .3 | 513.9 | 522.4 | 531.0 |


| Readin $r$ of Thermometer, Fahr. |  | Temp DewPoint, Fahr. | Force of <br> Vapor in <br> English <br> Inches. | $\frac{\begin{array}{c} \text { Wei } \\ \text { of Vi } \end{array}}{\text { In a }}$ | ght apur Reqd. for | $\begin{aligned} & \text { Hu- } \\ & \text { midity, } \\ & \text { Satura- } \\ & \text { tion }= \\ & 10 v 0 . \end{aligned}$ | Weight in Grains of a Cubic Poot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dry. | Wet |  |  | Air. | bic Ft. of Air. |  | in. | $\operatorname{in.}_{2}^{2} .5$ | $\operatorname{in.}_{29.0}$ | $29.5$ | $30.0$ | $30.5$ | ${ }_{\mathbf{i n} .}^{\text {in.0 }}$ |
| 76 | ${ }^{\circ}$ | 5. | in. <br> 0.450 | gr. 1.90 | gr. | 0.526 | gr. $79.7$ | $\begin{gathered} \mathrm{gr} . \\ 48 \times .2 \end{gathered}$ | $\begin{gathered} \text { gr. } \\ 496.5 \end{gathered}$ | gr. $505.3$ | gr. $513.9$ | gr. | gr. |
|  | 6 | 54.0 | 0.4 .98 | 4.66 | 4.6 .5 | 0.501 | . 9 | . 4 |  | 505.5 | 14.1 | . 6 | . 2 |
|  | 60 | 59.5 | 0.407 | 4.43 | 4.88 | 0.476 | 480.0 | 455.5 | 497.1 | 505.6 | 514.2 | 522.7 | $5: 31.3$ |
|  | 59 | 51.0 | 0.386 | 4.21 | 5.10 | 0.452 | 450.1 | 488.6 | 497.2 | 50.5 .7 | 514.3 | 522.s | $5: 31.4$ |
|  | 55 | 49.5 | 0.367 | 4.00 | 5.31 | 0.429 | 420.3 | 483.8 | 497.4 | 505.9 | 514.5 | 523.0 | 531.6 |
|  | 57 | 48.0 | 0.349 | 3.79 | 5.52 | 0.407 | 450.4 | 458.9 | 497.5 | 506.0 | 514.6 | 523.1 | 531.7 |
|  | 56 | 16.5 | 0.331 | 3.60 | 5.71 | 0.357 | 450.5 | 459.0 | $49 \% .6$ | 506.1 | 514.7 | 523.2 | 531.8 |
|  | 55 | 45.0 | 0.315 | 3.42 | 5.89 | 0.367 | 480.6 | 489.1 | 497.7 | 506.2 | 514.8 | 523.3 | 531.9 |
|  | 54 | 43.5 | 0.299 | 3.25 | 6.06 | 0.349 | 400.7 | 489.2 | 497.8 | 506.3 | 514.9 | 523.4 | 532.0 |
|  | 53 | 12.0 | 0.253 | 3.09 | 6.22 | 0.332 | 480.5 | 489.3 | 497.9 | 506.4 | 515.0 | 523.5 | 532.1 |
|  | 52 | 40.5 | 0.269 | 2.93 | 6.35 | 0.315 | 480.8 | 489.3 | 497.9 | 506.4 | 515.0 | 533.5 | 532.1 |
|  | 51 | 39.0 | 9.255 | 2.78 | 6.53 | 0.299 | 480.9 | 489.4 | 498.0 | 506.5 | 515.1 | 523.6 | 53.3 .2 |
|  | 50 | 37.5 | 0.242 | 2.64 | 6.67 | 0.284 | 481.0 | 489.5 | 498.1 | 506.6 | 515.2 | 523.7 | 532.3 |
|  | 49 | 36.0 | 0.230 | 2.51 | 6.80 | 0.270 | 4 S 1.1 | 459.6 | 498.2 | 506.7 | 515.3 | 523.8 | 532.4 |
|  | 48 | 34.5 | 0.218 | 2.39 | 6.92 | 0.257 | 451.2 | 489.7 | 498.3 | 506.5 | 515.4 | 523.9 | 532.5 |
|  | 76 | 76.0 | 0.882 | 9.60 | 0.00 | 1.000 | 476.3 | 484.8 | 493.3 | 501.8 | 510.3 | 519.8 | 507.3 |
|  | 75 | 74.5 | 0.840 | 9.14 | 0.46 | 0.952 | 476.6 | 485.1 | 493.6 | 502.1 | 510.6 | 519.1 | 527.6 |
|  | 74 | 73.0 | 0.801 | 8.71 | 0.89 | 0.907 | 476.5 | 485.3 | 493.8 | 502.3 | 510.8 | 519.3 | 527.8 |
|  | 73 | 71.5 | 0.763 | 8.30 | 1.30 | 0.865 | 477.0 | 48.5 .5 | 494.0 | 502.6 | 511.1 | 519.6 | 528.1 |
|  | 72 | 70.0 | 0.727 | 7.90 | 1.70 | 0.823 | 477.2 | 485.7 | 494.3 | 502.8 | 511.3 | 519.5 | 528.3 |
|  | 71 | 68.5 | 0.692 | 7.53 | 2.07 | 0.754 | 477.4 | 485.9 | 494.5 | 503.0 | 511.5 | 520.0 | 528.5 |
|  | 70 | 67.0 | 0.659 | 7.17 | 2.43 | 0.747 | 477.6 | 486.1 | 494.7 | 503.2 | 511.7 | 520.2 | 528.7 |
|  | 69 | 65.5 | 0.62 S | 6.53 | 2.77 | 0.711 | 477.8 | 486.3 | 494.9 | 503.4 | 511.9 | 520.4 | 528.9 |
|  | 65 | 64.0 | 0.597 | 6.49 | 3.11 | 0.676 | 477.9 | 486.4 | 49.5 .0 | 503.6 | 512.1 | 520.6 | 529.2 |
|  | 67 | 6.2 .5 | 0.56 s | 6.16 | 3.44 | 0.642 | 478.1 | 486.6 | 46.5 .2 | 503.8 | 512.3 | 520.8 | 529.4 |
|  | 66 | 61.0 | $0.5+1$ | 5.55 | 3.72 | 0.613 | 478.2 | 486.7 | 495.3 | 503.9 | 512.4 | 520.9 | 529.5 |
|  | 65 | 59.5 | 0.515 | 5.59 | 4.01 | 0.582 | 478.3 | 486.8 | 495.4 | 504.0 | 512.5 | 521.0 | 529.6 |
|  | 6 | 58.0 | 0.489 | 5.31 | 4.29 | 0.553 | 478.5 | 487.0 | 495.6 | 504.2 | 512.7 | 521.2 | 529.5 |
|  | 63 | 56.5 | 0.465 | 5.06 | 4.54 | $0.5 \cdot 7$ | 478.6 | 457.1 | 495.7 | 504.3 | 512.5 | 521.3 | 529.9 |
|  | 62 | 55.0 | 0.442 | 4.81 | 4.79 | 0.501 | 478.8 | 457.3 | 49.5 .9 | 504.5 | 513.0 | 521.5 | 530.1 |
|  | 61 | 53.5 | 0.421 | 4.57 | 5.03 | 0.476 | 479.0 | 437.5 | 496.1 | 504.7 | 513.2 | 521.7 | 530.3 |
|  | 60 | 52.0 | 0.400 | 4.34 | 5.26 | 0.452 | 479.1 | 457.6 | 496.2 | 504.8 | 513.3 | 521.8 | 530.4 |
|  | 59 | 50.5 | 0.380 | 4.13 | 5.47 | 0.430 | 499.2 | 487.7 | 496.3 | 504.9 | 513.4 | 521.9 | 530.5 |
|  | 58 | 49.0 | 0.361 | 3.92 | 5.65 | 0.405 | 499.3 | 487.8 | 496.4 | 50.5 .0 | 513.5 | 522.0 | 530.6 |
|  | 57 | 47.5 | 0.343 | 3.73 | 5.87 | 0.359 | 499.4 | 457.9 | 496.5 | 505.1 | 513.6 | 522.1 | 530.7 |
|  | 56 | 46.0 | 0.326 | 3.54 | 6.06 | 0.369 | 499.5 | 488.0 | 496.6 | 50.5 .2 | 513.7 | 522.2 | 530.8 |
|  | 55 | 44.5 | 0.309 | 3.36 | 6.24 | 0.351 | 499.6 | -158.1 | 496.7 | 50.5 .3 | 513.8 | 522.3 | 530.9 |
|  | 54 | 43.0 | 0.293 | 3.19 | 6.41 | 0.332 | 499.7 | 488.2 | 496.5 | 50.5 .4 | 513.9 | 52.2 .4 | 531.0 |
|  | 53 | 41.5 | 0.279 | 3.03 | 6.57 | 0.316 | 499.8 | 488.3 | 496.9 | 50.5 .5 | 514.0 | 522.5 | 531.1 |
|  | 52 | 40.0 | 0.264 | 2.89 | 6.72 | 0.301 | 499.9 | 488.4 | 497.0 | 50.5 .6 | 514.1 | 522.6 | 531.2 |
|  | 51 | 33.5 | 0.251 | 2.73 | 6.57 | 0.284 | 500.0 | 488.5 | 497.1 | 505.7 | 514.2 | 522.7 | 531.3 |
|  | 50 | 37.0 | 0.238 | 2.59 | 7.01 | 0.269 | 500.1 | 485.6 | 497.2 | 50.5 .5 | 514.3 | 522.8 | 531.4 |
|  | 49 | 3.5 .5 | 0.226 | 3.46 | 7.14 | 0.256 | 500.2 | 488.7 | 497.3 | 50.5 .9 | 514.4 | 522.9 | 531.5 |


| Reading of Thermometer, Fahr. |  | Temp. of DewPoint, Fahr. | Force of <br> Vapor in <br> English Inches. | Weight of Vapor |  | $\Pi и-$ midity, Saturation $=$ 1.000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a |  | Reqd. for Sat'n | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | bic Ft . of Air. |  | $\operatorname{in}_{28.0}$ | $28.5$ | $\operatorname{in}_{\mathbf{2 9 . 0}}$ | $\inf _{29.5}$ | $\begin{gathered} \operatorname{in.} \\ \mathbf{3 0 . 0} \end{gathered}$ | $\inf _{30.5}$ | ${ }_{3}^{\operatorname{in} .} 0$ |
| - | $\bigcirc$ |  | $\bigcirc$ | in. | gr. |  | gr. |  | gr. | gr. | gr. | gr. | gr. | gr. | gr . |
| 77 | 77 | 77.0 | 0.910 | 9.89 | 0.00 | 1.000 | 475.3 | 483.8 | 492.3 | 500.8 | 509.2 | 517.7 | 526.2 |
|  | 76 | 75.5 | 0.868 | 9.42 | 0.47 | 0.953 | 475.5 | +84.0 | 492.5 | 501.0 | 509.4 | 517.9 | 526.4 |
|  | 75 | 74.0 | 0.827 | 8.99 | 0.90 | 0.909 | 475.7 | 484.2 | 492.7 | 501.2 | 509.6 | 518.1 | 526.6 |
|  | 74 | 72.5 | 0.787 | 8.57 | 1.32 | 0.867 | 475.9 | 484.4 | 492.9 | 501.4 | 509.9 | 518.4 | 526.9 |
|  | 73 | 71.0 | 0.751 | 8.15 | 1.74 | 0.824 | 176.1 | 484.6 | 493.1 | 501.6 | 510.1 | 518.6 | 527.1 |
|  | 72 | 69.5 | 0.715 | 7.77 | 2.12 | 0.756 | 476.3 | 484.8 | 493.3 | 501.8 | 510.3 | 518.8 | 527.3 |
|  | 71 | 68.0 | 0.681 | 7.40 | 2.49 | 0.748 | 476.5 | 485.0 | 493.5 | 502.0 | 510.5 | 519.0 | 527.5 |
|  | 70 | 66.5 | 0.648 | 7.04 | 2.85 | 0.712 | 476.7 | 485.2 | 493.7 | 50.2 .2 | 510.7 | 519.2 | 527.7 |
|  | 69 | 65.0 | 0.617 | 6.71 | 3.18 | 0.678 | 476.9 | 485.4 | 493.9 | 502.4 | 510.9 | 519.4 | 527.9 |
|  | 68 | 63.5 | 0.598 | 6.37 | 3.52 | 0.641 | 477.0 | 485.6 | 494.1 | 502.6 | 511.1 | 519.6 | 528.1 |
|  | 67 | 62.0 | 0.5 .59 | 6.06 | 3.83 | 0.613 | 477.2 | 485.8 | 494.3 | 502.8 | 511.3 | 519.8 | 528.3 |
|  | 66 | 60.5 | 0.532 | 5.77 | 4.12 | 0.583 | 477.4 | 486.0 | 494.5 | 503.0 | 511.5 | 520.0 | 528.5 |
|  | 65 | 59.0 | 0.506 | 5.49 | 4.40 | 0.556 | 477.5 | 486.1 | 494.6 | 503.1 | 511.6 | 520.1 | 528.6 |
|  | 64 | 57.5 | 0.481 | 5.21 | 4.68 | 0.527 | 477.7 | 486.3 | 494.8 | 503.3 | 511.8 | 520.3 | 52S.8 |
|  | 63 | 56.0 | 0.45 S | 4.96 | 4.93 | 0.501 | 477.9 | 486.5 | 495.0 | 503.5 | 512.0 | 520.5 | 529.0 |
|  | 62 | 54.5 | 0.435 | 4.70 | 5.19 | 0.476 | 478.0 | 486.6 | 495.1 | 503.7 | 512.1 | 520.6 | 529.1 |
|  | 61 | 53.0 | 0.414 | 4.49 | 5.40 | 0.454 | 478.0 | 486.6 | 495.1 | 50:3.7 | 512.2 | 520.7 | 529.3 |
|  | 60 | 51.5 | 0.393 | 4.26 | 5.63 | 0.431 | 478.1 | 486.7 | 49.5 | 503.8 | 512.3 | 520.8 | 529.4 |
|  | 59 | 50.0 | 0.373 | 4.05 | 5.84 | 0.410 | 478.2 | 486.8 | 49.5 .3 | 503.9 | 512.4 | 520.9 | 529.5 |
|  | 58 | 48.5 | 0.355 | 3.85 | 6.0.4 | 0.389 | 478.3 | 486.9 | 495.4 | 504.0 | 512.5 | 521.0 | 529.6 |
|  | 57 | -17.0 | 0.337 | 3.65 | 6.24 | 0.369 | 478.5 | 487.1 | 495.6 | 504.1 | 512.7 | 521.2 | 529.8 |
|  | 56 | 45.5 | 0.320 | 3.47 | 6.42 | 0.351 | 478.6 | 487.2 | 495.7 | 504.2 | 512.8 | 521.3 | 529.9 |
|  | 55 | 44.0 | 0.304 | 3.29 | 6.60 | 0.333 | 478.7 | 487.3 | 495.8 | 50.1 .3 | 512.9 | 521.4 | 536.0 |
|  | 54 | 42.5 | 0.288 | 3.13 | 6.76 | 0.317 | 478.8 | 487.4 | 49.5 | 504.4 | 513.0 | 521.5 | 530.1 |
|  | 53 | 41.0 | 0.274 | 2.97 | 6.92 | 0.301 | 478.9 | 487.5 | 496.0 | 504.5 | 513.1 | 521.6 | 530.2 |
|  | 52 | 39.5 | 0.260 | 2.82 | 7.07 | 0.255 | 479.0 | 457.6 | 496.1 | 504.6 | 513.2 | 521.7 | 530.3 |
|  | 51 | 38.0 | 0.246 | 2.67 | 7.22 | 0.270 | 479.1 | 487.7 | 496.2 | 504.7 | 513.3 | 521.8 | 530.4 |
|  | 50 | 36.5 | 0.234 | 2.53 | 7.36 | 0.256 | 479.1 | 487.7 | 496.2 | 504.7 | 513.3 | 521.8 | 530.4 |
| 78 | 78 | 78.0 | 0.940 | 10.19 | 0.00 | 1.000 | 474.1 | 452.5 | 491.0 | 499.4 | 508.0 | 516.4 | 524.9 |
|  | 77 | 76.5 | 0.896 | 9.72 | 0.47 | 0.954 | 474.4 | 482.9 | 491.4 | 499.9 | 509.8 | 516.7 | 525.2 |
|  | 76 | 75.0 | 0.854 | 9.25 | 0.94 | 0.903 | 474.7 | 483.2 | 491.6 | 500.1 | 508.6 | 517.1 | 525.6 |
|  | 75 | 73.5 | 0.814 | 8.83 | 1.37 | 0.865 | 474.9 | 458.4 | 491.8 | 500.3 | 508.8 | 517.3 | 525.8 |
|  | 74 | 72.0 | 0.776 | 8.40 | 1.79 | 0.821 | 475.2 | 483.7 | 492.1 | 500.6 | 509.1 | 517.6 | 526.1 |
|  | 73 | 70.5 | 0.739 | 8.00 | 2.19 | 0.78 .5 | 475.4 | 483.9 | 492.3 | 500.8 | 500.3 | 517.8 | 526.3 |
|  | 72 | 69.0 | 0.704 | 7.62 | 2.57 | 0.748 | 475.6 | 484.1 | 492.5 | 501.0 | 509.5 | 518.0 | 526.5 |
|  | 71 | 67.5 | 0.670 | 7.25 | 2.94 | 0.711 | 475.5 | 484.3 | 492.7 | 501.2 | 509.7 | 518.2 | 526.7 |
|  | 70 | 66.0 | 0.638 | 6.91 | 3.28 | 0.678 | 475.9 | 484.4 | 492.9 | 501.4 | 509.9 | 518.4 | 526.9 |
|  | 69 | 64.5 | 0.607 | 6.58 | 3.61 | 0.616 | 476.1 | 484.6 | 493.1 | 501.6 | 510.1 | $51 . .6$ | 527.1 |
|  | 68 | 63.0 | 0.578 | 6.26 | 3.93 | 0.614 | 476.3 | 484.8 | 493.8 | 501.8 | 510.3 | 518.8 | 527.3 |
|  | 67 | 61.5 | 0.5 .50 | 5.96 | 4.23 | 0.585 | 476.4 | 484.9 | 493.4 | 501.9 | 510.4 | 518.9 | 527.4 |
|  | 66 | 60.0 | 0.523 | 5.66 | 4.53 | 0.55.5 | 476.6 | 485.1 | 493.6 | 502.1 | 510.6 | 519.1 | 527.6 |
|  | 6.5 | 58.5 | 0.498 | 5.35 | 4.51 | 0.528 | +76.8 | 485.3 | 493.5 | 502.3 | 510.5 | 519.8 | 527.8 |


| Reading of Thermometer, Fahr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dewr } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | Force of Vapor in English Inches. | Weight <br> of Vapor |  | $\begin{array}{\|c\|} \text { Hu- } \\ \text { nidity, } \\ \text { satnra- } \\ \text { tion } \\ 1000 . \\ 100 . \end{array}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { Reqd. } \\ & \text { for } \end{aligned}$ | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Foot of Air. | of act <br> of Air. |  | $\stackrel{\text { in. }}{28.0}$ | $\operatorname{in.}_{28.5}$ | $\operatorname{in}_{\mathbf{2 9 . 0}}$ | $\operatorname{in.}_{\substack{\text { in. } \\ \hline}}$ | $\operatorname{in.}_{\mathbf{3 0 . 0}}$ | $\begin{gathered} \text { in. } \\ \mathbf{3 0 . 5} \end{gathered}$ | $\mathbf{3}^{\text {in. }} \mathbf{0}$ |
| 78 | $\bigcirc$ |  | $\bigcirc$ | iv. | gr. |  | gr. |  | gr. | gr. | gr. | gr. | gr. | gr. | gr. |
|  | 65 | 58.5 | 0.498 | 5.38 | 4.81 | 0.528 | 476.8 | 485.3 | 493.8 | 502.3 | 510.8 | 519.3 | 527.8 |
|  | 64 | 57.0 | 0.473 | 5.12 | 5.07 | 0.502 | 476.8 | 485.3 | 493.9 | 502.4 | 510.9 | 519.4 | 527.9 |
|  | 63 | 55.5 | 0.450 | 4.88 | 5.31 | 0.479 | 476.9 | 485.4 | 494.0 | 50.5 | 511.0 | 519.5 | 528.0 |
|  | 62 | 54.0 | 0.428 | 4.63 | 5.56 | 0.454 | 477.1 | 485.6 | 494.2 | 50.2 .7 | 511.2 | 519.7 | 528.2 |
|  | 61 | 52.5 | 0.407 | 4.40 | 5.79 | 0.432 | 477.2 | 485.7 | 494.3 | 502.8 | 511.3 | 519.8 | 528.3 |
|  | 60 | 51.0 | 0.386 | 4.18 | 6.01 | 0.409 | 477.3 | 485.8 | 494.4 | 502.9 | 511.4 | 519.9 | 528.4 |
|  | 59 | 49.5 | 0.367 | 3.98 | 6.21 | 0.391 | 477.4 | 485.9 | 494.5 | 503.0 | 511.5 | 520.0 | 528.5 |
|  | 58 | 48.0 | 0.349 | 3.78 | 6.41 | 0.371 | 477.5 | 486.0 | 494.6 | 503.1 | 511.6 | 520.1 | 528.6 |
|  | 57 | 46.5 | 0.331 | 3.59 | 6.60 | 0.352 | 477.6 | 456.1 | 494.7 | 503.2 | 511.7 | 520.2 | 528.7 |
|  | 56 | 45.0 | 0.315 | 3.41 | 6.78 | 0.335 | 477.8 | 486.3 | 494.8 | 503.3 | 511.9 | 520.4 | 528.9 |
|  | 55 | 43.5 | 0.299 | 3.24 | 6.9 .5 | 0.315 | 477.9 | 486.4 | 494.9 | 503.4 | 512.0 | 520.5 | 529.0 |
|  | 54 | 42.0 | 0.253 | 3.07 | 7.12 | 0.301 | 478.0 | 486.5 | 495.0 | 503.5 | 512.1 | 520.6 | 529.1 |
|  | 53 | 40.5 | 0.269 | 2.92 | 7.27 | 0.257 | 478.1 | 486.5 | 495.0 | 503.5 | 512.1 | 520.6 | 529.1 |
|  | 52 | 39.0 | 0.255 | 2.77 | 7.42 | 0.272 | 478.2 | 486.6 | 495.1 | 503.6 | 512.2 | 520.7 | 529.2 |
|  | 51 | 37.5 | 0.242 | 2.63 | 7.56 | 0.258 | 478.3 | 486.7 | 495.2 | 503.7 | 512.3 | 520.8 | 529.3 |
| 79 | 79 | 79.0 | 0.970 | 10.50 | 0.00 | 1.000 | 473.1 | 481.5 | 490.0 | 493.4 | 506.9 | 515.3 | 523.8 |
|  | 78 | 77.5 | 0.925 | 10.01 | 0.49 | 0.953 | 473.4 | 481.8 | 490.3 | 495.7 | 507.2 | 515.6 | 524.1 |
|  | 77 | 76.0 | 0.582 | 9.54 | 0.96 | 0.909 | 473.7 | 482.1 | 490.6 | 499.0 | 507.5 | 515.9 | 524.4 |
|  | 76 | 74.5 | 0.840 | 9.10 | 1.40 | 0.867 | 473.8 | 482.2 | 490.7 | 499.2 | 507.7 | 516.2 | 524.7 |
|  | 75 | 73.0 | 0.801 | 8.66 | 1.54 | 0.525 | 474.0 | 482.4 | 490.9 | 499.4 | 507.9 | 516.4 | 524.9 |
|  | 74 | 71.5 | 0.763 | 8.25 | 2.25 | 0.786 | 474.3 | 482.7 | 491.2 | 499.7 | 508.2 | 516.7 | 525.2 |
|  | 73 | 70.0 | 0.727 | 7.86 | 2.64 | 0.749 | 474.5 | 482.9 | 491.4 | 499.9 | 508.4 | 516.9 | 525.4 |
|  | 72 | 68.5 | 0.692 | 7.48 | 3.02 | 0.712 | 471.7 | 483.1 | 491.6 | 500.1 | 508.6 | 517.1 | 52.5.6 |
|  | 71 | 67.0 | 0.659 | 7.12 | 3.38 | 0.678 | 474.9 | 453.4 | 491.9 | 500.1 | 508.8 | 517.3 | 525.8 |
|  | 70 | 65.5 | 0.628 | 6.79 | 3.71 | 0.647 | 475.1 | 453.6 | 462.1 | 500.6 | 509.0 | 517.5 | 526.0 |
|  | 69 | 64.0 | 0.597 | 6.45 | 4.05 | 0.614 | 475.3 | 483.8 | 492.3 | 500.8 | 509.2 | 517.7 | 526.2 |
|  | 68 | 62.5 | 0.565 | 6.14 | 4.36 | 0.555 | 475.4 | 483.9 | 492.4 | 500.9 | 509.3 | 517.8 | 526.3 |
|  | 67 | 61.0 | 0.541 | 5.84 | 4.66 | 0.556 | 475.6 | 484.1 | 492.6 | 501.1 | 509.5 | 518.0 | 526.5 |
|  | 66 | 59.5 | 0.515 | 5.55 | 4.95 | 0.529 | 475.7 | 484.2 | 492.7 | 501.2 | з09.6 | 518.1 | 526.6 |
|  | 65 | 58.0 | 0.489 | 5.28 | 5.22 | 0.503 | 475.8 | 484.3 | 492.8 | 501.3 | 509.8 | 518.3 | 526.8 |
|  | 64 | 56.5 | 0.465 | 5.02 | 5.48 | 0.478 | 476.0 | 484.5 | 493.0 | 501.5 | 510.0 | 518.5 | 527.0 |
|  | 63 | 55.0 | $0.44^{2}$ | 4.78 | 5.72 | 0.455 | 476.1 | 454.6 | 493.1 | 501.6 | 510.1 | 518.6 | 527.1 |
|  | 62 | 53.5 | 0.421 | 4.54 | 5.96 | 0.432 | 476.3 | 484.8 | 493.3 | 501.8 | 510.3 | 518.8 | 527.3 |
|  | 61 | 52.0 | 0.400 | 4.31 | 6.19 | 0.410 | 476.4 | 484.9 | 493.4 | 501.9 | 510.4 | 518.9 | 527.4 |
|  | 60 | 50.5 | 0.380 | 4.10 | 6.40 | 0.390 | 476.5 | 455.0 | 493.5 | 502.0 | 510.5 | 519.0 | 527.5 |
|  | 59 | 49.0 | 0.361 | 3.90 | 6.60 | 0.371 | 476.6 | 485.1 | 493.6 | 502.1 | 510.6 | 519.1 | 527.6 |
|  | 58 | 47.5 | 0.343 | 3.71 | 6.79 | 0.35:3 | 476.7 | 485.2 | 493.7 | 502.2 | 510.7 | 519.2 | 527.7 |
|  | 57 | 46.0 | 0.326 | 3.52 | 6.95 | 0.335 | 476.5 | 485.3 | 493.5 | 502.3 | 510.8 | 519.3 | 527.5 |
|  | 56 | 44.5 | 0.309 | 3.34 | 7.16 | 0.318 | 476.9 | 48.5 .4 | 493.9 | 502.4 | 510.9 | 519.4 | 527.9 |
|  | 55 | 43.0 | 0.293 | 3.17 | 7.33 | 0.301 | 477.0 | 485.5 | 494.0 | 502.5 | 511.0 | 519.5 | 528.0 |
|  | 54 | 41.5 | 0.279 | 3.01 | 7.49 | 0.257 | 177.1 | 48.6 | 494.1 | 502.6 | 511.1 | 519.6 | 528.1 |
|  | 53 | 40.0 | 0.264 | 2.86 | 7.64 | 0.272 | 477.2 | 455.7 | 494.2 | 502.7 | 511.2 | 519.7 | 528.2 |
|  | 52 | 35.5 | 0.2 .51 | 2.72 | 7.78 | 0.260 | 477.3 | 485.8 | 494.3 | 502.8 | 511.3 | 519.5 | 525.3 |


| Reading of Thermometer, Fithr. |  | Temp. of DewPoint, Fahr. | Force of <br> Vapor in <br> Enghish <br> Inches. | Weight of Vapor |  | IIn-Situration $\leftrightharpoons$ 1.000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a Cubic |  | Reqd. for Sat'n | Height of the Barometer in English Inches |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | bic Ft. of Air. |  | $18.8 .0$ | $\text { iv. } 28 . \frac{1}{8}$ | $\stackrel{\text { in. }}{24.0}$ | $\operatorname{in}_{199.5}$ | $\begin{array}{\|c\|c\|} \text { in. } \\ \mathbf{3 0 . 0} \end{array}$ | $\operatorname{in.}_{30.5}$ | $31.0$ |
|  | - |  | $\bigcirc$ | in. | gr |  | gr . |  | gr . | gr. | gr | gr. | gr | gr . | gr |
| S0 | 80 | 80.0 | 1.001 | 10.81 | 0.00 | 1.000 | 472.0 | 480.4 | 485.9 | 497.3 | 50.5 .7 | 5141 | 522.6 |
|  | 79 | 78.5 | 0.95 .5 | 10.31 | 0.50 | 0.954 | 472.3 | 480.7 | 489.1 | 497.5 | 506.0 | 514.4 | 522.9 |
|  | 78 | 77.0 | 0.910 | 9.53 | 0.98 | 0.909 | 472.5 | 480.9 | 4594 | 497.9 | 506.3 | 514.7 | 523.2 |
|  | 77 | 75.5 | 0.568 | 9.37 | 1.44 | 0.867 | 472.7 | 181.1 | 489.6 | $49 \mathrm{S}$. | 506.5 | 514.9 | 523.4 |
|  | 76 | 74.0 | 0.527 | 8.9:3 | 1.58 | $0 . .26$ | 173.0 | 481.4 | 489.9 | 498.4 | 506.8 | 515.2 | 523.7 |
|  | 75 | 72.5 | 0.787 | 8.50 | 2.31 | 0.786 | 473.2 | 481.6 | 490.1 | 498.6 | 507.0 | 515.4 | 523.9 |
|  | 74 | 71.0 | 0.751 | S. 11 | 2.70 | 0.750 | 473.4 | 451.8 | 4903 | 498.8 | 507.2 | 515.6 | 524.1 |
|  | 78 | 69.5 | $0.715^{\circ}$ | 7.71 | 3.10 | 0.713 | 473.6 | 482.1 | 490.6 | 499.1 | 507.5 | 515.9 | 524.4 |
|  | 72 | 65.0 | 0.681 | 7.35 | 3.46 | 0.680 | 473.8 | 48.2 .3 | 490.8 | 499.3 | 507.7 | 516.1 | 524.6 |
|  | 71 | 66.5 | 0.648 | 6.99 | 3.82 | 0.647 | 474.0 | 48.5 | 491.0 | 499.5 | 507.9 | 516.3 | 524.8 |
|  | 70 | 65.0 | 0.617 | 6.66 | 4.15 | 0.616 | 474.2 | 45.2 .7 | 491.2 | 499.7 | 50.1 | 516.5 | 525.0 |
|  | 69 | 63.5 | 0.558 | 6.33 | 4.48 | 0.586 | 474.4 | 482.9 | 491.4 | 499.9 | 505.3 | 516.7 | 525.2 |
|  | 65 | 62.0 | 0.559 | 6.03 | 4.78 | 0.558 | 474.5 | 483.0 | 491.5 | 500.0 | 508.4 | 516.8 | 525.3 |
|  | 67 | 60.5 | 0.532 | 5.74 | 5.07 | 0.531 | 474.7 | 483.2 | 491.7 | 500.2 | 509.6 | 517.0 | 525.5 |
|  | 66 | 59.0 | 0.506 | 5.45 | 5.36 | 0.501 | 474.9 | 483.4 | 491.9 | 500.4 | 508.8 | 517.2 | 525.7 |
|  | 65 | 57.5 | 0.451 | 5.18 | 5.63 | 0.179 | 475.0 | 483.5 | 492.0 | 500.5 | 508.9 | 517.3 | 525.8 |
|  | 64 | 56.0 | 0.458 | 4.93 | 5.96 | 0.456 | 475.2 | 483.7 | 492.2 | 500.7 | 509.1 | 517.5 | 526.0 |
|  | 6.3 | 54.5 | 0.43.5 | 4.69 | 6.12 | 0.484 | 175.3 | 483.5 | 492.3 | 500.8 | 509.2 | 517.6 | 526.1 |
|  | 62 | 53.0 | 0.414 | 4.46 | 6.35 | 0.413 | 475.4 | 483.9 | 492.4 | 500.9 | 509.3 | 517.7 | 526.2 |
|  | 61 | 51.5 | 0.393 | 4.23 | 6.58 | 0.391 | 475.5 | 484.0 | 492.5 | 501.0 | 509.4 | 517.8 | 526.3 |
|  | 60 | 50.0 | 0.373 | 4.02 | 6.79 | 0.372 | 475.6 | 484.1 | 492.6 | 501.1 | 509.5 | 517.9 | 526.4 |
|  | 59 | 48.5 | 0.355 | 3.82 | 6.99 | 0.353 | 475.7 | 484.2 | 492.7 | 501.2 | 509.6 | 518.0 | 526.5 |
|  | 58 | 47.0 | 0.337 | 3.63 | 7.18 | 0.336 | 17.5 .9 | 481.4 | 492.9 | 501.4 | 509.8 | 518.2 | 526.7 |
|  | 57 | 45.5 | 0.320 | 3.45 | 7.36 | 0.319 | 476.0 | 454.5 | 493.1 | 501.5 | 509.9 | 518.3 | 526.8 |
|  | 56 | 44.0 | 0.304 | 3.27 | 7.54 | 0.302 | 476.1 | 431.6 | 493.2 | 501.6 | 510.0 | 518.4 | 526.9 |
|  | 55 | 42.5 | 0.288 | 3.11 | 7.70 | 0.288 | 476.2 | 434.7 | 493.3 | 501.7 | 510.1 | 515.5 | 527.0 |
|  | 54 | 41.0 | 0.274 | 2.96 | 7.85 | 0.274 | 476.8 | 454.8 | 493.4 | 501.8 | 510.2 | 518.6 | 527.1 |
|  | 53 | 39.5 | 0.260 | 2.83 | 7.99 | 0.261 | 476.3 | 484.8 | 493.1 | 501.8 | 510.2 | 518.6 | 527.1 |
| 81 | 81 | 81.0 | 1.034 | 11.14 | 0.00 | 1.000 | -171.0 | 479.4 | 457.8 | 196.2 | 50.4 .6 | 513.0 | 521.1 |
|  | 80 | 79.5 | 0.986 | 10.62 | 0.52 | 0.9.5:3 | 471.3 | 479.7 | 485.1 | 496.5 | 501.9 | 513.3 | 521.7 |
|  | 79 | 78.0 | 0.910 | 10.13 | 1.01 | 0.910 | 471.5 | 479.9 | 485.1 | 496.8 | 50.5 .2 | . 513.6 | 522.1 |
|  | 78 | 76.5 | 0.596 | 9.6.2 | 1.49 | 0.566 | 471.7 | 450.1 | 488.6 | 497.0 | 50.5 .4 | 513.8 | 522.3 |
|  | 77 | 75.0 | 0.854 | 9.20 | 1.94 | 0.826 | 472.0 | 480.4 | 458.9 | 197.3 | 50.5. 7 | 314.1 | 522.6 |
|  | 76 | 73.5 | 0.814 | 8.77 | 2.37 | 0.787 | 472.2 | 480.6 | 189.1 | 497.5 | 50.5 .9 | 514.3 | 522.8 |
|  | 75 | 72.0 | 0.776 | 8.35 | 2.79 | 0.750 | 472.5 | 450.9 | -189. 1 | 497.8 | 506.2 | 514.6 | 523.1 |
|  | 74 | 70.5 | 0.739 | 7.9.5 | 3.19 | 0.713 | 472.6 | 481.0 | 189.5 | 497.9 | 506.1 | 514.8 | 523.3 |
|  | 73 | 69.0 | 0.701 | 7.57 | 3.57 | 0.680 | 472.8 | 451.2 | 189.7 | 49.1 | 506.6 | 515.0 | 523.5 |
|  | 72 | 67.5 | 0.670 | 7.21 | 3.93 | 0.647 | 173.0 | 481.4 | 189.!) | 498.3 | 506.8 | 515.2 | 523.7 |
|  | 71 | 66.0 | 0.638 | 6.87 | 4.27 | 0.617 | 473.2 | 451.6 | 490.1 | 498.5 | 507.0 | 515.4 | $5<0.9$ |
|  | 70 | 61.5 | 0.607 | 6.54 | 4.60 | 0.587 | 473.4 | 451.9 | 490.3 | $4!8.7$ | 507.2 | 515.6 | 5241 |
|  | 69 | 63.30 | 0.578 | 6.22 | 4.92 | 0.555 | 473.6 | 452.0 | 490.5 | 498.9 | 507.4 | 515.8 | 524.3 |
|  | 68 | 61.5 | 0.550 | 5.92 | 5.92 | 0.531 | 473.7 | 483.2 | 490.7 | 499.1 | 507.6 | 516.0 | 524.5 |


| Feading of Thermometer, Fahr. |  | Temp. of DewPoint, Fahr. | Force <br> Vapor in <br> English <br> Inches. | Weight. of Vapor |  | Humidity, Saturition $=$ 1.000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a for <br> Cubic Sat'n. Foot of of aCu- <br> Air. bic Ft. of Air . |  | Height of the Barometer in English Inches. |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Dry. | Wet. |  |  |  | in. |  | $\operatorname{in}_{28.5}$ | $\operatorname{in.}_{\mathbf{2 9} \mathbf{9} .0}$ | ${ }^{\text {in. }}$ | $\operatorname{ing}_{30.0}$ | $\operatorname{in.}_{\mathbf{3 0 . 5}}$ | $\sin _{\text {in. }}^{\text {Tin }}$ |
| $\begin{gathered} c \\ 81 \end{gathered}$ | 0 | $\bigcirc$ |  | in. | gr . |  | gr |  | gr. | gr. | gr. | g | gr . | gr. | gr . |
|  | 68 | 61.5 | 0.550 | 5.92 | 5.22 | 0.531 | 473.7 | 482.2 | 490.7 | 499.1 | 507.6 | 516.0 | 524.5 |
|  | 67 | 60.0 | 0.523 | 5.62 | 5.52 | 0.505 | 473.8 | 482.3 | 490.8 | 499.2 | 507.7 | 516.1 | 524.6 |
|  | 66 | 55.5 | 0.498 | 5.31 | 5.83 | 0.477 | 474.0 | 482.5 | 491.0 | 499.4 | 507.9 | 516.3 | 524.8 |
|  | 63 | 57.0 | 0.473 | 5.08 | 6.06 | 0.456 | 474.1 | 482.6 | 491.1 | 499.5 | 508.0 | 516.4 | 524.9 |
|  | 64 | 55.5 | 0.450 | 4.84 | 6.30 | 0.434 | 474.3 | 482.8 | 491.3 | 499.7 | 508.2 | 516.6 | 525.1 |
|  | 63 | 54.0 | 0.428 | 4.60 | 6.54 | 0.413 | 474.4 | 482.9 | 491.4 | 499.8 | 508.3 | 516.7 | 525.2 |
|  | 62 | 52.5 | 0.407 | 4.37 | 6.77 | 0.392 | 474.5 | 483.0 | 491.5 | 499.9 | 508.4 | 516.8 | 525.3 |
|  | 61 | 51.0 | 0.386 | 4.15 | 6.99 | 0.373 | 474.6 | 483.1 | 491.6 | 500.0 | 508.5 | 516.9 | 525.4 |
|  | 60 | 49.5 | 0.367 | 3.95 | 7.19 | 0.355 | 474.7 | 483.2 | 491.7 | 500.1 | 508.6 | 517.0 | 525.5 |
|  | 59 | 48.0 | 0.349 | 3.75 | 7.39 | 0.337 | 474.9 | 483.4 | 491.9 | 500.3 | 508.5 | 517.2 | 525.7 |
|  | 58 | 46.5 | 0.331 | 3.56 | 7.55 | 0.320 | 475.0 | 483.5 | 492.0 | 500.4 | 508.9 | 517.3 | 525.8 |
|  | 57 | 45.0 | 0.315 | 3.35 | 7.76 | 0.303 | 475.1 | 483.6 | 492.1 | 500.5 | 509.0 | 517.4 | 525.9 |
|  | 56 | 43.5 | 0.299 | 3.21 | 7.93 | 0.289 | 475.2 | 483.7 | 492.2 | 500.6 | 509.1 | 517.5 | 526.0 |
|  | 55 | 42 | 0.283 | 3.05 | 8.09 | 0.274 | 475.3 | 483.8 | 492.3 | 500.7 | 509.2 | 517.6 | 526.1 |
|  | 5 | . 10.5 | 0.269 | 2.90 | 8.24 | 0.260 | 475.3 | 483.8 | 492.3 | 500.7 | 509.2 | 517.6 | 526.1 |
| 82 | 82 | 82. | 1.067 | 11.47 | 0.00 | 1.00 | 470.0 | 478.4 | 486.8 | 495.2 | 503.5 | 511.9 | 520.3 |
|  | 81 | 80.5 | 1.017 | 10.91 | 0.53 | 0.954 | 470.3 | 478.7 | 457.0 | 49.5 .4 | 503.8 | 512.2 | 520.6 |
|  | 80 | 79.0 | 0.970 | 10.44 | 1.03 | 0.910 | 470.6 | 479.0 | 487.3 | 495.7 | 504.1 | 512.5 | 520.9 |
|  | 79 | 77.5 | 0.925 | 9.95 | 1.52 | 0.865 | 470.7 | 479.1 | 487.5 | 49.5 .9 | 504.3 | 512.7 | 521.1 |
|  | 78 | 76.0 | 0.882 | 9.49 | 1.98 | 0.827 | 471.0 | 479.4 | 487.8 | 496.2 | 504.6 | 513.0 | 521.4 |
|  | 77 | 74. | 0.840 | 9.03 | 2.44 | 0.757 | 471.2 | 179.6 | 488.0 | 496.4 | 504.8 | 513.2 | 521.6 |
|  | 76 | 73.0 | 0.801 | 8.60 | 2.37 | 0.750 | 471.5 | 479.9 | 488.3 | 496.7 | 505.1 | 513.5 | 521.9 |
|  | 75 | 71 | 0.763 | 8.19 | 3.25 | 0.714 | 471.6 | 480.0 | 488.5 | 496.9 | 505.3 | 513.7 | 522.1 |
|  | 74 | 70. | 0.727 | 7.81 | 3.66 | 0.68 | 471.8 | 480.2 | 458.6 | 497.1 | 505.5 | 513.9 | 522.4 |
|  | 73 | 68.5 | 0.692 | 7.43 | 4.04 | 0.645 | 472.0 | 480.4 | 488.8 | 497.3 | 505.7 | 514.1 | 522.6 |
|  | 72 | 67.0 | 0.6 .59 | 7.08 | 4.39 | 0.618 | 472.2 | 480.6 | 489.0 | 497.5 | 505.9 | 514.3 | 52.2 .8 |
|  | 71 | 65.5 | 0.628 | 6.75 | 1.72 | 0.588 | 472.4 | 480.8 | 489.2 | 497.7 | 506.1 | 514.5 | 523.0 |
|  | 70 | 64.0 | 0.597 | 6.41 | 5.06 | 0.559 | 472.5 | 480.8 | 489.4 | 497.9 | 506.3 | 514.7 | 523.2 |
|  | 69 | 62.5 | 0.568 | 6.10 | 5.37 | 0.532 | 472.6 | 481.0 | 489.5 | 498.0 | 506.4 | 514.8 | 523.3 |
|  | 68 | 61.0 | 0.541 | 5.81 | 5.66 | 0.507 | 472.8 | 481.2 | 489.7 | 498.2 | 506.6 | 515.0 | 523.5 |
|  | 67 | 59.5 | 0.515 | 5.52 | 5.95 | 0.481 | 473.0 | 481.4 | 489.9 | 498.4 | 506.8 | 515.2 | 523.7 |
|  | 66 | 58.0 | 0.489 | 5.25 | 6.22 | 0.458 | 473.1 | 481.5 | 490.0 | 498.3 | 506.9 | 515.3 | 523.8 |
|  | 65 | 56.5 | 0.465 | 4.99 | 6.15 | 0.435 | 473.2 | 481.6 | 490.1 | 498.6 | 507.0 | 515.4 | 523.9 |
|  | 64 | 55.0 | 0.442 | 4.75 | 6.72 | 0.414 | 473.4 | 481.8 | 4903 | 498.8 | 507.2 | 515.6 | 524.1 |
|  | 63 | 53.5 | 0.421 | 4.51 | 6.96 | 0.393 | 473.5 | 452.0 | 490.5 | 499.0 | 507.4 | 515.5 | 524.3 |
|  | 62 | 52.0 | 0.100 | 4.29 | 7.18 | 0.374 | 473.6 | 482.1 | 490.6 | 499.1 | 507.5 | 515.9 | 524.4 |
|  | 61 | 50.5 | 0.350 | 4.08 | 7.39 | 0.356 | 473.7 | 182.2 | 490.7 | 499.2 | 507.6 | 516.0 | 524.4 |
|  | 60 | 49.0 | 0.361 | 3.87 | 7.60 | 0.337 | 473.8 | 482.3 | 490.8 | 499.3 | 507.7 | 516.1 | $5 \leq 4.5$ |
|  | 59 | 47.5 | 0.313 | 3.68 | 7.79 | 0.320 | 473.9 | 482.4 | 490.9 | 499.4 | 507.9 | 516.2 | 524.6 |
|  | 55 | 46.0 | 0.326 | 3.50 | 7.97 | 0.305 | 474.0 | 482.5 | 491.0 | 499.5 | 507.9 | 516.3 | 524.7 |
|  | 57 | 44.5 | 0.309 | 3.32 | 8.15 | 0.289 | 474.1 | 482.6 | 491.1 | 499.6 | 50ヶ.0 | 516.4 | 524.8 |
|  | 56 | 43.0 | 0.293 | 3.15 | 8.32 | 0.274 | 474.2 | 482.7 | 491.2 | 499.7 | 508.1 | 516.5 | 524.9 |
|  | 55 | 41.5 | 0.279 | 2.99 | \% 8.48 | 0.260 | 474.3 | 482.8 | 491.3 | 499.8 | 508.2 | 516.6 | 525.1 |


| Reading of Thermometer, Fahr. |  | Temp. of DewPoint, Fabr. | Force of <br> Vapor in English Incues. | Weight of Vapor |  | IIumidity, Saturation $=$ 1.1000. | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Requd. <br> for | Height of the Barometer in Euglish Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air | bic Ft. of Aic. |  | $\left\lvert\, \begin{gathered} \text { in. } \\ 28.0 \end{gathered}\right.$ | $\frac{\mathrm{in} .}{28.5}$ | $\begin{gathered} \text { ins. } \\ \mathbf{2 4 . 0} \end{gathered}$ | $\operatorname{in}_{ \pm 8.5}$ | $\begin{gathered} \text { in. } \\ \mathbf{3 4 . 0} \end{gathered}$ | $\frac{\operatorname{in.}}{\mathbf{3} \mathbf{1} .5}$ | $\begin{array}{\|c} \text { in. } \\ \mathbf{3 1 . 0} \end{array}$ |
|  | $\bigcirc$ |  | $\bigcirc$ | in. | gr |  | gr . |  | gr. | gr. | gr | gr. | gr | gr. | gr. |
| 83 | 83 | 83.0 | 1.101 | 11.82 | 0.00 | 1.000 | 468.8 | 477.2 | 485.5 | 493.9 | 50.2 .3 | 510.6 | 519.0 |
|  | 82 | 81.5 | 1.050 | 11.27 | 0.55 | 0.953 | 469.1 | 477.5 | 485.8 | 49.4 .2 | 502.6 | 511.0 | 519.4 |
|  | SI | 80.0 | 1.001 | 10.75 | 1.07 | 0.909 | 469.4 | 477.8 | 4861 | 494.5 | 502.9 | 511.3 | 519.7 |
|  | 80 | 78.5 | 0.955 | 10.25 | 1.57 | 0.868 | 469.7 | 473.1 | 486.4 | 494.8 | 503.2 | 511.6 | 520.0 |
|  | 79 | 77.0 | 0.910 | 9.78 | 2.04 | 0.82 s | 470.0 | 478.4 | 486.7 | 49.\%. 1 | 503.5 | 511.9 | 520.3 |
|  | 78 | 75.5 | 0.568 | 9.31 | 2.51 | 0.786 | 470.3 | 478.7 | 487.0 | 495.1 | 503.8 | 512.2 | 520.6 |
|  | 77 | 74.0 | 0.827 | 8.85 | 2.94 | 0.751 | 470.5 | 478.9 | 487.2 | 495.6 | 504.0 | 512.4 | 520.8 |
|  | 76 | 72.5 | 0.757 | 8.45 | 3.37 | 0.715 | 470.6 | 479.0 | 487.4 | 49.5 .8 | 504.2 | 512.6 | 521.0 |
|  | 75 | 71.0 | 0.751 | 8.05 | 3.77 | 0.681 | 470.8 | 479.2 | 487.6 | 496.0 | 504.4 | 512.8 | 521.2 |
|  | 74 | 69.5 | 0.715 | 7.66 | 4.16 | 0.647 | 471.0 | 479.4 | 187.8 | 496.2 | 504.6 | 513.0 | 521.4 |
|  | 73 | 68.0 | 0.681 | 7.30 | 4.52 | 0.618 | 471.2 | 479.6 | 488.0 | 496.4 | 504.8 | 513.2 | 521.6 |
|  | 72 | 66.5 | 0.618 | 6.95 | 4.87 | 0.588 | 471.4 | 479.8 | 488.2 | 496.6 | 505.0 | 513.4 | 521.8 |
|  | 71 | 65.0 | 0.617 | 6.62 | 5.20 | 0.560 | 471.6 | 480.0 | 188.4 | 496.8 | 505.2 | 513.6 | 522.0 |
|  | 70 | 63.5 | 0.588 | 6.29 | 5.53 | 0.533 | 471.7 | 480.1 | 458.5 | 497.0 | 505.4 | 513.8 | 522.3 |
|  | 69 | 62.0 | 0.559 | 5.99 | 5.83 | 0.507 | 471.9 | 480.3 | 488.7 | 197.2 | 505.6 | 514.0 | 522.5 |
|  | 68 | 60.5 | 0.532 | 5.70 | 6.12 | 0.482 | 472.0 | 480.4 | 488.3 | 497.3 | 505.7 | 514.1 | 522.6 |
|  | 67 | 59.0 | 0.506 | 5.42 | 6.40 | 0.459 | 472.2 | 480.6 | 489.0 | 497.5 | 50.5 .9 | 514.3 | 522.8 |
|  | 66 | 57.5 | 0.451 | 5.15 | 6.67 | 0.435 | 472.4 | 480.5 | 159.2 | 497.7 | 506.1 | 514.5 | 523.0 |
|  | 65 | 56.0 | 0.458 | 4.90 | 6.92 | 0.114 | +72.4 | 480.8 | 459.3 | 497.8 | 506.2 | 514.6 | 523.1 |
|  | 64 | 54.5 | 0.135 | 4.66 | 7.18 | 0.394 | 472.5 | 480.9 | 489.4 | 497.9 | 506.3 | 514.7 | 523.2 |
|  | 63 | 53.0 | 0.414 | 4.43 | 7.39 | 0.375 | 472.7 | 481.1 | 489.6 | 498.1 | 506.5 | 514.9 | 523.4 |
|  | 62 | 51.5 | 0.393 | 4.21 | 7.61 | 0.356 | 472.8 | 481.2 | 489.7 | 498.2 | 506.6 | 515.0 | 523.5 |
|  | 61 | 50.0 | 0.373 | 1.00 | 7.82 | 0.339 | 472.9 | 4 S1.3 | 189.8 | 498.3 | 506.7 | 515.1 | 523.6 |
|  | 60 | 48.5 | 0.355 | 3.80 | 8.02 | 0.322 | 473.1 | 481.4 | 489.9 | 498.4 | 506.8 | 515.2 | 523.7 |
|  | 59 | 47.0 | 0.337 | 3.60 | 8.22 | 0.30 .5 | 473.2 | 481.5 | 490.0 | 498.5 | 506.9 | 51.5.3 | 523.8 |
|  | 58 | 4.5 .5 | 0.320 | 3.42 | 8.40 | 0.289 | 473.3 | 481.6 | 490.1 | 498.6 | 507.0 | 515.4 | 23.9 |
|  | 57 | 44.0 | 0.304 | 3.25 | 8.57 | 0.276 | 473.4 | 451.7 | 490.2 | 498.7 | 507.1 | 515.5 | 524.0 |
|  | 56 | 42.5 | 0.258 | 3.09 | 8.73 | 0.261 | 473.5 | 481.8 | 490.3 | 495.8 | 507.2 | 515.6 | 524.1 |
| 8.1 | 84 | 84.0 | 1.136 | 12.17 | 0.00 | 1.000 | 167.8 | 476.2 | 484.5 | 492.7 | 501.2 | 509.6 | 517.9 |
|  | 83 | 82.5 | 1.083 | 11.61 | 056 | 0.9 .54 | 468.1 | 476.4 | 481.8 | 493.2 | 501.5 | 509.8 | 518.2 |
|  | 82 | 81.0 | 1.034 | 11.07 | 1.10 | 0.910 | 468.4 | 476.7 | 48.5 .1 | 493.5 | 501.8 | 510.1 | 518.5 |
|  | 81 | 79.5 | 0.986 | 10.5 .5 | 1.62 | 0.867 | 469.6 | 476.9 | 15.5 .4 | 493.7 | 502.1 | 510.5 | 518.8 |
|  | 80 | 78.0 | 0.940 | 10.07 | 2.10 | 0.527 | 469.9 | 177.3 | 45.3 .7 | 49 4.0 | 502.1 | 510.8 | 519.1 |
|  | 79 | 76.5 | 0.896 | 9.59 | 2.58 | 0.788 | 169.1 | 477.5 | 485.9 | 494.2 | 502.6 | 511.0 | 519.3 |
|  | 78 | 75.0 | 0.854 | 9.14 | 3.03 | 0.751 | 469.4 | 477. $\times$ | 486.1 | 494.5 | 502.9 | 511.3 | 519.7 |
|  | 77 | 73.5 | 0.814 | 8.71 | 3.16 | 0.716 | 469.6 | 475.0 | $486: 3$ | 491.7 | 503.1 | 511.5 | 519.9 |
|  | 76 | 72.0 | 0.776 | 8.30 | 3.87 | 0.650 | 469.8 | 175.2 | 4865.5 | 494.9 | 503.83 | 511.7 | 520.1 |
|  | 75 | 70.5 | 0.739 | 7.90 | 4.27 | 0.619 | 470.1 | 478.5 | 466.8 | 46.5 .2 | 50:3.6 | 512.0 | 520.1 |
|  | 74 | 69.0 | 0.704 | 7.53 | 1.64 | 0.619 | 470.3 | +78.7 | 487.0 | 49.5 .4 | 503.8 | 512.2 | 520.6 |
|  | 73 | 67.5 | 0.670 | 7.17 | 5.00 | 0.589 | 470.5 | 478.9 | 487.2 | 49.5 .6 | 501.0 | 512.4 | 520.8 |
|  | 72 | 66.0 | 0.638 | 6.83 | 5.34 | 0.561 | 470.6 | 479.0 | 457.4 | 49.5 .8 | 504.2 | 512.6 | 521.0 |
|  | 71 | 64.5 | 0.607 | 6.50 | 5.67 | 0.531 | 470.7 | 479.1 | 487.) | 49.5 .9 | 504.3 | 512.7 | 521.1 |





| Reading of Thermometer, Fahr. |  | Temp. of DewPoint, Fabr. | Force of Vapor in <br> English Inches. | Weight of Vajor |  | Humidity, Saturation $=$ 1.000. | Weight in Grains of Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In a |  | $\begin{aligned} & \text { Reqd. } \\ & \text { for } \end{aligned}$ | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Air. | bic ft . of Air. |  | $\operatorname{in}_{8.0}^{8.0}$ | in. | $\operatorname{in}_{\mathbf{2} .}^{\mathbf{2} .0}$ | ${ }_{29.5}^{\text {in. }}$ | in. 30.0 | in. 30.5 | $3 \text { in. }$ |
| - 8 | - |  | $\begin{array}{r} \circ \\ \mathrm{S} 9 . \end{array}$ | $\begin{aligned} & \text { in. } \\ & 1.326 \end{aligned}$ | $\begin{gathered} g r \\ 14.08 \end{gathered}$ |  | $\mathrm{gr}$ | 1.000 |  | $\begin{gathered} \mathrm{gr} . \\ 470.6 \end{gathered}$ | $\begin{gathered} \mathrm{gr} \\ 478.9 \end{gathered}$ | gr. 107.1 |  | gr. $036$ | gr. <br> 11.9 |
|  | 88 | 87.5 | 1.266 | 13.14 | 0.64 | 0.954 | 46.3 .7 | 470.9 | 479.2 | 157.4 | 495.7 | 503.9 | 512.2 |
|  | 87 | 56.0 | 1.209 | 12.84 | 1.24 | 0.912 | 463.0 | 471.2 | 4795 | 187.8 | 496.1 | 504.4 | 512.7 |
|  | 86 | 84.5 | 1.153 | 12.24 | 1.54 | 0.869 | $46: 3.3$ | 471.5 | 479.8 | 188.1 | 496.4 | 504.7 | 513.0 |
|  | 85 | 83.0 | 1.101 | 11.68 | 2.40 | 0.830 | 163.6 | 471.8 | 450.1 | 458.4 | 496.7 | 505.0 | 513.3 |
|  | 84 | 81.5 | 1.050 | 1 I .18 | 2.95 | 0.791 | 464.0 | 472.2 | 450.5 | 485.8 | 497.1 | 505.4 | 513.7 |
|  | 83 | 80.0 | 1.001 | 10.62 | 3.46 | 0.754 | 464.2 | 472.5 | 480 s | 489.1 | 497.4 | 505.7 | 514.0 |
|  | 82 | 78.5 | 0.955 | 10.13 | 3.95 | 0.719 | 464.4 | 479.7 | 481.0 | 489.3 | 447.6 | 505.9 | 514.2 |
|  | S1 | 77.0 | 0.910 | 9.66 | 1.42 | 0.656 | 464.7 | 473.0 | 481.3 | 454.6 | 497.9 | 506.2 | 514.5 |
|  | 80 | 75.5 | 0.568 | 9.20 | 4.55 | 0.6.73 | 464.9 | 473.2 | 451.5 | 189.5 | 498.1 | 506.4 | 514.7 |
|  | 79 | 74.0 | 0.827 | $8.7 \%$ | 5.31 | 0.623 | 46.5 .2 | 473.5 | 451.8 | 490.1 | 498.4 | 506.7 | 515.0 |
|  | 78 | 72.5 | $0.75 \%$ | 8.35 | 5.73 | 0.593 | 46.5.4 | 473.7 | 482.0 | 490.3 | 495.6 | 506.9 | 515.2 |
|  | 77 | 71.0 | 0.751 | 7.96 | 6.12 | 0.565 | 46.5 .6 | 473.9 | 482.2 | 490.5 | 499.8 | 507.1 | 515.4 |
|  | 76 | 69.5 | 0.715 | 7.57 | 6.51 | 0.537 | 465.5 | 474.1 | 482.4 | 490.7 | 499.0 | 507.3 | 515.7 |
|  | 75 | 68. | 0.681 | 7.21 | 6.87 | 0.512 | 466.0 | 474.3 | 482.6 | 490.9 | 499.2 | 507.5 | 515.8 |
|  | 74 | 66.5 | 0.648 | 6.87 | 7.21 | 0.188 | 466.2 | 474.5 | 482.8 | 491.1 | 499.4 | 507.7 | 516.0 |
|  | 73 | 65.0 | 0.617 | 6.54 | 7.51 | 0.465 | 466.3 | 474.6 | 182.9 | 491.2 | 499.6 | 507.9 | 516.3 |
|  | 72 | 63.5 | 0.585 | 6.22 | 7.86 | 0.442 | 466.5 | 474.8 | 483.1 | 491.4 | 499.8 | 508.1 | 516.5 |
|  | 71 | 62.0 | 0.559 | 5.91 | 8.17 | 0.420 | 466.7 | 475.0 | 458.3 | 491.7 | 500.0 | 508.3 | 516.7 |
|  | 70 | 60.5 | 0.532 | 5.62 | 8.46 | 0.399 | 466.8 | 475.1 | 483.4 | 491.8 | 500.1 | 508.4 | 516.8 |
|  | 69 | 59.0 | 0.506 | 53.5 | 8.73 | 0.380 | 467.0 | 475.3 | 453.6 | 492.0 | 500.3 | 508.6 | 517.0 |
|  | 68 | 57.5 | 0.481 | 5.0 S | 9.00 | 0.361 | 467.1 | 475.4 | 483.7 | 492.1 | 500.4 | 508.7 | 517.1 |
|  | 67 | 56.0 | 0.458 | 4.84 | 9.24 | 0.343 | 467.2 | 475.5 | 453.5 | 492.2 | 500.5 | 508.8 | 517.2 |
|  | 66 | 54.5 | 0.435 | 4.61 | 9.47 | $0.3 \cdot 7$ | 467.4 | 475.7 | 483.9 | 492.4 | 500.7 | 509.1 | 517.4 |
|  | 65 | 53.0 | 0.414 | 4.39 | 9.69 | 0.312 | 467.5 | 475.5 | 484.1 | 492.5 | 500.8 | 509.2 | 517.5 |
|  | 64 | 51.5 | 0.393 | 4.17 | 9.91 | 0.296 | 467.6 | 175.9 | 484.2 | 492.6 | 500.9 | 509.8 | 517.6 |
|  | 63 | 50.0 | 0.373 | 3.96 | 10.12 | 0.281 | 467.7 | 476.1 | 454.3 | 49.2 .7 | 501.0 | 509.1 | 517.7 |
|  | 62 | 48.5 | 0.355 | 3.76 | $10.3 \pm$ | 0.267 | 467.8 | 476.2 | 454.4 | -192.8 | 501.1 | 509.5 | 517.8 |
| 90 | 90 | 90.0 | 1.368 | 14.50 | 0.00 | 1.000 | 461.3 | 469.5 | 477.8 | 486.0 | 494.3 | 502.5 | 510.8 |
|  | 89 | 88.5 | 1.306 | 13.84 | 0.66 | 0.9.54 | 461.6 | 469.8 | 478.1 | 486.3 | 494.6 | 502.8 | 511.1 |
|  | 88 | 87.0 | 1.247 | 13.22 | 1.23 | 0.910 | 462.0 | 470.2 | 478.5 | 486.7 | 49.5 .0 | 503.2 | 511.5 |
|  | 87 | 85.5 | 1.190 | 12.61 | 1.89 | 0.570 | 462.3 | 470.5 | 478.5 | 487.0 | 495.3 | 503.5 | 511.5 |
|  | 86 | S4.0 | 1.136 | 12.03 | 2.47 | 0.830 | 462.7 | 470.9 | 479.2 | 487.4 | 495.7 | 503.9 | 512.1 |
|  | 85 | S2.5 | 1.083 | 11.47 | 3.03 | 0.791 | 46:3.0 | 471.2 | 479.5 | 487.7 | 496.0 | 504.2 | 512.5 |
|  | 84 | 81.0 | 1.034 | 10.94 | 3.56 | 0.755 | 463.2 | 471.5 | 479.8 | 488.0 | 496.3 | 504.5 | 512.8 |
|  | 83 | 79.5 | 0.986 | 10.43 | 4.07 | 0.719 | 463.4 | 471.7 | 480.0 | 488.2 | 496.5 | 504.7 | 513.0 |
|  | 82 | 78.0 | 0.9 .40 | 9.95 | 4.55 | 0.686 | 463.7 | 472.0 | 480.3 | 488.5 | 196.8 | 505.0 | 513.3 |
|  | 81 | 76.5 | 0.896 | 9.48 | 5.02 | 0.653 | 464.0 | 472.3 | 480.6 | 488.8 | 497.1 | 505.3 | 513.6 |
|  | 80 | 75.0 | 0.854 | 9.03 | 5.47 | 0.622 | 464.2 | 472.5 | 480.7 | 488.9 | 497.3 | 505.5 | 513.9 |
|  | 79 | 73.5 | 0.814 | 8.61 | 5.89 | 0.594 | 464.3 | 472.6 | 450.9 | 489.1 | 497.5 | 505.7 | 514.1 |
|  | 78 | 72.0 | 0.776 | 8.20 | 6.30 | 0.565 | 464.5 | 472.8 | 451.1 | 489.3 | 497.7 | 505.9 | 514.3 |
|  | 77 | 70.5 | 0.739 | 7.50 | 6.70 | 0.538 | 464.7 | 473.0 | 481.3 | 489.5 | 497.9 | 506.1 | 514.5 |


| Reading of Thermometer, Fahr. |  | $\begin{aligned} & \text { Temp } \\ & \text { of } \\ & \text { Dew- } \\ & \text { Point, } \\ & \text { Fahr. } \end{aligned}$ | Force of <br> Vapor in Euglish Inches. | Weight of Viapor |  | $\begin{gathered} \text { IIu- } \\ \text { midity, } \\ \text { Saturis- } \\ \text { tion }= \\ 1000 . \end{gathered}$ | Weight in Grains of a Cubic Foot of Air. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Reqd. | Height of the Barometer in English Inches. |  |  |  |  |  |  |
| Dry. | Wet. |  |  | Foot of | bic Ft. of Air. |  | $2 \mathbf{i n .}$ | $\operatorname{in}_{28.5}$ | $\operatorname{in.}_{\mathbf{2 9} .0}$ | $\operatorname{inn}_{29.5}$ | in. | $\operatorname{in}_{\mathbf{3 0} .5}$ | $\operatorname{in}_{\mathbf{i n}}^{1.0}$ |
| 0 | 0 |  | 0 | in. | gr. |  | gr |  | gr. | gr. | gr. | gr. | gr . | gr. | gr. |
| 90 | 77 | 70.5 | 0.739 | 7.80 | 6.70 | 0.538 | 464.7 | 473.0 | 481.3 | 489.5 | 497.9 | 506.1 | 514.5 |
|  | 76 | 69.0 | 0.704 | 7.43 | 7.07 | 0.512 | 46.5 .0 | 473.3 | 451.6 | 489.8 | 498.2 | 506.4 | 514.8 |
|  | 7.5 | 67.5 | 0.670 | 7.08 | 7.42 | 0.458 | 46.5 .2 | 473.5 | 481.5 | 490.0 | 495.4 | 506.6 | 515.0 |
|  | 74 | 66.0 | 0.635 | 6.74 | 7.76 | 0.46. 5 | 46.5 .4 | 473.7 | 452.0 | 490.2 | 493.6 | 506.8 | 515.2 |
|  | 73 | 64.5 | 0.607 | 6.42 | 8.05 | 0.443 | 46.5.6 | 473.9 | 482.2 | 490.4 | 498.8 | 507.0 | 515.4 |
|  | 72 | 63.0 | 0.573 | 6.10 | 8.40 | 0.421 | 46.5 .7 | 474.0 | 450.3 | 490.5 | 493.9 | 507.1 | 515.5 |
|  | 71 | 61.5 | 0.550 | 5.81 | 8.69 | 0.400 | 465.9 | 474.2 | 482.5 | 490.7 | 499.1 | 507.3 | 515.7 |
|  | 70 | 60.0 | 0.523 | 5.52 | 5.98 | 0.381 | 466.1 | 474.4 | 482.8 | 491.0 | 499.3 | 507.5 | 515.9 |
|  | 69 | 58.5 | 0.498 | 5.25 | 9.3.) | 0.362 | 466.2 | 474.5 | +82.9 | 491.1 | 499.4 | 507.6 | 516.0 |
|  | 65 | 57.0 | 0.173 | 4.99 | 9.51 | 0.341 | 466.4 | 474.7 | 183.1 | 491.3 | 499.6 | 507.8 | 516.2 |
|  | 67 | 5.5.5 | 0.450 | 4.74 | 9.76 | 0.327 | 466.5 | 474.8 | 483.2 | 491.4 | 499.7 | 507.9 | 516.3 |
|  | 66 | 54.0 | 0.428 | 4.52 | 9.98 | 0.312 | 466.6 | 474.9 | 453.3 | 491.5 | 499.8 | 508.0 | 516.4 |
|  | 65 | 52.5 | 0.107 | 4.30 | 10.20 | 0.297 | 466.7 | 475.0 | 483.4 | 491.6 | 499.9 | $50 \mathrm{S.1}$ | 516.5 |
|  | 64 | 51.0 | 0.356 | 4.09 | 10.41 | 0.252 | 466.9 | 475.2 | 483.6 | 491.8 | 500.1 | 508.3 | 516.6 |
|  | 63 | 49.5 | 0.367 | 3.90 | 10.60 | 0.269 | 467.0 | 475.3 | 483.7 | 491.9 | 500.2 | 508.4 | 516.7 |

TABLE XIII.

FACTORS FOR COMPUTING THE FORCE OF VAPOR, FROM THE READINGS OF THE PSYCHROMETER, BY APJOHN'S FORMULA.

Dr. Apjohn's formala for deducing the fore of vapor, and the temperature of the dew-point, from the readings of the Psychrometer as given in the Proccedings of the Royal Irish Academy for 1840, is

$$
f^{\prime \prime}=f^{\prime}-\frac{d}{88} \times \frac{h}{30}
$$

when the readings of the wet-bulb thermometer are above $3 \mathfrak{2}^{\circ}$ Fahr., in which formula $f^{\prime \prime}=$ the force of vapor at the temperature of the dew-point in degrees of Fahr., $f^{\prime}=$ the foree of vapor at the temperature of evaporation given by the wet-bulb thermometer,
$d=$ the difference between the readings of the dry and wet thermometers,
$h^{\prime}=$ the beight of the barometer in Engush inches at the time of the observation.
When the readings of the wet-bulb thermometer are below $3 \mathfrak{Z}^{\circ}$ Fahr., and the bulb is covered with ice, the formula becomes

$$
f^{\prime \prime}=f^{\prime}-\frac{d}{96} \times \frac{h}{30^{*}}
$$

The factors in the following table, which is taken from the Greenwich Observations for 1813 , represent $\frac{d}{88} \times \frac{1}{30}$ and $\frac{d}{46} \times \frac{1}{30}$, computed for all differences between the wet and dry bulb thermometers, or values of $d$, from $0^{\circ}$ to $21^{\circ}$.

## Use of the Table.

To find out the force of vapor in the air, and the temperature of the dew-point, by means of these factors, let the factor corresponding to $d$, or the difference between the wet and dry thermometer in the first column, be multiplied moto the observed neight of the barometer, and subtract the result from the force of vapor, in Table XI., due to the temperature of evaporatian. indicated by the wet-bulb thermom+ter; the rest is the force of vapor in the air at the time of the observation; and the $e \mathrm{em}$ perature of the dew-point is that which is gue to it in Table XI.

## Example.

The observation gives,
Dry-bulb thermometer $=79^{\circ}$ Fahr., or the temperature of the air.
Wet-bulb " $=69^{\circ}$ " or temperature of evaporation.
Difference $\quad \mathbf{1 0}^{5}$
Height of barometer 29.7 English inches.
In the Table, $\mathfrak{D d}$ part, is found, - factor for a difference of $10^{\circ}=0.00379 \times 29.7$, o: height of barometer $=0.113$, which, subtracted from the force of vapor due to $69^{\circ}$, in Table NI., $=0.701-0.113$, gives force of vapor in the air $=0.591$ inches, and temperature of the dew-point $62^{\circ} .5$.

When the temperature of the wet bulb is below $3 \mathfrak{2}^{\circ}$ Fahrenheit, fine factors in the first part of the Table must be used.

177
XIII. FACTOR $\frac{a}{96} \times \frac{1}{30}$, FOR COMPUTING THE FORCE OF VAPOR BY APJOHN'S FOMMULA.

Below 320 Fahrenheit; the Wet Bulb covered with a Film of Ice.

| $\begin{gathered} \text { d, or } \\ \text { Difference } \\ \text { of Wet and } \\ \text { Dry Bulb } \\ \text { Therm. } \end{gathered}$ | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | 0.00000 | 0.00003 | 0.00007 | 0.00010 | $0.0001 \cdot$ | 0.00017 | 0.00020 | 0.0002 \& | 0.00027 | 0.00030 |
| 1 | . 00034 | . 00037 | . 00041 | . 00044 | . 00047 | . 00051 | . 00054 | .0005s | . 00061 | .00064 |
| 2 | . 00068 | . 00071 | . 00075 | . 00078 | . 00081 | . 00085 | . 00088 | . 00092 | . 00095 | . 00099 |
| 3 | . 00102 | . 00105 | . 00109 | . 00112 | . 00116 | . 00119 | . 00122 | . 00126 | . 00129 | . 00133 |
| 4 | . 00136 | . 00139 | . 00143 | . 00146 | . 00150 | . 00153 | . 00156 | . 00160 | . 00163 | . 00167 |
| 5 | . 00170 | . 00173 | .00177 | . 00180 | . 00184 | . 00187 | . 00190 | . 00194 | . 00198 | . 00201 |
| 6 | . 00204 | . 00207 | . 00211 | . 00214 | . 00218 | . 00221 | . 00224 | . 00228 | . 00231 | . 00235 |
| 7 | . 00238 | . 00241 | . 00245 | . 00248 | . 00252 | . 00255 | . 00255 | . 00262 | . 00265 | . 00269 |
| 8 | . 00272 | . 00275 | . 00279 | . 00282 | . 00285 | . 00289 | . 00292 | . 00296 | . 00299 | . 00302 |
| 9 | . 00306 | .00309 | . 00313 | . 00316 | . 00319 | . 00323 | . 00326 | . 00330 | . 00333 | . 00337 |
| 10 | . 00340 | . 00343 | .00347 | . 00350 | . 00354 | . 00357 | . 00360 | . 00364 | . 00367 | . 00370 |


| Reading of Wet-Bulb Thermometer above 320 Fahrenheit. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $d$, orDifferenceof Wet andDry BulbTherm. | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | 0.00000 | 0.00004 | 0.00008 | 0.00011 | 0.00015 | 0.00019 | 0.00023 | 0.00027 | 0.00030 | 0.00034 |
| 1 | . 00038 | . 00042 | . 00046 | . 00019 | .000.53 | . 00057 | . 00061 | . 00064 | . 00068 | .00072 |
| 2 | . 00076 | . 00080 | . 00083 | . 00087 | . 00091 | . 00095 | . 00098 | . 00102 | . 00106 | . 00110 |
| 3 | . 00114 | . 00118 | . 00121 | . 00125 | . 00129 | . 00132 | . 00137 | . 00140 | . 00144 | . 00148 |
| 4 | . 00151 | . 00135 | . 00159 | . 00163 | . 00167 | . 00171 | . 00174 | . 00178 | . 00182 | . 00186 |
| 5 | . 00189 | . 00193 | . 00197 | . 00201 | . 00205 | . 00209 | . 00212 | . 00216 | . 00220 | . 00224 |
| 6 | . 00228 | . 00231 | . 00235 | . 00239 | . 00242 | . 00246 | . 00250 | . 00254 | . 00258 | . 00261 |
| 7 | . 00265 | . 00269 | . 00273 | . 00277 | . 00280 | . 00284 | . 00288 | . 00292 | . 00295 | .00299 |
| 8 | . 00303 | . 00307 | . 00311 | .00315 | . 00318 | . 00322 | . 00326 | . 00330 | . 00333 | . 00337 |
| 9 | . 00341 | . 003.45 | . 00349 | . 00352 | . 00356 | . 00360 | . 00364 | . 00368 | . 00371 | . 00375 |
| 10 | . 00379 | . 00383 | . 00386 | . 00390 | . 00394 | . 00398 | . 00401 | . 00405 | . 00409 | . 00412 |
| 11 | . 00416 | . 00420 | . 00424 | . 00428 | . 00432 | . 00436 | . 00439 | . 00443 | . 00447 | . 00451 |
| 12 | . 00454 | . 00458 | . 00462 | . 00466 | . 00470 | . 00474 | . 00477 | . 00481 | . 00485 | .00459 |
| 13 | .00493 | . 00496 | . 00500 | .00504 | . 00508 | . 00511 | . 00515 | . 00519 | . 00522 | . 00526 |
| 14 | . 00530 | . 00534 | . 00538 | . 00541 | . 00545 | . 00549 | . 00553 | .00556 | . 00560 | . 00564 |
| 15 | . 00568 | . 00572 | . 00576 | . 00580 | . 00584 | . 00587 | . 00591 | . 00.595 | . 00598 | . 00602 |
| 16 | . 00606 | . 00610 | . 00614 | . 00618 | .00622 | . 00625 | . 00629 | . 00633 | .00636 | . 00640 |
| 17 | . 00644 | . 00648 | . 00652 | . 00655 | . 00659 | . 00663 | . 00666 | . 00670 | . 00674 | . 00678 |
| 18 | . 00632 | . 00686 | . 00690 | . 00693 | . 00697 | . 00701 | . 00704 | .00708 | . 00712 | . 00716 |
| 19 | . 00720 | .00724 | . 00728 | . 00731 | .00735 | . 00739 | . 00742 | . 00746 | .00750 | .00754 |
| 20 | . 00758 | . 00761 | . 00765 | . 00769 | .00773 | . 00777 | . 00780 | . 00784 | . 00788 | .00792 |

In the Greenwich Magnetic and Meteorological Observations for 1842 and 1843, Mr. Glaisher discussed the relation between the temperature of evaporation given by the Wet-bulb Thermometer and the temperature of the Dew-Point as given by Daniell's Hygrometer. Comparing the observations taken simultaneously every six hours with the Psychrometer, and with Daniell's Dew-Point Hygrometer, and dividing the average difference between the temperatures of the Wet and Dry bulb by the average difference of the temperature of the Dew-Point and of the Air, he obtained the empirical factors given in the following Table.

The observations from which they are deduced are those taken at the Observatory in the years 1841 to $\mathbf{1 8 4 5}$, for the temperatures below $35^{\circ} \mathrm{F}$., and in the years 1841 to 1843 , for the temperatures above $35^{\circ} \mathrm{F}$.

The observations made at Toronto Observatory, Canada West, in similar circumstances, in the years 1840 to 1842 , were also compared in the same manner, and the factors derived from them showed a very close accordance for temperatures above $30^{\circ} \mathrm{F}$., but were found smatler at temperatures below $30^{\circ} \mathrm{F}$.

The errors in the temperature of the Dew-Point, which may result by using the Greenwich factors, though frequently within half a degree, often amount, however, to $\pm 2$ or 3 degrees, and, in extreme cases, to $\pm 4$ or 5 degrees, as shown in the volume of the Greenwich Observations for 1842, p. 60 of the Abstracts.

## Use of the Table.

Multiply the difference between the Wet-bulb and Dry-bulb Thermometers by the factor standing in the Table opposite the reading of the Dry-bulb, and subtract the product from the reading of the Dry-bulb; the remainder will be the temperature of the Dew-Point.

Example. - Dry-bulb $=62^{\circ} \mathrm{F} . ;$ Wet-bulb $=55^{\circ} ;$ Difference $=7^{\circ}$.
Opposite $6 \mathfrak{Z}^{\circ}$, in the first column, stands the factor 1.7 , which multiplied by $7^{\circ}$, the difference, gives $11^{\circ} .9$, to be subtracted from the Dry-bulb; or $62^{\circ}-11^{\circ} .9=50^{\circ} .1$, temperature of the Dew-Point.
XIV. FACTORS TO FFND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE READINGS OF THE PSYCHROMETER. - GLAISHER.

| Dry-Bulb Therm. Fahreu. | Factors. | Dry-Bulb 'Therm. Fihren. | Factors. | Dry-Bulb Therm. Fahren. | Factors. | Dry-Bulb 'therm. Fahren. | Factors. | Dry-Bulb Therm. Fabren. | Factors. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $21^{\circ}$ | 8.5 | $35^{\circ}$ | 2.6 | $49^{\circ}$ | 2.2 | $63^{\circ}$ | 1.7 | $77^{\circ}$ | 1.5 |
| 22 | 8.5 | 36 | 2.6 | 50 | 2.1 | 64 | 1.7 | 78 | 1.5 |
| 23 | 8.5 | 37 | 2.5 | 51 | 2.1 | 65 | 1.7 | 79 | 1.5 |
| 24 | 7.3 | 38 | 2.5 | 52 | 2.0 | 66 | 1.6 | 80 | 1.5 |
| 25 | 6.4 | 39 | 2.5 | 53 | 2.0 | 67 | 1.6 | 81 | 1.5 |
| 26 | 6.1 | 40 | 2.4 | 54 | 2.0 | 68 | 1.6 | 82 | 1.5 |
| 27 | 5.9 | 41 | 2.4 | 55 | 2.0 | 69 | 1.5 | 83 | 1.5 |
| 28 | 5.7 | 42 | 2.4 | 56 | 1.9 | 70 | 1.5 | 84 | 1.5 |
| 29 | 5.0 | 43 | 2.4 | 57 | 1.9 | 71 | 1.5 | 85 | 1.5 |
| 30 | 4.6 | 44 | 2.3 | 58 | 1.9 | 72 | 1.5 | 86 | 1.5 |
| 31 | 3.6 | 45 | 2.3 | 59 | 1.8 | 73 | 1.5 | 87 | 1.5 |
| 32 | 3.1 | 46 | 2.3 | 60 | 1.8 | 74 | 1.5 | 88 | 1.5 |
| 33 | 2.8 | 47 | 2.2 | 61 | 1.8 | 75 | 1.5 | 89 | 1.5 |
| 34 | 2.6 | 48 | 2.2 | 62 | 1.7 | 76 | 1.5 | 90 | 1.5 |

XV. WEIGHT OF VAPOR, IN GRAINS Troy, CONTAINED IN A CUBIC FOOT OF SATURATED AIR, AT TEMPERATURES BETWEEN $0^{\circ}$ AND $94^{\circ}$ FAHRENiLEIT.

From the Greenwich Observations.

| Temper ature <br> Fahren. |  | Temperature of Air, <br> Fahres |  | Temperof Air, Fahren. | Weight of Vapor, <br> Grains. | Temperature <br> Fahren | $\begin{aligned} & \text { Weight } \\ & \text { of Yipor, } \end{aligned}$ $\stackrel{\text { m }}{\text { Grains. }}$ | Temperof Air <br> Fahren. | Weight of Viaror, Grains. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 0.78 | $19^{\circ}$ | 1.52 | $38^{\circ}$ | 2.59 | $57^{\circ}$ | 5.34 | $76^{\circ}$ | 9.60 |
| 1 | 0.81 | 20 | 1.58 | 39 | 2.99 | 58 | 5.51 | 77 | 9.89 |
| 2 | 0.84 | 21 | 1.63 | 40 | 3.09 | 59 | 5.69 | 78 | 10.19 |
| 3 | 0.57 | 22 | 1.69 | 41 | 3.19 | 60 | 5.57 | 79 | 10.50 |
| 4 | 0.90 | 23 | 1.75 | 42 | 3.30 | 61 | 6.06 | 80 | 10.81 |
| 5 | 0.93 | 24 | 1.81 | 43 | 3.41 | 62 | 6.25 | 81 | 11.14 |
| 6 | 0.97 | 25 | 1.87 | 44 | 3.52 | 63 | 6.45 | 82 | 11.47 |
| 7 | 1.00 | 26 | 1.93 | 45 | 3.64 | 64 | 6.65 | 83 | 11.52 |
| 8 | 1.04 | 27 | 2.00 | 46 | 3.76 | 65 | 6.87 | 84 | 12.17 |
| 9 | 1.07 | 28 | 2.07 | 47 | 3.58 | 66 | 7.08 | 85 | 12.53 |
| 10 | 1.11 | 29 | 2.14 | 48 | 4.01 | 67 | 7.30 | 86 | 12.91 |
| 11 | 1.15 | 30 | 2.21 | 49 | 4.14 | 68 | 7.53 | 87 | 13.29 |
| 12 | 1.19 | 31 | 2.29 | 50 | 4.28 | 69 | 7.76 | 88 | 13.68 |
| 13 | 1.24 | 32 | 2.37 | 51 | 4.42 | 70 | 8.00 | 89 | 14.08 |
| 14 | 1.23 | 33 | 2.45 | 52 | 4.56 | 71 | 8.25 | 90 | 14.50 |
| 15 | 1.32 | 34 | 2.53 | 53 | 4.71 | 72 | 8.50 | 91 | 14.91 |
| 16 | 1.37 | 35 | 2.62 | 54 | 4.86 | 73 | 8.76 | 92 | 15.33 |
| 17 | 1.41 | 36 | 2.71 | 55 | 5.02 | 74 | 9.04 | 93 | 15.76 |
| 18 | 1.47 | 37 | 2.80 | 56 | 518 | 75 | 9.81 | 94 | 16.22 |

XVI. FACTORS TO DEDUCE THE WEIGHT OF VAPOR CONTAINED IN A CUBIC FOOT OF AIR, AT THE TIME OF A GIVEN OBSERVATION, FROM THE indications of dew-point instruments. - Greenw. Obs.
$t=$ Temperature of Air; $\mathbf{t}^{\prime}=$ Temperature of Dew-Point.

| $\begin{aligned} & \text { Difference } \\ & \text { or } \\ & \mathbf{t}-\mathbf{t}^{\prime} . \end{aligned}$ | Factors. | $\begin{gathered} \text { Difference } \\ \text { or } \\ \mathbf{t}-\mathbf{t}^{\prime \prime} . \end{gathered}$ | Faetors | $\begin{gathered} \text { Difference } \\ \text { or } \\ \mathbf{t}-\mathbf{t}^{\prime \prime} . \end{gathered}$ | Factors. | $\left\lvert\, \begin{gathered} \text { Difference } \\ \text { or } \\ \mathbf{t}-\mathbf{t}^{\prime \prime} . \end{gathered}\right.$ | Factors. | $\begin{gathered} \text { Difference } \\ \text { or } \\ \mathbf{t}-\mathbf{t}^{\prime \prime} . \end{gathered}$ | Factors. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.999 | 9 | 0.982 | 17 | 0.966 | 2.5 | 0.9 .51 | 33 | 0.935 |
| 2 | 0.996 | 10 | 0.980 | 18 | 0.964 | 26 | 0.949 | 34 | 0.934 |
| 3 | 0.994 | 11 | 0.978 | 19 | 0.962 | 27 | 0.9 .47 | 35 | 0.932 |
| 4 | 0.992 | 12 | 0.976 | 20 | 0.960 | 28 | 0.945 | 36 | 0.930 |
| 5 | 0.990 | 13 | 0.974 | 21 | 0.9 .58 | 29 | 0.943 | 37 | 0.929 |
| 6 | 0.988 | 14 | 0.972 | 22 | 0.956 | 30 | 0.912 | 38 | 0.927 |
| 7 | 0.986 | 15 | 0.970 | 23 | 0.954 | 31 | 0.939 | 39 | 0.925 |
| 8 | 0.984 | 16 | 0.968 | 24 | 0.952 | 32 | 0.937 | 40 | 0.923 |

Use of Table XVI. - The difference between the temperatures of the air and of the Dew-Point being known, multiply the factor in the Table corresponding to that difference into the weight of a cubic foot of vapor at the temperature of the Dew-Point, as given in Table XV., and the product will be the weight of vapor in a cubic foot of air at the time of the observation.

Example. - Temperature of air $=60^{\circ} \mathrm{F} . ;$ Dew-Point $=52^{\circ}$; Diff. $=8^{\circ}$.
Table gives for a difference of $8^{\circ}$, factor 0.984 ; Table XV. gives weight of a cubic foot of vapor at temperature $5 \mathfrak{P}^{\circ}=4 . .^{\mathrm{gr}} 56$.

Hence, $0.984 \times 4.56=4^{\mathrm{gr} .} .49$, the weight of vapor required.

## TAミIE オT：














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## Enamit：








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Mr. Glaisher published in London, in 1856, another series of Hygrometrical Tables, which were unknown to the writer when the Second Edition of this volume was issued. They are based on Regnault's Table of Elastic Forces of Vapor, and on the coefficient of the expansion of the air as determined by the same physicist. The Psychrometrical 'Table, however, is not computed from Regnault's formula, but by first finding out, in the manner described on page 140, the temperatures of the dewpoint from the readings of the Psychrometer, by means of the empirical factors given below, in Table XIV'., and then taking the corresponding values of the force of vapor from Regnault's table. These factors have been derived from the combination of all simultaneons observations of the dry and wet bulb thermometers with those of Daniell's hygrometer, taken at the Royal Observatory, Greenwich, from the year 1841 to 1854, with some observations taken at high temperatures in India, and others at low and medium temperatures at Toronto; they are, therefore, more correct than those given in Table XIV. page 140. The results in this new Psychrometrical Table, nevertheless, by no means entirely coincide with those given by the formula, as a comparison with those in Table VII. will show.

XIV'. FACTORS TO FIND OUT THE TEMPERATURE OF THE DEW-POINT FROM THE readings of the psychroneter. - Glaisher.

| Dry-Bulb Therm. <br> Fahren. | Factors. | Dry-Bulb Therm. Fihren. | Factors. | Dry-Bulb Therm. Fahren. | Factors. | Dry-Bulb Therm. Fahren. | Factors. | Dry-Bulb Therm. Fahren. | Factors. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \circ \\ 10 \end{gathered}$ | 8.78 | $\begin{gathered} \circ \\ 28 \end{gathered}$ | 5.12 | $\begin{gathered} \circ \\ 46 \end{gathered}$ | 2.14 | $64$ | 1.83 | $\stackrel{\circ}{82}$ | 1.67 |
| 11 | 8.78 | 29 | 4.63 | 47 | 2.12 | 65 | 1.82 | 83 | 1.67 |
| 12 | 8.78 | 30 | 4.15 | 48 | 2.10 | 66 | 1.81 | 84 | 1.66 |
| 13 | 8.77 | 31 | 3.70 | 49 | 2.08 | 67 | 1.80 | 85 | 1.65 |
| 14 | 8.76 | 32 | 3.32 | 50 | 2.06 | 68 | 1.79 | 86 | 1.65 |
| 15 | 8.75 | 33 | 3.01 | 51 | 2.04 | 69 | 1.78 | 87 | 1.64 |
| 16 | 8.70 | 34 | 2.77 | 52 | 2.02 | 70 | 1.77 | 88 | 1.64 |
| 17 | 8.62 | 3.5 | 2.60 | 53 | 2.00 | 71 | 1.76 | 89 | 1.63 |
| 18 | 8.50 | 36 | 2.50 | 54 | 1.98 | 72 | 1.75 | 90 | 1.63 |
| 19 | 8.34 | 37 | 2.42 | 55 | 1.96 | 73 | 1.74 | 91 | 1.62 |
| 20 | 8.14 | 38 | 2.36 | 56 | 1.94 | 74 | 1.73 | 92 | 1.62 |
| 21 | 7.88 | 39 | 2.32 | 57 | 1.92 | 75 | 1.72 | 93 | 1.61 |
| 22 | 7.60 | 40 | 2.29 | 58 | 1.90 | 76 | 1.71 | 94 | 1.60 |
| 23 | 7.28 | 41 | 2.26 | 59 | 1.59 | 77 | 1.70 | 95 | 1.60 |
| 24 | 6.92 | 42 | 2.23 | 60 | 1.88 | 78 | 1.69 | 96 | 1.59 |
| 25 | 6.53 | 43 | 2.20 | 61 | 1.87 | 79 | 1.69 | 97 | 1.59 |
| 26 | 6.08 | 44 | 2.18 | 62 | 1.86 | S0 | 1.68 | 98 | 1.58 |
| 27 | 5.61 | 45 | 2.16 | 63 | 1.85 | 81 | 1.68 | 99 | 1.58 |
| 28 | 5.12 | 46 | 2.14 | 64 | 1.83 | 82 | 1.67 | 100 | 1.57 |

# MISCELLANE0US TABLES, 

FOR

COMPARING THE HYGROMETRICAL RESULTS OBTAINED BY DIFFERENT AUTHORITIES.147

## MISCELLANEOUS TABLES.

The object of these Tables is to afford the means of comparing the different determinations of the hygrometrical elements which have been obtained, or adopted, by various physicists, especially the values of the elastic forces of vapor given in other tables than those contained in the preceding pages.

Table XVIII., giving the elastic forces of vapor, expressed in millimetres of mercury, for Centigrade temperatures, was calculated by August from Dalton's experiments, and reduced to French measures in the translation of Kaemtz's Meteorology, by Chas. Martins, page 70, from which it has been taken. On these values are based the first psychrometrical tables published by August, in Berlin, 1825.

Table XIX. is the table computed by Kaemtz from his own experiments. It is found, reduced to French measures, in the same volume, page 68.

Table XX. furnishes the results of the experiments made by Professor Magnus, in Berlin, and published in Poggendorf's Aunalen, Tom. LXI. p. 226, and also in the Annales de Chimie et de Physique, $3^{\text {me }}$ série, Tom. XII. p. 88, from which this table was copied.

Table XXI. has been published by the Committee of Physics and Meteorology of the Royal Society, in their Report on the Objects of Scientific Inquiry in these Sciences, London, 1840, p. 89. The values which it contains are not derived from new experiments, but are probably computed from those existing at that time.

Table XXII. furnishes a synoptic view of the differences in the values of the force of vapor adopted by various authorities, prepared with the view of facilitating their comparison. A reference to their respective origin will be found below, page 152.

Table XXIII., showing the weight, in grammes, of the vapor contained in a cubic metre of saturated air, at different temperatures, is taken from Pouillet's Eléments de Physique, Tom. II. p. 707.
'Table XXIV. gives the weights as derived from August's experiments, in Kaemtz's Vorlesungen über Meteorologie. The table is copied from the French translation, by Martins, page 73. The tensions have been added, opposite the weights, and are extracted from August's table.

Table XXV. is found in Biot's Traité de Physique, Tom. I. p. 533.

## XVIII. ELASTIC FORCE OF AQUEOUS VAPOR,

EXPRESSED IN MILLIMETRES OF MERCURY FOR EVERY TENTH OF A CENTIGRADE DEGREE.

Catculated by AUGUST.

| Centigrade Degrees. | Tentlis of Degrees. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| $\bigcirc$ | Millim. | Millim. | Miliim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Mitlim |
| -31 | 0.45 | 0.45 | 0.45 | 0.44 | 0.44 | 0.43 | 0.43 | 0.42 | 0.42 | 0.41 |
| -30 | 0.50 | 0.49 | 0.49 | 0.48 | 0.18 | 0.47 | 0.47 | 0.46 | 0.46 | 0.45 |
| -29 | 0.5.4 | 0.54 | 0.54 | 0.53 | 0.53 | 0.52 | 0.52 | 0.51 | 0.51 | 0.50 |
| -28 | 0.59 | 0.58 | 0.58 | 0.57 | 0.57 | 0.56 | 0.56 | 0.55 | 0.55 | 0.54 |
| -27 | 0.63 | 0.63 | 0.63 | 0.62 | 0.62 | 0.61 | 0.61 | 0.60 | 0.60 | 0.59 |
| -26 | 0.70 | 0.69 | 0.68 | 0.68 | 0.67 | 0.66 | 0.66 | 0.65 | 0.64 | 0.64 |
| -25 | 0.77 | 0.76 | 0.75 | 0.75 | 0.74 | 0.73 | 0.73 | 0.72 | 0.71 | 0.71 |
| -24 | 0.83 | 0.83 | 0.82 | 0.82 | 0.81 | 0.80 | 0.80 | 0.79 | 0.78 | 0.78 |
| -23 | 0.90 | 0.89 | 0.88 | 0.88 | 0.87 | 0.86 | 0.86 | 0.85 | 0.84 | 0.84 |
| -22 | 0.99 | 0.98 | 0.97 | 0.96 | 0.95 | 0.95 | 0.94 | 0.93 | 0.92 | 0.91 |
| -21 | 1.06 | 1.05 | 1.04 | 1.04 | 1.03 | 1.02 | 1.02 | 1.01 | 1.00 | 1.00 |
| -20 | 1.15 | 1.14 | 1.13 | 1.12 | 1.11 | 1.11 | 1.10 | 1.09 | 1.08 | 1.07 |
| -19 | 1.26 | 1.25 | 1.24 | 1.23 | 1.22 | 1.21 | 1.20 | 1.18 | 1.17 | 1.16 |
| -18 | 1.33 | 1.32 | 1.31 | 1.31 | 1.30 | 1.29 | 1.29 | 1.28 | 1.27 | 1.27 |
| -17 | 1.44 | 1.43 | 1.42 | 1.41 | 1.40 | 1.39 | 1.38 | 1.36 | 1.35 | 1.34 |
| -16 | 1.56 | 1.54 | 1.53 | 1.52 | 1.51 | 1.50 | 1.49 | 1.47 | 1.46 | 1.45 |
| -15 | 1.69 | 1.68 | 1.67 | 1.65 | 1.64 | 1.63 | 1.61 | 1.60 | 1.59 | 1.57 |
| -14 | 1.80 | 1.79 | 1.78 | 1.77 | 1.76 | 1.75 | 1.74 | 1.72 | 1.71 | 1.70 |
| -13 | 1.96 | 1.94 | 1.93 | 1.91 | 1.89 | 1.88 | 1.86 | 1.85 | 1.83 | 1.82 |
| -12 | 2.12 | 2.10 | 2.09 | 2.07 | 2.05 | 2.04 | 2.02 | 2.01 | 1.99 | 1.98 |
| -11 | 2.30 | 2.28 | 2.26 | 2.25 | 2.23 | 2.21 | 2.19 | 2.17 | 2.16 | 2.14 |
| -10 | 2.48 | 2.46 | 2.44 | 2.43 | 2.41 | 2.39 | 2.37 | 2.35 | 2.34 | 2.32 |
| -9 | 2.66 | 2.64 | 2.62 | 2.61 | 2.59 | 2.57 | 2.55 | 2.53 | 2.52 | 2.50 |
| -8 | 2.86 | 2.84 | 2.82 | 2.80 | 2.78 | 2.76 | 2.74 | 2.72 | 2.70 | 2.68 |
| $-7$ | 3.09 | 3.06 | 3.04 | 3.02 | 3.00 | 2.97 | 2.95 | 2.93 | 2.91 | 2.88 |
| -6 | 3.32 | 3.29 | 3.27 | 3.25 | 3.23 | 3.20 | 3.18 | 3.16 | 3.14 | 3.11 |
| - 5 | 3.56 | 3.56 | 3.54 | 3.51 | 3.48 | 3.46 | 3.43 | 3.40 | 3.37 | 3.35 |
| $-4$ | 3.83 | 3.80 | 3.78 | 3.75 | 3.72 | 3.70 | 3.67 | 3.64 | 3.61 | 3.59 |
| - 3 | 4.11 | 4.07 | 4.05 | 4.02 | 3.99 | 3.97 | 3.94 | 3.91 | 3.88 | 3.86 |
| -. 2 | 4.40 | 4.37 | 4.34 | 4.32 | 4.29 | 4.26 | 4.23 | 4.20 | 4.17 | 4.14 |
| $-1$ | 4.71 | 4.68 | 4.65 | 4.62 | 4.59 | 4.56 | 4.53 | 4.49 | 4.46 | 4.43 |
| - 0 | 5.05 | 5.01 | 4.98 | 4.95 | 4.91 | 4.88 | 4.85 | 4.81 | 4.78 | 4.74 |
| + 0 | 5.05 | 5.09 | 5.12 | 5.16 | ๖. 19 | 5.23 | 5.27 | 5.30 | 5.34 | 5.37 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |



## NIX. ELASTIC FORCE OF AQUEOUS VAPOR,

Expressed in millimetres of mercury, for centigrade temperatures.
Br KAEMTZ

| Temperature CentiGrade. | Force of Vapor. | Temperature Centigrade. | Force of Vapor. | Temperature Centigrade. | Force of Vapor. | Temperature Centigrade. | Force of Vapor. | Temperature Centigrade | Force of Vapor. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ | Millim. | $\bigcirc$ | Millim. | $\bigcirc$ | Millim. | $\bigcirc$ | Millim. | $\bigcirc$ | Millim. |
| -2.5 | 0.65 | -12 | 1.92 | 0 | 4.58 | 12 | 10.24 | 24 | 21.43 |
| $-24$ | 0.72 | -11 | 2.05 | 1 | 4.92 | 13 | 10.91 | 25 | 22.74 |
| $-23$ | 0.79 | -10 | 2.21 | 2 | 5.26 | 14 | 11.62 | 26 | 24.16 |
| $-22$ | 0.86 | $-9$ | 2.39 | 3 | 5.64 | 15 | 12.38 | 27 | 25.56 |
| -21 | 0.92 | $-8$ | 2.57 | 4 | 6.01 | 16 | 13.17 | 28 | 27.07 |
| $-20$ | 1.01 | $-7$ | 2.78 | 5 | 6.45 | 17 | 14.03 | 29 | 28.67 |
| -19 | 1.10 | -6 | 2.98 | 6 | 6.90 | 18 | 14.93 | 30 | 30.36 |
| -18 | 1.20 | - 5 | 3.20 | 7 | 7.33 | 19 | 15.86 | 31 | 32.17 |
| -17 | 1.29 | $-4$ | 3.45 | 8 | 7.89 | 20 | 16.87 | 32 | 33.95 |
| -16 | 1.40 | $-3$ | 3.70 | 9 | 8.41 | 21 | 17.91 | 33 | 3.5 .95 |
| $-15$ | 1.51 | $-2$ | 3.97 | 10 | 9.00 | 22 | 19.04 | 34 | 37.99 |
| $-14$ | 1.62 | $-1$ | 4.26 | 11 | 9.58 | 23 | 20.21 | 35 | 40.15 |
| -13 | 1.76 | 0 | 4.58 | 12 | 10.24 | 24 | 21.43 | 36 | 42.40 |

XX. ELASTIC FORCE OF AQUEOLS VAPOR, EXPRESSED IN MILLIMETRES OF MERCERY, FOR CENTIGRADE TEMPERATCRES.

Br MAGNUS.

| Temperature Centi- | Force of Vapor. | Temperature grade. | Force of Vapor. |  | Force of Vapor. | Temperature grade gr | Force of Vapor. | Temperature grade. grad | Force of Vapor. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ | sillim. | $\bigcirc$ | sillim | - | Millim. | $\bigcirc$ | Millim. | $\bigcirc$ | Sillim. |
| -20 | 0.916 | -7 | 2.671 | 6 | 6.439 | 19 | 16.34. | 32 | 35.419 |
| -19 | 0.999 | -6 | 2.886 | 7 | 7.436 | 20 | 17.396 | 33 | 37.473 |
| -18 | 1.089 | -5 | 3.115 | 8 | 7.964 | 21 | 18.505 | 34 | 39.630 |
| -17 | 1.186 | -4 | 3.361 | 9 | 8.52. | 22 | 19.67 .5 | 35 | 41.893 |
| -16 | 1.290 | -3 | 3.624 | 10 | 9.126 | 23 | 20.909 | 36 | 4.265 |
| -15 | 1.403 | -2 | 3.905 | 11 | 9.751 | 24 | 22.211 | 37 | 46.758 |
| -14 | 1.525 | -1 | 4.205 | 12 | 10.421 | 25 | 23.582 | 38 | 49.368 |
| -13 | 1.655 | 0 | 4.525 | 13 | 11.130 | 26 | 25.026 | 39 | 52.103 |
| -12 | 1.796 | +1 | 4.867 | 14 | 11.882 | 27 | 26.547 | 40 | 54.964 |
| -11 | 1.947 | 2 | 5.231 | 15 | 12.677 | 28 | 28.148 | 41 | 57.969 |
| -10 | 2.109 | 3 | 5.619 | 16 | 13.519 | 29 | 29.832 | 42 | 61.109 |
| -9 | 2.284 | 4 | 6.032 | 17 | 14.409 | 30 | 31.602 | 43 | 64.396 |
| - 8 | 2.471 | 5 | 6.471 | 18 | 15.351 | 31 | 33.464 | 44 | 67.833 |

XXI. ELAStic FORCE OF AQUEOUS VAPOR,

EXPRESSED IN ENGLISH INCHES OF MERCURY, FOR TEMPERATURES OF FAIIRENHEIT.

From the Royal Society's Report.

| $\begin{aligned} & \text { Temperature } \\ & \text { of } \\ & \text { Air. } \end{aligned}$ | Force of Vapor. | $\begin{gathered} \text { Temperature } \\ \text { of } \\ \text { Air. } \end{gathered}$ | $\begin{aligned} & \text { Force } \\ & \text { of } \\ & \text { vapor. } \end{aligned}$ | $\begin{gathered} \text { Temperature } \\ \text { of } \\ \text { Air. } \end{gathered}$ | Foree of Vapor. | $\begin{aligned} & \text { Temperature } \\ & \text { of } \\ & \text { Air. } \end{aligned}$ | Force of Vapor. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahrenheit. | Eng. Inches. | Fahrenheit. | Eng Inches. | Fahrenheit. | Eng. Inches. | Fahrenheit. | Eng. Inches. |
| $0{ }^{\circ}$ | 0.0 .51 | $31^{\circ}$ | 0.179 | $62^{\circ}$ | 0.551 | $93{ }^{\circ}$ | 1.514 |
| 1 | 0.0 .38 | 32 | 0.186 | 63 | 0.570 | 94 | 1.562 |
| 2 | 0.056 | 33 | 0.193 | 64 | 0.590 | 95 | 1.610 |
| 3 | 0.0 .58 | 34 | 0.200 | 65 | 0.611 | 96 | 1.660 |
| 4 | 0.060 | 35 | 0.208 | 66 | 0.632 | 97 | 1.712 |
| 5 | 0.063 | 36 | 0.216 | 37 | 0.654 | 98 | 1.764 |
| 6 | 0.066 | 37 | 0.224 | 68 | 0.676 | 99 | 1.819 |
| 7 | 0.069 | 38 | 0.233 | 69 | 0.699 | 100 | 1.574 |
| 8 | 0.071 | 39 | 0.242 | 70 | 0.723 | 101 | 1.931 |
| 9 | 0.071 | 40 | 0.251 | 71 | 0.748 | 102 | 1.990 |
| 10 | 0.078 | 41 | 0.260 | 72 | 0.773 | 103 | 2.050 |
| 11 | 0.081 | 42 | 0.270 | 73 | 0.799 | 104 | 2.112 |
| 12 | 0.084 | 43 | 0.280 | 74 | 0.826 | 10.5 | 2.176 |
| 13 | 0.088 | 44 | 0.291 | 75 | 0.8 .54 | 106 | 2.241 |
| 14 | 0.092 | 45 | 0.302 | 76 | 0.882 | 107 | 2.307 |
| 15 | 0.095 | 46 | 0.313 | 77 | 0.911 | 108 | 2.376 |
| 16 | 0.099 | 47 | 0.324 | 78 | 0.942 | 109 | 2.447 |
| 17 | 0.103 | 48 | 0.336 | 79 | 0.973 | 110 | 2.519 |
| 18 | 0.107 | 49 | 0.349 | 80 | 1.005 | 111 | 2.593 |
| 19 | 0.112 | 50 | 0.361 | 81 | 1.036 | 112 | 2.669 |
| 20 | 0.116 | 51 | 0.375 | 82 | 1.072 | 113 | 2.747 |
| 21 | 0.121 | 52 | 0.389 | 83 | 1.106 | 114 | 2.826 |
| 22 | 0.126 | 53 | 0.402 | 84 | 1.142 | 115 | 2.908 |
| 23 | 0.131 | 5.4 | 0.417 | 85 | 1.179 | 116 | 2.992 |
| 24 | 0.136 | 55 | 0.432 | 86 | 1.217 | 117 | 3.078 |
| 25 | 0.142 | 56 | 0.447 | 87 | 1.256 | 118 | 3.166 |
| 26 | 0.147 | 57 | 0.463 | 88 | 1.296 | 119 | 3.257 |
| 27 | 0.153 | 58 | 0.480 | 89 | 1.337 | 120 | 3.349 |
| 28 | 0.159 | 59 | 0.497 | 90 | 1.380 | 121 | 3.444 |
| 29 | 0.165 | 60 | 0.514 | 91 | 1.423 | 122 | 3.542 |
| 30 | 0.172 | 61 | 0.332 | 92 | 1.468 | 123 | 3.641 |
| 31 | 0.179 | 62 | 0.551 | 93 | 1.514 | 124 | 3.743 |

B

## TABLE XXII.

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FOR SHOWING THE DIFFERENCES IN THE VALUES OF THE ELASTJC FORCE OF
    AQUEOUS VAPOR ADOPTED BY DIFFERENT AUTHORITIES.
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The following synoptic view of the values of the elastic force of vapor adopted by various authoritics, furnishes the means of readily comparing them, and of appreciating the amount of the differences which they exhibit. The values are given both in English and in French measures.

Dalton's values are copied from the Edinburgh Encyclopadia, Art. Hygrometry. Those adopted in the Greenwich Observations are found in the same article, and also in the volumes published annually by that Observatory. Biot's table of tensions is, in fact, the same, computed by Pouillet from Dalton's results, by Biot's formula, and published in Biot's Traité de Physique, Tom. I. p. 531. Dr. Ure's results are taken from his Memoir in the Philosophical Transactions for 1818, p. 347. In the column beaded "Daniell" are given the forces of vapor as found in the table published in his Meteorological Essays, 2 d edition, p. 596, a table computed by Galbraith, from Dr. Ure's expcriments, by the formula of Ivory.

For the columns headed Royal Society, August, Kaemtz, Magnus, and Regnault, see above, p. 147.

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B\(15 t\)
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xxif. FOR SHOWING THE DIfferences in the valles of the elastic FORCE OF AQUEOUS VAPOR, ADOPTED BY DIFFERENT AUTHORITIES.

FORCE OF VAPOR EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

| Temperature of Air, Fahrenheit. | Force of Vapor according to |  |  |  |  |  |  |  |  | Temperature of Air, Fahrenheit. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dalton. | ```Green- wich Observa- tions.``` | Ure. | Daniell. | Royal Society. | August. | Kaemtz. | Magnus. | Regnault. |  |
| $\bigcirc$ | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | $\bigcirc$ |
| 0 | 0.064 | 0.061 | . . . . | $0.068$ | $0.051$ | $0.053$ | $0.048$ | 0.044 | $0.043$ | 0 |
| 10 | 0.090 | 0.059 |  | 0.098 | 0.078 | 0.052 | 0.074 | 0.070 | 0.068 | 10 |
| 20 | 0.129 | 0.129 | -••• | 0.140 | 0.116 | 0.124 | 0.112 | 0.108 | 0.108 | 20 |
| 30 | 0.186 | 0.186 |  | 0.200 | 0.172 | 0.184 | 0.166 | 0.164 | 0.167 | 30 |
| 32 | 0.200 | 0.199 | 0.200 | 0.216 | 0.156 | 0.199 | 0.180 | 0.175 | 0.181 | 32 |
| 40 | 0.263 | 0.264 | 0.250 | 0.280 | 0.251 | 0.269 | 0.244 | 0.245 | 0.248 | 40 |
| 50 | 0.375 | 0.373 | 0.360 | 0.400 | 0.361 | 0.390 | 0.354 | 0.359 | 0.361 | 50 |
| 60 | 0.524 | 0.523 | 0.516 | 0.560 | 0.516 | $0.5 \downarrow 7$ | 0.505 | 0.517 | 0.518 | 60 |
| 70 | 0.721 | 0.727 | 0.726 | 0.770 | 0.723 | 0.766 | 0.710 | 0.733 | 0.733 | 70 |
| 80 | 1.000 | 1.001 | 1.010 | 1.060 | 1.005 | 1.058 | 0.958 | 1.025 | 1.023 | 80 |
| 90 | 1.360 | 1.368 | 1.360 | 1.430 | 1.380 | 1.442 | 1.354 | 1.412 | 1.410 | 90 |
| 95 | 1.580 | 1.594 | 1.640 | 1.636 | 1.562 | $1.67 \%$ | 1.581 | 1.649 | 1.647 | 95 |
| 100 | 1.560 | 1.852 | 1.860 | - • • | 1.871 |  |  | 1.921 | 1.918 | 100 |

FORCE OF VAPOR EXPRESSED IN MILLIMETRES FOR CENTIGRADE
TEAPERATURES.

| Temperature of Air, Centigrade. | Force of Yapor according to |  |  |  |  |  |  |  |  | Temperature of Air, C'entigrade. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dalton. | ```Green- wich Observa- tions.``` | Biot, | Daniell. | Royal Suciety. | August. | Kaemtz. | Magnus. | Regnauit. |  |
| $\bigcirc$ | Millim. | Millim. | Nillim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | $\bigcirc$ |
| -20 | -••• |  | 1.33 |  |  | 1.15 | 1.01 | 0.91 | 0.91 | $-20$ |
| -15 | 1.93 | 1.88 | I. 88 | 2.11 | 1.60 | 1.69 | 1.51 | 1.40 | 1.38 | -15 |
| $-10$ | 2.64 | 2.62 | 2.63 | 2.92 | 2.34 | 2.48 | 2.21 | 2.11 | 2.08 | $-10$ |
| $-5$ | 3.66 | 3.66 | 3.66 | 4.01 | 3.33 | 3.56 | 3.20 | 3.11 | 3.13 | $-5$ |
| 0 | 5.08 | 5.06 | 5.06 | 5.49 | 4.72 | 5.05 | 4.58 | 4.52 | 4.60 | 0 |
| + 5 | 6.93 | 6.95 | 6.95 | 7.42 | 6.60 | 7.08 | 6.45 | 6.47 | 6.53 | $+5$ |
| 10 | 9.52 | 9.48 | 9.47 | 10.16 | 9.17 | 9.90 | 9.00 | 9.13 | 9.16 | 10 |
| 15 | 12.88 | 12.55 | 12.84 | 13.79 | 12.62 | 13.44 | 12.38 | 12.65 | 12.70 | 15 |
| 20 | 17.17 | 17.30 | 17.31 | 18.3t | 17.17 | 18.20 | 16.57 | 17.10 | 17.39 | 20 |
| 25 | 23.11 | 23.12 | 23.09 | 24.54 | 23.14 | 24.15 | 22.74 | 23.58 | 23.55 | 25 |
| 30 | 30.73 | 30.70 | 30.64 | 32.33 | 30.91 | 32.39 | 30.36 | 31.60 | 31.55 | 30 |
| 35 | 40.13 | 10.47 | 40.40 | 41.55 | 40.89 | 42.59 | 40.15 | 41.89 | 41.83 | 35 |
| 40 |  | - | 53.00 |  | 53.64 |  | -••• | 54.96 | 54.91 | 40 |

xxili. Weight of vapor, in grammes, contained in a cubic metre of saturated air, at temperatures between - $20^{\circ}$ and + $40^{\circ}$ centigrade. - poulletet.

| Temperature of Dew-Point | Force Vapor. | $\begin{aligned} & \text { Weight } \\ & \text { of } \\ & \text { Vapor. } \end{aligned}$ | Temperature of Dew-Point. | $\begin{aligned} & \text { Foree } \\ & \text { of } \\ & \text { Vapor. } \end{aligned}$ | $\begin{aligned} & \text { Weight } \\ & \text { of } \\ & \text { Vapor. } \end{aligned}$ | Temperature of Dew-Point. | $\begin{gathered} \text { Foree } \\ \text { of } \\ \text { Vapor. } \end{gathered}$ | Weight Vapor. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Centigrade | Millim. | Grammes. | Centigrade. | Nillim. | Grammes. | Centigrade. | Millim | Grammes. |
| $-20^{\circ}$ | 1.3 | 1.5 | $11^{\circ}$ | 10.1 | 10.3 | $26^{\circ}$ | 24.4 | 23.9 |
| -15 | 1.9 | 2.1 | 12 | 10.7 | 10.9 | 27 | 25.9 | 25.1 |
| -10 | 2.6 | 2.9 | 13 | 11.4 | 11.6 | 28 | 27.4 | 26.4 |
| - 5 | 3.7 | 4.0 | 14 | 12.1 | 12.2 | 29 | 29.0 | 27.9 |
| 0 | 5.0 | 5.4 | 15 | 12.8 | 13.0 | 30 | 30.6 | 29.4 |
| +1 | 5.4 | 5.7 | 16 | 13.6 | 13.7 | 31 | 32.4 | 31.0 |
| 2 | 5.7 | 6.1 | 17 | 14.5 | 14.5 | 32 | 34.3 | 32.6 |
| 3 | 6.1 | 6.5 | 18 | 15.4 | 15.3 | 33 | 36.2 | 34.3 |
| 4 | 6.5 | 6.9 | 19 | 16.3 | 16.2 | 34 | 38.3 | 36.2 |
| 5 | 6.9 | 7.3 | 20 | 17.3 | 17.1 | 35 | 40.4 | 38.1 |
| 6 | 7.4 | 7.7 | 21 | 18.3 | 18.1 | 36 | 42.7 | 40.2 |
| 7 | 7.9 | 8.2 | 22 | 19.4 | 19.1 | 37 | 45.0 | 42.2 |
| 8 | 8.4 | 8.7 | 23 | 20.6 | 20.2 | 38 | 47.6 | 44.4 |
| 9 | 8.9 | 9.2 | 24 | 21.8 | 21.3 | 39 | 50.1 | 46.7 |
| 10 | 9.5 | 9.7 | 25 | 23.1 | 22.5 | 40 | 53.0 | 49.2 |

XXIV. WEIGHT of Vapor, in grammes, contained in a cubic metre of saturated air, at temperatures between - $25^{\circ}$ and $+36^{\circ}$ centigr. - kaemtz.

| Temperature of Dew-Point. | Force of Yapor | $\begin{aligned} & \text { Weight } \\ & \text { of } \\ & \text { Vapor. } \end{aligned}$ | Temiperature of Dew-Point. | Force of Yapor. | Weight of Yapor. | Temperature of Dew-Point. | $\begin{gathered} \text { Foree } \\ \text { of } \\ \text { Vapor. } \end{gathered}$ | Weight yapor. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Centigrade $-25^{\circ}$ | $\begin{gathered} \text { Millim. } \\ 0.77 \end{gathered}$ | $\begin{gathered} \text { Grammes. } \\ 0.93 \end{gathered}$ | Ceutigrale $-4^{\circ}$ | $\begin{gathered} \text { Millim. } \\ 3 .>3 \end{gathered}$ | Grammes $4.37$ | Centigrade. $16^{\circ}$ | Millim. <br> 14.28 | Grammes. $14.97$ |
| -24 | 0.83 | 1.01 | -3 | 4.11 | 4.70 | 17 | 15.20 | 15.84 |
| -23 | 0.90 | 1.10 | -2 | 4.40 | 5.01 | 18 | 16.08 | 16.76 |
| -22 | 0.99 | 1.19 | -1 | 4.71 | 5.32 | 19 | 17.01 | 17.75 |
| -21 | 1.06 | 1.26 | 0 | 5.05 | 5.66 | 20 | 18.20 | 18.77 |
| -20 | 1.15 | 1.38 | +1 | 5.41 | 6.00 | 21 | 19.33 | 19.82 |
| -19 | 1.26 | 1.47 | 2 | 5.80 | 6.42 | 22 | 20.51 | 20.91 |
| -18 | 1.3:3 | 1.60 | 3 | 6.20 | 6.34 | 23 | 21.75 | 22.09 |
| -17 | 1.44 | 1.74 | 4 | 6.63 | 7.32 | 24 | 23.01 | 23.36 |
| -16 | 1.56 | 1.84 | 5 | 7.08 | 7.77 | 25 | 24.18 | 24.61 |
| -15 | 1.69 | 2.00 | 6 | 7.58 | 8.25 | 26 | 25.81 | 25.96 |
| -14 | 1.80 | 2.14 | 7 | 8.10 | 8.79 | 26 | 27.39 | 27.34 |
| -13 | 1.96 | 2.33 | 8 | 8.64 | 9.30 | 28 | 28.96 | 28.81 |
| -12 | 2.12 | 2.18 | 9 | 9.23 | 9.86 | 29 | 30.63 | 30.35 |
| -11 | 2.30 | 2.63 | 10 | 9.90 | 10.57 | 30 | 32.39 | 31.93 |
| -10 | 2.48 | 2.87 | 11 | 10.49 | 11.18 | 31 | 34.24 | 33.65 |
| -9 | 2.66 | 3.08 | 12 | 11.17 | 11.33 | 32 | 36.18 | 35.45 |
| - 5 | 2.86 | 3.30 | 13 | 11.86 | 12.57 | 33 | 38.21 | 37.20 |
| - 7 | 3.09 | 3.53 | 14 | 12.66 | 13.33 | 34 | . 10.38 | 39.12 |
| -6 | 3.32 | 3.80 | 15 | 13.44 | 14.17 | 35 | 42.59 | 41.13 |
| -5 | 3.56 | 4.08 | 16 | 14.28 | 14.97 | 36 | 44.96 | 43.17 |

## xXV. FORCES OF VAPOR AND RELATIVE HUMIDITY,

CORRESPONDING TO THE DEGREES OF SAUSSURE'S HAIR-HYGROMETER, AT THE TEMPERATURE OF $10^{\circ}$ CENTIGRADE.

From the Experiments of Gay-Lussac.

The force of vapor is expressed in hundredths, the tension at full saturation heing represented by 100 .


TABLE

## EOR

## dedccing the relative humidity in hundredths, from the indications of Saussure's halr-hygrometer;

Caleulated from the Experiments of Melloni.

By M. T. Haeghens.

The Hair-Hygrometer of Saussure having been formerly used for long series of observations, and being still employed by some meteorologists, notwithstanding the imperfection of this instrument, on account of its giving directly the rclative humidity without calculation, it was desirable to ascertain the correspondence of the degrees of that hygrometer with the relative humidity cxpressed in hundredths, as in the preceding table. Though these instruments compared with each other, show very often great discrepancies in their indications, yet a large number of them agree sufficiently well with the experiments of Melloni, August, and others, to allow the following table of comparison to be constructed, which table may be considered as giring good approximations. For the calculation of it, Mr. Haeghens used the results of Melloni, which agree also satisfactorily with a series of observations very carefully made by M. Delcros. See Annuaire Météorologique de la France, pour 1850.

RELATIVE HUMIDITY IN HUNDREDTIS.


## TABLE XYVII.

The following Table shows the Relative Humidity, in hundredths, corresponding to the degrees of Saussure's Hair-Hygrometer, as determined by various physieists. It is found in Kaemtz, Vorlesungen über Meteorologie, page 100 ; also in the French translation by Martins, Cours de Méléorologie, page 80.
XXVI. RELATIVE HUMIDIty, CORRESponding to the degrees of Saussure's HAIR-HYGRONETER.

Saturation $=100$.

|  | Relative Ilumidity according to |  |  |  | DegreesofIlair-IIygrometer. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gay-Lussac. | Prinsep. | August. | Melloni. |  |
| $100^{\circ}$ | 100.0 | 100.0 | 100.0 | 100.0 | $100^{\circ}$ |
| 95 | 89.1 | 88.7 | 9.1 .0 | 90.8 | 95 |
| 90 | 79.1 | 78.2 | 86.0 | 83.1 | 90 |
| 85 | 69.6 | 68.3 | 79.0 | 76.5 | 8.5 |
| 80 | 61.2 | 59.2 | 71.0 | 6-. 9 | 80 |
| 7.5 | 53.8 | 50.6 | 64.0 | 62.0 | 75 |
| 70 | 47.2 | 43.6 | 56.0 | 5.5 | 70 |
| 65 | 41.4 | 37.2 | 48.0 | 49.6 | 6.5 |
| 60 | 36.3 | 31.5 | 41.0 | +4.0 | 60 |
| 55 | 31.8 | 26.3 | 36.0 | 39.1 | 55 |
| 50 | 27.9 | 21.8 | 31.0 | 34.6 | 50 |
| 45 | 24.1 | 17.7 | 27.0 | 29.8 | 45 |
| 40 | 20.5 | 14.3 | 23.0 | 27.0 | 40 |
| 35 | 17.7 | 11.4 | 19.0 | 23.5 | 35 |
| 30 | 14.8 | 9.1 | 16.0 | 19.0 | 30 |
| 25 | 12.0 | 7.1 | 13.0 | 16.1 | 2.5 |
| 20 | 9.4 | . 1.9 | 10.0 | 11.7 | 20 |
| 1.5 | 7.0 | 3.0 | 7.0 | 8.3 | 15 |
| 10 | 4.6 | 1.6 | 4.0 | 5.0 | 10 |
| 5 | 2.2 | 0.6 | 2.0 | 2.6 | 5 |
| 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 |
| B |  |  |  |  |  |

# A P P ENDIX 

co

THE HYGROMETRICAL TABLES.

FOR

## COMPARING THE QUAN'TI'IIES OF RAIN-WATER

' ${ }_{\text {He }}$ three kinds of measures which are most in use for noting the quantities of rain and melted snow, are the Centimetres and Mitlimetres in France, the Paris or French inches and lines in Germany, and the English inches and decimals in England, America, and also in Russia, the Russian foot being the same as the English foot. 'The following tables will facilitate the comparison of these various measures with each other.

A glance at the tables will show that the first column on the left contains the numbers to be converted, and the heads of the following columns the fractions of these numbers, or units, each of which is one tenth of those in the first column. Shorter tables, at the bottom, give, when necessary, the value of proportional parts still smaller than those found in the larger tables.

## Evample.

Let 13 Centimetres be converted into French inches and lines.
Take, in Table II., the line beginning with 10 Centimetres in the first column, follow that line as far as the column beaded 3 Centimetres, and there will be found the number of 4 inches 9.63 lines, which is the corresponding value in French inches of $10 \not-3$, or 13 Centimetres.

If the number is followed by a fraction, as for instance, 13.5 Centimetres, or 135 Millimetres, we find, -

$$
\begin{aligned}
& \text { In the larger table } 13 \text { Centimetres }=4.9,63 \\
& \text { In the smaller table at the bottom } 5 \text { Millimetres }=.2,216 \\
& \text { Or } \overline{\mathbf{1 3} .5} \text { Centimetres }=\overline{4.11,846}
\end{aligned}
$$

When the measures which are to be compared are both subdivided into decimal parts, the equivalents of the numbers greater than 9.9 may be found by moving the decimal point.

## Example.

Let 316.7 Centimetres be converted into English inches.
In Table I., in the column headed 4, on the fourth line, we find $\quad 3.4$ Centimetres $=1.3386$ English inches.
Moving the decimal point by two places we have
310 Centimetres $=$ 133.86 English inches.
Then, in the column lieaded 7 , on the
line begiming with 6 , we find
Making together
B
6.7 Centimetres $=\quad 2.64$
$\overline{346.7}$ Centimetres $=\overline{136.50}$ English inches. 163

1 Centimetre $=0.3937079$ English Inch.

| Centimetres. | Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng.Inch. | Eng.Luch. | Eng. Inch | Eng.lnch. | Eng.Inch. | Eng.Inch. | Eug. Inch. | Eng.Inch. | Eng.luch | Eng.Inch. |
| 0 | 0.0000 | 0.0394 | 0.0787 | 0.1181 | 0.1575 | 0.1969 | 0.2362 | 0.2756 | 0.3150 | 03543 |
| 1 | 0.3937 | 0.4331 | 0.4724 | 0.5118 | 0.5512 | 0.5906 | 0.6299 | 0.6633 | 0.8087 | 0.7480 |
| 2 | 0.7874 | 0.3268 | 0.8662 | 0.9055 | 0.9449 | 0.9843 | 1.0236 | 1.0630 | 1.1024 | 1.1418 |
| 3 | 1.1811 | 1.2205 | 1.2599 | 1.2992 | 1.3386 | 1.3780 | 1.4173 | 1.4567 | 1.4961 | 1.5355 |
| 1 | 1.5748 | 1.6142 | 1.6536 | 1.6929 | 1.7323 | 1.7717 | 1.8111 | 1.8504 | 1.8898 | 1.9292 |
| 5 | 1.9685 | 2.0079 | 2.0473 | 2.0867 | 2.1260 | 2.1654 | 2.2048 | 2.2441 | 2.2835 | 2.3229 |
| 6 | 2.3622 | 2.4016 | 2.4410 | 2.4804 | 2.5197 | 2.5591 | 2.5955 | 2.6378 | 2.6752 | 2.7166 |
| 7 | 2.7560 | 2.7953 | 2.8347 | 2.8741 | 2.9134 | 2.9528 | 2.9922 | 3.0316 | 3.0709 | 3.1103 |
| 8 | 3.1497 | 3.1890 | 3.2284 | 3.2678 | 3.3071 | 3.3465 | 3.3859 | 3.1253 | 3.4646 | 3.5040 |
| 9 | 3.5434 | 3.5827 | 3.62. 1 | 3.6615 | 8.7009 | 3.7402 | 3.7796 | 3.8190 | 3.8583 | 3.8977 |

II. CONVERSION OF CENTIMETRES INTO FRENCH INCHES, LINES, AND DECIMALS.

I Centimetre $=0$. inches 4.43296 Paris lines.

| Centimetres. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fr.1n. Lin | Lin. |  | Fr.In. Lin. | Fr.In. Lin. | Fr.In.Lin | Fr.In. ${ }^{\text {Li }}$ | In. Lin. | Fr.ln. Lin. | Fr.In, Lin |
| 0 | 0. 0,00 | 0. 4,43 | 0. 8,87 | 1. 1,30 | 1. 5,73 | 1.10,16 | 2. 2,60 | 2. 7,03 | 2.11,16 | 3. 3,90 |
| 10 | 3. 8,33 | 4. 0,76 | 4. 5,20 | 4. 9,63 | 5. 2,06 | 5. 6,49 | 5.10,93 | 6. 3,36 | 6. 7,79 | 7. 0,23 |
| 20 | 7. 4,66 | 7. 9,09 | 8. 1,53 | 8. 5,96 | S.10,39 | 9. 2,82 | 9. 7,26 | 9.11,69 | 10. 4,12 | 10. 8,56 |
| 30 | 11. 0,99 | 1. 5,42 | 11. 9,85 | 12. 2,29 | 12. 6,72 | 12.11,15 | 13. 3,59 | 3. 8,02 | 14. 0,45 | 1.1. 4,89 |
| 40 | 14. 9,32 | 5. 1,75 | 15. 6,18 | 15.10,62 | 16. 3,05 | 16. 7,48 | 16.11,92 | 7. 4,35 | 17. 5,78 | 18. 1,22 |
| 50 | 18. 5,65 | 8.10,0S | 19. 2,51 | 19. 6,9 | 19.11,38 | 20. 3,81 | 20. 5,25 | 1. 0,68 | 21. 5,11 | 21. 9,54 |
| 60 | 22. 1,98 | 6,41 | $22.10,54$ | 23. 3,28 | 3. 7,71 | 24. 0,14 | 24. 4,58 | 4. 9,01 | 25. 1,44 | 25. 5,97 |
| 70 | 25.10,31 | 2,74 | 26. 7,17 | 26.11,61 | 27. 4,04 | 27. 8,17 | 25. 0,90 | 8. 5,34 | 28. 9,77 | 29. 2,20 |
| 80 | 29. 6,64 | $9.11,07$ | 30.3,50 | 30. 7,93 | 31. 0,37 | 31. 4,50 | 31. 9,23 | 2. 1,67 | 32. 6,10 | $32.10,53$ |
| 90 | 33. 2,97: | 7,40 | 33.11,83 | 34. 4,26 | 4. 8,70 | 3.5. 1,13 | 35. 5,56 | 5.10,00 | 36. 2,43 | $36 \quad 6,96$ |

$\|_{\text {Centim. }} \mid$ Fr.In. Lin. $\mid$ Centim. Fr.In. Lin. $\mid$ Centim. Fr.In. Lin $|\mid$ Centim. Fr.In. Lin. $|$ Centim. Fr. In. Lin.


CONVERSION OF CENTIMETRES INTO FRENCH LINES AND DECINALS.

| Centimetres. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fr. Lines. | Fr. Lines. | Fr. Lines. | Fr. Lines. | Fr. Lines. | Fr. Lines. | Fr. Lines, | Fr. Lines. | Fr. Lines | Fr. Lines. |
| 0 | 0.00 | 4.43 | 8.87 | 13.30 | 17.73 | 22.16 | 26.60 | 31.03 | 3.5. 16 | 39.90 |
| 10 | 44.33 | 48.76 | 53.20 | 57.63 | 62.06 | 66.49 | 7093 | 75.36 | 79.79 | 84.23 |
| 20 | 85.66 | 93.09 | 97.53 | 101.96 | 106.39 | 110.92 | 115.26 | 119.69 | 124.12 | 128.56 |
| 30 | 132.99 | 137.42 | 141.85 | 146.29 | 150.72 | 155.15 | 159.59 | 164.02 | 168.45 | 172.89 |
| 40 | 177.32 | 181.75 | 186.18 | 190.62 | 195.0.5 | 199.48 | 203.92 | 208.3.) | 212.78 | 217.22 |
| 50 | 221.65 | 226.08 | 230.51 | 234.9 .5 | 239.38 | 243.81 | 248.25 | 2.23 .68 | 2.57 .11 | 261.54 |
| 60 | 26.5.98 | 270.41 | 274.84 | 279.28 | 283.71 | 288.14 | 292.58 | 297.01 | 301.44 | 30.5 .57 |
| 70 | 310.31 | 314.74 | 319.17 | 323.61 | 328.04 | 332.47 | 336.90 | 341.34 | 345.77 | 350.20 |
| S0 | 354.64 | 359.07 | 363.50 | 367.93 | 372.37 | 376.80 | 381.23 | 385.67 | 390.10 | 394.58 |
| 90 | 398.97 | 403.40 | 407.83 | 412.26 | 416.70 | $\underline{+21.13}$ | 42.5 .56 | 430.00 | 434.43 | 438.86 |

CONVERSION OF MILLIMETRES INTO FRENCH LINES AND DECIMALS.

|  | 10. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \|| Fr. Lines. | $\begin{array}{\|c\|} \hline \text { Fr. Lines. } \\ 0.443 \end{array}$ | $\begin{gathered} \text { Fr. Lines. } \\ 0.887 \end{gathered}$ | $\begin{array}{\|c\|} \text { Fr. Lines. } \\ 1.330 \end{array}$ | $\begin{array}{\|c\|} \text { Fr. Lines } \\ 1.773 \end{array}$ | $\begin{array}{\|c\|} \hline \text { Fr. Lines. } \\ 2.216 \end{array}$ | $\begin{gathered} \text { Fr. Lines. } \\ 2.660 \end{gathered}$ | $\left\lvert\, \begin{array}{\|c\|} \text { Fr. Lines. } \\ 3.103 \end{array}\right.$ | $\begin{array}{\|c\|} \hline \text { Fr. Lines. } \\ 3.546 \end{array}$ | $\begin{array}{\|c} \text { Fr. Lines. } \\ 3.990 \end{array}$ |
| B | 164 |  |  |  |  |  |  |  |  |  |

I English Inch $=2.53995$ Centimetres.


1 French Inch $=2.7070$ Centimetres.

| French luches. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 0 | Centim. 0.00 | Centim. 2.71 | Centim. 5.41 | Centim. 5.12 | Centim. 10.53 | Centim. <br> 13.53 | Centim. 16.94 | Centim. 18.95 | Centim. $21.66$ | Centim. $24.36$ |
| 10 | 27.07 | 29.78 | 32.48 | 35.19 | 37.90 | 40.60 | 43.31 | 46.02 | 48.73 | 51.43 |
| 20 | 54.14 | 56.85 | 59.5. | 62.26 | 64.97 | 67.67 | 70.35 | 73.09 | 75.80 | 78.50 |
| 30 | 81.21 | 83.92 | S6.62 | 89.33 | 92.04 | 94.74 | 97.45 | 100.16 | 102.87 | 105.57 |
| 40 | 108.28 | 110.99 | 113.69 | 116.40 | 119.11 | 121.81 | 124.52 | 127.23 | 129.94 | 132.64 |
| 50 | 135.35 | 138.06 | 140.76 | 143.47 | 146.18 | 148.88 | 151.59 | 154.30 | 157.01 | 159.71 |
| 60 | 162.42 | 165.13 | 167.83 | 170.54 | 172.25 | 175.95 | 178.66 | 181.37 | 184.08 | 186.78 |
| 70 | 189.49 | 192.20 | 194.90 | 197.61 | 200.32 | 203.02 | 20.7 .73 | 208.44 | 211.15 | 213.5 .5 |
| 80 | 216.56 | 219.07 | 2.21 .97 | 2.24 .65 | 227.39 | 230.09 | 232.80 | 235.51 | 238.22 | 240.92 |
| 90 | 243.63 | 246.34 | 249.04 | 2.51 .75 | 254.46 | 257.16 | 259.87 | 262.58 | 265.29 | 267.99 |
| 100 | 270.70 | 273.41 | 276.11 | 278.52 | 281.53 | 284.23 | $2 \bigcirc 6.94$ | 289.65 | 292.36 | 295.06 |
| 110 | 297.77 | 300.45 | 303.18 | 305.59 | 308.60 | 311.30 | 314.01 | 316.72 | 319.42 | 322.13 |
| 120 | 324.84 | 327.95 | 330.25 | 332.96 | 335.67 | 335.37 | 341.08 | 343.79 | 346.49 | 349.20 |
| 130 | 3.51 .91 | 354.62 | 357.32 | 360.03 | 362.74 | 365.44 | 865.15 | 370.86 | $3 \pi 3.56$ | 376.27 |
| 140 | 375.95 | 351.69 | 384.39 | 387.10 | 359.81 | 392.51 | 395.22 | 397.93 | 400.63 | 403.34 |
| 150 | 406.05 | 405.76 | 411.46 | 414.17 | 416.88 | 419.58 | 422.29 | 425.00 | 427.70 | 430.41 |
| 160 | 433.12 | 435.83 | 438.53 | 441.24 | 443.95 | 446.65 | 449.36 | 452.07 | 454.77 | 457.48 |
| 170 | 460.19 | 462.90 | 465.60 | 468.31 | 471.02 | 473.72 | 476.43 | 479.14 | 48184 | 484.55 |
| 180 | 487.26 | 489.97 | 492.67 | 495.35 | 498.09 | 500.79 | 503.50 | 506.21 | 508.91 | 511.62 |
| 190 | 514.33 | 517.04 | 519.74 | 522.45 | 52.5.16 | 527.86 | 530.57 | 533.28 | 535.98 | 538.69 |
| 200 | $5+1.40$ | 544.11 | 546.81 | 549.52 | 552.23 | 5.54 .93 | 5.57 .64 | 560.35 | 563.0.5 | 565.76 |
| Conversion of french lines into centimetres. |  |  |  |  |  |  |  |  |  |  |
| 1 French Line $=0.22558$ Centimetre , |  |  |  |  |  |  |  |  |  |  |
| French Lines. | Terths of a Line. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Centim. | Centim. | Centim. | Centim. | Centim. | Centim. | Centim. | Centim. | Cenim. | Centim. |
| 0 | 0.000 | 0.023 | 0.045 | 0.063 | 0.090 | 0.113 | 0.135 | 0.158 | 0.180 | 0203 |
| 1 | 0.226 | 0.248 | 0.271 | 0.293 | 0.316 | 0.338 | 0.361 | 0.383 | 0.406 | 0.429 |
| 2 | 0.451 | 0.474 | 0.496 | 0.519 | 0.541 | 0.564 | 0.557 | 0.609 | 0.632 | 0.6 .54 |
| 3 | 0.677 | 0699 | 0.722 | 0.744 | 0.767 | 0.790 | 0.812 | 0.535 | 0.857 | 0.880 |
| 4 | 0.902 | 0.925 | 0.947 | 0.970 | 0.993 | 1.015 | 1.038 | 1.060 | 1.083 | 1.105 |
| 5 | 1.128 | 1.150 | 1.173 | 1.196 | 1.218 | 1.241 | 1.263 | 1.286 | 1.308 | 1.331 |
| 6 | 1.353 | 1.376 | 1.399 | 1.421 | 1.444 | 1.466 | 1.489 | 1.511 | 1.534 | 1.557 |
| 7 | 1.579 | 1.602 | 1.624 | 1.647 | 1.669 | 1.692 | 1.714 | 1.737 | 1.760 | 1.782 |
| 8 | 1.505 | 1.527 | 1.850 | 1.872 | 1.895 | 1.917 | 1.940 | 1.963 | 1.985 | 2.008 |
| 9 | 2.030 | 2.053 | 2.075 | 2.095 | 2.120 | 2.143 | 2.166 | 2.188 | 2.211 | 2.233 |
| 10 | 2.256 | 2.278 | 2.301 | 2.324 | 2.346 | 2.369 | 2.391 | 2.414 | 2.436 | 2.459 |
| 11 | 2.481 | 2.504 | 2.527 | 2.549 | 2.572 | 2.594 | 2.617 | 2.639 | 2.662 | 2.684 |
| 12 | 2.707 | 2.730 | 2.752 | 2.775 | 2.797 | 2.820 | 2.842 | 2.86 .5 | 2.887 | 2.910 |
| B | 166 |  |  |  |  |  |  |  |  |  |

1 French Inch $=1.065765$ English Inch.


CONVERSION OF FRENCH LINES INTO ENGLISH INCHES.
1 French Line $=0.088814$ English Inch.

| French L!ues. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eug.Iuch. | Eng.Inch. | Eng.Inch. | Eng.Inch | Eng luch. | Eng. Jnch. | Eng luch. | Eng.Inch 0.0622 | Eng. Inch. 0.0711 | Eng lnch. $0.0799$ |
| 0 | 0.0000 | 0.0089 | 0.0178 | 0.0266 | 0.0355 | 0.0444 | 0.0533 | 0.0622 | 0.0711 |  |
| 1 | 0.0888 | 0.0977 | 0.1066 | 0.1155 | 0.1243 | 0.1332 | 0.1421 | 0.1510 | 0.1599 | 0.1687 |
| 2 | 0.1776 | 0.1865 | 0.1954 | 0.2013 | 0.2132 | 0.2220 | 0.2309 | 0.2398 | 0.2487 | 0.2576 |
| 3 | 0.2664 | 0.2753 | 0.2842 | 0.2931 | 0.3020 | 0.3108 | 0.3197 | 0.3286 | 0.3375 | 0.3464 |
| 4 | 0.3553 | 0.3641 | 0.3730 | 0.3819 | 0.3908 | 0.3997 | 0.1085 | 0.4174 | 0.1263 | 0.4352 |
| 5 | 0.4441 | 0.4530 | 0.4618 | 0.4707 | 0.4796 | 0.1885 | 0.4974 | 0.5062 | 0.5151 | 0.5240 |
| 6 | 0 | 0.5418 | 0.5506 | 0.5595 | 0.5684 | 0.5773 | 0.5862 | 0.5951 | 0.6039 | 0.6128 |
| 7 | 0.6217 | 0.6306 | 0.6395 | 0.6483 | 0.6572 | 0.6661 | 0.6750 | 0.6539 | 0.6927 | 0.7016 |
| 8 | 0.7105 | 0.7194 | 07283 | 0.7372 | 0.7460 | 0.7549 | 0.7638 | 0.7727 | 0.7816 | 0.7904 |
| 9 | 0.7993 | 0.8082 | 0.8171 | 0.8260 | 0.8349 | 0.8437 | 0.8526 | 0.8615 | 0.8704 | 0.8793 |
| 10 | 0.8881 | 0.8970 | 0.9059 | 0.9148 | 0.9237 | 0.9325 | 0.9414 | 0.9503 | 0.9592 | 0.9681 |
|  |  |  |  |  |  |  |  |  |  |  |
| 11 | 0.9770 | 0.9858 | 0.9947 | 1.0036 | 1.0125 | 1.0214 | 1.0302 | 1.0391 | 1.0480 | 1.0569 |
| 12 | 1.0658 | 1.0746 | 1.0835 | 1.0924 | 1.1013 | 1.1102 | 1.1191 | 1.1279 | 1.1365 | 1.1457 |

# METEOROLOGICAL TABLES. 

## SERIES IIL

BAROMETRICAL TABLES.

## C 0 NTENTS.

(The figures refer to the folio at the bottom of the page.)
For Comparing the different Barometrical Scales.
Table I. Comparison of the English and the Metrieal Barometers ..... 11
" II. Comparison of the English and the Old French Barometers ..... 15
" 1ll. Comparison of the Metrical and the English Barometers ..... 21
" IV. Comparison of the Metrical and the Oid Freneh Barometers ..... 27
" V. Comparison of the Old French and the English Barometers ..... 35
" VI. Comparison of the Old Freneh and the Metrical Barometers ..... 39
" Vll. Comparison of the Russian and the Metrieal Barometers ..... 46
" VIII. Comparison of the Russian and the Old French Barometers ..... 48
For Comparing Barometrical Differences.
"6 IX. Conversion of English Inches into Millimetres ..... 53
" X. Conversion of English lnches into French or Paris Lines ..... 53
" XI. Conversion of Millimetres into English Inches ..... 54
6 Xll. Conversion of Millimetres into French or Paris Lines ..... 55
" Xlll. Conversion of French or Paris Lines into Millimetres ..... 56
" XIV. Conversion of French or Paris Lines into English Inches ..... 56
" XV. Conversion of Russian Half-Lines into Millimetres ..... 57
" XVI. Conversion of Russian ITalf-Lines into Paris Lines ..... 57For Rechuing Barometrical Observations to the Freezing Point.
" XVII. Reduction of English Barometers with Brass Scales ..... 65
6 XVIIl. Reduction of English Barometers with Glass, or Wooden Scales ..... 72
" XIX. Reduction of the Metrical Earometer, by Delcros ..... 73
" XX. Reduction of the Metrical Barometer, by Haeghens ..... 81

* XXI. Reduction of the Old French Barometer, by Kaemtz ..... 124For Correcting Barometrical Obsereations for Capillary Action.
" XXIJ. Correction to be applied to English Barometers for Capillary Action ..... 131
" XXIII. Normal Height of Meniscus in Millimetres, by Deleros ..... 131
" XXIV. Correction to be applied to Metrical Barometers for Capillary Action, by Deleros ..... 139
" XXV. Depression of the Barometrical Column due to Capillary Action. - Pouillet ..... 133
" XXVI. Depression of the Barometrical Column due to Capillary Action. - Gehler's Wörterb. ..... 133
"XXVII. Depression of the Barometrical Column due to Capillary Action, reduced from Delcros' 'Table ..... 134
"XXVIII. Depression of the Barometrical Column due to Capillary Action. - Baily ..... 131



# COMPARISON 

of

## THE BAROMETRICAL SCALES,

VR

T A B L E S

FOR CONVERTLNG THE INDICATIONS OF THE ENGLISII, METRICAL, OLD FRENCH, AND RCSSAN BAROMETERS INTO EACH OTIER

## COMPARISON

OF

## 'I'HEBAROMETRICALSCALES.

The following tables are intended for converting into each other the four most tmportant Barometrical Scales. They are sufficiently detailed to save the labor of any calculation or even of interpolation for the ordinary wants of Meteorology. But before maxing use of them, for comparing the observations taken with barometers of different scales, it is necessary to reduce the observed heights to the temperatar: of the freezing point, or to any other temperature, provided it be the same for all, by means of the tables calculated for this purpose, and which will be found below. The reason of it may be readily understood.

The length of the bars of metal, or of other substances, which represent the stand ard measures of length which obtain among different nations, varying with the temperature, it was necessary to determine a fixed point of temperature at which they really ought to have the length adopted as the standard unit of measure. This temperature is the normal temperature of the standard, and the length of the stand-ard-bar, at this temperature, is the true length of it.

If the normal temperature of the various standards used for dividing Barometrical Scales were the same, the heights of the barometrical column, taken with these scales, could be compared directly, provided the seales be made of the same substance, brass, for instance, because their variations above or below this normal temperature would remain parallel with each other. But unfortunately it is not so. The English Yard is a standard at the temperature of $62^{\circ}$ Fabrenheit ; the Old French Toise, at $13^{\circ}$ Reaumur; the Metre, at the freezing point, or zero Centigrade. Thus metallic rods intended to represent these varions mits of measure give the trme or standard length only when at these respective temperatures; at any other temperature they are longer or shorter than the standard, and their subdivisions, inches, lines, or millimetres, partake of the error.

It is obvious, therefore, that the barometrical heights, taken with different scales, cannot be compared directly by means of the following tables, which give the relation between these scales at their respective normal temperatures. For suppose the temperature of the three barometers to be the freezing point, or $33^{\circ}$ Fuhrenheit, C
the scale of the Metrical Barometer alone will actually represent the standard len $n_{i}$ th and the millimeters will have the true length; while the inches and lines of the Old French and of the English Barometers will be too short, causing thus the barometrical column to appear too high. If the temperature of the instruments be $6 z^{\circ}$ Fahrenheit, the divisions of the English Barometer will have the true standard length, and those of the Old French Barometer nearly so ; but the millimeters of the Metrical Barometer will be too long, causing the barometrical column to appear too low. It is to neutralize the effect of those inequalitics arising from the expansion of the scale that it is necessary, before comparing the observations taken with the three barometers, to reduce them to the same temperature. This is done by means of the tables above mentioned, for reducing the barometer to the freezing point, which suppose the scales to be of brass from top to bottom, and which take into account the expansion or contraction they undergo by the variations of temperature.

But in doing so, we must be aware that the accuracy of the comparison depends in part upon the correctness of the indications of the attached thermometers, which determine the amount of the correction to be applicd for reducing the barometers to the freezing point. If the thermometers do not agree, an error is introduced which will affect the height of the reduced columns, and the fimal comparison. Therefore the correction of the attached thermometers ought to be ascertained and applied to tnem before the reduction is made; or if this correction is unknown, it will be well to place the instruments to be compared in the most favorable conditions for taking the same temperature, and then to take the temperature given by one of the thermometers to reduce both barometers. If the correction of the attached thermometer has not been applied before the reduction, it will be contained, after the reduction, in the total correction of the instrument. If it be so, this circumstance must be indicated.
In computing the following tables, the value of the Mctre, as determined by Capt. Kater, (Philosoph. Tramsact. for 1818, p. 109, and Baily's Astronomical Tables, p. 192, ) has been idopted, viz. 1 Metre, at $0^{\circ}$ Centigrade $=39.37079$ English inches, at $6 \exists^{\circ}$ Falhenheit. The relation of the Metre (legal) to the Old French system of measures is known to be 1 Metre $=443.296$ French or Paris lines. From these equations are derived the clements used in the computations, which are found at the head of each table.

Besides the larger Tables I. - VIII., a set of smaller ones, Tables IX. - XVI., has been added, which will be found useful for comparing Barometrical differences, such as runges, amount of variation in a given time, $\mathcal{\&} c$., expressed in measures of different scales, in which only small quantities occur that are not found in the large tables.
I. - II.

COMPARISON
of

## TIIE ENGLISII BAROMETER

WITII

TIIE METRICAL AND TIIE OLD FRENCI BAROMETERS,

OR

## T A B L E S

for converting exglisil inciles into milhimetres, and into frexcil or paris line and dechmals;

GIVING TIIE VALUES CORRESPONDING TO EVERY TENTU OF AN INCII, FROM 9 TO 19 INCIES ; AND TO EVERY IIINDREDTII, FROM

19 TO 3l.5 ENGLISH INCHES.

## C

## USE OF TABLE I.

Example.

The English Barometer reads 20.657 inches. What would be the corresponding beight in the Metrical Barometer?

In Table I., first column on the left, look out the line of 20 inches 6 tenths; on that line, in the sixth column, headed 5 hundredths, is found the value in millimetres for
20.65 inches $=524.50$ millimetres.

At the bottom of the page, for 0.007 " $=0.18$ " Or for $20.657 \quad "=524.68$ " which would be the reading of the Metrical Barometer.

This example may serve for all tables, throughout the volume, which are constructed on the same plan.

1 English Inch $=25.39954$ Millimetres.

| English Inches. | Tenths of an Inch. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 9 | $\begin{aligned} & \text { Millim. } \\ & 228.60 \end{aligned}$ | $\begin{array}{\|c} \text { Millim. } \\ 231.14 \end{array}$ | $\begin{array}{\|c} \text { Mıllim. } \\ 233.68 \\ \hline \end{array}$ | $\begin{gathered} \text { Millim. } \\ 236.22 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 238.76 \end{aligned}$ | $\begin{gathered} \text { Mutlim. } \\ 2+1.30 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 243.84 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 246.38 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 2+8.9 .2 \end{aligned}$ | $\begin{array}{\|c\|c\|} \text { Millim } \\ 2.51 .46 \end{array}$ |
| 10 | 254.00 | 256.54 | 259.08 | 261.62 | 264.16 | 266.70 | 269.24 | 271.78 | 274.32 | 276.85 |
| 11 | 279.39 | 281.93 | 284.47 | 257.01 | 289.55 | 292.09 | 294.63 | 297.17 | 299.71 | 302.25 |
| 12 | 304.79 | 307.33 | 309.87 | 312.41 | 314.9 .5 | 317.49 | 320.03 | 322.57 | 32.5 .11 | 327.65 |
| 13 | 330.19 | 332.73 | 335.27 | 337.81 | 340.35 | 342.89 | 345.43 | 347.97 | 350.51 | 353.05 |
| 14 | .355.59 | 358.13 | 360.67 | 363.21 | 365.75 | 368.29 | 370.83 | 373.37 | 375.91 | 378.45 |
| 15 | 380.99 | 383.53 | 386.07 | 358.61 | 391.15 | 393.69 | 396.23 | 398.77 | 401.31 | 403.85 |
| 16 | 406.39 | 408.93 | 411.47 | 414.01 | 416.55 | 419.09 | 421.63 | 424.17 | 426.71 | 429.25 |
| 17 | 431.79 | 434.33 | 436.87 | 439.41 | 441.95 | 444.49 | 447.03 | 449.57 | 452.11 | 454.65 |
| 18 | 457.19 | 459.73 | 462.27 | 464.81 | 467.35 | 469.89 | 472.13 | 474.97 | 477.51 | 400.05 |
| $\left\{\begin{array}{c} \text { English } \\ \text { Huches and } \\ \text { tenths } \end{array}\right.$ | Hundredths of an lach. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 19.0 | $\begin{aligned} & \text { Millim. } \\ & 482.59 \end{aligned}$ | $\begin{aligned} & \text { M1111m. } \\ & 482.85 \end{aligned}$ | $\begin{aligned} & \text { Millun. } \\ & 483.10 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 483.35 \end{aligned}$ | $\begin{aligned} & \text { Millim } \\ & 483.61 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 483.86 \end{aligned}$ | $\begin{aligned} & \text { Millim } \\ & \mathbf{4 5 4 . 1 2} \end{aligned}$ | $\begin{aligned} & \text { Minlim } \\ & 48+.37 \end{aligned}$ | $\begin{aligned} & \text { Millim } \\ & 184.62 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & +54.88 \end{aligned}$ |
| 1 | 485.13 | 485.39 | 48.5 .64 | 485.89 | 456.15 | 456.40 | 486.66 | 486.91 | 487.16 | 457.42 |
| 2 | 457.67 | 487.93 | 488.18 | 488.43 | 488.69 | 458.94 | 489.20 | 459.45 | 489.70 | 459.96 |
| 3 | 490.21 | 490.47 | 490.72 | 490.97 | 491.23 | 491.45 | 491.74 | 491.99 | 49.24 | 492.50 |
| 4 | 492.75 | 493.01 | 493.26 | 493.51 | 493.77 | 494.02 | 494.29 | 494.53 | 494.79 | 495.04 |
| 5 | 495.29 | 495.55 | 495.80 | 496.05 | 496.31 | 496.56 | 496.81 | 497.07 | 497.32 | 497.58 |
| 6 | 497.83 | 498.08 | 498.34 | 495.59 | 498.85 | 499.10 | 499.35 | 499.61 | 499.86 | 500.12 |
| 7 | 500.37 | 500.62 | 500.88 | 501.13 | 501.39 | 501.64 | 501.89 | 502.15 | 502.40 | 502.66 |
| 8 | 502.91 | 503.16 | 503.42 | 503.67 | 503.93 | 504.15 | 504.43 | 504.69 | 504.91 | 505.20 |
| 9 | 505.45 | 505.70 | 50596 | 506.21 | 506.47 | 506.72 | 505.97 | 507.23 | 507.45 | 507.74 |
| 20.0 | 507.99 | 505.24 | 508.50 | 508.75 | 509.01 | 509.26 | 509.51 | 509.77 | 510.02 | 510.28 |
| 1 | 510.53 | 510.78 | 511.04 | 511.29 | 511.55 | 511.80 | 512.05 | 512.31 | 512.56 | 512.82 |
| 2 | 513.07 | 513.32 | 513.58 | 513.83 | 514.09 | 514.34 | 514.59 | 514.85 | 515.10 | 515.36 |
| 3 | 515.61 | 515.86 | 516.12 | 516.37 | 516.63 | 516.88 | 517.13 | 517.39 | 517.64 | 517.90 |
| 4 | 518.15 | 518.40 | 518.66 | 518.91 | 519.17 | 519.42 | 519.67 | 519.93 | 520.18 | 520.44 |
| 5 | 520.69 | 520.94 | 521.20 | 521.4.5 | 521.71 | 521.96 | 522.21 | 522.47 | 522.72 | 522.98 |
| 6 | 523.23 | 523.48 | 523.74 | 523.99 | 524.2. | 524.50 | 521.75 | 525.01 | 525.26 | 32.5.\% 2 |
| 7 | 52.577 | 526.02 | 526.25 | 526.53 | 526.79 | 527.04 | 527.29 | 527.55 | 527.80 | 528.06 |
| 8 | 528.31 | 528.56 | 528.82 | 529.07 | 529.33 | 529.58 | 529.83 | 530.09 | 530.34 | 530.60 |
| 9 | 530.85 | 531.10 | 531.36 | 531.61 | 5:31.87 | 532.12 | 532.37 | 532.63 | 532.88 | 533.11 |

Thousandths of an foch.

| 0. | 1. | 2. | 3. | 4. | §. | 6. | 7. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0.03 | 0.05 | 0.08 | 0.10 | 0.13 | 0.15 | 0.18 | 0.20 | 0.23 |

C
11

| $\left\lvert\, \begin{gathered} \text { English } \\ \text { hiches athd } \\ \text { tenths. } \end{gathered}\right.$ | Hundredths of an lach. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 21.0 | $\begin{gathered} \text { Millim } \\ 533.39 \end{gathered}$ | $\begin{gathered} \text { Mıllim. } \\ 533.64 \end{gathered}$ | $\begin{gathered} \text { Mitlim } \\ 533.90 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 534.15 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 53.4 .41 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 534.66 \end{aligned}$ | $\begin{aligned} & \text { Mıllim. } \\ & 534.91 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 535.17 \end{aligned}$ | $\begin{aligned} & \text { M1lim. } \\ & 535.42 \end{aligned}$ | $\begin{gathered} \text { Milhm } \\ 53.5 .68 \end{gathered}$ |
| 1 | 535.93 | 536.18 | 536.44 | 5366.69 | 536.95 | 537.20 | 537.45 | 537.71 | 537.96 | 53822 |
| 2 | 538.47 | 538.72 | 538.98 | 539.23 | 5:39.19 | 539.74 | 539.99 | 540.25 | 540.50 | 54076 |
| 3 | 541.01 | 541.26 | 541.52 | 541.77 | 542.03 | 542.28 | 54253 | 542.79 | 543.04 | 543.30 |
| 4 | 543.55 | 543.80 | 544.06 | 24.4.31 | 544.57 | 544.82 | 545.07 | 545.33 | 545.58 | 545.84 |
| 5 | 546.09 | 546.34 | 546.60 | 546.85 | 517.11 | 547.36 | 547.61 | 547.87 | 548.12 | 518.38 |
| 6 | 548.63 | 548.88 | 549.14 | 549.39 | 519.65 | 549.90 | 550.15 | 550.41 | 550.66 | 550.92 |
| 7 | 551.17 | 5.31 .42 | 5.51 .68 | 5.51 .93 | 552.19 | 5.52 .4 | 5.52 .69 | 552.95 | 553.20 | 553.46 |
| 8 | 553.71 | 553.96 | 5.94 .22 | 554.47 | 554.73 | 554.98 | 555.23 | 55549 | 555.74 | 55600 |
| 9 | 556.25 | 556.50 | 556.76 | 557.01 | 557.27 | 557.52 | 557.77 | 558.03 | 558.28 | 558.54 |
| 29.0 | 558.79 | 559.04 | 559.30 | 559.55 | 559.81 | 560.06 | 560.31 | 560.57 | 560.82 | 561.08 |
| 1 | 561.33 | 561.58 | 561.84 | 562.09 | 562.35 | 56260 | 56.2 .85 | 563.11 | 563.36 | 563.62 |
| 2 | 563.57 | 564.12 | 564.38 | 564.63 | 564.89 | 565.14 | 56.5.39 | 56\%.65 | 565.90 | 566.16 |
| 3 | 566.41 | 566.66 | 566.92 | 567.17 | 567.43 | 567.68 | 567.93 | 568.19 | 568.44 | 568.70 |
| 4 | 568.95 | 569.20 | 569.46 | 569.71 | 569.97 | 570.22 | 570.47 | 570.73 | 570.98 | 571.24 |
| 5 | 571.49 | 571.74 | 572.00 | 572.25 | 572.51 | 572.76 | 573.01 | 573.27 | 573.52 | 573.78 |
| 6 | 574.03 | 574.28 | 574.54 | 574.79 | 575.05 | 575.30 | 575.55 | 575.81 | 576.06 | 576.32 |
| 7 | 576.57 | 576.82 | 577.08 | 57733 | 577.59 | 577.84 | 578.09 | 578.35 | 578.60 | 578.86 |
| 8 | 579.11 | 579.36 | 579.62 | 579.87 | 580.13 | 580.38 | 580.63 | 580.89 | 581.14 | 581.40 |
| 9 | 581.65 | 581.90 | 582.16 | 552.41 | 582.67 | 582.92 | 583.17 | 583.43 | 583.68 | 583.94 |
| 23.0 | 584.19 | 584.44 | 584.70 | 584.95 | 585.21 | 585.46 | 585.71 | 585.97 | 586.22 | 586.48 |
| 1 | 586.73 | 586.98 | 587.24 | 587.49 | 557.75 | 588.00 | 588.25 | 588.51 | 588.76 | 589.02 |
| 2 | 559.27 | 589.52 | 589.78 | 590.03 | 590.29 | 590.54 | 590.79 | 591.05 | 591.30 | 591..56 |
| 3 | 591.81 | 592.06 | 592.32 | 592.57 | 592.83 | 593.08 | 593.33 | 593.59 | 593.84 | 594.10 |
| 4 | 594.35 | 594.60 | 594.86 | 595.11 | 595.37 | 595.62 | 595.87 | 596.13 | 596.38 | 596.64 |
| 5 | 596.89 | 597.14 | 597.40 | 597.65 | 597.91 | 598.16 | 598.41 | 598.67 | 59892 | 599.18 |
| 6 | 599.43 | 599.68 | 599.94 | 600.19 | 600.45 | 600.70 | 600.95 | 601.21 | 601.46 | 601.72 |
| 7 | 601.97 | 602.22 | 602.48 | 602.73 | 602.99 | 60324 | 603.49 | 603.75 | 604.00 | 604.26 |
| 8 | 601.51 | 604.76 | 605.02 | 605.27 | 605.53 | 605.78 | 606.03 | 606.29 | 606.54 | 606.79 |
| 9 | 607.0.5 | 607.30 | 607.56 | 607.81 | 608.06 | 608.32 | 605.57 | 608.83 | 609.08 | 609.33 |
| 28.0 | 609.59 | 609.84 | 610.10 | 610.35 | 610.60 | 610.86 | 611.11 | 611.37 | 611.62 | 61187 |
| 1 | 612.13 | 612.38 | 61264 | 612.89 | 613.14 | 613.40 | 613.65 | 613.91 | 614.16 | 614.41 |
| 2 | 614.67 | 614.92 | 615.18 | 61543 | 615.68 | 615.9-4 | 616.19 | 616.45 | 616.70 | 616.9. |
| 3 | 617.21 | 617.46 | 617.72 | 617.97 | 618.22 | 618.48 | 618.73 | 618.99 | 619.24 | 619.49 |
| 4 | 619.75 | 620.00 | 620.26 | 620.51 | 620.76 | 621.02 | 621.27 | 621.53 | 621.78 | 622.03 |
|  |  |  |  | Thnusa | ndths of | n Inch. |  |  |  |  |
| O. | 1. | 2. | 3. | 4. | ) |  | 6. | 7. | 8. | 9. |
| 0.0 | 0.03 | 0.05 | 0.08 | 0.10 | 0.1 |  | . 15 | 0.18 | 0.20 | 0.23 |


| English fuchers and tenths. | Hundredths of an Inc h. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 24.5 | $\begin{aligned} & \text { Millim } \\ & 622.29 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 622.54 \end{aligned}$ | $\begin{aligned} & \text { Millim } \\ & 622.80 \end{aligned}$ | $\begin{aligned} & \text { Millim } \\ & 623.05 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 623.30 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 623.56 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 623.81 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 624.07 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 624.32 \end{aligned}$ | $\begin{aligned} & \text { Lillim. } \\ & 624.57 \end{aligned}$ |
| 6 | 624.83 | 625.08 | 625.34 | 625.59 | 625.84 | 626.10 | 626.35 | 626.61 | 626.86 | 627.11 |
| 7 | 627.37 | 627.62 | 627.88 | 628.13 | 628.38 | 628.64 | 628.59 | 629.15 | 629.40 | 629.65 |
| 8 | 629.91 | 630.16 | 630.12 | 630.67 | 630.92 | 631.15 | 631.43 | 631.69 | 631.94 | $632.1)$ |
| 9 | 632.15 | 632.70 | 632.96 | 633.21 | 633.46 | 633.72 | 633.97 | 634.23 | 634.48 | 634.73 |
| 25.0 | 634.99 | 635.24 | 635.50 | 637.75 | 636.00 | 636.26 | 636.51 | 636.77 | 637.02 | 637.27 |
| 1 | 637.53 | 637.78 | 638.04 | 638.29 | 638.54 | 038.50 | 639.05 | 639.31 | 639.56 | 639.81 |
| 2 | 640.07 | 640.32 | 640.58 | 640.83 | 641.08 | 641.34 | 641.59 | 641.85 | 642.10 | 642.35 |
| 3 | 642.61 | 642.86 | 643.12 | 643.37 | 643.62 | 643.85 | 644.13 | 644.39 | 644.64 | 614.89 |
| 4 | 645.15 | 645.40 | 645.66 | 645.91 | 646.16 | 616.42 | 646.67 | 616.93 | 647.18 | 647.43 |
| 5 | 647.69 | 617.94 | 648.20 | 648.45 | 648.70 | 618.96 | 619.21 | 649.47 | 649.72 | 649.97 |
| 6 | 650.23 | 6.50 .48 | 650.74 | 6.50 .99 | 651.24 | 651.50 | 651.75 | 652.01 | 652.26 | 6.52 .51 |
| 7 | 652.77 | 653.02 | 6.33 .28 | 653.53 | 653.78 | 651.04 | 6.54 .29 | 654.55 | 65.4 .80 | 655.05 |
| 8 | 6.55 .31 | 6.55 .56 | 655.82 | 6.56 .07 | 6.56 .32 | 6.56 .55 | 656.83 | 657.09 | 657.34 | 657.59 |
| 9 | 657.85 | 658.10 | 658.36 | 658.61 | 658.56 | 6.59 .12 | 659.37 | 659.63 | 659.88 | 660.13 |
| 26.0 | 660.39 | 660.64 | 660.90 | 661.15 | 661.40 | 661.66 | 661.91 | 662.17 | 662.42 | 66267 |
| 1 | 662.93 | 663.18 | 663.41 | 663.69 | 663.94 | 664.20 | 664.45 | 664.71 | 664.96 | 665.21 |
| 2 | 665.17 | 665.72 | 66.5 .98 | 666.23 | 666.48 | 666.74 | 666.99 | 667.25 | 667.50 | 667.7. |
| 3 | 668.01 | 668.26 | 665.52 | 665.77 | 669.02 | 669.28 | 669.53 | 669.79 | 670.04 | 670.29 |
| 4 | 670.55 | $670 \cdot 80$ | 671.06 | 671.31 | 671.56 | 671.82 | 672.07 | 672.33 | 672.58 | 672.83 |
| 5 | 67309 | 673.34 | 673.60 | 673.85 | 674.10 | 674.36 | 674.61 | 674.87 | 675.12 | 67537 |
| 6 | 675.63 | 675.88 | 676.14 | 676.39 | 676.64 | 676.90 | 677.15 | 677.41 | 677.66 | 677.91 |
| 7 | 678.17 | 678.12 | 678.68 | 678.93 | 679.18 | 679.44 | 679.69 | 679.93 | 680.20 | 680.45 |
| 8 | 680.71 | 680.96 | 681.22 | 651.47 | 681.72 | 681.98 | 652.23 | 68249 | 68.74 | 682.93 |
| 9 | 653.25 | 683.50 | 683.76 | 684.01 | 654.26 | 684.52 | 684.77 | 685.03 | 685.28 | 685.53 |
| 27.0 | 68.5 .79 | 686.04 | 686.30 | 656.55 | 686.80 | 697.06 | 687.31 | 687.57 | 657.82 | 68807 |
| 1 | 653.33 | 688.55 | 688.54 | 69909 | 659.34 | 659.60 | 689.85 | 690.11 | 690.36 | 690.61 |
| 2 | 690.87 | 691.12 | 691.38 | 691.63 | 691.88 | 692.14 | 692.39 | 692.65 | 692.90 | 693.15 |
| 3 | 693.11 | 693.66 | 693.92 | 694.17 | 694.42 | 694.65 | 694.93 | 695.19 | 69.3 .44 | 69.3.69 |
| 4 | 695.95 | 696.20 | 696.46 | 696.71 | 696.96 | 697.22 | 697.47 | 697.73 | 697.98 | 698.23 |
| 5 | 698.49 | 698.74 | 699.00 | 699.25 | 699.50 | 699.76 | 700.01 | 700.27 | 700.52 | 700.77 |
| 6 | 701.03 | 701.25 | 701.54 | 701.79 | 702.04 | 702.30 | 702.55 | 702.81 | 703.06 | 703.31 |
| 7 | 705.57 | 703.82 | 704.08 | 704.33 | 704.58 | 704.84 | 705.09 | 705.35 | 705.60 | 70.85 |
| 8 | 706.11 | 706.36 | 706.62 | 706.57 | 707.12 | 707.38 | 707.63 | 707.89 | 708.14 | 705.39 |
| 9 | 708.65 | 708.90 | 709.16 | 709.41 | 709.66 | 709.92 | 710.17 | 710.43 | 710.68 | 710.93 |
|  |  |  |  | Thou | sandths of | an Inch. |  |  |  |  |
| 0. | 1. | 2. | 3. |  |  | 5. | 6. | 7. | 8. | 9. |
| 0.0 | 0.03 | 0.05 | 0.08 |  |  | 13 | 0.15 | 0.18 | 0.20 | 0.23 |

C


1 English Inch $=11.2595$ French or Paris Lines.

| English Inches. | Tenths of an Inch. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| 11 | Par lines. 123.85 | Par.lines. | Par.lines. | Par.lines. 127.23 | Par.lines. 1.23.36 | Par lines. <br> 129. | Yar.lines, 130.61 | Par.liues. | Par.lines. | Par.lines. |
| 11 |  | 124.98 | 126.11 | 127.23 | 123.36 | 129.45 | 130.61 | 131.74 | 132.56 | 133.99 |
| 12 | 13.5.11 | 136.24 | 137.37 | 138.49 | 139.62 | 140.74 | 141.87 | 143.00 | 144.12 | 145.25 |
| 13 | 146.37 | 147.50 | 148.63 | 149.75 | 150.88 | 152.00 | 153.13 | 154.26 | 1.5 .5 .35 | 156.51 |
| 14 | 157.63 | 158.76 | 159.88 | 161.01 | 162.14 | 163.26 | 164.39 | 165.51 | 166.61 | 167.77 |
| 15 | 163.59 | 170.02 | 171.14 | 172.27 | 17340 | 174.52 | 175.65 | 176.77 | 177.90 | 179.03 |
| 16 | 150.15 | 181.28 | 182.40 | 183.53 | 184.66 | 185.78 | 186.91 | 185.03 | 189.16 | 190.29 |
| Hundredths of an Inch. |  |  |  |  |  |  |  |  |  |  |
| 0. | 1. | 2. | 3. | 4. |  |  | 6. | 7. | 8. | 9. |
| 0.000 | 0.113 | 0.22. | 0.338 | 0. | 0 0. | 563 | . 676 | 0.788 | 0.901 | 1.013 |
| $\begin{array}{\|c\|} \text { English } \\ \text { Inches and } \\ \text { Tenths. } \end{array}$ | Ifundredths of an Inch. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. |  | 5. | 6. | 7. | 8. | 9. |
| 17.0 | Par.lines. <br> 191.41 | Par.lines 191.52 | Par.lines. | Par.lines. 191.75 | Par.lines 191.86 | Par lines. <br> 19197 | Par.lines. 192.09 | Par-lines. | Par.lines. <br> 192.31 | Par.lines. |
| 1 | 192.54 | 192.6.5 | 192.76 | 192.85 | 192.99 | 193.10 | 193.21 | 193.33 | 193.44 | 193.5. 5 |
| 2 | 193.66 | 193.78 | 193.89 | 191.00 | 194.11 | 194.23 | 194.3 t | 194.45 | 194.56 | 194.68 |
| 3 | 194.79 | 194.90 | 195.01 | 195.13 | 195.24 | 195.35 | 195.46 | 19.5 .58 | 195.69 | 195.80 |
| 4 | 195.92 | 196.03 | 196.14 | 196.25 | 196.37 | 196.18 | 196.59 | 196.70 | 196.52 | 196.93 |
| 5 | 197.04 | 197.15 | 197.27 | 197.35 | 197.49 | 197.60 | 197.72 | 197.83 | 197.94 | 198.0.3 |
| 6 | 193.17 | 198.28 | 198.39 | 198.50 | 198.62 | 198.73 | 198.84 | 198.96 | 199.07 | 199.18 |
| 7 | 199.29 | 199.41 | 199.52 | 199.63 | 199.74 | 199.86 | 199.97 | 200.08 | 200.19 | 200.31 |
| 8 | 200.42 | 200.53 | 200.64 | 200.76 | 200.57 | 200.98 | 201.09 | 201.21 | 201.32 | 201.43 |
| 9 | 201.55 | 201.66 | 201.77 | 201.88 | 202.00 | 202.11 | 202.22 | 202.33 | 202.45 | 202.56 |
| 18.0 | 202.67 | 202.78 | 202.90 | 203.01 | 203.12 | 203.23 | 203.35 | 203.46 | 203.57 | 203.68 |
| 1 | 203.80 | 203.91 | 204.02 | 204.13 | 204.2 .5 | 204.36 | 204.47 | 204.59 | 204.70 | 204.51 |
| 2 | 201.92 | 205.04 | 20.7.15 | 205.26 | 205.37 | 205.49 | 20.5.60 | 20.5.71 | 20.5. 82 | 20.5.94 |
| 3 | 206.0.5 | 206.16 | 206.27 | 206.39 | 206.50 | 206.61 | 206.72 | 206.84 | 206.95 | 207.06 |
| 4 | 207.17 | 207.29 | 207.40 | 207.51 | 207.63 | 207.74 | 207.85 | 207.96 | 205.05 | 208.19 |
| 5 | 208.30 | 208.41 | 208.53 | 208.64 | 208.75 | 203.86 | 208.98 | 209.09 | 209.20 | 209.31 |
| 6 | 209.43 | 209.54 | 209.65 | 209.76 | 209.58 | 209.99 | 210.10 | 210.21 | 210.33 | 210.44 |
| 7 | 210.55 | 210.67 | 210.78 | 210.89 | 211.00 | 211.12 | 211.23 | 211.34 | 211.45 | 211.57 |
| 8 | 211.65 | 211.79 | 211.90 | 212.02 | 212.13 | 212.24 | 212.35 | 212.47 | 212.58 | 212.69 |
| 9 | 212.80 | 212.92 | 213.03 | 213.14 | 213.25 | 213.37 | 213.48 | 213.59 | 213.71 | 213.82 |
| 19.0 | 213.93 | 214.04 | 214.16 | 214.27 | 214.35 | 214.49 | 214.61 | 214.72 | 214.83 | 214.94 |
| 1 | 215.06 | 21.5 .17 | 215.28 | 215.39 | 215.51 | 215.62 | 215.73 | 215.54 | 215.96 | 216.07 |
| 2 | 216.18 | 216.29 | 216.41 | 216.52 | 216.63 | 216.75 | 216.86 | 216.97 | 217.08 | 217.20 |
| 3 | 217.31 | 217.42 | 217.53 | 217.65 | 217.76 | 217.57 | 217.98 | 218.10 | 218.21 | 218.32 |
| 4 | 218.43 | 218.55 | 218.66 | 218.77 | 218.88 | 219.00 | 219.11 | 219.22 | 219.34 | 219.45 |
| 5 | 219.56 | 219.67 | 219.79 | 219.90 | 220.01 | 220.12 | 220.24 | 220.35 | 220.46 | 220.57 |
| 6 | 220.69 | 220.80 | 220.91 | 221.02 | 221.14 | 221.25 | 221.36 | 221.47 | 221.59 | 221.70 |
| 7 | 221.81 | 221.92 | 22.24 | 222.15 | 222.26 | 222.35 | 222.49 | 222.60 | 222.71 | 222.83 |
| 8 | 222.94 | 223.0.5 | 223.16 | 223.28 | 223.39 | 223.50 | 223.61 | 223.73 | 223.84 | 223.95 |
| 9 | 224.06 | 224.18 | 224.29 | $2 \cdot 4.40$ | 224.51 | 224.63 | 224.74 | 221.85 | 224.96 | 225.08 |

1 English Inch $=11.2595$ French or Paris Lines.


1 English Inch $=11.2595$ French or Paris Lines.

| EuglishInches andTenths. | Ifundredths of an Inch. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\theta$. | 1. | 2. | 3. | 4. | 5. | 6. | 7 | 8. | P. |
|  | Par.lines. | Par.lines. | Par.lines. | Par lines. | Parlines. | Par.tines. | Par.lines | Par.lines | Par.lines. | Par.lines. |
| 21.0 | 270.23 | 270.34 | 270.45 | 270.57 | 270.68 | 270.79 | 270.90 | 271.02 | 271.13 | 271.24 |
| 1 | 271.35 | 271.47 | 271.58 | 271.69 | 271.80 | 271.92 | 272.03 | 27.14 | 272.25 | 272.37 |
| 2 | 272.15 | 272.59 | 272.71 | 272.82 | 272.93 | 273.04 | 273.16 | 273.27 | 273.35 | 273.49 |
| 3 | 273.61 | 273.72 | 273.83 | 273.94 | 274.06 | 274.17 | 274.28 | 274.39 | 274.51 | 274.62 |
| 4 | 271.73 | 274.84 | 274.96 | 275.07 | 275.18 | 275.29 | 275.41 | 275.52 | 275.63 | 275.75 |
| 5 | 275.86 | 275.97 | 276.08 | 276.20 | 276.31 | 276.42 | 276.53 | 276.65 | 276.76 | 276.87 |
| 6 | 276.93 | 277.10 | 277.21 | 277.32 | 277.43 | 277.55 | 277.66 | 277.77 | 277.5 | 27ヶ.00 |
| 7 | 278.11 | 278.22 | 278.33 | 278.45 | 278.56 | 278.67 | 275.79 | 278.90 | 279.91 | 279.12 |
| S | 279.24 | 279.35 | 279.46 | 279.57 | 279.69 | 279.50 | 279.91 | 280.02 | 200.14 | 250.2.; |
| 9 | 280.36 | 280.47 | 280.59 | 250.70 | 280.81 | 280.92 | 281.04 | 281.15 | 281.26 | 251.35 |
| 25.0 | 281.19 | 281.60 | 281.71 | 281.83 | 281.91 | 282.05 | 282.16 | 282.28 | 282.39 | 282.50 |
| 1 | 28.61 | 282.73 | 252.54 | 282.95 | 283.06 | 283.18 | 283.29 | 283. 40 | 253.51 | 283.63 |
| 2 | 283.74 | 283.85 | 283.96 | 234.08 | 284.19 | 284.30 | 28.4 .4 | 284.53 | 254.64 | 284.75 |
| 3 | 254.87 | 284.98 | 285.09 | 285.20 | 285.32 | 285.13 | 285.54 | 285.6.5 | 285.77 | 285.08 |
| 4 | 285.99 | 286.10 | 286.22 | 286.33 | 286.44 | 286.55 | 286.67 | 256.78 | 286.59 | 287.00 |
| 5 | 287.12 | 287.23 | 257.34 | 287.46 | 287.57 | 287.68 | 257.79 | 287.91 | 298.02 | 288.13 |
| 6 | 2-5.24 | 288.36 | 288.47 | 288.58 | 288.69 | 288.81 | 288.92 | 2-9.03 | 289.14 | 289.26 |
| 7 | 289.37 | 289.48 | 289.59 | 289.71 | 289.82 | 289.93 | 290.04 | 290.16 | 290.27 | 290.38 |
| 8 | 290.50 | 290.61 | 290.72 | 290.83 | 290.9. | 291.06 | 291.17 | 291.28 | 291.40 | 291.51 |
| 9 | 291.62 | 291.73 | 291.85 | 291.96 | 292.07 | 292.18 | 292.30 | 292.41 | 292.52 | 292.63 |
| 26.0 | 292.75 | 29.26 | 29.97 | 293.08 | 293.20 | 293.31 | 293.42 | 293.54 | 293.65 | 293.76 |
| 1 | 293.87 | 293.99 | $29+10$ | 294.21 | 294.32 | 294.44 | 294.55 | 294.66 | 294.77 | 294.89 |
| 2 | 293.00 | 295.11 | 295.22 | 295.34 | 295.45 | 29.5.56 | 295.67 | 295.79 | 29.5 .90 | 296.01 |
| 3 | 296.12 | 296.24 | 296.3.) | 296.16 | 296.58 | 296.69 | 296.80 | 296.91 | 297.03 | 297.14 |
| 4 | 297.25 | 297.36 | 297.48 | 297.59 | 297.70 | 297.81 | 297.93 | 298.04 | 298.15 | 298.26 |
| 5 | 295.38 | 298.49 | 298.60 | 298.71 | 298.83 | 298.94 | 299.05 | 299.17 | 299.28 | 299.39 |
| 6 | 299.50 | 299.62 | 299.73 | 299.84 | 299.95 | 300.07 | 300.15 | 300.29 | 300.10 | 300.52 |
| 7 | 300.63 | 300.74 | 300.85 | 300.97 | 301.08 | 301.19 | 301.30 | 301.42 | 301.53 | 301.64 |
| 8 | 30175 | 301.87 | 301.98 | 302.09 | 302.20 | 302.32 | 302.43 | 302.54 | 302.66 | 302.77 |
| 9 | 302.88 | 302.99 | 303.11 | 303.22 | 303.33 | 303.44 | 303.56 | 303.67 | 303.78 | 303.59 |
| 27.0 | 304.01 | 304.12 | 304.23 | 304.34 | 304.46 | 304.57 | 304.68 | 304.79 | 304.91 | 305.02 |
| 1 | 30.3.13 | 305.25 | 305.36 | 305.47 | 305.58 | 305.70 | 305.81 | 305.92 | 306.03 | 306.15 |
| 2 | 306.26 | 306.37 | 306.45 | 306.60 | 306.71 | 306.52 | 306.93 | 307.05 | 307.16 | 307.27 |
| 3 | 307.38 | 307.50 | 307.61 | 307.72 | 307.83 | 307.95 | 305.06 | 308.17 | 308.29 | 308.10 |
| 4 | 308.51 | 308.62 | 308.74 | 308.85 | 308.96 | 309.07 | 309.19 | 309.30 | 309.41 | 309.52 |
| 5 | 309.64 | 309.75 | 309.86 | 309.97 | 310.09 | 310.20 | 310.31 | 310.42 | 310.54 | 310.65 |
| 6 | 310.76 | 310.87 | 310.99 | 311.10 | 311.21 | 311.33 | 311.44 | 311.55 | 311.66 | 311.78 |
| 7 | 311.89 | 312.00 | 312.11 | 312.23 | 312.34 | 312.45 | 312.56 | 312.68 | 312.79 | 312.90 |
| 8 | 313.01 | 313.13 | 313.24 | 313.35 | 313.46 | 313.58 | 313.69 | 313.60 | 313.91 | 314.03 |
| 9 | 314.14 | 314.25 | 314.37 | 314.48 | 314.59 | 314.70 | 314.82 | 314.93 | 315.04 | 315.15 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1 English Inch $=11.2595$ French or Paris Lines.

| English Inches and Tenths. | Hundredths of an Iuch. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | Э. |
|  | Par.lines. | Par.lines. | Par.lines. | Par lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. |
| 28.0 | 315.27 | 315.38 | 315.49 | 315.60 | 315.72 | 315.53 | 315.94 | 316.05 | 316.17 | 316.28 |
| 1 | 316.39 | 316.50 | 316.62 | 316.73 | 316.54 | 316.95 | 317.07 | 317.18 | 317.29 | 317.41 |
| 2 | 317.52 | 317.63 | 317.74 | 317.86 | 317.97 | 318.08 | 318.19 | 318.31 | 318.42 | 318.53 |
| 3 | 318.64 | 318.76 | 318.87 | 318.98 | 319.09 | 319.21 | 319.32 | 319.43 | 319.54 | 319.66 |
| 4 | 319.77 | 319.88 | 319.99 | 320.11 | 320.22 | 320.33 | 320.45 | 320.56 | 320.67 | 3.30 .78 |
| 5 | 320.90 | 321.01 | 321.12 | 321.23 | 321.35 | 321.46 | 321.57 | 321.65 | 321.80 | 321.91 |
| 6 | 322.02 | 322.13 | 322.25 | 322.36 | 322.47 | 322.58 | 322.70 | 322.81 | 322.92 | 323.04 |
| 7 | 323.15 | 323.26 | 323.37 | 323.49 | 323.60 | 323.71 | 323.52 | 323.94 | 324.05 | 324.16 |
| 8 | 324.27 | 324.39 | 3.4 .50 | 324.61 | 324.72 | 324.84 | 324.95 | 325.06 | 325.17 | 325.29 |
| 9 | 325.40 | 325.51 | 325.62 | 325.74 | 325.85 | 325.96 | 326.08 | 326.19 | 326.30 | 326.41 |
| 29.0 | 326.53 | 326.64 | 326.75 | 326.56 | 326.98 | 327.09 | 327.20 | 327.31 | 327.43 | 327.54 |
| 1 | 327.6 .5 | 327.76 | 327.88 | 327.99 | 325.10 | 328.21 | 328.33 | 328.44 | 328.55 | 328.66 |
| 2 | 328.75 | 328.89 | 329.00 | 329.12 | 329.23 | 329.34 | 329.45 | 329.57 | 329.68 | 329.79 |
| 3 | 329.90 | 330.02 | 330.13 | 330.24 | 330.35 | 330.47 | 330.58 | 330.69 | 330.80 | 330.92 |
| 4 | 331.03 | 331.14 | 331.25 | 331.37 | 331.45 | 331.59 | 331.70 | 331.82 | 331.93 | 332.04 |
| 5 | 332.16 | 332.27 | 332.38 | 332.49 | 332.61 | 332.72 | 332.83 | 332.94 | 333.06 | 333.17 |
| 6 | 333.28 | 333.39 | 333.51 | 333.62 | 333.73 | 333.54 | 333.96 | 334.07 | 33-1.18 | 331.29 |
| 7 | 334.41 | 334.52 | 334.63 | 334.74 | 334.86 | 334.97 | 335.08 | 335.20 | 335.31 | 335.42 |
| 8 | 335.53 | 335.65 | 335.76 | 335.87 | 335.98 | 336.10 | 336.21 | 336.32 | 336.43 | 336.55 |
| 9 | 336.66 | 336.77 | 336.88 | 337.00 | 337.11 | 337.28 | 337.33 | 337.45 | 337.56 | 337.67 |
| 30.0 | 337.78 | 337.90 | 335.01 | 338.12 | 338.24 | 338.35 | 338.46 | 338.57 | 338.69 | 338.80 |
| 1 | 338.91 | 339.02 | 389.14 | 339.25 | 339.36 | 339.47 | 339.59 | 339.70 | 339.51 | 339.92 |
| 2 | 310.04 | 340.15 | 340.26 | 340.37 | 340.49 | 340.60 | 340.71 | 340.83 | 340.94 | 341.05 |
| 3 | 341.16 | 341.28 | 341.39 | 341.50 | 341.61 | 341.73 | 341.84 | 341.95 | 342.06 | 342.18 |
| 4 | 342.29 | 342.40 | 342.51 | 342.63 | 342.74 | 342.85 | 342.96 | 343.08 | 343.19 | 343.30 |
| 5 | 343.41 | 343.53 | 343.64 | 343.75 | 343.87 | 313.98 | 344.09 | 344.30 | 344.32 | 344.43 |
| 6 | 344.54 | 344.6. | 314.77 | 344.88 | 344.39 | 345.10 | 34.5 .22 | 345.33 | 345.44 | 345.55 |
| 7 | 345.67 | 345.78 | 345.89 | 346.00 | 346.12 | 346.23 | $3+6.34$ | 346.45 | 346.57 | 346.68 |
| 8 | 346.79 | 316.91 | $3+7.02$ | 347.13 | 347.24 | 347.36 | 347.47 | 347.58 | 347.69 | 347.81 |
| 9 | 347.92 | 348.03 | 348.14 | 348.26 | 348.37 | 318.18 | 348.59 | 348.71 | 348.82 | 348.93 |
| 31.0 | 349.04 | 349.16 | 349.27 | 349.38 | 349.49 | 349.61 | 349.72 | 349.53 | 349.95 | 350.06 |
| 1 | 350.17 | 350.28 | 350.40 | 350.51 | 350.62 | 350.73 | 350.85 | 350.96 | 351.07 | 351.18 |
| 2 | 351.30 | 3.51 .41 | 351.52 | 351.63 | 351.75 | 351.86 | 351.97 | 352.08 | 352.20 | 352.31 |
| 3 | 352.42 | 352.53 | 352.65 | 3.52 .76 | 352.87 | 3.52 .99 | 353.10 | 353.21 | 353.32 | 353.44 |
| 4 | 353.55 | 353.66 | 353.77 | 353.89 | 354.00 | 3.54 .11 | 354.22 | 354.34 | 354.45 | 354.56 |
| 5 | 354.67 | 354.79 | 354.90 | 355.01 | 355.12 | 35.5 .24 | : 55.35 | 355.46 | 355.57 | 355.69 |
| 6 | 3.5.5.80 | 355.91 | 356.03 | 356.14 | 356.25 | 356.36 | $\because 56.48$ | 356.59 | 356.70 | 356.81 |

Thousandths of an Inch.

| 0. | 1. | 9. | 3. | 4. | 5. | 6. | 7. | 8. | 3. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 0.011 | 0.023 | 0.034 | 0.045 | 0.056 | 0.068 | 0.079 | 0.090 | 0.101 |

III. - IV.

## C0MPARIS0N

of

## TIIE METRICAL BAROMETER

WITII

TIIE ENGLISH AND TIIE OLD FRENCH BAROMETERS,
or

TABLES

FOR CONVERTING MILLIMETREA INTO ENGLISII INCIIEA AND DECIMALS, AND INTG FRENCH OR PARIS LINES;

GIVING THE VALUES CORRESDONDING TO EVERY MLLLDETRE FROM 250 TO 600; AND TO EVERY TENTII OF A MLLIMETRE FROH 600 TO 800 MLLLMETRES.

C

1 Metre $=39.37079$ English Inches.


Tenths of Millimetres.

| 0. | 1. | 2. | 3. | 4. | す. | 6. | \%. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 0.004 | 0.005 | 0.012 | 0.016 | 0.020 | 0.024 | 0.028 | 0.031 | 0.035 |

1 Metre $=39.37079$ English Inches.

| Millime-tres | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eur In. | Eug. In. | Eng. In. | Eng In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 600 | 23.622 | 23.626 | 28.6830 | 23.634 | 23.635 | 23.642 | 23.646 | 23.650 | 23.654 | 23.658 |
| 601 | 23.662 | 23.666 | 23.670 | 23.674 | 23.678 | 23.652 | 23.685 | 23.659 | 23.693 | 23.697 |
| 60.2 | 23.701 | 23.705 | 23.709 | 23.713 | 23.717 | 23.721 | 23.725 | 23.729 | 23.733 | 23.737 |
| 693 | 23.741 | 23.745 | 23.745 | 23.752 | 23.756 | 23.760 | 23.764 | 23.768 | 23.772 | 23.776 |
| 604 | 23.780 | 23.784 | 23.755 | 23.792 | 23.796 | 23.500 | 23.804 | 23.808 | 23.811 | 23.815 |
| 60.5 | 23.519 | 23.823 | 23.527 | 23.831 | 23.835 | 23.639 | 23.843 | 23.847 | 23.851 | 23.555 |
| 606 | 23.5.59 | 23.863 | 23.867 | 23.871 | 23.97: | 23.675 | 23.852 | 23.886 | 23.590 | 23.894 |
| 607 | 23.898 | 23.902 | 23.906 | 23.910 | 23.914 | 23.915 | 23.922 | 23.926 | 23.930 | 23.934 |
| 608 | 23.937 | 23.941 | 23.945 | 23.949 | 23.953 | 23.957 | 23.961 | 23.965 | 23.969 | 23.973 |
| 609 | 23.977 | 23.951 | 23.985 | 23.959 | 23.993 | 23.996 | 24.000 | 24.004 | 24.008 | 24.012 |
| 610 | 24.016 | 24.020 | 24.024 | 24.028 | 24.032 | 24.036 | 24.010 | 24.044 | 24.048 | 24.052 |
| 611 | 24.056 | 24.0 .59 | 24.06 : | 24.067 | 24.071 | 21.075 | 24.079 | 24.083 | 24.057 | 24.091 |
| 612 | 24.09 .5 | 24.099 | 24.103 | 24.107 | 24.111 | 24.115 | 24.119 | 24.123 | 24.126 | 24.130 |
| 613 | 24.134 | 21.188 | 24.142 | 24.146 | 24.150 | 24.154 | 24.158 | 24.162 | 24.166 | 24.170 |
| 614 | 24.174 | 24.175 | 24.182 | 24.18 .5 | 24.189 | 24.193 | 24.197 | 24.201 | 24.205 | 24.209 |
| 615 | 24.213 | 24.217 | 24.221 | 24.22. | 24.229 | 24.238 | 24.237 | 24.241 | 24.245 | 24.248 |
| 616 | 24.252 | 24.256 | 21.260 | 24.264 | 24.265 | 21.272 | 24.276 | 24.280 | 24.284 | 24.288 |
| 617 | 24.292 | 24.296 | 24.300 | 24.304 | 24.305 | 24.311 | 24.315 | 24.319 | 24.323 | 24.327 |
| 615 | 24.331 | 24.335 | 24.339 | 24.343 | 24.347 | 24.3.51 | 24.355 | 24.359 | 24.363 | 24.367 |
| $619{ }^{\prime}$ | 24.371 | 24.374 | 24.378 | 24.382 | 24.386 | 24.390 | 24.394 | 24.398 | 24.402 | 24.406 |
| 620 | 24.110 | 24.414 | 24.418 | 24.422 | 24.426 | 24.430 | 24.434 | 24.437 | 24.441 | 24.445 |
| 621 | 24.449 | 24.4 .53 | 24.457 | 24.461 | 24.46 .5 | 24.169 | 24.473 | 24.177 | 21.481 | 24.485 |
| 622 | 24.459 | 24.493 | 24.497 | 24.500 | 24.504 | 24.50 S | 24.512 | 24.516 | 24.520 | 24.524 |
| 623 | 24.528 | 24.532 | 24.536 | 24.510 | 24.54 | 24.518 | 24.552 | 24.5 .56 | 24.559 | 24.563 |
| 624 | 24.567 | 24.571 | 24.575 | 24.579 | 24.583 | 24.587 | 24.591 | 24.595 | 24.509 | 24.503 |
| 6.25 | 24.607 | 24.611 | 24.615 | 24.619 | 24.622 | 24.626 | 24.630 | 24.634 | 24.638 | 24.642 |
| 626 | 24.616 | $2+.6 .50$ | 24.6 .54 | 24.6.55 | 24.669 | $\underline{2} 4.666$ | 24.670 | 21.674 | 24.678 | 24.682 |
| 627 | 24.695 | 24.659 | 24.693 | 24.697 | 24.701 | 24.70 .5 | 24.709 | 24.713 | 24.717 | 24.721 |
| 6. 25 | 24.72 .5 | 21.729 | 24.733 | 21.737 | 24.711 | 24.745 | 24.745 | 24.752 | 24.756 | 24.760 |
| 629 | 21.764 | 24.768 | 24.752 | 24.776 | 24.780 | 24.754 | 24.788 | 24.792 | 24.796 | 24.800 |
| 6.30 | 24.504 | 24.908 | 24.811 | 24.815 | 21.819 | 24.823 | 24.527 | 24.831 | 21.835 | 24.839 |
| 631 | $24.84 ;$ | 24.847 | 24.851 | 21.855 | 24.859 | 24.863 | 24.867 | 24.571 | 24.874 | 24.878 |
| 632 | 24.882 | 24.586 | 24.890 | 24.894 | 24.898 | 24.902 | 24.906 | 21.910 | 24.914 | 24.918 |
| 633 | 24.922 | 24.926 | 24.930 | 24.93 t | 24.937 | $24.9+1$ | 24.945 | 24.949 | 24.9.): | 24.957 |
| $6: 9$ | 24.961 | 24.96 .5 | 24.969 | $24.9 \% 3$ | 24.977 | 24.981 | 24.98 .5 | 24.989 | 24.993 | 24.997 |
| 63.5 | 2.5 .000 | 25.004 | 25.005 | 25.012 | 2.5 .016 | 25.020 | 25.024 | 25.028 | 25.032 | 25.036 |
| 636 | 25.040 | 2.5 .014 | 25.048 | 25.052 | 25.0.56 | 25.060 | 25.063 | 25.067 | 2.5 .071 | 25.075 |
| 63\% | 2.5 .079 | 25.083 | 2.5 .027 | 2.5 .091 | 25.09.5 | 25.099 | 25.103 | 25.107 | 25.111 | 25.115 |
| 635 | 2.5 .119 | 25.123 | 2.5.126 | 25.130 | 25.134 | 25.138 | 25.142 | 25.146 | 25.150 | 25.154 |
| 639 | 25.1.5 | 2.5 .162 | 2.5 .166 | 25.170 | 2.5 .174 | 2.5 .178 | 25.182 | 25.185 | 25.189 | 25.193 |
|  | 0. | 1. | 2. | 3. | 4 | 5 | 6. | 7. | 8. | D. |

1 Metre $=39.37079$ English Inches

|  | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3 | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eag. In. | Eng. In. | Eng. In. | Evg. In | Eng Ja. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | n. |
| 640 | 25.197 | 25.201 | 25.205 | 2.209 | 25.213 | 25.217 | 2.5.221 | 25.22 .5 | 2.5 .299 | 2.5.23:3 |
| 641 | 25.237 | 25.241 | 25.245 | 25.245 | 25.252 | 2.5256 | 25.260 | 25.261 | 25.268 | 25.272 |
| 642 | 25.276 | 25.280 | 25.284 | 25.288 | 25.292 | 25.296 | 25.300 | 25.30 .1 | 25.308 | 25.311 |
| 643 | 25.315 | 2.5 .319 | 25.323 | 25.327 | 25.3331 | 25.335 | 25.3:39 | 25.348 | 2.5 .347 | 2.5 .351 |
| 644 | 2.5 .355 | 25.359 | 25.363 | 2.5 .367 | 25.371 | 25.374 | 25.375 | 25.382 | 25.386 | 25.390 |
| 645 | 25.394 | 25.398 | 25.402 | 25.406 | 25.410 | 25.414 | 25.418 | 25.422 | 25.426 | 2.5. 130 |
| 646 | 2.543 .1 | 25.437 | 25.441 | 2.5 .445 | 25.449 | 25.453 | 25.457 | 25.161 | 2.5.46.5 | 2.5 .469 |
| 647 | 25.473 | 2.5.177 | 25.481 | 2.5 .18 .5 | 2.5 .489 | 25493 | 25.497 | 25.500 | 25.504 | 25.508 |
| 648 | 25.512 | 25.516 | 25.520 | 2.5.521 | 25.528 | 25.532 | 2.5.536 | 25.540 | 25.544 | 25.515 |
| 649 | 25.552 | 25.556 | 25.560 | 25.563 | 2.5 .567 | 25.571 | 25.575 | 25.579 | 25.583 | 2.5 .557 |
| 650 | 25.591 | 25.595 | 25.599 | 25.603 | 2.5.607 | 2.5 .611 | 25.615 | 25.619 | 25.623 | 2.5. 626 |
| 651 | 25.630 | 2.5.634 | 25.635 | 2.5 .642 | 25.646 | 2.5 .650 | 25.654 | 25.658 | 25.662 | 2.5 .666 |
| 652 | 2.5 .670 | 2.5.674 | 25.678 | 25.682 | 25.656 | 2.5 .689 | 2.5 .693 | 25.697 | 25.701 | 25.703 |
| 653 | 2.5 .709 | 2.5 .713 | 2.5 .717 | 25.721 | 2.5.72. | 2.5 .729 | 2.5 .733 | 25.737 | 25.741 | 25.745 |
| 654 | 2.5.745 | 25.752 | 25.756 | 25.760 | 25.764 | 25.768 | 25.772 | 25.776 | 25.780 | 25.784 |
| 655 | 25.788 | 2.5 .792 | 25.796 | 25.800 | 25.804 | 25.805 | 25.811 | 25.815 | 25.819 | 25.823 |
| 656 | 25.827 | 25.831 | 25.835 | 25.539 | 25.843 | 25.847 | 25.8 .51 | 25.855 | 25.859 | 25.863 |
| 657 | 25.867 | 2.5 .571 | 2.5 .574 | 25.575 | 25.882 | 25.586 | 25.590 | 2.5.894 | 25.898 | 25.902 |
| 658 | 2.5.906 | 2.5 .910 | 25.914 | 2.5 .918 | 2.5 .923 | 25.926 | 25.930 | 25.934 | 25.937 | 25.941 |
| 659 | 25.945 | 25.949 | 25.953 | 2.5 .957 | 25.961 | 25.965 | 25.969 | 25.973 | 25.977 | 25.981 |
| 660 | 25.985 | 2.5 .989 | 25.993 | 25.997 | 26.000 | 26.004 | 26.008 | 26.012 | 26.016 | 26.020 |
| 661 | 26.024 | 26.028 | 26.032 | 26.036 | 26.040 | 26.044 | 26.018 | 26.052 | 26.056 | 26.060 |
| 662 | 26.063 | 26.067 | 26.071 | 26.075 | 26.079 | 26.053 | 26.087 | 26.091 | 26.095 | $\supseteq 6.099$ |
| 663 | 26.103 | 26.107 | 26.111 | 26.115 | 26.119 | 26.123 | 26.126 | 26.130 | 26.134 | 26.138 |
| 664 | 26.142 | 26.146 | 26.150 | 26.154 | 26.158 | 26.162 | 26.166 | 26.170 | 26.174 | 26.178 |
| 665 | 26.182 | 26.186 | 26.189 | 26.193 | 26.197 | 26.201 | 26.205 | 26.209 | 26.213 | 26.217 |
| 666 | 26221 | 26.225 | 26.229 | 26.233 | 26.237 | 26.241 | 26.245 | 26.249 | 26.2.5 | 26.256 |
| 667 | 26.260 | 26.264 | 26.268 | 26.272 | 26.276 | 26.280 | 26.254 | 26.288 | 26.292 | 26.296 |
| 663 | 26.300 | 26.304 | 26.308 | 26.311 | 26.315 | 26.319 | 26.323 | 26.327 | 26.331 | 26.385 |
| 669 | 26.339 | 26.3.43 | 26.347 | 26.351 | 26.355 | 26.359 | 26.363 | 26.367 | 26.371 | 26.374 |
| 670 | 26.375 | 26.382 | 26.386 | 26.390 | 26.394 | 26.398 | 26.402 | 26.406 | 26.110 | 26.114 |
| 671 | 26.415 | 26.422 | 26.426 | 26.430 | 26.434 | 26.437 | 26.441 | 26.445 | 26.449 | 26.453 |
| 672 | 26.457 | 26.461 | 26.465 | 26.469 | 26.473 | 26.477 | 26.481 | 26.48 .5 | 26.489 | 26.493 |
| 673 | 26.497 | 26.500 | 26.504 | 26.50 s | 26.512 | 26.516 | 26.520 | 26.524 | 26.528 | 26.532 |
| 674 | 26.536 | 26.540 | 26.544 | 26.548 | 26.552 | 26.556 | 26.560 | 26.563 | 26.567 | 26.571 |
| 675 | 26.575 | 26.579 | 26.583 | 26.557 | 26.591 | 26.595 | 26.599 | 26.603 | 26.607 | 26.611 |
| 676 | 26.615 | 26.619 | 26.623 | 26.626 | 26.630 | 26.634 | 26.638 | 26.612 | 26.646 | 26.650 |
| 677 | 26.654 | 26.659 | 26.662 | 26.666 | 26.670 | 26.674 | 26.678 | 26.652 | 26.686 | 26.689 |
| 678 | 26.693 | 26.697 | 26.701 | 26.70 .5 | 26.709 | 26.713 | 26.717 | 26.721 | 26.725 | 26.729 |
| 679 | 26.733 | 26.737 | 26.741 | 26.745 | 26.749 | 26.752 | 26.756 | 26.760 | 26.764 | 26.768 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1 Metre $=39.8 .079$ English Inches.

| Millimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | \%. | 6. | $\gamma$. | 8. | B. |
|  | Eng. In. | Eng. In. | Eng. In. | Eng 1 n . | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 650 | 26.772 | 26.776 | 26.780 | 26.781 | 26.758 | 26.792 | 26.796 | 26.500 | 26.504 | 26.50s |
| 651 | 26.812 | 26.815 | 26.819 | $\underline{26.523}$ | 26.827 | 26.831 | 26.835 | 26.839 | 26.843 | 26.847 |
| 652 | 26.551 | 26.855 | 26.839 | 26.863 | 26.567 | 26.571 | 26.875 | 26.578 | 26.882 | 26.506 |
| 653 | 26.890 | 26.594 | 26.598 | 26.902 | 26.906 | 26.910 | 26.914 | 26.915 | 26.922 | $\stackrel{26.92}{ } 6$ |
| 634 | 26.930 | 26.934 | 26.937 | 26.941 | 26.945 | 26.949 | 26.953 | 26.957 | 26.961 | 26.965 |
| 685 | 26.969 | 26.973 | 26.977 | 26.981 | 26.985 | 26.959 | 26.993 | 26.997 | 27.000 | 27.004 |
| 686 | 27.005 | 27.012 | 27.016 | 27.020 | 27.024 | 27.025 | 27.032 | 27.036 | 27.040 | 27.044 |
| 687 | 27.045 | 27.0.72 | 27.056 | 27.060 | 27.063 | 27.067 | 27.071 | 27.075 | 27.079 | 27.083 |
| 658 | 27.087 | 27.091 | 27.095 | 27.099 | 27.103 | 27.107 | 27.111 | 27.115 | 27.119 | 27.123 |
| 689 | 27.126 | 27.130 | 27.134 | 27.138 | 27.142 | 27.146 | 27.150 | 27.154 | 27.158 | 27.162 |
| 690 | 27.166 | 27.170 | 27.174 | 27.178 | 27.182 | 27.186 | 27.189 | 27.193 | 27.197 | 27.201 |
| 691 | 27.205 | 27.209 | 27.213 | 27.217 | 27.221 | 27.225 | 27.229 | 27.233 | 27.237 | 27.241 |
| 692 | 27.245 | 27.249 | 27.252 | 27.256 | 27.260 | 27.26 .1 | 27.265 | 27.272 | 27.276 | 27.280 |
| 693 | 27.284 | 27.285 | 27.292 | 27.296 | 27.300 | 27.304 | 27.308 | 27.312 | 27.315 | 27.319 |
| 694 | 27.323 | 27.327 | 27.331 | 27.335 | 27.339 | 27.343 | 27.347 | 27.351 | 27.35. | 27.359 |
| 69.5 | 27.363 | 27.367 | 27.371 | 27.875 | 27.378 | 27.352 | 27.386 | 27.390 | 27.394 | 27.398 |
| 696 | 27.402 | 27.406 | 27.410 | 27.414 | 27.418 | 27.422 | 27.426 | 27.430 | 27.434 | 27.438 |
| 697 | 27.441 | 27.445 | 27.449 | 27.453 | 27.457 | 27.461 | 27.465 | 27.469 | 27.173 | 27.477 |
| 698 | 27.181 | 27.455 | 27.489 | 27.493 | 27.497 | 27.500 | 27.504 | 27.508 | 27.512 | 27.516 |
| 699 | 27.520 | 27.524 | 27.525 | 27.532 | 27.536 | 27.540 | 27.544 | 27.548 | 27.552 | 27.556 |
| 700 | 27.560 | 27.563 | 27.567 | 27.571 | 27.575 | 27.579 | 27.583 | 27.587 | 27.591 | 27.595 |
| 701 | 27.599 | 27.603 | 27.607 | 27.611 | 27.615 | 27.619 | 27.623 | 27.626 | 27.630 | 27.634 |
| 702 | 27.638 | 27.642 | 27.646 | 27.650 | 27.654 | 27.6 .98 | 27.662 | 27.666 | 27.670 | 27.674 |
| 703 | 27.675 | 27.682 | 27.686 | 27.689 | 27.693 | 27.697 | 27.701 | 27.705 | 27.709 | 27.713 |
| 704 | 27.717 | 27.721 | 27.725 | 27.729 | 27.733 | 27.737 | 27.741 | 27.745 | 27.749 | 27.752 |
| 70.5 | 27.756 | 27.760 | 27.764 | 27.765 | 27.772 | 27.776 | 27.780 | 27.781 | 27.788 | 27.792 |
| 706 | 27.796 | 27.500 | 27.804 | 27.808 | 27.812 | 27.815 | 27.519 | 27.523 | $27.8 \cdot 7$ | 27.831 |
| 707 | 27.535 | 27.839 | 27.543 | 27.847 | 27.551 | 27.855 | 27.859 | 27.863 | 27.867 | 27.571 |
| 705 | 27.875 | 27.575 | 27.882 | 27.886 | 27.590 | 27.894 | 27.598 | 27.902 | 27.906 | 27.910 |
| 709 | 27.914 | 27.918 | 27.922 | 27.926 | 27.930 | 27.934 | 27.938 | 27.941 | 27.945 | 27.949 |
| 710 | 27.953 | 27.957 | 27.961 | 27.965 | 27.969 | 27.973 | 27.977 | 27.981 | 27.985 | 27.989 |
| 711 | 27.993 | 27.997 | 28.001 | 28.004 | 28.005 | 28.012 | 28.016 | 28.020 | 28.024 | 28.028 |
| 712 | 28.032 | 28.036 | 28.010 | 28.044 | 28.045 | 25.052 | 28.0.26 | 28.060 | 28.063 | 28.067 |
| 713 | 28.071 | 28.075 | 28.079 | 28.083 | 25.087 | 28.091 | 28.095 | 28.099 | 25.103 | 28.107 |
| 714 | 28.111 | 28.115 | 28.119 | 28.123 | 23.126 | 28.130 | 28.134 | 28.138 | 2 S .142 | $2 \mathrm{S.146}$ |
| 715 | 23.150 | 25.154 | 28.158 | 28.162 | 28.166 | 28.170 | 28.174 | 28.178 | 28.182 | 28.156 |
| 716 | 28.189 | 28.193 | 23.197 | 28.201 | 28.205 | 25.209 | 28.213 | 28.217 | 28.221 | 28.225 |
| 717 | 28.229 | 28.233 | 28.237 | 29.241 | 28.245 | 28.249 | 28.252 | 28.256 | 28.260 | 28.264 |
| 718 | 28.268 | 25.272 | 28.276 | 25.280 | 28.284 | 29.285 | 28.292 | 28.296 | 28.300 | 28.304 |
| 719 | 28.308 | 28.312 | 29.315 | 28.319 | 28.323 | 25.327 | 28.331 | 28.335 | 28.339 | 28.343 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | D. |

1 Metre $=39.37079$ English Inches

| Millimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng. In. | Eng. In. | Eug. In. | Eng. In. | Eng In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 720 | 28.347 | 25.351 | 28.3.5. | 28.359 | 28.363 | 28.367 | 2S.3\%1 | 28.375 | 25.378 | 28.352 |
| 721 | 28.386 | 28.390 | 28.394 | 28.398 | 28.402 | 28.406 | 28.410 | 2R.414 | 25.418 | 28.422 |
| 722 | 28.126 | 28.430 | 28.434 | 28.438 | 28.441 | 28.445 | 28.449 | 28.453 | 28.457 | 28.461 |
| 723 | 2マ.46.5 | 25.469 | 28.473 | 28.477 | 2S.481 | 28.485 | 28.489 | 28.493 | 28.497 | 28.501 |
| 724 | 28.504 | 23.508 | 28.512 | 28.516 | 28.520 | $2 \mathrm{S.524}$ | 28.528 | 28.532 | 28.536 | 28.540 |
| $72 \%$ | 28.544 | 28.548 | 28.5 .52 | 28.5 .56 | 28.560 | 28.564 | 28.567 | 28.571 | 2 Q .575 | 28.579 |
| 726 | 28.583 | 25.587 | 28.591 | 28.595 | 25.599 | 25.603 | 28.607 | 28.611 | 28.615 | 28.619 |
| 727 | 28.62:3 | 29.6:37 | 28.630 | 28.634 | 28.638 | 28.642 | 28.646 | 28.650 | 25.6 .54 | 28.658 |
| 728 | 25.662 | 28.666 | 25.670 | 28.674 | 25.678 | 25.682 | 28.656 | 28.659 | 28.693 | 28.697 |
| 729 | 28.701 | 28.705 | 28.709 | 28.713 | 28.717 | 28.721 | 28.725 | 28.729 | 28.733 | 2 S .737 |
| 730 | 28.741 | 28.74.) | 28.749 | 28.752 | 28.756 | 28.760 | 28.764 | 28.768 | 28.772 | 28.7\%6 |
| 731 | 28.750 | 28.784 | 28.758 | 28.792 | 25.796 | $2 \mathrm{S}$. | 28.604 | 28.808 | 28.812 | 28.815 |
| 732 | 28.519 | 25.523 | 25.527 | 28.8:31 | 28.835 | 28.539 | 28.543 | 28.847 | 28.8 .51 | 28.855 |
| 738 | 28.859 | 95.863 | 28.967 | 25.871 | 28.875 | 25.975 | 28.882 | 28.886 | 28.890 | 28.59! |
| 734 | 28.898 | 28.902 | 28.906 | 28.910 | 28.914 | 28.918 | 28.922 | 28.926 | 28.930 | 28.934 |
| 735 | 28.935 | 28.941 | 28.945 | 28.949 | 28.953 | 28.957 | 25.961 | 28.965 | $2 \mathrm{S.969}$ | 28.978 |
| 736 | 28.977 | 25.981 | 28.985 | 28.989 | 28.993 | 28.997 | 29.001 | 29.004 | 29.008 | 29.012 |
| 737 | 29.016 | 29.020 | 29.024 | 29.025 | 29.032 | 29.036 | 29.040 | 29.044 | 29.015 | 29.052 |
| 738 | 29.0 .56 | 29.060 | 29.064 | $\underline{9} 9.067$ | 29.071 | 29.075 | 29.079 | 29.083 | 29.087 | 29.091 |
| 739 | 29.095 | 29.099 | 29.10:3 | 29.107 | 29.111 | 29.115 | 29.119 | 29.123 | 29.127 | 29.130 |
| 740 | 29.134 | 29.135 | 29.142 | 29.146 | 29.150 | 29.154 | 29.158 | 29.162 | 29.166 | 29.170 |
| 741 | 29.174 | 29.175 | 29.182 | 29.186 | 29.190 | 29.193 | 29.197 | 29.201 | 29.205 | 29.209 |
| 742 | 29.213 | 29.217 | 29.221 | 29.225 | 29.229 | 29.23:3 | 29.237 | 29.241 | 29.245 | 29.249 |
| 743 | 29.252 | 29.2.56 | 29.260 | 29.264 | 29.265 | 29.272 | 29.276 | 29.280 | 29.284 | 29.258 |
| 744 | 29.292 | 29.296 | 29.300 | 29.304 | 29.305 | 29.312 | 29.315 | 29.319 | 29.328 | 29.327 |
| 745 | 29.331 | 29.335 | 29.339 | 29.343 | 29.347 | 29.351 | 29.355 | 29.359 | 29.363 | 29.367 |
| 7.46 | 29.371 | 29.375 | 29.378 | 29.352 | 29.386 | 29.390 | 29.394 | 29.398 | 29.402 | 29.406 |
| 747 | 29.410 | 29.414 | 29.418 | 29.122 | 29.426 | 29.130 | 29.134 | 29.438 | 29.441 | 29.445 |
| 745 | 29.449 | 29.453 | 29.457 | 29.461 | 29.465 | 29.469 | 29.473 | 29.477 | 29.481 | 29.485 |
| 749 | 29.459 | 29.498 | 29.497 | 29.501 | $29.50 \downarrow$ | 29.508 | 29.512 | 29.516 | 29.520 | 29.524 |
| 750 | 29.528 | 29.582 | 29.536 | 29.540 | 29.544 | 29.548 | 29.552 | 29.556 | 29.560 | 29.564 |
| 751 | 29.567 | 29.571 | 29.575 | 29.579 | 29.583 | 29.557 | $29.59]$ | 29.595. | 29.599 | 29.603 |
| 752 | 29.607 | 29.611 | 29.615 | 29.619 | 29.623 | $29.6 \div 7$ | 29.630 | 29.634 | 29.638 | 29.642 |
| 753 | 29.646 | 29.6 .50 | 29.6 .54 | 29.6 .58 | 29.662 | 29.666 | 29.670 | 29.674 | 29.678 | 29.652 |
| 754 | $29.6 \times 6$ | 29.690 | 29.693 | 29.697 | 29.701 | 29.705 | 29.709 | 29.713 | 29.717 | 29.721 |
| 755 | 29.725 | 29.729 | 29.733 | 29.737 | 29.741 | 29.745 | 29.749 | 29.753 | 29.756 | 29.760 |
| 756 | 29.764 | 29.765 | 29.772 | 29.756 | 29.780 | 29.784 | 29.788 | 29.792 | 29.796 | 29.800 |
| 757 | 29.504 | 29.905 | 29.812 | 29.515 | 29.819 | 29.523 | 29.827 | 29.931 | 29.835 | 29.839 |
| 758 | 29.813 | 29.847 | 29.851 | 29.8 .55 | 29.859 | 29.868 | 29.867 | 29.871 | 29.875 | 29.878 |
| 759 | 29.882 | 29.586 | 29.890 | 29.894 | 29.598 | 29.902 | 29.906 | 29.910 | 29.914 | 29.918 |
|  | 0. | 1. | 2. | 3. | - 4. | 5. | 6. | 7. | 8. | Э. |

1 Metre $=39.37079$ English Inches.

| Nillimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | $\delta$. | 6. | 7. | 8. | D. |
|  | Eng. In. | Eng. In. | Eng. In. | Eng In. | Eng. In. | Eng. In. | Eng. In. | Eng. In | Eng. In. | Eng. In. |
| 760 | 29.922 | 29.926 | 29.930 | 29.934 | 29.938 | 29.941 | 29.945 | $29.949$ | 29.953 | 29.9 .57 |
| 761 | 29.961 | 29.965 | 29.969 | 29.973 | 29.977 | 29.981 | 29.985 | 39.989 | 29.993 | 29.997 |
| 762 | 30.001 | 30.004 | 30.008 | 30.012 | 30.016 | 30.020 | 30.024 | 30.028 | 30.032 | 30.036 |
| 763 | 30.040 | 30.044 | 30.048 | 30.052 | 30.056 | 30.060 | 30.064 | 30.067 | 30.071 | 30075 |
| 764 | 30.079 | 30.083 | 30.087 | 30.091 | 30.095 | 30.099 | 30.103 | 30.107 | 30.111 | 30.115 |
| 765 | 30.119 | 30.123 | 30.127 | 30.180 | 30.134 | 30.138 | 30.142 | 30.146 | 30.150 | 30.154 |
| 766 | 30.155 | ?0.162 | 30.166 | 30.170 | 30.174 | 30.178 | 30.182 | 30.156 | 30.190 | 30.193 |
| 767 | 30.197 | 30.201 | 30.30 .5 | 30.209 | 30.213 | 30.217 | 30.221 | 30.225 | 30.229 | 30.233 |
| 768 | 30.237 | 30.241 | 30.245 | 30.249 | 30.253 | 30.256 | 30.260 | 30.264 | 30.268 | 30.272 |
| 769 | 30.276 | 30.280 | 30.284 | 30.288 | 30.292 | 30.296 | 30.300 | 30.304 | 30.30 s | 30.312 |
| 770 | 30.316 | 30319 | 30.323 | 30.327 | 30.331 | 30.335 | 30.389 | 30.343 | 30.347 | 30.351 |
| 771 | 30.355 | 30.3 .59 | 30.363 | 30.367 | 30.371 | 30.375 | 30.379 | 30.382 | 30.356 | 30.390 |
| 772 | :30.394 | 30.393 | 30.402 | 30.406 | 30.410 | 30.414 | 30.418 | 30.422 | 30.126 | 30.430 |
| 773 | 30.184 | 30.438 | 30.411 | 30.145 | 30.449 | 30.453 | 30.457 | 30.461 | 30.465 | 30.169 |
| 774 | 30.473 | 30.477 | 30.481 | 30.485 | 30.489 | 30.493 | 30.497 | 30.501 | 30.504 | 30.508 |
| 775 | 30.512 | 30.516 | 30.520 | 30.524 | 30.528 | 30.532 | 30.536 | 30.540 | 30.544 | 30.548 |
| 776 | 30.5 .52 | 30.5 .56 | 30.560 | 30.561 | 30.567 | 30.571 | 30.575 | 30.579 | 30.583 | 30.557 |
| 777 | 30.591 | 30.595 | 30.599 | 30.603 | 30.607 | 30.611 | 30.615 | 30.619 | 30.623 | 30.627 |
| 778 | 30.630 | 30.634 | 30.638 | 30.612 | 30.616 | 30.650 | 30.6 .54 | 30.658 | 30.662 | 30.666 |
| 779 | 30.670 | 30.674 | 30.678 | 30.652 | 30.656 | 30.690 | 30.693 | 30.697 | 30.701 | 30.705 |
| 780 | 30.709 | 30.713 | 30.717 | 30.721 | 30.725 | 30.729 | 30.733 | 30.737 | 30.741 | 30.745 |
| 781 | 30.749 | 30.753 | 30.756 | 30.760 | 30.764 | 30.768 | 30.772 | 30.776 | 30.780 | 30.754 |
| 782 | :30.788 | 30.792 | 30.796 | 30.500 | 30.804 | 30.808 | 30.512 | 30.816 | 30.819 | 30.823 |
| 78.3 | 30.827 | 30.831 | 30.835 | 30.539 | 30.843 | 30.847 | 30.851 | 30.555 | 30.559 | 30.863 |
| 784 | 30.867 | 30.571 | 30.875 | 30.579 | 30.852 | 30.886 | 30.590 | 30.894 | 30.595 | 30.902 |
| 785 | 30.906 | 30.910 | 30.914 | 30.918 | 30.922 | 30.926 | 30.930 | 30.93-4 | 30.938 | 30.942 |
| 786 | 30.945 | 30.949 | 30.953 | 30.957 | 30.961 | 30.965 | 30.969 | 30.973 | 30.977 | 30.981 |
| $75^{*}$ | 30.955 | 30.989 | 30.993 | 30.997 | 31.001 | 31.004 | 31.008 | 31.012 | 31.016 | 31.020 |
| 788 | 31.024 | 31.028 | 31.032 | 31.036 | 31.040 | 31.044 | 31.048 | 31.0 .52 | 3].056 | 31.060 |
| 789 | 31.064 | 31.067 | 31.071 | 31.07 .7 | 31.079 | 31.083 | 31.087 | 31.091 | 31.095 | 31.099 |
| 790 | 31.103 | 31.107 | 31.111 | 81.115 | 31.119 | 31.123 | 31.127 | 31.130 | 31.131 | 31.138 |
| 791 | 31.142 | 31.116 | 31.150 | 31.154 | 31.158 | 31.162 | 31.166 | 31.170 | 31.174 | 31.175 |
| 792 | 31.152 | 31.186 | 31.190 | 31.193 | 31.197 | 31.201 | 31.20 .3 | 31.209 | 31.213 | 31.217 |
| 793 | 31.221 | 31.22 .5 | 31.229 | 31.233 | 31.237 | $31.2+1$ | 31.24 .5 | 31.249 | 31.253 | 31.256 |
| 994 | 31.260 | 31.261 | 31.265 | 31.272 | 31.276 | 31.280 | 31.284 | 31.258 | 31.292 | 31.296 |
| 795 | 31.300 | 31.304 | 31.308 | 31.312 | 31.316 | 31.319 | 31.323 | 31.327 | 31.331 | 31.335 |
| 796 | :31.339 | 31.843 | 31.347 | 31.351 | 31.355 | 31.359 | 31.36:3 | 31.367 | 31.371 | 31.375 |
| 797 | 31.379 | 31.382 | 31.386 | 31.390 | 31.394 | 31.398 | 31.102 | 31.406 | 31.410 | 31.414 |
| 798 | 31.418 | 31.122 | 31.426 | 31.130 | 31.434 | 31.438 | 31.412 | 31.445 | 31.149 | 31.453 |
| 799 | 31.457 | 31.161 | 31.46 .7 | 31.469 | 31.473 | 31.477 | 31.451 | 31.485 | 31.189 | 31.493 |
| 800 | 31.497 | 31.501 | 31.505 | 31.508 | 31.512 | 31.516 | 31.520 | 31.524 | 31.528 | 31.532 |
|  |  |  |  | IIundredth | s of Mill | etres. |  |  |  |  |
| 0. | 1. | 2. | 3. | 4. |  |  | b. | 7. | 8. | 9. |
| . 0000 | . 0004 | . 0008 | . 0012 | .0016 |  | 20 . 0 | 024 . 0 | 0028 | . 0031 | . 0035 |

1 Millimetre $=0.443296$ French or Paris Line.

| Millimetres <br> Tens. | Millimetres. Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 | 8. | 9. |
|  | Par.lines. | Par.lines | Par.lines | Par.lines | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | latr.lines, |
| 300 | 132.99 | 133.43 | 133.88 | 134.32 | 134.76 | 135.21 | 135.65 | 136.09 | 136.54 | 136.98 |
| 310 | 137.12 | 137.87 | 138.31 | 138.75 | 139.19 | 139.64 | 140.08 | 140.52 | 140.97 | 141.41 |
| 320 | 141.85 | 142.30 | 142.74 | 143.18 | 143.63 | 144.07 | 144.51 | 14.96 | 145.40 | 145.54 |
| 330 | 146.29 | 146.73 | 147.17 | 147.62 | 148.06 | 148.50 | 148.95 | 149.39 | 149.83 | 150.28 |
| 340 | 150.72 | 151.16 | 151.61 | 152.05 | 152.49 | 152.94 | 153.38 | 153.82 | 154.27 | 151.71 |
| 350 | 155.15 | 155.60 | 156.04 | 156.48 | 156.93 | 157.37 | 157.81 | 158.26 | 158.70 | 159.14 |
| 360 | 159.59 | 160.03 | 160.47 | 160.92 | 161.36 | 161.80 | 162.25 | 162.69 | 163.13 | 163.58 |
| 370 | 164.02 | 164.46 | 164.91 | 165.35 | 165.79 | 166.24 | 166.68 | 167.12 | 167.57 | 168.01 |
| 380 | 168.45 | 165.90 | 169.34 | 169.75 | 170.23 | 170.67 | 171.11 | 171.56 | 172.00 | 172.44 |
| 390 | 172.89 | 173.33 | 173.77 | 174.22 | 174.66 | 175.10 | 175.55 | 175.99 | 176.13 | 176.88 |
| 400 | 177.32 | 177.76 | 178.20 | 178.65 | 179.09 | 179.53 | 179.95 | 180.42 | 180.86 | 181.31 |
| 410 | 181.75 | 182.19 | 182.64 | 153.08 | 183.52 | 183.97 | 184.41 | 184.55 | 18.5 .30 | 185.74 |
| 420 | 186.18 | 186.63 | 187.07 | 187.51 | 187.96 | 188.10 | 188.84 | 189.29 | 189.73 | 190.17 |
| 430 | 190.62 | 191.06 | 191.50 | 191.95 | 192.89 | 192.83 | 193.28 | 193.72 | 194.16 | 194.61 |
| +40 | 195.05 | 195.49 | 195.94 | 196.38 | 196.82 | 197.27 | 197.71 | 198.15 | 198.60 | 199.04 |
| 450 | 199.48 | 199.93 | 200.37 | 200.81 | 201.26 | 201.70 | 202.14 | 202.59 | 203.03 | 203.17 |
| 460 | 203.92 | 204.36 | 204.50 | 205.25 | 205.69 | 206.13 | 206.58 | 207.02 | 207.46 | 207.91 |
| 470 | 208.35 | 208.79 | 209.24 | 209.68 | 210.12 | 210.57 | 211.01 | 211.45 | 211.90 | 212.34 |
| 450 | 212.78 | 213.23 | 213.67 | 214.11 | 214.56 | 215.00 | 215.44 | 21.5 .58 | 216.33 | 216.77 |
| 490 | 217.22 | 217.66 | 218.10 | 218.54 | 218.99 | 219.43 | 219.87 | 220.32 | 220.76 | 221.20 |
| 500 | 221.65 | 222.09 | 222.53 | 222.98 | 223.42 | 223.56 | 224.31 | 224.75 | 225.19 | 22.5 .64 |
| 510 | 226.08 | 226.52 | 226.97 | 227.41 | 227.55 | 228.30 | 228.74 | 229.18 | 229.63 | 2:3.07 |
| 520 | 230.51 | 230.96 | 231.40 | 231.84 | 232.29 | 232.73 | 233.17 | 233.62 | 234.06 | 234.50 |
| 530 | 234.95 | 235.39 | 235.83 | 236.28 | 236.72 | 237.16 | 237.61 | 238.05 | 238.49 | 235.94 |
| 540 | 239.38 | 239.52 | 240.27 | 240.71 | 241.15 | 241.60 | 242.04 | 242.48 | 212.93 | 243.37 |
| 5.50 | 243.81 | 244.26 | 244.70 | 2.15 .14 | 245.59 | 246.03 | 246.47 | 246.92 | 247.36 | 247.80 |
| 560 | 248.25 | 248.69 | 249.13 | 249.57 | 250.01 | 250.46 | 250.91 | 251.35 | 251.79 | 252.21 |
| 570 | 252.68 | 2.53 .12 | 253.57 | 254.01 | 254.45 | 254.90 | 255.34 | 255.78 | 256.23 | 256.67 |
| 580 | 2.57 .11 | 257.55 | 258.00 | 258.44 | 258.58 | 259.32 | 259.77 | 260.21 | 260.66 | 261.10 |
| 590 | 261.54 | 261.99 | 262.43 | 262.87 | 263.32 | 263.76 | 264.20 | 264.65 | 265.09 | 265.53 |
|  |  |  |  |  |  |  |  |  |  |  |

Tenths of Millimetres.

| 0. | 1. | 2. | 3. | 4. | お. | 6. | \%. | 8. | \%. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 0.044 | 0.089 | 0.133 | 0.177 | 0.222 | 0.266 | 0.310 | 0.355 | 0.399 |

Hundredths of Millimetres.

| 0.000 | 0.004 | 0.009 | 0.013 | 0.018 | 0.022 | 0.027 | 0.031 | 0.035 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

1 Nillimetre $=0.443290$ French Line．

| Millime－ tres． | Teaths of Millimetres． |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
|  | Par lines． | Partines． | Par．lines． | Par．hines． | P＇ar．lines． | Parlines． | Parlines． | Par．lines． | Par．li | Pir．lines． |
| 600 | 26.5 .95 | 266.02 | 266.07 | 266.11 | 2666.15 | 266.20 | 2665.24 | 266.29 | 266 | 266.38 |
| 601 | 266.42 | 266.47 | 266.51 | 2666.55 | 266.60 | 266.64 | 266.69 | 2666.73 | 266．75 | 2665.5 |
| 602 | 2666.86 | 266.91 | 266.95 | 267.00 | 267.04 | $\underline{267.09}$ | 267．1： | 207.17 | 267.22 | 267.26 |
| 603 | 267.31 | 2677.3 .5 | 267.10 | 267.41 | 267.45 | 267.93 | 267.67 | 267.62 | 267.66 | 267.71 |
| 60.4 | 267．7．5 | 267.50 | 267.84 | 267.58 | 267.93 | 267.97 | 268.02 | 265.06 | 265.11 | 26\％．15 |
| 60.5 | 268.19 | 268.24 | 268.28 | 26マ．33） | 268.37 | 265．42 | 26 P .16 | 268.50 | 269．5．） | 268.59 |
| 606 | 268.64 | 268.68 | 265.73 | 265.77 | 268.41 | 268.56 | 268.90 | 265.9 .5 | 268.99 | 269.04 |
| 607 | 269.08 | 269.13 | 269.17 | 269.21 | 269.26 | 269.39 | 269.85 | $26: 9.39$ | 269.44 | 269.15 |
| 608 | 269.52 | 269.57 | 269.61 | 269.66 | 269.70 | 269.75 | 269.79 | 269.83 | 269．ns | 269.92 |
| 609 | 269.97 | 270.01 | 270.06 | 270.10 | 270.14 | 270.19 | 270.23 | 270.23 | 270.32 | 270.37 |
| 610 | 270.41 | 270.5 | 270.50 | 270.54 | 270.59 | 270.63 | 270.68 | 27073 | 270.77 | 270.81 |
| 611 | 270.55 | 270.90 | 270.94 | 270.99 | 271.03 | 271.08 | 271.12 | 271.16 | 271.21 | 271.25 |
| 612 | 271.30 | 271.31 | 271.39 | 271.13 | 271.17 | 271.52 | 271.56 | 271.61 | 271.65 | 271.70 |
| 613 | 271.74 | 271.75 | 271.83 | 271.57 | 271.92 | 271.96 | 272．01 | 272.0 .5 | 272.10 | 272.14 |
| 614 | 27.15 | 272.23 | 272.27 | 272.32 | 272.36 | 272.41 | 272.45 | 272.19 | 272.54 | 272.58 |
| 61.5 | 272.63 | 272.67 | 272.72 | 272.76 | 272.50 | 272.85 | 272.89 | 2ここ．91 | 272.95 | 273.03 |
| 616 | 273.07 | 273.11 | 273.16 | 273.20 | 273.25 | 273.29 | 273.34 | 273.38 | 273.12 | 273.17 |
| 617 | 273.51 | 273.56 | 273.60 | 273.65 | 273.69 | 273.74 | 273.78 | 27：3．54 | 273.57 | 273.91 |
| 618 | 273.96 | 274.00 | 274.05 | 271.09 | 27.1 .13 | 274.19 | 274.22 | 271.27 | 274.31 | 271.36 |
| 619 | 274.10 | 271.11 | 274．49 | 274.53 | 271.58 | 274.62 | 274.67 | 271.71 | 274.75 | 274.60 |
| 620 | 274.51 | 274.59 | 271.93 | 274.98 | 27.5 .02 | 275.07 | 275.11 | 27.5 .15 | 275．20 | 275.24 |
| 621 | 275.29 | 275.33 | 275.38 | 27．3．42 | 27.5 .46 | 27.5 .51 | 275.55 | 27．5．60 | 275.64 | 275.69 |
| 622 | 275.73 | 275.77 | 27.5 .82 | 275.86 | 275.91 | 275．9．5 | 276.00 | 276.01 | 276.0 s | 276.13 |
| 623 | 276.17 | 276.22 | 276.26 | 276.31 | 276.35 | 276.35 | 276.44 | 276.15 | 276.53 | 276.57 |
| 621 | 276.62 | 276.66 | 276.71 | 276.75 | 276.79 | 276.84 | 276.88 | 27693 | 276.97 | 277.02 |
| 62.5 | 277.06 | 277.10 | 277.15 | 277.19 | 277.24 | 277.28 | 277.33 | 277.37 | 277.41 | 277.16 |
| 626 | 277.50 | 277.55 | 277.59 | 277.64 | 277.55 | 275．72 | 277.77 | 27\％．－1 | 277.46 | 277.90 |
| 627 | 277.95 | 277.99 | 278.04 | 278.08 | 27ヶ．12 | 275．17 | 27－21 | 2こく．26 | 27ヶ．30 | 278.35 |
| 628 | 278.39 | 278.43 | 278.48 | 278.52 | 278.57 | 275．61 | 27－．66 | 27ヶ．70 | 278.74 | 278.79 |
| 629 | 278.53 | 278.58 | 278.92 | 278.97 | 279.01 | 279.05 | 279.10 | 279.14 | 279.19 | 279.23 |
| 630 | 279.28 | 279.32 | 279.37 | 279.41 | 279.45 | 279.50 | 279.54 | 279.59 | 279.63 | 279.68 |
| 631 | 279.72 | 279.76 | 279.81 | 279.85 | 279.90 | 279．94 | 279.99 | 2～0．0．3 | $2 \bigcirc 0.0 \div$ | 2～0．12 |
|  | $2 \times 0.16$ | $2 \checkmark 0.21$ | 280．2．5 | 250.30 | 250．31 | 250．39 | 250.43 | $2 \times 0.17$ | 280.52 | 200．56 |
| 633 | 280.61 | 250.65 | 280.70 | 2－0．74 | 250．73 | 200.83 | 280.57 | 2－0．92 | 280.96 | 281.01 |
| 63 t | 281.05 | 281.09 | 281.14 | 281.18 | 281.23 | 281.27 | 281.32 | 281.36 | 281.40 | 281.45 |
| 63.5 | 281.49 | 281.54 | 281.58 | 281.63 | 281.67 | 281.71 | 281.76 | 281．80 | 281.85 | 281．89 |
| 636 | 281.94 | 281.98 | 282.02 | 282.07 | 282.11 | 282.16 | 282.20 | 282.2 .5 | 28.2 .29 | 25234 |
| $6: 7$ | $2 \times 2.38$ | 28.12 | 252.47 | 252．51 | 282.56 | 282.60 | 282.60 | $2 \times 2.69$ | 282．73 | 2 S 2.78 |
| 633 | 28.82 | 28.3 .87 | 282.91 | 282.96 | $\underline{283.00}$ | 283.04 | $2 \times 3.09$ | 283.13 | $2 \mathrm{2S3.18}$ | 283.22 |
| 639 | 283.27 | 253.31 | 283.35 | 283.40 | 283.44 | 283.49 | 283．53 | 283.58 | 253.62 | 283．67 |
|  | O． | 1 | 2. | 3. | 4. | 5 | 6. | 7. | 8. | 9. |

1 Millimetre $=0.443296$ French Line.

| Millimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
|  | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par lines. | Par.lines. | P:ar.lines. | Par.lines. | Par.lines. | Par.lines. |
| 640 | $2 \mathrm{S3} .71$ | 283.7. | 283.80 | 283.54 | 283.59 | 283.93 | 283.98 | 284.02 | 284.06 | 284.11 |
| 611 | 284.15 | 254.20 | 284.24 | 284.29 | 284.33 | 284.37 | 284.42 | 254.46 | 254.51 | 254.5 .5 |
| 642 | 284.60 | 284.61 | 254.68 | 284.73 | 284.77 | 284.82 | 254.86 | 284.91 | 284.95 | 254.99 |
| 643 | 255.04 | 285.08 | 285.13 | 23.5 .17 | 20.5 .22 | 285.26 | 285.31 | 28.5.35 | 28.5 .39 | 25.5 .44 |
| 644 | 285.45 | 285.53 | 285.57 | 285.62 | 28.5 .66 | 285.70 | 285.75 | 285.79 | 25.5 .84 | 285.58 |
| 64.7 | 25.5 .93 | 285.97 | 286.01 | 286.06 | 256.10 | 286.15 | 286.19 | 256.24 | 286.28 | 286.32 |
| 616 | 256.37 | 2 s 6.11 | 286.46 | 236.50 | 256.55 | 256.59 | 286.6t | 286.68 | 286.72 | $2 \checkmark 6.77$ |
| 647 | 256.51 | $2 \leq 6.86$ | 256.90 | 286.95 | $2 \bigcirc 6.99$ | 257.03 | 257.05 | 257.12 | 257.17 | 257.2: |
| 645 | 257.26 | 257.30 | 257.34 | 257.39 | 257.43 | 257.48 | 287.52 | 287.57 | 257.61 | 257.65 |
| 649 | 257.70 | 287.74 | 237.79 | 287.83 | 257.88 | 287.92 | 287.96 | 288.01 | 288.05 | 288.10 |
| 650 | 285.11 | 285.19 | 288.23 | 288.28 | 238.32 | 288.36 | 288.41 | 288.45 | 288.50 | 288.54 |
| 6.51 | 288.59 | 258.63 | 288.67 | 288.72 | 288.76 | 288.81 | 288.95 | 288.90 | 288.94 | 285.98 |
| 652 | 2-9.03 | 289.07 | 289.12 | 289.16 | 289.21 | 289.25 | 259.29 | 259.34 | 2~9.38 | 289.43 |
| 653 | 289.17 | 289.52 | 289.56 | 289.61 | 289.65 | 289.69 | 289.74 | 289.78 | 289.83 | 289.57 |
| 654 | 289.92 | 289.96 | 290.00 | 290.05 | 290.09 | 290.14 | 290.18 | 290.23 | 290.27 | 290.31 |
| 655 | 290.36 | 290.40 | 290.45 | 290.49 | 290.54 | 290.58 | 290.62 | 290.67 | 290.71 | 290.76 |
| 656 | 290.80 | 290.85 | 290.89 | 290.94 | 290.98 | 291.02 | 291.07 | 291.11 | 291.16 | 291.20 |
| 6.77 | 291.25 | 291.29 | 291.33 | 291.38 | 291.42 | 291.47 | 291.51 | 291.56 | 291.60 | 291.64 |
| 658 | 291.69 | 291.73 | 291.78 | 291.82 | 291.57 | 291.91 | 291.95 | 29.200 | 292.04 | 292.09 |
| 659 | 292.13 | 292.18 | 292.22 | 292.26 | 292.31 | 292.35 | 292.40 | 292.44 | 292.49 | 29.53 |
| 660 | 292.58 | 292.62 | 292.66 | 292.71 | 29.75 | 29.50 | 29.84 | 292.89 | 292.93 | 292.97 |
| 661 | 293.02 | 293.06 | 293.11 | 293.15 | 293.20 | 293.24 | 293.25 | 293.33 | 293.37 | 293.42 |
| 662 | 293.46 | 293.51 | 293.55 | 293.59 | 293.64 | 293.68 | 293.73 | 293.77 | 293.32 | 293.86 |
| 663 | 293.91 | 293.95 | 293.99 | 291.04 | 294.05 | 294.13 | 294.17 | 294.22 | 294.26 | 294.30 |
| 664 | 294.35 | 294.39 | 294.44 | 294.48 | 294.53 | 294.57 | 294.61 | 294.66 | 294.70 | 294.75 |
| 66.5 | 294.79 | 294.84 | 294.88 | 294.92 | 294.97 | 295.01 | 295.06 | 295.10 | 295.15 | 295.19 |
| 666 | 295.24 | 29.5 .23 | 29.5.32 | 29.3 .37 | 295.41 | 295.46 | 295.50 | 29.5.5. | 29.5.59 | 295.63 |
| 667 | 295.68 | 295.72 | 29.5 .77 | 29.5 .81 | 295.86 | 29.5 .90 | 29.5.94 | 29.5.99 | 296.03 | 296.08 |
| 663 | 296.12 | 296.17 | 296.21 | 296.2.5 | 296.30 | 296.34 | 296.39 | 296.43 | 296.48 | 296.52 |
| 669 | 296.56 | 296.61 | 29665 | 296.70 | 296.74 | 296.79 | 296.53 | 296.88 | 296.92 | 296.96 |
| 670 | 297.01 | 297.05 | 297.10 | 297.14 | 297.19 | 297.23 | 297.27 | 297.32 | 297.36 | 297.41 |
| 671 | 297.45 | 297.50 | 297.54 | 297.58 | 297.63 | 297.67 | 297.72 | 297.76 | 297.81 | 297.85 |
| 672 | 297.89 | 297.94 | 297.98 | 298.03 | 298.07 | 298.12 | 298.16 | 298.21 | 298.25 | 298.29 |
| 673 | 298.34 | 298.38 | 295.43 | 298.47 | 298.52 | 293.56 | 295.60 | 295.65 | 298.69 | 298.74 |
| 674 | 298.78 | 298.83 | 298.87 | 298.91 | 298.96 | 299.00 | 299.05 | 299.09 | 299.14 | 299.18 |
| 67.5 | 299.22 | 299.27 | 299.31 | 299.36 | 299.40 | 299.45 | 299.49 | 299.54 | 299.58 | 299.62 |
| 676 | 299.67 | 299.71 | 299.76 | 299.50 | 299.85 | 299.89 | 299.93 | 299.98 | 300.02 | 300.07 |
| 677 | 300.11 | 300.16 | 300.20 | 300.24 | 300.29 | 300.33 | 300.35 | 300.42 | 300.47 | 300.51 |
| 678 | 300.55 | 300.60 | 300.64 | 300.69 | 300.73 | 300.78 | 300.82 | 300.86 | 300.91 | 300.95 |
| 679 | 301.00 | 301.04 | 301.09 | 301.13 | 301.18 | 301.22 | 301.26 | 301.31 | 301.35 | 301.40 |
|  | 6. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1 Millimetre $=0.443296$ Freach 1 ine.

| Millimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Par lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines | Par.lines. | Par.lines. | Par.lines. | Par.lines. |
| 680 | 301.44 | 301.49 | 301.53 | 301.57 | 301.62 | 301.66 | 301.71 | 301.75 | 301.80 | 301.84 |
| 6 S | 301.58 | 301.93 | 301.97 | 302.02 | 302.06 | 302.11 | 302.15 | 302.19 | 302.24 | 302.28 |
| 692 | 302.33 | 302.37 | 302.42 | 302.46 | 302.51 | 302.55 | 302.59 | 302.64 | 302.68 | 302.73 |
| 693 | 302.77 | 302.92 | 302.86 | 302.90 | 302.95 | 302.99 | 303.04 | 303.05 | 303.13 | 303.17 |
| 634 | 303.21 | 303.26 | $30: 3.30$ | 303.35 | 303.39 | 303.44 | 303.15 | 303.52 | 303.57 | 303.61 |
| 685 | 303.66 | 303.70 | 303.75 | 303.79 | 30.3.83 | 30.8 .88 | 303.92 | 303.97 | 304.01 | 304.06 |
| 656 | 304.10 | 304.15 | 304.19 | 30.1 .23 | 304.25 | 304.32 | 304.37 | 304.41 | 304.46 | 304.50 |
| 687 | 304.54 | 301.59 | 304.63 | 304.65 | 304.72 | 304.77 | 304.81 | 304.85 | 304.90 | 304.91 |
| 689 | 304.99 | 30.5.0:3 | 305.08 | 30.5 .12 | 305.16 | 30.5 .21 | 305.25 | 30.5 .30 | 30.9 .34 | 30.5 .39 |
| 659 | 305.43 | 305.45 | 30.5 .52 | 305.56 | 305.61 | 305.65 | 305.70 | 305.71 | 305.79 | 305.83 |
| 690 | 30.5 .87 | 30.5.92 | 30.5 .96 | 306.01 | 306.05 | 306.10 | 306.14 | 306.18 | 306.23 | 306.27 |
| 691 | 306.32 | 306.36 | 306.41 | 306.45 | 306.19 | 306.51 | 306.58 | 306.63 | 306.67 | 306.72 |
| 692 | 306.76 | 306.81 | 306.85 | 306.59 | 306.94 | 306.95 | 307.03 | 307.07 | 307.12 | 307.16 |
| 693 | 307.20 | :307.2.5 | 307.29 | 307.34 | 307.38 | 307.43 | 307.47 | 307.51 | 307.56 | 307.60 |
| $69+$ | 307.65 | 307.69 | 307.74 | 307.78 | 307.82 | 307.87 | 307.91 | 307.96 | 308.00 | 308.05 |
| 69.5 | 308.09 | 309.13 | 308.18 | 305.22 | 308.27 | 305.31 | 308.36 | 308.40 | 308.45 | 308.49 |
| 696 | 30.8 .53 | $30 \mathrm{S.5}$ | 308.62 | 308.67 | 308.71 | 308.76 | 308.80 | 308.84 | 308.59 | 308.93 |
| 697 | 305.95 | 309.02 | 309.07 | 309.11 | 309.15 | 309.20 | 309.24 | 309.29 | 309.33 | 309.38 |
| 698 | 309.12 | 309.46 | 309.51 | 309.5 .5 | 309.60 | 309.64 | 809.69 | 309.73 | 309.78 | 309.52 |
| 699 | 309.86 | 309.91 | 309.95 | 310.00 | 310.04 | 310.09 | 310.13 | 310.17 | 310.22 | 310.26 |
| 700 | 310.31 | 310.35 | 310.40 | 310.44 | 310.48 | 310.53 | 310.57 | 310.62 | 310.66 | 310.71 |
| 701 | 310.75 | 310.79 | 310.84 | 310.83 | 310.93 | 310.97 | 311.02 | 311.06 | 311.11 | 311.15 |
| 702 | 311.19 | 311.24 | 311.23 | 311.3:3 | 311.37 | 311.42 | 311.46 | 311.50 | 311.55 | 311.59 |
| 70.3 | 311.64 | :311.68 | 311.73 | 311.77 | 311.81 | 311.86 | 311.90 | 811.95 | 311.99 | 312.04 |
| 704 | 312.08 | 312.12 | 312.17 | 312.21 | 312.26 | 312.30 | 312.35 | 312.39 | 312.43 | 312.45 |
| 70.5 | 312.52 | 312.57 | 312.61 | 312.66 | 312.70 | 312.75 | 312.79 | 312.83 | 312.85 | 312.92 |
| 706 | 312.97 | 313.01 | 313.06 | 313.10 | 313.14 | 313.19 | 313.23 | 313.25 | 313.32 | 313.37 |
| 707 | 313.41 | 313.45 | 313.50 | 313.54 | 313.59 | 313.63 | 313.65 | 318.72 | 313.76 | 313.81 |
| 708 | 313.85 | 313.90 | 313.94 | 313.99 | 314.03 | 314.05 | 314.12 | 314.16 | 314.21 | 314.25 |
| 709 | 311.30 | 314.34 | 314.39 | 314.43 | 314.47 | 314.52 | 314.56 | 314.61 | 314.65 | 314.70 |
| 710 | 314.71 | 314.88 | 314.83 | 311.87 | 314.92 | 314.96 | 315.01 | 315.0.) | 315.09 | 315.14 |
| 711 | 315.18 | 31.5 .23 | 315.27 | 315.32 | 315.36 | 315.41 | 315.45 | 315.49 | 315.54 | 315.58 |
| 712 | 315.63 | 315.67 | 315.72 | 315.76 | 315.80 | 315.8 .5 | 315.89 | 315.94 | 315.98 | 316.03 |
| 713 | 316.07 | 316.11 | 316.16 | 316.20 | 316.2 .5 | 316.29 | 316.34 | 316.38 | 316.12 | 316.47 |
| 714 | 316.51 | 316.56 | 316.60 | 316.65 | 316.69 | 316.73 | 316.78 | 316.82 | 316.87 | 316.91 |
| 715 | 316.96 | 317.00 | 317.05 | 317.09 | 317.13 | 317.18 | 317.22 | 317.27 | 317.31 | 317.36 |
| 716 | 317.10 | 317.4 | 317.49 | 317.53 | 317.58 | 317.62 | 317.67 | 317.71 | 317.75 | 317.80 |
| 717 | 317.84 | 317.59 | 317.93 | 317.98 | 318.02 | 318.06 | 318.11 | 318.15 | 318.20 | 318.24 |
| 718 | 318.29 | 315.33 | 318.38 | 318.42 | 318.46 | 318.51 | 318.5 .5 | 318.60 | 318.64 | 318.69 |
| 719 | 318.73 | 318.77 | 318.82 | 318.86 | 318.91 | 318.95 | 319.00 | 319.04 | 319.03 | 319.13 |
|  | 0. | 1. | $\stackrel{2}{2}$. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

C

1 Millimetre $=0.443296$ French Line

| Millimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7 | 8. | 9. |
|  | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. |
| 720 | 319.17 | 319.22 | 319.26 | 319.31 | 319.35 | 319.39 | 319.44 | 319.48 | 319.53 | 319.57 |
| 721 | 319.62 | 319.66 | 319.70 | 319.75 | 319.79 | 319.84 | 319.88 | 319.93 | 319.97 | 320.02 |
| 722 | 320.06 | 320.10 | 320.15 | 320.19 | 320.24 | 320.28 | 320.33 | 320.37 | 320.41 | 320.46 |
| 723 | 320.50 | 320.55 | 320.59 | 320.64 | 320.68 | 320.72 | 320.77 | 320.81 | 320.86 | 320.90 |
| 724 | 320.95 | 320.99 | 321.03 | 321.08 | 321.12 | 321.17 | 321.21 | 321.26 | 321.30 | 321.35 |
| 725 | 321.39 | 321.43 | 321.48 | 321.52 | 321.57 | 321.61 | 321.66 | 321.70 | 321.74 | 321.79 |
| 726 | 321.83 | 321.88 | 321.92 | 321.97 | 322.01 | 322.05 | 322.10 | 322.14 | 322.19 | 322.23 |
| 727 | 322.28 | 322.32 | 322.36 | 322.41 | 322.45 | :322.50 | 322.54 | 322.59 | 32.2 .63 | 322.65 |
| 728 | 322.72 | 322.76 | 322.81 | 32.2 .85 | 322.90 | 322.94 | 322.99 | 323.03 | 323.07 | 323.12 |
| 729 | 323.16 | 323.21 | 323.25 | 323.30 | 323.34 | 323.38 | 323.43 | 323.47 | 323.52 | 323.56 |
| 730 | 323.61 | 323.65 | 323.69 | 323.74 | 323.78 | 323.83 | 323.87 | 323.92 | 323.96 | 324.00 |
| 731 | 324.05 | 324.09 | 324.14 | 324.18 | 324.23 | 324.27 | 324.32 | 324.36 | 324.40 | 324.45 |
| 732 | 324.49 | 324.54 | 324.58 | 324.63 | 324.67 | 324.71 | 324.76 | 324.80 | 324.8 .3 | 324.89 |
| 733 | 324.94 | 324.98 | 325.02 | 325.07 | 325.11 | 325.16 | 325.20 | 325.25 | 325.29 | 325.33 |
| 734 | 325.38 | 325.42 | 325.47 | 325.51 | 325.56 | 32.7.60 | 325.65 | 325.69 | 325.73 | 325.78 |
| 735 | 325.82 | 325.57 | 325.91 | 335.96 | 326.00 | 326.04 | 326.09 | 326.13 | 326.18 | 326.22 |
| 736 | 326.27 | 326.31 | 326.35 | 326.40 | 326.44 | 326.49 | 326.53 | 326.58 | 326.62 | 326.66 |
| 737 | 326.71 | 326.75 | 326.80 | 326.84 | 326.59 | 326.93 | 326.98 | 327.02 | 327.06 | 327.11 |
| 738 | 327.15 | 327.20 | 327.24 | 327.29 | 327.33 | 327.37 | 327.42 | 327.16 | 327.51 | 327.55 |
| 739 | 327.60 | 327.64 | 327.68 | 327.73 | 327.77 | 327.82 | 327.86 | 327.91 | 327.95 | 327.99 |
| 740 | 325.04 | 328.05 | 328.13 | 328.17 | 328.22 | 328.26 | 328.30 | 328.35 | 328.39 | 320.11 |
| 741 | 328.48 | 328.53 | 328.57 | 328.62 | 328.66 | 328.70 | 328.75 | 328.79 | 328.84 | 328. 88 |
| 742 | 328.93 | 328.97 | 329.01 | 329.06 | 329.10 | 329.15 | 329.19 | 329.24 | 329.28 | 329.32 |
| 743 | 329.37 | 329.41 | 329.46 | 329.50 | 329.55 | 329.59 | 329.63 | 329.68 | 329.72 | 329.77 |
| 744 | 329.81 | 329.86 | 329.90 | 329.95 | 329.99 | 330.03 | 330.08 | 330.12 | 330.17 | 330.21 |
| 745 | 330.26 | 330.30 | 330.34 | 330.39 | 330.43 | 330.45 | 330.52 | 330.57 | 330.61 | 330.65 |
| 746 | 330.70 | 330.74 | 330.79 | 330.83 | 330.88 | 330.92 | 330.96 | 331.01 | 331.05 | 331.10 |
| 747 | 331.14 | 331.19 | 331.23 | 331.28 | 331.32 | 331.36 | 331.41 | 331.45 | 331.50 | 331.54 |
| 748 | 331.59 | 331.63 | 331.67 | 381.72 | 331.76 | 331.81 | 331.85 | 381.90 | 331.94 | 331.98 |
| 749 | 332.03 | 332.07 | 332.12 | 332.16 | 332.21 | 332.25 | 33.2 .29 | 332.34 | 332.38 | 332.43 |
| 750 | 332.47 | 332.52 | 332.56 | 332.60 | 332.65 | 332.69 | 332.74 | 332.78 | 332.83 | 332.87 |
| 751 | 332.92 | 332.96 | 333.00 | 333.05 | 333.09 | 333.14 | 333.18 | 333.23 | 333.27 | 333.31 |
| 752 | 333.36 | 333.40 | 333.45 | 333.49 | 333.54 | 333.58 | 333.62 | 333.67 | 333.71 | 333.76 |
| 75.3 | 333.80 | 333.85 | 333.89 | 333.93 | 333.98 | 334.02 | 334.07 | 334.11 | 334.16 | 334.20 |
| 754 | 334.25 | 334.29 | 334.33 | 334.38 | 334.42 | 334.47 | 334.51 | 334.56 | 334.60 | 334.64 |
| 755 | 334.69 | 334.73 | 334.78 | 334.82 | $3: 4.87$ | 334.91 | 334.95 | 335.00 | 335.04 | 335.09 |
| 756 | 335.13 | 335.18 | 335.22 | 335.26 | $3: 35.31$ | 335.35 | 335.40 | 335.44 | 335.49 | 335.53 |
| 757 | 335.58 | 335.62 | 335.66 | 335.71 | 335.75 | 335.80 | 335.84 | 335.89 | 335.93 | 335.97 |
| 758 | 336.02 | 336.06 | 336.11 | 336.15 | 336.20 | 336.24 | 336.28 | 336.33 | 386.37 | 336.42 |
| 759 | 336.46 | 336.51 | 336.55 | 336.59 | 3:6.64 | 336.68 | 336.73 | 336.77 | 336.82 | 336.56 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1 Millimetre $=0.443296$ French Line

| Millimetres. | Tenths of Millimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. | Par.lines. |
| 760 | 336.90 | 336.9 .5 | 336.99 | 337.04 | 337.05 | 337.13 | 337.17 | 337.22 | 337.26 | 337.30 |
| 761 | 337.35 | 337.39 | 337.44 | 337.48 | 337.53 | 337.57 | 337.61 | 337.66 | 337.70 | 337.75 |
| 762 | 337.79 | 337.54 | 337.58 | 337.92 | 337.97 | 338.01 | 338.06 | 338.10 | 338.15 | 335.19 |
| 763 | 335.23 | 338.25 | 335.32 | 338.37 | 338.41 | 338.46 | 335.50 | 338.55 | $3: 3.59$ | 338.63 |
| 764 | 333.65 | 338.72 | 338.77 | 338.51 | $33 \mathrm{S}$. | 335.90 | 338.94 | 335.99 | 339.03 | 339.08 |
| 76.5 | 339.12 | 339.17 | 339.21 | 339.25 | 339.30 | 339.34 | 339.39 | 339.43 | 339.48 | 339.52 |
| 766 | 339.56 | 339.61 | 339.65 | 339.70 | 339.74 | 339.79 | 339.83 | 339.87 | 339.92 | 339.96 |
| 767 | 340.01 | 340.0 .5 | 340.10 | 340.14 | 340.19 | 340.23 | 340.27 | 340.32 | 340.36 | 340.41 |
| 768 | 340.45 | 340.50 | 340.54 | 340.55 | 340.63 | 340.67 | 340.72 | 340.76 | 340.81 | 340.55 |
| 769 | 340.89 | 340.94 | 340.98 | 341.03 | 341.07 | 341.12 | 341.16 | $3+1.20$ | 341.25 | 341.29 |
| 770 | 341.34 | 341.38 | 341.43 | 341.47 | 341.52 | 341.56 | 341.60 | $3 \mathrm{H1.6.5}$ | 341.69 | 341.74 |
| 771 | 341.78 | 341.53 | 341.87 | 341.91 | 341.96 | 342.00 | 34.2 .05 | 342.09 | 312.14 | 342.18 |
| 772 | 312.22 | 342.27 | 342.3 I | 342.36 | 312.40 | 342.45 | 342.49 | 342.53 | 312.58 | 342.62 |
| 773 | 342.67 | 342.71 | 342.76 | 342.80 | 342.85 | 342.89 | 342.93 | 342.98 | 343.02 | 343.07 |
| 774 | 343.11 | 343.16 | 343.20 | 343.24 | 343.29 | 343.33 | 343.3 S | 343.42 | 343.47 | 343.51 |
| 775 | 343.55 | 343.60 | 343.64 | 348.69 | 343.73 | 343.78 | 343.82 | 343.86 | 343.91 | 343.95 |
| 776 | 314.00 | 344.04 | 344.09 | 344.13 | 344.17 | 344.22 | 344.26 | 344.31 | 344.35 | 344.10 |
| 777 | 344.4 | 344.49 | 344.53 | 344.57 | 344.62 | $3+4.66$ | 344.71 | 344.75 | 344.80 | 344.84 |
| 778 | 344.85 | 344.93 | 3.14 .97 | 345.02 | 34.3. 06 | 345.11 | 345.15 | 345.19 | 345.24 | 34.7 .28 |
| 779 | 345.33 | 345.37 | 345.42 | 345.46 | 345.50 | 345.55 | 345.59 | 345.64 | 345.68 | 345.73 |
| 780 | 34.5 .77 | 345.82 | 345.86 | 345.90 | 345.95 | 34.5 .99 | 346.04 | 346.08 | 346.13 | 346.17 |
| 781 | 346.21 | 346.26 | 346.30 | 346.35 | 346.39 | 346.44 | 346.45 | 346.52 | 346.57 | 346.61 |
| 752 | 346.66 | 346.70 | 346.75 | 346.79 | 346.83 | 346.88 | 346.92 | 346.97 | 347.01 | 347.06 |
| 783 | 347.10 | 347.15 | 347.19 | 347.23 | 347.25 | 347.32 | 347.37 | 347.41 | 347.46 | 347.50 |
| 784 | 347.54 | 347.59 | 347.63 | 347.68 | 347.72 | 347.77 | 347.81 | 347.85 | 347.90 | 347.94 |
| 785 | 347.99 | 348.03 | 348.08 | 348.12 | 348.16 | 348.21 | 348.25 | 348.30 | 348.34 | 348.39 |
| 786 | 348.43 | 348.47 | 348.52 | 345.56 | 348.61 | 348.6.5 | 348.70 | 348.74 | 348.79 | 348.83 |
| 787 | 348.57 | 348.92 | 348.96 | 349.01 | 349.05 | 349.10 | 349.14 | 349.18 | 349.23 | 349.27 |
| 788 | 349.32 | 349.36 | 349.41 | 349.45 | 349.49 | 349.54 | 349.38 | 349.63 | 349.67 | 349.72 |
| 789 | 349.76 | 349.80 | 349.85 | 349.89 | 349.94 | 349.9 S | 350.03 | 350.07 | 350.12 | 350.16 |
| 790 | 350.20 | 350.25 | 350.29 | 350.34 | 350.38 | 350.43 | 350.47 | 350.51 | 350.56 | 350.60 |
| 791 | 350.65 | 350.69 | 350.74 | 350.78 | 350.52 | 350.87 | 350.91 | 350.96 | 351.00 | 351.05 |
| 792 | 3.51 .09 | 351.13 | 351.18 | 3.51 .22 | 3.51 .27 | 351.31 | 351.36 | 351.40 | 351.44 | 351.49 |
| 793 | 351.53 | 351.58 | 351.62 | 351.67 | 351.71 | 351.76 | 3.51 .80 | 351.84 | 351.89 | 351.93 |
| 794 | 351.95 | 352.02 | 352.07 | 352.11 | 352.15 | 352.20 | 352.24 | 352.29 | 352.33 | 352.38 |
| 79.5 | 3.52 .42 | 352.46 | 352.51 | 352.55 | 3.52 .60 | 352.64 | 352.69 | 352.73 | 352.77 | 352.82 |
| 796 | 352.86 | 352.91 | 352.95 | 353.00 | 353.04 | 353.09 | 353.13 | 353.17 | 353.22 | 353.26 |
| 797 | 353.31 | 353.35 | 353.40 | 353.44 | 35.3.48 | 353.53 | 353.57 | 353.62 | 353.66 | 353.71 |
| 795 | 353.75 | 358.79 | 353.84 | 353.88 | 353.93 | 353.97 | 354.02 | 354.06 | 354.10 | 354.15 |
| 799 | 354.19 | 354.24 | 354.28 | 354.33 | 354.37 | 354.42 | 354.46 | 354.50 | 354.55 | 354.59 |
| 800 | 354.64 | 354.68 | 354.73 | 354.77 | 354.81 | 354.86 | 354.90 | 354.93 | 354.99 | 355.04 |
| - | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

## V. - VI.

COMPARISON
${ }^{07}$

## TIIE OLD FRENCII BAROMETER

WITH

TIIE ENGLISII AND TIIE METRICAL BAROMETERS,
or

TABLES

For converting frencil or paris line into enclisil inclies and decimals, and into millimetres:

GIVEN TIE VALUES CORRESPONDING TO EVERY PARIS LINE FROM 120 to 216 LINES, OR FROM 10 TO 18 INCHES ; AND TO EVEIV TENTII $O F$ A LINE FROM 216 TO 348 liNes, OR From 18 TO 29 FRENCH inches.

## TABLE V .

MM. J. J. Polil and J. Schabus have published, in the number for March, 1852, of the Proceetings of the Imperial Acarlemy of V'ienna, Class of Nathematics and Netural Philosophy, a set of short Thermometrical and Barometrical Reduction Tatbes, among which is found a table for the reduction of the Old French Barometrical Scale into the English. As this table shows slight discrepancies from the one given in the following pages, it may not be out of place to state that they arise from an aecidental error in the equation used by MM. Pohl and Schabus in computing their table. Adtopting, as they do, Bird's value of the metre, viz.

1 metre $=39.37062$ English inches,
the value of the Paris line is
1 Paris line $=0.055813$ English inches.
But the table seems to have been computed by using the equation
1 Paris line $=0.058823$ English inches,
which gives, at the end of the table, 345 lines $\times .058523=30.9104$ English inches,
instead of
thus causing an error

$$
\begin{aligned}
348 " \times .058513 & =30.9069 \quad " \\
& =0.0035
\end{aligned}
$$

which, of course, gradually diminishes in lower numbers.

1 Paris Line $=0.088814$ English Inch

| French or Paris Lines. Tens. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (1. | 1. | * | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{gathered} 10 \text { Inch. } \\ 120 \end{gathered}$ | Eug. In. 10.6 .58 | $\begin{aligned} & \text { Eny In. } \\ & 10.746 \end{aligned}$ | $\begin{aligned} & \text { Eng. In. } \\ & 10.835 \end{aligned}$ | $\begin{aligned} & \text { Eng. In } \\ & 10.9 .24 \end{aligned}$ | Eug In 11.013 | Eng. In. 11.102 | $\begin{aligned} & \text { Eng. In } \\ & 11.191 \end{aligned}$ | $\begin{aligned} & \text { Eng. In. } \\ & 11.279 \end{aligned}$ | Eng In. 11.365 | Eug In. 11.457 |
| 130 | 11.546 | 11.635 | 11.733 | 11.812 | 11.901 | 11.990 | 12.079 | 12.168 | 12.256 | 12.345 |
| 140 | 12.431 | 12.523 | 12.612 | 12.700 | 12.759 | 12.878 | 12.967 | 13.0 .56 | 13.144 | 13.23:3 |
| 150 | 13.32.2 | 13.411 | 13.500 | 13.559 | 13.67\% | 13.766 | 13.8.55 | 13.944 | 14.033 | 14.121 |
| 160 | 14.210 | 14.299 | 14.385 | 14.177 | 14.565 | 14.654 | 14.743 | 14.532 | 14.921 | 1.5 .010 |
| 170 | 15.095 | 15.187 | 15.276 | 15.36 .5 | 15.451 | 15.542 | 15.631 | 15.720 | 15.509 | 15.898 |
| 150 | 15957 | 16.075 | 16.164 | 16.253 | 16.342 | $16.4 \% 1$ | 16.519 | 16.605 | 16.697 | 16.7こ6 |
| 190 | 16.87. | 16.963 | 17.0 .52 | 17.111 | 17.230 | 17.319 | 17.408 | 17.496 | 17.58 .5 | 17.1,51 |
| 200 | 17.763 | 17.5.92 | 17.940 | 18.029 | 19.118 | 18.207 | 18.296 | 15.384 | 18.473 | 1-.562 |
| 210 | 18.6.3] | 18.710 | 18.529 | 18.917 | 19.006 | 19.09.) | 19.184 | 19.273 | 19.361 | 19.4.0 |
| Pariz Lines. | Tenths. |  |  |  |  |  |  |  |  |  |
|  | 6. | 1. | 2. | 33. | 4. | 3. | 6. | 8. | 8. | 3. |
| $\begin{gathered} 18 \text { Inch. } \\ 216 \end{gathered}$ | $\begin{aligned} & \text { Eng. In. } \\ & 19.194 \end{aligned}$ | Eng. ln. <br> 19.193 | $\begin{aligned} & \text { Eng } \ln \text {. } \\ & 19.20 .2 \end{aligned}$ | $\begin{gathered} \text { Eng In } \\ 19.210 \end{gathered}$ | $\begin{gathered} \text { Eng. In } \\ 19.219 \end{gathered}$ | $\begin{aligned} & \text { Eng. In } \\ & 19.2 .25 \end{aligned}$ | Eng. In. $19.287$ | Eng. In. $19.2+6$ | Eng. In. 19.955 | $\begin{aligned} & \text { Eng. In } \\ & 19.261 \end{aligned}$ |
| 217 | 19.273 | $19.2-2$ | 19.290 | 19.299 | 19.309 | 19.317 | 19.326 | 1938.5 | 19.344 | 9.353 |
| 218 | 19.361 | 19.370 | 19.379 | 19.385 | 19.397 | 19.406 | 19.415 | 19.129 | 19.-133 | 19.141 |
| 219 | 19.4.50 | 19.459 | 19.468 | $19.17 \%$ | 19.456 | 19.49.7 | 19.504 | 19.512 | 19.521 | 19.580 |
| 2.20 | 19.539 | 19.548 | 19.557 | 19.566 | 19.57. | 19.553 | 19.592 | 19.601 | 19.610 | 19.619 |
| $2 \cdot 1$ | 19.623 | 19.637 | 19.646 | 19.655 | 19.663 | 19.672 | 19.681 | 19.690 | 19.699 | 19.708 |
| 22.2 | 19.717 | 19.726 | 19.734 | 19.743 | 19.7.72 | 19.761 | 19.750 | 19.7\%9 | 19.788 | 19.797 |
| $2 \cdot 28$ | 19.806 | 19.811 | 19.52:3 | 19.532 | 19.840 | 19.850 | 19.559 | 19.865 | 19.87\% | 19.85 .5 |
| $2 \cdot 4$ | 19.994 | 19.903 | 19.912 | 19.921 | 19.930 | 19.939 | 19.948 | 19.957 | 19.965 | 19.974 |
| 2.).5 | $19.9 \leq 3$ | 19.992 | 20.001 | 20.010 | 20.019 | 20.02 s | 20.036 | 20.045 | 20.051 | 20.063 |
| 226 | 20.072 | 20.081 | 20.090 | 20.099 | 20.107 | 20.116 | 20.125 | 20.134 | 20.143 | 20.152 |
| 227 | 20.16 I | 20.170 | 20.179 | 20.187 | 20.196 | 20.205 | 20.214 | 20.223 | 20.232 | $20.2+1$ |
| 19 Inch. |  |  |  | 1 |  |  |  |  |  |  |
| 228 | 20.250 | 20.2 .75 | 20.267 | 20.276 | 20.25 .5 | 20.294 | 20.303 | 20.312 | 20.321 | 20.330 |
| $2 \cdot 9$ | 20.33 S | 20.317 | 20.3 .36 | 20.365 | 20.374 | 20.353 | 20.392 | 20.401 | 20.109 | 20.415 |
| 230 | 20.427 | 20.436 | 20.445 | 20.454 | 20.463 | 20.472 | 20.151 | 20.489 | 20.198 | $\because 0.507$ |
| 231 | 20.516 | 20.525 | 20.584 | 20.513 | 20.552 | 20.560 | 20.569 | 20.578 | 20.567 | 20.596 |
| 23.2 | 20.605 | 20.614 | 20.623 | 20.631 | 20.640 | 20.649 | 20.658 | 20.667 | 20.676 | 20.655 |
| 238 | 20.694 | 20.703 | 20.711 | 20.720 | 20.729 | 20.738 | 20.747 | 20.756 | 20.765 | 20.754 |
| 234 | 20.782 | 20.791 | 20.800 | 20.809 | 20.615 | 20.827 | 20.836 | 20.545 | 20.854 | 20.862 |
| 23.5 | 20.871 | 20.580 | 20.889 | 20.898 | 20.907 | 20.916 | 20.925 | 20.933 | 20.942 | 20.951 |
| 236 | 20.960 | 20.969 | 20.978 | 20.957 | 20.996 | 21.005 | 21.013 | 21.022 | 21.031 | 21.040 |
| 237 | 21.049 | 21.058 | 21.067 | 21.076 | 21.081 | 21.093 | 21.102 | 21.111 | 21.120 | 21.129 |
| 235 | 21.13 - | 21.147 | 21.155 | 21.164 | 21.173 | 21.182 | 21.191 | 21.200 | 21.209 | 21.218 |
| 239 | 21.227 | 21.235 | 21.244 | 21.253 | 21.262 | 21.271 | 21.280 | 21.289 | 21.292 | 21.806 |

Ifundredths of a Line.

| 0. | 1. | 2. | 3. | 4. | す. | 6. | \%. | 8. | (\%. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .000 | .001 | .002 | .003 | .004 | .004 | .005 | .006 | .007 | .008 |

1 Paris Line $=0.088814$ English Inch.

| French or ParisLines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 20 Inches. | Eng. In. | Eug. In. | Eng. In. | Eng. In. | Eng. In. | Evg. In. | g. In. | In. | ng. In. | In. |
| 240 | 21.315 | 21.324 | 21.333 | 21.342 | 21.351 | 21.360 | 21.369 | 21.375 | 21.386 | 21.395 |
| 241 | 21.104 | 21.413 | 21.422 | 21.431 | 21.440 | 21.449 | 21.457 | 21.466 | 21.475 | 21.484 |
| 212 | 21.493 | 21.502 | 21.511 | 21.520 | 21.529 | 21.537 | 21.546 | 21.555 | 21.564 | 21.573 |
| 243 | 21.582 | 21.591 | 21.600 | 21.608 | 21.617 | 21.626 | 21.635 | 21.644 | 21.653 | 21.662 |
| 244 | 21.671 | 21.679 | 21.688 | 21.697 | 21.706 | 21.715 | 21.724 | 21.733 | 21.742 | 21.751 |
| 245 | 21.759 | 21.765 | 21.777 | 21.756 | 21.795 | 21.504 | 21.813 | 21.522 | 21.830 | 21.839 |
| 246 | 21.819 | 21.957 | 21.866 | 21.875 | 21.884 | 21.593 | 21.902 | 21.910 | 21.919 | 21.928 |
| 217 | 21.937 | 21.946 | 21.95 .5 | 21.964 | 21.973 | 21.981 | 21.990 | 21.999 | 22.005 | 22.017 |
| 248 | 22.026 | 22.0335 | 22.044 | 22.053 | 22.061 | 22.070 | 22.079 | 22.088 | 22.097 | 22.106 |
| 219 | 22.11.5 | 22.124 | 22.132 | 22.141 | 22.150 | 22.159 | 22.168 | 22.177 | 22186 | 22.195 |
| 2.50 | 22.203 | 22.212 | 22.221 | 22.230 | 22.239 | 22.248 | 22.257 | 29.266 | 22.275 | 22.283 |
| 2.11 | 22.292 | 22.301 | 22.310 | 22.319 | 22.328 | 22.337 | 22.346 | 22.354 | 22.363 | 22.372 |
| $21 \mathrm{In} .=$ |  |  |  |  |  |  |  |  |  |  |
| 2.5 | 22.381 | 22.390 | 22.399 | 22.405 | 22.417 | 22.426 | 22.434 | 22.443 | 22.452 | 22.461 |
| 253 | 22.170 | 22.479 | 22.188 | 22.497 | 22.50.5 | 22.514 | 22.523 | 22.532 | 22.511 | 22.550 |
| 2.54 | 22.559 | 22.563 | 22.577 | 22.585 | 22.594 | 22.603 | 22.612 | 22.621 | 22.630 | 22.639 |
| 2.5 | 22.643 | 22.656 | 22.665 | 22.671 | 22.683 | 22.692 | 22.701 | 22.710 | 22.719 | 23.728 |
| 2.56 | 22.736 | 22.74.5 | 22.754 | 22.763 | 22.772 | 22.781 | 22.790 | 22.799 | 22.507 | 22.816 |
| 2.5 | 22.525 | 22.834 | 22.543 | 2.852 | 22.861 | 22.870 | 22.878 | 22.857 | 22.896 | 22.905 |
| 255 | 22.914 | 22.923 | 22.932 | 22.941 | 22.950 | 22.953 | 22.967 | 22.976 | 22.985 | 22.994 |
| 2.59 | 23.003 | 23.012 | 23.021 | 23.029 | 23.035 | 23.047 | 23.056 | 23.065 | 23.074 | 23.083 |
| 260 | 23.092 | 23.101 | 23.109 | 23.118 | 23.127 | 23.136 | 23.145 | 23.154 | 23.163 | 23.172 |
| 261 | 23.180 | 23.189 | 23.193 | 23.207 | 23.216 | 23.225 | 23.234 | 23.243 | 23.252 | 23.260 |
| 262 | 23.269 | 23.278 | 23.257 | 23.296 | 23.305 | 23.314 | 23.323 | 23.331 | 23.340 | 23.349 |
| 263 | 23.358 | 23.367 | 23.376 | 23.355 | 23.394 | 23.102 | 23.411 | 23.420 | 23.129 | 23.438 |
| $32 \mathrm{ln} .=$ |  |  |  |  |  |  |  |  |  |  |
| 264 | 23.447 | 23.456 | 23.465 | 23.474 | 23.182 | 23.191 | 23.500 | 23.509 | 23.518 | 23.527 |
| 26.3 | 23.536 | 23.54. | 23.553 | 23.562 | 23.571 | 23.580 | 23.589 | 23.598 | 23.607 | 23.616 |
| 266 | 23.625 | 23.6333 | 23.642 | 23.651 | 23.660 | 23.669 | 23.675 | 23.687 | 23.696 | 23.704 |
| 267 | 23.713 | 23.722 | 23.731 | 23.740 | 23.749 | 23.759 | 23.767 | 23.776 | 23.784 | 23.793 |
| 269 | 23.802 | 23.511 | 23.820 | 23.929 | 23.835 | 23.547 | 23.855 | 23.864 | 23.873 | 23.882 |
| 269 | 23.891 | 23.900 | 23.909 | 23.918 | 23.926 | 23.935 | 23.944 | 23.953 | 23.962 | 23.971 |
| 270 | 23.980 | 23.989 | 23.995 | 24.006 | 24.015 | 24.024 | 24.033 | 24.042 | 24.051 | 24.060 |
| 271 | 21.069 | 24.077 | 24.056 | 24.095 | 24.10 .1 | 24.113 | 24.122 | 24.131 | 24.140 | 24.149 |
| 272 | 21.157 | 24.166 | 24.17. | 24.184 | 21.193 | 24.202 | 24.211 | 24.220 | 24.228 | 24.237 |
| 273 | 21.246 | 24.25. | 21.264 | 24.273 | 24.252 | 24.291 | 24.300 | 24.308 | 24.317 | 24.326 |
| 274 | 21.335 | 24.344 | 24.353 | 21.362 | 24.371 | 24.379 | 24.388 | 24.397 | 24.406 | 24.415 |
| 275 | 24.421 | 24.433 | 24.442 | 24.450 | 24.459 | 24.468 | 24.477 | 24.486 | 24.49.5 | 24.504 |
|  |  |  |  |  |  |  |  |  |  |  |

Hundredths of a Line.


1 Paris Line $=0.08581 \pm$ English Inch.

| French or ParisLines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 23 Inches. | Eng. In. | Eng. In. | Eng. In. | Eng. Tr. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 276 | 24.513 | 24.522 | 24.530 | 24.539 | 24.548 | 24.557 | 24.566 | 24.575 | 24.584 | 24.593 |
| 277 | 24.601 | 24.610 | 24.619 | 24.628 | 24.637 | 24.646 | 24.655 | 24.664 | 24.673 | 24.681 |
| 278 | 24.690 | 24.699 | 24.703 | 24.717 | 24.726 | 24.735 | 24.744 | 24.752 | 24.761 | 24.770 |
| 279 | 24.779 | 24.788 | 24.797 | 24.806 | 24.815 | 24.824 | 24.532 | 24.841 | 24.850 | 24.559 |
| 280 | 24.868 | 24.577 | 24.586 | 24.895 | 24.903 | 24.912 | 24.921 | 24.930 | 24.939 | 24.945 |
| 231 | 24.957 | 24.966 | 24.974 | 24.983 | 24.992 | 25.001 | 25.010 | 25.019 | 25.028 | 25.037 |
| 282 | 25.046 | 25.054 | 25.063 | 25.072 | 25.681 | 25.090 | 25.099 | 25.108 | 25.117 | 25.125 |
| 283 | 25.131 | 25.143 | 25.152 | 25.161 | 25.170 | 25.179 | 25.188 | 25.197 | 25.205 | 25.214 |
| 284 | 25.223 | 25.232 | 25.241 | 25.250 | 25.259 | 25.265 | 25.276 | 25.285 | 25.294 | 25.303 |
| 285 | 25.312 | 25.321 | 25.330 | 25.339 | 25.348 | 25.356 | 25.365 | 25.374 | 25.383 | 25.392 |
| 286 | 25.401 | 25.410 | 25.419 | 25.427 | 25.436 | 25.445 | 25.454 | 25.463 | 25.472 | 25.481 |
| 287 | 25.490 | 25.498 | 25.507 | 25.516 | 25.525 | 25.534 | 25.513 | 25.552 | 25.561 | 25.570 |
| 24.10 |  |  |  |  |  |  |  |  |  |  |
| 288 | 25.578 | 25.587 | 25.596 | 25.605 | 25.614 | 25.623 | 25.632 | 25.641 | 25.649 | 25.658 |
| 289 | 25.667 | 25.676 | 25.655 | 25.694 | 25.703 | 25.712 | 25.721 | 25.729 | 25.738 | 25.747 |
| 290 | 25.756 | 25.765 | 25.784 | 25.783 | 25.792 | 25.800 | 25.809 | 25.518 | 25.827 | 25.536 |
| 291 | 25.845 | 25.554 | 25.863 | 25.872 | 25.880 | 25.589 | 25.898 | 25.907 | 25.916 | 25.925 |
| 292 | 25.934 | 25.943 | 25.951 | 25.960 | 25.969 | 25.978 | 25.987 | 25.996 | 26.005 | 26.014 |
| 293 | 26.023 | 26.031 | 26.040 | 26.049 | 26.058 | 26.067 | 26.076 | 26.085 | 26.094 | 26.102 |
| 294 | 26.111 | 26.120 | 26.129 | 26.138 | 26.147 | 26.156 | 26.165 | 26.173 | 26.182 | 26.191 |
| 295 | 26.200 | 26.209 | 26.218 | 26.227 | 26.236 | 26.245 | 26.253 | 26.262 | 26.271 | 26.280 |
| 296 | 26.289 | 26.298 | 26.307 | 26.316 | 26.324 | 26.333 | 26.342 | 26.351 | 26.360 | 26.369 |
| 297 | 26.378 | 26.387 | 26.396 | 26.404 | 26.413 | 26.122 | 26.431 | 26.440 | 26.449 | 26.458 |
| 298 | 26.467 | 26.475 | 26.484 | 26.493 | 26.50 3 | 26.511 | 26.520 | 26.529 | 26.538 | 26.547 |
| 299 | 26.555 | 26.564 | 26.573 | 26.582 | 26.591 | 26.600 | 26.609 | 26.618 | 26.626 | 26.635 |
| $25 \mathrm{In} .=$ |  |  |  |  |  |  |  |  |  |  |
| 300 | 26.644 | 26.653 | 26.662 | 26.671 | 26.680 | 26.689 | 26.697 | 26.706 | 26.715 | 26.724 |
| 301 | 26.733 | 26.742 | 26.751 | 26.760 | 26.769 | 26.777 | 26.786 | 26.795 | 26.804 | 26.813 |
| 302 | 26.822 | 26.831 | 26.840 | 26.848 | 26.857 | 26.566 | 26.575 | 26.854 | 26.593 | 26.902 |
| 303 | 26.911 | 26.920 | 26.928 | 26.937 | 26.946 | 26.955 | 26.964 | 26.973 | 26.982 | 26.991 |
| 304 | 26.999 | 27.008 | 27.017 | 27.026 | 27.085 | 27.044 | 27.053 | 27.062 | 27.071 | 27.079 |
| 305 | 27.083 | 27.097 | 27.106 | 27.115 | 27.124 | 27.133 | 27.142 | 27.150 | 27.159 | 27.168 |
| 306 | 27.177 | 27.186 | 27.195 | 27.204 | 27.213 | 27.221 | 27.230 | 27.239 | 27.248 | 27.257 |
| 307 | 27.266 | 27.275 | 27.284 | 27.293 | 27.301 | 27.310 | 27.319 | 27.328 | 27.337 | 27.346 |
| 308 | 27.355 | 27.364 | 27.372 | 27.381 | 27.390 | 27.399 | 27.408 | 27.417 | 27.426 | 27.435 |
| 309 | 27.44\% | 27.452 | 27.461 | 27.470 | 27.479 | 27.488 | 27.497 | 27.506 | 27.515 | 27.523 |
| 310 | 27.532 | 27.541 | 27.550 | 27.559 | 27.568 | 27.577 | 27.586 | 27.595 | 27.603 | 27.612 |
| 311 | 27.621 | 27.630 | 27.639 | 27.648 | 27.657 | 27.666 | 27.674 | 27.683 | 27.692 | 27.701 |
|  |  |  |  |  |  |  |  |  |  |  |

Hundredths of a Line.

| $\mathbf{0 .}$ | $\mathbf{1 .}$ | $\mathbf{2 .}$ | $\mathbf{3 .}$ | $\mathbf{4 .}$ | $\mathbf{\text { 5. }}$ | 6. | \%. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .0000 | .0009 | .0018 | .0027 | .0036 | .0044 | .0053 | .0062 | .0071 | .0080 |

1 Paris Line $=0.088814$ English Inch.

| French or ParisLines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 \% | 8. | 9. |
| 26 Inches. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | n. |
| 312 | 27.710 | 27.719 | 27.728 | 27.737 | 27.745 | 27.754 | 27.763 | 27.772 | 27.781 | 27.790 |
| 313 | 27.799 | 27.808 | 27.817 | 27.825 | 27.834 | 27.843 | 27.852 | 27.861 | 27.870 | 27.879 |
| 314 | 27.883 | 27.896 | 27.905 | 27.914 | 27.923 | 27.932 | 27.941 | 27.950 | 27.959 | 27.968 |
| 315 | 27.976 | 27.985 | 27.994 | 28.003 | 28.012 | 28.021 | 28.030 | 28.039 | 28.047 | 28.056 |
| 316 | 28.065 | 28.074 | 28.083 | 28.092 | 28.101 | 28.110 | 28.119 | 28.127 | 28.136 | 28.145 |
| 317 | 28.154 | 28.163 | 28.172 | 28.181 | 28.190 | 28.198 | 28.207 | 28.216 | 28.225 | 28.234 |
| 318 | 28.243 | 28.252 | 23.261 | 28.269 | 28.278 | 28.287 | 28.296 | 28.305 | 28.314 | 28.323 |
| 319 | 29.332 | 28.341 | 28.349 | 25.358 | 28.367 | 28.376 | 28.385 | 28.394 | 28.403 | 28.412 |
| 320 | 28.420 | 28.429 | 28.438 | 28.447 | 28.456 | 28.465 | 28.474 | 28.483 | 28.492 | 28.500 |
| 321 | 28.509 | 28.518 | 28.527 | 28.536 | 28.545 | 25.554 | 28.563 | 28.571 | 28.580 | 28.589 |
| 322 | 28.593 | 28.607 | 28.616 | 28.625 | 28.634 | 28.643 | 28.651 | 28.660 | 28.669 | 28.678 |
| 323 | 28.687 | 28.696 | 28.705 | 28.714 | 28.722 | 28.731 | 25.740 | 28.749 | 28.758 | 28.767 |
| $27 \mathrm{In} .=$ |  |  |  |  |  |  |  |  |  |  |
| 324 | 28.776 | 28.785 | 23.793 | 28.802 | 28.811 | 28.820 | 28.829 | 28.838 | 28.847 | 28.856 |
| 325 | 28.865 | 28.873 | 28.582 | 28.891 | 23.900 | 28.909 | 28.918 | 28.927 | 28.936 | 28.944 |
| 326 | 28.953 | 28.962 | 28.971 | 28.980 | 28.989 | 28.998 | 29.007 | 29.016 | 29.024 | 29.03:3 |
| 327 | 29.042 | 29.051 | 29.060 | 29.069 | 29.078 | 29.087 | 29.095 | 29.104 | 29.113 | 29.122 |
| 328 | 29.131 | 29.140 | 29.149 | 29.158 | 29.167 | 29.175 | 29.184 | 29.193 | 29.202 | 29.211 |
| 329 | 29.220 | 29.229 | 29.238 | 29.246 | 29.255 | 29.264 | 29.273 | 29.282 | 29.291 | 29.300 |
| 330 | 29.309 | 29.318 | 29.326 | 29.335 | 29.344 | 29.353 | 29.362 | 29.371 | 29.380 | 29.389 |
| 331 | 29.397 | 29.406 | 29.415 | 29.424 | 29.433 | 29.442 | 29.451 | 29.460 | 29.468 | 29.477 |
| 332 | 29.486 | 29.495 | 29.504 | 29.513 | 29.522 | 29.531 | 29.540 | 29.548 | 29.557 | 29.566 |
| 333 | 29.575 | 29.584 | 29.593 | 29.602 | 29.611 | 29.619 | 29.628 | 29.637 | 29.646 | 29.655 |
| 334 | 29.664 | 29.673 | 29.682 | 29.691 | 29.699 | 29.708 | 29.717 | 29.726 | 29.735 | 29.744 |
| 335 | 29.753 | 29.762 | 29.770 | 29.779 | 29.788 | 29.797 | 29.806 | 29.815 | 29.824 | 29.833 |
| $28 \mathrm{In} .=$ |  |  |  |  |  |  |  |  |  |  |
| 336 | 29.842 | 29.850 | 29.859 | 29.568 | 29.577 | 29.886 | 29.895 | 29.904 | 29.913 | 29.921 |
| 337 | 29.930 | 29.939 | 29.948 | 29.957 | 29.966 | 29.975 | 29.984 | 29.992 | 30.001 | 30.010 |
| 338 | 30.019 | 30.029 | 30.037 | 30.046 | 30.055 | 30.064 | 30.072 | 30.081 | 30.090 | 30.099 |
| 339 | 30.108 | 30.117 | 30.126 | 30.135 | 30.143 | 30.152 | 30.161 | 30.170 | 30.179 | 30.188 |
| 340 | 30.197 | 30.206 | 30.215 | 30.223 | 30.232 | 30.241 | 30.250 | 30.259 | 30.268 | 30.277 |
| 341 | 30.286 | 30.294 | 30.303 | 30.312 | 30.321 | 30.330 | 30.339 | 30.348 | 30.357 | 30.366 |
| 342 | 30.374 | 30.383 | 30.392 | 30.401 | 30.410 | 30.419 | 30.428 | 30.437 | 30.445 | 30.454 |
| 343 | 30.463 | 30.472 | 30.481 | 30.490 | 30.499 | 30.508 | 30.516 | 30.525 | 30.534 | 30.543 |
| 344 | 30.552 | 30.561 | 30.570 | 30.579 | 30.588 | 30.596 | 30.605 | 30.614 | 30.623 | 30.632 |
| 345 | 30.641 | 30.650 | 30.659 | 30.667 | 30.676 | 30.685 | 30.694 | 30.703 | 30.712 | 30.721 |
| 346 | 30.730 | 30.739 | 30.747 | 30.756 | 30.765 | 30.774 | 30.783 | 30.792 | 30.801 | 39.810 |
| 347 | 30.818 | 30.827 | 30.836 | 30.845 | 30.854 | 30.863 | 30.872 | 30.881 | 30.590 | 30.898 |
| $\begin{gathered} 29 \mathrm{In} .= \\ 348 \end{gathered}$ | 30.907 | 30.916 | 30.925 | 30.934 | 30.943 | 30.952 | 30.961 | 30.969 | 30.978 | 30.987 |

Mundredths of a Line.


1 Paris Line $=2.255829$ Milimetres

| French or ParisLines. Tens. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{gathered} 10 \text { Inch. } \\ 120 \end{gathered}$ | Millim. $270.70$ | $\begin{aligned} & \text { Millim. } \\ & 272.96 \end{aligned}$ | Millim. <br> 27.5.21 | Millim. <br> 277.47 | $\begin{gathered} \text { Millim. } \\ 279.72 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 281.98 \end{aligned}$ | Millim. 284.2 .3 | Millim. <br> 256.49 | Millim. $250.7 .5$ | Millim. $291.00$ |
| 130 | 293.26 | 295.51 | 297.77 | 300.03 | 302.28 | 304.54 | 306.79 | 309.05 | 311.30 | 313.56 |
| 140 | 315.82 | 318.07 | 320.33 | 32.58 | 324.54 | 327.10 | 329.35 | 331.61 | 333.56 | 336.12 |
| 150 | 335.37 | 340.63 | 312.59 | 345.14 | 347.40 | 349.65 | 3.51 .91 | 354.17 | 3.56 .42 | 358.68 |
| 160 | 360.93 | 363.19 | 365.44 | 367.70 | 369.96 | 372.21 | 374.47 | 376.72 | :75.95 | 381.24 |
| 170 | 383.49 | 385.75 | 338.00 | 390.26 | 392.51 | 394.77 | 397.03 | 399.28 | 401.54 | 403.79 |
| 180 | 406.0.5 | 408.30 | 410.56 | 412.52 | 415.07 | 417.33 | 419.58 | 421.84 | 424.10 | 426.35 |
| 190 | 425.61 | 430.86 | 433.12 | 435.37 | 4:7.63 | 439.59 | 442.14 | +4.40 | +16.65 | +48.91 |
| 200 | 451.17 | 453.42 | 45.5 .65 | 457.93 | 460.19 | 462.44 | 464.70 | 466.96 | 469.21 | 471.47 |
| 210 | +73.72 | 475.95 | 478.24 | 480.49 | 482.75 | 485.00 | 487.26 | 489.51 | 491.77 | 494.03 |
|  |  |  |  |  | Tenths | a Line. |  |  |  |  |
| Paris Lines. | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 18 Inch. | Nillim. <br> $+87.26$ |  | Millim. |  | Millim. | Millim. | Millim. <br> 488.61 | Millim. 188.84 | Millim. 159.06 | Millim. 189.99 |
|  |  |  |  |  |  |  |  | 491.09 | 491.32 |  |
| 217 |  | 459.74 | 489.97 | 490.19 | 490.42 | 490.64 | 490.87 | 491.09 | 491.32 | 491.5.) |
| 218 | 491.77 | 492.00 | 492.22 | 492.45 | 492.67 | 492.90 | 493.12 | 493.35 | 493.58 | 493.80 |
| 219 | 494.03 | 494.25 | 494.48 | 494.70 | 494.93 | 495.15 | 495.38 | 495.61 | 495.83 | 496.06 |
| 220 | 496.28 | 496.51 | 496.73 | 496.96 | 497.18 | 497.41 | 497.64 | 497.86 | 498.09 | 498.31 |
| 221 | 498.54 | 498.76 | 498.99 | 499.21 | 499.44 | 499.67 | 499.89 | 500.12 | 500.34 | 500.57 |
| 222 | 500.79 | 501.02 | 501.25 | 501.47 | 501.70 | 501.92 | 502.15 | 502.37 | 502.60 | 502.82 |
| 223 | 503.05 | 503.28 | 503.50 | 503.73 | 503.9. | 504.18 | 504.40 | 504.63 | 504.85 | 505.08 |
| 224 | 505.31 | 505.53 | 505.76 | 505.98 | 506.21 | 506.43 | 506.66 | 506.88 | 507.11 | 507.34 |
| 225 | 507.56 | 507.79 | 508.01 | 508.24 | 508.46 | 508.69 | 508.91 | 509.14 | 509.37 | 509.59 |
| 226 | -509.82 | 510.04 | 510.27 | 510.49 | 510.72 | 510.95 | 511.17 | 511.40 | 511.62 | 511.65 |
| 227 | 512.07 | 512.30 | 512.52 | 512.75 | 512.98 | 513.20 | 513.43 | 513.65 | 513.88 | 514.10 |
| 19 Inch. |  |  |  |  |  |  |  |  |  |  |
| 228 | 514.33 | 514.55 | 514.78 | 515.01 | 515.23 | 515.46 | 515.68 | 515.91 | 516.13 | 516.36 |
| 229 | 516.58 | 516.81 | 517.04 | 517.26 | 517.49 | 517.71 | 517.94 | 518.16 | 518.39 | 518.61 |
| 230 | 518.84 | 519.07 | 519.29 | 519.52 | 519.74 | 519.97 | 520.19 | 520.42 | 520.65 | 520.87 |
| 231 | 521.10 | 521.32 | 521.55 | 521.77 | 522.00 | 522.22 | 522.45 | 522.68 | 522.90 | 523.13 |
| 232 | 523.35 | 523.58 | 523.80 | 524.03 | 52-4.25 | 524.48 | 524.71 | 524.93 | 525.16 | 525.38 |
| 233 | 525.61 | 525.83 | 526.06 | 526.28 | 526.51 | 526.74 | 526.96 | 527.19 | 527.41 | 527.64 |
| 234 | 527.86 | 528.09 | $52 \mathrm{S.32}$ | 525.54 | 528.77 | 528.99 | 529.22 | 529.44 | 529.67 | 529.89 |
| 235 | 530.12 | 530.35 | 530.57 | 530.80 | 531.02 | 531.25 | 531.47 | 531.70 | 531.92 | 532.15 |
| 236 | 532.38 | 532.60 | 532.83 | 533.05 | 533.28 | 533.50 | 533.73 | 533.95 | 534.18 | 534.41 |
| 237 | 534.63 | 534.86 | 535.08 | 535.31 | 535.53 | 535.76 | 535.98 | 536.21 | 536.44 | 536.66 |
| 238 | 536.59 | 537.11 | 537.34 | 537.56 | 537.79 | 538.02 | 539.24 | 538.47 | 538.69 | 538.92 |
| 239 | 539.14 | 539.37 | 539.59 | 539.82 | 540.05 | 540.27 | 540.50 | 540.72 | 540.95 | 541.17 |

Tenths of a Line.

| 0. | 1. | 2. | 3. | 4. | 5. | 6. | \%. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 0.23 | 0.45 | 0.68 | 0.90 | 1.13 | 1.35 | 1.5 s | 1.80 | 2.03 |

1 Paris Line $=2.255829$ Millimetres.

| Paris or French Lines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 20 Inches. | Millim. | Millim. | Millim. | Nillim. | Millim. | Iillim. | Millim. | Millim. | Millim. | Millim. |
| 210 | 541.40 | 541.62 | 541.8 .5 | 512.08 | 542.30 | 512.53 | 542.75 | 542.98 | 543.20 | 543.43 |
| 211 | 543.65 | 543.85 | 544.11 | 544.33 | 544.56 | 544.78 | 545.01 | 545.23 | 545.46 | 545.69 |
| 212 | 54.5 .91 | 546.14 | 546.36 | 546.59 | 546.81 | 517.04 | 547.26 | 547.19 | 517.72 | 547.9 .1 |
| 24.3 | 543.17 | 548.39 | 518.62 | 5-n.S | 549.67 | -19.29 | 549.52 | 549.75 | 549.97 | 550.20 |
| 244 | 550.42 | 550.65 | 5.50 .87 | 551.10 | 551.32 | 551.55 | 551.75 | 552.00 | 552.23 | 552.45 |
| 245 | 552.68 | 552.90 | 553.13 | 5.53 .35 | 553.58 | 553.81 | 554.03 | 554.26 | 554.48 | 554.71 |
| 2.16 | 5.54 .93 | 55.5 .16 | 55.5 .39 | 555.61 | 555.84 | 556.06 | 556.29 | 556.51 | 556.74 | 556.96 |
| 217 | 557.19 | 557.42 | 557.61 | 557.87 | 558.09 | 558.32 | 558.54 | 5.58 .77 | 558.99 | 559.22 |
| 248 | 5.59 .45 | 559.67 | 559.90 | 560.12 | 560.35 | 560.57 | 560.80 | 561.02 | 561.25 | 561.45 |
| 249 | 561.70 | 561.93 | 56\%.15 | 562.38 | 562.60 | 562.83 | 563.05 | 563.28 | 563.51 | 563.73 |
| 2.50 | 563.96 | 564.15 | 564.41 | 564.63 | 564.86 | 565.09 | 56.5 .31 | 56.5 .54 | 56.5 .76 | 565.99 |
| 2.31 | 566.21 | 566.44 | $566.6{ }^{\circ}$ | 566.59 | 567.12 | 567.34 | 567.57 | 567.79 | 568.02 | 568.24 |
| 21 Inches. 2.52 | 568.47 | 568.69 | 568.92 | 569.15 | 569.37 | 569.60 | 569.82 | 570.05 | 570.27 | 570.50 |
| 25.3 | 570.72 | 570.95 | 571.18 | 571.40 | 571.63 | 571.85 | 572.08 | 572.30 | 572.53 | 572.75 |
| 254 | 572.98 | 573.21 | 573.43 | 573.66 | 573.88 | 574.11 | 574.83 | 574.56 | 574.79 | 575.01 |
| 25.5 | 575.24 | 575.46 | 575.69 | 575.91 | 576.14 | 576.36 | 576.59 | 576.82 | 577.04 | 577.27 |
| 256 | 577.49 | 577.72 | 577.94 | 578.17 | 578.39 | 578.62 | 575.85 | 579.07 | 579.30 | 579.52 |
| 257 | 579.75 | 579.97 | 580.20 | 580.42 | 550.65 | 580.85 | 581.10 | 581.33 | 581.55 | 581.78 |
| 258 | 582.00 | 582.33 | 592.46 | 582.68 | 582.91 | 583.13 | 583.36 | 583.5S | 553.81 | 584.03 |
| 259 | 584.26 | 584.49 | 584.71 | 584.94 | 585.16 | 585.39 | 585.61 | 585.84 | 586.06 | 586.29 |
| 260 | 586.52 | 586.74 | 556.97 | 587.19 | 587.42 | 587.64 | 587.8 | 588.09 | 588.32 | 588.55 |
| 261 | 588.77 | 589.00 | 589.22 | 589.45 | 589.67 | 589.90 | 590.12 | 590.35 | 590.58 | 590.80 |
| 26.2 | 591.03 | 591.25 | 591.18 | 591.70 | 591.93 | 592.16 | 592.38 | 592.61 | 592.83 | 593.06 |
| 263 | 593.28 | 593.51 | 593.73 | 593.96 | 594.19 | 594.41 | $59+.64$ | 594.86 | 595.09 | 595.31 |
| $2 \boldsymbol{2}$ Inches. 264 |  | 59 | 595.99 | 596. | 596.14 |  | 596 | 597. | 597.34 | 597.57 |
|  |  | 59 | 595.99 | 596. | 596.44 |  | 596 | .97 | 597 | 597.07 |
| 265 | 597.79 | 598.02 | 545.25 | 598.47 | 598.70 | 598.92 | 599.15 | 599.37 | 599.60 | 599.82 |
| 266 | 600.05 | 600.28 | 600.50 | 600.73 | 600.95 | 601.18 | 601.40 | 601.63 | 601.86 | 602.08 |
| 267 | 602.31 | 602.53 | 602.76 | 602.98 | 603.21 | 603.43 | 603.66 | 603.89 | 604.11 | 604.34 |
| 265 | 604.56 | 604.79 | 605.01 | 60.5 .24 | 605.46 | 605.69 | 605.92 | 606.11 | 606.37 | 606.59 |
| 269 | 606.82 | 607.04 | 607.27 | 607.49 | 607.72 | 607.95 | 608.17 | 608.10 | 605.62 | 608.55 |
| 270 | 609.07 | 609.30 | 609.52 | 609.75 | 609.98 | 610.20 | 610.43 | 610.65 | 610.85 | 611.10 |
| 271 | 611.38 | 611.56 | 611.78 | 612.01 | 612.23 | 612.46 | 612.68 | 612.91 | 613.13 | 613.36 |
| 272 | 613.59 | 613.81 | 614.04 | 614.26 | 614.49 | 614.71 | 614.94 | 615.16 | 615.39 | 615.62 |
| 273 | 615.84 | 616.07 | 616.29 | 616.52 | 616.74 | 616.97 | 617.19 | 617.42 | 617.65 | 617.87 |
| 274 | 615.10 | 619.32 | 618.55 | 618.77 | 619.00 | 619.23 | 619.45 | 619.68 | 619.90 | 620.13 |
| 275 | 620.35 | 620.55 | 620.50 | 6:21.03 | 621.26 | 621.48 | 621.71 | 621.93 | 622.16 | 622.38 |

Hundredths of a Line.

| 0. | 1. | 2. | 3. | 4. | お. | 6. | 7. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.000 | 0.023 | 0.045 | 0.068 | 0.090 | 0.113 | 0.135 | 0.158 | 0.180 |

1 Paris Line $=2.255829$ Millimetres.

| Paris or French Lines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | ¢. |
| 23 Inches. | Millim. | Millim. | Millim. | Millim. |  | lillim. | Millim. | Millim. | Millim. | Millim. |
| 276 | 622.61 | 622.83 | 623.06 | 623.29 | 623. | 623.74 | 623.96 | 624.19 | 624.41 | 624.64 |
| 277 | 624.56 | 625.09 | 625.32 | 625.54 | 625.77 | 625.99 | 626.22 | 626.44 | 626.67 | 626.59 |
| 278 | 627.12 | 627.35 | 627.57 | 627.80 | 628.02 | 628.25 | 628.47 | 628.70 | 628.93 | 629.15 |
| 279 | 629.38 | 629.60 | 629.83 | 630.05 | 630.28 | 630.50 | 630.73 | 630.96 | 6:31.18 | 631.41 |
| 280 | 631.63 | 631.86 | 632.08 | 632.31 | 632.53 | 632.76 | 632.99 | 633.21 | 633.14 | 633.66 |
| 231 | 633.89 | 634.11 | 634.34 | 634.56 | 634.79 | 635.02 | 635.24 | 635.47 | 635.69 | 635.92 |
| 252 | 636.14 | 636.37 | 636.59 | 636.52 | 637.05 | 637.27 | 637.50 | 637.72 | 637.95 | 638.17 |
| 283 | 638.40 | 638.63 | 638.85 | 639.05 | 639.30 | 639.53 | 639.75 | 639.98 | 640.20 | 640.43 |
| 284 | 640.66 | 640.83 | 641.11 | 641.33 | 641.56 | 641.78 | 642.01 | 642.23 | 643.16 | 642.69 |
| 285 | 642.91 | 643.14 | 643.36 | 643.59 | 643.81 | 644.04 | 644.26 | 644.49 | 644.72 | 644.94 |
| 286 | 645.17 | 64.5.39 | 645.62 | 645.84 | 646.07 | 646.30 | 646.52 | 646.75 | 646.97 | 647.20 |
| 297 | 617.42 | 647.65 | 647.87 | 648.10 | 648.33 | 648.55 | 648.78 | 649.00 | 649.23 | 649.45 |
| 2finches. |  |  |  |  |  |  |  |  |  |  |
| 288 | 649.68 | 649.90 | 650.13 | 650.36 | 650.58 | 650.81 | 651.03 | 651.26 | 651.48 | 651.71 |
| 289 | 651.93 | 652.16 | 652.39 | 652.61 | 652.84 | 653.06 | 653.29 | 653.51 | 653.74 | 653.96 |
| 290 | 6.54 .19 | 654.42 | 654.64 | 654.87 | 655.09 | 655.32 | 655.54 | 655.77 | 656.00 | 6.56 .22 |
| 291 | 656.45 | 656.67 | 656.90 | 657.12 | 657.35 | 657.57 | 657.80 | 658.03 | 658.25 | 658.48 |
| 292 | 6.58 .70 | 658.93 | 659.15 | 659.38 | 659.60 | 659.83 | 660.06 | 660.28 | 660.51 | 660.73 |
| 293 | 660.96 | 661.18 | 661.41 | 661.63 | 661.86 | 662.09 | 662.31 | 662.54 | 662.76 | 662.99 |
| 294 | 663.21 | 663.44 | 663.66 | 663.89 | 664.12 | 664.34 | 664.57 | 664.79 | 665.02 | 665.24 |
| 295 | 665.47 | 665.70 | 665.92 | 666.15 | 666.37 | 666.60 | 666.82 | 667.05 | 667.27 | 667.50 |
| 296 | 667.73 | 667.95 | 66 S .18 | 665.10 | 663.63 | 668.85 | 669.08 | 669.30 | 669.53 | 669.76 |
| 297 | 669.98 | 670.21 | 670.43 | 670.66 | 670.58 | 671.11 | 671.33 | 671.56 | 671.79 | 672.01 |
| 298 | 672.24 | 672.46 | 672.69 | 672.91 | 673.14 | 673.36 | 673.59 | 673.82 | 674.04 | 674.27 |
| 299 | 674.49 | 674.72 | 674.94 | 675.17 | 675.40 | 675.62 | 675.85 | 676.07 | 676.30 | 676.52 |
| $\begin{gathered} 25 \text { Inches. } \\ 300 \end{gathered}$ | 676.75 | 676.97 | 677.20 | 677.43 | 677.65 | 677.83 | 678.10 | 673.33 | 678.55 | 678.78 |
| 301 | 679.00 | 679.23 | 679.46 | 679.68 | 679.91 | 680.13 | 650.36 | 680.58 | 680.81 | 681.03 |
| 302 | 651.26 | 651.49 | 681.71 | 651.94 | 682.16 | 682.39 | 682.61 | 652.84 | 683.07 | 683.29 |
| 303 | 683.52 | 68:3.74 | 683.97 | 684.19 | 684.42 | 684.64 | 684.57 | 68.5 .10 | 685.32 | 685.55 |
| 304 | 655.77 | 686.00 | 656.22 | 656.45 | 656.67 | 636.90 | 657.13 | 657.35 | 687.58 | 657.80 |
| 305 | 685.03 | 688.25 | 688.48 | 688.70 | 688.93 | 659.16 | 689.38 | 689.61 | 689.83 | 690.06 |
| 306 | 690.28 | 690.51 | 690.73 | 690.96 | 691.19 | 691.41 | 691.64 | 691.86 | 692.09 | 692.31 |
| 307 | 692.54 | 692.77 | 692.99 | 693.22 | 693.44 | 693.67 | 693.89 | 694.12 | 694.34 | 694.57 |
| 308 | 694.80 | 695.02 | 695.25 | 695.47 | 695.70 | 69.5 .92 | 696.15 | 696.37 | 696.60 | 696.83 |
| 309 | 697.05 | 697.28 | 697.50 | 697.73 | 697.95 | 698.18 | 698.40 | 695.63 | 698.86 | 699.08 |
| 310 | 699.31 | 699.53 | 699.76 | 699.98 | 700.21 | 700.43 | 700.66 | 700.89 | 701.11 | 701.3-1 |
| 311 | 701.56 | 701.79 | 702.01 | 702.24 | 702.47 | 702.69 | 702.92 | 703.14 | 703.37 | 703.59 |

Hundredths of a Line.

| 0. | 1. | 2. | 3. | 4. | 5. | 6. | \%. | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 0.023 | 0.045 | 0.068 | 0.090 | 0.113 | 0.135 | 0.158 | 0.180 | 0.203 |

1 Paris Line $=2.255829$ Millimetres.

| Paris or French Lines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 26 Incbes. | Millim. | Millim. | Millinn. | Mill | Milli | Nillim. | . | Nillim. | Millim. | Nillim. |
| 312 | 703.82 | 704.04 | 704.27 | 704.50 | 704.72 | 704.95 | 705.17 | 705.40 | 705.62 | 705.85 |
| 313 | 706.07 | 706.30 | 706.53 | 706.75 | 706.98 | 707.20 | 707.43 | 707.65 | 707.88 | 708.10 |
| 314 | 705.33 | 705.56 | 708.75 | 7199.01 | 709.23 | 709.46 | 709.68 | 709.91 | 710.13 | 710.36 |
| 315 | 710.59 | 710.81 | 711.04 | 711.26 | 711.49 | 711.71 | 711.94 | 712.17 | 712.39 | 712.62 |
| 316 | 712.54 | 713.07 | 713.29 | 713.52 | 713.74 | 713.97 | 714.20 | 714.42 | 714.65 | 714.57 |
| 317 | 715.10 | 715.32 | 715.53 | 715.77 | 716.00 | 716.23 | 716.45 | 716.68 | 716.90 | 717.13 |
| 318 | 717.35 | 717.58 | 717.50 | 718.03 | 718.26 | 718.48 | 718.71 | 718.93 | 719.16 | 719.35 |
| 319 | 719.61 | 719.84 | 720.06 | 720.29 | 720.51 | 720.74 | 720.96 | 721.19 | 721.41 | 721.64 |
| 320 | 721.57 | 723.09 | 722.32 | 72.2 .54 | 722.77 | 722.99 | 723.22 | 723.44 | 723.67 | 723.90 |
| 321 | 724.12 | 724.35 | 724.57 | 724.80 | 725.02 | 725.25 | 725.47 | 725.70 | 725.93 | 726.15 |
| 322 | 726.35 | 726.60 | 726.53 | 727.05 | 727.25 | 727.50 | 727.73 | 727.96 | 728.18 | 728.41 |
| 323 | 728.63 | 728.86 | 729.08 | 729.31 | 729.54 | 729.76 | 729.99 | 730.21 | 730.44 | 730.66 |
| 27 Inches. |  |  |  |  |  |  |  |  |  |  |
| 325 |  | 731.11 | 731 | 731.5 | 731.79 | 732.02 | 73 | 732.47 | 732.69 | 2 |
|  |  |  |  |  |  |  | \% 3 | 734.72 | \%34. | 735.17 |
|  | 735.40 | 735.63 | 735.85 | 736.08 | 736.30 | 736.53 | 736.75 | 736.98 | 737.20 | 737.43 |
| 327 | 737.66 | 737.88 | 739.11 | 735.33 | 738.56 | 735.78 | 739.01 | 739.24 | 739.46 | 739.69 |
| 323 | 739.91 | 740.14 | 740.36 | 740.59 | 740.81 | 741.04 | 741.27 | 741.49 | 741.72 | 741.94 |
| 329 | 742.17 | 742.39 | 742.62 | 742.84 | 743.07 | 743.30 | 743.52 | 743.75 | 743.97 | 744.20 |
| 330 | 744.42 | 744.65 | $7+4.87$ | 745.10 | 745.33 | 745.55 | 745.78 | 746.00 | 746.23 | 746.45 |
| 331 | 746.65 | 746.90 | 747.13 | 747.36 | 747.58 | 717.81 | 745.03 | 748.26 | 748.48 | 748.71 |
| 332 | 75.94 | 749.16 | 749.39 | 719.61 | 749.54 | 750.06 | 750.29 | 750.51 | 750.74 | 750.97 |
| 333 | 7.51 .19 | 751.42 | 751.64 | 751.87 | 752.09 | 752.32 | 752.54 | 752.77 | 753.00 | 753.22 |
| 334 | 733.45 | 753.67 | 753.90 | 754.12 | 754.3.5 | 754.57 | 754.80 | 755.03 | 755.25 | 755.48 |
| 33.5 | 755.70 | 755.93 | 756.15 | 756.38 | 756.61 | 756.83 | 757.06 | 757.28 | 757.51 | 757.73 |
| 2x Inches. |  |  |  |  |  |  |  |  |  |  |
| 336 | 757.96 | 759.18 | 758.41 | 7.58 .64 | 758.86 | 759.09 | 759.31 | 759.54 | 759.76 | 759.99 |
| 337 | 760.21 | 760.44 | 760.67 | 760.89 | 761.12 | 761.34 | 761.57 | 761.79 | 762.02 | 762.24 |
| 338 | 762.47 | 762.70 | 762.92 | 763.15 | 763.37 | 763.60 | 763.5. | 764.05 | 764.27 | 764.50 |
| 339 | 764.73 | 764.95 | 765.18 | 76.5 .40 | 765.63 | 765.55 | 766.08 | 766.31 | 766.53 | 766.76 |
| 340 | 766.93 | 767.21 | 767.43 | 767.66 | 767.58 | 765.11 | 768.34 | 765.56 | 768.79 | 769.01 |
| 341 | 769.24 | 769.46 | 769.69 | 769.91 | 770.14 | 770.37 | 770.59 | 770.82 | 771.04 | 771.27 |
| 342 | 771.49 | 771.72 | 771.94 | 772.17 | 772.40 | 772.62 | 772.55 | 773.07 | 773.30 | 773.52 |
| 343 | 783.75 | 773.97 | 734.20 | 754.43 | 784.65 | 774.58 | 775.10 | 77.5 .33 | 775.55 | 775.75 |
| 344 | T76.0] | 776.23 | 776.46 | 776.68 | 786.91 | 777.13 | 777.36 | 777.58 | 777.81 | 778.04 |
| 345 | テ-26 | 778.49 | 78.71 | 738.94 | 779.16 | 779.39 | 779.61 | 779.84 | 780.07 | 780.29 |
| 346 | 750.52 | 780.74 | 780.97 | 781.19 | 781.42 | 781.64 | 751.87 | 782.10 | 782.32 | 782.55 |
| 317 | 782.75 | 753.00 | 783.22 | 753.45 | 783.67 | 783.90 | 754.13 | 784.35 | 784.58 | 784.50 |
| $\begin{gathered} 29 \text { Inches. } \\ 318 \end{gathered}$ | 78..03 | 7-5.25 | 78.5 .45 | 785.71 | 785.93 | 756.16 | 7S6.3 | 786.61 | 786.63 | 787.06 |

Mundreatths of a Line.

| 0. | 1. | 2. | 3. | 4. | す. | 6. | \%. | 8. | (.) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000 | 0.023 | 0.045 | 0.068 | 0.090 | 0.113 | 0.135 | 0.158 | 0.180 | 0.203 |

VII. - VIII.
comparison
$O F$

## THE RUSSIAN BAROMETER

WITH

THE METRICAL AND THE OLD FRENCI BAROMETERS,
or

## T A B L E S

FOR CONVERTING RUSSIAN HALF-LINES INTO MILLIMETRES, AND INTO FRENCII OR PARIS LINES;

GIVING THE VALUES CORRESPONDING TO EVERY HALf-Line froni 440 TO 540 , OR FROM 22 TO 27 INCHES; AND TO EVERY TENTH, FROM 540 TO 610 HALF-LINES, OR FROM 27 TO 30.5 ENGLISII INCHES.

## RUSSIANBAROMETER.

A fegular system of Meteorological Observations has been established by order of the Russian government throughout the extensive regions placed urater its sway, and a vast amount of observations made in Europe, in Asia, and in North America have already been published. The scale of the barometer employed in this system is divided in units, each of which is equal to one half of a Russian, or English decimal line, that is, $1=0.05$ of an inch, 600 half-lines of the Russian Barometer being $=30$ inches of the English Barometer.

The conversion of this scale, which is the English scale, slightly modified in its form, is easy. It suffices to divide the Russian heights by two, and to put back, by une figure, the decimal point, in order to have them converted into English inches and decimals. This transformation is so easy to effect, that a peculiar table for it would seem superfluous.

The normal temperature of the standard being the same as that of the English, that is, $13^{\circ} \frac{1}{3}$ Reaumur, or $62^{\circ}$ Fahrenheit, the reduction of the Russian Barometer to the freezing point can be made by means of the table for reducing the English Barometers. But the attached thermometer being that of Reaumur, its indications must be first converted into degrees of Fahrenheit.

Tables VII. and VIII., which follow, have been computed in order to render more easy the comparison and the use of the Barometrical Observations recorded in the large collection, published annually by order of the Emperor of Russia, under the name of Annuaire Météorologique et Magnétique du Corps des Ingénicurs des Mines.

1 Russian Half-Line $=1.269977$ Millimetres.

| Russian Half-Lines. | Units or Russian Half-Lines. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | Э. |
| ax lneh. | Millim. | Millim. 560.06 | Millim. <br> 56133 | Millin: <br> $56 \cdot 60$ | Millim. <br> 563.87 | Millim. | Millin. | Millim. | Dillim. <br> 569.95 | Millim. <br> 570.92 |
|  | 538.79 | 560.06 | 561.33 | 562.60 | 563.57 | 565.14 | 566.41 | 567.65 | 568.95 | 570.22 |
| 450 | 571.49 | 572.76 | 574.03 | 575.30 | 576.57 | 577.84 | 579.11 | 5S0.38 | 581.65 | 582.92 |
| 460 | 584.19 | 58.5 .46 | 586.73 | 588.00 | 589.27 | 590.54 | 591.81 | 593.05 | 594.35 | 595.62 |
| 470 | 596.89 | 598.16 | 599.43 | 600.70 | 601.97 | 603.24 | 604.51 | 605.78 | 607.05 | 60 S .32 |
| 480 | 609.59 | 610.86 | 612.13 | 613.40 | 614.67 | 615.94 | 617.21 | 618.48 | 619.75 | 621.02 |
| 24.5 In . |  |  |  |  |  |  |  |  |  |  |
| 490 | 622.29 | 623.56 | 624.83 | 626.10 | 627.37 | 628.64 | 629.91 | 631.18 | 632.45 | 633.72 |
| 500 | 634.99 | 636.26 | 637.53 | 635.80 | 640.07 | 641.34 | 642.61 | 6.13 .88 | 645.15 | 646.42 |
| 510 | 647.69 | 648.96 | 650.23 | 651.50 | 652.77 | 654.04 | 655.31 | 656.58 | 657.85 | 659.12 |
| 520 | 660.39 | 661.66 | 662.93 | 664.20 | 665.47 | 666.74 | 668.01 | 669.28 | 670.55 | 671.82 |
| 530 | 673.09 | 674.36 | 67.).63 | 676.90 | 678.17 | 679.44 | 650.71 | 681.98 | 683.25 | 684.52 |
| Russian Half-Lines | Tenths. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | D. |
| 27 Inch. | Millim. <br> 655.79 | Millim. 655.91 | Nillim. <br> 686.04 | Milim. 686.17 | Dillim. <br> 656.30 | Millim. <br> 656.42 | Millim. <br> 656.55 | Millim. 686.68 | Millim. <br> 686.80 | Millim. $686.93$ |
|  | 687.06 | 687.18 | 657.31 | 687.44 | 687.57 | 687.69 | 687.82 | 687.95 | 688.07 | 688.20 |
| 542 | 688.33 | 658.45 | 688.58 | 688.71 | 688.84 | 688.96 | 689.09 | 689.22 | 689.34 | 689.47 |
| 543 | 689.60 | 689.72 | 689.85 | 659.98 | 690.11 | 690.23 | 690.36 | 690.49 | 690.61 | 690.74 |
| 544 | 690.87 | 690.99 | 691.12 | 691.25 | 691.38 | 691.50 | 691.63 | 691.76 | 691.88 | 692.01 |
| 545 | 692.14 | 692.26 | 692.39 | 692.52 | 692.65 | 692.77 | 692.90 | 693.03 | 693.15 | 693.28 |
| 546 | 693.41 | 693.53 | 693.66 | 693.79 | 693.91 | 694.04 | 694.17 | 694.30 | 694.42 | 694.55 |
| 547 | 694.68 | 694.80 | 694.93 | 695.06 | 695.19 | 695.31 | 695.44 | 695.57 | 695.69 | 695.82 |
| 548 | 695.95 | 696.07 | 696.20 | 696.33 | 696.46 | 696.58 | 696.71 | 696.84 | 696.96 | 697.09 |
| 549 | 697.22 | 697.34 | 697.47 | 697.60 | 697.73 | 697.85 | 697.98 | 698.11 | 698.23 | 698.36 |
| 2\%.5 ln . |  |  |  |  |  |  |  |  |  |  |
| 550 | 698.49 | 698.61 | 698.74 | 698.87 | 699.00 | 699.12 | 699.25 | 699.38 | 699.50 | 699.63 |
| 551 | 699.76 | 699.88 | 700.01 | 700.14 | 700.27 | 700.39 | 700.52 | 700.65 | 700.77 | 700.90 |
| 552 | 701.03 | 701.15 | 701.28 | 701.41 | 701.54 | 701.66 | 701.79 | 701.92 | 702.04 | 702.17 |
| 553 | 702.30 | 702.42 | 702.55 | 702.68 | 702.81 | 702.93 | 703.06 | 703.19 | 70:3.31 | 703.44 |
| 554 | 703.57 | 703.69 | 703.82 | 703.95 | 704.08 | 704.20 | 704.33 | 704.46 | 704.58 | 704.71 |
| 555 | 704.84 | 704.96 | 705.09 | 705.22 | 705.35 | 705.47 | 705.60 | 705.73 | 705.85 | 705.98 |
| 556 | 706.11 | 706.23 | 706.36 | 706.49 | 706.62 | 706.74 | 706.57 | 707.00 | 707.12 | 707.25 |
| 557 | 707.38 | 707.50 | 707.63 | 707.76 | 707.89 | 708.01 | 708.14 | 708.27 | 708.39 | 708.52 |
| 558 | 705.6 .5 | 708.77 | 708.90 | 709.03 | 709.16 | 709.28 | 709.41 | 709.54 | 709.66 | 709.79 |
| 559 | 709.92 | 710.14 | 710.27 | 710.40 | 710.53 | 710.65 | 710.78 | 710.81 | 710.93 | 711.06 |
| 28 Inch. |  |  |  |  |  |  |  |  |  |  |
| 560 | 711.19 | 711.81 | 711.44 | 711.57 | 711.70 | 711.82 | 711.95 | 712.08 | 712.20 | 712.33 |
| 561 | 712.46 | 712.55 | 712.71 | 712.84 | 712.97 | 713.09 | 713.22 | 713.35 | 713.47 | 713.60 |
| 562 | 713.73 | 713.85 | 718.98 | 714.11 | 714.24 | 714.36 | 714.49 | 714.62 | 714.74 | 714.87 |
| 563 | 715.00 | 715.12 | 715.25 | 715.35 | 715.51 | 715.63 | 715.76 | 715.89 | 716.01 | 716.14 |
| 564 | 716.27 | 716.39 | 716.52 | 716.65 | 716.78 | 716.90 | 717.03 | 717.16 | 717.28 | 717.41 |
| 565 | 717.54 | 717.66 | 717.79 | 717.92 | 718.04 | 718.17 | 718.30 | 718.43 | 718.55 | 718.68 |
| 566 | 718.81 | 718.93 | 719.06 | 719.19 | 719.31 | 719.44 | 719.57 | 719.70 | 719.82 | 719.95 |
| 567 | 720.08 | 720.20 | 720.33 | 720.46 | 720.58 | 720.71 | 720.84 | 720.97 | 721.09 | 721.22 |
| 568 | 721.35 | 721.47 | 721.60 | 721.73 | 721.85 | 721.98 | 722.11 | 722.24 | 722.36 | 722.49 |
| 569 | 7.22.62 | 722.74 | 722.87 | 723.00 | 723.12 | 723.25 | 723.38 | 723.51 | 723.63 | 723.76 |

1 Russian Half-Line $=1.269977$ Millimetre.


1 Rnssian Half-Tine $=0.562966$ Paris Line.

| Russian Half-Linea. | Uuits or Russian Malf-Lines. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 2.2 Inch. | Par. line. | Par. line | Par. line | Par line. | Par line | Par line. | Par line | Par line | Par line. | Par. line. |
| 440 | 247.71 | 245.27 | 245.54 | 249.40 | 249.96 | 250.52 | 251.09 | 251.65 | 2.52 .21 | 252.78 |
| 4.50 | 253.31 | 253.90 | 2.54 .47 | 2.55 .03 | 255.59 | 256.15 | 25672 | 257.25 | 257.84 | 258.41 |
| 460 | 2.58 .97 | 259.53 | 260.09 | 260.66 | 261.22 | 263.78 | 262.3.) | $26 \div 3.91$ | 263.47 | 264.04 |
| 470 | 264.60 | 265.16 | 265.72 | 266.29 | 266.85 | 267.11 | 267.93 | 268.54 | 269.10 | 269.67 |
| 480 | 230.23 | 270.79 | 271.35 | 271.92 | 272.18 | 273.04 | 273.61 | 274.17 | 274.73 | 275.80 |
| 24.5 In. |  |  |  |  |  |  |  |  |  |  |
| 490 | 275.86 | 276.42 | 276.98 | 277.55 | 278.11 | 275.67 | 279.24 | 279.80 | 280.36 | 250.93 |
| 500 | 281.49 | 282.05 | 28.61 | 283.15 | 283.74 | 284.30 | 284.87 | 255.43 | 28.5 .99 | 286.55 |
| 510 | 287.12 | 257.65 | 288.24 | 288.81 | 259.37 | 289.93 | 290.50 | 291.06 | 291.62 | 292.18 |
| 520 | 29.2 .75 | 293.31 | 293.87 | 294.44 | 295.00 | 295.56 | 296.13 | 296.69 | 297.25 | 297.81 |
| 530 | 295.35 | 295.94 | 299.50 | 300.07 | 300.63 | 301.19 | 301.76 | 302.32 | 302.58 | 303.44 |
| Russian Halt-Lines | Tenths. |  |  |  |  |  |  |  |  |  |
|  | 0 | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 27 Iuch. | Par. line. | Par line. | Par line. | Par line. | Par. line | Par line. | Par. line. | Par. line | Par. line | Par. line. |
| 540 | 304.01 | 304.06 | 304.12 | 304.15 | 304.23 | 304.29 | 304.34 | 30.1 .40 | 304.16 | 304.51 |
| 541 | 304.57 | 304.63 | 304.68 | 304.74 | 304.80 | 304.85 | 304.91 | 304.96 | 305.02 | 305.08 |
| 542 | 305.13 | 305.19 | 305.25 | 305.30 | 305.36 | 305.41 | 305.47 | 30.5 .53 | 305.58 | 305.64 |
| 543 | 305.70 | 30.5 .75 | 305.81 | 305.86 | 305.92 | 305.98 | 306.03 | 306.09 | 306.15 | 306.20 |
| 544 | 306.26 | 306.32 | 306.37 | 306.43 | 306.18 | 306.54 | 306.60 | 306.65 | 306.71 | 306.77 |
| 515 | 306.52 | 306.89 | 306.93 | 306.99 | 307.05 | 307.10 | 307.16 | 307.22 | 307.27 | 307.33 |
| 546 | 307.33 | 307.44 | 307.50 | 307.55 | 307.61 | 307.67 | 307.72 | 307.78 | 307.84 | 307.89 |
| 547 | 307.95 | $30<.00$ | 305.06 | 308.12 | 308.17 | 305.23 | 308.29 | 305.34 | 308.40 | 308.45 |
| 548 | 308.51 | 308.57 | 308.62 | 308.65 | 308.74 | 308.79 | 308.85 | 308.90 | 308.96 | 309.02 |
| 549 | 309.07 | 309.13 | 309.19 | 309.24 | 309.30 | 309.36 | 309.41 | 309.47 | 309.52 | 309.58 |
| 27.5 In. |  |  |  |  |  |  |  |  |  |  |
| 550 | 309.64 | 309.69 | 309.75 | 309.81 | 309.86 | 309.92 | 309.97 | 310.03 | 310.09 | 310.14 |
| 551 | 310.20 | 310.26 | 310.31 | 310.37 | 310.42 | 310.48 | 310.54 | 310.59 | 310.65 | 310.71 |
| 552 | 310.76 | 310.82 | 310.88 | 310.93 | 310.99 | 311.04 | 311.10 | 311.16 | 311.21 | 311.27 |
| 553 | 311.33 | 311.38 | 311.44 | 311.49 | 311.55 | 311.61 | 311.66 | 311.72 | 311.78 | 311.83 |
| 554 | 311.89 | 311.95 | 312.00 | 312.06 | 312.11 | 312.17 | 312.23 | 312.28 | 312.34 | 312.40 |
| 555 | 312.15 | 312.51 | 312.56 | 312.62 | 312.68 | 312.73 | 312.79 | 312.85 | 312.90 | 312.96 |
| 556 | 313.01 | 313.07 | 313.13 | 313.15 | 313.24 | 313.30 | 313.35 | 313.41 | 313.47 | 313.52 |
| 557 | 313.56 | 313.63 | 313.69 | 313.75 | 313.80 | 313.86 | 313.92 | 313.97 | 314.03 | 314.08 |
| 558 | 314.14 | 314.20 | 314.25 | 314.31 | 314.37 | 314.42 | 314.15 | 314.53 | 314.59 | 314.65 |
| 559 | 314.70 | 314.76 | 314.82 | 314.87 | 314.93 | 314.99 | 315.04 | 315.10 | 315.15 | 315.21 |
| 28 Inch. |  |  |  |  |  |  |  |  |  |  |
| 560 | 315.27 | 315.32 | 315.38 | 315.44 | 315.49 | 315.55 | 315.60 | 315.66 | 315.72 | 315.77 |
| 561 | 315.83 | 315.89 | 315.94 | 316.00 | 316.05 | 316.11 | 316.17 | 316.22 | 316.28 | 316.34 |
| 562 | 316.39 | 316.45 | 316.51 | 316.56 | 316.62 | 316.67 | 316.73 | 316.79 | 316.84 | 316.90 |
| 563 | 316.96 | 317.01 | 317.07 | 317.12 | 317.18 | 317.24 | 317.29 | 317.35 | 317.41 | 317.46 |
| 564 | 317.52 | 317.57 | 317.63 | 317.69 | 317.74 | 317.80 | 317.86 | 317.91 | 317.97 | 318.03 |
| 565 | 318.08 | 318.14 | 318.19 | 318.25 | 318.31 | 318.36 | 318.42 | 318.48 | 315.53 | 318.59 |
| 566 | 318.64 | 318.70 | 318.76 | 318.81 | 318.57 | 318.93 | 318.98 | 319.04 | 319.09 | 319.15 |
| 567 | 319.21 | 319.26 | 319.32 | 319.39 | 319.43 | 319.49 | 319.55 | 319.60 | 319.66 | 319.71 |
| 568 | 319.77 | 319.S3 | 319.88 | 319.94 | 320.00 | 320.05 | 320.11 | 320.16 | 320.22 | 320.28 |
| 569 | 320.33 | 320.39 | 320.45 | 320.50 | 320.56 | 320.61 | 320.67 | 320.73 | 320.78 | 320.84 |

1 Russian Half-Line $=0.5629 .6$ Paris Line.

| Russian Half-Lines. | Tenths. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 28.5 Inch. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. linc. | Par. line. |
| 570 | 320.90 | 320.95 | 321.01 | 321.07 | 321.12 | 321.18 | 321.23 | 321.29 | 321.35 | 321.40 |
| 571 | 321.46 | 321.52 | 321.57 | 321.63 | 321.68 | 321.74 | 321.80 | 321.85 | 321.91 | 321.97 |
| 572 | 322.02 | 322.08 | 32.2 .13 | 32.219 | 322.25 | 322.30 | 322.36 | 322.42 | 322.47 | 322.53 |
| 573 | 322.59 | 32.2 .64 | 32.2 .70 | 322.75 | 322.81 | 322.87 | 322.92 | 322.98 | 323.04 | 323.09 |
| 574 | 323.15 | 323.20 | 323.26 | 323.32 | 323.37 | 323.43 | 323.49 | 323.54 | 323.60 | 323.65 |
| 575 | 323.71 | 323.77 | 323.82 | 323.85 | 323.94 | 323.99 | 324.05 | 324.11 | 324.16 | 324.22 |
| 576 | 324.27 | 324.33 | 324.39 | 324.41 | 324.50 | 324.56 | 324.61 | 324.67 | 321.72 | 324.78 |
| 577 | 324.84 | 324.89 | 324.95 | 325.01 | 325.06 | 325.12 | 325.17 | 325.23 | 325.29 | 325.34 |
| 578 | 325.40 | 32.5 .46 | 325.51 | 32.5 .57 | 325.63 | 325.68 | 325.74 | 325.79 | 325.85 | 325.91 |
| 579 | 325.96 | 326.02 | 326.05 | 326.13 | 326.19 | 326.24 | 326.30 | 326.36 | 326.41 | 326.47 |
| 29 Inch. |  |  |  |  |  |  |  |  |  |  |
| 590 | 326.53 | 326.58 | 326.64 | 326.69 | 326.75 | 326.81 | 326.86 | 326.92 | 326.95 | 327.13 |
| 581 | 327.09 | 327.15 | 327.20 | 327.26 | 327.31 | 327.37 | 327.43 | 327.48 | 327.54 | 327.60 |
| 582 | 327.65 | 327.71 | 327.76 | 327.82 | 327.88 | 827.93 | 327.99 | 325.05 | 328.10 | 328.16 |
| 583 | 328.22 | 328.27 | 325.33 | 328.35 | 328.44 | 325.50 | 328.55 | 328.61 | 328.67 | 325.72 |
| 584 | $32 \mathrm{S.78}$ | 328.83 | 328.89 | 328.95 | 329.00 | 329.06 | 329.12 | 329.17 | 329.23 | 329.25 |
| 58.5 | 329.34 | 329.40 | 329.45 | 329.51 | 329.57 | 329.62 | 329.68 | 329.74 | 329.79 | 329.85 |
| 586 | 329.90 | 329.96 | 330.02 | 330.07 | 330.13 | 330.19 | 330.24 | 330.30 | 330.35 | 330.41 |
| 587 | 330.47 | 330.52 | 330.58 | 330.64 | 330.69 | 330.75 | 330.80 | 330.86 | 330.92 | 330.97 |
| 588 | 331.03 | 331.09 | 331.14 | 331.20 | 331.26 | 331.31 | 331.37 | 331.42 | 331.48 | 331.54 |
| 589 | 331.59 | 331.65 | 331.71 | 331.76 | 331.82 | 331.57 | 331.93 | 331.99 | 332.04 | 332.10 |
| 29.5 Ic . |  |  |  |  |  |  |  |  |  |  |
| 590 | 332.16 | 332.21 | 332.27 | 332.32 | 332.38 | 332.44 | 332.49 | 332.55 | 332.61 | 332.66 |
| 591 | 332.72 | 332.78 | 332.53 | 332.59 | 332.94 | 333.00 | 333.06 | 333.11 | 333.17 | 333.23 |
| 592 | 333.28 | 333.34 | 333.39 | 333.45 | 333.51 | 333.56 | 333.62 | 333.68 | 333.73 | 333.79 |
| 593 | 3.33 .84 | 333.90 | 333.96 | 334.01 | 334.07 | 334.13 | 334.18 | 334.24 | 334.30 | 334.35 |
| 594 | 334.41 | 334.46 | 334.52 | 334.58 | 334.63 | 334.69 | 334.75 | 334.80 | 334.86 | 334.91 |
| 595 | 334.97 | 335.03 | 335.08 | 335.14 | 335.20 | 335.25 | 335.31 | 33.5 .36 | 335.42 | 335.48 |
| 596 | 335.53 | 335.59 | 335.67 | 335.70 | 335.76 | 335.82 | 335.87 | 335.93 | 335.98 | 336.04 |
| 6.97 | 336.10 | 336.15 | 336.21 | 336.27 | 336.32 | 336.38 | 336.43 | 336.49 | 336.55 | 336.60 |
| 598 | 336.66 | 336.72 | 336.77 | 336.83 | 336.88 | 336.94 | 337.00 | 337.05 | 337.11 | $3: 37.17$ |
| 599 | 337.22 | 337.2 S | 337.34 | 337.39 | 337.45 | 337.50 | 337.56 | 337.62 | 337.67 | 337.73 |
| 30 Inch. |  |  |  |  |  |  |  |  |  |  |
| 600 | 337.79 | 337.84 | 337.90 | 337.95 | 338.01 | 338.07 | 338.12 | 335.18 | 388.24 | 338.29 |
| 601 | 335.35 | 335.40 | 338.46 | 338.52 | 338.57 | 338.63 | 335.69 | 338.74 | 338.80 | 338.86 |
| 602 | 388.91 | 338.97 | 339.02 | 339.08 | 339.14 | 339.19 | 339.25 | 339.31 | 339.36 | 339.42 |
| 603 | 339.47 | 339.53 | 339.59 | 339.64 | 339.70 | 339.76 | 339.81 | 339.57 | 339.92 | 389.98 |
| 604 | 340.04 | 340.09 | 340.15 | 340.21 | 340.26 | 340.32 | 340.38 | 340.43 | 810.49 | 340.54 |
| 60.5 | 340.60 | 340.66 | 340.71 | 340.77 | 340.83 | 340.58 | 340.94 | 340.99 | 341.05 | 341.11 |
| 606 | 341.16 | 341.22 | 341.28 | 341.33 | 341.39 | 341.44 | 341.50 | 341.56 | 311.61 | $311.6 \%$ |
| 607 | 341.73 | 341.78 | 341.84 | 341.90 | 341.95 | 342.01 | 342.06 | 342.12 | 342.18 | 342.23 |
| 608 | 342.29 | 342.35 | 342.40 | 342.46 | 342.51 | 342.57 | 342.63 | 342.65 | 312.74 | 342.80 |
| 609 | 342.85 | 342.91 | 342.96 | 343.02 | 343.08 | 343.13 | 343.19 | 343.25 | 313.30 | 343.36 |
| Hundredths. |  |  |  |  |  |  |  |  |  |  |
| 0.000 | 0.006 | 0.011 | 0.017 | 0.022 | 20.02 |  | 034 | . 039 | 0.045 | 0.051 |

## IX. - XVI.

$$
\text { C } 0 \text { MPARIS } 0 \mathrm{~N}
$$

OF

## BAROMETRICAL DIFFERENCES

Expressed In measubes of Different scales,
or

TABLES

FOR CONVERTING ENGLISF/ INCIIES, MILLIMETRES, PARIS LINES, AND RUSSIAN HALF-LINES INTO EACH OTHER.

1 English Inch $=25.3995+$ Milhimetres.

| $\begin{array}{\|c\|} \text { English } \\ \text { Inches and } \\ \text { Tenthis. } \end{array}$ | Lundredths of an Inch. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Millim. | Millim. | Millim. | Millim. | Millim. | Nillim. | Millim. | Millim. | Millim. | Millim. |
| 0.0 | 0.000 | 0.254 | 0.508 | 0762 | 1.016 | 1.270 | 1.524 | 1.778 | 2.032 | 2.286 |
| 0.1 | 2.540 | 2.794 | 3.048 | 3.302 | 3.556 | 3.810 | 4.064 | 4.318 | 4.572 | 4.826 |
| 0.2 | 5.050 | 5.334 | 5.588 | 5.842 | 6.096 | 6.350 | 6.604 | 6.558 | 7.112 | 7.366 |
| 0.3 | 7.620 | 7.874 | 8.128 | 8.382 | 8.636 | 8.890 | 9.144 | 9.398 | 9.652 | 9.906 |
| 0.4 | 10.160 | 10.414 | 10.668 | 10.922 | 11.176 | 11.430 | 11.684 | 11.938 | 12.192 | 12.446 |
| 0.5 | 12.700 | 12.954 | 13.208 | 13.462 | 13.716 | 13.970 | 14.224 | 14.478 | 14.732 | 14.986 |
| 0.6 | 15.240 | 15.49 .4 | 15.748 | 16.002 | 16.256 | 16.510 | 16.764 | 17.018 | 17.272 | 17.526 |
| 0.7 | 17.780 | 18.034 | 18.288 | 18.542 | 18.796 | 19.050 | 19.304 | 19.558 | 19.812 | 20.066 |
| 0.8 | 20.320 | 20.574 | 20.828 | 21.082 | 21.336 | 21.590 | 21.844 | 22.098 | 22.352 | 22.606 |
| 0.9 | 22.860 | 23.114 | 23.368 | 23.622 | 23.876 | 24.130 | 24.384 | 24.638 | 24.592 | 25.146 |
| 1.0 | 25.400 | 25.654 | 25.908 | 26.162 | 26.416 | 26.670 | 26.924 | 27.178 | 27.432 | 27.685 |
| 1.1 | 27.939 | 28.193 | 28.447 | 28.701 | 28.955 | 29.209 | 29.463 | 29.717 | 29.971 | 30.225 |
| 1.2 | 30.479 | 30.733 | 30.987 | 31.241 | 31.495 | 31.749 | 32.003 | 32.257 | 32.511 | 32.765 |
| 1.3 | 33.019 | 33.273 | 33.527 | 33.781 | 34.035 | 34.289 | 34.543 | 34.797 | 35.051 | 35.305 |
| 1.4 | 35.559 | 35.813 | 36.067 | 36.321 | 36.575 | 36.829 | 37.083 | 37.337 | 37.591 | 37.845 |
| 1.5 | 38.099 | 38.353 | 38.607 | 38.861 | 39.115 | 39.369 | 39.623 | 39.877 | 40.131 | 40.355 |
| 1.6 | 40.639 | 40.893 | 41.147 | 41.401 | 41.655 | 41.909 | 42.163 | 42.417 | 42.671 | 42.925 |
| 1.7 | 43.179 | 43.433 | 43.657 | 43.941 | 44.195 | 44.449 | 44.703 | 44.957 | 45.211 | 45.465 |
| 1.8 | 45.719 | 45.973 | 46.227 | 46.481 | 46.735 | 46.989 | 47.243 | 47.497 | 47.751 | 48.005 |

X. CONVERSION OF ENGLISH INCHES INTO FRENCH OR PARIS LINES.

1 English Inch $=11.259515$ Paris Lines.

| $\begin{gathered} \text { English } \\ \text { Inches and } \\ \text { Tenths. } \end{gathered}$ | Hundreaths of an Inch. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
|  | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. |
| 0.0 | 0.000 | 0.113 | 0.225 | 0.338 | 0.450 | 0.563 | 0.676 | 0.758 | 0.901 | 1.013 |
| 0.1 | 1.126 | 1.239 | 1.351 | 1.464 | 1.576 | 1.689 | 1.802 | 1.914 | 2.027 | 2.139 |
| 0.2 | 2.252 | 2.364 | 2.477 | 2.590 | 2.702 | 2.815 | 2.927 | 3.040 | 3.153 | 3.265 |
| 0.3 | 3.378 | 3.490 | 3.603 | 3.716 | 3.528 | 3.941 | 4.053 | 4.166 | 4.279 | 4.391 |
| 0.4 | 4.50 .4 | 4.616 | 4.729 | 4.842 | 4.954 | 5.067 | 5.179 | 5.292 | 5.405 | 5.517 |
| 0.5 | 5.630 | 5.742 | 5.855 | 5.968 | 6.080 | 6.193 | 6.305 | 6.418 | 6.531 | 6.643 |
| 0.6 | 6.756 | 6.868 | 6.981 | 7.093 | 7.206 | 7.319 | 7.431 | 7.544 | 7.656 | 7.769 |
| 0.7 | 7.882 | 7.994 | 8.107 | 8.219 | 8.332 | 8.445 | 8.557 | 8.670 | 8.782 | 8.895 |
| 0.8 | 9.003 | 9.120 | 9.233 | 9.345 | 9.458 | 9.571 | 9.683 | 9.796 | 9.908 | 10.021 |
| 0.9 | 10.134 | 10.246 | 10.359 | 10.471 | 10.584 | 10.697 | 10.809 | 10.922 | 11.034 | 11.147 |
| 1.0 | 11.260 | 11.372 | 11.485 | 11.597 | 11.710 | 11.822 | 11.935 | 12.048 | 12.160 | 12.273 |
| 1.1 | 12.385 | 12.498 | 12.611 | 12.723 | 12.836 | 12.945 | 13.061 | 13.174 | 13.286 | 13.399 |
| 1.2 | 13.511 | 13.624 | 13.737 | 13.849 | 13.962 | 14.074 | 14.187 | 14.300 | 14.412 | 14.525 |
| 1.3 | 14.637 | 14.750 | 14.563 | 14.975 | 15.088 | 15.200 | 15.313 | 15.426 | 15.538 | 15.651 |
| 1.4 | 15.763 | 15.876 | 15.988 | 16.101 | 16.214 | 16.326 | 16.439 | 16.551 | 16.664 | 16.777 |
| 1.5 | 16.889 | 17.002 | 17.114 | 17.227 | 17.340 | 17.452 | 17.565 | 17.677 | 17.790 | 17.903 |
| 1.6 | 18.015 | 18.128 | 18.240 | 18.353 | 18.466 | 18.578 | 18.691 | 18.803 | 18.916 | 19.029 |
| 1.7 | 19.141 | 19.254 | 19.366 | 19.479 | 19.592 | 19.704 | 19.817 | 19.929 | 20.042 | 20.155 |
| 1.8 | 20.267 | 20.380 | 20.492 | 20.605 | 20.717 | 20.530 | 20.943 | 21.055 | 21.168 | 21.280 |

1 Metre $=39.37079$ English Inches

| Millimetres. | Tenths of a Millimetre. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
|  | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 0 | 0.0000 | 0.0039 | 0.0079 | 0.0118 | 0.0157 | 0.0197 | 0.0236 | $0.02 \div 6$ | 0.0:315 | 0.0354 |
| 1 | 0.0391 | 0.0433 | 0.0472 | 0.0512 | 0.0 .5 .51 | 0.0591 | 0.0630 | 0.0669 | 0.0709 | 0.0748 |
| 2 | 0.0787 | 0.0527 | 0.0866 | 0.0906 | 0.0945 | 0.0984 | 0.1024 | 0.1063 | 0.1102 | 0.1142 |
| 3 | 0.1181 | 0.1220 | 0.1260 | 0.1299 | 0.1339 | 0.1375 | 0.1417 | 0.1457 | 0.1496 | 0.1535 |
| 4 | 0.1575 | 0.1614 | 0.1654 | 0.1693 | 0.1732 | 0.1772 | 0.1511 | 0.1850 | 0.1590 | 0.1929 |
| 5 | 0.1969 | 0.2005 | 0.2047 | 0.2087 | 0.2126 | 0.2165 | 0.2205 | 0.2244 | 0.2283 | 0.2323 |
| 6 | 0.2362 | 0.2402 | 0.2441 | 0.2450 | 0.2520 | 0.25 .59 | 0.2595 | 0.2638 | 0.2677 | 0.2717 |
| 7 | 0.2756 | 0.2795 | 0.2835 | 0.2874 | 0.2913 | 0.2953 | 0.2992 | 0.3032 | 0.3071 | 0.3110 |
| 8 | 0.3150 | 0.3189 | 0.3228 | 0.3268 | 0.3307 | 0.3347 | 0.3386 | 0.3425 | 0.3465 | 0.3504 |
| 9 | 0.3543 | 0.3553 | 0.3622 | 0.3661 | 0.3701 | 0.3740 | 0.3780 | 0.3819 | 0.3858 | 0.3898 |
| 10 | 0.3937 | 0.3976 | 0.4016 | 0.4055 | 0.4095 | 0.4134 | 0.4173 | 0.1213 | 0.4252 | 0.4291 |
| 11 | 0.4331 | 0.4370 | 0.4410 | 0.4449 | 0.4488 | 0.4528 | 0.4567 | 0.4606 | 0.4646 | 0.1685 |
| 12 | 0.4724 | 0.4764 | 0.1803 | 0.4813 | 0.4882 | 0.4921 | 0.4961 | 0.5000 | 0.5039 | 0.5079 |
| 13 | 0.5118 | 0.5158 | 0.5197 | 0.5236 | 0.5276 | 0.5315 | 0.5354 | 0.5394 | 0.5433 | 0.5473 |
| 14 | 0.5512 | 0.5551 | 0.5591 | 0.5630 | 0.5669 | 0.5709 | 0.5748 | 0.5788 | 0.5527 | 0.5866 |
| 15 | 0.5906 | 0.594 .7 | 0.5954 | 0.6024 | 0.6063 | 0.6102 | 0.6142 | 0.6181 | 0.6221 | 0.6260 |
| 16 | 0.6299 | 0.6339 | 0.6378 | 0.6417 | 0.6457 | 0.6496 | 0.6536 | 0.6575 | 0.6614 | 0.6654 |
| 17 | 0.6693 | 0.6732 | $0.67 \% 2$ | 0.6511 | 0.68 .51 | 0.6890 | 0.6929 | 0.6969 | 0.7008 | 0.7047 |
| 18 | 0.7087 | 0.7126 | 0.716 .5 | 0.7205 | 0.7244 | 0.7284 | 0.7823 | 0.7362 | 0.7402 | 0.7441 |
| 19 | 0.7480 | 0.7520 | 0.7559 | 0.7599 | 0.7638 | 0.7677 | 0.7717 | 0.7756 | 0.7795 | 0.7835 |
| 20 | 0.7874 | 0.7914 | 0.79 .3 .3 | 0.7992 | 0.8032 | 0.8071 | 0.8110 | 0.8150 | 0.8189 | 0.8228 |
| 21 | 0.8265 | 0.6307 | 0.5347 | 0.8386 | 0.8425 | 0.846 .3 | 0.8504 | 0.5543 | 0.8583 | 0.5622 |
| 22 | 0.8662 | 0.5701 | 0.5740 | 0.8780 | 0.8519 | 0.58 .55 | 0.8598 | 0.8937 | 0.5977 | 0.9016 |
| 23 | 0.9055 | 0.9095 | 0.9134 | 0.9173 | 0.9213 | 0.9252 | 0.9292 | 0.9331 | 0.9370 | 0.9410 |
| 24 | 0.9449 | 0.9458 | 0.9528 | 0.9 .567 | 0.9606 | 0.9616 | 0.9685 | 0.9725 | 0.9764 | 0.9803 |
| 25 | 0.9843 | 0.9852 | 0.9921 | 0.9961 | 1.0000 | 1.0040 | 1.0079 | 1.0118 | 1.0155 | 1.0197 |
| 26 | 1.0236 | 1.0276 | 1.0315 | 1.035.5 | 1.0394 | 1.0433 | 1.0473 | 1.0512 | 1.0551 | 1.0591 |
| 27 | 1.0630 | 1.0669 | 1.0709 | 1.0748 | 1.07*8 | 1.0527 | 1.0866 | 1.0906 | 1.0945 | 1.0954 |
| 28 | 1.1024 | 1.1063 | 1.1103 | 1.1142 | 1.1181 | 1.1221 | 1.1260 | 1.1299 | 1.1339 | 1.1378 |
| 29 | 1.1418 | 1.1457 | 1.1496 | 1.1536 | 1.1575 | 1.1614 | 1.1654 | 1.1693 | 1.1732 | 1.1772 |
| 30 | 1.1811 | 1.1851 | 1.1890 | 1.1929 | 1.1969 | 1.2008 | 1.2047 | 1.2087 | 1.2126 | 1.2166 |
| 31 | 1.220 .5 | 1.2244 | 1.2234 | 1.2323 | 1.2362 | 1.2402 | 1.2441 | 1.2481 | 1.2520 | 1.2559 |
| 32 | 1.2599 | 1.2638 | 1.2677 | 1.2717 | 1.2756 | 1.2796 | 1.2835 | 1.2874 | 1.2914 | 1.29 .53 |
| 33 | 1.2992 | 1.3032 | 1.3071 | 1.3110 | 1.3150 | 1.3159 | 1.3229 | 1.3268 | 1.3307 | 1.3347 |
| 31 | 1.3356 | 1.3425 | 1.3465 | 1.3504 | 1.3544 | 1.3583 | 1.3622 | 1.3662 | 1.3701 | 1.3740 |
| 3.5 | 1.3780 | 1.3819 | 1.3859 | 1.3898 | 1.3937 | 1.3977 | 1.4016 | 1.4055 | 1.4095 | 1.4134 |
| 36 | 1.4173 | 1.4213 | 1.4252 | 1.4292 | 1.4331 | 1.4370 | 1.4410 | 1.4449 | 1.4488 | 1.1528 |
| 37 | 1.4567 | 1.4607 | 1.4646 | 1.4695 | 1.4725 | 1.4764 | 1.1803 | 1.4843 | 1.4882 | 1.4922 |
| 33 | 1.4961 | 1.5000 | 1.5010 | 1.5079 | 1.5118 | 1.5158 | 1.5197 | 1.5236 | 1.5276 | 1.5315 |
| 39 | 1.5355 | 1.5394 | 1.5438 | 1.5473 | 1.5512 | 1.55 .51 | 1.5591 | 1.5630 | 1.5670 | 1.5709 |
| 40 | 1.5745 | 1.5788 | 1.5827 | 1.5566 | 1.5906 | 1.594 .5 | 1.5985 | 1.6024 | 1.6063 | 1.6103 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | Э. |

1 Millimetre $=0.443296$ Paris Line.

| Millimetres | Tenths of a Millimetre. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line | Par. line. |
| 0 | 0.000 | 0.044 | 0.089 | 0.133 | 0.177 | 0.222 | 0.266 | 0.310 | 0.355 | 0.399 |
| 1 | 0.443 | 0.488 | 0.532 | 0.576 | 0.621 | 0.665 | 0.709 | 0.754 | 0.795 | 0.842 |
| 2 | 0.557 | 0.931 | 0.975 | 1.020 | 1.064 | 1.108 | 1.153 | 1.197 | 1.241 | 1.2s6 |
| 3 | 1.330 | 1.374 | 1.419 | 1.463 | 1.507 | 1.552 | 1.596 | 1.640 | 1.685 | 1.729 |
| 4 | 1.773 | 1.818 | 1.862 | 1.906 | 1.950 | 1.995 | 2.039 | 2.083 | 2.128 | 2.172 |
| 5 | 2.216 | 2.261 | 2.305 | 2.349 | 2.394 | 2.438 | 2.482 | 2.527 | 2.571 | 2.615 |
| 6 | 2.660 | 2.701 | 2.748 | 2.793 | 2.837 | 2.881 | 2.926 | 2.970 | 3.014 | 3.059 |
| 7 | 3.103 | 3.147 | 3.192 | 3.236 | 3.280 | 3.32 .5 | 3.369 | 3.413 | 3.458 | 3.502 |
| 8 | 3.546 | 3.591 | 3.635 | 3.679 | 3.724 | 3.768 | 3.812 | 3.857 | 3.901 | 3.945 |
| 9 | 3.990 | 4.034 | 4.078 | 4.123 | 4.167 | 4.211 | 4.256 | 4.300 | 4.344 | 4.389 |
| 10 | 4.433 | 4.477 | 4.522 | 4.566 | 4.610 | 4.655 | 4.699 | 4.743 | 4.788 | 4.832 |
| 11 | 4.576 | 4.921 | 4.965 | 5.009 | 5.054 | 5.098 | 5.142 | 5.187 | 5.231 | 5.275 |
| 12 | 5.320 | 5.364 | 5.408 | 5.453 | 5.497 | 5.541 | 5.586 | 5.630 | 5.674 | 5.719 |
| 13 | 5.763 | 5.807 | 5.851 | 5.896 | 5.940 | 5.984 | 6.029 | 6.073 | 6.117 | 6.162 |
| 14 | 6.206 | 6.2.50 | 6.295 | 6.339 | 6.383 | 6.428 | 6.472 | 6.516 | 6.561 | 6.605 |
| 15 | 6.649 | 6.694 | 6.738 | 6.782 | 6.827 | 6.871 | 6.915 | 6.960 | 7.004 | 7.048 |
| 16 | 7.093 | 7.137 | 7.151 | 7.226 | 7.270 | 7.314 | 7.359 | 7.403 | 7.447 | 7.492 |
| 17 | 7.536 | 7.580 | 7.625 | 7.669 | 7.713 | 7.758 | 7.802 | 7.846 | 7.891 | 7.935 |
| 18 | 7.979 | 8.021 | 8.068 | 8.112 | 8.157 | 8.201 | 8.245 | 8.290 | $8.33!$ | 8.378 |
| 19 | 8.423 | 8.467 | 8.511 | 8.556 | 8.600 | 8.644 | 8.689 | 8.733 | 8.777 | 8.822 |
| 20 | 8.866 | 8.910 | 8.953 | 8.999 | 9.043 | 9.058 | 9.132 | 9.176 | 9.221 | 9.26 .5 |
| 21 | 9.309 | 9.3 .54 | 9.398 | 9.442 | 9.487 | 9.531 | 9.575 | 9.620 | 9.664 | 9.708 |
| 22 | 9.753 | 9.797 | 9.541 | 9.886 | 9.930 | 9.974 | 10.018 | 10.063 | 10.107 | 10.151 |
| 23 | 10.196 | 10.240 | 10.284 | 10.329 | 10.373 | 10.417 | 10.462 | 10.506 | 10.550 | 10.595 |
| 24 | 10.639 | 10.653 | 10.728 | 10.772 | 10.816 | 10.861 | 10.905 | 10.949 | 10.994 | 11.038 |
| 25 | 11.082 | 11.127 | 11.171 | 11.215 | 11.260 | 11.304 | 11.348 | 11.393 | 11.437 | 11.481 |
| 26 | 11.526 | 11.570 | 11.614 | 11.6 .59 | 11.703 | 11.747 | 11.792 | 11.836 | 11.880 | 11.925 |
| 27 | 11.969 | 12.013 | 12.058 | 12.102 | 12.146 | 12.191 | 12.235 | 12.279 | 12.324 | 12.368 |
| 28 | 12.412 | 12.457 | 12.501 | 12.545 | 12.590 | 12.634 | 12.678 | 12.723 | 12.767 | 12.811 |
| 29 | 12.556 | 12.900 | 12.944 | 12.989 | 13.033 | 13.077 | 13.122 | 13.166 | 13.210 | 13.255 |
| 30 | 13.299 | 13.343 | 13.388 | 13.432 | 13.476 | 13.521 | 13.565 | 13.609 | 13.654 | 13.698 |
| 31 | 13.742 | 13.786 | 13.831 | 13.575 | 13.919 | 13.964 | 14.008 | 14.052 | 14.097 | 14.141 |
| 32 | 14.185 | 14.2:30 | 14.274 | 14.318 | 14.363 | 14.407 | 14.451 | 14.496 | 14.540 | 14.584 |
| 33 | 14.629 | 14.673 | 14.717 | 14.762 | 14.806 | 14.850 | 14.895 | 14.939 | 14.983 | 15.028 |
| 34 | 1.3.072 | 15.116 | 15.161 | 15.205 | 15.249 | 15.294 | 15.338 | 15.382 | 15.427 | 15.471 |
| 35 | 15.515 | 15.560 | 15.604 | 15.648 | 15.693 | 15.737 | 15.781 | 15.826 | 15.870 | 15.914 |
| 36 | 15.959 | 16.003 | 16.047 | 16.092 | 16.136 | 16.180 | 16.225 | 16.269 | 16.313 | 16.358 |
| 37 | 16.102 | 16.446 | 16.491 | 16.535 | 16.579 | 16.624 | 16.668 | 16.712 | 16.757 | 16.801 |
| 38 | 16.845 | 16.890 | 16.934 | 16.978 | 17.023 | 17.067 | 17.111 | 17.156 | 17.200 | 17.24.4 |
| 39 | 17.289 | 17.333 | 17.377 | 17.422 | 17.466 | 17.510 | 17.555 | 17.599 | 17.643 | 17.688 |
| 40 | 17.732 | 17.776 | 17.820 | 17.865 | 17.909 | 17.953 | 17.998 | 18.042 | 18.086 | 18.131 |
|  | ©. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |

260 xili conversion of the french or paris lines into millimetres.
1 Paris Line $=2.255529$ Millimetres.

| Paris Lines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. |
| 0 | 0.000 | 0.226 | 0.451 | 0.677 | 0.902 | 1.128 | 1.353 | 1.579 | 1.805 | 2.030 |
| 1 | 2.256 | 2.481 | 2.707 | 2.933 | 3.158 | 3.384 | 3.609 | 3.835 | 4.060 | 4.286 |
| 2 | 4.512 | 4.737 | 4.963 | 5.188 | 5.414 | 5.640 | 5.865 | 6.091 | 6.316 | 6.542 |
| 3 | 6.767 | 6.993 | 7.219 | 7.444 | 7.670 | 7.895 | 8.121 | 8.347 | 8.572 | 8.798 |
| 4 | 9.023 | 9.249 | 9.474 | 9.700 | 9.926 | 10.151 | 10.377 | 10.602 | 10.828 | 11.054 |
| 5 | 11.279 | 11.505 | 11.730 | 11.956 | 12.181 | 12.407 | 12.633 | 12.558 | 13.084 | 13.309 |
| 6 | 13.53 .5 | 13.761 | 13.986 | 14.212 | 14.437 | 14.663 | 14.888 | 15.114 | 15.340 | 15.565 |
| 7 | 15.791 | 16.016 | 16.242 | 16.468 | 16.693 | 16.919 | 17.144 | 17.370 | 17.59 .5 | 17.821 |
| 8 | 18.047 | 18.27\% | 18.498 | 18.723 | 18.949 | 19.175 | 19.400 | 19.626 | 19.851 | 20.077 |
| 9 | 20.302 | 20.528 | 20.754 | 20.979 | 21.205 | 21.430 | 21.656 | 21.88. | 22.107 | 22.333 |
| 10 | 22.558 | 22.784 | 23.009 | 23.235 | 23.461 | 23.656 | 23.912 | 24.137 | 24.363 | 24.589 |
| 11 | 24.814 | 25.040 | 25.265 | 25.491 | 25.716 | 25.942 | 26.168 | 26.393 | 26.619 | 26.844 |
| 12 | 27.070 | 27.296 | 27.521 | 27.747 | 27.972 | 28.198 | 28.423 | 28.649 | 28.575 | 29.100 |
| 13 | 29.326 | 29.551 | 29.777 | 30.003 | 30.228 | 30.454 | 30.679 | 30.905 | 31.130 | 31.356 |
| 14 | 31.582 | 31.807 | 32.033 | 32.258 | 32.485 | 32.711 | 32.936 | 33.162 | 33.387 | 33.613 |
| 15 | 33.837 | 34.063 | 34.289 | 34.514 | 34.740 | 34.965 | 35.191 | 35.417 | 35.642 | 35.865 |
| 16 | 36.093 | 36.319 | 36.544 | $36.7 \% 0$ | 36.996 | 37.221 | 37.447 | 37.672 | 37.898 | 38.124 |
| 17 | 35.349 | 38.575 | 38.800 | 39.026 | 39.251 | 39.477 | 39.703 | 39.928 | 40.154 | 40.379 |
| 18 | 40.605 | 40.831 | 41.056 | 41.282 | 41.507 | 41.733 | 41.9 .58 | 42.154 | 42.410 | 42.635 |

XIV. CONVERSION OF FRENCH OR PARIS LINES INTO ENGLISH INCHES.

1 Paris Line $=0.088814$ English Inch.

| Paris <br> Lines. | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In | Eng. In. | Eng. In. | Eng. In. | Eng. In. | Eng. In. |
| 0 | 0.0000 | 0.0089 | 0.0178 | 0.0266 | 0.0355 | 0.0444 | 0.0533 | 0.06.22 | 0.0711 | 0.0799 |
| 1 | 0.0588 | 0.0977 | 0.1066 | 0.1155 | 0.1243 | 0.1832 | 0.1421 | 0.1510 | 0.1599 | 0.1687 |
| 2 | 0.1776 | 0.1565 | 0.1954 | 0.2043 | 0.2132 | 0.2220 | 0.2309 | 0.2398 | 0.2487 | 0.2576 |
| 3 | 0.2664 | 0.2753 | 0.2842 | 0.2931 | 0.3020 | 0.3108 | 0.3197 | 0.3286 | 0.3375 | 0.3464 |
| 4 | 0.3553 | 0.3641 | 0.3730 | 0.3819 | 0.3908 | 0.3997 | 0.4085 | 0.4174 | 0.4263 | 0.4352 |
| 5 | 0.4441 | 0.4530 | 0.4618 | 0.4707 | 0.4796 | 0.4885 | 0.4974 | 0.5062 | 0.5151 | 0.5240 |
| 6 | 0.5329 | 0.5418 | 0.5506 | 0.5595 | 0.5684 | 0.5773 | 0.5862 | 0.5951 | 0.6039 | 0.6128 |
| 7 | 0.6217 | 0.6306 | 0.6395 | 0.6483 | 0.6572 | 0.6661 | 0.6750 | 0.6839 | 0.6927 | 0.7016 |
| 8 | 0.7105 | 0.7194 | 0.7283 | 0.7372 | 0.7460 | 0.7549 | 0.7638 | 0.7727 | 0.7816 | 0.7904 |
| 9 | 0.7993 | 0.5082 | 0.8171 | 0.8260 | 0.8349 | 0.8437 | 0.8526 | 0.8615 | 0.8704 | 0.8793 |
| 10 | 0.8881 | 0.8970 | 0.9059 | 0.9148 | 0.9237 | 0.9325 | 0.9414 | 0.9503 | 0.9592 | 0.9681 |
| 11 | 0.97\%0 | 0.9855 | 0.9947 | 1.0036 | 1.0125 | 1.0214 | 1.0302 | 1.0391 | 1.0480 | 1.0569 |
| 12 | 1.0658 | 1.0746 | 1.0835 | 1.0924 | 1.1013 | 1.1102 | 1.1191 | 1.1279 | 1.1368 | 1.1457 |
| 13 | 1.1546 | 1.1635 | 1.1723 | 1.1812 | 1.1901 | 1.1990 | 1.2079 | 1.2168 | 1.2256 | 1.2345 |
| 14 | 1.2434 | 1.2523 | 1.2612 | 1.2700 | 1.2789 | 1.2878 | 1.2967 | 1.3056 | 1.3144 | 1.3233 |
| 15 | 1.3322 | 1.3411 | 1.3500 | 1.3589 | 1.3677 | 1.3766 | 1.3855 | 1.3944 | 1.4033 | 1.4121 |
| 16 | 1.4210 | 1.4299 | 1.4388 | 1.4477 | 1.4565 | 1.4654 | 1.4743 | 1.4832 | 1.4921 | 1.5010 |
| 17 | 1.5098 | 1.5187 | 1.5276 | 1.5365 | 1.5454 | 1.5542 | 1.5631 | 1.5720 | 1.5809 | 1.5898 |
| 18 | 1.5987 | 1.6075 | 1.6164 | 1.62 .53 | 1.6342 | 1.6431 | 1.6519 | 1.6608 | 1.6697 | 1.6786 |

1 Russian Half-Line $=1.269977$ Millimetres.

| Russian Half-Lines. | Tenths. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Millim. | Millim. | Millim. | Millim. | Millim. | Nillim. | Milli | Milli | Millim. |  |
| 0 | 0.000 | 0.127 | 0.254 | 0.381 | 2.508 | . 635 | 0.762 | 0.889 | 1.016 | 1.143 |
| 1 | 1.270 | 1.397 | 1.524 | 1.651 | .. 778 | 1.905 | 2.032 | 2.159 | 2.286 | 2.413 |
| 2 | 2.540 | 2.667 | 2.794 | 2.921 | 3.048 | 3.175 | 3.302 | 3.429 | 3.556 | 3.683 |
| 3 | 3.810 | 3.937 | 4.064 | 4.191 | 4.318 | 4.445 | 4.572 | 4.699 | 4.826 | 4.953 |
| 4 | 5.080 | 5.207 | 5.334 | 5.461 | 5.588 | 5.715 | 5.8 .42 | 5.969 | 6.096 | 6.223 |
| 5 | 6.350 | 6.477 | 6.604 | 6.731 | 6.858 | 6.985 | 7.112 | 7.239 | 7.366 | 7.493 |
| 6 | 7.620 | 7.747 | 7.874 | 8.001 | 8.128 | 8.255 | 8.382 | 8.509 | 8.636 | 8.763 |
| 7 | 8.890 | 9.017 | 9.144 | 9.271 | 9.398 | 9.525 | 9.652 | 9.779 | 9.906 | 10.033 |
| 8 | 10.160 | 10.287 | 10.414 | 10.541 | 10.668 | 10.795 | 10.922 | 11.049 | 11.176 | 11.303 |
| 9 | 11.430 | 11.557 | 11.684 | 11.811 | 11.938 | 12.065 | 12.192 | 12.319 | 12.446 | 12.573 |
| 10 | 12.700 | 12.827 | 12.954 | 13.081 | 13.208 | 13.335 | 13.462 | 13.589 | 13.716 | 13.843 |
| 11 | 13.970 | 14.097 | 14.224 | 14.351 | 14.478 | 14.605 | 14.732 | 14.859 | 14986 | 15.113 |
| 12 | 15.240 | 15.367 | 15.494 | 15.621 | 15.748 | 15.875 | 16.002 | 16.129 | 16.256 | 16.383 |
| 13 | 16.510 | 10.637 | 16.764 | 16.891 | 17.018 | 17.145 | 17.272 | 17.399 | 17.526 | 17.653 |
| 14 | 17.780 | 17.907 | 18.034 | 18.161 | 18.288 | 18.415 | 18.542 | 18.669 | 18.796 | 18.923 |
| 15 | 19.050 | 19.177 | 19.304 | 19.431 | 19.558 | 19.685 | 19.812 | 19.939 | 20.066 | 20.193 |
| 16 | 20.320 | 20.447 | 20.574 | 20.701 | 20.828 | 20.955 | 21.082 | 21.209 | 21.336 | 21.463 |
| 17 | 21.590 | 21.717 | 21.844 | 21.971 | 22.098 | 22.225 | 22.352 | 22.479 | 22.606 | 22.733 |
| 18 | 22.860 | 22.987 | 23.114 | 23.241 | 23.368 | 23.495 | 23.622 | 23.749 | 23.576 | 24.003 |

XVI. CONVERSION OF RUSSIAN HALF-LINES INTO PARIS LINES.

1 Russian Half-Line $=0.562976$ Paris Line.

| Russian Half-Lines. | Tenths. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Par. line | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. line. | Par. iine. |
| 0 | 0.000 | 0.056 | 0.113 | 0.169 | 0.225 | 0.281 | 0.338 | 0.394 | 0.450 | 0.507 |
| 1 | 0.563 | 0.619 | 0.676 | 0.732 | 0.788 | 0.8.4. | 0.901 | 0.957 | 1.013 | 1.070 |
| 2 | 1.126 | 1.182 | 1.239 | 1.295 | 1.351 | 1.407 | 1.464 | 1.520 | 1.576 | 1.633 |
| 3 | 1.689 | 1.745 | 1.802 | 1.558 | 1.914 | 1.970 | 2.027 | 2.083 | 2.139 | 2.196 |
| 4 | 2.252 | 2.308 | 2.364 | 2.421 | 2.477 | 2.533 | 2.590 | 2.646 | 2.702 | 2.759 |
| 5 | 2.815 | 2.871 | 2.927 | 2.984 | 3.040 | 3.096 | 3.153 | 3.209 | 3.265 | 3.322 |
| 6 | 3.378 | 3.434 | 3.490 | 3.547 | 3.603 | 3.659 | 3.716 | 3.772 | 3.823 | 3.885 |
| 7 | 3.941 | 3.997 | 4.053 | 4.110 | 4.166 | 4.222 | 4.279 | 4.335 | 4.391 | 4.448 |
| 8 | 4.504 | 4.560 | 4.616 | 4.673 | 4.729 | 4.755 | 4.842 | 4.898 | 4.954 | 5.010 |
| 9 | 5.067 | 5.123 | 5.179 | 5.236 | 5.292 | 5.348 | 5.405 | 5.461 | 5.517 | 5.573 |
| 10 | 5.630 | 5.686 | 5.742 | 5.799 | 5.855 | 5.911 | 5.968 | 6.024 | 6.080 | 6.136 |
| 11 | 6.193 | 6.249 | 6.305 | 6.362 | 6.418 | 6.474 | 6.531 | 6.587 | 6.643 | 6.699 |
| 12 | 6.756 | 6.812 | 6.868 | 6.925 | 6.981 | 7.037 | 7.093 | 7.150 | 7.206 | 7.262 |
| 13 | 7.319 | 7.375 | 7.431 | 7.488 | 7.544 | 7.600 | 7.656 | 7.713 | 7.769 | 7.825 |
| 14 | 7.882 | 7.938 | 7.994 | 8.051 | 8.107 | 8.163 | 8.219 | 8.276 | 8.332 | 8.388 |
| 15 | 8.445 | 8.501 | 8.557 | 8.614 | 8.670 | 8.726 | 8.782 | 8.839 | 8.895 | 8.951 |
| 16 | 9.008 | 9.064 | 9.120 | 9.177 | 9.233 | 9.289 | 9.345 | 9.402 | 9.458 | 9.514 |
| 17 | 9.571 | 9.627 | 9.683 | 9.739 | 9.796 | 9.852 | 9.908 | 9.965 | 10.021 | 10.077 |
| 18 | 10.134 | 10.190 | 10.246 | 10.302 | 10.359 | 10.415 | 10.471 | 10.528 | 10.584 | 10.640 |

## T A B L E S

FOR

# REDUCING BAROMETRICAL OBSERVATIONS, 

 TAKEN AT ANY TEMPERATURE,to the temperature of the freezing point.

## TABLES

## FOR

## 日EDUCING THE BAROMETRICAL OBSERVATIONS TAKEN AT ANY TEMPERATURE TO GIE TEMPERATURE OF THE FREEZING POINT.

The variations of the mercurial column in a stationary barometer are due to two causes, the changes of atmospheric pressure and the variations of temperature of the mercury, which affect the length of the column by changing its density. The variations of atmospheric pressure, which alone the barometer is destined to ascertain, are therefore hidden, and their observation falsified by the expansion or contraction of the mercury due to changes of temperature. For, supposing that, while the atmospheric pressure remains the same, the temperature of the instrument becomes lower, the mercurial column wi.: bccome shorter, and the barometer will appear to fall ; if the pressure becomes less, but the temperature increases, the expansion of the mercury will tend to compensate the diminution of pressure, and the barometer may remain stationary, or even may rise, while it ought to be falling ; in other cases the action of temperature will tend to increase the amount of the changes of the barometrical height. It is therefore evident that successive observations, with the same barumeter, do not give directly the actual changes of atmospheric pressure, unless they have been taken exactly at the same temperature, a case which, in practice, seldom occurs. Likewise simultaneous observations, taken with various barometers, do not geve directly the actual differences of the absolute pressure of the atmosphere above the instruments. To obtain the true barometrical heights, that is, the action of the atmospheric pressure alone, the influence of the temperature must first be eliminated from the observed heights. This is done by reducing, by means of the following Tables, the various barometrical columns to the length they would have at a given temperature, which is the same for all. For the sake of convenient comparison, the freezing point has been almost universally adopted as the standard temperature to which all observations are to be reduced.

## Construction of the Tables.

In all the following Tables the barometers are supposed to be furnished with brass scales, extending from the surface of the mercury in the cistern to the top of the mercurial column. The correction to be applied is therefore composed of two elements : the correction for the expansion of the mercury, and that for the expansion of the scale; both of which ought to be. and have been, taken into account.

Indeed, the correction for the expansion of mercury is not sufficient to reduce the readings to the height which the barometer would indicate, under the same pressure, at the temperature of the freezing point. For when the temperature rises the mer curial column expands; but then the scale also grows longer, and this will tend to lower the reading of the height. The correction for the expansion of the mercury S.
must thus be diminished by the amount of that of the scale, that is, by nearly ${ }_{1} \frac{1}{0}$ : this being the proportion between the expansion of brass and that of mercury.

It is also the expausion of the scale which causes an apparent anomaly in the Tables for the Reduction of the English and Old French Barometers. It can be seen, that, though the observations are to be reduced to the freezing point, or to $32^{\circ}$ Fahrenheit and zero Reaumur, the Tables give still a correction for observations taken at that temperature. The reason of it is, that the normal length of the English and (Old French standards has not been determined at the temperature of the freezing point, as is the case with the metre, but respectively at the temperatures of $62^{\circ}$ Fahrenheit and $13^{\circ}$ Reaumur. It is thus only at these temperatures that the scales graduated with these standards have their true length. Above and below, the inches of the scales are longer or shorter than the inches of the standards. At the freezing point, therefore, the correction for the expansion of the mercury is null, but that for the expansion of the scale is not. The scale bemg too short, the reading will be too high, and a subtractive correction must still be applied, which will be gradually compensated at lower temperatures by the now additive correction of the mercurial column. Thus the point of no correction will occur at $28^{\circ} .5$ Fahrenheit, instead of $32^{\circ}$, in the English Barometer, and at - $1^{\circ} .5$ Reaumur, instead of zero, in the Old French.

Schumacher has calculated and published in his Collection of Tables, \&c., and in his Jahr?uch for 1836, 1837, and 1838, extensive tables for the reduction of the Enylish, Old French, and Metrical Barometers, using the following general formula : -

Let $h=$ observed height.
" $t=$ temperature of the attached thermometer.
" $T=$ temperature to which the observed height is to be reduced.
" $m=$ expansion, in volume, of mercury.
" $l=$ linear expansion of brass.
" $\vartheta=$ normal temperature of the standard scale.
The reduction to the freezing point will be given by the formula, -

$$
h \cdot \frac{m(t-T)-l(t-\vartheta)}{1+m(t-T)}
$$

The following tables, which may be found more convenient for ordinary use, have been calculated from the same formula. Table XVII., published in the Instructions of the Royal Society of London, is mostly abstracted from the table of Sehumacher. It gives the reduction of the English Barometer, adopting the following values: -

Let $h=$ observed height in English inches.
" $t=$ temperature of attached thermometer in degrees of Fahrenheit.
" $m=$ expansion, in volume, of mercury for one degree Fahrenheit $=0.0001001$.
" $l=$ linear expansion of brass for one degree Fahrenheit $=0.0000104344$.
The normal temperature of standard being $=6 \mathfrak{Z}^{\circ}$.
The reduction to $3 \mathfrak{I}^{\circ}$ Fahrenheit will be given then by the formula,

$$
H-h . \frac{m(t-32)-l(t-62)}{1+m(t-32)}
$$

The elements for the other tables are found at the head of each.
XVII.

ENGLISH BAROMETFR.

## TABLE

giving the correction to be applied to english BAROMETERS,

With brass scales extending from the cistern to the top of the mercurial column, for reducing the observations to thirty-two degrees fahrenheit.

## Table XVII.

The following Table, calculated after that of Schumacher, has been adopted by the Cummittee of Physics and Meteorology of the Royal Society of London. It gives immediately the correction for every degree of Fahrenheit, and for every half-inch from 20 up to 31 inches. The scale of the barometer is supposed to be of brass, extending from the cistern to the top of the mercurial column. The difference of expansion of brass and mercury is taken into account. The standard temperature of the yard being $62^{\circ}$ Fahr., and not $32^{\circ}$ Fahr., the difference of expansion of the scale and of the mercurial column carries the point of no correction down to $29^{\circ}$ Fahr. Therefore, from $29^{\circ}$ up the correction mui Le iubtracted from, from $29^{\circ}$ down it must be added to, the observed height.

## Examples of Calculation.

Barometer, observea helght, . . . . . 30.231
Attached thermometer $82^{\circ}$ Fahr.
See in the last page the column of 30 inches; go down as far as the horizontal lime corresponding with $82^{\circ}$ in the first vertical column, which contains the temperatures ; you will find there the correction -.143. We have thus:-


It will be easy to apply also the correction for fractions of a degree Fahrenheit for example : -

Barometer, observed height, . . . . . 28.358
Attached thermometer 71.3
In the column of 28.5 inches, we find that the difference between the correction for $71^{\circ}$ and that for $72^{\circ}$ is .003 ; dividing this difference proportionally to the fraction, we have for three tenths of a degree a correction of -.001 , which added to -.108 , the correction for ${ }^{7} 1^{\circ}$, makes a total correction of, . . . . -. 109

$$
\text { And barometer at } 32^{\circ} \text { Fahr., . . . } \overline{28.249}
$$

| Degraes of Fahrenhet. | English Inches. |  |  |  |  |  |  |  | Degrees of Fihrenheit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 | 20.5 | 21 | 21.5 | 22 | 22.5 | 23 | 23.5 |  |
| 0 | +.051 | $+.053$ | + 054 | + 055 | +. 056 | +. 058 | +. 059 | $+.060$ | $\stackrel{0}{0}$ |
| 1 | . 049 | . 051 | .052 | . 053 | . 054 | . 056 | 057 | . 058 | 1 |
| 2 | . 048 | . 049 | . 050 | . 051 | . 052 | . 054 | . 055 | . 056 | 2 |
| 3 | . 046 | . 047 | . 048 | . 049 | . 050 | 052 | . 053 | . 054 | 3 |
| 4 | . 044 | . 045 | . 046 | . 047 | . 048 | . 050 | . 051 | . 052 | 4 |
| 5 | . 042 | . 043 | . 044 | . 045 | . 046 | . 048 | . 049 | . 050 | 5 |
| 6 | $+040$ | $+.042$ | +. 042 | +. 044 | +.044 | $+.046$ | +. 047 | +. 048 | 6 |
| 7 | . 039 | . 040 | . 041 | 042 | . 042 | . 044 | . 044 | . 046 | 7 |
| 8 | 037 | . 038 | .039 | . 040 | . 041 | . 041 | . 042 | . 043 | 8 |
| 9 | . 035 | . 036 | . 037 | . 038 | . 039 | . 039 | . 040 | . 041 | 9 |
| 10 | . 033 | . 034 | . 035 | . 036 | . 037 | . 037 | . 038 | . 039 | 10 |
| 11 | +.031 | +.032 | +.033 | +.034 | $+.035$ | $+.035$ | +. 036 | +.037 | 11 |
| 12 | . 030 | . 030 | 031 | 032 | . 033 | . 033 | . 034 | . 035 | 12 |
| 13 | . 028 | . 029 | . 029 | . 030 | . 031 | . 031 | . 032 | . 033 | 13 |
| 14 | . 026 | . 027 | . 027 | . 028 | . 029 | . 029 | . 030 | . 031 | 14 |
| 15 | . 024 | . 025 | . 026 | . $0 \geq 6$ | . 027 | . 027 | . 028 | . 029 | 15 |
| 16 | +.022 | +.023 | +.024 | +.024 | +. 025 | +.025 | +. 026 | +. 026 | 16 |
| 17 | . 021 | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 | . 024 | 17 |
| 18 | . 019 | . 019 | . 020 | . 020 | . 021 | . 021 | . 022 | . 022 | 18 |
| 19 | . 017 | . 018 | . 018 | . 018 | . 019 | . 019 | . 020 | . 020 | 19 |
| 20 | . 015 | . 016 | . 016 | . 016 | . 017 | . 017 | . 018 | . 018 | 20 |
| 21 | +.014 | +.014 | +014 | +.015 | +. 015 | +.015 | +. 015 | +.016 | 21 |
| 22 | . 012 | . 012 | 012 | . 013 | . 013 | . 013 | . 013 | . 014 | 22 |
| 23 | . 010 | . 010 | . 010 | . 011 | . 011 | . 011 | . 011 | . 012 | 23 |
| 24 | . 008 | . 008 | . 009 | . 009 | . 009 | . 009 | . 009 | . 010 | 24 |
| 25 | . 006 | . 007 | . 007 | . 007 | .007 | . 007 | . 007 | . 007 | 25 |
| 26 | $+.005$ | +.005 | $+.005$ | +. 005 | $+.005$ | +. 005 | +. 005 | +. 005 | 20 |
| 27 | . 003 | . 003 | . 003 | . 00.3 | . 003 | . 003 | . 003 | . 003 | 27 |
| 28 | . 001 | . 001 | . 001 | . 001 | . 001 | . 001 | . 001 | . 001 | 28 |
| 29 | -.001 | $-.001$ | -001 | -. 001 | -. 001 | $-.001$ | -. 001 | -. 001 | 29 |
| 30 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | 30 |
| 31 | -. 005 | -. 005 | $-.005$ | -. 005 | -. 005 | -. 005 | -. 005 | -. 005 | 31 |
| 32 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | 32 |
| 33 | . 008 | . 008 | . 008 | . 009 | . 009 | . 009 | . 009 | . 010 | 33 |
| 34 | . 010 | . 010 | . 010 | . 011 | . 011 | . 011 | . 011 | . 012 | 34 |
| 35 | .012 | . 012 | . 012 | . 013 | . 013 | . 013 | . 013 | . 014 | 35 |
| 36 | -. 013 | -. 014 | $-.014$ | -. 014 | -. 015 | -. 015 | -. 016 | -016 | 36 |
| 37 | . 015 | . 016 | . 016 | . 016 | . 017 | . 017 | . 018 | . 018 | 37 |
| 38 | . 017 | . 017 | . 018 | . 018 | . 019 | . 019 | . 020 | . 020 | 38 |
| 39 | . 019 | . 019 | . 020 | . 020 | . 021 | . 021 | . 022 | . 02.2 | 39 |
| 40 | . 021 | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 | . 024 | 40 |
| 41 | -. 022 | -. 023 | -. 024 | -. 024 | -. 025 | -. 025 | -. 026 | -.026 | 41 |
| 42 | . 024 | . 025 | . 025 | . 026 | . 027 | . 027 | . 028 | . 028 | 42 |
| 43 | . 026 | . 027 | . 027 | . 028 | . 029 | . 029 | . 030 | .031 | 43 |
| 44 | . 028 | . 029 | . 029 | . 030 | . 031 | .03] | . 032 | . 033 | 44 |
| 45 | . 030 | . 030 | . 031 | . 032 | . 033 | . 033 | . 034 | . 035 | 45 |
| 46 | -.031 | $-.032$ | $-.033$ | -. 034 | -. 035 | -. 035 | $-.036$ | -. 037 | 46 |
| 17 | . 033 | . 034 | . 035 | . 036 | . 036 | . 037 | . 038 | . 039 | 47 |
| 18 | . 035 | 036 | . 037 | . 038 | . 038 | . 039 | . 040 | . 041 | 48 |
| 49 | . 037 | . 038 | .039 | . 040 | . 040 | . 041 | . 042 | . 043 | 49 |
| 50 | . 038 | . 039 | . 040 | . 041 | . 042 | 043 | 044 | . 045 | 50 |



| Degrees of Fahrenhert. | English Inches. |  |  |  |  |  |  |  | Degrees of Falirenheit. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24 | 24.5 | 25 | 25.5 | 26 | 26.5 | 27 | 27.5 |  |
| ${ }_{0}$ | +. 061 | +. 063 | +.064 | +. 065 | +. 067 | +. 068 | +. 069 | +.071 | 0 |
| 1 | . 059 | . 061 | . 062 | . 063 | . 064 | . 065 | . 067 | . 068 |  |
| 2 | . 057 | . 058 | . 060 | . 061 | . 062 | . 063 | . 064 | . 066 | 2 |
| 3 | . 055 | . 056 | . 057 | . 059 | . 060 | . 061 | . 062 | . 063 | 3 |
| 4 | . 053 | .054 | . 055 | . 056 | . 057 | . 058 | . 059 | . 061 | 4 |
| 5 | . 051 | . 052 | . 053 | . 054 | . 055 | . 056 | . 057 | . 058 | 5 |
| 6 | +. 049 | $+.050$ | +.051 | $+.052$ | +.053 | $+.054$ | +. 055 | +. 056 |  |
| 7 | . 046 | . 047 | . 048 | . 049 | . 050 | . 051 | . 052 | . 053 | 7 |
| 8 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | . 051 | 8 |
| 9 | . 042 | . 043 | . 044 | . 045 | . 046 | . 046 | . 047 | . 048 | 9 |
| 10 | . 040 | . 041 | . 042 | . 042 | . 043 | . 044 | . 045 | . 046 | 10 |
| 11 | +.038 | +. 039 | +.039 | $+.040$ | +. 041 | +. 042 | +. 042 | +. 043 | 11 |
| 12 | . 036 | . 036 | . 037 | . 038 | . 039 | . 039 | . 040 | . 041 | 12 |
| 13 | . 033 | . 034 | . 035 | . 036 | . 036 | . 037 | . 038 | . 038 | 13 |
| 14 | . 031 | . 032 | . 033 | . 033 | . 034 | . 035 | . 035 | . 036 | 14 |
| 15 | . 029 | . 030 | . 030 | . 031 | .032 | . 032 | . 033 | . 033 | 15 |
| 16 | +. 027 | +.028 | +. 028 | +. 029 | +. 029 | +. 030 | +. 030 | +. 031 | 16 |
| 17 | . 02.5 | . 025 | . 026 | . 026 | . 027 | . 027 | . 028 | . 028 | 17 |
| 18 | . 023 | . 023 | . 024 | . 024 | . 025 | . 025 | . 025 | . 026 | 18 |
| 19 | . 021 | . 021 | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 | 19 |
| 20 | . 018 | . 019 | . 019 | . 020 | . 020 | . 020 | . 021 | . 021 | z0 |
| 21 | $+.016$ | $+.017$ | +.017 | +. 017 | +. 018 | +. 018 | +. 018 | +. 019 | 21 |
| 22 | . 014 | . 014 | . 015 | . 015 | . 015 | . 016 | . 016 | . 016 | 22 |
| 23 | . 012 | . 012 | . 012 | . 013 | . 013 | . 013 | . 013 | . 014 | 23 |
| 24 | . 010 | . 010 | . 010 | . 010 | . 011 | . 011 | . 011 | . 011 | 24 |
| 25 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 009 | . 009 | 25 |
| 26 | +. 005 | $+.006$ | $+.006$ | $+.006$ | $+.006$ | +. 006 | +. 006 | +. 006 | 26 |
| 27 | . 003 | . 003 | . 003 | . 003 | . 004 | . 004 | . 004 | . 004 | 27 |
| 28 | . 001 | . 001 | . 001 | . 001 | . 001 | .001 | . 001 | . 001 | 28 |
| 29 | -. 001 | -. 0001 | -001 | -.001 | -. 001 | -.001 | -. 001 | -. 001 | 29 |
| 30 | . 003 | . 003 | . 003 | . 004 | . 004 | . 004 | . 004 | . 004 | 30 |
| 31 | -. 005 | -. 006 | -. 006 | -. 006 | -. 006 | -. 006 | -.006 | -. 006 | 31 |
| 32 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 009 | 32 |
| 33 | . 010 | . 010 | . 010 | . 010 | . 011 | . 011 | . 011 | . 011 | 33 |
| 34 | . 012 | . 012 | . 012 | . 013 | . 013 | . 013 | .013 | . 014 | 34 |
| 35 | . 014 | . 014 | . 015 | . 015 | . 015 | . 015 | . 016 | 016 | 35 |
| 36 | -. 016 | -. 017 | $-.017$ | -. 017 | -. 017 | -. 018 | -. 018 | -. 019 | 36 |
| 37 | '. 018 | . 019 | . 019 | . 019 | . 020 | . 020 | . 021 | . 021 | 37 |
| 38 | . 020 | . 021 | . 021 | . 022 | . 022 | . 023 | . 023 | . 023 | 38 |
| 39 | . 023 | . 023 | . 024 | . 024 | . 024 | . 025 | . 025 | . 026 | 39 |
| 40 | . 025 | . 025 | . 026 | . 026 | . 027 | . 027 | . 028 | . 028 | 40 |
| 41 | -. 027 | -. 027 | -. 028 | -. 029 | -. 029 | -. 030 | -. 030 | -.031 | 41 |
| 42 | . 029 | . 030 | . 030 | . 031 | . 031 | 032 | . 033 | . 033 | 42 |
| 43 | . 031 | . 032 | . 032 | . 033 | . 034 | . 034 | . 035 | . 036 | 43 |
| 44 | . 033 | . 034 | . 035 | . 035 | . 036 | . 037 | . 037 | . 038 | 44 |
| 45 | . 035 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 | . 041 | 45 |
| 46 | $-.038$ | -. 038 | -. 039 | -. 040 | -. 041 | -. 042 | -. 042 | -. 043 | 46 |
| 47 | . 040 | . 041 | . 041 | . 042 | . 043 | . 044 | . 045 | . 046 | 47 |
| 48 | . 042 | . 043 | . 044 | . 045 | . 045 | . 046 | . 047 | . 048 | 48 |
| 49 | .044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | . 050 | 49 |
| 50 | . 046 | . 047 | . 048 | . 049 | . 050 | . 051 | . 052 | . 053 | 50 |


| Degrees of Fahrenheit. | English Inches. |  |  |  |  |  |  |  | Degrees of Fahrenheit. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24 | 24.5 | 25 | 25.5 | 26 | 26.5 | 27 | 27.5 |  |
| 51 | -. 048 | -. 049 | -. 050 | -. 051 | -052 | -. 053 | -. 054 | -. 055 | 51 |
| 52 | . 050 | . 052 | . 0.53 | . 054 | . 055 | . 056 | . 057 | . 058 | 52 |
| 53 | . 053 | . 054 | . 055 | . 056 | . 057 | . 058 | . 059 | . 060 | 53 |
| 54 | . 055 | . 056 | . 057 | . 058 | . 059 | 060 | . 062 | . 063 | 54 |
| 55 | . 057 | . 058 | . 059 | . 060 | . 062 | . 063 | . 064 | . 065 | 55 |
| 56 | -. 059 | -. 060 | -. 061 | -. 06.3 | -. 064 | -. 065 | -. 066 | -. 068 | 56 |
| 57 | . 061 | . 062 | . 064 | . 065 | . 066 | . 068 | . 069 | . 070 | 57 |
| 58 | . 063 | . 065 | . 066 | . 067 | . 069 | . 070 | . 071 | . 073 | 58 |
| 59 | . 065 | . 067 | . 068 | . 070 | . 071 | . 072 | . 074 | . 075 | 59 |
| 60 | . 068 | . 069 | . 070 | . 072 | . 073 | . 075 | . 076 | . 077 | 60 |
| 61 | $-.070$ | -. 071 | -. 073 | -. 074 | -. 075 | -. 077 | -. 078 | -. 080 | 61 |
| 62 | . 072 | . 073 | . 075 | . 076 | . 078 | . 079 | . 081 | . 082 | 62 |
| 63 | . 074 | . 076 | . 077 | . 079 | . 080 | . 188 | . 083 | . 085 | 63 |
| 64 | . 076 | . 078 | . 079 | . 081 | . 082 | . 084 | . 086 | . 087 | 64 |
| 65 | . 078 | . 080 | . 082 | . 083 | . 085 | . 086 | . 088 | . 090 | 65 |
| 66 | $-.080$ | -. 082 | -. 084 | -. 085 | -. 087 | -. 089 | -. 090 | -. 092 | 66 |
| 67 | . 083 | . 084 | . 086 | . 088 | . 089 | . 091 | . 093 | . 095 | 67 |
| 68 | . 085 | . 086 | . 088 | . 090 | . 092 | . 094 | . 095 | . 097 | 68 |
| 69 | . 087 | . 089 | . 090 | . 092 | . 094 | . 096 | . 098 | . 100 | 69 |
| 70 | . 089 | . 091 | . 093 | . 095 | . 096 | . 098 | . 100 | . 102 | 70 |
| 71 | -. 091 | $-.093$ | -. 095 | -. 097 | -. 099 | -. 101 | -. 102 | -. 104 | 71 |
| 72 | . 093 | . 095 | . 097 | . 099 | .101 | . 103 | . 105 | . 107 | 72 |
| 73 | . 095 | . 097 | . 099 | . 101 | . 103 | . 105 | .107 | . 109 | 73 |
| 74 | . 097 | . 099 | . 102 | . 104 | . 106 | . 108 | . 110 | . 112 | 74 |
| 75 | . 100 | . 102 | . 104 | . 106 | . 108 | . 110 | .112 | . 114 | 75 |
| 76 | -. 102 | -. 104 | -. 106 | -. 108 | -. 110 | -. 112 | -. 114 | -. 117 | 76 |
| 77 | . 104 | . 106 | . 108 | . 110 | . 112 | . 115 | 117 | . 119 | 77 |
| 78 | . 106 | . 108 | . 110 | . 113 | . 115 | . 117 | . 119 | . 122 | 78 |
| 79 | . 108 | . 110 | . 113 | . 115 | .117 | . 119 | . 122 | . 124 | 79 |
| 80 | . 110 | . 113 | . 115 | . 117 | . 119 | . 122 | . 124 | . 126 | 80 |
| 81 | -. 112 | -. 115 | $-117$ | -. 119 | -. 122 | -. 124 | $-.126$ | -. 129 | 81 |
| 82 | . 114 | . 117 | . 119 | . 122 | . 124 | . 126 | . 129 | . 131 | 82 |
| 83 | . 117 | . 119 | . 121 | . 124 | . 126 | . 129 | . 131 | . 134 | 83 |
| 84 | . 119 | . 121 | . 124 | . 126 | . 129 | . 131 | . 134 | . 136 | 84 |
| 85 | .121 | . 123 | . 126 | . 128 | . 131 | . 133 | . 136 | . 139 | 85 |
| 86 | -. 123 | -. 126 | -. 128 | -. 131 | -. 133 | -. 136 | -. 138 | -. 141 | 86 |
| 87 | . 125 | . 128 | . 130 | . 133 | . 136 | . 138 | . 141 | . 143 | 87 |
| 88 | . 127 | . 130 | . 133 | . 135 | . 138 | .141 | . 143 | . 146 | 88 |
| 89 | . 129 | . 132 | . 135 | . 137 | . 140 | . 143 | . 146 | . 148 | 89 |
| 90 | . 131 | . 134 | . 137 | . 140 | . 142 | . 145 | . 148 | . 151 | 90 |
| 91 | -. 134 | --. 136 | -. 139 | -. 142 | -. 145 | -. 148 | -. 150 | -. 153 | 91 |
| 92 | . 136 | . 139 | . 141 | . 144 | . 147 | . 150 | . 153 | . 156 | 92 |
| 93 | . 138 | . 141 | . 144 | . 147 | . 149 | . 152 | . 155 | . 158 | 93 |
| 94 | . 140 | . 143 | . 146 | . 149 | . 152 | . 155 | . 157 | . 161 | 94 |
| 95 | . 142 | . 145 | . 148 | . 151 | . 154 | . 157 | . 160 | . 163 | 95 |
| 96 | -. 144 | -. 147 | -. 150 | -. 153 | -. 156 | -. 159 | -. 162 | -. 165 | 96 |
| 97 | . 146 | . 149 | . 152 | . 156 | . 159 | . 162 | . 165 | . 168 | 97 |
| 98 | . 148 | . 152 | . 155 | . 158 | . 161 | . 164 | . 167 | . 170 | 98 |
| 99 | . 151 | . 154 | . 157 | . 160 | . 163 | . 166 | . 169 | . 173 | 99 |
| 100 | . 153 | . 156 | . 159 | . 162 | . 165 | . 169 | . 172 | . 175 | 100 |
|  |  |  |  |  |  |  |  |  |  |


| Degrees of Fahren. heit. | English Inches. |  |  |  |  |  |  | Degrees of Fahrenheit. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28 | 28.5 | 29 | 29.5 | 30 | 30.5 | 31 |  |
| $\stackrel{0}{0}$ | +. 072 | +.073 | +.074 | +. 076 | +. 077 | +. 078 | +. 080 | ${ }_{0} 0$ |
| 1 | . 069 | . 071 | . 072 | . 073 | . 074 | . 076 | . 077 | 1 |
| 2 | . 067 | . 068 | . 069 | .070 | .072 | . 073 | . 074 | 2 |
| 3 | 064 | . 065 | . 067 | . 068 | . 069 | .070 | . 071 | 3 |
| 4 | . 062 | . 063 | . 064 | . 065 | . 066 | . 067 | . 068 | 4 |
| 5 | . 059 | . 060 | . 061 | . 062 | . 063 | . 065 | . 066 | 5 |
| 6 | +.057 | +.058 | + 059 | +. 060 | +. 061 | +. 062 | +. 063 | 6 |
| 7 | . 054 | . 055 | . 056 | 057 | .058 | . 059 | . 060 | 7 |
| 8 | . 052 | . 053 | . 054 | . 054 | . 055 | . 056 | . 057 | 8 |
| 9 | . 049 | . 050 | . 051 | . 052 | . 053 | . 054 | . 054 | 9 |
| 10 | . 047 | . 047 | . 048 | . 049 | . 050 | . 051 | . 052 | 10 |
| 11 | +.044 | +. 045 | + 046 | +. 046 | +. 047 | +. 048 | +. 049 | 11 |
| 12 | . 042 | . 042 | . 043 | . 044 | . 045 | . 045 | . 046 | 12 |
| 13 | . 039 | . 040 | . 040 | . 041 | . 042 | . 043 | . 043 | 13 |
| 14 | . 037 | . 037 | . 038 | . 038 | . 039 | . 040 | . 040 | 14 |
| 15 | . 034 | . 035 | . 035 | . 036 | . 036 | . 037 | . 038 | 15 |
| 16 | +.032 | +.032 | +.033 | +.033 | +.034 | +. 034 | +. 035 | 16 |
| 17 | . 029 | . 030 | . 030 | . 031 | . 031 | . 032 | . 032 | 17 |
| 18 | . 026 | . 027 | . 027 | . 028 | . 028 | . 029 | . 029 | 18 |
| 19 | . 024 | .024 | . 025 | . 025 | . 026 | . 026 | . 027 | 19 |
| 20 | . 021 | . 022 | . 022 | .023 | . 023 | . 023 | . 024 | 20 |
| 21 | +. 019 | $+.019$ | $+.020$ | +. 020 | +. 020 | +. 021 | +. 021 | 21 |
| 22 | . 016 | . 017 | . 017 | . 017 | . 018 | . 018 | . 018 | 22 |
| 23 | . 014 | . 014 | . 014 | . 015 | . 015 | . 015 | . 015 | 23 |
| 24 | . 011 | . 012 | 012 | . 012 | . 012 | . 012 | . 013 | 24 |
| 25 | . 009 | . 009 | . 009 | -.009 | . 009 | . 010 | . 010 | 25 |
| 26 | $+.006$ | +. 005 | $+.007$ | +. 007 | +. 007 | +. 007 | $+.007$ | 26 |
| 27 | .004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | 27 |
| 28 | . 001 | . 001 | .001 | . 001 | . 001 | . 001 | . 001 | 28 |
| 29 | -.001 | -. 0001 | -001 | -.001 | -.001 | -. 001 | -.001 | 29 |
| 30 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | 30 |
| 31 | $-.006$ | -. 006 | -007 | $-.007$ | $-.007$ | -. 007 | -. 007 | 31 |
| 32 | . 009 | . 003 | . 009 | . 009 | . 009 | . 010 | . 010 | 32 |
| 33 | . 011 | . 012 | . 012 | . 012 | . 012 | . 012 | . 012 | 33 |
| 34 | . 014 | . 014 | 014 | . 015 | . 015 | . 015 | . 015 | 34 |
| 35 | . 016 | . 017 | . 017 | . 017 | . 018 | . 018 | . 018 | 35 |
| 36 | -. 019 | -. 019 | -. 020 | -. 020 | -. 020 | -021 | $-.021$ | 36 |
| 37 | . 021 | . 022 | . 022 | .02? | .023 | . 023 | . 024 | 37 |
| 48 | . 024 | . 024 | . 025 | . 025 | . 026 | . 026 | . 026 | 38 |
| 39 | . 026 | . 027 | . 027 | . 028 | . 028 | . 029 | . 029 | 39 |
| 40 | . 029 | . 029 | . 030 | . 030 | . 031 | . 031 | . 032 | 40 |
| 41 | $-.031$ | $-.032$ | -. 033 | -. 033 | $-.034$ | -. 034 | -. 035 | 41 |
| 42 | . 034 | . 034 | . 035 | . 036 | . 036 | . 037 | . 037 | 42 |
| 43 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 | . 040 | 43 |
| 44 | . 039 | . 040 | . 040 | . 041 | . 042 | . 042 | . 043 | 44 |
| 45 | . 041 | . 042 | . 043 | . 044 | . 044 | . 045 | . 046 | 45 |
| 46 | -. 044 | $-.045$ | -. 04.5 | -. 046 | $-.047$ | -. 048 | -. 049 | 46 |
| 47 | . 046 | . 047 | . 048 | . 049 | 050 | . 051 | . 051 | 47 |
| 48 | . 049 | . 050 | . 051 | . 052 | . 052 | . 053 | . 054 | 48 |
| 49 | . 051 | . 052 | . 053 | . 054 | . 055 | . 056 | . 057 | 49 |
| 50 | . 054 | . 0.55 | . 056 | 057 | . 058 | . 059 | . 060 | 50 |


| Degrees of Fahrenheit. | English Inches. |  |  |  |  |  |  | Degrees of Fatuenheit. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28 | 28.5 | 29 | 29.5 | 30 | 30.5 | 31 |  |
| 51 | -. 056 | -. 057 | -. 058 | -. 059 | -. 060 | -. 061 | -. 062 | 51 |
| 52 | . 059 | . 060 | . 061 | . 062 | . 063 | . 064 | . 065 | 52 |
| 53 | . 061 | . 063 | 064 | . 065 | . 066 | . 067 | . 068 | 53 |
| 54 | . 064 | . 065 | . 066 | . 067 | . 068 | . 070 | . 071 | 54 |
| 55 | . 066 | . 068 | . 069 | . 070 | . 071 | . 072 | . 073 | 55 |
| 56 | -. 069 | -. 070 | -. 071 | -. 073 | -. 074 | -. 075 | -. 076 | 56 |
| 57 | . 071 | . 073 | . 074 | . 075 | . 076 | .078 | .079 | 57 |
| 58 | . 074 | . 075 | . 077 | . 078 | . 079 | .081 | . 082 | 58 |
| 59 | . 076 | . 078 | . 079 | . 080 | . 082 | . 083 | . 085 | 59 |
| 60 | . 079 | . 080 | . 082 | . 083 | . 085 | . 086 | . 087 | 60 |
| 61 | -. 081 | -. 083 | $-.084$ | $-.086$ | -. 087 | -. 089 | -. 090 | 61 |
| 62 | . 084 | . 085 | . 087 | . 088 | . 090 | . 091 | . 093 | 62 |
| 63 | . 086 | . 088 | .089 | . 091 | . 093 | . 094 | . 096 | 63 |
| 64 | . 089 | . 090 | . 092 | . 094 | . 095 | . 097 | . 098 | 64 |
| 65 | . 091 | . 093 | . 095 | . 096 | . 098 | . 100 | . 101 | 65 |
| 66 | -. 094 | -. 096 | -. 097 | -. 099 | -. 101 | -. 102 | -104 | 66 |
| 67 | . 096 | . 098 | . 100 | . 102 | . 103 | 10.5 | . 107 | 67 |
| 68 | . 099 | .101 | . 102 | 104 | . 106 | . 108 | . 109 | 68 |
| 69 | . 101 | . 103 | . 105 | . 107 | . 109 | . 110 | .112 | 69 |
| 70 | . 104 | .106 | . 108 | . 109 | . 111 | . 113 | . 115 | 70 |
| 71 | -. 106 | -. 108 | -. 110 | -. 112 | -. 114 | -. 116 | -. 118 | 71 |
| 72 | . 109 | . 111 | . 113 | . 115 | . 117 | . 119 | . 120 | 72 |
| 73 | . 111 | . 113 | . 115 | . 117 | . 119 | . 121 | .123 | 73 |
| 74 | .114 | . 116 | . 118 | . 120 | .122 | . 124 | . 126 | 74 |
| 75 | . 116 | . 118 | . 120 | .122 | . 125 | . 127 | . 129 | 75 |
| 76 | -. 119 | -. 121 | -. 123 | - 12.5 | -. 127 | -. 129 | - 131 | 76 |
| 77 | . 121 | . 123 | . 126 | 128 | .130) | . 132 | . 134 | 77 |
| 78 | . 124 | .126 | .128 | . 130 | . 133 | . 135 | . 137 | 78 |
| 79 | . 126 | . 128 | . 131 | . 133 | . 135 | . 137 | . 140 | 79 |
| 80 | . 129 | . 131 | . 133 | . 136 | . 138 | . 140 | . 143 | 80 |
| 81 | -. 131 | -. 134 | -.136 | -. 138 | -. 141 | -. 143 | -. 145 | 81 |
| 82 | . 134 | . 136 | . 138 | .141 | .143 | . 146 | . 148 | 82 |
| 83 | . 136 | . 139 | .141 | . 14.3 | . 146 | . 148 | . 151 | 83 |
| 84 | . 139 | . 141 | . 144 | . 146 | . 149 | . 151 | ist | 84 |
| 85 | . 141 | . 144 | . 146 | . 149 | .151 | . 154 | . 156 | 85 |
| 86 | -. 144 | -. 146 | -. 149 | -. 151 | -. 154 | -. 156 | -. 159 | 86 |
| 87 | . 146 | . 149 | . 151 | . 154 | . 157 | . 159 | . 162 | 87 |
| 88 | . 149 | . 151 | . 154 | . 157 | . 159 | . 162 | . 165 | 88 |
| 89 | . 151 | . 154 | . 156 | . 159 | .162 | . 165 | . 167 | 89 |
| 90 | . 153 | . 156 | . 159 | . 162 | . 164 | . 167 | . 170 | 90 |
| 91 | -. 156 | -. 159 | -. 162 | -. 165 | -. 167 | - 170 | $-173$ | 91 |
| 92 | . 158 | . 161 | 164 | . 167 | .170 | .172 | . 175 | 92 |
| 93 | . 161 | . 164 | . 167 | . 170 | .172 | . 75 | . 178 | 93 |
| 94 | . 163 | . 166 | . 169 | . 172 | . 175 | .177 | . 180 | 94 |
| 95 | . 166 | . 169 | . 172 | . 175 | . 178 | . 180 | . 183 | 95 |
| 96 | -. 168 | -. 171 | -.174 | -. 178 | -. 181 | -. 183 | -. 186 | 96 |
| 97 | . 171 | . 174 | . 177 | . 180 | . 183 | . 186 | . 189 | 97 |
| 98 | . 173 | . 176 | . 179 | . 183 | . 186 | . 188 | . 191 | 98 |
| 99 | . 176 | . 179 | . 182 | . 185 | . 188 | . 191 | . 194 | 99 |
| 100 | . 178 | . 181 | . 184 | . 188 | . 191 | . 194 | 197 | 100 |

## TABLE XVIJ.

## FOR REDUCING THE INDICATIONS OF ENGLISH BAROMETERS, WITH WOODEN OR glass scales, to the freezing point.

In most of the common barometers the seale is engraved upon a short plate of brass, or of ivory, fixed upon the wooden frame of the instrument. In such a case, the compound expansion of the two substances can only be guessed at, and the correction to be applied to the observations for reducing them to the freezing point cannot be determined with precision. As a near approximation for such imperfect instruments, the following table may be used. In computing this table, the expansion of glass, which is less than that of brass and greater than that of wood, has been substituted for that of brass, as an approximate value for a scale composed of these last two substances. The table thus gives the true correction, in English inches, for the barometers, the graduation of which is engraved on the glass tube itself. It answers equally for any English barometer with wooden scale, whatever be the substance of which the short plate bearing the graduation is made.

CORRECTIONS TO BE APPLIED TO ENGLISH BAROMETERS, WITH WOODEN OR GLASS SCALES, TO REDUCE THE OBSERYATIONS TO THE FREEZING POINT.

Expansion of Mercury for $1^{\circ}$ Fahr. $=0.0001001$; of Glass for $1^{\circ}$ Fahr. $=0.00000444$.

| Attached <br> Thermom- <br> eter, <br> Fanren- <br> heit | Barometer in English Inches. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26 | -26.5 | 27 | 27.5 | 28 | 28.5 | 29 | 29.5 | 30 | 30.5 | 31 |
| 0 | +.076 | $+.077$ | $+.079$ | $+.080$ | +. 082 | $+.059$ | $+.085$ | $+.086$ | $+.088$ | $+.089$ | $+.090$ |
| 1 | +.073 | +.075 | +.076 | +. 078 | +. 079 | +.0s0 | +.082 | +.083 | +.085 | +.086 | +.088 |
| 2 | +.071 | +.072 | +.074 | +.075 | +.076 | +.078 | +.079 | $+.080$ | +.082 | +. 083 | +.085 |
| 3 | $+.068$ | +.070 | $+.071$ | +.072 | +.074 | +.075 | $+.076$ | +.078 | +. 079 | $+.080$ | +.082 |
| 4 | $+.066$ | +.067 | +. 069 | $+.070$ | +. 071 | +.072 | +.074 | $+.075$ | $+.076$ | $+.077$ | +. 079 |
| 5 | +.064 | +.065 | $+.066$ | $+.067$ | $+.068$ | +.070 | +. 071 | +. 072 | $+.073$ | +.074 | +.076 |
| 6 | +.061 | +.062 | $+.063$ | +.065 | +. 066 | +.067 | +.068 | +. 069 | +. 070 | +.072 | +.073 |
| 7 | +.059 | +.060 | +.061 | $+.062$ | +. 063 | +.064 | +.065 | +.067 | $+.065$ | $+.069$ | $+.070$ |
| 8 | +. 056 | +.037 | +.059 | +.059 | $+.060$ | +. 061 | +.063 | +.064 | +. 065 | $+.066$ | +. 067 |
| 9 | $+.054$ | +.05. | +.056 | $+.057$ | +.038 | +.059 | $+.060$ | ${ }^{+}+.061$ | $+.062$ | $+.063$ | $+.064$ |
| 10 | $+.051$ | $+.0 .92$ | +.05\% | $+.054$ | $+.0 .55$ | $+.0 .56$ | $+.057$ | +.058 | +. 059 | $+.060$ | +. 061 |
| 11 | +. 049 | +.050 | +.031 | $+.051$ | +.052 | +.053 | $+.054$ | +.0.55 | +.056 | $+.057$ | +.058 |
| 12 | +. 046 | $+.047$ | $+.048$ | +.049 | $+.050$ | +.0.51 | $+.052$ | $+.052$ | +.053 | $+.054$ | +.055 |
| 13 | $+.044$ | $+.045$ | +.04.5 | $+.046$ | $+.047$ | +. 048 | +. 049 | $+.0 .50$ | +. 050 | +. 051 | +. 052 |
| 14 | +.041 | $+.042$ | $+.043$ | +.044 | +. 044 | +. 045 | $+.046$ | $+.047$ | $+.048$ | $+.048$ | $+.049$ |
| 15 | +. 039 | +. 039 | $+.040$ | $+.041$ | $+.042$ | $+.042$ | $+.043$ | +.044 | $+.045$ | $+.045$ | +. 046 |
| 16 | +.036 | +.037 | +.035 | +.038 | $+.039$ | $+.040$ | $+.010$ | +.041 | $+.042$ | $+.043$ | +.043 |
| 17 | +.034 | +.034 | +.035 | $+.036$ | $+.036$ | +.037 | +.038 | $+.038$ | +.039 | +. 040 | $+.040$ |
| 18 | +.031 | +.032 | +.032 | +.033 | +.034 | +.034 | +.035 | +. 036 | +. 036 | +.037 | +. 037 |
| 19 | +.029 | +.029 | $+.030$ | +.030 | +.031 | +.032 | +. 032 | +.033 | $+.033$ | +.034 | +.034 |
| 20 | $+.026$ | +.027 | +.027 | +. 028 | $+.028$ | $+.029$ | +.029 | $+.030$ | $+.030$ | +.031 | +.031 |

Barometer with Glass or Wooden Scale.

| Attached <br> Thermoneter, <br> Fahrenheit. | Barometer in English Inches. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26 | 26.5 | 27 | 27.5 | 28 | 28.5 | 29 | 29.5 | 30 | 30.5 | 31 |
| $21{ }^{\circ}$ | +.024 | +.02t | +. 025 | +.02.5 | $+.026$ | $+.026$ | +. 027 | $+.027$ | +.028 | +. 028 | +.028 |
| 22 | +.021 | $+.022$ | $+.022$ | +.023 | $+.022$ | $+.023$ | $+.024$ | $+.024$ | $+.025$ | $+.025$ | +.025 |
| 23 | +. 019 | $+.019$ | $+.020$ | $+.020$ | $+.020$ | $+.021$ | $+.021$ | $+.021$ | +.022 | $+.022$ | +.023 |
| 21 | +. 016 | $+.017$ | $+.017$ | $+.017$ | +.018 | +.018 | +.015 | $+.019$ | $+.019$ | $+.019$ | $+.020$ |
| 25 | $+.014$ | $+.014$ | +.014 | $+.015$ | $+.015$ | $+.015$ | $+.016$ | $+.016$ | +. 016 | $+.016$ | $+.017$ |
| 26 | +. 011 | $+.012$ | $+.012$ | +.012 | +.012 | $+.013$ | $+.013$ | $+.013$ | $+.013$ | $+.013$ | +.014 |
| 27 | +. 009 | +. 009 | $+.009$ | +. 009 | +.010 | +.010 | +. 010 | +. 010 | +. 010 | +.011 | +.011 |
| 28 | +.006 | +.007 | +. 007 | +.007 | $+.007$ | +. 007 | +.007 | +.007 | $+.007$ | $+.008$ | $+.008$ |
| 29 | +.004 | $+.004$ | +.004 | $+.004$ | $+.004$ | $+.004$ | $+.004$ | +.005 | +. 005 | +. 005 | +. 005 |
| 30 | $+.002$ | $+.002$ | $+.002$ | $+.002$ | $+.002$ | $+.002$ | $+.002$ | $+.002$ | +.002 | +.002 | +. 002 |
| 31 | -. 001 | -. 001 | -.001 | -. 001 | -. 001 | -. 001 | -. 001 | -. 001 | -. 001 | $-.001$ | -. 001 |
| 32 | -. 003 | $-.004$ | -.004 | -.004 | -.004 | $-.004$ | -.004 | -. 004 | -. 004 | -.004 | -.004 |
| 33 | -. 006 | -. 006 | -.006 | -. 006 | -. 006 | -. 007 | -. 007 | -.007 | -. 007 | -. 007 | -. 007 |
| 34 | -. 008 | $-.009$ | $-.009$ | -. 009 | -.009 | -. 009 | -. 009 | -. 010 | -. .10 | $-.010$ | $-.010$ |
| 35 | -. 011 | $-.011$ | -. 911 | -. 012 | -. 012 | -. 012 | -. 012 | -. 012 | -. 613 | -. 013 | -. 013 |
| 36 | -. 013 | -. 014 | -.014 | -. 014 | -. 014 | -. 015 | -. 015 | -. 015 | -. 015 | --. 016 | -. 016 |
| 37 | -. 016 | -. 016 | -. 017 | -. 017 | -. 017 | -. 017 | -. 018 | -. 018 | -. 018 | -. 019 | -. 019 |
| 38 | -. 018 | $-.019$ | -. 019 | $-.019$ | $-.020$ | $-.020$ | $-.020$ | $-.021$ | -. 021 | -. 022 | -. 022 |
| 39 | -.021 | $-.021$ | $-.022$ | $-.022$ | -. 022 | $-.023$ | -.023 | $-.024$ | -. 024 | -.024 | -. 025 |
| 40 | $-.023$ | -.024 | -.024 | -. 025 | -.025 | $-.026$ | -. 026 | $-.026$ | -. 027 | -. 027 | -.028 |
| 41 | -. 026 | $-.026$ | -. 027 | $-.027$ | -. 028 | -. 028 | -. 029 | $-.029$ | $-.030$ | $-.030$ | -.031 |
| 42 | -.025 | -. 029 | -.029 | -.030 | -.030 | -. 031 | -.032 | -.032 | -. 033 | -.033 | -.034 |
| 43 | -.031 | -. 031 | -. 032 | $-.033$ | -.033 | -.034 | -. 033 | -. 035 | -.036 | -.036 | -.037 |
| 4.4 | -.033 | -.034 | -.035 | -. 035 | -.036 | -. 036 | -. 036 | -.035 | -. 038 | -.039 | -. 040 |
| 45 | $-.036$ | -. 036 | -. 037 | -.033 | -.038 | -. 039 | -. 039 | -. 041 | -. 0.41 | -. 042 | $-.043$ |
| 46 | -.038 | -. 039 | $-.040$ | -. 040 | $-.041$ | $-.042$ | -. 042 | $-.043$ | $-.044$ | -. 045 | $-.046$ |
| 47 | -.041 | -. 041 | $-.042$ | $-.043$ | -.044 | -. 045 | $-.044$ | $-.016$ | -. 047 | -. 048 | -. 049 |
| 48 | -. 013 | -. 041 | -. 045 | $-.046$ | -. 047 | $-.047$ | $-.047$ | -. 049 | -. 050 | -. 0.51 | -.0.51 |
| 49 | -. 046 | -. 046 | $-.047$ | -. 048 | -. 019 | -.050 | -.050 | -.0.52 | -.0.93 | $-.054$ | $-.054$ |
| 50 | -.048 | -. 049 | $-.050$ | -.051 | -.052 | -.053 | $-.054$ | -.0̄5 | -. 056 | -. 056 | -. 057 |
| 51 | -. 051 | $-.052$ | -. 053 | $-.054$ | -. 055 | -. 055 | -.0.56 | -. 057 | $-.0 .58$ | $-.059$ | $-.060$ |
| 52 | -.0.53 | -. 054 | -. 055 | -.056 | -. 0.57 | -.0.58 | -.0.59 | -. 060 | -. 061 | -. 062 | -. 063 |
| 53 | -.0.56 | $-.057$ | -. 055 | -.059 | -. 060 | $-.061$ | -.062 | -. 063 | -. 064 | -. 06.5 | -. 066 |
| 54 | -.058 | -.0.59 | -. 060 | -. 061 | -.063 | -.064 | -.06.) | -. 066 | -. 067 | -. 068 | -. 069 |
| 55 | -. 061 | $-.062$ | $-.063$ | $-.064$ | -. 065 | $-.066$ | -. 068 | $-.069$ | -. 070 | $-.071$ | -. 072 |
| 56 | -. 063 | -. 064 | -. 06.5 | -. 067 | -. 068 | -. 069 | -. 070 | -. 071 | -. 073 | -. 074 | -. 075 |
| 57 | -. 065 | -. 067 | -. 068 | -. 069 | -. 071 | $-.072$ | $-.073$ | -. 074 | -. 076 | -. 077 | -. 078 |
| 53 | -. 068 | -. 069 | -. 071 | -.072 | -. 073 | -.074 | -.076 | -. 077 | -. 078 | -. 080 | -. 081 |
| 59 | -.070 | -.072 | -. 073 | $-.074$ | -. 076 | -. 077 | -. 079 | -. 080 | -. 081 | -.083 | -.054 |
| 60 | -. 073 | -.074 | -. 076 | -.077 | -. 079 | -.080 | -. 081 | $-.083$ | -. 084 | -. 085 | -. 087 |

Barometer with Glass or Wooden Scale.

| Attached <br> Thermom eter, Fahrenheit. | Barometer in English Inches. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26 | 26.5 | 27 | 27.5 | 28 | 28.5 | 29 | 29.5 | 30 | 30.5 | 31 |
| 61 | -.075 | -. 077 | -. 075 | -. 080 | -. 051 | -. 083 | -.084 | -. 086 | -. 087 | -. 088 | -. 090 |
| 62 | -. 078 | -. 079 | -.0ъ1 | -.032 | -.084 | -.085 | $-.087$ | -.058 | -. 090 | -. 091 | -. 093 |
| 63 | -.080 | -.082 | -. 083 | -.08.5 | -.086 | -. 08 s | -. 090 | -. 091 | -. 093 | -.094 | $-.096$ |
| 61 | -.083 | -.084 | -. 086 | -. 088 | -.089 | -. 091 | -.092 | -.094 | -. 096 | -. 097 | -. 099 |
| 65 | $-.055$ | -.007 | -. 089. | -. 090 | -. 092 | -. 093 | -.095 | -. 097 | -. 098 | $-.100$ | -. 102 |
| 66 | -. 098 | -. 039 | -. 091 | $-.093$ | -. 091 | -. 096 | -. 098 | -. 100 | -. 101 | -. 103 | -. 104 |
| 67 | -. 030 | -.092 | -. 094 | -.09.5 | -. 097 | -. 099 | -. 101 | $-.102$ | -. 104 | -. 106 | -. 108 |
| 68 | -.093 | -.094 | -. 096 | -.095 | -. 100 | -. 102 | -.103 | -. 105 | -. 107 | -. 109 | $-.110$ |
| 69 | -.09. | -. 097 | -. 099 | -. 101 | $-.102$ | -. 101 | $-.106$ | -. 108 | -. 110 | -. 112 | -. 113 |
| 70 | $-.093$ | -. 099 | -. 101 | -. 103 | -. 105 | -. 107 | -. 109 | -. 111 | -. 113 | -.114 | -. 116 |
| 71 | -. 100 | -. 102 | -. 104 | -. 106 | -. 108 | -. 110 | $-.112$ | -. 114 | -. 115 | -. 117 | -. 119 |
| 72 | -.103 | -.10. | -. 106 | -. 103 | -. 110 | -.112 | -.114 | -. 116 | -. 118 | -. 120 | -. 122 |
| 73 | -.105 | -. 107 | -. 109 | -. 111 | -. 113 | -.115 | -. 117 | -. 119 | -. 121 | -. 123 | -. 125 |
| 7.4 | -. 107 | -. 110 | -. 112 | -.114 | -. 116 | -. 118 | -. 120 | $-.122$ | -.124 | -.126 | $-.128$ |
| 75 | -. 110 | -.112 | -. 114 | -. 116 | -. 118 | -. 121 | $-.123$ | -. 125 | -. 127 | -. 129 | -. 131 |
| 76 | -.112 | -. 115 | -. 117 | -. 119 | -. 121 | -. 123 | -. 125 | -. 128 | $-.130$ | -. 132 | -. 134 |
| 77 | -.115 | -. 117 | -. 119 | $-.121$ | -.124 | -. 126 | -. 128 | -. 130 | -.133 | -. 135 | -. 137 |
| 78 | -. 117 | $-.120$ | $-.122$ | -.121 | -.126 | -. 129 | -.131 | -.13: | -. 135 | -. 138 | $-.140$ |
| 79 | -. 120 | -.122 | -.124 | -. 127 | -. 129 | -. 131 | -.134 | -. 136 | -. 135 | $-.141$ | $-.143$ |
| so | -.122 | -. 125 | $-.127$ | $-.129$ | -. 132 | -. 134 | -. 136 | -. 139 | -.141 | -. 143 | -. 146 |
| 81 | -.12.5 | $-.127$ | -. 130 | -.132 | -. 134 | -. 137 | -. 139 | -. 142 | -.144 | -. 146 | -. 149 |
| 82 | -.127 | -.1:30 | -.132 | -.135 | -. 137 | -. 139 | -.142 | -.141 | -. 147 | -. 119 | -. 152 |
| 83 | -.130 | -.132 | -.13) | -.137 | -. 140 | $-.142$ | $-.115$ | -. 147 | -.150 | -. 152 | $-.155$ |
| 84 | -.132 | -. 135 | -. 137 | $-.140$ | $-.142$ | $-.14 .5$ | $-.147$ | -. 150 | $-.152$ | -.155 | -. 158 |
| 85 | -.135 | -. 137 | $-.140$ | $-142$ | -.14.5 | -. 147 | -. 150 | -. 153 | -. 155 | -. 158 | -. 160 |
| 86 | $-137$ | -. 140 | -.142 | -.14. | -. 142 | -. 150 | $-.153$ | -.15.5 | -.158 | -. 161 | -. 163 |
| 87 | -. 139 | $-142$ | -. 145 | -. 148 | -. 150 | -.153 | -. 156 | -. 1.15 | -. 161 | $-.164$ | -. 166 |
| 88 | -.142 | -.14. | -. 147 | $-.150$ | -.1.53 | -. 156 | -.155 | -. 161 | -. 164 | -. 167 | -. 169 |
| s9 | -. 144 | -. 147 | -. 150 | $-.153$ | -.156 | -. 158 | -. 161 | -. 16.4 | -. 167 | -. 169 | -.172 |
| 90 | -. 147 | -. 150 | -. 153 | -. 15.5 | -. 158 | -. 161 | -. 164 | -. 167 | -. 169 | $-.172$ | -. 175 |
| 91 | -. 149 | -.152 | -. 155 | -. 158 | -. 161 | -.164 | -. 167 | -. 169 | -.172 | -.17. | -.178 |
| 92 | -.152 | -.15\% | -. 158 | -. 161 | -. 163 | -. 166 | -. 169 | -.172 | -. 175 | -. 178 | -. 181 |
| 93 | -.154 | -.1.57 | -. 160 | -.163 | -. 166 | $-.169$ | $-.172$ | -.17.5 | -.178 | -. 181 | -.184 |
| 94 | -. 1.57 | -. 160 | -. 163 | -. 166 | $-.169$ | $-.172$ | -. 175 | -. 178 | -. 181 | -.184 | -. 157 |
| 9.5 | -. 159 | $-.162$ | -. 165 | -. 165 | -.171 | -.17.4 | -. 178 | -. 181 | -. 184 | $-.157$ | $-.190$ |
| 96 | -. 162 | -.16.5 | -. 168 | -. 171 | -.174 | -.177 | -. 180 | -. 183 | -. 186 | $-.190$ | -. 193 |
| 97 | -. 164 | -. 167 | -. 170 | -.174 | $-.177$ | -. 180 | $-.183$ | -. 186 | -. 189 | -.192 | -. 196 |
| 98 | -. 167 | -. 170 | -. 173 | -.176 | -. 179 | -. 183 | $-.186$ | -. 189 | -. 192 | -. 195 | -. 199 |
| 99 | -. 169 | $-.172$ | -.17.5 | -.179 | -. 182 | -.185 | $-.183$ | -.192 | -. 195 | -. 198 | -. 201 |
| 109 | -.171 | -.17.) | -.179 | -.1-1 | -.155 | -. 185 | -. 191 | -:191 | -.198 | -.201 | -. 204 |

## XIX.

## METRICAL BAROMETER.

## T A B L E

FOR

## \&EDUCING 10 THE FREEZING POINT THE P 4 ROMETRICAI COLUMN,

MEASURED BY BRASS SCALES, EXTENDING FRON THE CISTERN sO THE TOP; CALCULATED FROM 260 TO 865 MILLIMETRES, AND FOR EACH DEGREE CENTIGRADE.

By M. T. Delcrus.

C

Table XIX.
'This table has been calculated by using the following coefficients of dilatation : Brass, linear dilatation, from Laplace and Lavoisier for $100^{\circ} \mathrm{C} .=0.0018782$. Mercury, dilatation in volume, from Dulong and Petit for $100^{\circ} \mathrm{C} .=0.0180180$.
Dilatation of the mercurial column for $100^{\circ} \mathrm{C}$. . . $=0.0161398$.
Dilatation of the mercurial column for $1^{\circ} \mathrm{C}$. . . $=0.0001614$.
Observed height reduced to freezing point,

$$
H=h-h(0.0001614) . \quad T=h-h\left(\frac{T}{6196}\right) .
$$

The second term of this last formula is given by the table. when the temperature $T$ and the height $h$ of $t a s$ barometer are known; this correction must be subtracted from the observed height $h$, when the temperature is above freezing point; it is to be added when the temperature is below zero, or freezing point.

This table allows the barometrical heights taken at the highest summits, and 'n the deepest mines, to be corrected.

## Examples of Calculation.




| Heightof Ule Barone ter. | temperatulie centigrade. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4{ }^{\circ}$ | $5^{\circ}$ | 6 | $7{ }^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |
| Millim | Millim. | Millim. | Millim. | Millim. | Millim | Millim, | Millim. | Nillim. | Millim. |
| 460 | 0.0742 | 0.1485 | 0.2227 | 0.2970 | 0.371 | 0.445 | 0.520 | 0.594 | 0.668 |
| 465 | 0.0750 | 0.1501 | 0.2251 | 0.3002 | 0.375 | 0.450 | 0.525 | 0.600 | 0.675 |
| 470 | 0.0759 | 0.1517 | 0.2276 | 0.303 .4 | 0.379 | 0.455 | 0.531 | 0.607 | 0.683 |
| 475 | 0.0767 | 0.1533 | 0.2300 | 0.3066 | 0.383 | 0.460 | 0.537 | 0.613 | 0.690 |
| 480 | 0.0775 | 0.1549 | 0.2324 | 0.3099 | 0.387 | 0.465 | 0.542 | 0.620 | 0.697 |
| 485 | 0.0783 | 0.1565 | 0.2348 | 0.3131 | 0.391 | 0.470 | 0.548 | 0.626 | 0.704 |
| 490 | 0.0791 | 0.1582 | 0.2373 | 0.3163 | 0.395 | 0.474 | 0.554 | 0.633 | 0.712 |
| 49.5 | 0.0800 | 0.1598 | 0.2397 | 0.3195 | 0.399 | 0.479 | 0.559 | 0.639 | 0.719 |
| 510 | 0.0807 | 0.1614 | 0.2421 | 0.3228 | 0.403 | 0.484 | 0.565 | 0.646 | 0.726 |
| 505 | 0.0815 | 0.1630 | 0.2445 | 0.3260 | 0.407 | 0.489 | 0.570 | 0.652 | 0.734 |
| 510 | 0.0823 | 0.1646 | 0.2469 | 0.3293 | 0.412 | 0.494 | 0.576 | 0.658 | 0.741 |
| 515 | 0.0831 | 0.1662 | 0.2493 | 0.3325 | 0.416 | 0.499 | 0.582 | 0.665 | 0.748 |
| 520 | 0.0839 | 0.1679 | 0.2518 | 0.3357 | 0.420 | 0.504 | 0.587 | 0.671 | 0.755 |
| 525 | 0.0847 | 0.1695 | 0.2542 | 0.3359 | 0.424 | 0.508 | 0.593 | 0.678 | 0.763 |
| 530 | 0.0555 | 0.1711 | 0.2566 | 0.3422 | 0.428 | 0.513 | 0.599 | 0.684 | 0.770 |
| 535 | 0.0863 | 0.1727 | 0.2.590 | 0.3454 | 0.432 | 0.518 | 0.604 | 0.691 | 0.777 |
| 540 | 0.0872 | 0.1743 | 0.2615 | 0.3486 | 0.436 | 0.523 | 0.610 | 0.697 | 0.784 |
| 545 | 00879 | 0.1759 | 0.2639 | 0.3518 | 0.440 | 0.528 | 0.616 | 0.704 | 0.792 |
| 550 | 0.0888 | 0.1775 | 0.2663 | 0.3551 | 0.444 | 0.533 | 0.621 | 0.710 | 0.799 |
| 555 | 0.0896 | 0.1791 | 0.2687 | 0.3583 | 0.448 | 0.537 | 0.627 | 0.717 | 0.806 |
| 560 | 0.0904 | 0.1808 | 0.2712 | 0.3615 | 0.452 | 0.542 | 0.633 | 0.723 | 0.813 |
| 56.5 | 0.0912 | 0.1824 | 0.2736 | 0.3647 | 0.456 | 0.547 | 0.638 | 0.730 | 0.521 |
| 570 | 0.0920 | 0.1840 | 0.2760 | 0.3680 | 0.460 | 0.552 | 0.644 | 0.736 | 0.828 |
| 575 | 0.0928 | 0.1856 | 0.2784 | 0.3712 | 0.464 | 0.557 | 0.650 | 0.742 | 0.835 |
| 580 | 0.0936 | 0.1872 | 0.2808 | 0.3744 | 0.468 | 0.562 | 0.655 | 0.749 | 0.842 |
| 585 | 0.0944 | 0.1888 | 0.2833 | 0.3777 | 0.472 | 0.566 | 0.661 | 0.755 | 0.850 |
| 590 | 00952 | 0.1904 | 0.2557 | 0.3809 | 0.476 | 0.571 | 0.667 | 0.762 | 0.857 |
| 595 | 0.0960 | 0.1921 | 0.2881 | 0.3841 | 0.450 | 0.576 | 0.672 | 0.768 | 0.864 |
| 600 | 0.0968 | 0.1937 | 0.2905 | 0.387 t | 0.484 | 0.581 | 0.678 | 0.775 | 0.872 |
| 605 | 0.0976 | 0.1953 | 0.2929 | 0.3906 | 0.488 | 0.586 | 0.683 | 0.781 | 0.879 |
| 610 | 0.0985 | 0.1969 | 0.2954 | 0.3938 | 0.492 | 0.591 | 0.689 | 0.788 | 0.886 |
| 615 | 0.0993 | 0.198 .5 | 0.2978 | 0.3970 | 0.496 | 0.595 | 0.695 | 0.794 | 0.893 |
| 620 | 0.1001 | 0.2001 | 0.3002 | 0.4003 | 0.500 | 0.600 | 0.700 | 0.800 | 0.901 |
| 625 | 0.1009 | 0.2017 | 0.3026 | 0.4035 | 0.504 | 0.605 | 0.706 | 0.807 | 0.908 |
| 630 | 0.1017 | 0.2034 | 0.3050 | 0.4067 | 0.50 s | 0.610 | 0.712 | 0.813 | 0.915 |
| 635 | 0.1025 | 0.2050 | 0.3074 | 0.4099 | 0.512 | 0.615 | 0.717 | 0.820 | 0.922 |
| 640 | 0.1033 | 0.2066 | 0.3099 | 0.4132 | 0.516 | 0.620 | 0.723 | 0.826 | 0.930 |
| 645 | 0.1041 | 0.2082 | 0.3123 | 0.4164 | 0.520 | 0.625 | 0.729 | 0.833 | 0.937 |
| 650 | 0.1049 | 0.2098 | 0.3147 | 0.4196 | 0.524 | 0.629 | 0.734 | 0.839 | 0.944 |
| 655 | 0.1057 | 0.2114 | 0.3172 | 0.4229 | 0.529 | 0.634 | 0.740 | 0.846 | 0.951 |
| 660 | 0.1065 | 0.2130 | 0.3196 | 0.4261 | 0.533 | 0.639 | 0.746 | 0.852 | 0.959 |
|  | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4{ }^{\circ}$ | $5^{\circ}$ | 6 | $7{ }^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |


| Height of the Barome ter. | TEMPERATURE CENTIGRADE. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1{ }^{\circ}$ | $2^{\circ}$ | $3{ }^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9{ }^{\text {P }}$ |
| Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millien. |
| 665 | 0.1073 | 0.2146 | 0.3220 | 0.4293 | 0.537 | 0.644 | 0.751 | 0.859 | 0.966 |
| 670 | 0.1081 | 0.2163 | 0.3244 | 0.4326 | 0.541 | 0.649 | 0.757 | 0.565 | 0.973 |
| 675 | 0.1089 | 0.2179 | 0.3265 | 0.4358 | 0.545 | 0.654 | 0.763 | 0.871 | 0.950 |
| 650 | 0.1097 | 0.2195 | 0.3292 | 0.4390 | $\cdot 0.549$ | 0.658 | 0.768 | 0.878 | 0.958 |
| 685 | 0.1106 | 0.2211 | 0.3317 | 0.4423 | 0.553 | 0.663 | 0.774 | 0.884 | 0.995 |
| 690 | 0.1114 | 0.2227 | 0.3341 | 0.4455 | 0.557 | 0.668 | 0.780 | 0.591 | 1.002 |
| 695 | 0.1122 | 0.2233 | 0.336 .5 | 0.4487 | 0.561 | 0.673 | 0.785 | 0.897 | 1.010 |
| 700 | 0.1130 | 0.2260 | 0.3389 | 0.4520 | 0.565 | 0.678 | 0.791 | 0.904 | 1.017 |
| 705 | 0.1138 | 0.2276 | 0.3414 | 0.4552 | 0.569 | 0.683 | 0.797 | 0.910 | 1.024 |
| 710 | 0.1146 | 0.2292 | 0.3438 | 0.4584 | 0.573 | 0.688 | 0.502 | 0.917 | 1.031 |
| 715 | 0.1154 | 0.2308 | 0.3462 | 0.4616 | 0.577 | 0.691 | 0.808 | 0.923 | 1.039 |
| 720 | 0.1162 | 0.2324 | 0.3486 | 0.4648 | 0.581 | 0.697 | 0.813 | 0.930 | 1.046 |
| 725 | 0.1170 | 0.2340 | 0.3510 | 0.4650 | 0.585 | 0.702 | 0.819 | 0.936 | 1.053 |
| 730 | 0.1178 | 0.2356 | 0.3535 | 0.4713 | 0.589 | 0.707 | 0.825 | 0.943 | 1.060 |
| 735 | 0.1186 | 0.2372 | 0.3559 | 0.4745 | 0.593 | 0.712 | 0.830 | 0.949 | 1.065 |
| 740 | 0.1104 | 0.2389 | 0.3583 | 0.4777 | 0.597 | 0.717 | 0.836 | 0.955 | 1.075 |
| 745 | 0.1202 | 0.2405 | 0.3607 | 0.4509 | 0.601 | 0.721 | 0.542 | 0.962 | 1.082 |
| 750 | 0.1210 | 0.2421 | 0.3631 | 0.4842 | 0.605 | 0.726 | 0.847 | 0.968 | 1.089 |
| 75.5 | 0.1218 | 0.2437 | 0.3655 | 0.4874 | 0.609 | 0.731 | 0.853 | 0.975 | 1.097 |
| 760 | 0.1227 | 0.2453 | 0.3680 | 0.4906 | 0.613 | 0.736 | 0.859 | 0.981 | 1.104 |
| 765 | 0.1235 | 0.2469 | 0.3704 | 0.4939 | 0.617 | 0.741 | 0.864 | 0.988 | 1.111 |
| 770 | 0.1243 | 0.2456 | 0.3729 | 0.4971 | 0.621 | 0.746 | 0.870 | 0.994 | 1.118 |
| 775 | 0.1251 | 0.2502 | 0.3752 | 0.5003 | 0.625 | 0.750 | 0.876 | 1.001 | 1.126 |
| 750 | 0.1259 | 0.2518 | 0.3777 | 0.5036 | 0.629 | 0.755 | 0.581 | 1.007 | 1.133 |
| 785 | 0.1267 | 0.2534 | 0.3801 | 0.5068 | 0.633 | 0.760 | 0.888 | 1.014 | 1.140 |
| 790 | 0.1275 | 0.2550 | 0.3825 | 0.5100 | 0.637 | 0.765 | 0.893 | 1.020 | 1.148 |
| 795 | 0.1283 | 0.2566 | 0.3849 | 0.5132 | 0.641 | 0.770 | 0.898 | 1.026 | 1.155 |
| 800 | 0.1291 | 0.2582 | 0.3574 | 0.516 .5 | 0.646 | 0.775 | 0.904 | 1.033 | 1.162 |
| 805 | 0.1299 | 0.2598 | 0.3898 | 0.5197 | 0.650 | 0.780 | 0.909 | 1.039 | 1.169 |
| 810 | 0.1307 | 0.2615 | 0.3922 | 0.5230 | 0.654 | 0.784 | 0.915 | 1.046 | 1.177 |
| 815 | 0.1315 | 0.2621 | 0.3946 | 0.5262 | 0.658 | 0.789 | 0.921 | 1.052 | 1.184 |
| 820 | 0.1323 | 0.2647 | 0.3970 | 0.5294 | 0662 | 0.794 | 0.926 | 1.059 | 1.191 |
| 825 | 0.1331 | 0.2653 | 0.3994 | 0.3326 | 0.666 | 0.799 | 0.932 | 1.065 | 1.198 |
| 830 | 0.1340 | 0.2679 | 0.4019 | 0.5358 | 0.670 | 0.804 | 0.938 | 1.072 | 1.206 |
| 835 | 0.1348 | $0 . £ 695$ | 0.4043 | 0.5391 | 0.674 | 0.509 | 0.943 | 1.078 | 1.213 |
| 840 | 0.13 .56 | 0.2712 | 0.4067 | 0.5423 | 0.678 | 0.513 | 0.949 | 1.085 | 1.220 |
| 845 | 0.1364 | 0.2729 | 0.4091 | 0.545 .5 | 0.682 | 0.518 | 0.955 | 1.091 | 1.227 |
| 850 | 0.1372 | 0.2744 | 0.4116 | 0.5488 | 0.686 | 0.823 | 0.960 | 1.097 | 1.235 |
| 855 | 0.1350 | 0.2760 | 0.4140 | 0.5520 | 0.690 | 0.828 | 0.966 | 1.101 | 1.242 |
| 860 | 0.1358 | 0.2776 | 0.4164 | 0.5552 | 0.694 | 0.833 | 0.972 | 1.110 | 1.249 |
| 86.5 | 0.1396 | 0.2792 | 0.4198 | 0.5584 | 0.698 | 0.838 | 0.977 | 1.117 | 1.256 |
|  | $1{ }^{\circ}$ | $\mathbf{2}^{\circ}$ | $3{ }^{\circ}$ | $4{ }^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |

## XX .

## METRICAL BAROMETER.

## T A BLE

FOR
REDUCING T0 THE FREEZING POINT THE BAROMETRICAL
COLUMN,
i!SURED BY BRASS SCALES, EXTENDING FROM THE CISTERN TO THE TOP; CAC. CUlated for the heights between 605 and 800 millimetres, and for every tenth of a degree, from $0^{\circ}$ to $\dagger$ and - $35^{\circ}$ centigrade.

By M. T. Haeghens.

## TABLEXX.

'Inis table has been calculated by using the same coefficients of dilatation as in the preceding table, viz.: -

Brass, linear dilatation, from Laplace ard Lavoisier for $100^{\circ} \mathrm{C}=0.0018782$.
Mercury, dilatation in volume, from Dulong and Petit for $100^{\circ} \mathrm{C}=0.0180180$.
Dilatation of the mercurial column for $100^{\circ} \mathrm{C}$. . . $=0.0161398$.
Dilatation of the mercurial column for $1^{\circ} \mathrm{C}$. . . . $=0.0001614$.
This table, calculated for the reduction of long series of meteorological observations, gives immediately the value of the correction for each tenth of a degree up to $35^{\circ} \mathrm{C}$. above, and down to $35^{\circ} \mathrm{C}$. below, the freezing point, and for mercurial columns extending from 605 to 800 millimetres.

## Examples of Calculation.

Barometer, observed height, . . . . . $\quad 754.17$
Temperature of the attached thermometer, $+17^{\circ} .8$.

For finding the correction, seek in the horizontal column, headed barometer, at the head of the pages, the corresponding height of the barometer; it will be found, p. 31,
 containing the temperatures, $17^{\circ}$, follow then horizontally this line as far as the column of 8 tenths, and you find there 2.17 millimetres, which is the correction, or the quantity to be subtracted for reducing the observed height to zero. We have thus: -


If the temperature is below zero, the correction will be additive.

| Observed height, |  | $7 \times 972$ |
| :---: | :---: | :---: |
| Temperature of the attached thermometer, - $8^{\circ} .4$. |  |  |
| Additive correction. | . . . | +0.99 |
|  | Barometer at zero, | 730.71 |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $605^{\mathrm{mm} .}$ (from 602.51 to 607.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\stackrel{\circ}{\circ}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 .4 \end{gathered}$ | $\begin{array}{\|c} \text { Millim. } \\ 0.05 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Nillim. } \\ 0.09 \end{gathered}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.21 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 |
| 3 | 0.29 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 |
| 4 | 0.39 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 |
| 5 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 |
| 6 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 |
| 7 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 |
| 8 | 0.78 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 |
| 9 | 0.88 | 0.89 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 |
| 10 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.05 | 1.06 |
| 11 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 |
| 12 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 |
| 13 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 |
| 14 | 1.37 | 1.38 | 1.39 | 1.40 | 1.11 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 |
| 15 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 |
| 16 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 |
| 17 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 |
| 18 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 |
| 19 | 1.86 | 1.87 | 1.87 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 |
| 20 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 |
| 21 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 |
| 22 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 |
| 23 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 |
| 24 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 |
| 25 | 2.44 | 2.45 | 2.46 | 2.47 | 2.18 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 |
| 26 | 2.54 | 2.5 .5 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 |
| 27 | 2.64 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 | 2.71 | 2.72 |
| 28 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 |
| 29 | 2.83 | 2.84 | 2.85 | 2.86 | 2.87 | 2.58 | 2.89 | 2.90 | 2.91 | 2.92 |
| 30 | 2.93 | 2.91 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 |
| 31 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 |
| 32 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 |
| 33 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 |
| 34 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 |
| 35 | 3.42 | 3.13 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.51 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $610^{\mathrm{mm} .}$ (from 607.51 to 619.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\stackrel{0}{0}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millım. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Mıllin. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millım. } \\ 0.09 \end{gathered}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
| 3 | 0.30 | 0.31 | 0.32 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 |
| 4 | $0.39{ }^{\circ}$ | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 |
| 5 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 |
| 6 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 |
| 7 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 |
| 8 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 |
| 9 | 0.59 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.96 | 0.97 |
| 10 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 |
| 11 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 |
| 12 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 |
| 13 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 |
| 14 | 1.38 | 1.39 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 |
| 15 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 |
| 16 | 1.58 | 1.59 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 |
| 17 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 |
| 18 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 |
| 19 | 1.87 | 1.88 | 1.59 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 . | 1.95 | 1.96 |
| 20 | 1.97 | 1.93 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 |
| 21 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 |
| 22 | 2.17 | 2.15 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.23 | 2.24 | 2.25 |
| 23 | 2.26 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 |
| 24 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 | 2.44 | 2.45 |
| 25 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 |
| 26 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 |
| 27 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 |
| 28 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.53 | 2.54 | 2.85 |
| 29 | 2.86 | 2.86 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.91 |
| 30 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 |
| 31 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 |
| 32 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 |
| 33 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 |
| 34 | 3.35 | 3.36 | 3.37 | 3.33 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 |
| 35 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 | 3.5: | 3.54 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Cen'i- } \\ \text { grade } \\ \text { g: } 5 \times 38 \end{gathered}$ | BAROMETER : $615{ }^{\text {mm. }}$ (from 612.51 to 617.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | D. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\stackrel{u}{0}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{aligned} & \text { Millem } \\ & 0 . \mathrm{cl} \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millım. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.21 | 0.32 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
| 3 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
| 4 | 0.40 | 0.41 | 0.42 | 0.13 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 |
| 5 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 |
| 6 | 0.69 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.68 |
| 7 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 |
| 8 | 0.79 | 0.50 | 0.81 | 0.52 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 |
| 9 | 0.59 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 |
| 10 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 |
| 11 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 |
| 12 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 |
| 13 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 |
| 14 | 1.39 | 1.10 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 |
| 15 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 |
| 16 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 |
| 17 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 |
| 18 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 |
| 19 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 |
| 20 | 1.99 | 2.00 | 2.01 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 |
| 21 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 |
| 22 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 |
| 23 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 |
| 24 | 2.38 | 2.39 | 2.40 | 2.41 | 2.12 | 2.43 | 2.44 | 2.45 | 2.46 | 2.47 |
| 25 | 2.48 | 2.19 | 2.50 | \%.51 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 |
| 26 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 |
| 27 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 |
| 28 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.85 | 2.86 | 2.87 |
| 29 | 2.58 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 |
| 30 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 |
| 31 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 |
| 32 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 |
| 33 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.36 |
| $3 \cdot 1$ | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.46 |
| 35 | 3.47 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 |
|  | O. | 1. | $\stackrel{2}{ }$ | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigrade Degrees. | BAROMETER : $620^{\mathrm{mm} .}$ (from 617.51 to 622.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | *. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | Millim. 0.01 | Millim. 0.02 | Milinn. 0.03 | Millım. 0.0 .4 | Millim. 0.05 | Millim. 0.06 | Millim. 0.07 | $\begin{gathered} \text { Millim } \\ \hline 0.0 \mathrm{~s} \end{gathered}$ | Millim. 0.09 |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
| 3 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
| 4 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 |
| 5 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 |
| 6 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 |
| 7 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 |
| 8 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 |
| 9 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 |
| 10 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 |
| 11 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 |
| 12 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 |
| 13 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 |
| 14 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.17 | 1.48 | 1.49 |
| 15 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 |
| 16 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 |
| 17 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 |
| 18 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 | 1.89 |
| 19 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 |
| 20 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 |
| 21 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 |
| 22 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 |
| 23 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 |
| 24 | 2.40 | 2.41 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 |
| 25 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 |
| 26 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.65 | 2.69 |
| 27 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 |
| 28 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.85 | 2.86 | 2.87 | 2.88 | 2.89 |
| 29 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 |
| 30 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 |
| 31 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 |
| 32 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 |
| 33 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 |
| 34 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.16 | 3.47 | 3.48 | 3.49 |
| 35 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigrade Degrees. | BAROMETER : $625^{\text {mm. }}$ (from 622.51 to 627.50), |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | \$. | 9. |
| $\bigcirc$ | Millim. 0.00 | Millim. 0.01 | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | Millim. 0.03 | Millim. | $\begin{aligned} & \text { Millim. } \\ & 0.05 . \end{aligned}$ | Millim. 0.06 | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
| 3 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 |
| 4 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 |
| 5 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.60 |
| 6 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 |
| 7 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 |
| 8 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.90 |
| 9 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 |
| 10 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 |
| 11 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 |
| 12 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 |
| 13 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 |
| 14 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 |
| 15 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 |
| 16 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 |
| 17 | 1.71 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 |
| 18 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 | 1.89 | 1.90 | 1.91 |
| 19 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 . | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 |
| 20 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 | 2.05 | 2.09 | 2.10 | 2.11 |
| 21 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 |
| 22 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 |
| 23 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 |
| 24 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 |
| 25 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 |
| 26 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 |
| 27 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 |
| 28 | 2.82 | 2.83 | 2.84 | 2.85 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 |
| 29 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 |
| 30 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 |
| 31 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 |
| 32 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 |
| 33 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.12 |
| 34 | 3.43 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 |
| 35 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.61 | 3.62 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigrade Ilegrees. | BAROMETER : $630^{\mathrm{mm}}$. (from 627.51 to 632.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\bigcirc$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{array}{\|c} \text { Millim. } \\ 0.05 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | Millim. 0.07 | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 |
| 3 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 |
| 4 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 |
| 5 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 |
| 6 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 |
| 7 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 |
| 8 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.90 |
| 9 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 |
| 10 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 |
| 11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 |
| 12 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 |
| 13 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.41 |
| 14 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.52 |
| 15 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 |
| 16 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 |
| 17 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 |
| 18 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 |
| 19 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 |
| 20 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.13 |
| 21 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 |
| 22 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 |
| 23 | 2.34 | 2.35 | 236 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 |
| 24 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 |
| 25 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 |
| 26 | 2.64 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 | 2.73 | 2.74 |
| 27 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 |
| 28 | 2.85 | 2.86 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 |
| 29 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 |
| 30 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 |
| 31 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 |
| 32 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.34 | 3.35 |
| 33 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 |
| 34 | 3.46 | 3.47 | 3.18 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 |
| 35 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

C

| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROME'TER : $635{ }^{\text {mm. }}$ ( from 632.5l to 637.50). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\circ$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.01 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.04 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millum. } \\ 0.09 \end{gathered}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 |
| 2 | 0.20 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 |
| 3 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 |
| 4 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 |
| 5 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 |
| 6 | 0.61 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 |
| 7 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 |
| 8 | 0.52 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.90 | 0.91 |
| 9 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 |
| 10 | 1.02 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 |
| 11 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 |
| 12 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 |
| 13 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.41 | 1.42 |
| 14 | 1.43 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 |
| 15 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 |
| 16 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 |
| 17 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 | 1.50 | 1.81 | 1.82 | 1.83 |
| 18 | 1.54 | 1.86 | 1.87 | 1.85 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 |
| 19 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 |
| 20 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 |
| 21 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 |
| 22 | 2.25 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 |
| 23 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 | 2.44 | 2.45 |
| 24 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 |
| 25 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 |
| 26 | 2.66 | 2.67 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 |
| 27 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.85 | 2.86 |
| 28 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 |
| 29 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 |
| 30 | 3.07 | 3.08 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 |
| 31 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 |
| 32 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 |
| 83 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 | 3.13 | 3.44 | 3.45 | 3.46 | 3.47 |
| 34 | 3.48 | 3.49 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 |
| 35 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 |
|  | (1. | 1. | 2. | 3. | 4. | 5. | 6. | 7 \% | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROME'TER : $640^{\mathrm{mm} .}$ (from 637.51 to 642.50 ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7 | - | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millım. } \\ 0.03 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.04 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~S} \end{gathered}$ | $\begin{aligned} & \text { Millım. } \\ & 0.09 \end{aligned}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.17 | 0.18 | 0.19 | 0.20 |
| 2 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.23 | 0.29 | 0.30 |
| 3 | 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.35 | 0.39 | 0.40 |
| 4 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.50 | 0.51 |
| 5 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 |
| 6 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 |
| 7 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.80 | 0.81 | 0.82 |
| 8 | 0.53 | 0.8.4 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.90 | 0.91 | 0.92 |
| 9 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 |
| 10 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.11 | 1.12 | 1.13 |
| 11 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 |
| 12 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 |
| 13 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.42 | 1.43 | 1.44 |
| 14 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 |
| 15 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 |
| 16 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.74 | 1.75 |
| 17 | 1.76 | 1.77 | 1.78 | 1.79 | 1.50 | 1.81 | 1.82 | 1.53 | 1.84 | 1.85 |
| 18 | 1.86 | 1.57 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 |
| 19 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.05 | 2.06 |
| 20 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 |
| 21 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 |
| 22 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.36 | 2.37 |
| 23 | 2.38 | 2.39 | 2.40 | 2.41 | 2.12 | 2.43 | 2.44 | 2.45 | 2.16 | 2.47 |
| 24 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 |
| 25 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.68 |
| 26 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 |
| 27 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.55 | 2.86 | 2.87 | 2.85 |
| 28 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.99 |
| 29 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 |
| 30 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 |
| 31 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.30 |
| 32 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 |
| 33 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.46 | 3.47 | 3.45 | 3.49 | 3.50 |
| 34 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.53 | 3.59 | 3.60 |
| 35 | 3.62 | 3.63 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 | 3.70 | 3.71 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { crate } \\ \text { geryres. } \end{gathered}$ | BAROMETER : $645{ }^{\text {mm. }}$ (from 642.51 to 647.50 ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | o. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | $s$. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim } \\ 0.00 \end{gathered}$ | $\begin{gathered} \hline \text { Mullim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Milum. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Mıllım. } \\ 0.04 \end{gathered}$ | $\begin{array}{\|c} \hline \begin{array}{c} \text { Milim. } \\ 0.05 \end{array} \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millin. } \\ 0.08 \end{gathered}$ | $\begin{aligned} & \text { Millım. } \\ & 0.09 \end{aligned}$ |
| 1 | 0.10 | 0.11 | 0.12 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 |
| 2 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.25 | 0.29 | 0.30 |
| 3 | 0.31 | 0.32 | 0.33 | 0.34 | 0.3.5 | 0.36 | 0.37 | 0.39 | 0.40 | 0.41 |
| 4 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 |
| 5 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 |
| 6 | 0.62 | 0.64 | 0.65 | 0.66 | 0.67 | 0.63 | 0.69 | 0.70 | 0.71 | 0.72 |
| 7 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 | 0.82 |
| 8 | 0.53 | 0.54 | 0.55 | 0.86 | 0.87 | 0.88 | 0.90 | 0.91 | 0.92 | 0.93 |
| 9 | 0.94 | 0.9.5 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 |
| 10 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 |
| 11 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 |
| 12 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 |
| 13 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 |
| 14 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 |
| 15 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.66 |
| 16 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 |
| 17 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 |
| 18 | 1.87 | 1.88 | 1.59 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 |
| 19 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 |
| 20 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.17 | 2.18 |
| 21 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 |
| 22 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.31 | 2.35 | 2.36 | 2.37 | 2.38 |
| 23 | 2.39 | 2.40 | 2.42 | 2.43 | 2.44 | 2.4. | 2.46 | 2.47 | 2.48 | 2.49 |
| 24 | 2.50 | 2.51 | 2.92 | 2.53 | 2.54 | 2.95 | 2.56 | 2.57 | 2.58 | 2.59 |
| 25 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.69 | 2.70 |
| 26 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 |
| 27 | 2.01 | 2.82 | 2.83 | 2.81 | 2.85 | 2.86 | 2.87 | 2.88 | 2.59 | 2.90 |
| 29 | 2.9, | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 |
| 29 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 |
| 30 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 |
| 31 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 |
| 32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 |
| 33 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 |
| 34 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 |
| 35 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 | 3.73 |
|  | o. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |



| $\begin{gathered} \text { Centi. } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $655^{\mathrm{mm} .}$ (from 652.51 to 657.50). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millım. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 |
| 2 | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 |
| 3 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.33 | 0.39 | 0.40 | 0.41 |
| 4 | 0.42 | 0.43 | 0.44 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 |
| 5 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 |
| 6 | 0.63 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 |
| 7 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 | 0.83 | 0.84 |
| S | 0.85 | 0.86 | 0.57 | 0.88 | 0.89 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 |
| 9 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.02 | 1.03 | 1.04 | 1.05 |
| 10 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 |
| 11 | 1.16 | 1.17 | 1.18 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 |
| 12 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 |
| 13 | 1.37 | 1.39 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 |
| 14 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.54 | 1.55 | 1.57 | 1.58 |
| 15 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 |
| 16 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.76 | 1.77 | 1.78 | 1.79 |
| 17 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 | 1.89 |
| 18 | 1.90 | 1.91 | 1.92 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 |
| 19 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 |
| 20 | 2.11 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 |
| 21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.31 | 2.32 |
| 22 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 | $2.4 '$ | 2.41 | 2.42 |
| 23 | 2.43 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.50 | 2.51 | 2.52 | 2.53 |
| 24 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 |
| 25 | 2.64 | 2.65 | 2.66 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 |
| 26 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 |
| 27 | 2.85 | 2.87 | 2.58 | 2.59 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 |
| 28 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.05 | 3.06 |
| 29 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 |
| 30 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.24 | 3.25 | 3.26 | 3.27 |
| 31 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 |
| 32 | 3.35 | 3.39 | 3.40 | 3.42 | 3.43 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 |
| 33 | 3.49 | 3.50 | 3.51 | 3.52 | 3.583 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 |
| 34 | 3.59 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 |
| 35 | 3.70 | 3.71 | 3.72 | 3.73 | 3.74 | 3.75 | 3.76 | 3.77 | 3.79 | 3.80 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centi grade Jegrees. | BAROMETER : $660^{\mathrm{mm} .}$ (from 657.51 to 662.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 0 | Millim. 0.00 | Millim. 0.01 | Millim. 0.02 | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.08 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 |
| 2 | 0.21 | 0.22 | 0.23 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 |
| 3 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.41 | 0.42 |
| 4 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 |
| 5 | 0.53 | 0.54 | 0.55 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 |
| 6 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.74 |
| 7 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 |
| 8 | 0.85 | 0.86 | 0.87 | 0.88 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 |
| 9 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.06 |
| 10 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 |
| 11 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 |
| 12 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 |
| 13 | 1.39 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 |
| 14 | 1.49 | 1.50 | 1.51 | 1.52 | 1.53 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 |
| 15 | 1.60 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 |
| 16 | 1.70 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 |
| 17 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.88 | 1.89 | 1.90 | 1.91 |
| 18 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 |
| 19 | 2.02 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 |
| 20 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.21 | 2.22 | 2.23 |
| 21 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 |
| 22 | 2.34 | 2.35 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.12 | 2.43 | 2.44 |
| 23 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.53 | 2.54 | 2.55 |
| 24 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 |
| 25 | 2.66 | 2.67 | 2.68 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 |
| 26 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.86 | 2.87 |
| 27 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 |
| 28 | 2.98 | 2.99 | 3.00 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 |
| 29 | 3.09 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 319 |
| 30 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 |
| 31 | 3.30 | 3.31 | 3.32 | 3.33 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 |
| 32 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.51 |
| 33 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.61 |
| 34 | 3.62 | 3.63 | 3.64 | 3.65 | 3.66 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 |
| 35 | 3.73 | 3.74 | 3.75 | 3.76 | 3.77 | 3.75 | 3.79 | 3.80 | 3.81 | 3.82 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{aligned} & \text { Centi- } \\ & \text { grade } \\ & \text { Degrees. } \end{aligned}$ | BAROMETER : $665{ }^{\mathrm{mm}}$. (from 662.51 to 667.50 ), |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\stackrel{\bigcirc}{0}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.05 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { M1llim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 011 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 |
| 2 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 |
| 3 | 0.32 | 0.33 | 0.34 | 0.35 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 |
| 4 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 |
| 5 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 |
| 6 | 0.64 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 |
| 7 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 |
| 8 | 0.86 | 0.57 | 0.88 | 0.89 | 0.90 | 0.91 | 0.92 | 0.93 | 0.95 | 0.96 |
| 9 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 |
| 10 | 1.07 | 1.08 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 |
| 11 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.25 | 1.26 | 1.27 | 1.28 |
| 12 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.39 |
| 13 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 |
| 14 | 1.50 | 1.51 | 1.52 | 1.51 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 |
| 15 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.69 | 1.70 | 1.71 |
| 16 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 |
| 17 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 |
| 18 | 1.93 | 1.94 | 1.95 | 1.96 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 |
| 19 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.13 | 2.14 |
| 20 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 |
| 21 | 2.25 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 |
| 22 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 |
| 23 | 2.17 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.56 | 2.57 |
| 24 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 |
| 25 | 2.68 | 2.69 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 |
| 26 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.86 | 2.87 | 2.88 | 2.89 |
| 27 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 3.00 |
| 28 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 |
| 29 | 3.11 | 3.12 | 3.13 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 5.21 |
| 30 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.30 | 3.31 | 3.32 |
| 31 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 |
| 32 | 3.44 | 345 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 |
| 33 | 3.54 | 3.55 | 3.56 | 3.57 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 |
| 34 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 | 3.74 | 3.7\% |
| 35 | 3.76 | 3.77 | 3.78 | 3.79 | 3.85 | 3.81 | 3.82 | 3.83 | 3.84 | 3.85 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centi- grade <br> Degrees. | BAROMETER • $670^{\mathrm{mm} .}$ (from 667.51 to 67250. ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.05 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.20 | 0.21 |
| 2 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 |
| 3 | 0.32 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 |
| 4 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 |
| 5 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 |
| 6 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.73 | 0.74 | 0.75 |
| 7 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 |
| 8 | 0.87 | 0.58 | 0.59 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 |
| 9 | 0.97 | 0.98 | 1.00 | 1.01 | 1.02 | 1.03 | 104 | 1.05 | 1.06 | 1.07 |
| 10 | 1.08 | 1.09 | 1.10 | 1.11 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 |
| 11 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.27 | 1.28 | 1.29 |
| 12 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.40 |
| 13 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 |
| 14 | 1.51 | 1.53 | 1.54 | 1.53 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 |
| 15) | 1.62 | 1.63 | 1.64 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 |
| 16 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 | 1.80 | 1.81 | 1.82 | 1.83 |
| 17 | 1.84 | 1.85 | 1.86 | 1.57 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 | 1.94 |
| 18 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 |
| 19 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 |
| 20 | 2.16 | 2.17 | 2.18 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 |
| 21 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 |
| 22 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 | 2.44 | 2.46 | 2.47 | 2.48 |
| 23 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 | 2.59 |
| 24 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 |
| 25 | 2.70 | 2.71 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.50 |
| 26 | 2.81 | 2.82 | 2.83 | 2.84 | 2.56 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 |
| 27 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.99 | 3.00 | 3.01 | 3.02 |
| 28 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.13 |
| 29 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 |
| 30 | 3.24 | 3.26 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 |
| 31 | 3.35 | 3.36 | 3.37 | 3.39 | 3.40 | 3.41 | 3.42 | $3 \cdot 43$ | 3.44 | 3.45 |
| 32 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 |
| 33 | 3.57 | 3.58 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.66 | 3.67 |
| 34 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 | 3.73 | 3.74 | 3.75 | 3.76 | 377 |
| 35 | 3.79 | 3.50 | 3.81 | 3.82 | 3.83 | 3.84 | 385 | 3.86 | 3.87 | 3.58 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


|  | BAROME'TER : $675^{\mathrm{mm}}$ ( from 679.51 to 677.50). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | Millim. 0.03 | Millim. 0.04 | Millim. 0.05 | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~S} \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | Millim. $0.10$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.19 | 0.20 | 0.21 |
| 2 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 |
| 3 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 |
| 4 | 0.44 | 0.45 | 0.46 | 0.17 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 |
| 5 | 0.54 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 |
| 6 | 0.65 | 0.66 | 0.63 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 |
| 7 | 0.76 | 0.77 | 0.78 | 0.80 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.56 |
| 8 | 0.57 | 0.58 | 0.89 | 0.90 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 |
| 9 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.05 | 1.06 | 1.07 | 1.08 |
| 10 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.17 | 1.18 | 1.19 |
| 11 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.29 | 1.30 |
| 12 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.41 |
| 13 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 |
| 14 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 |
| 15 | 1.63 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 |
| 16 | 1.74 | 1.75 | 1.76 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 |
| 17 | 1.85 | 1.86 | 1.87 | 1.88 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 |
| 18 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 |
| 19 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.14 | 2.15 | 2.16 | 2.17 |
| 20 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.26 | 2.27 | 2.28 |
| 21 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 | 2.38 | 2.39 |
| 22 | 2.40 | 2.41 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 |
| 23 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 |
| 24 | 2.61 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 |
| 25 | 2.72 | 2.73 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 |
| 26 | 2.93 | 2.84 | 2.85 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 |
| 27 | 2.94 | 2.95 | 2.96 | 2.97 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 |
| 28 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.12 | 3.13 | $3 \cdot 14$ | 3.15 |
| 29 | 3.16 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 | 3.22 | 3.24 | 3.25 | 3.26 |
| 30 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.36 | 3.37 |
| 31 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.46 | 3.48 |
| 32 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 |
| - 33 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 |
| 34 | 3.70 | 3.72 | 3.73 | 3.74 | 3.75 | 3.76 | 3.77 | 3.78 | 3.79 | 3.50 |
| 35 | 3.51 | 3.82 | 3.83 | 3.85 | 3.86 | 3.87 | 3.88 | 3.89 | 3.90 | 3.91 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | D. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $680{ }^{\text {mm. }}$ ( from 677.51 to 682.50 ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\bigcirc$ | Millim | Millim. | Millim. | Millim. | Millim | Millim. | Millim. | Millim. | Millim. | Millim. |
| 0 | 0.00 | 0.01 | 0.02 | 0.03 | 0.01 | 0.05 | 0.07 | 0.08 | 0.09 | 0.10 |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.21 |
| 2 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.29 | 0.30 | 0.31 | 0.32 |
| 3 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.43 |
| 4 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.52 | 0.53 | 0.54 |
| 5 | 9.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.63 | 0.64 | 0.65 |
| 6 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.74 | 0.75 | 0.76 |
| 7 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.85 | 0.86 | 0.87 |
| 8 | 0.88 | 0.89 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.97 | 0.98 |
| 9 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.08 | 1.09 |
| 10 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.19 | 1.20 |
| 11 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.30 | 1.31 |
| 12 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.42 |
| 13 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.53 |
| 14 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.64 |
| 15 | 1.65 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.75 |
| 16 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 |
| 17 | 1.87 | 1:88 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 |
| 18 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 |
| 19 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 |
| 20 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 |
| 21 | 2.30 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 |
| 22 | 2.41 | 2.43 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 |
| 23 | 2.52 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 |
| 24 | 2.63 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 |
| 25 | 2.74 | 2.75 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 |
| 26 | 2.85 | 2.86 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 |
| 27 | 2.96 | 2.97 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 |
| 28 | 3.07 | 3.08 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 |
| 29 | 3.18 | 3.19 | 3.20 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 |
| 30 | 3.29 | 3.30 | 3.31 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 |
| 31 | 3.40 | 3.41 | 3.42 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 |
| 32 | 3.51 | 3.52 | 3.53 | 3.54 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.61 |
| 33 | 3.62 | 3.63 | 3.64 | 3.65 | 3.67 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 |
| 34 | 3.73 | 3.74 | 3.75 | 3.76 | 3.78 | 3.79 | 3.80 | 3.81 | 3.82 | 3.83 |
| 35 | 3.84 | 3.85 | 3.86 | 3.87 | 3.89 | 3.90 | 3.91 | 3.92 | 3.93 | 3.94 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7 。 | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROME'TER : $685{ }^{\text {mm. }}$ (from 682.51 to 687.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7 \% | 8. | 9. |
| $\bigcirc$ | Millim. | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{array}{\|c} \text { Millim } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Mıllim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.17 | 0.18 | 0.19 | 0.20 | 0.21 |
| 2 | 0.22 | 0.23 | 0.24 | 0.25 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
| 3 | 0.33 | 0.34 | 0.35 | 0.36 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.43 |
| 4 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 |
| 5 | 0.55 | 0.56 | 0.57 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 |
| 6 | 0.66 | 0.67 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 |
| 7 | 0.77 | 0.78 | 0.80 | 0.81 | 0.82 | 0.53 | 0.84 | 0.85 | 0.86 | 0.87 |
| 8 | 0.88 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 |
| 9 | 1.00 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 |
| 10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.21 |
| 11 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.32 |
| 12 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.42 | 1.43 |
| 13 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.53 | 1.54 |
| 14 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.63 | 1.64 | 1.65 |
| 15 | 1.66 | 1.67 | 1.68 | 1.69 | 1.70 | 1.71 | 1.72 | 1.74 | 1.75 | 1.76 |
| 16 | 1.77 | 1.78 | 1.79 | 1.50 | 1.81 | 1.82 | 1.84 | 1.55 | 1.86 | 1.87 |
| 17 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.95 | 1.96 | 1.97 | 1.98 |
| 18 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 |
| 19 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 |
| 20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.26 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 |
| 21 | 2.32 | 2.33 | 2.34 | 2.35 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 |
| 22 | 2.43 | 2.44 | 2.45 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 |
| 23 | 2.54 | 2.55 | 2.56 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 |
| 24 | 2.65 | 2.66 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 |
| 25 | 2.76 | 2.78 | 2.79 | 2.50 | 2.81 | 2.82 | 2.83 | 2.84 | 2.55 | 2.86 |
| 26 | 2.57 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 |
| 27 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 |
| 28 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.20 |
| 29 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 5.31 |
| 30 | 3.32 | 3.33 | 3.34 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.41 | 3.42 |
| 31 | 3.43 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.52 | 3.53 |
| 32 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.62 | 3.63 | 3.64 |
| 33 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 | 3.70 | 3.71 | 3.73 | 3.74 | 3.75 |
| 34 | 3.76 | 3.77 | 3.78 | 3.79 | 3.80 | 3.81 | 3.83 | 3.84 | 3.8.5 | 3.86 |
| 35 | 3.87 | 3.58 | 3.59 | 3.90 | 3.91 | 3.92 | 3.94 | 3.95 | 3.96 | 3.97 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi. } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $690^{\mathrm{mm}}$. (from 687.51 to 69250 ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.04 \end{aligned}$ | $\begin{array}{\|c} \text { Millin. } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | Millim. $0.09$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.14 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.21 |
| 2 | 0.22 | 0.23 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 |
| 3 | 0.33 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.43 |
| 4 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.55 |
| 5 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.65 | 0.66 |
| 6 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.74 | 0.75 | 0.76 | 0.77 |
| 7 | 0.78 | 0.79 | 0.85 | 0.81 | 0.82 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 |
| 8 | 0.59 | 0.90 | 0.91 | 0.92 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 |
| 9 | 1.00 | 1.01 | 1.02 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 |
| 10 | 1.11 | 1.12 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 |
| 11 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.20 | 1.31 | 1.33 |
| 12 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.41 | 1.43 | 1.44 |
| 13 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.53 | 1.54 | 1.55 |
| 14 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.63 | 1.64 | 1.65 | 1.66 |
| 15 | 1.67 | 1.68 | 1.69 | 1.70 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 |
| 16 | 1.78 | 1.79 | 1.80 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 |
| 17 | 1.89 | 1.90 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 |
| 18 | 2.00 | 2.02 | 2.03 | 2.0 .1 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 |
| 19 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.21 | 2.22 |
| 20 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.31 | 2.32 | 2.33 |
| 21 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 | 2.41 | 2.42 | 2.43 | 2.44 |
| 22 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 | 2.51 | 2.52 | 2.53 | 2.54 | 2.55 |
| 23 | 2.56 | 2.57 | 2.58 | 2.59 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 |
| 24 | 2.67 | 2.68 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 |
| 25 | 2.78 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.85 | 2.86 | 2.87 | 2.58 |
| 26 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 3.00 |
| 27 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.10 | 3.11 |
| 28 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 | 3.21 | 3.22 |
| 29 | 2.23 | 3.24 | 3.25 | 3.26 | 3.27 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 |
| 30 | 3.34 | 3.35 | 3.36 | 3.37 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 |
| 31 | 3.45 | 3.46 | 3.47 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 |
| 32 | 3.56 | 3.57 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 | 3.66 |
| 33 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 | 3.73 | 3.74 | 3.75 | 3.76 | 3.78 |
| 3.4 | 3.79 | 3.80 | 3.81 | 3.82 | 3.83 | 3.84 | 3.85 | 3.86 | 3.88 | 3.89 |
| 35 | 3.90 | 3.91 | 3.92 | 3.93 | 3.94 | 3.95 | 3.96 | 3.98 | 3.99 | 4.00 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigrate Degrees. | BAROME'TER : $695{ }^{\text {mm. }}$ (from 692.51 to 697.50) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{array}{\|c} \hline \text { Millim. } \\ 0.00 \\ \hline \end{array}$ | $\begin{gathered} \text { Nillim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.03 \end{aligned}$ | $\begin{gathered} \text { Millim } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.13 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.21 |
| 2 | 0.22 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 |
| 3 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 |
| 4 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.52 | 0.53 | 0.54 | 0.55 |
| 5 | 0.56 | 0.57 | 0.58 | 0.59 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 |
| 6 | 0.67 | 0.68 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 |
| 7 | 0.79 | 0.80 | 0.81 | 0.52 | 0.83 | 0.54 | 0.85 | 0.86 | 0.87 | 0.89 |
| 8 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.98 | 0.99 | 1.00 |
| 9 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 |
| 10 | 1.12 | 1.13 | 1.14 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 |
| 11 | 1.23 | 1.25 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 |
| 12 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.41 | 1.42 | 1.44 | 1.45 |
| 13 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.54 | 1.55 | 1.56 |
| 14 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 |
| 15 | 1.68 | 1.69 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.78 |
| 16 | 1.79 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 | 1.88 | 1.90 |
| 17 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 | 1.97 | 1.99 | 2.00 | 2.01 |
| 18 | 2.02 | 2.03 | 2.04 | 2.05 | 2.06 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 |
| 19 | 2.13 | 2.14 | 2.15 | 2.16 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 |
| 20 | 2.24 | 2.25 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 |
| 21 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 | 2.45 | 2.16 |
| 22 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.55 | 2.56 | 2.57 |
| 23 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 | 2.64 | 2.65 | 2.66 | 2.67 | 2.65 |
| 24 | 2.69 | 2.70 | 2.71 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.75 | 2.79 |
| 25 | 2.50 | 2.82 | 2.83 | 2.84 | 2.85 | 2.86 | 2.57 | 2.88 | 2.89 | 2.91 |
| 26 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 3.00 | 3.01 | 3.02 |
| 27 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.10 | 3.11 | 3.12 | 3.13 |
| 28 | 3.14 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 |
| 29 | 3.25 | 3.26 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 |
| 30 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.47 |
| 31 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.56 | 3.57 | 3.58 |
| 32 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.65 | 3.66 | 3.67 | 3.68 | 3.69 |
| 33 | 3.70 | 3.71 | 3.72 | 3.74 | 3.75 | 3.76 | 3.77 | 3.78 | 3.79 | 3.80 |
| 34 | 3.81 | 3.83 | 3.84 | 3.85 | 3.86 | 3.57 | 3.58 | 3.59 | 3.90 | 3.91 |
| 35 | 3.93 | 3.94 | 3.95 | 3.96 | 3.97 | 3.98 | 3.99 | 4.00 | 4.02 | 4.03 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $700^{\text {nin. }}$ (from 697.51 to 702.50) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 0 | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.02 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 0.03 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.12 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.21 |
| 2 | 0.23 | 024 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 | 0.33 |
| 3 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 |
| 4 | 0.4.) | 0.46 | 0.17 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 |
| 5 | 0.56 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 |
| 6 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.75 | 0.76 | 0.77 | 0.78 |
| 7 | 0.79 | 0.50 | 0.81 | 0.82 | 0.84 | 0.85 | 0.86 | 0.57 | 0.88 | 0.89 |
| 8 | 0.90 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.01 |
| 9 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.10 | 1.11 | 1.12 |
| 10 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 |
| 11 | 1.24 | 1.25 | 1.27 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 |
| 12 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.41 | 1.42 | 1.43 | 1.45 | 1.46 |
| 13 | 1.47 | 1.45 | 1.49 | 1.50 | 1.51 | 1.53 | 1.54 | 1.55 | 1.56 | 1.57 |
| 14 | 1.58 | 1.59 | 1.60 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 |
| 15 | 1.69 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.77 | 1.79 | 1.50 |
| 16 | 1.81 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.88 | 1.89 | 1.90 | 1.91 |
| 17 | 1.92 | 1.93 | 1.94 | 1.95 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 |
| 18 | 2.03 | 2.04 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.14 |
| 19 | 2.15 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.21 | 2.23 | 2.24 | 2.25 |
| 20 | 2.26 | 2.27 | 2.28 | 2.99 | 2.30 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 |
| 21 | 2.37 | 2.35 | 2.40 | 2.41 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 | 2.17 |
| 22 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.5 .5 | 2.56 | 2.58 | 2.59 |
| 23 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 |
| 24 | 2.71 | 2.72 | 2.73 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 |
| 25 | 2.82 | 2.84 | 2.85 | 2.86 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.93 |
| 26 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.01 | 3.02 | 3.03 | 3.04 |
| 27 | 3.05 | 3.06 | 3.07 | 3.08 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 |
| 28 | 3.16 | 3.17 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.27 |
| 29 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.34 | 3.36 | 3.37 | 3.38 |
| 30 | 3.39 | 3.40 | 3.41 | 3.42 | 3.43 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 |
| 31 | 3.50 | 3.51 | 3.52 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 |
| 32 | 3.62 | 3.63 | 3.64 | 3.6 .5 | 3.66 | 3.67 | 3.68 | 3.69 | 3.71 | 3.72 |
| 33 | 3.73 | 3.74 | 3.75 | 3.76 | 3.77 | 3.78 | 3.80 | 3.81 | 3.82 | 3.83 |
| 34 | 3.84 | 3.55 | 3.86 | 3.88 | 3.89 | 3.90 | 3.91 | 3.92 | 3.93 | 3.94 |
| 35 | 3.95 | 3.97 | 3.98 | 3.99 | 4.00 | 4.01 | 4.02 | 4.03 | 4.04 | 4.06 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | \%. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $705{ }^{\text {mm. }}$ ( from 702.51 to 707.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.05 \end{aligned}$ | $\begin{array}{\|c\|c} \text { Millim. } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~s} \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.22 |
| 2 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.30 | 0.31 | 0.32 | 033 |
| 3 | 0.34 | 0.35 | 0.36 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 |
| 4 | 0.46 | 0.47 | 0.18 | 0.19 | 0.50 | 0.51 | 0.52 | 0.53 | 0.55 | 0.56 |
| 5 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 |
| 6 | 0.68 | 0.69 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.79 |
| 7 | 0.50 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.88 | 0.89 | 0.90 |
| 8 | 0.91 | 0.92 | 0.93 | 0.94 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 |
| 9 | 1.02 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 109 | 1.10 | 1.12 | 1.13 |
| 10 | 1.14 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.21 | 1.22 | 1.23 | 1.24 |
| 11 | 1.25 | 1.26 | 1.27 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 |
| 12 | 1.37 | 1.38 | 1.39 | 1.40 | 1.41 | 1.42 | 1.43 | 1.45 | 1.46 | 1.47 |
| 13 | 1.48 | 1.49 | 1.50 | 1.51 | 1.52 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 |
| 14 | 1.59 | 1.60 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.70 |
| 15 | 1.71 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.78 | 1.79 | 1.80 | 1.81 |
| 16 | 1.82 | 1.83 | 1.84 | 1.85 | 1.57 | 1.58 | 1.89 | 1.90 | 1.91 | 1.92 |
| 17 | 1.93 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.00 | 2.01 | 2.03 | 2.04 |
| 18 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 |
| 19 | 2.16 | 2.17 | 2.18 | 2.20 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 |
| 20 | 2.28 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.36 | 2.37 | 2.38 |
| 21 | 2.39 | 2.40 | 2.41 | 2.42 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 |
| 22 | 2.50 | 2.51 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.59 | 2.61 |
| 23 | 2.62 | 2.63 | 2.64 | 2.6 .5 | 2.66 | 2.67 | 2.69 | 2.70 | 2.71 | 2.72 |
| 24 | 2.73 | 2.74 | 2.75 | 2.77 | 2.78 | 2.79 | 2.80 | 2.81 | 2.52 | 2.83 |
| 25 | 2.84 | 2.86 | 2.87 | 2.85 | 2.89 | 2.90 | 2.91 | 2.92 | 2.94 | 2.95 |
| 26 | 2.96 | 2.97 | 2.98 | 2.99 | 3.00 | 3.02 | 3.03 | 3.04 | 3.05 | 3.06 |
| 27 | 3.07 | 3.08 | 3.10 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 |
| 28 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.27 | 3.28 | 3.29 |
| 29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 |
| 30 | 3.41 | 3.42 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.49 | 3.50 | 3.52 |
| 31 | 3.53 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.60 | 3.61 | 3.62 | 3.63 |
| 32 | 3.64 | 3.65 | 3.66 | 3.65 | 3.69 | 3.70 | 3.71 | 3.72 | 3.73 | 3.74 |
| 33 | 3.75 | 3.77 | 3.78 | 3.79 | 3.80 | 3.81 | 3.82 | 3.53 | 3.55 | 3.86 |
| 34 | 3.87 | 3.58 | 3.89 | 3.90 | 3.91 | 3.93 | 3.94 | 3.95 | 3.96 | 3.97 |
| 35 | 3.98 | 3.99 | 4.01 | 4.02 | 4.03 | 4.04 | 4.05 | 4.06 | 4.07 | 4.08 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigraile Degrees | BAROMETER : $710^{\mathrm{mm} .}$ (from 707.51 to 712.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 0 | Millim. 0.00 | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.11 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.21 | 0.22 |
| 2 | 0.23 | 0.24 | 0.25 | 0.26 | 0.25 | 0.29 | 0.30 | 0.31 | 0.32 | 0.33 |
| 3 | 0.34 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 |
| 4 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.52 | 0.53 | 0.54 | 0.5.) | 0.56 |
| 5 | 0.57 | 0.58 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.63 | 0.66 | 0.68 |
| 6 | 0.69 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.76 | 0.77 | 0.78 | 0.79 |
| 7 | 0.80 | 0.81 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.91 |
| 8 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.99 | 1.00 | 1.01 | 1.02 |
| 9 | 1.03 | 1.04 | 1.05 | 1.07 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 |
| 10 | 1.15 | 1.16 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.23 | 1.24 | 1.25 |
| 11 | 1.26 | 1.27 | 1.28 | 1.29 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 |
| 12 | 1.38 | 1.39 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.46 | 1.47 | 1.45 |
| 13 | 1.49 | 1.50 | 1.51 | 1.52 | 1.54 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 |
| 14 | 1.60 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.68 | 1.70 | 1.71 |
| 15 | 1.72 | 1.73 | 1.74 | 1.75 | 1.76 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 |
| 16 | 1.83 | 1.84 | 1.86 | 1.87 | 1.88 | 1.89 | 1.90 | 1.91 | 1.93 | 1.94 |
| 17 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 |
| 18 | 2.06 | 2.07 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.17 |
| 19 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.2 .5 | 2.26 | 2.27 | 2.28 |
| 20 | 2.29 | 2.30 | 2.31 | 2.33 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.40 |
| 21 | 2.41 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 | 2.48 | 2.49 | 2.50 | 2.51 |
| 22 | 2.52 | 2.53 | 2.54 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.62 |
| 23 | 2.64 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.70 | 2.72 | 2.73 | 2.74 |
| 24 | 2.75 | 2.76 | 2.77 | 2.78 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.85 |
| 25 | 2.86 | 2.88 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.95 | 2.96 | 2.97 |
| 26 | 2.98 | 2.99 | 3.00 | 3.01 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 |
| 27 | 3.09 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 |
| 28 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 |
| 29 | 3.32 | 3.33 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.41 | 3.43 |
| 30 | 3.44 | 3.45 | 3.46 | 3.47 | 3.48 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 |
| 31 | 3.55 | 3.56 | 3.58 | 3.59 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.66 |
| 32 | 3.67 | 3.68 | 3.69 | 3.70 | 3.71 | 3.72 | 3.74 | 3.75 | 3.76 | 3.77 |
| 33 | 3.78 | 3.79 | 3.80 | 3.82 | 3.83 | 3.84 | 3.85 | 3.86 | 3.87 | 3.58 |
| 34 | 3.90 | 3.91 | 3.92 | 3.93 | 3.94 | 3.95 | 3.96 | 3.98 | 3.99 | 4.00 |
| 35 | 4.01 | 4.02 | 4.03 | 4.05 | 4.06 | 4.07 | 4.08 | 4.09 | 4.10 | 4.11 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grate } \\ \text { Degrees } \end{gathered}$ | BAROMETER : 715 ${ }^{\text {min. }}$ (from 712.51 to 717.50) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{gathered} \circ \\ 0 \end{gathered}$ | $\begin{gathered} \text { Millitn. } \\ 0.00 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.01 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Tillim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~s} \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.20 | 0.21 | 0.22 |
| 2 | 0.23 | 0.24 | 0.25 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 | 0.33 |
| 3 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 | 0.45 |
| 4 | 0.16 | 0.47 | 0.48 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.57 |
| 5 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.65 | 0.66 | 0.67 | 0.68 |
| 6 | 0.69 | 0.70 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.80 |
| 7 | 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.87 | 0.88 | 0.89 | 0.90 | 0.91 |
| 8 | 0.92 | 0.93 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.02 | 1.03 |
| 9 | 1.04 | 1.05 | 1.06 | 1.07 | 1.08 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 |
| 10 | 1.15 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.25 | 1.26 |
| 11 | 1.27 | 1.28 | 1.29 | 1.30 | 1.32 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 |
| 12 | 1.35 | 1.40 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.47 | 1.48 | 1.49 |
| 13 | 1.50 | 1.51 | 1.52 | 1.53 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 |
| 11 | 1.62 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.65 | 1.70 | 1.71 | 1.72 |
| 15 | 1.73 | 1.71 | 1.75 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.83 |
| 16 | 1.85 | 1.56 | 1.87 | 1.88 | 1.89 | 1.90 | 1.92 | 1.93 | 1.94 | 1.95 |
| 17 | 1.96 | 1.97 | 1.98 | 2.00 | 2.01 | 2.02 | 2.03 | 2.04 | 2.05 | 2.07 |
| 18 | 2.08 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.15 | 2.16 | 2.17 | 2.18 |
| 19 | 2.19 | 2.20 | 2.22 | 2.23 | 2.24 | 2.25 | 2.26 | 2.27 | 2.28 | 2.30 |
| 20 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 | 2.37 | 2.38 | 2.39 | 2.40 | 2.41 |
| 21 | 2.42 | 2.13 | 2.45 | 2.46 | 2.47 | 2.45 | 2.49 | 2.50 | 2.52 | 2.53 |
| 22 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 |
| 23 | 2.65 | 2.67 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.74 | 2.75 | 2.76 |
| 24 | 2.77 | 2.75 | 2.79 | 2.80 | 2.82 | 2.83 | 2.84 | 2.85 | 2.86 | 2.87 |
| 25 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.97 | 2.98 | 2.99 |
| 26 | 3.00 | 3.01 | 3.02 | 3.04 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 |
| 27 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 | 3.21 | 3.22 |
| 28 | 3.23 | 3.24 | 3.25 | 327 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.34 |
| 29 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.42 | 3.43 | 3.44 | 3.45 |
| 30 | 3.46 | 3.47 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.55 | 3.57 |
| 31 | 3.58 | 3.59 | 3.60 | 3.61 | 3.62 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 |
| 32 | 3.69 | 3.70 | 3.72 | 3.73 | 3.74 | 3.75 | 3.76 | 3.77 | 3.79 | 3.80 |
| 33 | 3.81 | 3.92 | 3.83 | 3.84 | 3.55 | 3.57 | 3.88 | 3.89 | 3.90 | 3.41 |
| 34 | 3.92 | 394 | 3.95 | 3.96 | 3.97 | 3.98 | 3.99 | 4.00 | 4.02 | 4.03 |
| 35 | 4.04 | 4.05 | 4.06 | 4.07 | 4.09 | 4.10 | 4.11 | 4.12 | 4.13 | 4.14 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : 720 mm ( from 717.51 to 722.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{aligned} & \text { Mıllim. } \\ & 0.01 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Miilim. } \\ 0.03 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.05 \end{aligned}$ | $\begin{array}{\|c\|c} \text { Millim } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ |
| 1 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 |
| 2 | 0.23 | 0.24 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 | 0.34 |
| 3 | 0.35 | 0.36 | 0.37 | 0.38 | 0.40 | 0.11 | 0.42 | 0.43 | 0.44 | 0.45 |
| 4 | 0.46 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.55 | 0.56 | 0.57 |
| 5 | 0.58 | 0.59 | 0.60 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.69 |
| 6 | 0.70 | 0.71 | 0.72 | 0.73 | 0.74 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 |
| 7 | 0.81 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.91 | 0.92 |
| 8 | 0.93 | 0.94 | 0.95 | 0.96 | 0.98 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 |
| 9 | 1.05 | 1.06 | 1.07 | 1.08 | 1.09 | 1.10 | 1.12 | 1.13 | 1.14 | 1.1.5 |
| 10 | 1.16 | 1.17 | 1.19 | 1.20 | 1.21 | 1.22 | 1.23 | 1.24 | 1.26 | 1.27 |
| 11 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.34 | 1.35 | 1.36 | 1.37 | 1.38 |
| 12 | 1.39 | 1.41 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.48 | 1.49 | 1.50 |
| 13 | 1.51 | 1.52 | 1.53 | 1.55 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.62 |
| 14 | 1.63 | 1.64 | 1.65 | 1.66 | 1.67 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 |
| 15 | 1.74 | 1.75 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.82 | 1.84 | 1.85 |
| 16 | 1.86 | 1.87 | 1.88 | 1.89 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.96 |
| 17 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.05 | 2.06 | 2.07 | 2.08 |
| 18 | 2.09 | 2.10 | 2.11 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.18 | 2.20 |
| 19 | 2.21 | 2.22 | 2.23 | 2.24 | 2.25 | 2.27 | 2.28 | 2.29 | 2.30 | 2.31 |
| 20 | 2.32 | 2.34 | 2.35 | 2.36 | 2.37 | 2.38 | 2.39 | 2.41 | 2.42 | 2.43 |
| 21 | 2.44 | 2.45 | 2.46 | 2.48 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 |
| 22 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.63 | 2.64 | 2.65 | 2.66 |
| 23 | 2.67 | 2.68 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 | 2.77 | 2.78 |
| 24 | 2.79 | 2.80 | 2.81 | 2.82 | 2.84 | 2.85 | 2.86 | 2.87 | 2.88 | 2.89 |
| 25 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.99 | 3.00 | 3.01 |
| 26 | 3.02 | 3.03 | 3.04 | 3.06 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.13 |
| 27 | 3.14 | 3.15 | 3.16 | 3.17 | 3.18 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 |
| 25 | 3.25 | 3.27 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.34 | 3.35 | 3.36 |
| 29 | 3.37 | 3.38 | 3.39 | 3.40 | 3.42 | 3.43 | $3 \cdot 44$ | 3.45 | 3.46 | 5.47 |
| 30 | 3.49 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 | 3.56 | 3.57 | 3.58 | 3.59 |
| 31 | 3.60 | 3.61 | 3.63 | 3.64 | 3.65 | 3.66 | 3.67 | 3.68 | 3.70 | 3.71 |
| 32 | 3.72 | 3.73 | 3.74 | 3.75 | 3.77 | 3.78 | 3.79 | 3.80 | 3.81 | 3.82 |
| 33 | 3.83 | 3.85 | 3.86 | 3.87 | 3.88 | 3.59 | 3.90 | 3.92 | 3.93 | 3.94 |
| 34 | 3.95 | 3.96 | 3.97 | 3.99 | 4.00 | 4.01 | 4.02 | 4.03 | 4.04 | 4.06 |
| 35 | 4.07 | 4.08 | 4.09 | 4.10 | 4.11 | 4.13 | 4.14 | 4.15 | 4.16 | 4.17 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi. } \\ \text { grate } \\ \text { Degrees } \end{gathered}$ | BAROMETER : $725^{\text {nmm. }}$ (from 722.51 to 72750 ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 . | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Mullim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{array}{\|c} \text { Millim. } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \mathrm{M} \mathrm{H}_{1 \mathrm{lim}} . \\ 0.09 \end{gathered}$ | Millim. $0.11$ |
| 1 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.21 | 0.22 |
| 2 | 0.23 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.32 | 0.33 | 0.34 |
| 3 | 0.35 | 0.36 | 0.37 | 0.39 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.46 |
| 4 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 |
| 5 | 0.59 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.68 | 0.69 |
| 6 | 0.70 | 0.71 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.80 | 0.81 |
| 7 | 0.82 | 0.83 | 0.84 | 0.85 | 0.87 | 0.88 | 0.89 | 0.90 | 0.91 | 0.92 |
| 8 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.01 | 1.02 | 1.03 | 1.0.4 |
| 9 | 1.05 | 1.06 | 1.08 | 1.09 | 1.10 | 1.11 | 1.12 | 1.14 | 1.15 | 1.16 |
| 10 | 1.17 | 1.18 | 1.19 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.26 | 1.28 |
| 11 | 1.29 | 1.30 | 1.31 | 1.32 | 1.33 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 |
| 12 | 1.40 | 1.42 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.49 | 1.50 | 1.51 |
| 13 | 1.52 | 1.53 | 1.54 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.63 |
| 14 | 1.64 | 1.65 | 1.66 | 1.67 | 1.69 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 |
| 15 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 | 1.81 | 1.83 | 1.84 | 1.85 | 1.86 |
| 16 | 1.87 | 1.88 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.95 | 1.97 | 1.98 |
| 17 | 1.99 | 2.00 | 2.01 | 2.02 | 2.04 | 2.05 | 2.06 | 2.07 | 2.08 | 2.09 |
| 18 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.16 | 2.18 | 2.19 | 2.20 | 2.21 |
| 19 | 2.22 | 2.23 | 2.25 | 2.26 | 2.27 | 2.28 | 2.29 | 2.31 | 2.32 | 2.33 |
| 20 | 2.34 | 2.35 | 2.86 | 2.38 | 2.39 | 2.40 | 2.41 | 2.42 | 2.43 | 2.45 |
| 21 | 2.46 | 2.47 | 2.48 | 2.49 | 2.50 | 2.52 | 2.53 | 2.54 | 2.55 | 2.56 |
| 22 | 2.57 | 2.59 | 2.60 | 261 | 2.62 | 2.63 | 2.64 | 2.66 | 2.67 | 2.68 |
| 23 | 2.69 | 2.70 | 2.71 | 2.73 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.80 |
| 24 | 2.81 | 2.82 | 2.83 | 2.84 | 2.86 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 |
| 25 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 | 2.98 | 3.00 | 3.01 | 3.02 | 3.03 |
| 26 | 3.04 | 3.05 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 | 3.14 | 3.15 |
| 27 | 3.16 | 3.17 | 3.18 | 3.19 | 3.21 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 |
| 28 | 3.28 | 3.29 | 3.30 | 3.31 | 3.32 | 3.33 | 3.35 | 3.36 | 3.37 | 3.38 |
| 29 | 3.39 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.16 | 3.48 | 3.49 | 3.50 |
| 30 | 3.51 | 3.52 | 3.53 | 3.55 | 3.56 | 3.57 | 3.58 | 3.59 | 3.60 | 3.62 |
| 31 | 3.63 | 3.64 | 3.65 | 3.66 | 3.67 | 3.69 | 3.70 | 3.71 | 3.72 | 3.73 |
| 32 | 3.74 | 3.76 | 3.77 | 3.78 | 3.79 | 3.80 | 3.81 | 3.83 | 3.84 | 3.55 |
| 33 | 3.86 | 3.87 | 3.88 | 3.90 | 3.91 | 3.92 | 3.93 | 3.94 | 3.96 | 3.97 |
| 34 | 3.98 | 3.99 | 4.00 | 4.01 | 4.03 | 4.04 | 4.05 | 4.06 | 4.07 | 4.08 |
| 35 | 4.10 | 4.11 | 4.12 | 4.13 | 4.14 | 4.15 | 4.17 | 4.18 | 4.19 | 4.20 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi. } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $730^{\text {mm. }}$ (from 727.51 to 732.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \hline \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Mıllim. } \\ 0.01 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.02 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 0.01 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.06 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.07 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.09 \end{aligned}$ | Millim. $0.11$ |
| 1 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.21 | 0.22 |
| 2 | 0.24 | 025 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 | 0.33 | 0.34 |
| 3 | 035 | 0.37 | 0.38 | 0.39 | 0.40 | 0.41 | 0.12 | 0.44 | 0.45 | 0.46 |
| 4 | 0.47 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.57 | 0.58 |
| 5 | 0.59 | 0.60 | 0.61 | 0.62 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.70 |
| 6 | 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.77 | 0.78 | 0.79 | 0.80 | 0.81 |
| 7 | 0.82 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 090 | 0.91 | 0.92 | 0.93 |
| 8 | 0.94 | 0.9.) | 0.97 | 0.98 | 0.99 | 1.00 | 1.01 | 1.03 | 1.04 | 1.05 |
| 9 | 1.06 | 1.07 | 1.05 | 1.10 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.17 |
| 10 | 1.18 | 1.19 | 1.20 | 1.21 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.28 |
| 11 | 1.30 | 1.31 | 1.32 | 1.33 | 1.34 | 1.35 | 1.37 | 1.38 | 1.39 | 1.40 |
| 12 | 1.41 | 1.43 | 1.44 | 1.45 | 1.46 | 1.47 | 1.48 | 1.50 | 1.51 | 1.52 |
| 13 | 1.53 | 1.54 | 1.56 | 1.57 | 1.58 | 1.59 | 1.60 | 1.61 | 1.63 | 1.64 |
| 14 | 1.65 | 1.66 | 1.67 | 1.68 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.76 |
| 15 | 1.77 | 1.75 | 1.79 | 1.80 | 1.81 | 1.83 | 1.84 | 1.85 | 1.86 | 1.87 |
| 16 | 1.89 | 1.90 | 1.91 | 1.92 | 1.93 | 1.94 | 1.96 | 1.97 | 1.98 | 1.99 |
| 17 | 2.00 | 201 | 2.03 | 2.04 | 2.05 | 2.06 | 2.07 | 2.09 | 2.10 | 2.11 |
| 18 | 2.12 | 2.13 | 2.14 | 2.16 | 2.17 | 2.18 | 2.19 | 2.20 | 2.22 | 2.23 |
| 19 | 2.24 | 2.25 | 2.26 | 2.27 | 2.29 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 |
| 20 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 |
| 21 | 2.47 | 2.49 | 2.50 | 2.51 | 2.52 | 2.53 | 2.54 | 2.56 | 2.57 | 2.58 |
| 22 | 2.59 | 2.60 | 2.62 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.69 | 2.70 |
| 23 | 2.71 | 2.72 | 2.73 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.80 | 2.82 |
| 24 | 2.83 | 2.84 | 2.85 | 2.86 | 2.87 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 |
| 25 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 |
| 26 | 3.06 | 3.08 | 3.09 | 3.10 | 3.11 | 3.12 | 3.13 | 3.15 | 3.16 | 3.17 |
| 27 | 3.18 | 3.19 | 3.20 | 3.22 | 3.23 | 3.24 | 3.25 | 3.26 | 3.28 | 3.29 |
| 28 | 3.30 | 3.31 | 3.32 | 3.33 | 3.35 | 3.36 | 3.37 | 3.38 | 3.39 | 3.41 |
| 29 | 3.42 | 3.43 | 3.44 | 3.45 | 3.46 | 3.48 | 3.49 | 3.50 | 3.51 | 5.52 |
| 30 | 3.53 | 3.5.5 | 3.56 | 3.57 | 3.58 | 3.59 | 3.61 | 3.62 | 3.63 | 3.64 |
| 31 | 3.65 | 3.66 | 3.68 | 3.69 | 3.70 | 3.71 | 372 | 3.73 | 3.75 | 3.76 |
| 32 | 3.77 | 3.78 | 3.79 | 3.81 | 3.82 | 3.83 | 3.84 | 3.85 | 3.56 | 3.58 |
| 33 | 3.89 | 3.90 | 3.91 | 3.92 | 3.94 | 3.95 | 3.96 | 3.97 | 3.98 | 3.99 |
| 34 | 4.01 | 4.02 | 4.03 | 4.04 | 4.05 | 4.06 | 4.07 | 4.09 | 4.10 | 4.11 |
| 35 | 4.12 | 4.14 | 4.15 | 4.16 | 4.17 | 4.18 | 4.19 | 4.21 | 4.22 | 4.23 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |



| Centigrade Degrees. | BAROMETER : $740{ }^{\text {mm. }}$ ( from 737.51 to 742.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | ©. | 1 | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~s} \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.12 | 0.13 | 0.14 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.21 | 0.23 |
| 2 | 0.24 | 0.25 | 0.26 | 0.27 | 0.29 | 0.30 | 0.31 | 0.32 | 0.33 | 0.35 |
| 3 | 0.36 | 0.37 | 0.38 | 0.39 | 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.47 |
| 4 | 0.48 | 0.49 | 0.50 | 0.51 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.59 |
| 5 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 |
| 6 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.78 | 0.79 | 0.50 | 0.81 | 0.82 |
| 7 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 |
| 8 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 | 1.02 | 1.03 | 1.04 | 1.05 | 1.06 |
| 9 | 1.07 | 1.09 | 1.10 | 1.11 | 1.12 | 1.13 | 1.15 | 1.16 | 1.17 | 1.18 |
| 10 | 1.19 | 1.21 | 1.22 | 1.23 | 1.24 | 1.25 | 1.27 | 1.28 | 1.29 | 1.30 |
| 11 | 1.31 | 1.33 | 1.34 | 1.35 | 1.36 | 1.37 | 1.39 | 1.40 | 1.41 | 1.42 |
| 12 | 1.43 | 1.45 | 1.46 | 1.47 | 1.48 | 1.49 | 1.50 | 1.52 | 1.53 | 1.54 |
| 13 | 1.55 | 1.56 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.64 | 1.65 | 1.66 |
| 14 | 1.67 | 1.68 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.76 | 1.77 | 1.78 |
| 15 | 1.79 | 1.80 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.88 | 1.89 | 1.90 |
| 16 | 1.91 | 1.92 | 1.93 | 1.95 | 1.96 | 1.97 | 1.98 | 1.99 | 2.01 | 2.02 |
| 17 | 2.03 | 2.04 | 2.05 | 2.07 | 2.08 | 2.09 | 2.10 | 2.11 | 2.13 | 2.14 |
| 18 | 2.15 | 2.16 | 2.17 | 2.19 | 2.20 | 2.21 | 2.22 | 2.23 | 2.25 | 2.26 |
| 19 | 2.27 | 2.28 | 2.29 | 2.31 | 2.32 | 2.33 | 2.34 | 2.35 | 2.36 | 2.38 |
| 20 | 2.39 | 2.40 | 2.41 | 2.42 | 2.44 | 2.45 | 2.46 | 2.47 | 2.48 | 2.50 |
| 21 | 2.51 | 2.52 | 2.53 | 2.54 | 2.56 | 2.57 | 2.58 | 2.59 | 2.60 | 2.62 |
| 22 | 2.63 | 2.64 | 2.65 | 2.66 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.74 |
| 23 | 2.75 | 2.76 | 2.77 | 2.78 | 2.79 | 2.81 | 2.82 | 2.83 | 2.84 | 2.85 |
| 24 | 2.87 | 2.88 | 2.89 | 2.90 | 2.91 | 2.93 | 2.94 | 2.95 | 2.96 | 2.97 |
| 25 | 2.99 | 3.00 | 3.01 | 3.02 | 3.03 | 3.05 | 3.06 | 3.07 | 3.08 | 3.09 |
| 26 | 3.11 | 3.12 | 3.13 | 3.14 | 3.15 | 3.17 | 3.18 | 3.19 | 3.20 | 3.21 |
| 27 | 3.22 | 3.24 | 3.25 | 3.26 | 3.27 | 3.28 | 3.30 | 3.31 | 3.32 | 3.33 |
| 28 | 3.34 | 3.36 | 3.37 | 3.38 | 3.39 | 3.40 | 3.42 | 3.43 | 3.44 | 3.45 |
| 29 | 3.46 | 3.48 | 3.49 | 3.50 | 3.51 | 3.52 | 3.54 | 3.55 | 3.56 | 3.57 |
| 30 | 3.58 | 3.60 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 | 3.67 | 3.68 | 3.69 |
| 31 | 3.70 | 3.71 | 3.73 | 3.74 | 3.75 | 3.76 | 3.77 | 3.79 | 3.80 | 3.81 |
| 32 | 3.82 | 3.83 | 3.85 | 3.86 | 3.57 | 3.88 | 3.89 | 3.91 | 3.92 | 3.93 |
| 33 | 3.94 | 3.95 | 3.97 | 3.98 | 3.99 | 4.00 | 4.01 | 4.02 | 4.04 | 4.05 |
| 34 | 4.06 | 4.07 | 4.08 | 4.10 | 4.11 | 4.12 | 4.13 | 4.14 | 4.16 | 4.17 |
| 35 | 4.18 | 4.19 | 4.20 | 4.22 | 4.23 | 4.24 | 4.25 | 4.26 | 4.28 | 4.29 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { gratle } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $745^{\mathrm{mm}}$. (from $\mathbf{7 4 2 . 5 1}$ to $\mathbf{7 4 7 . 5 0}$ ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { M1llim. } \\ 0.02 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.04 \end{aligned}$ | $\begin{gathered} \text { Millim } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.07 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 0.0 \mathrm{~s} \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 0.10 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.12 | 0.13 | 0.14 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 | 0.22 | 0.23 |
| 2 | 0.24 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.32 | 0.34 | 0.35 |
| 3 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.46 | 0.47 |
| 4 | 0.15 | 0.49 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.57 | 0.58 | 0.59 |
| 5 | 0.60 | 0.61 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.69 | 0.70 | 0.71 |
| 6 | 0.72 | 0.73 | 0.7.) | 0.76 | 0.77 | 0.78 | 0.79 | 0.81 | 0.82 | 0.83 |
| 7 | 0.84 | 0.85 | 0.57 | 0.85 | 0.59 | 0.90 | 0.91 | 0.93 | 0.94 | 0.95 |
| 8 | 0.96 | 0.97 | 0.99 | 1.00 | 1.01 | 1.02 | 1.03 | 1.05 | 1.06 | 1.07 |
| 9 | 1.08 | 1.09 | 1.11 | 1.12 | 1.13 | 1.14 | 1.15 | 1.17 | 1.18 | 1.19 |
| 10 | 1.20 | 1.21 | 1.23 | 1.24 | 1.25 | 1.26 | 1.27 | 1.29 | 1.30 | 1.31 |
| 11 | 1.32 | 1.33 | 1.35 | 1.36 | 1.37 | 1.38 | 1.39 | 1.41 | 1.42 | 1.43 |
| 12 | 1.44 | 1.45 | 1.47 | 1.48 | 1.49 | 1.50 | 1.52 | 1.53 | 1.54 | 1.55 |
| 13 | 1.56 | 1.58 | 1.59 | 1.60 | 1.61 | 1.62 | 1.64 | 1.65 | 1.66 | 1.67 |
| 14 | 1.68 | 1.70 | 1.71 | 1.72 | 1.73 | 1.74 | 1.76 | 1.77 | 1.78 | 1.79 |
| 15 | 1.80 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.88 | 1.89 | 1.90 | 1.91 |
| 16 | 1.92 | 1.94 | 1.95 | 1.96 | 1.97 | 1.98 | 2.00 | 2.01 | 2.02 | 2.03 |
| 17 | 2.04 | 2.06 | 2.07 | 2.08 | 2.09 | 2.10 | 2.12 | 2.13 | 2.14 | 2.15 |
| 18 | 2.16 | 2.18 | 2.19 | 2.20 | 2.21 | 2.22 | 2.24 | 2.25 | 2.26 | 2.27 |
| 19 | 2.28 | 2.30 | 2.31 | 2.32 | 2.33 | 2.34 | 2.36 | 2.37 | 2.38 | 2.39 |
| 20 | 2.40 | 2.42 | 2.43 | 2.44 | 2.45 | 2.46 | 2.48 | 2.49 | 2.50 | 2.51 |
| 21 | 2.53 | 2.54 | 2.55 | 2.56 | 2.57 | 2.59 | 2.60 | 2.61 | 2.62 | 2.63 |
| 22 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 | 2.71 | 2.72 | 2.73 | 2.74 | 2.75 |
| 23 | 2.77 | 2.75 | 2.79 | 2.80 | 2.81 | 2.83 | 2.54 | 2.85 | 2.86 | 2.87 |
| 24 | 2.89 | 2.90 | 2.91 | 2.92 | 2.93 | 2.95 | 2.96 | 2.97 | 2.98 | 2.99 |
| 25 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 | 3.07 | 3.08 | 3.09 | 3.10 | 3.11 |
| 26 | 3.13 | 3.14 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 | 3.21 | 3.22 | 3.23 |
| 27 | 3.25 | 3.26 | 3.27 | 3.28 | 3.29 | 3.31 | 3.32 | 3.33 | 3.34 | 3.35 |
| 28 | 3.37 | 3.38 | 3.39 | 3.10 | 3.41 | 3.43 | 3.44 | 3.45 | 3.46 | 3.48 |
| 29 | 3.49 | 3.50 | 3.51 | 3.52 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.60 |
| 30 | 3.61 | 3.62 | 3.63 | 3.64 | 3.66 | 3.67 | 3.68 | 3.69 | 3.70 | 3.72 |
| 31 | 3.73 | 3.74 | 3.75 | 3.76 | 3.75 | 3.79 | 3.80 | 3.81 | 3.82 | 3.84 |
| 32 | 3.85 | 3.86 | 3.87 | 3.88 | 3.90 | 3.91 | 3.92 | 3.93 | 3.94 | 3.96 |
| 33 | 3.97 | 3.98 | 3.99 | 4.00 | 4.02 | 4.03 | 4.04 | 4.05 | 4.06 | 4.08 |
| 34 | 4.09 | 4.10 | 4.11 | 4.12 | 4.14 | 4.15 | 4.16 | 4.17 | 4.18 | 4.20 |
| 35 | 4.21 | 4.22 | 4.23 | 4.24 | 4.26 | 4.27 | 4.28 | 4.29 | 4.30 | 4.32 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $750{ }^{\text {mm. }}$ ( from 747.51 to 752.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | $\%$ \% | 8. | 9. |
| 0 | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.01 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 0.02 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.05 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.07 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.0 \mathrm{~s} \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.12 | 0.13 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.21 | 0.22 | 0.23 |
| 2 | 0.24 | 0.25 | 0.27 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 | 0.34 | 0.35 |
| 3 | 0.36 | 0.35 | 0.39 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.46 | 0.47 |
| 4 | 0.48 | 0.50 | 0.51 | 0.52 | 0.53 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 |
| 5 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 |
| 6 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.79 | 0.80 | 0.81 | 0.82 | 0.84 |
| 7 | 0.85 | 0.86 | 0.87 | 0.58 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.96 |
| 8 | 0.97 | 0.98 | 0.99 | 1.00 | 1.02 | 1.03 | 1.04 | 1.05 | 1.07 | 1.08 |
| 9 | 1.09 | 1.10 | 1.11 | 1.13 | 1.14 | 1.15 | 1.16 | 1.17 | 1.19 | 1.20 |
| 10 | 1.21 | 1.22 | 1.23 | 1.25 | 1.26 | 1.27 | 1.28 | 1.30 | 1.31 | 1.32 |
| 11 | 1.33 | 1.34 | 1.36 | 1.37 | 1.38 | 1.39 | 1.40 | 1.42 | 1.43 | 1.44 |
| 12 | 1.45 | 1.46 | 1.48 | 1.49 | 1.50 | 1.51 | 1.53 | 1.54 | 1.55 | 1.56 |
| 13 | 1.57 | 1.59 | 1.60 | 1.61 | 1.62 | 1.63 | 1.65 | 1.66 | 1.67 | 1.68 |
| 14 | 1.69 | 1.71 | 1.72 | 1.73 | 1.74 | 1.76 | 1.77 | 1.78 | 1.79 | 1.80 |
| 15 | 1.82 | 1.83 | 1.84 | 1.85 | 1.86 | 1.88 | 1.89 | 1.90 | 1.91 | 1.92 |
| 16 | 1.94 | 1.95 | 1.96 | 1.97 | 1.99 | 2.00 | 2.01 | 2.02 | 2.03 | 2.05 |
| 17 | 2.06 | 2.07 | 2.08 | 2.09 | 2.11 | 2.12 | 2.13 | 2.14 | 2.15 | 2.17 |
| 18 | 2.18 | 2.19 | 2.20 | 2.21 | 2.23 | 2.24 | 2.25 | 2.26 | 2.28 | 2.29 |
| 19 | 2.30 | 2.31 | 2.32 | 2.34 | 2.35 | 2.36 | 2.87 | $\underline{2} .38$ | 2.40 | 2.41 |
| 20 | 2.42 | 2.43 | 2.45 | 2.46 | 2.47 | 2.48 | 2.49 | 2.51 | 2.52 | 2.53 |
| 21 | 2.54 | 2.55 | 2.57 | 2.58 | 2.59 | 2.60 | 2.61 | 2.63 | 2.64 | 2.65 |
| 22 | 2.66 | 2.68 | 2.69 | 2.70 | 2.71 | 2.72 | 2.73 | 2.75 | 2.76 | 2.77 |
| 23 | 2.78 | 2.80 | 2.81 | 2.82 | 2.83 | 2.84 | 2.86 | 2.87 | 2.88 | 2.89 |
| 24 | 2.91 | 2.92 | 2.93 | 2.94 | 2.95 | 2.97 | 2.98 | 2.99 | 3.00 | 8.01 |
| 25 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 | 3.09 | 3.10 | 3.11 | 3.12 | 3.14 |
| 26 | 3.15 | 3.16 | 3.17 | 3.18 | 3.20 | 3.21 | 3.22 | 3.23 | 3.24 | 3.26 |
| 27 | 3.27 | 3.28 | 3.29 | 3.30 | 3.32 | 3.33 | 3.34 | 3.35 | 3.37 | 3.38 |
| 28 | 3.39 | 3.40 | 3.41 | 3.43 | 3.44 | 3.4.5 | 3.46 | 3.47 | 3.49 | 3.50 |
| 29 | 3.51 | 3.52 | 3.54 | 3.55 | 3.56 | 3.57 | 3.58 | 3.60 | 3.61 | 3.62 |
| 30 | 3.63 | 3.64 | 3.66 | 3.67 | 3.68 | 3.69 | 3.70 | 3.72 | 3.73 | 3.74 |
| 31 | 3.75 | 3.76 | 3.78 | 3.79 | 3.80 | 3.81 | 3.83 | 3.84 | 3.85 | 3.86 |
| 32 | 3.57 | 3.59 | 3.90 | 3.94 | 3.92 | 3.93 | 3.95 | 3.96 | 3.97 | 3.98 |
| 33 | 3.99 | 4.01 | 4.02 | 4.03 | 4.04 | 4.06 | 4.07 | 4.08 | 4.09 | 4.10 |
| 34 | 4.12 | 4.13 | 4.14 | 4.15 | 4.16 | 4.18 | 4.19 | 4.20 | 4.21 | 4.22 |
| 35 | 4.24 | 4.25 | 4.26 | 4.27 | 4.29 | 4.30 | 4.31 | 4.32 | 4.33 | 4.35 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |



| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROME'TER : $760{ }^{\text {mm. }}$ ( from 757.51 to 762.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Mıllim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Mıllim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Mıllim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.12 | 0.13 | 0.15 | 0.16 | 0.17 | 0.18 | 0.20 | 0.21 | 0.22 | 0.23 |
| 2 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 | 0.33 | 0.34 | 0.36 |
| 3 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 |
| 4 | 0.49 | 0.50 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.60 |
| 5 | 0.61 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.69 | 0.70 | 0.71 | 0.72 |
| 6 | 0.74 | 0.75 | 0.76 | 0.77 | 0.79 | 0.80 | 0.81 | 0.82 | 0.83 | 0.85 |
| 7 | 0.86 | 0.87 | 0.88 | 0.90 | 0.91 | 0.92 | 0.93 | 0.94 | 0.96 | 0.97 |
| 8 | 0.98 | 0.99 | 1.01 | 1.02 | 1.03 | 1.04 | 1.05 | 1.07 | 1.08 | 1.09 |
| 9 | 1.10 | 1.12 | 1.13 | 1.14 | 1.15 | 1.17 | 1.18 | 1.19 | 1.20 | 1.21 |
| 10 | 1.23 | 1.24 | 1.25 | 1.26 | 1.28 | 1.29 | 1.30 | 1.31 | 1.32 | 1.34 |
| 11 | 1.35 | 1.36 | 1.37 | 1.39 | 1.40 | 1.41 | 1.42 | 1.44 | 1.45 | 1.46 |
| 12 | 1.47 | 1.48 | 1.50 | 1.51 | 1.52 | 1.53 | 1.55 | 1.56 | 1.57 | 1.58 |
| 13 | 1.59 | 1.61 | 1.62 | 1.63 | 1.64 | 1.66 | 1.67 | 1.68 | 1.69 | 1.71 |
| 14 | 1.72 | 1.73 | 1.74 | 1.75 | 1.77 | 1.78 | 1.79 | 1.50 | 1.82 | 1.83 |
| 15 | 1.84 | 1.85 | 1.56 | 1.88 | 1.89 | 1.90 | 1.91 | 1.93 | 1.94 | 1.95 |
| 16 | 1.96 | 1.97 | 1.99 | 2.00 | 2.01 | 2.02 | 2.04 | 2.05 | 2.06 | 2.07 |
| 17 | 2.09 | 2.10 | 2.11 | 2.12 | 2.13 | 2.15 | 2.16 | 2.17 | 2.18 | 2.20 |
| 18 | 2.21 | 2.22 | 2.23 | 2.24 | 2.26 | 2.27 | 2.28 | 2.29 | 2.31 | 2.32 |
| 19 | 2.33 | 2.34 | 2.36 | 2.37 | 2.38 | 2.39 | 2.40 | 2.42 | 2.43 | 2.44 |
| 20 | 2.45 | 2.47 | 2.48 | 2.49 | 2.50 | 2.51 | 2.53 | 2.54 | 2.55 | 2.56 |
| 21 | 2.58 | 2.59 | 2.60 | 2.61 | 2.63 | 2.64 | 2.65 | 2.66 | 2.67 | 2.69 |
| 22 | 2.70 | 2.71 | 2.72 | 2.74 | 2.75 | 2.76 | 2.77 | 2.78 | 2.80 | 2.81 |
| 23 | 2.92 | 2.83 | 2.85 | 2.86 | 2.87 | 2.88 | 2.89 | 2.91 | 2.92 | 2.93 |
| 24 | 2.94 | 2.96 | 2.97 | 2.98 | 2.99 | 3.01 | 3.02 | 3.03 | 3.04 | 3.05 |
| 25 | 3.07 | 3.08 | 3.09 | 3.10 | 3.12 | 3.13 | 3.14 | 3.15 | 3.16 | 3.18 |
| 26 | 3.19 | 3.20 , | 3.21 | 3.23 | 3.24 | 3.25 | 3.26 | 3.28 | 3.29 | 3.30 |
| 27 | 3.31 | $3 \cdot 32$ | 3.34 | 3.35 | 3.36 | 3.37 | 3.39 | 3.40 | 3.41 | 3.42 |
| 28 | 3.43 | $3 \cdot 45$ | 3.46 | 3.47 | 3.48 | 3.50 | 3.51 | 3.52 | 3.53 | 3.54 |
| 29 | 3.56 | 3.57 | 3.58 | 3.59 | 3.61 | 3.62 | 3.63 | 3.64 | 3.66 | S.67 |
| 30 | 3.68 | 3.69 | 3.70 | 3.72 | 3.73 | 3.74 | 3.75 | 3.77 | 3.78 | 3.79 |
| 31 | 3.80 | 3.81 | 3.83 | 3.84 | 3.85 | 3.86 | 3.88 | 3.59 | 3.90 | 3.91 |
| 32 | 3.93 | 3.94 | 3.95 | 3.96 | 3.97 | 3.99 | 4.00 | 4.01 | 4.02 | 4.04 |
| 33 | 4.05 | 4.06 | 4.07 | 4.08 | 4.10 | 4.11 | 4.12 | 4.13 | 4.15 | 4.16 |
| 34 | 4.17 | $4 \cdot 18$ | 4.20 | 4.21 | 4.22 | 4.23 | 4.24 | 4.26 | 4.27 | 4.28 |
| 35 | 4.29 | 4.31 | 4.32 | 4.33 | 4.34 | 4.35 | 4.37 | 4.35 | 4.39 | 4.40 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : 765 ${ }^{\text {mm. }}$ (from 762.51 to 76750 ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{array}{\|c} \hline \text { Millim. } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millım. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.11 \end{gathered}$ |
| 1 | 0.12 | 0.14 | 0.15 | 0.16 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 | 0.23 |
| 2 | 0.25 | 0.26 | 0.27 | 0.25 | 0.30 | 0.31 | 0.32 | 0.33 | 0.35 | 0.36 |
| 3 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.43 | 0.44 | 0.46 | 0.47 | 0.48 |
| 4 | 0.49 | 0.51 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.58 | 0.59 | 0.61 |
| 5 | 0.62 | 0.63 | 0.64 | 0.65 | 0.67 | 0.68 | 0.69 | 0.70 | 0.72 | 0.73 |
| 6 | 0.74 | 0.75 | 0.77 | 0.78 | 0.79 | 0.80 | 0.82 | 0.53 | 0.84 | 0.85 |
| 7 | 0.86 | 0.88 | 0.89 | 0.90 | 0.91 | 0.93 | 09.4 | 0.95 | 0.96 | 0.98 |
| 8 | 0.99 | 1.00 | 1.01 | 1.02 | 1.04 | 1.05 | 1.06 | 1.07 | 1.09 | 1.10 |
| 9 | 1.11 | 1.12 | 1.14 | 1.15 | 1.16 | 1.17 | 1.19 | 1.20 | 1.21 | 1.22 |
| 10 | 1.23 | 1.25 | 1.26 | 1.27 | 1.28 | 1.30 | 1.31 | 1.32 | 1.33 | 1.35 |
| 11 | 1.36 | 1.37 | 1.38 | 1.40 | 1.41 | 1.42 | 1.43 | 1.4 | 1.46 | 1.47 |
| 12 | 1.48 | 1.49 | 1.51 | 1.52 | 1.53 | 1.54 | 1.56 | 1.57 | 1.58 | 1.59 |
| 13 | 1.61 | 1.62 | 1.63 | 1.64 | 1.65 | 1.67 | 1.65 | 1.69 | 1.70 | 1.72 |
| 14 | 1.73 | 1.74 | 1.75 | 1.77 | 1.78 | 1.79 | 1.50 | 1.82 | 1.83 | 1.54 |
| 15 | 1.85 | 1.86 | 1.88 | 1.89 | 1.90 | 1.91 | 1.93 | 1.94 | 195 | 1.96 |
| 16 | 1.98 | 1.99 | 2.00 | 2.01 | 2.02 | 2.04 | 2.05 | 2.06 | 2.07 | 2.09 |
| 17 | 2.10 | 2.11 | 2.12 | 2.14 | 2.15 | 2.16 | 2.17 | 2.19 | 2.20 | 2.21 |
| 18 | 2.22 | 2.23 | 2.25 | 2.26 | 2.27 | 2.28 | 2.30 | 2.31 | 2.32 | 2.33 |
| 19 | 2.35 | 2.36 | 2.37 | 2.38 | 2.10 | 2.41 | 2.42 | 2.43 | 2.44 | 2.46 |
| 20 | 2.47 | 2.18 | 2.49 | 2.51 | 2.52 | 2.53 | 2.54 | 2.56 | 2.57 | 2.58 |
| 21 | 2.59 | 2.61 | 2.62 | 2.63 | 2.64 | 2.65 | 2.67 | 2.68 | 2.69 | 2.70 |
| 22 | 2.72 | 2.73 | 2.74 | 2.75 | 2.77 | 2.78 | 2.79 | 2.80 | 2.82 | 2.83 |
| 23 | 2.84 | 2.85 | 2.86 | 2.88 | 2.89 | 2.90 | 2.91 | 2.93 | 2.94 | 2.95 |
| 24 | 2.96 | 2.98 | 2.99 | 3.00 | 3.01 | 3.03 | 3.04 | 3.05 | 3.06 | 3.07 |
| 25 | 3.09 | 3.10 | 3.11 | 3.12 | 3.14 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 |
| 26 | 3.21 | 3.22 | 3.23 | 3.25 | 3.26 | 3.27 | 3.28 | 3.30 | 3.31 | 3.32 |
| 27 | 3.33 | 3.35 | 3.36 | 3.37 | 3.38 | 3.40 | 3.41 | 3.42 | 3.43 | 3.44 |
| 28 | 3.46 | 3.47 | 3.48 | 3.49 | 3.51 | 3.52 | 3.53 | 3.54 | 3.56 | 3.57 |
| 29 | 3.58 | 3.59 | 3.61 | 3.62 | 3.63 | 3.64 | 3.65 | 3.67 | 3.68 | 3.69 |
| 30 | 3.70 | 3.72 | 3.73 | 3.74 | 3.75 | 3.77 | 3.78 | 3.79 | 3.50 | 3.82 |
| 31 | 3.83 | 3.84 | 3.85 | 3.86 | 3.88 | 389 | 3.90 | 3.91 | 3.93 | 3.94 |
| 32 | 3.95 | 3.96 | 3.98 | 3.99 | 4.00 | 4.01 | 4.03 | 4.04 | 4.05 | 4.06 |
| 33 | 4.07 | 4.09 | 4.10 | 4.11 | 4.12 | 4.14 | 4.15 | 4.16 | 4.17 | 4.19 |
| 34 | 4.20 | 4.21 | 4.22 | 4.24 | 4.25 | 4.26 | 4.27 | 4.28 | 4.30 | 4.31 |
| 35 | 4.32 | 4.33 | 4.35 | 4.36 | 4.37 | 4.38 | 4.40 | 4.41 | 4.42 | 4.43 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| C |  |  |  |  | 114 |  |  |  |  |  |


| Centigrade Degrees | BAROME'ГER : $770^{\mathrm{mm}}$ ( from 767.51 to $77 \mathbf{2} .50$ ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.02 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.07 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.12 | 0.14 | 0.15 | 0.16 | 0.17 | 0.19 | 0.20 | 0.21 | 0.22 | 0.24 |
| 2 | 0.25 | 0.26 | 0.27 | 0.29 | 0.30 | 0.31 | 0.32 | 0.34 | 0.35 | 0.36 |
| 3 | 0.37 | 0.39 | 0.40 | 0.41 | 0.42 | 0.43 | 0.45 | 0.46 | 0.47 | 0.48 |
| 4 | 0.50 | 0.51 | 0.52 | 0.53 | 0.55 | 0.56 | 0.57 | 0.58 | 0.60 | 0.61 |
| 5 | 0.62 | 0.63 | 0.65 | 0.66 | 0.67 | 0.68 | 0.70 | 0.71 | 0.72 | 0.73 |
| 6 | 0.75 | 0.76 | 0.77 | 0.78 | 0.50 | 0.81 | 0.82 | 0.53 | 0.85 | 0.86 |
| 7 | 0.87 | 0.58 | 0.89 | 0.91 | 0.92 | 0.93 | 0.94 | 0.96 | 0.97 | 0.98 |
| 8 | 0.99 | 1.01 | 1.02 | 1.03 | 1.04 | 1.06 | 1.07 | 1.08 | 1.09 | 1.11 |
| 9 | 1.12 | 1.13 | 1.14 | 1.16 | 1.17 | 1.18 | 1.19 | 1.21 | 1.22 | 1.23 |
| 10 | 1.24 | 1.26 | 1.27 | 1.28 | 1.29 | 1.30 | 1.32 | 1.33 | 1.34 | 1.35 |
| 11 | 1.37 | 1.38 | 1.39 | 1.40 | 1.42 | 1.43 | 1.44 | 1.45 | 1.47 | 1.48 |
| 12 | 1.49 | 1.50 | 1.52 | 1.53 | 1.54 | 1.55 | 1.57 | 1.58 | 1.59 | 1.60 |
| 13 | 1.62 | 1.63 | 1.64 | 1.65 | 1.67 | 1.68 | 1.69 | 1.70 | 1.72 | 1.73 |
| 14 | 1.74 | 1.75 | 1.76 | 1.78 | 1.79 | 1.80 | 1.81 | 1.83 | 1.84 | 1.55 |
| 15 | 1.86 | 1.88 | 1.89 | 1.90 | 1.91 | 1.93 | 1.94 | 1.95 | 1.96 | 1.98 |
| 16 | 1.99 | 2.00 | 2.01 | 2.03 | 2.04 | 2.05 | 2.06 | 2.08 | 2.09 | 2.10 |
| 17 | 2.11 | 2.13 | 2.14 | 2.15 | 2.16 | 2.17 | 2.19 | 2.20 | 2.21 | 2.22 |
| 18 | 2.24 | 2.25 | 2.26 | 2.27 | 2.29 | 2.30 | 2.31 | 2.32 | 2.34 | 2.35 |
| 19 | 2.36 | 2.37 | 2.39 | 2.40 | 2.41 | 2.42 | 2.44 | 2.45 | 2.46 | 2.47 |
| 20 | 2.49 | 2.50 | 2.51 | 2.52 | 2.54 | 2.55 | 2.56 | 2.57 | 2.58 | 2.60 |
| 21 | 2.61 | 2.62 | 2.63 | 2.65 | 2.66 | 2.67 | 2.68 | 2.70 | 2.71 | 2.72 |
| 22 | 2.73 | 2.75 | 2.76 | 2.77 | 2.78 | 2.80 | 2.81 | 2.82 | 2.83 | 2.85 |
| 23 | 2.86 | 2.87 | 2.88 | 2.90 | 2.91 | 2.92 | 2.93 | 2.95 | 2.96 | 2.97 |
| 24 | 2.98 | 3.00 | 3.01 | 3.02 | 3.03 | 3.04 | 3.06 | 3.07 | 3.08 | 3.09 |
| 25 | 3.11 | 3.12 | 3.13 | 3.14 | 3.16 | 3.17 | 3.18 | 3.19 | 3.21 | 3.22 |
| 26 | 3.23 | 3.24 | 3.26 | 3.27 | 3.28 | 3.29 | 3.31 | 3.32 | 3.33 | 3.34 |
| 27 | 3.36 | 3.37 | 3.38 | 3.39 | 3.41 | 3.42 | 3.43 | 3.44 | 3.45 | 3.47 |
| 28 | 3.48 | 3.49 | 3.50 | 3.52 | 3.53 | 3.54 | 3.55 | 3.57 | 3.58 | 3.59 |
| 29 | 3.60 | 3.62 | 3.63 | 3.64 | 3.65 | 3.67 | 3.68 | 3.69 | 3.70 | 3.72 |
| 30 | 3.73 | 3.74 | 3.75 | 3.77 | 3.78 | 3.79 | 3.50 | 3.82 | 3.53 | 3.8 .4 |
| 31 | 3.85 | 3.87 | 3.88 | 3.89 | 3.90 | 3.91 | 3.93 | 3.94 | 3.95 | 3.96 |
| 32 | 3.98 | 3.99 | 4.00 | 4.01 | 4.03 | 4.04 | 4.05 | 4.06 | 4.08 | 4.09 |
| 33 | 4.10 | 4.11 | 4.13 | 4.14 | 4.15 | 4.16 | 4.18 | 4.19 | 4.20 | 4.21 |
| 34 | 4.23 | 4.24 | 4.25 | 4.26 | 4.28 | 4.29 | 4.30 | 4.31 | 4.32 | 4.34 |
| 35 | 4.35 | 4.36 | 4.37 | 4.39 | 4.40 | 4.41 | 4.42 | 4.44 | 4.45 | 4.46 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centigrade Degrees. | BAROMETER : $775^{\text {mm. }}$ ( from 772.51 to 777.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | Millim. 0.03 | $\begin{gathered} \text { Millim. } \\ 0.0 .4 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.05 \end{gathered}$ | Millim. 0.06 | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.13 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 |
| 2 | 0.25 | 0.26 | 0.28 | 0.29 | 0.30 | 0.31 | 0.33 | 0.3.1 | 0.35 | 0.36 |
| 3 | 0.38 | 0.39 | 0.40 | 0.41 | 0.43 | 0.44 | 0.45 | 0.16 | 0.48 | 0.49 |
| 4 | 0.50 | 0.51 | 0.53 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.60 | 0.61 |
| 5 | 0.63 | 0.64 | 0.65 | 0.66 | 0.68 | 0.69 | 0.70 | 0.71 | 0.73 | 0.74 |
| 6 | 0.75 | 0.76 | 0.78 | 0.79 | 0.80 | 0.81 | 0.83 | 0.84 | 0.85 | 0.86 |
| 7 | 0.88 | 0.89 | 0.90 | 0.91 | 0.93 | 0.94 | 0.95 | 0.96 | 0.98 | 0.99 |
| 8 | 1.00 | 1.01 | 1.03 | 1.04 | 1.05 | 1.06 | 1.09 | 1.09 | 1.10 | 1.11 |
| 9 | 1.13 | 1.14 | 1.15 | 1.16 | 1.18 | 1.19 | 1.20 | 1.21 | 1.23 | 1.24 |
| 10 | 1.25 | 1.26 | 1.28 | 1.29 | 1.30 | 1.31 | 1.33 | 1.34 | 1.35 | 1.36 |
| 11 | 1.38 | 1.39 | 1.40 | 1.41 | 1.43 | 1.44 | 1.45 | 1.46 | 1.48 | 1.49 |
| 12 | 1.50 | 1.51 | 1.53 | 1.54 | 1.55 | 1.56 | 1.58 | 1.59 | 1.60 | 1.61 |
| 13 | 1.63 | 1.64 | 1.65 | 1.66 | 1.68 | 1.69 | 1.70 | 1.71 | 1.73 | 1.74 |
| 14 | 1.75 | 1.76 | 1.78 | 1.79 | 1.50 | 1.81 | 1.83 | 1.84 | 1.85 | 1.86 |
| 15 | 1.88 | 1.89 | 1.90 | 1.91 | 1.93 | 1.94 | 1.95 | 1.96 | 1.98 | 1.99 |
| 16 | 2.00 | 2.01 | 2.03 | 2.04 | 2.05 | 2.06 | 2.08 | 2.09 | 2.10 | 2.11 |
| 17 | 2.13 | 2.14 | 2.15 | 2.16 | 2.18 | 2.19 | 2.20 | 2.21 | 2.23 | 2.24 |
| 18 | 2.25 | 2.26 | 2.98 | 2.29 | 2.30 | 2.31 | 2.33 | 2.34 | 2.35 | 2.36 |
| 19 | 2.38 | 2.39 | 2.40 | 2.41 | 2.43 | 2.44 | 2.45 | 2.46 | 2.48 | 2.49 |
| 20 | 2.50 | 2.51 | 2.53 | 2.54 | 2.55 | 2.56 | 2.58 | 2.59 | 2.60 | 2.61 |
| 21 | 2.63 | 2.64 | 2.65 | 2.66 | 2.68 | 2.69 | 2.70 | 2.71 | 2.73 | 2.74 |
| 22 | 2.75 | 2.76 | 2.78 | 2.79 | 2.80 | 2.81 | 2.83 | 2.84 | 2.85 | 2.86 |
| 23 | 2.58 | 2.89 | 2.90 | 2.91 | 2.93 | 2.94 | 2.95 | 2.96 | 2.98 | 2.99 |
| 24 | 3.00 | 3.01 | 3.03 | 3.04 | 3.05 | 3.06 | 3.08 | 3.09 | 3.10 | 3.11 |
| 25 | 3.13 | 3.14 | 3.15 | 3.16 | 3.18 | 3.19 | 3.20 | 3.21 | 3.23 | 3.24 |
| 26 | 3.25 | S. 26 | 3.28 | 3.29 | 3.30 | 3.31 | 3.33 | 3.34 | 3.35 | 3.36 |
| 27 | 3.38 | 3.39 | 3.40 | 3.41 | 3.43 | 3.44 | 3.45 | 3.46 | 3.48 | 3.49 |
| 28 | 3.50 | 3.51 | 3.53 | 3.54 | 3.55 | 3.56 | 3.58 | 3.59 | 3.60 | 3.61 |
| 29 | 3.63 | 3.64 | 3.65 | 3.66 | 3.68 | 3.69 | 3.70 | 3.72 | 3.73 | 3.74 |
| 30 | 3.75 | 3.77 | 3.78 | 3.79 | 3.80 | 3.82 | 3.83 | 3.84 | 3.85 | 3.87 |
| 31 | 3.88 | 3.89 | 3.90 | 3.92 | 3.93 | 3.94 | 3.95 | 3.97 | 3.98 | 3.99 |
| 32 | 4.00 | 4.02 | 4.03 | 4.04 | 4.05 | 4.07 | 4.08 | 4.09 | 4.10 | 4.12 |
| 33 | 4.13 | 4.14 | 4.15 | 4.17 | 4.18 | 4.19 | 4.20 | 4.22 | 4.23 | 4.24 |
| 34 | 4.25 | 4.27 | 4.28 | 4.29 | 4.30 | 4.32 | 4.33 | 4.34 | 4.35 | 4.37 |
| 35 | 4.38 | 4.39 | 4.40 | 4.42 | 4.43 | 4.44 | 4.45 | 4.47 | 4.48 | 4.49 |
|  | (1). | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| $\begin{gathered} \text { Centi- } \\ \text { grade } \\ \text { Degrees. } \end{gathered}$ | BAROMETER : $780{ }^{\mathrm{mm} .}$ (from 777.51 to 782.50 ) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.01 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~s} \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.13 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.21 | 0.23 | 0.24 |
| 2 | 0.25 | 0.26 | 0.25 | 0.29 | 0.30 | 0.31 | 0.33 | 0.34 | 0.3.) | 0.37 |
| 3 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 | 0.45 | 0.47 | 0.48 | 0.49 |
| 4 | 0.50 | 0.52 | 0.53 | 0.54 | 0.55 | 0.57 | 0.58 | 0.59 | 0.60 | 0.62 |
| 5 | 0.63 | 0.64 | 0.65 | 0.67 | 0.68 | 0.69 | 0.70 | 0.72 | 0.73 | 0.74 |
| 6 | 0.76 | 0.77 | 0.78 | 0.79 | 0.81 | 0.82 | 0.83 | 0.84 | 0.86 | 0.87 |
| 7 | $0 . \varepsilon$ | 0.89 | 0.91 | 0.92 | 0.93 | 0.94 | 0.96 | 0.97 | 0.98 | 0.99 |
| 8 | 1.01 | 1.02 | 1.03 | 1.0 t | 1.06 | 1.07 | 1.08 | 1.10 | 1.11 | 1.12 |
| 9 | 1.13 | 1.15 | 1.16 | 1.17 | 1.18 | 1.20 | 1.21 | 1.22 | 1.23 | 1.2.) |
| 10 | 1.26 | 1.27 | 1.28 | 1.30 | 1.31 | 1.32 | 1.33 | 1.35 | 1.36 | 1.37 |
| 11 | 1.38 | 1.40 | 1.41 | 1.42 | 1.44 | 1.45 | 1.46 | 1.47 | 1.49 | 1.50 |
| 12 | 1.51 | 1.52 | 1.54 | 1.55 | 1.56 | 1.57 | 1.59 | 1.60 | 1.61 | 1.62 |
| 13 | 1.64 | 1.65 | 1.66 | 1.67 | 1.69 | 1.70 | 1.71 | 1.72 | 1.74 | 1.75 |
| 14 | 1.76 | 1.78 | 1.79 | 1.80 | 1.81 | 1.83 | 1.84 | 1.85 | 1.56 | 1.88 |
| 15 | 1.89 | 1.90 | 1.91 | 1.93 | 1.94 | 1.95 | 1.96 | 1.98 | 1.99 | 2.00 |
| 16 | 2.01 | 2.03 | 2.04 | 2.05 | 2.06 | 2.08 | 2.09 | 2.10 | 2.11 | 2.13 |
| 17 | 2.14 | 2.15 | 2.17 | 2.18 | 2.19 | 2.20 | 2.22 | 2.23 | 2.24 | 2.25 |
| 18 | 2.27 | 2.28 | 2.29 | 2.30 | 2.32 | 2.33 | 2.34 | 2.35 | 2.37 | 2.38 |
| 19 | 2.39 | 2.40 | 2.42 | 2.43 | 2.44 | 2.45 | 2.47 | 2.48 | 2.49 | 2.51 |
| 20 | 2.52 | 2.53 | 2.54 | 2.56 | 2.57 | 2.58 | 2.59 | 2.61 | 2.62 | 2.63 |
| 21 | 2.64 | 2.66 | 2.67 | 2.68 | 2.69 | 2.71 | 2.72 | 2.73 | 2.74 | 2.76 |
| 22 | 2.77 | 2.78 | 2.79 | 2.81 | 2.82 | 2.83 | 2.85 | 2.86 | 2.57 | 2.88 |
| 23 | 2.90 | 2.91 | 2.92 | 2.93 | 2.95 | 2.96 | 2.97 | 2.98 | 3.00 | 3.01 |
| 24 | 3.02 | 3.03 | 3.05 | 3.06 | 3.07 | 3.08 | 3.10 | 3.11 | 3.12 | 3.14 |
| 25 | 3.15 | 3.16 | 3.17 | 3.19 | 3.20 | 3.21 | 3.22 | 3.24 | 3.25 | 3.26 |
| 26 | 3.27 | 3.29 | 3.30 | 3.31 | 3.32 | 3.34 | 3.35 | 3.36 | 3.37 | 3.39 |
| 27 | 3.40 | 3.41 | 3.42 | 3.44 | 3.45 | 3.46 | 3.47 | 3.49 | 3.50 | 3.51 |
| 28 | 3.52 | 3.54 | 3.55 | 3.56 | 3.58 | 3.59 | 3.60 | 3.61 | 3.63 | 3.64 |
| 29 | 3.65 | 3.66 | 3.68 | 3.69 | 3.70 | 3.71 | 3.73 | 3.74 | 3.75 | 5.76 |
| 30 | 3.78 | 3.79 | 3.80 | 3.81 | 3.83 | 3.84 | 3.85 | 3.86 | 3.88 | 3.59 |
| 31 | 3.90 | 3.92 | 3.93 | 3.94 | 3.95 | 3.97 | 3.98 | 3.99 | 4.00 | 4.02 |
| 32 | 4.03 | 4.04 | 4.05 | 4.07 | 4.08 | 4.09 | 4.10 | 4.12 | 4.13 | 4.14 |
| 33 | 4.15 | 4.17 | 4.18 | 4.19 | 4.20 | 4.22 | 4.23 | 4.24 | 4.26 | 4.27 |
| 34 | 4.28 | 4.29 | 4.31 | 4.32 | 4.33 | 4.34 | 4.36 | 4.37 | 4.38 | 4.39 |
| 35 | 4.41 | 4.42 | 4.43 | 4.44 | 4.46 | 4.47 | 4.48 | 4.49 | 4.51 | 4.52 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. |  | 8. | 9. |


| $\left\lvert\, \begin{gathered} \text { Centi } \\ \text { grade } \\ \text { Degrees. } \end{gathered}\right.$ | BAROMETER : $785{ }^{\text {mm. }}$ ( from 782.51 to 787.50 ) . |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Tenths of | Degrees. |  |  |  |  |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Millhm. } \\ 0.00 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.01 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.03 \end{gathered}$ | $\begin{aligned} & \text { Mıllim. } \\ & 0.04 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.05 \end{gathered}$ | $\begin{array}{\|c} \hline \text { Millim. } \\ 0.06 \end{array}$ | $\begin{gathered} \text { Millim. } \\ 0.0 \mathrm{~s} \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.13 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.22 | 0.23 | 0.24 |
| 2 | 0.25 | 0.27 | 0.28 | 0.29 | 0.30 | 0.32 | 0.33 | 0.34 | 0.35 | 0.37 |
| 3 | 0.38 | 0.39 | 0.41 | 0.42 | 0.43 | 0.44 | 0.46 | 0.47 | 0.48 | 0.49 |
| 4 | 0.51 | 0.52 | 0.53 | 0.54 | 0.56 | 0.57 | 0.58 | 0.60 | 0.61 | 0.62 |
| 5 | 0.63 | 0.65 | 0.66 | 0.67 | 0.68 | 0.70 | 0.71 | 0.72 | 0.73 | 0.75 |
| 6 | 0.76 | 0.77 | 0.79 | 0.50 | 0.81 | 0.82 | 0.84 | 0.85 | 0.86 | 0.87 |
| 7 | 0.89 | 0.90 | 0.91 | 0.92 | 0.94 | 0.95 | 0.96 | 0.98 | 0.99 | 1.00 |
| 8 | 1.01 | 1.03 | 1.04 | 1.05 | 1.06 | 1.05 | 1.09 | 1.10 | 1.11 | 1.13 |
| 9 | 1.11 | 1.15 | 1.17 | 1.18 | 1.19 | 1.20 | 1.22 | 1.23 | 1.24 | 1.25 |
| 10 | 1.27 | 1.28 | 1.29 | 1.30 | 1.32 | 1.33 | 1.34 | 1.36 | 1.37 | 1.38 |
| 11 | 1.39 | 1.41 | 1.42 | 1.43 | 1.44 | 1.46 | 1.47 | 1.48 | 1.50 | 1.51 |
| 12 | 1.52 | 1.53 | 1.55 | 1.56 | 1.57 | 1.58 | 1.60 | 1.61 | 1.62 | 1.63 |
| 13 | 1.65 | 1.66 | 1.67 | 1.69 | 1.70 | 1.71 | 1.72 | 1.74 | 1.75 | 1.76 |
| 14 | 1.77 | 1.79 | 1.80 | 1.81 | 1.82 | 1.84 | 1.85 | 1.86 | 1.88 | 1.89 |
| 15 | 1.90 | 1.91 | 1.93 | 1.94 | 1.95 | 1.96 | 1.98 | 1.99 | 2.00 | 2.01 |
| 16 | 2.03 | 2.04 | 2.05 | 2.07 | 2.08 | 2.09 | 2.10 | 2.12 | 2.13 | 2.14 |
| 17 | 2.15 | 2.17 | 2.18 | 2.19 | 2.20 | 2.22 | 2.23 | 2.24 | 2.26 | 2.27 |
| 18 | 2.28 | 2.29 | 2.31 | 2.32 | 2.33 | 2.34 | 2.36 | 2.37 | 2.38 | 2.39 |
| 19 | 2.11 | 2.42 | 2.43 | 2.45 | 2.46 | 2.47 | 2.48 | 2.50 | 2.51 | 2.52 |
| 20 | 2.53 | 2.55 | 2.56 | 2.57 | 2.58 | 2.60 | 2.61 | 2.62 | 2.64 | 2.65 |
| 21 | 2.66 | 2.67 | 2.69 | 2.70 | 2.71 | 2.72 | 2.74 | 2.75 | 2.76 | 2.77 |
| 22 | 2.79 | 2.80 | 2.81 | 2.83 | 2.84 | 2.85 | 2.86 | 2.88 | 2.89 | 2.90 |
| 23 | 2.91 | 2.93 | 2.94 | 2.95 | 2.96 | 2.98 | 2.99 | 3.00 | 3.02 | 3.03 |
| 24 | 3.04 | 3.05 | 307 | 3.08 | 3.09 | 3.10 | 3.12 | 3.13 | 3.14 | 3.15 |
| 25 | 3.17 | 3.18 | 3.19 | 3.21 | 3.22 | 3.23 | 3.24 | 3.26 | 3.27 | 3.28 |
| 26 | 3.29 | 3.31 | 3.32 | 3.33 | 3.34 | 3.36 | 3.37 | 3.38 | 3.40 | 3.41 |
| 27 | 3.12 | 3.43 | 3.45 | 3.46 | 3.47 | 3.48 | 3.50 | 351 | 3.52 | 3.53 |
| 28 | 3.5.) | 3.56 | 3.57 | 3.59 | 3.60 | 3.61 | 3.62 | 3.64 | 3.65 | 3.66 |
| 29 | 3.67 | 3.69 | 3.70 | 3.71 | 3.72 | 3.74 | 3.7.) | 3.76 | 3.78 | 3.79 |
| 30 | 3.80 | 3.81 | 3.83 | 3.84 | 3.85 | 3.86 | 3.88 | 3.89 | 3.90 | 3.91 |
| 31 | 3.93 | 3.94 | 3.95 | 3.97 | 3.98 | 3.99 | 4.00 | 4.02 | 4.03 | 4.04 |
| 32 | 4.05 | 4.07 | 4.09 | 4.09 | 4.11 | 4.12 | 4.13 | 4.14 | 4.16 | 4.17 |
| 33 | 4.15 | 4.19 | 4.21 | 4.22 | 4.23 | 4.24 | 4.26 | 4.27 | 4.28 | 4.30 |
| 34 | 4.31 | 4.32 | 4.33 | 4.35 | 4.36 | 4.37 | 4.35 | 4.40 | 4.41 | 4.42 |
| 35 | 4.43 | 4.45 | 4.46 | 4.17 | 4.49 | 4.50 | 4.51 | 4.52 | 4.54 | 4.55 |
|  | ©. | 1. | 2. | 3. | 4. | 3. | 6. | 7 | 8. | 9. |


| $\begin{array}{\|c\|} \text { Centi- } \\ \text { grate } \\ \text { Degrees. } \end{array}$ | BAROMETER : 790 ${ }^{\text {mm. }}$ (from 787.51 to 792.50). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tenths of Degrees. |  |  |  |  |  |  |  |  |  |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $\begin{gathered} \text { Mıllim. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { M1llim. } \\ 0.01 \end{gathered}$ | $\begin{aligned} & \text { Millim. } \\ & 0.03 \end{aligned}$ | $\begin{gathered} \text { Millim. } \\ 0.04 \end{gathered}$ | $\begin{gathered} \text { Millim } \\ 0.05 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.08 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.09 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.10 \end{gathered}$ | $\begin{gathered} \text { Millim. } \\ 0.11 \end{gathered}$ |
| 1 | 0.13 | 0.14 | 0.15 | 0.17 | 0.18 | 0.19 | 0.20 | 0.22 | 0.23 | 0.24 |
| 2 | 0.26 | 0.27 | 0.28 | 0.29 | 0.31 | 0.32 | 0.33 | 0.34 | 0.36 | 0.37 |
| 3 | 0.38 | 0.10 | 0.41 | 0.42 | 0.43 | 0.45 | 0.46 | 0.47 | 0.48 | 0.50 |
| 4 | 0.51 | 0.52 | 0.54 | 0.55 | 0.56 | 0.57 | 0.59 | 0.60 | 0.61 | 0.62 |
| 5 | 0.64 | 0.65 | 0.66 | 0.68 | 0.69 | 0.70 | 0.71 | 0.73 | 0.74 | 0.75 |
| 6 | 0.77 | 0.78 | 0.79 | 0.80 | 0.82 | 0.83 | 0.84 | 0.85 | 0.87 | 0.98 |
| 7 | 0.89 | 0.91 | 0.92 | 0.93 | 0.94 | 0.96 | 0.97 | 0.98 | 0.99 | 1.01 |
| 8 | 1.02 | 1.03 | 1.05 | 1.06 | 1.07 | 1.08 | 1.10 | 1.11 | 1.12 | 1.13 |
| 9 | 1.15 | 1.16 | 1.17 | 1.19 | 1.20 | 1.21 | 1.22 | 1.24 | 1.25 | 1.26 |
| 10 | 1.28 | 1.29 | 1.30 | 1.31 | 1.33 | 1.34 | 1.35 | 1.36 | 1.38 | 1.39 |
| 11 | 1.40 | 1.42 | 1.43 | 1.44 | 1.45 | 1.47 | 1.48 | 1.49 | 1.50 | 1.52 |
| 12 | 1.53 | 1.54 | 1.56 | 1.57 | 1.58 | 1.59 | 1.61 | 1.62 | 1.63 | 1.64 |
| 13 | 1.66 | 1.67 | 1.68 | 1.70 | 1.71 | 1.72 | 1.73 | 1.75 | 1.76 | 1.77 |
| 14 | 1.79 | 1.80 | 1.81 | 1.82 | 1.84 | 1.85 | 1.86 | 1.87 | 1.89 | 1.90 |
| 15 | 1.91 | 1.93 | 1.94 | 1.95 | 1.96 | 1.98 | 1.99 | 2.00 | 2.01 | 2.03 |
| 16 | 2.04 | 2.05 | 2.07 | 2.08 | 2.09 | 2.10 | 2.12 | 2.13 | 2.14 | 2.15 |
| 17 | 2.17 | 2.18 | 2.19 | 2.21 | 2.22 | 2.23 | 2.24 | 2.26 | 2.27 | 2.28 |
| 18 | 2.30 | 2.31 | 2.32 | 2.33 | 2.35 | 2.36 | 2.37 | 238 | 2.40 | 2.41 |
| 19 | 2.42 | 2.44 | 2.45 | 2.46 | 2.47 | 2.49 | 2.50 | 2.51 | 2.52 | 2.54 |
| 20 | 2.55 | 2.56 | 2.58 | 2.59 | 2.60 | 2.61 | 2.63 | 2.64 | 2.65 | 2.66 |
| 21 | 2.68 | 2.69 | 2.70 | 2.72 | 2.73 | 2.74 | 2.75 | 2.77 | 2.78 | 2.79 |
| 22 | 2.81 | 2.82 | 2.83 | 2.84 | 2.86 | 2.87 | 2.88 | 2.89 | 2.91 | 2.92 |
| 23 | 2.93 | 2.95 | 2.96 | 2.97 | 2.98 | 3.00 | 3.01 | 3.02 | 3.03 | 3.05 |
| 24 | 3.06 | 3.07 | 3.09 | 3.10 | 3.11 | 3.12 | 3.14 | 3.15 | 3.16 | 3.17 |
| 25 | 3.19 | 3.20 | 3.21 | 3.23 | 3.24 | 3.25 | 3.26 | 3.28 | 3.29 | 3.30 |
| 26 | 3.32 | 333 | 3.34 | 3.35 | 3.37 | 3.38 | 3.39 | 3.40 | 3.42 | 3.43 |
| 27 | 3.44 | 3.46 | 3.47 | 3.48 | 3.49 | 3.51 | 3.52 | 3.53 | 3.54 | 3.56 |
| 28 | 3.55 | 3.58 | 3.60 | 3.61 | 3.62 | 3.63 | 3.6 .5 | 3.66 | 3.67 | 3.68 |
| 29 | 3.70 | 3.71 | 3.72 | 3.74 | 3.75 | 3.76 | 3.77 | 3.79 | 3.80 | 3.81 |
| 30 | 3.83 | 3.84 | 3.85 | 3.86 | 3.88 | 3.89 | 3.90 | 3.91 | 3.93 | 3.94 |
| 31 | 3.95 | 3.97 | 3.98 | 3.99 | 4.00 | 4.02 | 4.03 | 4.04 | 4.05 | 4.07 |
| 32 | 4.08 | 4.09 | 4.11 | 4.12 | 4.13 | 4.14 | 4.16 | 4.17 | 4.18 | 4.19 |
| 33 | 4.21 | 4.22 | 4.23 | 4.25 | 4.26 | 4.27 | 4.28 | 4.30 | 4.31 | 4.32 |
| 34 | 4.34 | 4.35 | 436 | 4.37 | 4.39 | 4.40 | 4.41 | 4.42 | 4.44 | 4.45 |
| 35 | 4.46 | 4.48 | 4.49 | 4.50 | 4.51 | 4.53 | 4.54 | 4.55 | 4.56 | 4.58 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 4. |
| C |  |  |  |  | 119 |  |  |  |  |  |




## XXI.

## OLD FRENCH BAROMETER.

## T A B L E

FOR
reducing to the freezing point the observations taken with old frencif baroneters,

PROVIDED WITH BRASS SCALES, EXTENDING FROM THE CISTERN TO THE TOP OF THE MERCURIAL COLUMN; CALCULATED FROM 240 TO 345 LiNES, OR FROM 23 INCHES 4 LINES TO 28 inches 9 Lines. By Kaemtz.

## TABLE XYI

This table is taken from Kaemrz's Lehrbuch der Meteorologie, Vol. II. p. 236. To render it more useful, the first page, giving the corrections for Barometrical Heights between 210 and 280 Paris lines, has been added.
The values adopted by Kaemtz for reducing the Old French Barometer are the following: -

Let $h=$ observed height in French lines.
" $t=$ temperature of attached thermometer in degrees of Reaumur.
" $m=$ expansion of mercury between 0 and $80^{\circ}$ Reaumur $=0.018018$.
" $l=$ linear expansion of brass between 0 and $80^{\circ}$ Reaumur $=0.0018782$.
The normal temperature of standard being $=13^{\circ}$ Reaumur.
And the formula becomes, -

$$
-h \cdot \frac{m \times t-l(t-13)}{1+m \times t}
$$

The Table gives the corrections only for full degrees and for every fifth line; but the intermediate values can easily be found by an interpolation at sight.

## Example of Rerluction.

Observed height . . . . . . $=395.32$ lines.
Attached thermometer . . . . . $=12.5$ Ie aumur.
In the line beginning with $12^{\circ}$, and in the vertical column headed 325 ines,
we find, $\quad$ Correction for $1 \mathfrak{Z}^{\circ}=-0.89$ lines.
Interpolation for $0^{\circ} .5=-0.03 \quad$ "
Correction for $1 \beth^{\circ} .5=-0.92$ "
And we have,


Height at the freezing point $=324.40$ lines.

Normal Temperature of the Scale $=130$ Reaumur.

| Attached <br> Thermometer. <br> Degrees of Reaumur. | Barometer in Paris Lines. |  |  |  |  |  |  |  | Attached <br> Thermometer. <br> Degrees ot Reacmur. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 240 | 245 | 2.50 | 255 | 260 | 265 | 270 | 275 |  |
| 0 | Par. Lines. | Par Lines. | Par. Lines. | Par Lines. | Par. Lines. | Par. Lines | Par. Lines. | Par. Lines | $\bigcirc$ |
| -15 | +0.65 | +0.66 | +0.68 | +0.69 | +0.70 | $+0.72$ | +0.73 | $+0.75$ | -15 |
| -14 | 0.60 | 0.61 | 0.63 | 0.64 | 0.65 | 0.67 | 0.68 | 0.69 | -14 |
| -13 | 0.55 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.64 | -13 |
| -12 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | -12 |
| -11 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.52 | -11 |
| -10 | 0.41 | 0.42 | 0.43 | 0.44 | 0.44 | 0.45 | 0.46 | 0.47 | -10 |
| $-9$ | +0.36 | +0.37 | +0.38 | +0.33 | $+0.39$ | +0.40 | +0.41 | +0.41 | -9 |
| -8 | 0.31 | 0.32 | 0.33 | 0.33 | 0.34 | 0.35 | 0.35 | 0.36 | -8 |
| $-7$ | 0.27 | 0.27 | 0.28 | 0.23 | 0.29 | 0.29 | 0.30 | 0.30 | $-7$ |
| $-6$ | 0.22 | 0.22 | 0.23 | 0.23 | 0.24 | 0.24 | 0.24 | 0.25 | -6 |
| - 5 | 0.17 | 0.17 | 0.18 | 0.18 | 0.18 | 0.19 | 0.19 | 0.19 | -5 |
| - 4 | +0.12 | +0.12 | +0.13 | +0.13 | +0.13 | +0.13 | +0.14 | +0.14 | -4 |
| - 3 | 0.07 | 0.07 | 0.08 | 0.08 | 0.08 | 0.03 | 0.08 | 0.08 | - 3 |
| - 2 | +0.02 | +0.03 | +0.03 | +0.03 | $+0.03$ | +0.03 | +0.03 | +0.03 | - 2 |
| - 1 | -0.02 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -1 |
| 0 | -0.07 | -0.07 | -0.08 | -0.03 | -0.03 | -0.08 | -0.08 | -0.08 | 0 |
| +1 | -0.12 | -0.12 | -0.13 | -0.13 | -0.13 | -0.13 | -0.14 | -0.14 | +1 |
| 2 | 0.17 | 0.17 | 0.18 | 0.18 | 0.18 | 0.19 | 0.19 | 0.19 | 2 |
| 3 | 0.22 | 0.22 | 0.23 | 0.23 | 0.24 | 0.24 | 0.24 | 0.25 | 3 |
| 4 | 0.27 | 0.27 | 0.28 | 0.25 | 0.29 | 0.29 | 0.30 | 0.30 | 4 |
| 5 | 0.31 | 0.32 | 0.33 | 0.33 | 0.34 | 0.35 | 0.35 | 0.36 | 5 |
| $+6$ | -0.36 | -0.37 | -0.38 | -0.38 | -0.39 | -0.40 | -0.41 | -0.41 | $+6$ |
| 7 | 0.41 | 0.42 | 0.43 | 0.44 | 0.44 | 0.45 | 0.46 | 0.47 | 7 |
| 8 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.52 | 8 |
| 9 | 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 9 |
| 10 | 0.55 | 0.57 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.64 | 10 |
| $+11$ | -0.60 | -0.61 | -0.63 | -0.64 | -0.65 | -0.67 | -0.68 | -0.69 | $+11$ |
| 12 | 0.65 | 0.66 | 0.68 | 0.69 | 0.70 | 0.72 | 0.73 | 0.75 | 12 |
| 13 | 0.70 | 0.71 | 0.73 | 0.74 | 0.76 | 0.77 | 0.79 | 0.80 | 13 |
| 14 | 0.75 | 0.76 | 0.78 | 0.79 | 0.81 | 0.82 | 0.84 | 0.86 | 14 |
| 15 | 0.80 | 0.81 | 0.83 | 0.84 | 0.86 | 0.53 | 0.89 | 0.91 | 15 |
| +16 | -0.84 | -0.86 | -0.88 | -0.90 | -0.91 | -0.93 | -0.95 | -0.97 | +16 |
| 17 | 0.89 | 0.91 | 0.93 | 0.95 | 0.97 | 0.98 | 1.00 | 1.02 | 17 |
| 18 | 0.94 | 0.96 | 0.98 | 1.00 | 1.02 | 1.04 | 1.06 | 1.08 | 18 |
| 19 | 0.99 | 1.01 | 1.03 | 1.05 | 1.07 | 1.09 | 1.11 | 1.13 | 19 |
| 20 | 1.04 | 1.06 | 1.08 | 1.10 | 1.12 | 1.14 | 1.17 | 1.19 | 20 |
| +21 | -1.08 | -1.11 | -1.13 | -1.15 | -1.17 | -I. 20 | -1.22 | -1.24 | +21 |
| 22 | 1.13 | 1.16 | 1.18 | 1.20 | 1.23 | 1.25 | 1.27 | 1.30 | 22 |
| 23 | 1.18 | 1.20 | 1.23 | 1.25 | 1.28 | 1.30 | 1.33 | 1.35 | 23 |
| 24 | 1.23 | 1.25 | 1.28 | 1.31 | 1.33 | 1.36 | 1.38 | 1.41 | 24 |
| 25 | 1.28 | 1.30 | 1.33 | 1.36 | 1.38 | 1.41 | 1.44 | 1.46 | 25 |

Normal Temperature of the Scale $=13^{\circ}$ Reaumur.

| Attached Thermometer. <br> Degrees of Reaumir. | Barmmeter in Paris Lines. |  |  |  |  |  |  | Attached Thermom. eter. <br> Degrees of Reaumur. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 280 | 28.5 | 290 | 295 | 300 | 305 | 310 |  |
| $\begin{array}{r} 0 \\ -15 \end{array}$ | $\begin{gathered} \text { Par Lin } \stackrel{s}{ } . \\ +0.77 \end{gathered}$ | $\begin{gathered} \text { Par. Lines. } \\ +0.78 \end{gathered}$ | Par. Lines. $+0.79$ | Par Lines. $+0.81$ | Par. Lines. $+0.82$ | Par. Lines. $+0.84$ | Par. Lides. $+0.85$ | $-15$ |
| -14 | 0.71 | 073 | 0.74 | 0.75 | 0.76 | 0.77 | 0.79 | -14 |
| -13 | 0.65 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | -13 |
| -12 | 0.60 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | -12 |
| -11 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | -11 |
| $-10$ | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.54 | $-10$ |
| $-9$ | $+0.43$ | +0.44 | +0.44 | $+0.45$ | $+0.46$ | $+0.46$ | $+0.47$ | $-9$ |
| $-8$ | 0.37 | 0.38 | 0.38 | 0.39 | 0.40 | 0.40 | 0.41 | -8 |
| $-7$ | 0.31 | 0.32 | 0.32 | 0.33 | 0.34 | 0.34 | 0.35 | $-7$ |
| $-6$ | 0.26 | 0.26 | 0.26 | 0.27 | 0.27 | 0.28 | 0.28 | $-6$ |
| $-5$ | 0.20 | 0.20 | 0.21 | 0.21 | 0.21 | 0.22 | 0.22 | $-5$ |
| $-4$ | +0.14 | $+0.15$ | $+0.15$ | $+0.15$ | $+0.15$ | +0.16 | +0.16 | $-4$ |
| -3 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | $-3$ |
| $-2$ | $+0.03$ | $+0.03$ | $+0.03$ | $+0.03$ | $+0.03$ | +0.03 | $+0.03$ | $-2$ |
| $-1$ | -0.03 | -0.03 | $-0.03$ | $-0.03$ | -0.03 | -0.03 | -0.03 | $-1$ |
| 0 | $-0.08$ | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | -0.09 | 0 |
| $+1$ | $-0.14$ | -0.14 | $-0.15$ | $-0.15$ | -0.15 | -0.15 | -0.16 | $+1$ |
| 2 | 0.20 | 0.20 | 0.21 | 0.21 | 0.21 | 0.22 | 0.22 | 2 |
| 3 | 0.26 | 0.26 | 0.27 | 0.27 | 0.27 | 0.28 | 0.28 | 3 |
| 4 | 0.31 | 0.32 | 0.32 | 0.33 | 0.33 | 0.34 | 0.35 | 4 |
| 5 | 0.37 | 0.37 | 0.38 | 0.39 | 0.40 | 0.40 | 0.41 | 5 |
| $+6$ | $-0.43$ | $-0.43$ | $-0.44$ | $-0.45$ | $-0.46$ | $-0.46$ | -0.47 | $\pm 6$ |
| 7 | 0.48 | 0.49 | 0.50 | 0.51 | 0.52 | 0.53 | 0.53 | 7 |
| 8 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 8 |
| 9 | 0.60 | 0.61 | 0.62 | 0.63 | 064 | 0.65 | 0.66 | 9 |
| 10 | 0.65 | 0.66 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 10 |
| +11 | $-0.71$ | $-0.72$ | -0.74 | $-0.75$ | $-0.76$ | $-0.77$ | -0.79 | +11 |
| 12 | 0.77 | 0.78 | 0.80 | 0.81 | 0.82 | 0.84 | 0.85 | 12 |
| 13 | 0.52 | 0.84 | 0.85 | 0.57 | 0.88 | 0.90 | 0.91 | 13 |
| 14 | 0.88 | 0.90 | 0.91 | 0.93 | 0.94 | 0.96 | 0.98 | 14 |
| 15 | 0.94 | 0.95 | 0.97 | 0.99 | 1.00 | 1.02 | 1.0t | 15 |
| $+16$ | -0.99 | -1.01 | -1.03 | -1.05 | -1.07 | -1.08 | -1.10 | +16 |
| 17 | 1.05 | 1.07 | 1.09 | 1.11 | 1.13 | 1.15 | 1.16 | 17 |
| 18 | 1.11 | 1.13 | 1.15 | 1.17 | 1.19 | 1.21 | 1.23 | 18 |
| 19 | 1.16 | 1.18 | 1.21 | 1.23 | 1.25 | 1.27 | 1.29 | 19 |
| 20 | 1.22 | 1.24 | 1.27 | 1.29 | 1.31 | 1.33 | 1.35 | 20 |
| +21 | -1.28 | $-1.30$ | -1.33 | -1.35 | -1.37 | -1.39 | -1.42 | +21 |
| 22 | 1.34 | 1.36 | 1.38 | 1.41 | 1.43 | 1.45 | 1.48 | 22 |
| 23 | 1.39 | 1.41 | 1.44 | 1.47 | 1.49 | 1.52 | 1.54 | 23 |
| 24 | 1.45 | 1.47 | 1.50 | 1.53 | 1.55 | 1.58 | 1.60 | 24 |
| 25 | 1.50 | 1.53 | 1.56 | 1.59 | 1.61 | 1.64 | 1.67 | 25 |

Normal Temperature of the Scale $=13^{\circ}$ Reaumur.

| Attached <br> Thermom. eter. <br> Degrees of Reaumur. | Barometer in Paris Lines. |  |  |  |  |  |  | Attacherl <br> Thermometer. <br> Degrees of Reaumur |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 315 | 320 | 325 | 330 | 335 | 340 | 315 |  |
| 15 | Par. Lines. +0.86 | Par, Lines, $+0.88$ | $\begin{gathered} \text { Par. Lines. } \\ +0.59 \end{gathered}$ | Par. Lines. $+0.90$ | Par. Lines. $+0.92$ | Par. Lines. $+0.93$ | Par. Lines. $+0.9 .5$ | $\begin{array}{r} 5 \\ -15 \end{array}$ |
| -14 | 0.80 | 081 | 0.83 | 0.54 | 0.85 | 0.56 | 0.88 | -14 |
| -13 | 0.74 | 0.75 | 0.76 | 0.78 | 0.78 | 0.79 | 0.81 | -13 |
| -12 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.73 | 0.74 | -12 |
| -11 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | -11 |
| -10 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | -10 |
| -9 | +0.18 | +0.49 | +0.50 | $+0.50$ | +0.51 | +0.52 | +0.53 | -9 |
| -8 | 0.42 | 0.42 | 0.43 | 0.41 | 0.44 | 0.45 | 0.46 | -8 |
| $-7$ | 0.35 | 0.36 | 0.36 | 0.37 | 0.37 | 0.38 | 0.39 | - 7 |
| - 6 | 0.29 | 0.29 | 0.30 | 0.30 | 0.31 | 0.31 | 0.32 | - 6 |
| $-5$ | 0.22 | 0.23 | 0.23 | 0.24 | 0.24 | 0.24 | 0.25 | - 5 |
| $-4$ | +0.16 | +0.16 | $\pm 0.17$ | $+0.17$ | +017 | $+0.17$ | +0.18 | - 1 |
| -3 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.11 | - 3 |
| - 2 | +0.03 | $\pm 0.03$ | $+0.03$ | - 0.03 | $+0.03$ | +0.03 | $+0.04$ | -2 |
| -1 | -0.03 | -0.03 | $-0.03$ | -0.03 | -0.03 | -0.03 | -0.03 | - 1 |
| 0 | -0.10 | -0.10 | $-0.10$ | -0.10 | -0.10 | -0.10 | -0.10 | 0 |
| +1 | -0.16 | -0.16 | $-0.16$ | -0.17 | -0.17 | -0.17 | -0.17 | $+1$ |
| 2 | 0.22 | 0.23 | 0.23 | 0.23 | 0.24 | 0.24 | 0.24 | 2 |
| 3 | 0.29 | 0.29 | 0.30 | 0.30 | 0.31 | 0.31 | 0.31 | 3 |
| 4 | 0.35 | 0.36 | 0.36 | 0.37 | 0.37 | 0.38 | 0.35 | 4 |
| 5 | 0.42 | 0.42 | 0.43 | 0.4 | 0.44 | 0.45 | 0.45 | 5 |
| $+6$ | -0.48 | -0.49 | -0.49 | -0.50 | -0.51 | -0.52 | -0.53 | $+6$ |
| 7 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 | 7 |
| 8 | 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 8 |
| 9 | 0.67 | 0.68 | 0.69 | 0.70 | 0.71 | 0.72 | 0.74 | 9 |
| 10 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.81 | 10 |
| +11 | -0.80 | -0.81 | -0.82 | -0.84 | -0.85 | -0.86 | -0.88 | +11 |
| 12 | 0.86 | 0.88 | 0.59 | 0.90 | 0.92 | 0.93 | 0.95 | 12 |
| 13 | 0.93 | 0.94 | 0.96 | 0.97 | 0.99 | 1.00 | 1.02 | 13 |
| 14 | 0.99 | 1.01 | 1.02 | 1.04 | 1.0.5 | 1.07 | 1.09 | 14 |
| 15 | 1.05 | 1.07 | 1.09 | 1.10 | 1.12 | 1.14 | 1.16 | 15 |
| +16 | -1.12 | -1.14 | -1.15 | -1.17 | -1.19 | -1.21 | -1.23 | $+16$ |
| $17^{4}$ | 1.18 | 1.20 | 1.22 | 1.24 | 1.26 | 1.25 | 1.30 | 17 |
| 18 | 1.25 | 1.27 | 1.29 | 1.31 | 1.33 | 1.35 | 1.37 | 18 |
| 19 | 1.31 | 1.33 | 135 | 1.37 | 1.39 | 1.41 | 1.44 | 19 |
| 20 | 1.37 | 1.40 | 1.42 | $\therefore$ 2.: | 1.46 | 1.48 | 1.51 | 20 |
| +21 | -1.44 | -1.46 | $-1.48$ | -1.51 | $-1.53$ | -1.55 | -1.58 | +21 |
| 22 | 1.50 | 1.53 | 1.55 | 1.57 | 1.60 | 1.62 | 1.65 | 22 |
| 23 | 1.57 | 1.59 | 1.62 | 1.64 | 1.67 | 1.69 | 1.72 | 23 |
| 24 | 1.63 | 1.66 | 1.68 | 1.71 | 1.73 | 1.76 | 1.79 | 24 |
| 25 | 1.69 | 1.72 | 1.75 | 1.78 | 1.80 | 1.83 | 1.56 | 25 |

## TABLES

## FOR CORRECTING THE

DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

## CORRECTION FOR CAPILLARY ACTION.

Ir is known that the effects of capillary action are not the same in different liquids. In a tube plunged in water, the liquid in the tube rises higher than the level of the water in the vessel, and terminates by a concave surface, which is called a concare meniscus. In a tube plunged in mercury the liquid in the tube stands lower than the mercury in the vessel, and terminates by a convex surface, or a convex meniscus. It is thus evident that the mereurial column in the tube of a Barometer does not rise to its true height, and that it needs to be corrected for the depression due to capillarity, before it indicates the real pressure of the atmosphere.

La Place, in the Mécanique Céleste, Tom. IV., has shown that the value of that correction depends upon the form of the meniscus, and gave a formula to compute it. As this form varies in tubes of different bores, so does the depression, which diminishes as the diameter of the tube increases. The form of the meniscus, however, was supposed to be the same in tubes of the same diameter, and constant in the same tube; and on this supposition the tables generally used for correcting the capiltary action have been computed. But more accurate observations have proved that, owing to various causes not yet all well understood, the form of the meniscus is often different in tubes of the same diameter, and that it is even variable in the tube of the same instrument.

It thus became necessary to construct new tables, taking into consideration, in a given case, both the diameter of the tube and the form of the meniscus. Such tables, with a double entry, have been given by Schleiermacher, in the Bibliothèque Universelle de Genève, Tom. VIII.; by Bravais, in the Amatcs de Physique et de Chimie, Tom. V. p. 508 ; and by Delcros. The numbers in these tables agree very closely; but as Delcros's table is more extended than that of Schleirmacher, and in a more convenient form than that of Bravais, it is given below, together with a reduction of it to English measures, for the ordinary use.

The other tables may serve for comparison.
Table XXII., from the Report of the Committee of Physics and Meteorology of the Royal Society of London, 1840 , gives the correction to be applied to English barometers for capillary action in boiled and momiled tubes. It takes into account the diameter of the tube, but not the variations of the height of the meniscus, or of the convexity which terminates the barometrical column. This last element is supposed to be in its normal state, and constant.

Tables XXIII. and XXIV., by Deleros, in the Annnaire Météorologique de France, for 1849, give the means of finding the true correction to be applied to metrical barometers for capillary action.

The first shows the normal height of the meniscus when in contact with the air (as is the case in the inferior branch of a siphon barometer), and in the barometric vacuum at the top of the column, in tubes of different bores. It enables the observer to judge better of its variations.

Table XXIV. has been calculated by Delcros after the formulas of Schleiermacher, making the constant $x$ equal to $6^{n m m} .5278$, being the mean value between that of GayLussac $=6^{m \mathrm{~m} .} .5262$, and that of Schleiermacher $=6^{\mathrm{mm} .} .5295$. It gives the amount of the capillary action in millimetres of mercury, taking into account both the size of the bore, or the internal radius of the tube, which will be found in the vertical argument, and the height of the meniscus, given in the horizontal argument. The internal radius of the tube is supposed to be known; the height of the meniscus, or the vertical distance from the base, that is, from the sharp line where the mercury ceases to be in contact with the walls of the tube, to the very top of the convexity, can be ascertained by measuring it several times by means of the vernier.

Example: - Suppose the internal radius of the tube to be $3{ }^{\mathrm{mm} .} .2$, and the height of the meniscus to be $0^{\mathrm{mm}} .8$; seek in the first vertical column the number $3^{\mathrm{mm}} .2$; follow then the horizontal line as far as the vertical column headed $0^{m \mathrm{~m} .} .8$, you find there the number $0^{\mathrm{mm} .776}$, which is the amount of the depression due to capillary action, or the value of the correction to be added to the observation.

Table XXV. is taken from Pouillet's Eléments de Physique, Vol. II. p. 698 (1853).
Table XXVI. is found in Gehter's Physicalisches Wörterbuch, and in Schubarth, Physicalische Tabellen, p. 21.

Table XXVII., which is Deleros's table reduced into English measures, gives the means of correcting with more accuracy the indications of the English barometers. For its use, see, above, the explanation to Table XXIV.

Table XXVIII. is from Baily's Astronomical Tables.
XXII. Table for the Correction to be added to Englisil Baroneters for Capillary Action.

| Diameter <br> of Tube. | Correction for |  |
| :---: | :---: | :---: |
|  | Unhoiled <br> Tubes. | Boiled <br> Tubes. |
|  | Inch. | Inch. |
| 0.60 | 0.004 | 0.002 |
| 0.50 | 0.007 | 0.003 |
| 0.45 | 0.010 | 0.005 |
| 0.40 | 0.014 | 0.007 |
| 0.35 | 0.020 | 0.010 |
| 0.30 | 0.023 | 0.014 |
| 0.25 | 0.040 | 0.020 |
| 0.20 | 0.060 | 0.029 |
| 0.15 | 0.083 | 0.044 |
| 0.10 | 0.142 | 0.070 |

XXIII. Table of the Meight of tee Meniscus of the Baronetrical Colume.


131

|  |  |  |  | $\begin{array}{lccc} 0 \text { N } \\ \infty & \infty \\ \infty & \infty \\ \hline \end{array}$ |  | $09+\infty \infty$ <br>  | $0 \omega+\infty \infty$ － 0000 | $\bigcirc$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| － | 0 | $\text { 刍 }=:=\approx=$ | $z=7 \pm y$ | \＃$=$ こ | z $=$ z |  |  | $\stackrel{9}{6}$ |
|  | ＊ |  | $\pm \pm=5$ | $z=\therefore=\begin{aligned} & \infty \\ & \infty \\ & 0\end{aligned}$ |  |  |  | $\infty$ <br> 0 <br> 0 |
|  | ${ }^{*}$ | $\text { 寄 }=:=\approx=$ |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  | 구오요 ล61～ー $00000$ | a1 $\stackrel{12}{0}$ 0 |
|  | 18 |  | $\pm \pm \pm \pm$ |  | $\begin{aligned} & \infty 10 \\ & 0 \\ & 0 \\ & 10 \\ & 10 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned} 0$ |  |  | $\stackrel{10}{7}$ |
|  | － | $\text { 要 }=:==$ | $=\Xi=\overrightarrow{2}$ |  |  |  |  | $\stackrel{\infty}{\infty}$ |
|  | 0 | $\left\lvert\, \frac{\dot{\Xi}}{\underset{\Xi}{\Xi}}=:=\div\right.$ | $==\underset{\sim}{6}$ | $\begin{aligned} & 9.0 .80 \\ & N=0 \\ & =1000 \\ & -1000 \end{aligned}$ |  |  |  | $\stackrel{9}{9}$ |
|  | 0 |  | $==$ |  |  |  |  | $\stackrel{1}{1}$ $\stackrel{1}{0}$ 0 |
|  |  | 离 $=:=$ | $=\begin{aligned} & n \\ & \infty \\ & \infty \\ & 0 \\ & \cdots \end{aligned}$ |  | $\begin{aligned} & \text { H. } \\ & \text { N } \\ & 0 \end{aligned}$ |  |  | Ј Ј |
|  |  |  |  |  |  |  |  | $\stackrel{12}{8}$ $\stackrel{-1}{0}$ |
|  | － | $\text { 音 }=:==\begin{gathered} \text { GU } \\ \text { GU } \\ \text { Gi } \end{gathered}$ |  | $\begin{aligned} & 1210 \\ & 10 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned} 0$ |  |  | $\underset{6}{6} \underset{6}{6} \underset{6}{0}$ | 10 8 8 0 |
|  | e |  |  | $\begin{array}{llll} 0 & 0 & 10 & 8 \\ 0 & 1 & 1 \\ 0 & 0 & 10 & 0 \\ 0 & 0 & 0 \end{array}$ |  |  |  | 10 0 8 0 |
|  |  |  |  | $\begin{array}{llll} 8 & -7 & \\ 0 & 0 \\ 0 & 0 \\ 0 & 10 \\ 0 & 0 & 0 \end{array}$ | $\begin{aligned} & \overrightarrow{0} \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ |  |  | 10 0 0 0 |
|  | $\bigcirc$ |  |  | $\begin{array}{llll} \infty & 10 & 10 & 0 \\ 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 \end{array}$ | $\begin{array}{llll} 9 & 0 & 0 & 19 \\ 10 & 12 \\ 0 & 61 \\ 0 & 61 \\ 0 & 0 & 0 \\ 0 \end{array}$ |  |  | $\xrightarrow{10}$ |
|  | 18 |  |  |  |  | $\begin{aligned} & \overrightarrow{6}=\frac{\infty}{6} \\ & \hdashline-0 \\ & 0 \\ & 0 \end{aligned}$ |  | 10 10 0 0 |
|  | 3 |  |  |  |  | $\begin{aligned} & 0 \\ & =9 \\ & \vdots=0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  | 7 <br>  <br> 0 |
|  | 6 |  |  |  |  | $\begin{aligned} & \infty 10 \\ & =0 \\ & 60 \\ & 0 \\ & 0 \\ & 0 \end{aligned} 0=0$ |  | $\stackrel{¢}{\text { ®ิ }}$ |
|  | 0 |  |  |  |  |  |  | 11 0 0 0 |
|  | $\cdots$ |  |  |  | $\begin{array}{lll} 0 & 1 \\ 6 & 1 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 \end{array}$ |  | $\begin{aligned} & 9 \\ & -0 \\ & 0 \\ & 0 \end{aligned} \frac{120}{0} 00$ | O |
|  |  | - |  | $\begin{array}{lll} 0 & \infty \\ \Leftrightarrow<\infty & \infty \\ \infty \end{array}$ | $\begin{gathered} 0 \\ \dot{\sim}+\underset{j}{+}+\infty \\ \rightarrow+i \end{gathered}$ |  | ف | $\bigcirc$ |

C
XXV. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

From Pouillet.

| Internal Diameter of Tube. | Depression | Differences. | Internal Diameter of Tube. | Depression. | Differences. | Internal Diameter of Tube | Depression. | Differences |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Millimetres. | Millimetres. | Millimet. | Millimetres. | Millimetres. | Millimet. | Millimetres. | Nillimetres. | Millimet. |
| 2.00 | 4.579 |  | 8.50 | 0.604 |  | 15.00 | 0.127 |  |
| 2.50 | 3.595 | 0.985 | 9.00 | 0.534 | 0.070 | 15.50 | 0.112 | 0.015 |
|  |  | 0.692 |  |  | 0.06 I | 16.00 | 0.099 | 0.013 |
| 3.00 | 2.902 | 0.487 | 9.50 | 0.473 | 0.051 | 16.00 | 0.099 | 0.012 |
| 3.50 | 2.415 |  | 10.00 | 0.419 | 0.054 | 16.50 | 0.087 | 0.010 |
| 4.00 | 2.053 | 0.362 | 10.50 | 0.372 | 0.047 0.042 | 17.00 | 0.077 | 0.010 0.009 |
| 4.50 | 1.752 |  | 11.00 | 0.330 |  | 17.50 | 0.068 |  |
| 5.00 | 1.507 | 0.245 | 11.50 | 0.293 | 0.037 | 18.00 | 0.060 | 0.008 |
| 5.50 | 1.306 | 0.201 | 12.00 | 0.260 | 0.033 | 18.50 | 0.053 | 0.007 |
|  |  | 0.170 |  |  | 0.030 | 19.00 | 0.0 .17 | 0.006 |
| 6.00 | 1.136 | 0.141 | 12.50 | 0.230 | 0.026 | 19.00 | $0.0 \cdot 17$ | 0.006 |
| 6.50 | 0.995 | $0.118$ | 13.00 | 0.204 | 0.023 | 19.50 | 0.041 | 0.005 |
| 7.00 | 0.877 |  | 13.50 | 0.181 |  | 20.00 | 0.036 |  |
| 7.50 | 0.775 | 0.102 | 14.00 | 0.161 | 0.020 | 20.50 | 0.032 | 0.004 |
| 8.00 | 0.684 | 0.09 I | 14.50 | 0.143 | 0.018 | 21.00 | U.028 | 0.004 |
|  |  | 0.080 |  |  | 0.016 |  |  |  |

XXVI DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION.

| Internal Diameter of Tube. | Depression according to |  |  |  | Internal Diameter of Tube. | Depression according to |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | La Place | Young. | Ivory. | Cavendish. |  | La Place. | Young | Ivory. | Cavendish |
| Millimetres. $2.00$ | $\begin{aligned} & \text { Millim. } \\ & \mathbf{4 . 4 5 4} \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 4.587 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 4.888 \end{aligned}$ | $\begin{array}{r} \text { Millim. } \\ 4.472 \end{array}$ | Nillimetres. 11.50 | $\begin{gathered} \text { Millim. } \\ 0.315 \end{gathered}$ | Nillim. | Millim. | Nillim. |
| 2.50 | 3.568 |  |  |  | 12.00 | 0.281 | 0.242 | 0.253 | 0.200 |
| 3.00 | 2.918 | 2.986 | 2.988 | 3.054 | 12.50 | 0.250 |  |  |  |
| 3.50 | 2.442 |  |  |  | 13.00 | 0.223 | 0.188 | 0.196 | 0.170 |
| 4.00 | 2.068 | 2.063 | 2.066 | 2.187 | 13.50 | 0.198 |  |  |  |
| 4.50 | 1.774 |  |  |  | 14.00 | 0.176 | 0.144 | 0.15: | 0.150 |
| 5.00 | 1.534 | 1.510 | 1.513 | 1.735 | 14.50 | 0.156 |  |  |  |
| 5.50 | 1.337 |  |  |  | 15.00 | 0.137 | 0.111 | 0.118 | 0.131 |
| 6.00 | 1.171 | 1.139 | 1.134 | 1.377 | 15.50 | 0.121 |  |  |  |
| 6.50 | 1.030 |  |  |  | 16.00 | 0.107 | 0.088 | 0.087 |  |
| 7.00 | 0.909 | 0.869 | 0.868 | 1.073 | 16.50 | 0.094 |  |  |  |
| 7.50 | 0.803 |  |  |  | 17.00 | 0.083 | 0.068 | 0.071 |  |
| 8.00 | 0.712 | 0.669 | 0.673 | 0.820 | 17.50 | 0.073 |  |  |  |
| 8.50 | 0.632 |  |  |  | 18.00 | 0.064 | 0.053 | 0.054 |  |
| 9.00 | 0.562 | 0.517 | 0.521 | 0.608 | 18.50 | 0.056 |  |  |  |
| 9.50 | 0.500 |  |  |  | 19.00 | 0.049 | 0.041 | 0.042 |  |
| 10.00 | 0.445 | 0.402 | 0.406 | 0.406 | 19.50 | 0.043 |  |  |  |
| 10.50 | 0.397 |  |  |  | 20.00 | 0.038 | 0.031 | 0.031 |  |
| 11.00 | 0.354 | 0.311 | 0.316 | 0.270 | 20.50 | 0.034 |  |  |  |
| 11.50 | 0.815 |  |  |  | 21.00 | 0.030 | 0.024 | 0.024 |  |

XXVII. DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY ACTION, REDUCED INTO ENGLISH INCHES FROM DELCROS'S TABLE.

|  | Height of Meniscus in Thousandths of an English Inch. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tube. | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 |
| Eng. In. | Iuch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 0.10 | 0.040 | 0.076 | 0.109 | 0.136 | 0.155 |  |  |  |  |  |  |  |  |  |
| 0.12 | . 027 | . 053 | . 076 | . 097 | . 114 |  |  |  |  |  |  |  |  |  |
| 0.14 | . 019 | . 038 | . 036 | . 071 | .085 | 0.097 |  |  |  |  |  |  |  |  |
| 0.16 | . 015 | . 029 | . 042 | . 055 | . 066 | . 076 | 0.084 |  |  |  |  |  |  |  |
| 0.18 | . 011 | . 022 | . 033 | . 043 | . 052 | . 060 | . 067 | 0.073 |  |  |  |  |  |  |
| 0.20 | . 009 | . 018 | . 026 | . 034 | . 042 | . 049 | . 055 | . 060 | 0.064 |  |  |  |  |  |
| 0.22 | . 007 | . 014 | . 021 | . 028 | . 034 | . 040 | . 045 | . 049 | . 053 | 0.057 |  |  |  |  |
| 0.24 | . 006 | . 012 | . 017 | .023 | . 025 | . 033 | . 037 | . 041 | . 045 | . 048 | 0.050 |  |  |  |
| 0.26 | . 00.5 | . 010 | . 014 | . 019 | . 023 | . 027 | . 031 | . 035 | . 038 | . 040 | . 043 | 0.045 |  |  |
| 0.28 | . 004 | . 005 | . 012 | . 016 | . 019 | . 023 | . 026 | . 029 | . 032 | . 034 | . 036 | . 038 |  |  |
| 0.30 | . 003 | . 007 | . 010 | . 013 | . 016 | . 019 | . 022 | . 025 | . 027 | . 029 | . 031 | . 033 | 0.034 |  |
| 0.32 | . 003 | . 006 | . 009 | . 011 | . 014 | . 016 | . 019 | . 021 | . 023 | . 025 | . 027 | . 028 | . 030 |  |
| 0.34 | . 002 | .005 | . 007 | . 010 | . 012 | . 014 | . 016 | . 018 | . 020 | . 032 | .023 | . 024 | . 026 |  |
| 0.36 | . 002 | . 004 | . 006 | . 005 | . 010 | . 012 | . 014 | . 016 | . 017 | . 019 | . 020 | . 021 | .022 |  |
| 0.38 | . 002 | . 004 | . 005 | . 007 | . 009 | . 010 | . 012 | . 013 | . 015 | . 016 | . 017 | . 018 | . 019 |  |
| 0.40 | . 002 | . 003 | . 005 | . 006 | . 008 | . 009 | . 010 | . 012 | . 013 | . 014 | . 015 | . 016 | . 017 |  |
| 0.42 | . 001 | . 003 | . 004 | . 005 | . 007 | . 003 | . 009 | . 010 | . 011 | .012 | . 013 | . 014 | . 015 | 0.015 |
| 0.44 | . 001 | . 002 | . 004 | . 005 | . 006 | . 007 | . 008 | . 009 | . 010 | . 011 | . 011 | . 012 | . 013 | . 013 |
| 0.46 | . 001 | . 002 | . 003 | . 004 | . 005 | . 006 | . 007 | . 008 | . 008 | . 009 | . 010 | . 011 | . 011 | . 012 |
| 0.48 | . 001 | . 002 | . 003 | . 004 | . 004 | . 005 | . 006 | . 007 | . 007 | . 008 | . 009 | . 009 | . 010 | . 010 |
| 0.50 | . 001 | . 002 | . 002 | .003 | . 004 | . 004 | . 005 | . 006 | . 006 | . 007 | . 008 | . 008 | . 008 | . 009 |
| 0.52 | . 001 | . 001 | . 002 | .003 | . 003 | . 004 | . 005 | . 005 | . 006 | . 006 | . 007 | . 007 | . 007 | . 008 |
| 0.54 | . 001 | . 001 | . 002 | . 002 | . 003 | . 003 | . 004 | . 004 | . 005 | . 005 | . 006 | . 006 | . 006 | . 007 |
|  | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 5.5 | 60 | 65 | 70 |

XXVII: DEPRESSION OF THE BAROMETRICAL COLUMN DUE TO CAPILLARY action, expressed in english inches. - Baily.

| Diameter of Tube. | Depression according to |  |  | Diameter of Tube. | Depression according to |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ivory. | Young. | La Place. |  | Ivory. | Young. | La Place. |
| Eng. Inch. 0.05 | Eng. Inch. $0.2949$ | Eug. Inch. 0.2964 | $\begin{gathered} \text { Eng. Inch. } \\ 0 . \text {. . . } \end{gathered}$ | Eng. Inch. 0.35 | Eng Inch. $0.0212$ | Eng. Inch. $0.0196$ | Eng. Inch. $0.0216$ |
| 0.10 | . 1404 | . 1424 | .1394 | 0.10 | . 0154 | . 0139 | . 0159 |
| 0.15 | .0965 | . 0880 | .0554 | 0.45 | . 0112 | . 0100 | . 0117 |
| 0.20 | . 0.583 | . 0589 | .0550 | 0.50 | . 0082 | .0074 | . 0087 |
| 0.25 | . 0409 | . 0404 | . 0412 | 0.60 | . 0043 | . 0045 | . 0046 |
| 0.30 | . 0293 | . 0250 | . 0296 | 0.70 | . 0023 |  | . 0024 |
| 0.35 | 0.0212 | 0.0196 | 0.0216 | 0.50 | 0.0012 | 0... | 0.0013 |

# METE0R0L0GICAL TABLES 

sERIES IV.

HYPSOMETRICAL TABLES.

## C 0 NTENTS.

(The figures refer to the folio at the bottom of the page.)

## 1. Baronetrical Measurement of Heights.

Page
On the Tables and Formulæ ..... 7
Tables based on Laplace's Constants
Table I. Delcros' Tables, in Metrical Measures ..... 9
" II. Guyot's Tables, in English Measures ..... 31
" III. Loomis' Tables, in English Measures ..... 47
" IV. Gauss' Tables, modified by Dippe, Old French Measures ..... 52
" V. Dippe's Tables, for reducing Barometrical Observations to anotherLevel, and for computing Heights, Old French Measures58
" VI. Babinet's Modification of Laplace's Formula ..... 66
" VII. Baily's Tables, in English Measures ..... 67
Tables based on Bessel's Formula.
" VIII. Plantamour's Tables, in Metrical Measures ..... 70
Miscellaneous Tables." IX. Correction for the Hour of the Day at which the Observations havebeen taken, Coefficients by Berghaus78
" X. Correction for the Hour of the Day, Old French Measures ..... 79" XI. Correction to be applied to the Half-Sums of the Temperaturesobserved at Geneva and St. Bernard, and its Value in Metres atall Hours and Seasons of the Year, by Plantamour80
Computing Altitudes by the Height of the Barometer at the Sea- Level ..... 81
" XII. Mean Height of the Barometer at the Level of the Sea in various Latitudes ..... 83
" XIII. Mean Height of the Barometer in all Months of the Year ..... 84
" XIV. Mean Height of the Barometer at all Hours of the Day ..... 84
" XV. Tropic Hours of Daily Variation at Halle ..... 85
" XV'. Amplitude of Daily Variations in Various Latitudes ..... $8 \overline{5}$
Reducing the Barometer to the Level of the Sea ..... 86
" XVI. Height, in English Feet, of a Column of Air corresponding to a Tenth of an Inch in the Barometer ..... 87
" XVII. Height, in French Feet, of a Column of Air corresponding to a Paris Line in the Barometer ..... 87
Table XVIII. Height, in Metres, of a Column of Air corresponding to a Page
Millimetre in the Barometer . . . . . . .
" XIX. Height, in Metres, of a Column of Air corresponding to a Millimetre in the Barometer at different Temperatures and Elevations89
" $\mathrm{XIX}^{\prime}$. Height, in English Feet, of a Column of Air, corresponding to a Tenth of an Inch in the Barometer, at different Temperatures and Elevations . . . . . . . 90
" XX. Correction to be app!ied to the Means of the Hours of Observation to obtain the True Mean Barometical Pressure, Philadelphia 91
" XXI. Correction to be applied to the Means of the Hours of Observation to obtain the true Mean Barometrical Pressure, Greenwich 92
XXII. For reducing Minutes into Decimals of an Hour . . . 93
XXIII. Correction for Curvature and Refraction . . . . 94
2. Thermometrical Measurement of Heights.
" XXIV. Regnault's Barometric Pressures corresponding to the Temperature of Boiling Water
" XXV. Regnault's Barometric Pressures corresponding to the Temperature of Boiling Water, revised by Moritz, in Metrical Measures 102
" XXVI. Regnault's Barometric Pressures corresponding to the Temperature of Boiling Water, revised by Moritz, in English Measures 104

## BAR0METRICAL

# MEASUREMENT OF HEIGHTS, 

OR

TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

# IIYPSOMETRICAL TABLES 

FOR

## COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.

Numerous determinations of altitude are one of the great desiderata of physical science, and no more ready means for obtaining them is at the disposal of the seientifie man than the Barometer. A traveller, furnished with the improved and convenient instruments we can now command, and with some experience in using them, can take a large number of barometric observations for determining heights, at the cost of little trouble or time. It is, however, quite otherwise with the eomputations by which the results are obtained. The prospect of that tedious and time-robbing labor not only too often cools the zeal of the observer, but a vast amount of data aetually collected remain of no avail from the want of having been computed.

The object of this much enlarged set of Hypsometrical Tables is to facilitate the task of the computer. It contains practical tables adapted to the three usual barometrical scales, and, among them, No. I., II., and V. are so disposed as to dispense with the use of logarithms, and to reduce the computation to the simplest arithmetieal operations. The others suppose the use of logarithms, a method which may still be preferred by some observers.

As these various tables represent the development of the principal formulæ which have been proposed, the computer is enabled to compare the results obtained by each of them, and to select that which he most approves.

These formulæ may be referred to two classes, the respective types of which are Laplace's and Bessel's formulæ.

Laplace, in the Mécanique Céleste, Tom. IV. p. 292, gave a complete solution of the problem, and proposed a formula which soon superseded the older and less aceurate formulæ of De Lue, Shuckburgh, and others. The coefficients which enter in it were derived from the best determinations of the needed physical constants which science could then furnish, the most important of which are the relative weight of the air and of the mercury, and the rate of expansion of air by heat. The first was assumed to be ${ }_{\overline{10} \frac{1}{4} \overline{4} 7}$, according to the experiments of Biot and Arago; and the barometrical coefficient deduced from it, 18317 metres. This coefficient was, however, empirically increased to $\mathbf{1 8 3 3 6}$ metres, in order to adjust the results of the formula to those furnished by the careful trigonometrical measurements made by Ramond for the purpose of testing its correctness. It becomes 18393 metres when including the correction due to the effect of the decrease of gravity with the height on the density of the mereurial column and of the air. The coefficient expressing the expansion of the air by heat, as determined by Gay-Lussae, viz. 0.00375 of its bulk for one Centigrade degree, was adopted, but Laplace inereased it to 0.004 , in order to take into the account the effect of the greater expansive power of the vapors contained in the atmosphere.

These values have been retained in the different formulæ proposed later by Gauss, in Schumacher's Jahrbuch for 1840, by Schmidt, Mathem. und Physische Geographie, II. p. 205, and by Baily, Astronomical Tables, p. 183, which, therefore, only change the form without changing the results. D'Aubuisson, in his formula and tables, Traité de Géognosie, p. 488, only reduced the barometrical coefficient to its theoretical value, which he determined to be 18365 metres, leaving unchanged the other coefficients of Laplace's formula.

Bessel first introduced, in his formula, Astronomische Nachrichten, No. 356, a separate correction for the effect of moisture. The correction for the temperature of the air is computed in his tables for two values of the coefficient, that of Gay-Lussac, 0.00375 , and that of Rudberg, 0.00365 . Laplace's barometrical coefficient is retained, but the correction for the decrease of gravity is considerably modified.

In Elie Ritter's formula, in the Mémoires de la Societé de Physique de Genève, Tom. XIII. p. 343 , the corrections for temperature and moisture are also separated; but other values of the barometrical and thermometrical coefficients, derived from Regnault's determinations, are used, and a new method is proposed for applying the correction due to the expansion of air, which is made proportional to the square of the difference between the observed temperatures at each station.

Baeyer's formula, recently published in Poggendorf's Annalen der Physik und Chemie, Tom. XCVIII. p. 371, does not belong to either of the two classes just mentioned; for while it keeps Laplace's barometrical and thermometrical coefficients, it corrects the effect of temperature by a method analogous to that of Ritter, and it entirely neglects the effect of aqueous vapor.

In the following set the tables of Delcros, Guyot, and Loomis develop the formula of Laplace. The much larger tables of Delcros render unnecessary those of Oltmanns, which are yearly reprinted in the Annuaire du Bureau des Longitudes. Instead of Gauss's tables will be found the tables of Dippe, which are computed from the same formula, but are more extended. Baily's tables close the first series. The tables of Plantamour, computed from Bessel's formula, are given here in preference to Bessel's tables, because Plantamour substituted for Laplace's barometrical coefficient that derived from the probably more accurate determination of the relative weight of the air and mercury by Regnault, viz. 18404.8 metres. E. Ritter's tables, computed from his own formula, give perhaps, in extreme cases, better results; but as, in ordinary circumstances, the altitudes obtained do not much differ from those furnished by the less complicated tables of Plantamour, they were not reprinted here.

The miscellaneous tables which follow furnish useful materials for solving several questions connected with the barometrical measurements.

Regnault's table of Barometric Pressures corresponding to Temperatures of the Boiling Point of Water, revised by Moritz, and its reduction to English measures, will be found a valuable addition for thermometrical measurements of heights.

## I.

## TABLES

## FOR

DETERMINING DIFFERENCES OF LEVEL BY MEANS OF BAROMETRICAL OBSERVATIONS,

Computed from the complete formula of laplace,
By M. T. Delcros.

## Construction of the Tables.

If we take $z=$ difference of level of the two barometers,
$a=$ earth's mean radius $=6366200$ metres,
$\mathrm{L}=$ mean latitude between the two stations,
and further: -

$$
\text { At Station. }\left\{\begin{array}{l}
\text { Lower. }\left\{\begin{array}{l}
h=\text { observed height of the barometer, } \\
\text { T=temperature of the barometer, } \\
t=\text { temperature of the air, } \\
\text { Upper. }\left\{\begin{array}{l}
h^{\prime}=\text { observed height of the barometer, } \\
\Gamma^{\prime}=\text { temperature of the barometer } \\
t^{\prime}=\text { temperature of the air }
\end{array}\right.
\end{array}\right. \text {, }
\end{array}\right.
$$

and if we make finally $\mathrm{H}=h+h^{\prime}$. $\left(\frac{\mathrm{T}-\mathrm{T}^{\prime}}{6196}\right)$,
we shall have, according to Laplace, the following general and complete equation :-

$$
z=18336 \text { metres } \times\left\{\begin{array}{l}
\left(1+\frac{2 \cdot\left(t+t^{\prime}\right)}{1000}\right) \\
(1+0.0028371 \cos .2 \cdot \mathrm{~L}) \\
\left(\left(1+\frac{z}{a}\right) \cdot \log \cdot\left(\frac{h}{\mathrm{H}}\right)+\frac{z}{a} 0.868589\right)
\end{array}\right\}
$$

after the proper transformations this equation becomes:-
introducing into this expression the value in metres of $a$, the eurth's mean radius making $z=\log .\left(\frac{h}{H}\right) 18336$ and $\log .\left(\frac{h}{H}\right)=\left(\frac{z}{18336}\right)$, which can be done without sensible error, the above formula takes the following form, sufficiently accurate for practical purposes : -

$$
z=\log \cdot\left(\frac{h}{H}\right) \cdot 18336 \text { metres } \times\left\{\begin{array}{l}
\left(1+\frac{\left(2 .\left\langle t+t^{\prime}\right.\right.}{1000}\right) \\
(1+0.0028371 \cos .2 . L) \\
\left(1+\frac{z+15926}{63662200}\right)
\end{array}\right\}
$$

the four factors of which can easily be developed in tables, as has been done by Mr. Oltmanns. But though this savant chose to develop also the second factor, I found it better not to do so, partly because the calculation of it is very easy, and also or account of the great extent it would have been necessary to give to this table, in order to avoid troublesome interpolations.

In the calculation of $h^{\prime}$. $\left(\frac{T-T T^{\prime}}{615 t^{\prime}}\right)$, Mr. Oltmanns used the constant coefficient of the absolute expansion of the mercurial column; I took that of the relative expansion of the mereury and of the brass scale. It is obvious, therefore, that if the scale of the barometer employed was of wood, glass, iron, or of another substance, it would be necessary to make use of as many different coefficients, and the Table II. could not be used. Moreover, Oltmanns combined the last two factors of the general formula in one single table with double entry. This table I have calculated, extending it sufficiently to avoid a double interpolation; but as it seemed to me much too extensive, I substituted for it Tables III. and IV., which are more condensed. without rendering any troublesome interpolation necessary.

I carried the calculation of these tables beyond the limits at which Oltmanns chose to stop, in order that they may answer for the most extreme cases.

At the head of each table will be found the factor of which it is the development; this makes any other explanation superfluous.

All these tables give, at sight, the numbers wanted; only when very great precision is desired, a slight interpolation, at sight, and very easy to apply, may be required. My principal object was to relieve the computer of the troublesome and annoying labor of interpolations.

1 added to these four tables the small Table V., taken from the Annuaire $d u$ Bureau des Longitudes of Paris. It will be seldom used.

When calculating differences of level, in the same order, with the tables, and by the complete formula of Laplace, the results thus obtained never differ by more than one decimetre in the most extreme cases. The following example will illustrate this statement. I take the observation made in a balloon, by Cay-Lussac, at Paris, as an extreme case, which is very well adapted to manifest the errors of the tables, if there were any, by comparing the results obtained by means of them with those of the direct calculation according to the complete formula of Laplace, from which they are derived.

Example of Calculation by the complete Formula of Laplace and by the Tables Height of the Balloon of Gay-Lussac.
The observation gave: -
Bailoon $h^{\prime}=328.80 \quad \mathrm{~T}^{\prime}=-9.5 \quad t^{\prime}=-9^{\circ} .5$
Paris $\quad h=765.68 \quad \mathrm{~T}=+30.8 \quad t=+30.8$

$$
\mathrm{T}-\mathrm{T}^{\prime}=+40.3 \quad\left(t+t^{\prime}\right)=+21.3 \text { et } 2\left(t+t^{\prime}\right)=42^{\circ} .6
$$

With these data the formula of Laplace gives the following calculation : -
Log. $h^{\prime} .=398.80 \quad=2.5169318$

Log. $\left(\mathrm{T}-\mathrm{T}^{\prime}\right)=+40.3=1.6053050$
Log. dilat. coefficient $=0.0001614=6.2079035$
Corr. $a=+\quad \underset{298.14}{\text { Milli. }} \log .=\overline{0.3301403}$


Log. cos. $2 \mathrm{~L}=97^{\circ} 40^{\prime}=-\quad 9.1251872$
Log. constant $=0.0028371=+\quad \mathbf{7 . 4 5 2 8 7 4 6}$
$\log .(\mathrm{A}+a)=6679.79 .=+\quad 3.8247629$
$\log .((0.0028371 . \operatorname{Cos.} 2 \mathrm{~L}) \times(\mathrm{A}+a))=-0.4028247$

Corr. temp. air $=v=284.45 \quad=(6.677 \times 42.6)$

$(\mathrm{A}+a+\beta+v+\delta)=6986.74$
Altitude barom. Paris $=48.70$
Altitude of balloon $=7035.44$ by the formula of Laplace.

Now iet us calculate by the tables, placing side by side the corresponding results given by the formula of Laplace.

| Balloon $h^{\prime}=\begin{gathered}\text { Millim. } \\ 328.80\end{gathered} \quad \mathrm{~T}^{\prime}=-9.5 \quad t^{\circ}=$ | 9.5 |
| :---: | :---: |
| Paris $h=765.68 \quad \mathrm{~T}=+30.8 \quad t=+$ |  |
| with $\left\{\begin{array}{l}h^{\prime}=328.80 \\ h=765.68\end{array}\right\}$ Table I. gives $\left\{\begin{array}{l}1478.4 \\ 8209.8\end{array}\right.$ | By the formu Laplace we f |
| with $\left(\mathrm{T}^{\prime}-\mathrm{T}\right)=-40^{\circ} .3$, Table II. gives $a=-52.0$ |  |
| $(\mathrm{A}+a)=6679.4$ | $\begin{gathered} \text { Meetres. } \\ 6679.79 \end{gathered}$ |
| with $\mathrm{L}=48^{\circ} 50^{\prime}$, Table III. gives $a=-2.3$ | 2.53 |
| $(\mathrm{A}+a+\beta)=6677.1$ | 6677.26 |
| with $2\left(t+t^{\prime}\right)$ direct calculation gives $v=$ + 284.5 | + 284.45 |
| $(\mathrm{A}+a+\beta+v)=6961.6$ | 6961.71 |
| with 6960, Table IV. gives $\delta=$ 25.1 | + 25.03 |
| $(\mathrm{A}+a+\beta+v+\delta)=6986.7$ | 6986.74 |
| Altitude of barometer at Paris $=+48.7$ | + 48.70 |
| Therefore altitude of balloon $=7035.4$ | 7035.44 |

Two results which are sensibly identical. This ought not to astonish us; the tables being the exact development of the formula, they ought to give the same results, provided in both cases nothing has been neglected, and the four factors have been calculated in the same relative order.

## Delcros.

## Disposition and Use of the Tables.

The disposition of the tables is the following : -
In Table I., the first column on the left contains the height of the barometer in millimetres, corrected for the error of the instrument.

The second column headed N (number), gives in metres the first two figures of the number corresponding to each height of the barometer in the first column ; the third column, headed 0.0 , gives the remaining figures for the full number of millimetres; the following columns give the remaining figures for the same number of millimetres and each decimal fraction of a millimetre which may follow it. The value of the hundredths is to be found in the last column.

Example: - Height of Barometer $=761.00$.
We look out in the first column for the number 761, and we find on the same line in the second column, 81 ; in the third column, headed 0.0 , or full number, 61.1. The corresponding number is thus 8161.1 metres.

Height of barometer $=761.35$.
The second column gives 81 ; the column headed 0.3 gives, on the same line, 64.2. The corresponding number is then 8164.2 . Adding the value of five hundredths of milim., being $0^{\circ} .5$, as indicated in the last column, we have 8164.7 metres, corresponding to 761.35 millim.

The other four tables need no further explanation.
To calculate, by means of the tables, a difference of level from two barometrical observations, proceed in the following manner:--

1. Take the height of the barometer at the lower station, or $h$, and seek in Table I. the number corresponding to this height. Seek likewise the number corresponding to the height of the barometer at the upper station. Subtract the second from the first. The remainder is the approximate difference of level between the two stations. Then apply the following corrections.
2. Correction to be applied for the temperature of the barometers.

If ' $\mathrm{T}^{\prime}$ be the temperature of the attached thermometer at the upper station, and T that of the attached thermometer at the lower station, take the difference, or ' $\mathrm{T}^{\prime}$ - ' T , and seek in Table II. the number corresponding to this difference.

When $\mathrm{T}^{\prime}$ is smaller than T , that is, when the temperature of the attached thermometer of the upper station is lower than that of the lower station, the correction is to be subtracted from the approximate height; when $\mathrm{T}^{\prime}$ is greater than T , it is to be added.
3. Correction for the temperature of the air.

The first correction having been applied, multiply the number obtained, or N, by the double sum of the temperatures of the air at both stations, and divide the prodnet by 1000 ; the number thus found, or the quantity expressed by $\frac{\mathrm{N}}{1100)}$. $2\left(t+t^{\prime}\right)$ is the correction in metres which is to be added to the preceding number N.
4. Tables III. and IV. give two corrections; the first due to the decrease of gravitation in latitude, which is to be added when the mean latitude of the places of observation is between the 45 th parallel and the equator ; and to be subtracted when it is between the same parallel and the poles, as indicated at the head of the columns. The second correction, due to the decrease of gravitation on the vertical line, is always additice.
5. Table V. gives another small correction to be added in the case of the lower station being very clevated above the level of the ocean.

Examples of Calculation.
Measurement of the Height of Guanaxuato. By M. de Humboldt.

Barometer at the upper station,
Barometer at the level of the sea, D

$$
\begin{array}{lll}
h^{\prime}=600.95 & \mathrm{~T}^{\prime}=21.3 & t^{\prime}=21.3 \\
h=763.15 & \mathrm{~T}=25.3 & t=25.3
\end{array}
$$

$$
10
$$

Table I. gives the corresponding numbers,
$\left\{\begin{array}{l}h=8183.5 \\ h^{\prime}=6280.8\end{array}\right.$

Difference,
1902.7

Table II. gives for $\mathrm{T}^{\prime}$ - T ,
Difference,
$\frac{\mathrm{N}}{100 .} \cdot 2\left(t+t^{\prime}\right)=1.897 \times 93.2$,
Table III. gives for mean latitude of $21^{\circ}$,
Table IV. gives for decrease of gravitation in the vertical line,
Hence altitude of Guanaxuato above the ocean,
Sum,
$-\frac{5.2}{1897.5}=\mathrm{N}$
$+176.8$
2074.3
$+\quad 4.3$
$+6.0$
2084.6

Measurement of the height of Mont Blanc, August 29, 1844. By MM. Bravais and Martins.


Table I. gives for numbers corresponding to

$$
\left\{\begin{array}{l}
h=7826.0 \\
h^{\prime}=\frac{3504.4}{4321.6}
\end{array}\right.
$$

Table II. gives for $\mathrm{T}^{\prime}-\mathrm{T}$,
Difference,


TABLE I. - Giving $\mathrm{A}=18336 \times \log . \mathrm{H}$ or $h \ldots$, , argument H or $h$ in Millimetres.

| $\begin{aligned} & \text { Barom- } \\ & \text { eter } \\ & H \text { or } \mathrm{h} . \end{aligned}$ | N . | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\left\lvert\, \begin{gathered} \text { Parts } \\ \text { for cach } \\ \text { o.01tmm. } \end{gathered}\right.$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Metres | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 288 | 4 | 23.4 | 26.2 | 28.9 | 31.7 | 34.4 | 37.2 | 40.0 | 42.7 | 45.5 | 48.2 | 10.3 |
| 289 | 4 | 51.0 | 53.8 | 56.5 | 59.3 | 62.0 | 64.8 | 67.5 | 70.3 | 73.0 | 75.8 | 20.5 |
| 290 | 4 | 78.5 | 81.3 | 84.0 | 86.7 | 89.5 | 92.2 | 95.0 | 97.7 |  |  |  |
| 290 | 5 |  |  |  |  |  |  |  |  | 00.4 | 03.2 | 41.1 |
| 291 | 5 | 05.9 | 08.7 | 11.4 | 14.1 | 16.8 | 19.6 | 22.3 | 25.0 | 27.8 | 30.5 | $5{ }_{5} 1.4$ |
| 292 | 5 | 33.2 | 36.0 | 38.7 | 41.4 | 44.1 | 46.8 | 49.6 | 52.3 | 55.0 | 57.7 | 6 6 1.6 |
| 293 | 5 | 60.5 | 63.2 | 65.9 | 68.6 | 71.3 | 74.0 | 76.7 | 79.5 | 82.2 | 84.9 | 71.9 |
| 294 | 5 | 87.6 | 90.3 | 93.0 | 95.7 | 98.4 |  |  |  |  |  | 88.2 |
| 294 | 6 |  |  |  |  |  | 01.1 | 03.8 | 06.5 | 09.2 | 11.9 | 9 2.4 |
| 295 | 6 | 14.6 | 17.3 | 20.0 | 22.7 | 25.4 | 28.1 | 30.8 | 33.5 | 36.2 | 38.9 |  |
| 296 | 6 | 41.6 | 44.3 | 47.0 | 49.6 | 52.3 | 55.0 | 57.7 | 60.4 | 63.1 | 65.8 |  |
| 297 | 6 | 68.4 | 71.1 | 73.8 | 76.5 | 79.1 | 81.8 | 84.5 | 87.2 | 89.9 | 92.5 |  |
| 298 | 6 | 95.2 | 97.9 |  |  |  |  |  |  |  |  |  |
| 298 | 7 |  |  | 00.5 | 03.2 | 05.9 | 08.6 | 11.2 | 13.9 | 16.6 | 19.2 |  |
| 299 | 7 | 21.9 | 24.5 | 27.2 | 29.9 | 32.5 | 35.2 | 37.8 | 40.5 | 43.2 | 45.8 |  |
| 300 | 7 | 48.5 | 51.1 | 53.8 | 56.4 | 59.1 | 61.7 | 64.4 | 67.0 | 69.7 | 72.3 |  |
| 301 | 7 | 75.0 | 77.6 | 80.3 | 82.9 | 85.5 | 88.2 | 90.8 | 93.5 | 96.1 | 98.7 |  |
| 302 | 8 | 01.4 | 04.0 | 06.6 | 09.3 | 11.9 | 14.5 | 17.2 | 19.8 | 22.4 | 25.1 |  |
| 303 | 8 | 27.7 | 30.3 | 33.0 | 35.6 | 38.2 | 40.8 | 43.5 | 46.1 | 48.6 | 51.3 |  |
| 304 | 8 | 54.0 | 56.6 | 59.2 | 61.8 | 64.4 | 67.0 | 69.6 | 72.3 | 74.9 | 77.5 |  |
| 305 | 8 | 80.1 | 82.7 | 85.3 | 87.9 | 90.5 | 93.1 | 95.7 | 98.3 |  |  |  |
| 305 | 9 |  |  |  |  |  |  |  |  | 01.0 | 03.6 |  |
| 306 | 9 | 06.2 | 08.8 | 11.4 | 14.0 | 16.6 | 19.2 | 21.8 | 24.4 | 27.0 | 29.6 | 1 - 0.3 |
| 307 | 9 | 32.1 | 34.7 | 37.3 | 39.9 | 42.5 | 45.1 | 47.7 | 50.3 | 52.9 | 55.5 | 2 0.5 |
| 308 | 9 | 58.0 | 60.6 | 63.2 | 65.8 | 68.4 | 70.9 | 73.5 | 76.1 | 78.7 | 81.3 | 3 0.8 |
| 309 | 9 | 83.9 | 86.4 | 89.0 | 91.6 | 94.1 | 96.7 | 99.3 |  |  |  | 41.0 |
| 309 | 10 |  |  |  |  |  |  |  | 01.9 | 04.4 | 07.0 | 51.3 |
| 310 | 10 | 09.6 | 12.1 | 14.7 | 17.3 | 19.8 | 22.4 | 25.0 | 27.5 | 30.1 | 32.7 | 611.5 |
| 311 | 10 | 35.2 | 37.8 | 40.3 | 42.9 | 45.5 | 48.0 | 50.6 | 53.1 | 55.7 | 58.2 | 71.8 |
| 312 | 10 | 60.8 | 63.3 | 65.9 | 68.4 | 71.0 | 73.5 | 76.1 | 78.6 | 81.2 | 83.7 | 8 2.1 |
| 313 | 10 | 86.3 | 88.8 | 91.4 | 93.9 | 96.4 | 99.0 |  |  |  |  | 9 2.3 |
| 313 | 11 |  |  |  |  |  |  | 01.5 | 04.1 | 06.6 | 09.1 |  |
| 814 | 11 | 11.7 | 14.2 | 16.7 | 19.3 | 21.8 | 24.3 | 26.9 | 29.4 | 31.9 | 34.5 |  |
| 315 | 11 | 37.0 | 39.5 | 42.0 | 44.6 | 47.1 | 49.6 | 52.1 | 54.7 | 57.2 | 59.7 |  |
| 316 | 11 | 62.2 | 64.8 | 67.3 | 69.8 | 72.3 | 74.8 | 77.3 | 79.9 | 82.4 | 84.9 |  |
| 317 | 11 | 87.4 | 89.9 | 92.4 | 94.9 | 97.4 | 99.9 |  |  |  |  |  |
| 317 | 12 |  |  |  |  |  |  | 02.4 | 05.0 | 07.5 | 10.0 |  |
| 318 | 12 | 12.5 | 15.0 | 17.5 | 20.0 | 22.5 | 25.0 | 27.5 | 30.0 | 32.5 | 35.0 |  |
| 319 | 12 | 37.5 | 40.0 | 42.5 | 45.0 | 47.5 | 50.0 | 52.4 | 54.9 | 57.4 | 59.9 |  |
| 320 | 12 | 62.4 | 64.9 | 67.4 | 69.9 | 72.3 | 74.8 | 77.3 | 79.8 | 82.3 | 84.8 |  |
| 321 | 12 | 87.2 | 89.7 | 92.2 | 94.7 | 92.1 | 99.6 |  |  |  |  |  |
| 321 | 13 |  |  |  |  |  |  | 02.1 | 04.6 | 07.1 | 09.5 |  |
| 322 | 13 | 12.0 | 14.5 | 17.0 | 19.4 | 21.9 | 24.4 | 26.8 | 29.3 | 31.8 | 34.2 |  |
| 323 | 13 | 36.7 | 39.2 | 41.6 | 44.1 | 46.6 | 49.0 | 51.5 | 53.9 | 56.4 | 58.9 |  |
| 324 | 13 | 61.3 | 63.8 | 66.2 | 68.7 | 71.1 | 73.6 | 76.1 | 78.5 | 81.0 | 83.4 |  |
| 325 | 13 | 85.9 | 88.3 | 90.8 | 93.2 | 95.7 | 98.1 |  |  |  |  |  |
| 32.5 | 14 |  |  |  |  |  |  | 00.5 | 03.0 | 05.4 | 07.9 |  |
| Barometer Hor h. | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0. 4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\left\|\begin{array}{c} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} . \end{array}\right\|$ |

326 to $\mathbf{3 6 4} 4^{\mathrm{mn}}$.

| $\begin{aligned} & \text { Barom- } \\ & \begin{array}{l} \text { eter } \\ H \text { or } \mathrm{h} \end{array} \end{aligned}$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\left\lvert\, \begin{gathered} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} \end{gathered}\right.$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Metres. | Metres. | Metres. | Netres. | Metres | Metres. | TIetres. | Metres. | Metres. | Metres. | Metr. |
| 326 | 14 | 10.3 | 12.8 | 15.2 | 17.6 | 20.1 | 22.5 | 25.0 | 27.4 | 29.8 | 32.3 | ${ }^{1} \mid 0.2$ |
| 327 | 14 | 34.7 | 37.2 | 39.6 | 12.0 | 44.5 | 46.9 | 49.3 | 51.7 | 54.2 | 56.6 | 20.5 |
| 325 | 14 | 59.0 | 615 | 63.9 | 66.3 | 68.7 | 71.2 | 73.6 | 76.0 | 78.4 | 80.9 | 3 0.7 |
| 329 | 14 | 83.3 | 85.7 | 88.1 | 90.5 | 92.9 | 95.4 | 97.8 |  |  |  | 41.0 |
| 329 | 15 |  |  |  |  |  |  |  | 00.2 | 02.6 | 05.0 | 51.2 |
| 330 | 15 | 07.4 | 09.9 | 12.3 | 14.7 | 17.1 | 19.5 | 21.9 | 24.3 | 26.7 | 29.1 | 611.5 |
| 331 | 15 | 31.5 | 33.9 | 36.3 | 38.7 | 41.2 | 43.6 | 46.0 | 48.4 | 50.8 | 53.2 | 7 1.7 |
| 3:32 | 15 | 55.6 | 58.0 | 60.4 | 62.8 | 6.5 .1 | 67.5 | 69.9 | 72.3 | 74.7 | 77.1 | $8 \quad 2.0$ |
| 333 | 15 | 79.5 | 81.9 | 84.3 | 86.7 | 89.1 | 91.4 | 93.8 | 96.2 | 98.6 |  | 92.2 |
| 333 | 16 |  |  |  |  |  |  |  |  |  | 01.0 |  |
| 331 | 16 | 03.4 | 05.8 | 08.1 | 10.5 | 12.9 | 15.3 | 17.7 | 20.0 | 22.4 | 24.8 |  |
| 335 | 16 | 27.2 | 29.6 | 31.9 | 34.3 | 36.7 | 39.1 | 41.4 | 43.8 | 46.2 | 48.8 |  |
| 336 | 16 | 50.9 | 53.3 | 55.7 | 58.0 | 60.4 | 62.5 | 65.1 | 67.5 | 69.9 | 72.2 | 110.2 |
| 337 | 16 | 74.6 | 77.0 | 79.3 | 81.7 | 84.0 | 86.4 | 88.8 | 91.1 | 93.5 | 95.8 | 2 0.4 |
| 338 | 16 | 98.2 |  |  |  |  |  |  |  |  |  | 3 0.7 |
| 338 | 17 |  | 00.5 | 02.9 | 05.2 | 07.6 | 10.0 | 12.3 | 14.7 | 17.0 | 19.4 | 41.0 |
| 339 | 17 | 21.7 | 24.1 | 26.4 | 28.8 | 31.1 | 33.4 | 35.5 | 38.1 | 40.5 | 42.8 | 51.2 |
| 340 | 17 | 45.2 | 47.5 | 49.8 | 52.2 | 54.5 | 56.9 | 59.2 | 61.5 | 63.9 | 66.2 | 6 1.5 |
| 341 | 17 | 68.6 | 70.9 | 73.2 | 75.6 | 77.9 | s0.2 | 82.6 | 84.9 | 87.2 | 89.5 | 71.7 |
| 342 | 17 | 91.9 | 94.2 | 96.5 | 98.9 |  |  |  |  |  |  | 8 1.9 |
| 312 | 18 |  |  |  |  | 01.2 | 03.5 | 05.8 | 08.2 | 10.5 | 12.8 | 92.2 |
| 343 | 18 | 15.1 | 17.4 | 19.8 | 22.1 | 24.4 | 26.7 | 29.0 | 31.4 | 33.7 | 36.0 |  |
| 344 | 18 | 38.3 | 40.6 | 42.9 | 4.5 .2 | 17.6 | 49.9 | 52.2 | 54.5 | 56.8 | 59.1 |  |
| 34.5 | 18 | 61.4 | 63.7 | 66.0 | 63.3 | 70.6 | 73.0 | 75.3 | 77.6 | 79.9 | 82.2 |  |
| 346 | 18 | 84.5 | 86.8 | 89.1 | 91.4 | 93.7 | 96.0 | 98.3 |  |  |  |  |
| 346 | 19 |  |  |  |  |  |  |  | 00.6 | 02.9 | 05.2 |  |
| 3.17 | 19 | 07.5 | 09.6 | 12.0 | 14.3 | 16.6 | 18.9 | 21.2 | 23.5 | 25.8 | 28.1 |  |
| 348 | 19 | 30.4 | 32.7 | 34.9 | 37.2 | 39.5 | 11.8 | 4.1 | 46.4 | 18.6 | 50.9 |  |
| 349 | 19 | 53.2 | 55.5 | 57.8 | 60.1 | 62.3 | 64.6 | 66.9 | 69.2 | 71.5 | 73.7 |  |
| 350 | 19 | 76.0 | 78.3 | 80.6 | 82.8 | 85.1 | 87.4 | 89.6 | 91.9 | 94.2 | 96.5 |  |
| 8.51 | 19 | 95.7 |  |  |  |  |  |  |  |  |  | $\begin{array}{lll}2 & 0.4\end{array}$ |
| 351 | 20 |  | 01.0 | 03.3 | 05.5 | 07.8 | 10.1 | 12.3 | 14.6 | 16.8 | 19.1 | 3 0.7 |
| 352 | 20 | 21.4 | 23.6 | 25.9 | 28.2 | 30.4 | 32.7 | 34.9 | 37.2 | 39.5 | 41.7 | 40.9 |
| 353 | 20 | 44.0 | 46.2 | 48.5 | 50.7 | 53.0 | 55.2 | 57.5 | 59.7 | 62.0 | 64.2 | 51.1 |
| 3.54 | 20 | 66.5 | 68.7 | 71.0 | 73.2 | 75.5 | 77.7 | 80.0 | 82.2 | 84.5 | 86.7 | 6 1.3 |
| 355 | 20 | 89.0 | 91.2 | 93.4 | 95.7 | 97.9 |  |  |  |  |  | 71.6 |
| 355 | 21 |  |  |  |  |  | 00.2 | 02.4 | 04.6 | 06.9 | 09.1 | 81.8 |
| 356 | 21 | 11.4 | 13.6 | 15.8 | 18.1 | 20.3 | 22.5 | 24.8 | 27.0 | 29.2 | 31.5 | $\begin{array}{lll}9 & 2.1\end{array}$ |
| 357 | 21 | 33.7 | 35.9 | 38.2 | 40.4 | 42.6 | 4.8 | 47.1 | 49.3 | 51.5 | 53.7 |  |
| 358 | 21 | 56.0 | 58.2 | 60.4 | 62.6 | 64.9 | 67.1 | 69.3 | 71.5 | 73.7 | 76.0 |  |
| 359 | 21 | 78.2 | 80.1 | 82.6 | 84.8 | 87.0 | 89.3 | 91.5 | 93.7 | 95.9 | 98.1 |  |
| 360 | 22 | 00.3 | 02.5 | 04.8 | 07.0 | 09.2 | 11.4 | 13.6 | 15.8 | 18.0 | 20.2 |  |
| 361 | 22 | 22.4 | 24.6 | 26.8 | 29.0 | 31.2 | 33.4 | 35.6 | 37.9 | 40.1 | 42.3 |  |
| 362 | 22 | 4.5 | 46.7 | 48.9 | 51.0 | 53.2 | 55.4 | 57.6 | 59.8 | 62.0 | 64.2 |  |
| 363 | 22 | 66.4 | 68.6 | 70.8 | 73.0 | 75.2 | 77.4 | 79.6 | 81.8 | 83.9 | 86.1 |  |
| 36.4 | 22 | 88.3 | 90.. 5 | 92.7 | 91.9 | 97.1 | 99.3 |  |  |  |  |  |
| 364 | 23 |  |  |  |  |  |  | 01.4 | 03.6 | 05.8 | 08.0 |  |
| $\begin{aligned} & \text { Broni } \\ & \text { eter } \\ & \text { IHorh. } \end{aligned}$ | N | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} \\ \hline \end{gathered}$ |

365 to $\mathbf{4 0 3}^{\mathrm{mm} .}$

| Barometer Horh. | N. | 0.0 | 0.1 | O.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for each 0.01 mm . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Metres. | Metres. | Metres | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 365 | 23 | 10.2 | 12.4 | 14.5 | 16.7 | 18.9 | 21.1 | 23.2 | 25.4 | 27.6 | 29.8 | 10.2 |
| 366 | 23 | 32.0 | 34.1 | 36.3 | 38.5 | 40.7 | 42.8 | 45.0 | 47.2 | 49.3 | 51.5 | 20.4 |
| 367 | 23 | 53.7 | 55.9 | 58.0 | 60.2 | 62.4 | 64.5 | 66.7 | 65.9 | 71.0 | 73.2 |  |
| 368 | 23 | 75.4 | 77.5 | 79.7 | 81.8 | 84.0 | 86.2 | 88.3 | 90.5 | 92.6 | 94.8 | 40.9 |
| 369 | 23 | 97.0 | 99.1 |  |  |  |  |  |  |  |  | 51.1 |
| 369 | 24 |  |  | 01.3 | 03.4 | 05.6 | 07.7 | 09.9 | 12.1 | 14.2 | 16.4 | $6{ }_{6} 1.3$ |
| 370 | 24 | 18.5 | 20.6 | 22.8 | 24.9 | 27.1 | 29.2 | 31.4 | 33.5 | 35.7 | 37.8 | 71.5 |
| 371 | 24 | 40.0 | 42.1 | 44.3 | 46.4 | 48.6 | 50.7 | 52.9 | 55.0 | 57.2 | 59.3 | 8 1.7 |
| 372 | 24 | 61.5 | 63.6 | 65.8 | 67.9 | 70.1 | 72.2 | 74.3 | 76.5 | 78.6 | 80.8 | 9 \| 1.9 |
| 373 | 24 | 82.9 | 85.0 | 87.2 | 89.3 | 91.4 | 93.6 | 95.7 | 97.8 | 99.9 |  |  |
| 373 | 25 |  |  |  |  |  |  |  |  |  | 02.1 |  |
| 374 | 25 | 04.2 | 06.3 | 08.4 | 10.6 | 12.7 | 14.8 | 16.9 | 19.0 | 21.2 | 23.3 |  |
| 375 | 25 | 25.4 | 27.5 | 29.6 | 31.8 | 33.9 | 36.0 | 38.1 | 40.2 | 42.4 | 44.5 |  |
| 376 | 25 | 46.6 | 48.7 | 50.8 | 53.0 | 55.1 | 57.2 | 59.3 | 61.4 | 63.6 | 65.7 |  |
| 377 | 25 | 67.8 | 69.9 | 72.0 | 74.1 | 76.2 | 78.3 | 80.5 | 82.6 | 84.7 | 86.8 |  |
| 378 | 25 | 88.9 | 91.0 | 93.1 | 95.2 | 97.3 | 99.4 |  |  |  |  |  |
| 378 | 26 |  |  |  |  |  |  | 01.5 | 03.6 | 05.7 | 07.8 |  |
| 379 | 26 | 09.9 | 12.0 | 14.1 | 16.2 | 18.3 | 20.4 | 22.5 | 24.6 | 26.7 | 28.8 |  |
| 380 | 26 | 30.9 | 33.0 | 35.1 | 37.2 | 39.3 | 41.3 | 43.4 | 45.5 | 47.6 | 49.7 |  |
| 381 | 26 | 51.8 | 53.9 | 56.0 | 58.1 | 60.2 | 62.2 | 64.3 | 66.4 | 65.5 | 70.6 |  |
| 38.2 | 26 | 72.7 | 74.8 | 76.9 | 78.9 | 81.0 | 83.1 | 85.2 | 87.3 | 89.3 | 91.4 |  |
| 383 | 26 | 93.5 | 95.6 | 97.7 | 99.7 |  |  |  |  |  |  |  |
| 383 | 27. |  |  |  |  | 01.8 | 03.9 | 06.0 | 08.1 | 10.1 | 12.2 | 1.0 .2 |
| 384 | 27 | 14.3 | 16.4 | 18.4 | 205 | 22.6 | 24.6 | 26.7 | 28.8 | 30.9 | 32.9 | 2.0 .4 |
| 385 | 27 | 35.0 | 37.1 | 39.1 | 41.2 | 43.2 | 45.3 | 47.4 | 49.4 | 51.5 | 53.5 | 30.6 |
| 386 | 27 | 55.6 | 57.7 | 59.7 | 61.8 | 63.8 | 65.9 | 68.0 | 70.0 | 72.1 | 74.1 | 40.9 |
| 357 | 27 | 76.2 | 78.3 | 80.3 | 82.4 | 84.4 | 86.5 | 88.6 | 90.6 | 92.7 | 94.7 | $5 \begin{array}{ll}5 & 1.1\end{array}$ |
| 388 | 27 | 96.8 | 98.8 |  |  |  |  |  |  |  |  | $\begin{array}{lll}6 & 1.3\end{array}$ |
| 388 | 28 |  |  | 00.9 | 02.9 | 05.0 | 07.0 | 09.1 | 11.1 | 13.2 | 15.2 | $7 \quad 1.5$ |
| 389 | 28 | 17.3 | 19.3 | 21.4 | 23.4 | 25.5 | 27.5 | 29.6 | 31.6 | 33.7 | 35.7 | 8 1.7 |
| 390 | 28 | 37.8 | 39.8 | 41.9 | 43.9 | 46.0 | 48.0 | 50.0 | 52.1 | 54.1 | 56.2 | 9 1.9 |
| 391 | 28 | 58.2 | 60.2 | 62.3 | 64.3 | 66.3 | 68.3 | 70.4 | 72.4 | 74.4 | 76.5 |  |
| 392 | 28 | 78.5 | S0.5 | 82.6 | 84.6 | 86.6 | 88.6 | 90.7 | 92.7 | 94.7 | 96.8 |  |
| 393 | 28 | 98.8 |  |  |  |  |  |  |  |  |  |  |
| 393 | 29 |  | 00.8 | 02.8 | 04.9 | 06.9 | 08.9 | 10.9 | 12.9 | 15.0 | 17.0 |  |
| 394 | 29 | 19.0 | 21.0 | 23.0 | 25.1 | 27.1 | 29.1 | 31.1 | 33.1 | 35.2 | 37.2 |  |
| 395 | 29 | 39.2 | 41.2 | 43.2 | 45.2 | 47.2 | 49.2 | 51.3 | 53.3 | 55.3 | 57.3 |  |
| 396 | 29 | 59.3 | 61.3 | 63.3 | 65.3 | 67.3 | 69.3 | 71.4 | 73.4 | 75.4 | 77.4 |  |
| 397 | 29 | 79.4 | 81.4 | 83.4 | 85.4 | 87.4 | 89.4 | 91.5 | 93.5 | 95.5 | 97.5 |  |
| 398 | 29 | 99.5 |  |  |  |  |  |  |  |  |  |  |
| 398 | 30 |  | 01.5 | 03.5 | 0.5 .5 | 07.5 | 09.5 | 11.5 | 13.5 | 15.5 | 17.5 |  |
| 399 | 30 | 19.5 | 21.5 | 23.5 | 25.5 | 27.5 | 29.4 | 31.4 | 33.4 | 35.4 | 37.4 |  |
| 400 | 30 | 39.4 | 41.4 | 43.4 | 45.4 | 47.4 | 49.4 | 51.3 | 53.3 | 55.3 | 57.3 |  |
| 401 | 30 | 59.3 | 61.3 | 63.3 | 65.2 | 67.2 | 69.2 | 71.2 | 73.2 | 75.1 | 77.1 |  |
| 402 | 30 | 79.1 | 81.1 | 83.1 | 85.0 | 87.0 | 89.0 | 91.0 | 93.0 | 94.9 | 96.9 |  |
| 403 | 30 | 98.9 |  |  |  |  |  |  |  |  |  |  |
| $\left\|\begin{array}{c} \text { ?arom- } \\ \text { eter } \\ \therefore \text { or } \mathrm{t} . \end{array}\right\|$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { fir each } \\ 0.01 \mathrm{~mm} . \end{gathered}$ |

403 to $442^{\mathrm{mm}}$.

| $\left\lvert\, \begin{gathered} \text { Barom- } \\ \text { eter } \\ \text { Hor h. } \end{gathered}\right.$ | $N$. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for each 10.01 mm . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr | Metres. | Metres. | Metres. | Metres. | Metres | Metres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 403 | 31 |  | 00.9 | 02.8 | 04.8 | 06.8 | 08.7 | 10.7 | 12.7 | 14.7 | 16.6 | 10.2 |
| 404 | 31 | 18.6 | 20.6 | 22.5 | 24.5 | 26.5 | 28.4 | 30.4 | 32.4 | 34.4 | 36.3 |  |
| 405 | 31 | 38.3 | 40.3 | 42.2 | 44.2 | 46.1 | 48.1 | 50.1 | 52.0 | 54.0 | 55.9 |  |
| 406 | 31 | 57.9 | 59.9 | 61.8 | 63.8 | 65.7 | 67.7 | 69.7 | 71.6 | 73.6 | 75.5 | 40.8 |
| 407 | 31 | 77.5 | 79.5 | 81.4 | 83.4 | 85.3 | 87.3 | 89.3 | 91.2 | 93.2 | 95.1 | 51.0 |
| 408 | 31 | 97.1 | 99.0 |  |  |  |  |  |  |  |  |  |
| 408 | 32 |  |  | 01.0 | 02.9 | 04.9 | 06.8 | 08.8 | 10.7 | 12.7 | 14.6 | $7 \begin{array}{ll}7 & 1.4\end{array}$ |
| 409 | 32 | 16.6 | 18.5 | 20.5 | 22.4 | 24.4 | 26.3 | 28.2 | 30.2 | 32.1 | 34.1 |  |
| 410 | 32 | 36.0 | 37.9 | 39.9 | 41.8 | 43.8 | 45.7 | 47.6 | 49.6 | 51.5 | 53.5 | $\begin{array}{ll}9 & 1.8\end{array}$ |
| 411 | 32 | 55.4 | 57.3 | 59.3 | 61.2 | 63.2 | 65.1 | 67.0 | 69.0 | 70.9 | 72.9 |  |
| 412 | 32 | 74.8 | 76.7 | 78.7 | 50.6 | 82.5 | 84.4 | 86.4 | 88.3 | 90.2 | 92.2 |  |
| 413 | 32 | 94.1 | 96.0 | 97.9 | 99.9 |  |  |  |  |  |  |  |
| 413 | 33 |  |  |  |  | 01.8 | 03.7 | 05.6 | 07.5 | 09.5 | 11.4 |  |
| 414 | 33 | 13.3 | 15.2 | 17.1 | 19.1 | 21.0 | 22.9 | 2.48 | 26.7 | 25.7 | 30.6 |  |
| 415 | 33 | 32.5 | 34.4 | 36.3 | 38.3 | 40.2 | 42.1 | 44.0 | 45.9 | 47.9 | 49.8 |  |
| 416 | 33 | 51.7 | 53.6 | 55.5 | 57.4 | 59.3 | 61.2 | 63.2 | 65.1 | 67.0 | 68.9 |  |
| 417 | 33 | 70.8 | 72.7 | 74.6 | 76.5 | 78.4 | 80.3 | 82.3 | 84.2 | 86.1 | 88.0 |  |
| 418 | 33 | 89.9 | 91.8 | 93.7 | 95.6 | 97.5 | 99.4 |  |  |  |  |  |
| 418 | 34 |  |  |  |  |  |  | 01.3 | 03.2 | 05.1 | 07.0 |  |
| 419 | 34 | 08.9 | 10.8 | 12.7 | 14.6 | 16.5 | 18.4 | 20.3 | 22.2 | 24.1 | 26.0 |  |
| 420 | 34 | 27.9 | 29.8 | 31.7 | 33.6 | 35.5 | 37.3 | 39.2 | 41.1 | 43.0 | 44.9 |  |
| 421 | 34 | 46.8 | 48.7 | 50.6 | 52.5 | 54.4 | 56.2 | 58.1 | 60.0 | 61.9 | 63.8 |  |
| 422 | 34 | 65.7 | 67.6 | 69.5 | 71.4 | 73.3 | 75.1 | 77.0 | 78.9 | 80.8 | 82.7 | 10.2 |
| 423 | 34 | 84.6 | 86.5 | 88.4 | 90.2 | 92.1 | 94.0 | 95.9 | 97.8 | 99.6 |  | 2 0.4 |
| 423 | 35 |  |  |  |  |  |  |  |  |  | 01.5 | 3 3, 0.6 |
| 424 | 35 | 03.4 | 05.3 | 07.2 | 09.0 | 10.9 | 12.8 | 14.7 | 16.6 | 18.4 | 20.3 | 4 0.8 |
| 425 | 35 | 22.2 | 24.1 | 25.9 | 27.8 | 29.6 | 31.5 | 33.4 | 35.2 | 37.1 | 38.9 | 5 1.0 <br> 6 1.2 |
| 426 | 35 | 40.8 | 42.7 | 44.5 | 46.4 | 48.3 | 50.1 | 52.0 | 53.9 | 55.8 | 57.6 | 71.4 |
| 427 | 35 | 59.5 | 61.4 | 63.2 | 65.1 | 67.0 | 68.8 | 70.7 | 72.6 | 74.5 | 76.3 | 881.6 |
| 428 | 35 | 78.2 | 80.1 | 81.9 | 83.8 | 85.6 | 87.5 | 89.4 | 91.2 | 93.1 | 91.9 | 9 1.8 |
| 429 | 35 | 96.8 | 98.6 |  |  |  |  |  |  |  |  |  |
| 429 | 36 |  |  | 00.5 | 02.3 | 04.2 | 06.0 | 07.9 | 09.7 | 11.6 | 13.4 |  |
| 430 | 36 | 15.3 | 17.1 | 19.0 | 20.8 | 22.7 | 24.6 | 26.4 | 28.2 | 30.1 | 31.9 |  |
| 431 | 36 | 33.8 | 35.6 | 37.5 | 39.3 | 41.2 | 43.0 | 44.8 | 46.7 | 48.5 | 50.4 |  |
| 432 | 36 | 52.2 | 54.0 | 5.5.9 | 57.7 | 59.6 | 61.4 | 63.2 | 6.5 .1 | 66.9 | 68.8 |  |
| 433 | 36 | 70.6 | 72.4 | 74.3 | 76.1 | 78.0 | 79.8 | 81.6 | 83.5 | 85.3 | 87.2 |  |
| 434 | 36 | 89.0 | 90.8 | 92.7 | 94.5 | 96.3 | 98.1 |  |  |  |  |  |
| 434 | 37 |  |  |  |  |  |  | 00.0 | 01.8 | 03.6 | 05.5 |  |
| 435 | 37 | 07.3 | 09.1 | 11.0 | 12.8 | 14.6 | 16.4 | 18.3 | 20.1 | 21.9 | 238 |  |
| 436 | 37 | 25.6 | 27.4 | 29.2 | 31.1 | 32.9 | 34.7 | 36.5 | 38.3 | 40.2 | 42.0 |  |
| 437 | 37 | 43.8 | 45.6 | 47.5 | 49.3 | 51.1 | 52.9 | 54.8 | 56.6 | 58.4 | 60.3 |  |
| 438 | 37 | 62.1 | 63.9 | 6.9 .7 | 67.6 | 69.4 | 71.2 | 73.0 | 74.8 | 76.7 | 78.5 |  |
| 439 | 37 | 80.3 | 82.1 | 83.9 | 85.7 | 87.5 | 89.3 | 91.2 | 93.0 | 94.8 | 96.6 |  |
| 440 | 37 | 98.4 |  |  |  |  |  |  |  |  |  |  |
| 440 | 38 |  | 00.2 | 02.0 | 03.8 | 0.5 .6 | 07.5 | 09.3 | 11.1 | 12.9 | 14.7 |  |
| 441 | 38 | 16.5 | 18.3 | 20.1 | 21.9 | 23.7 | 25.5 | 27.3 | 29.1 | 30.9 | 32.7 |  |
| 442 | 38 | 34.5 | 36.3 | 38.1 | 39.9 | 41.7 | 43.5 | 45.3 | 47.1 | 48.9 | 50.7 |  |
| $\begin{aligned} & \text { Brom- } \\ & \text { eter } \\ & \text { B or } h . \end{aligned}$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for each 001 mm . |

443 to $482^{\mathrm{mm} .}$

| BaromH orh | N. | Tenth of Millimetre. |  |  |  |  |  |  |  |  |  | $\left\|\begin{array}{c} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} . \end{array}\right\|$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |  |
| Milli. | Metr. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 443 | 38 | 52.5 | 54.3 | 56.1 | 57.9 | 59.7 | 61.4 | 63.2 | 65.0 | 66.8 | 68.6 |  |
| 444 | 38 | 70.4 | 72.2 | 74.0 | 75.8 | 77.6 | 79.3 | 81.1 | 82.9 | 84.7 | S6.5 |  |
| 445 | 38 | 88.3 | 90.1 | 91.9 | 93.7 | 95.5 | 97.2 | 99.0 |  |  |  |  |
| 445 | 39 |  |  |  |  |  |  |  | 00.8 | 02.6 | 04.4 |  |
| 446 | 39 | 06.2 | 08.0 | 09.8 | 11.5 | 13.3 | 15.1 | 16.9 | 18.7 | 20.4 | 22.2 |  |
| 4.47 | 39 | 24.0 | 25.9 | 27.6 | 29.3 | 31.1 | 32.9 | 34.7 | 36.5 | 38.2 | 40.0 |  |
| 4.48 | 39 | 41.8 | 43.6 | 45.4 | 47.1 | 48.9 | 50.7 | 52.5 | 54.3 | 56.0 | 57.8 |  |
| 449 | 39 | 59.6 | 61.4 | 63.1 | 64.9 | 66.7 | 68.4 | 70.2 | 72.0 | 73.8 | 75.5 |  |
| 450 | 39 | 77.3 | 79.1 | 80.8 | 82.6 | 84.3 | 86.1 | 87.9 | 89.6 | 91.4 | 93.1 |  |
| 451 | 39 | 94.9 | 96.7 | 98.4 |  |  |  |  |  |  |  |  |
| 451 | 40 |  |  |  | 00.2 | 02.0 | 03.7 | 05.5 | 07.3 | 09.1 | 10.8 |  |
| 452 | 40 | 12.6 | 14.4 | 16.1 | 17.9 | 19.6 | 21.4 | 23.2 | 24.9 | 26.7 | 28.4 |  |
| 453 | 40 | 30.2 | 32.0 | 33.7 | 35.5 | 37.2 | 39.0 | 40.8 | 42.5 | 44.3 | 46.0 |  |
| 454 | 40 | 47.8 | 49.5 | 51.3 | 53.0 | 54.8 | 56.5 | 58.3 | 60.0 | 61.8 | 63.5 |  |
| 455 | 40 | 65.3 | 67.0 | 63.8 | 70.5 | 72.3 | 74.0 | 75.8 | 77.5 | 79.3 | 81.0 | 10.2 |
| 456 | 40 | 82.8 | 84.5 | 86.3 | 88.0 | 89.8 | 91.5 | 93.2 | 9.3.0 | 96.7 | 98.5 | 20.3 |
| 457 | 41 | 00.2 | 01.9 | 03.7 | 05.4 | 97.2 | 08.9 | 10.6 | 12.4 | 14.1 | 15.9 | 3 O |
| 458 | 41 | 17.6 | 19.3 | 21.1 | 22.8 | 246 | 26.3 | 28.0 | 29.8 | 31.5 | 33.3 | 40.7 |
| 459 | 41 | 35.0 | 36.7 | 35.5 | 40.2 | 41.3 | 43.6 | 45.4 | 47.1 | 45.8 | 50.6 | 50.9 |
| 160 | 41 | 52.3 | 54.0 | 55.8 | 57.5 | 59.2 | 60.9 | 62.7 | 64.4 | 66.1 | 67.9 | 61.0 |
| 461 | 41 | 69.6 | 71.3 | 73.1 | 74.8 | 76.5 | 78.2 | 80.0 | 81.7 | 83.4 | 85.2 | 71.2 |
| 462 | 41 | 86.9 | 88.6 | 90.3 | 92.1 | 93.5 | 95.5 | 97.2 | 98.9 |  |  | 8 8 1.4 |
| 462 | 42 |  |  |  |  |  |  |  |  | 00.7 | 02.3 | 911.6 |
| 463 | 42 | 04.1 | 05.8 | 07.5 | 09.3 | 11.0 | 12.7 | 14.4 | 16.1 | 17.9 | 19.6 |  |
| 464 | 42 | 21.3 | 23.0 | 24.7 | 26.4 | 28.1 | 29.8 | 31.6 | 33.3 | 35.0 | 36.7 |  |
| 465 | 42 | 38.4 | 40.1 | 41.8 | 43.5 | 45.2 | 46.9 | 48.7 | 50.4 | 52.1 | 53.5 |  |
| 466 | 42 | 55.5 | 57.2 | 58.9 | 60.6 | 62.3 | 64.0 | 65.8 | 67.5 | 69.2 | 70.9 |  |
| 467 | 42 | 72.6 | -74.3 | 76.0 | 77.7 | 79.4 | 81.1 | S2.8 | 84.5 | 86.2 | 87.9 |  |
| 463 | 42 | 89.6 | 91.3 | 93.0 | 94.7 | 96.4 | 98.1 | 99.8 |  |  |  |  |
| 468 | 43 |  |  |  |  |  |  |  | 01.5 | 03.2 | 04.9 |  |
| 469 | 43 | 06.6 | 08.3 | 10.0 | 11.7 | 13.4 | 15.1 | 16.8 | 18.5 | 20.2 | 21.9 |  |
| 470 | 43 | 23.6 | 25.3 | 27.0 | 28.7 | 30.4 | 32.0 | 33.7 | 3.7.4 | 37.1 | 38.8 |  |
| 471 | 43 | 40.5 | 42.2 | 43.9 | 45.6 | 47.3 | 48.9 | 50.6 | 52.3 | 54.0 | 55.7 |  |
| 472 | 43 | 57.4 | 59.1 | 60.8 | 62.5 | 64.2 | 65.8 | 67.5 | 69.2 | 70.9 | 72.6 |  |
| 473 | 43 | 74.3 | 76.0 | 77.7 | 79.3 | 81.0 | 82.7 | 84.4 | 86.1 | 87.7 | 89.4 |  |
| 474 | 43 | 91.1 | 92.8 | 94.5 | 96.1 | 97.8 | 99.5 |  |  |  |  |  |
| 474 | 44 |  |  |  |  |  |  | 01.2 | 02.9 | 04.5 | 06.2 |  |
| 475 | 44 | 07.9 | 09.6 | 11.2 | 12.9 | 14.6 | 16.2 | 17.9 | 19.6 | 21.3 | 22.9 |  |
| 476 | 44 | 24.6 | 26.3 | 27.9 | 29.6 | 31.3 | 33.9 | 35.6 | 37.3 | 39.0 | 40.6 |  |
| 477 | 44 | 41.3 | 43.0 | 44.6 | 46.3 | 48.0 | 49.6 | 51.3 | 53.0 | 54.7 | 56.3 |  |
| 478 | 44 | 58.0 | 59.7 | 61.3 | 63.0 | 64.7 | 66.3 | 68.0 | 69.7 | 71.4 | 73.0 |  |
| 479 | 44 | 74.7 | 76.4 | 78.0 | 79.7 | 81.3 | 83.0 | 84.7 | 86.3 | 88.0 | 89.6 |  |
| 480 | 44 | 91.3 | 93.0 | 94.6 | 96.3 | 97.9 | 99.6 |  |  |  |  |  |
| 480 | 45 |  |  |  |  |  |  | 01.3 | 02.9 | 04.6 | 06.2 |  |
| 481 | 45 | 07.9 | 09.5 | 11.2 | 12.8 | 14.5 | 16.1 | 17.7 | 19.4 | 21.0 | 22.7 |  |
| 482 | 45 | 24.3 | 25.9 | 27.6 | 29.2 | 30.9 | 32.5 | 34.2 | 35.8 | 37.5 | 39.1 |  |
| Baromeler Horh. | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{mn} . . \end{gathered}$ |

483 to $524^{\mathrm{mm}}$.

| $\begin{aligned} & \text { Barm- } \\ & \text { eter } \\ & \text { eor } \mathrm{ct} \text {. } \end{aligned}$ | N . | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} . \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Metres. | Metres. | Metres. | Metres. | Netres | Metres. | Metres. | Metres. | Metres, | Metres. | Merr. |
| 453 | 45 | 40.6 | 42.4 | 4.4 | 45.7 | 47.4 | 49.0 | 50.7 | 52.3 | 54.0 | 55.6 | 10.2 |
| 184 | 45 | 57.3 | 58.9 | 60.6 | 62.2 | 63.9 | 655 | 67.1 | 68.8 | 70.4 | 72.1 |  |
| 185 | 45 | 73.7 | 75.3 | 77.0 | 78.6 | 80.3 | 81.9 | 83.6 | 85.2 | 86.9 | 88.5 |  |
| 486 | 45 | 90.2 | 91.8 | 93.5 | 95.1 | 96.8 | 98.4 |  |  |  |  | 40.6 |
| 486 | 46 |  |  |  |  |  |  | 00.0 | 01.7 | 03.3 | 05.0 | 5 0.8 |
| 457 | 46 | 06.6 | 0 S 2 | 09.9 | 11.5 | 13.1 | 14.7 | 16.4 | 18.0 | 19.6 | 21.3 | $\begin{array}{lll}6 & 1.0\end{array}$ |
| 488 | 46 | 22.9 | 24.5 | 26.2 | 27.8 | 29.4 | 31.0 | 32.7 | 34.3 | 35.9 | 37.6 | 71.1 |
| 489 | 46 | 39.2 | 40.8 | 42.4 | 44.1 | 45.7 | 17.3 | 48.9 | 50.5 | 52.2 | 53.8 | $8 \quad 1.3$ |
| 490 | 46 | 55.4 | 57.0 | 58.6 | 60.3 | 61.9 | 63.5 | 65.1 | 66.7 | 68.4 | 70.0 | 981.4 |
| 491 | 46 | 71.6 | 73.2 | 74.9 | 76.5 | 78.1 | 79.7 | 81.4 | 83.0 | 84.6 | 86.3 |  |
| 492 | 46 | 87.9 | 89.5 | 91.1 | 92.8 | 94.4 | 96.0 | 97.6 | 99.2 |  |  |  |
| 492 | 47 |  |  |  |  |  |  |  |  | 00.9 | 02.5 |  |
| 493 | 47 | 04.1 | 05.7 | 07.3 | 08.9 | 10.5 | 12.1 | 13.8 | 15.4 | 17.0 | 18.6 |  |
| 494 | 47 | 20.2 | 21.8 | 23.4 | 25.0 | 26.6 | 28.2 | 29.9 | 31.5 | 33.1 | 34.7 |  |
| 495 | 47 | 36.3 | 37.9 | 39.5 | 41.1 | 42.7 | 4.3 | 45.9 | 47.5 | 49.1 | 507 |  |
| 496 | 47 | 52.3 | 53.9 | 55.5 | 57.1 | 58.7 | 60.3 | 61.9 | 63.5 | 65.1 | 66.7 |  |
| 497 | 47 | 68.3 | 69.9 | 71.5 | 73.1 | 74.7 | 76.3 | 78.0 | 79.6 | 81.2 | 82.8 |  |
| 498 | 47 | 84.4 | 86.0 | 87.6 | 89.2 | 90.8 | 92.4 | $9+.0$ | 95.6 | 97.2 | 95.8 |  |
| 499 | 18 | 00.4 | 02.0 | 03.6 | 05.2 | 06.5 | 08.3 | 09.9 | 11.5 | 13.1 | 14.7 |  |
| 500 | 48 | 16.3 | 17.9 | 19.5 | 21.1 | 22.7 | 24.2 | 25.8 | 27.4 | 89.0 | 30.6 |  |
| 501 | 48 | 32.2 | 33.8 | 35.4 | 37.0 | 38.6 | 40.1 | 41.7 | 43.3 | 44.9 | 46.5 |  |
| 502 | 48 | 48.1 | 49.7 | 51.3 | 52.9 | 54.5 | 56.0 | 57.6 | 59.2 | 60.8 | 62.4 |  |
| 503 | 48 | 64.0 | 65.6 | 67.2 | 68.7 | 70.3 | 71.9 | 73.5 | 75.1 | 76.6 | 78.2 |  |
| 504 | 48 | 79.8 | 81.4 | 83.0 | 84.5 | S6.1 | 87.7 | 89.3 | 90.9 | 92.4 | 9.4.0 |  |
| 50.5 | 48 | 95.6 | 97.2 | 93.7 |  |  |  |  |  |  |  |  |
| 50.5 | 49 |  |  |  | 00.3 | 01.9 | 03.4 | 05.0 | 06.6 | 08.2 | 09.7 |  |
| 506 | 49 | 11.3 | 12.9 | 14.4 | 16.0 | 17.6 | 19.1 | 20.7 | 2.23 | 23.9 | 25.4 |  |
| 507 | 49 | 27.0 | 28.6 | 30.1 | 31.7 | 33.3 | 34.8 | 36.4 | 38.0 | 39.6 | 41.1 |  |
| 508 | 49 | 42.7 | 44.3 | 45.8 | 47.4 | 49.0 | 50.5 | 52.1 | 53.7 | 55.3 | 56.8 |  |
| 509 | 49 | 58.4 | 60.0 | 61.5 | 63.1 | 64.6 | 66.2 | 67.8 | 69.3 | 70.9 | 72.4 |  |
| 510 | 49 | 74.0 | 75.6 | 77.1 | 78.7 | 80.2 | 81.8 | 83.4 | 84.9 | 86.5 | 88.0 |  |
| 511 | 49 | 89.6 | 91.2 | 92.7 | 91.3 | 95.8 | 97.4 | 99.0 |  |  |  |  |
| 511 | 50 |  |  |  |  |  |  |  | 00.5 | 02.1 | 03.6 |  |
| 512 | 50 | 05.2 | 06.7 | 08.3 | 09.8 | 11.4 | 12.9 | 14.5 | 16.0 | 17.6 | 19.1 |  |
| 513 | 50 | 20.7 | 22.2 | 23.8 | 25.3 | 26.9 | 28.4 | 30.0 | 31.5 | 3: 1 | 31.6 |  |
| 314 | 50 | 36.2 | 37.7 | 39.3 | 40.8 | 42.4 | 43.9 | 45.5 | 46.0 | 48.6 | 50.1 |  |
| 515 | 50 | 51.7 | 53.2 | 54.8 | 56.3 | 57.9 | 59.4 | 61.0 | 62.5 | 64.1 | 65.6 |  |
| 516 | 50 | 67.2 | 68.7 | 70.3 | 71.8 | 73.4 | 74.9 | 76.4 | 78.0 | 79.5 | 81.1 |  |
| 517 | 50 | S2.6 | 84.1 | 55.7 | 87.2 | 88.7 | 90.2 | 91.8 | 93.3 | 94.8 | 96.4 |  |
| 518 | 50 | 97.9 | 99.4 |  |  |  |  |  |  |  |  |  |
| 518 | 51 |  |  | 01.0 | 02.5 | 04.1 | 05.6 | 07.1 | 08.7 | 10.2 | 11.8 |  |
| 319 | 51 | 13.3 | 14.8 | 16.4 | 17.9 | 194 | 20.9 | 22.5 | 24.0 | 25.5 | 27.1 |  |
| 520 | 51 | 28.6 | 30.1 | 31.7 | 33.2 | 34.7 | 36.2 | 37.8 | 39.3 | 40.8 | 42.4 |  |
| 521 | 51 | 43.9 | 45.4 | 47.0 | 48.5 | 50.0 | 51.5 | 53.1 | 51.6 | 56.1 | 57.7 |  |
| 522 | 51 | 59.2 | 60.7 | 62.2 | 63.8 | 6.5 .3 | 66.5 | 68.3 | 69.8 | 71.4 | 72.9 |  |
| 523 | 51 | 74.4 | 75.9 | 77.5 | 79.0 | 80.5 | 82.0 | 83.6 | 85.1 | 86.6 | 88.2 |  |
| 524 | 51 | 59.7 | 91.2 | 92.7 | 94.3 | 95.8 | 97.3 | 98.8 |  |  |  |  |
| $\begin{aligned} & \text { Sarom. } \\ & \text { eter } \\ & \text { Hor } . \end{aligned}$ | N. | 0.0 | 0.1 | 0.9 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { for rach } \\ \text { ontmen. } \end{gathered}$ |

524 to $565{ }^{\mathrm{mm}}$.

| Bavm. eter Hor h . | N. | 0.0 | 0.1 | 0.9 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for each 0.01 mm . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. 524 | Neir. 52 | Metres. | Metres. | Metres. | Metres. | Metres | Metres. | Metres. | Merres. 00.3 | Metres. $01.9$ | Metres $03.4$ | Metr. |
| 525 | 52 | 04.9 | 06.4 | 07.9 | 09.4 | 10.9 | 12.4 | 14.0 | 15.5 | 17.0 | 18.5 |  |
| 526 | 52 | 20.0 | 21.5 | 23.0 | 24.5 | 26.0 | 27.5 | 29.1 | 30.6 | 32.1 | 33.6 |  |
| 527 | 52 | 35.1 | 36.6 | 38.1 | 39.6 | 41.1 | 42.6 | 44.2 | 45.7 | 47.2 | 48.7 |  |
| 528 | 52 | 50.2 | 51.7 | 53.2 | 54.7 | 56.2 | 57.7 | 59.3 | 60.8 | 62.3 | 63.8 |  |
| 529 | 52 | 65.3 | 66.8 | 65.3 | 69.8 | 71.3 | 72.8 | -4.3 | 75.8 | 77.3 | 78.8 | 10.1 |
| 530 | 52 | 80.3 | 81.8 | 83.3 | 84.8 | 86.3 | 87.8 | 89.3 | 90.8 | 92.3 | 93.8 | 20.3 |
| 531 | 52 | 95.3 | 96.8 | 98.3 | 99.8 |  |  |  |  |  |  | S 0.4 |
| 531 | 53 |  |  |  |  | 01.3 | 02.8 | 04.3 | 05.8 | 07.3 | 05.8 | 40.6 |
| 532 | $5: 3$ | 10.3 | 11.8 | 13.3 | 14.8 | 16.3 | 17.8 | 19.3 | 20.8 | 22.3 | 23.5 | 50.7 |
| 533 | 53 | 25.3 | 26.8 | 28.3 | 29.8 | 31.3 | 32.7 | 34.2 | 3.5 .7 | 37.2 | 38.7 | 60.9 |
| 534 | 53 | 40.2 | 41.7 | 43.2 | 44.7 | 46.2 | 47.6 | 49.1 | 50.6 | 52.1 | 53.6 | 71.0 |
| 533 | 53 | 55.1 | 56.5 | 58.1 | 59.6 | 61.1 | 62.5 | 64.0 | 65.5 | 67.0 | 65.5 | $8 \quad 1.2$ |
| 536 | 53 | 70.0 | 71.5 | 73.0 | 74.4 | 75.9 | 77.4 | 75.9 | 80.4 | 81.8 | 83.3 | $9 \quad 1.3$ |
| 537 | 53 | S 4.8 | 86.3 | 87.8 | 89.2 | 90.7 | 92.2 | 93.7 | 95.2 | 96.6 | 98.1 |  |
| 538 | 53 | 99.6 |  |  |  |  |  |  |  |  |  |  |
| 538 | 54 |  | 01.1 | 02.6 | 04.0 | 05.5 | 07.0 | 08.5 | 10.0 | 11.4 | 12.9 |  |
| 539 | 54 | 14.4 | 15.9 | 17.4 | 18.8 | 20.3 | 21.8 | 23.3 | 24.8 | 26.2 | 27.7 |  |
| 540 | 54 | 29.2 | 30.7 | 32.1 | 33.6 | 35.1 | 36.5 | 38.0 | 39.5 | 41.0 | 42.4 |  |
| 541 | 54 | 43.9 | 45.4 | 46.8 | 48.3 | 49.8 | 51.2 | 52.7 | 54.2 | 55.7 | 57.1 |  |
| 542 | 54 | 58.6 | 60.1 | 61.5 | 63.0 | 64.5 | 66.0 | 67.4 | 65.9 | 70.4 | 71.8 |  |
| 543 | 54 | 73.3 | 74.8 | 76.2 | 77.7 | 79.1 | 80.6 | 82.1 | 83.5 | 85.0 | 86.4 |  |
| 544 | 54 | 87.9 | 89.4 | 90.8 | 92.3 | 93.7 | 95.2 | 96.7 | 98.1 | 99.6 |  |  |
| 544 | 55 |  |  |  |  |  |  |  |  |  | 01.0 |  |
| 545 | 55 | 02.5 | 04.0 | 05.4 | 06.9 | 08.4 | 09.5 | 11.3 | 12 S | 14.3 | 15.7 |  |
| 546 | 55 | 17.2 | 18.7 | 20.1 | 21.6 | 23.0 | 24.5 | 26.0 | 27.4 | 28.9 | 30.3 |  |
| 547 | 55 | 31.8 | 33.3 | 34.7 | 36.1 | 37.6 | 39.0 | 40.5 | 41.9 | 43.4 | 44.8 |  |
| 548 | 55 | 46.3 | 47.7 | 49.2 | 50.6 | 52.1 | 53.5 | 55.0 | 56.4 | 57.9 | 59.3 |  |
| 549 | 55 | 60.8 | 62.2 | 63.7 | 65.1 | 66.6 | 68.0 | 69.5 | 70.9 | 72.4 | 73.8 |  |
| 550 | 55 | 75.3 | 76.7 | 78.2 | 79.6 | 81.1 | 82.5 | 84.0 | 85.4 | 86.9 | 88.3 |  |
| 551 | 55 | 89.8 | 91.2 | 92.7 | 94.1 | 95.6 | 97.0 | 98.4 | 99.9 |  |  |  |
| 551 | 56 |  |  |  |  |  |  |  |  | 01.3 | 02.8 | 10.1 |
| 552 | 56 | 04.2 | 05.6 | 07.1 | 08.5 | 10.0 | 11.4 | 12.8 | 14.3 | 15.7 | 17.2 | 20.3 |
| 553 | 56 | 18.6 | 20.0 | 21.5 | 22.9 | 24.4 | 23.8 | 27.2 | 28.7 | 30.1 | 31.6 | 30.4 |
| 554 | 56 | 33.0 | 34.4 | 3.5 .9 | 37.3 | 38.8 | 40.2 | 41.6 | 43.1 | 41.5 | 46.0 | 40.6 |
| 555 | 56 | 47.4 | 48.8 | 50.3 | 51.7 | 53.1 | 54.5 | 56.0 | 57.4 | 58.8 | 60.3 | $5,0.7$ |
| 556 | 56 | 61.7 | 63.1 | 64.6 | 66.0 | 67.4 | 68.5 | 70.3 | 71.7 | 73.1 | 746 | 610.3 |
| 557 | 56 | 76.0 | 77.4 | 78.9 | 80.3 | 81.7 | 83.1 | 84.6 | 86.0 | 87.4 | 85.9 | 71.0 |
| 5.58 | 57 | 90.3 | 91.7 | 93.2 | 94.6 | 96.0 | 97.4 | 98.9 |  |  |  | 81.2 |
| 558 | 57 |  |  |  |  |  |  |  | 00.3 | 01.7 | 03.2 | 9) 1.3 |
| 559 | 57 | 04.6 | 06.0 | 07.4 | 08.9 | 10.3 | 11.7 | 13.1 | 14.5 | 16.0 | 17.4 |  |
| 560 | 57 | 18.8 | 20.2 | 21.6 | 28.1 | 24.5 | 25.9 | 27.3 | 28.7 | 30.2 | 31.6 |  |
| 561 | 57 | 33.0 | 34.4 | 3.5 .8 | 37.3 | 38.7 | 40.1 | 41.5 | 42.9 | 4.4 .4 | 45.8 |  |
| 562 | 57 | 47.2 | 48.6 | 50.0 | 51.4 | 52.8 | 542 | 55.7 | 57.1 | 58.5 | 59.9 |  |
| 563 | 57 | 61.3 | 627 | 64.1 | 65.5 | 66.9 | 68.3 | 69.8 | 71.2 | 72.6 | 74.0 |  |
| 564 | 57 | 75.4 | 76.8 | 78.2 | 79.6 | 81.0 | 82.4 | 83.9 | 85.3 | 86.7 | 88.1 |  |
| 565 | 57 | 89.5 | 90.9 | 92.4 | 93.8 | 95.2 | 96.6 | 98.0 | 99.4 |  |  |  |
| $\left\{\begin{array}{l} \text { Birom- } \\ \text { eter } \\ \text { Horh } \end{array}\right.$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for pab 0.01 mm . |

56.5 to $605^{m \mathrm{~m}}$.

| Burnin. eter Horh. | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\left\|\begin{array}{c} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} . \end{array}\right\|$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. $58$ | Metres. | Metres. | Metres. | Netres. | Metres. | Metres. | Metres. | Metres. | Metres. 00.8 | Metres 02.2 | Metr. |
| 566 | 58 | 0:3.6 | 0.5 .0 | 06.4 | 07.8 | 09.2 | 10.6 | 12.1 | 13.5 | 14.9 | 16.3 |  |
| 567 | 58 | 17.7 | 19.1 | 20.5 | 21.9 | 23.3 | 24.7 | 26.1 | 27.5 | 28.9 | 30.3 |  |
| 568 | 58 | 31.7 | 33.1 | 34.5 | 3.9.9 | 37.3 | 38.7 | 40.1 | 41.5 | 42.9 | 44.3 |  |
| 569 | 58 | 45.7 | 47.1 | 49.5 | 49.9 | 51.3 | 52.7 | 54.1 | 55.5 | 56.9 | 58.3 |  |
| 570 | 58 | 59.7 | 61.1 | 62.5 | 63.9 | 65.3 | 66.7 | 68.1 | 69.5 | 70.9 | 72.3 |  |
| 571 | 58 | 73.7 | 75.1 | 76.5 | 77.9 | 79.3 | 80.6 | 82.0 | 83.4 | 84.8 | 86.2 |  |
| 572 | 58 | 87.6 | 89.0 | 90.4 | 91.8 | 93.2 | 94.5 | 95.9 | 97.3 | 98.7 |  |  |
| 572 | 59 |  |  |  |  |  |  |  |  |  | 00.1 |  |
| 573 | 59 | 01.5 | 02.9 | 04.3 | 0.5 .7 | 07.1 | 08.4 | 09.8 | 11.2 | 12.6 | 14.0 |  |
| 574 | 59 | 15.4 | 16.8 | 18.2 | 19.6 | 21.0 | 23.3 | 23.7 | 25.1 | 26.5 | 27.9 |  |
| 575 | 59 | 29.3 | 30.7 | 32.1 | 33.4 | 34.8 | 36.2 | 37.6 | 39.0 | 40.3 | 41.7 |  |
| 576 | 59 | 43.1 | 44.5 | 45.9 | 47.2 | 48.6 | 50.0 | 51.4 | 52.8 | 54.1 | 55.5 | 10.1 |
| 577 | 59 | 50.9 | 58.3 | 59.7 | 61.0 | 62.4 | 63.8 | 65.2 | 66.6 | 67.9 | 69.3 | $2{ }^{2} \mathbf{0 . 3}$ |
| 578 | 59 | 70.7 | 72.1 | 73.5 | 74.8 | 76.2 | 77.6 | 79.0 | 80.4 | 81.7 | 83.1 |  |
| 579 | 59 | 84.5 | S5.9 | 87.2 | 88.6 | 90.0 | 91.3 | 92.7 | 94.1 | 95.5 | 96.8 |  |
| 550 | 59 | 98.2 | 99.6 |  |  |  |  |  |  |  |  | $\begin{array}{ll}5 & 0.7\end{array}$ |
| 580 | 60 |  |  | 00.9 | 02.3 | 03.7 | 05.0 | 06.4 | 07.8 | 09.2 | 10.5 | $6{ }_{6}^{6} 0.8$ |
| 581 | 60 | 11.9 | 13.3 | 14.6 | 16.0 | 17.4 | 18.7 | 20.1 | 21.5 | 22.9 | 24.2 | 71.0 |
| 582 | 60 | 25.6 | 27.0 | 28.3 | 29.7 | 31.1 | 32.4 | 33.8 | 35.2 | 36.6 | 37.9 | 8 1.1 |
| 583 | 60 | 39.3 | 40.7 | 42.0 | 43.4 | 44.7 | 46.1 | 47.5 | 48.8 | 50.2 | 51.5 | 91.2 |
| 584 | 60 | 52.9 | 54.3 | 5.5 | 57.0 | 58.4 | 59.7 | 61.1 | 62.5 | 63.9 | 65.2 |  |
| 585 | 60 | 66.6 | 68.0 | 69.3 | 707 | 720 | 73.4 | 74.8 | 76.1 | 77.5 | 78.8 |  |
| 596 | 60 | 50.2 | 81.6 | 82.9 | 84.3 | 85.6 | 87.0 | 88.4 | 89.7 | 91.1 | 92.4 |  |
| 587 | 60 | 93.8 | 95.1 | 96.5 | 97.8 | 99.2 |  |  |  |  |  |  |
| 587 | 61 |  |  |  |  |  | 00.5 | 01.9 | 03.2 | 04.6 | 0.5 .9 |  |
| 588 | 61 | 07.3 | 08.6 | 10.0 | 11.3 | 12.7 | 14.0 | 15.4 | 16.7 | 18.1 | 19.4 |  |
| 589 | 61 | 20.8 | 22.1 | 23.5 | 24.8 | 26.2 | 27.5 | 28.9 | 30.2 | 31.6 | 32.9 |  |
| 590 | 61 | 34.3 | 35.6 | 37.0 | 38.3 | 39.7 | 41.0 | 12.4 | 43.7 | 45.1 | 46.4 |  |
| 591 | 61 | 47.8 | 49.1 | 50.5 | 51.8 | 53.2 | 54.5 | 55.9 | 57.2 | 58.6 | 59.9 |  |
| 592 | 61 | 61.3 | 62.6 | 64.0 | 65.3 | 66.7 | 68.0 | 69.3 | 70.7 | 72.0 | 73.4 |  |
| 593 | 61 | 74.7 | 76.0 | 77.4 | 78.7 | 80.1 | 81.4 | 82.7 | 84.1 | 85.4 | 86.8 |  |
| 594 | 61 | 88.1 | 89.4 | 90.8 | 92.1 | 93.5 | 94.8 | 96.1 | 97.5 | 98.8 |  |  |
| 594 | 62 |  |  |  |  |  |  |  |  |  | 00.2 |  |
| 59.5 | 62 | 01.5 | 02.8 | 04.2 | 05.5 | 06.9 | 08.2 | 09.5 | 10.9 | 12.2 | 13.6 |  |
| 596 | 62 | 14.9 | 16.2 | 17.6 | 18.9 | 20.2 | 21.5 | 22.9 | 24.2 | 25.5 | 26.9 |  |
| 597 | 62 | 28.2 | 29.5 | 30.9 | 32.2 | 33.6 | 34.9 | 36.2 | 37.6 | 38.9 | 40.3 |  |
| 598 | 62 | 41.6 | 42.9 | 44.3 | 45.6 | 46.9 | 48.2 | 49.6 | 50.9 | 52.2 | 53.6 |  |
| 599 | 62 | 54.9 | 56.2 | 57.6 | 58.9 | 60.2 | 61.5 | 62.9 | 64.2 | 65.5 | 66.9 |  |
| 600 | 62 | 68.2 | 69.5 | 70.8 | 72.2 | 73.5 | 74.8 | 76.1 | 77.1 | 78.8 | 80.1 |  |
| 601 | 62 | 81.4 | 82.7 | 84.1 | 85.4 | 86.7 | 88.0 | 89.4 | 90.7 | 92.0 | 93.4 |  |
| 602 | 62 | 94.7 | 96.0 | 97.3 | 98.7 |  |  |  |  |  |  |  |
| 602 | 63 |  |  |  |  | 00.0 | 01.3 | 02.6 | 03.9 | 05.3 | 06.6 |  |
| $(6) 3$ | 63 | 07.9 | 09.2 | 10.5 | 11.9 | 13.2 | 14.5 | 15.8 | 17.1 | 18.5 | 19.8 |  |
| 604 | 63 | 21.1 | 22.4 | 23.7 | 25.1 | 26.4 | 27.7 | 29.0 | 30.3 | 31.7 | 33.0 |  |
| 605 | 63 | 34.3 | 35.6 | 36.9 | 38.2 | 39.5 | 40.8 | 12.2 | 43.5 | 44.8 | 46.1 |  |
| $\begin{aligned} & \text { Rarom. } \\ & \text { eler } \\ & \text { Horb } \end{aligned}$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\left\|\begin{array}{c} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} \end{array}\right\|$ |

606 to $61^{\mathrm{mm}}$.

| Burorr eter H or h . | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\left\|\begin{array}{c} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} . \end{array}\right\|$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. M | Metr | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Netres. |  |  | Metr. |
| 606 | 63 | 47.4 | 48.7 | 50.0 | 51.3 | 2. | 53.9 | 5.5.3 | 6.6 | 7.9 | 59. |  |
| 607 | 63 | 60.5 | 61.8 | 63.1 | 64.5 | 63.8 | 67.1 | 68.4 | 69.7 | 71.1 | 72.4 |  |
| 608 | 63 | 73.7 | 75.0 | 76.3 | 77.6 | 78.9 | 802 | 81.5 | 82.8 | 84.1 | 8.5 .4 |  |
| 609 | 63 | 86.7 | 88.0 | 89.3 | 90.6 | 91.9 | 93.2 | 94.6 | 95.9 | 97.2 | 98.5 |  |
| 610 | 63 | 99.3 |  |  |  |  |  |  |  |  |  |  |
| 610 | 61 |  | 01.1 | 02.4 | 03.7 | 05.0 | 063 | 07.6 | 08.9 | 10.2 | 11.5 |  |
| 611 | 64 | 12.8 | 141 | 15.4 | 16.7 | 18.0 | 19.3 | 20.7 | 22.0 | 233 | 24.6 |  |
| 312 | 64 | 25.9 | 27.2 | 28.5 | 29.8 | 31.1 | 32.4 | 33.7 | 35.0 | 36.3 | 37.6 |  |
| 613 | 64 | 35.9 | 40.2 | 41.5 | 42.8 | 44.1 | 45.4 | 46.7 | 48.0 | 49.3 | 50.6 |  |
| 614 | 64 | 51.9 | 53.2 | 54.5 | 55.8 | 57.1 | 58.3 | 59.6 | 60.9 | 6.2 | 63.5 |  |
| 615 | 61 | 64.8 | 66.1 | 67.4 | 68.7 | 70.0 | 71.2 | 72.5 | 73.8 | 75.1 | 76.4 |  |
| 616 | 64 | 77.7 | 79.0 | 50.3 | 81.6 | 82.9 | 84.2 | 85.5 | 86.8 | 88.1 | 89.4 |  |
| 617 | 64 | 90.7 | 92.0 | 93.3 | 94.6 | 93.9 | 97.1 | 98.4 | 99.7 |  |  |  |
| 617 | 65 |  |  |  |  |  |  |  |  | 01.0 | 02.3 |  |
| 618 | 65 | 03.6 | 04.9 | 06.2 | 07.4 | 03.7 | 10.0 | 11.3 | 12.6 | 13.8 | 15.1 |  |
| 619 | 6.5 | 16.4 | 17.7 | 19.0 | 20.3 | 21.6 | 22.8 | 24.1 | 25.4 | 26.7 | 28.0 |  |
| 620 | 6.5 | 29.3 | 30.6 | 31.9 | 33.1 | 34.4 | 35.7 | 37.0 | 38.3 | 39.5 | 40.8 |  |
| 621 | 6.5 | 42.1 | 43.4 | 4.4 | 45.9 | 47.2 | 48.5 | 49.8 | 51.1 | 52.3 | 53.6 | $1{ }^{1} 0.1$ |
| 622 | 65 | 54.9 | 56.2 | 57.5 | 58.7 | 60.0 | 61.3 | 62.6 | 639 | 65.1 | 66.4 | 20.2 |
| 623 | 65 | 67.7 | 69.0 | 70.3 | 71.5 | 72.8 | 74.1 | 75.4 | 76.7 | 77.9 | 79.2 | 30.4 |
| 624 | 6.5 | 80.5 | 81.8 | 83.0 | 84.3 | 85.6 | S6.8 | 88.1 | 89.4 | 90.7 | 91.9 | 4 0.5 <br> 5 0.6 |
| 62.5 | 6.5 | 93.2 | 94.5 | 95.8 | 97.0 | 98.3 | 99.6 |  |  |  |  | 6 0.8 <br> 7 0.9 |
| 62.5 | 66 |  |  |  |  |  |  | 00.9 | 02.2 | 03.4 16.2 | 01.7 17.4 | $\begin{array}{ll}7 & 0.9 \\ 8 & 1.9\end{array}$ |
| 626 | 66 | 06.0 | 07.3 | 08.5 | 09.8 | 11.1 | 12.3 | 13.6 | 14.9 27.6 | 16.2 28.9 | 17.4 30.1 | $\begin{array}{ll} 8 & 1.0 \\ 9 & 1.1 \end{array}$ |
| 627 | 66 | 18.7 | 20.0 | 21.2 | 22.5 | 23.3 | 25.0 | 26.3 | 27.6 | 28.9 | 30.1 | $9 \quad 1.1$ |
| 628 | 66 | 31.4 | 32.7 | 33.9 | 36.2 | 56.4 | 37.7 | 39.0 | 40.2 | 41.5 | 12.7 |  |
| 629 | 66 | 44.0 | 45.3 | 46.5 | 47.8 | 49.1 | 50.3 | 51.6 | 52.9 | 54.2 | 5.5 |  |
| 630 | 66 | 56.7 | 58.0 | 59.2 | 60.5 | 61.7 | 63.0 | 64.3 | 65.5 | 66.3 | 68.0 |  |
| 631 | 66 | 69.3 | 70.6 | 71.8 | 73.1 | 74.4 | 75.6 | 76.9 | 78.2 | 79.5 | 80.7 |  |
| 632 | 66 | 82.0 | 83.2 | 84.5 | 85.7 | 87.0 | 88.2 | 89.5 | 90.7 | 92.0 | 93.2 |  |
| 633 | 66 | 94.5 | 95.8 | 97.0 | 98.3 | 99.5 |  |  |  |  |  |  |
| 6:3 | 67 |  |  |  |  |  | 00.8 | 02.1 | 03.3 | 04.6 | 05.8 |  |
| 63.4 | 67 | 07.1 | 08.4 | 09.6 | 10.9 | 12.1 | 13.4 | 14.7 | 15.9 | 17.2 | 18.4 |  |
| 63.5 | 67 | 19.7 | 20.9 | 2.2 | 23.4 | 24.7 | 2.5 .9 | 27.2 | 25.4 | 29.7 | 30.9 |  |
| 6336 | 67 | 32.2 | 33.4 | 34.7 | 35.9 | 37.2 | 38.4 | 39.7 | 40.9 | 42.2 | 43.4 |  |
| 6\%7 | 67 | 4.7 | 45.9 | 47.2 | 48.4 | 49.7 | 50.9 | 52.2 | 53.4 | 54.7 | 55.9 |  |
| 635 | 67 | 57.2 | 58.4 | 59.7 | 60.9 | 62.2 | 63.4 | 64.7 | 65.9 | 67.2 | 68.4 |  |
| 639 | 67 | 69.7 | 70.9 | 72.2 | 73.4 | 74.7 | 75.9 | 77.1 | 75.4 | 79.6 | 80.9 |  |
| 6 \% | 67 | 82.1 | 83.3 | 84.6 | 85.8 | 87.1 | 88.3 | 89.6 | 90.8 | 92.1 | 93.3 |  |
| 641 | 67 | 9 4.6 | 95.8 | 97.1 | 98.3 | 99.6 |  |  |  |  |  |  |
| 6.41 | 68 |  |  |  |  |  | 00.8 | 02.0 | 03.3 | 16.9 | 0.9 .8 18.2 |  |
| 642 | 63 | 07.0 | 08.2 | 09.5 | 10.7 | 12.0 | 13.2 | 14.4 | 13.7 | 16.9 | 15.2 30.5 |  |
| 643 | 68 | 19.4 | 20.6 | 21.9 | 23.1 | 24.3 | 2.5.5 | 26.8 |  |  | 30.5 |  |
| 644 | 65 | 31.7 | 32.9 | 34.2 | 35.4 | 36.7 | 37.9 | 39.1 |  |  | 42.9 55.2 |  |
| 64.5 | 69 | 4.1 | 45.3 | 46.6 | 47.8 | 49.0 | 50.2 | 51.5 | 52.7 | 53.9 | 63.2 |  |
| 646 | 68 | 56.4 | 57.6 | 58.9 | 60.1 | 61.3 | 62.5 | 63.8 | 6.5 .0 | 66.2 | 67.5 |  |
| 647 | 68 | 68.7 | 69.9 | 71.2 | 72.4 | 73.6 | 74.8 | 76.1 | 77.3 | 78.5 | 79.8 |  |
| Brom- eter Horh. | N | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts fir each 0.04 mm 0.1 mm |

648 to $689^{\mathrm{mm} .}$.

| Barom eter H or h . | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.1 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { for each } \\ 0.01 \mathrm{~mm} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Netres. | Metres. | Metres. | IIetres. | Netres. | Metres. | Metres. | Netres. | Metres. | Metres. | Metr. |
| 648 | 68 | 81.0 | 52.2 | 83.5 | 84.7 | 85.9 | 87.1 | 88.4 | 89.6 | 90.8 | 92.1 |  |
| 649 | 68 | 93.3 | 94.5 | 95.8 | 97.0 | 98.2 | 99.4 |  |  |  |  |  |
| 619 | 69 |  |  |  |  |  |  | 00.7 | 01.9 | 03.1 | 04.4 |  |
| 6.30 | 69 | 05.6 | 06.8 | 09.0 | 09.3 | 10.5 | 11.7 | 12.9 | 14.1 | 15.4 | 16.6 |  |
| 6.51 | 69 | 17.8 | 19.0 | 20.2 | 21.5 | 22.7 | 23.9 | 25.1 | 26.3 | 27.6 | 25.8 |  |
| 6.52 | 69 | 30.0 | 31.2 | 32.4 | 33.7 | 34.9 | 36.1 | 37.3 | 38.5 | 39.8 | 41.0 |  |
| 6.33 | 69 | 42.2 | 43.4 | 44.6 | 45.9 | 17.1 | 48.3 | 19.5 | 50.7 | 52.0 | 53.2 |  |
| 6.94 | 69 | 54.4 | 5.6 | 56.8 | 58.1 | 59.3 | 60.5 | 61.7 | 62.9 | 64.2 | 65.4 |  |
| 6.55 | 69 | 66.6 | 67.8 | 69.0 | 70.2 | 71.4 | 72.6 | 73.9 | 75.1 | 76.3 | 77.5 |  |
| 6.56 | 69 | 78.7 | 79.9 | 81.1 | S.2.4 | 83.6 | 84.8 | 86.0 | 87.2 | 88.5 | 59.7 |  |
| $6.5 \%$ | 69 | 90.9 | 92.1 | 93.3 | 94.5 | 95.7 | 96.9 | 98.2 | 99.4 |  |  |  |
| 6.57 | 70 |  |  |  |  |  |  |  |  | 00.6 | 01.8 |  |
| 6.58 | 70 | 03.0 | 04.2 | 05.4 | 06.6 | 07.8 | 09.0 | 10.3 | 11.5 | 12.7 | 13.9 |  |
| 6.59 | 70 | 15.1 | 16.3 | 17.5 | 18.7 | 19.9 | 21.1 | 2.2.4 | 23.6 | 24.8 | 26.0 |  |
| 660 | 70 | 27.2 | 28.4 | 29.6 | 30.8 | 32.0 | 33.2 | 34.4 | 35.6 | 36.8 | 35.0 | 10.1 |
| 661 | 70 | 39.2 | 40.4 | 41.6 | 42.8 | 44.0 | 45.2 | 46.4 | 47.6 | 48.8 | 50.0 | 20.2 |
| 662 | 70 | 51.2 | 52.4 | 53.6 | 54.8 | 56.0 | 57.2 | 58.5 | 59.7 | 60.9 | 62.1 | $3{ }^{3} \mathbf{0 , 4}$ |
| 663 | 70 | 63.3 | 64.5 | 65.7 | 66.9 | 65.1 | 69.3 | 70.5 | 71.7 | 72.9 | 74.1 | 40.5 |
| 664 | 70 | 75.3 | 76.5 | 77.7 | 78.9 | S0.1 | 81.2 | 8.4 | \$3.6 | S4.8 | 86.0 | 50.6 |
| 66.5 | 70 | 87.2 | 88.4 | S9.6 | 90.8 | 92.0 | 93.2 | 94.4 | 95.6 | 96.8 | 98.0 | 60.7 |
| 666 | 70 | 99.2 |  |  |  |  |  |  |  |  |  | 70.8 |
| 666 | 71 |  | 00.4 | 01.6 | 02.8 | 04.0 | 05.2 | 06.4 | 07.6 | 08.8 | 10.0 | 81.0 |
| 667 | 31 | 11.2 | 12.4 | 13.6 | 14.8 | 16.0 | 17.1 | 18.3 | 19.5 | 20.7 | 21.9 | 9 l 1.1 |
| 668 | 71 | 23.1 | 24.3 | 2.5 | 26.7 | 27.9 | 29.0 | 30.2 | 31.4 | 32.6 | 33.8 |  |
| 669 | 71 | 35.0 | 36.2 | 37.4 | 38.6 | 39.8 | 40.9 | 42.1 | 43.3 | 44.5 | 45.7 |  |
| 670 | 71 | 46.9 | 48.1 | 49.3 | 50.5 | 51.7 | 52.8 | 54.0 | 55.2 | 56.4 | 57.6 |  |
| 671 | 71 | 58.8 | 60.0 | 61.2 | 62.3 | 63.5 | 64.7 | 65.9 | 67.1 | 68.2 | 69.4 |  |
| 672 | 71 | 70.6 | 71.8 | 73.0 | 74.2 | 75.4 | 76.5 | 77.7 | 78.9 | 80.1 | 81.3 |  |
| 673 | 71 | 82.5 | 83.7 | 84.9 | 86.0 | 87.2 | 88.4 | 89.6 | 90.8 | 91.9 | 93.1 |  |
| 674 | 71 | 94.3 | 95.5 | 96.7 | 97.8 | 99.0 |  |  |  |  |  |  |
| 634 | 72 |  |  |  |  |  | 00.2 | 01.4 | 02.6 | 03.7 | 04.9 |  |
| 675 | 22 | 06.1 | 07.3 | 08.5 | 09.6 | 10.8 | 12.0 | 13.2 | 14.4 | 15.5 | 16.7 |  |
| 676 | 72 | 17.9 | 19.1 | 20.3 | 21.4 | 22.6 | 23.8 | 2.5.0 | 26.2 | 27.3 | 28.5 |  |
| 677 | 72 | 29.7 | 30.9 | 32.0 | 33.2 | 34.4 | 35.5 | 36.7 | 37.9 | 39.1 | 40.2 |  |
| 678 | 72 | 41.4 | 42.6 | 43.8 | 44.9 | 16.1 | 47.3 | 18.5 | 49.7 | 50.8 | 52.0 |  |
| 679 | 72 | 53.2 | 54.4 | 55.5 | 56.7 | 57.9 | 59.0 | 60.2 | 61.4 | 62.6 | 63.7 |  |
| 650 | 72 | 64.9 | 66.1 | 67.2 | 68.4 | 69.6 | 70.7 | 71.9 | 73.1 | 74.3 | 75.4 |  |
| 681 | 72 | 76.6 | 77.8 | 78.9 | 80.1 | 81.3 | 82.4 | 83.6 | 84.8 | 86.0 | 87.1 | 1 \| 0.1 |
| 682 | 72 | 88.3 | 89.5 | 90.6 | 91.8 | 93.0 | 94.1 | 95.3 | 96.5 | 97.7 | 98.8 | 20.2 |
| 653 | 73 | 00.0 | 01.2 | 02.3 | 03.5 | 04.6 | 05.8 | 07.0 | 08.1 | 09.3 | 10.4 | 3 0.3 |
| 634 | 73 | 11.6 | 12.8 | 13.9 | 15.1 | 16.2 | 17.4 | 18.6 | 19.7 | 20.9 | 22.0 | 40.5 |
| 655 | 73 | 23.2 | 24.4 | 2.5.5 | 26.7 | 27.8 | 29.0 | 30.2 | 31.3 | 32.5 | 33.6 | $5 \quad 0.6$ |
| 656 | 73 | 34.8 | 36.0 | 37.1 | 38.3 | 39.4 | 40.6 | 41.5 | 42.9 | 44.1 | 45.2 | $\begin{array}{lll}6 & 0.7\end{array}$ |
| 657 | 73 | 46.4 | 47.6 | 48.7 | 49.9 | 51.0 | 52.2 | 53.4 | 54.5 | 55.7 | 56.8 | 70.8 |
| 658 | 73 | 58.0 | 59.2 | 60.3 | 61.5 | 62.6 | 63.8 | 65.0 | 66.1 | 67.3 | 68.4 | 8 0.9 |
| 689 | 73 | 69.6 | 70.7 | 71.9 | 73.0 | 74.2 | 75.3 | 76.5 | 77.6 | 78.8 | 79.9 | 91.1 |
| $\begin{aligned} & \text { Barom. } \\ & \text { eter } \\ & \text { Hor } h \end{aligned}$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{aligned} & \text { Parts } \\ & \text { finr each } \\ & 001 \text { mo. } \end{aligned}$ |

690 to $730^{\mathrm{mm}}$.

| $\left\{\begin{array}{l} \text { B irom- } \\ \text { eter } \\ \mathrm{H} \text { or } \mathrm{h} . \end{array}\right.$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{aligned} & \text { Parts } \\ & \text { for each } \\ & 0.01 \mathrm{~mm} . \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milti. | Metr | Metres. | Metres. | Metres | Metres. | Metres. | Netres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 690 | 73 | 81.1 | 82.3 | 83.4 | 84.6 | 85.7 | 86.9 | 88.1 | 89.2 | 90.4 | 91.5 |  |
| 691 | 73 | 92.7 | 93.8 | 95.0 | 96.1 | 97.3 | 98.4 | 99.6 |  |  |  |  |
| 691 | 74 |  |  |  |  |  |  |  | 00.7 | 01.9 | 03.0 |  |
| 692 | 74 | 04.2 | 05.3 | 06.5 | 07.6 | 08.8 | 09.9 | 11.1 | 12.2 | 13.4 | 14.5 |  |
| 693 | 74 | 15.7 | 16.8 | 18.0 | 19.1 | 20.3 | 21.4 | 22.6 | 23.7 | 24.9 | 26.0 |  |
| 694 | 74 | 27.2 | 28.3 | 29.5 | 30.6 | 31.8 | 32.9 | 34.1 | 35.2 | 36.4 | 37.5 |  |
| 695 | 74 | 35.7 | 39.8 | 41.0 | 42.1 | 43.3 | 44.4 | 45.5 | 46.7 | 47.8 | 49.0 |  |
| 696 | 74 | 50.1 | 51.2 | 52.4 | 53.5 | 54.7 | 5.5 .8 | 56.9 | 58.1 | 59.2 | 60.4 |  |
| 697 | 74 | 61.5 | 62.6 | 63.8 | 64.9 | 66.1 | 67.2 | 68.3 | 69.5 | 70.6 | 71.8 |  |
| 698 | 74 | 72.9 | 74.0 | 75.2 | 76.3 | 77.5 | 78.6 | 79.7 | 80.9 | 82.0 | 83.2 |  |
| 699 | 74 | 84.3 | 85.4 | 86.6 | 87.7 | 88.9 | 90.0 | 91.1 | 92.3 | 93.4 | 94.6 |  |
| 700 | 74 | 95.7 | 96.8 | 98.0 | 99.1 |  |  |  |  |  |  |  |
| 700 | 75 |  |  |  |  | 00.3 | 01.4 | 02.5 | 03.7 | 04.8 | 06.0 |  |
| 701 | 75 | 07.1 | 08.2 | 09.4 | 10.5 | 11.6 | 12.7 | 13.9 | 15.0 | 16.1 | 17.3 |  |
| 702 | 75 | 18.4 | 19.5 | 20.7 | 21.8 | 23.0 | 24.1 | 25.2 | 26.4 | 27.5 | 28.7 |  |
| 703 | 75 | 29.8 | 30.9 | 32.1 | 33.2 | 34.3 | 35.4 | 36.6 | 37.7 | 32.8 | 40.0 |  |
| 704 | 75 | 41.1 | 42.2 | 43.4 | 4.5 | 45.6 | 46.7 | 47.9 | 49.0 | 50.1 | 51.3 |  |
| 705 | 75 | 52.4 | 53.5 | 54.7 | 55.8 | 56.9 | 59.0 | 59.2 | 60.3 | 61.4 | 62.6 |  |
| 706 | 75 | 63.7 | 64.8 | 66.0 | 67.1 | 68.2 | 69.3 | 70.5 | 71.6 | 72.7 | 73.9 |  |
| 707 | 75 | 75.0 | 76.1 | 77.2 | 78.4 | 79.5 | 80.6 | 81.7 | 82.8 | 84.0 | 85.1 |  |
| 708 | 75 | 86.2 | 87.3 | 88.5 | 89.6 | 90.7 | 91.8 | 93.0 | 94.1 | 95.2 | 96.4 |  |
| 709 | 75 | 97.5 | 98.6 | 99.7 |  |  |  |  |  |  |  |  |
| 709 | 76 |  |  |  | 00.9 | 02.0 | 03.1 | 04.2 | 05.3 | 06.5 | 07.6 |  |
| 710 | 76 | 08.7 | 09.8 | 10.9 | 12.1 | 13.2 | 14.3 | 15.4 | 16.5 | 17.7 | 18.8 |  |
| 711 | 76 | 19.9 | 21.0 | 2.2 .1 | 23.3 | 24.4 | 25.5 | 26.6 | 27.7 | 28.9 | 30.0 |  |
| 712 | 76 | 31.1 | 32.2 | 33.3 | 34.4 | 35.5 | 36.6 | 37.8 | 38.9 | 40.0 | 41.1 | 10.1 |
| 713 | 76 | 42.2 | 43.3 | 44.4 | 45.6 | 46.7 | 47.5 | 45.9 | 50.0 | 51.2 | 52.3 | 20.2 |
| 714 | 76 | 53.4 | 54.5 | 55.6 | 56.8 | 57.9 | 59.0 | 60.1 | 61.2 | 62.4 | 63.5 | 30.3 |
| 715 | 76 | 64.6 | 65.7 | 66.8 | 67.9 | 69.0 | 70.1 | 71.3 | 72.4 | 73.5 | 74.6 | 40.4 |
| 716 | 76 | 75.7 | 76.5 | 77.9 | 79.0 | 80.1 | 81.2 | 82.4 | 83.5 | 84.6 | 85.7 | 50.5 |
| 717 | 76 | 86.8 | 87.9 | 89.0 | 90.1 | 91.2 | 92.3 | 93.5 | 94.6 | 95.7 | 96.8 | 60.7 |
| 718 | 76 | 97.9 | 99.0 |  |  |  |  |  |  |  |  | 70.8 |
| 718 | 77 |  |  | 00.1 | 01.2 | 02.3 | 03.4 | 04.6 | 05.7 | 06.8 | 07.9 | $8 \quad 0.9$ |
| 719 | 77 | 09.0 | 10.1 | 11.2 | 12.3 | 13.4 | 14.5 | 13.7 | 16.9 | 17.9 | 19.0 | 91.0 |
| 720 | 77 | 20.1 | 21.2 | 22.3 | 23.4 | 24.5 | 2.5. 6 | 26.7 | 27.8 | 28.9 | 30.0 |  |
| 721 | 77 | 31.1 | 32.2 | 33.3 | 34.4 | 35.5 | 36.6 | 37.7 | 38.8 | 39.9 | 41.0 |  |
| 722 | 77 | 42.1 | 43.2 | 4.3 | 45.4 | 46.5 | 47.6 | 18.7 | 49.8 | 50.9 | 52.0 |  |
| 723 | 77 | 53.1 | 54.2 | 55.3 | 56.4 | 57.5 | 55.6 | 59.8 | 60.9 | 62.0 | 63.1 |  |
| 724 | 77 | 64.2 | 65.3 | 66.4 | 67.5 | 68.6 | 69.6 | 70.7 | 71.8 | 72.9 | 74.0 |  |
| 725 | 77 | 75.1 | 76.2 | 77.3 | 78.4 | 79.5 | 80.6 | 81.7 | 82.8 | 83.9 | 85.0 |  |
| 726 | 77 | 86.1 | 87.2 | 58.3 | 89.4 | 90.5 | 91.6 | 9.2 .7 | 93.8 | 94.9 | 96.0 |  |
| 727 | 77 | 97.1 | 98.2 | 99.3 |  |  |  |  |  |  |  |  |
| 727 | 78 |  |  |  | 00.4 | 01.5 | 02.5 | 03.6 | 04.7 | 05.8 | 06.9 |  |
| 729 | 78 | 08.0 | 09.1 | 10.2 | 11.3 | 12.4 | 135 | 14.6 | 15.7 | 16.8 | 17.9 |  |
| 724 | 78 | 19.0 | 201 | 21.2 | 22.3 | 23.4 | 24.4 | 25.5 | 26.6 | 27.7 | 28.8 |  |
| 730 | 78 | 29.9 | 31.0 | 32.1 | 33.3 | 34.3 | 353 | 36.4 | 37.5 | 38.6 | 39.7 |  |
| $\left\lvert\, \begin{aligned} & \text { Barmm- } \\ & \text { eter } \\ & \text { Hor h. } \end{aligned}\right.$ | N. | 0.0 | 0.1 | O. ${ }^{2}$ | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | $\begin{gathered} \text { Parts } \\ \text { for each } \\ 001 \mathrm{~mm} . \end{gathered}$ |

731 to $\mathbf{7 7 0}^{\mathrm{mm}}$.

| Barom eter Horh. | N. | 0.0 | 6.1 | O.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for sawn 0.01 mm . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Metres. | Metres. | Metres | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 731 | 78 | 40.8 | 41.9 | 43.0 | 4.1 | 45.2 | 46.2 | 47.3 | 48.4 | 49.5 | 50.6 |  |
| 732 | 78 | 51.7 | 52.8 | 53.9 | 54.9 | 56.0 | 57.0 | 58.2 | 59.3 | 60.3 | 61.4 |  |
| 733 | 78 | 62.5 | 63.6 | 64.7 | 65.8 | 66.9 | 67.9 | 69.0 | 70.1 | 71.2 | 72.3 |  |
| 734 | 78 | 73.4 | 74.5 | 75.6 | 76.6 | 77.7 | 78.8 | 79.9 | 81.0 | 82.0 | 83.1 |  |
| 735 | 78 | 84.2 | 85.3 | 86.4 | 87.5 | 88.6 | 89.6 | 90.7 | 91.8 | 92.9 | 94.0 |  |
| 736 | 78 | 95.1 | 96.2 | 97.3 | 98.3 | 99.4 |  |  |  |  |  |  |
| 736 | 79 |  |  |  |  |  | 00.5 | 01.6 | 02.7 | 03.7 | 04.8 |  |
| 737 | 79 | 05.9 | 07.0 | 08.1 | 09.1 | 10.2 | 11.3 | 12.4 | 13.5 | 14.5 | 15.6 |  |
| 738 | 79 | 16.7 | 17.8 | 18.9 | 19.9 | 21.0 | 22.1 | 23.2 | 24.3 | 25.3 | 26.4 |  |
| 739 | 79 | 27.5 | 28.6 | 29.6 | 30.7 | 31.8 | 32.8 | 33.9 | 35.0 | 36.1 | 37.1 |  |
| 740 | 79 | 38.2 | 39.3 | 40.4 | 41.4 | 42.5 | 43.6 | 44.7 | 45.8 | 46.8 | 47.9 |  |
| 741 | 79 | 49.0 | 501 | 51.1 | 52.2 | 53.3 | 54.3 | 5.5 .4 | 56.5 | 57.6 | 58.6 |  |
| 742 | 79 | 59.7 | 60.8 | 61.8 | 62.9 | 64.0 | 65.0 | 66.1 | 67.2 | 68.3 | 69.3 |  |
| 743 | 79 | 70.4 | 71.5 | 72.6 | 73.6 | 74.7 | 75.8 | 76.9 | 78.0 | 79.0 | 80.1 |  |
| 744 | 79 | 81.2 | 82.3 | 83.3 | 84.4 | 85.5 | 86.5 | 87.6 | 88.7 | 89.8 | 90.8 |  |
| 745 | 79 | 91.9 | 93.0 | 94.0 | 95.1 | 96.1 | 97.2 | 98.3 | 99.3 |  |  |  |
| 745 | 80 |  |  |  |  |  |  |  |  | 00.4 | 01.4 |  |
| 746 | 80 | 02.5 | 03.6 | 04.6 | 05.7 | 06.8 | 07.8 | 08.9 | 10.0 | 11.1 | 12.3 |  |
| 747 | 80 | 13.2 | 14.3 | 15.3 | 16.4 | 17.4 | 18.5 | 19.6 | 20.6 | 21.7 | 22.7 |  |
| 748 | 80 | 23.8 | 24.9 | 25.9 | 27.0 | 28.0 | 29.1 | 30.2 | 31.2 | 32.3 | 33.3 |  |
| 749 | 80 | 34.4 | 35.5 | 36.5 | 37.6 | 38.7 | 39.7 | 40.8 | 41.9 | 43.0 | 44.0 |  |
| 750 | S0 | 45.1 | 46.2 | 47.3 | 48.4 | 49.4 | 50.5 | 51.6 | 52.6 | 53.7 | 54.7 |  |
| 751 | 80 | 55.7 | 56.8 | 57.8 | 58.9 | 59.9 | 61.0 | 62.1 | 63.1 | 64.2 | 65.2 |  |
| 752 | 80 | 66.3 | 67.4 | 68.4 | 69.5 | 70.5 | 71.6 | 72.7 | 73.7 | 74.8 | 75.8 |  |
| 753 | 80 | 76.9 | 78.0 | 79.0 | 80.1 | 81.1 | 82.2 | 83.3 | 84.3 | 85.4 | 86.4 |  |
| 754 | 80 | 87.5 | 88.5 | 89.6 | 90.6 | 91.7 | 92.7 | 93.8 | 94.8 | 95.9 | 96.9 | ${ }_{1} 0.1$ |
| 755 | 80 | 98.0 | 99.1 |  |  |  |  |  |  |  |  | $\begin{array}{lll}2 & 0.2\end{array}$ |
| 755 | 81 |  |  | 00.1 | 01.2 | 02.2 | 03.3 | 04.4 | 05.4 | 06.5 | 07.5 | 30.3 |
| 756 | 81 | 08.6 | 09.6 | 10.7 | 11.7 | 12.8 | 13.8 | 14.9 | 15.9 | 17.0 | 18.0 | 40.4 |
| 757 | 81 | 19.1 | 20.1 | 21.2 | 22.2 | 23.3 | 24.3 | 25.4 | 26.4 | 27.5 | 28.5 | 5 0.5 |
| 758 | 81 | 29.6 | 30.6 | 31.7 | 32.7 | 33.8 | 34.8 | 35.9 | 36.9 | 38.0 | 39.0 | 60.6 |
| 759 | 81 | 40.1 | 41.1 | 42.2 | 43.2 | 44.3 | 45.3 | 46.4 | 47.4 | 48.5 | 49.5 | 7 0.7 <br> 8 0.8 |
| 760 | 81 | 50.6 | 51.6 | 52.7 | 53.7 | 54.8 | 55.8 | 56.9 | 57.9 | 59.0 | 60.0 | 9 0.9 |
| 761 | 81 | 61.1 | 62.1 | 63.2 | 64.2 | 65.3 | 66.3 | 67.3 | 68.4 | 69.4 | 70.5 |  |
| 762 | 81 | 71.5 | 72.5 | 73.6 | 74.6 | 75.7 | 76.7 | 77.8 | 78.8 | 79.9 | 80.9 |  |
| 763 | 81 | 82.0 | 83.0 | 84.1 | 85.1 | 86.2 | 87.2 | 88.2 | 89.3 | 90.3 | 91.4 |  |
| 764 | 81 | 92.4 | 93.4 | 94.5 | 95.5 | 96.6 | 97.6 | 98.6 | 99.7 |  |  |  |
| 76.4 | 82 |  |  |  |  |  |  |  |  | 00.7 | 01.8 |  |
| 76.5 | 82 | 02.8 | 03.8 | 04.9 | 0.5 .9 | 07.0 | 08.0 | 09.0 | 10.1 | 11.1 | 12.2 |  |
| 766 | 82 | 13.2 | 14.2 | 15.3 | 16.3 | 17.4 | 18.4 | 19.4 | 20.5 | 21.5 | 22.6 |  |
| 767 | 82 | 23.6 | 24.6 | 25.7 | 26.7 | 27.8 | 28.8 | 29.8 | 30.9 | 31.9 | 33.0 |  |
| 768 | 82 | 34.0 | 35.0 | 36.1 | 37.1 | 38.2 | 39.2 | 40.2 | 41.3 | 42.3 | 43.4 |  |
| 769 | 82 | 44.4 | 45.4 | 46.5 | 47.5 | 48.5 | 49.5 | 50.6 | 51.6 | 52.6 | 53.7 |  |
| 770 | 82 | 54.7 | 55.7 | 56.8 | 57.8 | 58.8 | 59.8 | 60.9 | 61.9 | 62.9 | 64.0 |  |
| $\left\lvert\, \begin{aligned} & \text { Barom- } \\ & \text { eler } \\ & \text { Hor or } . \end{aligned}\right.$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts <br> for each <br> $0.01: \mathrm{mm}$. |

771 to $810^{\text {man. }}$

| $\left\lvert\, \begin{aligned} & \text { Barom- } \\ & \text { eter } \\ & \text { Horh. } \end{aligned}\right.$ | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts for each 0.01 mm . |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Milli. | Metr. | Metres. | Metres. | Metres | Metres. | Metres. | Merres. | Metres. | Metres. | Metres. | Metres. | Metr. |
| 771 | 82 | 65.0 | 66.0 | 67.1 | 68.1 | 69.2 | 70.2 | 71.2 | 72.3 | 73.3 | 74.4 |  |
| 772 | 82 | 75.4 | 76.4 | 77.5 | 78.5 | 79.5 | 80.5 | 81.6 | 82.6 | 83.6 | 84.7 |  |
| 773 | 82 | 85.7 | 86.7 | 87.8 | 88.8 | 89.8 | 90.8 | 91.9 | 92.9 | 93.9 | 95.0 |  |
| 774 | 82 | 96.0 | 97.0 | 98.0 | 99.1 |  |  |  |  |  |  |  |
| 774 | 83 |  |  |  |  | 00.1 | 01.1 | 02.1 | 03.1 | 04.2 | 05.2 |  |
| 775 | 83 | 06.2 | 07.2 | 08.3 | 09.3 | 10.3 | 11.3 | 12.4 | 13.4 | 14.4 | 15.5 |  |
| 776 | 83 | 16.5 | 17.5 | 18.5 | 19.6 | 20.6 | 21.6 | 22.6 | 23.6 | 24.7 | 25.7 |  |
| 777 | 83 | 26.7 | 27.7 | 28.8 | 29.8 | 30.8 | 31.8 | 32.9 | 33.9 | 34.9 | 36.0 |  |
| 778 | 83 | 37.0 | 38.0 | 39.0 | 40.1 | 41.1 | 42.1 | 43.1 | 44.1 | 45.2 | 46.2 |  |
| 779 | 83 | 47.2 | 48.2 | 49.2 | 50.3 | 51.3 | 52.3 | 53.3 | 54.3 | 55.4 | 56.4 |  |
| 780 | 83 | 57.4 | 58.4 | 59.4 | 60.5 | 61.5 | 62.5 | 63.5 | 64.5 | 65.6 | 66.6 |  |
| 781 | 83 | 67.6 | 68.6 | 69.6 | 70.7 | 71.7 | 72.7 | 73.7 | 74.7 | 75.8 | 76.8 |  |
| 782 | 83 | 77.8 | 78.8 | 79.8 | 80.9 | 81.9 | 82.9 | 83.9 | 84.9 | 86.0 | 87.0 |  |
| 783 | 83 | 88.0 | 89.0 | 90.0 | 91.1 | 92.1 | 93.1 | 94.1 | 95.1 | 96.2 | 97.2 |  |
| 784 | 83 | 98.2 | 99.2 |  |  |  |  |  |  |  |  |  |
| 78.1 | 84 |  |  | 00.2 | 01.2 | 02.2 | 03.2 | 04.3 | 05.3 | 06.3 | 07.3 |  |
| 785 | 84 | 08.3 | 09.3 | 10.3 | 11.4 | 12.4 | 13.4 | 14.4 | 15.4 | 16.5 | 17.5 |  |
| 756 | 84 | 18.5 | 19.5 | 20.5 | 21.5 | 22.5 | 23.5 | 24.6 | 25.6 | 26.6 | 27.6 |  |
| 787 | 84 | 28.6 | 29.6 | 30.6 | 31.6 | 32.6 | 33.6 | 34.7 | 35.7 | 36.7 | 37.7 |  |
| 788 | 84 | 38.7 | 39.7 | 40.7 | 41.7 | 42.7 | 43.7 | 44.8 | 45.8 | 46.8 | 47.8 |  |
| 789 | 84 | 48.8 | 49.8 | 50.8 | 51.8 | 52.8 | 53.8 | 54.9 | 55.9 | 56.9 | 57.9 |  |
| 790 | 84 | 58.9 | 59.9 | 60.9 | 61.9 | 62.9 | 63.9 | 65.0 | 66.0 | 67.0 | 68.0 |  |
| 791 | 84 | 68.9 | 69.9 | 70.9 | 71.9 | 72.9 | 73.9 | 75.0 | 76.0 | 77.0 | 78.0 | $1{ }^{1} 0.1$ |
| 792 | 84 | 79.0 | 80.0 | 81.0 | 82.0 | 83.0 | 84.0 | 85.0 | 86.0 | 87.0 | 88.0 | $2 \begin{array}{lll}2 & 0.2\end{array}$ |
| 793 | 84 | 89.0 | 90.0 | 91.0 | 92.0 | 93.0 | 94.0 | 95.1 | 96.1 | 97.1 | 98.1 | $3{ }^{3} 0.3$ |
| 79 ¢ | 84 | 99.1 |  |  |  |  |  |  |  |  |  | 40.4 |
| 79. | 85 |  | 00.1 | 01.1 | 02.1 | 03.1 | 04.1 | 05.1 | 06.1 | 07.1 | 08.1 | 50.5 |
| 79.5 | 85 | 09.1 | 10.1 | 11.1 | 12.1 | 13.1 | 14.1 | 15.1 | 16.1 | 17.1 | 18.1 | 60.6 |
| 796 | 85 | 19.1 | 20.1 | 21.1 | 22.1 | 23.1 | 24.1 | 25.1 | 26.1 | 27.1 | 28.1 | $7 \begin{array}{ll}7 & 0.7\end{array}$ |
| 797 | 85 | 29.1 | 30.1 | 31.1 | 32.1 | 33.1 | 34.1 | 35.1 | 36.1 | 37.1 | 38.1 | 880.8 |
| 798 | 85 | 39.1 | 40.1 | 41.1 | 42.1 | 43.1 | 44.1 | 45.1 | 46.1 | 47.1 | 48.1 | 9 0.9 |
| 799 | 85 | 49.1 | 50.1 | 51.1 | 52.0 | 53.0 | 54.1 | 55.0 | 56.0 | 57.0 | 58.0 |  |
| 800 | 85 | 59.0 | 60.0 | 61.0 | 62.0 | 63.0 | 64.0 | 65.0 | 66.0 | 67.0 | 68.0 |  |
| 801 | 85 | 69.0 | 70.0 | 70.9 | 71.9 | 72.9 | 73.9 | 74.9 | 75.9 | 76.9 | 77.9 |  |
| 802 | 85 | 78.9 | 79.9 | 80.9 | 81.9 | 82.9 | 83.9 | 84.9 | 85.8 | 86.8 | 87.8 |  |
| 803 | 85 | 88.8 | 89.8 | 90.8 | 91.8 | 92.8 | 93.8 | 94.8 | 95.8 | 96.7 | 97.7 |  |
| 804 | 85 | 98.7 | 99.7 |  |  |  |  |  |  |  |  |  |
| 804 | 86 |  |  | 00.7 | 01.7 | 02.7 | 03.7 | 04.7 | 05.7 | 06.6 | 07.6 |  |
| 805 | 86 | 08.6 | 09.6 | 10.6 | 11.6 | 12.6 | 13.6 | 14.6 | 15.5 | 16.5 | 17.5 |  |
| 806 | 86 | 18.5 | 19.5 | 20.5 | 21.5 | 22.5 | 23.4 | 24.4 | 25.4 | 26.4 | 27.4 |  |
| 807 | 86 | 28.4 | 29.4 | 30.4 | 31.3 | 32.3 | 33.3 | 34.3 | 35.3 | 36.3 | 37.3 |  |
| 808 | 86 | 38.3 | 39.2 | 40.2 | 41.2 | 42.2 | 43.2 | 44.2 | 45.1 | 46.1 | 47.1 |  |
| 809 | 86 | 48.1 | 49.1 | 50.1 | 51.1 | 52.0 | 53.0 | 54.0 | 55.0 | 56.0 | 57.0 |  |
| 810 | 86 | 57.9 | 58.9 | 59.9 | 60.9 | 61.9 | 62.8 | 63.8 | 64.8 | 65.8 | 66.8 |  |
| Barom. eter Hor h. | N. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | Parts fir eact 0.01 mm . |

TABLE II. Correction for Difference of Temperature of Attached Thermometers.

| Temperature of Darometers at Station $\left\{\begin{array}{l}\text { Upyer }=\mathrm{T}^{\prime} \\ \text { Luwer }=\text { T }\end{array}\right.$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $T^{\prime}-T$ <br> Centig. | Correct. <br> Metres. | $\mathrm{T}^{\prime}-\mathrm{T}$ <br> Centigrade. | Correct. <br> Metres. | $\mathrm{T}^{\prime}-\mathrm{T}$ <br> Centigrade. | Correct. <br> Metres. | $\mathbf{T}^{\prime}-\mathrm{T}$ <br> Centigrade. | Correct. <br> Metres. | $\mathrm{T}^{\prime}-\mathrm{T}$ <br> Centigrade. | Correct. <br> Metres. |
| 0.0 | 0.0 | 8.0 | 10.3 | 16.0 | 20.6 | 24.0 | 30.9 | 32.0 | 41.3 |
| 0.2 | 0.3 | 8.2 | 10.6 | 16.2 | 20.9 | 24.2 | 31.2 | 32.2 | 41.5 |
| 0.4 | 0.5 | 8.4 | 10.8 | 16.4 | 21.1 | 24.4 | 31.5 | 32.4 | 41.8 |
| 0.6 | 0.8 | 8.6 | 11.1 | 16.6 | 21.4 | 24.6 | 31.7 | 32.6 | 42.0 |
| 0.5 | 1.0 | 8.8 | 11.3 | 16.8 | 21.7 | 24.5 | 32.0 | 32.8 | 42.3 |
| 1.0 | 1.3 | 9.0 | 11.6 | 17.0 | 21.9 | 25.0 | 32.2 | 33.0 | 42.5 |
| 1.2 | 1.5 | 9.2 | 11.9 | 17.2 | 2.2.2 | 25.2 | 32.5 | 33.2 | 42.8 |
| 1.4 | 1.8 | 9.4 | 12.1 | 17.4 | 22.4 | 25.4 | 32.7 | 33.4 | 43.1 |
| 1.6 | 2.1 | 9.6 | 12.4 | 17.6 | 22.7 | 25.6 | 33.0 | 33.6 | 43.3 |
| 1.8 | 2.3 | 9.8 | 12.6 | 17.8 | 22.9 | 25.8 | 33.3 | 33.8 | 43.6 |
| 2.0 | 2.6 | 10.0 | 12.9 | 18.0 | 23.2 | 26.0 | 33.5 | 34.0 | 43.8 |
| 2.2 | 2.8 | 10.2 | 13.1 | 18.2 | 23.5 | 26.2 | 33.8 | 34.2 | 4.1 |
| 2.4 | 3.1 | 10.4 | 13.4 | 18.4 | 23.7 | 26.4 | 34.0 | 34.4 | 44.3 |
| 2.6 | 3.4 | 10.6 | 13.7 | 18.6 | 24.0 | 26.6 | 34.3 | 34.6 | 44.6 |
| 2.8 | 3.6 | 10.8 | 13.9 | 18.8 | 24.2 | 26.8 | 34.6 | 34.8 | 44.9 |
| 3.0 | 3.9 | 11.0 | 14.2 | 19.0 | 24.5 | 27.0 | 34.8 | 35.0 | 45.1 |
| 3.2 | 4.1 | 11.2 | 14.5 | 19.2 | 24.8 | 27.2 | 35.1 | 35.2 | 45.4 |
| 3.4 | 4.4 | 11.4 | 14.7 | 19.4 | 25.0 | 27.4 | 35.3 | 35.4 | 45.6 |
| 3.6 | 4.6 | 11.6 | 15.0 | 19.6 | 25.3 | 27.6 | 35.6 | 35.6 | 45.9 |
| 3.8 | 4.9 | 11.8 | 15.2 | 19.8 | 25.5 | 27.8 | 35.8 | 35.8 | 46.2 |
| 40 | 5.2 | 12.0 | 15.5 | 20.0 | 25.8 | 28.0 | 36.1 | 36.0 | 46.4 |
| 4.2 | 5.4 | 12.2 | 15.5 | 20.2 | 26.0 | 28.2 | 36.4 | 36.2 | 46.7 |
| 1.1 | 5.7 | 12.4 | 16.0 | 20.4 | 26.3 | 28.4 | 36.6 | 36.4 | 46.9 |
| 4.6 | 5.9 | 12.6 | 16.3 | 20.6 | 26.6 | 29.6 | 36.9 | 36.6 | 47.2 |
| 4.8 | 6.2 | 12.8 | 16.5 | 20.8 | 26.8 | 28.8 | 37.1 | 36.8 | 47.4 |
| 5.0 | 6.4 | 13.0 | 16.8 | 21.0 | 27.1 | 29.0 | 37.4 | 37.0 | 47.7 |
| 5.2 | 6.7 | 13.2 | 17.0 | 21.2 | 27.3 | 29.2 | 37.6 | 37.2 | 48.0 |
| 5.4 | 7.0 | 13.4 | 17.3 | 21.4 | 27.6 | 29.4 | 37.9 | 37.4 | 48.2 |
| 5.6 | 7.2 | 13.6 | 17.5 | 21.6 | 27.8 | 29.6 | 38.2 | 37.6 | 48.5 |
| 58 | 7.5 | 13.8 | 17.8 | 21.8 | 28.1 | 29.8 | 38.4 | 37.8 | 48.7 |
| 6.0 | 7.7 | 14.0 | 18.0 | 2.0 | 28.4 | 30.0 | 38.7 | 38.0 | 49.0 |
| 6.2 | 8.0 | 14.2 | 18.3 | 22.2 | 28.6 | 30.2 | 38.9 | 38.2 | 49.2 |
| 6.4 | 8.3 | 14.4 | 18.5 | $2 \cdot .4$ | 28.9 | 30.4 | 39.2 | 38.4 | 49.5) |
| 6.6 | 8.5 | 14.6 | 18.8 | 22.6 | 29.1 | 30.6 | 39.5 | 38.6 | 49.8 |
| 6.8 | 8.8 | 14.8 | 19.0 | 22.8 | 29.4 | 30.8 | 39.7 | 38.8 | 50.0 |
| 70 | 9.0 | 15.0 | 19.3 | 23.0 | 29.7 | 31.0 | 40.0 | 39.0 | 50.3 |
| 7.2 | 9.3 | 15.2 | 19.6 | 23.2 | 29.9 | 31.2 | 40.2 | 39.2 | 50.5 |
| 7.4 | 9.5 | 15.4 | 198 | 23.4 | 30.2 | 31.4 | 40.5 | 39.4 | 50.8 |
| 7.6 | 9.8 | 15.6 | 20.1 | 23.6 | 30.4 | 31.6 | 40.7 | 39.6 | 51.1 |
| 7.9 | 10.1 | 15.8 | 20.3 | 23.8 | 30.7 | 31.8 | 41.0 | 39.8 | 51.3 |
| 8.0 | 10.3 | 16.0 | 20.6 | 24.0 | 30.9 | 32.0 | 41.3 | 40.0 | 516 |

This Table supposes the scale to be of brass from the top to the cistern. If it were of glass or of wood, the argument $\mathrm{T}^{\prime}$ - T ought to be diminished at the ratio of $5+$ to $6:$.

In computing by the formula of Laplace, we begin by reducing the barometers to the same temperature by means of the following formula: $\mathrm{H}=h^{\prime}+h^{\prime}\binom{\mathrm{T}-\mathrm{T}}{6196}$. Table II. saves this tronble, and gives, in metres, the correction due to the difference of temperature of the barometers.

TABLE III. Correction for Decrease of Gravitation in Latitude.

$$
\boldsymbol{\beta}=(0.0028371 \operatorname{cosin} .2 L) . \quad(A+\alpha+\boldsymbol{\beta})
$$

The Argument is the Mean Latitude between the two Stations.

| LAT | DE. | Correction, in metres, for |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | on. | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | $9{ }_{0}^{\circ}$ | 2.8 | 5.7 | 8.5 | 11.3 | 14.2 | 17.0 | 199 | 22.7 | 25.7 |
| 1 | 89 | 2.8 | 5.7 | 8.5 | 11.3 | 14.2 | 17.0 | 19.8 | 22.7 | 25.6 |
| 2 | 88 | 2.8 | 5.7 | 8.5 | 11.3 | 14.1 | 17.0 | 19.8 | 22.6 | 25.5 |
| 3 | 87 | 2.8 | 5.6 | 8.5 | 11.3 | 14.1 | 16.9 | 19.7 | 22.6 | 25.4 |
| 4 | 86 | 2.8 | 5.6 | 8.4 | 11.2 | 14.0 | 16.9 | 19.7 | 22.5 | 25.3 |
| 5 | 85 | 2.8 | 5.6 | 8.4 | 11.2 | 14.0 | 16.8 | 19.6 | 22.3 | 25.1 |
| 6 | 84 | 2.8 | 5.5 | 8.3 | 11.1 | 13.9 | 16.6 | 19.4 | 22.2 | 25.0 |
| 7 | 83 | 2.7 | 5.5 | 8.2 | 11.0 | 13.8 | 16.5 | 19.3 | 22.0 | 24.8 |
| 8 | 82 | 2.7 | 5.4 | 8.2 | 10.9 | 13.6 | 16.4 | 19.1 | 21.8 | 24.5 |
| 9 | 81 | 2.7 | 5.4 | 8.1 | 10.8 | 13.5 | 16.2 | 18.9 | 21.6 | 24.3 |
| 10 | 80 | 2.7 | 5.3 | 8.0 | 10.7 | 13.3 | 16.0 | 18.7 | 21.3 | 24.0 |
| 11 | 79 | 2.6 | 5.2 | 7.9 | 10.5 | 13.1 | 15.8 | 18.4 | 21.0 | 23.7 |
| 12 | 78 | 2.6 | 5.2 | 7.8 | 10.4 | 13.0 | 15.5 | 18.1 | 20.7 | 23.3 |
| 13 | 77 | 2.5 | 5.1 | 7.6 | 10.2 | 12.7 | 15.3 | 17.8 | 20.4 | 22.9 |
| 14 | 76 | 2.5 | 5.0 | 7.5 | 10.0 | 12.5 | 15.0 | 17.5 | 20.0 | 22.5 |
| 15 | 75 | 2.5 | 4.9 | 7.4 | 9.8 | 12.3 | 14.7 | 17.2 | 19.7 | 22.1 |
| 16 | 74 | 2.4 | 4.8 | 7.2 | 9.6 | 12.0 | 14.4 | 16.8 | 19.2 | 21.6 |
| 17 | 73 | 2.4 | 4.7 | 7.0 | 9.4 | 11.8 | 14.1 | 16.5 | 18.8 | 21.2 |
| 18 | 72 | 2.3 | 4.6 | 6.9 | 9.2 | 11.5 | 13.8 | 16.1 | 18.4 | 20.7 |
| 19 | 71 | 2.2 | 4.5 | 6.7 | 8.9 | 11.2 | 13.4 | 15.6 | 17.9 | 20.1 |
| 20 | 70 | 2.2 | 4.3 | 6.5 | 8.7 | 10.9 | 13.0 | 15.2 | 17.4 | 19.6 |
| 21 | 69 | 2.1 | 4.2 | 6.3 | 8.4 | 10.5 | 12.6 | 14.7 | 16.9 | 19.0 |
| 22 | 68 | 2.0 | 4.1 | 6.1 | 8.2 | 10.2 | 12.2 | 14.3 | 16.3 | 18.4 |
| 23 | 67 | 2.0 | 3.9 | 5.9 | 7.9 | 9.8 | 11.8 | 13.8 | 15.8 | 17.7 |
| 24 | 66 | 1.9 | 3.8 | 5.7 | 7.6 | 9.5 | 11.4 | 13.3 | 15.2 | 17.1 |
| 25 | 63 | 1.8 | 3.6 | 5.5 | 7.3 | 9.1 | 10.9 | 12.8 | 14.6 | 16.4 |
| 26 | 64 | 1.7 | 3.5 | 5.2 | 7.0 | 8.7 | 10.5 | 12.2 | 14.0 | 15.7 |
| 27 | 63 | 1.7 | 3.3 | 5.0 | 6.7 | 8.3 | 10.0 | 11.7 | 13.3 | 15.0 |
| 28 | 62 | 1.6 | 3.2 | 4.8 | 6.3 | 7.9 | 9.5 | 11.1 | 12.7 | 14.3 |
| 29 | 61 | 1.5 | 3.0 | 4.5 | 6.0 | 7.5 | 9.0 | 10.5 | 12.0 | 13.5 |
| 30 | 60 | 1.4 | 2.8 | 4.3 | 5.7 | 7.1 | 8.5 | 9.9 | 11.3 | 12.8 |
| 31 | 59 | 1.3 | 2.7 | 4.0 | 5.3 | 6.6 | 8.0 | 9.3 | 106 | 12.0 |
| 32 | 58 | 1.2 | 2.5 | 3.7 | 5.0 | 6.2 | 7.5 | 8.7 | 9.9 | 11.2 |
| 33 | 57 | 1.1 | 2.3 | 3.5 | 4.6 | 5.8 | 6.9 | 8.1 | 9.2 | 10.4 |
| 34 | 56 | 1.1 | 2.1 | 3.2 | 4.2 | 5.3 | 6.4 | 7.4 | 8.5 | 9.6 |
| 3.5 | 55 | 1.0 | 1.9 | 2.9 | 3.9 | 4.8 | 5.8 | 6.8 | 7.8 | 8.7 |
| 36 | 54 | 0.9 | 1.7 | 2.6 | 3.5 | 4.4 | 5.3 | 6.1 | 7.0 | 79 |
| 37 | 53 | 0.8 | 1.6 | 2.3 | 3.1 | 3.9 | 4.7 | 5.5 | 6.2 | 7.0 |
| 38 | 52 | 0.7 | 1.4 | 2.1 | 2.7 | 3.4 | 4.1 | 4.8 | 5.5 | 6.2 |
| 39 | 51 | 0.6 | 1.2 | 1.8 | 2.4 | 2.9 | 3.5 | 4.1 | 4.7 | 5.3 |
| 40 | 50 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.4 | 3.9 | 4.4 |
| 41 | 49 | 0.4 | 0.8 | 1.2 | 1.6 | 2.0 | 2.4 | 2.8 | 3.2 | 3.5 |
| 42 | 48 | 0.3 | 0.6 | 0.9 | 1.2 | 1.5 | 1.8 | 2.1 | 2.4 | 2.7 |
| 43 | 47 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 |
| 44 | 46 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 45 | 45 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Table IV. Correction for Decrease of Gravitation on a Vertical Line.

$$
\begin{gathered}
\delta=\left(\frac{A+\alpha+\hat{\beta}+v+15296}{6366200}\right) \times \mathbf{A}(+\alpha+\beta+v) . \\
\text { Argument }=(A+\alpha+\beta+v) .
\end{gathered}
$$

| Approximate Difference of Level. | Correspond. Correction Positive. | Approximate Difference of Level. | Correspond. Correction Positive. | Approximate Difference of Level. | Correspond. Correction Positive. | Approximate Ditference of Level. | Correspond. <br> Correction <br> Positive. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Merres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. |
| 100 | 0.2 | 2100 | 6.0 | 4100 | 12.9 | 6100 | 21.1 |
| 200 | 0.5 | 2200 | 6.3 | 4200 | 13.3 | 6200 | 21.6 |
| 300 | 0.8 | 2300 | 6.6 | 4300 | 13.7 | 6300 | 22.0 |
| 400 | 1.0 | 2400 | 6.9 | 4400 | 14.1 | 6400 | 22.5 |
| 500 | 1.3 | 2500 | 7.3 | 4500 | 14.5 | 6500 | 22.9 |
| 600 | 1.6 | 2600 | 7.6 | 4600 | 14.9 | 6600 | 23.4 |
| 700 | 1.8 | 2700 | 7.9 | 4700 | 15.3 | 6700 | 23.9 |
| 800 | 2.1 | 2800 | 8.3 | 4800 | 15.7 | 6800 | 24.3 |
| 900 | 2.4 | 2900 | 8.6 | 4900 | 16.1 | 6900 | 24.8 |
| 1000 | 2.7 | 3000 | 8.9 | 5000 | 16.5 | 7000 | 25.3 |
| 1100 | 2.9 | 3100 | 9.3 | 5100 | 16.9 | 7100 | 25.7 |
| 1200 | 3.2 | 3200 | 9.6 | 5200 | 17.3 | 7200 | 26.2 |
| 1300 | 3.5 | 3300 | 10.0 | 5300 | 17.7 | 7300 | 26.7 |
| 1400 | 3.8 | 3400 | 10.3 | 5400 | 18.1 | 7400 | 27.2 |
| 1500 | 4.1 | 3500 | 10.7 | 5500 | 18.5 | 7500 | 27.7 |
| 1600 | 4.4 | 3600 | 11.1 | 5600 | 19.0 | 7600 | 28.1 |
| 1700 | 4.7 | 3700 | 11.4 | 5700 | 19.4 | 7700 | 28.6 |
| 1800 | 5.0 | 3800 | 11.8 | 5800 | 19.8 | 7800 | 29.1 |
| 1900 | 5.3 | 3900 | 12.2 | 5900 | 20.3 | 7900 | 29.6 |
| 2000 | 5.6 | 4000 | 12.5 | 6000 | 20.7 | 8000 | 30.1 |

TABLE V. Correction for the Elevation of the Lower Station above Ocean.
Argument $=$ Height of Barometer at Lower Station.

| Anproximate Difference of Level. | Height of Barometer at Lower Station in Millimetres. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 |
| Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. |
| 1000 | 1.7 | 1.4 | 1.1 | 0.9 | 0.6 | 0.4 | 0.2 | 0.0 |
| 2000 | 3.4 | 2.8 | 2.2 | 1.7 | 1.3 | 0.8 | 0.4 | 0.1 |
| 3000 | 5.1 | 4.2 | 3.3 | 2.6 | 1.9 | 1.3 | 0.7 | 0.1 |
| 4000 | 6.8 | 5.6 | 4.4 | 3.4 | 2.5 | 1.7 | 0.9 | 0.1 |
| 5000 | 8.5 | 6.9 | 5.5 | 4.3 | 3.1 | 2.1 | 1.1 | 0.1 |
| 6000 | 10.3 | 8.3 | 6.7 | 5.2 | 3.8 | 2.5 | 1.3 | 0.2 |
| 7000 | 12.0 | 9.7 | 7.8 | 6.0 | 4.4 | 2.9 | 1.5 | 0.2 |
| 8000 | 13.7 | 11.1 | 8.9 | 6.9 | 5.0 | 3.4 | 1.8 | 0.2 |
| 9000 | 15.4 | 12.5 | 10.0 | 7.7 | 5.7 | 3.8 | 2.0 | 0.3 |

## I I.

## TABLES

FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS.
BY A. GUYOT.
Tables which, like the preceding ones by Delcros, in metrical measures, are sufficiently extensive to save the necessity of interpolations, relieve the computer of most of his trouble, and considerably reduce the chances of error in the computations. They thus render to science itself a real service, by inducing observers to determine a larger number of points, and to secure the accuracy of the results by repeating their observations at the same point in various atmospheric circumstances, both of which they can do without fear of being overwhelmed by the labor of the computation.

Similar tables are here offered to the observers who use instruments graduated to English measures. Like those of Delcros, the new tables are based on Laplace's formula, with a slight modification of only one constant. They dispense with the use of logarithms, and give the differences of level corresponding to every thousandth of an inch from 12 to 31 inches by means of the simplest arithmetical operations, so that the data being prepared and corrected, the computation of an elevation takes but a few minutes, and is done with scarcely any chance of error.

Laplace's formula and constants were adopted for the computation of the tables in preference to others found in the following sets for reasons which a few words will explain.

It has been remarked, page 9, that, in consequence of Laplace's constants having been retained in Gauss's, Schmidt's, and Baily's formule, they all give similar results; but that Bessel's formula differs in separating the correction due to the moisture of the air from that due to its temperature, while in Laplace's, and in the formulæ just mentioned, both are united. To introduce a separate correction for the expansion of aqueous vapor is, in the writer's view, a doubtful improvement. The laws of the distribution and transmission of moisture through the atmosphere are too little known, and its amount, especially in mountain regions, is too variable, and depends too much upon local winds and local condensation, to allow a reasonable hope of obtaining the mean humidity of the layer of air between the two stations by means of hygrometrical observations taken at each of them. 'These doubts are confirmed by the experience of the author and of many other observers, which shows that, on an average, Laplace's method works not only as well as the other, but more uniformly well. At any rate, the gain, if there is any, is not clear enough to compensate for the undesirable complication of the formula.

Though the several co-efficients of Laplace's formula need perhaps to be modified according to more recent and probably more accurate determinations of the physical constants on which they depend, as has been proposed by Plantamour, E. Ritter, and lately by the writer himself in a paper read before the American Association for the Advancement of Science at their meeting in Montreal, they have been retained in preparing the following tables, partly because it was found that the errors due to
the various co-efficients nearly compensate each other ; partly on the ground that, until a severe test, by means of actual comparative measurements made for the purpose, has shown the expediency of these modifications, it seemed desirable to adhere to the old constants, and thus to preserve a uniformity in the results with the tables of Oltmans, Delcros, Gauss, Baily, and others, which have already been extensively used. The substitution of the co-efficient 0.00260 , expressing, according to Schmidt's computation (Mathem. und Physic. Geogr., Il. p. 202), the variation of gravity in latitude, for the value 0.002837 , does not sensibly alter the altitudes obtained.

The close agrecment of the determinations furnished by Laplace's formula, in barometrical measurements carefully conducted, marle in favorable circumstances, and during the warm season, with those obtained from repeated trigonometrical observations, or by the spirit-level, strongly testifies in favor of its general correctness. A few striking examples will suffice to show it.

The altitude of Mont Blanc, measured by the barometer, by MM. Bravais and Martins, on the 29th of August, 1844, and computed by Delcros, by means of nine corresponding stations situated on all siles of the mountain (see Anmuaire Météorologique de France, for 1851 , p. 274), was found to be 4810 metres. The altitude of the same point, being the mean of seven of the most elaborate and reliable geodetic measurements, which cost nearly twenty years of labor, is 4809.6 metres.

For smaller elcvations the formula seems to answer equally well.
The barometrical measurement of Mount Washington, in New Hampshire, by the author, on the 8th and 9 th of August, 1851, gave, by Delcros's Tables, for the mean of eight observations, taken at different hours of the day, 5466.7 English feet above Gorham, N. H., 6285.7 above high tide, and 6291.7 feet above the mean level of the ocean in Portland harbor. In August, 1852, W. A. Goodwin, Civil Engineer, starting from Gorham Railroad Station, found, by the spirit-level, Mount Washington to be 6285.5 feet above mean tide. In September, 1853, Captain T. J. Cram, of the Topographical Engineers, executed, in behalf of the Coast Survey, a careful measurement with the spirit-level, on the same line, for the purpose of testing the various methods of measuring altitudes, and found Mount Washington to be 6:93 English feet above the mean level of the ocean.

In lower latitudes the formula showed equally good results. By a barometrical measurement in July, 1856, the altitude of the highest peak of the Black Mountain, North Carolina, about Lat. $36^{\circ}$, was found by the author to be 6701 English feet; and that of the highest Mountain House 5248 feet. In September, 1857, Major T. C. Turner, Chief Engineer of the Morganton Railroad, ran a line of levels from the same point which was used as the lower station for the barometrical measurement, to the top of the highest peak, and found its altitude to be 6711 English feet, and that of the Mountain House 5246 feet. Other points on the line agreed equally well.

Such an agreement, in so considerable elevations, is all that can be desired.
These figurcs show conclusively, that, when the errors which may arise from the great variability of the data furnished by the instruments have been removed by a repetition, in various states of the atmosphere, and by a proper combination of simultaneous observations at stations not too distant from each other, those which remain and may be attributed to the formula cannot be considerable. But, on the other
band, we have no right to expect such results from single observations, taken, perhaps, in unsettled weather, without paying any regard to the time of the day at which they were made, to the distance or the non-simultaneity of the corresponding observations, or to other unfavorable circumstances. It is too well known that in such cases large errors may and do actually occur ; but for these the formula ought not to be held responsible.

## Arrangement of the Tables.

If' we call
$h=$ the observed height of the barometer
$\left.\begin{array}{l}\tau=\text { the temperature of the barometer } \\ t=\text { the temperature of the air }\end{array}\right\}$ at the lower station;
$h^{\prime}=$ the observed height of the barometer
$\tau^{\prime}=$ the temperature of the barometer $\}$ at the upper station.
$t^{\prime}=$ the temperature of the air
If we make, further,
$Z=$ the difference of level between the two barometers ;
$L=$ the mean latitude between the two stations;
$H=$ the height of the barometer at the upper station reduced to the temperature of the barometer at the lower station ; or,
$H=h^{\prime}\left\{1+0.00008967\left(\tau-\tau^{\prime}\right)\right\}$;
The expansion of the mercurial column, measured by a brass seale, for $1^{\circ}$ Fahrenheit $=0.00008967$;
The increase of gravity from the equator to the poles $=0.00520048$, or 0.00260 to the 45 th degree of latitude ;

The earth's mean radius $=20,886,860$ English feet;
Then, Laplace's formula, reduced to English.measures, reads as follows :

$$
Z=\log \frac{h}{H} \times 60158.6 \text { English feet }\left\{\begin{array}{l}
\left(1+\frac{t+t^{\prime}-64}{900}\right) \\
(1+0.00260 \cos 2 L) \\
\left(1+\frac{z+52952}{20886860}+\frac{h}{10443430}\right)
\end{array}\right.
$$

Table I. gives, in English feet, the value of $\log H$ or $h \times 60158.6$ for every hundredth of an inch, from 12 to 31 mehes in the barometer, together with the value of the additional thousandths, in a separate column. These values have been diminished by a constant, which does not alter the difference required.

Table II. gives the correction 2.343 feet $\times\left(\tau-\tau^{\prime}\right)$ for the difference of the temperatures of the barometers at the two stations, or $\tau-\tau^{\prime}$. As the temperature at the upper station is generally lower, $\tau-\tau^{\prime}$ is usually positive, and the correction negative. It becomes positive when the temperature of the upper barometer is higher, and $\boldsymbol{\tau}-\boldsymbol{\tau}^{\prime}$ negative. When the heights of the barometers have been reduced to the same temperature, or to the freezing point, this table will not be used.

Table IV. shows the correction $D^{\prime} \frac{\tilde{z}+52252}{20886860}$ to be applied to the approximate altitude for the decrease of gravity on a vertical acting on the density of the mercurial column. It is always additive.

Table V. furnishes the small correction $\frac{h}{10443430}$ for the decrease of gravity on a vertical acting on the density of the air ; the height of the barometer $h$ at the lower station representing its approximate altitude. Like the preceding correction, it is always additive.

## Use of the Tables.

In Table I. find first the numbers corresponding to the observed beights of the barometer $h$ and $h^{\prime}$. Suppose, for instance, $h=\mathbf{9 9 . 3 4 5} \mathrm{in}$.; find in the first column on the left the number 29.3 ; on the same horizontal line, in the column headed 0.4 , is given the number corrosponding to $29.34=28121.7$; in the last column but one on the right, we find for $.005=4.5$, or for $29.345=28126.2$. Take likewise the value of $h^{\prime}$, and find the difference.

If the barometrical heights have not been previously reduced to the same temperature, or to the freezing point, apply to the difference the correction found in Table II. opposite the number representing $\tau-\tau^{\prime}$; we thus obtain the approximate difference of level, $D$.

For computing the correction due to the expansion of the air according to its temperature, or $D \times\left(\frac{t+t^{\prime}-64}{900}\right)$, make the sum of the temperatures, subtract from that sum 64 ; multiply the rest into the approximate difference $D$, and divide the product by 900 . This correction is of the same sign as $\left(t+t^{\prime}-64\right)$. By apply. ing it, we obtain a second approximate difference of level, $D^{\prime}$.

In Table III., with $D^{\prime}$ and the mean latitude of the stations, find the correction for variation of gravity in latitude, and add it to $D^{\prime}$, paying due attention to the sign.

In Table IV. with $D^{\prime}$, and in 'Tablc V. with $D^{\prime}$ and the height of the barometer at the lower station, take the corrections for the decrease of gravity on a vertical, and add them to the approximate difference of level.

The sum thus found is the true difference of level between the two stations, or $Z$; by alding the elevation of the lower station above the level of the sca, when known, we obtain the altitude of the upper station.

The use of the small table, VI., by means of which approximate differences of level can be obtained by a single multiplication, is explained below, page 90.

## Example 1.

Measurement of Mount Washington, New Hampshire, by A. Guyot, August 8th, 1851, 4 P. м. ; the barometer at the lower station being at 825 English feet above the mean level of the sea; at the upper station at one foot below the summit.

The observation gave,

| Gorham, <br> Mount Washington, | Barometer. | Attached Thermometer. | Temperature of Air. |
| :---: | :---: | :---: | :---: |
|  | $h=29.272 \mathrm{in}$. | $\tau=70^{\circ} .70 \mathrm{~F}$. | $t=72^{\circ} .05 \mathrm{~F}$. |
|  | $h^{\prime}=24.030{ }^{\text {a }}$ | $\tau^{\prime}=54^{\circ} .52 \mathrm{~F}$. | $t^{\prime}=50^{\circ} .54 \mathrm{~F}$. |
|  |  | $\tau^{\prime}=16^{\circ} .38 \mathrm{~F}$. | $\begin{array}{r} 122^{\circ} .59 \mathrm{~F} . \\ -64^{\circ} \end{array}$ |
|  |  | $t+t^{\prime}$ | $64=58^{\circ} .59 \mathrm{~F}$. |



## Example 2.

Measurement of the highest peak of the Black Mountain, in North Carolina, July 11th, 1856, by A. Guyot.

By observation we have at,


Table I. gives for $h=24.934$. . . . . 23,870.4
" " for $h^{\prime}=23.662$. . . . 22,502.4
Difference, . . . . 1,368.0
Table II. gives for $\tau-\tau^{\prime}=2.7$. . . . -6.3
Approximate difference, $D=1,361.7$
$\frac{D \times\left(t+t^{\prime}-64\right)}{900}=\frac{1362 \times 56.7}{900}=\quad 85.8$
Second approximate difference, $D^{\prime}=1,447.5$
Table III. gives for $D^{\prime}=1448$ and Lat. $36^{\circ}$. . 1.2
Table IV. gives for $D^{\prime}=1448$. . . . 3.8
Table V. gives for $D^{\prime}=1448$ and $h=25 \quad$. . 0.7
Highest peak above Mountain House, or . . $Z=1,453.2$
Mountain House above the sea . . . . 5,248.4
Black Mountain, highest peak above the sea, or altitude, 6,701.6 Eng. ft.


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| 16.0 | 12.279 .6 | 12295.9 | 12312.2 | 12328.5 | 12344.8 | 12361.1 | 12377.4 | 12393.6 | 12409.9 | 12426.1 |  | Feet. | 16.0 |
| 16.1 | $12+42.4$ | 12458.6 | 12474.8 | 12191.0 | 12507.2 | 12523.4 | 12539.6 | 12.555 .7 | 12571.9 | 12588.0 |  | Feet. | 16.1 |
| 16.2 | 12604.2 | 12620.3 | 12636.4 | 12652.5 | 12668.6 | 12684.7 | 12700.8 | 12716.9 | 12732.9 | 1274~. 9 | 1 | 1.6 | 16.2 |
| 16.3 | 12765.0 | 12781.0 | 12797.0 | 12813.0 | 12829.0 | 12845.0 | 12861.0 | 12376.9 | 12592.9 | 12908.8 | 2 | 3.1 | 16.3 |
| 16.4 | 12924.8 | 12940.7 | 12956.6 | 12972.5 | 12988.4 | 13004.3 | 13020.2 | 13036.0 | 13051.9 | 13067.7 | 3 | 4.7 | 16.4 |
| 16.5 | 13053.6 | 13099.4 | 13115.2 | 13131.0 | 13146.8 | 13162.6 | 13178.4 | 13194.2 | 13210.0 | 13225.7 | 4 | 6.3 | 16.5 |
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| 16.7 | 13392.4 | 13414.0 | $13+29.6$ | 13445.2 | 13160.8 | 13476.4 | 13492.0 | 13507.6 | 13523.2 | 13538.7 | 6 | 9.4 | 16.7 |
| 16.8 | 13554.3 | 13569.8 | 13.555 .1 | 13600.9 | 13616.4 | 13631.9 | 13647.4 | 13662.9 | 13678.4 | 13693.9 | 7 | 11.0 | 16.8 |
| 16.9 | 13709.4 | 13724.8 | 13740.3 | 13755.7 | 13771.1 | 13756.5 | 13501.9 | 13517.3 | 13832.7 | 13848.1 | 8 | 12.5 | 16.9 |
| 17.0 | 13863.5 | 13878.8 | 13891.2 | 13909.6 | 13924.9 | 13940.2 | 13955.6 | 13970.9 | 13986.2 | 14001.5 | 9 | 14.1 | 17.0 |
| 17.1 | 11016.8 | 14032.0 | 14047.3 | 14062.6 | 14077.8 | 14093.0 | 14108.3 | 14123.5 | 14138.7 | 14153.9 |  |  | 17.1 |
| 17.2 | 14169.1 | 14184.3 | 14199.4 | 14214.6 | 142.29 .8 | 14244.9 | 14.260 .1 | 14275.2 | 14290.3 | 14305.5 |  |  | 17.2 |
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| 17.6 | 14769.8 | 14754.6 | 14799.4 | 14814.3 | 14829.1 | 14843.9 | 14858.7 | 14873.5 | 14888.2 | 14903.0 | 3 | 4.4 | 17.6 |
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| 17.8 | 1506.5 .0 | 1.5079 .6 | 1509 4.3 | 15109.0 | 15123.6 | 15138.2 | 15152.9 | 15167.5 | 15182.1 | 15196.7 | 5 | 7.3 | 17.8 |
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| 18.1 | 1.5501 .5 | 15516.0 | 15530.4 | 15544.8 | 15559.2 | 15.573 .6 | 15588.0 | 15602.4 | 15616.8 | 15631.2 | 8 | 11.7 | 18.1 |
| 12.2 | 15645.5 | 15659.9 | 15674.2 | 15688.5 | 15702.9 | 15717.2 | 15731.5 | 15745.8 | 15760.1 | 15774.4 | 9 | 13.1 | 18.2 |
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|  | $\begin{array}{ll}\circ \\ 0 \\ 0 \\ 0 & 0 \\ -1\end{array}$ |  |  | O |  |  |
|  | $\bigcirc$ |  |  |  |  |  |
|  | － 0 |  |  |  | $\underset{\sim}{\infty} \underset{\sim}{\circ} \underset{\sim}{\circ} \underset{\sim}{\circ}$ |  |
|  | － |  |  |  |  |  |
|  | $\stackrel{\circ}{\circ}_{0}^{\circ}$ |  |  |  |  |  |
|  | $\bigcirc$ |  |  | 的 |  |  |
|  | － |  |  |  | No |  |
|  | － |  | $\dot{\infty} \dot{\theta} \dot{\theta} \dot{\theta}$ |  |  |  |
|  | －${ }_{\text {¢ }}$ | 芴或 |  |  |  |  |
|  | $\bigcirc$ |  | ミニロ O |  |  |  |
|  |  |  | $\begin{array}{lcc} 0 & 0 & 0 \\ \underline{0}-8 \\ \hline \end{array}$ |  | $\begin{array}{lll} 0 & 0 \\ \dot{O} \\ \hline \end{array}$ |  |
|  | $\bigcirc$ |  |  |  |  |  |
|  | －${ }^{-1}$ | $\underset{\sim}{\dot{\otimes}} \underset{\sim}{\dot{N}} \underset{\sim}{\circ} \underset{\sim}{\circ} \underset{\sim}{\circ}$ | Hoccoc |  |  | $\overline{4}$ |
|  | $\bigcirc{ }^{\circ} \mathrm{O}$ |  |  |  |  |  |
|  | $\bigcirc$ |  |  |  |  |  |
|  |  |  | $\begin{array}{lll} 8 \\ 8 \\ 8 & 8 \\ 8 & 8 \\ \hline \end{array}$ |  |  |  |


| IV. Coblection FOR |  |  | V. Correction for tile Heigilt of the Lower Station. - Positice. |  |  |  |  |  |  | VI. Height of a Column of Air, corresponifng to One Tentif of an INci in the Barometer. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approximate Dif- |  | $\begin{aligned} & \text { we of } \\ & \text { on a } \\ & \text { ical. } \\ & \text { cive. } \end{aligned}$ | ILeight of the Barometer, in English Inehes, at Lower Station. |  |  |  |  |  |  | Barometer Keading in English Inehes. | Temperature of the Air, Fahrenheit, being |  |  |  |  |  |  |  |  |  |
| of Level. |  | +500 | 16 | 18 | 20 | $2{ }^{2}$ | 1 |  | 28 |  | $40^{\circ}$ | $45^{\circ}$ | $50{ }^{\circ}$ | $5.5{ }^{\circ}$ | $60^{\circ}$ | $65^{\circ}$ | $70^{\circ}$ | 8.50 | $80^{\circ}$ | $8.5{ }^{\circ}$ |
| Enr Feet $1000$ | Feet. | Feet. 3.9 | Feet. | Feet 1.3 | $\begin{aligned} & \text { Feet } \\ & \text { 1. } 0 \end{aligned}$ | $\begin{array}{r} \text { Feet. } \\ 0.5 \end{array}$ | $\begin{array}{r} \text { Feet. } \\ 0.6 \end{array}$ | Feet. $0.4$ | Feet. $0.2$ | 18.5 | Feet. <br> 14.6 | Feet. <br> 146.1 | $\begin{aligned} & \text { Feet. } \\ & 147.7 \end{aligned}$ | $\begin{gathered} \text { Feet. } \\ 149.3 \end{gathered}$ | $\begin{gathered} \text { Feet. } \\ 150.9 \end{gathered}$ | $\begin{gathered} \text { Feet. } \\ 152.5 \end{gathered}$ | Feet. $154.0$ | $\begin{aligned} & \text { Feet. } \\ & 155.7 \end{aligned}$ | $\begin{gathered} \text { Feet. } \\ 157.2 \end{gathered}$ | $\begin{aligned} & \text { Feet. } \\ & 15.8 .8 \end{aligned}$ |
| 2000 | 5.2 | 6.6 | 3.1 | 2.5 | 2.0 | 1.5 | 1.1 | 0.7 | 0.3 | 19.0 | 140.8 | 142.3 | 143.5 | 145.4 | 146.9 | 148.4 | 150.0 | 151.5 | 153.1 | 154.6 |
| 3000 | 7.9 | 9.3 | 4.7 | 3.8 | 3.0 | 2.3 | 1.7 | 1.1 | 0.5 | 19.5 | 137.1 | $13 \bigcirc .6$ | 140.1 | 141.6 | 143.1 | 144.6 | 146.1 | 147.6 | 149.1 | 150.6 |
| 4000 | 10.8 | 12.2 | 6.3 | 5.1 | 4.0 | 3.1 | 2.2 | 1.4 | 0.7 | 20.0 | $13: 3.7$ | 135.2 | 136.6 | 138.1 | 1:39.6 | 141.0 | 142.5 | 143.9 | 14.5 .4 | 146.9 |
| 5000 | 13.7 | 15.2 | 7.8 | 6.4 | 5.0 | 3.8 | 2.8 | 1.8 | 0.8 | 20.5 | 130.5 | 131.9 | 13:3 3 | 134.7 | 136.1 | 1:7.6 | 139.0 | 140.1 | 141.8 | 143.3 |
| 6000 | 16.7 | 18.3 | 9.1 | 7.6 | 6.0 | 4.6 | 3.3 | 2.1 | 1.0 | 21.0 | 127.3 | 120.7 | 130.1 | 181.5 | 182.9 | 131.3 | 13.5 .7 | 137.0 | 138.4 | 139.8 |
| 7000 | 19.9 | 21.5 | 11.0 | 8.9 | 7.1 | 5.4 | 3.9 | 2.5 | 1.2 | 21.5 | 121.3 | 12.5 .7 | 127.0 | 128.4 | 129.7 | 131.1 | 132.4 | 133.8 | 125.1 | 1:6.5 |
| 8000 | 23.1 | 21.7 | 12.5 | 10.2 | 8.1 | 6.2 | 4.1 | 2.8 | 1.3 | 22.0 | 121.5 | $12 \cdot 3.9$ | 124.2 | 125.5 | 126.8 | 128.2 | 129.5 | 130.8 | 132.2 | 123.5 |
| 9000 | 26.4 | 23.1 | 14.1 | 11.4 | 9.1 | 6.9 | 5.0 | 3.2 | 1.5 | 2.3 .5 | 118.9 | 120.1 | 121.4 | 12.2 .7 | 124.0 | 125.3 | 126.6 | 127.9 | 129.2 | 130.5 |
| 10000 | 29.8 | 31.5 | 1.5 .7 | 12.7 | 10.1 | 7.7 | 5.5 | 3.5 | 1.7 | 2:3.0 | 116.2 | 11\%.5 | 118.6 | 120.0 | 121.3 | 122.6 | 123.8 | 125.1 | 126.4 | 127.7 |
| 11000 | :33.3 | 35.1 | 17.2 | 14.0 | 11.1 | 8.7 | 6.1 | 3.9 | 1.8 | 23.5 | 113.7 | 115.0 | 1162 | 117.5 | 11.8 .7 | 120.0 | 121.2 | 122.5 | 123.7 | 124.9 |
| 12000 | 3.3 .9 | 38.7 | 18.8 | 15.3 | 12.1 | 9.2 | 6.6 | 4.2 | 2.0 | 24.0 | 111.3 | 112. i | 113.8 | 1150 | 116.2 | 117.4 | 118.6 | 119.9 | 121.1 | 122.3 |
| 13000 | 40.6 | 42.5 | 20.4 | 16.5 | 1.2.1 | 10.0 | 7.2 | 4.6 | 2.2 | 24.5 | 109.1 | 110.3 | 111.5 | 112.6 | 113.8 | 115.0 | 116.2 | 117.3 | 118.6 | 119.8 |
| 14000 | 4.4 | 46.3 | 21.9 | 17.8 | 14.1 | 10.8 | 7.7 | 4.9 | 2.3 | 2.9 .0 | 106.9 | 10.3.1 | 109.3 | 110.4 | 111.6 | 112.8 | 113.9 | 115.1 | 116.3 | 117.4 |
| 15000 | 48.3 | 50.3 | 23.5 | 19.1 | 1.5 .1 | 11.5) | 8.3 | 5.3 | 2.5 | 2.5 .5 | 104.8 | 105.9 | 10\%.1 | 108.2 | 109.3 | 110.5 | 111.6 | 112.8 | 113.9 | 115.1 |
| 16000 | 52.3 | 54.3 | 25.1 | 20.3 | 16.1 | 12.3 | 8.3 | 5.6 | 2.7 | 26.0 | 102.7 | 10:3.9 | 10.5.0 | 106.1 | $10: .2$ | 108.4 | 109.5 | 110.6 | 111.7 | 112.8 |
| 17000 | 56.4 | 58.4 | 26.6 | 21.6 | 17.1 | 1:3.1 | 9.1 | 6.0 | 2.8 | 26.5 | 100.9 | 102.0 | 103.1 | 101.2 | 10.5.3 | 106.4 | 107.5 | 108.6 | 109.7 | 110.8 |
| 18000 | 60.5 | 62.6 | 28.2 | 22.9 | 18.1 | 13.8 | 9.9 | 6.3 | 3.0 | 27.0 | 99.0 | 100.] | 101.2 | 112:3 | 103.3 | 104.4 | 10.5 .5 | 106.6 | 107.6 | 10. 7 |
| 19000 | 64.8 | 67.0 | 29.8 | 21.1 | 19.2 | 14.6 | 10.5 | 6.7 | 3.2 | 27.5 | 97.2 | 98.2 | 99.3 | 10¢.3 | 101.4 | 102.5 | 103.5 | 104.6 | 10.5 .6 | 106.7 |
| 20000 | 6.9 .2 | 71.4 | 31.3 | 2.5 .4 | 20.2 | 15.4 | 11.0 | 7.0 | 3.3 | 28.0 | 9.).4 | 965 | 97.5 | 98.6 | 99.6 | 100.7 | 101.7 | 102.8 | 103.8 | 104.8 |
| 21000 | 73.6 | 75.9 | 32.9 | 26.7 | 21.2 | 16.1 | 11.6 | 7.4 | 3.5 | 28.5 | 93.8 | 94.8 | 95.8 | 96.9 | 97.9 | 98.9 | 99.9 | 100.9 | 101.9 | 103.0 |
| $2 \cdot 3000$ | 78.2 | 80.5) | 34.5 | 28.0 | 22.2 | 16.9 | 12.1 | 7.7 | 3.7 | 29.0 | 92.1 | 93.1 | 91.1 | 95.1 | 96.2 | 97.2 | 98.2 | 99.2 | 100.2 | 101.2 |
| 23000 | 8.3 .9 | 85.2 | 36.0 | 29.2 | 23.2 | 17.7 | 12.7 | 8.1 | 3.8 | 29.5 | 90.6 | 91.6 | 92.6 | $9: 3.6$ | 91.5 | 9.5 .5 | 96.5 | 97.5 | 98.5 | 99.5 |
| 24000 | 87.6 | 90.0 | 37.6 | 30.5 | 24.2 | 18.5 | 13.2 | 8.4 | 4.0 | 30.0 | 89.1 | 90.0 | 91.0 | 92.0 | 92.9 | 93.9 | 94.9 | 95.9 | 96.8 | 97.8 |
| 25000 | 93.5 | 91.9 | 39.1 | 31.8 | 25.2 | 19.2 | 13.8 | 8.8 | 4.1 | 30.5 | 87.6 | 88.5 | 89.5 | 904 | 91.1 | 923 | 93.3 | 94.2 | 95.2 | 96.1 |

## TABLE

## for

## compting the difference in the heights of two places py means of the barometer.

By Prof. Elias Loomis.

This table was computed from the formula of Laplace, modified in accordance with the results of more recent determinations.

Suppose that we have observed

$$
\begin{aligned}
& \text { At the lower station. }\left\{\begin{array}{l}
\mathrm{H}, \text { the height of the barometer, } \\
\mathrm{T}, \text { the temperature of the barometer, } \\
t, \text { the temperature of the air, }
\end{array}\right. \\
& \text { At the upper station. }\left\{\begin{array}{l}
h^{\prime}, \text { he height of the barometer, } \\
\mathrm{T}^{\prime}, \text { the temperature of the barometer, } \\
t^{\prime}, \text { the temperature of the air. }
\end{array}\right.
\end{aligned}
$$

Represent by $s$ the height of the lower station above the level of the sea, by $L$ the lat.tude of the place, and by $h$ the observed height $h^{\prime}$ reduced to the temperature $\boldsymbol{\Gamma}$.

The difference of level $x$ between the two stations is given by the formula,

$$
x=60158.6 \mathrm{ft} . \times \log \cdot \frac{\mathrm{H}}{h} \times\left\{\begin{array}{c}
\left(1+\frac{t+t^{\prime}-64}{2010}\right) \\
(1+0.00265 \cos .2 \mathrm{~L}) \\
\left(1+\frac{x+52251}{20586629}+\frac{s}{104+4315}\right)
\end{array}\right\}
$$

But $h$ represents the height $h^{\prime}$ reduced from the temperature $\mathrm{T}^{\prime}$ to the temperature T. The expansion of mercury for $1^{\circ}$ Fahr. is 0.0001000 ; that of the brass which forms the scale of the barometer is 0.0000104 ; the difference is 0.0000896 . Hence we have $h=h^{\prime}\left\{1+0.0000896\left(\mathrm{~T}-\mathrm{T}^{\prime}\right)\right\}$.

Therefore,

$$
\text { 60158. } 6 \mathrm{ft} . \log \cdot \frac{\mathrm{H}}{h}=60158.6 \mathrm{ft} . \log . \frac{\mathrm{H}}{h^{\prime}}-2.3409 \mathrm{ft} .\left(\mathrm{T}-\mathrm{T}^{\prime}\right) .
$$

Part I. of the accompanying Table furnishes in English feet the value of the expression $60158.6 \log$. H for heights of the barometer from 11 to 31 inches; only they have all been diminished by the constant 27541.5 feet which does rot change the difference

$$
60158.6 \text { log. } \mathrm{H}-60158.6 \log . h .
$$

Part II. furnishes the correction - $2.3409\left(\mathrm{~T}-\mathrm{T}^{\prime}\right)$ depending upon the difference ' $\mathrm{T}-\mathrm{T}$ ' of the temperatures of the barometers at the two stations. This cor-
rection is generally negative. It would be positive if $\mathrm{T}-\mathrm{T}^{\prime}$ were negative; that is if the temperature ' $\mathrm{T}^{\prime}$ of the barometer at the upper station exceeded the temperature T at the lower station.

Part III. gives the correction $\mathrm{A} \times 0.00265 \cos .2 \mathrm{~L}$, to be applied to the approximate altitude $A$, and which arises from the variation of gravity from the latitude of 45 degrees, to the latitude L of the place of observation. This correction has the same sign as cos. 2 L ; that is, it is positive from the equator to 45 degrees, and negative from 45 degrees to the pole.

Part IV. gives the correction $A \times \frac{A+5223}{20>629}$, which is always to be added to the approximate height $A$, and which is due to the diminution of gravity on the vertical.

Part V. furnishes for the approximate difference of Ievel A the small correction $\mathrm{A} \times \frac{s}{104+4315}$ corresponding to several values of the height $s$ of the lower station. But in place of $s$ there has been substituted as the argument of the table, the height H of the barometer at this station.

## IMethod of Computation.

Take from Part I. the two numbers corresponding to the observed barometric heights H and $h^{\prime}$. From their difference subtract the correction 2.3409 ( T - ' I ', found in Part II. with the difference T - $\mathrm{T}^{\prime}$ of the thermometers attached to the barometers. We thus obtain an approximate altitude $a$.

We then calculate the correction $a \frac{t+t^{t}-64}{900}$ for the temperature of the air, by multiplying the nine-hundredth part of $a$ by the sum of the temperatures $t$ and $t^{\prime}$ diminished by 64 . This correction is of the same sign as $t+t^{\prime}-64$. We thus obtain a second approximate altitude A.

With A and the latitude of the place L , we seek in Part III. the correction $\mathrm{A} \times$ $0.00265 \cos .2 \mathrm{~L}$ arising from the variation of gravity with the latitude.

For the approximate height $A$, Part IV. gives the correction $A \times \frac{A+522 \pi 1}{210 \sim 629}$ arising from the diminution of gravity on a vertical. This correction is always additive.

Finally, when the height $s$ of the lower station is considerable, the small correction $\mathrm{A} \times \frac{s}{1041315}$ may be found in Part V. This correction is always additive.

## Example 1.

M. Humboldt made the following observations on the mountain of Guanaxuato, in Mexico, in Latitude $21^{\circ}$, viz.

|  | Upper station. | Lower station near the sea. |
| :--- | :---: | :---: |
| Thermometer in open air, | $t^{\prime}=70^{\circ} .3$ | $t=77^{\circ} .5$ |
| Thermometer to barometer, $\mathrm{T}^{\prime}=70^{\circ} .3$ | $\mathrm{~T}=77^{\circ} .5$ |  |
| Barometer, | $h^{\prime}=23.66$ | $\mathrm{H}=30.046$ |

Required the difference in the height of the two stations.

$$
\begin{array}{ll}
\mathrm{D} & 48
\end{array}
$$

| Part I. gives $\left\{\begin{array}{l}\text { for } \mathrm{H}=30.046 \text { inches } \\ \text { for } h=23.66 \text { inches }\end{array}\right.$ | $\begin{aligned} & 27649.7 \\ & 2 i 406.9 \end{aligned}$ |
| :---: | :---: |
| Difference | 6242.8 |
| Part II. gives for $\mathrm{T}-\mathrm{T}^{\prime}=7^{\circ} .2$, | -16.9 |
| Approximate altitude $a$, | 6225.9 |
| $\frac{a}{900}\left(t+t^{\prime}-64\right)=6.918 \times 83.8$, | +579.7 |
| Second approximate altitude A, | 6805.6 |
| Part III. gives for $\mathrm{A}=6806$, and $\mathrm{L}=21^{\circ}$, | +13.3 |
| Part IV. gives for 6806, | +19.3 |
| Height above the sea, | 6838.2 |

## Example 2.

M. Gay Lussac in his celebrated balloon ascent in 1805 , found his barometer to indicate 12.945 English inches, the temperature being $14^{\circ} .9$ Fahrenheit. The barometer at Paris at the same time indicated 30.145 English inches with a temperature of $87^{\circ} .44$ Fahrenheit. Required the elevation of the balloon above Paris.

| $\text { Part I. gives }\left\{\begin{array}{l} \text { for } \mathrm{H}=30.145 \text { inches } \\ \text { for } h^{\prime}=12.945 \text { inches } \end{array}\right.$ | 27735.6 <br> 5650.4 |
| :---: | :---: |
| Difference, | 22085.2 |
| Part II. gives for $\mathrm{T}-\mathrm{T}^{\prime}=72^{\circ} .54$, | -169.9 |
| Approximate altitude $a$, | 21915.3 |
| $\frac{a}{900}\left(t+t^{\prime}-64\right)=24.35 \times 38.34$, | +933.6 |
| Second approximate altitude A, | 22848.9 |
| Part III. gives for $\mathrm{A}=22848$, and $\mathrm{L}=48^{\circ} 50^{\circ}$ | -8.2 |
| Part IV. gives for 22848, | +82.1 |
| Height of balloon above Paris, | 22922.8 |

D

| PART I. <br> Argument, the observed IIeight of the Barometer at either Station, |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Diff. | Inches. | Feet. | Diff. | Inches. | Feet. | Diff. | Inches. | Feet. | Diff. |
| 11.0 | 1396.9 |  | 16.0 | 11186.3 |  | 21.0 | 18291.0 |  | 26.0 | 23871.0 |  |
| 11.1 | 1633.3 |  | 16.1 | 11349.1 |  | 21.1 | 18415.1 |  | 26.1 | 23971.3 | 0.3 |
| 11.2 | 1567.6 |  | 16.2 | 11510.9 |  | 21.2 | 18538.7 |  | 26.2 | 24071.2 | 9 |
| 11.3 | 2099.9 |  | 16.3 | 11671.7 |  | 21.3 | 15661.6 |  | 26.3 | 24170.7 | 99.5 |
| 11.4 | 2330.1 |  | 16.4 | 11831.5 |  | 21.4 | 18784.0 |  | 26.4 | 24269.8 | 99.1 |
| 11.5 | 2558.3 |  | 16.5 | 11990.3 | 158.8 | 21.5 | 18905.8 |  | 26.5 | 24368.6 | 98.8 |
| 11.6 | 2784.5 |  | 16.6 | 12148.2 | 157.9 | 21.6 | 19027.0 |  | 26.6 | 24467.0 | 98.4 |
| 11.7 | 3008.7 |  | 16.7 | 12305. 1 | 156.9 | 21.7 | 19147.7 | 120.7 | 26.7 | 24565.1 | 98.1 |
| 11.8 | 3231.1 |  | 16.8 | 12461.0 | 15 | 21.8 | 19267.8 | 120.1 | 26.8 | 24662.7 | 97.6 |
| 11.9 | 3451.6 |  | 16.9 | 12616.1 | 155.1 | 21.9 | 19387.4 | 119.6 | 26.9 | 24760.0 | 97.3 |
| 12.0 | 3670.2 | 2 | 17.0 | 12770.2 | 15 | 22.0 | 19506.4 | 119.0 | 27.0 | 24857.0 | 97.0 |
| 12.1 | 3887.0 | 6.8 | 17.1 | 12923.5 | 153.3 | 22.1 | 19624.9 | 118.5 | 27.1 | 24953.6 | 96.6 |
| 12.2 | 4102.0 | 215.0 | 17.2 | 13075.8 | 152.3 | 22.2 | 19742.9 | 118.0 | 2 | 25049.8 | 96.2 |
| 12.3 | 5315.3 | 213.3 | 17.3 | 13227.3 | 151.5 | 22.3 | 19860.3 | 117.4 | 3 | . 7 | 95.9 |
| 12.4 | 4526.9 | 211.6 | 17.4 | 13377.9 | 150.6 | 22.4 | 19977.2 | 116.9 | , | 2 | 95.5 |
| 12.5 | 4736.7 | 209.8 | 17.5 | 13527.6 | 149.7 | 22.5 | 20093.6 | 116.4 | 27.5 | 25336.4 | 95.2 |
| 12.6 | 4944.9 | 208.2 | 17.6 | 13676.5 | 148.9 | 22.6 | 20209.4 | 115.8 | 27.6 |  | 94.8 |
| 12.7 | 5151.4 | 206.5 | 17.7 | 13S24.5 | 148.0 | 22.7 | 20324.8 | 115.4 | 27.7 |  | 94.5 |
| 12.8 | 5356.4 | 205.0 | 17.8 | 13971.7 | 147.2 | 22.8 | 20439.6 | 114.8 | 27.8 |  | 94.2 |
| 12.9 | 5559.7 | 203.3 | 17.9 | 14118.0 | 116.3 | 22.9 | 20554.0 | 114.4 | 27.9 | 25713.7 | 93.8 |
| 13.0 | 51761.4 |  | 18.0 | 14263.6 | 145.6 | 23.0 | 20667.8 | 113.8 | 28.0 | 25807.1 | 93.4 |
| 13.1 | 5961.6 |  | 18.1 | 14408.3 | $1+$ | 23.1 | 20781.1 | 113.3 | 28.1 | 25900.3 | 93.2 |
| 13.2 | 6160.3 | 198.7 | 18.2 | 14552.3 | $14+0$ | 23.2 | 20894.0 | 112.9 | 28.2 | 25993.1 | 92.8 |
| 13.3 | 57.5 | 19 | 18.3 | 14695.4 | 143.1 | 23.3 | 21006.4 | 112.4 | . 3 | 26085.6 | 92.5 |
| 13.4 | 65.53 .2 | 195.7 | 18.4 | 14837.8 | 142.4 | 23.4 | 21118.3 | 111.9 | 28.4 | 26177.7 | 92.1 |
| 13.5 | 6747.5 | 19 | 18.5 | 14979.4 | 141.6 | 23.5 | 21229.7 | 111.4 | 28.5 | 26269.6 | 91.9 |
| 13.6 | 6940.3 | 19 | 18.6 | 15120.3 | 140.9 | 23.6 | 21340.6 | 110.9 | 28.6 | 26361.1 | 91.5 |
| 13.7 | 7131.7 | 19 | 18.7 | 15260.3 | 140.0 | 23.7 | 21451.1 | 110.5 | 28.7 | 6452.3 | 91.2 |
| 13.8 | 7321.7 | 190.0 | 18.8 | 15399.7 | 139.4 | 23.8 | 21561.1 | 110.0 | 28.8 | 26543.2 | 90.9 |
| 13.9 | 7.510 .3 | 188.6 | 18.9 | 15538.3 | 138.6 | 23.9 | 21670.6 | 109.5 | 28.9 | 26633.7 | 90.5 |
| 14.0 | 7697.6 | 187.3 | 19.0 | 15676.2 | 137.9 | 24.0 | 21779.7 | 109.1 | 29.0 | 26724.0 | 90.3 |
| 14.1 | 7883.6 |  | 19.1 | 15818.3 |  | 24.1 | 21888.4 |  | 29.1 | 26813.9 | 89.9 |
| 14.2 | 8068.2 |  | 19.2 | 15949.8 |  | 24.2 | 21996.6 |  | 29.2 | 26903.5 | 89.6 |
| 14.3 | 82.51 .5 |  | 19.3 | 16085.5 |  | 21.3 | 22104.3 | 107.7 | 29.3 | 26992.8 | 89.3 |
| 14.4 | 8433.6 |  | 19.4 | 16220.5 |  | 24. | 22211.6 | 10 | 29.4 | 27081.9 | 89.1 |
| 14.5 | 8614.4 |  | 19.5 | 16354.8 | 134.3 | 24.5 | 22318.4 | 10 | 29.5 | 27170.6 | 85.7 |
| 14.6 | 8794.0 |  | 19.6 | 16488.5 | 133.7 | 21.6 | 22.124 .8 | 106.4 | 29.6 | 27259.0 | 88.4 |
| 14.7 | 8972.3 |  | 19.7 | 16621.4 | 132.9 | 24.7 | 22.530 .8 | 106.0 |  | 7347.1 | 88.1 |
| 14.8 | 9149.5 |  | . 8 | 16753.7 | 132.3 | 24.8 | 23 | 105.6 |  |  | 87.8 |
| 14.9 | 9325.5 |  | 19.9 | 16855.3 | 131.6 |  |  | 105 |  | - | 87.6 |
| 15.0 | 9500.3 | 17 | 20.0 | 17016.3 | 131.0 | 25.0 |  | 104.8 |  |  | 87.2 |
| 15.1 | 9673.8 | 17 | 20.1 | 17146.6 | 130.3 | 25.1 |  | 104.3 |  |  | 86.9 |
| 15.2 | 9846.2 | 172.4 | 20.2 | 17276.3 | 129.7 | 25.2 |  | 103.5 |  |  | 56.7 |
| 15.3 | 10017.5 | 171.3 | 20.3 | 17405.3 | 129.0 | ? 5.3 |  | 103.5 |  |  | 86.4 |
| 15.4 | 10157.7 | 170.2 | 20.4 | 17533.7 | 128.4 | 25.4 |  | 103.1 |  |  | 86.9 |
| 15.5 | 10356.8 | 169.1 | 20.5 | 17661.4 | 127.7 | 25.5 |  | 102.6 |  |  | 85.8 |
| 15.6 | 10524.5 | 168.0 | 20.6 | 17788.6 | 127.2 | 25.6 |  | 102.3 |  |  | 85.6 |
| 15.7 | 10691.8 | 167.0 | 20.7 | 17915.1 | 126.5 | 25.7 |  | 101.8 |  | 51 | 85.2 |
| 15.8 | 10857.7 | 165.9 | 20.8 | 18041.0 | 12.5 .9 | 25.8 |  | 101.5 |  |  | 85.0 |
| 15.9 | 11022.5 | 164.8 | 20.9 | 18166.3 | 125.3 | 25.9 |  | 101.1 |  | 25297.3 | 84.7 |
| 16.0 | 11186.3 | 163.8 | 21.0 | 18291.0 | 124.7 | 2.9 .9 | 23871.0 | 100.7 | 30.9 31.0 | 28382.0 28466.4 | 84.4 |

PART II.
Correction due to $\mathrm{T}-\mathrm{T}^{\prime}$, or the Difference of the Temperatures of the Barometers at the two Stations.
This Correction is Negative when the Temperature at the Upper Station is louest, and wipe vers t.

| T $-\mathrm{T}^{\prime}$. | Correction. | $\mathrm{T}-\mathrm{T}^{\text {d }}$. | Correetion. | T- $\mathrm{T}^{\prime}$. | Correction. | T-T. | Correction. | $\mathrm{T}-\mathrm{I}^{\text {\% }}$ | Correction. | T- T'. | Correetion. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fah't. | Feet. | Fah't. | Feet. | Fah't. | Feet. | Fah't. | Feet. | Fah't. | Foet. | Fah't. | Feet. |
| - |  | 1 |  | $\bigcirc$ |  | $\bigcirc$ |  | $\bigcirc$ |  | 6 |  |
| 1 | 2.3 | 14 | 32.8 | 27 | 63.2 | 40 | 93.6 | 53 | 124.1 | 66 | 154.5 |
| 2 | 4.7 | 15 | 35.1 | 28 | 6.5 .5 | 41 | 96.0 | 54 | 126.4 | 67 | 156.8 |
| 3 | 7.0 | 16 | 37.5 | 29 | 67.9 | 42 | 98.3 | 55 | 128.7 | 68 | 159.2 |
| 4 | 9.4 | 17 | 39.8 | 30 | 70.2 | 43 | 100.7 | 56 | 131.1 | 69 | 161.5 |
| 5 | 11.7 | 18 | 42.1 | 31 | 72.6 | 44 | 103.0 | 57 | 133.4 | 70 | 163.9 |
| 6 | 14.0 | 19 | 44.5 | 32 | 74.9 | 45 | 105.3 | 58 | 135.5 | 71 | 166.2 |
| 7 | 16.4 | 20 | 46.8 | 33 | 77.3 | 46 | 107.7 | 59 | 138.1 | 72 | 168.6 |
| 8 | 18.7 | 21 | 49.2 | 34 | 79.6 | 47 | 110.0 | 60 | 140.4 | 73 | 170.9 |
| 9 | 21.1 | 22 | 51.5 | 35 | 81.9 | 48 | 112.4 | 61 | 142.8 | 74 | 173.3 |
| 10 | 23.4 | 23 | 53.8 | 36 | 84.3 | 49 | 114.7 | 62 | 145.1 | 75 | 175.6 |
| 11 | 25.8 | 24 | 56.2 | 37 | 86.6 | 50 | 117.0 | 63 | 147.5 | 76 | 177.9 |
| 12 | 28.1 | 25 | 58.5 | 38 | 89.0 | 51 | 119.4 | 64 | 149.8 | 77 | 180.3 |
| 13 | 30.4 | 26 | 60.9 | 39 | 91.3 | 52 | 121.7 | 65 | 152.2 | 78 | 182.6 |


| App. <br> Alt. | PART III. <br> Correction due to the Change of Gravity from the Latitnde of 450 to the Latitude of the Ilace of Observation. <br> Positice from Lat. 00 to 450 ; Negative from Lat. 450 to 900 . |  |  |  |  |  | $\begin{aligned} & \text { PART } \\ & \text { IV. } \\ & \text { Correction } \\ & \text { for } \\ & \text { Decrease } \\ & \text { of Gravity } \\ & \text { on a } \\ & \text { Vertical. } \\ & \text { Always } \\ & \text { Positive. } \end{aligned}$ | PART V. <br> Correction due to the Height of the Lower Station. <br> Always Positive. |  |  |  |  |  |  | AppAlt. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Latitude. |  |  |  |  |  |  | Height of Barometer at Lower Station. |  |  |  |  |  |  |  |
|  | 00 | 100 | 200 | 300 | 400 |  |  |  |  |  |  |  |  |  |  |
|  | 900 | 0 | 700 | 600 | 500 |  |  | 16 in. | 18 in. | 0 in. | 22 in. | $24 \mathrm{in}$. | 26 in. | in. |  |
| Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | t. | t. | t. | t. | Feet. | Feet. | Feet. | 'eet. |
| 100 | 6 | . 5 | . 0 | 1.3 | 0.5 | 0 | 2.5 | . 6 | 1.3 | 1.0 | 0.8 | 0.6 | 0.4 | 0.2 | 1000 |
| 2000 | 5.3 | 5.0 | 4.1 | 2.6 | 0.9 | 0 | 5.2 | 3.1 | 2.5 | 2.0 | 1.5 | 1.1 | 0.7 | 0.3 | 2000 |
| 3000 | 7.9 | 7.5 | 6.1 | 4.0 | 1.4 | 0 | 7.9 | 4.7 | 3.8 | 3.0 | 2.3 | 1.7 | 1.1 | 0.5 | 3000 |
| 4000 | 10.6 | 10.0 | 8.1 | 5.3 | 1.8 | 0 | 10.8 | 6.3 | 5.1 | 4.0 | 3.1 | 2.2 | 1.4 | 0.7 | 4000 |
| 5000 | 13.2 | 12.4 | 10.1 | 6.6 | 2.3 | 0 | 13.7 | 7.8 | 6.4 | 5.0 | 3.8 | 2.8 | 1.8 | 0.8 | 5000 |
| 6000 | 15.9 | 14.9 | 12.2 | 7.9 | 2.8 | 0 | 16.7 | 9.4 | 7.6 | 6.0 | 4.6 | 3.3 | 2.1 | 1.0 | 6000 |
| 7000 | 18.5 | 17.4 | 14.2 | 9.3 | 3.2 | 0 | 19.9 | 11.0 | 8.9 | 7.1 | 5.4 | 3.9 | 2.5 | 1.2 | 7000 |
| 8000 | 21.2 | 19.9 | 16.2 | 10.6 | 3.7 | 0 | 23.1 | 12.5 | 10.2 | 8.1 | 6.2 | 4.4 | 2.8 | 1.3 | s000 |
| 9000 | 23.8 | 22.4 | 18.3 | 11.9 | 4.1 | 0 | 26.4 | 14.1 | 11.4 | 9.1 | 6.9 | 5.0 | 3.2 | 1.5 | 9000 |
| 10000 | 26.5 | 24.9 | 20.3 | 13.2 | 4.6 | 0 | 29.8 | 15.7 | 12.7 | 10.1 | 7.7 | 5.5 | 3.5 | 1.7 | 10000 |
| 11000 | 29.1 | 27.4 | 22.3 | 14.6 | 5.1 | 0 | 33.3 | 17.2 | 14.0 | 11.1 | 8.5 | 6.1 | 3.9 | 1.8 | 11000 |
| 12000 | 31.8 | 29.9 | 24.4 | 15.9 | 5.5 | 0 | 36.9 | 18.8 | 15.3 | 12.1 | 9.2 | 6.6 | 4.2 | 2.0 | 12900 |
| 13000 | 34.4 | 32.4 | 26.4 | 17.2 | 6.0 | 0 | 40.6 | 20.4 | 16.5 | 13.1 | 10.0 | 7.2 | 4. | 2.2 | 1:000 |
| 14000 | 37.1 | 34.9 | 28.4 | 18.5 | 6.4 | 0 | 44.4 | 21.9 | 17.8 | 14.1 | 10.8 | 7.7 | 4.9 | 2.3 | 14000 |
| 15000 | 39.7 | 37.3 | 30.4 | 19.9 | 6.9 | 0 | 48.3 | 23.5 | 19.1 | 15.1 | 11.5 | 8.3 | 5.3 | 2.5 | 15000 |
| 16000 | 42.4 | 39.8 | 32.5 | 21.2 | 7.4 | 0 | 52.3 | 25.1 | 20.3 | 16.1 | 12.3 | 8.5 | 5.6 | 2.7 | 16000 |
| 17000 | 45.0 | 42.3 | 34.5 | 22.5 | 7.8 | 0 | 56.4 | 26.6 | 21.6 | 17.1 | 13.1 | 9.4 | 6.0 | 2.8 | 17000 |
| 18000 | 47.7 | 44.8 | 36.5 | 23.8 | 8.3 | 0 | 60.5 | 28.2 | 22.9 | 18.1 | 13.8 | 9.9 | 6.3 | 3. | 18000 |
| 19000 | 50.3 | 47.3 | 38.6 | 25.2 | 8.7 | 0 | 64.8 | 29.8 | 24.1 | 19.2 | 14.6 | 10.5 | 6.7 | 3.2 | 19000 |
| 20000 | 53.0 | 49.8 | 40.6 | 26.5 | 2 | 0 | 69.2 | 31.3 | 25.4 | 20.2 | 15.4 | 11.0 | 7.0 | 3.3 | 20000 |
| 21000 | 55.6 | 52.3 | 42.6 | 27.8 | 9.7 | 0 | 73.6 | 32.9 | 26.7 | 21.2 | 16.1 | 11.6 | 7.4 | 3. | 21000 |
| 22000 | 58.3 | 54.8 | 44.7 | 29.1 | 10.1 | 0 | 78.2 | 34.5 | 28.0 | 22.2 | 16.9 | 12. | 7.7 | 3.7 | 22000 |
| 23000 | 60.9 | 57.3 | 16.7 | 30.5 | 10.6 | 0 | 82.9 | 36.0 | 29.2 | 23.2 | 17.7 | 12. | 8.1 | 3.8 | 23000 |
| 24000 | 63.6 | 59.8 | 48.7 | 31.8 | 11.0 | 0 | 87.6 | 37.6 | 30.5 | 24.2 | 18.5 | 13.2 | 8.4 | 4.0 | 24000 |
| 25000 | 66.2 | 62.2 | 50.7 | 33.1 | 11.5 | 0 | 92.5 | 39.1 | 31.8 | 25.2 | 19.2 | 13.8 | 8.8 |  | 25000 |

## I V.

TABLES

FOR REDUCING RAROMETRICAL OBSERVATIONS TO THE LEVEL OF THE SEA, OR TO ANY OTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.

The following tables, published by M. C. Dippe, in the Astronomische Nachrichten, No. 1056, November, 1856, are a modification and extension of Gauss's tables, published in Schumacher's Jahrbuch, for 1836 and the following years, which are based on the formula of Laplace. In this new form they answer a double purpose. They give the means of solving a problem which often occurs in Meteorology, viz. : The difference of clevation between two stations, and the temperature of the air at both, being known, to reluce the height of the barometer at one of the stations to the height it would have at the other. They are likewise adapted to the computation of heights from baromerrical observations.

The formola of Laplace, which has been used, the Metres being reduced to Toises, and the Centigrade degrees to degrees of Reammur, reads as follows:

$$
h=9407.73\left(1+\begin{array}{c}
t+t^{\prime} \\
400
\end{array}\right)(1+a \cos 2 \phi)\left(1+\frac{h}{r}\right)\left\{\log \frac{b}{b^{\prime}}+2 \log \left(1+\frac{h}{r}\right)\right\} .
$$

Where $t$ and $t^{\prime}=$ the temperatures of the air, in degrees of Reaumur, at the lower and upper station,
$b$ and $b^{\prime}=$ the height of the barometer, in any seale, reduced to the freezing point, at the lower and upper station,
$h=$ the difference of level, in toises, between the two stations,
$r=$ the distance, in toises, of the lower station to the centre of the Earth,
$\phi=$ the latitude of the place of observation,
$a=$ the inerease of gravity from the equator to the poles.
Making, besides, $m=$ the modulus of the common logarithms, the formula becomes, with sufficient accuracy,

$$
\log b-\log b^{\prime}=h\left\{\begin{array}{c}
1 \\
9407.73
\end{array} \cdot \frac{1}{1++_{400}^{t+t^{\prime}}}-\frac{2 m}{r}\right\} \cdot 1+\begin{gathered}
1 \\
1+a \cos 2 \phi
\end{gathered} \frac{1}{1+\frac{h}{r}} .
$$

Assuming $r$, or the radins of the Earth, at $45^{\circ}$ latitude $=3266631$ toises, and $a=0.002595$, instead of 0.002845 adopted in Gauss's tables, and making

$$
\begin{aligned}
& u=\log b-\log b^{\prime}, \\
& a=\log \left(\begin{array}{c}
1 \\
9407.73
\end{array} \cdot \frac{1}{1+{ }_{400^{-}}^{t+t^{i}}}-\frac{2 m}{r}\right), \\
& c=-m a \cos 2 \phi, \\
& c^{\prime}=-\frac{m h}{r},
\end{aligned}
$$

then the reduction of the height of the barometer to another level is given by the formula,

> 1. $\quad \log u=\log h+a+c+c^{\prime} ;$
> 2. $\quad \log b=\log b^{\prime}+u$.

Table I. contains the values of $a$ for the argument $t+t^{\prime} ; 10$ units are to be subtracted from the characteristic.

Table II. gives the values of $c$ for the argument $\phi$, or the correction for the change of gravity in latitude, which is negative from $0^{\circ}$ to $45^{\circ}$, positive from $45^{\circ}$ to $90^{\circ}$.

Table III. furnishes the values of $c^{\prime}$ for the argument $h$ in toises, or the correction for the decrease of gravity on the vertical. Both in Tables II. and III. the values of $c$ and $c^{\prime}$ are given in units of the fifth decimal place.

The difference of elevation of the two stations is given by the formula,

$$
\begin{aligned}
& \text { 1. } \quad u=\log b-\log b^{\prime} \\
& \text { 2. } \quad \log h=\log u+\mathrm{A}+c+c^{\prime}
\end{aligned}
$$

in which A is the arithmetical complement of $a$, and the corrections $c$ and $c^{\prime}$ receive contrary signs. For the sake of convenience, the values of $A$ have been placed in Table I., and in Table III. the correction for A is found in another column, with the more convenient argument $v=\log u+\mathrm{A}$.

If the heights of the barometers have not been reduced to the freezing point, then, B and $\mathrm{B}^{\prime}$ being the unreduced heights of the barometers, and T and $\mathrm{T}^{\prime}$ the temperature of the attached thermometer in degrees of Reaumur,

$$
b: b^{\prime}=\frac{\mathrm{B}}{1+\mathrm{T}_{4440}}: \frac{\mathrm{B}^{\prime}}{1+{ }_{4440}^{\mathrm{T}^{\prime}}},
$$

and making ${ }_{4440}^{m}=\beta$,

$$
u=\log b-\log b^{\prime}=(\log \mathrm{B}-\beta \mathrm{T})-\left(\log \mathrm{B}^{\prime}-\beta \mathrm{T}^{\prime}\right)
$$

Instead of $\beta=0.000098$, we can write with sufficient accuracy 0.00010 .

## Use of the Tables.

These tables can be used in any latitude, and for any barometrical scale; but the indications of the barometers must be reduced to the freezing point; and the temperatures of the air must be given in degrecs of Reaumur. The tables suppose the use of logarithms with 5 decimals, such as those of Lalande, and give the results in toises.

## I. For Reducing Barometrical Observations to another Level.

$$
\text { Given } h \text { in toises, } t, t^{\prime}, \phi, \text { and } b \text { or } b^{\prime}
$$

To find $b$ or $b^{\prime}$.
In Table I. with the argument $t+t^{\prime}$, take $a$,
In Table II. with the argument $\phi$, take $c$,
In Table III. with the argument $h$, take $c^{\prime}$,
the last two corrections being given in units of the fifth decimal, making $\log h+a+c+c^{\prime}-10$ (whole units) $=\log u$.
Then we have

> for a level lower by $h$ toises, $\log b=\log b^{\prime}+u$; for a level higher by $h$ toises, $\log b^{\prime}=\log b-u$.

If $h$, or the difference of elevation, is given in metres, take $c^{\prime}$, which is always negative, from Table III. (for A) with the argument $v=\log h+9.71$, and write

$$
\log u=9.71018+\log h+a+c+c^{\prime}-10 \text { (whole units). }
$$

Then again is $\log b=\log b^{\prime}+u$.
D

## Erample 1.

Suppose the height of the barometer, reduced to the freezing point, to be $b^{\prime}=$ 295.39 Paris lines; the temperature of the air $t^{\prime}=11^{\circ} .8$ Reammur, and the latitude $\phi=51^{\circ} 48^{\prime}$; the increase of heat downwards being $1^{\circ}$ Reaummr for 100 toises. What is the beight of the barometer, reduced to the freezing point, at a station lower by $h=498.2$ toises ?

$$
\text { In th case } t=t^{\prime}+4^{\circ} .98=16^{\circ} .78 \text {, and } t+t^{\prime}=\mathbf{2} 8^{\circ} .58
$$

Then

|  | $\log h=$ | 2.69740 |
| :---: | :---: | :---: |
| Table I. for $28^{\circ} .58$ gives | Table I. or 25.58 gives $\quad a=\quad .99538$ | 5.99538 |
| Table II. for $51^{\circ} 48^{\prime}$ gives $\quad c=+0.000 \geq 6$ <br> Table III, for 498 toises gives $c^{\prime}=-0.00007$ |  |  |
|  |  |  |
| $\log u=$ |  | $\begin{aligned} & 8.69297 \\ & 0.04931 \end{aligned}$ |
| $\log b^{\prime}=$ |  | 2.47010 |
| $\log b=$ |  | 251971 |
| Barometer at the lower station $b=$ |  | 330.90 |

## Example 2.

Suppose the reduced barometer $b^{\prime}=598.6$ millimetres; the temperature of the arr $t^{\prime}=18^{\circ} .0$ Centigrade $=14^{\circ} .4$ Reaumur ; the difference of cheration $h=2: 17$ metres, $\phi=3^{\circ}$. The temperature of the an the lower station $t=22^{\circ} .5$ Centigrade $=22^{\circ} .0$ Reaumur, and $t+t^{\prime}=36^{\circ} .4$ Reaumur.

$$
\begin{aligned}
& \text { Then } \quad \log h=\left\{\begin{array}{r}
\log 2217=\quad 3.34577 \\
+\quad 9.71018
\end{array}\right. \\
& 3.05595 \quad v=3.06 \\
& a=5.98750 \\
& c=-0.00112 \\
& c^{\prime}=-0.00015 \\
& \log u=9.01218-10 \\
& u=011020 \\
& \log b^{\prime}=9.77714 \\
& \log b=9.88734 \\
& \text { Barometer at the lower station } \delta=771.5 \text { millimetres. }
\end{aligned}
$$

## 2. For Computing Differences of Eleration from Barometrical Observations.

Given the unreduced height of the barometer at the lower and upper station, $B$ and $B^{\prime}$; the temperatures of the attached thermometers, $T$ and ' $\Gamma^{\prime}$; the temperatures of the air, $t$ and $t^{\prime}$; and the latitude, $\phi$.

To find $h$, or the difference of elevation between the two stations.
Subtract $\left(\log \mathrm{B}^{\prime}-10 \mathrm{~T}^{\prime}\right)$ from $(\log \mathrm{B}-10 \mathrm{~T})$, paying due attention to the nature of the signs of T and $\mathrm{T}^{\prime}$, and taking the numbers $10{ }^{\mathrm{T}} \mathrm{T}$ and $10^{\prime} \mathrm{T}^{\prime}$ as units of the fifth decimal. Calling then $(\log \mathrm{B}-10 \mathrm{C})-\left(\log \mathrm{B}^{\prime}-10 \mathrm{~T}^{\prime}\right)=u$, or if the heights of the Barometers are reduced to the freezing point, $\log b-\log b^{\prime}=u$, take,

In Table I., A with the argument $t+t^{\prime}$, and make $r=\log u+\mathrm{A}$.
In Tible Il., with the argument $\phi$, take $c$ reversing the sign.

In Table III., for A, with the argument $v$, take $c^{\prime}$, which, in this case, is always positive ; then, remembering that the values of $c$ and $c^{\prime}$ are given in units of the fifth decimal, we have,

| $v+c+c^{\prime}$ | $=\log h$ in toises, |
| :--- | :--- |
| $v+c+c^{\prime}+0.28982$ | $=\log h$ in metres, |
| $v+c+c^{\prime}+0.80584$ | $=\log h$ in English feet. |

Example 1.

U. station $\mathrm{B}^{\prime}=268.215$ Paris lines $; \mathrm{T}^{\prime}=+8.40 \mathrm{R} . ; t=+7.92 \mathrm{R}$.

$$
t+t^{\prime}=\quad 23.88 \mathrm{R}
$$

$$
\begin{aligned}
& \log B=2.51722-10 \times 15.88=2.51563 \\
& \log B=2.42848-10 \times 8.4=2.42764 \\
& u=0.08799 \\
& \log u=\quad 8.94443 \\
& \mathrm{~A}=3.9998{ }^{2} \\
& r=\quad 2.9495 \\
& c=-0.00002 \\
& c^{\prime}=+0.00012 \\
& \log h=\quad 2.94435 \\
& h=879.74 \text { toises. }
\end{aligned}
$$

Example 2.
L. stition $\mathrm{B}=763.15$ millımetres $; \mathrm{T}=t=20.3 \mathrm{Cent}=20.24 \mathrm{R} . ; \phi=21$.
U. station $\mathrm{B}^{\prime}=600.95$ millimetres $; ~ \mathrm{~T}^{\prime}=t^{\prime}=21.3$ Cent. $=17.04 \mathrm{R}$.

$$
\begin{aligned}
& t+t^{\prime}=37.28 \mathrm{R} . \\
& \log \mathrm{B}=9.89261-10 \times 20.24=9.88059 \\
& \log \mathrm{~B}^{\prime}=9.77884-10 \times 17.04=9.77714 \\
& u=0.10345 \\
& \log u=9.01473 \\
& \mathrm{~A}=4.01337 \\
& v=3.02810 \\
& c=+0.00084 \\
& c^{\prime}=+0.00014 \\
& \log h=3.02908 \text { for toises. } \\
& \log h=0.28982 \\
& \log h=3.31890 \text { for metres. } \\
& \\
& \log h=3.02908 \text { for toises. } \\
& 0.30584
\end{aligned}
$$

I. Argument: Sum of the Temperatures of the Air in Degrees of Reaumur.

| $\left\lvert\, \begin{gathered} t+t^{\prime} \\ \text { Reaumur. } \end{gathered}\right.$ | Correctiou for |  |  | $t+t^{\prime}$ <br> Reaumur | Correction for |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | a | Difference. | A |  | ${ }^{\prime}$ | Difference. | A |
| $-60^{\circ}$ | 6.09617 |  | 3.90383 | $-0^{\circ}$ | 6.0.1776 |  | 3.952 .24 |
| -59 | 6.09189 | 128 | 3.90511 | -19 | 6.04661 | 1.9 | 3.95339 |
| -58 | 6.09362 | 127 | 3.90638 | -18 | 6.04547 | 114 | 3.95453 |
| -5\% | 6.09235 | 127 | 3.90765 | -17 | 6.04431 | 11.3 | 3.95566 |
| -56 | 6.09108 | 127 | 3.90092 | -16 | 6.04320 | 114 | 3.95680 |
| -5.5 | 6.0898. |  | 3.91018 | -15 | 6.01207 |  | 3.95793 |
| -54 | 6.00.56 | 126 | 3.91144 | -14 | 6.0409 t | 11.3 | 3.95906 |
| -5.3 | 6.0-330 | 126 | 3.91270 | -13 | 6.03981 | 11. | 3.96019 |
| -52 | $6.0-60.5$ | 123 | 3.9139 .5 | -12 | 6.0:3069 | 11. | 3.96131 |
| -51 | 6.00150 | 125 | 3.91520 | -11 | 6.03757 | 112 | 3.96243 |
| $-50$ | 6.083 .56 |  | 3.91644 | -10 | 6.03645 |  | 3.963 .55 |
| $-49$ | $6.0-281$ | 120 | 3.91769 | -9 | 6.035.33 | 112 | 3.96467 |
| -48 | $6.0 \times 108$ | 1.0 | 3.91592 | -8 | 6.0342 | 111 | 3.96578 |
| $-47$ | 6.07984 | 124 | 3.92016 | $-7$ | 6.03311 | 111 | $3.966<9$ |
| $-46$ | 6.07861 |  | 3.92139 | -6 | 6.03201 | 110 | 3.96799 |
| -45 | 6.07738 |  | 3.92262 | - 5 | 6.03090 |  | 3.96910 |
| -4t | 6.07016 | 122 | 3.92354 | $-4$ | 18.02950 | 110 | 3.97020 |
| -13 | 6.07494 | 12. | 3.92506 | - 3 | 6.02 s 71 | 109 | 3.97129 |
| $-42$ | $6.07: 372$ | 122 | 3.12628 | - 2 | 6.02761 | 110 | 3.97239 |
| $-41$ | 6.07250 | 122 | 3.92750 | - 1 | 6.02652 | 109 | 3.97345 |
|  |  | 121 |  |  |  | 109 |  |
| $-40$ | 6.07129 |  | 3.92871 | 0 | 6.02543 |  | 3.97457 |
| -39 | 6.07009 |  | 3.92991 | +1 | 6.02 .434 | 109 | 3.97566 |
| -38 | 6.06-48 | 121 | 83.93112 | 2 | 6.02326 | jes | 3.97674 |
| -:37 | 6.06768 | 120 | 3.93232 | 3 | 6.02217 | 109 | 3.97783 |
| -36 | 6.06645 | 120 | 3.93352 | 4 | 6.02109 | 108 | 3.97891 |
| -3.5 | 6.065 .59 |  | 3.93471 | 5 | 6.02002 |  | 3.97998 |
| -:31 | 6.06410 |  | 3.93590 | 6 | 6.01895 | 107 | 3.9810 .5 |
| -33 | 6.0629 .9 |  | 3.93709 | 7 | 6.01787 | 10 | 3.98213 |
| -32 | 6.06178 | 118 | 3.93827 | 8 | 6.01680 | 107 | $398: 20$ |
| -31 | 6.0505 .5 |  | 3.93945 | 9 | 6.01574 | 106 | 3.98126 |
|  |  | 118 |  |  |  | 106 |  |
| -30 | 6.0 .5937 |  | 3.91063 | 10 | 6.01468 |  | 3.98 .532 |
| -29 | 6.05519 | 118 | 3.94181 | 11 | 6.01362 | 106 | 3.98638 |
| -28 | 6.0 .5702 | 117 | 3.94298 | 12 | 6.01256 | 106 | 3.94744 |
| --27 | 6.0 .585 | 117 | 3.94415 | 13 | 6.01150 | 106 | 3.98550 |
| -26 | 6.05469 | 116 | 3.94531 | 14 | 6.01045 | 105 | 3.98955 |
| -6 | 6.0.54 | 117 | 3.915 | 1 |  | 105 |  |
| -25 | 6.053 .52 |  | 3.94648 | 15 | 6.00940 |  | 3.99060 |
| $-24$ | 6.05236 |  | 3.94764 | 16 | 6.00835 |  | 3.99165 |
| -23 | 6.05121 | 110 | 3.94879 | 17 | 6.00731 | 104 | 3.99269 |
| -22 | 6.0 .5005 | 116 | 3.94995 | 15 | 6.00626 | 105 | 3.99374 |
| -21 | 6.04890 | 115 | 3.9 .5110 | 19 | 6.00532 | 104 | 3.99478 |
| -20 | 6.04776 | 114 | 3.95224 | +20 | 6.00418 | 104 | 3.99 .582 |
|  |  |  |  |  |  |  |  |

(Continued.)

| $t+t^{\prime}$ <br> Reauniur. | Correction for |  |  |  | Correction for |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ( $\ell$ | Difference. | A | Reanmur. | a | Difference. | A |
| $+20^{\circ}$ | 6.00418 | 103 | 3.99582 | $+40^{\circ}$ | $5.9 \times 393$ | 09 | 4.01607 |
| 21 | 6.00315 | 103 | 3.99685 | 41 | 5.94294 | 99 | 4.01706 |
| 22 | 6.00212 | 103 | 3.99788 | 42 | 5.98195 | 99 | 4.01805 |
| 23 | 6.00108 | 104 | 3.99592 | 43 | 5.9 .9097 | 98 | 4.01903 |
| 24 | 6.00006 | 102 | 3.99994 | 44 | 5.97998 | 99 | 4.02002 |
| 25 | 5.99903 |  | 4.00097 | 45 | 5.97900 |  | 4.02100 |
| 26 | 5.99801 | 102 | 4.00199 | 46 | 5.97503 | 98 | 4.02197 |
| 27 | 5.99699 | 102 | 4.00301 | 47 | 5.97705 | 98 | 4.02295 |
| 28 | 5.99597 | 102 | 4.00403 | 48 | 5.97603 | 97 | 4.02392 |
| 29 | 5.99495 | 10. | 4.00505 | 49 | 5.97511 | 97 | 4.02489 |
|  |  | 101 |  |  |  | 97 |  |
| 30 | 5.99394 |  | 4.00606 | 50 | 5.97414 |  | 4.02556 |
| 31 | 5.992 ! ${ }^{3}$ | 101 | 4.00707 | 51 | 5.97317 | 97 | 4.02653 |
| 32 | 5.99192 | 101 | 4.00808 | 52 | 5.97221 | 96 | 4.02779 |
| 33 | 5.99091 | 101 | 4.00909 | 53 | 5.97124 | 97 | 4.02576 |
| 34 | 5.98991 | 100 | 4.01009 | 54 | 5.97028 | 96 | 4.02972 |
|  |  | 101 |  |  |  | 95 | - |
| 35 | 5.98890 |  | 4.01110 | 55 | 5.96933 |  | 4.03067 |
| 36 | 5.98790 |  | 4.01210 | 56 | 5.96837 | 96 | 4.03163 |
| 37 | 5.95691 | 99 | 4.01309 | 57 | 5.96512 | 95 | 4.03255 |
| 38 | 5.93591 | 100 | 4.01409 | 59 | 5.96646 | 96 | 4.038 .54 |
| 39 | 5.98492 | 99 | 4.01509 | 59 | 5.96551 | 9. | 4.034 .49 |

II. Latitude. - Correction for a.

| For A reverse the Signs of $c$. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\phi$ | $c$ | $\phi$ | $\phi$ | $c$ | $\phi$ | $\phi$ | c | $\phi$ |
| $\bigcirc$ |  | - | - |  | - | $\bigcirc$ |  | - |
| 0 | -113+ | 90 | 15 | - $93+$ | 75 | 30 | $-56+$ | 60 |
| 1 | 113 | 89 | 16 | 96 | 74 | 31 | 53 | 59 |
| 2 | 112 | 88 | 17 | 93 | 73 | 32 | 49 | 58 |
| 3 | 112 | S7 | 18 | 91 | 72 | 33 | 46 | 57 |
| 4 | 112 | 86 | 19 | 89 | 71 | 34 | 42 | 56 |
| 5 | 111 | 85 | 20 | 86 | 70 | 35 | 39 | 55 |
| 6 | 110 | 84 | 21 | 84 | 69 | 36 | 35 | 54 |
| 7 | 109 | 83 | 22 | 81 | 68 | 37 | 31 | 53 |
| 8 | 103 | 82 | 23 | 78 | 67 | 38 | 27 | 52 |
| 9 | 107 | 81 | 24 | 75 | 66 | 39 | 23 | 51 |
| 10 | 106 | 80 | 2.5 | 72 | 6.5 | 40 | 20 | 50 |
| 11 | 104 | 79 | 26 | 69 | 61 | 41 | 16 | 49 |
| 12 | 103 | 78 | 27 | 66 | 63 | 42 | 12 | 48 |
| 13 | 101 | 77 | 28 | 63 | 62 | 43 | 8 | 47 |
| 14 | 100 | 76 | 29 | 60 | 61 | 44 | 4 | 46 |
| 15 | -98+ | 75 | 30 | $-56+$ | 60 | 45 | -0+ | 45 |

III. Decrease of Giravity on the Vertical. - Correction

| For $a$, argument $h$, in Toises, $c^{\prime}$ always Negative |  |  |  | For A, arg. ${ }^{2}$, $c^{\prime}$ always l'ositive. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $h$ | $c^{\prime}$ | 11 | $c^{\prime}$ | \% | $c^{\prime}$ |
| 100 | 1 | 1600 | 21 | 1.8 | 1 |
| 200 | 3 | 1760 | 23 | 1.9 | 1 |
| 300 | 4 | 1800 | 21 | 2.0 | 1 |
| 400 | 5 | 1900 | 25 | 2.1 | 2 |
| 500 | 7 | 2000 | 27 | 2.2 | 2 |
|  |  |  |  | 2.3 | 3 |
| 600 | 8 | 2100 | 29 | 2.4 | 8 |
| 700 | 9 | 2200 | 29 | 2.5 | 4 |
| 800 | 11 | 2:30 | 31 | 2.6 | 5 |
| 900 | 12 | 2400 | 32 | 2.7 | 7 |
| 1000 | 18 | 2560 | 33 | 2.3 | 8 |
|  |  |  |  | 2.9 | 11 |
| 1100 | 1.7 | 2600 | 35 | 3.0 | 13 |
| 1200 | 16 | 2700 | 36 | 3.1 | 17 |
| 1300 | 17 | 2800 | 37 | 3.2 | 21 |
| 1400 | 19 | 2900 | 39 | 3.3 | 27 |
| 1500 | 20 | 3000 | 40 | 3.4 | 33 |
|  |  |  |  | 3.5 | 42 |
| 1600 | 21 | 3500 | 47 | 3.6 | 53 |

## V.

## TABLES

## FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING

 ' DIFFFRENCES OF ELEVATION MEASURED BY THE BAROMETER, BY M. C. DIPPE.In No. 1088 of the Astronomische Nachrichten, published in June, 1857, Dr. Dipre gives the following set of Tables for reducing barometrical observations to another level, and for computing heights. These tables, being based, as the preceding ones (IV.), on the formula of Laplace, and computed with the same constants, give results nearly identical, but dispense with the use of logarithms.

## Use of the Tables.

The tables suppose the height of the barometer to be expressed in French inches or Paris lines, and the temperature in degrees of Reaumur; they give the differences of level in French toises.

The signs used have the following signification : -

$$
\begin{gathered}
\text { At Lower } \\
\text { Station. }
\end{gathered}\left\{\begin{array}{l}
\mathrm{B}=\text { Observed Height of Barometer in Paris lines. } \\
\mathrm{T}=\text { Attached Thermometer in degrees of Reaumur. } \\
b=\text { Barometer reduced to the freezing point. } \\
t=\text { Temperature of the air, detached Thermometer. }
\end{array}\right.
$$

I. For Reducing Barometrical Olservations to another Level.

Given, $h$ in toises, $t, t^{\prime}, \phi$, and $b$ or $b^{\prime}$.
To find $l$ or $b^{\prime}$.

D

$$
\text { Make first } \mathcal{Q} \tau={ }_{2}^{t+t} \text { and } \tau, \text { and }
$$

In 'Table I., with the argument $2 \tau$, take $\tau^{\prime}$;
In Table III., with the arguments $h$ and $r$, take C ;
In 'Table IV., with the arguments $h$ and $\phi$, take $\mathrm{C}^{\prime}$;
Make, further,

$$
u=h+\mathrm{C}+\mathrm{C}^{\prime} \text { and }{ }_{100}^{u} \tau^{\prime}
$$

And if $b^{\prime}$ be given, and $b$ required,
In Table II., with the argument $l$, take II ;
then is

$$
\mathrm{H}=\mathrm{II}+\left(u-\frac{u}{100} \tau^{\prime}\right)
$$

and the height of the barometer, in Table II., due to II, is $b$ required.
If $b$ be given, and $b^{\prime}$ required for a level higher by $h$ toises, then,
In Table II., with the argument $b$, take $\mathrm{H}^{i}$.
Make, further,

$$
\mathrm{H}^{\prime}=\mathrm{H}-\left(u-\frac{u}{100} \tau^{\prime}\right),
$$

and $b^{\prime}$ is the height of the barometer in Table II., corresponding to $\mathrm{H}^{\prime}$.

## Example 1.

Suppose the height of the barometer reduced to the freezing point to be $b^{\prime}=$ 295.39 Paris lines; the temperature of the air $t^{\prime}=11^{\circ} .8$ Reammur; and the latitude $\phi=51^{\circ} .48$; the increase of heat downwards being $1^{\circ}$ Reammur for 100 toises. What is the height of the barometer reduced to the freezing point, at a station lower by $h=498.2$ toises?

In this case,

$$
\begin{gathered}
t^{\prime}=11^{\circ} .8 ; t=11^{\circ} .8+4^{\circ} .98 ; t+t^{\prime}=98^{\circ} .58 ; \\
2 \tau=\frac{t+t}{2}=14^{\circ} .29 ; \tau=7^{\circ} .15
\end{gathered}
$$

and according to Table I.

$$
\tau^{\prime}=+6.67
$$

With $h$ and $\tau$, in Table III., we find $\mathrm{C}=-1.4$
With $h$ and $\phi$, in Table IV., we find $\mathrm{C}^{\prime}=+0.3$

$$
\text { We add } h=498.2
$$

and we have $u=497.1$;

$$
-{ }_{100}^{u} \tau=-33.15
$$



$$
\mathrm{H}=\overline{831.81}
$$

Finally, with H, in Table II., we find $b=330.91$ Paris lines, which is the required height of the barometer at the lower station. Gauss's tables (IV.) would give $b=$ 330.90 lines.

## Example 2.

Suppose $b^{\prime}=330.46$ Paris lines ; $t^{\prime}=-12^{\circ} .3$ Reaumur ; $h^{\prime}=99.7$ toises; $\phi=62^{\circ}$.

In this case, assuming $t=t^{\prime}$,

$$
2 \tau=\frac{t+t^{\prime}}{2}=-12^{\circ} .3 ; \tau=-6.15 ;
$$

and according to Table I. $\quad \tau^{\prime}=-6.55$.
With $h$ and $\tau$, in Table III., take $\mathrm{C}=-0.2$
With $h$ and $\phi$, in Table IV., take $\mathrm{C}^{\prime}=+0.1$
Add $h=$ 92. $\%$


$$
H=924.89
$$

With H, in Table II., we find $b=338.53$ Paris lines. Gauss's tables (IV.) wou'd give $b=338.54$ lines.

## II. For Computing Differences of Elevation from Barometrical Olservations.

Suppose to be given $\mathrm{B}, \mathrm{B}^{\prime}, \mathrm{T}, \mathrm{T}^{\prime}, t, t^{\prime}, \phi$; required $h$.

$$
\text { Make first } \tau=\frac{t+t^{\prime}}{4} \text { and } \mathrm{T}-\mathrm{T}^{\prime}
$$

Then in Table II., with the argument $\left\{\begin{array}{l}\mathrm{B} \text { take } \mathrm{H}, \\ \mathrm{B}^{\prime} \text { take } \mathrm{H}^{\prime},\end{array}\right.$ and make

$$
u=\left(\mathrm{H}-\mathrm{H}^{\prime}\right)+\frac{\mathrm{H}}{100} \mathrm{H}^{\prime} \tau-\left(\mathrm{T}-\mathrm{T}^{\prime}\right)
$$

in which each full degree of ' $\mathrm{T}-\mathrm{T}^{\prime}$ corresponds to a toise.
Further, in Table III., with $u$ and $\tau$, take C reversing the sign;
in 'Table IV., with $u$ and $\phi$, take $\mathrm{C}^{\prime}$ reversing the sign ;
in Table V., with $T-T^{\prime}$ and $\tau$, take $\mathrm{C}^{\prime}$ with the signs of $\mathrm{T}-\mathrm{T}^{\prime}$.
Then the difference of elevation required is

$$
h=u+\mathrm{C}+\mathrm{C}^{\prime}+\mathrm{C}^{\prime \prime}
$$

If the heights of the barometer, reduced to the freezing point, or $b$ and $b^{\prime}$, are given,
then in Table II., with the argument, $\left\{\begin{array}{l}b \text { take } H \\ b^{\prime} \text { take } I^{\prime},\end{array}\right.$
and make

$$
u=\mathrm{H}-\mathrm{H}^{\prime}+\frac{\mathrm{H}-\mathrm{H}^{\prime}}{100} \tau .
$$

Further, in Table III., take C reversing the sign ;
in Table IV., take C reversing the sign ;
and

$$
h=u+\mathrm{C}+\mathrm{C}^{\prime} .
$$

D

## Example 1.

Suppose to be given,
$\mathrm{B}=333.6$ Paris lines; $\mathrm{T}=+17^{\circ} .0$ Reaumur ; $t=+19^{\circ} .0 \mathrm{R} . ; \phi=48^{\circ}$.
$\mathrm{B}^{\prime}=289.9$ Paris lines $; \mathrm{T}^{\prime}=+16^{\circ} .3$ Reammur $; t^{\prime}=+15^{\circ} .2 \mathrm{R}$.

$$
\begin{array}{rlrl}
\mathrm{T}-\mathrm{T}^{\prime}=0^{\circ} .7 & t+t^{\prime} & =+34^{\circ} .2 \\
r & =+8.55
\end{array}
$$

In Table II. with B take $\mathrm{H}=864.9$
" with $\mathrm{B}^{\prime}$ take $\mathrm{H}^{\prime}=291.2$

In Table III., with $u$ and $\tau$, take $\mathrm{C}=+1.8$
In 'Table IV., with $u$ and $\phi$, take $\mathrm{C}^{\prime}=-0.2$
In Table V., with $\mathrm{T}-\mathrm{T}^{\prime}$ and $r$ take $\mathrm{C}^{\prime \prime}=0.0$
Difference of elevation, or $h=623.66$ toises.
Gauss's Tables give 623.64 toises.

## Example 2.

Suppose to be given,
$b=342.68$ Paris lines $; t=-10^{\circ} .38$ Reaumur $; \phi=65^{\circ}$.
$b^{\prime}=285.47$ Paris lines ; $t^{\prime}=-14^{\circ} .94$ Reaumur ; $\mathrm{T}-\mathrm{T}^{\prime}=0^{\circ}$. R.

$$
\begin{aligned}
t+t^{\prime} & =-25^{\circ} .32 \\
\tau & =-6.33
\end{aligned}
$$

In Table II. with $b$ take $\mathrm{H}=974.58$
" with $b^{\prime}$ take $\mathrm{H}^{\prime}=228.28$

$$
\begin{aligned}
& \mathrm{H}-\mathrm{H}^{\prime}=746.30 \\
& \mathrm{H}-\mathrm{H}^{\prime} \\
& 100=-47.24 \\
& u=699.06
\end{aligned}
$$

In Table III., with $u$ and $\tau$, take $\mathrm{C}=+1.8$

$$
\mathrm{II}_{\mathbf{1 0 0}} \mathrm{II}^{\prime}{ }_{\tau}-47.2 t
$$

In Table IV., with $u$ and $\phi$, take $\mathrm{C}^{\prime}=-1.2$
$h=699.66$
Gauss's Tables give $h=699.72$ toises.

$$
\begin{aligned}
& \mathrm{H}-\mathrm{H}^{\prime}=\overline{\mathbf{5 7}} .7 \\
& { }_{-100}^{\mathrm{H}-\mathrm{H}^{\prime}} \tau=49.06 \\
& -\left(\mathrm{T}-\mathrm{T}^{\prime}\right)=-0.7
\end{aligned}
$$

$$
\begin{aligned}
& u=62 \mathrm{~S} .06
\end{aligned}
$$

## TABLES

FOR REDUCING BAROMETRICAL OBSERVATIONS TO ANOTHER LEVEL, AND FOR COMPUTING DIFFERENCES OF ELEVATION, BY M. C. DIPPE.

Table I. - Argument, the observed Meight of the Barometer at either Station.

| Barometeris l'aris lines. <br> $B$ or $B^{\prime}$ | Tenths of a Line. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  | If or $\mathrm{II}^{\prime}$ in Toises $=$ |  |  |  |  |  |  |  |  |  |
| 270 | 0.7 | 2.2 | 3.7 | 5.2 | 6.7 | 8.2 | 9.7 | 11.2 | 12.8 | 14.3 |
| 271 | 15.8 | 17.3 | 18.3 | 20.3 | 21.8 | 23.3 | 24.8 | 26.3 | 27.8 | 29.3 |
| 272 | 30.5 | 32.3 | 33.8 | 35.3 | 36.8 | 33.3 | 39.8 | 41.3 | 42.8 | 44.3 |
| 273 | 45.8 | 47.3 | 48.5 | 50.3 | 51.8 | 53.3 | 54.8 | 56.3 | 57.8 | 59.3 |
| 274 | 60.8 | 62.2 | 63.7 | 6.5 .2 | 66.7 | 68.2 | 69.7 | 71.2 | 72.7 | 74.1 |
| 27.5 | 75.6 | 77.1 | 78.6 | 80.1 | 81.6 | 83.1 | 84.5 | S6.0 | 87.5 | 89.0 |
|  |  |  |  |  |  |  |  |  |  |  |
| $276$ | 90.5 | 91.9 | 93.4 | 94.9 | 96.4 | 97.9 | 99.3 | 100.8 | 102.3 | 103.5 |
| 277 | 10.5.2 | 106.7 | 108.2 | 109.7 | 111.1 | 112.6 | 114.1 | 115.6 | 117.0 | 118.5 |
| 278 | 120.0 | 121.4 | 122.9 | 124.4 | 12.5. 5 | 127.3 | 123.8 | 130.2 | 131.7 | 133.2 |
| 279 | 131.6 | 136.1 | 137.6 | 139.0 | 140.5 | 142.0 | 143.4 | 144.9 | 146.3 | 147.8 |
| 280 | 149.3 | 150.7 | 152.2 | 153.6 | 155.1 | 156.5 | 158.0 | 159.5 | 160.9 | 162.4 |
| 281 | 163.8 | 165.3 | 166.7 | 168.2 | 169.6 | 171.1 | 172.5 | 174.0 | 175.4 | 176.9 |
| 282 | 178.3 | 179.8 | 181.2 | 182.7 | 184.1 | 185.6 | 157.0 | 188.5 | 189.9 | 191.4 |
| 253 | 192.8 | 194.2 | 195.7 | 197.1 | 198.6 | 200.0 | 201.4 | 202.9 | 204.3 | 205.8 |
| 284 | 207.2 | 208.6 | 210.1 | 211.5 | 213.0 | 214.4 | 215.8 | 217.3 | 218.7 | 220.1 |
| 285 | 221.6 | 223.0 | 2.24 .4 | 225.9 | 227.3 | 228.7 | 230.2 | 231.6 | 233.0 | 234.5 |
| 286 | 235.9 | 237.3 | 238.7 | 240.2 | 241.6 | 243.0 | 244.4 | 245.9 | 247.3 | 248.7 |
| 287 | 250.1 | 251.6 | 253.0 | 254.4 | 255.8 | 257.3 | 235.7 | 260.1 | 261.5 | 262.9 |
|  |  |  |  |  |  |  |  |  |  |  |
| 289 | 278.5 | 279.9 | 281.3 | 282.5 | 281.2 | 285.6 | 257.0 | 288.4 | 289.8 | 291.2 |
| 290 | 292.6 | 294.0 | 29.4 | 296.8 | 298.3 | 299.7 | 301.1 | 302.5 | 303.9 | 30.5 .3 |
| 291 | 306.7 | 308.1 | 309.5 | 310.9 | 312.3 | 313.7 | 315.1 | 316.5 | 317.9 | 319.3 |
| 292 | 320.7 | 3221 | 323.5 | 324.9 | 326.3 | 3.7 .7 | 329.1 | 3:30.5 | 331.9 | 333.3 |
| 293 | 334.7 | 336.1 | 3:37.5 | 335.9 | 340.2 | 341.6 | 343.0 | 34.4 | 345.8 | 347.2 |
| 29 t | 348.6 | 350.0 | 351.1 | 352.8 | 354.2 | 355.5 | 356.9 | 358.3 | 359.7 | 361.1 |
| 29.5 | 362.5 | 363.9 | 36.5.2 | 366.6 | 368.0 | 369.4 | 370.8 | 372.2 | 373.5 | 374.9 |
| 296 | 376.3 | 377.7 | 379.1 | 300.4 | 351.8 | 383.2 | $3 ¢ 4.6$ | 35.5 .9 | 357.3 | 388.7 |
| 297 | 390.1 | 391.5 | 392.8 | 394.2 | 395.6 | 397.0 | 398.3 | 399.7 | 401.1 | 402.4 |
| 293 | 403.8 | 40.5 .2 | 406.5 | 407.9 | 409.3 | 410.7 | 412.0 | 413.4 | 414.8 | 416.1 |
| 299 | 417.5 | 418.9 | 420.2 | 421.6 | 423.0 | 424.3 | 425.7 | 427.1 | 428.4 | 429.5 |
| 25 Inch |  |  |  |  |  |  |  |  |  |  |
| 1300 | 431.1 | 433.5 | 433.9 | 435.2 | 436.6 | 487.9 | 439.3 | 440.7 | 42.0 | 44.4 |
| 301 | +41.7 | 446.1 | 477.5 | 44.8 | 4.50 .2 | 4.51 .5 | +52.9 | 454.2 | 455.6 | 4.56 .9 |
| 302 | 458.3 | 459.6 | 461.0 | 462.3 | 463.7 | 465.0 | 466.4 | 467.8 | 469.1 | 470.5 |
| 303 | 471.9 | 473.1 | 474.5 | 475.8 | 477.2 | 478.5 | 479.9 | 451.2 | 45.26 | 483.9 |
| 304 | 485.3 | 486.6 | 487.9 | 489.3 | 490.6 | 492.0 | 493.3 | 491.7 | 496.0 | 497.3 |
| 305 | 498.7 | 500.0 | 501.4 | 502.7 | 504.0 | 505.4 | 506.7 | 508.0 | 509.4 | 510.7 |
| 306 | 512.0 | 513.4 | 514.7 | 516.0 | 517.4 | 518.7 | 520.1 | 521.4 | 522.7 | 524.0 |

Table I. Contimued.

| Barometer in l'aris Lines. |  |  |  |  | Tenths of a Line. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 306 | 512.0 | 513.4 | 514.7 | 516.0 | 517.4 | 518.7 | 520.1 | 521.4 | 522.7 | 524.0 |
| 307 | 525.4 | 526.7 | 528.0 | 529.4 | 530.7 | 532.0 | 533.4 | 534.7 | 536.0 | 537.4 |
| 308 | 533.7 | 540.0 | 541.3 | 542.6 | 544.0 | 545.3 | 546.6 | 547.9 | 549.3 | 550.6 |
| 309 | 551.9 | 553.2 | 554.6 | 5.5.5.9 | 5.57 .2 | 558.5 | 559.8 | 561.2 | 562.5 | 563.8 |
| 310 | 565.1 | 566.4 | 567.8 | 569.1 | 570.4 | 571.7 | 573.0 | 574.3 | 575.6 | 576.9 |
| 311 | 578.3 | 579.6 | 580.9 | 582.2 | 583.5 | 584.8 | 586.1 | 587.5 | 588.8 | 590.1 |
| 26 Inch |  |  |  |  |  |  |  |  |  |  |
| 312 | 591.4 | 592.7 | 594.0 | 59.5 .3 | 596.6 | 597.9 | 599.2 | 600.6 | 601.9 | 603.2 |
| 318 | 604.5 | 60.5 .8 | 607.1 | 605.4 | 609.7 | 611.0 | 612.3 | 613.6 | 614.9 | 616.2 |
| 314 | 617.5 | 618.9 | 620.1 | 621.4 | 62.2 .7 | 624.0 | 625.3 | 626.6 | 627.9 | 629.2 |
| 315 | 630.5 | 681.8 | 633.1 | 634.4 | 635.7 | 637.0 | 638.3 | 639.5 | 640.8 | 642.1 |
| 316 | 643.4 | 644.7 | 646.0 | 647.3 | 618.6 | 649.9 | 651.2 | 652.5 | 633.8 | 655.1 |
| 317 | 656.3 | 657.6 | 655.9 | 660.2 | 661.5 | 662.8 | 664.1 | 665.4 | 666.6 | 667.9 |
| 319 | 669.2 | 670.5 | 671.8 | 673.1 | 674.3 | 675.6 | 676.9 | 678.2 | 679.5 | 650.8 |
| 319 | 652.0 | 683.3 | 684.6 | 685.9 | 687.2 | 688.4 | 689.7 | 691.0 | 692.3 | 693.6 |
| 320 | 691.8 | 696.1 | 697.4 | 698.7 | 699.9 | 701.2 | 702.5 | 703.8 | 705.0 | 706.3 |
| 321 | 707.6 | 705.9 | 710.1 | 711.4 | 712.7 | 713.9 | 715.2 | 716.5 | 717.7 | 719.0 |
| 322 | 720.3 | 721.6 | 722.8 | 724.1 | 72.5 .1 | 726.6 | 727.9 | 729.2 | 730.4 | 731.7 |
| 323 | 733.0 | 734.2 | 735.5 | 736.7 | 738.0 | 739.3 | 740.5 | 741.8 | 743.1 | 744.3 |
| 28 Inch. |  |  |  |  |  |  |  |  |  |  |
| 324 | 745.6 | 746.8 | 748.1 | 749.4 | 750.6 | 751.9 | 753.2 | 754.4 | 75.5 .7 | 756.9 |
| 325 | 755.2 | 739.4 | 760.7 | 761.9 | 763.2 | 764.5 | 76.5 .7 | 767.0 | 768.2 | 769.5 |
| 326 | 770.7 | 772.0 | 773.2 | 774.5 | 775.7 | 777.0 | 778.2 | 779.5 | 750.7 | 782.0 |
| 3.7 | 753.2 | 784.5 | 78.5 .7 | 787.0 | 783.2 | 759.5 | 790.7 | 792.0 | 793.2 | 794.5 |
| 328 | 79.5 .7 | 797.0 | 799.2 | 799.4 | S00.7 | 801.9 | 803.2 | 804.4 | 80.3 .7 | 806.9 |
| 329 | S08.2 | 809.4 | S10.6 | S11.9 | 813.1 | 814.4 | S15.6 | S16.8 | 818.1 | 819.3 |
| 330 | 820.6 | 821.8 | 823.0 | S24.3 | 825.5 | 826.7 | 828.0 | S29.2 | 830.4 | 831.7 |
| 331 | 8:32.9 | \$34.2 | 835.4 | S3(i.6 | 8:37.9 | 839.1 | 840.3 | 841.6 | 842.S | 844.0 |
| 332 | 845.2 | 846.5 | 847.7 | 848.9 | 8.50.2 | 851.4 | 8.52 .6 | 8.53.9 | 8.55 .1 | 8.56 .8 |
| 3:3:3 | 857.5 | S.58.3 | 860.0 | 861.2 | 862.4 | 84.3 .7 | 864.9 | 866.1 | 867.3 | 865.6 |
| 331 | 869.8 | S71.0 | 872.2 | 873.4 | 874.7 | 88.5 .9 | 877.1 | 878.3 | 8796 | 880.8 |
| 33.5 | S82.0 | 883.2 | 854.4 | 883.7 | 886.9 | 888.1 | 889.3 | 890.5 | 891.7 | 893.0 |
| 28 Inch |  |  |  |  |  |  |  |  |  |  |
| $3 \cdot 36$ | 894.2 | 89.5 .4 | 896.6 | 897.8 | 899.0 | 900.3 | 901.5 | 902.7 | 90.3 .9 | 90.5 .1 |
| $3: 77$ | 909.3 | 907.5 | 908.7 | 909.9 | 911.2 | 912.4 | 913.6 | 914.8 | 916.0 | 917.2 |
| 338 | 918.4 | 919.6 | 920.9 | 92.2 | 92:3.3 | 9.24 .5 | 925.7 | 926.9 | 925.1 | 929.3 |
| 339 | 930.5 | 931.7 | 932.9 | 931.1 | 935.3 | 936.5 | 937.7 | 935.9 | 940.1 | 911.3 |
| 340 | 912.5 | 913.7 | $9+1.9$ | 9.46 .1 | 947.3 | 918.5 | 949.7 | 950.9 | 9.52 .1 | 953.3 |
| 341 | 9545 | 9557 | 956.9 | 958.1 | 959.3 | 9605 | 961.7 | 962.9 | 964.1 | 965.3 |
| 3.12 | 966.5 | 967.7 | 968.9 | 970.1 | 971.3 | 9725 | 973.7 | 974.5 | 976.0 | 977.2 |
| 313 | 978.4 | 979.6 | 9 K 0.8 | 98.0 | $9 \div 3.2$ | $9 \mathrm{si4.4}$ | $9-.5 .6$ | 986.8 | 9 - . 9 | 9.9 .1 |
| 344 | 990.3 | 991.5 | 992.7 | 993.9 | 99.5.1 | 996.2 | 997.4 | 998.6 | 999.8 | 1001.0 |
| 31.5 | 1002.2 | 1003.4 | 1004.5 | 1005.7 | 1006.9 | 100<. 1 | 1009.8 | 1010.5 | 1011.6 | 1012.8 |
| 346 | 1014.0 | 1015.2 | 1016.4 | 1017.5 | 1018.7 | 1019.9 | 1021.1 | 1022.3 | 102:3.4 | 1024.6 |
| 317 | 102.5. 8 | 1027.0 | 1028.1 | 1029.3 | 1030.5 | 1031.7 | 1032.8 | 1031.0 | 1035.2 | 1036.4 |
| $\begin{gathered} 29 \text { Inch } \\ 318 \end{gathered}$ | 1037.5 | 10.32 .7 | 1039.9 | 1011.1 | 1042.2 | 1048.4 | 1044.6 | 104.5. 5 | 11)469 | 1048.1 |

D

Table II.
correction for the temperature of the air.
Argument, $2 \tau=\begin{gathered}t+t^{\prime} \\ 2\end{gathered}$.

| 2 I | $\tau^{\prime}$ | Diff. | 2 I | $\tau^{\prime}$ | Diff. | $2 \tau$ | $\tau^{\prime}$ | Dift. | $2 \tau$ | $\tau^{\prime}$ | Diff. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -25 | -14.29 |  | -12 | -6.38 |  | + 1 | +0.50 |  | +14 | + 6.54 |  |
| -24 | -13.64 |  | -11 | -5.82 | . 56 | 2 | 0.99 | - 49 | 15 | 6.98 | 0.44 |
| -23 | -13.00 | . 64 | -10 | -5.26 | 0.26 | 3 | 1.18 | . 49 | 16 | 7.41 | . 43 |
| -22 | -12.36 | 64 | -9 | -4.71 | 0.55 | 4 | 1.96 | . 18 | 17 | 7.83 | 0.42 |
| -21 | -11.73 |  | - 8 | -4.17 |  | 5 | 2.14 | 0.48 | 18 | 8.26 | . 13 |
|  |  | 0.62 |  |  | 0.54 |  |  | 0.47 |  |  | 0.42 |
| $-20$ | -11.11 |  | $-7$ | -3.63 |  | 6 | 2.91 |  | 19 | 8.68 |  |
| -19 | -10.50 |  | -6 | -8.09 |  | 7 | 3.38 |  | 20 | 9.09 |  |
| -18 | - 9.59 | 0.61 | - 5 | -2.56 | 0.53 | 8 | 3.85 | 0.47 | 21 | 9.50 | 0.41 |
| -17 | - 9.29 | 0.60 | - 4 | -2.04 | 0.52 | 9 | 4.31 | 0.46 | 22 | 9.91 | 0.41 |
| -16 | - 8.70 |  | $-3$ | -1.52 |  | 10 | 1.86 |  | 23 | 10.31 |  |
|  |  | 0.59 |  |  | 0.51 |  |  | 0.45 |  |  | 0.10 |
| -15 | -8.11 |  | - 2 | -1.0 |  | 11 | 5.21 |  | 24 | 10.71 |  |
| -14 | - 7.53 |  | - 1 | -0.50 |  | 12 | 5.66 |  | 25 | 11.11 |  |
| -13 | -6.9.5 |  | 0 | 0.00 |  | 13 | 6.10 |  | 26 | 11.50 |  |
| -12 | -6.38 | 0.57 | +1 | +0.50 |  | +14 | +6.51 | 0.44 | +27 | +11.89 | 0.39 |

Table III. for $C$.
Arguments, $h$ and $\tau$.
In computing Heights reverse the signs of $C$. Arguments, $\tau$ and $u$

| $\begin{aligned} & h,(1) \\ & \text { Toises. } \end{aligned}$ | $\tau$, in Degrees of Reaumur $=$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | -19 ${ }^{\circ}$ | -8 ${ }^{\circ}$ | -10 | $0^{\circ}$ | $+4^{\circ}$ | $+8^{\circ}$ | +120 | $+16^{\circ}$ |
| 50 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 100 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 150 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 200 | 0.4 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 |
| 2.50 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.7 |
| 300 | 0.7 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 |
| 350 | 0.8 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 | 1.0 | 1.0 | 1.1 |
| 400 | 0.9 | 0.9 | 1.0 | 1.0 | 1.0 | 1.1 | 1.1 | 1.2 | 1.2 |
| 450 | 1.0 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 |
| 500 | 1.1 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 | 1.5 |
| 550 | 1.2 | 1.3 | 1.4 | 1.4 | 1.5 | 1.5 | 1.6 | 1.6 | 1.7 |
| 600 | 1.4 | 1.4 | 1.5 | 1.6 | 1.6 | 1.7 | 1.7 | 1.8 | 1.9 |
| 650 | 1.5 | 1.6 | 1.6 | 1.7 | 1.5 | 1.8 | 1.9 | 1.9 | 2.0 |
| 700 | 1.6 | 1.7 | 1.8 | 1.8 | 1.9 | 2.0 | 2.0 | 2.1 | 2.2 |
| 750 | 1.7 | 1.8 | 1.9 | 2.0 | 2.0 | 2.1 | 2.2 | 2.3 | 2.3 |
| 800 | 1.9 | 2.0 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.4 | 2.5 |
| 850 | 2.0 | 2.1 | 2.2 | 2.3 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 |
| 900 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 |
| 9.50 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.7 | 2.9 | 3.0 | 3.1 |
| 1000 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.1 | 3.2 | 3.3 |

Table lV. for C'.
CORRECTION IN TOISES FOR THE CHANGE OF GRAVITY IN LATITUDE.


| Latitude. |  | Approximate Difference of Level, in Toises. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | + | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 804 | 900 | 1000 |
| 0 | 90 | 0.3 | 0.5 | 0.8 | 1.0 | 1.3 | 1.6 | 1.8 | 2.1 | 2.3 | 2.6 |
| 5 | 85 | 0.3 | 0.5 | 0.5 | 1.0 | 1.3 | 1.5 | 1.8 | 2.0 | 2.3 | 2.6 |
| 10 | ¢0 | 0.3 | 0.5 | 0.7 | 1.0 | 1.2 | 1.5 | 1.7 | 2.0 | 22 | 2.4 |
| 15 | 7.) | 0.2 | 0.4 | 0.7 | 0.9 | 1.1 | 1.3 | 1.6 | 1.8 | 2.0 | 9.3 |
| 20 | 70 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 | 2.0 |
| 2.5 | 65 | 0.2 | 0.3 | 0.5 | 0.7 | 0.8 | 1.0 | 1.2 | 1.3 | 1.5 | 1.7 |
| 30 | 60 | 0.1 | 0.3 | 0.4 | 0.5 | 0.6 | 0.8 | 0.9 | 1.0 | 1.2 | 1.3 |
| 35 | 5.5 | 0.1 | 0.2 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 36 | 54 | 0.1 | 0.2 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.6 | 0.7 | 0.8 |
| 37 | 53 | 0.1 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.5 | 0.6 | 0.6 | 0.7 |
| 38 | 52 | 0.1 | 0.1 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.6 | 0.6 |
| 39 | 51 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.5 |
| 40 | 50 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 |
| 41 | 49 | 0.0 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.4 |
| 42 | 48 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 | 0.2 | 0.3 |
| 43 | 47 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| 44 | 46 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 45 | 45 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Table V. for C".
Arguments $\tau$ and $T-T^{\prime}$. To be ased only in computing Heights.

| $\mathrm{T}-\mathrm{T}^{\text {t }}$ | Correction for T-T, in Toises, with the same sign ; ${ }^{\text {r }}=$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Re:umur | -120 | $-10^{\circ}$ | -80 | $-6{ }^{\circ}$ | $-401-20$ | $0^{\circ}$ | +20 | $+4^{\circ}$ | $+6^{\circ}$ |
| 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1 | 0.2 | 0.2 | 0.2 | 0.1 | $0.1 \quad 0.1$ | 0.1 | 0.1 | 0.0 | 0.0 |
| 2 | 0.4 | 03 | 0.3 | 0.3 | 0.20 .2 | 0.2 | 0.1 | 0.1 | 0.0 |
| 3 | 0.6 | 0.5 | 0.5 | 0.4 | $0.4 \quad 0.3$ | 0.2 | 0.2 | 0.1 | 0.1 |
| 4 | 0.5 | 0.7 | 0.6 | 0.5 | 0.50 .4 | 0.3 | 0.2 | 0.2 | 0.1 |
| 5 | 1.0 | 09 | 0.8 | 0.7 | 0.60 .5 | 04 | 0.3 | 0.2 | 0.1 |
| 6 | 1.1 | 1.0 | 0.9 | 0.8 | $0.7 \quad 0.6$ | 0.5 | 0.1 | 0.3 | 0.1 |
| 7 | 1.3 | 1.2 | 1.1 | 0.9 | 0.8 0.7 | 0.6 | 0.4 | 0.3 | 0.2 |
| 8 | 1.5 | 1.4 | 12 | 1.1 | 0.9 0.8 | 0.6 | 0.5 | 0.3 | 0.2 |
| 9 | 1.7 | 1.6 | 1.4 | 1.2 | 1.109 | 0.7 | 0.6 | 0.4 | 0.2 |
| 10 | 1.9 | 1.7 | 1.5 | 1.4 | 1.21 .0 | 0.8 | 0.6 | 0.4 | 0.2 |
| Correction for $\mathbf{T}-\mathrm{T}^{\prime}$ with contrary sign ; ${ }^{\top}=$ |  |  |  |  |  |  |  |  |  |
| T- $\mathbf{T}^{\prime}$ | $+8^{\circ}$ | $+10^{\circ}$ | +120 | $+11^{\circ}$ | $\mathbf{T}-\mathbf{T}^{\prime}$ | $+8^{\circ}$ | $+10^{\circ}$ | +130 | $+10^{\circ}$ |
| 1 | 0.0 | 0.0 | 0.0 | 0.0 | 6 | 0.0 | 0.1 | 0.2 | 0.3 |
| 2 | 0.0 | 0.0 | 0.1 | 0.1 | 7 | 0.0 | 0.1 | 0.2 | 0.3 |
| 3 | 0.0 | 0.0 | 0.1 | 0.1 | 8 | 0.0 | 0.1 | 0.2 | 0.4 |
| 4 | 0.0 | 0.0 | 0.1 | 0.2 | 9 | 0.0 | 0.1 | 0.2 | 0.4 |
| 5 | 0.0 | 0.1 | 0.2 | 0.2 | 10 | 0.0 | 0.1 | 0.3 | 0.4 |

D
65

## LAPLACE'S FORMULA FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS, MODIFIED BY BABINET.

In the Comptes Rendus de l'Académie des Sciences for March, 1851, M. Babinet propose's the following modification of Laplace's formula, the object of which is to dispetse both with the use of logarithms and with tables of any kind.

Laplace's formula is,

$$
z=18393 \text { metres }(\log \mathrm{H}-\log h)\left[1+\frac{2(\mathrm{~T}+t)}{1000^{-}}\right]
$$

$\approx$ being the difference of level between the two stations,
$H$, the height of barometer at the lower station,
$h$, the height of barometer at the upper station,
' F , temperature of air at the lower station,
$t$, temperature of air at the upper station.
The two barometers are supposed to be reduced to the same temperature. The small correction for the latitude is omitted.

For elevations less than 1000 metres, and even for much greater elevations, if approximate results only are needed, the formula may be transformed into the following :

$$
z=16000 \text { metres } \frac{\mathrm{II}-h}{\mathrm{H}+h}\left[1+\frac{2(\mathrm{~T}+t)}{1000}\right] .
$$

## Example 1.

Suppose,
at lower station, barometer at zero Cent. $=755^{\mathrm{mm}}$; temperature of air $15^{\circ}$ Cent. at upper station, barometer at zero Cent. $=745^{\mathrm{mm}}$; temperature of air $10^{\circ}$ Cent.

$$
\begin{array}{lc}
\mathrm{H}-h=10^{\mathrm{mm} .} & \mathrm{T}+t=25^{\circ} \text { Cent. } \\
\mathrm{II}+h=1500^{\mathrm{min} .} & 2(\mathrm{~T}+t)={ }_{\mathrm{T}}^{500 \sigma}=.05 .
\end{array}
$$

Then $\quad z=16000_{\frac{10}{150} \sigma} \times(1.05)=112$ metres.
Laplace's formula, by Deleros's tables, would give 111.6 metres.

## Example 2.

Suppose,
at luwer station, harometer at zero Cent. $=730^{\mathrm{mm}}$; temperature of air $20^{\circ}$ Cent. at upper station, barometer at zero Cent. $=635^{m m}$; temperature of air $15^{\circ}$ Cent.

$$
\begin{aligned}
\mathrm{H}-h & =95^{\mathrm{mm} .} & \mathrm{T}+t & =35^{\circ} \text { Cent. } \\
\mathrm{H}+h & =1365^{\mathrm{mm} .} & 2(\mathrm{~T}+t) & =\mathrm{T}^{70} \overline{0} \bar{\sigma}=.07 .
\end{aligned}
$$

Then $\quad z=16000_{1} \frac{95}{3} \frac{5}{5} \times(1.07)=1191.5$ metres.
Laplace's formula, by Deleros's tables, would give 1191.1 metres.
For greater elevations an intermediate station may be supposed.
Babinet's formula reduced to English measures becomes,

$$
\left.z=52494 \text { English feet } \begin{array}{l}
\mathrm{II}-h+h
\end{array} \mathrm{II}+\frac{(\mathrm{T}+t-64)}{900}\right]
$$

but as, in this form, it loses the simplicity of its coefficient, it will be found, on trial, that its use requires rather more computing than the author's tables (II.), p. 38, which give more accurate results.

## VII.

## TABLES

FOR COMPUTING THE DIFFFRENCE IN THE HEIGHTS OF TWO PLACES BY MEANS OF THE BAROMETER. - BAILY.

Baily, in his Astronomical Tables and Formula, page 111, gives the following final formula :

$$
\begin{aligned}
x= & 60345.51\left\{1+.0011111\left(t+t^{\prime}-64^{\circ}\right)\right\} \\
& \times \log \text { of }\left\{\begin{array}{l}
1 \\
\left.\beta^{\prime} \times \frac{1}{1+.0001\left(\tau-\tau^{\prime}\right)}\right\}
\end{array}\right\} \times\{1+.002695 \cos 2 \phi\}
\end{aligned}
$$

Where $\phi=$ the latitude of the place,
$\left.\begin{array}{l}\beta=\text { the height of the barometer, } \\ \tau=\text { the temperature, Fahrenheit, of the mercury, } \\ t=\text { the temperature, Fahrenheit, of the air, }\end{array}\right\} \begin{aligned} & \text { at the lower } \\ & \text { station. }\end{aligned}$
$\beta^{\prime}=$ the height of the barometer,
$\left.\begin{array}{l}\tau^{\prime}=\text { the temperature, Fahrenheit, of the mercury, } \\ t^{\prime}=\text { the temperature, Fahrenheit, of the air. }\end{array}\right\} \begin{gathered}\text { at the upper } \\ \text { station. }\end{gathered}$
The numerical values assumed are as follows:-
The constant barometrical coefficient
The expansion of moist air for $1^{\circ}$ Fahrenheit
$=60158.53$ English feet.

The expansion of mercury for $1^{\circ}$ Fahrenheit
$=.0022222$.

The increase of gravitation from Equator to Poles
$=.0001001$.

The radius of the Earth at $\phi$
$=.00539$.
The height of lower station assumed
$=20898: 40$ English feet.
$=4000$ English feet.

$$
\begin{aligned}
\text { Make } A & =\text { the } \log \text { of the first term, in English feet. } \\
B & =\text { the } \log \text { of } 1+.0001\left(\tau-\tau^{\prime}\right) . \\
\mathrm{C} & =\text { the } \log \text { of the last term. } \\
\mathrm{D} & =\log \beta-\left(\log \beta^{\prime}+\mathrm{B}\right) .
\end{aligned}
$$

Then, by the tables which follow, the logarithm of the difference of altitude in English feet

$$
=\mathrm{A}+\mathrm{C}+\log \mathrm{D}
$$

Baily's Tables have been recomputed and extended by Downes, for Lee's Collection of Tables and Formulce (2d edit. pp. 84, 85). These new tables are given here as revised by Mr. Downes for this volume.
I. Thermoneters in the Open Air.

| $t+t^{\prime}$ | A | $t+t^{\prime}$ | A | $t+t^{\prime}$ | A | $t+t^{\prime}$ | A | $t+t^{\prime}$ | A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ |  | $\bigcirc$ |  | - |  | $\bigcirc$ |  | $\bigcirc$ |  |
| 1 | 4.74913 | 37 | 4.76742 | 73 | 4.78497 | 109 | 4.90183 | 145 | 4.81807 |
| 2 | 4.74965 | 38 | 4.76791 | 74 | 4.78544 | 110 | 4.50229 | 146 | 4.818 .51 |
| 3 | 4.75016 | 39 | 4.76811 | 75 | 4.78592 | 111 | 4.80275 | 147 | 4.81896 |
| 4 | 4.75068 | 40 | 4.76591 | 76 | 4.786 .10 | 112 | 4.80321 | 148 | 4.81940 |
| 5 | 4.75120 | 41 | 4.76940 | 77 | 4.78687 | 113 | 4.50367 | 149 | 4.81984 |
| 6 | 4.75171 | 42 | 4.76990 | 78 | 4.78735 | 114 | $4.80+13$ | 150 | 4.82028 |
| 7 | 4.75233 | 43 | 4.77039 | 79 | 4.78782 | 115 | 4.80458 | 151 | 4.82072 |
| 8 | 4.75274 | 44 | 477089 | 80 | 4.78330 | 116 | 4.50 .504 | 152 | 4.82116 |
| 9 | 4.75326 | 45 | 4.75138 | 81 | 4.78875 | 117 | 4.80550 | 153 | 4.82160 |
| 10 | 4.75377 | 46 | 4.77187 | 82 | 4.78925 | 118 | 4.80595 | 154 | 4.82204 |
| 11 | 4.75429 | 47 | 4.77236 | 83 | 4.75972 | 119 | 4.80641 | 155 | 4.82248 |
| 12 | 4.75480 | 48 | 4.77285 | 84 | 4.79019 | 120 | 4.80688 | 156 | 4.52291 |
| 13 | 4.75531 | 49 | 4.77335 | 85 | 4.79066 | 121 | 4.80731 | 157 | 4.8233 .7 |
| 14 | 475582 | 50 | 4.77384 | 86 | 4.79113 | 122 | 4.60777 | 158 | 4.82379 |
| 15 | 4.75633 | 51 | 4.77433 | 87 | 4.79160 | 123 | 4.80822 | 159 | 4.82423 |
| 16 | 4.75684 | 52 | 4.77482 | 88 | 4.79207 | 124 | 4.80867 | 160 | 4.82466 |
| 17 | 4.75735 | 53 | 4.77530 | 89 | 4.792 .54 | 125 | 4.80913 | 161 | 4.82510 |
| 18 | 4.75786 | 54 | 4.77579 | 90 | 4.79301 | 126 | 4.80958 | 162 | 4.52553 |
| 19 | 4.75837 | 55 | 4.77628 | 91 | 4.79318 | 127 | 4.81003 | 163 | 4.82597 |
| 20 | 4.75588 | 56 | 4.77677 | 92 | 4.79395 | 128 | 4.81048 | 164 | 4.826 .40 |
| 21 | 4.75938 | 57 | 4.77725 | 93 | $479+42$ | 129 | 4.81093 | 165 | 4.92684 |
| 22 | 4.75989 | 58 | 4.77374 | 94 | 4.79489 | 130 | 4.81138 | 166 | 4.82727 |
| 23 | 4.76040 | 59 | 4.77523 | 9.5 | 4.79535 | 131 | 4.81183 | 167 | $4.827 \% 0$ |
| 24 | 4.76090 | 60 | 4.77871 | 96 | 4.79 .582 | 132 | 4.81228 | 168 | 4.82814 |
| 25 | 4.76141 | 61 | 4.77919 | 97 | 4.79628 | 133 | 4.81273 | 169 | 4.82857 |
| 26 | 4.76191 | 62 | 4.77968 | 98 | 4.79675 | 1:'4 | 4.81317 | 170 | 4.82900 |
| 27 | 4.76241 | 63 | 4.78016 | 99 | 4.79721 | 135 | 4.81362 | 171 | 4.82943 |
| 28 | 4.76292 | 64 | 4.78065 | 100 | 4.79768 | 136 | 4.81407 | 172 | 4.82986 |
| 29 | 4.76342 | 6.5 | 4.78113 | 101 | 4.79814 | 137 | 4.81452 | 173 | 4.53029 |
| 30 | 4.76392 | 66 | 4.78161 | 102 | 4.79861 | 138 | 4.81496 | 174 | 4.83078 |
| 31 | 4.76412 | 67 | 4.78209 | 103 | 4.79907 | 139 | 4.815 .41 | 175 | 4.8311 b |
| 32 | 4.76492 | 68 | 4.78257 | 104 | 4.79953 | 140 | 4.81585 | 176 | 4.83158 |
| 33 | 4.76542 | 69 | 4.75305 | 10.5 | 4.79999 | 141 | 4.81630 | 177 | 4.83201 |
| 34 | 4.76592 | 70 | 4.78353 | 106 | 4.80045 | 142 | 4.61674 | 178 | $4.832+4$ |
| 35 | 4.76642 | 71 | 4.78401 | 107 | 4.80091 | 143 | 4.81719 | 179 | 4.83257 |
| 36 | 4.76692 | 72 | $4.78+49$ | 108 | 4.80137 | 144 | 4.81763 | 180 | 4.83330 |


| $\tau-\tau^{\prime}$ | II. | Attached | 'Thermoneter. |  | 13 | III. Latitude of the Place. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | B | $\tau-\tau^{\prime}$ | B | $\boldsymbol{\tau}-\tau^{\prime}$ |  | $\phi$ | C |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | 0.00000 | 20 | 0.00087 | $\begin{array}{r} \circ \\ 40 \end{array}$ | 0.00174 | $\bigcirc$ | 0.00117 |
| 1 | 0.00 .10 t | 21 | 0.00091 | 41 | 0.00175 | 5 | 0.00115 |
| 2 | 0.00009 | 22 | 0.00096 | 42 | 0.00182 | 10 | 0.00110 |
| 3 | 0.00018 | 23 | 0.00100 | 43 | 0.00187 | 15 | 0.00101 |
| 4 | 0.00017 | 24 | 0.00104 | 44 | 0.00191 | 20 | 0.00090 |
| 5 | 0.00022 | 25 | 0.00109 | 45 | 0.0019 .5 | 25 | 0.00075 |
| 6 | 0.00026 | 26 | 0.00113 | 46 | 0.00200 | 30 | 0.00058 |
| 7 | 0.000:0 | 27 | 0.00117 | 47 | $0.00 \cdot 0 \cdot 4$ | 35 | 0.00040 |
| 8 | 0.0003 .5 | 28 | 0.00122 | 48 | 0.00208 | 40 | 0.00020 |
| 9 | 0.00039 | 29 | 0.00126 | 49 | 0.00212 | 45 | 0.00000 |
| 10 | 0.00043 | 30 | 0.00130 | 50 | 0.00217 | 50 | 9.99980 |
| 11 | 0.00018 | 31 | 000135 | 51 | 000221 | 5.5 | 9.99960 |
| 12 | 0.00052 | 32 | 0.00139 | 52 | 0.00225 | 60 | 9.99942 |
| 13 | 0.00056 | 33 | $0.001+3$ | 53 | 0.00230 | 65 | 9.99925 |
| 14 | 0.00001 | 34 | 0.00148 | 54 | 0.00234 | 70 | 9.99910 |
| 15 | 0.00065 | 35 | 0.00152 | 55 | 0.00238 | 75 | 9.99900 |
| 16 | 0.00069 | 36 | 0.00156 | 56 | 0.00213 | s0 | 9.99890 |
| 17 | 0.00074 | 37 | 0.00161 | 57 | 0.00247 | 85 | 9.99885 |
| 18 | 0.00078 | 33 | 000165 | 58 | 0.00251 | 90 | 9.99853 |
| 19 | 0.00083 | 39 | 0.00169 | 59 | 0.00256 |  |  |

Example.
Upper Station. Lower Station.
'Thermometer in open air, $\quad t^{\prime}=70.4, \quad t=77.6$.
Attached Thermometer $, \quad \tau^{\prime}=70.4, \quad \tau=77.6$.
Barometer,
$\beta^{\prime}=23.66$ inches, $\beta=30.05$ inches.
Latitude of the place $\quad \phi=21^{\circ}$.

$$
\begin{aligned}
& \mathrm{B}=0.00031 \\
& \log \beta^{\prime}=1.37401 \\
& 1.37432 \\
& \log \beta=1.47784 \\
& \mathrm{D}=0.10352
\end{aligned}
$$

## VIII.

## TABLES

```
FOR COMPUTING DIFFERENCES OF ELEVATION FROM BAROMETRICAL OBSERVATIONS; BASED ON BESSEL'S FORMULA.
```

By E. PLANTAMOUR.
[These Tables, computed by Professor E. Plantamour, Director of the Observatory at Geneva, Switzerland, are foum in Vol. XIH. P'urt 1, of the Mémoires de la Société de Physique, $\oint$ c. de Genève, p. 63, together with the following explanations.]

In No. 356 of the Astronomische Nachrichten, Bessel published a paper on the measurement of heights by means of the barometer, in which he deduces a formula which contains a factor depending on the humidity of the air. This formula is:

$$
\log \frac{\mathrm{P}}{\mathrm{P}^{\prime}}=\frac{(g) . \mathrm{H}^{\prime}-\mathrm{H}}{\mathrm{~L}(1+\mathrm{K} \mathrm{~T})}\left[1-a \frac{0.002561}{\gamma \mathrm{PP}^{\prime}} \cdot 10^{0.0279712 \mathrm{~T}-0.0000625826 \mathrm{~T}^{2}}\right]
$$

where the various quantities have the following signification: -
$h$ being the elevation of the lower station, and
$h^{\prime}$ the elevation of the upper station above the level of the sea,
$a=$ the radius of the Earth,
$\mathrm{H}=\frac{\mathrm{a} h}{\mathrm{a}+h}$,
$\mathrm{H}^{\prime}=\frac{\mathrm{a} h^{\prime}}{\mathrm{a}+h^{\prime}}$;
$\mathrm{P}=$ the weight of the atmosphere at the lower station,
$\mathrm{P}^{\prime}=$ the weight of the atmosphere at the upper station, the unit of weight assumed being the pressure of a column of mercury
of 336.905 Paris lines, at the temperature of the freezing point, or zero Reaumur, and under the 45 th degree of latitude.
$(g)=$ the gravity, at the level of the sea, in the mean latitude between the two places of observation.

Therefore, calling $\phi$ the latitude,
$(g)=1-0.0026257 \cos \phi$,
$\mathrm{L}=$ the constant barometrical coefficient depending on the relative density of the mercury and of the air,
$K=$ the coefficient of the expansion of the air,
$\mathrm{T}=$ the mean temperature of the layer of air between the lower and upper station,
$a=$ the fraction of saturation of the same layer.

The second term in the parenthesis, destined to take into account the aqueous vapor in the air, was obtained by assuming that the elastic force of vapor for a temperature T is represented, in unit of weight, by the expression,

$$
p=0.0067407 \times 10^{0.0279712 \mathrm{~T}-0.0000625826 \mathrm{~T}^{2} .}
$$

Multiplying the second member by 336.905 we find the expression of the elastic force of vapor that Laplace deduced from Dalton's experiments. Substituting, in the computation, Regnault's results, the numerical value of these coefficients is somewhat changed, and we find then

$$
p=0.0060527 \times 10^{0.0301975 \mathrm{~T}-0.000080170 \mathrm{~T} .}
$$

Bessel's tables give the difference of elevation in toises. The logarithm of the difference is obtained by the sum of four logarithms. The same form is preserved in the following tables; but the differences of elevation are given in metres.

The term due to the expansion of the air is computed in Bessel's tables for two values of the coefficient, viz. that of Gay-Lussac, 0.00375 , and that of Rudberg, 0.003648 ; in the new tables it is only computed for that of Regnault, 0.003665 .

The relative density of dry air at the freezing point, under a barometrical pressure of $0^{m .} .76$, and at the 45 th degree of latitude, and of mercury in the same circumstances, adopted by Bessel, is that determined by the experiments of Biot and Arago, viz. $10466.8^{\circ}$. The value of that constant derived from Regnault's experiments has been substituted. Regnault found the weight of a litre of dry air, at zero Centigrade, under a pressure of $0^{\mathrm{m}} .76$, and at the latitude of Parss, to be 1.293187 grammes, which, reduced to the gravity of the 45 th degree of latitude, becomes 1.292732 grammes. The weight of a litre of mercury, at zero Centigrade, he found to be 13596 grammes; the ratio is thus:

$$
\mathrm{D}=\frac{1}{10517.3}
$$

or about ² $_{2} \frac{1}{9}$ smaller than the value adopted by Bessel. If the constant coefficient L is expressed by $\mathrm{L}=\frac{0^{\mathrm{m} .} \cdot 76}{\mathrm{D} \cdot \mu^{\mu}}$, $\mu$ being the modulus of the common logarithms, its numerical valuc becomes

$$
\mathrm{L}=18404^{\mathrm{m}} .8
$$

In order to reduce the formula into tables, Bessel caused it to undergo several modifications, which we have followed, introducing the values of the constants above mentioned.

Let $b$ and $b^{\prime}$ be the heights of the barometer, expressed in the metrical scale, at the two stations; $t$ and $t^{\prime}$, the temperatures of the mercury measured with a brass scale; we have,

$$
\mathrm{P}=\underset{0^{\mathrm{m} \cdot} \cdot 76}{l} \cdot(g) \cdot\binom{a}{a+h}^{2}(1+0.00001879 t),
$$

and

$$
\mathrm{P}^{\prime}=\frac{\psi^{\prime}}{0^{\mathrm{m}} \cdot 76} \cdot(g) \cdot\binom{\mathrm{a}}{\mathrm{a}+h^{\prime}}^{2}\left(1+0.00001879 t^{\prime}\right) .
$$

Therefore,
$\log \mathrm{P}=\log b+\log (g)-\log 0^{\mathrm{m} .76}-\frac{2 \mathrm{II} \mu}{\mathrm{a}}-\mu t[0.00018018-0.00001879]$, $\log \mathrm{P}^{\prime}=\log b^{\prime}+\log (g)-\log 0^{m} .76-{ }^{2} \mathrm{H}^{\prime} \mu-\mu t^{\prime}[0.00018018-0.00001879]$.

If we call $\mathrm{B}, \mathrm{B}^{\prime}$ the heights of the barometer reducel to the freezing point, which we obtain by making

$$
\begin{gathered}
\log \mathrm{B}=\log b-t \cdot 0.000070095 ; \quad \log \mathrm{B}^{\prime}=\log b^{\prime}-t^{\prime} \cdot 0.000070095 \\
\log \frac{\mathrm{P}}{\mathrm{P}^{\prime}}=\log \mathrm{B}-\log \mathrm{B}^{\prime}+\underset{7329755}{\mathrm{IH}-\mathrm{II}}
\end{gathered}
$$

and with sufficient accuracy,

$$
\sqrt{ } \mathrm{PP}^{\prime}=\underset{0^{m} \cdot .76^{\circ}}{V B B^{\prime}}
$$

Substituting these expressions in the formula, it becomes,

$$
\log B-\log B^{\prime}=
$$



If we set instead of $a$ the half sum $\frac{a+a}{2}$ of the fraction of saturation observed at both stations, we fiud, after some transformations,

D

$$
\begin{aligned}
& \log \mathrm{B}-\log \mathrm{B}^{\prime}=\frac{(g)\left(\mathrm{H}^{\prime}-\mathrm{II}\right)(397.25-\mathrm{KT})}{398.25 \cdot \mathrm{~L}(1+\mathrm{KT})} \times \\
& \quad\left[1-\frac{\left(a+a^{\prime}\right) \cdot 0.34807}{\left(397.25-\mathrm{K} \mathrm{~T}^{2}\right) \vee \mathrm{BB}^{\prime}} \cdot 10^{0.0301975 \mathrm{~T}-0.000080170 \mathrm{~T}^{2}}\right] .
\end{aligned}
$$

Making further,

$$
\begin{gathered}
\mathrm{V}=\frac{398.25}{397.25-\mathrm{KT}} \mathrm{~L}(\mathrm{l}+\mathrm{KT}) \\
\mathrm{W}=\begin{array}{c}
0.34807 \\
397.25-\mathrm{KT}
\end{array} \cdot 10^{0.0301975 \mathrm{~T}-0.000080170 \mathrm{~T}^{2}}
\end{gathered}
$$

we shall have for the logarithm of the approximate difference of level between the two stations $\mathrm{H}^{\prime}-\mathrm{H}$,

$$
\begin{aligned}
& \log \left(\mathrm{H}^{\prime}-\mathrm{H}\right)=\log \left[\log \mathrm{B}-\log \mathrm{B}^{\prime}\right] \\
& \quad+\log \mathrm{V}+\log \frac{1}{1-W^{a}+a^{\prime}}+\log \underset{1}{(g) B^{\prime}}
\end{aligned}
$$

Table I. gives the values of $\log \mathrm{V}$ and $\log \mathrm{W}$, both of which only depend on the temperature; the argument is the sum of the temperature of the air, $\tau$ and $\tau^{\prime}$, observed at both stations, supposing $\tau+\tau^{\prime}=2^{\prime} \Gamma$.

Table II. gives the factor depending on the humidity of the air; with the argument

$$
\mathrm{W} \cdot \log \frac{\left(a+a^{\prime}\right)}{\sqrt{ } B^{\prime}},
$$

we obtain

$$
\log \frac{1}{1-W \begin{array}{c}
\left(a+a^{\prime}\right) \\
V \mathrm{~B} B^{\prime}
\end{array}}=\log \mathrm{V}
$$

Table III. gives the factor depending on the latitude for every degree, viz.

$$
\log \mathrm{G}^{\prime}=\log \begin{gathered}
1 \\
(g)
\end{gathered}
$$

The logarithm of the approximate difference is thus given by the sum of four logarithms. To obtain the exact elevation, the small correction found in Table IV. must be added to the number corresponding to that logarithm. For we have, with the necessary accuracy,

$$
h^{\prime}-h=\mathrm{H}^{\prime}-\mathrm{H}+\mathrm{H}^{\prime 2}-\frac{\mathrm{H}^{2}}{\mathrm{a}}
$$

Table IV. gives, for every 200 metres, the quantity $\frac{H^{2}}{a}$; the number in the table corresponding to $\frac{\mathrm{H}^{\prime}{ }^{2}}{\mathrm{a}}$ must be added to the approximate elevation; and the number corresponding to $\frac{H^{2}}{a}$ must be subtracted from the same.

D

## Use of the Tables.

Reduce first the observed height of the barometer at both stations to the freezing point by means of the usual tables, or by the logarithmic formula,

$$
\log \mathrm{B}=\log b-t \cdot 0.00007, \quad \log \mathrm{~B}^{\prime}=\log b^{\prime}-t^{\prime} 0.00007
$$

$b$ and $b^{\prime}$ being, in fractions of metre, the observed heights at the temperatures $t$ and $t^{\prime}$ marked by the attached thermometers; and B and $\mathrm{B}^{\prime}$ the reduced height at the lower and upper station.

Take the difference of $\log B$ and $\log B^{\prime}$, and find, in the tables of the common logarithms, the lograthm of that difference, viz. $\log \left(\log B-\log B^{\prime}\right) ;$ find also the logarithm of the product $\sqrt{ } \mathrm{BB}^{\prime}$, or

$$
\log \sqrt{ } B B^{\prime}=\frac{\log B+\log B^{\prime}}{2}
$$

Make further the sum $\tau+\tau^{\prime}$ of the temperature of the air at both stations, and likewise the sum of $a+a^{\prime}$ of the fraction of saturation.

Then, in Table I., with argument $\tau+\tau^{\prime}$, take $\log \mathrm{V}$ and $\log \mathrm{W}$; further, to $\log \mathrm{W}$ add $\log \left(a+a^{\prime}\right)$, and subtract $\log \sqrt{ } \mathrm{BB}^{\prime}$; and with the logarithm thus obtained as argument, take in Table II. $\log \mathrm{V}^{\prime}$.
'Table III. with the mean latitude of the stations gives $\log \mathrm{G}^{\prime}$.
$\mathrm{H}^{\prime}$ - II being the approximate difference of level between the two stations, we have

$$
\log \left(H^{\prime}-H\right)=\log \left(\log B-\log B^{\prime}\right)+\log V+\log V^{\prime}+\log C^{\prime}
$$

The altitude of the lower station being known, we deduce from $\mathrm{H}^{\prime}-\mathrm{H}$ the approximate altitude, $\mathrm{HI}^{\prime}$, of the upper station ; $h^{\prime}$, the exact altitude, or $h^{\prime}-h$, the difference of elevation, is given by the formula,

$$
h^{\prime}-h=\mathrm{H}^{\prime}-\mathrm{H}+\frac{\mathrm{I}^{\prime 2}}{\mathrm{a}}-\frac{\mathrm{H}^{2}}{\mathrm{a}} .
$$

Table IV. gives the values of $\frac{\mathrm{I}^{\prime 2}}{\mathrm{a}}$ and $\frac{\mathrm{H}^{2}}{\mathrm{a}}$ for the values of $\mathrm{H}^{\prime}$ or H for every $\geq 00$ metres.

## Example 1.

Computing the height of St. Bernard, taking Geneva, 407 metres above the level of the sea, as the lower station. The observation gives,

$$
\begin{aligned}
\mathrm{B}= & 796.43 \text { millimetres } \\
\tau= & +8^{\circ} .97 \text { Centigrade } \\
a= & 0.77 \\
& \log \mathrm{~B}=9.86119 \\
\log \mathrm{~B}^{\prime}= & 9.75100 \\
& \log \mathrm{~B}-\log \mathrm{B}^{\prime}=0.11019
\end{aligned}
$$

$$
\begin{aligned}
& \mathrm{B}^{\prime}=563.64 \text { millimetres } \\
& \tau^{\prime}=-1^{\circ} .89 \text { Centig. } \tau+\tau^{\prime}=+7^{\circ} .08 \\
& a^{\prime}=0.80 \quad a+a^{\prime}=157
\end{aligned}
$$

$$
\log \sqrt{ }\left(\mathrm{BB}^{\prime}\right)=9.8061
$$

$$
\text { Table I. } \log W=7.0511
$$

$$
\log \left(a+a^{\prime}\right)=0.1959
$$

$$
\log \begin{gathered}
\left(a+a^{\prime}\right) \\
\left(B B^{\prime}\right.
\end{gathered} \cdot W=\overline{7.4409}
$$

$$
\log \left[\log B-\log B^{\prime}\right]=\mathbf{9 . 0 4 2 1 5}
$$

In Table I. argt. $\tau+\tau^{\prime}=+7.08, \log \mathrm{~V}=4.27164$
In Table II. argt. 7.4409, $\quad \log \mathrm{V}^{\prime}=\quad 0.00120$
In Table III. argt. $46^{\circ}, \quad \log \mathrm{G}^{\prime}=-0.00004$
$\log \left(\mathrm{H}^{\prime}-\mathrm{H}\right)=\overline{3.31495}$

$$
\mathrm{H}^{\prime}-\mathrm{H}=2065.1 \text { metres. }
$$

In Table IV. $\frac{\mathrm{H}^{\prime 2}}{\mathrm{a}}-\frac{\mathrm{H}^{2}}{\mathrm{a}}=+0.9$
$h^{\prime}-h=2066.0$
Geneva altitude $h=407.0$
St. Bernard above the level of the sea $h^{\prime}=2473.0$ metres.

## Example 2.

Computing the height of Mont Blane from the observations of Bravais and Martins, on the 29th of August, 1844, taking St. Bernard (2473.0 metres) as the lower station. The observation gives,


| TABLE I.$\text { Argument }=\tau+\tau^{\prime} . \text { Centigrade Degrees. }$ |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { TABLE IV. } \\ & \text { Arg't. = Height. } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\tau+{ }^{t}$. | log. V. | $\log$. W. | + -1 . | log. V. | log. W. | + ${ }^{1}$ | log. V. | Iog. W. | $\begin{aligned} & \mathbf{H}^{\mathbf{H}} . \end{aligned}$ | $\pm$ |
| $\bigcirc$ |  |  | O |  |  | $\bigcirc$ |  |  | Metres. | Metres. |
| -24 | 4.24644 | 6.5362 | $+15$ | 4.27783 | 7.1692 | +54 | 4.30711 | 7.7033 | 200 | 0.01 |
| -23 | 4.24728 | 6.5441 | +16 | 4.27561 | 7.1539 | +55 | 4.30784 | 7.7160 | 400 | 0.03 |
| -22 | 4.24811 | 6.5620 | +17 | 4.27938 | 7.1985 | +56 | 4.30856 | 7.7287 | 600 | 0.06 |
| -21 | 4.24894 | 6.5797 | +18 | 4.28016 | 7.2131 | +57 | 4.30929 | 7.7413 | 800 | 0.10 |
| -20 | 4.24977 | 6.5974 | +19 | 4.28093 | 7.2275 | +58 | 4.31001 | 7.7539 | 1000 | 0.16 |
| -19 | 4.25059 | 6.6157 | +20 | 4.28170 | 7.2420 | +59 | 4.31073 | 7.7664 | 1200 | 0.23 |
| -18 | 4.25142 | 6.6341 | +21 | 4.28247 | 7.2564 | +60 | 4.31145 | 7.7789 | 1400 | 0.31 |
| -17 | 4.25225 | 6.6521 | +22 | 4.28323 | 7.2708 | +61 | 4.31217 | 7.7914 | 1600 | 0.40 |
| -16 | 4.25307 | 6.6700 | $+23$ | 4.28400 | 7.2850 | $+62$ | 4.31288 | 7.8038 | 1800 | 0.51 |
| -15 | 4.25389 | 6.6879 | +24 | 4.28477 | 7.2993 | +63 | 4.31360 | 7.8161 | 2000 | 0.63 |
| -14 | 4.25471 | 6.7057 | +25 | 4.28553 | 7.3135 | +64 | 4.31432 | 7.8285 | 2200 | 0.76 |
| -13 | 4.25553 | 6.7232 | +26 | 4.28629 | 7.3276 | +65 | 4.31503 | 7.8407 | 2400 | 0.90 |
| -12 | 4.25634 | 6.7407 | +27 | 4.28705 | 7.3417 | +66 | 4.31574 | 7.8530 | 2600 | 1.06 |
| -11 | 4.25716 | 6.7581 | +28 | 4.28781 | 7.3557 |  |  |  | 2800 | 1.23 |
| -10 | 4.25797 | 6.7755 | +29 | 4.25857 | 7.3697 |  |  |  | 3000 | 1.41 |
| -9 | 4.25878 | 6.7926 | +30 | 4.28933 | 7.3837 |  |  |  | 3200 | 1.61 |
| -8 | 4.25959 | 6.8096 | +31 | 4.29008 | 7.3975 |  |  |  | 3400 | 1.82 |
| -7 | 4.26040 | 6.8266 | +32 | 4.29084 | 7.4114 |  |  |  | 3600 | 2.04 |
| -6 | 4.26121 | 6.8436 | +33 | 4.29159 | 7.4252 |  |  |  | 3800 | 2.27 |
| $-5$ | 4.26202 | 6.8603 | +34 | 4.29234 | 7.4389 |  |  |  | 4000 | 2.51 |
| -4 | 4.26282 | 6.8770 | +35 | 4.29319 | 7.4526 |  |  |  | 4200 | 2.77 |
| - 3 | 4.26362 | 6.8935 | +36 | 4.29384 | 7.4662 |  |  |  | 4400 | 3.04 |
| - 2 | 4.26443 | 6.9100 | +37 | 4.29459 | 7.4798 |  |  |  | 4600 | 3.32 |
| - 1 | 4.26523 | 6.9263 | +38 | 4.29534 | 7.4933 |  |  |  | 4800 | 3.62 |
| 0 | 4.26603 | 6.9426 | +39 | 4.29608 | 7.5068 |  |  |  | 5000 | 3.93 |
| $+1$ | 4.26682 | 6.9581 | +40 | 4.29683 | 7.5202 |  |  |  | 5200 | 4.25 |
| $+2$ | 4.26762 | 6.9736 | +41 | 4.29757 | 7.5836 |  |  |  | 5400 | 4.58 |
| + 3 | 4.26841 | 6.9889 | + 42 | 4.29831 | 7.5470 |  |  |  | 5600 | 4.93 |
| + 4 | 4.26921 | 7.0043 | $+43$ | 4.29905 | 7.5602 |  |  |  | 5800 | 5.28 |
| $+5$ | 4.27000 | 7.0195 | +44 | 4.29979 | 7.5735 |  |  |  | 6000 | 5.65 |
| + 6 | 4.27079 | 7.0347 | + 45 | 4.30053 | 7.5867 |  |  |  | 6200 | 6.04 |
| + 7 | 4.27157 | 7.0499 | $+46$ | 4.30127 | 7.5999 |  |  |  | 6400 | 6.43 |
| +8 | 4.27236 | 7.0650 | $+47$ | 4.30200 | 7.6130 |  |  |  | 6600 | 6.84 |
| + 9 | 4.27315 | 7.0800 | +48 | 4.30273 | 7.6260 |  |  |  | 6800 | 7.26 |
| +10 | 4.27393 | 7.0950 | +49 | 4.30347 | 7.6390 |  |  |  | 7000 | 7.70 |
| +11 | 4.27471 | 7.1099 | +50 | 4.30420 | 7.6519 |  |  |  | 7200 | 8.14 |
| +12 | 4.27550 | 7.1248 | +51 | $4.30-493$ | 7.6618 |  |  |  | 7400 | 8.60 |
| +13 | 4.27628 | 7.1397 | +52 | 4.30566 | 7.6777 |  |  |  |  |  |
| +14 | 4.27705 | 7.1545 | +53 | 4.30639 | 7.6905 |  |  |  |  |  |
| +15 | 4.27783 | 7.1692 | +54 | 4.30711 | 7.7033 |  |  |  |  |  |


| TABLE II.$\text { Argument }=\log . \mathrm{W} \cdot \frac{\left(\kappa+x^{\prime}\right)}{\left(\mathbf{B} \overline{\mathbf{B}^{\prime}}\right.} .$ |  |  |  |  |  | TABLE III. <br> Argument $=$ Latitude. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Argum't. | $\log . \mathrm{V}^{\prime}$. | Argun't. | $\log . V^{\prime}$. | Argum't. | log. $\mathrm{V}^{\prime}$. | ¢. | lig. G'. | $c$. | $\log . \mathrm{G}^{\prime}$. |
| 6.5 | 0.00014 | 7.70 | 0.00218 | 8.09 | 0.00538 | $\bigcirc$ | +0.00114 | + | +0.00020 |
| 6.6 | 0.00017 | 7.71 | 0.00223 | 8.10 | 0.00550 | 1 | +0.00114 | 41 | $+0.00016$ |
| 6.7 | 0.00022 | 7.72 | 0.00229 | 8.11 | 0.00563 | 2 | +0.00114 | 42 | +0.00012 |
| 6.8 | 0.00027 | 7.73 | 0.00234 | 8.12 | 0.00576 | 3 | +0.00114 | 43 | +0.00008 |
| 6.9 | 0.00034 | 7.74 | 0.00239 | 8.13 | 0.00590 | 4 | $+0.00113$ | 44 | $+0.00004$ |
| 7.0 | 0.00043 | 7.75 | 0.00245 | 8.14 | 0.00604 | 5 | +0.00112 | 45 | 0.00000 |
| 7.1 | 0.00055 | 7.76 | 0.00251 | 8.15 | 0.00618 | 6 | +0.00112 | 46 | -0.00004 |
| 7.2 | 0.00069 | 7.77 | 0.00256 | 8.16 | 0.00632 | 7 | +0.00111 | 47 | -0.00008 |
| 7.3 | 0.00087 | 7.78 | 0.00262 | 8.17 | 0.00647 | 8 | $+0.00110$ | 48 | -0.00012 |
| 7.4 | 0.00109 | 7.79 | 0.00269 | 8.18 | 0.00662 | 9 | +0.00109 | 49 | -0.00016 |
| 7.41 | 0.00112 | 7.80 | 0.00275 | 8.19 | 0.00678 | 10 | $+0.00107$ | 50 | -0.00020 |
| 7.42 | 0.00114 | 7.81 | 0.00281 | 8.20 | 0.0069 + | 11 | +0.00106 | 51 | -0.00024 |
| 7.43 | 0.00117 | 7.82 | 0.00288 | 8.21 | 0.00710 | 12 | +0.00104 | 52 | -0.00028 |
| 7.44 | 0.00120 | 7.83 | 0.00295 | 8.22 | 0.00727 | 13 | +0.00103 | 53 | -0.00031 |
| 7.45 | 0.00123 | 7.84 | 0.00302 | 8.23 | 0.00744 | 14 | +0.00101 | 54 | -0.00035 |
| 7.46 | 0.00125 | 7.55 | 0.00309 | 8.24 | 0.00761 | 15 | +0.00099 | 55 | -0.00039 |
| 7.47 | 0.00128 | 7.86 | 0.00316 | 8.25 | 0.00779 | 16 | +0.00097 | 56 | -0.000 43 |
| 7.48 | 0.00131 | 7.57 | 0.00323 | 8.26 | 0.00798 | 17 | +0.00095 | 57 | $-0.00046$ |
| 7.49 | 0.00134 | 7.58 | 0.00331 | 8.27 | 0.00816 | 18 | $+0.00092$ | 58 | -0.00050 |
| 7.50 | 0.00138 | 7.89 | 0.00338 | 8.28 | 0.00835 | 19 | +0.00090 | 59 | -0.00054 |
| 7.51 | 0.00141 | 7.90 | 0.00346 | 8.29 | 0.00855 | 20 | +0.00087 | 60 | -0.00057 |
| 7.52 | 0.00144 | 7.91 | 0.00354 | 8.30 | 0.00875 | 21 | +0.0008.5 | 61 | -0.00060 |
| 7.53 | 0.00147 | 7.92 | 0.00363 | 8.31 | 0.00596 | 22 | +0.00082 | 62 | -0.00064 |
| 7.54 | 0.00151 | 7.93 | 0.00371 | 8.32 | 0.00917 | 23 | $+0.00079$ | $6: 3$ | -0.00067 |
| 7.55 | 0.00154 | 7.94 | 0.00380 | 8.33 | 0.00939 | 24 | +0.00076 | 64 | -0.00070 |
| 7.56 | 0.00158 | 7.95 | 0.00389 | 8.34 | 0.00961 | 25 | +0.00073 | 65 | $-0.00073$ |
| 7.57 | 0.00162 | 7.96 | 0.00398 | 8.35 | 0.00933 | 26 | $+0.00070$ | 66 | -0.00076 |
| 7.58 | 0.00165 | 7.97 | 0.00407 |  |  | 27 | +0.00067 | 67 | -0.00079 |
| 7.59 | 0.00169 | 7.98 | 0.00417 |  |  | 28 | +0.00064 | 68 | -0.00082 |
| 7.60 | 0.00173 | 7.99 | 0.00427 |  |  | 29 | +0.00060 | 69 | -0.00085 |
| 7.61 | 0.00177 | 8.00 | 0.00437 |  |  | 30 | +0.00057 | 70 | -0.00087 |
| 7.62 | 0.00181 | 8.01 | 0.00447 |  |  | 31 | +0.00054 | 71 | -0.00690 |
| 7.63 | 0.00186 | 8.02 | 0.00457 |  |  | 32 | +0.00050 | 72 | -0.000932 |
| 7.64 | 0.00190 | 8.03 | 0.00468 |  |  | 33 | +0.000 46 | 73 | -0.60094 |
| 7.65 | 0.00194 | 8.04 | 0.00479 |  |  | 34 | $+0.000 \div 3$ | 74 | -0.00097 |
| 7.66 | 0.00199 | 8.05 | 0.00490 |  |  | 35 | +0.00039 | 75 | -0.00099 |
| ${ }^{7} .67$ | 0.00201 | 8.06 | 0.00502 |  |  | 36 | +0.00035 | 76 | -0.00101 |
| 7.68 | 0.00208 | 8.07 | 0.00513 |  |  | 37 | +0.00031 | 77 | -0.00102 |
| 7.69 | 0.00213 | 8.08 | 0.00525 |  |  | 38 | +0.00028 | 78 | -0.00104 |
| 7.70 | 0.00218 | 8.09 | 0.00538 |  |  | 39 | +0.00024 | 79 | -0.00106 |
|  |  |  |  |  |  | 40 | +0.00020 | s0 | -0.00107 |

## CORRECTION

FOR TIHE HOUR OF THE DAY AND THE SEASON OF THE YEAR AT WHLCII TIIE OBSERVATIONS IIAVE BEEN TAKEN.

In all the precedmg tables, the mean temperature of the layer of air between the two stations is assumed to be given by the half-sum of the temperatures observed at each station, or by $\frac{t+t^{\prime}}{2}$. Experience, however, has proved that this assumption is not true under all meteorological circumstances, and that, not to speak of more irregular influences, the temperature expressed by $\frac{t+t^{\prime}}{2}$ differs in + or - from the true mean temperature by a quantity which considerably varics with the hour of the day, the season of the year, and the elevation at which the observations are taken. The amount of the correction for the temperature of the air, as given by the various formulas, thus needs to be modified accordingly. In the absence of the dita necessary for establishing the law of the decrease of heat on the vertical in the various layers of the atmosphere, at the different periods of the day and of the year, and in different latitudes, which alone would furnish the means of determining the true value of this correction in these various circumstances, the following empirical tables enable us to form a judgment of the mportance of that correction.

Tables IX. and X. are taken from Berghans, Grundriss der Geographie, p. 91, and in the Tables accompanying the same work, p. 71. The correction to be applied for the hour of the day at which the observations have been taken, is found by multiplying the approximate height obtained by the factors in Table IX, giving to the correction the sign of the factor. This table and the following are calculated to be used in the climate of Germany, and for elevations not much exceeding 5,000 feet. The influence of the seasons on the correction is not taken into the account; jurging from Table X., the correction may be, perhaps, too small for the summer months, and may better answer for the autumn. Using these factors, we obtain for the differences of level, in toises, placed at the head of each column, in 'Table X., the correction corresponding to each hour, from $6 \mathrm{~A} . \mathrm{M}$. to $10 \mathrm{P} . \mathrm{M}$.

> TABLE IX.

CORLECTION FOR THE HOUR OF THE DAY.

| Hour. | Factor, | Hour. | Factor | Hous. | Factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A. M. 6 | $+0.0075$ | Noon. | -0.0054 | P. M. 5 | -0.0011 |
| 7 | +0.0050 | P. M. 1 | -0.0057 | 6 | +0.0013 |
| 8 | +0.0025 | 2 | -0.00.59 | 7 | +0.0022 |
| 9 | -0.0005 | 3 | -0.0045 | 8 | +0.0032 |
| 10 | -0.0035 | 4 | -0.0031 | 9 | +0.00 +3 |
| 11 | -0.0044 | 5 | -0.0011 | 10 | +0.0054 |

# TABI.E X. <br> CORRECTION FOR THE HOUR OF THE DAY. 

Argument, the Ilour, and the Approvimate Heigut in toises.

| Correction, in Toises, for |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hour. | 100 | 200 | 300 | 400 | 500 | 600 | 800 | 800 | 900 | Hour. |
| A. M. 6 | $+0.7$ | $+1.5$ | +2.2 | $+3.0$ | $+3.7$ | $+4.5$ | $+5.2$ | $+6.0$ | $+6.7$ | $6 \mathrm{~A} . \mathrm{M}$. |
| 7 | $+0.5$ | +1.0 | $+1.5$ | $+2.0$ | +2.5 | $+3.0$ | +3.5 | $+4.0$ | $+4.5$ | 7 |
| 8 | $+0.2$ | $+0.5$ | $+0.7$ | $+1.0$ | +1.2 | $+1.5$ | +1.8 | $+2.0$ | +2.3 | 8 |
| 9 | $-0.0$ | $-0.1$ | -0.1 | $-0.2$ | -0.2 | -0.3 | -0.3 | -0.4 | -0.4 | 9 |
| 10 | $-0.3$ | -0.7 | $-1.0$ | -1.4 | -2.1 | -2.4 | -2.8 | -3.1 | -3.5 | 10 |
| 11 | -0.1 | -0.9 | -1.3 | -1.8 | -2.2 | -2.7 | -3.1 | -3.6 | -4.0 | 11 |
| Noon. | -0.7 | -1.1 | -1.6 | -2.2 | -2.7 | -3.3 | -3.8 | -4.4 | -1.9 | Noon. |
| P. M. 1 | -0.6 | $-1.1$ | -1.7 | -2.3 | -2.8 | -3.4 | -4.0 | -4.5 | -5.1 | $1 \mathrm{P} . \mathrm{M}$. |
| 2 | -0.6 | $-1.2$ | -1.8 | -2.4 | -3.0 | -3.5 | $-1.1$ | $-4.7$ | -5.3 | 2 |
| 3 | -0.4 | $-0.9$ | $-1.3$ | -1.9 | -2.2 | -2.7 | -31 | -3.6 | $-4.0$ | 3 |
| 4 | -0.3 | $-0.6$ | $-0.9$ | $-1.2$ | $-1.5$ | -1.8 | -2.1 | -2.4 | -2.7 | 4 |
| 5 | $-0.1$ | -0.2 | -0.3 | $-0.4$ | $-0.5$ | $-0.6$ | -0.7 | -0.8 | -0.9 | 5 |
| 6 | $+0.1$ | $+0.2$ | $+0.4$ | $+0.5$ | $+0.5$ | $+0.8$ | $+0.9$ | $+1.0$ | +1.1 | 6 |
| 7 | $+0.2$ | $+0.4$ | $+0.7$ | $+0.9$ | $+1.1$ | $+1.3$ | $+1.6$ | +1.8 | $+2.0$ | 7 |
| 8 | $+0.3$ | $+0.6$ | $+0.9$ | +1.3 | +1.6 | $+1.9$ | $+2.2$ | +2.5 | +2.9 | 8 |
| 9 | $+0.4$ | $+0.9$ | +1.3 | +1.7 | $+2.1$ | $+2.6$ | $+3.0$ | +3.4 | +3.9 | 9 |
| 10 | $+0.5$ | $+1.1$ | +1.6 | $+2.1$ | $+2.7$ | +3.2 | $+2.8$ | +4.3 | +4.8 | 10 |

Table XI. is found in the Résumé des Observations Thermométrique et Barométriques faites à Genère et au Grand St. Bernard pendant les dix amnéps 1841 à 1ヶ50, a very elaborate paper by Professor E. Plantamour, Director of the Observatory at Geneva, published in Vol. XIII. of the Mémoires de la Société de. Physique de Genève. The author, after having determined the difference of clevation between Geneva ( 407.0 metres above the level of the sca) and the Great St. Bernard, by means of the corresponding observations, made during these 10 years, and using his own tables given above, reversed the problem. Assuming the difference of level thus fond, viz. 2066 metres, to be the true height of the layer of air between the two stations, and its weight being given by the barometrical observations, he deduced from these data its mean density, and from the density its mean temperature at every even hour in every month of the year. Comparing these mean temperatures with those given at the same hours by the half-sum of the temperatures taken at the upper and the lower station, he found the differences contained in Table Xl., which are the corrections to be applied to the half-sums of the temperatures to obtain, in this particular case, the true mean temperatures. The second part of the table has been computed by multiplying each temperature in the first by 7.5 metres, in order to show the value of that correction in barometrical measurements.

D

## TABLE XI.

CORRECTION TO BE APPLIED TO THE HALF-SUMS OF THE TEMPERATURES OF TIIE AIR, OBSERVED AT GENEVA AND AT THE GREAT ST, BERNARD, TO OBTAIN THE TRUE MEAN TEMPERATURE OF THE AIR BETWEEN THE TWO STATIONS.

| Correction, in Ceutigrade Degrees, for |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hour | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| Noon. | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
|  | $-0.5$ | -1.7 | -3.0 | -3.9 | $-4.1$ | -4.4 | $-44$ | -3.8 | -2.7 | $-1.6$ | -0.4 | $+0.7$ | $-2.5$ |
| 2 | $\begin{aligned} & -0.2 \\ & +0.4 \end{aligned}$ | $-1.5$ | -2.8 | $-3.7$ | $-4.0$ | $-1.4$ | $-4.4$ | -3.8 | -2.6 | $-1.5$ | $-0.2$ | $+0.7$ | $-2.3$ |
| 4 |  | $-0.6$ | $-1.6$ | -2.5 | $-2.7$ | -3.4 | -3.6 | $-2.9$ | $-1.7$ | $-0.7$ | $+0.4$ | +1.3 | -1.5 |
| 6 | $+1.2$ | $+0.7$ | $-0.2$ | $-0.9$ | $-1.3$ | -2.1 | -2.2 | $-1.6$ | -0.5 | $+0.4$ | $+1.3$ | $+2.1$ | $-0.3$ |
| 8 | $+1.5$ | $+1.4$ | $+0.6$ | 0.0 | 0.0 | -0.6 | -0.7 | -0.5 | +0.3 | +1.3 | +1.7 | $+2.6$ | $+0.6$ |
| 10 | $+1.7$ | $+1.5$ | +1.2 | $+0.6$ | $+0.7$ | +0.5 | -0.1 | $+0.1$ | $+0.8$ | $+1.7$ | $+1.5$ | $+2.6$ | +1.1 |
| Midnight. | $+1.9$ | $+1.8$ | $+1.9$ | $+1.3$ | $+1.8$ | $+1.6$ | $+0.9$ | $+1.2$ | $+1.3$ | $+2.3$ | $+2.1$ | $+2.5$ | $+1.7$ |
| 2 | $+2.0$ | $+2.2$ | $+2.5$ | $+1.9$ | $+2.2$ | $+2.0$ | $+1.5$ | $+2.0$ | +1.9 | $+2.5$ | +2.4 | $+2.6$ | $+2.2$ |
| 4 | $+2.3$ | $+2.5$ | $+2.6$ | $+1.8$ | $+1.7$ | +1.4 | +1.1 | +1.8 | $+2.1$ | $+2.5$ | $+2.7$ | +29 | $+2.1$ |
| 6 | $+2.0$ | $+2.0$ | $+1.7$ | $+0.7$ | $+0.1$ | $+0.1$ | 0.0 | $+0.7$ | $+1.5$ | $+1.7$ | $+2.3$ | $+2.9$ | $+1.3$ |
| 8 | $+1.5$ | +1.1 | 0.0 | -1.3 | $-2.0$ | -2.2 | -2.4 | $-1.7$ | $-0.4$ | +0.6 | $+1.7$ | $+25$ | -0.3 |
| 10 | $+0.4$ | -0.4 | $-2.0$ | -3.1 | -3.5 | -3.8 | $-3.7$ | -3.1 | -2.0 | -1.0 | $+0.3$ | $+1.3$ | $-1.7$ |
| Mean, | $+1.2$ | +0.8 | $+0.1$ | $-0.8$ | $-0.9$ | -1.2 | $-1.5$ | $-0.9$ | $-0.2$ | $+0.7$ | $+1.3$ | $+2.1$ | 0.0 |
|  | Correction, in Metres, for |  |  |  |  |  |  |  |  |  |  |  |  |
| Hour. | Jin. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| Noon. | $-3.7-12.7$ |  | $-22.5$ | $-29.2$ | -30.7 | $-33.0$ | $-33.0$ | -28.5 | -20.2 | $-12.0$ | $-3.0$ | $+5.2$ | $-18.7$ |
| 2 | $-1.5-11.2$ |  | $-21.0$ | $-27.7$ | $-30.0$ | $-33.0$ | -33.0 | $-28.5$ | $-19.5$ | $-11.2$ | $-1.5$ | $+5.2$ | $-17.2$ |
| 4 | $+3.0-4.5$ |  | $-12.0$ | $-18.7$ | $-20.2$ | -05.5 | $-27.0$ | -21.7 | $-12.7$ | $-5.2$ | + 3.0 | $+9.7$ | $-11.2$ |
| 6 | $+9.0+5.2$ |  | $-1.5$ | $-6.7$ | $-9.7$ | -15.7 | -16.5 | $-12.0$ | $-3.7$ | $+3.0$ | + 9.7 | $+15.7$ | $-2.2$ |
| 8 | $+11.2+10.5$ |  | $+4.5$ | 0.0 | 0.0 | $-4.5$ | $-5.2$ | $-3.7$ | $+2.2$ | $+9.7$ | +12.7 | $+19.5$ | + 4.5 |
| 10 | $+12.7$ | $+11.2$ | $+9.0$ | $+4.5$ | $+5.2$ | $+3.7$ | $-0.7$ | $+0.7$ | $+6.0$ | $+12.7$ | $+13.5$ | $+19.5$ | $+8.5$ |
| Milluight. | $+14.5+13.5$ |  | $+14.5$ | $+9.7$ | $+13.5$ | $+12.0$ | $+6.7$ | $+9.0$ | $+9.7$ | $+17.2$ | $+15.7$ | $+18.7$ | $+12.7$ |
| 2 | $+15.0$ | $+16.5$ | $+18.7$ | $+14.2$ | $+16.5$ | $+15.0$ | +11.2 | $+15.0$ | $+14.2$ | $+18.7$ | $+18.0$ | $+19.5$ | $+16.5$ |
| 4 | +17.2 | $+18.7$ | ' +19.5 | $+13.5$ | $+12.7$ | $+10.5$ | $+8.2$ | +13.5 | $+15.7$ | $+18.7$ | $+20.2$ | $+21.7$ | $+15.7$ |
| 6 | +15.0 | $+15.0$ | $+12.7$ | + 5.2 | $+3.0$ | $+0.7$ | 0.0 | + 5.2 | +11.2 | $+12.7$ | $+17.2$ | $+21.7$ | $+9.7$ |
| 8 | $\begin{aligned} & +11.2 \\ & +\quad 3.0 \end{aligned}$ | $+8.2$ | 0.0 | $-9.7$ | -15.0 | $-16.5$ | $-18.0$ | $-12.7$ | $-3.0$ | $+4.5$ | $+12.7$ | $+18.7$ | $-2.2$ |
| 10 |  | $-3.0$ | $-15.0$ | -33.2 | $-26.2$ | -28.5 | $-27.7$ | -23.2 | $-15.0$ | $-7.5$ | $+2.2$ | $+9.7$ | $-12.7$ |
| Mean, | $+9.0$ | $+6.0$ | $+0.7$ | -6.0 | $-6.7$ | $-9.0$ | $-11.2$ | $-6.7$ | $-1.5$ | $+5.2$ | $+9.7$ | $+15.7$ | 0.0 |

The elevation of a place in the interior of a continent where regular meteorological observations are made, may be ascertained by taking the yearly means of the barometer reduced to the freezing point, and of the temperature of the air, as data for the upper station, and the yearly means of the reduced barometer and of the free thermometer at the level of the sea, as the data for the lower station. The Hypsometric Tables then will give the difference of level. As observation, however, has shown that the mean height of the barometer at the level of the sea is not the same in all latitudes, it is necessary to take for such a comparison the mean height of the barometer which belongs to the latitude of the station the elevation of which is to be computed, or that which is nearest to it.
'Table Nll., published by Schouw, in Porgendorf's Annalen, and in the Comptes Rendus de l'Académie des Sciences, 'Tom. III. p. 573, gives in Paris lines the mean height of the barometer in various latitudes. The reduction into millimetres is from Martins's French translation of Kaemtz's Meteorology, p. 278 ; the corresponding values in English inches, and the new stations, Savannah, (ia., Philadelphia, Pa., and Cambridge, Mass., have been added. The mean heights last mentioned have been derived from three years of observations at Savannah, by Dr. John F. P'osey, from June, $\mathbf{1 8 5 3}$, to Jme, 1856 , published in the American Almanac; from four years of hourly observations at (rirard College, Philadelphia, by I'rof. A. D. Bache ; and from ten years of observations at Cambridge Observatory. They have been reduced to a common absolute standard and to mean tide-water at the respective places.

These mean barometric heights, corrected for the variation of gravity in latitude, according to the proposition of Poggendorf, by the formula $b=b 45$ ( $1-0.0025935$ $\cos \rightleftharpoons \phi$ ), where $b$ is the height of the barometer in latitude $\phi$, and $b 45$ the corresponding height at the forty-fifth degree of latitude, are found in another column. For computing the elevations, the uncorrected heights are to be used.

The mean barometric pressure, as shown by 'Table XIII. from Kaemtz's Précis de Météorologie, French translation, p. 281, is not the same in all seasons, and the monthly means differ by a quantity which also varies with the latitude. If, therefore, the height of an inland station is to be ascertained from the barometrical means of one or more months only, the computation must be made with the mean pressure in the corresponding months at the level of the sea; or if this is not known, the yearly means taken from Table XII. must be corrected for the difference between the monthly means of the given month, or months, and the annual mean in the same latitnde, as derived from the comparison of the numbers in Table XIII.

## Example.

Suppose an inland station, in latitude $40^{\circ} \mathrm{N}$.; the mean barometric pressure for July is 26.30 iuches, and its elevation is to be computed from it.

Table XII. gives for latitude $40^{\circ}$, at Philadelphia, reduced to the level of the sea, 30.053 inches. Table XIII. gives as the mean for July, at the same place, 759.80 millimetres, and for the year, 760.25 milimetres (both not reduced to the levet of the sea), difference - 0.45 millimetres $=-0.017$ English inches, which is to be subtracted from the annual mean, 30.053 , to reduce it to the mean of July; or D
$30.053-0.017=30.036$. This last number is to be used in the computation, with the mean temperature of July at both stations.

Towards the tropical regions, the irregular or non-periodic variations of the barometer, which in high and middle latitudes are so considemble as to render simultaneous observations indispensable for the measurement of heights, gradually decrease and nearly cease to exist, while the monthly and daily periodic variations, which are small in high latitudes, considerably increase. Within the tropics, therefore, the oscilations of the barometer being far more uniform, observations made during a short period of time, or even single observations, may be used for computing heights, without corresponding observations, by referring them to the mean pressure at the level of the sea as to a constant, provided this last has been corrected for the monthly and daily periodic variation at the place.

Table XIII. fumishes the means of applying the correction for the monthly variation, as deseribed above. 'Table XIV., which gives the mean beight of the barometer at all hours of the day in various latitudes, enables the observer to correct the data according to the hour at which the observations have been taken. This table is from Kaemtz's Vorlesungen über Meteorologie, French translation, p. 249. 'The column Bossekop is from the observations of the French Scientific Expedition in the North; the column Philadelphia, from the observations at Girard College, has been added.

The correction for the hourly variation is found by taking the difference between the mean of the hour of observation and the daily mean, and eorrecting accordingly, with due regard to the signs, either the yearly mean at the sea level, or the observation at the upper station.

## Example.

The barometer at Caracas, latitude $10^{\circ} 30^{\prime} \mathrm{N}$., on the 20 th of August, at 4 o'clock P. M., reads 680.57 millimetres.

In Table XII the mean height of the barometer at La Guayra, lat. $10^{\circ} \mathrm{N} . \quad$. . . . . $=760.17$ millimetres,

By 'Table XIII, we find for August a correction . . $=-\quad 2.95$
Mean barometer in August . . . . . $=757.22$
In Table XIV. daily mean - mean at 4 P. M. gives for 4 P. M. a correction . . . . . . . = - 1.17

Nean barometer at La Guayra in August, at 4 P. M. $\quad=\quad 756.05$ millimetres, which is the number to be used for the computation of the beight of Caracas. In this case, however, the monthly correction, being derived from a higher latitude, may be too small. Both corrections can of course be applied, with contrary signs, to the observation at Caracas, leaving then the mean height at the level of the sea as a constant.

TABLE XII.

## mean height of the barometer,

IN VARIOUS LATITUDES, REDUCED TO THE LEVEL OF THE SEA, AND TO THE
FREEZING POINT.


XIIf. MEAN HEGGE UF THE BARONETER, N ALL MONTHS OF THE YEAK, N Varioés Latitides.
$\mathrm{v}:$ : n-lucel to the Lerel of the sea.

| Pace: <br> Latiaie. | $\begin{aligned} & \mathrm{H}, 5 \mathrm{Na} \\ & 23=y \end{aligned}$ | $\begin{gathered} \text { CML } \\ \text { CiII } \\ 2 \div=3: 3 \end{gathered}$ | $\begin{aligned} & \mathrm{M}_{\mathrm{ACa}} \\ & 22=11^{\prime} \end{aligned}$ | $\begin{aligned} & I_{11 F O} \\ & 30=2^{\prime} \end{aligned}$ | $\begin{gathered} \therefore 1- \\ \cdots S_{1} \\ 32^{\circ} 5^{\prime} \end{gathered}$ | $\begin{aligned} & \text { PHILA- } \\ & \text { FELPAIA. } \\ & 39=5 s^{\prime} \end{aligned}$ | $\begin{aligned} & \text { Case } \\ & \text { ERIDGE } \\ & 420.23^{\prime} \end{aligned}$ | P, ह1: $t E^{\circ} 50^{\prime}$ | $\begin{gathered} \text { st. PE- } \\ \text { TERSBLR } \\ 590 \quad 5 b^{\prime} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jian. | -55.24 | 764.57 | 707.93 | 76.20 | 762.50 | 760.97 | 761.37 | 758.86 | 762.54 |
| Fer. | 700.15 | 75.5.0 0 | 705.01 | - | 763.76 | 759.63 | 260.90 | 7.59 .09 | 763.10 |
| March. | 700.us | 756.24 | -06.03 | 7.59 .43 | -63.0.5 | 760.51 | - 59.09 | 756.33 | 760.76 |
| Amil. | -59.5 | 753.53 | 901.93 | 760.10 | 763.10 | 760.0 .5 | 759.37 | 755.15 | 761.19 |
| May. | 758.14 | 750.-1 | 761.64 | 75:.23 | 763.39 | 759.09 | 7.59 .63 | 75.5 .61 | 760.94 |
| June. | 760.67 | 745.10 | 757.31 | 754.42 | 764.37 | 759.22 | 75:.91 | 73.85 | 759.23 |
| Jriv, | 260.67 | 717.54 | 757.91 | 7.53 .90 | 764.02 | 754.00 | 760.34 | 756.52 | 75.25 |
| Ave | 758.33 | 7i5..53 | 757.91 | 754.06 | 765.54 | 760.54 | 761.11 | 756.74 | 7.59.94 |
| $\bigcirc$ | 735.45 | 751.93 | 7102.22 | 758.70 | 763.36 | 761.25 | 261.83 | 7.56 .61 | 761.19 |
| It. | 75..19 | 755.25 | 703.37 | 259.70 | 763.13 | 760.6 E | 761.07 | 754.42 | 760.52 |
| Nor. | 751.25 | 7:3\% | 760.17 | 700.76 | 763.41 | 760.49 | 760.55 | 755.75 | 7.50 .05 |
| Dec. | 763.62 | 7100.59 | 708.65 | 761.32 | 761.12 | 760.92 | 760.50 | 755.09 | 76.0 .22 |
| Iear. | 800.25 | 7.54.54 | 763.15 | 75.3 .32 | 763.41 | 760.25 | 760.44 | 7.56 .46 | 760.57 |

Nif. MEAN height of the barometer, at all holrs of the day, w Variots latitides.
So: reluced to the Lerel of the Sea.

| Piaces. |  | Cumata. | $\mathrm{L}_{\mathrm{L}_{\mathrm{A}}}$ | $\underset{\text { CliL }}{\text { Cita. }}$ | PhiladelPHIA. | Padta. | Halle | $\begin{gathered} \text { St. PEE } \\ \text { TEFSBLRG } \end{gathered}$ | Boremor. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Latisule. | 020 | $10=2$ | $0=35^{\prime \prime}$ s | 20 |  | $45^{\circ}-24^{\prime} \times$ | - 29'x. |  | 90 58's. |
| Onserers. | Horner. | $\begin{aligned} & \text { LIum- } \\ & \text { indit. } \end{aligned}$ | Bous-intralt | Balfour | Bache | Ciminello. | Kaemtz | Kupffer. | Erarais. |
|  | $\frac{\text { Milim. }}{202}$ | Milim. $7.56 .-6$ | $\begin{aligned} & \text { Millim. } \\ & 7.59 .654 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 7.5=.50 \end{aligned}$ | Milim. 760.49 | Millim <br> 757.01 | $\begin{aligned} & \text { Millim. } \\ & \text { i53.23 } \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 759.3 .5 \end{aligned}$ | Millim. $754.90$ |
| 1 | 7-50.2) | -76.53 | 759.34 | 75-6.62 | 760.45 | 756.90 | 753.14 | -• | .. |
| 2 | 751.7 | 7.56 .21 | 753.05 | 75.57 | 760.41 | 7.56 .54 | 753.05 | 759.32 | 7.54 .79 |
| 3 | 751.63 | 75.5 .29 | $75=.81$ | 758.49 | 760.34 | 750.78 | 752.99 | -• | - |
| 4 | 751.32 | 75.5 .166 | 75.65 | 75.47 | 760.89 | 756.74 | 752.99 | 759.32 | 754.80 |
| 5 | -51.6.5 | 75.5.79 | 750.0.5 | 7.59 .44 | 760.49 | 7.56 .75 | 753.34 | -• | . |
| 6 | 7.51 .45 | 7.56 .15 | 759.32 | 759.69 | 760.75 | 7540.99 | 753.12 | 7.59 .39 | 7.54 .65 |
| 7 | 759.43 | 756.55 | -59.94 | 759.16 | 761.00 | 7.515 .99 | 753.24 | - | .- |
| $s$ | 752.9.5 | 7.53 .93 | 760.50 | 7.59.35 | 761.15 | 757.01 | 7.53.37 | 7.59 .49 | 7.54.7.5 |
| 9 | 253.16 | 757.31 | 7.59.63 | 760.11 | 761.22 | 757.08 | 753.44 | . ${ }^{\text {c }}$ | . ${ }^{\text {a }}$ |
| 1) | -53.1.5 | 7-57.32 | 760.50 | -160.19 | \%61.17 | 757.14 | 7.53 .46 | 7.59 .51 | 7.54 .96 |
| 11 | 752.00 | 75.501 | 7.59.99 | 76).09 | 760.97 | 757.07 | 753.40 | -* | -• |
| Som. | 752.35 | 3.54 .57 | 7.59.41 | 759.61 | 760.56 | 757.02 | 7.53.29 | 759.47 | 75.01 |
| 1 | 751.05 | 7.5.5.97 | 7.5.91 | -59.23 | 760.13 | 756.5 | 753.11 | -* | '. |
| 2 | 7.51.55 | 75.5.4 | 753.41 | 755.39 | 7.59 .53 | 7.56 .67 | 752.99 | T59.35 | 754.96 |
| 3 | -51.15 | -5.5.14 | 758.12 | \%.53.12 | 759.65 | 7.56 .54 | 752.89 | -6 | -• |
| 4 | \%1.02 | 754.945 | 75.05 | 7.57 .91 | 759.65 | 7.56 .47 | 753.54 | 759.82 | 754.82 |
| 5 | 7.51 .31 | 7.55 .14 | 7.5. 10 | 7.57 .43 | 7.59 .70 | 7.56 .46 | 752.56 | - | -• |
| 6 | 751.71 | 755.41 | 7.58 .10 | 7.55 .01 | 7.59.65 | 756.50 | 7.52 .91 | 759.31 | 754.57 |
| 7 | 751.93) | 75.5.91 | 7-5.90 | 75.02 | 760.05 | 756.63 | 753.02 | -• | . |
| 5 | 753.3. | 7.56.21 | 759.19 | 758.54 | 760.31 | 756.79 | 753.14 | 759.32 | 754.59 |
| 9 | 7.5.74 | 7.53.59 | 7.59 .69 | 759.24 | 760.49 | 756.92 | 7:3.24 | ' | -6 |
| 1.9 | 7.52.5 | 7.53 .97 | -79.93 | 7.59 .33 | 760.59 | 7.57 .02 | 753.31 | \%59.36 | 754.92 |
| 11 | 752.-6 | 75\%.15 | 7.59 .93 | 75.09 | 760.72 | 7.57 .02 | 753.29 | -• | .. |
| Mean. | 7.3. 3.13 | 7.50 .33 | 7.39.22 | 7.58 .57 | 760.43 | 7.56 .83 | 783.19 | 7.59 .35 | 754.65 |

Table XIV. shows that, after all irregular variations of the barometer have been eliminated. there remains a double period of rise and fall within the twenty-iour hours, and that the amplitude of these daily oscillations is greatesi within the tropics, and goes on diminishing towards the polar regions.

According to Kaemtz, the mean time of the daily maxima and minima, or the mean tropic hours for the northern hemisphere, are as follows:-

> | The minimum of the afternoon is reached at $4.05 \mathrm{P} . \mathrm{M}$. |
| :--- |
| The maximum of the evening is reached at |
| $0.11 \mathrm{P} . \mathrm{M}$. |
| The minimum of the night is reached at |
| The maximum of the morning is reached at |
| Th. |
| $.35 \mathrm{~A} . \mathrm{A}$. |

Even in temperate and high latitudes these diurnal variations, though small, must be taken into account. if great accuracy is required. in reduciner corresponding ubservations made at a somewhat different hour to the time of the observation at the station the height of which is to be determined. But in so doing, it must be remembered that the times of the minima and maxima change with the seasons, as is shown by 'Table XV. from Kaemiz, p. 251 of the French translation.
XV. TROPIC HOURS OF THE DAILY TARIATION OF THE BARONETER AT HALLE.

LAT. $51^{2} 30 \mathrm{~N}$.

| Month. | $\left.\right\|_{\text {P. M. }} ^{\text {Mimum, }}$ | $\begin{gathered} \text { Maximum. } \\ \text { P. I. } \end{gathered}$ | Minimum. A. M. | Maximum. <br> A. M. | Month. | $\begin{gathered} \text { Minimum. } \\ \text { P. } 3 . \end{gathered}$ | $\begin{gathered} \text { Maximum } \\ \text { P } 1 . \text {. } \end{gathered}$ | $\underset{A . \mathrm{M}}{\mathrm{Minimum.}}$ | $\begin{aligned} & \text { Maximum, } \\ & \text { A y. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | h | h. | h . | h . |  | h. | h. | h. | h. |
| Jan. | 2.81 | 9.17 | 4.91 | 9.91 | Juls, | 5.21 | 11.04 | 3.04 | 2.73 |
| Fef) | 3.43 | 9.46 | 3.:6 | $9.6{ }^{\circ}$ | Aur. | 4.86 | 10.66 | 3.06 | 8.46 |
| March, | 3.52 | 9.00 | 3.5 | 10.10 | Supt. | 4.95 | 10.45 | 3.45 | 9.71 |
| April, | 4.46 | 10.27 | 3.53 | 9.53 | Oct. | 4.17 | 10.24 | 3.97 | 10.07 |
| May, | 5.43 | 10.93 | 3.03 | 9.13 | Nus. | 3.52 | 9.55 | 4.65 | $10.0=$ |
| June, | 5.20 | 10.93 | 2.83 | 8.83 | Dec. | 3.15 | 9.11 | 4.91 | 10.15 |

This shifting of the times of maxima and minima with the seasons diminishes with the latitude, and tends to disappear towards the equator. with the inequali:y of the days and nights. The elevation above the level of the sea also canses a change in the tropic hours of the daily variation which is not yet sufficiently studied.

Table XIV. gives evidence that the amplitude of the hourly oscilation is greatest under the equator, and gradually decreases towards the pole. Katm:z computes its mean value in various latitudes and at the level of the sea, as follows:-

XV'. AMPLITLDE OF DAILY VARIATIONS IN VARIOCS LATITUDES.

| Latitude | Variation. | Latitude. | Variation | Latitude. | Variation | Latitude | Variation. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Millim. | $\bigcirc 1$ | Nillim. | 01 | Millim. | $\bigcirc$ | Mthim. |
| $0 \quad 0$ | 2.23 | 2355 | 1.50 | 394 | 1.13 | 5233 | 0.45 |
| $526 \times$. | 2.26 | 29.98 | 1.55 | 4334 | 0.90 | 5717 | 0.23 |
| 1752 | 2.033 | $3+26$ | 1.8 .5 | 4) 1 | 0.67 | 62.5 | 0.00 |

The amplitude also decreases with the elevation, at least in our latitudes: it was found to be on the Faulhorn, in Swizerland, 9000 feet above the sea level, $0: 27$ millimetres, while it was 0.90 millimetres at Geneva.

To reduce barometric means taken at a given elevation to the height they would have if taken at the level of the sea, or barometric observations made at different elevations to a common level, in order to eliminate the influence of altitude in the comparison of barometric pressures, is a problem, the solution of which is often neederl in meteorolosy.

For a complete and aecurate reduction, embracing all cases, Tables IV. and V., by Dippe, given above, pages 54 et seq., may be-used. But when the difference of height between the two stations, or above the sea-level, does not exceed a few hundred feet, the small tables XVI. to XIX., in three different scales, will be found more convenient.
'Tables XVI. and XVII, have been computed from the constants of Laplace's formula, the barometric cocfficient, ineluding the correetion for the decrease of gravity on a vertical, being respectively $60,345.51$ English feet and $56,6: 1.83$ Paris feet; and the coefficient for expansion of moist air 0.00222 and 0.005 .

In 'Table XVIII. the coefficient 18,120 metres, deduced from Regnault's experiments (see Proccedings of the Amer. Assoc. for Adv. of Science, 1857), and his coefficient for expansion of dry air, 0.003665 , increased to 0.0039 , in order to include the effect of moisture, have been used.

## Use of the Tables.

The correction for reducing the barometer to the level of the sca is found by the formula

$$
\mathrm{C}=\frac{f}{\mathrm{~N}} \times \frac{h^{\prime}}{h},
$$

where C is the correction required ; $f$, the elevation of the station; N , the number in the tables; $h^{\prime}$, the reading of the barometer; $h$, the normal height of barometer at the sea-level.

## Example.

At Cambridge Observatory, Massachusetts, at 71.34 English feet above mean tide, the incan barmeter is $=29.939$ inches; the mean temperature $47^{\circ} .3$ Fahrenheit; what would be the height at the level of the sea?

In Table XVI, we tike for $47^{\circ} .3=90.49$, or, in order to get the correction in a fraction of an inch, 901.9 .

Then

$$
\mathrm{C}=\frac{71.34}{904.9} \times \frac{29.939}{30}=0.079, \text { correction required }
$$

and
$29.939+0.079=: 30.018$ inches, height of the barometer at the level of the sea.
It will be seen that the quantity represented by the second member can be neglected without causing a sensible error in the eorrection. In this case the error does not amoms to .001 ; it scarcely would reach .002 for 250 feet of elevation; so that the reduction can be made in most cases by a simple division; viz. $\frac{t^{\prime}}{\mathrm{N}}$.
x VI. heigit, in english feet, of a column of air corresponding to a tenth of an exglish incil in the barometer, at temperatures between $32^{\circ}$ AND $100^{\circ}$ FAHRENHEIT,
The Barometrie Pressure at the Lower Station being $=30$ English Inehes.

| Temperature of Air, | $\begin{gathered} \text { Meight } \\ \text { in } \\ \text { Luriixh } \\ \text { Eeet. } \end{gathered}$ | Temperature of Air, Fahren. | Height ${ }_{\text {in }}^{\text {in }}$ Feet | Temperature of Air, Fahren. | Hejght <br> English Feet. | Temperature of Fahren. | Height in English Feet. | Temperatule of Air, Fahren. | $\begin{aligned} & \text { Height } \\ & \text { in } \\ & \text { English } \\ & \text { Fett. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $32^{\circ}$ | 87.51 | $46^{\circ}$ | 90.23 | $60^{\circ}$ | 92.9.5 | $74^{\circ}$ | 95.67 | $87^{\circ}$ | 98.20 |
| 33 | 87.70 | 47 | 90.42 | 61 | 93.15 | 75 | 9.5 .87 | 88 | 98.40 |
| 31 | 87.90 | 48 | 90.62 | 62 | 93.34 | 76 | 96.06 | 89 | 98.59 |
| 35 | 88.09 | 49 | 90.81 | 63 | 93.53 | 77 | 96.26 | 90 | 98.79 |
| 36 | 85.23 | 50 | 91.01 | 6. | 93.73 | 78 | 96.45 | 91 | 98.68 |
| 37 | 84.19 | 51 | 91.20 | 6.5 | 93.92 | 79 | 96.65 | 92 | 99.17 |
| 38 | 82.67 | 52 | 91.40 | 66 | 94.12 | so | 96.84 | 93 | 99.37 |
| 39 | $8 \times .57$ | 53 | 91.59 | 67 | 94.31 | 81 | 97.04 | 94 | 99.56 |
| 40 | 89.96 | 54 | 91.78 | 65 | 91.51 | 82 | 97.23 | 9.5 | 99.76 |
| 41 | 89.26 | 55 | 91.98 | 69 | 91.70 | 83 | 97.42 | 96 | 99.95 |
| 42 | 89.15 | 56 | 92.17 | 70 | 94.90 | 84 | 97.62 | 97 | 100.15 |
| 43 | 89.65 | 57 | 92.37 | 71 | 95.09 | 8.5 | 97.81 | 98 | 100.34 |
| 44 | 89.51 | 58 | 92.56 | 72 | 9.5 .29 | ¢ 6 | 98.01 | 99 | 100.5-4 |
| 4.) | 90.03 | 59 | 92.76 | 73 | 95.48 | 87 | 98.20 | 100 | 100.73 |

XVII. HEIGHT, IN FRENCH FEET, OF A COLUMN OF AIR CORRESPONDING TO A paris line in the barometer, at temperatures of the air BETWEEN $0^{\circ}$ AND $34^{\circ}$ REAUMUR,

The Barometric Pressure at the Lower Station being $=337$ Paris Lines.

| Temperature of Air. <br> Reaumor. | Iheight $\stackrel{\text { in }}{\text { French }}$ Feet. | Temperature of Air, <br> Reaumur | $\begin{aligned} & \text { Height } \\ & \text { in } \\ & \text { French } \\ & \text { Feet. } \end{aligned}$ | Temperature of Air Reaumur. | Height <br> French <br> Feet. | Temperature of Air, Reaumur. | $\begin{aligned} & \text { Height } \\ & \text { in } \\ & \text { Freneh } \\ & \text { Feet. } \end{aligned}$ | Temperatture of Air, Leamur. | $\begin{aligned} & \text { Height } \\ & \text { in } \\ & \text { French } \\ & \text { Heet } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 73.08 | $7^{\circ}$ | 75.63 | $14^{\circ}$ | 78.19 | $21^{\circ}$ | 80.75 | $23^{\circ}$ | 83.31 |
| 1 | 73.44 | 8 | 76.00 | 1.5 | 78.56 | 22 | 81.11 | 29 | 83.67 |
| 2 | 73.51 | 9 | 76.36 | 16 | 78.92 | 23 | \$1.48 | 30 | 81.04 |
| 3 | 71.17 | 10 | 76.73 | 17 | 79.29 | 24 | 81.85 | 31 | 84.40 |
| 4 | 74.5t | 11 | 77.10 | 18 | 79.65 | 2.5 | 82.21 | 32 | 84.77 |
| 5 | 74.90 | 12 | 77.46 | 19 | 80.02 | 26 | 82.58 | 33 | 8.5.13 |
| 6 | 75.27 | 13 | 77.83 | 20 | 80.38 | 27 | 82.94 | 34 | 85.50 |

XVili. height, in metres, of a column of alr corresponding to a millimetre in the barometer, at temperatures between
$0^{\circ}$ AND $39^{\circ}$ CEntigrade,
The Barometric Pressure at the Lower Station being $=767$ Millimetres.

| Temperature of Air, Centigr | $\begin{aligned} & \text { II imight } \\ & \text { int } \\ & \text { netres } \end{aligned}$ | Temperature of $\xrightarrow{\text { Air, }}$ | $\begin{gathered} \text { Height } \\ \text { in } \\ \text { Metres. } \end{gathered}$ | Temperature of Air, Ceutigr. | $\begin{aligned} & \text { Height } \\ & \text { int } \\ & \text { metres. } \end{aligned}$ | Temperature of Air, Centigr. | $\begin{aligned} & \text { light } \begin{array}{l} \text { in } \\ \text { metre } \end{array} \end{aligned}$ | Temper- ature of ature Centigr | $\begin{aligned} & \text { Height } \\ & \text { in } \\ & \text { metres. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 10.54 | $5^{\circ}$ | 10.86 | $16^{\circ}$ | 11.19 | $24^{\circ}$ | 11.52 | $32^{\circ}$ | 11.85 |
| 1 | 10.58 | 9 | 10.91 | 17 | 11.23 | 2.5 | 11.56 | 33 | 11.89 |
| 2 | 10.62 | 10 | 10.95 | 18 | 11.28 | 26 | 11.60 | 31 | 11.93 |
| 3 | 10.66 | 11 | 10.99 | 19 | 11.32 | 27 | 11.64 | 35 | 11.97 |
| 4 | 10.70 | 12 | 11.03 | 20 | 11.36 | 23 | 11.69 | 36 | 12.01 |
| 5 | 10.74 | 13 | 11.07 | 21 | 11.40 | 29 | 11.73 | 37 | 12.06 |
| 6 | 10.78 | 14 | 11.11 | 22 | 11.44 | 80 | 11.77 | 28 | 12.14 |
| 7 | 10.82 | 15 | 11.15 | 23 | 11.48 | 31 | 11.81 | 39 | 12.14 |

Table XIX. gives, in metrical measure, the values of a millimetre in the barometer at different elevations and Centigrade temperatures. The values are derived from Laplace's eonstants, as in 'Tables XVI. and XVIt.

This table may be used, as the preceding ones, for reducing barometricat observations to the level of the sea, and also to any other level by a similar process.

## Example.

Suppose the barometer to read 700 millimetres at the altitude of 750 metres, the temperature of air being $=16^{\circ}$ Centigrade; what would be the readmg at a station lower by 350 metres, assuming the temperature of the air downwards to increase at the rate of $1^{\circ}$ Centigrade for 185 metres?

The temperature of air at lower station will be $16^{\circ}+1^{\circ} .9=17^{\circ} .9$
The approximate height of barometer about 73 eentimetres.
Then, in Table NIX. we find for $16^{\circ}$ and 70 centimetres, $12.15-$
$\because \quad 6 \quad 6$ for $17^{\circ} .9$ and 73 centimetres, 11.73
Nean 11.94
And
${ }_{11.94}^{350}=\mathbf{2 9 . 3 1}$, or barometer at lower station $700+29.31=799.31$ millimetres.
Delcros's tables, with these data, would give for the difference of level 319.76 , instead of 350 metres; the corresponding error in the height of the barometrieal column does not exceed 0.08 millimetre, and thus remains within the limits of error which may be expected in an ordinary observation.

The prineipal object of this table, however, is to furnish the scicntific traveller with the means of readily computing on the spot approximate differences of level, by simply multiptying the difference between the readings of the barometer at each station by the half sum of the numbers in the table corresponding to the data given by the observations.

## Excomple.

Suppose the barometer at the lower station to rad 739.5, and at the upper station 703.2 millimetres; the temperature of the air being respectively $18^{\circ}$ and $16^{\circ}$ Centigrade.

The difference of the barometers, supposed to be reduced to the same temperature, is 29.3 millimetres.

Then, Table XIX. gives for $18^{\circ}$ Centigrade and 73 eentimetres, 11.73
" " for $16^{\circ}$ Centigrade and 70 centimetres, 12.15

$$
\text { Half sum, or mean, } \quad 11.94
$$

And, $99.3 \times 11.94=349.8$ metres $=$ difference of level requred.
By the large tables of Deleros, we find for the same data 350.1 metres.
'This table ean be considered as a complement to Deleros's tables, and may save the traveller the trouble of carrying the larger tables.

A similar table in English measures is found above, at the end of the author's larger tables ('Table Vl.), page 48 of this series, and another, more extensive one, below, page $9 \%$, the use of which is explained by the examples just given. JIEIGHT, IN METRES, OF A COLUMN OF AIR, CORRESPONDING TO A MILLIMETRE, IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

| Temperature of $\xrightarrow{\text { Air, }}$ Clis. | Barometer at the Lower Station, Reading in Centimetres. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 76 | 75 | 71 | 73 | 78 | 71 | 70 | 69 | 68 | 67 |
| - | Metres. | Metres | Metres. | Metres. | Metres | Metres. | Metres | Netres | Metres. | Metres. |
| 0 | 10.52 | 10.66 | 10.s0 | 10.94 | 11.10 | 11.26 | 11.42 | 11.59 | 11.75 | 11.93 |
| 2 | 10.60 | 10.74 | 10.89 | 11.03 | 11.19 | 11.35 | 11.51 | 11.68 | 11.85 | 12.03 |
| 4 | 10.69 | 10.83 | 10.97 | 11.12 | 11.28 | 11.44 | 11.60 | 11.77 | 11.94 | 12.13 |
| 6 | 10.77 | 10.91 | 11.06 | 11.20 | 11.37 | 11.53 | 11.69 | 11.86 | 12.04 | 12.22 |
| 8 | 10.85 | 11.00 | 11.15 | 11.29 | 11.46 | 11.62 | 11.78 | 11.96 | 12.13 | 12.32 |
| 10 | 10.94 | 11.08 | 11.23 | 11.38 | 11.55 | 11.71 | 11.57 | 12.05 | 12.22 | 12.41 |
| 12 | 11.02 | 11.17 | 11.32 | 11.47 | 11.63 | 11.80 | 11.97 | 12.14 | 12.32 | 12.51 |
| 14 | 11.11 | 11.25 | 11.41 | 11.55 | 11.72 | 11.69 | 12.06 | 12.23 | 12.41 | 12.60 |
| 16 | 11.19 | 11.34 | 11.49 | 11.64 | 11.81 | 11.98 | 12.15 | 12.33 | 12.51 | 12.70 |
| 18 | 11.27 | 11.43 | 11.58 | 11.73 | 11.90 | 12.07 | 12.24 | 12.42 | 12.60 | 12.79 |
| 20 | 11.36 | 11.51 | 11.67 | 11.82 | 11.99 | 12.16 | 12.33 | 12.51 | 12.69 | 12.89 |
| 22 | 11.44 | 11.60 | 11.75 | 11.90 | 12.08 | 12.25 | 12.42 | 12.61 | 12.79 | 12.99 |
| 24 | 11.53 | 11.68 | 11.84 | 11.99 | 12.17 | 12.34 | 12.51 | 12.70 | 12.88 | 13.08 |
| 26 | 11.61 | 11.77 | 11.93 | 12.03 | 12.26 | 12.13 | 12.61 | 12.79 | 12.98 | 13.18 |
| 28 | 11.70 | 11.85 | 12.01 | 12.17 | 12.35 | 12.52 | 12.70 | 12.88 | 13.07 | 13.27 |
| 30 | 11.78 | 11.94 | 12.10 | 12.2.5 | 12.43 | 12.61 | 12.79 | 12.98 | 13.16 | 13.37 |
| 32 | 11.86 | 12.02 | 12.18 | 12.34 | 12.52 | 12.70 | 12.88 | 13.07 | 13.26 | 13.46 |
| 34 | 11.95 | 12.11 | 12.27 | 12.43 | 12.61 | 12.79 | 12.97 | 13.16 | 13.35 | 13.56 |
| 36 | 12.03 | 12.19 | 12.36 | 12.52 | 12.70 | 12.98 | 13.06 | 13.25 | 13.45 | 13.65 |
| 35 | 12.12 | 12.28 | 12.44 | 12.60 | 12.79 | 12.97 | 13.15 | 13.35 | 13.54 | 13.75 |
| emper- |  |  |  |  | ometer in | Centimetr |  |  |  |  |
| $\xrightarrow[\text { Air. }]{\text { Centiy }}$ | 63 | 65 | 61 | 63 | 62 | 61 | 60 | 59 | 58 | 57 |
| $\begin{aligned} & \circ \\ & 0 \end{aligned}$ | Metres $12.11$ | Metres. $12.30$ | Metres. $12.49$ | Metres. $12.69$ | Metres. $12.89$ | Metres. $1: 3.10$ | Metres. <br> 13.32 | Metres <br> 13.55 | Metres. $13.78$ | Metres. $14.03$ |
| 2 | 12.21 | 12.40 | 12.59 | 12.79 | 13.00 | 13.21 | 13.43 | 13.66 | 13.89 | 14.14 |
| 4 | 12.31 | 12.50 | 12.69 | 12.89 | 13.10 | 13.31 | 13.54 | 13.77 | 14.00 | 14.25 |
| 6 | 12.10 | 12.60 | 12.79 | 13.00 | 13.20 | 13.12 | 13.64 | 13.58 | 14.11 | 14.36 |
| S | 12.50 | 12.69 | 12.89 | 13.10 | 13.31 | 13.52 | 13.75 | 13.98 | 14.22 | 14.47 |
| 10 | 12.60 | 12.79 | 12.99 | 13.20 | 13.41 | 13.63 | 13.56 | 14.09 | 14.34 | 14.59 |
| 12 | 12.69 | 12.89 | 13.09 | 13.30 | 13.51 | 13.73 | 13.96 | 14.20 | 14.45 | 14.70 |
| 14 | 12.79 | 12.99 | 13.19 | 13.10 | 13.62 | 13.84 | 14.07 | 14.31 | 14.56 | 14.81 |
| 16 | 12.89 | 13.09 | 13.29 | 1350 | 13.72 | 13.94 | 14.18 | 14.42 | 14.67 | 14.92 |
| 13 | 12.98 | 13.19 | 13.39 | 13.61 | 13.82 | 14.05 | 14.28 | 14.53 | 14.78 | 15.04 |
| 20 | 13.09 | 13.28 | 13.49 | 13.71 | 13.93 | 14.15 | 14.39 | 14.63 | 14.89 | 15.15 |
| 22 | 13.18 | 13.38 | 13.59 | 13.81 | 14.03 | 14.26 | 14.50 | 14.74 | 15.00 | 15.26 |
| 24 | 13.27 | 13.18 | 13.69 | 13.91 | 14.13 | 14.26 | 14.60 | 14.85 | 15.11 | 15.37 |
| 26 | 13.37 | 13.58 | 13.79 | 14.01 | 14.24 | 14.47 | 14.71 | 14.96 | 15.22 | 15.48 |
| 28 | 13.47 | 13.68 | 13.89 | 14.11 | 14.34 | 14.57 | 14.82 | 15.07 | 15.33 | 15.60 |
| 30 | 13.67 | 13.78 | 13.99 | 14.22 | 14.41 | 14.68 | 14.92 | 15.18 | 15.44 | 15.71 |
| 32 | 13.66 | 13.87 | 14.09 | 14.32 | 14.35 | 14.75 | 15.03 | 15.28 | 15.55 | 15.82 |
| 34 | 13.76 | 13.97 | 14.19 | 14.4 .4 | 14.65 | 14.89 | 15.14 | 15.39 | 15.66 | 15.93 |
| 36 | 13.56 | 14.07 | 14.29 | 14.52 | 14.75 | 1499 | 15.24 | 15.50 | 15.77 | 16.05 |

XIX. HEIGIT, IN ENGLISH FEET, OF A COLUMN OF AIR, CORRESPONDING TO A TENTH OF AN INCH IN THE BAROMETER, AT DIFFERENT TEMPERATURES AND ELEVATIONS.

| Barometer Hewting in English Inches. | Temperature of the Air, Fahrenheit, being |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $40^{\circ}$ | $43^{\circ}$ | $50^{\circ}$ | $55^{\circ}$ | $60^{\circ}$ | 6.50 | $70^{\circ}$ | 8.50 | $80^{\circ}$ | $85^{\circ}$ | $90^{\circ}$ | $95^{\circ}$ |
| 22.0 | 121.5 | 122.8 | 124.2 | 125.5 | 126.8 | 128.2 | 129.5 | 130.8 | 132.1 | 133.5 | 134.8 | 136.1 |
| 22.2 | 120.4 | 121.7 | 123.1 | $124+$ | 125.7 | 127.0 | 128.3 | 129.6 | 130.9 | 132.2 | 133.6 | 134.9 |
| 22.4 | 119.3 | 120.6 | 121.9 | 123.2 | 124.6 | 125.9 | 127.2 | 128.5 | 129.8 | 131.1 | 132.4 | 133.7 |
| 22.6 | 118.2 | 119.5 | 120.8 | 12.2 .1 | 123.1 | 124.7 | 126.0 | 127.3 | 128.6 | 129.9 | 131.2 | 132.4 |
| 22.8 | 117.2 | 118.5 | 119.8 | 121.1 | 122.3 | 123.6 | 124.9 | 126.2 | 127.5 | 128.5 | 130.0 | 131.3 |
| 23.0 | 116.2 | 117.5 | 118.7 | 120.0 | 121.3 | 122.6 | 123.8 | 12.5 .1 | 126.4 | 127.6 | 129.9 | 130.2 |
| 23.2 | 115.2 | 116.5 | 117.7 | 119.0 | 120.2 | 121.5 | 122.7 | 124.0 | 125.3 | 126.5 | 127.8 | 129.0 |
| 23.1 | 114.2 | 115.5 | 116.7 | 118.0 | 119.2 | 120.5 | 121.7 | 123.0 | 124.2 | 125.4 | 126.7 | 127.9 |
| 23.6 | 1132 | 111.1 | 11.37 | 116.9 | 118.1 | 119.4 | 120.6 | 121.8 | 123.1 | 121.3 | 125.5 | 1268 |
| 23.8 | 112.3 | 113.5 | 114.8 | 116.0 | 1172 | 118.4 | 119.7 | 120.9 | 122.1 | 123.3 | 124.6 | 12.5 .8 |
| 24.0 | 111.4 | 112.6 | 113.8 | 11.5 .0 | 116.2 | 117.4 | 118.7 | 119.9 | 121.1 | 122.3 | 123.5 | 124.7 |
| 21.2 | 110.5 | 111.7 | 112.9 | 111.1 | 115.3 | 116.5 | 117.7 | 118.9 | 120.1 | 121.3 | 122.5 | 123.7 |
| 21.1 | 109.5 | 110.7 | 111.9 | 113.1 | 114.3 | 115.5 | 116.7 | 117.9 | 119.1 | 120.3 | 121.5 | 122.7 |
| 24.6 | 103.6 | 109.8 | 111.0 | 112.2 | 113.4 | 114.6 | 115.8 | 116.9 | 118.1 | 119.3 | 120.5 | 121.7 |
| 24.8 | 107.8 | 108.9 | 110.1 | 111.3 | 112.5 | 113.7 | 114.8 | 116.0 | 117.2 | 118.4 | 119.5 | 120.7 |
| 25.0 | 106.9 | 108.1 | 109.2 | 110.4 | 111.6 | 112.7 | 113.9 | 115.1 | 116.2 | 117.4 | 118.6 | 119.7 |
| 25.2 | 106.0 | 107.2 | 10.8 .4 | 109.5 | 110.7 | 111.8 | 113.0 | 114.1 | 115.3 | 116.5 | 117.6 | 118.8 |
| 2.5 .4 | 105.2 | 106.4 | 107.5 | 105.7 | 109.8 | 111.0 | 112.I | 113.3 | 114.4 | 115.6 | 116.7 | 117.9 |
| 2.5 .6 | 101.4 | 10.5.5 | $10 \stackrel{5}{ } 7$ | 107.3 | 103.9 | 110.1 | I11.2 | 112.4 | 113.5 | 111.6 | 115.8 | 116.9 |
| 25.8 | 103.6 | 104.7 | 10.5 .8 | 107.0 | 102. 1 | 109.2 | 110.4 | 111.5 | 112.6 | 113.8 | 114.9 | 116.0 |
| 26.0 | 102.8 | 103.9 | 105.0 | 106.] | 107.3 | 108.4 | 109.5 | 110.6 | 111.8 | 112.9 | 114.0 | 115.1 |
| 26.2 | 102.0 | 103.1 | 104.2 | 105.3 | 106.5 | 107.6 | 108.7 | $10 \% .8$ | 110.9 | 112.0 | $11: 3.1$ | 111.2 |
| 26.1 | 101.2 | 102.3 | 103.4 | 101.6 | 105.7 | 106.8 | 107.9 | 109.0 | 110.1 | 111.2 | 112.3 | 113.4 |
| 26.6 | 1005 | 101.6 | 102.7 | $10: .8$ | 104.9 | 106.0 | 107.1 | 108.2 | 109.3 | 110.4 | 111.4 | 112.5 |
| 26.8 | 99.7 | 100.8 | 101.9 | 103.0 | 104.1 | 10.5.2 | 106.3 | 107.4 | 108.5 | 109.5 | 110.6 | 111.7 |
| 27.0 | 99.0 | 100.1 | 101.2 | 102.2 | 103.3 | 104.1 | 10.5 .5 | 106.6 | 107.6 | 108.7 | 109.8 | 110.9 |
| 27.2 | 9 マ. 3 | 99.3 | 100.4 | 101..5 | 102.6 | 103.6 | 104.7 | 10.9 .8 | 106.8 | 107.9 | 109.0 | 110.1 |
| 27.1 | 97.5 | 98.6 | 99.7 | 100.7 | 101.8 | 102.9 | 103.9 | 105.0 | 106.1 | 107.1 | 105.2 | 109.3 |
| 27.6 | 96.8 | 97.9 | 98.9 | 100.0 | 101.1 | 102.1 | 103.2 | 104.2 | 105.3 | 106.3 | 167.4 | 108.5 |
| 27.8 | 96.1 | 97.2 | 98.2 | 99.8 | 100.3 | 101.1 | 102.4 | 103.5 | 104.5 | 10.5 .6 | 106.6 | 107.7 |
| 28.0 | 95.1 | 96.5 | 97.5 | 98.6 | 99.6 | 100.6 | 101.7 | 102.7 | 103.8 | 104.8 | 1059 | 106.9 |
| 28.2 | 91.8 | 9.5 .8 | 96.8 | 97.9 | 95.9 | 99.9 | 101.0 | 102.0 | 103.0 | 10.1 .1 | 105.1 | 106.1 |
| 23.4 | 94.1 | 9.5 .1 | 96.1 | 97.2 | 98.2 | 99.2 | 100.2 | 101.3 | 102.3 | 103.3 | 164.3 | 105.4 |
| 28.6 | 93.4 | 94.4 | 9.3.. | 96.5 | 97.5 | 98.5 | 99.5 | 100.6 | 101.6 | 102.6 | 103.6 | 10.4 .6 |
| 23.8 | 92.5 | 93.8 | 94.8 | 95.8 | 96.8 | 97.8 | 98.8 | 998 | 100.8 | 101.8 | 102.8 | 103.8 |
| 29.0 | 92.1 | 93.1 | 91.1 | 9.5 .1 | 96.2 | 97.2 | 98.2 | 99.2 | 100.2 | 101.2 | 1022 | 103.2 |
| 29.2 | 91.3 | 92.5 | 93.5 | 94.5 | 95.5 | 96.5 | 97.5 | 9.土.5 | 99.5 | 100.5 | 101.5 | 102.5 |
| 29.4 | 90.9 | 91.9 | 92.9 | 93.9 | 91.8 | 95.8 | 96.8 | 97.8 | 98.8 | 998 | 100.8 | 101.8 |
| 29.6 | 90.3 | 91.3 | 92.2 | 93.2 | 91.2 | 95.2 | 96.2 | 97.2 | 98.2 | 99.1 | 100.1 | 101.1 |
| 29.8 | 89.7 | 90.6 | 91.6 | 92.6 | 93.6 | 94.5 | 9.5 .5 | 96.5 | 97.5 | 98.5 | 99.4 | 100.4 |
| 30.0 | 89.1 | 90.0 | 91.0 | 92.0 | 92.9 | 93.9 | 91.9 | 9.5 .9 | 96.8 | 97.8 | 98.8 | 99.7 |
| 30.2 | 88.5 | 89.1 | 90.4 | 91.4 | 92.3 | 93.3 | 91.3 | 9.5 .2 | 96.2 | 97.2 | 98.1 | 99.1 |
| 30.4 | 87.9 | 88.8 | 89.8 | 90.8 | 91.7 | 92.71 | 93.6 | 91.6 | 9.9 .6 | 96.5 | 97.5 | 98.4 |

When the Barometrical means to be used have been derived from observations taken at such hours of the day as, if combined, do not give the true mean pressure, they must be reduced to the true means by using the Tables XX. and XXI. These tables give the corrections to be applied to the hourly means, in each month, for reducing them to the means which would have been given by observations made at each of the twenty-four hours. The correction for any given set of hours is found by taking the mean of the corrections due to each of the combined hours, paying due attention to the signs. Table XX. has been computed from the hourly observations made under the superintendence of Professor A. D. Bache, at Girard College, Philadelphia. Table XXI. is from the Greenwich Observations, by Glaisher.

## XX.

## Nortif America. - Philadelpila. Lat. $39^{\circ} 53^{\prime} \mathrm{N} . ~ L o n g .75^{\circ} 11^{\prime}$ W. Greemu.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Barometric Pressure of the respective Days, Months, and of the Year.

Barometer in English Inches.

| Hour | Jan. | Feb. | March | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec | Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Iuch. | Inch. -.0099 | Inch. -.007 | In | Iuch |  |  | Inch. |  |  |  |  |  |
| 1 |  |  | -.002 | -. 001 | 03 | +. 00 | 1 | 001 | +.005 | $+.007$ | +.007 | 11 | 7 |
| 2 | -. |  | -. 001 | +.00 | 7 | +.010 | +. 001 | 00.1 | +. 010 | +.011 | +.011 | . 016 | +. 0030 |
| 3 | -.00- | +.002 | 9 | +. | 7 | +. | 3 | 0.5 | +. 009 | +. 011 | +.007 | 4 | 6 |
| 4 | -.00:3 | $+.003$ | +. 0099 |  |  | +. 002 | . 000 | 001 | 005 | +.007 |  | . 010 | +. 0038 |
| 5 | -00.3 | . 000 | $+.002$ | -. 0 | .006 | -. 00 | . 0 | 00 | . 006 | -. 0 | -.006 | -. 008 | -.0050 |
|  | -. 00 | -. 004 | $-.011$ | $-.02$ | 9 | -. 0 | -. 019 | -.017 | -.016 | -. 012 | -.012 | 1.5 | $-.0147$ |
| 7 | -. | 13 |  |  | 6 | -. 0 | 02.5 | -.023 | -. 023 |  | 019 | $-.023$ | -.0222 |
| 8 |  |  |  | -.0: | I | -. 02 | -.02ム | -.026 | 029 | -.030 | S | 029 | -. 0290 |
| 9 | -. 040 | 026 | -.02s | $-.03$ | -.02~ | -. 02 | $-.027$ | -. 0 | 0 | -. 029 | -. 0 | .0:0 | $-.0807$ |
| 10 | $-.0$ | 026 | -. 02 | $-.03$ | -. 021 | -. 02 | $-.026$ | -.030 | $-.029$ | -. 02 | -.038 | 032 | $-.0296$ |
| 11 |  | - | - | -.02:3 | 8 | $-.019$ | -. 019 | ' | -. 021 | -.014 | - -017 | 11 | 55 |
| Noon. |  |  |  | - | 6 | -. 0 | 12 | -. 012 | 009 | $+.001$ | +.006 | $+.005$ | -0037 |
| , |  | +. 017 | +.014 | +. 006 | 005 | . 000 | , 00 | . 000 | +.00. | $+.006$ | + +.023 | $+.024$ | +. 0107 |
| 2 | +. 037 | $+.032$ | +.031 | $+.021$ | 017 | $+.011$ | +.011 | $+.012$ | $+.020$ | +.02- | +.033 | +.031 | +.0240 |
| 3 | +.034 | +. 031 | $+.034$ | +. 03 | $+.028$ | +. 019 | $+.020$ | $+.022$ | $+.024$ | 8 | +.033 | 031 | . 0287 |
| 4 |  | +.032 | + | + | 2 | $+.027$ | + 027 | +.027 |  | 8 | +.027 | 0 | +.0306 |
| s | + | +.021 | +.02. | +.036 | 034 | +.030 | $+.028$ | +.029 | 02\% | . 021 | 01 | 26 | . 0268 |
| 6 | + | +.014 | +. 016 | $+.031$ | $+.027$ | $+.023$ | $+.025$ | $+.02 \mathrm{~S}$ | .023 | +.012 | $+.00 .5$ | 021 | +.0202 |
| 7 | +. 003 | +. 006 | +.007 | +.022 | $+.016$ | +. 018 | $+.021$ | +.018 | $+.016$ | +.001 | -. 00 | 8 | +.0123 |
| 8 |  | . 000 | -.003 | + | +.002 | +. 010 | +.011 | + . 008 | 7 | . 009 | -. 00 | 013 | +. 0040 |
| 9 | -. 002 | -. 008 | -.010 | +.00 | -. 010 | . 000 | +. 00 | +.003 | 1 | -.013 | -.00 | 012 | -. 0027 |
| 10 | -.003 | -. 012 | -. 011 | -. 00 | -. 018 | $-.00$ | -. 00 | . 001 | -. 005 | -. 016 | -. 010 | 08 | -.0065 |
| 11 | $+.002$ | 011 | -. 017 | -. 0 | -. 019 | -. 005 | $-.00$ | $-.002$ | $-.004$ | -. 009 | ,-.003 | 005 | -.0064 |
| 2, 10 | +. 008 | $+.005$ | +.00\% | -. 0 | . $00:$ | -. 00 | -. 0 | . 002 | . 000 | . 000 | $+.00$ | . 009 | +.001 |
| $7,2,9$ | +. 008 | +. 004 | . 000 | -. | $-.00$ | -. |  | -. 003 | . 00 | -. 002 | $+.002$ | $+.005$ | . 000 |
| $9,12,3,9$ | . 000 | $-.001$ | -.001 | - |  |  |  |  |  | -. 003 | -. 001 | +.00;) | . 0 |

Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Barometric Pressure for the respective Months.-Glaisher.

Engliah Inches

| Hours. | Jan. | Feb. | March | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inch. | Inch. | In | Inch. | lnch. | Inc |  | Luch. | Inch. | $\overline{\text { Iuch. }}$ |  | Inch. |  |
| Midn |  |  |  |  |  |  |  |  |  |  | -. 011 |  | . 005 |
| 1 | . 001 | . 004 | . 013 | . 000 | . 002 | . 004 | . 000 | . 000 | . 000 | . 004 | -. 005 | . 001 | . 002 |
| 2 | . 002 | . 008 | . 020 | . 007 | . 004 | . 005 | . 003 | . 007 | . 005 | 010 | . 003 | . 006 | . 007 |
| 3 | . 005 | . 012 | . 023 | . 010 | . 005 | . 004 | . 005 | . 011 | . 010 | . 015 | . 008 | 010 | . 009 |
| 4 | . 011 | . 014 | .022 | . 011 | . 005 | . 001 | . 005 | . 014 | . 012 | . 020 | . 013 | . 012 | . 012 |
| 5 | . 015 | 15 | 19 | . 011 | 96 | -. 002 | . 006 | . 011 | . 014 | .022 | . 016 | . 014 | . 012 |
| 6 | . 015 | . 012 | . 012 | . 006 | . 006 | -.006 | . 002 | . 005 | . 010 | . 018 | . 015 | . 011 | . 009 |
| 7 | . 010 | . 007 | . 005 | -.003 | . 006 | -. 010 | -. 004 | . 000 | . 001 | . 008 | . 010 | . 006 | . 003 |
| 8 | . 003 | . 000 | -. 004 | -.008 |  | -. 012 |  | -. 007 | -. 006 | -. 003 | 03 | 4 | . 003 |
| 9 | -. 003 | -. 008 | -.010 | -. 011 | . 007 | -. 012 | -. 010 | -. 008 | -. 011 | -. 009 | -. 005 | -. 010 | -. 009 |
| 10 | -. 010 | -. 015 | -.015 | -.014 | 09 | -. 011 | -. 010 | -. 009 | -. 013 | -. 014 | -. 007 | -.015 | -. 012 |
| 11 | -. 014 | -.016 | -. 015 | -.011 | -. 006 | -. 009 | -. 009 | -. 008 | -.010 | -. 014 | -. 005 | -. 015 | -. 011 |
| Noon | -. |  | -. | - | 2 | - | -. 006 | 05 | 3 | -. 010 | , | -. 009 | -. 006 |
| 1 | . 002 | -.006 | -. 005 | -. 004 | 000 | -. 003 | -.003 | . 000 | . 000 | -. 003 | . 007 | . 003 | -. 001 |
| 2 | . 005 | 3 | . 000 | . 003 | .003 | 03 | . 001 | . 003 | . 004 | . 004 | 011 | 08 | 004 |
| 3 | . 004 | . 006 | 003 | . 009 | . 006 | . 007 | . 00.5 | . 005 | . 008 | . 005 | . 010 | . 010 | . 006 |
| 4 | . 002 | 08 | . 00.5 | . 004 | . 010 | . 013 | . 009 | . 009 | . 010 | . 003 | . 008 | 09 | 007 |
| 5 | .000 | 96 | 04 | 14 | . 014 | 17 | 13 | . 011 | . 011 | . 000 | . 004 | . 006 | . 008 |
| 6 | -.003 | .002 | . 000 | . 011 | . 015 | . 017 | .013 | . 011 | . 006 | -.005 | . 000 | . 002 | . 006 |
| 7 | -. 00 | -.004 | -. 006 | -.007 | . 010 | . 014 | . 010 | . 005 | . 000 | -. 008 | -. 006 | -.003 | . 000 |
| 8 | -. |  |  | -. 005 | 00 | . 008 | - | - | -. 005 | -. 011 | -. 012 | -. 006 | -. 005 |
| 9 | -. 0 | -.009 | -. 0 | -. | -. 006 | . 003 | -. 001 | -. 010 | 09 | -. 014 | -. 017 | -. 0.9 | -. 008 |
| 10 | -. | -. 007 | -. 012 | -. | -.008 | -.002 | - | - | -. 011 | -. 012 | -. 019 | -.010 | -.010 |
| 11 | -. 004 | -.009 | -. 010 | -. 012 | -. 008 | -. 002 | -.012 | -.015 | -. 011 | -. 009 | -. 017 | -. 009 | -. 009 |
| 6. 6 | . 006 | 7 | 6 | . 008 | . 011 | . 005 | S | . 008 | . 008 | . 006 | . 007 | . 006 | . 008 |
| 7. 7 | 02 | 2 | . 000 | -. 005 | . 008 | . 002 | .003 | . 002 | . 000 | . 000 | . 002 | .02 | . 001 |
| 8. 8 | -.002 | 03 | -. 008 | -. 006 | .002 | 02 | 2 | -. 006 | -. 006 | -. 007 | -.004 | -. 001 | -. 004 |
| 99 | -. 007 | . 000 | -.013 | -. 010 | -. 006 | -. 004 |  |  | , | -. 012 | 1 | -. 009 | -. 009 |
| 10.10 | -. 007 | -. 011 | -. 011 | -.013 | -. 009 | -. 006 | -. 007 | -. 012 | . 012 | -.013 | -.013 | -. 012 | -. 011 |
| 7. 2. 9 | . 003 | . 001 | -.003 | -.003 | . 001 | -. 001 | -. 001 | -. 002 | -. 001 | -.001 | . 001 | . 002 | . 001 |
| 6. 28 | . 005 | 003 | . 000 | . 001 | . 003 | . 002 | . 002 | . 001 | 003 | . 004 | . 005 | . 00 | . 003 |
| 6. 210 | 5 | . 003 | 00 | -. 001 | . 000 | -. 002 | -. 001 | -.002 | . 001 | . 003 | . 002 | . 003 | . 001 |
| 6. 2: 6 | .006 | . 006 | . 004 | . 007 | . 008 | -. 005 | . 005 | . 006 | . 007 | . 006 | . 009 | . 007 | . 006 |
| 7. 2 | . 007 | . 005 | . 003 | . 000 | . 004 | -. 001 | -. 001 | . 002 | .002 | .006 | . 010 | . 007 | . 003 |
| 8. 2 | . 004 | . 002 | -.002 | -.002 | . 003 | -. 004 | -. 003 | -. 002 | -. 001 | . 000 | . 007 | . 006 | . 001 |
| 8. 1 | . 002 | -. 003 | -.004 | -006 | . 001 | -. 007 | -. 006 | -. 003 | -. 003 | -. 003 | . 00.5 | . 003 | -. 002 |
| 1 | . 006 | . 001 | . 000 | -.003 | . 003 | -.006 | -. | . 000 | .00 | . 00 | . 008 | . 004 | . 001 |
| 9.12.3.9 | -. 004 | -.00.5 | -. 008 | -. 005 | -.002 | -. 002 | 3 | -. 004 | -. 004 | -. 007 | -. 002 | . 004 | -. 004 |

The numbers without sign must be added: those with the sign - must be subtracted.

# XXII. TABLE TO REDUCE, BY INTERPOLATION, 

THE OBSERVATIONS TO THE SAME ABSOLUTE TIME.

## DECIMALS OF AN HOUR.

| Min. | Decimal. | Min. | Decimal. | Min. | Decimal. | Min. | Decimal. | Min. | Decimal. | Min. | Decimal. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | .017 | 11 | .183 | 21 | .350 | 31 | .517 | 41 | .683 | 51 | .850 |
| 2 | .033 | 12 | .200 | 22 | .367 | 32 | .533 | 42 | .700 | 52 | .867 |
| 3 | .050 | 13 | .217 | 23 | .383 | 33 | .550 | 43 | .717 | 53 | .583 |
| 4 | .067 | 14 | .233 | 24 | .400 | 34 | .567 | 44 | .733 | 54 | .900 |
| 5 | .053 | 15 | .250 | 25 | .417 | 35 | .583 | 45 | .750 | 55 | .917 |
| 6 | .100 | 16 | .267 | 26 | .433 | 36 | .600 | 46 | .767 | 56 | .933 |
| 7 | .117 | 17 | .283 | 27 | .450 | 37 | .617 | 47 | .783 | 57 | .950 |
| 8 | .133 | 18 | .300 | 28 | .467 | 38 | .633 | 48 | .800 | 58 | .967 |
| 9 | .150 | 19 | .317 | 29 | .483 | 39 | .650 | 49 | .817 | 59 | .983 |
| 10 | .167 | 20 | .333 | 30 | .500 | 40 | .667 | 50 | .833 | 60 | 1000 |

## Table for Correction of Curvature and Refraction.

From a mountain, when furnished with a barometer, or with an apparatus for determining the temperature of boiling water, and a pocket level, an observer can find the elevations of distant points, which are in sight, but lower than the mountain itself on which he stands. He has only to seek, with the level, the point on the slope of the mountain which corresponds to the point at a distance that he wishes to determine, and to take there a barometrical, or a boiling point observation. This observation is to be calculated in the usual way, but the result must be corrected for the curvature of the surface of the globe, and for the atmospheric refraction, by means of the following Table.

This method, which furnishes the means of multiplying, without much trouble, the measurements of heights, gives approximations which are sufficient for most of the purposes of Physical Geography. It may even seem preferable to direct measurements for determining the mean elevation of certain physical lines, which are best estimated when seen from a distance; such as the :opper limit of the growth of trees, the limits of different kinds of vegetation, that of permanent snow, that of the mean elevation of the crest of a mountain range, \&c.
'rable XXIII. is taken from Captain Lee's Collection of Tables and Formula, 2 d edit., page 81.

D

Showing the Difference of the Apparent and True Level, in feet and decimals, for Distances in feet and miles.

| Distances in Feet. | Correction in Feet. |  |  | Distances in Miles. | Correction in Feet. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | For Curvature. | For Re. fraction. | For Curva. ture and Refraction. |  | For Curvature. | For Refraction. | For Curvature and Refraction. |
| 100 | . 00024 | . 00004 | . 00020 | $\frac{1}{4}$ | . 0417 | . 0060 | . 0357 |
| 150 | . 00054 | . 00008 | . 00046 | $\frac{1}{2}$ | . 1668 | . 0238 | . 1430 |
| 200 | . 00094 | . 00013 | . 00083 | ${ }_{4}^{3}$ | .3752 | . 0536 | . 3216 |
| 250 | . 00149 | . 00021 | . 00128 | 1 | . 6670 | . 0953 | . 5717 |
| 300 | . 00215 | . 00031 | . 00184 | $1 \frac{1}{2}$ | 1.5008 | . 2144 | 1.2864 |
| 330 | . 00293 | . 00042 | . 00251 | 2 | 2.6680 | . 3811 | 2.2869 |
| 400 | . 00383 | . 00055 | . 00328 | $2 \frac{1}{2}$ | 4.1688 | . 5955 | 35733 |
| 450 | . 00484 | . 00069 | . 00415 | 3 | 6.0030 | . 8561 | 5.1469 |
| 500 | . 00598 | . 00085 | . 00513 | $3 \frac{1}{2}$ | 8.1708 | 1.1673 | 7.0035 |
| 550 | .00724 | . 00103 | . 00621 | 4 | 10.6720 | 1.5246 | 9.1474 |
| 600 | . 00861 | . 00123 | . 00738 | $4 \frac{1}{2}$ | 13.5468 | 1.9295 | 11.5773 |
| 650 | . 01010 | . 00144 | . 00866 | 5 | 16.6750 | 2.3821 | 14.2929 |
| 700 | . 01172 | . 00167 | . 01005 | $5 \frac{1}{2}$ | 20.1769 | 2.8824 | 17.2945 |
| 750 | . 01345 | . 00192 | . 01153 | 6 | 24.0120 | 3.4303 | 20.5817 |
| 800 | . 01531 | . 00219 | . 01312 | $6 \frac{1}{2}$ | 28.1809 | 4.0258 | 24.1551 |
| 850 | . 01728 | . 00247 | . 01481 | 7 | 32.6830 | 4.6690 | 28.0143 |
| 900 | . 01938 | . 00277 | . 01661 | $7 \frac{1}{2}$ | 37.5190 | 5.3599 | 32.1591 |
| 950 | . 02159 | . 00308 | . 01851 | S | 42.6880 | 6.0997 | 36.5883 |
| 1000 | . 02392 | . 00333 | . 02059 | $8 \frac{1}{2}$ | 48.1910 | 6.8844 | 413066 |
| 1050 | . 02638 | . 00377 | . 02261 | 9 | 54.0270 | 7.7181 | 46.3089 |
| 1100 | . 02895 | .00414 | . 02481 | $9 \frac{1}{2}$ | 60.1971 | 8.5996 | 51.5975 |
| 1150 | .03164 | . 00452 | . 02712 | 10 | 66.7000 | 9.5286 | 57.1714 |
| 1200 | . 03445 | . 00492 | . 02953 | 11 | 80.7070 | 11.5296 | 69.1774 |
| 1250 | . 03738 | .00.534 | . 03204 | 12 | 96.0480 | 13.7211 | 82.3269 |
| 1300 | . 04043 | . 00578 | . 03465 | 13 | 112.7230 | 16.1033 | 96.6197 |
| 1350 | . 04361 | . 00623 | . 03738 | 14 | 130.7320 | 18.6760 | 112.0 .560 |
| 1400 | . 04659 | .00670 | . 04019 | 15 | 150.0750 | 21.4393 | 128.63.77 |
| 1450 | . 05030 | . 00719 | . 04311 | 16 | 170.7520 | 24.3931 | 116.3 .589 |
| 1500 | . 05383 | . 00769 | . 04614 | 17 | 192.7630 | 27.5376 | 165.22.54 |
| 1550 | . 05748 | . 00821 | . 04927 | 18 | 216.1086 | 30.8727 | 185.2359 |
| 1600 | . 06125 | . 00875 | . 0.5250 | 19 | 240.7870 | 34.3981 | 206.3889 |
| 1650 | . 06514 | . 00931 | . 05583 | 20 | 266.8000 | 38.1143 | 228.6557 |
| 1700 | . 06914 | . 00988 | . 05926 |  |  |  |  |
| 1750 . | . 07327 | . 01047 | . 06280 |  |  |  |  |
| 1800 | . 07752 | . 01107 | . 06645 |  |  |  | . |
| 1850 | . 08188 | . 01170 | . 07018 |  |  |  |  |
| 1900 | . 08637 | . 01234 | . 07403 |  |  |  |  |
| 1950 | . 09098 | . 01300 | . 07798 |  |  |  |  |
| 2000 | . 09570 | . 01367 | . 08203 |  |  |  |  |
|  |  |  |  |  |  |  |  |

## THERM0METRICAL

# MEASUREMENT OF HEIGHTS, 

or

## TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM OBSERVATIONS OF THE TEMPERATURE OF BOILING WATER.

# TIIERMOMETRICAL MEASUREMENT OF HEIGHTS. 

TABLES

FOR DEDUCING DIFFERENCES OF LEVEL FROM THE TFMPERATURE OF TIIE
BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of the vapors produced from it gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam cscapes rapidly in large bubbles, and the water boils. The temperature at which, in the open air, water boils, thus depends upon the weight of the atmospheric column above it, and under a less barometrie pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the higher the station where an observation is taken, the lower the temperature at which water boils at that station will be.

The difference of elevation between two places, therefore, can be deduced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and, the atmospheric pressures at both places being known, to compute the difference of level by a formula, or by the tables given above for computing heights from barometrical observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deluced from barometrical observations. Both derive the difference of altitudc from the difference of atmospheric pressure. But the temperature of boiling water gives only indirectly the atmospheric pressure, which is given dircctly by the barometer. This method is thus liable to all the chances of error which may affect the measurements by means of the barometer, besides adding to them new ones peculiar to itself, the prineipal of which, not to speak of the differences exhibited in the various tables of the foree of vapor, is the diffieulty of ascertaining with the necessary aecuracy the true temperature of boiling water. In the present state of thermometry it would hardly be safe, indeed, 10 answer, in the most favorable cireumstanees, for quantities so small as hundredths of degrees, even when the thermometer has been constructed with the utmost care ; moreover, the quality of the glass of the instrumen, the form and the substance of the vessel containing the water, the nature of the water itself, the place at which the butb of the thermometer is placed, whether in the current of steam or in the water, --- all these cireumstances canse no inconsidemble variations to take place in the indications of thermometers observed under the same atmospheric
pressure. Owing to these various causes, an observation of the boiling point, differing by one tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one tenth of a degree Centigrade in the temperature of boiling water would canse an error of $\Omega$ millimetres in the barometric pressure, or of from 70 to 80 feet in the final result, white with a good barometer the error of pressure will hardly ever exceed one tenth of a millimetre, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer, or thermobarometer, is of the greatest utility to travellers traversing distant or rough countries, on account of its being more conveniently transporterl, and much less liable to accidents than the mereurial barometer. The best form for it is that contrived and deseribed by Regnault in the Amales de Chimie et de Physique, Tom. XIV. p. 202. It consists of an aceurate thermometer with long degrecs, subdivided into tenths, whose bulb is placed, about $\mathfrak{2}$ or $\mathbf{3}$ centimetres above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp. The whole instrument when closed is about 6 inches long; when drawn out for observation, about 14 inches.

Table XXIV. of barometric pressures corresponding to temperatures of boiling water, has been calculated by Regnault from his Tables of Forces of Vapor, and published in the Amales de Chimie et de Physique, Tom. XIV. p. $\approx 00$. It gives, in millimetres of mercury, the barometric pressures corresponding to every tenth of a Centigrade degree ; for greater convenience, the values for every hundredth have been added.

The accuracy of this table has been tested by dircet observation by Mr. Wisse, a traveller competent in such matters, who noted down simultancously the temperatures of the boiling point of water and the height of the barometer, in various parts of the Andes, up to the summit of the voleano of Pichincha, ineluding in his observations barometrical pressures ranging from 752 to 430 millimetres of mercury. The agreement between the barometric pressures given here by Regnault and those found by Wisse are very satisfactory, the differences never exceeding a few tenths of a millimetre. See Annales de Chimie et de Physique, Tom. XXVIII. p. $1 \supseteq 3$.

Table XXV. is the same table, revised by A. Moritz, who, in a communication to the Académie des Sciences, in October, 1856, called the attention to some slight errors of computation in Regnault's table, and gave the corrected numbers for every whole degree from $40^{\circ}$ to $102^{\circ}$ Centigrade. Those numbers are given here from E $0^{\circ}$ upwards, as published in the Journal de l'Institut; the values for every tenth of a degree, and their differences, bave been computed to fit the table for practical use. The comparison of the two tables will show that the corrections mostly amount to a few hundredths, and never exceed one tenth of a millimetre.

Table XXVl. is table XXV. reduced to English measures.
XXIV. BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF BOILING WATER. I

| Centig. <br> Degrees. | Hundredths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| - | Millim. | Nillim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. |
| 8.5 .0 | 433.04 | 433.21 | 433.38 | 433.55 | 433.72 | 433.69 | 434.07 | 434.24 | 434.41 | 434.58 |
| 85.1 | 434.75 | 434.92 | 435.09 | 43.5 .26 | 435.43 | 435.60 | 43.5 .78 | 435.95 | 436.12 | 436.29 |
| 8.5.2 | 436.46 | 436.63 | 436.80 | 436.97 | 437.14 | 437.31 | 437.49 | 437.66 | 437.83 | 438.00 |
| 85.3 | 438.17 | 438.34 | 438.51 | 438.69 | 438.56 | 439.03 | 439.20 | 439.37 | 439.55 | 439.72 |
| 85.4 | 439.59 | 440.06 | 440.23 | 440.41 | 440.58 | 440.75 | 440.93 | 441.10 | 441.27 | 441.45 |
| 83.5 | 441.62 | 441.79 | 441.97 | 442.14 | 142.31 | 442.48 | 442.66 | 442.83 | 443.00 | 443.18 |
| 85.6 | 443.35 | 433.52 | 443.70 | 443.87 | 44.05 | 44.22 | 44.39 | 4457 | 44.74 | 444.92 |
| 85.7 | 445.09 | 445.26 | 445.44 | 445.61 | 445.79 | 445.96 | 446.14 | 446.31 | 446.49 | 446.67 |
| 85.8 | 446.84 | 447.01 | 447.19 | 447.36 | 447.54 | 447.71 | 447.89 | 448.06 | 448.24 | 448.41 |
| 85.9 | 448.59 | 448.76 | 488.94 | 449.11 | 449.29 | 449.46 | 449.64 | 449.81 | 449.99 | 450.16 |
| 86.0 | 450.34 | 450.52 | 4.50 .69 | 450.87 | 451.04 | 451.22 | 451.40 | 451.57 | 451.75 | 451.92 |
| 86.1 | 452.10 | 452.28 | 452.45 | 452.63 | 452.81 | 452.98 | 453.16 | 453.34 | 453.52 | 453.69 |
| 86.2 | 453.87 | 454.05 | 454.22 | 454.40 | 454.58 | 454.75 | 454.93 | 455.11 | 455.29 | 455.46 |
| 86.3 | 455.64 | 45.5 .82 | 456.00 | 456.17 | 456.35 | 456.53 | 456.71 | 456.89 | 457.06 | 457.24 |
| 86.4 | 457.42 | 457.60 | 457.78 | 457.96 | 458.14 | 458.31 | 458.49 | 458.67 | 458.85 | 4.59 .03 |
| 86.5 | 459.21 | 459.39 | 459.57 | 459.75 | 459.93 | 460.10 | 460.28 | 460.46 | 460.64 | 460.82 |
| 86.6 | 461.00 | 461.18 | 461.36 | 461.54 | 461.72 | 461.90 | 462.08 | 462.26 | 462.44 | 462.62 |
| 86.7 | 462.80 | 46298 | 463.16 | 463.34 | 463.52 | 463.70 | 463.88 | 464.06 | 464.24 | 164.42 |
| 86.8 | 464.60 | 464.78 | 464.96 | 465.14 | 465.32 | 465.50 | 465.69 | 465.87 | 466.05 | 466.23 |
| 86.9 | 466.41 | 466.59 | 466.77 | 466.95 | 467.13 | 467.31 | 467.50 | 467.68 | 467.86 | 465.04 |
| 87.0 | 468.22 | 468.40 | 468.58 | 468.77 | 468.9.5 | 469.13 | 469.31 | 469.49 | 469.68 | 469.86 |
| 87.1 | 470.01 | 470.22 | 470.41 | 470.59 | 470.77 | 470.95 | 471.14 | 471.32 | 471.50 | 471.69 |
| 87.2 | 471.87 | 472.05 | 472.24 | 472.42 | 472.60 | 472.78 | 472.97 | 473.15 | 473.33 | 473.52 |
| 87.3 | 473.70 | 473.88 | 474.07 | 174.25 | 474.44 | 474.62 | 474.50 | 474.99 | 475.77 | 47.5 .36 |
| 87.4 | 475.54 | 475.72 | 475.91 | 476.09 | 476.28 | 476.46 | 476.64 | 476.83 | 477.01 | 477.20 |
| 87.5 | 477.38 | 477.56 | 477.75 | 477.93 | 479.12 | 478.30 | 478.49 | 478.67 | 478.86 | 479.04 |
| 87.6 | 479.23 | 479.41 | 479.60 | 479.78 | 479.97 | 450.15 | 450.34 | 480.52 | 480.71 | 480.89 |
| 87.7 | 481.08 | 481.27 | 481.45 | 481.64 | 481.82 | 482.01 | 482.20 | 48238 | 482.57 | 482.75 |
| 57.8 | 452.94 | 453.13 | 483.31 | 483.50 | 483.69 | 183.57 | 484.06 | 484.2. | 484.44 | 484.62 |
| 87.9 | 484.81 | 485.00 | 485.19 | 485.37 | 485.56 | 485.75 | 485.94 | 486.13 | 486.31 | 486.50 |
| 85.0 | 486.69 | 486.58 | 487.07 | 487.2.5 | 487.44 | 487.63 | 487.82 | 488.01 | 498.19 | 488.38 |
| 88.1 | 485.57 | 488.76 | 188.9.7 | 489.13 | 489.32 | 489.51 | 489.70 | 489.89 | 490.07 | 490.26 |
| 88.2 | 490.45 | 490.64 | 490.83 | 491.02 | 491.21 | 491.39 | 491.58 | 491.77 | 491.96 | 192.15 |
| 88.3 | 492.34 | 492.53 | 492.72 | 492.91 | 493.10 | 493.29 | 493.48 | 493.67 | 493.86 | 494.0 .5 |
| 88.4 | 494.24 | 49.43 | 494.62 | 494.81 | 495.00 | 495.19 | 495.39 | 495.58 | 49.5 .77 | 495.96 |
| 88.5 | 496.15 | 496.34 | 496.53 | 496.72 | 496.91 | 497.10 | 497.30 | 497.49 | 497.68 | 497.87 |
| 88.6 | 49806 | 498.25 | 498.44 | 498.64 | 498.83 | 499.02 | 499.21 | 499.40 | 499.60 | 499.79 |
| 88.7 | 499.98 | 500.17 | 500.36 | 500.56 | 500.75 | 500.94 | 501.13 | 501.32 | 501.52 | 501.71 |
| 88.8 | 501.90 | 502.09 | 502.28 | 502.48 | 502.67 | 502.56 | 503.0.) | 503.24 | 503.44 | 503.63 |
| 88.9 | 503.82 | 504.01 | 504.21 | 504.40 | 504.60 | 504.79 | 504.98 | 505.18 | 50.5 .37 | 505.57 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

2 barometric pressures corhesponding to temperatures of boaling water

| Centig. <br> Degrees. | Hundredths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 9, | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millim. | Millin. | Millim. |
| 89.0 | 505.76 | 505.95 | 506.15 | 506.34 | 506.54 | 506.73 | 506.92 | 507.12 | 507.31 | 507.51 |
| 89.1 | 507.70 | 507.89 | 508.09 | 505.28 | 508.48 | 508.67 | 508.87 | 509.06 | 509.26 | 509.45 |
| 89.2 | 509.65 | 509.84 | 510.04 | 510.23 | 510.43 | 510.62 | 510.52 | 511.01 | 511.21 | 511.40 |
| 89.3 | 511.60 | 511.80 | 511.99 | 512.19 | 512.38 | 512.58 | 512.78 | 512.97 | 513.17 | 513.36 |
| 89.4 | 513.56 | 513.76 | 513.95 | 514.15 | 514.35 | 514.54 | 514.74 | 514.94 | 515.14 | 515.33 |
| 89.5 | 515.53 | 515.73 | 515.92 | 516.12 | 516.32 | 516.51 | 516.71 | 516.91 | 517.11 | 517.30 |
| 89.6 | 517.50 | 517.70 | 517.90 | 518.09 | 518.29 | . 518.49 | 518.69 | 518.89 | 519.08 | 519.28 |
| 89.7 | 519.48 | 519.68 | 519.88 | 520.07 | 520.27 | 520.47 | 520.67 | 520.87 | 521.06 | 521.26 |
| 89.8 | 521.46 | 521.66 | 521.86 | 522.06 | 522.26 | 522.46 | 522.66 | 522.86 | 523.05 | 523.25 |
| 89.9 | 523.45 | 523.65 | 523.85 | 524.05 | 524.25 | 524.45 | 524.65 | 524.85 | 525.05 | 52.5 .25 |
| 90.0 | 525.45 | 525.65 | 525.85 | 526.05 | 526.25 | 526.45 | 526.65 | 526.85 | 527.05 | 527.25 |
| 90.1 | 527.45 | 527.65 | 527.8.5 | 528.05 | 528.25 | 528.45 | 528.66 | 528.86 | 529.06 | 529.26 |
| 90.2 | 529.46 | 529.66 | 529.86 | 530.07 | 530.27 | 530.47 | 530.67 | 530.87 | 531.08 | 531.28 |
| 90.3 | 531.48 | 531.68 | 531.85 | 532.09 | 532.29 | 532.49 | 532.69 | 532.89 | 533.10 | 533.30 |
| 90.4 | 533.50 | 533.70 | 533.91 | 534.11 | 534.31 | 534.51 | 534.72 | 534.92 | 535.12 | 535.33 |
| 90.5 | 535.53 | 535.73 | 535.94 | 536.14 | 536.35 | 536.55 | 536.75 | 536.96 | 537.16 | 537.37 |
| 90.6 | 537.57 | 537.77 | 537.98 | 538.18 | 538.39 | 538.59 | 538.79 | 539.00 | 539.20 | 539.41 |
| 90.7 | 539.61 | 539.81 | 540.02 | 540.22 | 540.43 | 540.63 | 540.84 | 541.04 | 541.25 | 541.45 |
| 90.8 | 541.66 | 541.87 | 542.07 | 542.28 | 542.48 | 542.69 | 542.90 | 543.10 | 543.31 | 543.51 |
| 90.9 | 513.72 | 543.93 | 544.13 | 544.34 | 544.54 | 541.75 | 544.96 | 545.16 | 545.37 | 545.57 |
| 91.0 | 545.78 | 545.99 | 546.19 | 546.40 | 546.61 | 546.8] | 547.03 | 547.23 | 547.44 | 547.61 |
| 91.1 | 547.85 | 548.06 | 548.26 | 548.47 | 548.68 | 548.88 | 549.09 | 549.30 | 549.51 | 549.71 |
| 91.2 | 549.92 | 550.13 | 550.34 | 5.50 .54 | 550.75 | 550.96 | 551.17 | 551.38 | 551.58 | 551.79 |
| 91.3 | 552.00 | 552.21 | 552.42 | 552.63 | 552.84 | 553.04 | 553.25 | 553.46 | 553.67 | 553.88 |
| 91.4 | 554.09 | 554.30 | 554.51 | 554.72 | 554.93 | 5.55 .14 | 555.35 | 555.56 | 555.77 | 555.98 |
| 91.5 | 556.19 | 556.40 | 556.61 | 5.56 .82 | 5.57.03 | 5.57 .24 | 557.45 | 557.66 | 557.87 | 558.08 |
| 91.6 | 558.29 | 558.50 | 5.58 .71 | 558.92 | 559.13 | 559.34 | 559.55 | 559.76 | 559.97 | 560.18 |
| 91.7 | 560.39 | 560.60 | 560 sl | 561.03 | 561.24 | 561.45 | 561.66 | 561.87 | 562.09 | 562.30 |
| 91.8 | 562.51 | 562.72 | 562.93 | 563.15 | 563.36 | 563.57 | 563.78 | 563.99 | 564.21 | 564.42 |
| 91.9 | 564.63 | 564.86 | 565.06 | 565.27 | 565.48 | 565.69 | 565.91 | 566.12 | 566.33 | 566.55 |
| 92.0 | 566.76 | 566.97 | 567.19 | 567.40 | 567.61 | 567.85 | 568.04 | 568.25 | 568.46 | 568.68 |
| 92.1 | 568.89 | 569.10 | 569.32 | 569.53 | 569.75 | 569.96 | 570.17 | 570.39 | 570.60 | 570.82 |
| 92.2 | 571.03 | 571.24 | 571.46 | 571.67 | 571.89 | 572.10 | 572.32 | 572.53 | 572.75 | 572.96 |
| 92.3 | 573.18 | 573.40 | 573.61 | 573.83 | 574.04 | 574.26 | 574.48 | 571.69 | 574.91 | 575.12 |
| 92.4 | 575.34 | 575.56 | 575.77 | 575.99 | 576.20 | 576.42 | 576.64 | 576.85 | 577.07 | 577.28 |
| 92.5 | 577.50 | 577.72 | 577.93 | 578.15 | 578.37 | 578.58 | 578.80 | 579.02 | 579.24 | 579.45 |
| 92.6 | 579.67 | 579.89 | 550.10 | 580.32 | 580.54 | 580.75 | 580.97 | 581.19 | 581.41 | 581.62 |
| 92.7 | 581.84 | 582.06 | 582.28 | 582.49 | 582.71 | 582.93 | 583.15 | 583.37 | 583.58 | 583.80 |
| 92.8 | 584.02 | 584.24 | 584.46 | 584.65 | 584.90 | 58.5 .11 | 555.33 | 585.55 | 58.577 | 585.99 |
| 92.9 | 586.21 | 586.43 | 586.65 | 586.87 | 587.09 | 587.31 | 587.53 | 587.75 | 557.97 | 588.19 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |


| Centig.Degrees. | Hundredths of a Degree. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 93.0 | Slillim. | Tiillim. | Nillim. 505.85 | Inllim. | $\begin{aligned} & \text { Millim. } \\ & 589.29 \end{aligned}$ | Millim. 589.51 | $\begin{aligned} & \text { Millim. } \\ & 589.73 \end{aligned}$ | $\begin{aligned} & \text { Millim. } \\ & 5 \$ 9.9 . \end{aligned}$ | Millim. 590.17 | Millim. 590.39 |
| 93.0 | 508.41 | $5=5.63$ | 553.55 | 589.07 | $589.29$ | 589.51 | 5s9.73 | 559.95 |  |  |
| 93.1 | 590.61 | 590.83 | 591.05 | 591.27 | 591.49 | 591.71 | 591.94 | 59.16 | 592.38 | 592.60 |
| 93.2 | 592.52 | 593.04 | 593.26 | 593.49 | 593.71 | 593.93 | 594.15 | 594.37 | 594.60 | 594.82 |
| 93.3 | 59.04 | 595.26 | 595.43 | 595.71 | 595.93 | 596.15 | 596.37 | 59659 | 596.82 | 597.04 |
| 93.4 | 597.26 | 597.48 | 597.71 | 597.93 | 598.15 | 598.37 | 598.60 | 598.52 | 599.04 | 599.27 |
| 93.5 | 599.49 | 599.71 | 599.94 | 600.16 | 600.38 | 600.60 | 600.83 | 601.05 | 601.27 | 601.50 |
| 93.6 | 601.72 | 601.94 | 602.17 | 602.39 | 602.62 | 602.84 | 603.07 | 603.29 | $603 . \mathrm{T}$ 2 | 603.74 |
| 93.7 | 603.97 | 604.19 | 604.42 | 604.64 | 604.37 | 605.09 | 605.32 | 605.54 | 605.74 | 60.5 .99 |
| 93.3 | 606.22 | 606.45 | 606.67 | 606.90 | 607.12 | 607.3.5 | 607.55 | 607.50 | 605.03 | 608.25 |
| 93.9 | 605.45 | 605.71 | 603.93 | 609.16 | 609.35 | 609.61 | 609.84 | 610.06 | 610.29 | 61051 |
| 94.0 | 610.74 | 610.97 | 611.19 | 611.42 | 611.65 | 611.57 | 612.10 | 612.33 | 612.56 | 612.78 |
| 94.1 | 613.01 | 613.24 | 613.47 | 613.69 | 613.92 | 614.15 | 614.38 | 614.61 | 614.83 | 615.06 |
| 94.2 | 61.5 .29 | 61.5 .52 | 615.75 | 615.97 | 616.21 | 616.43 | 616.66 | 616.89 | 617.12 | 617.35 |
| 94.3 | 617.58 | 617.51 | 618.04 | 618.27 | 618.50 | 615.72 | 618.95 | 619.18 | 619.41 | 619.64 |
| 94.4 | 619.57 | 620.10 | 620.33 | 620.56 | 620.79 | 621.02 | 621.25 | 621.48 | 621.71 | 621.94 |
| 94.5 | 62.17 | 622.40 | 622.63 | 62.2 .86 | 623.09 | 623.32 | 623.56 | 623.79 | 624.02 | 624.2.5 |
| 94.6 | 624.45 | 624.71 | 62.94 | 625.17 | 62.5 .40 | 625.63 | 62.5 .87 | 626.10 | 626.33 | 626.56 |
| 94.7 | 626.79 | 627.02 | 627.25 | 627.49 | 627.72 | 62795 | 628.18 | 628.41 | 628.6 .5 | 628.88 |
| 94.5 | 629.11 | 629.34 | 629.58 | 629.81 | 630.04 | 630.27 | 630.51 | 630.74 | 630.97 | 631.21 |
| 94.9 | 631.44 | 631.67 | 631.91 | 632.14 | 632.35 | 632.61 | 63.34 | 633.08 | 633.31 | 633.5.5 |
| 95.0 | 633.78 | 634.01 | 634.25 | 634.48 | 634.72 | 634.9.5 | 635.18 | 635.42 | 635.65 | 635.89 |
| 9.9 .1 | 636.12 | 636.3.) | 636.59 | 6:36.82 | 637.06 | 637.29 | 637.53 | 637.76 | 638.00 | 638.23 |
| 9.92 | 635.47 | 635.71 | 638.94 | 639.18 | 639.41 | 639.65 | 639.89 | 640.12 | 640.36 | 640.59 |
| 95.3 | 640.83 | 641.07 | 641.30 | 641.54 | 641.77 | 642.01 | 642.25 | 64248 | 642.72 | 642.95 |
| 95.4 | 643.19 | 643.4: | 643.67 | 643.90 | 644.14 | 644.38 | 644.62 | 644.86 | 645.09 | 645.33 |
| 95.5) | 64.5 .57 | 645.81 | 646.05 | 646.28 | 646.52 | 646.76 | 647.00 | 647.24 | 647.47 | 647.71 |
| 9.5 | 647.95 | 645.19 | 645.43 | 648.697 | 645.91 | 649.14 | 649.39 | 649.62 | 649.86 | 6.50 .10 |
| 95.7 | 6.50 .34 | 650.58 | 6.50 .52 | 6.51 .06 | 6.51 .30 | $6.31 . .38$ | 6.51 .77 | 652.0] | 6.52 .25 | 6.52 .49 |
| 95.8 | 6.52 .73 | 6.52 .97 | 6.33 .21 | 6.53.4.3 | 653.69 | 653.93 | 654.17 | 6.54.41 | 654.65 | 654.89 |
| 95.9 | 65.5 .13 | 6.55 .37 | 6.55 .61 | 655.5 .5 | 656.09 | 6.56 .33 | 656.58 | 656.s2 | 657.06 | 657.30 |
| 96.0 | 6.57 .54 | 6.37 .78 | 6.58 .02 | 658.26 | 6.58 .50 | 658.74 | 6.58 .99 | 6.99 .23 | 659.47 | 659.71 |
| 96.1 | 6.59 .95 | 660.19 | 66043 | 660.63 | 660.92 | 661.16 | 661.40 | 661.64 | 661.89 | 662.13 |
| 96.2 | 66.37 | 662.61 | 662.56 | 663.10 | 663.34 | 663.58 | 663.53 | 664.07 | 664.31 | 664.56 |
| 96.3 | 664.50 | 655.04 | 66.29 | 66.5 .53 | 665.7s | 666.02 | 666.26 | 666.51 | 666.75 | 667.00 |
| 96.4 | 667.24 | 667.48 | 667.73 | 667.97 | 668.22 | 668.16 | 668.71 | 665.95 | 669.20 | 669.44 |
| 96.5 | 669.69 | 669.93 | 670.18 | 670.42 | 670.67 | 670.91 | 671.16 | 671.10 | 671.65 | 671.99 |
| 96.6 | 67.14 | 672.39 | 672.63 | 672.58 | 673.12 | 673.37 | 673.62 | 67386 | 674.11 | 674.35 |
| 967 | 674.60 | 674.55 | 675.09 | 675.34 | 675.59 | 675.83 | 676.08 | 676.33 | 676.58 | 676.82 |
| 96.8 | 677.07 | 677.32 | 677.57 | 677.81 | 675.06 | 675.31 | 675.56 | 678.81 | 679.05 | 679.30 |
| 96.9 | 679.55 | 679.80 | $6 \times 0.05$ | 650.29 | $650 . \overline{4}$ | 680.79 | 681.04 | 681.29 | 681.53 | 681.78 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | $\%$ \% | 8. | 9. |

f barometric pressures corresponding to temperatures of bolling water.


## TABLE XXV.

BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF THE BOILING POINT OF WATER,

EXPRESSED IN MILLIMETRES OF MERCURY FOR CENTIGRADE TEMPERATURES.

By Regnallt, Revised by Moritz.

| Boiling Point, Centigrade. | $\begin{gathered} \text { Barometer } \\ \text { in } \\ \text { Millimetres. } \end{gathered}$ | Difference. | Boiling Point, Centigrade | $\begin{gathered} \text { Barometer } \\ \text { in } \\ \text { Millimetres. } \end{gathered}$ | Difference. | Boiling Point, Centigrade. | $\begin{gathered} \text { Barometer } \\ \text { in } \\ \text { nillimetres. } \end{gathered}$ | Difference. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ |  |  | $\bigcirc$ |  |  | - |  |  |
| 80.0 | 354.62 |  | 83.0 | 400.07 |  | 86.0 | 450.30 |  |
| 80.1 | 3.56 .06 | 1.44 | 83.1 | 401.66 | 1.60 | 86.1 | 452.06 | 1.76 |
| 80.2 | 357.50 | 1.45 | 83.2 | 403.26 | 1.60 | 86.2 | 4.53.83 | 1.77 |
| 80.3 | 3.58 .96 | 1.45 | 83.3 | 404.87 | 1.61 | 86.3 | 455.60 | 1.77 |
| 80.4 | 360.41 | 1.46 | 83.4 | 406.48 | 1.61 | 86.4 | 457.33 | 1.78 |
|  |  | 1.46 |  |  | 1.62 |  | 457.33 | 1.78 |
| 80.5 | 361.87 |  | 83.5 | 408.10 |  | 86.5 | 459.17 |  |
| 80.6 | 363.34 | 1.47 | 83.6 | 409.72 | 1.62 | S6. 6 | 460.96 | 1.79 |
| S0.7 | 364.51 | 1.47 | 83.7 | 411.35 | 1.63 | 86.7 | -10.96 | 1.80 |
| 80.9 | 366.29 | 1.45 | 83.8 | 412.98 | 1.63 | 86.8 | 615 | 1.80 |
| 80.9 | 367.77 | 1.48 | 83.9 | \$14.62 | 1.64 | 86.9 | 466.36 | 1.81 |
|  |  | 1.49 |  |  | 1.64 |  | 466.36 | 1.81 |
| 81.0 | 369.26 |  | 84.0 | 416.26 |  | 87.0 | 468.17 |  |
| 81.1 | 370.75 | 1.49 | 84.1 | 417.91 | 1.65 | 87.1 | 469.99 | 1.82 |
| 81.2 | 372.25 | 1.50 | 84.2 | 419.57 | 1.66 | 87.2 | 471.52 | 1.83 |
| 81.3 | 373.75 | 1.50 | 84.3 | 421.23 | 1.66 | 87.3 | 473.65 | 1.83 |
| 81.4 | 375.25 | 1.51 | 84.4 | 42.89 | 1.67 | 87.4 | $475.49$ | 1.84 |
|  |  | 1.51 |  |  | 1.67 |  | 175.4 | 1.84 |
| 81.5 | 376.77 | 1.5 | 84.5 | 421.56 |  | 87.5 | 477.33 |  |
| 81.6 | 378.28 | 1.52 | 84.6 | 426.24 | 1.68 | 87.6 | 479.18 | 1.85 |
| 81.7 | 379.81 | 1.52 | 84.7 | 427.92 | 1.68 | 87.7 | 481.0.4 | 1.86 |
| 81.8 | 381.3:3 | 1.53 | 84.8 | 429.61 | 1.69 | 87.8 | $482.90$ | 1.86 |
| 81.9 | 352.87 | 1.53 | 84.9 | 431.30 | 1.69 |  |  | 1.87 |
|  |  | 1.54 |  | 431.30 | 1.70 | 87.9 | 484.76 | 1.87 |
| 82.0 | 384.40 |  | 85.0 | 433.00 |  | 88.0 | 486.64 |  |
| 82.1 | 355.93 | 1.54 | 85.1 | 434.71 | 1.70 | \$8.1 | 485.52 | 1.88 |
| 82.2 | 357.49 | 1.05 | 85.2 | 436.42 | 1.71 | 88.2 | $490.40$ | 1.89 |
| 82.3 | 389.0 .5 | 1.55 | 85.3 | 438.13 | 1.72 | 85.3 | 49.299 | 1.89 |
| 82.4 | 390.61 | 1.56 | 85.4 | 439.85 | 1.72 | 88.4 | 494.19 | 1.90 |
|  |  | 1.56 |  |  | 1.73 |  | 49.19 | 1.90 |
| 82.5 | 392.17 |  | 85.5 | 441.58 |  | 88.5 | 496.09 |  |
| 82.6 | 393.74 | 1.57 | 85.6 | 443.31 | 1.73 | 88.6 | $498.00$ | 1.91 |
| 82.7 | 395.31 | 1.57 | 85.7 | 445.05 | 1.74 | 88.7 | $500.92$ | 1.92 |
| 82.8 | 396.89 | 1.58 | 85.8 | 446.80 | 1.74 | 83.8 |  | 1.92 |
| 82.9 | 39 P .18 | 1.58 | 85.9 | 448.55 | 1.75 | 88.9 |  | 1.93 |
| 83.0 | 400.07 | 1.59 | 86.0 | 450.30 | 1.76 | 89.0 | $50.5 .70$ | 1.93 |

D
102

| Boiling Boint, Centigrade. | $\begin{aligned} & \text { Barometer } \\ & \text { in } \\ & \text { villimetres. } \end{aligned}$ | Difference. | Roiling l'oint, Centigrade | $\begin{gathered} \text { Barometer } \\ \text { in } \\ \text { Milliuletres. } \end{gathered}$ | Difference. | Boiling Point, Centigrade | Barometer in Nillimetres. | Difference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ |  |  | $\bigcirc$ |  |  | $\bigcirc$ |  |  |
| 89.0 | 50.3 .70 | 1.94 | 93.0 | 588.33 | $2 \cdot 10$ | 97.0 | 651.93 | 2.49 |
| 89.1 | 507.65 | 1.94 | 93.1 | 590.53 | 2.8 | 97.1 | 684.42 | 2.49 |
| 89.2 | 509.59 | 1.93 | 93.2 | 592.74 | 2.21 | 97.2 | $6 \times 6.92$ | $2 . .00$ |
| 89.3 | 511.51 | 1.95 | 93.3 | 59.1 .96 | 2.22 | 97.3 | $6-9.42$ | 2.51 |
| . 4 | 513.50 | 1.96 | 93.4 | 597.18 | 2.22 | 97.4 | 691.94 | 2.51 |
|  |  | 1.97 |  |  | 2.23 |  |  | 2.52 |
| 89.5 | 515.47 |  | 93.5 | 599.41 |  | 97.5 | 694.46 |  |
| 89.6 | 517.41 | 1.97 | 93.6 | 601.65 | 2.26 | 97.6 | 696.98 | 2.53 |
| 89.7 | 519.42 | 1.98 | 93.7 | 603.89 | 2.24 | 97.7 | 694.52 | 2.54 |
| 89.8 | 521.40 | 1.95 | $9: 3.8$ | 606.14 | $2 \cdot 25$ | 97.8 | 702.06 | 2.54 |
| 89.9 | 523.39 | 1.99 | 9:3.9 | 608.40 | 2.26 | 97.9 | 704.62 | 2.55 |
|  |  | 2.60 |  |  | 2.26 | . |  | 2.56 |
| 90.0 | 525.39 |  | 91.0 | 610.66 |  | 98.0 | 707.17 |  |
| 90.1 | 5.27 .40 | 2.10 | 94.1 | 612.93 | 2.27 | 98.1 | 709.74 | 2.57 |
| 90.2 | 529.41 | 2.01 | 94.2 | 615.21 | 2.25 | 98.2 | 712.31 | 2.57 |
| 90 | 531.19 | 2.02 | 94.3 | 6 | 2.29 | 95.3 | 714.90 | 2.58 |
|  |  | 2.02 |  |  | 2.29 |  |  | 2.59 |
| 90.4 | 533.44 | 2.63 | 94.4 | 619.79 | 2.30 | 93.4 | 717.49 | 2.60 |
| 90.5 | 53.3.47 |  | 94.5 | 622.09 |  | 98.5 | 720.08 |  |
| 90.6 | 537.51 | 2.04 | 94.6 | $62+.39$ | 2.31 | 98.6 | 722.69 | . 61 |
| 90.7 | 539.55 | 2.04 | $9+.7$ | 626.71 | 2.3 | 98.7 | 725.30 | 2.61 |
| 90.5 | $5+1.60$ | 2.05 | 94.8 | 629.93 | 2.32 | 98.8 | 727.93 | 2.62 |
| 90.9 | $5+3.65$ | 2.05 | 9.4 .9 | 631.36 | 2.33 | 98.9 | 730.55 | 2.63 |
| 90.9 | $5+3.65$ | 2.06 | 94.9 | 6.3136 | 2.33 |  | 730.55 | 2.64 |
| 91.0 | 54.5 .71 |  | 95.0 | 633.69 |  | 99.0 | 733.19 |  |
| 91.1 | 547.78 | 2.07 | 95.1 | 636.03 | 2.34 | 99.1 | $7: 35.84$ | 2.64 |
| 91.2 | 549.86 | 2.07 | 9.5 .2 | 638.38 | 2.35 | 99.2 | 738.49 | $\because .65$ |
|  | $5 \pm .86$ | 2.08 | 9.5 |  | 2.36 | 09.3 | 711.15 | 2.66 |
| 91.3 | 551.9 t | 2.09 | 9.5 .3 | 640.74 | 2.36 | $99 . .3$ | 741.1: | 2.67 |
| 91.4 | 554.03 | 2.09 | 95.4 | 643.10 | 2.37 | 99.4 | 743.52 | 2.68 |
| 91.5 | 556.12 |  | 95.5 | 615.48 |  | 99.5 | 716.50 |  |
| 91.6 | 558.23 | 2.10 | 9.5 .6 | 647.86 | 2.38 | 99.6 | 749.18 | 2.68 |
|  |  | 2.11 |  |  | 2.39 |  |  | 2.69 |
| 91.7 | 560.33 | 2.11 | 95.7 | 650.24 | 2.39 | 99.7 | 7.51 .67 | 2.70 |
| 91.8 | 562.14 | 2.1 | 95.5 | 652.63 |  | 99.8 | 754.37 |  |
| 91.9 | 564.56 | 2.12 | 95.9 | 655.04 | 2.40 | 99.9 | 75728 | 2.71 |
|  |  | 2.13 |  |  | 2.41 |  |  | 2.72 |
| 92.0 | 566.69 |  | 96.0 | 657.44 |  | 100.0 | 760.00 |  |
| 92.1 | 568.82 | 2.13 | 96.1 | 659.86 | 2.42 | 100.1 | 762.73 | 2.73 |
|  |  | 2.14 |  |  | 2.42 | 100.9 | 765.16 | 2.73 |
| 92.2 | 570.96 | 2.15 | 96.2 | 662.25 | 2.43 | 100.2 | 76.9 .46 | 2.74 |
| 92.3 | 573.11 | 2.15 | 96.3 | 664.71 | 2.4. | 100.3 | 768.20 | 2.75 |
| 92.4 | 575.27 | 2.15 | 96.4 | 667.15 | 2.44 | 100.4 | 770.95 | 2.65 |
|  |  | 2.16 |  |  | 2.44 |  |  | 2.76 |
| 92.5 | 577.43 |  | 965 | 669.59 |  | 100.5 | 773.71 |  |
| 92.6 | 57 | 2.17 | 96.6 | 672.05 | 2.15 | 100.6 | 776.47 | 2.77 |
|  | 57.59 | 2.17 |  |  | 2.46 |  |  | 2.77 |
| 92.7 | 581.77 | 2.18 | 96.7 | 674.51 | 2.47 | 100.7 | 779.25 | 2.78 |
| 92.8 | 588.95 | 2.18 | 96.8 | 676.97 | 2.47 | 100.8 | 7 72.03 | 2.18 |
| 92.9 | 586.14 | 2.19 | 96.9 | 679.45 | 2.47 | 100.9 | 784.82 | 2.79 |
| 9:3.0 | $58 \times .33$ | 2.19 | 97.0 | 681.93 | 2.48 | 101.0 | 787.62 | 2.60 |
|  |  |  |  |  |  |  |  |  |

## T A BLE X X VI。

BAROMETRIC PRESSURES CORRESPONDING TO TEMPERATURES OF TIE BOLLING POINT OF WATER,

EXPRESSED IN ENGLISH INCHES FOR TEMPERATURES OF FAHRENHEIT.

Reduced from Regiadlt's Table, revised by Moritz.

| $\begin{aligned} & \text { Boiling } \\ & \text { Print, } \\ & \text { Fahreu. } \end{aligned}$ | $\begin{aligned} & \text { Barom- } \\ & \text { eter } \\ & \text { in } \\ & \text { English } \\ & \text { Inches. } \end{aligned}$ | Difference | $\begin{aligned} & \text { Boiling } \\ & \text { Print, } \\ & \text { Fahren. } \end{aligned}$ | Barom- <br> eter 11 Engrish Inches. | Differeuce. | $\begin{aligned} & \text { Boiling } \\ & \text { Point, } \\ & \text { Fahren } \end{aligned}$ | $\begin{aligned} & \text { Barom- } \\ & \text { eter } \\ & \text { in } \\ & \text { Enylish } \\ & \text { Inches. } \end{aligned}$ | Differeace. | $\begin{aligned} & \text { Boiling } \\ & \text { Point, } \\ & \text { Fahren. } \end{aligned}$ | $\begin{aligned} & \text { Barma- } \\ & \text { eter } \\ & \text { in } \\ & \text { English } \\ & \text { Inches. } \end{aligned}$ | Difference. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{array}{r} 0.037 \\ .037 \\ .037 \\ .037 \\ .038 \end{array}$ | $\stackrel{\circ}{158.0}$ | $18.195$ | 0.039 | $\bigcirc$ | $19.407$ | 0.042 | $\stackrel{\circ}{194.0}$ | $20.685$ | 0.044 |
| 135.0 | 17.045 |  |  |  |  | 191.0 |  |  |  |  |  |
| 185.1 | 17.08 .5 |  | 188.1 |  |  | 191.1 |  |  | 194.1 | $20.729$ |  |
| 185.2 | 17.122 |  | 188.2 | 18.274 | . 039 | 191.2 | 19.490 | .04.2 | 194.2 | 20.773 | 4 |
| 185.3 | 17.160 |  | 188.3 | 18.314 | . 039 | 191.3 | 19.532 | . 042 | 194.3 | 20.817 | .044 |
| 155.4 | 17.197 |  | 188.4 | 18.353 | $\begin{array}{r} 040 \\ .040 \end{array}$ | 191.4 | $19573$ | $\begin{aligned} & .042 \\ & .042 \end{aligned}$ | 194.4 | 20.861 | $\begin{aligned} & .044 \\ & .044 \end{aligned}$ |
| 185.5 | 17.235 |  | 188.5 | 18.393 | . 040 | $\begin{aligned} & 191.5 \\ & 191.6 \end{aligned}$ | $19.615$ | . $0+2$ | $\begin{aligned} & 194.5 \\ & 194.6 \end{aligned}$ | 20.905 | . 044 |
| 18.5 .6 | 17.272 | .038 | 189.6 | 18.483 |  |  |  |  |  | $\begin{aligned} & 20.949 \\ & 20.993 \end{aligned}$ |  |
| 185.7 | 17.310 | . 038 | 188.7 | 18.472 | 40 | $\begin{aligned} & 191.6 \\ & 191.7 \end{aligned}$ | $\begin{aligned} & 19.657 \\ & 19.699 \end{aligned}$ | . 042 | 194.7 |  | $\begin{aligned} & .044 \\ & .044 \end{aligned}$ |
| 18.5 .8 | 17.:34 | . 038 | 188.8 | 18.512 | $\begin{aligned} & .040 \\ & .040 \end{aligned}$ | $\begin{aligned} & 191.5 \\ & 191.9 \end{aligned}$ | $\begin{aligned} & 19.7 .71 \\ & 19.783 \end{aligned}$ | 042 | $\begin{aligned} & 194.8 \\ & 194.9 \end{aligned}$ | $\begin{aligned} & 21.038 \\ & 21.082 \end{aligned}$ |  |
| 185.9 | 17.3.5 | . 038 | 188.9 | 18.552 |  |  |  | 042 |  |  | $\begin{aligned} & .044 \\ & .044 \end{aligned}$ |
|  |  | . 038 |  |  | . 040 |  |  | .042 |  |  |  |
| 186.0 | 17.423 |  |  | 18.5 | . 040 | 19 | 19 | .042 | 195.0 | 21.126 | . 045 |
| $1: 6.1$ | 17.161 |  | 159.1 | 18.632 |  | 192.1 | 19.865 |  |  | $\begin{aligned} & 21.171 \\ & 21.216 \end{aligned}$ |  |
| $3 \sim 6.2$ | 17.499 |  | 189.2 | 18.672 |  |  | 19.910 | . 0.42 | 195.2 |  | .04.) |
| 186.3 | 17.537 | .038 | 159.3 | 18.712 | . 040 | 192.3 | $\begin{aligned} & 19.9 .52 \\ & 19.995 \end{aligned}$ | .042 | 19.5.3 | 21.260 | $\begin{aligned} & .045 \\ & .045 \end{aligned}$ |
| 186.1 | 17.575 | 38 | 189.4 | 18.753 | $.040$ |  |  | . 043 | 195.4 | 21.805 |  |
|  |  | . 038 |  |  |  |  |  |  |  |  | . 045 |
| 186.5 | 17.614 | . 038 | $189.5$ | 18.793 | . 040 | $\begin{aligned} & 192.5 \\ & 192.6 \end{aligned}$ | 20.037 | - 0.13 | $\begin{aligned} & 195.5 \\ & 19.5 .6 \end{aligned}$ | 21.350 | . 045 |
| 186.6 | 17.6.92 |  |  | 18.833 |  |  | 20.050 |  |  | 21.395 |  |
| 186.7 | 17.630 |  | 189.7 | 18.854 |  | 192.7 | 20.123 | . 043 | 195.7 | 21.440 | .045.045 |
| 186.9 | 17.729 |  | 159.8 | 18.914 | . 041 <br> . 041 | $\begin{aligned} & 192.8 \\ & 192.9 \end{aligned}$ | 20.166 | $\begin{aligned} & .043 \\ & .043 \\ & .043 \end{aligned}$ | $\begin{aligned} & 195.8 \\ & 195.9 \end{aligned}$ | $\begin{aligned} & 21.185 \\ & 21.530 \end{aligned}$ |  |
| 186.9 | 17.767 |  | 159.9 | 18955 |  |  | 20.208 |  |  |  | $\begin{aligned} & .045 \\ & .045 \end{aligned}$ |
|  |  | . 039 |  |  |  |  |  |  |  |  |  |
| 187.0 | 17.806 |  | $190.0$ | $18.996$$19036$ | . 041 | $\begin{aligned} & 193.0 \\ & 193.1 \end{aligned}$ | $\begin{aligned} & 20.251 \\ & 20.294 \end{aligned}$ | . 043 | $\begin{aligned} & 196.0 \\ & 196.1 \end{aligned}$ | 21.576 | .fi45 |
| 157.1 | 17.844 | .039 |  |  |  |  |  |  |  | 21.621 |  |
| 157.2 | 17.88:3 |  | $190.2$ | 19.077 | . 041 | 193.2 | 20.338 | $\begin{aligned} & .043 \\ & .043 \end{aligned}$ | $\begin{aligned} & 196.2 \\ & 196.3 \end{aligned}$ | 21.666 | . 0.46 |
| 157.3 | 17.922 | $\begin{aligned} & .039 \\ & .039 \end{aligned}$ | $\begin{aligned} & 190.3 \\ & 190.4 \end{aligned}$ | $\begin{aligned} & 19.118 \\ & 19.159 \end{aligned}$ | $\begin{aligned} & .0+1 \\ & .0+1 \end{aligned}$ | $\begin{aligned} & 193.3 \\ & 193.4 \end{aligned}$ | $\begin{aligned} & 20.341 \\ & 20.424 \end{aligned}$ |  |  | 21.712 |  |
| 157.4 | 17.961 |  |  |  |  |  |  | $\begin{aligned} & .043 \\ & .043 \end{aligned}$ | 196.4 | 21.758 | $\begin{array}{r} .046 \\ .046 \end{array}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 187.5 | 18.000 | $\begin{array}{r} .039 \\ .039 \\ .039 \\ 039 \\ \mathbf{0 . 0 3 9} \end{array}$ | $\begin{aligned} & 190.5 \\ & 190.6 \\ & 190.7 \\ & 190.8 \\ & 190.9 \\ & 191.0 \end{aligned}$ | $\begin{aligned} & 19.200 \\ & 19.241 \\ & 19.253 \\ & 19.324 \\ & 19.36 .5 \\ & 19.407 \end{aligned}$ | $\begin{array}{r} .041 \\ .041 \\ .041 \\ .041 \\ 0.041 \end{array}$ | $\begin{aligned} & 193.5 \\ & 193.6 \\ & 193.7 \\ & 193.8 \\ & 193.9 \\ & 194.0 \end{aligned}$ | $\begin{aligned} & 20.467 \\ & 20.511 \\ & 20.554 \\ & 20.598 \\ & 20.641 \\ & 20.685 \end{aligned}$ | $\begin{gathered} .043 \\ .043 \\ .044 \\ .044 \\ 0.044 \end{gathered}$ | $\begin{aligned} & 196.5 \\ & 196.6 \\ & 196.7 \\ & 196.8 \\ & 196.9 \\ & 197.0 \end{aligned}$ |  | $\begin{array}{r} .046 \\ .046 \\ .046 \\ .046 \\ 0.046 \end{array}$ |
| 187.6 | 18.039 |  |  |  |  |  |  |  |  |  |  |
| 157.7 | 18.078 |  |  |  |  |  |  |  |  |  |  |
| 157.8 | 19.117 |  |  |  |  |  |  |  |  |  |  |
| 187.9 | 18.156 |  |  |  |  |  |  |  |  |  |  |
| 189.0 | 18.195 |  |  |  |  |  |  |  |  |  |  |


| Boiling Pont, Fuhren | $\begin{gathered} \text { Barom- } \\ \text { eter } \\ \text { in } \\ \text { Eurgish1 } \\ \text { luches } \end{gathered}$ | Difference | Boiling Point. Fathren | $\begin{aligned} & \text { Barom- } \\ & \text { eter } \\ & \text { in } \\ & \text { English } \\ & \text { lucbes. } \end{aligned}$ | Difference | Boiling Point, Pr Fahren | $\begin{aligned} & \text { Barom- } \\ & \text { eter } \\ & \text { in } \\ & \text { English } \\ & \text { lnches. } \end{aligned}$ | Difference. | $\begin{aligned} & \text { Boiling } \\ & \text { Proint, } \\ & \text { Fahren. } \end{aligned}$ | $\begin{aligned} & \text { Barom- - } \\ & \text { eter } \\ & \text { in } \\ & \text { English } \\ & \text { Inches. } \end{aligned}$ | Differeuce. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ |  | $\begin{gathered} 0.046 \\ .046 \\ .046 \\ .046 \\ .046 \end{gathered}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & 23.943 \\ & 23.993 \end{aligned}$ | $\begin{array}{r} 0.049 \\ .050 \end{array}$ | $\bigcirc$ | $\begin{aligned} & 25.990 \\ & 26.043 \end{aligned}$ |  | $209.0$ <br> 209.1 | $\begin{aligned} & 28.180 \\ & 98.937 \end{aligned}$ | 0.057 |
| 197.0 | 22.033 |  | 201.0 |  |  | 205.0 |  |  |  |  |  |
| 197.1 | 22.079 |  | 201.1 |  |  | 205.1 |  |  |  |  |  |
| 197.2 | 22.125 |  | $\begin{aligned} & 201.2 \\ & 201.3 \end{aligned}$ | $\begin{aligned} & 23.993 \\ & 24.042 \end{aligned}$ |  | 205.2 | 26.096 | . 053 | 209.2 | 28.293 | .0.57 |
| 197.3 | 2.272 |  |  | $\begin{aligned} & 24.042 \\ & 24.092 \end{aligned}$ | . 050 | 205.3 | 26.149 | $\begin{aligned} & .053 \\ & .053 \end{aligned}$ | $\begin{aligned} & 209.3 \\ & 209.4 \end{aligned}$ | $\begin{aligned} & 28.3 .50 \\ & 28.407 \end{aligned}$ | . 057 |
| 197.4 | 22.218 |  | 201.4 | 24.142 | $\begin{aligned} & .050 \\ & .050 \end{aligned}$ | 205.4 | 26.19 26202 |  |  |  | . 057 |
| 197.5 | 22.264 | . 047 | $\begin{aligned} & 201.5 \\ & 201.6 \end{aligned}$ | 24.191 | . 050 | $\begin{aligned} & 205.5 \\ & 205.6 \end{aligned}$ | 26.255 | . 053 | $\begin{aligned} & 209.5 \\ & 209.6 \end{aligned}$ | 28.464 | . 057 |
| 197.6 | 22.311 |  |  | 24.241 |  |  | 26.309 |  |  |  |  |
| 197.7 | 22.358 | $\begin{aligned} & .047 \\ & .047 \end{aligned}$ | 201.7 | $24.291$ | . 050 | 205.7 | 26.362 | . 054 | 209.7 | 28.579 | . 057 |
| 197.8 | 22.404 |  | 201.8 | 24.341 | .050 | $\begin{aligned} & 205.8 \\ & 205.9 \end{aligned}$ | $\begin{aligned} & 26.416 \\ & 26.470 \end{aligned}$ | .054 | 209.8 | 23.636 | . 057 |
| 197.9 | 22.451 | . 047 | 201.9 | 24.391 | $\begin{aligned} & .050 \\ & .050 \end{aligned}$ |  |  | $\begin{aligned} & .054 \\ & .054 \end{aligned}$ | 209.9 | 28.693 | . 058 |
| 195.0 | 22.198 | . 047 | 202.0 | 24.442 | . 050 | $\begin{aligned} & 206.0 \\ & 206.1 \end{aligned}$ | 26.52326.577 | .054 | $\begin{aligned} & 210.0 \\ & 210.1 \end{aligned}$ | $\begin{aligned} & 28.751 \\ & 28.809 \end{aligned}$ | . 058 |
| 192.1 | 22.545 | . 047 | $202.1$ | 24.492 |  |  |  |  |  |  |  |
| 198.2 | 22.592 |  |  | 21.542 | . 050 | $\begin{aligned} & 206.1 \\ & 206.2 \end{aligned}$ | 26.577 26.631 | . 054 | 210.2 | 28.866 | $\begin{aligned} & .058 \\ & .058 \end{aligned}$ |
| 198.3 | 22.639 | $\text { . } 047$ | $\begin{aligned} & 202.3 \\ & 202.4 \end{aligned}$ | $\begin{aligned} & 24.593 \\ & 24.644 \end{aligned}$ | $\begin{aligned} & .050 \\ & .051 \end{aligned}$ | $\begin{aligned} & 206.3 \\ & 206.4 \end{aligned}$ | $\begin{aligned} & 26.685 \\ & 26.740 \end{aligned}$ | $\begin{array}{r} .054 \\ .054 \end{array}$ | 210.3 | $\begin{aligned} & 28.924 \\ & 28.982 \end{aligned}$ |  |
| 198.4 | 22.686 |  |  |  |  |  |  |  | 210.4 |  | . 058 |
| 198.5 | 22.731 | 047 | 20.5 | 24.694 | . 051 |  | 26.794 | .054 | $210.5$ | 29.040 | . 058 |
| 198.6 | 22.781 |  | $202.6$ | 24.745 |  | 206.6 | $26.848$ |  |  | 29.098 |  |
| 198.7 | 22.829 | . 047 |  | 24.796 | .051 | 206.7 |  | . 054 | 210.7 | 29.156 | $\begin{aligned} & .058 \\ & .058 \end{aligned}$ |
| 192.8 | 22.676 | .048 | 202.8 | 24.847 | . 05 | $\begin{aligned} & 206.8 \\ & 206.9 \end{aligned}$ | $\begin{aligned} & 26.957 \\ & 27.012 \end{aligned}$ | $\begin{aligned} & .055 \\ & .055 \end{aligned}$ | 210.8 | 29.215 |  |
| 195.9 | 22.924 | . 048 | 202.9 | 24.593 | . 051 |  |  |  | 210.9 | 29.273 | . 058 |
|  |  |  |  |  |  |  |  | .05\% |  |  | . 059 |
| 199.0 | 22.971 | . 048 | 203.0 |  | . 051 | , | 27 | . 035 | 211.0 | 29.331 |  |
| 199.1 | 2:3.019 |  | $\begin{aligned} & 203.1 \\ & 203.2 \end{aligned}$ | 25.000 |  | 207.1 | 27.121 |  | 211.1 | 29.390 | $0.59$ |
| 199.2 | 23.067 | . 048 |  | 25.0 .51 | . 051 | 207.2 | 27.176 | 5 | 211.2 | 29.449 |  |
| 199.3 | 23.115 |  | $\begin{aligned} & 203.3 \\ & 203.4 \end{aligned}$ | $\begin{aligned} & 2.5 .103 \\ & 25.154 \end{aligned}$ | 051 | 207.3207.4 | $\begin{aligned} & 27.231 \\ & 27.286 \end{aligned}$ | $\begin{aligned} & .05 \overline{5} \\ & .055 \\ & .055 \end{aligned}$ | $\begin{aligned} & 211.3 \\ & 211.4 \end{aligned}$ | $\begin{aligned} & 29.508 \\ & 29.566 \end{aligned}$ | $\begin{aligned} & .059 \\ & .059 \\ & .059 \end{aligned}$ |
| 199.4 | 23.163 | . 048 |  |  | .051 |  |  |  |  |  |  |
|  |  | . 043 |  |  | . 052 |  |  |  |  |  |  |
| 199.5 | 23.211 |  | 203.5 | 25.206 | 052 | $\begin{aligned} & 207.5 \\ & 207.6 \end{aligned}$ | $\begin{aligned} & 27.341 \\ & 27.397 \end{aligned}$ | .055 | $\begin{aligned} & 211.5 \\ & 211.6 \end{aligned}$ | 29.625 | -0.99 |
| 199.9; | 23.259 | . 045 | 203.6 | 25.257 |  |  |  |  |  | 29.684 |  |
| 199.7 | 23.308 |  | 203.7 | 25.309 |  | 207.7 | 27.452 |  | 211.7 | 29.744 | . 059 |
| 199.8 | 23.356 |  | 203.8 | 25.361 | .05 | 207.8 | 27.507 |  | 211.8 | 29.803 | .059 |
| 199.9 | 23.40.5 |  | 203.9 | 25.413 |  | 207.9 | 27.563 |  | 211.9 | 29.862 | . 05 |
|  |  | . 049 |  |  | .052 |  |  | . 056 |  |  | .059 |
| 200.0 | 23.453 |  | 204.0 | 25.465 |  | 208.0 | 27.618 |  | 212.0 | 29.922 |  |
| 200.1 | 23.502 |  | 204.1 | 25.517 |  | 208.1 | 27.671 |  | 212.1 | 29.981 | .060 |
| 200.2 | 23.550 |  | 204.2 | 25.569 |  | 208.2 | 27.730 |  | 212.2 | 30.041 | .06 |
| 20.3 | 23.599 |  | 204.3 | 25.621 |  | 208.3 | 27.786 |  | 212.3 | 30.101 |  |
| 200.4 | 23.648 |  | 204.4 | 2.9.674 |  | 208.4 | 27.842 |  | 212.4 | 30.161 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 200.5 | 23.697 |  | 204.5 | 2.5.726 |  | 208.5 | 27.898 |  | 212.5 | 30.221 |  |
| 200.6 | 23.746 |  | 204.6 | 25.779 |  | 208.6 | 27.954 | . 056 | 212.6 | 30.281 | . 060 |
| 200.7 | 23.79 .5 |  | 204.7 | 25.831 | . 053 | 208.7 | 28.011 | . 0 | 212.7 | 30.341 | . 060 |
| 200.8 | 23.845 |  | 204.8 | 25.884 | -053 | 208.8 | 28.067 | . 05 | 212.8 | 30.401 | . 060 |
| 200.9 | 23.594 | . 049 | 204.9 | 25.937 | .053 | 208.9 | 28.123 | . 056 | 212.9 | 30.461 | . 060 |
| 201.0 | 23.943 | 0.049 | 205.0 | 25.990 | 0.053 | 209.0 | 28.180 | 0.057 | 213.0 | 30.522 | 0.060 |
|  |  |  |  |  |  |  |  |  |  |  |  |

# METEOROLOGICAL AND PHYSICAL TABLES. 

## geographical measures.

SERIES V.<br>AN APPENDIX TO THE HYPSONETRIC TABLES.

## TABLES

## FOR COMPARING THE MOST IMPORTANT GEOGRAPHICAL MEASURES OF LENGTH AND OF SURFACE.

a) Tables for comparing the most important measures of lexgtif used for indicating altitudes.
b) Tables for comparing the most mportant meastres of geographical distances.
c) Tables for comparing the most important measures of geographical surfaces.

# a) TABLES 

FOR

COMPARING THE MOST IMPORTANT MEASURES OF LENGTH USED FOR INDICATING ALTITUDES.

## CONTENTS.

> (The figures refer to the folio at the bottom of the page.)

# TABLES FOR COMPARING TIIE MOST IMPORTANT MEASURES OF LENGTU USED FUR INDICATING ALTITUDES. 

PAGE
On the Various Standards of Measure, and their Relations . . . 7

Comparison of the Measures of Length most generally used for indicating Altitudes.
Table I. Conversion of French Toises into Metres . . . . 11
" II. Conversion of Fremeh Toises into Paris Feet . . . 14
" III. Conversion of French Toises into English Feet . . . 1.j
" IV. Conversion of French Toises into Rhine Feet . . . 1.)

For converting Metres into different Measures.
" V. Conversion of Metres into Toises . . . . . . 1 i)
" VI. Conversion of Metres into Paris Feet . . . . . 17
" VII. Conversion of Metres into English Fpet . . . . . 20
"V VIII. Conversion of Metres into Rhine or Prossian Feet . . 2s
" IX. Concersion of Metres into Feet of Vienna . . . . 2s

For converting Paris or French Feet into different Measures.
" X. Conversion of Paris Feet into Toises . . . . . 29
" XI. Conversion of Paris Feet into Metres . . . . . 30
" XII. Conversion of Paris Feet into English Feet . . . :31
" XIII. Conversion of Paris Feet into Rhine Feet . . . . 82
" XIV. Conversion of Paris Feet into Feet of Vienna . . . 33

For converting English Yards and Feet into different Measures.
" XV. Conversion of English Yards into French 'Toises . . . 34
" XVI. Conversion of English Yards into Metres . . . . 34
" XVII. Conversion of English Fpet into Metres . . . . . 3.5
" XVIII. Conversion of English Feet into Paris Fpet . . . 36
" XIX. Conversion of English Feet into Rhine Fept . . . . 87
" XX. Conversion of English Feet into Feet of Vienna. . . 38 E
Fur converting Klafter and Feet of Vienna into different Measures.
Table XXI. Conversion of Klatter of Viema into Metres ..... 39
،. XXII. Conversion of Klatter of Viema into Paris Feet ..... 40
" XXIII. Conversion of Klatter of Viemna into English Feet ..... 40
" XXIV. Consersion of Feet of Viemat into Metres ..... 41
" XXV. Conversion of Feet of Viema into Paris Feet ..... 4.
" XXVI. Comversion of Feet of Viema into English Feet ..... $4: 3$
" XXVII. Conversion of Feet of Vienna into Rhine Feet ..... 44
For concerting lime or Prussian Feet into different Measures.
" XXVIII. Conversion of Rhine Feet into French Toises ..... 45
" XXIX. Conversion of Rhine Feet into Metres ..... 45
" XXX. Conversion of Rline Feet into Paris Feet ..... 46
" XXXI. Conversion of Rhine Feet into English Feet ..... 46
" XXXII. Conversion of Rhine Feet into Feet of Vienna ..... 47
" XXXIII. Consersion of Bavarian Feet into Metres ..... 47
For converting Spanish, Mexican, and Bolivian Varas and Feet into different Measures.
" XXXIV. Conversion of Old Spanish or Castilian Varas into Metres ..... 48
". XXXV. Conversion of Old Spanish Feet into Metres ..... 48
" XXXVI. Consersion of Mexican Varas into Metres ..... $4!$
" XXXVII. Conversion of Mexican Feet into Metres ..... $4!$
" XXXVIII. Conversion of Mexican Feet into English Feet ..... 49
" XXXIX. Conversion of Bolivian Varas into Metres ..... 50
" XL. Consersion of Bolivian Feet into Metres ..... 50
". XLI. Conversion of Bolivian Feet into English Feet ..... 50
For converting Fractional Parts of a Toise and of a Foot into each other.
" XLII. Conversion of Inches into Duodecimal Lines ..... 51
" XLIII. Conversion of Decimals of a Toise into Feet and Inches ..... 51
" XLIV. Conversion of Decimals of a Foot into Inches and Deci- mals ..... 52
" XLV. Conversion of Decimals of a Foot into Inches and Duo- decimal Lines ..... 52
" XLVI. Conversion of Inches and Duodecimal Lines into Decimals of a Foot ..... 52
" XLVII. Table for comparing the most important Measures of Length ..... 5:
" XLVIII. Table for the conversion of English Fathoms into Metres ..... 54
" XLIX. Table for the conversion of Metres into English Fathoms ..... $54^{-}$

## COMPARISON

OF THE

## MEASURES OF LENGTH MOST GENERALLY CSED FOR INDICATING ALTITUDES.

Ir is too well known that the measures used in scientific researches among civilized nations are not uniform, as the convenience of all would require. In France the metre is employed; in England and North America, the yard and its third part, the English foot; in Germany, most commonly, the Old French or Paris foot, the sixth part of the French toise called the Toise du Pérou; at the same time, however, though not so extensively, the Rhine foot, in Denmark and Holland, and especially in Prussia, where it has been declared, moder the name of Prussian foot, the legal measure in that kingdom; in Austria, the klafter of Vienna and its sixth part, the foot of Vienna; in Switzerland, the Swiss or federal foot, which has been adjusted to the metrical system, and is three-tenths of a metre; and so on.

The numerous altitudes ascertained, either by private efforts, or in connection with the public works, and especially with the extensive geodetic olerations carried on by the governments of these varions countries for the survey of a regular map, are expressed in the measures respectively adopted by each of them. These heights, however, before they can be compared, require to be uniformly reduced to one of these measures. Their relation to each other, therefore, is given here, together with numerous reduction tables, designed to save both the useless expenditure of time and the almost unavoidable errors arising from so numerous reductions.

The exact relation of the standard measures above mentioned is not easily ascertained, and the numbers given by the best authorities by no means always agree; for the manufacture of exact copies of a standard scale, and the accurate comparison of it, require considerable skill, and belong to the most delicate operations of physics. The numbers used for computing the following tables have been adopted, after a careful review of the authorities, as the most reliable. A few words on the most important original legal standards of measures may not be unwelcome. For further details on the subject the reader is referred principally to Dove's work, Maus und Messen, 2d edition, Berlin, 1835.

The principal original, legal standards are the following :-

1. The Toise du Pérou, the old Freneh standard, made in 1735, in Paris, by Langlois, under the direction of Godin, is a bar of iron which has its standard length at the temperature of $13^{\circ}$ Réaumur. It is known as the Toise du Péron, because it was used by the French Academicians Bouguer and La Condamine in their measurement
of an arc of the meridian in Peru. What follows will show that it may almost be called the only common standard, to which all the others are referred for comparison.
2. The Mètre is a standard bar of platina, made by Lenoir in Paris, which has its normal length at the temperature of zero Centigrade, or the freezing point. Its length is intended to make it a natural standard, and to represent the ten-millionth part of the terrestrial are comprised between the equator and the pole, or of a quarter of the meridian. The length of this are given by the measurement, ordered for the purpose by the Assemblée Nationale, of the are of the meridian between Barcelona, through France, to Dunkirk, combincd with the measurements previously made in Peru and in Lapland, gave for the distance of the equator from the pole 5, 130,740 toises, with an ellipticity of $\frac{1}{3} \frac{1}{4}$, and for the length of the metre 443.29596 lines of the toise du Pérou, assumed to be 443.296 lines, or 3 feet 11.296 lines. This last quantity was declared in 1799 to be the length of the legal metre, and vrai et définitif', and is the length of Lenoir's platina standarl. Later, and more extensive measurements in various parts of the globe, however, seem to indicate that this quantity is somewhat too small. The results of these various measurements, carefully combined and computed by Bessel, would make the quarter of the meridian $10,000,856$ metres, and the metre $=443.29979$ Paris lines ; Schmidt's computation would make it 443.29977 lines, and both numbers are confirmed by Airy's results. The legal metre is thns, in fact, as Dove remarks, a legalized part of the toise du l'érou, and this last remains the primitive standard. But it must be arded that a natural standard, in the absolute sense of the word, is a utopian one, which everchanging Nature never will give us. The metre is, for all practical purposes, what it was intended to be, a natural standard; though it must be confessed that, in practice, the question is not whether, and how far, a standard is a natural or a conventional one, but how readily and accurately it can be obtained, or recovered when lost.
3. The English Stundard Fard is a brass bar, made by Bird in 1760 , which was declared, by act of Parliament, 1st May, 1825, the legal measure of length when at the temperature of $62^{\circ}$ Fahreulitit, under the name of Imperial Standard. Another standard, sometimes also called Parliamentary Standard, was made by Bird in 17.58. Sir George Shuckburgh found both to be nearly identical, at least within 0.0002 of an inch. (Philos. Trans. for 1798, p. 170.)

Another scale of brass, however, made by Troughton for Sir George Shuckburgh, described in the Philosophical Transactions for 1798, and known as Shuckburgh's scale, obtained among scientific men, perhaps, a higher degree of authority, on account of the great aceuracy of its division, and of its apparatus, devised by Troughton, for delicate comparisons. The scale was used by Captain Kater, in 1818, in his researches for determining the length of the pendulum beating a second at London, and also the length of the metre, expressed in English inches of the imperial standard. (IMilos. Trens. for 1818.)

Numerous attempts to determine the relation between the English and the French meakures show no inconsiderable discrepancies in their results. Omitting the older comparisons with the toise, we give here the value of the metre in English imperial inches as resulting from the most reliable comparisons.

A standard scale made and divided by Troughton, and in all particulars identical with Shuckburgh's scale, was brought to France in 1801 by Pictet. The comparison of it with the standard metre, made by Prony, Legendre, and Méchain, gave, after due reduction of the two standards to their respective normal temperatures,

1 metre at $32^{\circ}$ Fahr. $=39.371$ English imperial inches at $62^{\circ}$ Fahr.
This determination was adopted for all reductions in Kelly's Universal Cambist, and in the French translation of the work, published in Paris in 1823.

A new comparison was made with great care by Captain H. Kater, in 1818. (See Philos. Trans. for 1818 , p. 103.) The standards used were a brass scale metre, by Fortin, terminated with parallel planes (mètre à bouts), and a bar of platina on whieh the length of the metre was marked by two very fine lines (mètre à traits). Both were compared with Shuckburgh's scale, and a double series of experiments gave as the mean result:-
Brass metre at $32^{\circ}$ Fahr. $=39.37076$ inches of Shuckburgh's scale at $62^{\circ}$ Fahr. Platina metre at $32^{\circ}$ Fahr. $=\frac{39.37081}{39.37079}$ Mean $\quad$ " $\quad$ " $\quad$ " $\quad$ "

On this value of the metre are based the reduction tables by Matthieu, published yearly in the Annucire du Bureau des Lougitudes ; and it has come into general use, both in Europe and in this country.

Captain Kater gives besides, in the same paper, p. 109, note, the value of the metre compared with Bird's Parliamentary standard as being
1 metre at $32^{\circ} \mathrm{F}=39.37062 \mathrm{imp}$. inches of Bird's Parliamentary standard at $62^{\circ} \mathrm{F}$. This value has been adopted by Dove, as being the legal one, in his reduction tables in his work Matas und Messen, p. 175, etc., and by many German authorities.

According to Bailey's experiments, made in 1835, when engaged in constructing a new standard for the Royal Astronomical Society (Memoirs R. Ast. Soc., vol. ix.), the value of the metre is (Lee, Collection of T'ables and Formula, p. 62)

1 metre at $32^{\circ} \mathrm{F} .=39.370092$ imperial standard inches at $62^{\circ} \mathrm{F}$.
The original legal standards having been lost in the fire which destroyed, in 1834, the Parliament Houses, an act of Parliament provided for the construction of new ones. An extensive and most careful comparison of the standards of length of England, Belgium, Prussia, Russia, India, Australia, was made at the Ordnance Survey office at Southampton by Capt. A. R. Clarke, R.E., under the direction of Sir Henry James, Director, the results of which were published in London in 1866. This comparison gives the relation of the imperial standard to the metre as

1 metre at $32^{\circ} \mathrm{F} .=39.370488$ inches of the imperial standard at $62^{\circ} \mathrm{F}$.
The value adopted in computing the tables in this volume, before this last comparison was made, is that determined by Capt. Kater in 1818, viz. :-
1 metre at $32^{\circ} \mathrm{F} .=39.37079$ English inches of the imperial standard at $62^{\circ} \mathrm{F}$.
The difference between these two equivalents of the metre is so small that, for practical purposes, the substitution of Clarke's value, implying such laborious com-
putations, would hardly be justified. For the present, therefore, it seems best not to introduce here this new value, which, after all, may not be a final one.

It may not be out of place to remark that Schumacher, in the first edition of his Sammlung von Hiulfstafeln, used the value 1 metre $=39.3827$ English inches, as given in the Base du Système Métrique; but this number, which expresses the relation of both standards when at the freezing point, becomes 39.37079 when they are respectively reduced to their normal temperatures. Schumacher's tables, therefore, must be corrected accordingly.
4. The actual standard of length of the United States is a brass scale of eightytwo inches in length, prepared for the Coast Survey of the United States, by Troughton of London, meant to be identical with the English Imperial Standard, and deposited in the office of weights and measures. The temperature at which it is a standard is $62^{\circ}$ Falurenheit, and the yard measure is traced between the 27 th and 63 d inches of the scale. (See Report on the Construction and Distribution of Weights and Mertsures, by Prof. A. D. Bache, 1857.)

IIassler, first Superintendent of the United States Coast Survey, made an elaborate comparison of eleven different standard metres with the brass scale of eighty-two inches, by Troughton. Three of the standard metres, certified to be correct by high authorities, seem to deserve especial confidence: 1. An iron metre, presented to Mr. Hassler by Tralles, which was one of the three that Tralles had made by Lenoir at the same time with those distributed to the committee on the weights and measures. 2. Another metre of iron, also by Lenoir, verified by Bouvard and Arago, and declared by them to be identical with the original. 3. A platina standard by Fortin verified by Arago, and found to be $\mathrm{TO}_{\mathrm{TO}}^{\mathrm{I}} \mathrm{O}$ of a millimetre too long, for which error allowance was made. Their comparison with the Troughton scale at the temperature of the freezing point gave :-

1. Iron metre of Tralles $=39.3809171$ inches of the Troughton scale.
2. Iron metre of Lenoir $=39.3799487$ " " "
3. Platina metre of Fortin $=39.3804194 \quad$ " ${ }^{4}$

Or, correcting for expansion, and reducing them to their respective standard tem peratures :-

1. Iron metre of Tralles at $32^{\circ}-\mathrm{F} .=39.36850$ English inches of the
2. Iron metre of Lenoir at $\left.32^{\circ} \mathrm{F} .=39.36754\right\}$ Troughton scale of
3. Platina metre of Fortin at $32^{\circ} \mathrm{F} .=39.36789$ (inches at $62^{\circ} \mathrm{F}$.

Hassler, in his Report to Congress on Weights and Measures, in 1832, adopts the first value, viz. :-

1 metre at $32^{\circ} \mathrm{F} .=39.3809171$ inches of the Troughton scale at $32^{\circ} \mathrm{F} . ;$
which reduced by Prof. A. Bache, his successor, by means of the coefficient of expansion by heat used by Hassler, became

1 metre at $32^{\circ}=39.36850535$ United States standard inches at $62^{\circ} \mathrm{F}$.
This scale and its metric equivalent was regarded as the United States standard from which copies were to be made.

This value differs materially from those given by other careful comparisons, while, on the other hand, the close accordance of the numbers corresponding to the
various standard metres proved the accuracy of Hassler's method of comparison. But as the yard of the Troughton scale had been accepted as the standard of length of the United States (see Report on Weights and Measures, by Prof. Bache, 1857) it seemed advisable to call it, as is done in the Coast Survey Reports, the American yard, and its subdivisions, the American foot and inch, and to consider it as a new standard similar to, but not identical with, the English imperial standard. (Coast Survey Report for 1853.)

In 1856, however, two copies of the new British standards, viz., a bronze standard, No. 11, and a wrought-iron standard, No. 57, were presented by the British govermnent to the United States. A series of elaborate comparisons of these new standards with the Troughton scale of 82 inches were made from 1876-1878 by Prof. J. E. Hilgard, now Superintendent of the Coast Survey, the results of which were published in 1880, in Appendix No. 12, of Report for 1877. These researehes prove that, taking into account the influence of the nature of the material of the standards, and using new, and more correct, coefficients for expansion by heat to reduce them to the same temperature, no material difference is found to exist between the American yard on the Troughton scale and the English imperial yard; only the Troughton scale at $62^{\circ} \mathrm{F}$. is 0.00083 inch longer than the imperial yard at $62{ }^{\circ} \mathrm{F}$. ; or, otherwise expressed, the mean yard of the United States at $59^{\circ} .62 \mathrm{~F}$. is equal to the British standard yard at $62^{\circ} \mathrm{F}$.

In confirmation of this conclusion it is well to remark that the value of the metre derived from Hassler's comparisons and reduced to $62^{\circ}$ by Prof. Bache, as above stated, when properly corrected with the new elements, stands as follows :-

Hassler's value of the metre reduced to $62^{\circ} \mathrm{F} . \quad=39.36851$ Eng. inches.
Correction for difference in rate of expansion + .00109 "
Correction for excess of Troughton scale in one metre +.00090 "
Hassler's comparison corrected reduction $\quad=39.37050 \quad$ " which is almost identical with Clarke's valne.

Thus the American yard, as a distinct one from the Engtish standard yard, is happily abolished. In consequence the tables for the conversion of the American yards and feet have been omitted in the present edition.
5. The Klufter of Vienna is a silver line let into a prismatic bar of iron, on which the length of the klafter was engraved by Voigtänder. It has its normal length at $13^{\circ}$ Ré mmur, and was declared by law, in 1816 , the standard Klafter of Vienna. On the same silver line the French toise is marked, from the standard toise sent, in 1760, by La Caille and La Condamine to the Observatory of Vienna. Comparisons made by lrof. Stamper with this standard gave for its value in metres 1 Klafter of Viema $=1.8366657$ metre, which value was universally used until about 1850.

New comparisons of the Vienna standard with various French standards deposited in the Russian Imperial Observatory, made in 1850 by the Astronomer W. Struve, with the utmost care and scientific precision, gave as a result

$$
1 \text { Klafter of Vienna }=1.8964843 \text { metre, }
$$

which value is now admitted as the most reliable. (Memoirs of the Austrian Acadeny of Sciences, vol. v. p. 117, and Sitzungs Berichte, Muthemut. Nutur-
wissench. Klasse, vol. xliv.) Struve's value has been adopted in computing the tables in this edition.
6. The Prussiun Foot is marked on a standard iron bar, 3 feet long, made by Pistor in Berlin; it is a standard at the temperature of $13^{\circ}$ Réaumur. The length of the Prussian foot was declared by law to be $=139.13$ lines of the toise du Pérou.
7. Spain and the old Spantish Colonies of America. The French metrical system of weights and measures was introduced into Spain by law in July, 1849 ; but its introduction was only finished in 1859. The old measures, however, continued to have a considerable local significance. Among the different values assigned to them the most important are those of the Castilian Vara, or Vara de Burgos, and of the Castilian foot, the relation of which to the metre is given officially in the Anuario de la Direccion de Hidrografia, Madrid, 1863, as follows :-

1 Castilian foot $=0.278635$ metre; hence
1 Castilian vara $=0.8359050$ metre
1 Castilian foot $=0.9141732$ English foot.
These values have been used in computing the tables in this fourth edition, in preference to the older ones, from which the tables in the previous editions were derived.

In the late Spanish Colonies of Mexico and South America the measures of the mother country continued to be in use after their separation from it. But owing, no doubt, to the imperfection of local standards, cousiderable divergences were found to exist, which caused no little confusion in the practical use of these measures. To obviate this inconvenience some of the States, as Mexico in 1862, Chile already in 1848, decreed the introduction of the French metric system. But as in practice the people continued to use the old measures, most of the States found it necessary to fix a legal value for the vara in relation to the metre. Thus Mexico determined by law, in 1845, the legal value of the Mexican vara to be

$$
\begin{aligned}
& 1 \text { vara }=0.838 \text { metre } ; \text { hence } \\
& 1 \text { Mexican foot }=0.2793333 \\
& 1 \text { Mexican foot }=0.9164645 \text { English foot. }
\end{aligned}
$$

Guatemala, San Salvador, Honduras, Nicaragua, Costa Rica use the Mexican rara and foot.

Arcording to Col. T. Ondarza, one of the authors of the official map of Bolivia, the Bolivian government has declared the value of the $\mathrm{S}_{\text {panish }}$ vara to be in the ratio of 100 metres $=118$ varas. This value was adopted by him in publishing his altitudes. Thus

$$
\begin{aligned}
& 1 \text { Bolivian vara }=1.18 \quad \text { metre; hence } \\
& 1 \text { Bolivian foot }=0.28248 .59 \quad \text { " } \\
& 1 \text { Bolivian foot }=0.92680776 \text { English foot. }
\end{aligned}
$$

Chile and Peru use the same value of the vara and foot as Bolivia. Venezuela, New Granada, and Ecuador have adopted a value of the vara very nearly equal to the old Caștilian, viz.:-

$$
\begin{aligned}
1 \text { vara } & =0.836 \quad \text { metre. } \\
1 \text { foot } & =0.278664 \quad \cdots \\
& 12
\end{aligned}
$$

New tables derived from the above values of the Spanish measures are given in this edition instead of those found in the previous ones.

In the Argentine Confederation, the Spanish vara was made

> 1 Spanish vara $=0.866 \quad$ metre ; hence
> 1 Spanish foot $=0.288667 \quad$ "
> 1 Spanish foot $=0.9470703$ English foot.

In Brazil the old Portuguese measures are still in force with only very slight changes for adjustment to the metre.
1 palmo $\quad=0.22000$ metre
1 vara, $\quad 5$ palmos $=1.1000$ metre or 1 metre $=3.030303$ vara.
1 foot, Pé, 1 $\frac{1}{2}$ palmos $=0.33000$ metre or 1 metre $=0.9090909$ foot, Pé.

The above information on the old Spanish measures is gathered from Belm's Geographisches Juhrbuch, Band I. and II. The three general "Tables for comparing the most important measures of length, of distances, and of surface," are taken from the same source.

At the head of each table will be found the value from which it was computed.
The tables give directly the reduction of any whole number not exceeding four figures, and larger numbers, within the limits needed for altitudes, by means of a single addition.

## Example.

Reduce 25,351 English feet into metres.
In Table XVII., on the line beginning with 25,000 and in the column headed 300 , take for
$25,300=7711.30$ metres.
In the second part of the table, on the line beginning' with 50 , and in column headed 1 , take for

$$
\text { English feet } \frac{51}{25,351}=\sqrt{3726.84} \quad "
$$

When Clarke's spheroid (1866) is used-
German mile $\quad=\frac{1}{15}$ equatorial degree $=7421.3802$ metres, $\log 3.87048468$
Nautical league $=\frac{1}{20}$ equatorial degree $=5566.0351$ metres, $\log 3.74554594$
French league $=\frac{1}{2}$ equatorial degree $=4452.8281$ metres, $\log 3.64863593$
Naut. or geog. mile $=\frac{1}{60}$ equatorial degree $=1855.3450$ metres, $\log 3.26842469$
The tables for the conversion of fathoms into metres, and for the conversion of metres into fathoms, need the following explanation: The exact equivalent of any desired depth in either measure between 100 and 9900 can be obtained directly from the table; for any depth below 100, the equivalent can be found by looking for the value corresponding to the same number as though it were hundreds, and then remove the decimal point the required number of places to the left.

## Example.

Reduce 62 fathoms to metres.
In the first line of the table under 600 we find 60 fathoms $=109.726$ metres.
In the first line of the table under 200 we find $2 \quad "=3.657$ "
Therefore 62 " $=113.383$ "

## E

 13
## TO CONVERT

## FRENCH TOISES

## INTO DIFFERENT MEASURES OF LENGTH.

1. CONVERSION OF FRENCH TOISES INTO METRES.

1 Toise $=1.94903631$ Metre .


1 Toise $=6.3945916$ English Feet .

| Toises. Teus. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | \%. | s. | 9. |
|  | Eus. feet | Eng. feet | Eng. feet | Eug. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet | Eng. fee | ng. feet |
| 0 | 0.000 | 6.395 | 12.789 | 19.184 | 25.578 | 31.973 | 38.368 | 44.763 | 51.157 | 57.551 |
| 10 | 63.946 | 70.340 | 76.735 | 83.130 | 89.524 | 95.919 | 102.313 | 108.708 | 115.103 | 121.497 |
| 20 | 127.592 | 134.286 | 140.681 | 147.076 | 153.470 | 159.865 | 166.259 | $17 \pm .654$ | 179.049 | 43 |
| 30 | 191.838 | 198.232 | 204.627 | 211.021 | 217.416 | 233.811 | 230.205 | 236.600 | 242.994 | 389 |
| 40 | 255.784 | 262.178 | 268.573 | 274.967 | 281.362 | 287.757 | 294.151 | 300.546 | 306.940 | 313.335 |
| 50 | 319.729 | 326.124 | 332.519 | 338.913 | 345.308 | 351.702 | 358.097 | 364.492 | 370.886 | 377.281 |
| 60 | 383.675 | 390.070 | $396.4{ }^{\text {c5 }}$ | 402.859 | 409.254 | 415.648 | 422.043 | 428.438 | 434.832 | 441.227 |
| 70 | 47.621 | 454.016 | 460.410 | 466.805 | 473.200 | 479.594 | 485.989 | 492.383 | 498.778 | 505.173 |
| 80 | 511.567 | 517.962 | 524.356 | 530.751 | 537.146 | . 43.540 | 549.935 | 556.329 | 562.724 | 569.119 |
| 90 | 575.513 | 581.90 s | 588.302 | 594.697 | 601.091 | 607.486 | 613.881 | 620.275 | 626.670 | 633.06 + |
| Thousands. | Handreds. |  |  |  |  |  |  |  |  |  |
|  | 0. | 100. | 200. | 300. | 100. | 500. | 600. | 700. | S00. | 900. |
|  | Eng. feet | Eus. feet | Eng. feet | Eng. feet | Eng. feet | Eog.feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet |
| 0 | 0.0 | 639.5 | 1278.9 | 1918.4 | 2557.8 | 3197.3 | 3836.8 | 4476.2 | 5115.7 | 5755.1 |
| 1000 | 6394.6 | 7034.0 | 7673.5 | 8313.0 | 8952.4 | 9591.9 | 10231.3 | 10870.8 | 11510.3 | 12149.7 |
| 2000 | 12789.2 | 13428.6 | 14068.1 | 14707.6 | 15347.0 | 15986.5 | 16625.9 | 17265.4 | 17904.9 | 18544.3 |
| 3000 | 19183.8 | 19823.2 | 20462.7 | 21102.1 | 21741.6 | 22381.1 | 23020.5 | 23660.0 | 24299.4 | 24938.9 |
| 4000 | -25578.4 | 26217.8 | 26857.3 | 327496.7 | 28136.2 | 28775.7 | 29415.1 | 30054.6 | 30694.0 | 31333.5 |
| 5000 | \|31972.9 | 32612. 4 | 33251.9 | 33891.3 | 34530.6 | 35170.2 | 35809.7 | 36449.2 | 37088.6 | 37725.1 |

IV. CONVERSION OF FRENCII TOISES INTO RHINE OR PRUSSIAN FEET.

1 Toise $=6.2100194$ Rhine Feet.

| Toises. <br> Tens. | Uuits. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | \%. | 8. | 9. |
|  | Rhine ft 0.000 | Rhine ft. 6.210 | Rhine ft. | Rhine ft. 18.630 | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. | Rhiue ft. 49.680 | Rhine ft. |
| 10 |  |  | 12.420 74.520 | 0 |  |  |  |  |  |  |
| 10 | 62.100 124.200 | 130.410 | 136.620 | 80.730 14.830 |  |  |  |  |  | ${ }^{\circ}$ |
| 20 | 124.200 | 130.410 | 136.620 | 142.830 | 149.040 | 155.250 | 161.461 |  |  | 1 |
| 30 | 186.301 | 192.511 | 198.721 | 204.931 | 211.141 | 217.351 | 223.561 | 229.771 | 235.981 | 242.191 |
| 40 | 248.401 | 254.611 | 260.821 | 267.031 | 273.241 | 279.451 | 285.661 | 291.871 | 298.081 | 304.291 |
| 50 | 310.501 | 316.711 | 322.921 | 329.131 | 335.341 | 341.551 | 347.761 | 353.971 | 360.181 | 366.391 |
| 60 | 372.601 | 378.811 | 385.021 | 391.231 | 397.441 | 403.651 | 409.861 | 416.071 | 42.281 | 428.491 |
| 70 | 434.701 | 440.911 | 447.121 | 453.331 | 459.541 | 465.751 | 471.961 | 478.171 | 484.382 | 490.592 |
| 80 | 496.802 | 503.012 | 509.222 | 515.432 | 521.642 | 527.852 | 534.062 | 540.272 | 546.482 | 552.692 |
| 90 | 558.90 | . 112 | 571.322 | 577.532 | 583.742 | 589.952 | 596.162 | 602 | 08.582 | 314.792 |
| Thousands. | Hundreds. |  |  |  |  |  |  |  |  |  |
|  | 0. | 100. | 200. | 300. | 409. | 500. | 680. | 700. | 500. | 900. |
|  | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. |
| 0 | 0.0 | 621.0 | 1242.0 | 1863.0 | 2484.0 | 3105.0 | 3726.0 | 4347.0 | 4968.0 | 5589.0 |
| 1000 | 6210.0 | 6831.0 | 7452.0 | 8073.0 | 8694.0 | 9315.0 | 9936.0 | 10570.0 | 11178.0 | 11799.0 |
| 2000 | 12420.0 | 13041.0 | 13662.0 | 14283.0 | 14904.0 | 15525.0 | 16146.1 | 16767.1 | 17388.1 | 18009.1 |
| 3000 | 18630.1 | 19251.1 | 19872.1 | 20493.1 | 21114.1 | 21735.1 | 22356.1 | 22977.1 | 23598.1 | 24219.1 |
| 4000 | 24840.1 | 25461.1 | 26082.1 | 26703.1 | 27324.1 | 27945.1 | 28566.1 | 29187.1 | 29808.1 | 30429.1 |
| 5000 | 31050.1 | $316 \% 1.1$ | 32292.1 | 32913.1 | 33534.1 | 34155.1 | 34776.1 | 35397.1 | 36018.1 | 36639.1 |

## TO CONVERT

## METRES

## into different measures of length.

1 LEGAL METRE $=443.296$ FRENCH OR PARIS LINES.
V. CONVERSION OF METRES INTO TOISES AND DECIMALS.

1 Metre $=0.513074074$ Toise.


1 Metre $=3.078444$ Paris Feet.

| Metres. <br> Tens. | res. Un |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr Feet. | Fr. Feet. |
| 0 | 0.00 | 3.05 | 6.16 | 9.24 | 12.31 | 15.39 | 18.47 | 21.55 | 24.63 | 27.71 |
| 10 | 30.78 | 33.86 | 36.94 | 40.02 | 43.10 | 46.18 | 49.26 | 52.33 | 55.41 | 58.49 |
| 20 | 61.57 | 64.65 | 67.73 | 70.30 | 73.88 | 76.96 | 80.04 | 83.12 | 86.20 | 89.27 |
| 30 | 92.35 | 95.43 | 98.51 | 101.59 | 104.67 | 107.75 | 110.82 | 113.90 | 116.98 | 120.06 |
| 40 | 123.14 | 126.22 | 129.29 | 132.37 | 135.45 | 138.53 | 141.61 | 144.69 | 147.77 | 150.84 |
| 50 | 153.92 | 157.00 | 160.08 | 163.16 | 166.24 | 169.31 | 172.39 | 175.47 | 178.55 | 181.63 |
| 60 | 184.71 | 187.79 | 190.86 | 193.94 | 197.02 | 200.10 | 203.18 | 206.26 | 209.33 | 212.41 |
| 70 | 215.49 | 218.57 | 221.65 | 224.73 | 227.80 | 230.88 | 233.96 | 237.04 | 240.12 | 243.20 |
| 80 | 246.28 | 249.35 | 252.43 | 255.51 | 258.59 | 261.67 | 264.75 | 267.82 | 270.90 | 273.98 |
| 90 | 277.06 | 280.14 | 283.22 | 286.30 | 289.37 | 292.45 | 295.53 | 298.61 | 301.69 | 304.77 |
| 100 | 307.84 | 310.92 | 314.00 | 317.08 | 320.16 | 323.24 | 326.32 | 329.39 | 332.47 | 335.55 |
| 110 | 338.63 | 341.71 | 344.79 | 347.86 | 350.94 | 354.02 | 357.10 | 360.18 | 363.26 | 366.33 |
| 120 | 369.41 | 372.49 | 375.57 | 378.65 | 381.73 | 384.81 | 387.88 | 390.96 | 394.04 | 397.12 |
| 130 | 400.20 | 403.28 | 406.35 | 409.43 | 412.51 | 415.59 | 418.67 | 421.75 | 424.83 | 427.90 |
| 140 | 430.98 | 434.06 | 437.14 | 440.22 | 443.30 | 446.37 | 449.45 | 452.53 | 455.61 | 458.69 |
| 150 | 461.77 | 464.85 | 467.92 | 471.00 | 474.08 | 477.16 | 480.24 | 483.32 | 486.39 | 489.47 |
| 160 | 492.55 | 495.63 | 498.71 | 501.79 | 504.86 | 507.94 | 511.02 | 514.10 | 517.18 | 520.26 |
| 170 | 523.34 | 526.41 | 529.49 | 532.57 | 535.65 | 538.73 | 541.81 | 544.88 | 547.96 | 551.04 |
| 180 | 554.12 | 557.20 | 560.28 | 563.36 | 566.43 | 569.51 | 572.59 | 575.67 | 578.75 | 581.83 |
| 190 | 584.90 | 587.98 | 591.06 | 594.14 | 597.22 | 600.30 | 603.38 | 606.45 | 609.53 | 612.61 |
| 200 | 615.69 | 618.77 | 621.85 | 624.92 | 628.00 | 631.08 | 631.16 | 637.24 | 640.32 | $6+3.39$ |
| 210 | 646.47 | 649.55 | 652.63 | 655.71 | 658.79 | 661.87 | $66+.94$ | 668.02 | 671.10 | 674.18 |
| 220 | 677.26 | 680.34 | 683.41 | 656.49 | 689.57 | 692.65 | 695.73 | 698.81 | 701.89 | 704.96 |
| 230 | 708.04 | 711.12 | 714.20 | 717.28 | 720.36 | 723.43 | 726.51 | 729.59 | 732.67 | 735.75 |
| 240 | 738.83 | 741.90 | 744.98 | 748.06 | 751.14 | 754.22 | 757.30 | 760.38 | 763.45 | 766.53 |
| 250 | 769.61 | 772.69 | 775.77 | 778.85 | 781.92 | 785.00 | 788.08 | 791.16 | 794.24 | 797.32 |
| 260 | 800.40 | 803.47 | 806.55 | S09.63 | 812.71 | 815.79 | 818.87 | 821.94 | 825.02 | 828.10 |
| 270 | 831.18 | 834.26 | 837.34 | S40.42 | 843.49 | 846.57 | 849.65 | 852.73 | 855.81 | 858.89 |
| 280 | 861.96 | 865.04 | 868.12 | \$71.20 | 874.28 | 877.36 | 880.43 | 883.51 | 886.59 | 889.67 |
| 290 | 892.75 | 895.83 | 898.91 | 901.98 | 905.06 | 908.14 | 911.22 | 914.30 | 917.38 | 920.45 |
| 300 | 923.53 | 926.61 | 929.69 | 932.77 | 935.85 | 938.93 | 942.00 | 945.08 | 948.16 | 951.24 |
| 310 | 954.32 | 957.40 | 960.47 | 963.55 | 966.63 | 969.71 | 972.79 | 975.87 | 978.95 | 982.02 |
| 320 | 95.50 | 988.18 | 991.26 | 994.34 | 997.42 | 1000.49 | 1003.57 | 1006.65 | 1009.73 | 1012.81 |
| 330 | 1015.89 | 1018.96 | 1022.04 | 1025.12 | 1028.20 | 1031.28 | 1034.36 | 1037.44 | 1040.51 | 1043.59 |
| 340 | 1046.67 | 1049.75 | 1052.83 | 1055.91 | 1058.98 | 1062.06 | 1065.14 | 1065.22 | 1071.30 | 1074.38 |
| 350 | 1077.46 | 1080.53 | 1083.61 | 1086.69 | 1089.77 | 1092.85 | 1095.93 | 1099.00 | 1102.08 | 1105.16 |
| 360 | 1108.21 | 1111.32 | 1114.40 | 1117.48 | 1120.55 | 1123.63 | 1126.71 | 1129.79 | 1132.87 | 1135.95 |
| 370 | 1139.02 | 1142.10 | 1145.18 | 1148.26 | $1151.3+$ | 1154.42 | 1157.49 | 1160.57 | 1163.6 .5 | 1166.73 |
| 350 | 1169.81 | 1172.89 | 1175.97 | 1179.04 | 1182.12 | 1185.20 | 1189.28 | 1191.36 | 1194.44 | 1197.51 |
| 390 | 1200.59 | 1203.67 | 1206.75 | 1209.83 | 1212.91 | 1215.99 | 1219.06 | 1222.14 | 1225.22 | 1225.30 |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1 Metre $=3.078444$ Paris Feet.

| Metres. <br> Tens. | Metres. Units |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. Feet. | Fr. F | Fr Feet. | Fr. Feet. |
| 400 | 1231.38 | 1234.46 | 1237.53 | 1240.61 | 1243.69 | 1246.77 | 1249.85 | 1252.93 | 1256.01 | 1259.05 |
| 410 | 1262.16 | 126.5.24 | 1268.32 | 1271.40 | 1274.18 | 1277.55 | 1280.63 | 1283.71 | 1286.79 | 1289.87 |
| 420 | 1292.95 | 1296.02 | 1299.10 | 1302.18 | 1305.26 | 1308.34 | 1311.42 | 1314.50 | 1317.57 | 1320.65 |
| 430 | 1323.73 | 1326.81 | 1329.59 | $1: 332.97$ | 1336.04 | 1339.12 | 1342.20 | 1345.28 | 1348.36 | 1351.44 |
| 440 | 1354.52 | 1357.59 | 1360.67 | 1363.75 | 1366.83 | 1369.91 | 1372.99 | 1376.06 | 1379.14 | 1352.22 |
| 450 | 1385.30 | 1388.38 | 1391.46 | 1394.54 | 1397.61 | 1400.69 | 1403.77 | 1406.85 | 1409.93 | 1413.01 |
| 460 | 1416.08 | 1419.16 | 1422.24 | 1425.32 | 1428.10 | 1431.48 | 1434.55 | 1437.63 | 1440.71 | 1443.79 |
| 470 | 1446.87 | 1449.95 | 1458.03 | 1456.10 | 1459.1 S | 1462.26 | 146.7 .34 | 1468.12 | 1471.50 | 1474.57 |
| 480 | 1477.65 | 1480.73 | 1483.81 | 1486.89 | 1489.97 | 1493.05 | 1496.12 | 1499.20 | 1502.28 | 1505.36 |
| 490 | 1503.44 | 1511.52 | 1514.59 | 1517.67 | 1520.75 | 1523.83 | 1526.91 | 1529.99 | 1533.07 | 1536.14 |
| 500 | 1539.22 | 1542.30 | 1545.38 | 1548.16 | 1551.54 | 1554.61 | 1.557 .69 | 1560.77 | 1563.85 | 1566.93 |
| 510 | 1570.01 | 1573.08 | 1576.16 | 1579.24 | 1582.32 | 158.5 .40 | 1588.48 | 1591.56 | 1594.63 | 1597.71 |
| 520 | 1600.79 | 1603.87 | 1606.95 | 1610.03 | 1613.10 | 1616.18 | 1619.26 | 1622.34 | 1625.42 | 1628.50 |
| 530 | 1631.58 | 1634.65 | 1637.73 | 1640.81 | 1643.89 | 1646.97 | 1650.05 | 1653.12 | 1656.20 | 1659.28 |
| 540 | 1662.36 | 1665.44 | 1668.52 | 1671.60 | 1674.67 | 1677.75 | I 680.83 | 1653.91 | 1686.99 | 1690.07 |
| 550 | 1693.14 | 1696.22 | 1699.30 | 1702.35 | 1705.46 | 1708.54 | 1711.61 | 1714.69 | 1717.77 | 1720.85 |
| 560 | 1723.93 | 1727.01 | 1730.09 | 1733.16 | 1736.24 | 1739.32 | 1742.10 | 1745.45 | 1748.56 | 1751.63 |
| 570 | 1751.71 | 1757.79 | 1760.87 | 1763.95 | 1767.03 | 1770.11 | 1773.18 | 1776.26 | 1779.34 | 1782.42 |
| 580 | 1785.50 | 1758.55 | 1791.65 | 1794.73 | 1797.81 | 1800.89 | 1803.97 | 1807.05 | 1810.13 | 1813.20 |
| 590 | 1816.38. | 1819.36 | 1522.44 | 1525.52 | 1528.60 | 1831.67 | 1834.75 | 1837.83 | 1840.91 | 1843.99 |
| 600 | 1847.07 | 18.50.14 | 1853.22 | 1556.30 | 1859.38 | 1862.46 | 1865.54 | 1868.62 | 1871.69 | 1874.77 |
| 610 | 1877.85 | 1880.93 | 1884.01 | 1587.09 | 1890.16 | 1893.24 | 1896.32 | 1899.10 | 1902.48 | 1905.56 |
| 620 | 1908.64 | 1911.71 | 1914.79 | 1917.87 | 1920.95 | 1924.03 | 1927.11 | 1930.18 | 1933.26 | 1936.34 |
| 630 | 1939.42 | 1942.50 | 1945.55 | 1948.66 | 1951.73 | 1954.81 | 1957.89 | 1960.97 | $196+.05$ | 1967.13 |
| 640 | 1970.20 | 1973.28 | 1976.36 | 1979.44 | 1982.52 | 1955.60 | 1988.67 | 1991.75 | 1994.83 | 1997.91 |
| 650 | 2000.99 | 2004.07 | 2007 | 2010.22 | 2013.30 | 2016.38 | 2019.46 | 2022.54 | 2025.62 | 2028.69 |
| 660 | 2031.77 | 2034.85 | 2037.9 | 2041.01 | 2044.09 | 2047.17 | 20.50 .24 | 2053.32 | 2056.40 | 2059.48 |
| 670 | 2062.56 | 2065.64 | 2068.7 | 2071.79 | 2074.87 | 2077.95 | 2081.03 | 2054.11 | 2087.19 | 2090.26 |
| 680 | 2093.34 | 2096.42 | 2099.50 | 2102.58 | 2105.66 | 2108.73 | 2111.81 | 2114.89 | 2117.97 | 2121.05 |
| 690 | 2124.13 | 2127.20 | 2130.28 | 2133.36 | 2136.44 | 2139.52 | 2142.60 | 2145.68 | 2148.75 | 2151.83 |
| 700 | 2154.91 | 2157.99 | 2161.07 | 2164.15 | 2167.22 | 2170.30 | 2173.38 | 2176.46 | 2179.54 | 2182.62 |
| 710 | 218.5 .70 | 2185.77 | 2191.85 | 2194.93 | 2198.01 | 2201.09 | 2204.17 | 2207.24 | 2210.32 | 2213.40 |
| 720 | 2216.48 | 2219.56 | 2222.64 | 2225.72 | 2228.79 | 2231.87 | 2234.95 | 2238.03 | $22+1.11$ | 2244.19 |
| 730 | 22.47 .26 | 22.30 .34 | 2253.42 | 22.56 .50 | 22.59..38 | 2262.66 | 2265.73 | 2268.81 | 2271.89 | 2274.97 |
| 740 | 2278.0.5 | 2281.13 | 2284.21 | 2287.28 | 2290.36 | 2293.44 | 2296.52 | 2299.60 | 2302.68 | 2305.75 |
| 750 | 2308.83 | 2311.91 | 2314.99 | 2318.07 | 2321.15 | 2324.23 | 2327.30 | 2330.38 | 2333.46 | 2336.54 |
| 760 | 2339.62 | 2342.70 | $23+5.77$ | 2348.85 | 23.11 .93 | 2355.01 | 2358.09 | 2361.17 | 2364.24 | 2367.32 |
| 770 | 2370.40 | 2373.48 | 2376.56 | 2379.64 | 2382.72 | 2385.79 | 2388.87 | 2391.95 | 2395.03 | 2398.11 |
| 780 | 2401.19 | 2404.26 | 2407.34 | 2410.42 | 2413.50 | 2416.58 | 2419.66 | 2122.74 | 2425.81 | 2428.89 |
| 790 | 2431.97 | 2435.05 | 2438.13 | 2441.21 | 2444.28 | 2447.36 | 2450.44 | 2453.52 | 2456.60 | 2459.68 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1 Metre $=3.0 \mathbf{7} 8444$ Paris Feet.


1 Metre $=3.23089917$ English Feet.

| Hetres. | Metres. (Units.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eug. Feet. | Eug. Feet. | Eng.Feet. | Eng. Feet. | Eng.Feet. | Eng.Feet. | Eng Feet. | Eng. Feet. | Eng Feet. | Eng. Fect. |
| 0 | 0.0 | 3.28 | 6.56 | 9.84 | 13.12 | 16.40 | 19.69 | 22.97 | 26.25 | 29.53 |
| 10 | 32.51 | 36.09 | 39.37 | 42.65 | 45.93 | 49.21 | 52.49 | 55.78 | 59.06 | 62.34 |
| 20 | 6.5 .62 | 68.90 | 72.15 | 75.46 | 78.74 | 82.02 | 85.30 | 88.58 | 91.87 | 95.15 |
| 30 | 98.13 | 101.71 | 104.99 | 108.27 | 111.55 | 114.83 | 118.11 | 121.39 | 124.67 | 127.96 |
| 40 | 131.24 | 134.52 | 137.80 | 141.08 | 14.36 | 147.64 | 150.92 | 154.20 | 157.48 | 160.76 |
| 50 | 164.04 | 167.33 | 170.61 | 173.89 | 177.17 | 180.45 | 183.73 | 187.01 | 190.29 | 193.57 |
| 60 | 196.85 | 200.13 | 203.42 | 206.70 | 209.98 | 213.26 | 216.54 | 219.82 | 223.10 | 226.38 |
| 70 | 299.66 | 232.94 | 236.22 | 239.51 | 242.79 | 246.07 | 249.35 | 252.63 | 255.91 | 259.19 |
| so | 262.17 | 265.75 | 269.03 | 272.31 | 275.60 | 278.88 | 282.16 | 255.44 | 288.72 | 292.00 |
| 90 | 295.28 | 293.56 | 301.84 | 305.12 | 308.40 | 311.69 | 314.97 | 318.25 | 321.53 | 324.81 |
| 100 | 328.09 | 331.37 | 334.65 | 337.93 | 341.21 | 344.49 | 347.78 | 351.06 | 354.34 | 357.62 |
| 110 | 360.90 | 364.18 | 367.46 | 370.74 | 374.02 | 377.30 | 380.58 | 388.87 | 387.15 | 390.43 |
| 120 | 393.71 | 396.99 | 400.27 | 403.55 | 406.83 | 410.11 | 413.39 | 416.67 | 419.96 | 423.24 |
| 130 | 426.52 | 129.50 | 433.08 | 436.36 | 439.64 | 442.92 | 446.20 | 4.49 .48 | 452.78 | 456.04 |
| 140 | 459.33 | 462.61 | 465.89 | 469.17 | 472.45 | 475.73 | 479.01 | 482.29 | 485.57 | 488.85 |
| 150 | 492.13 | 495.42 | 495.70 | 501.98 | 505.26 | 508.54 | 511.82 | 515.10 | 518.38 | 521.66 |
| 160 | 521.94 | 528.22 | 531.51 | 534.79 | 538.07 | 541.35 | 544.63 | 547.91 | 551.19 | 554.47 |
| 170 | 557.75 | 561.03 | 564.31 | 567.60 | 570.88 | 574.16 | $57 \% .44$ | 580.72 | 584.00 | 587.28 |
| 180 | 590.56 | 593.54 | 597.12 | 600.40 | 603.69 | 606.97 | 610.25 | 613.53 | 616.81 | 620.09 |
| 190 | 623.37 | 626.65 | 629.93 | 633.21 | 636.49 | 639.75 | 643.06 | 646.34 | 649.62 | 652.90 |
| 200 | 6.76 .18 | 659.46 | 662.74 | 666.02 | 669.30 | 672.58 | 675.87 | 679.15 | 682.43 | 685.71 |
| 210 | 688.99 | 692.27 | 695.55 | 698.83 | 702.11 | 705.39 | 708.67 | 711.96 | 715.24 | 718.52 |
| 220 | 721.50 | 725.08 | 728.36 | 731.64 | 734.92 | 738.20 | 741.48 | 744.76 | 748.05 | 751.33 |
| 230 | 754.61 | 757.89 | 761.17 | 764.45 | 767.73 | 771.01 | 774.29 | 777.57 | 780.85 | 784.13 |
| 240 | 787.42 | 790.70 | 793.98 | 797.26 | 800.54 | 803.82 | 807.10 | 810.38 | \$13.66 | 816.94 |
| 250 | 820.22 | 823.51 | 826.79 | 8:30.07 | 833.35 | S36.63 | 839.91 | 843.19 | 846.47 | 849.75 |
| 260 | 853.0:3 | 8.56 .31 | 559.60 | 862.85 | 866.16 | 869.44 | 872.72 | 876.00 | 879.28 | 882.56 |
| 270 | 855.54 | 889.12 | 892.40 | 595. 69 | 898.97 | 902.25 | 905.53 | 908.81 | 912.09 | 915.37 |
| 280 | 918.65 | 921.93 | 925.21 | 928.19 | 931.78 | 935.06 | 938.34 | 941.62 | 944.90 | 948.18 |
| 290 | 951.46 | 954.74 | 958.02 | 961.30 | 964.58 | 967.87 | 971.15 | 974.43 | 977.71 | 980.99 |
| 300 | 984.27 | 987.5.5 | 990.83 | 994.11 | 997.39 | 1000.67 | 1003.96 | 1007.24 | 1010.52 | 1013.80 |
| 310 | 1017.08 | 1020.36 | 1023.64 | 1026.92 | 1030.20 | 1033.48 | 1036.76 | 1040.05 | 1043.33 | 1046.61 |
| 320 | 1049.59 | 1053.17 | 10.56 .45 | 1059.73 | 1063.01 | 1066.29 | 1069.57 | 1072.85 | 1076.13 | 1079.42 |
| 330 | 1052.70 | 1085.98 | 1089.26 | 1092.54 | 1095.92 | 1099.10 | 1102.38 | 1105.66 | 1108.94 | 1112.22 |
| 340 | 1115.51 | 1118.79 | 1122.07 | 112.5.35 | 1128.63 | 1131.91 | 1135.19 | 1138.47 | 1141.75 | 1145.03 |
| 350 | 1148.31 | 1151.60 | 1154.88 | 1158.16 | 1161.44 | 1164.72 | 1168.00 | 1171.28 | 1174.56 | 1177.84 |
| 360 | 1181.12 | 1184.40 | 1157.69 | 1190.97 | 1194.25 | 1197.53 | 1200.81 | 1204.09 | 1207.37 | 1210.65 |
| 370 | 1213.93 | 1217.21 | 1220.49 | 1223.78 | 1227.06 | 1230.34 | 1233.62 | 1236.90 | 1240.18 | 1243.46 |
| 380 | 1246.74 | 1250.02 | 1253.30 | 1256.58 | 1259.87 | 1263.15 | 1266.43 | 1269.71 | 1272.99 | 1276.27 |
| 390 | 1279.55 | 1292.83 | 1286.11 | 1289.39 | 1292.67 | 1295.96 | 1299.24 | 1302.52 | 1305.80 | 1309.08 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

400 to $\mathbf{8 9 9}$.


800 to 1199.

| Metros. | Metres. (Units.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng.Feet. | Eng.Feet. | Eng.Feet. | Eng. Ftet. | Eug. Feet. | Eng.Feet. | Eng.Feet. | Eug. Feer. | Eng.Fet. | Eng.Feet. |
| S00 | 2624.72 | 2628.00 | 2631.25 | 2634.56 | $26: 37.84$ | 2641.12 | 2644.40 | 2647.69 | 2650.97 | 2654.25 |
| 810 | 2657.53 | 2660.81 | 2664.09 | 2667.37 | 2670.65 | 2673.93 | 2677.21 | 2680.49 | 2683.78 | 2687.06 |
| S20 | 2690.34 | 2693.62 | 2696.90 | 2700.18 | 2703.46 | 2706.74 | 2710.02 | 2713.30 | 2716.55 | 2719.87 |
| 830 | 2723.15 | 2726.43 | 2729.71 | 2732.99 | 2736.27 | 2739.55 | 2742.83 | 2746.11 | 2749.39 | 2752.67 |
| 840 | 2755.96 | 2759.24 | 2762.52 | 2765.50 | 2769.08 | 2772.36 | 2775.64 | 2778.92 | 2782.20 | 2785.48 |
| 850 | 2788.76 | 2792.05 | 2795.33 | 2798.61 | 2501.89 | 2505.17 | 2808.45 | 2811.73 | 2815.01 | 2818.29 |
| 860 | 2821.57 | 2824.85 | 2825.14 | 2-31.42 | 2834.70 | 2837.98 | 2841.26 | 2844.54 | 28.47 .82 | 2551.10 |
| 870 | 2854.38 | 28.57 .66 | 2860.94 | 2864.22 | 2867.51 | 2870.79 | 2874.07 | 2577.55 | 2880.63 | 2883.91 |
| 880 | 2887.19 | 2590.47 | 2893.75 | 2597.03 | 2900.31 | 2903.60 | 2906.88 | 2910.16 | 2913.44 | 2916.72 |
| 890 | 2920.00 | 2923.28 | 2926.56 | 2929.54 | 2933.12 | 2936.40 | 2939.69 | $29+2.97$ | 2946.25 | 2949.53 |
| 900 | 29.92.81 | 2956.09 | 2959.37 | 2962.65 | 2965.93 | 2969.21 | 2972.49 | 2975.78 | 2979.06 | 2982.34 |
| 910 | 2985.62 | 2985.90 | 2992.15 | 2995.46 | 2998.74 | 3002.02 | 3005.30 | 3005.58 | 3011.57 | 3015.15 |
| 920 | 3018.43 | 3021.71 | 3024.99 | 3028.27 | 8031.55 | 3034.53 | 3035.11 | 3041.89 | $30+4.67$ | 3047.96 |
| 930 | 3051.24 | 3054.52 | 3057.80 | 3061.05 | 3064.36 | 3067.64 | 3070.92 | 307420 | 3077.4 | 3080.76 |
| 940 | 3084.05 | 3087.33 | 3090.61 | 3093.89 | 3097.17 | 3100.45 | 3103.7 \% | 3107.01 | 3110.29 | 3113.57 |
| 950 | 3116.85 | 3120.14 | 3123.42 | 3126.70 | 3129.98 | 3133.26 | 3136.54 | 3139.82 | 3143.10 | 3146.38 |
| 960 | 3149.66 | 3152.94 | 3156.22 | 3159.51 | 3162.79 | 3166.07 | 3169.3.5 | 3172.63 | :3175.91 | 3179.19 |
| 980 | 3182.47 | 3185.75 | :159.03 | 3192.31 | 3195.60 | 3198.8s | 3202.16 | 3205.44 | 3208.72 | 3212.00 |
| 980 | 3215.28 | 3218.56 | 3221.84 | 3225.12 | 3228.40 | 3231.69 | 3234.97 | 32:38.25 | 3241.53 | 3244.81 |
| 990 | 3248.09 | 3251.37 | 32.54 .65 | 3257.9:3 | 3261.21 | :3264.49 | 3267.75 | 3271.06 | 3271.34 | 3277.62 |
| 1000 | 3280.90 | 3294.18 | 3287.46 | 3290.74 | 3291.02 | 3297.30 | 3300.58 | 3309.87 | 3307.15 | 3310.43 |
| 1010 | 3:313.71 | 3316.99 | 3320.27 | 3323.55 | 3326.83 | 3330.11 | 3333.89 | 3336.67 | 3339.96 | 3343.24 |
| 1020 | 3346.52 | $33+9.80$ | 3353.08 | 3356.36 | 3359.64 | 3362.92 | 3366.20 | 3369.48 | 3372.76 | 3376.05 |
| 1030 | 3:799.33 | 3382.61 | 3385.89 | 3389.17 | 3392.45 | 3395.73 | 3399.01 | 3402.29 | 3405.57 | 3108.85 |
| 10.40 | 3412.14 | 3415.42 | 3418.70 | 3421.98 | 3425.26 | 3428.54 | 3431.82 | 343.5.10 | 3438.38 | 3441.66 |
| 1050 | 344.94 | 3448.22 | :3551.51 | 34.54.79 | 3458.07 | 3461.35 | 3464.63 | 3167.91 | 3471.19 | 3474.47 |
| 1060 | 3177.7 .3 | 3481.03 | 3484.31 | 3157.60 | 3490.88 | 3494.16 | 3497.44 | 3500.72 | 3504.00 | 3507.28 |
| 10\%0 | 3.510 .56 | 3.513 .84 | 3.517 .12 | 3520.40 | 35.3 .69 | 3526.97 | $35: 30.25$ | 3533.53 | 3536.81 | 3540.09 |
| 1080 | 3543.37 | 3.546 .65 | 3549.93 | 3353.21 | 3556.19 | 35.59 .78 | 356:3.06 | 3566.34 | 3569.62 | 3572.90 |
| 1090 | 3576.18 | 3379.16 | 3582.74 | 3586.02 | 3589.3 ) | 3592.58 | 3595.87 | 3599.15 | 3602.43 | 3605.71 |
| 1100 | 3608.99 | 3612.27 | 3615.5 .5 | 3618.83 | 3622.11 | 3625.39 | 3628.67 | 3631.96 | 3635.24 | 3638.52 |
| 1110 | 3641.50 | 3645.08 | $36+8.36$ | 3651.64 | 3654.92 | 36.5. 20 | 36661.48 | 3664.76 | 3668.05 | 3671.33 |
| 1120 | 3671.61 | 3677.59 | 3681.17 | 3684.45 | 3687.73 | 3691.01 | :3694.29 | 3697.57 | 3700.85 | 3704.14 |
| 1130 | 3707.42 | 3710.70 | 3713.98 | 3717.26 | 3720.54 | 3723.52 | 3827.10 | 37:30 38 | 3733.66 | 3736.94 |
| 1140 | 3740.22 | 3743.51 | 3746.79 | 3750.07 | 3753.35 | 37.66 .63 | 3759.91 | 37663.19 | 3766.47 | 3769.75 |
| 1150 | 3773.03 | 377631 | 3779.60 | 3782.88 | 3786.16 | 3759.44 | 3792.72 | 3796.00 | 3799.28 | 3802.56 |
| 1160 | 3805.84 | 3809.12 | 3812.40 | 381.5.69 | 3818.97 | 3820.25 | 3255.53 | 3828.81 | 3832.09 | 3835.37 |
| 1170 | 3838.65 | 3841.93 | 3845.21 | 3848.49 | 3851.78 | 3855. 06 | 38.58.:3 4 | 3561.62 | 3564.90 | 3868.18 |
| 1180 | 3571.46 | 3574.71 | 3878.02 | 3581.30 | 3854.58 | 3587.87 | 3891.15 | 3594.43 | 3597.71 | 3900.99 |
| 1190 | 3904.27 | 3907.55 | 3910.83 | 3914.11 | 3917.39 | 3920.67 | 3923.96 | 3927.24 | 3930.52 | 3933.80 |
|  | (. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

1200 to 1599.

| Metres. | Metres. (Units.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng.Feet. | Eng.Feet. | Eng.Feet. | Eng. Feet. | Fing. Feet. | Eng. Feet. | Eng. Feet. | Eng.Feet. | Eng.Feet. | Eng.Feet. |
| 1200 | 3937.08 | 3940.36 | 3943.64 | 3946.92 | 395020 | 39.35 .45 | 3956.76 | 3960.05 | 3963.33 | 3966.61 |
| 1210 | 3969.59 | 3973.17 | 3976.45 | 3979.73 | 3983.01 | 3986.29 | 3989.57 | 3992.85 | 3996.14 | 3999.42 |
| 1220 | 4002.70 | 1005.98 | 4009.26 | 4012.54 | 4015.82 | 4019.10 | 1022.38 | 4025.66 | 4028.94 | 4032.23 |
| 1230 | 4035.51 | 40:38.79 | $40+2.07$ | 4015.35 | 4048.63 | 4051.91 | 405.5.19 | 1058.47 | 1061.75 | 1065.03 |
| 1240 | 4068.31 | 4071.60 | 4074.88 | 4078.16 | 4081.44 | 4054.72 | 1088.00 | 4091.28 | $409+.56$ | 4097.84 |
| 12.50 | 4101.12 | 4104.40 | 4107.69 | 1110.97 | 4111.25 | 4117.53 | 4120.81 | 4124.09 | 4127.37 | 4130.6 .3 |
| 1260 | +133.93 | 4137.21 | 4140.49 | 4143.78 | 4147.06 | 4150.34 | 4153.62 | 4156.90 | 4160.18 | 4163.46 |
| 1270 | 4166.74 | 4170.02 | 4173.30 | 4176.58 | 4179.87 | 4853.15 | 4186.43 | 4189.71 | 4192.99 | 4196.27 |
| 1250 | 4199.5 .5 | 4202.83 | 4206.11 | 4209.39 | 4212.67 | 4215.96 | 4219.24 | 1222.52 | 4225.50 | 1299.68 |
| 1290 | 4232.36 | 4235.64 | 4238.92 | 4212.20 | 4245.48 | 4248.76 | 4252.05 | 4255.33 | 4255.61 | 4261.59 |
| 1300 | 4265.17 | 4268.45 | 4271.73 | 4275.01 | 4278.29 | 4281.57 | 4284.55 | 4288.14 | 4291.42 | 4294.70 |
| 1310 | 4297.98 | 4301.26 | 4304.54 | 4307.82 | 4311.10 | 4314.35 | 4317.66 | 4320.94 | 4324.23 | 4327.51 |
| 1320 | 4330.79 | 4334.07 | 4337.35 | 4340.63 | 4343.91 | 4347.19 | 4350.47 | 4353.75 | 4357.03 | 4360.31 |
| 1330 | 4363.60 | 1366.88 | 4370.16 | 4373.44 | 4376.72 | 4380.00 | 4383.28 | 4386.56 | 4359.84 | 4393.12 |
| 1340 | 4396.40 | 4399.69 | 4402.97 | 4406.25 | 4409.53 | 4412.81 | 416.09 | 4419.37 | 4.122 .65 | 425.93 |
| 1350 | 4429.21 | 4432.49 | 4435.78 | 4439.06 | 4 42.34 | 4455.62 | 4448.90 | 4452.18 | 445.56 | 4458.74 |
| 1360 | 4462.02 | 465.30 | 4468.58 | 4471.87 | 4775.15 | 4478.43 | 481.71 | 4484.99 | +189.27 | 4491.55 |
| 1370 | 449 4.83 | 4493.11 | 4501.39 | 4504.67 | 4507.96 | 4511.24 | 4514.52 | 4517.80 | 4521.08 | 4524.36 |
| 1380 | 4.227 .64 | 4530.92 | 4534.20 | 4537.48 | 4540.76 | 4544.05 | 4547.33 | 4.50 .61 | 4553.69 | 4.57 .17 |
| 1390 | 4560.45 | 4563.73 | 4567.01 | 4570.29 | 4573.57 | 4576.85 | 4580.14 | 4583.42 | 4586.70 | 4589.98 |
| 1400 | 4593.26 | 4596.54 | 4599.82 | 4603.10 | 4606.38 | 4609.66 | 461294 | 4616.23 | 4619.51 | 4622.79 |
| 1410 | 4626.07 | 4629.35 | 4632.63 | 4635.91 | 4639.19 | 4642.47 | 4645.75 | $46+9.03$ | 4652.31 | 4655.60 |
| 1420 | 46.58 .88 | 4662.16 | 466.5.44 | 4668.72 | 4(672.00 | 4675.28 | 4678.56 | 4681.84 | 4655.12 | 4688.40 |
| 1430 | 4691.69 | 4694.97 | 4698.25 | 4701.53 | 4704.81 | 4708.09 | 4711.37 | 4714.65 | 4717.93 | 4721.21 |
| 1440 | 4724.49 | 4727.78 | 4731.06 | 4734.34 | 4737.62 | 4740.90 | 4744.18 | 4747.46 | 4750.74 | 4754.02 |
| 1450 | 4757.30 | 4760.58 | 4763.87 | 4767.15 | 4770.43 | 4773.71 | 4776.99 | 4780.27 | 4783.55 | 4786.83 |
| 1460 | 4790.11 | 4793.39 | 4796.67 | 4799.96 | 4803.24 | 4806.52 | 4809.50 | 4813.08 | 4816.36 | 1819.64 |
| 1470 | 4522.92 | 1826.20 | 4829.48 | 4832.76 | 4836.05 | 4839.33 | 48.2 .61 | 4845.89 | 4849.17 | 4852.45 |
| 1480 | 455.73 | 4859.01 | 4862.29 | 486.5 .57 | 1268.85 | 4872.14 | 4875.42 | 4878.70 | 4881.98 | 4885.26 |
| 1490 | 4588.54 | 4891.s2 | 1595.10 | 4898.38 | 4901.66 | 4904.94 | 4908.23 | 4911.51 | 4914.79 | 4918.07 |
| 1500 | 4921.3 .5 | 4924.63 | 4927.91 | 4931.19 | 4934.47 | 4937.75 | 4941.03 | 4944.31 | 4947.60 | 4950.85 |
| 1510 | 49.4 .16 | 4957.44 | 4960.72 | 4964.00 | 4967.28 | 4970.56 | 4973.84 | 4977.12 | 4980.40 | 4983.69 |
| 1.520 | 4986.17 | 4990.25 | 4993.53 | 4996.81 | 5000.09 | 5003.37 | 5006.65 | 5009.93 | 5013.21 | . 3016.49 |
| 1530 | 5019.78 | 5023.06 | 5026.34 | 5029.62 | 5032.90 | 5036.18 | 5039.46 | 5042.74 | 5016.02 | 5049.30 |
| 1540 | 50.52.5S | 5055.87 | 5059.15 | 5062.43 | 506.5 .71 | .5068.99 | 5072.27 | 5075.55 | 5078.53 | 5082.11 |
| 15.50 | 5085.39 | 5058.67 | 5091.96 | 509.5.24 | 5098.52 | 5101.80 | 510.5.08 | 5108.36 | 5111.64 | 5111.92 |
| 1.560 | 5118.20 | 5121.48 | 5124.76 | 5128.05 | 51:31.33 | 513161 | 5137.59 | 5141.17 | 5144.45 | 5147.73 |
| 1570 | 5151.01 | 5154.29 | 5157.57 | 5160.55 | 5164.14 | 5167.42 | 5170.70 | 5173.98 | 5177.26 | 5180.51 |
| 1580 | 5183.82 | 5187.10 | 5190.38 | 5193.66 | 5196.94 | 5200.23 | 5203.51 | 5206.79 | 5210.07 | 5213.35 |
| 1590 | 5216.63 | 5219.91 | 5223.19 | 5226.17 | 5229.75 | 5233.03 | 5236.32 | 5239.60 | . 2242.88 | 5246.16 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7 . | 8. | 9. |

1600 to 2000.

| Metres. | Metres. (Units.) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng. Feet. | Eug. Feet. | Eng. Feet. | Eng. Feet. | Enr Feet. | Eng.Feet. | Fing. Feet. | Eug. Feet. | Eng Feet. | Fug. Feet. |
| 3600 | 5249.44 | 5252.72 | 5256.00 | 5259.25 | 5262.56 | 5265.84 | 5269.12 | 5272.40 | 5275.69 | 5275.97 |
| 1610 | 5282.25 | 525.5 .53 | 5288.51 | 5292.09 | 5295.37 | 5298.65 | 5301.93 | 5305.21 | 5305.49 | 5311.78 |
| 1620 | 5315.06 | 5:315.34 | 5321.62 | 5324.90 | 532\%.1s | 5331.46 | 5334.74 | 5338.02 | 5341.30 | $53+4.58$ |
| 1630 | 5347.87 | 53.51.15 | 5354.43 | 5357.71 | 5360.99 | 5364.27 | 5367.55 | 5370.85 | 5371.11 | 5377.39 |
| 1640 | 5350.67 | 5383.96 | 5357.24 | 5390.52 | 5393.50 | 5397.08 | 5400.36 | 5403.64 | 5406.92 | 5410.20 |
| 1650 | 5413.18 | 5416.76 | 5420.0 .5 | 5423.33 | 5426.61 | 5429.59 | 5433.17 | 5436.45 | 5439.73 | 5443.01 |
| 1660 | 5416.29 | 5449.57 | 5452.85 | 5456.14 | 54.59 .42 | 5.462 .70 | 5465.98 | 5469.26 | 5472.54 | 5475.82 |
| 1670 | 5479.10 | 5482.38 | 5485.66 | 5488.9 .4 | $5492 \cdot 2: 3$ | 549.5 .51 | 5495.79 | 5502.07 | 5505.35 | 5508.63 |
| 1680 | 5511.91 | 5515.19 | 5515.47 | 5521.75 | 5525.03 | 5528.32 | 5531.60 | 5534.88 | 5538.16 | 55.11 .44 |
| 1690 | 5544.72 | 5548.00 | 5551.28 | 5554.56 | 5557.84 | 5561.12 | 5564.40 | 5567.69 | 5570.97 | 5574.25 |
| 1700 | 5577.33 | 5590.81 | 5584.09 | 5587.37 | 5590.65 | 5593.93 | 5597.21 | 5600.49 | 5603.78 | 5607.06 |
| 1710 | 5610.34 | 5613.62 | 5616.90 | 5620.18 | 5623.46 | 5626.74 | 5630.02 | 5633.30 | 5636.58 | 5639.57 |
| 1720 | 5643.15 | 5646.43 | 5649.71 | 5652.99 | 56.56 .27 | 5659.55 | 5662.83 | 5666.11 | 5669.39 | 5672.67 |
| 1730 | 5675.96 | 5679.24 | 5682.52 | 5685.80 | 5689.08 | 5692.36 | 5695.64 | 5698.92 | 5702.20 | 5705.48 |
| 1740 | 5708.76 | 5712.05 | 5715.33 | 5718.61 | 5721.89 | 5725.17 | 5728.45 | 5731.73 | 5735.01 | 5738.29 |
| 1750 | 5741.57 | 5744.85 | 5718.14 | 5751.42 | 5754.70 | 5757.98 | 5761.26 | 5764.54 | 5767.82 | 5771.10 |
| 1760 | 5774.38 | 5777.66 | 5780.94 | 5784.23 | 5757.51 | 5790.79 | 5794.07 | 5797.35 | 5800.63 | 5803.91 |
| 1770 | 5807.19 | 5810.47 | 5813.75 | 5S17.03 | 5820.32 | 5 5 23.60 | 5826.88 | 5830.16 | 5833.14 | 5836.72 |
| 1780 | 5840.00 | . 8483.28 | 5846.56 | 5849.84 | 5853.12 | 58.66 .10 | 5859.69 | 5862.97 | 5866.25 | 5869.53 |
| 1790 | 5872.81 | 5576.09 | 5879.37 | 5882.65 | 5555.93 | 5889.21 | 5892.49 | 5895.78 | 5899.06 | 5902.34 |
| 1800 | 5905.62 | 5908.90 | 5912.18 | 5915.46 | 5918.74 | 5922.02 | 5925.30 | 5928.58 | 5931.87 | 5935.15 |
| 1810 | 59:35.13 | 5941.71 | $59+4.99$ | $59+8.27$ | 5951.55 | 5954.53 | 5958.11 | 5961.39 | 5964.67 | 5967.96 |
| 1520 | 5971.24 | 5974.52 | 5977.80 | 5981.08 | 5984.36 | 5987.64 | 5990.92 | 5994.20 | 5997.48 | 6000.76 |
| 1830 | 6004.0 .5 | 6007.3: | 6010.61 | 6013.89 | 6017.17 | 6020.45 | 6023.73 | 6027.01 | 6030.29 | 6033.57 |
| 1840 | 60:36.85 | 6010.14 | 6043.42 | 6046.70 | 6049.98 | 6053.26 | 6056.54 | 6059.82 | 6063.10 | 6066.38 |
| 1850 | 6069.66 | 6072.94 | 6076.23 | 6079.51 | 6082.79 | 6086.07 | 6089.35 | 6092.63 | 6095.91 | 6099.19 |
| 1560 | 6102.17 | 610.7.75 | 6109.03 | 6112.32 | 6115.60 | 6118.58 | 6122.16 | (i125.44 | 6128.72 | 6132.00 |
| 1870 | 613.5 .28 | 61:88.56 | 6141.84 | 6145.12 | 6148.40 | 6151.69 | 61.54 .97 | 6155.25 | 616].53 | 6164.81 |
| 1880 | 6168.09 | 6171.37 | 6174.65 | 6177.93 | 6181.21 | 6184.19 | 6187.78 | 6191.06 | 6194.34 | 6197.62 |
| 1890 | 6200.90 | 6204.15 | 6207.46 | 6210.74 | 6214.02 | 621730 | 6230.58 | 6223.87 | 6227.15 | 6230.43 |
| 1900 | 6233.71 | 6236.99 | 6240.27 | 6243.55 | 6246.83 | (62.50.1] | 62.53 .39 | 6256.67 | 6259.96 | 6263.24 |
| 1910 | 6266.52 | 6269.80 | 6273.08 | 6276,36 | 6279.6 .1 | 6282.92 | 6286.20 | 62-9.18 | 6292.76 | 6296.05 |
| 1920 | 6299.3: | 6302.61 | 630589 | 6309.17 | $6: 312.15$ | (331.5.7:3 | 6.929 .01 | 6322.29 | 6325.57 | 63.28 .85 |
| 1930 | 633214 | 63:3.7. 42 | 6338.70 | 6341.98 | 6345.26 | 6315.54 | 6.351 .82 | 6355.10 | 6358.38 | 6361.66 |
| 1940 | 6364.94 | 6368.23 | 6371.51 | 6374.79 | 6375.07 | 63.1 .35 | 6354.63 | 6387.91 | 6391.19 | 6394.47 |
| 19.70 | 6397.75 | 16101.03 | 6104.32 | 6407.60 | 6130.88 | 6414.16 | (i417.44 | 6120.72 | 6424.00 | 6127.28 |
| 1960 | 6430.56 | 6433.84 | 6137.12 | $6 \pm 40.41$ | 6443.69 | 6446.97 | 6450.2 .5 | 6453.53 | 6456.81 | 6460.09 |
| 1970 | 6463.37 | 6466.65 | 6469.93 | 6473.21 | 6.476.49 | 6479.78 | 648:3.06 | $6486.3+$ | 6489.62 | 6492.90 |
| 1980 | 6196.18 | 6499.4t | 6502.74 | 6506.02 | 6.509 .30 | 6.512 .58 | 6.515 .87 | 6.119 .15 | 6522.43 | 6525.71 |
| 1990 | 6528.99 | 6.532 .27 | 6535.5 .5 | 6538.83 | 6542.11 | 6.545 .39 | 6.548 .67 | 6.551 .96 | 65.55 .24 | 6558.52 |
| 2000 | 6561.80 | 6565.08 | 6568.36 | 6571.64 | 6.574 .92 | 6.578 .20 | 6.581 .48 | 6584.76 | 6588.05 | 6591.33 |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

2000 to $\mathbf{2 3 9 9}$.

| Metres. | Metrea. (Units) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. |  |  | 7. | 8. | 9. |
|  | Eng.Feet. | Eng.Feet. | Eng.Feet. | Eng.Feet. | Eng. Feel | Eng.Feet | Eng. | Ig.Feet | Eug.Feet. | Eny Fret. |
| 2000 | 6561.80 | 6565.08 | 6568.36 | 6571.64 | 6574.92 | 6578.20 | 6581.18 | 6554.76 | 6588.05 | 6591.33 |
| 2010 | 6594.61 | 6597.89 | 6601.17 | 6604.45 | 6607.73 | 6611.01 | 6614.29 | 6617.57 | 6620.85 | 6624.14 |
| 2020 | 662742 | 6630.70 | 6633.98 | 6637.26 | 6640.54 | 6643.82 | 6647.10 | 6650.38 | 6653.66 | 6656.94 |
| 2030 | 6660.23 | 6663.51 | 6666.79 | 6670.07 | 6673.35 | 6676.63 | 6679.91 | 6653.19 | 6686.47 | 6659.75 |
| 2040 | 6693.03 | 6696.32 | 6699.60 | 6702.88 | 6706.16 | 6709.44 | 6712.72 | 6716.00 | 6719.25 | 6722.56 |
| 2050 | 6725.84 | 6729.12 | 6732.41 | 6735.69 | 6738.97 | 6742.25 | 6745.53 | 6748.81 | 6752.09 | 6755.37 |
| 2060 | 6758.65 | 6761.93 | 6765.21 | 6768.49 | 6771.78 | 6775.06 | 6778.34 | 6781.62 | 6784.90 | 6755.18 |
| 2070 | 6791.46 | 6794.74 | 6798.02 | 6801.30 | 6804.58 | 6807.87 | 6811.15 | 6814.43 | 6817.71 | 6820.99 |
| 2080 | 6824.27 | 6527.55 | 6830.83 | 6834.11 | 6837.39 | 6840.67 | 6843.96 | 6847.24 | 6850.52 | 6853.80 |
| 2090 | 6857.08 | 6860.36 | 6563.64 | 6866.92 | 6870.20 | 6873.48 | 6576.76 | 6880.05 | 6883.33 | 6886.61 |
| 2100 | 6889.89 | 6893.17 | 6896.45 | 6899.73 | 6903.01 | 6906.29 | 6909.57 | 6912.85 | 6916.14 | 6919.42 |
| 2110 | 6922.70 | 6925.98 | 6929.26 | 6932.54 | 6935.82 | 6939.10 | 69 12.38 | 6945.66 | 6948.94 | 6952.23 |
| 2120 | 695.51 | 6958.79 | 6962.07 | 6965.35 | 6968.63 | 6971.91 | 6975.19 | 6978.47 | 6981.75 | $698 . \overline{0} 03$ |
| 2130 | 6988.32 | 6991.60 | 6994.88 | 6998.16 | 7001.44 | 7004.72 | 7008.00 | 7011.28 | 7014.56 | 7017.84 |
| 2140 | 7021.12 | 7024.41 | 7027.69 | 7030.97 | 7034.25 | 7037.53 | 7040.81 | 7044.09 | 7047.37 | 7050.65 |
| 2150 | 7053.93 | 7057.21 | 7060.49 | 7063.78 | 7067.06 | 7070.34 | 7073.62 | 7076.90 | 7080.18 | 7083.46 |
| 2160 | 7086.74 | 7090.02 | 7093.30 | 7096.58 | 7099.87 | 7103.15 | 7106.43 | 7109.71 | 7112.99 | 7116.27 |
| 2170 | 7119.55 | 7122.83 | 7125.11 | 7129.39 | 7132.67 | 7135.96 | 7139.24 | 7142.52 | 7145.80 | 7149.08 |
| 2180 | 7152.36 | 7155.64 | 7158.92 | 7162.20 | 7165.48 | 7168.76 | 7172.05 | 7175.33 | 7178.61 | 7181.89 |
| 2190 | 7185.17 | 7188.45 | 7191.73 | 7195.01 |  | 7201.57 | 7204.85 | 7208.14 | 7211.42 | 7214.70 |
| 2200 | 7217.98 | 7221.26 | 7224.54 | 7227.82 | 7231.10 | 7234.3 | 7237.66 | 7240.94 | 7244.23 | 7247.51 |
| 2210 | 7250.79 | 7254.07 | 7257.35 | 7260.63 | 7263.91 | 7267.19 | 7270.47 | 7273.75 | 7277.03 | 7250.32 |
| 2220 | 7283.60 | 7286.88 | 7290.16 | 7293.44 | 7296.72 | 7300.00 | 7303.28 | 7306.56 | 7309.84 | 7313.12 |
| 2230 | 7316.41 | 7319.69 | 7322.97 | 7326.25 | 7329.53 | 7332.81 | 7336.09 | 7339.37 | 7342.65 | 7345.93 |
| 2240 | 7349.21 | 7352.49 | 7355.78 | 7359.06 | 7362.34 | 7365.62 | 7368.90 | 7372.18 | 7375.46 | 7378.74 |
| 2250 | 7382.02 | 7385.30 | 7388.58 | 7391.87 | 7395.15 | 7398.43 | 7401.71 | 7404.99 | 7408.27 | 7411.55 |
| 2260 | 7414.83 | 7418.11 | 7421.39 | 7424.67 | 7427.96 | 7431.24 | 7434.52 | 7437.80 | 7441.05 | 744.36 |
| 2270 | 7447.64 | 7450.92 | 7454.20 | 7457.48 | 7460.76 | 7464.05 | 7467.33 | 7470.61 | 7473.89 | 7477.17 |
| 2280 | 7480.45 | 7483.73 | 7487.01 | 7490.29 | 7493.57 | 7496.85 | 7500.14 | 7503.42 | 7506.70 | 7509.98 |
| 2290 | 7513.26 | 7516.54 | 7519.82 | 7523.10 | 7526.38 | 7529.66 | 7532.94 | 7536.23 | 7539.51 | 7542.79 |
| 2300 | 7546.07 | 7549.35 | 7552.64 | 7555.91 | 7559.19 | 7562.47 | 7565.75 | 7569.03 | 7572.32 | 7575.60 |
| 2310 | 7578.85 | 7582.16 | 7585.44 | 7588.72 | 7592.00 | 7595.28 | 7598.56 | 7601.84 | 7605.12 | 7608.41 |
| 2320 | 7611.69 | 7614.97 | 7618.25 | 7621.53 | 7624.81 | 7628.09 | 7631.37 | 7634.65 | 7637.93 | 7641.21 |
| 2330 | 7644.50 | 7647.78 | 7651.06 | 7654.34 | 76.37 .62 | 7660.90 | 7664.18 | 7667.46 | 7670.74 | 7674.02 |
| 2340 | 7677.30 | 7680.58 | \%683.87 | 7687.15 | 7690.43 | 7693.71 | 7696.99 | 7700.27 | 7703.55 | 7706.83 |
| 2350 | 7710.11 | 7713.39 | 7716.67 | 7719.96 | 7723.24 | 7726.52 | 7729.50 | 7733.08 | 7736.36 | 7739.64 |
| 2360 | 7742.92 | 7746.20 | 7749.48 | 7752.76 | 7756.05 | 7759.33 | 7762.61 | 7765.89 | 7769.17 | 7772.45 |
| 2370 | 7775.73 | 7779.01 | 7782.29 | 7785.57 | 7788.85 | 7792.14 | 7795.42 | 7798.70 | 7801.98 | 7805.26 |
| 2380 | 7808.54 | 7811.82 | 7815.10 | 7818.38 | 7821.66 | 7824.94 | 7828.23 | 7831.51 | 7834.79 | 7838.07 |
| 2390 | 7841.35 | 7844.63 | 7847.91 | 7851.19 | 7854.47 | 7857.75 | 7861.03 | 7864.32 | 7867.60 | 7870.88 |
|  | ©. | 1 | 2. | 3. | 4 | 5 | 6. | 7. | 8. | 9. |

E
$\mathbf{2 1 0 0}$ to $\mathbf{2 7 9 9 .}$

| Metres. | Metres. (Units) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (1). | 1. | $\pm$. | 3. | . | 5. | 6. | 8. | 8. | 9. |
|  | Etg.F | is.Feet. | Eng.Feet. | Eng Fees | Eng.Fer. | Eng.Ftel | Eur.Feet. | Ens Fent | Eng.Feet | Eng Frel. |
| 2100 | 7874.16 | 7877.44 | 7880.72 | 7884.00 | 7857.25 | 7890.56 | 7893.04 | 7897.12 | 7900.41 | 7903.69 |
| 2410 | 7906.97 | 7910.25 | 791:3.53 | 7916.81 | 7920.09 | 7923.3.37 | 7926.65 | 7929.93 | 7933.21 | 7936.50 |
| 2120 | 7939.78 | 7913.06 | 7916.34 | $79+9.62$ | 79.52 .90 | 7956.15 | 79.59 .46 | 7962.74 | 7966.02 | 7969.30 |
| 2130 | 7972.59 | 797.5 .57 | 7979.15 | 7983.43 | 790.5 .71 | 7988.94 | 7992.27 | 799.5 .5 .5 | 7995.83 | 8002.11 |
| 2110 | -00.5.39 | 8008.67 | 8011.96 | 8015.24 | 5015.52 | 5021.80 | 802.).05 | 8028.36 | 5031.64 | 5034.92 |
| 21.50 | 8038.20 | 3041.48 | 3044.76 | 80-18.0.5 | S051.33 | 80.54 .61 | 5057.89 | 8061.17 | 8064.45 | 8067.73 |
| 2160 | -071.01 | 8071.29 | 8077.57 | $80 \times 0.85$ | s08.1.14 | 8087.42 | 8090.70 | 8093.95 | 8097.26 | 8100.54 |
| 2170 | 810.3.82 | 8107.10 | 811038 | 8113.66 | S116.94 | 8120.22 | 8123.51 | 8126.79 | 81:30.07 | S133.35 |
| 2100 | -136.6:3 | 8139.41 | 8143.19 | 8116.47 | S149.75 | 8153.03 | S156.32 | S159.60 | S162. ¢ | 8166.16 |
| 2190 | 8169.44 | 8172.72 | 8176.00 | 8179.2\% | 8182.56 | 815.5.84 | 8159.12 | 8192.41 | 8195.69 | 8198.97 |
| 2.500 | 820.3.2.5 | 820.7.53 | 8.308.81 | 8212.09 | 221.5 .37 | 2018.6.7 | 8221.93 | 8.235.21 | 8228.50 | 8231.78 |
| 2.510 | 2.235.06 | 8.2.38.31 | $82+1.62$ | $82+4.90$ | 8.2fo.15 | 52.71.16 | -254.74 | 8.258.02 | 8261.30 | 5264.59 |
| 2.520 | $\checkmark 267.87$ | 3271.15 | 8274.43 | 8277.71 | 8.280 .99 | 8281.27 | 8257.55 | 5290.83 | 6291.11 | 5297.39 |
| 2.530 | 5300.67 | 23033.96 | 8307.24 | 8310.52 | ¢3I3.80 | 8317.0s | 8320.36 | 3323.64 | 8326.92 | 8330.20 |
| 2.510 | 8333.48 | 5336.76 | 8310.05 | 8343.33 | $83+6.61$ | 8319.89 | 8353.17 | 5356.45 | $8: 359.73$ | 8363.01 |
| 2.5 .30 | 8366.29 | 8369.37 | 8372.8.5 | 8376.14 | 8379.42 | 8382.70 | 8385.98 | 8359.26 | 8392.54 | 8395.82 |
| 2.560 | 8399.10 | 8402.35 | 8105.66 | 8108.94 | S412.23 | 8455.51 | 8+15.79 | 8422.07 | 8425.35 | 84.28 .63 |
| 2570 | 8431.91 | 8435.19 | 8483.47 | 8441.75 | S445.03 | 8448.32 | 8451.60 | 8454.88 | 8458.16 | 8461.44 |
| 2.530 | 8461.72 | 8468.00 | S171.28 | $8+74.56$ | 8477.84 | 8481.12 | 84S4.41 | 8487.69 | 8490.97 | 8494.25 |
| 2.590 | 5497.53 | 5500.81 | S504.09 | 8507.37 | 8510.65 | 8513.93 | 8517.21 | 5520.50 | 8523.7S | 8527.06 |
| 2600 | 5.530 .34 | 5533.62 | 8.536.90 | 8510.18 | 85.43.46 | 8.546 .74 | 8550.02 | 8553.30 | S556.58 | 8559.87 |
| 2630 | 8.563 .15 | 8566.43 | 5569.71 | 6.572.99 | 5.76 .27 | 8579.55 | 8582.83 | 8586.11 | 8589.39 | 8592.67 |
| 2620 | 859.5 .96 | 8599.24 | 8602.52 | 860.3.80 | 8609.08 | 8612.36 | 8615.64 | 8618.92 | 8622.20 | 8625.48 |
| 2630 | -628.76 | 86:32.0.) | 8635.33 | 8638.61 | 8641.89 | 864.5 .17 | 5648.45 | S651.73 | 86.55 .01 | S658.29 |
| 2640 | 8661.57 | 5664.85 | 8665.14 | 8671.42 | 8674.70 | 8677.98 | 8681.26 | 8684.54 | S687.82 | S691.10 |
| 26.50 | 8691.39 | 5697.66 | 8700.94 | 5701.23 | 8707.51 | \$710.79 | 3714.07 | 8717.35 | 8720.63 | 8723.91 |
| 2660 | 8727.19 | 8730.47 | S733.7.7 | 8737.03 | 8740.32 | 8713.60 | $87+16.88$ | 8750.16 | 5753.41 | 8756.72 |
| 2670 | 8760.00 | 876:3.2S | 8766.56 | 8769.81 | 8773.12 | 8776.4] | 8779.69 | 8782.97 | 8786.25 | 8789.53 |
| 2650 | -792. 1 | 87!6.0.9 | 8799.37 | 880.2.6.3 | S805.93 | 8809.21 | 8812.50 | 8815.75 | 8819.06 | 8822.34 |
| 2690 | 5825.62 | 8828.90 | 883:.18 | 8835.46 | 8838.74 | $88+2.02$ | 8845.30 | 8848.59 | 8851.87 | 8855.15 |
| 2700 | 8858.43 | 8861.71 | 8861.99 | 8868.27 | 8871.55 | 8874.83 | 8878.11 | 8881.39 | 8884.67 | 8887.96 |
| 2710 | 8891.24 | 8591.52 | 8897.80 | 8901.08 | 8904.36 | 8907.64 | 8910.92 | $891+.20$ | 8917.48 | 8920.76 |
| 2720 | 8926.0.) | 8927.33 | 89:30.61 | 8933.89 | 8937.17 | 8940.45 | S943.73 | $89+7.01$ | 8950.29 | 8953.57 |
| 2730 | 59.56.8.) | 8960.14 | 896:3.42 | 8966.70 | 8969.98 | 8973.26 | 8976.54 | 8979.82 | 8983.10 | 8986.38 |
| 2710 | S989.66 | 8992.91 | 8996.23 | 8999.ち1 | 9002.79 | 9006.07 | 9009.35 | 9012.63 | 9015.91 | 9019.19 |
| 2750 | 9022.17 | 902.5.75 | 9029.03 | 9032.32 | 903.5 .60 | 9038.88 | 9042.16 | 9045.44 | 9018.72 | 9052.00 |
| 2760 | 90.55 .28 | 90.58.56 | 9061.84 | 9065. | 9068.41 | 9071.69 | 9074.97 | 9075.2.5 | 9081.53 | 9081.81 |
| 2770 | 9085.09 | 9091.:37 | $909+.65$ | 9097.9 | 9101.21 | 9104.50 | 9107.78 | 9111.06 | 9114.34 | 9117.62 |
| 2780 | 9120.90 | 9124.18 | 9127.16 | 9130.74 | $913+.02$ | 9137.30 | 9140.59 | 9143.87 | 9147.15 | 9150.43 |
| 2790 | 9153.71 | 9156.99 | 9160.27 | 9163.55 | 9166.83 | 9170.11 | 9173.39 | 9176.68 | 9179.96 | 9183.24 |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |

2800 to 3000.

| Metres. | Metres. (Units) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ©. | $1 .$ | $\underline{2}$ | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Enute | Es.Feet. | Eng Feet. | Eıg.Feel. | Eng Fret. | E $!$ Feet. | Ende.Feer. | Eug Feet. | Eng.Fept. | Eng.Feet. |
| 2800 | 9186.53 | 9189.50 | 9193.08 | 9196.36 | 9199.64 | 9202.92 | 9206.20 | 9209.15 | 9212.76 | 9216.05 |
| 2810 | 9219.33 | 9222.61 | 922.5.89 | 9229.17 | 9232.45 | 9235.73 | 92:39.01 | 9242.29 | 924.5 .57 | 92.18 .55 |
| 2520 | 9232.14 | 925.5 .12 | 9258.70 | 9261.90 | 9265.26 | 9268.54 | 9271.82 | 9275.10 | 9275.38 | 9281.66 |
| 2830 | 9254.94 | 9285.23 | 9291.51 | 9291.79 | 9295.07 | 9301.35 | $930-4.64$ | 9307.91 | 4311.19 | 9314.47 |
| 2840 | 9317.75 | 9:321.03 | 9321.32 | 9327.60 | 9:330.58 | 19334.16 | 9337.44 | 9340.72 | 9344.00 | 9347.28 |
| 2850 | 9350.56 | 933.33.84 | 9357.12 | 9360.11 | 9363.69 | 9366.97 | 9370.25 | 9373.53 | 9376.81 | 9380.09 |
| 2960 | 93833.37 | 9356.65 | 9389.9:3 | 9:393 21 | $9: 396.50$ | 9899.7 | 9403.06 | 9406.34 | 9409.62 | 9412.90 |
| 2870 | 9416.18 | 9419.16 | 9422.74 | 9426.02 | 94.29 .30 | 94:32.59 | 9435.87 | 9439.15 | 9442.43 | $9+45.71$ |
| 2850 | 9448.99 | 9152.27 | 9455.55 | 9458.43 | 9462.11 | 9465.39 | 9468.65 | 9471.96 | 9475.24 | 9478.52 |
| 2890 | 9481.80 | 948.5 .08 | 9488.36 | 9491.64 | 9494.92 | 9498.20 | 9501.48 | 9504.76 | 9505.05 | 9511.33 |
| 2900 | 9514.61 | 9.517 .89 | 9521.17 | 9.524 .45 | 9.527 .73 | 9531.01 | 95:34.29 | 9537.57 | 9540.85 | 9544.14 |
| 2910 | 9547.12 | 9.5 .50 .70 | '9553.98 | 9.5.57.26 | 9560.54 | 9563.82 | 9567.10 | 9570.38 | 9573.66 | 9576.94 |
| 2920 | 9580.23 | 9583.51 | '9556.79 | 9.590 .07 | 9593.35 | 9596.63 | 9599.91 | 9603.19 | 9606.47 | 9609.75 |
| 2930 | 9613.03 | 9616.32 | 9619.60 | 962.85 | 9626.16 | 9629.44 | 9632.72 | 9636.00 | 9639.28 | 9642.56 |
| 2940 | 9645.54 | 9649.12 | 9652.41 | 9655.69 | 9658.97 | 966:2.2 | 3665.53 | 9665.81 | 9672.09 | 9675.37 |
| 2950 | 9678.62 | 9691.93 | 9685.21 | 9688.50 | 9691.78 | 9695.06 | 9698.34 | 9701.62 | 9704.90 | 9708.18 |
| 2960 | 9711.16 | 9714.74 | 9718.02 | 9721.30 | $972+.59$ | 9727.87 | 9731.15 | 9734.43 | 9737.71 | 9740.99 |
| 2970 | 9744.27 | 9847.55 | 97.50 .83 | 9754.11 | 97.57 .39 | 9760.68 | 9763.96 | 9767.24 | 9770.52 | 9773.80 |
| 2950 | 9777.08 | 9780.36 | 9783.64 | 9786.92 | 9790.20 | 9793.48 | 9796.76 | 9800.05 | 8803.38 | 9806.61 |
| 2990 | 9809.8.9 | 9813.17 | 9816.45 | 9819.73 | 982:3.01 | 9826.29 | 9829.57 | 9832.85 | S36.14 | 9839.42 |
| 3000 | \|9842.70| | 9845.98 | 9849.26 | 98.32.54 | 9555.82 | 9859.10 | 9562.38 | 9865.66 | 9868.94 | 9572.23 |

Proportional Parts.

VIII. conversion of metres into rhine or prussian feet and decimals.

1 Metre $=3.1861995$ Rhine Feet.

| Metres. Thousands. | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (1). | 100. | 200. | 300. | 400. | 500. | (i00. | 700. | 800. | 900. |
| 0 | Rhine ft. | Rhineft. | Mhine ft. <br> 637.9 | MLineft. | $\begin{array}{r} \text { Rhineft. } \\ 197+6 \end{array}$ | Rhine ft. $1593.1$ | Rhineft. 1911.7 | Rhiue ft. <br> 0.0.30. 3 | Rhine ft. | Rhine ft. |
| 0 |  | 318.6 | 637.2 | 955.9 | 1274.5 | 1593.1 | 1911.7 | 230.3 | 2549.0 | . 6 |
| 1000 | 3186.2 | 3504.8 | 3823.4 | 4142.1 | 4460.7 | 4779.3 | 5097.9 | 5416.5 | 5735.2 | 6053.8 |
| 2000 | 6372.4 | 6691.0 | 7009.6 | 7328.3 | 7646.9 | 7965.5 | 8284.1 | 8602.7 | 8921.4 | 9240.11 |
| 3000 | 9558.6 | 9877.2 1 | 10195. 8 | 10514.5 | 10833.1 | 11151.7 | 11470.3 | 11788.9 | 12107.6 | $12+26.2$ |
| 4000 | 12744.8 | 13063.4 | 13382.01 | 13700.7 | 14019.3 | 14337.9 | 14656.5 | 14975.1 | 15293.8 | 15612.4 |
| 5000 | 15931.0 | 16249.6 | 16568.2 | 16886.9 | 5.5 | 17524.1 | 17842.7 | 18161.3 | 1848 |  |
| 6000 | 19117.2 | 19435.8 | 19 | 20073.1 | 20391.7 | 07 | 21028.9 | 21347.5 | 21666 |  |
| 7000 | 22303.4 | $22(62.0$ | 22940.6 | 23259.3 | 577.9 | 23896 | 24215.1 | 24533.7 | 2485 |  |
| 8000 | 25489.6 | 25808.2 | 26126.8 | 26445.5 | 26764.1 | 27082.7 | 7401.3 | . 9 | 28038 | 28357.2 |
| 9000 | 28675.8 |  | 29313.0 | 29631.7 | 29950.3 | 30268.9 | 30587.5 | 30906.1 | 31224.8 | 31543.4 |
| IX. conversion of metres into feet of vienna. 1 Metre $=3.1637488$ Vienna Feet. |  |  |  |  |  |  |  |  |  |  |
| Metres. Thousands. | Hundreds. |  |  |  |  |  |  |  |  |  |
|  | (1) | D0. | -200. | 300. | 400. | 500. | 600. | 904. | 800. | 900. |
| 0 | Vieu. ft. 0.00 | $\begin{aligned} & \text { Vieu. ft. } \\ & 316.37 \end{aligned}$ | $\begin{array}{r} \text { Vien. } \mathrm{ft} . \\ 632.75 \end{array}$ | $\begin{aligned} & \text { Vien. ft. } \\ & 949.12 \end{aligned}$ | $\begin{gathered} \text { Vien. ft. } \\ 1265.50 \end{gathered}$ | $\left\lvert\, \begin{gathered} \text { Vien. ft. } \\ 1581.87 \end{gathered}\right.$ | $\begin{gathered} \text { Vien.ft. } \\ 1898.25 \end{gathered}$ | Vien. ft. 2214.62 | Vien. ft. 2531.00 | $\begin{aligned} & \text { Vien. ft. } \\ & 2847.37 \end{aligned}$ |
| 1000 | 3163.7 | 3480.1 | 3796.5 | 4112.9 | 4429.2 | 4745.6 | 5062.0 | 5378.4 | 5694.7 | 6011.1 |
| 2000 | 6327.5 | 6653.9 | 6960.2 | 7276.6 | 7593.0 | 7909.4 | 8205.7 | 8542.1 | 8858.5 | 9174.9 |
| 3000 | 9491.2 | 9807.6 | 10124.0 | 10440.4 | 10756.8 | 11073.1 | 11389.5 | 11705.9 | 12022.3 | 12338.6 |
| 4000 | 12655.0 | 12971.4 | 13257.7 | 13604.1 | 13920.5 | 14236.9 | 14553.3 | 14869.6 | 15186.0 | 15502.4 |
| 5000 | 15818.7 | 16135.1 | 16451.5 | 16767.9 | 17084.2 | 17400.6 | 17717.0 | 18033.4 | 18349.7 | 18666.1 |
| 6000 | 18.982 .5 | 19298.9 | 19615.2 | 19931.6 | 20248.0 | 20564.4 | 20880.7 | 21197.1 | 21513.5 | 21829.9 |
| 7000 | $\because 2146.2$ | 22460.6 | 22.79 .0 | 23095.4 | 23411.7 | 23728.1 | 24044.5 | 24360.9 | 24677.2 | -4993.6 |
| 81000 | 25310.0 | 126.4 | 25942.8 | 26259.1 | 265575.5 | 26891.9 | 27208.2 | 27524.6 | 27841.0 | 28157.4 |
| 9000 | 2483.7 | $2-790.1$ | 29106.5 | 29422.9 | 29739.2 | 30055.6 | 30372.0 | 30688.4 | 31004.7 | 31321.1 |
| Tens. | Units. |  |  |  |  |  |  |  |  |  |
|  | D. |  | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Vien. ft. | Vien. ft | Vien. ft. | Vien. ft. | Vien. ft. | Vien. ft. | Vien. ft. | Vien. ft. | Vien, ft. | Vien. ft. |
| 0 | $0.00$ | 3.16 | 6.33 | 9.49 | 12.65 | 15.82 | 18.98 | 22.15 | 25.31 | 28.47 |
| 10 | 31.64 | 34.80 | 37.96 | 41.13 | 44.29 | 47.46 | 50.62 | 53.78 | 56.93 | 60.11 |
| 20 | 63.27 | 66.54 | 69.60 | 72.77 | 75.93 | 79.09 | 82.26 | 85.42 | 88.58 | 91.75 |
| 30 | 94.91 | 98.08 | 101.24 | 104.40 | 107.57 | 110.73 | 113.69 | 117.06 | 120.22 | 123.39 |
| 40 | 126.55 | 129.71 | 132.88 | 136.04 | 139.20 | 142.37 | 145.53 | 148.70 | 151.86 | 155.02 |
| 50 | 158.19 | 161.35 | 164.51 | 167.68 | 170.84 | 174.01 | 177.17 | 180.33 | 183.50 | 186.66 |
| 60 | 189.82 | 192.99 | 196.15 | 199.32 | 202.48 | 205.64 | 208.81 | 211.97 | 215.13 | 218.30 |
| 70 | 221.46 | ㄴ.4.63 | $\underline{2} 7.79$ | 230.95 | 234.12 | 237.28 | 240.44 | 243.61 | 246.77 | 249.94 |
| 80 | 253.10 | 256.26 | 259.43 | 262.59 | 265.75 | 268.92 | 272.08 | 275.25 | 278.41 | 281.57 |
| 90 | 284.74 | 287.90 | 291.06 | 294.23 | 297.39 | 300.56 | 303.72 | 306.88 | 310.05 | 313.21 |

## TO CONVERT

## PARIS OR FRENCH FEET

## INTO DIFFERENT MEASURES OF LENGTH.

X. CONVERSION OF PARIS OR FRENCH FEET INTO TOISES.

1 French Foot $=0.1666666$ Toise.

|  | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | 800. | 900. |
| 0 | Toises. $0.00$ | Toises. $16.67$ | Toises. $33.33$ | Toises. $50.00$ | Toises. $66.67$ | Toises $83.33$ | Toises. $100.00$ | Toises. $116.67$ | Toises. $133.33$ | $\begin{aligned} & \text { Toises. } \\ & 150.00 \end{aligned}$ |
| 1000 | 166.67 | 183.33 | 200.00 | 216.67 | 233.33 | 250.00 | 266.67 | 283.33 | 300.00 | 316.67 |
| 2000 | 333.33 | 350.00 | 366.67 | 383.33 | 400.00 | 416.67 | 433.33 | 450.00 | 466.67 | 483.33 |
| 3000 | 500.00 | 516.67 | 533.33 | 550.00 | 566.67 | 583.33 | 600.00 | 616.67 | 633.33 | 650.00 |
| 4000 | 666.67 | 683.33 | 700.00 | 716.67 | 733.33 | 750.00 | 766.67 | 753.33 | 800.00 | 816.67 |
| 5000 | 833.33 | 850.00 | 866.67 | 883.33 | 900.00 | 916.67 | 933.33 | 950.00 | 966.67 | 983.33 |
| 6000 | 1000.00 | 1016.67 | 1033.33 | 1050.00 | 1066.67 | 1083.33 | 1100.00 | 1116.67 | 1133.33 | 1150.00 |
| 7000 | 1166.67 | 1183.33 | 1200.00 | 1216.67 | 1233.33 | 12.50 .00 | 1266.67 | 1283.33 | 1300.00 | 1316.67 |
| 8000 | 1333.33 | 1350.00 | 1366.67 | 1383.33 | 1400.00 | 1416.67 | 1433.33 | 1450.00 | 1466.67 | 1483.33 |
| 9000 | 1500.00 | 1516.67 | 1533.33 | 1550.00 | 1566.67 | 1583.33 | 1600.00 | 1616.67 | 1633.33 | 1650.00 |
| 10000 | 1666.67 | 1683.33 | 1700.00 | 1716.67 | 1733.33 | 1750.00 | 1766.67 | 1783.33 | 1800.00 | 1816.67 |
| 11000 | 1833.33 | 1850.00 | 1866.67 | 1883.33 | 1900.00 | 1916.67 | 1933.33 | 1950.00 | 1966.67 | 1983.33 |
| 12000 | 2000.00 | 2016.67 | 2033.33 | 2050.00 | 2066.67 | 2083.33 | 2100.00 | 2116.67 | 2133.33 | 2150.00 |
| 13000 | 2166.67 | 2183.33 | 2200.00 | 2216.67 | 2233.33 | 2250.00 | 2266.67 | 2283.33 | 2300.00 | 2316.67 |
| 14000 | 2333.33 | 2350.00 | 2366.67 | 2383.33 | 2400.00 | $2 \pm 16.67$ | 2433.33 | 2450.00 | 2466.67 | 2483.33 |
| 15000 | 2500.00 | 2516.67 | 2533.33 | 2550.00 | 2566.67 | 2583.33 | 2600.00 | 2616.67 | 2633.33 | 2650.00 |
| 16000 | 2666.67 | 2683.33 | 2700.00 | \|2716.67 | 2733.33 | 2750.00 | 2766.67 | 2783.33 | 2800.00 | 2816.67 |
| 17000 | 2833.33 | $2 \checkmark 50.00$ | 2866.67 | 2883.33 | 2900.00 | 2916.67 | 2933.33 | 2950.00 | 2966.67 | 2953.33 |
| 18000 | 3000.00 | 3016.67 | 3033.33 | 3050.00 | 3066.67 | 3083.33 | 3100.00 | 3116.67 | 3133.33 | 3150.00 |
| 19000 | 3166.67 | 3183.33 | 3200.00 | 3216.67 | 3233.33 | 3250.00 | 3266.67 | 3253.33 | 3300.00 | 3316.67 |
| 20000 | 3333.33 | 3350.00 | 3366.67 | 3383.33 | 3400.00 | 3416.67 | 3433.33 | 3450.00 | 3466.67 | 3483.33 |
| 21000 | 3500.00 | 3516.67 | 3533.33 | 35.50 .00 | 3566.67 | 3583.33 | 3600.00 | 3616.67 | 3633.33 | 3650.00 |
| 22000 | 3666.67 | 3653.33 | 3700.00 | 3716.67 | 3733.33 | 3750.00 | 3766.67 | 3783.33 | 3800.00 | 3816.67 |
| 23000 | 3833.33 | 3850.00 | 3866.67 | 3583.33 | 3900.00 | 3916.67 | 3933.33 | 3950.00 | 3966.67 | 3983.33 |
| 24000 | 4000.00 | 4016.67 | 4033.33 | 4050.00 | 4066.67 | 4083.33 | 4100.00 | 4116.67 | 4133.33 | 4150.00 |
| 25000 | 4166.67 | 4183.33 | 4200.00 | 4216.67 | 4233.33 | 42.50 .00 | 4266.67 | 428:3.33 | 4300.00 | 4316.67 |
| 26000 | 4333.33 | 4350.00 | 4366.67 | 4383.33 | 4400.00 | 4416.67 | 4433.33 | 4450.00 | 4466.67 | 4483.33 |


|  | Hus incis． |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 100. | 200. | 300. | 100. | 500． | 600. | 700. | 800. | 900. |
| 0 | Me:es. | Me：ses $3 .+2$ | $\begin{aligned} & M_{0}=2=8 \\ & n \neq .0 \end{aligned}$ | $\begin{aligned} & \text { Moses. } \\ & 4: 4.4 \bar{n} \end{aligned}$ | $\begin{aligned} & \text { Yeses. } \\ & 120.44 \end{aligned}$ | $\begin{aligned} & \text { Me:zes } \\ & 102+2 \end{aligned}$ | $\begin{aligned} & \text { Me:2s. } \\ & 19+64) \end{aligned}$ | $\begin{aligned} & \text { Me: es } \\ & 22: .34 \end{aligned}$ | $\begin{aligned} & \text { Metere } \\ & 234=9 \end{aligned}$ | $\begin{aligned} & \text { Metres } \\ & 242.34 \end{aligned}$ |
| 300？ | $\therefore 2 \pm$－ | 259．32 | S－0．？1 | 422．20 | ＋5．$=$ |  | 514．74 | 5．5．2． | 5－4．：1 | 617.19 |
| 2000 | － | $0-2.10$ | －114．n5 | $\therefore-13$ | －：4．61 | －12．10 | －46．3－ | －－． | 404.85 | $4+2.03$ |
| 20？${ }^{\text {a }}$ | ソーがこ | 1．1：－） |  | 1071．42 | 1104.45 | $1130.4+$ | 1109．42 | 1011.91 | 1234.34 | 1260．0： |
| 403 | 1294.36 | 1831．04 | 1364.33 | 1340．： | $1+20 \cdot 20$ | 1+611.: | $1+24.26$ | 15215.75 | 1550.23 | $1501 . \% 1$ |
| 570 | $152+29$ | 1ヶ゙かった | 10．0．10 | 1：21．65 | 1：54．38 | $15-6.2$ | 1－19．10 | －31．0 | 18～4．07 | 19168.55 |
| 5ima | $14.4 .9+$ | $14-1.52$ | 2014.0 | $23^{2}+6.4$ | －－－ 4 － | 2111．46 | $21+3.44$ | 2160.42 | $290-.91$ | $22+1.39$ |
| －0） 0 | －2－3．． | 2S in．3n | －385－6t | $23: 1.33$ | 240301 | 2435．3n | －40ッ－： | 2 O 11.20 | 2533.7 | 2.906 .23 |
| － 210 | $270-72$ | 2031.27 | 26からカー | 2645．1： | 2720.651 | －8081．14 | －43．5 | －6．10 | $2-5 \cdot .59$ | 2－41．07 |
| 0000 | 20.3 .55 | 20.93 .04 | $24-5.52$ | 022．01 | 3053.49 | $30-54$ | 115.46 | 150．9 | 31.3 .43 | 3215.41 |
| 1009？ | $32=-34$ |  | 313.35 | 345 | $335-33$ | －10 | $3+43.30$ |  | 3505.2 | 3540.75 |
| 1107 | 8590．3．23 | Sncs． 2 | 3038.30 | 3 B 00.04 | 3503.17 | 3－35．8．55 | 3.65 .14 | 3－00．62 | 3－33．11 | 3－65． 59 |
| 1278 | 3－0．0： | 34330.51 | 39.33 .04 | 304532 | 402－（1） | $1+600.49$ | 4092．4， | 4125．46 | 4157.94 | 4190.43 |
| 13007 | 422.41 | 4255．49 | 4－3－：－ | ＋320．36 | ＋352．－5 | 43－5．33 | 417．．2 | 44.10 .30 | 4＋2． $5=$ | 4515．29 |
| $1+009$ | 4547.85 | $45=0.24$ | 4612.72 | 4645.10 | $40: 7.59$ | 4710.07 | 4742.56 | 4：73．04 | t－07．5？ | $t=40.01$ |
| 15079 | 4502.50 | 49050.05 | 4487.56 | 49010.04 | 5002.53 | 5035.01 | 5065.49 | 5094.45 | 5132．46 | 5164.95 |
| 16） | 519\％．43 | 5224.41 | 3282040 | 3244.9 | 5327．37 | 5359．：5 | 5382.33 | $5+2.20$ | 545\％．30 | 54－6．79 |
| 1707 | 552.27 | 55.54 .25 | $55=-2.2+$ | 的14．\％2 | 56.52 .21 |  | 517．17 | 5749.66 | 5ご2．14 | $5-14.63$ |
| 1507） | $5 \times 2.811$ | $5-7.4 .34$ | 541200 | 3444.55 | 547－．05 | 50009．53 | （1） 2.01 | 6054.50 | 6106.9 | 6139．75 |
| 14000 | 01：1．05 | 6204.43 | 5238.42 | 5254.40 | 6301．－ | 6334.37 | 6360.55 | 0894.34 | 6431.5 | 6．464．30 |
| 2017）？ | 544n．－4 | 5.529 .27 | 6551．－7 | 5.594 .24 | 65.26 .72 | 56.59 .21 | 6591.69 | 6724.15 | 85.56 .66 | 6．59．14 |
| 210 m | 5021.53 | 6－54．11 | ricebibu | $6419.0=$ | 5451.55 | 6u－4．015 | －016．33 | － 044.02 | 7081.50 | 7113.93 |
| 22070 | ：14nit： | ：17－．95 | －211．4t | ：243．9．2 | 7250 | 730－．99 | －341．37 | －373．－6 | 7406.34 | 7435.32 |
| 23007 | 7－7．31 | －503．79 | 7536.2 － | 730．8．06 | 7601．24 | 7633．73 | －666．21 | －n9 54 | 7：31．1＝ | ：：63．66 |
| $2+009$ | ：－90．15 | $\therefore 2.53$ | $7=61.11$ | $\therefore 93.60$ | －923．0． | －953．5： | －991．05 | －023．53 | ＝056．02 | －0 $0=2.50$ |
| 23009 | －120．90 | －153．17 | － 155.95 | －2］5．44 | $\therefore 251.92$ | －233．41 | 5815.59 | －415．37 | 583＝0．56 | S 413.34 |
| 2009 | － 445.93 | － 4 T： 31 | －510．－4 $=$ | 2－543．2－ | －5：5．7i5 | －60－24 | －640．73 | － 5.3 .3 .21 | $-.05 .70$ | $=-738.15$ |
| 25 | $\therefore \therefore 0.0$ ¢ | $\cdots 33.15$ | $\cdots 2.68$ | －85．12 | － 4 mon ．n0 | －933．0＝ | －965．5．57 | －442－．05 | 90：30．54 | 9063.02 |

Tni？s．

|  | 0. | 1. | 2. | 3. | 1. | 5. | 6. | $\%$ | 8. | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  | $\begin{aligned} & 14=5=5 \\ & 10.32+0 \end{aligned}$ | $\begin{aligned} & 1+5=5 \\ & 0.0+47 \end{aligned}$ | $\begin{aligned} & \text { Meses. } \\ & 0.4 .45 \end{aligned}$ | $\begin{aligned} & \text { Yetres. } \\ & 1.2494 \end{aligned}$ | $\begin{aligned} & \text { Me:res. } \\ & 1.6242 \end{aligned}$ | $\begin{aligned} & \text { Metres } \\ & 1.4490 \end{aligned}$ | $\begin{aligned} & \text { Me:res. } \\ & 2.2739 \end{aligned}$ | Meites． $2.54=7$ | $\begin{aligned} & \text { Yetres. } \\ & 2.9236 \end{aligned}$ |
| 10 | 3.24 .4 | 3.53 .32 | $3.90-1$ | 4.2229 | 4．54\％ | $4.0-26$ | 5．19：4 | 5.3223 | 5．547］ | 6.1719 |
| 20 | $6.496=$ | 5．－215 | －． 1455 | 7．4：33 | 7.7981 | － 21210 | －．44．5 | $\therefore .707$ | 9．095．5 | 9.4203 |
| 30 | 4.7452 | 17．0：00 | $10.39+4$ | 10.7147 | 11.044 .5 | 11.3594 | 11.6942 | 12.0141 | 12.3439 | 12.565 |
| 40 | $12.4 \times 35$ | 13．31 3 4 | 13．5433 | 13.9651 | 14.2929 | 14．617＝ | 14.9426 | 15.2675 | 15.5923 | 15．9171 |
| 50 | 15.2429 | 16.5659 | 15．541n | 1：．215．5 | 17．5413 | 1\％．5562 | 15.1910 | 5．515 | 18．8407 | 19.16 .55 |
| 69 | 19．44）4 | $19: 152$ | 20.1400 | 20.4549 | 20．7－97 | 21．114ti | 21.439 | 1．－542 | 2.0591 | 22.4139 |
| 70 | 22．83＝ | 23.0538 | 23.3 － 4 | 23.7133 | 24.0351 | $\underline{-2.3530}$ | $2465:$ | 25.0126 | 25.3375 | 25.6623 |
| 50 | 25．9－72 | 25.3120 | $25.535=$ | 25.9517 | 27.2 －6． | －2－6．6114 | $27.93 \square^{2}$ | $2=.2610$ | 28.5559 | 5.9107. |
| 90 | 29.2355 | 29.5304 | 29．8552 | 30.2101 | 30.5349 | 30．8．597 | 31.1546 | 31.5094 | 31.8343 | 32.1591 |

גII．CONVERSION OF PARIS OR FRENCH FEET INTO FNOTISH FEET AND DECIKAES．


|  | Haclueds． |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands． | 0. | 100. | 200. | 300. | 100. | 500. | 600. | 700. | 500. | 900. |
| 0 | $\begin{gathered} \text { Erge fest } \\ 0.0 \end{gathered}$ | $\begin{gathered} E n \geq f 6: \\ 105.6 \end{gathered}$ | $\begin{aligned} E_{D} & =f \in e t . \\ & 213.2 \end{aligned}$ | $\begin{aligned} \text { En }=\text { Snt } \\ 319.7 \end{aligned}$ | $\begin{gathered} E_{L I}=f \text { fer. } \\ +26.3 \end{gathered}$ | $\begin{array}{r} \text { Etz } \mathrm{Enct} \\ 53.2 .9 \end{array}$ | $\begin{array}{r} E_{E}: \text { Et: } \\ 639.5 \end{array}$ | $\begin{aligned} x_{2} z \\ i+0.0 \end{aligned}$ | $\begin{aligned} E_{n}= & =52.5 \\ & =52 \end{aligned}$ | EIE E6e 959.2 |
| 1000 | 1065．${ }^{\text {a }}$ | 1172．3 | 12：－9．9 | 13.5 .5 | 1492.1 | 159－6 | 1：05．2 | 1－11．0 | 1915.4 | 2025.0 |
| 2000 | $2131 . .5$ | $2.3=.1$ | $23+4.7$ | 24.51 .3 | $255 \%$ | 2564.4 | 2：71．0 | 2－5\％．b | $29=4.1$ | 2040.7 |
| 3000 | 3197.3 | 3303.9 | 3410.4 | 3517．0 | 3623.6 | 3730.2 | 3－36． | 3943.83 | ＋049．9 | 4150.5 |
| 4000 | 4263.1 | 4359.6 | 4455.2 | $45=2.6$ | 4659.4 | 479．3．9 | 4902.5 | 5009.1 | 5115.7 | 5223.3 |
| 5000 | 5325.5 | 5435.4 | 5542.0 | 564 5.6 | 5：5．5． 1 | 5－61．7 | 5965.3 | 6074．9 | $61-1.4$ | 620：．0 |
| 6090 | 63394.6 | 6501.2 | 5607.7 | 6514.3 | か－20．9 | 5927.5 | 70：34．1 | 7140.5 | 724.2 | 7353．$=$ |
| \％000 | i460．4 | － 5 964．9 | 76.3 .5 | Ti＝0．1 | 7－－6．7 | 7993． 2 | ＝049．－ | $\because 200.4$ | －313．9 | － 414.5 |
| $=000$ | 5526.1 | 5632.7 | $=739.3$ | S－45．9 | －953．4 | 90.59 .9 | 916.5 .6 | $92: 2.2$ | 9378 | 4.453 |
| 9000 | 9.991 .9 | 9659.5 | $9=05.0$ | 9y11．6 | 1001－．2 | 10124.8 | 10231．3 | 10337.9 | 10444.5 | 105.51 .1 |
| 10000 | 1055\％．7 | 1075：．2 | 10こ：0．5 | 10978.4 | 11054.0 | 11197.5 | 11297.1 | 11403.7 | 11510.3 | 1516.5 |
| 11000 | 11：23． | $11=33.0$ | 11935.6 | 12043.1 | 12144.7 | 12250.3 | 12362.4 | 12.54 .5 | 12595.0 | 2ヶこ2．5 |
| 12000 | 127－9．2 | 12995． | 13002.8 | $1310-.9$ | 13215.5 | 13：32．1 | 13＋2－．5 | 13535．2 | 186＋1．$=$ | 183が， 4 |
| 13000 | $13=55.0$ | 13961.5 | $1406 \leq .1$ | 1417．7 | $142=1.3$ | 143こ\％． | 1449＋．4 | $1+5{ }^{\circ} 1$ | 14707.6 | 14614.1 |
| 14000 | 14920.7 | 1.5027 .3 | 1.5133 .9 | 1.2240 .4 | 15347.0 | 15453.6 | 1.5550 .2 | 15ヶロら：－ | 15748.3 | $15=-8.9$ |
| 15000 | 15956.5 | 16093.1 | 16199.6 | 15305．2 | 15412．5 | 16519.4 | 6625.9 | 6．32．5 | 5839.1 | 16945．7 |
| 16009 | 17052．2 | 1715s． | 17255.4 | 1：3：2．0 | $174 \%$ ．6 | $175=3.1$ | 1：59］．7 | 17：3－．3 | 17914.9 | 1－011．4 |
| 17030 | 1511－．0 | 1－224．5 | 1－331．2 | $1=437.7$ | $1-544.3$ | 15650.9 | 1：575．5 | $1=-64.0$ | 1－970．5 | 14275 |
| 1－030 | 191－3． | 19290.4 | 19395.9 | 14.503 .5 | 19610.1 | 19715.7 | 19023.2 | 19929． | 20035.4 | 20143.0 |
| 19000 | 20249.5 | 20356.1 | 20462.7 | 20.569 .3 | 20575.5 | 207：2．4 | $20=99.0$ | 20945.5 | 21102.2 | $2120 \cdot 7$ |
| 20000 | 21315.3 | 21421.9 | 21523.5 | 21635.0 | 21741.6 | 2155.2 | 22054.5 | 2.151 .8 | 22158.9 | 22274.5 |
| 21000 | 22351.1 | $22+56.7$ | 22594.2 | 22700.5 | 22000.4 | 22914.0 | 23020.5 | 23127.1 | 23233.7 | $238+0.3$ |
| 22000 | $23+46 .=$ | 23.553 .4 | 23550.0 | 23750 | 23－ 23.1 | 23479.7 | $240-6.3$ | $2+142.4$ | 22.404 .5 | $2+405.0$ |
| 23090 | 24512.6 | 24519.2 | 24－25： | 24532.3 | $2493-9$ | 25045.5 | 25152.1 | $2525=.15$ | 25355.2 | 25＋i］．$=$ |
| 24000 | $255 \%$－4 | 25654.9 | 25791.5 | $25 \leq 9 \leq .1$ | 26004.7 | 26111.3 | 25217.5 | 20324.4 | 26431.0 | 25537.6 |
| 25000 | 26644.1 | 26750.7 | 26534．3 | 26953.9 | 28050.4 | 2717.0 | ごご33．5 | 27390.2 | $27+96.7$ | $2: 803.3$ |
| 26000 | 27509.9 | $2 こ 16.5$ | 27923.1 | $2<029.6$ | $2-13 n .2$ | $2-242.5$ | 2－344．4 | $2=455.9$ | $2-552.5$ | 2－5i5．1 |
| 27000 | 25755．7 | 2ごく？．2 | 2－995．8 | 24095.4 | 24202.0 | $2930-.5$ | 29415.1 | 29521.7 | 24525.3 | 24784.9 |

ப品：

|  | 0. | 1. | 2. | 3. | 1. | ．）． | 6. | $\%$ | 9 | 9. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $\begin{gathered} E_{n}=f \text { fet } \\ 0.000 \end{gathered}$ | $\begin{gathered} E_{0 y} \text { fere } \\ 1.056 \end{gathered}$ | $\begin{array}{r} \text { Enz. Feez } \\ 2.132 \end{array}$ | $\begin{array}{r} \text { Enz feet } \\ 3.197 \end{array}$ | $\begin{array}{r} \text { En=fus! } \\ 4.2+3! \end{array}$ | $\begin{array}{r} \text { Enz } \\ 5.304 \end{array}$ | $\begin{gathered} E_{n}=f=: \\ 6.395 \end{gathered}$ | $\begin{gathered} E_{5}=\text { iem: } \\ 7.400 \end{gathered}$ | $\begin{gathered} \text { En }=\text { fer: } \\ =.520 \end{gathered}$ | $\begin{array}{r} \text { ED }=20+ \\ 4.592 \end{array}$ |
| 10 | 10.655 | 11.823 | 12.759 | 13．9．53 | 14．421 | $15.9 \leq 6$ | 17．052 | 1：．11： | 19.1 － 4 | 20.2511 |
| 20 | 21.315 | $2 \cdot 2.3=1$ | 23.445 | $\underline{24.513}$ | $25.5 \%$ | 25.644 | 27.710 | 2．8．75 | 29．－4］ | 30.467 |
| 30 | 31.973 | 33.039 | 34.104 | 35.150 | 36.236 | 37．302 | 32．365 | 39.433 | 40． 499 | 555 |
| 40 | 42.631 | 43.696 | ＋4．762 | 45.20 | 45.294 | ＋7．9．59 | 49.025 | 50.041 | 51.157 | 52.223 |
| 50 | 53.259 | 54.354 | 55.420 | 56．4－6 | 57．5．51 | 53．617 | 59．63．3 | 50.759 | 51.514 | 52．：30 |
| 60 | 63.946 | 65.012 | 66.05 | 67.143 | 65.204 | 64.35 | －0．341 | －1．40n | －2．4：2 | －3．5．53 |
| 70 | 74.604 | 75．669 | 76．735 | 7\％．001 | 78.567 | 79．933 | 50.995 | E2nnt | －3．130 | － 4.195 |
| 80 | S5．261 | 56.327 | E7．393 | －8．4．99 | －9．52t | 90.590 | 91.655 | 92.722 | 63．7－5 | 94.853 |
| 90 | 95.919 | 96．9E5 | 98.050 | 99.116 | $100.1=2$ | 101．24 | 102.318 | 103．85：9 | 104.445 | 10.5 .511 |

## 478

XIII. conversion of paris or french feet into rhine or prussian feet.

1 Paris Foot $=1.03,00323$ Rhine Foot.

| French | Hundreds |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | -300. | 300. | 100. | 5000. | 609. | 700. | S00. | 980. |
| 0 | $\begin{array}{r} \text { Rhiseft. } \\ 0.00 \end{array}$ | Rhiuett. <br> 103.50 | Rhine ft. 207.00 | Rhiue ft . $310.50$ | $\begin{array}{r} \text { Rhine ft. } \\ 414.00 \end{array}$ | $\begin{array}{r} \text { Rhine ft. } \\ 517.50 \end{array}$ | Rhane fi. 621.00 | $\begin{aligned} & \text { Rhine ft. } \\ & 7 \because 4.50 \end{aligned}$ | Rhiue ft. と2. 000 | $\begin{array}{r} \text { Thine ft. } \\ 931.50 \end{array}$ |
| 1000 | 1035.00 | 1138.50 | $12+2.00$ | 1345.50 | 1449.00 | 1552.50 | 1650.00 | 1759.51 | 1863.01' | 1966.51 |
| 2000 | 2070.01 | 2173.51 | 2277.01 | 2380.51 | 2484.01 | 2587.51 | 2691.01 | 2764.51 | 2898.01 | 3001.51 |
| 3000 | 310.5 .01 | 3208.51 | 3312.01 | 3415.51 | 3519.01 | 3622.51 | 37.26 .01 | 3829.51 | 3933.01 | 4036.51 |
| 4000 | 4140.01 | 4243.51 | 4307.01 | 4450.51 | 4554.01 | 4657.51 | 4761.01 | 4864.51 | 4968.01 | 5071.51 |
| 5000 | 5175.01 | 5278.52 |  | .52 | 5589.02 | 5692.52 | 5796.02 | 5899.52 | 6003.02 | 6106.52 |
| 6000 | ${ }^{1} 210.02$ | 6313.52 | (6417.02 | 0.52 | 6694.02 | 15727.52 | 8831.02 | 6934.52 | 7035.02 | 7141.52 |
| 7000 | T-45.02 | 7345.52 | 7552.02 | 5.5 | 7659.02 | 7762. | 60.02 | 7669.52 | 8073.02 | 8176.52 |
| 8000 | 8280.102 | -3-3.52 | -457.02 | 8590.52 | 5684.03 | 8797.53 | 8907.03 | 9014.53 | 9108.03 | 9211.53 |
| 9000 | 9315.03 | 418.53 | 2522.03 | 9625.53 | 9729.03 | 9832.53 | 9936.03 | 10039.53 | 10143.03 | 10246.53 |
| 10000 | 10350.0 | 10453.5 | 105.57 .0 | 10660.5 | 10764.0 | 10867.5 | 10971.0 | 11074.5 | 11178.0 | 11281.5 |
| 11000 | 11355.0 | 11458.5 | 11592.0 | 11695.5 | 11799.0 | 11902.5 | 12006.0 | 12109.5 | 12213.0 | 12316.5 |
| 12000 | 12420.0 | 12523.5 | 12627.0 | 12730.5 | 12834.0 | 12937.5 | 13041.0 | $131+4.5$ | 13245.0 | 13351.5 |
| 13000 | 13455.0 | 13558.5 | 13662.0 | 13765.5 | 13569.0 | 13972.5 | 14076.0 | 1417:9.5 | 14283.0 | 11386.5 |
| 14000 | 14490.0 | 14593.5 | 14697.0 | 14800.5 | 14904.0 | 15007.5 | 15111.0 | 15.214 .5 | 15318.0 | 15421.5 |
| 15000 | 15525.0 | 15608.4 | 32.0 | 15835.5 | 15939.0 | 16042.5 | 16146.0 | 1624.9.5 | 16353.0 | 16456.6 |
| 16000 | 16560.1 | 16663.6 | 16767.1 | 16570.6 | 16974.1 | 17077.6 | 17181.1 | 17284.6 | 17385.1 | 17491.6 |
| 17000 | 17595.1 | 176998.6 | 17502. 1 | 17905.6 | 18009.1 | 18112.6 | 18216.1 | 18:319.6 | 15423.1 | 18526.6 |
| 15900 | 18630.1 | 15733.6 | 1-837.1 | 18940.6 | 19044.1 | 19147.6 | 19251.1 | 19354.6 | 19458.1 | 19561.6 |
| 19000 | 19665.1 | 19768.6 | 19572.1 | 19 | 20079.1 | 20182.6 | 20286.1 | 20389.6 | 20493.1 | 20596.6 |
| 20000 | 20700.1 | 20803.6 | 20907.1 | 21010.6 | 21114.1 | -17.0 | 21321.1 | 21424.6 | 21528.1 | 21631.6 |
| 21600 | 21735.1 | $21 \sim 38.6$ | 21942.1 | 22045.6 | 2.214! 1 | 22052. | 22356.1 | 22459.6 | 22563.1 | 22666.6 |
| 22000 | 22770.1 | 2.253 .6 | 22977.1 | 23080.6 | 23184.1 | 23287. | 23391.1 | 28.494 .6 | 23598.1 | 23701.6 |
| 23000 | 23805.1 | 23908.6 | 24012.1 | $2+115.6$ | $2+219.1$ | 24322.6 | $2+426.1$ | 24529.6 | 24633.1 | 24736.6 |
| 24000 | -4 40.0 | 24943.6 | 25047.1 | 25150.6 | 25254.1 | 25357.6 | 25461.1 | 25564.6 | 25668.1 | 25771.6 |
| 25000 | 25875. | 978.6 | 26082.1 | 26185.6 | 26289.1 | 26392.6 | 26596.1 | 26699.6 | 26703.1 | 26806.6 |
| 26000 | -6910. | 013.6 | 27117.1 | 27220.6 | 27321.1 | 27427.6 | 27.51 .1 | 27634.6 | 27738.1 | 27841.6 |
| 27000 | 2794 | 14 | $2-152.1$ | 255. | 28359.1 | 28462.6 | 28566.1 | 28669.6 | 8773.1 | -876.6 |
| 2-400 | 2s! | 183 | 1 | 29290.6 | 29394.1 | 29497. | 29601.0 | 29714.6 | 29808.0 | 29911.6 |
|  |  |  |  |  |  | nits. |  |  |  |  |
|  | d. | 1. | 2. | 3. | 4. | 5. | 6. | 8. | 5. | 9. |
| 0 | Rhine ft <br> 0.00 | Rhine ft. 1.04 | Rhiueft. | Rhineft. $3.11$ | Rhine ft. $4.14$ | Rhiue ft. 5. 18 | Rhine ft. <br> 6.21 | Phine ft. 7.25 | $\begin{gathered} \text { Rhine ft. } \\ 8.28 \end{gathered}$ | Rhine ft. $9.32$ |
| 10 | 10.35 | 11.39 | 12.42 | 13.46 | 14.49 | 15.53 | 16.56 | 17.60 | 18.63 | 19.67 |
| 20 | 20.71 | 21.74 | 22.77 | 23.81 | 24.84 | 25.88 | 24.91 | 27.95 | 28.98 | 30.02 |
| 30 | 31.05 | 32.09 | 33.12 | 34.16 | 35.19 | 31.23 | 37.26 | 38.30 | 39.33 | 41.37 |
| 40 | 41.40 | 42.44 | 43.47 | 4.51 | 45.54 | 46.58 | 47.61 | 48.65 | 49.68 | 50.72 |
| 50 | 51.75 | 52.79 | 53.82 | 54.86 | 55.89 | 56.93 | 57.96 | 59.00 | 60.03 | 61.07 |
| 60 | 62.10 | 63.14 | 64.17 | 65.21 | 66.84 | 67.28 | 68.31 | 69.35 | 70.38 | 71.42 |
| 70 | 72.45 | 73.49 | 74.52 | 75.56 | 76.59 | 77.63 | 78.66 | 79.70 | 80.73 | S1.77 |
| 80 | 82.80 | 83.84 | 84.87 | 85.91 | 86.94 | 87.98 | 89.01 | 90.05 | 91.08 | 92.12 |
| 90 | 93.15 | 94.19 | 95.22 | 96.26 | 97.29 | 98.33 | 99.36 | 100.40 | 101.43 | 102.47 |

1 Paris Foot $=1.027710$.

| rench | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tho | 0 | 100. | 200 | 300. | 400. | 500. | 600. | 700. | 860. | 900. |
| 0 | Vien. ft. 0.00 | $\begin{aligned} & \text { Vien. ft. } \\ & 102.77 \end{aligned}$ | Vien. ft. 205.54 | Vien. ft. $308.31$ | Vien. it. 411.08 | $\begin{array}{r} \text { Vien. ft. } \\ 513.85 \end{array}$ | Vieu. ft. 616.63 | Vieu. ft. 719.40 | Vien, ft. 822.17 | Vien. ft. $924.94$ |
| 1000 | 1027.71 | 1130.48 | 1233.25 | 1336.02 | 1438.79 | 1541.56 | $16+4.34$ | 1747.11 | 1849.88 | 1952.65 |
| 2000 | 2055.42 | 2158.19 | 2260.96 | 2363.73 | 2466.50 | 2569.27 | 2672.05 | 2774.62 | 2877.59 | 2980.36 |
| 3000 | 3083.13 | 3155.90 | 67 | 3391.44 | 3494.21 | 3596.98 | 3699.76 | 3802.53 | 3905.30 | 4008.07 |
| 4000 | 4110.84 | 4213.61 | 4316.38 | 419.15 | 4521.92 | 4624.69 | 4727.47 | 4830.24 | 4933.01 | 5035.78 |
| 5000 |  | 5 | 5344.09 | 5446.86 | 5549.63 | 5652.40 | 5755.18 | 5857.95 | 5960.72 | 6063.49 |
| 6000 | 6166.26 | 6269.03 | 6371.80 | . 57 | 6577.34 | 6680.11 | 6762.89 | 6885.66 | 6988.43 | 7091.20 |
| 7000 | 7193.97 | 7296.74 | 7399.51 | 7502.28 | 7605.05 | 7707.82 | 7810.60 | 7913.37 | 8016.14 | 8118.91 |
| 8000 | ¢221.68 | 8324.45 | 8427.2 | 8529.99 | 8632.76 | 5735.53 | 8838.31 | 8941.08 | 9043.85 | 9146.62 |
| 9000 | 9949.39 | 9352.1 | ! | 7.70 | 9660.47 | 9763.24 | 9866.02 | 9968.79 | 10071.56 | 10174.33 |
| 10000 | 10277.1 | 10379.9 | 10 | . 4 | 10688.2 | 10791.0 | 10893.7 | 10996.5 | 11099.3 | 11202.0 |
| 11000 | 11304.8 | 11407.6 | 11510. | 11613.1 | 11715.9 | 11818.7 | 11921.4 | 12024.2 | 12127.0 | 12220.7 |
| 12000 | 12332.5 | 12435. | 38.1 | 12640.8 | 12743.6 | 12846.4 | 12949.1 | 13051.9 | 13154.7 | 13257.5 |
| 13000 | 13360.2 | 13463.1 | 13565. | 13668.5 | 13771.3 | 13874.1 | 13976.9 | 14079.6 | 14182.4 | $14 \div 85.2$ |
| 14000 | 14357.9 | 14490.7 | 14593.5 | 14696.3 | 14799.0 | 14901.8 | 15004.6 | 15107.3 | 15210.1 | 15313.6 |
| 15000 | 15415.6 | 15518.4 | 15621.2 | 15724.0 | 15826.7 | 15929.5 | 16032.3 | 16135.0 | 16237.8 | 16340.6 |
| 16000 | 16443.4 | 16546.1 | 16648.9 | 16751.7 | 16854.4 | 16957.2 | 17060.0 | 17162.6 | 17265.5 | 17368.3 |
| 17000 | 17471.1 | 17573.8 | 17 |  | 17882.2 | 17984.9 | 18087.7 | 18190.5 | 18293.2 | 18306.0 |
| 18000 | 18498.8 | 18601.6 | 18704. 3 | 18807.0 | 18903.9 | 19012.6 | 19115.4 | 19218.2 | 19320.9 | 19423.7 |
| 19000 | 19526.5 | 19629.3 | 19732.0 | 19834. 8 | 19937.6 | 20040.3 | 20143.1 | 20245.9 | 20348.7 | 20451.4 |
| 20000 | 20554.2 | 20657.0 | 20759.7 | 20862.5 | 20965.3 | 21068.1 | 21170.8 | 21273.6 | 21376.4 | 21479.1 |
| 21000 | 21581.9 | 21684.7 | 21757.5 | 21890.2 | 21993.0 | 22095.8 | 22198.5 | 22301.3 | 22404.1 | 22506.8 |
| 22000 | 22609.6 | 22712.4 | 22815. | 22917.9 | 23020.7 | 23123.5 | 23226.2 | 23329.0 | 23431.8 | 23534.6 |
| 23000 | 23637.3 | 23740.1 | 23842 | 23945.6 | 24048.4 | -24151.2 | 224254.0 | 24356.7 | 24459.5 | 24562.3 |
| 24000 | 24665.0 | 24767.8 | 24570.6 | 24973.4 | 25076.1 | 25178.9 | 25281.7 | 25384.4 | 25487.2 | 25589.0 |
| 25000 | 25692.7 | 25795.5 | 25898.3 | 26001.1 | 26103.8 | 26206.6 | - 26309.4 | 26412.1 | 26514.9 | 26617.7 |
| 26000 | 26720.5 | 26823.2 | 26926.0 | 27028.8 | 27131.5 | 27243.3 | 27337.1 | 27439.9 | 27542.6 | 27645.4 |
| 27000 | 27748.2 | 27850.9 | 27953.7 | 28056.5 | 28159.3 | 28262.0 | 128364.8 | 28467.6 | 28570.3 | 28673.1 |
| 28000 | 28775.9 | 28878.7 | 28981 | '29084.2 | 29187.0 | 129289.7 | 29392.5 | 29495.3 | 29598.0 | 29700.8 |

Units.

| Tens. | Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 1. | 2. | 3. | 4. | 5. | 6. | \%. | S. | 9. |
|  | Vien. ft. | Vien. ft. | Vien. ft. | Vien. ft . | Vien. ft. | Vien. ft. | Vien, ft. | Vien. ft. $7.19$ | Yien. ft. 8 の.) | Vieu. ft. $9 \cdot 95$ |
| 0 | 0.00 | 1.03 | 2.06 | 3.08 | 4.11 | 5.14 | 6.17 | 7.19 | 8.22 | 9.25 |
| 10 | 10.28 | 11.30 | 12.33 | 13.36 | 14.39 | 15.42 | 16.44 | 17.47 | 18.50 | 19.53 |
| 20 | 20.55 | 21.58 | 22.61 | 23.64 | 24.67 | 25.69 | 26.72 | 27.75 | 28.78 | 29.80 |
| 30 | 30.83 | 31.86 | 32.89 | 33.91 | 34.94 | 35.97 | 37.00 | 38.03 | 39.05 | 40.08 |
| 40 | 41.11 | 42.14 | 43.16 | 4.19 | 45.22 | 46.25 | 47.27 | 48.30 | 49.33 | 50.36 |
| 50 | 51.39 | 52.41 | 53.44 | 54.47 | 55.50 | 56.52 | 57.55 | 58.58 | 59.61 | 60.63 |
| 60 | 61.66 | 62.69 | 63.72 | 64.75 | 65.77 | 66.80 | 67.83 | 68.86 | 69.88 | 70.91 |
| 70 | 71.94 | 72.97 | 74.00 | 75.02 | 76.05 | 77.08 | 78.11 | 79.13 | 80.16 | 81.19 |
| 80 | 82.22 | 83.24 | 84.27 | 85.30 | 86.33 | 87.36 | 88.38 | 89.41 | 90.44 | 91.47 |
| 90 | 92.49 | 93.52 | 94.55 | 95.58 | 96.60 | 97.63 | 98.66 | 99.69 | 100.72 | 101.74 |

## TO CONVERT

# ENGLISH YARDS AND FEET 

## INTO DIFFERENT MEASURES OF LENGTH.

## XV. CONVERSION OF ENGLISH YARDS INTO FRENCH TOISES.

1 English Yard $=0.4691465$ Toise.

|  | Hundreis. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | 800. | \$00. |
|  | Toises | Toises. | Toises | Toises. | Toises | Toises. | Toises | Toises. | Toises. | Toises. |
| 0 | 0.00 | 46.91 | 93.83 | 140.74 | 1*7.66 | 234.57 | 281.49 | 32840 | 375.32 | 422.23 |
| 1000 | 169.15 | 516.06 | 562.98 | 609.89 | 656.80 | 703.72 | 750.63 | 797.55 | 844.46 | 891.38 |
| 2000 | 935.29 | 95.21 | 1032.12 | 1079.04 | 1125.95 | 1172.87 | 1219.78 | 1266.70 | 1313.61 | 1360.52 |
| 3000 | 1407.44 | 1454.35 | 1501.27 | 1545.18 | 159.5 .10 | 1642.01 | 1688.93 | 1735.84 | 1782.76 | 1839.67 |
| 4000 | 1876.59 | 1923.50 | 1970.41 | 2017.33 | 2064.24 | 2111.16 | 2158.07 | 2.204 .99 | 2251.90 | 2298.82 |
| 5000 | 23.4.73 | 2392.65 | 2439.56 | 2486.18 | 2533.39 | 2580.31 | 2627.29 | 2674.13 | 2721.0 .7 | 2767.96 |
| 6000 | 2514.88 | 2561.79 | 2908.71 | 2955.62 | 3002.54 | 3049.45 | 3096.37 | 3143.28 | 3190.20 | 22:37.11 |
| 7000 | 3284.02 | 3830.94 | 3377.85 | 3424.77 | 3471.68 | 3518.60 | 3565.51 | 3612.43 | 3659.34 | 3706.26 |
| 8000 | 3753.17 | 3800.09 | 3847.00 | 3593.92 | 3910.83 | 3987.74 | 4034.66 | 4081.57 | 4128.49 | 4175.40 |
| 9000 | +292.32 | 4269.23 | $4: 316.15$ | 4363.06 | 4109.98 | 4456.89 | 4503.81 | +550.72 | 4597.63 | 4644.55 |

XVI. CONVERSION OF ENGLISH YARDS INTO METRES.

1 English Fard $=0.91438348$ Metre.

|  | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | 800. | 900. |
| 0 | Metres. 0.00 | Metres. 91.44 | $\begin{aligned} & \text { Metres } \\ & 182.88 \end{aligned}$ | Metres. $274.32$ | Metres. 365.75 | Metres. $457.19$ | Metres. $548.63$ | Metres. $6+0.07$ | Metres. <br> 731.51 | Metres $822.95$ |
| 1000 | 914.38 | 100.5.82 | 1097.26 | 1188.70 | 1280.14 | 1371.58 | 1463.01 | 1554.45 | 1645.89 | 1737.33 |
| 2000 | 1828.77 | 1920.21 | 2011.64 | 2103.08 | 2194.52 | 228.5.96 | 2377.40 | 2468.84 | 2.560 .27 | 2651.71 |
| 3000 | 2743.15 | 2834.59 | 2926.03 | 3017.47 | 3108.90 | 3200.34 | 3291.78 | 3383.22 | 3474.66 | 3566.10 |
| 4000 | 3657.53 | 3718.97 | 3840.41 | 3931.85 | 402:3.29 | 1114.73 | +206.16 | 4297.60 | 4389.04 | 480.48 |
| 5000 | 4571.92 | 4663.36 | 1754.79 | 4846.23 | 4937.67 | 5029.11 | 5120.55 | 5211.99 | 5303.42 | 5.994 .86 |
| 6000 | 5486.30 | 5577.74 | 5669.18 | 5760.62 | 5852.05 | 5943.49 | 6034.93 | 6126.37 | 6217.81 | 6309.25 |
| 7000 | 6100.65 | 6492.12 | 6583.56 | 6675.00 | 6766.44 | 6857.88 | 6949.31 | 7040.75 | 7132.19 | 7223.63 |
| 8000 | 7315.07 | 7406.51 | 7197.94 | 7589.38 | 7680.82 | 7772.26 | 7863.70 | 7955.14 | 8046.57 | 8138.01 |
| 9000 | 8229 45 | 8320.59 | 8412.33 | 8503.77 | 8595.20] | 8656.64 | 8778.08 | 8869.52 | 8960.96 | 9052.40 |

1 English Foot $=0.30479449$ Metre.

|  | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T | O. | 100. | 200. | 300. | 100. | 500. | 600. | 700. | 800. | 900. |
| 0 | $\begin{gathered} \text { Metres. } \\ 000.000 \end{gathered}$ | $\begin{gathered} \text { Metres. } \\ 30.4794 \end{gathered}$ | $\begin{gathered} \text { Metres. } \\ 60.9 .589 \end{gathered}$ | $\begin{gathered} \text { Metres. } \\ 91.4383 \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { Metres. } \\ 121.918 \\ \hline \end{array}$ | Metres. $152.397$ | $\begin{gathered} \text { Metres. } \\ 182.877 \end{gathered}$ | $\begin{gathered} \text { Metres. } \\ 213.356 \end{gathered}$ | $\begin{gathered} \text { Metres. } \\ 243.836 \end{gathered}$ |  |
| 1000 | 304.794 | 335.274 | 365.763 | 396.233 | 426.712 | 457.192 | 187.671 | \$18.151 | 548.630 | 579.110 |
| 2000 | 609.589 | 640.068 | 670.548 | 701.027 | 731.507 | 761.986 | 792.466 | 822.945 | 853.425 | 883.904 |
| 3000 | 914.383 | 944.563 | 975.342 | 1005.82 | 1036.30 | 1066.78 | 1097.26 | 1127.74 | 1158.22 | 1188.70 |
| 4000 | 1219.18 | 1249.66 | 1280.14 | 1310.62 | 1341.10 | 1371.58 | 1402.05 | 1432.53 | 1463.01 | 1493.49 |
| 5000 | 1523.97 | 1554.45 | 1584.93 | 1615.41 | 1645.89 | 1676.37 | 1706.85 | 1737.33 | 1767.81 | 1798.29 |
| 6000 | 1828.77 | 1859.25 | 1859.73 | 1920.21 | 1950.68 | 1981.16 | 2011.64 | 2042.12 | 2072.60 | 2103.08 |
| 7000 | 2133.56 | 2164.04 | 2194.52 | 2225.00 | 2255.4S | 2285.96 | 2316.44 | 2346.92 | 2377.40 | 2407.88 |
| 8000 | 2438.36 | 2468.84 | 2499.31 | 2529.79 | 2560.27 | 2590.75 | 2621.23 | 2651.71 | 2682,19 | 2712.67 |
| 9000 | 2743.15 | 2773.63 | 2804.11 | 2834.59 | 2865.07 | 289.5 .55 | 2926.03 | 2956.51 | 2986.99 | 3017.17 |
| 10000 | 3047.94 | 3078.42 | 3108.90 | 3139.38 | 3169.86 | 3200.34 | 3230.82 | 3261.30 | 3291.75 | 3322.26 |
| 11000 | 3352.74 | 3383.22 | 3413.70 | 344.18 | 3474.66 | 3505.14 | 3535.62 | 3566.10 | 3596.57 | 3627.05 |
| 12000 | 3657.53 | 3688.01 | 3718.49 | 3748.97 | 3779.45 | 3809.93 | 3840.41 | 3870.89 | 3901.37 | 3931.55 |
| 13000 | 3962.33 | 3992.81 | 4023.29 | 4053.77 | 4084.25 | 4114.73 | 4145.21 | 1175.68 | 1206.16 | 4236.64 |
| 1.1000 | 4267.12 | 4297.60 | 4228.08 | 4358.56 | 4359.04 | 4119.52 | 4450.00 | 4480.48 | 4510.96 | 4541.44 |
| 15000 | 4571.92 | 4602.40 | 4632.88 | 4663.36 | 4693.84 | +724.31 | 4754.79 | 4785.27 | 4815.75 | 4846.23 |
| 16000 | 4876.71 | 4907.19 | 4937.67 | 4968.15 | 4998.63 | 5029.11 | 5059.59 | 5090.07 | 5120.55 | 5151.03 |
| 17000 | 5181.51 | 5211.99 | 5242.47 | 5272.94 | 5303.42 | 5333.90 | 5364.38 | 5394.86 | 542.5.34 | 5455.82 |
| 18000 | 5486.30 | 5516.78 | 5547.26 | 5577.74 | 5608.22 | 5638.70 | 5669.18 | 5699.66 | 5730.14 | 5760.62 |
| 19000 | 5791.10 | 5821.57 | 5852.05 | 5882.53 | 5913.01 | 5943.49 | 5973.97 | 6004.45 | 6034.93 | 6065.41 |
| 20000 | 6095.59 | 6125.37 | 6156.85 | 6157.33 | 6217.81 | 6248.29 | 6278.77 | 6309.2 : | 6339.73 | 6370.20 |
| 21000 | 6400.68 | 6431.16 | 6461.64 | 6492.12 | 6522.60 | 6553.08 | 6583.56 | 6614.01 | 6644.52 | 6675.00 |
| 22000 | 6705.48 | 6735.96 | 6766.44 | 6796.92 | 6827.40 | 6857.88 | 6888.36 | 6918.83 | 6949.31 | 6979.79 |
| 23000 | 7010.27 | 7040.75 | 7071.23 | 7101.71 | 7132.19 | 7162.67 | 7193.15 | 7223.63 | 7254.11 | 7284.59 |
| 24000 | 7315.07 | 7345.55 | 7376.03 | 7406.51 | 7436.99 | 7467.47 | 7497.94 | 7528.42 | 75.58 .90 | 7589.38 |
| 25000 | 7619.86 | 7650.34 | 7650.82 | 7711.30 | 7741.78 | 7772.26 | 7802.74 | 7833.2 | 7863.70 | 7894.18 |
| 26000 | 7921.66 | 7955.14 | 7985.62 | S016.10 | 8046.57 | 8077.05 | 8107.53 | 8138.01 | 8168.49 | 8198.97 |
| 27000 | 8229.45 | 82.59.93 | 8290.41 | 8320.89 | 5351.37 | 8381.85 | 8412.33 | 8442.81 | 8473.29 | 8503.77 |
| 28000 | 8534.25 | 8564.73 \| | 8595.20 | 8625.68 | 8656.16 | 8686.64 | 8717.12 | 8747.60 | 78.08 | 8508.56 |
|  |  |  |  |  | Uni |  |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Metres. | Metres | M | Netres. | Metres. | Metres. | Met | Metres. | Metres. | Metres. |
| 0 | 0.00000 | 0.30479 | 0.60959 | 0.91438 | 1.21918 | 1.52397 | 1.82877 | 2.13356 | 2.43836 | 2.74315 |
| 10 | 3.04794 | 3.35274 | 3.65753 | 3.96233 | 4.26712 | 4.57192 | 4.57671 | 5.18151 | 5.48630 | 5.79110 |
| 20 | 6.09589 | 6.40068 | 6.70548 | 7.01027 | 7.31507 | 7.61986 | 7.92466 | S.22945 | 8.53425 | 8.83904 |
| 30 | 9.14383 | 9.44863 | 9.75342 | 10.0582 | 10.3630 | 10.6678 | 10.9726 | 11.2774 | 11.5822 | 11.8870 |
| 40 | 12.1918 | 12.4966 | 12.8014 | 13.1062 | 13.4110 | 13.7158 | 14.0205 | 14.3253 | 14.6301 | 14.9349 |
| 50 | 15.2397 | 15.5445 | 15.8493 | 16.1541 | 16.4589 | 16.7637 | 17.0685 | 17.3733 | 17.6781 | 17.9829 |
| 60 | 18.2877 | 18.5925 | 18.8973 | 19.2021 | 19.5068 | 19.8116 | 20.1164 | 20.4212 | 20.7260 | 21.0308 |
| 70 | 21.3356 | 21.6404 | 21.9452 | 22.2500 | 22.5548 | 22.8596 | 23.1644 | 2:3.4692 | 23.7740 | 24.0789 |
| 80 | 24.3836 | 24.6884 | 24.9931 | 25.2979 | 25.6027 | 25.9075 | 26.2123 | 26.5171 | 26.8219 | 27.1267 |
| 90 | 27.4315 | 27.7363 | 28.0411 | 28.3459 | 28.6507 | 28.9555 | 29.2603 | 29.5651 | 29.8699 | 30.1747 |

XVIII CONVERSION OF FNGLISH FEIT INTO FRENCH OR PARIS FEET AND DECIMALS.

1 English Foot $=0.938292$. Paris Foot.

|  | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | ©. | 100. | -180. | 300. | 100. | 500. | 600. | 700. | 800. | ¢05. |
|  | Par. Feet. | Par Fuet. | Par. Feet | Par Feet | lar jet | * | Par | I'ar Feet | Par Feet | Par feet. |
| 0 | 000.0 | 93.5 | 158.7 | 2-1.5 | 375.: | 469.1 | 56\%.0 | 656.8 | 7.90 .6 | 844.5 |
| 1000 | 938.3 | 10.32. 1 | 1126.0 | 1219.5 | 1313.6 | 1407.1 | 1501.3 | 159.5 .1 | 16.5 -. 9 | 1752.8 |
| 2000 | 1876.6 | 1970.4 | 2064.2 | 2155.1 | 2251.9 | 234.5 .7 | 2439.6 | 2.533 .4 | 2627.2 | $2 \% 21.0$ |
| 3000 | 2811.9 | 2908.7 | 3002.5 | 3096.4 | 3190.2 | 3281.0 | $38 \div 7.9$ | 3471.7 | 3.56 .5 .5 | 3659.3 |
| 4000 | 3753.2 | 3847.0 | 3910.8 | 4031.7 | 4128.5 | 12:2.3 | 4316.1 | +410.0 | 4.503 .8 | 4.997 .6 |
| 5000 | 4691.5 | 4785.3 | 4879.1 | 4973.0 | 50666.8 | 5160.6 | 52.54.4 | $53+8.3$ | 5442.1 | 5535.3 |
| 6000 | 5629.5 | 5723.6 | 5817.4 | 5911.2 | 6005.1 | $609 ¢ .9$ | 6192.7 | 6286.6 | 6380.4 | 6474.2 |
| 7000 | 6568.0 | 6661.9 | 675.5 .7 | 6819.5 | 69 I3.4 | 7037.2 | 7181.0 | 7224.9 | 7318.7 | 7112.5 |
| 8000 | 7.506 .3 | $76 \mathrm{no.2}$ | 7694.0 | 7787.8 | 7881.7 | 7975.5 | 5069.3 | S163.1 | 82.77 .0 | 8350.8 |
| 9000 | S $4+1.6$ | 8538.5 | 8632.3 | 5726.1 | 8820.0 | 5913.8 | 9007.6 | 9101.4 | 9195.3 | 9289.1 |
| 10000 | 9382.9 | 9476.8 | 9570.6 | 9661.1 | 9758.2 | 9852.1 | 9945.9 | 10039.7 | 10133.6 | 1022\%.4 |
| 11000 | 10321.2 | 10415.0 | 10.308.9 | 10602.7 | 10696.5 | 10790.4 | 10854.2 | 10978.0 | 11071.9 | 11165.7 |
| 12000 | 11259.5 | 11353.8 | 11417.2 | 11.541 .0 | 116:34.8 | 1725.7 | 11822.5 | 11916.3 | 12010.1 | 12104.0 |
| 13000 | 12197.8 | 12291.6 | 12385.5 | 12479.3 | 12573.1 | 12667.0 | 12760.8 | 12854.6 | 12948.1 | 13042.3 |
| 14000 | 13136.1 | 13239.9 | 13323.8 | 13417.6 | 13511.4 | 13605.2 | 13699.1 | 13792.9 | 13886.7 | 13980.6 |
| 1.9000 | 11071.1 | 14165.2 | 14262.0 | 14355.9 | 11449.7 | 4.543 .5 | 14637.4 | 14731.2 | 14825.0 | 14918.9 |
| 16000 | 15012.7 | 15106.5 | 1.5200 .3 | 1.5294 .2 | $153 \times 5.0$ | 15181.8 | 1.5 .75 .7 | 1.5669 .5 | 15763.3 | 158.77.1 |
| 17000 | 1.5951 .0 | 16014.8 | 161:38.6 | 16232.5 | 16326.3 | 16120.1 | 16.514 .0 | 16607.5 | 16701.6 | 16795.4 |
| 15030 | 16ss9.:3 | 16983.1 | 17076.9 | 17170.8 | 172616 | 17355.4 | 17452.2 | 17546.1 | 17639.9 | 17733.7 |
| 19000 | 17827.6 | 17921.1 | 18015.2 | 18109.0 | 18202.9 | 18296.7 | 18390.5 | 18434.4 | 15575.2 | 18672.0 |
| 20000 | 1876.3.9 | 188.59.7 | 189.33.5 | 19047.3 | $19] 41.2$ | 1923.5 .0 | 19328.8 | 19422.7 | 19.516 .5 | 19610.3 |
| 21000 | 19704.1 | 19798. 0 | 19891.8 | 19955.6 | $20079 . .5$ | 20173.3 | 20267.1 | 20361.0 | 20454.8 | 20.548 .6 |
| 22000 | 20642.4 | 20736.3 | 20830.1 | 20923.9 | 21017.8 | 21111.6 | 2120.5 .4 | 21299.2 | 21393.1 | 21456.9 |
| 23000 | 21550.7 | 21674.6 | 21768.4 | 21562.2 | 219.56 .0 | 22049.9 | 22143.7 | 22237.5 | 22331.4 | 22425.2 |
| 24090 | 22519.0 | 22612.9 | 22706.7 | 22300.5 | 22894.3 | 22958.2 | 23082.0 | 23175.8 | 23269.7 | 23363.5 |
| 25000 | 291.57 .3 | 235.51 .1 | 23645.0 | 23738.5 | 23832.6 | 23926.5 | 24020.3 | 24114.1 | 24208.0 | 21301.8 |
| 26000 | $24: 395.6$ | 24459.4 | 24583.3 | 24677.1 | 21750.9 | 24864.8 | 24958.6 | 25052.4 | 2.5146 .2 | 25240.1 |
| 27000 | 253:33.9 | 25427.7 | 25521.6 | 25615.4 | 25709.2 | 25803.1 | 2.5896 .9 | 25990.7 | 26084.5 | 26178.1 |
| 2 SO 0 | 26.72 .2 | 26366.0 | 26459.9 | 26.553 .7 | 26647.5 | 6741. | 26535.2 | 26929.0 | 27022.8 | 27116.7 |
|  |  |  |  |  | Uni |  |  |  |  |  |
|  | O. | 1. |  | 3. |  |  | 6. | 3. | 8. | 9. |
|  | Par. Feet. | Par. Feet. | Par Fect. | Par. Feet. | Par keet | ar. Feet | l'ar. Feet. | Par. Feet. | Par.Feet. | 1 'ar Feet. |
| 0 | 0.00 | 0.94 | 1.85 | 2.81 | 3.75 | 4.69 | 563 | 6.57 | 7.51 | 8.44 |
| 10 | 9.38 | 10.32 | 11.26 | 12.20 | 13.14 | $14.0 \%$ | 15.01 | 15.95 | 16.59 | 17.83 |
| 20 | 18.77 | 19.70 | 20.61 | 21.58 | 22.52 | 23.16 | 24.40 | 25.33 | 26.27 | 27.21 |
| 80 | 28.15 | 29.09 | 30.03 | 30.96 | 31.90 | 32.84 | 33.75 | 34.72 | 35.66 | 36.59 |
| 40 | 37.5.3 | 38.47 | 39.41 | 40.35 | 41.2 S | 42.22 | 43.16 | 44.10 | 45.01 | 45.98 |
| 50 | 46.91 | 47.85 | 48.79 | 49.73 | 50.67 | 51.61 | 52.54 | 53.48 | 54.42 | 55.36 |
| 60 | 56.30 | 57.24 | 58.17 | 59.11 | 60.05 | 60.99 | 61.93 | 62.87 | 63.80 | 64.7 -1 |
| 70 | 65.65 | 66.62 | 67.56 | 68.50 | 69.13 | 70.37 | 71.31 | 72.25 | 73.19 | 74.13 |
| 80 | 75.06 | 76.00 | 76.91 | 77.88 | 78.82 | 79.75 | 80.69 | 81.63 | 8.2 .57 | 83.51 |
| 90 | 84.4. | 85.38 | 86.32 | 87.26 | 88.20 | 89.14 | 90.08 | 91.01 | 91.95 | 92.89 |

1 Eughos Fout $=0.9711362$ Rhine Fout.

| Euglish | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thonsauds. | 0. | 100. | 200. | 3046 | 400. | 504. | 600. | 800. | stob. | 900. |
| 0 | Phine tt. 0.00 | Rametr. 97.11 97.11 | Hhine It. 194.23 | Rhinett. 291.34 | $\begin{aligned} & \text { Khine } \\ & 38 \text {. } \end{aligned}$ | Rhine it. 485.57 |  | Rhatit. | Rame 1t. | libine 1 t -74.02 |
| 1060 | 971.14 | 1068.25 | 1165.36 | 1262.48 | 1359.59 | 1456.70 | 1553.68 | 1650.93 | 1748 | 16 |
| 2000 | 1942.27 | 2039.35 | 2136.50 | 2233.61 | 2330.75 | 2427.84 | 2524.95 | 2620.07 | 2719.1 | ¢16.29 |
| 3000 | 2913.41 | 3010.52 | 3117.64 | 3204.75 | 3301.86 | 3398.98 | 3496.09 | 3593.20 | 3690 | 787.43 |
| 4000 | 3884.54 | 3981.66 | 4078.77 | 4175.69 | 4273.00 | 4370.11 | 4467.23 | 4564.34 | 4661. | 4758.57 |
| 5000 | 4855.68 | 4952.79 | 5049.91 | 5147.02 | 5244.14 | 5341.25 | 5438.36 | 5535.48 | 5632.59 | 729.70 |
| 6000 | 5826.82 | 5923.93 | 5021.04 | 6118.16 | 6215.27 | 6312.39 | 409.50 | 6506.61 | 6603.73 | 15700.84 |
| 7000 | ¢797.95 | 16895.07 | 6992.18 | 7089.29 | 7186.41 | 7283.52 | 7380.64 | 7477.75 | 7574.86 | 7671.98 |
| 8000 | 7769.09 | 7866.2u | 7963.32 | 8060.43 | 8157.54 | 8254.66 | 8351.77 | -448.88 | 8546.00 | 8643.11 |
| 9000 | 8740.23 | 8837.34 | 8:334.45 | 9031.57 | $9128.68^{\circ}$ | '9225.79 | 9322.91 | 9420.02 | '9517.13 | 9614.25 |
| 10.100 | 9611.4 | 9808.5 | 9905.6 |  | $10$ |  | 10294.0 | 10391.2 |  |  |
| 11000 | 10683.5 | 10779.9 | 10876.7 |  | 11071.0 |  | 11265.2 | 11362.3 |  |  |
| 12000 | 11653.6 | 11750.7 | 11847.9 | 11945.0 | 12042.1 | 1~139.2 | 12236.3 | 12333.4 | 12430. | 10527.7 |
| 13000 | 12624.8 | 12721.9 | 12819.0 | 12916.1 | 13013.2 | 13110.3 | 13207.5 | 13304.6 | 13-401. | 13498.8 |
| 14000 | 13595.9 | 13693.0 | 13790.1 | 13887.2 | 13984.4 | 14081.5 | 14178.6 | 14275.7 | 14372. | 14469.9 |
| 15000 | 14567.0 | 14664.2 | 61.3 | 14858.4 | 14955.5 |  | 15149.7 | 15 | 15344 | 1.1 |
| 16000 | 15539.2 | 15635. | 15732.4 | 15529.5 | 15926.6 | 16023.7 | 16120.9 | 16218.0 | 16315.1 | 16412.2 |
| 17000 | 16509.3 | 16606.4 | 16703.5 | 14800.7 | 16897.8 | 16994.9 | 17092.0 | 17189.1 | 17286. | 17383.3 |
| 18000 | 17480.5 | 17577.6 | 74.7 | 17771.8 | 17868.9 | 17966.0 | 18063.1 | 18160.2 | 18257 | 6354.5 |
| 19000 | 18451.6 | 18545.7 | 18645.8 | 18742.9 | 18840.0 | 18937.2 | 19034.3 | 19131.4 | 19228. | 19325.6 |
| 20000 | $19+22.7$ | 19519.8 | 19617.0 | 19714.1 | 19811.2 | 19908.3 | 20005.4 | 20102.5 | 20199 | 20296.7 |
| 21000 | 20393.9 | 20491.0 | 20585.1 | 20685.2 | 20782.3 | -(i879.4 | 20976.5 | 21073.7 | 21170. | 21267.9 |
| 22000 | 21365.0 | 214162.1 | 21559.2 | 21656.3 | $21753 .:$ | 21850.6 | 21947.7 | 22044. | 22141 | 22833.0 |
| 23000 | 22336.1 | $224: 3.2$ | 22.350 .4 | 22627.5 | 22724 | 20821.7 | 22918.6 | 23015.9 | 23113. | 23210.2 |
| 240.00 | 23307.3 | 23404.4 | 23501.5 | 23598.6 | $23695^{\circ} 7$ | 23792.8 | 23589.0 | 23987.1 | 24084. | 4181.3 |
| 25000 | 24278.4 | 24375.5 | 2472.6 | 24569.7 | 24566.9 | 24764.0 | 24861.1 | 2495 | 505 | 25152.4 |
| 21000 | 25249.5 | 25346.7 | 25443.8 | 25540.9 | 25638.0 | 25735.1 | 25832.2 | 929 | 26026. | 3.6 |
| 27000 | 26220.7 | 26317.8 | $26 \pm 14.9$ | 26512.0 | 26609.1 | 26706.2 | 26803.4 | 26900.5 | 26997. | 27094.7 |
| 28000 | 27191 | 27288.9 | 27386.0 | 483.2 | 27580.3 | 27677.4 | 27774.5 | ?787 | 27968. | 8065.8 |
|  |  |  |  |  | Uni | its. |  |  |  |  |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | $\%$ | 8. | 9. |
|  | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. | Rhine ft. | Rhineft. | Rhine ft. | Khine tt . | Rhine ft. |
| 0 | 0.00 | 0.97 | 1.94 | 2.91 | 3.88 | 4.86 | 5.83 | 6.60 | 7.77 | 8.74 |
| 10 | 9.71 | 10.68 | 11.65 | 12.62 | 13.60 | 14.57 | 15.54 | 16.51 | 17.48 | 18.45 |
| 20 | 19.42 | 20.39 | 21.36 | 22.34 | 23.31 | 24.28 | 25.25 | 26.22 | 27.19 | 28.16 |
| 30 | 29.13 | 30.11 | 31.08 | 32.05 | 33.02 | 33.99 | 34.96 | 35.93 | 36.90 | 37.87 |
| 40 | 38.85 | 39.82 | 40.79 | 41.76 | 42.73 | 43.70 | 44.67 | 45.64 | 46.61 | 47.59 |
| 50 | 48.56 | 49.53 | 50.50 | 51.47 | 52.44 | 53.41 | 54.38 | 55.35 | 56.33 | 57.30 |
| 60 | 58.27 | 59.24 | 60.21 | 61.18 | 62.15 | 63.12 | 64.09 | 65.07 | 66.04 | 67.01 |
| 70 | 67.98 | 68.95 | 69.92 | 70.89 | 71.86 | 72.84 | 73.81 | 74.78 | 75.75 | 76.72 |
| 80 | 77.69 | 78.66 | 79.63 | 80.60 | 81.58 | 82.55 | 83.52 | 84.49 | 85.46 | 86.43 |
| 90 | 87.40 | 88.37 | 89.34 | 90.32 | 91.29 | 92.26 | 93.23 | 94.20 | 95.17 | 96.14 |

1 English Foot $=0.9642932$ Foot of Vienna.

| $\begin{aligned} & \text { Engtish } \\ & \text { Feet. } \end{aligned}$ <br> Thousands. | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | 500. | 900. |
| 0 | Yien. ft. 0.00 | Vien. 1t. 96.43 | $\begin{array}{r} \text { Vien. ft. } \\ 192.86 \end{array}$ | Vien. ft. $289.29$ | Vien. ft. $385.72$ | $\begin{array}{\|c} \hline \text { Vien. ft. } \\ 482.15 \end{array}$ | Vien. ft. 578.58 | Vien. ft. $675.01$ | Vien. fit 771.4 | ien. tt. <br> 867.86 |
| 1000 | 964.29 | 1060.72 | 1157.15 | 1253.58 | 1350.01 | 1446.44 | 1542.87 | 1639.30 | 1735.73 | 832.16 |
| 2000 | 1928.59 | 2025.02 | 2121.45 | 2217.87 | 2314.30 | 2410.73 | 2507.16 | 2603.59 | 2700.12 | 2796.45 |
| 3000 | 2892.85 | 2989.31 | 3055.74 | 3182.17 | 3278.60 | 3375.03 | 3471.46 | 3567.88 | 3664.31 | 760.74 |
| 4000 | 3857.17 | 3953.60 | 4050.03 | 4146.46 | 4242.89 | 4339.32 | 4435.75 | 4532.18 | 4628.61 | 4725.04 |
| 5000 | 4821.47 | 4917.90 | 5014.32 | 5110.75 | 5207.18 | 5303.31 | 5400.04 | 5496.47 | 5592.90 | 5689.33 |
| 6000 | 5785.76 | 5882.19 | 5978.62 | '6075.05 | 6171.48 | 6267.91 | 6364.34 | 6460.76 | 6557.19 | 6653.62 |
| 7000 | 6750.05 | 6846.48 | 6942.91 | 7039.34 | 7135.77 | 7232.20 | 7328.63 | 7425.06 | 7521.49 | 7617.92 |
| 8000 | 7714.35 | 7810.77 | 7907.20 | 8003.63 | 8100.06 | 8196.49 | 8292.92 | 8389.35 | 8485.78 | '8582.21 |
| 9000 | 8678.64 | 8775.07 | 8871.50 | 8967.93 | 9064.36 | 9160.79 | 9257.21 | 9353.6 | 0.07 | 546.50 |
| 10000 | 9642.93 | 9739.36 | 9835.79 | 9932.22 | 10028.6 | 10125.1 | 10221.5 | 10317.9 | 10414.4 | 10510.8 |
| 11000 | 10607.2 | 10703.7 | 10800.1 | 10896.5 | 10992.9 | 11089.4 | 11185.8 | 11282.2 | 11378.7 | 5.1 |
| 12000 | 11571.5 | 11667.9 | 11764.4 | 11860.8 | 11957.2 | 12053.7 | 12150.1 | 12246.5 | 12343.0 | 12439.4 |
| 13000 | 12535.8 | 12632.2 | 12728.7 | 12825.1 | 12921.5 | 13018.0 | 13114.4 | 13210.8 | 13307.2 | 13403.7 |
| 14000 | 13500.1 | 13596.5 | 13693.0 | 13789.4 | 13885.8 | 13982.3 | 14078.7 | 14175.1 | 14271.5 | 14368.0 |
| 15000 | 14464.4 | 14560.8 | 14657.3 | 14753.7 | 14850.1 | 14946.5 | 15043.0 | 15139.4 | 5235.8 | 15332.3 |
| 16000 | 15428.7 | 15525.1 | 15621.5 | 15718.0 | 15814.4 | 15910.8 | 16007.3 | 16103.7 | 6200. 1 | 6296.6 |
| 17600 | 16393.0 | 16489.4 | 16585.6 | 16682.3 | 16788.7 | 16885.1 | 16971.6 | 17068.0 | 7164.4 | 7260.8 |
| 18000 | 17357.3 | 17453.7 | 17550.1 | 17646.6 | 17743.0 | 17839.4 | 17935.9 | 18032.3 | 1812s.7 | 18205.1 |
| 19000 | 18321.6 | 18418.0 | 18514.4 | 18610.9 | 18707.3 | 18803.7 | 18900.1 | 18996.6 | 19093.0 | 19189.4 |
| 20000 | 19285.9 | 19382.3 | 19478.7 | 19575.2 | 19671.6 | 19768.0 | 19864.4 | 19960.9 | 20057.3 | 20153.7 |
| 21000 | 20250.2 | 0346.6 | 20443.0 | 20539.4 | 20635.9 | 20732.3 | 20828.7 | 20925. | 21021. | 21118.0 |
| 22000 | 21214. | 21310.9 | 21407.3 | 21503.7 | 21600.2 | 21696.6 | 21793.0 | 21889. | 21.985 .9 | 22082.3 |
| 23000 | 22178.7 | 22275. | 22371.6 | 22468.0 | 22564.5 | 22660.9 | 29757.3 | 22853.7 | 22950.2 | 23046.6 |
| 24000 | 23143.0 | 23239.5 | 23335.9 | 23432.3 | 23528.8 | 23625.2 | 23721.6 | 23818.0 | 23914.5 | 24010.9 |
| 25000 | 24107.3 | 24203.8 | 24300.2 | 24396.6 | 24493.0 | 24589.5 | 24685.9 | 24782.3 | 24878.8 | 24975.2 |
| 26000 | 25071.6 | 25168.1 | 25264.5 | 25360.9 | 25457.3 | 25553.8 | 25650.2 | 25746.6 | 25843.1 | 25939.5 |
| 27000 | 26035.9 | 26132.3 | 26228.8 | 26325.2 | 26421.6 | 26518.1 | 26614.5 | 26710. | 26807 | 26903.8 |
| 28000 | 2700 | 27096 | 27193.1 | 27289.5 | 27385.9 | 2748 | 27578.8 | ,75 | 771 | 7868.1 |
|  |  |  |  |  |  | nits. |  |  |  |  |
|  | O. | 1 | 2. | 3. | 4. | 5. | 6. | $\%$. | 8. | 9. |
|  | Vien. ft. | Vien. ft | Vien. ft. | Vien. ft. | Vien. ft. | Yien. ft. | Vien. ft. | Vien. ft. | Vien. ft. | Vien. ft. |
| 0 | 0.00 | 0.96 | . 92 | 2. | 3.85 | ) | 5.78 | 6.75 | 7.71 | 8.68 |
| 10 | 9.64 | 10.61 | 11.57 | 12.54 | 13.50 | 14.46 | 15.43 | 16.39 | 17.36 | 18.32 |
| 20 | 19.29 | 20.25 | 21.21 | 22.18 | 23.14 | 24.11 | 25.07 | 26.04 | 27.00 | 27.96 |
| 30 | 28.93 | 29.89 | 30.86 | 31.89 | 32.79 | 33.75 | 34.71 | 35.68 | 36.64 | 37.61 |
| 40 | 38.57 | 39.54 | 40.50 | 41.46 | 42.43 | 43.39 | 44.36 | 45.32 | 46.29 | 47.25 |
| 50 | 48.21 | 49.18 | 50.14 | 51.11 | 52.07 | 53.04 | 54.00 | 54.96 | 55.93 | 56.89 |
| 60 | 57.86 | 58.82 | 59.79 | 60.75 | 61.71 | 62.68 | 63.64 | 64.61 | 65.57 | 66.54 |
| 70 | 67.50 | 68.46 | 69.43 | 70.39 | 71.36 | 72.32 | 73.29 | 74.25 | 75.21 | 76.18 |
| 80 | 77.14 | 78.11 | 79.07 | 80.04 | 81.00 | 81.96 | 82.93 | 83.89 | 84.86 | 85.82 |
| 90 | 86.79 | 87.75 | 88.71 | 89.68 | 90.64 | 91.61 | 92.57 | 93.54 | 94.50 | 95.47 |

# TO CONVERT 

区LAFTERAND FEET OF VIENNA

## INTO DIFFERENT MEASURES OF LENGTH.

XXI. conversion of hlafter of vienna into metres.

1 Klatter of Vieuna $=1.5964843$ Metres.

| Klafter of Vieuna. Thousands. | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | S00. | 900. |
| 0 | $\begin{array}{r} \text { Metres. } \\ 0.00 \end{array}$ | Metres. $189.65$ | Metres. 379.30 | $\begin{gathered} \text { Metres. } \\ 568.95 \end{gathered}$ | Metres. <br> 758.59 | Metres. $948.24$ | $\begin{gathered} \text { Metres. } \\ 1137.89 \end{gathered}$ | Metres. 1327.54 | Mtares. 1517.19 | $\begin{gathered} \text { Metres. } \\ 1706.84 \end{gathered}$ |
| 1000 | 1896.48 | 2086.13 | 2275.78 | 2465.43 | 2655.08 | 2844.73 | 3034.37 | 3224.02 | 3413.67 | 3603.32 |
| 2000 | 3792.97: | 3982.62 | 172.27 | 4361.91 | 4551.56 | 4741.21 | 4930.36 | 5120.51 | 5310.16 | 5499.80 |
| 3000 | 5689.45 | 5879.10 | 6068.75 | 6258.40 | 6446.05 | 6637.69 | 6827.34 | 7016.99 | 7206.64 | 7396.29 |
| 4000 | 7585.94 | 7775.59 | 7965.23 | 8154.88 | 8344.53 | 8534.18 | 8723.83 | 8913.45 | 9103.12 | 9292.76 |
| 5000 | 9482.4 | 9672.1 | 9861.7 | 10051.4 | 10241.0 | 10430.7 | 10620.3 | 10810.0 | 10999.6 | 11189.3 |
| 6000 | 11378.9 | 11568.6 | 11758.2 | 11947.9 | 12137.5 | 12327.2 | 12516.8 | 12706.4 | 12596.1 | 13085.7 |
| 7000 | 13275.4 | 13465.0 | 13654.7 | 13844.3 | 14034.0 | 14223.6 | 14413.3 | 14602.9 | 14792.6 | 14982.2 |
| 8000 | 15171.9 | 15361.5 | 15551.2 | 15740.8 | 15930..) | 16120.1 | 16309.8 | 16499.4 | 16689.1 | 6878.7 |
| 9000 | 17068. | 17258.0 | 17447.7 | 76 | 17827.0 | 1801. | 18206 | $18395 .!$ | 18585. | 18775.2 |
| Klafter. |  |  |  |  | Uni | its. |  |  |  |  |
| Tens. | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. |
| 0 | 0.00 | 1.90 | 3.79 | 5.69 | 7.59 | 9.48 | 11.38 | 13.28 | 15.17 | 17.07 |
| 10 | 18.96 | 20.86 | 22.76 | 24.65 | 26.55 | 28.45 | 30.34 | 32.24 | 34.14 | 36.03 |
| 20 | 37.93 | 39.83 | 41.72 | 43.62 | 45.52 | 47.41 | 49.31 | 51.21 | 53.10 | 55.00 |
| 30 | 56.89 | 58.79 | 60.69 | 62.58 | 64.48 | 66.38 | 68.27 | 70.17 | 72.07 | 73.96 |
| 40 | 75.86 | 77.76 | 79.65 | 81.55 | 83.45 | 85.34 | 87.24 | 89.13 | 91.03 | 92.93 |
| 50 | 94.82 | 96.72 | 98.62 | 100.51 | 102. 41 | 104.31 | 106.20 | 108.10 | 110.00 | 111.89 |
| 60 | 113.79 | 115.69 | 117.58 | 119.48 | 121.37 | 123.27 | 125.17 | 127.06 | 128.96 | 130.86 |
| 70 | 132.75 | 134.65 | 136.55 | 138.44 | 140.34 | 142.24 | 144.13 | 146.03 | 147.93 | 149.82 |
| 80 | 151.72 | 153.62 | 155.51 | 157.41 | 159.30 | 161.20 | 163.10 | 164.99 | 166.89 | 168.79 |
| 90 | 170.68 | 172.58 | 174.48 | 176.37 | 178.27 | 180.17 | 182.06 | 183.96 | 185.86 | 187.75 |
| E |  |  |  |  | 39 |  |  |  |  |  |

1 Klafter of Vituuat $=5$ s 382220 Paris Feet.

| Klatter | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tliousands | 0. | 140. | 200. | 300. | 100. | 500. | 600. | \%80. | st0. | seo. |
| ${ }^{1}$ | Paris ft . 0.1 | Paris ft. 583. | Paris ft. <br> 1167.6 | Paris ft. <br> 1751.5 | $\begin{gathered} \hline \text { Paris ft. } \\ 2335.3 \end{gathered}$ | Paris to. 2919.1 | Patas ti. 3.02 .9 | ft . | $\xrightarrow{\text { Paris } t 1}$ | Pall is it |
| 1000 | 5838.2 | 64423.0 | 7005.9 | 7585.7 | 8173.5 | 8757.3 | 93-41.2 | 9925.0 | 10508.8 | 11092.0 |
| 2000 | 11676.4 | 122060.3 | $128+4.1$ | 13427.9 | 14011.7 | 14595.6 | 15179.4 | 15763.2 | 16347.0 | 169.30.と |
| 3000 | 17514.7 | 18098.5 | 18683.3 | 19266.1 | 19850.0 | 20433. | 21117. | 21601.4 | $\cdots 2185.2$ | 2969.1 |
| 4000 | 23352 | 23936 | 24 | 25 | 20,488.2 | 21 | 26855 | 27439 6 | 2-10.3.5 | 2 |
| $k$ lafter. | Units. |  |  |  |  |  |  |  |  |  |
| Teus. | 0. | 1. | 2. | 3. |  | 5. | 6. | 7. | s. | 9. |
| 0 | $\begin{array}{r} \text { Paris ft. } \\ 0.00 \end{array}$ | $\begin{array}{r} \text { Paris } \mathrm{ft} . \\ 5.84 \end{array}$ | Paris ft. <br> 11.68 | $\begin{array}{r} \text { Paris } \mathrm{ft} \text {. } \\ 17.51 \end{array}$ | $\begin{gathered} \text { l'aris } \mathrm{ft} \\ 2.3 .35 \\ . \end{gathered}$ | $\begin{array}{r} \hline \text { Paris ft. } \\ 29.19 \end{array}$ | Paris ft. $35.0 ;$ | Paris ft. 40.57 | Paris ft 46.71 | $\begin{aligned} & \text { P:aris ft. } \\ & 52.54 \end{aligned}$ |
| 10 | 58.35 | 64.22 | 70.06 | 75.90 | 81.74 | 87.57 | 93.41 | 99.25 | 105.02 | 110.93 |
| 20 | 116.76 | 122.60 | 128.44 | 134.28 | 141.12 | 145.96 | 151.79 | 157.63 | 163.47 | 16.3 .31 |
| 30 | 175.15 | 181.98 | 186.82 | 192.68 | 195.50 | 204.34 | 210.1 | 216.01 | 201.85 | $2-7.69$ |
| 40 | 233.53 | 239.37 | 245.21 | 251.04 | 256.88 | 262.72 | 268.51 | 274.40 | 280.23 | 286.17 |
| 50 | 291.91 | 297.75 | 303.55: | 309.43 | 315.26 | 321.10 | .296.92 | 332.78 | 338.62 | 344.46 |
| ${ }^{6} 0$ | 350.29 | 356.13 | 361.97 | 367.81 | 373.65 | 379.48 | 345.3: | 391.16 | 397.01 | 402.84 |
| 70 | 408.65 | 414.51 | 420.3: | 426.19 | 432.03 | 437.87 | 443.71 | 449.54 | 455.36i | 461.22 |
| 80 | 417.11 | 420.90 | 478.7: | 4.4 .57 | 490.41 | 496.25 | 502.0. | 507.93 | 513. | 519.60 |
| 90 | 625.44 | 531.28 | 537.1: | 042.95 | 548.7! | 554.623 | 560.45 | 5ti6.31 | 572.15 | 577.98 |

XXill. conversion of klafter of vienna into englisil feet.
1 Klafter of Vienna $=6.229173$ English Fect.

| Klafter of | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thunsands. | D. | 140. | $\therefore$ C0. | 360. | 400. | 500. | (i)0. | 910 | \$00. | SCO. |
| 0 | $\begin{array}{\|} \text { Eug. feet } \\ 0.0 \end{array}$ | $\begin{gathered} \text { Eng. feet } \\ 622.2 \end{gathered}$ | Exy.feet | $\begin{gathered} \text { Eug. feet } \\ 1866.7 \end{gathered}$ | Eug. fret | $\left.\begin{array}{\|c\|} \hline \text { Fug. freet } \\ 31111 \end{array} \right\rvert\,$ | $\begin{array}{r} \text { Eng. feet } \\ 3733.3 \end{array}$ | Ens.feet | $\begin{array}{r} \text { Eng, fret } \\ 4977.7 \end{array}$ | $\begin{gathered} \text { Eng. feet } \\ 5600.0 \end{gathered}$ |
| 1000 | 922.2 | 6844.4 | 7466.13 | 8088.8 | 8711.0 | 9333.3 | 9955.5 | 10577.7 | 11199.9 | 11 S22. 1 |
| 2000 | 12444.3 | 13066.6 | 13685.8 | 14311.0 | 14933.2 | 1:555.4 | 16177.6 | 16799.9 | 17422.1 | 18144.3 |
| 3000 | 18666.5 | 19288.7 | 19911.0 | 20533.2 | 21155.3 | 21777.c | 23390.8 | 23020.0 | 23644. | 42(6.5 |
| 4000 | 24488.7 | 25.510 .9 | 133.1 | 26755.3 | 27377.6 | 27999. | -8692. | -44. | -98fik. | 0.488.6 |
| Kiafter. |  |  |  |  | Uni | its. |  |  |  |  |
| Tens. | 0. | 1. | -2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Eng. feet | Eng. freet | Erg.feel | Eng. feet | Eng. feet | Eng. feet | Eus. fret | Eng. feei | Euc. fre: | Eny. feet |
| 0 | 0.00 | 6.22 | 12.4- | 18.67 | 24.85 | 31.11 | 37.33 | 43.56 | 49.76 | 56,00 |
| 10 | 62.22 | 68.47 | 74.67 | 80.89 | 87.11 | 93.83 | 99.55 | 10.5.78 | 112.04 | 118.22 |
| 20 | 124.44 | 130.67 | 136.80 | 143.11 | 149.38 | 155.55 | 161.78 | 168.00 | 174.20 | 180.44 |
| 30 | 186.67 | 192.89 | 199.11 | 205.33 | 211.55 | 217.78 | 224.00 | 230.22 | 236.44 | 242.66 |
| 40 | 248.89 | 255.11 | 261.33 | 267.55 | 273.78 | 280.00 | 286.22 | 292.44 | 298.65 | 304.89 |
| 50 | 311.11 | 317.33 | 323.55 | 329.78 | 336.00 | 342.20 | 348.44 | 354.66 | 360.89 | 367.11 |
| 60 | 373.33 | 379.55 | 385.77 | 392.00 | 398.22 | 404.44 | 410.66 | 416.89 | 423.11 | 429.38 |
| 70 | 435.55 | 441.76 | 448.00 | 454.22 | 460.44 | 466.66 | 472.84 | 479.11 | 485.3.3 | 491.55 |
| 80 | 497.77 | 504.00 | 510.22 | 514.44 | 52.266 | 528.86 | 535.11 | 541.33 | 547.55 | 553.77 |
| 80 | 560.00 | 546.22 | 572.44 | 578.66 | 584.88 | \| 591.11 | 597.38 | 603.55 | 6e9. 77 | 616.0 cm |

1 Fout of Vienta $=03$ itusor Metre.

| Feet of | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 300. | 400. | 500. | 600. |  | SDO. | 306. |
|  | Metres. | Metren. |  | Metres. |  | Metres. | Net | Me | . |  |
| 0 | 0.00 | 31.61 | (3). $2: 2$ | 94.50 | 126.43 | 158.04 | 189.65 | $2: 1.26$ | 252.86 | $2-4.47$ |
| 1000 | 316.08 | 347.69 | 379.30 | 410.90 | +42.51 | 474.12 | 505.73 | 537.34 | 568.95 | 600.55 |
| 2000 | 632.16 | 663.77 | 695.38 | 726.94 | 758.59 | 790.20 | $8: 1.81$ | 853.42 | 855.03 | \$116.63 |
| 3000 | 948.24 | 979.55 | 1011.46 | 1043.07 | 1074.67 | 1106.2 s | 1137.8! | 1169.50 | 1201.11 | 1232.71 |
| 4000 | 1264.32 | 1295.93 | 1327.54 | 1359.15 | 1390.761 | 1423.36 | 1453.97 | 1485.58 | 1517.19 | 1548.80 |
| 5000 | 1580.40 | 1612.01 | 1643.60 | 1675.23 | 1706.84 | 38.44 | 1770.05 | 1801.66 | 7 | 68 |
| 6000 | 18.16 .45 | 1928.09 | 1959.70 | 1:991.31 | 2022.92 | 2054.52 | 2086.13 | $\underline{2} 117.7$ | 149.3.9 | 2180.96 |
| 7000 | 2212.56 | 2244.17 | 2-25.75 | 2:307.3! | $2339.00 \mid$ | 2370.61 | 2402.21 | 2433. | 465. | $2+47.04$ |
| stare | $25 \pm 5.65$ | 2560.25 | 2591.86 | 2623.47 | 2655.08 | 2686.69 | 2718.29 | 2749.9 | 781.5 | 2813.12 |
| 9000 | 2844.73 | 2876.33 | 2907.94 | 2939.55 |  | 002.75 | 3034.37 | 3065.98 | 3097.59 | 3129.20 |
| 10000 | 3160.81 | 3192.42 | 32.24 .0 | 3255.64 | 3287.24 | 3318.85 | . 350.46 | 3382.06 | 13. | . 28 |
| 11000 | 3476.89 | 3508.50 | . 35411.14 | 3.571 .71 | 3603.323 | 3634.95 | 36666.54 | 3698.1 | 72 | . 36 |
| 12000 | 3792.97 | 38.24 .58 | 3856.1c | Scs7.79 | 3919.403 | 951.01 | .3982. 62 | 4014.2 | 1045. | 1077.44 |
| 13000 | 4109.05 | 4140.66 | 1172.ご | 1203.87 | 42:5. 48 | 267.05 | 4298.711 | 4230.3 | 4361.91 | 893.52 |
| 14000 | 4425.13 | 4456.74 | 4488.35 | 4.519 .95 | 4551.56 | 583.17 | 4614.78 | $4646.3!$ | 4677. | 4709.60 |
| 15090 | 4741.21. | 472.82 | 4814.43 | 45315.03 | 4867.64 | 4899.25 | 4930.86 | 4962.47 | 4994. 08 | 025.68 |
| 16600 | 50.77 .29 | 5085.90 | .120.51 | $\bigcirc 152.12$ | 5183.725 | $215.3: 3$ | -246.94 | 5278.55 | 5310.1 | 41.76 |
| 17000 | 5373.37 | 5444.98 | 5436.59 | -148.20 | $54!49.80$ | 531.41 | 5563.02 | 5594.63 | 5626 | 657.4 |
| Is.100 | 5089.45 | 5721.06 | -752.67 | 5784.28 | 5815.88 | 47.4 | 5879.10 | 5910.71 | 5942.3 | 73.93 |
| 19000 | 6005.53 | 6037.14 | 0058.75 | 6700.36 |  | 63.57 | 15195.18 | 6226.79 | 6255.4 | 6290.01 |
| 20600 | (3321.61 | 4353.22 | i384.83 | 6416.44 | 6448.056 | 479.6. | i511.26 | 6542.87 | 6574.4 | 3606.09 |
| 21000 | 6633.69 | 4609.30 | ;700.91 | 732.52 | 6764.13 | 795.7-4 | -207.3 | 6858.95 | 15990.5 | 922. 17 |
| 22000 | 6983.78 | (19)85.35 | 7016.99 | 7048.60 | 7080.217 | 111.62 | 7143. | 7175.03 | 7206.6 | .25 |
| 23600 | 7289.86 | 7301.415 | 7333.07 | 7364.68 | 7396.297 | 7427.90 | 7459.50 | 491.11 | 5 | 554.33 |
| $\because 4000$ | 7555.94 | 7617.54 | 7649.15 | 7680.76 |  | 7743.92 | -775.5! | 7807.20 | 7535.6 | 270.41 |
| 25000 | 7902.02 | 7933.63 | 7965.23 | 7996.84 | 8028.45 | 8060.06 | -091.67 | 123.27 | R154 | 186.49 |
| 2.0100 | ع̌28.10 | $-249.71$ | 8281.31 | $8: 312.92$ | $8: 3+4.53$ | 376.14 | $-407.7$ | 8439.3 | 8471.9 | 5.012 .57 |
| 27000 | 5334.16 | 8565.79 | 5.597 .4 | 8629.00 | 8660.61 | 6992.22 | -723. | 555. | 87 | \$18.65 |
| 25000 | 80.50 .2 |  |  |  | 8976.69 | 08.301 | , 1439. |  | 103. | . 733 |
| Fect of |  |  |  |  | Unit |  |  |  |  |  |
| Tens. | 0. | 1. | 2. | 3. | 1. | 5. | 6. | \%. | S. | 9. |
|  | Metres. | Metres. | Metres. | M+tro. | Metres. | Tetres. | Metres. | Metres. | Metres. | M + He |
| 0 | 0.00 | 0.32 | 0.63 | 0.95 | 1.26 | 1.58 | 1.90 | 2.21 | 2.53 | 2.84 |
| 10 | 3.16 | 3.48 | 3.79 | 4.11 | 4.43 | 4.74 | 5.06 | 5.37 | 5.69 | 6.01 |
| 20 | 13.32 | 6.64 | 6.95 | 7.27 | 7.59 | 7.90 | 8.22 | 8.53 | 8.85 | 9.17 |
| 30 | 9.49 | 9.80 | 10.11 | 10.43 | 10.75 | 11.06 | 11.38 | 11.69 | 12.01 | 12.33 |
| 40 | 12.64 | 12.96 | 13.28 | 13.59 | 13.91 | 14.23 | 14.54 | 14.86 | 15.17 | 15.49 |
| 50 | 15.80 | 16.12 | 16.44 | 16.75 | 17.07 | 17.38 | 17.70 | 18.02 | 18.33 | 18.65 |
| 60 | 18.96 | 19.28 | 19.60 | 19.91 | 20.23 | 20.55 | 20.86 | 21.18 | 21.4! | 21.¢1 |
| 70 | 22.13 | 22.44 | 22.76 | 23.07 | 23.39 | 23.71 | 24.02 | 24.34 | 24.65 | 24.97 |
| 80 | 25.29 | 25.60 | 25.92 | 26.23 | 26.55 | 26.57 | 27.18 | 27.50 | 27.82 | 28.13 |
| 90 | 29.45 | 28.76 | 29.08 | 29.40 | 29.71 | 30.03 | 30.34 | 30.66 | 30.98 | 31.29 |

1 Foot of Vienua $=0.9730370$ Paris Foot.

| Feet of | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousauds. | 0. | 140. | 200. | 300. | 400. | 500. | 600. | 700. | s00. | 900. |
| 0 | $\begin{aligned} & \text { Parisft. } \\ & 0.00 \end{aligned}$ | $\begin{array}{r} \text { Paris it. } \\ 97.30 \end{array}$ | $\begin{aligned} & \text { Pais } \mathrm{ft} \\ & 19 . \\ & 19 . \mathrm{ti} \end{aligned}$ | Paris ft <br> 201.91 | $\left\|\begin{array}{r} \text { Paris } \mathrm{ft} \\ 389.21 \end{array}\right\|$ | $\left\lvert\, \begin{gathered} \text { Paris ft. } \\ 486.52 \end{gathered}\right.$ | l'aris ft. 583.80 | $\begin{gathered} \text { P'aris it. } \\ 681.13 \end{gathered}$ | Paris ft. 778.43 | $\begin{aligned} & \text { Patis } \mathrm{ft} \\ & 875.73 \end{aligned}$ |
| 1000 | 973.04 | 1070.34 | 1167.64 | 1264.95 | 1362.25 | 1459.56 | 1556.86 | 1654.16 | 1751.47 | 1848.77 |
| 2000 | 1946.07 | 2043.38 | 2140.68 | 2937.99 | 2335.29 | 2432.59 | 2529.90 | 2627.20 | 27.4 .50 | 2821.81 |
| 3000 | 2919.11 | 3016.41 | 3113.72 | 3211.02 | 3308.33 | 3405.63 | 3502.93 | 3600.24 | 3697.54 | 794.84 |
| 4000 | 38.92 .15 | 3989.45 | 4086.76 | 4184.06 | 4281.36 | 4378.67 | 4475.97 | 4573.27 | 4670.58 | 4767.88 |
| 5000 | 4865.18 | 4962.49 | 5059.79 | 5157.10 | 5254.40 | 5351.70 | 5449.01 | 5546.31 | 5643.61 | 5740.93 |
| 6000 | 58.38 .22 | 59:35.53 | 6032.83 | 6130.13 | 6227.44 | 3324.74 | 6422. 04 | 6519.35 | ti616.65 | 6713.96 |
| 7000 | 6811.26 | 6908.56 | 7005.87 | 7103.17 | 7200.47 | 7297.78 | 7395.08 | 7492.38 | 7589.69 | 7686.99 |
| 8000 | 7784.30 | 7881.60 | 7978.94 | 2076.21 | 8173.51 | 8870.81 | -368.12 | 8465.42 | 8562. 73 | 8666.03 |
| 90000 | 8757.38 | -5.54.64 | S951.94 | 9049.24 | 9146.55 | 9243.65 | 9341.16 | 9438.46 | 9535.76 | 91633.07 |
| 10000 | 9730.37 | 9827.67 | 9924.91 | 10022. 3 | 10119.6 | 10216.9 | 10314.2 | 10411.5 | 10508.8 | 10606.1 |
| 11000 | 10703.4 | 10800.7 | 10898.1 | 10995.3 | 11092.6 | 11189.9 | $7 . \geq$ | $113 \times 4.5$ | 11481.8 | 11579.1 |
| 12000 | 111676.4 | 11773.7 | 11871.1 | 11968.4 | 12065.7 | 12163.0 | 12260.3 | 12957.6 | 12454.9 | 12552.2 |
| 13000 | 12644. 5 | 12746.8 | $12 \times 4.1$ | 12941.4 | 13038.7 | 13136.0 | 3233.3 | 13330.6 | 13427.9 | 13525.2 |
| 14000 | 13622.5 | 13719.8 | 13817.1 | 13914.4 | 14011.7 | 14109.0 | 4206.3 | 14303.6 | 14400.9 | 14498.3 |
| 15000 | 14595.6 | 14692.9 | 14790.2 | 14887.5 | 14984.8 | 15082.1 | 15179.4 | 15276.7 | 15374.1 | 15471.3 |
| 16000 | 15506.6 | 15665.9 | 15763.2 | 15860.5 | 15957.8 | 16055.1 | 16152.4 | 16249.7 | $1(3347.0$ | 16.44 .3 |
| 17000 | 16541.6 | 16638.9 | 16736.2 | 16833.5 | 16930.8 | 17028.1 | 17125.5 | 17222. 6 | 17320.1 | 17417.4 |
| 18000 | 17514.7 | 17612.0 | 17709.3 | 17806.6 | 17903.9 | 18001.2 | 18098.5 | 18195.6 | 15393.1 | 18350.4 |
| 19000 | 18487.7 | 18585.0 | 18682. 3 | 18779.6 | 18876.9 | 18974.2 | 19071.5 | 19168.8 | 19266.1 | 19363.4 |
| 20000 | 19460.7 | 19 | (1) | , | 19850.0 |  | 6 | 20141.9 | 20239 | 20336.5 |
| 21000 | $20433 . \mathrm{c}$ | 20531. | - | 207 | 20883.0 | 20920. | 21017 | 21114.9 | 2121 | 21309.5 |
| 22000 | 21406.5 | 21504.1 | 21601.4 | 21698. | 21796.0 | 21893.3 | 21990 | 22087.9 | 22185. | 20.2 .5 |
| 23000 | 22379.9 | 22477.2 | 22574.5 | 22 (\%) | 22769.1 | 22866.4 | 22913.7 | 23061. | 23158. | 23255.6 |
| 24000 | 23352.9 | 23450.2 | 23547.5 | 23644.8 | 23742.1 | 23539.4 | 23936.6 | 24034.0 | 24131.3 | 24228.6 |
| 25000 | 24325.9 | 24 | 4590.5 | 24617. | 24715.1 | -4812. | 7 | 7.1 | 25104. | 01.7 |
| 26000 | 25299.1 | 25396.3 | 25493.6 | 25590.9 | 25688.2 | 25785.5 | 25882.8 | 25980.1 | 26077. | 26174.7 |
| 27040 | 26272.11 | 26369.3 | 26466.6 | 26563.9 | 26661.2 | 2758.5 | 9085 | 26953.1 | 27050.4 | 27147.7 |
| 28040 |  |  |  |  | 27634.8 | -731 | のT80 | 27906 |  | 120.8 |
| et of |  |  |  |  | Unit | its. |  |  |  |  |
| Tens. | 0. | 1. | 2. | 3. |  | 5. | 6. | 7. | 8. | 9. |
| 0 | $\begin{gathered} \text { Parin ft. } \\ 0.00 \end{gathered}$ | Parisft. $0.97$ | $\begin{gathered} \text { Paris ft. } \\ 1.95 \end{gathered}$ | Paris ft. 2.92 | $\begin{gathered} \text { Paris ft. } \\ 3.89 \end{gathered}$ | $\begin{gathered} \text { 1atrsit } \\ 4.87 \end{gathered}$ | $\begin{gathered} \text { Paris } \mathrm{ft} \\ 5.84 \end{gathered}$ | $\begin{gathered} \text { Paris ft. } \\ 6.81 \end{gathered}$ | $\begin{gathered} \hline 1 \text { arso } \mathrm{ft} . \\ 7.78 \end{gathered}$ | $\begin{gathered} \text { Paris ft. } \\ 8.76 \end{gathered}$ |
| 10 | 9.73 | 10.70 | 11.68 | 12.65 | 13.62 | 14.60 | 15.57 | 16.54 | 17.51 | 18.49 |
| 20 | 19.4i | 20.43 | 21.41 | 22.38 | 23.35 | ¢4.33 | 25.30 | 26.97 | 27.25 | 28.22 |
| 30 | 29.19 | 30.16 | 31.14 | 32.11 | 33.08 | 34.06 | 35.03 | 36.00 | 36.98 | 37.95 |
| 40 | 38.92 | 39.89 | 40.87 | 41.84 | 42.81 | 43.79 | 4.76 | 45.73 | 46.71 | 47.68 |
| 50 | 48.65 | 49.62 | 50.60 | 51.57 | 52. 5.4 | 53.52 | 54.49 | 55.46 | 56.44 | 57.41 |
| 60 | 58.38 | 59.36 | 60.33 | 61.30 | 62.27 | 63.25 | 64.22 | 65.19 | 66.17 | 67.14 |
| 70 | 68.11 | 69.09 | 70.06 | 71.03 | 72.00 | 72.98 | 73.95 | 74.92 | 75.90 | 76.87 |
| 80 | 77.84 | 78.82 | 79.79 | 80.76 | 81.74 | 82.71 | 83.68 | 84.65 | 85.63 | Sti.c) |
| 90 | 87.57 | 88.55 | 89.52 | 90.49 | 91.47 | 92.44 | 93.41 | 94.36 | 95.36; | ! . 38 |

1 Foot of Vienna $=1.037029$ Egglish Feet.

| Feet of | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | S00. | D00. |
|  | Eug. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet | Enc. | Eng. feet | Eng. feet | Eng. feet |
| 0 | 0.00 | 103.70 | 207.41 | 311.11 | 414.81 | 518.51 | 622.22 | 725.92 | 829.62 | 933.33 |
| 1000 | 1037.03 | 1140.73 | 1244.43 | 1348.14 | 1451.84 | 1555.54 | 1659.25 | 762.95 | 1866.65 | 1970.36 |
| 2000 | 2074.06 | 2177.76 | 2281.46 | 2385.17 | 2488.87 | 2592.57 | 2696.28 | 2799.98 | 2903.68 | 3007.38 |
| 3000 | 3111.09 | 3246.79 | 3318.49 | 3422.20 | 3525.90 | 3629.60 | 3733.30 | 3837.01 | 3940.71 | 4044.41 |
| 4000 | 4148.12 | 4251.82 | 4355.52 | 4459.22 | 4562.93 | 4660.63 | 4770.33 | 4874.04 | 4977.74 | 5081.44 |
| 5000 | 5185.14 | 5988.85 | 5392.55 | 5496.25 | 5599.96 | 5703.66 | 5807.36 | 5911.07 | 16014.77 | 6118.47 |
| 6000 | 6232.17 | 6325.88 | 6429.58 | 6533.28 | 6636.99 | 6740.69 | 6844.39 | 6948.09 | 7051.80 | 7155.50 |
| 7000 | 7259.20 | 7362.91 | 7466.61 | 7570.31 | 7674.01 | 7777.72 | 7881.42 | 7985.12 | 8088.83 | -192.53 |
| 8000 | 8296.23 | 8399.93 | 8503.64 | 8607.34 | 8711.04 | 8814.75 | 8918.45 | 902. 15 | 9125.86 | 9229.56 |
| 9000 | 9333.26 | 9436.96 | 9540.67 | 9644.37 | 97.45 .07 | 9851.78 | 9955.48 | 10059.2 | 10162.9 | 10266.6 |
| 10000 | 10370.3 | 10474.0 | 10577.7 | 10681.4 | 10785.1 | 10888.8 | 10992.5 | 11096.2 | 11199.9 | 11303.6 |
| 11000 | 11407.3 | 11511.0 | 11614.7 | 11718.4 | 11822.1 | 11925.8 | 12029.5 | 12133. | 12236.9 | 12340.6 |
| 12000 | 12444.4 | 125.48.1 | 12651.8 | 12755.5 | 12859.2 | 12962.9 | 13066.6 | 13170. | 13274.0 | 13377.7 |
| 13000 | 13481.4 | 13585.1 | 13688.8 | 13792.5 | 13596.2 | 13999.9 | 14103.6 | 14207. | 14311.0 | 14414.7 |
| 14000 | 14518.4 | $1462 \mathrm{S}$. | 14725.8 | 14829.5 | 14933.2 | 1503 b. 9 | 15140.6 | 15244.3 | 15348.0 | 15451.7 |
| 15000 | 15555.4 | 15659.1 | 15762.8 | 15866.5 | 15970.3 | 16074.0 | 16177.7 | 16281.4 | 16385.1 | 16488.8 |
| 16000 | 16592.5 | 16690.2 | 16799.9 | 16903.6 | 17007.3 | 17111.0 | 17214.7 | 17318.4 | 17422.1 | 17525.8 |
| 17000 | 17629.5 | 17733.2 | 17836.9 | 17940.6 | 18044.3 | 18148.0 | 18251.7 | 18355. 4 | 18459.1 | 18562.8 |
| 18000 | 18666.5 | 18770.2 | 18873.9 | 18977.6 | 19081.3 | 19185.0 | 19288.7 | 19392.4 | 19496.1 | 9600.0 |
| 19000 | 19703.6 | 19807.3 | 19911.0 | 20014.7 | 20118.4 | 20222.1 | 20325.5 | 20429.5 | 20533.2 | 20636.9 |
| 20000 | 20740.6 | 20844.3 | 20948.0 | 21051.7 | 21155.4 | 21259.1 | 21362.8 | 21466.5 | 21570. | 21673.9 |
| 21000 | 21777.6 | 21881.3 | 21985.0 | 22088.7 | 22192.4 | 22296.1 | 22399.8 | 29503.5 | 22607 | 710.9 |
| 22000 | 22814.6 | 22918. | 23022.0 | 23125.8 | 33229.5 | 23333.2 | 23436.9 | 23540.6 | -3644 | 23748.0 |
| 23000 | 23851.7 | 23955.4 | 24059.1 | 24162.8 | $2+266.5$ | 24370.2 | 2473.9 | 24577.6 | 24681. | 24785.0 |
| 24000 | 24888.7 | 24992.4 | 25096.1 | 25199.8 | 25303.5 | 25407.2 | 25510.9 | 25014.6 | 25718.3 | 25822.0 |
| 25000 | 2.925 .7 | 26029.4 | 26133.1 | 26236.8 | 20340.5 | 26444.2 | 26547.9 | 26651.6 | 26755.4 | 26859.1 |
| 26000 | 26962.8 | 27066.5 | 27170.2 | 27273.9 | 27377.6 | 27481.3 | 27585.0 | 27688.7 | 27792 | 27896.1 |
| 27000 | 27999.8 | 28103. | 28207. | 28310.9 | 28414.6 | 28518.3 | 28622.0 | 28725.7 | 28829 | 8933.1 |
| 28000 | $\underline{2903}$ |  |  |  | 2917 |  | 39659 | -9762.7 | $2986+$ | 29970.1 |
| of |  |  |  |  | Uni | its. |  |  |  |  |
| Tens. | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 5. | 9. |
|  | Eng. feet | Eng. feet | Eng. feet | Eug. feet | Ens. feet | Eug. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet |
| 0 | 0.00 | 1.04 | 2.07 | 3.11 | 4.15 | 5.19 | 6.22 | 7.26 | 8.30 | 9.33 |
| 10 | 10.37 | 11.41 | 12.44 | 13.48 | 14.52 | 15.56 | 16.59 | 17.63 | 18.67 | 19.70 |
| 20 | 20.74 | 21.78 | 22.81 | 23.85 | 24.89 | 25.93 | 26.96 | 28.00 | 29.04 | 30.07 |
| 30 | 31.11 | 32.15 | 33.18 | 34.22 | 35.26 | 36.30 | 37.33 | 38.37 | 39.41 | 40.44 |
| 40 | 41.48 | 42.52 | 43.56 | 44.59 | 45.63 | 46.67 | 47.70 | 48.74 | 49.78 | 50.81 |
| 50 | 51.85 | 52.89 | 53.93 | 54.96 | 56.00 | 57.04 | 58.07 | 59.11 | 60.15 | 61.18 |
| 60 | 62.22 | $6: 3.26$ | 64.30 | 65.33 | 66.37 | 67.41 | 68.44 | 69.48 | 71.52 | 71.56 |
| 70 | 72.59 | 73.63 | 74.67 | 75.70 | 76.74 | 77.78 | 78.81 | 79.85 | 80.89 | 81.93 |
| 80 | 82.96 | 84.00 | 85.04 | 86.07 | 87.11 | 88.15 | 89.18 | 90.22 | 91.26 | 92.30 |
| 90 | 93.33 | 94.37 | 95.41 | 96.44 | 97.48 | 98.52 | 99.55 | 100.59 | 101.63 | 102.67 |

## XXVIl. conversion of feet of vienna into rhine or prussian feet.

1 Foot of Vienna $=1.007096$ Rhine Feet.

| Feet ot | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 6. | 100. | 200. | 300. | 400. | \%00. | 600. | 700. | 800. | 380. |
| 0 | Rhine ft 0.00 | Rhine tt. $100.71$ | Rhine ft. 201.42 | $\begin{array}{\|r\|} \text { Rhine ft. } \\ 302.13 \end{array}$ | $\begin{gathered} \text { Rhine it } \\ 402.84 \end{gathered}$ | $\begin{array}{r} \text { Rhine ft. } \\ 503.55 \end{array}$ | Rhine ft. $60.4 .26$ | $704.97$ | $\begin{aligned} & \text { Rhume } \mathrm{ft} \\ & 8(1.5 .68 \end{aligned}$ | $\begin{aligned} & \text { hinurft. } \\ & 906.39 \end{aligned}$ |
| 1000 | 1007.10 | 1107.81 | 1208.52 | 1309.20 | 409.93 | 1510.64 | 1611.35 | 712. | 12. | 13.45 |
| 2000 | 2014.19 | 2114.90 | 2215.61 | 2316.32 | 2417.03 | 2517.74 | 2618.4 | 719.1 | 19. | 20.58 |
| 3000 | 3021.29 : | 3028.00 | 3222.71 | 3323.42 | $3+24.13$ | 3524.84 | 3625.55 | T | 826.9 | 27.67 |
| 4000 | 4108.3 s | 4129.09 | 4239.80 | 4330.51 | 4431.22 | 4531.93 | 4632. | 33.3 | 4834. | 93-4.77 |
| 5000 | 5035.48 | 5136.19 | 5236.90 | 5337.61 | 5438.32 | 39.03 |  |  |  |  |
| 6000 | 6042.58 | 6143.29 | 6244.00 | 6344.70 | (644\%). 41 | 65546.12 | 6646.8 | 747. | 6.45. | 94-.96 |
| 7000 | 7144.9.67 | 7150.38 | 7251.09 | 7351.80 | 7452.51 | 7503.22 | 7653.93 | 54.6 | 555. | 956.06 |
| 8000 | -056.75 | ¢157.48 | 8258.19 | -358.90 | $\pm 459.61$ | 8560.32 | 8661.03 | 761.7 | 8662. | 163.15 |
| 9000 | 9063.86 | 9164.57 | 9265.28 | 9365.99 | 9466.70 | 95067.41 | 9668.1 | 768. | 69 | 5 |
| 10000 | 10071.0 | 10171.7 | 10272.4 | 10373.1 | 10473.8 | 1574.5 | 10 | 775 | 10876 | . 3 |
| 11000 | 11078.1 | 11178.8 | 11279.5 | 11380.2 | 11450.9 | 11581.6 | 11688. | 1783 | 1883. | 1984.4 |
| 12000 | 12055.2 | $12 \pm 85.9$ | 12086.6 | 12387.3 | 12488.0 | 12508.7 | 126E9.4 | 2790.1 | 2c910. | 2991.5 |
| 13000 | 13093.2 | 13193.0 | 13293.7 | 13394.4 | 13495.1 | 13595.6 | 13696.5 | 3797. | 38.97. | 3998.5 |
| 14000 | 14099.3 | 14200.1 | 14300.8 | 14401.5 | 14502.2 | 14602.9 | 14703.6 | 480 | 4905 | 5005.7 |
| 15000 | 15106.4 | 1.507 .1 | 15307.9 | 1.7408 .6 | 15509.3 | 15610.0 | 15710.7 | 15811.4 | 5912. | 16012.8 |
| 16000 | 16113.5 | 16214.2 | 16315.0 | 16415.7 | 16516.4 | 16617.1 | 16717.8 | 1681 | 6919 | . 9 |
| 170018 | 17120.6 | 17221.3 | 17322.1 | 17422.8 | 17523.5 | 17624.2 | 17724. | 7825 | 7992. | 8107.0 |
| 18000 | 18127.7 | 18228.4 | 18329.1 | 18429.9 | 18530.6 | 18631.3 | 18732.0 | 188:2. | 18933. | 19084.1 |
| 19000 | 19134. 6 | 19235.5 | 19336.2 | 19437.0 | $19537.7$ | 19638.4 | 19739.1 | 19839.8 | 19940.5 | 20041.2 |
| 20000 | 20141.9 | 20242.6 | 20343.3 | 20444.0 | 2054.8 | 20645.5 | 20746.2 | 20846.9 | 20947.6 | 21048.3 |
| 21000 | 21145.0 | 21249.7 | 21350.4 | 21451.1 | 21551.9 | 21652.6 | 21753. | 21854. | 2954. | 2955.4 |
| 22000 | 22156.1 | 22956.8 | $2 \pm 357.5$ | 22458.2 | 22559.0 | 22659.7 | 22760. | 2861 | 22961 | 23062.5 |
| 23000 | 23163.2 | 23263.9 | 23364.6 | 23465.3 | 23566.0 | 231666.8 | 23767 | 3868 | 23968 | 24069.6 |
| 24000 | $\because 4170.3$ | - 4231.0 | 24371.7 | 24172 | 24573.1 | 24673.9 | 2477 | 24875 | 24976. | 25076.7 |
| 25000 | 25177.4 | 25278.1 | 2.3378 .8 | 25479.5 | 25580.2 | 25188.9 | 25781 | 5882 | 25983. | $\underline{96083.8}$ |
| 26000 | 26184.5 | 26285 | 26385.9 | 26486.6 | 26587.3 | 26688.1 | 2175 | S88 | 69910 | 7090.9 |
| 27000 | $\because 191.6$ | 27292 | -7393.0 | 27493. | 27594.4 | 7695.1 | 27795. | 889. | 799 | 50:8.0 |
| 28000 | 2 |  | 08100.1 |  | 28601.5 | 5702 | - | 8903 | 900 | 9105. 1 |
| of |  |  |  |  |  | its. |  |  |  |  |
| Tens. | O. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Phineft. | Rhineft. | Rhineft. | Rhine ft. | Rhine it | Rhine ft . | Rhine ft | Mhneft. | Hhine ft . | Rhineft. |
| 0 | 0.00 | 1.01 | 2.01 | 3.02 | 4.03 | 5.04 | 6.04 | 7.05 | 8.06 | 9.06 |
| 10 | 10.07 | 11.08 | 12.09 | 13.09 | 14.10 | 15.11 | 16.11 | 17.12 | 18.13 | 19.13 |
| 20 | 20.14 | 21.15 | 22.16 | 23.16 | 24.17 | 28.18 | 26.18 | 27.19 | 28.20 | 29.21 |
| 30 | 30.21 | 31.22 | 32.23 | 33.23 | 34.24 | 35.25 | 36.26 | 37.26 | 38.27 | 39.28 |
| 40 | 40.28 | 41.89 | 42.30 | 43.31 | 44.31 | 45.32 | 46.33 | 47.33 | 48.34 | 49.35 |
| 50 | 50.35 | 51.36 | 52.37 | 53.38 | 54.38 | 55.39 | 56.40 | 57.40 | 58.41 | 59.42 |
| 60 | 60.43 | 61.43 | 62.44 | 63.45 | (64.45 | (65.46 | 66.47 | 67.48 | 68.48 | 69.49 |
| 70 | 70.50 | 71.50 | 72.51 | 73.52 | 74.53 | 75.53 | 76.54 | 77.55 | 78.55 | 79.56 |
| 80 | 80.57 | 81.57 | 82.58 | 83.59 | 84.60 | 85.60 | 86.61 | 87.62 | 88.62 | 89.63 |
| 90 | 00.64 | 91.65 | 92.65 | 93.66 | 94.67 | 95.178 | 96.68 | 97.69 | 98.70 | 99.70 |

## TO CONVERT

## RHINE OR PRUSSIAN FEET

## 1NTO DIFFERENT MEASURES OF LENGTH.

XXVIII. conversion of riline or prussian feet into frencil toises.

1 Rhiue Foot $=0.1610301$ Toise.

| Khine f | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | S660. | 900. |
| 0 | Toises. $0.00$ | Tuises. $16.10$ | Tuises. <br> 32.21 | Toisen. $48.31$ | $\begin{gathered} \text { Tuises. } \\ 64.41 \end{gathered}$ | Toises. 80.52 | Tuises. $96.62$ | Toises. 112.72 | $\begin{aligned} & \text { Tuises. } \\ & 128.8 \end{aligned}$ | Toines. $14.93$ |
| 1000 | 161.03 | 177.13 | 193.24 | 209.34 | 225.4t | 241.55 | 257.65 | 273.75 | 259.65 | 305.96 |
| 2000 | 322.06 | 338.16 | 354.27 | 370.37 | 386.47 | 402.58 | 418.68 | 434.78 | 450.88 | 466.99 |
| 3000 | 483.09 | 499.19 | 515.30 | 531.411 | 547.50 | 563.61 | 579.71 | 595.81 | 611.91 | 62.02 |
| 4009 | 634.12 | 650.22 | 666.33 | 692.43 | 708.53 | 724.64 | 740.74 | 756.84 | 772.94 | 789.05 |
| XXIX. conversion of rhine or prussian feet into metres. 1 Rhine Foot $=0.31305350$ Metre. |  |  |  |  |  |  |  |  |  |  |
| Rhine feet. <br> Thonsands. | Rhine Fect. Ifundreds. |  |  |  |  |  |  |  |  |  |
|  | 0. | 100. | 0800. | 300. | 100. | D90. | 600. | 300. | 800. | 900. |
|  | Metres. | Metres | Metres | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | M.tres. |
| 0 | 0.00 | 31.39 | 62.77 | 94.16 | 125.54 | 156.93 | 188.31 | 219.70 | 251.08 | 282.47 |
| 1000 | 313.85 | 345.24 | 376.62 | 408.01 | 439.39 | 470.75 | 502.17 | 533.55 | 564.94 | 596.32 |
| 2000 | 627.71 | 659.0 ! | 690.4 | 721.86 | 753.25 | 784.63 | 816.02 | 847.40 | 578.90 | 910.18 |
| 3000 | 941.56 | 972.95 | 1004.33 | 1035.72 | 1067.10 | 1098.49 | 1129.87 | 1161.26 | 1192.64 | 1224.03 |
| 4000 | 1255.41 | 1286.80 | 1318.18 | 1349.57 | 1380.96 | 1412.34 | 1443.73 | 1475.11 | 1506.50 | 1537.88 |
| 5000 | 1569.27 | 1600.65 | 1632.04 | 1663.42 | 1694.81 | 1726.19 | 1757.58 | 1788.97 | 1520.35 | 1851.74 |
| 6000 | 1883.12 | 1914.51 | 1945.89 | 1977.2 | 2008.66 | 2040.05 | 2071.43 | 2102.82 | 2134.20 | 2165.59 |
| 7000 | 2196.97 | 2238.30 | 2259.75 | 2291.13 | 2322.52 | 2353.90 | 2385.29 | 2416.15 | $2+48.0$ | 2479.44 |
| 8000 | 2510.8 | 2542.21 | 2573.60 | 2604.9 | 2636.37 | 2667.76 | 2699.14 | 2730.53 | 2761.9 | 793.30 |
| 9000 | 2824 | -550.07 |  | 918. | 50.22 | 2981.61 | 3012.9 | 304 4.38 | 3075 | 107.15 |
| Rhine feet. Tens. | Uuits. |  |  |  |  |  |  |  |  |  |
|  | 0. | 1. | 2. | 3 | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metre | Metres | Mctres. |
| 0 | 0.00 | 0.31 | 0.63 | 0.94 | 1.26 | 1.57 | 1.88 | 2.211 | 2.51 | 2.82 |
| 10 | 3.14 | 3.45 | 3.77 | 4.08 | 4.39 | 4.71 | 5.02 | 5.84 | 5.65 | 5.96 |
| 20 | 6.28 | 6.59 | 6.90 | 7.22 | 7.53 | 7.85 | 8.16 | 8.47 | 8.79 | 9.10 |
| 30 | 9.42 | 9.73 | 10.04 | 10.36 | 10.67 | 10.98 | 11.30 | 11.61 | 11.93 | 12.24 |
| 40 | 12.55 | 12.87 | 13.18 | 13.50 | 13.81 | 14.12 | 14.44 | 14.75 | 15.06 | 15.38 |
| 50 | 15.69 | 16.01 | 16.32 | 16.63 | 16.95 | 17.26 | 17.58 | 17.89 | 18.20 | 18.52 |
| 60 | 18.83 | 19.15 | 19.46 | 19.77 | 20.09 | 20.40 | 20.71 | 21.03 | 21.34 | 21.66 |
| 70 | 21.97 | 22.28 | 22.60 | 22.91 | 23.23 | 23.54 | 23.85 | 24.17 | 24.48 | 24.79 |
| 80 | 25.10 | 25.42 | 25.74 | 26.05 | 26.36 | 26.68 | 26.99 | 27.31 | 27.62 | 27.93 |
| 90 | 28.25 | 28.56 | 28.87 | 29.19 | 29.50 | 29.82 | 30.13 | 30.44 | 30.76 | 31.07 |

XXX. conversion of rhine or prussian feet into french feet and DECIMALS.
1 Rhine Foot $=0.96615056$ French Foot.

| Rhine Feet. | Rhine Feet. Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | (1). | 100. | 2200. | 300. | 400. | 500. | 600. | 700. | S00. | 90 (1). |
| 0 | $\begin{array}{r} \text { Fr. teet. } \\ 0.00 \end{array}$ | Fr. teet. 96.62 | Fr. teet. <br> 193.94 | Fr. feet. 289.85 | $\begin{gathered} \hline \text { Fr. feet. } \\ 386.47 \end{gathered}$ | $\begin{gathered} \text { Fr. feet. } \\ 483.09 \end{gathered}$ | $\begin{array}{r} \text { Fr. feet } \\ 579.71 \end{array}$ | Fr. feet. 676.33 | Fr. feet. $772.94$ | $\begin{array}{\|c\|} \text { Fr. feet. } \\ 869.56 \end{array}$ |
| 1000 | 966.18 | 1062.80 | 1159.42 | 1256.03 | 1352.65 | 1449.27 | 1545.89 | 1642.51 | 1739.13 | 1835.74 |
| 2000 | 1932.36 | 2028.98 | 2125.60 | 2202.22 | 2318.83 | 2415.45 | 2512.07 | 2608.69 | 2705.31 | 2801.92 |
| 3000 | 2898.54 | 2995.16 | 3091.78 | 3188.40 | 3285.01 | 3381.63 | 3478.25 | 3574.87 | 3671.49 | 3781.10 |
| 4000 | 3864.72 | 3961.34 | 4057.96 | 4154.58 | 4251.19 | 4347.81 | 4444.43 | 4541.05 | 4637.67 | 4734.28 |
| 5000 | 4830.90 | 4927.52 | 5034.14 | 5120.76 | 5217.38 | 5313.99 | 5410.61 | 5507.23 | 5603.85 | 5700.47 |
| 6000 | 5797.08 | 5893.70 | 5990.32 | 6086.94 | 6183.56 | 6280.17 | 6376.79 | 6473.41 | 6570.03 | 6666.65 |
| 7000 | 6763.26 | 6859.88 | 6956.50 | 7053.12 | 7149.74 | 7246.35 | 7342.97 | 7439.59 | 7536.21 | 7632.83 |
| 8000 | 7629.44 | 7526.06 | 7922.68 | 8019.30 | 8115.92 | 8212.53 | 8309.15 | 8405.77 | 8502.39 | 8509.01 |
| 9000 | 8695.63 | 8792.24 | 5858.86 | 8985.48 | 9082.10 | 9178.72 | 9275.33 | 9371.95 | $9468.57$ | 9565.19 |

XXXI. Conversion of rhine or prussian feet into english feet.

1 Rhine Foot $=1.0297217$ English Feet.

| Rhine Feet. | Hondreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thonsands. | (1). | 100. | 200. | 300. | 400. | 509. | 600. | 700. | 800. | 300. |
| 0 | Eng. <br> (1.1) <br> (1) | Eng. ft. $102.97$ | Eng. ft. 205.94 | $\begin{gathered} \text { Eng. ft. } \\ 305.92 \end{gathered}$ | $\begin{gathered} \hline \text { Eng. ft. } \\ 411.89 \end{gathered}$ | $\begin{aligned} & \text { Eng. ft. } \\ & 514.86 \end{aligned}$ | $\begin{gathered} \text { Eng. ft. } \\ 617.83 \end{gathered}$ | Eng. ft. $720.81$ | Eng. ft. 823.78 | $\begin{gathered} \text { Eng. ft. } \\ 926.75 \end{gathered}$ |
| 1000 | 1029.72 | 1132.69 | 1235.67 | 1338.64 | 1411.61 | 1544.58 | 1647.55 | 1750.53 | 1853.50 | 1956.47 |
| 2000 | 2059.44 | 2162.42 | 2265.39 | 2368.36 | 2471.33 | 2574.30 | 2677.28 | 2780.25 | 2883.22 | 2986.19 |
| 3000 | 3089.17 | 3192.14 | 3295.11 | 3398.08 | 3501.05 | 3604.03 | 3707.00 | 3809.97 | 3912.94 | 4015.92 |
| 4000 | 4118.59 | 4221.86 | 4324.83 | 4427.80 | 4530.78 | 4633.75 | 4736.72 | 4839.69 | 4942.66 | 5045.64 |
| 5000 | 5148.61 | 5251.58 | ,5354.55 | 5457.53 | 5560.50 | 5663.47 | 5766.44 | 5869.41 | 5972.39 | 6075.36 |
| 6000 | ${ }^{1} 6178.33$ | 6281.30) | 6384.28 | 6487.25 | 6590.22 | 6693.19 | 6796.16 | 6899.14 | 7002.11 | 7105.08 |
| 7000 | 7208.05 | $7311.0{ }^{\circ}$ | 7414.00 | 7516.97 | 7619.94 | 7722.91 | 7825.89 | 7928.86 | 8031.83 | 8134.80 |
| 8000 | 8837.77 | 83-40.75, | S443.72 | 8546.69 | 8649.66 | 8752. 64 | 8855.61 | 8958.5¢ | 9061.55 | 9164.52 |
| 9000 | 9267.50 | 9370.47 | 9473.44 | 9576.41 | 9679.38 | 9782.36 | 9885.33 | 9988.30 | 10091.3 | 10194.2 |
| Rhine Feet. |  |  |  |  | Uni | its. |  |  |  |  |
| Tens. | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | s. | 9. |
| 0 | $\begin{gathered} \text { Eng. ft. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { Eng. ft. } \\ 1.03 \end{gathered}$ | $\begin{aligned} & \text { Eng. ft } \\ & 2.06 \end{aligned}$ | $\begin{gathered} \text { Eng. ft. } \\ 3.09 \end{gathered}$ | $\begin{gathered} \text { Eag ft. } \\ 4.12 \end{gathered}$ | $\begin{gathered} \text { Eng. ft. } \\ 5.15 \end{gathered}$ | $\begin{array}{r} \hline \text { Eug. ft. } \\ 6.18 \end{array}$ | $\begin{array}{r} \text { Eng. ft } \\ 7.21 \end{array}$ | $\begin{gathered} \text { Eng. } \mathrm{ft} \\ 8.24 \end{gathered}$ | $\begin{gathered} \text { Eng. ft. } \\ 9.27 \end{gathered}$ |
| 10 | 10.30 | 11.33 | 12.36 | 13.39 | 14.42 | 15.45 | 16.48 | 17.51 | 18.53 | 19.56 |
| 20 | 20.69 | 21.62 | 22.65 | 23.68 | 24.71 | 25.74 | 26.77 | 27.80 | 28.83 | 29.86 |
| 30 | 30.89 | 31.92 | 32.95 | 33.98 | 35.01 | 36.04 | 37.07 | 38.10 | 39.13 | 40.16 |
| 40 | 41.19 | 42.22 | 43.25 | 44.28 | 45.31 | 46.34 | 47.37 | 48.40 | 49.43 | 50.46 |
| 50 | 51.49 | 52.52 | 53.55 | 54.58 | 55.60 | 56.63 | 57.66 | 58.69 | 59.72 | 60.75 |
| 60 | 61.78 | 62.81 | 63.84 | 64.87 | 65.90 | 66.93 | 67.96 | 68.99 | 70.02 | 71.05 |
| 70 | 72.08 | 73.11 | 74.14 | 75.17 | 76.20 | 77.23 | 78.26 | 79.29 | 80.32 | 81.35 |
| 80 | 82.38 | 83.41 | 8.4 .44 | 85.47 | 86.50 | 87.53 | 88.56 | 89.59 | 90.62 | 91.65 |
| 90 | 92.67 | 93.70 | 94.73 | 95.76 | 96.79 | 97.82 | 98.85 | 99.88 | 100.91 | 101.94 |

XXXII. conversion of rhine or prussian feet into feet of vienna.

1 Rhine Foot $=0.9929336$ Foot of Vienua.

| Rhine feet. <br> Thousands. | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (b. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | sob. | 900. |
| 0 | Vien. ft. 0.00 | Vien. ft. 99.30 | Vien. ft. $198.59$ | Vien. ft. 297.89 | $\begin{array}{\|r} V i e n, f t . \\ 397.18 \end{array}$ | Vien. ft . 496.48 | Vien. ft. $595.77$ | Vien. ft. $695.07$ | $\begin{array}{\|r\|} \hline \text { Vien. ft. } \\ 794.36 \end{array}$ | Vien. ft. 893.66 |
| 1000 | 992.95 | 1092.25 | 1191.54 | 1290.84 | 1390.14 | 1489.43 | 1588.73 | 1688.02 | 1787.32 | 1886.61 |
| 2000 | 1985.91 | 2085.20 | 2184.50 | 2283.79 | 2383.09 | 2482.38 | 2581.68 | 2680.97 | 2780.27 | 2879.57 |
| 3000 | 2978.86 | 3078.16 | 3177.45 | 3276.75 | 3376.04 | 3475.34 | 3574.63 | 3673.93 | 3773.22 | 3872.52 |
| 4000 | 3971.81 | 4071.11 | 4170.41 | $4 \geq 69.70$ | 4369.00 | +468.29 | 4567.59 | 4666.88 | 4766.18 | 4865.47 |
| 5000 | 4964.77 | 5064.06 | 5163.36 | 5262.65 | 5361.95 | 5461.24 | 5560.54 | 5659.84 | 5759.13 | 5858.43 |
| 6000 | 5957.72 | 6057.02 | 6156.31 | 6255.61 | 6354.90 | 6454.20 | 6553.49 | 6652.79 | 6752.08 | 6851.38 |
| 7000 | 6950.68 | 7049.97 | 7149.27 | 7248.56 | 7347.86 | 747.15 | 7546.45 | 7645.74 | 7745.04 | 7844.33 |
| 8000 | 7943.63 | 8042.92 | 8142.22 | 8241.51 | 8340.81 | 8440.11 | 8539.40 | 8638.70 | 8737.99 | 8837.29 |
| 9000 | S936.58 | 9035.88 | 9135.17 | 9234.47 | 9333.76 | 9433.06 | 9532.35 | 9631.65 | 9730.95 | 9830.24 |
|  |  |  |  |  |  |  |  |  |  |  |
| Rhine feet. |  |  |  |  | Uni | its. |  |  |  |  |
| Tens. | 0. | 1. | 2. | 3. | 4. | 5. | 6. | \%. | 8. | 9. |
|  | Vien. ft. | Vien. ft. | Vien ft. | Vien. ft. | Vien ft. | Vien. ft. | Vien. ft . | Vien. ft. | Vien. ft. | Vien. ft. |
| 0 | 0.00 | 0.99 | 1.99 | 2.98 | 3.97 | 4.96 | 5.96 | 6.95 | 7.94 | 8.94 |
| 10 | 9.93 | 10.92 | 11.92 | 12.91 | 13.90 | 14.89 | 15.89 | 16.88 | 17.87 | 18.87 |
| 20 | 19.86 | 20.85 | 21.84 | 22.84 | 23.83 | 24.82 | 25.82 | 26.81 | 27.80 | 28.80 |
| 30 | 29.79 | 30.78 | 31.77 | 32.77 | 33.76 | 34.75 | 35.75 | 36.74 | 37.73 | 38.73 |
| 40 | 39.72 | 40.71 | 41.70 | 42.70 | 43.69 | 44.68 | 45.68 | 46.67 | 47.66 | 48.65 |
| 50 | 49.65 | 50.64 | 51.63 | 52.63 | 53.62 | 54.61 | 55.61 | 56.60 | 57.59 | 58.58 |
| 60 | 59.58 | 60.57 | 61.56 | 62.56 | 63.55 | 64.54 | 65.53 | 66.53 | 67.52 | 68.51 |
| 70 | 69.51 | 70.50 | 71.49 | 72.49 | 73.48 | 74.47 | 75.46 | 76.46 | 77.45 | 78.44 |
| 80 | 79.44 | 80.43 | 81.42 | 82.42 | 83.41 | 84.40 | 85.39 | S6.39 | 87.38 | 88.37 |
| 90 | 89.37 | 90.36 | 91.35 | 92.34 | 93.34 | 94.33 | 95.32 | 96.32 | 97.31 | 98.30 |

XXXIII. conversion of bavarian feet into metres.

1 Batvarian Foot $=0.2918 .992$ Metre

| Bavarian | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | O. | 100. | 200. | 300. | 400. | 500. | 600. | 700. | S00. | 900. |
|  | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. |  | Metres. |  |
| 0 | 0.00 | 29.19 | 58.37 | S7.56 | 116.74 | 145.93 | 175.12 | 204.30 | 233.49 | 262.67 |
| 1000 | 291.86 | 321.05 | 350.23 | 379.42 | 408.60 | 437.79 | 466.97 | 496.16 | 525.35 | 554.53 |
| 2000 | 583.72 | 612.90 | 642.09 | 671.28 | 700.46 | 729.65 | 758.83 | 788.02 | 817.21 | 846.39 |
| 3000 | 875.58 | 904.76 | 933.95 | 963.14 | 992.32 | 1021.51 | 1050.69 | 1079.88 | 109.06 | 25 |
| 4000 | 1167.44 | 1196.62 | 1225.81 | 1254.99 | 1284.18 | 1313.37 | 1342.55 | 1371.74 | 1400.92 | 1430.11 |
| 5000 | 1459.30 | 1488.48 | 1517.67 | 1546.85 | 1576.04 | 1605.23 | 1634.41 | 1663.60 | 1692.78 | 1721.97 |
| 6000 | 1751.16 | 1780.34 | 1809.53 | 1838.71 | 1867.90 | 1597.08 | 1926.27 | 1955.46 | 1984.6 | 013.83 |
| 7000 | 2043.01 | 2072.20 | 2101.39 | 2130.57 | 2159.76 | 2188.94 | 2218.13 | 2247.32 | 2276.50 | 2305.69 |
| 8000 | 2334.87 | 2364.06 | 2393.25 | 2422.43 | 2451.62 | -480.80 | 2509.99 | 2539.17 | 2568.36 | 2597.55 |
| 9000 | 2626.73 | 2655.92 | 2685.10 | 2714.29 | 2743.48 | 2772.66 | 2801.85 | 2831.03 | 2860.22 | 2889.41 |

TO CONVERT

THE OLD SPANISH, MEXICAN, AND BOLIVIAN VARAS AND FEE'T

INTO DIFFERENT MEASURES OF LENGTH.


#### Abstract

YXXIV. CONVERSION OF SPANISH VARAS INTO METRES. 1 spani h Vara $=0.83590$ io Metre.




1 Mexicau Vara $=0.038$ Metre.

| Mexican | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 300. | 409. | 500. | 600. | 700. | cose | 900. |
| 0 | Metres. $0.0$ | Metres. $83.8$ | Metres. $167.6$ | Metres. <br> 251.4 | $\begin{gathered} \text { Metres. } \\ 335.2 \end{gathered}$ | Merres. $419.0$ | Metres. $50-2$ | Metres. 586.6 | Metres. <br> 670.4 | $\begin{array}{r} \text { Metres. } \mid \\ 754.2 \end{array}$ |
| 1000 | 838.0 | 921.8 | 1005.6 | 1089.4 | 1173.2 | 1257.0 | 1340.8 | 1434.6 | 1508.4 | 1592.2 |
| 2000 | 1676.0 | 1759.8 | 1843.6 | 1927.4 | 2011.2 | 2095.0 | 2178.8 | 2262.6 | 2346.4 | 2430.2 |
| 3000 | 2514.0 | 2597.8 | 2681.6 | 2765.4 | 2849.2 | 2933.4 | 3016.8 | 3100.6 | 3184.4 | 3268.2 |
| 4000 | 3352.0 | 3435.8 | 3519.6 | 3603.4 | 3687.2 | 3771.0 | 3554.8 | 3938.6 | 402.2.4 | 4106.2 |
| 5000 | 4190.0 | 4273.8 | 4357.6 | 4441.4 | 45.25 .2 | 4609.0 | 4692.8 | 4776.6 | 4860.4 | 494.2 |
| 6000 | 51428.0 | 5111.8 | 5195.6 | 5279.4 | 5363.2 | 5447.0 | 5530.8 | 5614.6 | 5695.4 | 578..2 |
| 7000 | 5886.0 | 5949.8 | 6033.6 | 6117.4 | 6201.2 | 6285.1 | 6368.8 | 6452.6 | 6536.4 | 6620.2 |
| Sinoo | 6704.0 | 6787.8 | 6871.6 | 6955.4 | 7039.2 | 7123.0 | 7206.8 | 7290.6 | 73.4 .4 | 7458.2 |
| SOPO) | 7542.0 | 76925.8 | 7709.6 | 7793.4 | 7877.2 | 7961.11 | 8044.8 | 8128.6 | 8212.4 | 8296.2 |
| XXXVII. Conversion of mexican feet into metres. 1 Mexican Foot $=0.2793333$ Metre. |  |  |  |  |  |  |  |  |  |  |
| Mexican | Huadreds. |  |  |  |  |  |  |  |  |  |
| Thonsands. | 0. | 10 | (1). | 300. | 100. | 5(1). | 600. | 300. | 8000 | 9009. |
|  | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Menes. | Metres. |
| 0 | 0.00 | 27.93 | 55.87 | 83.80 | 111.73 | 139.67 | 167.60 | 195.53 | 2.23 .47 | 251.40 |
| 1000 | 279.33 | 307.27 | 335.20 | 363.13 | 391.07 | 419.00 | 446.93 | 474.87 | 502.80 | 530.73 |
| 2000 | 558.67 | 586.60 | 614.53 | 642.46 | 670.40 | 698.33 | 726.27 | 754.20 | 782.13 | 810.07 |
| 3000 | 838.00 | 865.93 | 893.57 | 021.80 | 949.73 | 977.67 | 1005.60 | 1033.53 | $10<1.47$ | 1089.4 |
| 4000 | 1117.33 | 1145.27 | 1173.20 | 1201.13 | 1229.07 | 1257.00 | 1284.93 | 1312.87 | $13 \div 0.80$ | 1368.73 |
| 5000 | 1396.67 | 1424.60 | 1452.53 | 1480.47 | 1508.40 | 1536.33 | 1564.27 | 1592.20 | 1620.13 | 1448.07 |
| 6000 | 1676.00 | 1703.93 | 1731.87 | 1759.80 | 1787.73 | 1815.67 | 1843.60 | 1871.53 | 1890.15 | 1927.40 |
| 7000 | 1955.33 | 1983.27 | 2011.20 | 2039.13 | 2067.07 | 2095.00 | 2122.93 | 2150.87 | $\because 178.80$ | 2206.73 |
| 8000 | 2234.67 | 2262.60 | 2290.53 | 2318.47 | 2346.40 | 2374.33 | 2402.27 | 2430.20 | -2158.1 | 2486.07 |
| 98000 | 2514.00 | 25.41 .93 | 25,69.87 | 2597.81 | 2425.73 | 2653.67 | 2681.60 | 2709.53 | 2787.47 | 2765.40 |

XXXVIII. conversion of mexican feet into englisil feet.

1 Mexican Fout $=0.91640477$ English Fuot.

| Mexican | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands | (1). | 100. | $\because 00$. | 300. | 100. | 5000. | 6 (10). | \% 0 (1). | E0N. | 980. |
|  | Ens. feet | Eng. feet | Eng. feet | Eug. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet | Eng. feet |
| 0 | 0.00 | 91.65 | 183.29 | 27.4 .94 | 366.59 | 458.23 | 549.88 | 641.53 | 733.17 | 824.82 |
| 1000 | 916.4 ; | 1008.81 | 1099.76 | 1191.40 | 1283.0.5 | 1374.70 | 1466.34 | 1557.99 | 1649.64 | 1741.28 |
| 2000 | 1832.93 | 1924.58 | 2016.22 | 2107.87 | 2199.51 | 2291.16 | $\underline{382.81}$ | $2+74.45$ | 2506.10 | 2657.75 |
| 3000 | 2749.39 | 2841.04 | 2932.69 | 3024.33 | 3115.94 | 3207.63 | 3299.27 | 3390.92 | 3452.56 | 3574.21 |
| 4000 | 3665.86 | 3757.50 | 3849.15 | 3940.80 | 4032.44 | 4124.09 | 4215.74 | 4307.38 | 4399.03 | 4490.68 |
| 5000 | 4582.32 | 4673.97 | 4765.62 | 4857.26 | 4948.91 | 5040.16 | 5132.20 | 5223.85 | 5315.49 | 5407.14 |
| 6090 | 5498.79 | 5590.43 | 5682.08 | 5773.73 | 5865.37 | 5957.02 | 6048.67 | 6140.31 | 6291.96 | 6323.60 |
| 7000 | 6415.25 | 15506.90 | 6598.54 | 6690.19 | 6781.84 | 6873.48 | 6965.13 | 7056.75 | 7148.42 | 7210.07 |
| S000 | 7331.72 | 7423.36 | 7515.01 | 7606.66 | 7698.30 | 7789.95 | 7881.59 | 7973.24 | 80c-2.89 | '8150.53 |
| 9000 | 18248.18 | 8339.83 | 8431.47 | 8523.12 | 8614.77 | 8706.41 | 8798.06 | 8889.71 | 8981.35 | 9073.00 |

XXXIX. conversion of bolivian, chlilan, and peruvian varas into metres.

1 Bolivian, Chilian, and Peruvian Yara $=0.5474576$ Metre.

| Bolivian | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousands. | 0. | 100. | 200. | 360. | 400. | 500. | 600. | 760. | S00. | 900. |
| 1000 |  |  |  |  |  |  |  |  | 677.97 | 762.71 |
| 2000 |  |  |  |  |  |  | 355.93 | 1440.68 | 1525.42 | 1610.17 |
| 2000 | 1694 | 1779.66 | 18 | 1949.15 | 3.90 | 2118.64 | 2203.39 | 2288.14 | 2372.88 | 2457.63 |
| 3000 | 2542.37 | 2627.12 | 2711.86 | 2796.61 | 2881.36 | 2966.10 | 3050.85 | 3135.59 | 3220.34 | 3305.08 |
| 4000 | 3389.83 | 3474.58 | 3559.32 | 3644.07 | 3728.81 | 3813.56 | 3898.30 | 3983.05 | 4067.80 | 4152.54 |
| 5000 | 4237.29 | 4322.03 | 4406.78 | 4491.53 | 4576.27 | 4661.02 | 4745.76 | 4820.51 | 4915.25 | 5000.00 |
| 6000 | 5084.75 | 5169.49 | 5254.24 | 5338.98 | 5423.73 | 5508.47 | 5593.22 | 5677.97 | 5762.71 | 5847.46 |
| 7000 | 5932.20 | 6016.95 | 6101.69 | 6186.44 | 6271.19 | 6355.93 | 6440.68 | 6525.4* | 6610.17 | 6694.92 |
| 8000 | 6779.66 | 6864.41 | 6949.15 | 7038.90 | 7118.64 | 7203.39 | 7288.14 | 7372.88 | 7457.63 | 7542.37 |
| 9000 | 7627.12 | 7711.86 | 7796.61 | 7881.36 | 7966.10 | 8050.85 | 8135.59 | 8200.34 | 8305.08 | 8389.83 |

XL. conversion of bolivian, chilian, and peruvian feet into metres. 1 Bolivian Foot $=0.25248587$ Metre.

| Bolivian | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousauds. | 0. | 100. | 200. | 300. | 400. | 500. | 600. | \%00. | S80. | 900. |
|  | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. |
| 0 | 0.00 | 28.25 | 56.50 | 84.75 | 112.99 | 141.24 | 169.49 | 197.74 | 225.99 | 254.24 |
| 1000 | 282.49 | 310.73 | 338.98 | 367.23 | 395.48 | 423.73 | 451.98 | 480.23 | 508.47 | 536.72 |
| 2000 | 564.97 | 593.22 | 621.47 | 649.72 | 677.97 | 706.21 | 734.46 | 762.71 | 790.96 | 819.2 |
| 3000 | 847.46 | 875.71 | 903.95 | 932.20 | 960.45 | 988.70 | 1016.95 | 1045.20 | 1073.45 | 1101.69 |
| 4000 | 1129.94 | 1158.19 | 1186.44 | 1214.69 | 1242.94 | 1271.19 | 1299.44 | 1327.68 | 1355.93 | 1384.18 |
| 5000 | 1412.43 | 1440.68 | 1468.93 | 1497.18 | 1525.42 | 1553.67 | 1581.92 | 1610.17 | 1638.42 | 1666.67 |
| 6000 | 1694.92 | 1723.16 | 1751.41 | 1779.66 | 1807.91 | 1836.16 | 1864.41 | 1892.66 | 1920.90 | 1949.15 |
| 7000 | 1977.40 | 2005.65 | 033.90 | 2062.15 | 2090.40 | 2118.64 | 2146.89 | 2175.14 | 2203.39 | 2231.64 |
| 8000 | 2259.89 | 2288.14 | 2316.38 | 2344.63 | 2372.88 | 2401.13 | 2429.38 | 2457.63 | 2485.88 | 2514.12 |
| 9000 | 2042.37 | 2570.62 | 2598.87 | 2627.12 | 2655.37 | 2683.62 | 2711.86 | 27.10 .11 | 2768.36 | 2796.61 |

XLI. conversion of bolivian, chilian, and peruvian feet into english feet.
1 Bolivian Foot $=0.9265078$ English Foot.

| Bolivian | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thousauds | 0. | 100. | 200. | 300. | 400. | 50. | 600. | '900. | SOO. | 500. |
|  | Eng. feet | Eng. feet | Eng.feet | Eng. feet | Eng. fert | Eng. feet | Enc. fuet | Eng. feet | Eng. feet | Eng. feet |
| 0 | 0.00 | 32.68 | 185.36 | 278.04 | 370.72 | 463.40 | 556.08 | 648.77 | 741.45 | 834.13 |
| 1000 | 926.81 | 1019.49 | 1112.17 | 1204.85 | 1297.53 | 1390.21 | 1482.89 | 1575.57 | 1668.25 | 1760.9: |
| 2000 | 1853.62 | 1946.30 | 2038.98 | 2131.66 | 2924.34 | 2317.02 | 2409.70 | 2502.38 | 2595.06 | 2687.74 |
| 3000 | 2780.42 | 2878.10 | 2965.78 | 3058.47 | 3151.15 | 3243.83 | 3386.51 | 3429.19 | 3521.87 | 3614.55 |
| 4000 | 3707.23 | 3799.91 | 3892.59 | 3985.27 | 4077.95 | 4170.64 | 4263.32 | 4356.00 | 4448.68 | 4541.36 |
| 5000 | 4634.04 | 4726.72 | 4819.40 | 4912.08 | 5004.76 | 5097.44 | 5190.12 | 5282.80 | 5375.49 | 5468.17 |
| 6000 | 5560.85 | 5653.53 | 5746.21 | 5838.89 | 5931.57 | 6024.25 | 6116.93 | 6209.61 | 6302.29 | 6394.97 |
| 7000 | 6.487 .65 | 6580.34 | 6673.02 | 6765.70 | 6858.38 | 6951.06 | 7043.74 | 7136.42 | 7229.10 | 7321.78 |
| 8000 | 7414.46 | 7507.14 | 7599.82 | 7692.50 | 7785.19 | 7877.87 | 7970.55 | S063.23 | 8155.91 | 8248.59 |
| 9090 | 8341.27 | 8433.95 | 8526.63 | 8619.31 | 8711.99 | 8804.67 | 8897.35 | 8090.04 | 9082.72 | 9175.40 |

## TO CONVERT

## FRAC'IIONAL PARTS OF A TOISE AND OF A FOOT

## INTO EACH OTHER.

XLII. CONVERSION OF INCHES INTO DUODECIMAL LINES.

1 Inch $=12$ lines.

| Inches. Tens. | . Inches. Units. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Lines. | Lines. | Lines. | Lines. | Lines | Lines | Lines. | Lines. | Lines. | Lines. |
| 0 | 0 | 12 | 24 | 36 | 48 | 60 | 72 | 84 | 96 | 108 |
| 10 | 120 | 132 | 144 | 156 | 168 | 180 | 192 | 204 | 216 | 22; |
| 20 | 240 | 252 | 264 | 276 | 288 | 300 | 312 | 324 | 336 | 348 |
| 30 | 360 | 372 | 384 | 396 | 408 | 420 | 432 | 444 | 456 | 468 |
| 40 | 480 | 492 | 504 | 516 | 528 | 540 | 552 | 564 | 576 | 588 |
| 50 | 600 | 612 | 624 | 636 | 648 | 660 | 672 | 684 | 696 | 708 |
| 60 | 720 | 732 | 744 | 756 | 768 | 780 | 792 | 804 | 816 | 828 |
| 70 | 840 | 852 | 864 | 876 | 888 | 900 | 912 | 924 | 936 | 948 |
| 80 | 960 | 972 | 984 | 996 | 1008 | 1020 | 1032 | 1041 | 1056 | 1068 |
| 90 | 1080 | 1092 | 1104 | 1116 | 1128 | 1110 | 1152 | 1164 | 1176 | 1188 |
| 100 | 1200 | 1212 | 1224 | 1236 | 1248 | 1260 | 1272 | 1284 | 1296 | 1305 |

XLIII. CONVERSION OF DECIMALS OF A TOISE INTO FEET AND INCHES.

1 Toise $=6$ Feet $=72$ Inches $=864$ Lines.

|  | Hundredths of a Toise. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tenths | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
| 0.0 | ft in lin 0.0.0.00 | ft. in. lin <br> 0. $0.8,64$ | ft. in. lin <br> 0. 1. 5,28 | ft. in. lin. $0.2 .1,92$ | ft . in lin. 0. $2 \cdot 10,56$ | ft. in. lin. <br> 0. 3.7,20 | ft. in. lin. 0. 4. 3,84 | ft.in. lin. | ft. in. lin | ft. in. lin |
| 0.1 | $0.7 .2,40$ | 0. $7.11,04$ | 0. 8. 7,68 | 0. 9. 4,32 | 0.10. 0,96 | 0.10.9,60 | 6,24 | 2,88 | 0.11,52 | . 8,16 |
| 0.2 | 1.2.4,50 | 1. 3. 1,14 | 1. $3 \cdot 10,08$ | 1. 4. 6,72 | 1. 5. 3,36 | 1. $6.0,00$ | 1. 6. 8,64 | 1.7. 5,28 | 1. 8. 1,92 | 1. $8.10,56$ |
| 0.3 | 1.9.7,20 | 1.10. 3,84 | 1.11. 0,45 | 1.11. 9,12 | 2. 0. 5,76 | 2. 1.2,40 | 2. 1.11,0t | 2.2. 7,68 | 2. 3. 4,32 | 2. 4. 0,96 |
| 0.4 | 2.4.9,60 | 2. 5. 6,24 | 2. 6. 2,88 | 2. $6.11,52$ | 2. 7. 8,16 | 2. 8.4,50 | 2. 9. 1,44 | 2.9.10,08 | 2.10.6,72 | 2.11. 3,36 |
| 0.5 | 3.0.0,00 | 3. $0.8,64$ | 3. 1. 5,28 | 3. 2. 1,92 | 3. $2 \cdot 10,56$ | 3. 3.7,20 | 3. 4. 3,84 | 3.5. 0,48 | 3. 5. 9,12 | 3. 6. 5,76 |
| 0.6 | 3.7.2,40 | 3. $7.11,04$ | 3. 8. 7,68 | 3. 9. 1,32 | 3.10. 0,96 | 3.10.9,60 | 3.11. 6,24 | 4.0. 2,88 | 4. $0.11,52$ | 4. 1. 8,16 |
| 0.7 | 4.2.4,80 | 4. 3. 1,44 | 4. 3.10,08 | 4. 4. 6,72 | +. 5. 3,36 | 4. 6.0,00 | 4. 6. 8,64 | 4.7. 5,28 | 4. 8. 1,92 | 4. 8.10,56 |
| 0.8 | 4.9.7,20 | 4.10. 3,84 | 4.11. 0,48 | 4.11. 9,12 | 5. 0. 5,76 | 5. 1.2,40 | 5. 1.11,04 | 5.2. 7,68 | 5. 3. 4,325 | 5. 4. 0,96 |
| 0.9 | 5.4.9,60 | 5. 5. 6,24 | 5. 6. 2,88 | 5. 6.11,52 | 5. 7. 8,16 | 5. 8.4,80 | 5. 9. 1,44 | 5.9.10,08 | 5.10. 6,72 | 5.11. 3,36 |


| Feet. <br> Tentlis. | Hundreaths of a Foot. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ©. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. |
|  | Inches. | Inches | Inches | Inches. | Inches | Inches. | Inches. | Inches. | Inches | Inches. |
| 0.0 | 0.00 | 0.12 | 0.24 | 0.36 | 0.48 | 0.60 | 0.72 | 0.84 | 0.96 | 1.08 |
| 0.1 | 1.20 | 1.32 | 1.44 | 1.56 | 1.68 | 1.80 | 1.92 | 2.04 | 2.16 | 2.28 |
| 0.2 | 2.10 | 2.52 | 2.64 | 2.76 | 2.88 | 3.00 | 3.12 | 3.24 | 3.36 | 3.48 |
| 0.3 | 3.60 | 3.72 | 3.84 | 3.96 | 4.08 | 4.20 | 4.32 | 4.44 | 4.56 | 4.68 |
| 0.4 | 4.80 | 4.92 | 5.04 | 5.16 | 5.28 | 5.40 | 5.52 | 5.64 | 5.76 | 5.88 |
| 0.5 | 6.00 | 6.12 | 6.24 | 6.36 | 6.48 | 6.60 | 6.72 | 6.84 | 6.96 | 7.08 |
| 0.6 | 7.20 | 7.32 | 7.44 | 7.56 | 7.68 | 7.80 | 7.92 | 8.04 | 8.16 | 8.25 |
| 0.7 | 8.10 | 8.52 | 8.64 | 8.76 | 8.88 | 9.00 | 9.12 | 9.24 | 9.36 | 9.48 |
| 0.8 | 9.60 | 9.72 | 9.84 | 9.96 | 10.08 | 10.20 | 10.32 | 10.44 | 10.56 | 10.68 |
| 0.9 | 10.80 | 10.92 | 11.04 | 11.16 | 11.28 | 11.40 | 11.52 | 11.64 | 11.76 | 11.88 |

XLV. CONVERSION OF DECIMALS OF A FOOT INTO INCHES AND DUODECIMAL LINES.

|  | Hundredths of a Foot |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tenths. | 0. 1. | 2. | 3.14. | 5. | 6. | 7. | 8. | 9. |
|  | In. Line. In Line. | In Line. | In. Line. In. Line. | In Line | In. Line | In Line | Line | In. Line. |
| 0.0 | 0.0,00 0. 1,44 | 0. 2,38 | 0. 4,32 $0.5,76$ | 0.7,20 | 0. 8,64 | 0.10,08 | 0.11,52 | 1. 0,96 |
| 0.1 | 1.2, 10 1. 3,84 | 1. 5,28 | 1. 6,72 1. 8,16 | 1.9,60 | 1.11,04 | 2. 0,48 | 2. 1,92 | 2. 3,36 |
| 0.2 | 2.4,50 2. 6,21 | 2. 7,68 | 2. 9,12 $2.10,56$ | 3.0,00 | 3. 1,44 | 3. 2,88 | 3. 4,32 | 3. 5,76 |
| 0.3 | 3.7,20 3. 8,64 | 3.10,08 | 3.11,52 4. 0,96 | 4.2,40 | 4. 3, 44 | 4. 5,28 | 4. 6,72 | 4. 8,16 |
| 0.4 | $49,60 \quad 4.11,04$ | 5. 0,48 | 5. 1,92 5. 3,36 | 5.4,50 | 5. 6,24 | 5. 7,68 | 5. 9,12 | 5.10,56 |
| 0.5 | 6.0.00 6. 1,44 | 6. 2,58 | 6. 4,32 6. 5,76 | 6.7,20 | 6. 8,64 | 6.10,08 | 6.11,52 | 7. 0,96 |
| 0.6 | $7.2,10 \quad 7.3,84$ | 7. 5,29 | 7. 6,72 7. 8,16 | 7.9,60 | 7.11,04 | 8. 0,48 | 8. 1,92 | 8. 3,36 |
| 0.7 | $8.4,50$ 8. 6,24 | 8. 7,68 | 8. 9,12 8.10,56 | 9.0,00 | 9. 1,44 | 9. 2,58 | 9. 4,32 | 9. 5,76 |
| 0.8 | 9.7,20 9. 8,64 | 9.10,08 | 9.11,52 10. 0,96 | 10.2,40 | 10. 3,84 | 10. 5,28 | 10. 6,72 | 10. 8,16 |
| 0.9 | 10.9.60 10.11,04 | 11. 0,45 | 11. 1,92 11. 3,36 | 11.4,50 | 11. 6,24 | 11. 7,68 | 11. 9,12 | 11.10,56 |

XLVI. CONVERSION OF INCHES AND DUODECIMAL LINES INTO DECIMALS OF A FOOT.

1 Inch $=008333$ of a Foot. $\quad 1$ Line $=\mathbb{C} 006944$ of a Foot.

| Inches. | Lines |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | 8. | 9. | 10. | 11. |
|  | Foot. | Foot. | Foot | Foot. | Foot. | Foot. | Foot. | Foot. | Foot | Foot. | Foot | Foot. |
| 0 | 0.0000 | 0.0069 | 0.0139 | 0.0208 | 0.0278 | 0.0347 | 0.0417 | 0.0486 | 0.0556 | 0.0625 | 0.0694 | 0.0764 |
| 1 | 0.0333 | 0.0903 | 0.0972 | 0.1042 | 0.1111 | 0.1181 | 0.1250 | 0.1319 | 0.1389 | 0.1458 | 0.1528 | 0.1597 |
| 2 | 0.1667 | 0.1736 | 0.1806 | 0.1875 | 0.1944 | 0.2014 | 0.2083 | 0.2153 | 0.2222 | 0.2292 | 0.2361 | 0.2431 |
| 3 | 0.2500 | 0.2569 | 0.2639 | 0.2708 | 0.2778 | 0.2847 | 0.2917 | 0.2986 | 0.3056 | 0.3125 | 0.3194 | 0.3264 |
| 4 | 0.3533 | 0.3103 | 0.3172 | 0.3542 | 0.3611 | 0.3681 | 0.3750 | 0.3819 | 0.3889 | 0.3958 | 0.1028 | 0.4097 |
| 5 | 0.4167 | 0.4236 | 0.4306 | 0.4375 | 0.444 | 0.4514 | 0.4583 | 0.4653 | 0.4722 | 0.4792 | 0.4861 | 0.4931 |
| 6 | 0.5000 | 0.5069 | 0.5139 | 0.5208 | 0.5278 | 0.5347 | 0.5417 | 0.5-186 | 0.5556 | 0.562 .5 | 0.5694 | 0.5764 |
| 7 | 0.5833 | 0.5903 | 0.5972 | 0.6042 | 0.6111 | 0.6181 | 0.6250 | 0.6319 | 0.6389 | 0.6458 | 0.6528 | 0.6597 |
| 8 | 0.6667 | $0.6736^{\prime}$ | 0.6806 | 0.6575 | 0.6944 | 0.7014 | 0.7083 | 0.7153 | 0.7222 | 0.7292 | 0.7361 | 0.7431 |
| 9 | 0.7500 | 0.7569 | 0.7639 | 0.7708 | 0.7778 | 0.7847 | 0.7917 | 0.7986 | 0.8056 | 0.8125 | 0.8194 | 0.8264 |
| 10 | 0.8333 | 0.8403 | 0.8472 | 0.8542 | 0.8611 | 0.8681 | 0.8750 | 0.8819 | 0.8889 | 0.8958 | 0.9028 | 0.9097 |
| 11 | 0.9167 | 0.9236 | 0.9306 | 0.9375 | 0.9444 | 0.9514 | 0.9583 | 0.9653 | 0.9722 | 0.9792 | 0.9861 | 0.9931 |

XLVII. TABLE FOR COMPARING THE MOST IMPORTANT MEASURES OF LENGTH.

| French metre. | French toise. | Foot of Paris. | English, or Russian foot. | Swedish foot. | $\begin{aligned} & \text { Norwegian } \\ & \text { foot. } \end{aligned}$ | Rhine, or Prussian foot. | Austrian, or Klafter of Vienna. | Austrian, or foot of Vienna. | Spanish vara. | Spanish foot. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 0.5130741 | 3.078444 | 3.280899 | 3.368126 | 3.187116 | 3.186200 | 0.5272915 | 3.163749 | 1.196308 | 3.588925 |
|  | 9.7101801 | 0.4883313 | 0.5159929 | 0.5273883 | 0.5033979 | 0.5032730 | 9.7220507 | 0.5002020 | 0.0778431 | 0.5549644 |
| 1.949036 | 1 | 6.000000 | 6.394592 | 6.564599 | 6.211805 | 6.210019 | 1.027710 | 6.166261 | 2.331648 | 6.994945 |
| 0.2898199 |  | 0.7781513 | 0.8058128 | 0.8172082 | 0.7432128 | 0.7930929 | 0.0118707 | 0.7900219 | 0.3676630 | 0.8447843 |
| 0.3248394 | 0.1666667 | I | 1.065765 | 1.094100 | 1.035301 | 1.035003 | 0.1712850 | 1.027710 | 0.3886080 | 1.165824 |
| 95116687 | 9.2218487 |  | 0.0276615 | 0.0390570 | 0.0150666 | 0.0149417 | 9.2337194 | 0.0118707 | 9.5595117 | 0.0666330 |
| 0.3047945 | 0.1563822 | 0.9382930 | I | 1.026586 | 0.9714155 | 0.9711362 | 0.1607155 | 0.9642932 | 0.3646282 | 1.093885 |
| 9.4840071 | 9.1941872 | 9.9723385 |  | 0.0113954 | 9.9574050 | 9.9872801 | 9.2060579 | 9.9542091 | 9.5618502 | 0.0369715 |
| 0.2969010 | 0.1523322 | 0.9139933 | 0.9741024 | 1 | 0.9462580 | 0.9459860 | 0.1565534 | 0.9393202 | 0.3551851 | 1.065555 |
| 9.4726117 | 9.1827918 | 9.9609430 | 9.9856046 |  | 9.9760096 | 9.9758847 | 9.1946624 | 9.9728137 | 9.5504518 | 0.0275761 |
| 0.3137633 | 0.1609838 | 0.9659028 | 1.029426 | 1.056794 | I | 0.9997125 | 0.1654447 | 0.9926682 | 0.3753576 | 1.126073 |
| 9.4966021 | 9.2067822 | 9.9549334 | 0.0125950 | 0.0239904 |  | 9.9998751 | 9.2186508 | 9.9965041 | 9.5744452 | 0.0515665 |
| 0.3138535 | 0.1610301 | 0.9661806 | 1.029722 | 1.057098 | 1.000288 | I | 0.1654923 | 0.9929536 | 0.3754655 | 1.126397 |
| 9.4967270 | 9.2069071 | 9.9850583 | 0.0127199 | 0.0241153 | 0.0001249 |  | 0.2187777 | 9.9969290 | 9.574.5701 | 0.0516913 |
| 1.896484 | 0.9730370 | 5.838222 | 6.222173 | 6.387598 | 6.044316 | 6.042579 | 1 | 6.000000 | 2.268780 | 6.806339 |
| 0.2779193 | 9.9881293 | 0.7662806 | 0.7939421 | 0.8033376 | 0.7813472 | 0.7812223 |  | 0.7781513 | 0.3557923 | 0.8329136 |
| 0.3160807 | 0.1621728 | 0.9730370 | 1.037029 | 1.064600 | 1.007386 | 1.007096 | 0.1666667 | I | 0.3781300 | 1.134390 |
| 9.4997950 | 9.2099781 | 9.9881293 | 0.0157909 | 0.0271863 | 0.0031959 | 0.0030710 | 9.2218487 |  | 9.5776411 | 0.0547624 |
| 0.8359050 | 0.4288812 | 2.573287 | 2.742520 | 2.815433 | 2.664126 | 2.663360 | 0.4407656 | 2.644593 | I | 3.000000 |
| 9.9221.569 | 9.6323370 | 0.4104883 | 0.4381498 | 0.4495452 | 0.4255548 | 0.4254299 | 9.6442077 | 0.4223589 |  | 0.4771213 |
| 0.2786350 | 0.1429604 | 0.8577623 | 0.9141732 | 0.9384777 | 0.8880421 | 0.8877868 | 0.1469219 | 0.8815311 | 0.333333 | 1 |
| 9.44503.56 | 9.1552157 | 9.9333670 | 9.9610285 | 9.9721239 | 9.9484335 | 9.9483087 | 9.1670864 | 9.9452376 | 9.5228787 |  |

In this table each measure named at the head of its vertical column, occurs once as unit, and all the numbers, on the same horizontal line,
XLVHII CONVLRSIGN OF ENGLASH FATHODS INTO METRES.

| Fatioms. | Hundreds. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O. | 100. | 200. | 300. | 400. | 500. | 600. | '900. | 808. | 500. |
| Thousands. <br> 0 | Metres. $0.00$ | Metres. $182.88$ | Metres. <br> 365.75 | Metres. 548.63 | Metres. <br> 731.51 | Metres. 914.38 | Metres. $1097.26$ | $\begin{gathered} \text { Metres. } \\ 1 \because 80.14 \end{gathered}$ | $\begin{gathered} \text { Metres. } \\ 1463.01 \end{gathered}$ | Metres. 1645.89 |
| 1000 |  |  |  |  |  | 914.38 | 1097.26 | 1280.14 | 1463.11 | 1645.89 |
| 1000 | 1828.77 | 2011.65 | 2194.52 | 2377.40 | 2560.28 | 2743.15 | 2926.03 | 3105.91 | 3291.78 | 3474.66 |
| 2000 | 3657.53 | 38.40 .41 | 4023.28 | 4206.16 | 4389.04 | 4571.91 | 4754.79 | 4937.67 | 5120.54 | 5303.42 |
| 3000 | 5486.30 | 5669.18 | 5852.05 | 6034.93 | 6217.81 | 6400.68 | 6583.56 | 6766.44 | 6949.31 | 7132.19 |
| 4000 | 7315.07 | 7497.95 | 7680.82 | 7863.70 | 8046.58 | 8229.45 | 8412.33 | 8595.21 | 8778.08 | 8960.96 |
| 5000 | 9143.83 | 9326.71 | 9509.58 | 9692.46 | 9875.34 | 10058.21 | 10241.09 | 10423.97 | 10606.84 | 10789.72 |
| 6000 | 10972.60 | 11155.48 | 11338.35 | 11521.23 | 11704.11 | 11886.98 | 12069.86 | 12252.73 | 12435.61 | 12618.49 |
| 7000 | 12801.37 | 12984.25 | 13167.12 | 13350.00 | 13535.88 | 13715.75 | 13898.63 | 14081.51 | 14264.38 | 14447.26 |
| 8000 | 14630.14 | 14813.02 | 14995.89 | 15178.77 | 15361.65 | 15544.52 | 15727.40 | 15910.27 | 16093.15 | 16276.03 |
| 9000 | 16.458 .90 | 16641.78 | 16824.65 | 17007.53 | 17190.41 | 17373.28 | 17556.16 | 17739.04 | 17921.92 | 18104.80 |

XIIX. CONVERSIon of METRES into English fathoms.
( 1 Metre $=0.546817$ English Fathoms [0.7375420].)


## b) TABLES

FOR

COMPARING fHE MOST IMPORTANT MEASURES OF GEOGRAPHICAL DISTANCAS.

## CONTENTS.

(The figures refer to the folio at the bottom of the page.)

TABLES FOR COMPARING TIIE MOST IMPORTANT MEASURES OF GEOGRAPHICAL DISTANCES.

Conversion of the different litinerary Measures into each other.
Table I. Conversion of Kilometres into Austrian Miles-Prussian MilesGerman Miles-Nautical Leagnes-French Leagues-Geographical Miles - English Statute Miles-Russian Wersts
" II. Conversion of Austrian Miles into Kilometres-Prussian MilesGerman Miles—Nautical Leagues-French Leagues-Geographical Miles_English Statute Miles-Russian Wersts
onversion of Prussian Miles into Kilometres-Austrian MilesGerman Miles-Nautical Leagues-French Leagues-Geographical Miles-English Statute Miles-Russian Wersts .

65
Conversion of German Miles into Kilometres-Austrian Miles-
Prussian Miles_Nautical Leagues_French Leagues-Geographical Miles—English Statute Miles_Russian Wersts . . 68
، V. Conversion of Nautical Leagues into Kilometres-Austrian Miles _Prussian Miles_German Miles_French Leagues_Geographical Miles—English Statute Miles_Russian Wersts . . . 71
" VI. Conversion of French Leagues into Kilometres-Austrian MilesPrussian Miles_German Miles_Nautical Leagues_Geographical Miles_English Statute Miles_Russian Wersts .
" VII. Conversion of Geographical Miles into Kilometres-Austrian Miles
_Prussian Miles_German Miles_Nautical Leagues_French Leagues_English Statute Miles—Russian Wersts
"VIII. Conversion of English Statute Miles into Kilometres-Austrian Miles - Prussian Miles_German Miles_Nautical Leagnes_ French Leagues_Geographical Miles-Russian Wersts80
" IX. Conversion of Russian Wersts into Kilometres-Austrian Miles-
Prussian Miles - German Miles-Nantical Leagues - French
Leagues_Geographical Miles_English Statute Miles . . 83
" X. Table for comparing the most important Itinerary Measures . 86

| Kilometres. | $\begin{aligned} & \text { Austrian } \\ & \text { Miles. } \end{aligned}$ | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ \mathbf{1 5}=1^{\circ} \text { Eq. } \end{gathered}$ | Nautical <br> Leagues. $20=1^{\circ}$ Eq. $20=10 \mathrm{Eq} .$ | $\begin{gathered} \text { French } \\ \text { Leagues. } \\ 25=1^{\circ} \text { Eq. } \end{gathered}$ | Geograpli'l <br> or Nautical Miles. $60=1^{\circ} \mathrm{Eq}$ | English Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 131.82 | 132.76 | 134.76 | 179.68 | 224.60 | 539.05 | 621.38 | 937.40 |
| 2,000 | 263.65 | 265.52 | 269.53 | 359.37 | 449.21 | 1078.10 | 1242.77 | 1874.80 |
| 3,000 | 395.47 | 398.27 | 404.29 | 539.05 | 673.81 | 1617.16 | 1864.15 | 2812.20 |
| 4,000 | 527.29 | 531.03 | 539.05 | 718.74 | 898.42 | 2156.21 | 2485.53 | 3749.60 |
| 5,000 | 659.11 | 663.79 | 673.81 | 898.42 | 1123.02 | 2695.26 | 3106.91 | 4687.00 |
| 6,000 | 790.94 | 796.55 | 808.58 | 1078.10 | 1347.63 | 3234.31 | 3728.30 | 5624.40 |
| 7,000 | 922.76 | 929.31 | 943.34 | 1257.79 | 1572.23 | 3773.36 | 4349.68 | 6561.80 |
| 8,000 | 1054.58 | 1062.07 | 1078.10 | 1437.47 | 1796.84 | 4312.41 | 4971.06 | 7499.20 |
| 9,000 | 1186.41 | 1194.82 | 1212.87 | 1617.16 | 2021.44 | 4851.46 | 5592.44 | 8436.60 |
| 10,000 | 1318.23 | 1327.58 | 1347.63 | 1796.84 | 2246.05 | 5390.52 | 6213.82 | 9374.00 |
| 100 | 13.18 | 13.28 | 13.48 | 17.97 | 22.46 | 53.91 | 62.14 | 93.74 |
| 200 | 26.36 | 26.55 | 26.95 | 35.94 | 44.92 | 107.81 | 124.28 | 187.48 |
| 300 | 39.55 | 39.83 | 40.43 | 53.91 | 67.38 | 161.72 | 186.42 | 281.22 |
| 400 | 52.73 | 53.10 | 53.91 | 71.87 | 89.84 | 215.62 | 248.55 | 374.96 |
| 500 | 65.91 | 66.38 | 67.38 | 89.84 | 112.30 | 269.53 | 310.69 | 468.70 |
| 600 | 79.09 | 79.65 | 80.86 | 107.81 | 134.76 | 323.43 | 372.83 | 562.44 |
| 700 | 92.28 | 92.93 | 94.33 | 125.78 | 157.22 | 377.34 | 434.97 | 60.6 .18 |
| 800 | 105.46 | 106.21 | 107.81 | 143.75 | 179.68 | 431.24 | 497.11 | 749.92 |
| 900 | 118.64 | 119.48 | 121.29 | 161.72 | 202.14 | 485.15 | 559.24 | 843.66 |
| 1000 | 131.82 | 132.76 | 134.76 | 179.68 | 224.60 | 539.05 | 621.38 | 937.40 |
| 1 | 0.13 | 0.13 | 0.13 | 0.18 | 0.22 | 0.54 | 0.62 | 0.94 |
| 2 | 0.26 | 0.27 | 0.27 | 0.36 | 0.45 | 1.08 | 1.24 | 1.87 |
| 3 | 0.40 | 0.40 | 0.40 | 0.54 | 0.67 | 1.62 | 1.86 | 2.81 |
| 4 | 0.53 | 0.53 | 0.54 | 0.72 | 0.90 | 2.16 | 2.49 | 3.75 |
| 5 | 0.66 | 0.66 | 0.67 | 0.90 | 1.12 | 2.70 | 3.11 | 4.69 |
| 6 | 0.79 | 0.80 | 0.81 | 1.08 | 1.35 | 3.23 | 3.73 | 5.62 |
| 7 | 0.92 | 0.93 | 0.94 | 1.26 | 1.57 | 3.77 | 4.35 | 6.56 |
| 8 | 1.06 | 1.06 | 1.08 | 1.44 | 1.80 | 4.31 | 4.97 | 7.50 |
| 9 | 1.19 | 1.19 | 1.21 | 1.62 | 2.02 | 4.85 | 5.59 | 8.44 |
| 10 | 1.32 | 1.33 | 1.35 | 1.80 | 2.25 | 5.39 | 6.21 | 9.37 |
| 11 | 1.45 | 1.46 | 1.48 | 1.98 | 2.47 | 5.93 | 6.84 | 10.31 |
| 12 | 1.58 | 1.59 | 1.62 | 2.16 | 2.70 | 6.47 | 7.46 | 11.25 |
| 13 | 1.71 | 1.73 | 1.75 | 2.34 | 2.92 | 7.01 | 8.08 | 12.19 |
| 14 | 1.85 | 1.86 | 1.89 | 2.52 | 3.14 | 7.55 | 8.70 | 13.12 |
| 15 | 1.98 | 1.99 | 2.02 | 2.70 | 3.37 | 8.09 | 9.32 | 14.06 |
| 16 | 2.11 | 2.12 | 2.16 | 2.87 | 3.60 | 8.62 | 9.94 | 15.00 |
| 17 | 2.24 | 2.26 | 2.29 | 3.05 | 3.82 | 9.16 | 10.56 | 15.94 |
| 18 | 2.37 | 2.39 | 2.43 | 3.23 | 4.04 | 9.70 | 11.18 | 16.87 |
| 19 | 2.50 | 2.52 | 2.56 | 3.41 | 4.27 | 10.24 | 11.81 | 17.81 |
| 20 | 2.64 | 2.66 | 2.70 | 3.59 | 4.49 | 10.78 | 12.43 | 18.75 |

kilometres into different geographical measures of distance.

| $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \text { Eq. } . \end{gathered}$ | $\begin{gathered} \text { Nautical } \\ \text { Leagues. } \\ 20=1^{\circ} \mathrm{Eq} . \end{gathered}$ | $\begin{gathered} \text { French } \\ \text { Leayues. } \\ 25=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Geograph'l <br> or Nautical Miles. $60=1^{\circ} \mathrm{Eq}$. | English Statute Miles. | Rnsslan Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 2.77 | 2.79 | 2.83 | 3.77 | 4.72 | 11.32 | 13.05 | 19.69 |
| 22 | 2.90 | 2.92 | 2.96 | 3.95 | 4.94 | 11.86 | 13.67 | 20.62 |
| 23 | 3.03 | 3.05 | 3.10 | 4.13 | 5.17 | 12.40 | 14.29 | 21.56 |
| 24 | 3.16 | 3.19 | 3.23 | 4.31 | 5.39 | 12.94 | 14.91 | 22.50 |
| 25 | 3.30 | 3.32 | 3.37 | 4.49 | 5.62 | 13.48 | 15.53 | 23.44 |
| 26 | 3.43 | 3.45 | 3.50 | 4.67 | 5.84 | 14.02 | 16.16 | 24.37 |
| 27 | 3.56 | 3.58 | 3.64 | 4.85 | 6.06 | 14.55 | 16.78 | 25.31 |
| 28 | 3.69 | 3.72 | 3.77 | 5.03 | 6.29 | 15.09 | 17.50 | 26.25 |
| 29 | 3.82 | 3.85 | 3.91 | 5.21 | 6.51 | 15.63 | 18.02 | 27.18 |
| 30 | 3.95 | 3.98 | 4.04 | 5.39 | 6.74 | 16.17 | 18.64 | 28.12 |
| 31 | 4.09 | 4.12 | 4.18 | 5.57 | 6.96 | 16.71 | 19.26 | 29.06 |
| 32 | 4.22 | 4.25 | 4.31 | 5.75 | 7.19 | 17.25 | 19.88 | 30.00 |
| 33 | 4.35 | 4.38 | 4.45 | 5.43 | 7.41 | 17.79 | 20.51 | 30.93 |
| 34 | 4.48 | 4.51 | 4.58 | 6.11 | 7.64 | 18.33 | 21.13 | 31.87 |
| 35 | 4.61 | 4.65 | 4.72 | 6.29 | 7.86 | 18.87 | 21.75 | 32.81 |
| 36 | 4.75 | 4.78 | 4.85 | 6.47 | 8.09 | 19.41 | 22.37 | 33.75 |
| 37 | 4.88 | 4.91 | 4.99 | 6.65 | 8.31 | 19.94 | 22.99 | 34.68 |
| 38 | 5.01 | 5.04 | 5.12 | 6.83 | 8.53 | 20.48 | 23.61 | 35.62 |
| 39 | 5.14 | 5.18 | 5.26 | 7.01 | 8.76 | 21.02 | 24.23 | 36.56 |
| 40 | 5.27 | 5.31 | 5.39 | 7.19 | 8.98 | 21.56 | 24.86 | 37,50 |
| 41 | 5.40 | 5.44 | 5.53 | 7.37 | 9.21 | 22.10 | 25.48 | 38.43 |
| 42 | 5.54 | 5.58 | 5.66 | 7.55 | 9.43 | 22.64 | 26.10 | 39.37 |
| 43 | 5.67 | 5.71 | 5.79 | 7.73 | 9.66 | 23.18 | 26.72 | 40.31 |
| 44 | 5.80 | 5.84 | 5.93 | 7.91 | 9.88 | 23.72 | 27.34 | 41.25 |
| 45 | 5.93 | 5.97 | 6.06 | 8.09 | 10.11 | 24.26 | 27.96 | 42.18 |
| 46 | 6.06 | 6.11 | 6.20 | 8.27 | 10.33 | 24.80 | 28.58 | 43.12 |
| 47 | 6.80 | 6.24 | 6.33 | 8.45 | 10.56 | 25.34 | 29.21 | 44.06 |
| 48 | 6.33 | 6.37 | 6.47 | 8.62 | 10.78 | 25.87 | 29.83 | 45.00 |
| 49 | 6.46 | 6.51 | 6.60 | 8.80 | 11.01 | 26.41 | 30.45 | 45.93 |
| 50 | 6.59 | 6.64 | 6.74 | 8.98 | 11.23 | 26.95 | 31.07 | 46.87 |
| 51 | 6.72 | 6.77 | 6.87 | 9.16 | 11.45 | 27.49 | 31.69 | 47.81 |
| 52 | 6.85 | 6.90 | 7.01 | 9.34 | 11.68 | 28.03 | 32.31 | 48.74 |
| 53 | 6.99 | 7.03 | 7.14 | 9.52 | 11.90 | 28.57 | 32.93 | 49.68 |
| 54 | 7.12 | 7.17 | 7.28 | 9.70 | 12.13 | 29.11 | 33.55 | 50.62 |
| 55 | 7.25 | 7.30 | 7.41 | 9.88 | 12.35 | 29.65 | 34.18 | 51.56 |
| 56 | 7.38 | 7.43 | 7.55 | 10.06 | 12.58 | 30.19 | 34.90 | 52.49 |
| 57 | 7.51 | 7.57 | 7.68 | 10.24 | 12.80 | 30.73 | 35.42 | 53.43 |
| 58 | 7.65 | 7.70 | 7.82 | 10.42 | 13.03 | 31.27 | 36.04 | 54.37 |
| 59 | 7.78 | 7.83 | 7.95 | 10.60 | 13.25 | 31.80 | 36.66 | 55.31 |
| 60 | 7.91 | 7.97 | 8.09 | 10.78 | 13.48 | 32.33 | 37.28 | 56.24 |

KILOMETRES INTO DIFFERENT GEOGRAPHCAL MEASURES OF DISTANCE. 507

| $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Nautical <br> Leagues. $20=1^{\circ} \mathrm{Eq}$. | French <br> Leagues. $25=1^{\circ} \mathrm{Eq} .$ | Geograph'l or Nautical Miles. $60=1^{\circ} \mathrm{Eq}$. | English Statute Miles. | Russian <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 8.04 | 8.10 | 8.22 | 10.96 | 13.70 | 32.88 | 37.90 | 57.18 |
| 62 | 8.17 | 8.23 | 8.36 | 11.14 | 13.93 | 33.42 | 38.53 | 58.12 |
| 63 | 8.30 | 8.36 | 8.49 | 11.32 | 14.15 | 33.96 | 39.15 | 59.06 |
| 64 | 8.44 | 8.50 | 8.62 | 11.50 | 14.37 | 34.50 | 39.77 | 59.99 |
| 65 | 8.57 | 8.63 | 8.76 | 11.68 | 14.60 | 35.04 | 40.39 | 60.93 |
| 66 | 8.70 | 8.76 | 8.89 | 11.86 | 14.82 | 35.58 | 41.01 | 61.87 |
| 67 | 8.83 | 8.89 | 9.03 | 12.04 | 15.05 | 36.12 | 41.63 | 62.81 |
| 68 | 8.96 | 9.03 | 9.16 | 12.22 | 15.27 | 36.66 | 42.25 | 63.74 |
| 69 | 9.10 | 9.16 | 9.30 | 12.40 | 15.50 | 37.19 | 42.88 | 64.68 |
| 70 | 9.23 | 9.29 | 9.43 | 12.58 | 15.72 | 37.73 | 43.50 | 65.62 |
| 71 | 9.36 | 9.43 | 9.57 | 12.76 | 15.95 | 38.27 | 44.12 | 66.56 |
| 72 | 9.49 | 9.56 | 9.70 | 12.94 | 16.17 | 38.81 | 44.74 | 67.49 |
| 73 | 9.62 | 9.69 | 9.84 | 13.12 | 16.40 | 39.35 | 45.36 | 68.43 |
| 74 | 9.75 | 9.82 | 9.97 | 13.30 | 16.62 | 39.89 | 45.98 | 69.37 |
| 75 | 9.89 | 9.96 | 10.11 | 13.48 | 16.85 | 40.43 | 46.60 | 70.31 |
| 76 | 10.02 | 10.09 | 10.24 | 13.65 | 17.07 | 40.97 | 47.23 | 71.24 |
| 77 | 10.15 | 10.22 | 10.38 | 13.84 | 17.29 | 41.51 | 47.85 | 72.18 |
| 78 | 10.28 | 10.36 | 10.51 | 14.02 | 17.52 | 42.05 | 48.47 | 73.12 |
| 79 | 10.41 | 10.49 | 10.65 | 14.20 | 17.74 | 42.59 | 49.09 | 74.05 |
| 80 | 10.55 | 10.62 | 10.78 | 14.37 | 17.97 | 43.12 | 49.71 | 74.99 |
| 81 | 10.68 | 10.75 | 10.92 | 14.55 | 18.19 | 43.66 | 50.33 | 75.93 |
| 82 | 10.81 | 10.89 | 11.05 | 14.73 | 18.42 | 44.20 | 50.95 | 76.87 |
| 83 | 10.94 | 11.02 | 11.19 | 14.91 | 18.64 | 44.74 | 51.57 | 77.80 |
| 84 | 11.07 | 11.15 | 11.32 | 15.09 | 18.87 | 45.28 | 52.20 | 78.74 |
| 85 | 11.20 | 11.28 | 11.45 | 15.27 | 19.09 | 45.82 | 52.82 | 79.68 |
| 86 | 11.34 | 11.42 | 11.59 | 15.45 | 19.32 | 46.36 | 53.44 | 80.62 |
| 87 | 11.47 | 11.55 | 11.72 | 15.63 | 19.54 | 46.90 | 54.06 | 81.55 |
| 88 | 11.60 | 11.68 | 11.86 | 15.81 | 19.77 | 47.44 | 54.68 | 82.49 |
| 89 | 11.73 | 11.82 | 11.99 | 15.99 | 19.99 | 47.98 | 55.30 | 83.43 |
| 90 | 11.86 | 11.95 | 12.13 | 16.17 | 20.21 | 48.51 | 55.92 | 84.37 |
| 91 | 12.00 | 12.08 | 12.26 | 16.35 | 20.44 | 49.05 | 56.55 | 85.30 |
| 92 | 12.13 | 12.21 | 12.40 | 16.53 | 20.66 | 49.59 | 57.17 | 86.24 |
| 93 | 12.26 | 12.35 | 12.53 | 16.71 | 20.89 | 50.13 | 57.79 | 87.18 |
| 94 | 12.39 | 12.48 | 12.67 | 16.89 | 21.11 | 50.67 | 58.41 | 88.12 |
| 95 | 12.52 | 12.61 | 12.80 | 17.07 | 21.34 | 51.21 | 59.03 | 89.05 |
| 96 | 12.66 | 12.74 | 12.94 | 17.25 | 21.56 | 51.74 | 59.65 | 89.99 |
| 97 | 12.79 | 12.88 | 13.07 | 17.43 | 21.79 | 52.29 | 60.27 | 90.93 |
| 98 | 12.92 | 13.01 | 13.21 | 17.61 | 22.01 | 52.83 | 60.90 | 91.87 |
| 99 | 13.05 | 13.14 | - 13.34 | 17.79 | 22.24 | 53.37 | 61.52 | 92.80 |
| 100 | 13.18 | 13.28 | 13.48 | 17.97 | 22.46 | 53.91 | 62.14 | 93.74 |

E

508
II. austrian miles into different geographical measures of distance.

| $\begin{aligned} & \text { Austrian } \\ & \text { Miles. } \end{aligned}$ | Kilo- metres. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 1 \dot{j}=1^{\circ} \text { Eq. } \end{gathered}$ | Nautical Leagues. $20=1^{\circ} \mathrm{Eq}$. | French <br> Leagues. $2 \overline{5}=1^{\circ} \mathrm{Eq} .$ | Geograph'l or Nautical Miles. $60=1^{\circ} \mathrm{Eq}$. | English Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 7585.94 | 1007.10 | 1022.30 | 1363.07 | 1703.84 | 4089.21 | 4713.77 | 7111.06 |
| 2,000 | 15171.87 | 2014.19 | 2044.61 | 2726.14 | 3407.68 | 8178.42 | 9427.54 | 14222.11 |
| 3,000 | 22757.81 | 3021.29 | 3066.91 | 4089.21 | 5111.52 | 12267.64 | 14141.30 | 21333.17 |
| 4,000 | 30343.75 | 4028.39 | 4089.21 | 5452.28 | 6815.35 | 16356.85 | 18855.07 | 28444.22 |
| 5,000 | 37929.69 | 5035.48 | 5111.52 | 6815.35 | 8519.19 | 20446.06 | 23568.84 | 35555.28 |
| 6,000 | 45515.62 | 6042.58 | 6133.82 | 8178.42 | 10223.03 | 24535.27 | 28282.61 | 42666.33 |
| 7,000 | 53101.56 | 7049.67 | 7156.12 | 9541.50 | 11926.87 | 28624.49 | 32996.38 | 49777.39 |
| 8,000 | 60687.50 | 8056.77 | 8178.42 | 10904.57 | 13630.71 | 32713.70 | 37710.14 | 56888.45 |
| 9,000 | 68273.43 | 9063.87 | 9200.73 | 12267.64 | 15334.55 | 36802.91 | 42423.91 | 63999.50 |
| 10,000 | 75859.37 | 10070.96 | 10223.03 | 13630.71 | 17038.38 | 40892.12 | 47137.68 | 71110.56 |
| 100 | 75859 | 100.71 | 102.23 | 136.31 | 170.38 | 408.92 | 471.38 | 711.11 |
| 200 | 151719 | 201.42 | 204.46 | 272.61 | 340.77 | 817.84 | 942.75 | 1422.21 |
| 300 | 2275.78 | 302.13 | 306.69 | 408.92 | 511.15 | 1226.76 | 1414.13 | 2133.32 |
| 400 | 3034.37 | 402.84 | 408.92 | 545.23 | 681.54 | 1635.68 | 1885.51 | 2844.42 |
| 500 | 3792.97 | 503.55 | 511.15 | 681.54 | 851.92 | 2044.61 | 2356.88 | 3555.53 |
| 600 | 4551.56 | 604.26 | 613.38 | 817.84 | 1022.30 | 2453.53 | 2828.26 | 4266.63 |
| 700 | 5310.16 | 704.97 | 715.61 | 954.15 | 1192.69 | 2862.45 | 3299.64 | 4977.74 |
| 800 | 6068.75 | 805.68 | 817.84 | 1090.46 | 1363.07 | 3271.37 | 3771.01 | 5688.84 |
| 900 | 6827.34 | 906.39 | 920.07 | 1226.76 | 1533.45 | 3680.29 | 4242.39 | 6399.95 |
| 1000 | 7585.94 | 1007.10 | 1022.30 | 1363.07 | 1703.84 | 4089.21 | 4713.77 | 7111.06 |
| 1 | 7.59 | 1.01 | 1.02 | 1.36 | 1.70 | 4.09 | 4.71 | 7.11 |
| 2 | 15.17 | 2.01 | 2.04 | 2.73 | 3.41 | 8.18 | 9.43 | 14.22 |
| 3 | 22.76 | 3.02 | 3.07 | 4.09 | 5.11 | 12.27 | 14.14 | 21.33 |
| 4 | 30.34 | 4.03 | 4.09 | 5.45 | 6.82 | 16.36 | 18.86 | 28.44 |
| 5 | 37.93 | 5.04 | 5.11 | 6.82 | 8.52 | 20.45 | 23.57 | 35.56 |
| 6 | 45.52 | 6.04 | 6.13 | 8.18 | 10.22 | 24.54 | 28.28 | 42.67 |
| 7 | 53.10 | 7.05 | 7.16 | 9.54 | 11.93 | 28.62 | 33.00 | 49.78 |
| 8 | 60.69 | 8.06 | 8.18 | 10.90 | 13.63 | 32.71 | 37.71 | 56.89 |
| 9 | 68.27 | 9.06 | 9.20 | 12.27 | 15.33 | 36.80 | 42.42 | 64.00 |
| 10 | 75.86 | 10.07 | 10.22 | 13.63 | 17.04 | 40.89 | 47.14 | 71.11 |
| 11 | 83.45 | 11.08 | 11.25 | 14.99 | 18.74 | 44.98 | 51.85 | 78.22 |
| 12 | 91.03 | 12.09 | 12.27 | 16.36 | 20.45 | 49.07 | 56.57 | 85.33 |
| 13 | 98.62 | 13.09 | 13.29 | 17.72 | 22.15 | 53.16 | 61.28 | 92.44 |
| 14 | 106.20 | 14.10 | 14.31 | 19.08 | 23.85 | 57.25 | 65.99 | 99.55 |
| 15 | 113.79 | 15.11 | 15.33 | 20.45 | 25.56 | 61.34 | 70.71 | 106.67 |
| 16 | 121.37 | 16.11 | 16.36 | 21.81 | 27.26 | 65.43 | 75.42 | 113.78 |
| 17 | 128.96 | 17.12 | 17.38 | 23.17 | 28.97 | 69.52 | 80.13 | 120.89 |
| 18 | 136.55 | 18.13 | 18.40 | 24.54 | 30.67 | 73.61 | 84.85 | 128.00 |
| 19 | 144.13 | 19.13 | 19.42 | 25.90 | 32.37 | 77.70 | 89.56 | 135.11 |
| 20 | 151.72 | 20.14 | 20.45 | 27.26 | 34.08 | 81.78 | 94.28 | 142.22 |

aUSTrian mles into different geographical mfasures of distance.

| $\begin{aligned} & \text { Austrian } \\ & \text { Miles. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | $\begin{aligned} & \text { Prussian } \\ & \text { Mnles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Milies. } \\ 15=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Nautical <br> Leagues. $20=1^{\circ} \mathrm{Eq}$. | French <br> Learues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical Miles. $60=1^{\circ}$ Eq. | English <br> statute <br> Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\because 1$ | 159.30 | 21.15 | 21.47 | 28.62 | 35.78 | 85.87 | 98.99 | 149.33 |
| 22 | 166.89 | 22.16 | 22.49 | 29.99 | 37.48 | 89.96 | 103.70 | 156.44 |
| 23 | 174.48 | 23.16 | 23.51 | 31.35 | 39.19 | 94.05 | 108.42 | 163.55 |
| 24 | 182.06 | 24.17 | 24.54 | 32.71 | 40.89 | 98.14 | 113.13 | 170.67 |
| 25 | 189.65 | 25.18 | 25.56 | 34.08 | 42.60 | 102.23 | 117.84 | 177.75 |
| 26 | 197.23 | 26.18 | 26.58 | 35.44 | 44.30 | 106.32 | 122.56 | 184.89 |
| 27 | 204.82 | 27.19 | 27.60 | 36.80 | 46.00 | 110.41 | 127.27 | 192.00 |
| 28 | 212.41 | 28.20 | 28.62 | 38.17 | 47.71 | 114.50 | 131.99 | 199.11 |
| 29 | 219.99 | 29.21 | 29.65 | 39.53 | 49.41 | 118.59 | 136.70 | 206.22 |
| 30 | 227.58 | 30.21 | 30.67 | 40.89 | 51.12 | 122. 68 | 141.41 | 213.33 |
| 31 | 235.16 | 31.22 | 31.69 | 42.26 | 52.82 | 126.77 | 146.13 | 220.44 |
| 32 | 242.75 | 32.23 | 32.71 | 43.62 | 54.52 | 130.85 | 150.84 | 227.55 |
| 33 | 250.34 | 33.23 | 33.74 | 44.98 | 56.23 | 134.94 | 155.55 | $234.66^{\circ}$ |
| 34 | 257.92 | 34.24 | 34.76 | 46.34 | 57.93 | 139.03 | 160.27 | 241.78 |
| 35 | 265.51 | 35.25 | 35.78 | 47.71 | 59.63 | 143.12 | 164.98 | 248.89 |
| 36 | 273.09 | 36.26 | 36.80 | 49.07 | 61.34 | 147.21 | 160.70 | 256.00 |
| 37 | 280.68 | 37.26 | 37.83 | 50.43 | 63.04 | 151.30 | 174.41 | 263.11 |
| 38 | 288.27 | 38.27 | 38.85 | 51.80 | 64.75 | 155.39 | 179.12 | 270.22 |
| 39 | 295.85 | 39.28 | 39.87 | 53.16 | 66.45 | 159.48 | 183.84 | 277.33 |
| 40 | 303.44 | 40.28 | 40.89 | 54.52 | 68.15 | 163.57 | 188.55 | 284.44 |
| 41 | 311.02 | 41.29 | 41.91 | 55.89 | 69.86 | 167.66 | 193.26 | 291.55 |
| 42 | 318.61 | 42.30 | 42.94 | 57.25 | 71.56 | 171.75 | 197.98 | 298.66 |
| 43 | 326.20 | 43.31 | 43.96 | 58.61 | 73.27 | 175.84 | 202.69 | 305.78 |
| 44 | 333.78 | 44.31 | 44.98 | 59.98 | 74.97 | 179.93 | 207.41 | 312.89 |
| 45 | 341.37 | 45.32 | 46.00 | 61.34 | 76.67 | 184.01 | 212.12 | 320.00 |
| 46 | 348.95 | 46.33 | 47.03 | 62.70 | 78.38 | 188.10 | 216.83 | 327.11 |
| 47 | 356.54 | 47.33 | 48.05 | 64.06 | 80.08 | 192.19 | 221.55 | 334.22 |
| 48 | 364.12 | 48.34 | 49.07 | 65.43 | 81.78 | 196.28 | 226.26 | 341.33 |
| 49 | 371.71 | 49.35 | 50.09 | 66.79 | 83.49 | 200.37 | 230.97 | 348.44 |
| 50 | 379.30 | 50.35 | 51.12 | 68.15 | 85.19 | 204.46 | 235.69 | 355.55 |
| 51 | 386.58 | 51.36 | 52.14 | 69.52 | 86.90 | 208.55 | 240.40 | 362.66 |
| 52 | 394.47 | 52.37 | 53.16 | 70.88 | 88.60 | 212.64 | 245.12 | 369.77 |
| 53 | 402.05 | 53.38 | 54.18 | 72.24 | 90.30 | 216.73 | 249.83 | 376.89 |
| 54 | 409.64 | 54.38 | 55.20 | 73.61 | 92.01 | 220.82 | 254.54 | 384.00 |
| 55 | 417.23 | 55.39 | 56.23 | 74.97 | 93.71 | 224.91 | 259.26 | 391.11 |
| 56 | 424.81 | 56.40 | 57.25 | 76.33 | 95.41 | 229.00 | 263.97 | 398.22 |
| 57 | 432.40 | 57.40 | 58.27 | 77.70 | 97.12 | 233.69 | 268.68 | 405.33 |
| 58 | 439.98 | 58.41 | 59.29 | 79.06 | 98.82 | 237.17 | 273.40 | 412.44 |
| 59 | 447.57 | 59.42 | 60.32 | 80.42 | 100.53 | 241.26 | 278.11 | 419.55 |
| 60 | 455.16 | 60.43 | 61.34 | 81.78 | 102.23 | 245.35 | 282.83 | 426.66 |

510
aUstrian miles into different geographical measures of distance.

| $\begin{aligned} & \text { Anstrian } \\ & \text { Miles. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical Learues. $20=10 \mathrm{Eq}$ $20=1^{\circ} \mathrm{Eq}$. | French Leagues. $2 \overline{5}=1^{\circ}$ Eq. | Geograph'i or Nautical Miles. $60=1^{\circ} \mathrm{Eq}_{\mathrm{q}}$. | English statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 462.74 | 61.43 | 63.36 | 83.15 | 103.93 | 249.44 | 287.54 | 433.77 |
| 62 | 470.33 | 62.44 | 63.38 | 84.51 | 105.64 | 253.53 | 292.25 | 440.89 |
| 63 | 477.91 | 63.45 | 64.41 | 85.87 | 107.34 | 257.62 | 296.97 | 448.00 |
| 64 | 485.50 | 64.45 | 65.43 | 87.24 | 109.05 | 261.71 | 301.68 | 455.11 |
| 65 | 493.09 | 65.46 | 66.45 | 88.60 | 110.75 | 265.80 | 306.39 | 462.22 |
| 66 | 500.67 | 66.47 | 67.47 | 89.96 | 112.45 | 269.89 | 311.11 | 469.33 |
| 67 | 508.26 | 67.48 | 68.49 | 91.33 | 114.16 | 273.98 | 315.82 | 476.44 |
| 68 | 515.84 | 68.48 | 69.52 | 92.69 | 115.86 | 278.07 | 320.54 | 483.55 |
| 69 | 523.43 | 69.49 | 70.54 | 94.05 | 117.56 | 282.16 | 325.25 | 490.66 |
| 70 | 531.02 | 70.50 | 71.56 | 95.41 | 119.27 | 286.24 | 329.96 | 497.77 |
| 71 | 538.60 | 71.50 | 72.58 | 96.78 | 120.97 | 290.33 | 334.68 | 504.88 |
| 72 | 546.19 | 72.51 | 73.61 | 98.14 | 122.68 | 294.42 | 339.39 | 512.00 |
| 73 | 553.77 | 73.52 | 74.63 | 99.50 | 124.38 | 298.51 | 344.11 | 519.11 |
| 74 | 561.36 | 74.53 | 75.65 | 100.87 | 126.08 | 302.60 | 348.82 | 526.22 |
| 75 | 568.95 | 75.53 | 76.67 | 102.23 | 127.79 | 306.69 | 353.53 | 533.33 |
| 76 | 576.53 | 76.54 | 77.70 | 103.59 | 129.49 | 310.78 | 358.25 | 540.44 |
| 77 | 584.12 | 77.55 | 78.72 | 104.98 | 131.20 | 314.87 | 362.96 | 547.55 |
| 78 | 591.70 | 78.55 | 79.74 | 106.32 | 132.90 | 318.96 | 367.67 | 554.66 |
| 79 | 599.29 | 79.56 | 80.76 | 107.68 | 134.60 | 323.05 | 372.39 | 561.77 |
| S0 | 606.57 | 80.57 | 81.78 | 109.05 | 136.31 | 327.14 | 377.10 | 568.88 |
| 81 | 614.46 | 81.57 | 82.81 | 110.41 | 138.01 | 331.23 | 381.82 | 576.00 |
| 82 | 622.05 | 82.58 | 83.83 | 111.77 | 139.71 | 335.32 | 386.53 | 583.11 |
| 83 | 629.63 | 83.59 | 84. 85 | 113.13 | 141.42 | 339.40 | 391.24 | 590.22 |
| 84 | 637.22 | 84.60 | 85.87 | 114.50 | 143.12 | 343.49 | 395.96 | 597.33 |
| 85 | 644.80 | 85.60 | 86.90 | 115.86 | 144.83 | 347.58 | 400.67 | 604.44 |
| 86 | 652.39 | 86.61 | 87.92 | 117.22 | 146.53 | 351.67 | 405.38 | 611.55 |
| 87 | 659.98 | 87.62 | 88.94 | 118.59 | 148.23 | 355.76 | 410.10 | 618.66 |
| 88 | 667.56 | 88.62 | 89.96 | 119.95 | 149.94 | 359.85 | 414.81 | 625.77 |
| 89 | 675.15 | 89.63 | 90.98 | 121.31 | 151.64 | 363.94 | 419.53 | 632.88 |
| 90 | 682.73 | 90.64 | 92.01 | 129.68 | 153.35 | 368.03 | 424.24 | 640.00 |
| 91 | 690.32 | 91.65 | 93.03 | 124.04 | 155.05 | 372.12 | 428.95 | 647.11 |
| 92 | 697.91 | 92.65 | 94.05 | 125.40 | 156.75 | 376.21 | 433.67 | 654.22 |
| 93 | 705.49 | 93.66 | 95.07 | 126.77 | 158.46 | 380.30 | 438.38 | 661.33 |
| 94 | 713.08 | 94.67 | 96.10 | 128.13 | 160.16 | 384.39 | 443.09 | 668.44 |
| 95 | 720.66 | 95.67 | 97.12 | 129.49 | 161.86 | 388.48 | 447.81 | 675.55 |
| 96 | 728.25 | 96.68 | 98.14 | 130.85 | 163.57 | 392.56 | 452.52 | 682.66 |
| 97 | 735.84 | 97.69 | 99.16 | 132.22 | 165.27 | 396.65 | 457.24 | 689.77 |
| 98 | 743.42 | 98.70 | 100.19 | 133.58 | 166.98 | 400.74 | 461.95 | 696.88 |
| 99 | 751.01 | 99.70 | 101.21 | 134.94 | 168.68 | 404.83 | 466.67 | 703.99 |
| 100 | 758.59 | 100.71 | 102.23 | 136.31 | 170.38 | 408.92 | 471.38 | 711.11 |

III. prussian miles into different geographical measures of distance. 511

| $\begin{aligned} & \text { Prassian } \\ & \text { Miles. } \end{aligned}$ | Kilometres. | Austrian Miles. | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical Learues. $20=1^{\circ} \mathrm{Eq}$. $20=1^{\circ} \mathrm{Eq}$. | French Leagues. $25=10 \mathrm{Eq}$. | $\begin{aligned} & \text { Geograph'l } \\ & \text { or Nautical } \\ & \text { Milies. } \\ & 60=1^{\circ} \mathbf{E}_{q} . \\ & \hline \end{aligned}$ | English statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 7532.48 | 992.95 | 1015.10 | 1353.47 | 1691.83 | 4060.40 | 4680.55 | 7060.95 |
| 2,000 | 15064.97 | 1985.91 | 2030.20 | 2706.93 | 3383.67 | 8120.80 | 9361.11 | 14121.90 |
| 3,000 | 22597.45 | 2978.86 | 3045.30 | 4060.40 | 5075.50 | 12181.19 | 14041.66 | 21182.85 |
| 4,000 | 30129.94 | 3971.81 | 4060.40 | 5413.86 | 6767.33 | 16241.59 | 18722.21 | 28243.79 |
| 5,000 | 37662.42 | 4964.77 | 5075.50 | 6767.33 | 8459.16 | 20301.99 | 23402.77 | 35304.74 |
| 6,000 | 45194.90 | 5957.72 | 6090.60 | 8120.80 | 10151.00 | -4362.39 | 28083.32 | 42365.69 |
| 7,000 | 52727.39 | 6950.68 | 7105.70 | 9474.26 | 11842.83 | 28422.79 | 32763.87 | 49426.64 |
| 8,000 | 60259.87 | 7943.63 | 8120.80 | 10827.73 | 13534.66 | 32483.19 | 37444.43 | 56487.59 |
| 9,000 | 67992.36 | 8936.58 | 9135.90 | 12181.19 | 15226.49 | 36543.58 | 42124.98 | 63548.54 |
| 10,000 | 75324.84 | 9929.54 | 10151.00 | 13534.66 | 16918.33 | 40603.98 | 46805.53 | 70609.49 |
| 100 | 753.25 | 99.30 | 101.51 | 135.35 | 169.18 | 406.04 | 468.06 | 706.09 |
| 200 | 1506.50 | 198.59 | 203.02 | 270.69 | 338.37 | 812.08 | 936.11 | 1412.19 |
| 300 | 2259.75 | 297.89 | 304.53 | 406.04 | 507.55 | 1218.12 | 1404.17 | 2118.28 |
| 400 | 3012.99 | 397.18 | 406.04 | 541.39 | 676.73 | 1624.16 | 1872.22 | 2824.38 |
| 500 | 3766.24 | 496.48 | 507.55 | 676.73 | 845.92 | 2030.20 | 2340.28 | 3530.47 |
| 600 | 4519.49 | 595.77 | 609.06 | 812.08 | 1015.10 | 2436.24 | 2808.33 | 4236.57 |
| 700 | 5272.74 | 695.07 | 710.57 | 947.43 | 1184.28 | 2842.28 | 3276.39 | 4942.66 |
| 800 | 6025.99 | 794.36 | 812.08 | 1082.77 | 1353.47 | 3248.32 | 3744.44 | 5648.76 |
| 900 | 6799.24 | 893.66 | 913.59 | 1218.12 | 1523.65 | 3654.36 | 4212.50 | 6354.85 |
| 1000 | 7532.48 | 992.95 | 1015.10 | 1353.47 | 1691.83 | 4060.40 | 4680.55 | 7060.95 |
| 1 | 7.53 | 0.99 | 1.02 | 1.35 | 1.69 | 4.06 | 4.68 | 7.06 |
| 2 | 15.06 | 1.99 | 2.03 | 2.71 | 3.38 | 8.12 | 9.36 | 14.12 |
| 3 | 22.60 | 2.98 | 3.05 | 4.06 | 5.08 | 12.18 | 14.04 | 21.18 |
| 4 | 30.13 | 3.97 | 4.06 | 5.41 | 6.77 | 16.24 | 18.72 | 28.24 |
| 5 | 37.66 | 4.96 | 5.08 | 6.77 | 8.46 | 20.30 | 23.40 | 35.30 |
| 6 | 45.19 | 5.96 | 6.09 | 8.12 | 10.15 | 24.36 | 28.08 | 42.37 |
| 7 | 52.73 | 6.95 | 7.11 | 9.47 | 11.84 | 28.42 | 32.76 | 49.43 |
| 8 | 60.26 | 7.94 | 8.12 | 10.83 | 13.53 | 32.48 | 37.44 | 56.49 |
| 9 | 67.79 | 8.94 | 9.14 | 12.18 | 15.23 | 36.54 | 42.12 | 63.55 |
| 10 | 75.32 | 9.93 | 10.15 | 13.53 | 16.92 | 40.60 | 46.81 | 70.61 |
| 11 | 82.86 | 10.92 | 11.17 | 14.89 | 18.61 | 44.66 | 51.49 | 77.67 |
| 12 | 90.39 | 11.92 | 12.18 | 16.24 | 20.30 | 48.72 | 56.17 | 84.73 |
| 13 | 97.92 | 12.91 | 13.20 | 17.60 | 21.99 | 52.79 | 60.85 | 91.79 |
| 14 | 105.45 | 13.90 | 14.21 | 18.95 | 23.69 | 56.85 | 65.53 | 98.85 |
| 15 | 112.99 | 14.89 | 15.23 | 20.30 | 25.38 | 60.91 | 70.21 | 105.91 |
| 16 | 120.52 | 15.89 | 16.24 | 21.66 | 27.07 | 64.97 | 74.89 | 112.98 |
| 17 | 128.05 | 16.88 | 17.26 | 23.01 | 28.76 | 69.03 | 79.57 | 120.04 |
| 18 | 135.58 | 17.87 | 18.27 | 24.36 | 30.45 | 73.09 | 84.25 | 127.10 |
| 19 | 143.12 | 18.87 | 19.29 | 25.72 | 32.14 | 77.15 | 88.93 | 134.16 |
| 20 | 150.65 | 19.86 | 20.30 | 27.07 | 33.84 | 81.21 | 93.61 | 141.22 |

512
prussian miles into different geographical measures of distance.

| Prussian Miles. | Kilometres. | Austrian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \mathbf{E q} . \end{gathered}$ | Nautical <br> Leagues. $20=1^{\circ} \mathrm{Eq}$. | French <br> Leagues. $25=1^{\circ} \mathrm{Eq}$ - | Geograph'1 or Nauticai Miles. $60=1^{\circ} \mathrm{Eq}$. | English <br> statute <br> Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 158.18 | 20.85 | 21.32 | 28.42 | 35.53 | 85.27 | 98.29 | 148.28 |
| 22 | 165.71 | 21.84 | 22.33 | 29.78 | 37.22 | 89.33 | 102.97 | 155.34 |
| 23 | 173.25 | 22.84 | 23.35 | 31.13 | 38.91 | 93.39 | 107.65 | 162.40 |
| 24 | 180.78 | 23.83 | 24.36 | 32.48 | 40.60 | 97.45 | 112.33 | 169.46 |
| 25 | 188.31 | 24.82 | 25.38 | 33.84 | 42.30 | 101.51 | 117.01 | 176.52 |
| 26 | 195.84 | 25.81 | 26.39 | 35.19 | 43.99 | 105.57 | 121.69 | 183.58 |
| 27 | 203.38 | 26.81 | 27.41 | 36.54 | 45.68 | 109.63 | 126.37 | 190.65 |
| 28 | 210.91 | 27.80 | 28.42 | 37.90 | 47.37 | 113.69 | 131.06 | 197.71 |
| 29 | 218.44 | 28.80 | 29.44 | 39.25 | 49.06 | 117.75 | 135.74 | 204.77 |
| 30 | 225.97 | 29.79 | 30.45 | 40.60 | 50.75 | 121.81 | 140.42 | 211.83 |
| 31 | 233.51 | 30.78 | 31.47 | 41.96 | 52.45 | 125.87 | 145.10 | 218.89 |
| 32 | 241.04 | 31.77 | 32.48 | 43.31 | 54.14 | 129.93 | 149.78 | 225.95 |
| 33 | 248.57 | 32.77 | 33.50 | 44.66 | 55.83 | 133.99 | 154.46 | 233.01 |
| 34 | 256.10 | 33.76 | 34.51 | 46.02 | 57.52 | 138.05 | 159.14 | 240.07 |
| 35 | 263.64 | 34.75 | 35.53 | 47.37 | 59.21 | 142.11 | 163.82 | 247.13 |
| 36 | 271.17 | 35.75 | 36.54 | 48.72 | 60.91 | 146.17 | 168.50 | 254.19 |
| 37 | 278.70 | 36.74 | 37.56 | 50.08 | 62.60 | 150.24 | 173.18 | 261.26 |
| 38 | 286.23 | 37.73 | 38.57 | 51.43 | 64.39 | 154.30 | 177.86 | 268.32 |
| 39 | 293.77 | 38.73 | 39.59 | 52.79 | 65.98 | 158.36 | 182.54 | 275.38 |
| 40 | 301.30 | 39.72 | 40.60 | 54.14 | 67.67 | 162.42 | 187.22 | 282.44 |
| 41 | 308.83 | 40.71 | 41.62 | 55.49 | 69.37 | 166.48 | 191.90 | 289.50 |
| 42 | 316.36 | 41.70 | 42.63 | 56.85 | 71.06 | 170.54 | 196.58 | $\underline{296.56}$ |
| 43 | 323.90 | 42.70 | 43.65 | 58.20 | 72.75 | 174.60 | 201.26 | 303.62 |
| 44 | 331.43 | 43.69 | 44.66 | 59.55 | 74.44 | 178.66 | 205.94 | 310.68 |
| 45 | 338.96 | 44.68 | 45.69 | 60.91 | 76.13 | 182.72 | 210.62 | 317.74 |
| 46 | 346.49 | 45.68 | 46.69 | 62.26 | 77.82 | 186.78 | 215.31 | 324.80 |
| 47 | 353.03 | 46.67 | 47.72 | 63.61 | 79.52 | 190.84 | 219.99 | 331.86 |
| 48 | 361.56 | 47.66 | 48.72 | 64.97 | 81.21 | 194.90 | 224.67 | 335.93 |
| 49 | 369.09 | 48.65 | 49.75 | 66.32 | 82.90 | 198.96 | 229.35 | 345.99 |
| 50 | 376.62 | 49.65 | 50.75 | 67.67 | 84.59 | 203.02 | 234.03 | 353.05 |
| 51 | 384.16 | 50.64 | 51.77 | 69.03 | 86.28 | 207.08 | 238.71 | 360.11 |
| 52 | 391.69 | 51.63 | 52.79 | 70.38 | 87.98 | 211.14 | 243.39 | 367.17 |
| 53 | 399.22 | 52.63 | 53.80 | - 71.73 | 89.67 | 215.20 | 248.07 | 374.23 |
| 54 | 406.75 | 53.62 | 54.82 | 73.09 | 91.36 | 219.26 | 252.75 | 381.29 |
| 55 | 414.29 | 54.61 | 55.83 | 74.44 | 93.05 | 223.32 | 257.43 | 388.35 |
| 56 | 421.82 | 55.61 | 56.85 | 75.79 | 94.74 | 227.38 | 262.11 | 395.41 |
| 57 | 429.35 | 56.60 | 57.86 | 77.15 | 96.43 | 231.44 | 266.79 | 402.47 |
| 58 | 436.88 | 57.59 | 58.88 | 78.50 | 98.13 | 235.50 | 271.47 | 409.53 |
| 59 | 444.42 | 58.58 | 59.89 | 79.85 | 99.82 | 239.56 | 276.15 | 416.60 |
| 60 | 451.95 | 59.58 | 60.91 | 81.21 | 101.51 | 243.62 | 280.83 | 423.66 |

PRUSSIAN MILES INTO DIFFERENT GEOGRAPHICAL MEASURES OF DISTANCE.

| $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{gathered} \text { German } \\ \text { Mile } \\ 15=1-E_{1} . \end{gathered}$ | $\begin{aligned} & \text { Nautical } \\ & \text { Leagues } \\ & 20=1^{0} \mathrm{E}_{4} . \end{aligned}$ | $\begin{gathered} \text { French } \\ \text { Leatabes. } \\ 25=10 \text { E.4. } \end{gathered}$ | $\begin{gathered} \text { Gergraph't } \\ \text { or Nautical } \\ \text { Miles. } \\ 60=1^{\circ} \mathrm{Eq} . \end{gathered}$ | En livh statute Miles. | $\begin{aligned} & \text { Russian } \\ & \text { Wersts. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 459.48 | 60.57 | 61.92 | 82.56 | 103.20 | 247.68 | 285.51 | 430.72 |
| 62 | 467.01 | 61.56 | 62.94 | 83.91 | 104.89 | 251.74 | 290.19 | 437.78 |
| 63 | 474.55 | 63.56 | 63.95 | 85.27 | 106.59 | 255.81 | 294.87 | 44.84 |
| 64 | 483.08 | 63.55 | 64.97 | 86.62 | 108.28 | 259.87 | 299.56 | 451.90 |
| 65 | 489.61 | 64.54 | 65.98 | 87.98 | 109.97 | 263.93 | 304.24 | 455.96 |
| 66 | 497.14 | 65.53 | 67.00 | 89.33 | 111.66 | 267.99 | 308.92 | 466.02 |
| 67 | 504.68 | 66.53 | 68.01 | 90.68 | 113.35 | 272.05 | 313.60 | 473.118 |
| 68 | 512.21 | 67.52 | 69.03 | 92.04 | 115.04 | 276.11 | 318.28 | 480.14 |
| 69 | 519.74 | 68.51 | 70.14 | 93.39 | 116.74 | 280.17 | 322.96 | 487.21 |
| 70 | 527.27 | 69.51 | 71.06 | 94.74 | 118.42 | 284.23 | 327.64 | 494.27 |
| 71 | 534.81 | 70.50 | 72.07 | 96.10 | 120.12 | 288.29 | 332.32 | 501.33 |
| 72 | 542.34 | 71.49 | 73.09 | 97.45 | 121.81 | 292.35 | 337.00 | 508.33 |
| 73 | 549.87 | 72.49 | 74.10 | 98.80 | 123.50 | 296.41 | 341.68 | 515.45 |
| 74 | 557.40 | 73.48 | 75.12 | 100.16 | 125.20 | 300.47 | 346.36 | 522.51 |
| 75 | 564.94 | 74.47 | 76.13 | 101.51 | 126.89 | 304.53 | 351.04 | 529.57 |
| 76 | 572.47 | 75.46 | 77.15 | 102.86 | 128.58 | 308.59 | 355.72 | 536.63 |
| 77 | 580.00 | 76.46 | 78.16 | 104.22 | 130.27 | 312.65 | 360.40 | 543.69 |
| 78 | 587.53 | 77.45 | 79.18 | 105.57 | 131.96 | 316.71 | 365.08 | 550.75 |
| 79 | 595.07 | 78.44 | 80.19 | 106.92 | 133.65 | 320.77 | 369.76 | 557.81 |
| 80 | 602.60 | 79.44 | 81.21 | 108.28 | 135.35 | 324.83 | 374.44 | 564.88 |
| 81 | 610.13 | 80.43 | 82.22 | 109.63 | 137.04 | 328.89 | 379.12 | 571.94 |
| 82 | 617.66 | 81.42 | 83.84 | 110.98 | 138.73 | 332.95 | 383.81 | 578.10 |
| 83 | 625.20 | 82.42 | 84.25 | 112.34 | 140.42 | 337.01 | 388.49 | 586.06 |
| 84 | 632.73 | 83.41 | 85.27 | 113.69 | 142.11 | 341.07 | 393.17 | 593.12 |
| 85 | 640.26 | 84.40 | 88.08 | 115.04 | 143.81 | 345.13 | 397.85 | 600.18 |
| 86 | 647.79 | 85.39 | 87.30 | 116.40 | 145.50 | 349.19 | 402.53 | 607.24 |
| 87 | 655.33 | 86.39 | 88.31 | 117.75 | 147.19 | 353.25 | 407.21 | 614.30 |
| 88 | 662.86 | 87.38 | 89.33 | 119.11 | 148.58 | 357.32 | 411.89 | 621.36 |
| 89 | 670.39 | 88.37 | 90.34 | 120.46 | 150.57 | 361.38 | 416.57 | 628.42 |
| 90 | 677.92 | 89.37 | 91.36 | 121.81 | 152.26 | 365.44 | 421.25 | 635.49 |
| 91 | 685.46 | 90.36 | 92.37 | 123.17 | 153.96 | 369.50 | 425.93 | 642.55 |
| 92 | 692.99 | 91.35 | 93.39 | 124.52 | 155.65 | 373.56 | 430.61 | 649.61 |
| 93 | 700.52 | 92.34 | 94.40 | 125.87 | 157.34 | 377.62 | 435.29 | 656.67 |
| 94 | 708.0 .5 | 93.34 | 95.42 | 127.23 | 159.03 | 381.68 | 439.97 | 663.73 |
| 95 | 715.59 | 94.33 | 96.43 | 128.58 | 160.72 | 385.74 | 444.65 | 670.79 |
| 96 | 723.12 | 95.32 | 97.45 | 129.93 | 162.42 | 359.80 | 449.33 | 677.85 |
| 97 | 730.65 | 96.32 | 98.46 | 131.29 | 164.11 | 393.86 | 454.01 | 684.91 |
| 98 | 738.18 | 97.31 | 99.48 | 132.64 | 165.80 | 397.92 | 458.69 | 691.97 |
| 99 | 745.72 | 98.30 | 100.49 | 133.99 | 167.49 | 401.98 | 463.38 | 699.03 |
| 100 | 753.25 | 99.30 | 101.51 | 135.35 | 169.18 | 406.04 | 468.06 | 706.09 |

## 514

IV. german miles into different geographical measures of distance.

| German Miles. | Kilowetres. | Austrian Miles. | Prussian Miles. | Nautical Leagues. $20=1^{\circ} \mathrm{Eq}$. | French Leagues. $25=1^{\circ}$ Eq. | Geograph'l or Nantical Miles. $60=1^{\circ} \mathrm{Eq} q$. | English statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 7420.44 | 978.18 | 985.13 | 1333.33 | 1666.67 | 4000.00 | 4610.93 | 6955.92 |
| 2,000 | 14840.88 | 1956.37 | 1970.25 | 2666.67 | 3333.33 | 8000.00 | 9221.86 | 13911.83 |
| 3,000 | 22261.32 | 2934.55 | 2955.38 | 4000.00 | 5000.00 | 12000.00 | 13832.79 | 20867.75 |
| 4,000 | 29681.75 | 3912.73 | 3940.51 | 5333.33 | 6666.67 | 16000.00 | 18443.72 | 27823.67 |
| 5,000 | 37102.19 | 4890.92 | 4925.63 | 6666.67 | 8333.33 | 20000.00 | 23054.66 | 34779.59 |
| 6,000 | 44522.63 | 5869.10 | 5910.75 | 8000.00 | 10000.00 | 24000.00 | 27665.59 | 41735.50 |
| 7,000 | 51943.07 | 6847.28 | 6895.88 | 9333.33 | 11666.67 | 28000.00 | 32276.52 | 48691.42 |
| 8,000 | 59363.51 | 7825.47 | 7881.00 | 10666.67 | 13333.33 | 32000.00 | 36887.45 | 55647.34 |
| 9,000 | 66783.95 | 8803.65 | 8866.13 | 12000.00 | 15000.00 | 36000.00 | 41498.38 | 62603.26 |
| 10,000 | 74204.39 | 9781.83 | 9851.25 | 13333.33 | 16666.66 | 40000.00 | 46109.31 | 69559.17 |
| 100 | 742.04 | 97.82 | 98.51 | 133.33 | 166.67 | 400.00 | 461.09 | 695.59 |
| 200 | 1484.09 | 195.64 | 197.03 | 266.67 | 333.33 | 800.00 | 922.19 | 1391.18 |
| 300 | 22.6 .13 | 293.46 | 295.54 | 400.00 | 500.00 | 1200.00 | 1383.28 | 2086.78 |
| 400 | 2968.18 | 391.27 | 394.05 | 533.33 | 666.67 | 1600.00 | 1844.37 | 2782.37 |
| 500 | 3710.22 | 489.09 | 492.56 | 666.67 | 833.33 | 2000.00 | 2305.47 | 3477.96 |
| 600 | 4452.26 | 586.91 | 591.08 | 800.00 | 1000.00 | 2400.00 | 2766.56 | 4173.55 |
| 700 | 5194.31 | 684.73 | 689.59 | 933.33 | 1166.67 | 2800.00 | 3227.65 | 4869.14 |
| 800 | 5936.35 | 782.55 | 788.10 | 1066.67 | 1333.33 | 3200.00 | 3688.74 | 5564.73 |
| 900 | 6678.39 | 880.37 | 886.61 | 1200.00 | 1500.00 | 3600.00 | 4149.84 | 6260.33 |
| 1000 | 7420.44 | 978.18 | 985.13 | 1333.33 | 1666.67 | 4000.00 | 4610.93 | 6955.92 |
| 1 | 7.42 | 0.98 | 0.99 | 1.33 | 1.67 | 4.00 | 4.61 | 6.96 |
| 2 | 14.84 | 1.96 | 1.97 | 2.67 | 3.33 | 8.00 | 9.22 | 13.91 |
| 3 | 22.26 | 2.93 | 2.96 | 3.00 | 5.00 | 12.00 | 13.83 | 20.87 |
| 4 | 29.68 | 3.91 | 3.94 | 5.33 | 6.67 | 16.00 | 18.44 | 27.82 |
| 5 | 37.10 | 4.89 | 4.93 | 6.67 | 8.33 | 20.00 | 23.05 | 34.78 |
| 6 | 44.52 | 5.87 | 5.91 | 8.00 | 10.00 | 24.00 | 27.67 | 41.74 |
| 7 | 51.94 | 6.85 | 6.90 | 9.33 | 11.67 | 28.00 | 32.28 | 48.69 |
| 8 | 59.36 | 7.83 | 7.88 | 10.67 | 13.33 | 32.00 | 36.89 | 55.65 |
| 9 | 66.78 | 8.80 | 8.87 | 12.00 | 15.00 | 36.00 | 41.50 | 62.60 |
| 10 | 74.20 | 9.78 | 9.85 | 13.33 | 16.67 | 40.00 | 46.11 | 69.56 |
| 11 | 81.62 | 10.76 | 10.84 | 14.67 | 18.33 | 44.00 | 50.72 | 76.52 |
| 12 | 89.05 | 11.74 | 11.82 | 16.00 | 20.00 | 48.00 | 55.33 | 83.47 |
| 13 | 96.47 | 12.72 | 12.81 | 17.33 | 21.67 | 52.00 | 59.94 | 90.43 |
| 14 | 103.89 | 13.69 | 13.79 | 18.67 | 23.33 | 56.00 | 64.55 | 97.38 |
| 15 | 111.31 | 14.67 | 14.78 | 20.00 | 25.00 | 60.00 | 69.16 | 104.34 |
| 16 | 118.73 | 15.65 | 15.76 | 21.33 | 26.67 | 64.00 | 72.77 | 111.29 |
| 17 | 126.15 | 16.62 | 16.75 | 22.67 | 28.33 | 68.00 | 78.39 | 118.25 |
| 18 | 133.57 | 17.61 | 17.73 | 24.00 | 30.00 | 72.00 | 83.00 | 125.21 |
| 19 | 140.99 | 18.59 | 18.72 | 25.33 | 31.67 | 76.00 | 87.61 | 132.16 |
| 20 | 148.41 | 19.56 | 19.70 | 26.67 | 33.33 | 80.00 | 92.22 | 139.12 |

german miles into different geograpiilcal measures of distance.

german miles into difperent geugraphical measures of distance.

| $\begin{aligned} & \text { German } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { Kilo- } \\ \text { metres. } \end{gathered}$ | $\begin{aligned} & \text { Anstrian } \\ & \text { Miles. } \end{aligned}$ | Prussian Miles. | Nautical <br> Leagues. <br> $20=1^{\circ} \mathrm{Eq}$. | French Leagues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'1 <br> or Nautical $\begin{gathered} \text { Miles. } \\ =1^{\circ} \\ \text { Eq. } \end{gathered}$ | English statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 45.2 .65 | 59.67 | 60.09 | 81.33 | 101.67 | 244.00 | 281.27 | 424.31 |
| 62 | 450.07 | 60.65 | 61.08 | 82.67 | 103.33 | 248.00 | 285.88 | 431.27 |
| 63 | 467.49 | 61.63 | 62.06 | 84.00 | 105.00 | 252.00 | 290.49 | 438.22 |
| 64 | 474.91 | 62.60 | 63.05 | 85.33 | 106.67 | 256.00 | 295.10 | 445.18 |
| 65 | 4 2.33 | 63.58 | 6.4 .03 | 80.67 | 108.33 | 260.00 | 299.71 | 452.13 |
| 66 | 489.75 | 64.56 | 65.02 | 88.00 | 110.00 | 264.00 | 304.32 | 459.09 |
| 67 | 497.17 | 65.54 | 66.00 | 89.33 | 111.67 | 268.00 | 308.93 | 466.05 |
| 68 | 504.59 | 66.52 | 63.99 | 90.67 | 113.33 | 272.00 | 313.54 | 473.00 |
| 69 | 512.01 | 67.49 | 67.97 | 92.00 | 115.00 | 276.00 | 318.15 | 479.96 |
| 70 | 519.43 | 68.47 | 68.96 | 93.33 | 116.67 | 250.00 | 322.77 | 486.91 |
| 71 | 526.85 | 69.45 | 69.94 | 94.66 | 118.33 | 284.00 | 327.38 | 493.87 |
| 72 | 534.27 | 70.43 | 70.93 | 96.00 | 120.00 | 285.00 | 331.99 | 500.83 |
| 73 | 541.69 | 71.41 | 71.91 | 97.33 | 121.67 | 292.00 | 336.60 | 507.78 |
| 74 | 543.11 | 72.39 | 72.90 | 95.66 | 123.33 | 296.00 | 341.21 | 514.74 |
| 75 | 556.53 | 73.36 | 73.85 | 100.00 | 125.00 | 300.00 | 345.82 | 521.69 |
| 76 | 563.95 | 74.34 | 74.87 | 101.33 | 126.67 | 304.00 | 350.43 | 528.65 |
| 77 | 571.37 | 75.32 | 75.85 | 102.67 | 128.33 | 305.00 | 355.64 | 535.61 |
| 78 | 578.79 | 76.30 | 76.84 | 104.00 | 130.00 | 31.00 | 359.65 | 542.56 |
| 79 | 588.21 | 77.28 | 77.82 | 105.33 | 131.67 | 316.00 | 364.26 | 549.52 |
| 80 | 593.64 | 75.25 | 78.81 | 106.67 | 133.33 | 320.00 | 368.87 | 556.47 |
| 81 | 601.106 | 79.23 | 79.80 | 108.00 | 135.00 | 324.00 | 373.49 | 563.43 |
| 82 | 608.40 | 80.21 | 80.78 | 109.33 | 136.67 | 328.00 | 378.10 | 570.39 |
| 83 | 615.90 | 81.19 | 81.74 | 110.67 | 135.33 | 33.00 | 352.71 | 577.34 |
| 64 | 623.32 | 82.17 | 82.75 | 112.00 | 140.00 | 336.00 | 357.32 | 584.30 |
| 8.5 | 630.74 | 83.15 | 83.74 | 113.33 | 141.67 | 340.00 | 391.93 | 591.25 |
| 86 | 638.16 | 84.12 | 84.72 | 114.67 | 143.33 | 344.00 | 396.54 | 598.21 |
| 67 | 645.5 | ع5.10 | 85.71 | 116.00 | 145.00 | 34800 | 401.15 | 605.16 |
| \&s | 653.00 | 86.05 | 86.69 | 117.33 | 146.67 | 352.00 | 405.76 | $61 \% .12$ |
| 89 | 660.42 | 85.06 | 87.68 | 118.67 | 148.33 | 356.00 | 410.97 | 619.08 |
| 90 | 667.54 | 88.04 | 88.66 | 120.00 | 150.00 | 360.00 | 414.95 | 626.03 |
| 91 | 675.25 | 89.01 | 89.65 | 121.33 | 151.67 | 364.00 | 419.60 | 632.99 |
| 92 | 682.65 | 89.99 | 90.63 | 122.67 | 153.33 | 365.00 | 424.21 | 639.94 |
| 93 | 690.10 | 90.97 | 91.62 | 124.00 | 155.00 | 372.00 | 428.82 | 646.90 |
| 94 | 697.52 | 91.95 | 92.60 | 125.33 | 156.67 | 376.00 | 433.43 | 653.86 |
| 95 | 704.94 | 92.93 | 93.59 | 126.67 | 155.33 | 380.00 | 438.04 | 660.81 |
| 96 | 712.36 | 93.91 | 94.57 | 128.00 | 160.00 | 38400 | 442.65 | 667.77 |
| 97 | 719.78 | 94.65 | 95.56 | 129.33 | 161.67 | 359.00 | 447.26 | 674.72 |
| 98 | 727.20 | 95.86 | 96.54 | 130.67 | 163.33 | 392.00 | 451.87 | 681.68 |
| 99 | 734.62 | 96.84 | 97.53 | 132.00 | 165.00 | 396.00 | 456.48 | 688.64 |
| 100 | 742.64 | 97.82 | 98.51 | 133.33 | 166.67 | 400.00 | 441.09 | 795.59 |

V. nautical leagues into different geographical measures of distance.

| Nautical Leagues. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \text { Eq. } \end{gathered}$ | $\begin{gathered} \text { French } \\ \text { Leagues. } \\ 25=10 \text { Eq. } \end{gathered}$ | Geograph'l or Nautical miles. $60=1^{\circ} \mathrm{Eq}$. | English Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 5565.33 | 733.64 | 738.84 | 750.00 | 1250.00 | 3000.00 | 3458.20 | 5216.94 |
| 2,000 | 11130.66 | 1467.28 | 1477.69 | 1500.00 | 2500.00 | 6000.00 | 6916.40 | 10433.88 |
| 3,000 | 16695.99 | 2200.91 | 2216.53 | 2250.00 | 3750.00 | 9000.00 | 10374.59 | 15650.81 |
| 4,000 | 22261.32 | 2934.55 | 2955.38 | 3000.00 | 5000.00 | 12000.00 | 13832.79 | 20867.75 |
| 5,000 | 27826.64 | 3668.19 | 3694.22 | 3750.00 | 6250.00 | 15000.00 | 17291.00 | 26084.69 |
| 6,000 | 33391.98 | 4401.83 | 44.33 .06 | 4500.00 | 7500.00 | 18000.00 | 20749.19 | 31301.63 |
| 7,000 | 38957.30 | 5135.46 | 5171.91 | 5250.00 | 8750.00 | 21000.00 | 24207.39 | 36518.57 |
| 8,000 | 44522.63 | 5869.10 | 5910.75 | 6000.00 | 10000.00 | 24000.00 | 27665.58 | 41735.50 |
| 9,000 | 50057.96 | 6602.74 | 6649.59 | 6750.00 | 11250.00 | 27000.00 | 31123.78 | 46952.44 |
| 10,000 | 55653.29 | 7336.38 | 7388.44 | 7500.00 | 12500.00 | 30000.00 | 34581.98 | 52169.38 |
| 100 | 556.53 | 73.30 | 73.88 | 75.00 | 125.00 | 300.00 | 345.82 | 521.69 |
| 200 | 1113.07 | 146.73 | 147.77 | 150.00 | 250.00 | 600.00 | 691.64 | 10.43 .39 |
| 300 | 1669.60 | 220.09 | 221.65 | 225.00 | 375.00 | 900.00 | 1037.46 | 1565.08 |
| 400 | 2226.13 | 293.46 | 295.54 | 300.00 | 500.00 | 1200.00 | 1383.28 | 2086.78 |
| 500 | 2782.66 | 366.82 | 369.42 | 375.00 | 625.00 | 1500.00 | 1729.10 | 2608.47 |
| 600 | 3339.20 | 440.18 | 443.31 | 450.00 | 750.00 | 1800.00 | 2074.92 | 3130.16 |
| 700 | 3895.73 | 513.55 | 517.19 | 525.00 | 875.00 | 2100.00 | 2420.74 | 3651.86 |
| 800 | 4452.26 | 586.91 | 591.08 | 600.00 | 1000.00 | 2400.00 | 2766.56 | 4173.55 |
| 900 | 5008.80 | 660.27 | 664.96 | 675.00 | 1125.00 | 2700.00 | 3112.38 | 4695.24 |
| 1000 | 5565.33 | 733.64 | 738.84 | 750.00 | 1250.00 | 3000.00 | 3458.20 | 5216.94 |
| 1 | 5.57 | 0.73 | 0.74 | 0.75 | 1.25 | 3.00 | 3.46 | 5.22 |
| 2 | 11.13 | 1.47 | 1.48 | 1.50 | 2.50 | 6.00 | 6.92 | 10.43 |
| 3 | 16.70 | 2.20 | 2.22 | 2.25 | 3.75 | 9.00 | 10.37 | 15.65 |
| 4 | 22.26 | 2.93 | 2.96 | 3.00 | 5.00 | 12.00 | 13.83 | 20.87 |
| 5 | 27.83 | 3.67 | 3.69 | 3.75 | 6.25 | 15.00 | 17.29 | 26.08 |
| 6 | 33.39 | 4.40 | 4.43 | 4.50 | 7.50 | 18.00 | 20.75 | 31.30 |
| 7 | 38.96 | 5.14 | 5.17 | 5.25 | 8.75 | 21.00 | 24.21 | 36.52 |
| 8 | 44.52 | 5.87 | 5.91 | 6.00 | 10.00 | 24.00 | 27.67 | 41.74 |
| 9 | 50.09 | 6.60 | 6.65 | 6.75 | 11.25 | 27.00 | 31.12 | 46.95 |
| 10 | 55.65 | 7.34 | 7.39 | 7.50 | 12.50 | 30.00 | 34.5 S | 52.17 |
| 11 | 61.22 | 8.07 | 8.13 | 8.25 | 13.75 | 33.00 | 38.04 | 57.39 |
| 12 | 66.78 | 8.80 | 8.87 | 9.00 | 15.00 | 36.00 | 41.50 | 62.60 |
| 13 | 72.35 | 9.54 | 9.60 | 9.75 | 16.25 | 39.00 | 44.96 | 67.82 |
| 14 | 77.91 | 10.27 | 10.34 | 10.50 | 17.50 | 42.00 | 48.41 | 73.04 |
| 15 | 83.48 | 11.00 | 11.08 | 11.25 | 18.75 | 45.00 | 51.87 | 78.25 |
| 16 | 89.05 | 11.74 | 11.82 | 12.00 | 20.00 | 48.00 | 55.33 | 83.47 |
| 17 | 94.61 | 12.47 | 12.56 | 12.75 | 21.25 | 51.00 | 58.79 | 88.69 |
| 18 | 100.18 | 13.21 | 13.30 | 13.50 | 22.50 | 54.00 | 62.25 | 93.90 |
| 19 | 105.74 | 13.94 | 14.04 | 14.25 | 23.75 | 57.00 | 65.71 | 99.12 |
| 20 | 111.31 | 14.67 | 14.78 | 15.00 | 25.00 | 60.00 | 69.16 | 104.34 |

NAUTICAL LEAGUES INTO DIFFERENT GEOGRAPIICAL MEASURES OF DISTANCE.

| Nautical <br> Leagues. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \mathrm{E}_{4} . \end{gathered}$ | $\begin{gathered} \text { French } \\ \mathbf{L} \text { Lengues. } \\ 20=10 \mathbf{E q} . \end{gathered}$ | Geograph'l or Nautical Miles. $60=1^{\circ}$ Eq. | English statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 116.87 | 15.41 | 15.52 | 15.75 | 26.25 | 63.00 | 72.62 | 109.56 |
| 22 | 123.44 | 16.14 | 16.25 | 16.50 | 27.50 | 66.00 | 75.08 | 114.77 |
| 23 | 128.00 | 16.87 | 16.99 | 17.25 | 28.75 | 69.00 | 79.54 | 11999 |
| 24 | 133.57 | 17.61 | 17.73 | 18.00 | 30.00 | 72.00 | 83.00 | 125.21 |
| 25 | 139.13 | 18.34 | 18.47 | 18.75 | 31.25 | 75.00 | 86.46 | 130.42 |
| 26 | 144.70 | 19.07 | 19.21 | 19.50 | 32.50 | 78.00 | 89.91 | 135.64 |
| 27 | 150.26 | 19.81 | 19.95 | 20.25 | 33.75 | 81.00 | 93.37 | 140.86 |
| 28 | 155.83 | 20.54 | 20.69 | 21.00 | 35.00 | 84.00 | 96.83 | 146.07 |
| 29 | 161.39 | 21.28 | 21.43 | 21.75 | 36.25 | 87.00 | 100.2.' | 151.29 |
| 30 | 166.96 | 22.01 | 22.17 | 22.50 | 37.50 | 90.00 | 103.75 | 156.51 |
| 31 | 172.53 | 22.74 | 22.90 | 23.25 | 38.75 | 93.00 | 107.20 | 161.73 |
| 32 | 178.09 | 23.48 | 23.64 | 24.00 | 40.00 | 96.00 | 110.66 | 166.94 |
| 33 | 183.66 | 24.21 | 24.38 | 24.75 | 41.25 | 99.00 | 114.12 | 172.16 |
| 34 | 159.22 | 24.94 | 25.12 | 25.50 | 42.50 | 102.00 | 117.58 | 177.38 |
| 35 | 194.79 | 25.68 | 25.86 | 26.25 | 43.75 | 105.00 | 121.04 | 182.59 |
| 36 | 200.35 | 26.41 | 26.60 | 27.00 | 45.00 | 108.00 | 124.50 | 187.81 |
| 37 | 205.92 | 27.14 | 27.33 | 27.75 | 46.25 | 111.00 | 127.95 | 193.03 |
| 38 | 211.48 | 27.88 | 28.08 | 28.50 | 47.50 | 114.00 | 131.41 | 198.24 |
| 39 | 217.05 | 28.61 | 28.81 | 29.25 | 48.75 | 117.00 | 134.87 | 203.46 |
| 40 | 222.61 | 29.35 | 29.55 | 30.00 | 50.00 | 120.00 | 138.33 | 208.68 |
| 41 | 228.18 | 30.08 | 30.29 | 30.75 | 51.25 | 123.00 | 141.79 | 213.90 |
| 42 | 233.74 | 30.81 | 31.03 | 31.50 | 52.50 | 126.00 | 145.24 | 219.12 |
| 43 | 239.31 | 31.55 | 31.77 | 32.25 | 53.75 | 129.00 | 148.70 | 224.33 |
| 44 | 244.87 | 32.28 | 32.51 | 33.00 | 55.00 | 132.00 | 152.16 | 229.55 |
| 45 | 250.44 | 33.01 | 33.25 | 33.75 | 56.25 | 135.00 | 155.62 | 234.76 |
| 46 | 256.01 | 33.75 | 33.99 | 34.50 | 57.50 | 138.00 | 159.08 | 239.98 |
| 47 | 261.57 | 34.48 | 34.73 | 35.25 | 58.75 | 141.00 | 162.54 | 245.20 |
| 48 | 267.14 | 35.21 | 35.46 | 36.00 | 60.00 | 144.00 | 165.99 | 250.41 |
| 49 | 272.70 | 35.95 | 36.20 | 36.75 | 61.25 | 147.00 | 169.45 | 255.63 |
| 50 | 278.26 | 36.68 | 36.94 | 37.50 | 62.50 | 150.00 | 172.91 | 260.85 |
| 51 | 283.83 | 37.42 | 37.68 | 38.25 | 63.75 | 153.00 | 176.37 | 266.06 |
| 52 | 289.40 | 38.15 | 38.42 | 39.00 | 65.00 | 156.00 | 179.83 | 271.28 |
| 53 | 294.96 | 38.88 | 39.16 | 39.75 | 66.25 | 159.00 | 183.28 | 276.50 |
| 54 | 300.53 | 39.62 | 39.90 | 40.50 | 67.50 | 162.00 | 186.74 | 281.79 |
| 55 | 306.09 | 40.35 | 40.64 | 41.25 | 68.75 | 165.00 | 190.20 | 286.93 |
| 56 | 311.66 | 41.08 | 41.38 | 42.00 | 70.00 | 168.00 | 193.66 | 292.15 |
| 57 | 317.22 | 41.82 | 42.11 | 42.75 | 71.25 | 171.00 | 197.12 | 297.37 |
| 58 | 322.79 | 42.55 | 42.85 | 43.50 | 72.50 | 174.00 | 200.58 | 302.58 |
| 59 | 328.35 | 43.28 | 43.59 | 44.25 | 73.75 | 177.00 | $\bigcirc 04.03$ | 307.80 |
| 60 | 333.92 | 4.02 | 44.33 | 45.00 | 75.00 | 180.00 | 207.49 | 313.02 |

naUtical Leagues into different geographical measures of distance.

| Nantical Leagues. | $\begin{gathered} \text { Kilo- } \\ \text { metres. } \end{gathered}$ | Austrian Miles. | $\begin{aligned} & \text { Prussiau } \\ & \text { Miles. } \end{aligned}$ | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \text { Eq. } \end{aligned}$ | $\begin{gathered} \text { French } \\ \text { Leagues. } \\ 25=1^{0} \mathrm{Eq} . \end{gathered}$ | Geograph'l <br> or Nautical Miles. $60=1^{\circ}$ Eq. | English Statute Miles. | Russian Werets. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 339.49 | 44.75 | 45.07 | 45.75 | 76.25 | 183.00 | 210.95 | 318.23 |
| 62 | 345.05 | 45.49 | 45.81 | 46.50 | 77.50 | 186.00 | 214.41 | 323.45 |
| 63 | 350.62 | 46.22 | 46.55 | 47.25 | 78.75 | 189.00 | 217.87 | 328.67 |
| 64 | 356.18 | 46.95 | 47.29 | 48.00 | 80.00 | 192.00 | 221.33 | 333.88 |
| 65 | 361.75 | 47.69 | 48.02 | 48.75 | 81.25 | 195.00 | 224.78 | 339.10 |
| 66 | 367.31 | 48.42 | 48.76 | 49.50 | 82.50 | 198.00 | 228.24 | 34.3 .32 |
| 67 | 372.88 | 49.15 | 49.50 | 50.25 | 83.75 | 201.00 | 231.70 | 349.54 |
| 68 | 378.44 | 49.89 | 50.24 | 51.00 | 85.00 | 204.00 | 235.16 | 354.75 |
| 69 | 384.01 | 50.62 | 50.98 | 51.75 | 86.25 | 207.00 | 238.62 | 359.97 |
| 70 | 389.57 | 51.35 | 51.72 | 52.50 | 87.50 | 210.00 | 242.07 | 365.19 |
| 71 | 395.14 | 52.09 | 52. 46 | 53.25 | 88.75 | 213.00 | 245.53 | 370.40 |
| 72 | 400.70 | 52.82 | 53.20 | 54.00 | 90.00 | 216.00 | 248.99 | 375.62 |
| 73 | 406.27 | 53.56 | 53.94 | 54.75 | 91.25 | 219.00 | 252.45 | 380.84 |
| 74 | 411.83 | 54.29 | 54.67 | 55.50 | 92.50 | 22.00 | 255.91 | 386.05 |
| 75 | 417.40 | 55.02 | 55.41 | 56.25 | 93.75 | 225.00 | 259.37 | 391.27 |
| 76 | 422.96 | 55.76 | 56.15 | 57.00 | 95.00 | 228.00 | 262.82 | 396.49 |
| 77 | 428.53 | 56.49 | 56.89 | 57.75 | 96.25 | 231.00 | 266.28 | 401.70 |
| 78 | 434.10 | 57.22 | 57.63 | 58.50 | 97.50 | 234.00 | 269.74 | 406.92 |
| 79 | 439.66 | 57.96 | 58.37 | 59.25 | 98.75 | 237.00 | 273.20 | 412.14 |
| 80 | 445.23 | 58.69 | 59.11 | 60.00 | 100.00 | 240.00 | 276.66 | 417.36 |
| 81 | 450.79 | 59.42 | 59.85 | 60.75 | 101.25 | 243.00 | 280.11 | 422.57 |
| 82 | 456.36 | 60.16 | 60.59 | 61.50 | 102.50 | 246.00 | 283.57 | 427.79 |
| 83 | 461.92 | 60.89 | 61.32 | 62.25 | 103.75 | 249.00 | 287.03 | 433.01 |
| 84 | 467.49 | 61.63 | 62.06 | 63.00 | 105.00 | 252.00 | 290.49 | 438.22 |
| 85 | 473.05 | 62.36 | 62.80 | 63.75 | 106.25 | 255.00 | 293.95 | 443.44 |
| 86 | 478.62 | 63.09 | 63.54 | 64.50 | 107.50 | 258.00 | 297.41 | 448.66 |
| 87 | 484.18 | 63.83 | 64.28 | 65.25 | 108.75 | 261.00 | 300.86 | 453.87 |
| 88 | 489.75 | 64.56 | 65.02 | 66.00 | 110.00 | 264.00 | 304.32 | 459.09 |
| 89 | 495.31 | 65.29 | 65.76 | 66.75 | 111.25 | 267.00 | 307.78 | 464.31 |
| 90 | 500.88 | 66.03 | 66.50 | 67.50 | 112.50 | 270.00 | 311.24 | 469.53 |
| 91 | 506.44 | 66.76 | 67.23 | 68.25 | 113.75 | 273.00 | 314.70 | 474.74 |
| 92 | 512.01 | 67.49 | 67.97 | 69.00 | 115.00 | 276.00 | 318.15 | 479.96 |
| 93 | 517.58 | 68.23 | 68.71 | 69.75 | 116.25 | 279.00 | 321.61 | 485.18 |
| 94 | 523.14 | 68.96 | 69.45 | 70.50 | 117.50 | 282.00 | 325.07 | 490.39 |
| 95 | 528.71 | 69.70 | 70.19 | 71.25 | 118.75 | 285.00 | 328.53 | 495.61 |
| 96 | 534.27 | 70.43 | 70.93 | 72.00 | 120.00 | 288.00 | 331.99 | 500.83 |
| 97 | 539.84 | 71.16 | 71.67 | 72.75 | 121.25 | 291.00 | 335.45 | 506.04 |
| 98 | 545.40 | 71.90 | 72.41 | 73.50 | 122.50 | 294.00 | 338.90 | 511.26 |
| 99 | 550.97 | 72.63 | 73.15 | 74.25 | 123.75 | 297.00 | 342.36 | 516.48 |
| 100 | 556.53 | 73.36 | 73.88 | 75.00 | 125.00 | 300.00 | 345.82 | 521.69 |

TI. french leagues into different geugraphical measures of distance.

| $\begin{aligned} & \text { French } \\ & \text { Leagues. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { M11es. } \\ 15=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Nautical Leasues. $20=1^{\circ} \mathrm{E}_{1}$. | $\begin{gathered} \text { Geugraph }{ }^{\prime} \\ \text { or Nautacal } \\ \text { Miles. } \\ 60=1^{\circ} \mathrm{E} q . \end{gathered}$ | English statute Miles. | $\begin{aligned} & \text { Rnssian } \\ & \text { Wersts. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 4452.26 | 586.91 | 591.07 | 600.00 | 800.00 | 2400.00 | 2766.56 | 4173.55 |
| 2,000 | 8904.53 | 1173.82 | 118.2 .15 | 1200.00 | 1600.00 | 4806.00 | 5533.12 | 8347.10 |
| 3,000 | 13356.79 | 1760.73 | 1773.22 | 1800.00 | 2400.00 | 7200.00 | 8299.67 | 12520.65 |
| 4.000 | 17809.05 | 2347.64 | 2364.30 | 2400.00 | 3200.00 | 9600.00 | 11066.23 | 16694.20 |
| 5,000 | 22261.32 | 2934.55 | 2955.38 | 3000.00 | 4000.00 | 12000.00 | 13832.79 | 20867.75 |
| 6,000 | 23713.58 | 3521.46 | 3546.45 | 3600.00 | 4800.00 | 14400.00 | 16599.35 | 25041.30 |
| 7,000 | 31165.84 | 4108.37 | 4137.53 | +200.00 | 5600.00 | 16800.00 | 19365.91 | 29214.85 |
| 8,000 | 35618.10 | 469\%.28 | 4728.60 | 4800.00 | 6400.00 | 19200.00 | 22132.46 | 33388.40 |
| 9,000 | 40070.37 | 5282.19 | 5319.68 | 5400.00 | 7200.00 | 21600.00 | 24899.02 | 37561.95 |
| 10,000 | 44523.63 | 5869.10 | 5910.75 | 6000.00 | 8000.00 | 24000.00 | 27665.58 | 41735.50 |
| 100 | 44.23 | 58.69 | 59.11 | 60.00 | 80.00 | 240.00 | 276.66 | 417.36 |
| 200 | 890.45 | 117.38 | 118.22 | 120.00 | 160.00 | 480.00 | 553.31 | 834.71 |
| 300 | 1335.68 | 176.07 | 177.32 | 180.00 | 240.00 | 720.00 | 829.97 | 1252.07 |
| 400 | 1780.91 | 234.76 | 236.43 | 240.00 | 320.00 | 960.00 | 1106.62 | 1669.42 |
| 500 | 2226.13 | 293.46 | 295.54 | 300.00 | 400.00 | 1200.00 | 1383.28 | 2086.78 |
| 600 | 2671.36 | 352.15 | 354.65 | 360.00 | 480.00 | 1440.00 | 1859.93 | 2504.13 |
| 700 | 3116.58 | 410.84 | 413.75 | 420.00 | 560.00 | 1680.00 | 1936.59 | 2921.49 |
| 800 | 3561.81 | 469.53 | 472.86 | 480.00 | 640.00 | 1920.00 | 2213.25 | 3338.84 |
| 900 | 4007.04 | $52 \mathrm{S.22}$ | 531.97 | 540.00 | 720.00 | 2160.00 | 2489.90 | 3756.20 |
| 1000 | 452.26 | 586.91 | 591.07 | 600.00 | 800.00 | 2400.00 | 2766.56 | 4173.55 |
| 1 | 4.45 | 0.59 | 0.59 | 0.60 | 0.80 | 2.40 | 2.77 | 4.17 |
| 2 | 8.90 | 1.17 | 1.18 | 1.20 | 1.60 | 4.80 | 5.53 | 8.35 |
| 3 | 13.36 | 1.76 | 1.77 | 1.80 | 2.40 | 7.20 | 8.30 | 12.52 |
| 4 | 17.81 | 2.35 | 2.36 | 2.40 | 3.20 | 9.60 | 11.07 | 16.69 |
| 5 | 22.26 | 2.93 | 2.96 | 3.00 | 4.00 | 12.00 | 13.83 | 20.87 |
| 6 | 26.71 | 3.52 | 3.55 | 3.60 | 4.80 | 14.40 | 16.60 | 25.04 |
| 7 | 31.17 | 4.11 | 4.14 | 4.20 | 5.60 | 16.80 | 19.37 | 29.21 |
| 8 | 35.62 | 4.70 | 4.73 | 4.80 | 6.40 | 19.20 | 22.13 | 33.39 |
| 9 | 40.07 | 5.28 | 5.32 | 5.40 | 7.20 | 21.60 | 24.90 | 37.56 |
| 10 | 44.52 | 5.87 | 5.91 | 6.00 | 8.00 | 24.00 | 27.67 | 41.74 |
| 11 | 48.97 | 6.46 | 6.50 | 6.60 | 8.80 | 26.40 | 30.43 | 45.91 |
| 12 | 53.43 | 7.04 | 7.09 | 7.20 | 9.60 | 28.80 | 33.20 | 50.08 |
| 13 | 57.88 | 7.63 | 7.68 | 7.80 | 10.40 | 31.20 | 35.97 | 54.26 |
| 14 | 62.33 | 8.22 | 8.28 | 8.40 | 11.20 | 33.60 | 38.73 | 58.43 |
| 15 | 66.78 | 8.80 | 8.87 | 9.00 | 12.00 | 36.00 | 41.50 | 62.60 |
| 16 | 71.24 | 9.39 | 9.46 | 9.60 | 12.80 | 38.40 | 44.26 | 66.78 |
| 17 | 75.69 | 9.98 | 10.05 | 10.20 | 13.60 | 40.80 | 47.03 | 70.95 |
| 18 | 80.14 | 10.56 | 10.64 | 10.80 | 14.40 | 43.20 | 49.80 | 75.12 |
| 19 | 84.59 | 11.15 | 11.23 | 11.40 | 15.20 | 45.60 | 52.56 | 79.30 |
| 20 | 89.05 | 11.74 | 11.82 | 12.00 | 16.00 | 48.00 | 55.33 | 83.47 |

FRENCH LEAGUES INTO DIFFERENT GEOGRAPHICAL MEASURES OF DISTANCE.

| $\begin{aligned} & \text { French } \\ & \text { Leagues. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \mathrm{Eq.} . \end{gathered}$ | $\begin{aligned} & \text { Nautical } \\ & \text { Leacues. } \\ & 20=10 \text { Eq. } \end{aligned}$ | Geograph'l <br> or Nantical Miles. $60=1^{\circ}$ Eq. | English Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 93.50 | 12.33 | 12.41 | 12.60 | 16.80 | 50.40 | 58.10 | 87.64 |
| 22 | 97.95 | 12.91 | 13.00 | 13.20 | 17.60 | 52.80 | 60.86 | 91.82 |
| 23 | 102.40 | 13.50 | 13.59 | 13.80 | 18.40 | 55.20 | 63.63 | 95.99 |
| 24 | 106.85 | 14.09 | 14.19 | 14.40 | 19.20 | 57.60 | 66.40 | 100.17 |
| 25 | 111.31 | 14.67 | 14.78 | 15.00 | 20.00 | 60.00 | 69.16 | 104.34 |
| 26 | 115.76 | 15.26 | 15.37 | 15.60 | 20.80 | 62.40 | 71.93 | 108.51 |
| 27 | 120.21 | 15.85 | 15.96 | 16.20 | 21.60 | 64.80 | 74.70 | 112.69 |
| 28 | 124.66 | 16.43 | 16.55 | 16.80 | 22.40 | 67.20 | 77.46 | 116.86 |
| 29 | 129.12 | 17.02 | 17.14 | 17.40 | 23.20 | 69.60 | 80.23 | 121.03 |
| 30 | 133.57 | 17.61 | 17.73 | 18.00 | 24.00 | 72.00 | 83.00 | 125.21 |
| 31 | 138.02 | 18.19 | 18.32 | 18.60 | 24.80 | 74.40 | 85.76 | 129.38 |
| 32 | 142.47 | 18.78 | 18.91 | 19.20 | 25.60 | 76.80 | 88.53 | 133.55 |
| 33 | 146.92 | 19.37 | 19.51 | 1980 | 26.40 | 79.20 | 91.30 | 137.73 |
| 34 | 151.38 | 19.95 | 20.10 | 20.40 | 27.20 | 81.60 | 94.06 | 141.90 |
| 35 | 155.83 | 20.54 | 20.69 | 21.00 | 28.00 | 84.00 | 96.83 | 146.07 |
| 36 | 160.28 | 21.13 | 21.28 | 21.60 | 28.80 | 86.40 | 99.60 | 150.25 |
| 37 | 164.73 | 21.72 | 21.87 | 22.20 | 29.60 | 88.80 | 102.36 | 154.42 |
| 38 | 169.19 | 22.30 | 22.46 | 22.80 | 30.40 | 91.20 | 105.13 | 158.59 |
| 39 | 173.64 | 22.89 | 23.05 | 23.40 | 31.20 | 93.60 | 107.90 | 162.77 |
| 40 | 178.09 | 23.48 | 23.64 | 24.00 | 32.00 | 96.00 | 110.66 | 166.94 |
| 41 | 182.54 | 24.06 | 24.23 | 24.60 | 32.80 | 98.40 | 113.43 | 171.12 |
| 42 | 187.00 | 24.65 | 24.83 | 25.20 | 33.60 | 100.80 | 116.20 | 175.29 |
| 43 | 191.45 | 25.24 | 25.42 | 25.80 | 34.40 | 103.20 | 118.96 | 179.46 |
| 44 | 195.90 | 25.82 | 26.01 | 26.40 | 35.20 | 105.60 | 121.73 | 183.64 |
| 45 | 200.35 | 26.41 | 26.60 | 27.00 | 36.00 | 108.00 | 124.50 | 187.81 |
| 46 | 204.80 | 27.00 | 27.19 | 27.60 | 36.80 | 110.40 | 127.26 | 191.98 |
| 47 | 209.26 | 27.58 | 27.78 | 28.20 | 37.60 | 112.80 | 130.02 | 196.16 |
| 48 | 213.71 | 28.17 | 28.37 | 28.80 | 38.40 | 115.20 | 132.79 | 200.33 |
| 49 | 218.16 | 28.76 | 28.96 | 29.40 | 39.20 | 117.60 | 135.56 | 204.50 |
| 50 | 222.61 | 29.35 | 29.55 | 30.00 | 40.00 | 120.00 | 138.33 | 208.68 |
| 51 | 227.07 | 29.93 | 30.14 | 30.60 | 40.80 | 122.40 | 141.09 | 212.85 |
| 52 | 231.52 | 30.52 | 30.74 | 31.20 | 41.60 | 124.80 | 143.86 | 217.02 |
| 53 | 235.97 | 31.11 | 31.33 | 31.80 | 42.40 | 127.20 | 146.63 | 221.20 |
| 54 | 240.42 | 31.69 | 31.92 | 32.40 | 43.20 | 129.60 | 149.39 | 225.37 |
| 55 | 244.87 | 32.28 | 32.51 | 33.00 | 44.00 | 132.00 | 152.16 | 229.55 |
| 56 | 249.33 | 32.87 | 33.10 | 33.60 | 44.80 | 134.40 | 154.93 | 233.72 |
| 57 | 253.78 | 33.45 | 33.69 | 34.20 | 45.60 | 136.80 | 157.69 | 237.69 |
| 58 | 258.23 | 34.04 | 34.28 | 34.80 | 46.40 | 139.20 | 160.46 | 242.67 |
| 59 | 262.68 | 34.63 | 34.87 | 35.40 | 47.20 | 141.60 | 163.23 | 246.24 |
| 60 | 267.14 | 35.21 | 35.46 | 36.00 | 48.00 | 144.00 | 165.99 | 250.41 |

french leagues into different geographical measures of distance.

| $\begin{aligned} & \text { French } \\ & \text { Leagues. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austriau Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Nautical Leagues. $20=10$ $20=1^{\circ} \mathrm{E} 4$. | $\begin{gathered} \text { Geograph1’ } \\ \text { or Nautical } \\ \text { Miles. } \\ 60=1^{\circ} \text { Eq. } \\ \hline \end{gathered}$ | Euglish <br> statute <br> Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 271.59 | 35.80 | 36.06 | 36.60 | 48.80 | 146.40 | 168.76 | 254.59 |
| 62 | 276.04 | 36.39 | 36.65 | 37.20 | 49.60 | 148.80 | 171.53 | 258.76 |
| 63 | 280.49 | 36.98 | 37.24 | 37.80 | 50.40 | 151.20 | 174.29 | 262.93 |
| 64 | 284.94 | 37.56 | 37.83 | 38.40 | 51.20 | 153.60 | 177.06 | 267.11 |
| 65 | 289.40 | 38.15 | 35.42 | 39.00 | 52.00 | 156.00 | 179.83 | 271.28 |
| 66 | 293.85 | 38.74 | 39.01 | 39.60 | 52.80 | 158.40 | 182.59 | 275.45 |
| 67 | 298.30 | 39.32 | 39.60 | 40.20 | 53.60 | 160.80 | 185.36 | 279.63 |
| 68 | 302.75 | 39.91 | 40.19 | 40.80 | 54.40 | 163.20 | 188.13 | 283.80 |
| 69 | 307.21 | 40.50 | 40.78 | 41.40 | 55.20 | 165.60 | 190.69 | 287.97 |
| 70 | 311.66 | 41.08 | 41.38 | 42.00 | 56.00 | 168.00 | 193.66 | 292.15 |
| 71 | 316.11 | 41.67 | 41.97 | 42.60 | 56.80 | 170.40 | 196.43 | 296.32 |
| 72 | 320.56 | 42.26 | 42.56 | 43.20 | 57.60 | 172.80 | 199.19 | 300.50 |
| 73 | 325.02 | 42.84 | 43.15 | 43.80 | 58.40 | 175.20 | 201.96 | 304.67 |
| 74 | 329.47 | 43.43 | 43.74 | 44.40 | 59.20 | 177.60 | 204.73 | 308.84 |
| 75 | 333.92 | 44.02 | 44.33 | 45.00 | 60.00 | 180.00 | 207.49 | 313.02 |
| 76 | 338.37 | 44.61 | 44.92 | 45.60 | 60.80 | 182.40 | 210.26 | 317.19 |
| 77 | 342.82 | 45.19 | 45.51 | 46.20 | 61.60 | 184.80 | 213.03 | 321.36 |
| 78 | 347.28 | 45.78 | 46.10 | 41.80 | 62.40 | 187.20 | 215.79 | 325.54 |
| 79 | 351.73 | 419.37 | 46.69 | 47.40 | 63.20 | 189.60 | 218.56 | 329.71 |
| 80 | 356.18 | 46.95 | 47.29 | 48.00 | 64.00 | 192.00 | 221.32 | 333.88 |
| 81 | 360.63 | 47.54 | 47.88 | 48.60 | 64.80 | 194.40 | 224.09 | $338.00^{2}$ |
| 82 | 36509 | 48.13 | 48.47 | 49.20 | 65.60 | 196.80 | 226.86 | 342.23 |
| 83 | 369.54 | 45.71 | 49.06 | 49.80 | 66.40 | 199.20 | 229.62 | 346.40 |
| 84 | 373.99 | 49.30 | 49.65 | 50.40 | 67.20 | 201.60 | 232.39 | 350.58 |
| 85 | 378.44 | 49.89 | 50.24 | 51.00 | 68.00 | 204.00 | 235.16 | 354.75 |
| 86 | 382.89 | 50.47 | 50.83 | 51.60 | 68.80 | 206.40 | 237.92 | 358.93 |
| s7 | 387.35 | 51.06 | 51.42 | 52.20 | 69.60 | 208.80 | 240.69 | 363.10 |
| 88 | 391.80 | 51.65 | 52.01 | 52.80 | 70.40 | 211.20 | 243.46 | 367.27 |
| 89 | 396.25 | 52.24 | 52.61 | 53.40 | 71.20 | 213.60 | 246.22 | 371.45 |
| 90 | 400.70 | 52.82 | 53.20 | 54.00 | 72.00 | 216.00 | 248.99 | 375.62 |
| 91 | 405.16 | 53.41 | 53.79 | 54.60 | 72.80 | 218.40 | 251.76 | 379.79 |
| 92 | 409.61 | 54.00 | 54.38 | 55.20 | 73.60 | 220.80 | 254.52 | 383.97 |
| 93 | 414.06 | 54.58 | 54.97 | 55.80 | 74.40 | 223.20 | 257.29 | 388.14 |
| 94 | 418.51 | 55.17 | 55.56 | 56.40 | 75.20 | 225.60 | 260.06 | 392.31 |
| 95 | 422.96 | 55.76 | 56.15 | 57.00 | 76.00 | 228.40 | 262.82 | 396.49 |
| 96 | 427.42 | $56 . \dot{3} 4$ | 56.74 | 57.60 | 76.80 | 230.40 | 265.59 | 400.66 |
| 97 | 431.57 | 56.93 | 57.33 | 58.20 | 77.60 | 232.80 | 268.36 | 404.83 |
| 98 | 436.32 | 57.52 | 57.93 | 58.80 | 78.40 | 235.20 | 271.12 | 409.01 |
| 99 | 440.77 | 58.10 | 58.52 | 59.40 | 79.20 | 237.60 | 273.89 | 413.18 |
| 100 | 445.23 | 58.69 | 59.11 | 60.00 | 80.00 | 240.00 | 276.66 | 417.36 |

VII. aeographical or nautical miles into different geographical measures of distange.

| Geographical Miles. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \mathbf{E}_{\mathrm{I}} . \end{gathered}$ | Nautical Leagues. $20=10 \mathrm{Eq}$ $20=1^{\circ} \mathrm{Eq}$. | FrenchLeagues. <br> $25=10$ $25=1^{\circ} \mathrm{Eq}$ | English Statute Miles. | Russian <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 1855.11 | 244.55 | 246.28 | 250.00 | 333.33 | 416.67 | 1152.73 | 1738.98 |
| 2,000 | 3710.22 | 489.09 | 492.56 | 500.00 | 666.67 | 833.33 | 2305.47 | 3477.96 |
| 3,000 | 5565.33 | 733.64 | 738.84 | 750.00 | 1000.00 | 1250.00 | 3458.20 | 5216.94 |
| 4,000 | 7420.44 | 978.18 | 985.13 | 1000.00 | 1333.33 | 1666.67 | 4610.93 | 6955.92 |
| 5,000 | 9275.55 | 1202.73 | 1231.41 | 1250.00 | 1666.67 | 2083.33 | 5763.66 | 8694.90 |
| 6,000 | 11130.66 | 1467.28 | 1477.69 | 1500.00 | 2000.00 | 2500.00 | 6916.40 | 10433.88 |
| 7,000 | 12985.77 | 1711.82 | 1783.97 | 1750.00 | 2333.33 | 2916.67 | 8069.13 | 12172.86 |
| 8,000 | 14840.88 | 1956.37 | 1970.25 | 2000.00 | 2666.67 | 3333.33 | 9221.66 | 13911.83 |
| 9,000 | 16695.99 | 2200.91 | 2216.53 | 2250.00 | 3000.00 | 3750.00 | 10374.59 | 15650.81 |
| 10,000 | 18551.10 | 2445.46 | 2462.81 | 2500.00 | 3333.33 | 4166.67 | 11527.33 | 17389.79 |
| 100 | 185.51 | 24.45 | 24.63 | 25.00 | 33.33 | 41.67 | 115.27 | 173.90 |
| 200 | 371.02 | 48.91 | 49.26 | 50.00 | 66.67 | 83.33 | 230.55 | 347.80 |
| 300 | 556.53 | 73.36 | 73.88 | 75.00 | 100.00 | 125.00 | 345.82 | 521.69 |
| 400 | 742.04 | 97.82 | 98.51 | 100.00 | 133.33 | 166.67 | 461.09 | 695.59 |
| 500 | 927.56 | 122.27 | 123.14 | 125.00 | 166.67 | 208.33 | 576.37 | 869.49 |
| 600 | 1113.07 | 146.73 | 147.77 | 150.00 | 200.00 | 250.00 | 691.64 | 10.43 .39 |
| 700 | 1298.58 | 171.18 | 172.40 | 175.00 | 233.33 | 291.67 | 806.91 | 1217.29 |
| 800 | 1484.09 | 195.64 | 197.03 | 200.00 | 266.67 | 333.33 | 922.19 | 1391.18 |
| 900 | 1669.60 | 220.09 | 221.65 | 225.00 | 300.00 | 375.00 | 1037.46 | 1565.08 |
| 1000 | 1855.11 | 244:55 | 246.28 | 250.00 | 333.33 | 410.67 | 1152.73 | 1738.98 |
| 1 | 1.86 | 0.24 | 0.25 | 0.25 | 0.33 | 0.42 | 1.15 | 1.74 |
| 2 | 3.71 | 0.49 | 0.49 | 0.50 | 0.67 | 0.83 | 2.31 | 3.48 |
| 3 | 5.57 | 0.73 | 0.74 | 0.75 | 1.00 | 1.25 | 3.46 | 5.22 |
| 4 | 7.42 | 0.98 | 0.99 | 1.00 | 1.33 | 1.67 | 4.61 | 6.96 |
| 5 | 9.28 | 1.22 | 1.23 | 1.25 | 1.67 | 2.08 | 5.76 | 8.69 |
| 6 | 11.13 | 1.47 | 1.48 | 1.50 | 2.00 | 2.50 | 6.92 | 10.43 |
| 7 | 12.99 | 1.71 | 1.72 | 1.75 | 2.33 | 2.92 | 8.07 | 12.17 |
| 8 | 14.84 | 1.96 | 1.97 | 2.00 | 2.67 | 3.33 | 9.22 | 13.91 |
| 9 | 16.70 | 2.20 | 2.22 | 2.25 | 3.00 | 3.75 | 10.37 | 15.65 |
| 10 | 18.55 | 2.45 | 2.46 | 2.50 | 3.33 | 4.17 | 11.53 | 17.39 |
| 11 | 20.41 | 2.69 | 2.71 | 2.75 | 3.67 | 4.58 | 12.68 | 19.13 |
| 12 | 22.26 | 2.93 | 2.96 | 3.01 | 4.00 | 5.00 | 13.83 | 20.87 |
| 13 | 24.12 | 3.18 | 3.20 | 3.25 | 4.33 | 5.42 | 14.99 | 22.61 |
| 14 | 25.97 | 3.42 | 3.45 | 3.50 | 4.67 | 5.83 | 16.14 | 24.35 |
| 15 | 27.83 | 3.67 | 3.69 | 3.75 | 5.00 | 6.25 | 17.29 | 26.08 |
| 16 | 29.68 | 3.91 | 3.94 | 4.00 | 5.33 | 6.67 | 18.44 | 27.82 |
| 17 | 31.54 | 4.16 | 4.19 | 4.25 | 5.67 | 7.08 | 19.60 | 29.56 |
| 18 | 33.39 | 4.40 | 4.43 | 4.50 | 6.00 | 7.50 | 20.75 | 31.30 |
| 19 | 35.25 | 4.65 | 4.68 | 4.75 | 6.33 | 7.97 | 21.90 | 33.04 |
| 20 | 37.10 | 4.89 | 4.93 | 5.00 | 6.67 | 8.33 | 23.05 | 34.78 |

Gevgraphical or nautical miles intu different geographical measures of DISTANCE.

| Geogralhical Miles. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Mile } \\ 15=1^{\circ} \text { Eq. } \end{gathered}$ | Nautical Leagues. $20=1^{\circ} \mathrm{E}_{1}$. | $\begin{gathered} \text { Freuch } \\ \text { Leataes. } \\ 2 \bar{j}=1^{\circ} \mathrm{Eq} . \end{gathered}$ | English Scatute Miles. | $\begin{aligned} & \text { Russian } \\ & \text { Wersts. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 38.96 | 5.14 | 5.17 | 5.25 | 7.00 | 8.75 | 24.21 | 36.52 |
| 22 | 40.81 | 5.38 | 5.42 | 5.50 | 7.33 | 9.17 | 25.36 | 35.26 |
| 23 | 42.67 | 5.62 | 5.66 | 5.75 | 7.67 | 9.58 | 26.51 | 40.00 |
| -4 | 44.52 | 5.87 | 5.91 | 6.00 | 8.00 | 10.00 | 27.67 | 41.74 |
| 25 | 46.38 | 6.11 | 6.16 | 6.25 | 8.33 | 10.42 | 28.82 | 43.47 |
| 26 | 48.23 | 6.36 | 6.40 | 6.50 | 8.67 | 10.83 | 29.97 | 4.51 |
| 27 | 50.09 | 6.60 | 6.65 | 6.75 | 9.00 | 11.25 | 31.12 | 46.95 |
| 28 | 51.94 | (6. 5.5 | 6.90 | 7.00 | 9.33 | 11.67 | 32.28 | 48.69 |
| 29 | 53.80 | 7.09 | 7.14 | 7.25 | 9.67 | 12.08 | 33.43 | 50.43 |
| 30 | 55.65 | 7.34 | 7.39 | 7.50 | 10.00 | 12.41 | 34.58 | 52.17 |
| 31 | 57.51 | 7.58 | 7.63 | 7.75 | 10.33 | 12.92 | 35.73 | 53.91 |
| 32 | 59.36 | 7.83 | 7.88 | 8.100 | 10.67 | 13.33 | 36.85 | 55.65 |
| 33 | 61.22 | 8.07 | 8.13 | 8.25 | 11.00 | 13.75 | 38.04 | 57.39 |
| 34 | 63.67 | 8.31 | 8.37 | 8.50 | 11.33 | 14.17 | 39.19 | 59.13 |
| 35 | 64.93 | 8.56 | 8.62 | 8.75 | 11.67 | 14.58 | 40.35 | 60.86 |
| 36 | 66.78 | 8.80 | 8.87 | 9.00 | 12.00 | 15.00 | 41.50 | 62.60 |
| 37 | 68.64 | 9.05 | 9.11 | 9.25 | 12.33 | 15.42 | 42.65 | 64.34 |
| 38 | 70.49 | 9.24 | 9.36 | 9.50 | 12.67 | 15.83 | 43.80 | 66.08 |
| 39 | 72.35 | 9.54 | 9.60 | 9.75 | 13.00 | 16.25 | 4.96 | 67. 2 |
| 40 | 74.20 | 9.78 | 9.85 | 10.00 | 13.33 | 16.67 | 46.11 | 69.56 |
| 41 | 76.06 | 10.03 | 10.10 | 10.25 | 13.67 | 17.08 | 47.26 | 71.30 |
| 42 | 77.91 | 10.27 | 10.34 | 10.50 | 14.00 | 17.49 | 48.41 | 73.04 |
| 43 | 79.77 | 10.52 | 10.59 | 10.75 | 14.33 | 17.92 | 49.57 | 74.78 |
| 44 | 81.62 | 10.76 | 10.84 | 11.00 | 14.67 | 18.33 | 50.72 | 76.52 |
| 45 | 83.48 | 11.00 | 11.08 | 11.25 | 15.00 | 18.75 | 51.87 | 78.25 |
| 46 | 85.34 | 11.25 | 11.33 | 11.50 | 15.33 | 19.17 | 53.03 | 79.99 |
| 47 | 87.19 | 11.49 | 11.58 | 11.75 | 15.67 | 19.58 | 54.18 | 81.73 |
| 48 | 89.05 | 11.74 | 11.82 | 12.00 | 16.00 | 20.00 | 55.33 | 83.47 |
| 49 | 90.90 | 11.98 | 12.07 | 12.25 | 16.33 | 20.42 | 56.48 | 85.21 |
| 50 | 92.76 | 12.23 | 12.31 | 12.50 | 16.67 | 20.83 | 57.64 | 86.95 |
| 51 | 94.61 | 12.47 | 12.56 | 12.75 | 17.00 | 21.25 | 58.79 | 88.69 |
| 52 | 96.47 | 12.72 | 12.81 | 13.00 | 17.33 | 21.67 | 59.94 | 90.43 |
| 53 | 98.32 | 12.96 | 13.05 | 13.25 | 17.67 | 22.108 | 61.09 | 92.17 |
| 54 | 100.18 | 13.21 | 13.30 | 13.50 | 18.00 | 22.50 | 62.25 | 93.90 |
| 55 | 102.03 | 13.45 | 13.55 | 13.75 | 18.33 | 22.92 | 63.40 | 95.64 |
| 56 | 103.89 | 13.69 | 13.79 | 14.00 | 18.67 | 23.33 | 64.55 | 97.38 |
| 57 | 105.74 | 13.94 | 14.04 | 14.25 | 19.00 | 23.75 | 65.71 | 99.12 |
| 58 | 107.60 | 14.18 | 14.28 | 14.50 | 19.33 | 24.17 | 66.86 | 100.86 |
| 59 | 109.45 | 14.43 | 14.53 | 14.75 | 19.67 | 24.58 | 68.01 | 102.60 |
| 60 | 111.31 | 14.67 | 14.78 | 15.00 | 20.00 | 25.00 | 69.16 | 104.34 |

geograpilical or nautical miles intu different geographical measurfs of Distance.

| Geographical miles. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \dot{E}_{1} . \end{gathered}$ | $\begin{aligned} & \text { Nautical } \\ & \text { Learatas. } \\ & 20=10 \text { Eq. } \end{aligned}$ | $\begin{aligned} & \text { French } \\ & \text { Leatues. } \\ & 2.5=1^{0} \text { Eq. } \end{aligned}$ | English <br> statute <br> Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 113.16 | 14.92 | 15.02 | 15.25 | 20.33 | 25.42 | 70.32 | 106.08 |
| 62 | 115.02 | 15.16 | 15.27 | 15.50 | 20.67 | 25.83 | 71.47 | 107.82 |
| 63 | 116.87 | 15.41 | 15.52 | 15.75 | 21.00 | 26.25 | 72.62 | 109.56 |
| 64 | 118.73 | 15.65 | 15.76 | 16.00 | 21.33 | 26.67 | 73.77 | 111.29 |
| 65 | 120.5 s | 15.90 | 16.01 | 16.25 | 21.67 | 27.08 | 74.93 | 113.03 |
| 66 | 122.44 | 16.14 | 16.25 | 16.50 | 22.00 | 27.50 | 76.17 | 114.77 |
| 67 | 124.29 | 16.38 | 16.50 | 16.75 | 22.33 | 27.92 | 77.23 | 116.51 |
| 68 | 126.15 | 16.63 | 16.75 | 17.00 | 22.67 | 28.33 | 78.39 | 118.25 |
| 69 | 128.00 | 16.87 | 16.99 | 17.25 | 23.00 | 28.75 | 79.54 | 119.99 |
| 70 | 129.86 | 17.12 | 17.24 | 17.50 | 23.33 | 29.17 | 80.69 | 121.73 |
| 71 | 131.71 | 17.36 | 17.49 | 17.75 | 23.67 | 29.58 | 81.84 | 123.47 |
| 72 | 133.57 | 17.61 | 17.73 | 18.00 | 24.00 | 30.00 | 83.00 | 125.21 |
| 73 | 135.42 | 17.85 | 17.98 | 18.25 | 24.33 | 30.42 | 84.15 | 126.95 |
| 74 | 137.28 | 18.10 | 18.22 | 18.50 | 24.67 | 30.83 | 85.30 | 128.68 |
| 75 | 139.13 | 18.34 | 18.47 | 18.75 | 25.00 | 31.25 | 86.46 | 130.42 |
| 76 | 140.99 | 18.59 | 18.72 | 19.00 | 25.33 | 31.67 | 87.61 | 132.16 |
| 77 | 142.84 | 18.83 | 18.96 | 19.25 | 25.67 | 32.08 | 88.76 | 133.90 |
| 78 | 144.70 | 19.07 | 19.21 | 19.50 | 26.00 | 32.50 | 89.91 | 135.64 |
| 79 | 146.55 | 19.32 | 19.46 | 19.75 | 26.33 | 32.82 | 91.07 | 137.38 |
| 80 | 148.41 | 19.56 | 19.70 | 20.00 | 26.67 | 33.33 | 92.29 | 139.12 |
| 81 | 150.26 | 19.81 | 19.95 | 20.25 | 27.00 | 33.75 | 93.37 | 140.86 |
| 82 | 152.12 | 20.05 | 20.20 | 20.50 | 27.33 | 34.17 | 94.52 | 142.60 |
| 83 | 153.97 | 20.30 | 20.44 | 20.75 | 27.67 | 34.58 | 05.68 | 144.34 |
| 84 | 155.83 | 20.54 | 20.69 | 21.00 | 28.00 | 35.00 | 96.83 | 146.07 |
| 85 | 157.68 | 20.79 | 20.93 | 21.25 | 28.33 | 35.42 | 97.98 | 147.81 |
| 86 | 159.54 | 21.03 | 21.18 | 21.50 | 28.67 | 35.83 | 99.13 | 149.55 |
| 87 | 161.39 | 21.28 | 21.43 | 21.75 | 29.00 | 36.25 | 100.29 | 151.89 |
| 88 | 163.25 | 21.52 | 21.67 | 22.00 | 29.33 | 36.67 | 101.44 | 153.03 |
| 89 | 165.10 | 21.76 | 21.92 | 22.25 | 29.67 | 37.08 | 102.59 | 154.77 |
| 90 | 166.96 | 22.01 | 22.17 | 22.50 | 30.00 | 37.50 | 103.75 | 156.51 |
| 91 | 168.82 | 22.25 | 22.41 | 22.75 | 30.33 | 37.92 | 104.90 | 158.25 |
| 92 | 170.67 | 22.50 | 23.66 | 23.00 | 30.67 | 38.33 | 106.05 | 159.99 |
| 93 | 172.53 | 22.74 | 22.90 | 23.25 | 31.00 | 38.75 | 107.20 | 1161.73 |
| 94 | 174.38 | 22.99 | 23.15 | 23.50 | 31.33 | 39.17 | 108.36 | 163.46 |
| 95 | 176.24 | 23.23 | 23.40 | 23.75 | 31.67 | 39.58 | 109.51 | 165.20 |
| 96 | 178.09 | 23.48 | 23.64 | 24.00 | 32.00 | 40.00 | 110.66 | 166.94 |
| 97 | 179.95 | 23.72 | 23.89 | 24.25 | 32.33 | 40.42 | 111.82 | 168.68 |
| 98 | 181.80 | 23.97 | 24.14 | 24.50 | 32.67 | 40.83 | 112.97 | 170.42 |
| 99 | 183.66 | 24.21 | 24.38 | 24.75 | 33.00 | 41.25 | 114.12 | 172.17 |
| 100 | 185.51 | 24.45 | 24.63 | 25.00 | 33.33 | 41.67 | 115.27 | 173.90 |

VIII. english statute miles into different qeograpiital measures of DISTANCE

| English <br> statute <br> Miles. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \text { Eq. } \end{gathered}$ | $\begin{aligned} & \text { Nautical } \\ & \text { Learues. } \\ & 20=1^{\circ} \mathbf{E q}_{1} . \end{aligned}$ | $\begin{gathered} \text { French } \\ \text { Leagues. } \\ 2=1^{\circ} \text { Eq. } \end{gathered}$ | Geograph'l or Nautical Miles. $60=1^{\circ} \mathrm{E}_{4}$. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 1609.31 | 212.14 | 213.65 | 216.88 | 289.17 | 361.46 | 867.50 | 1508.57 |
| 2,000 | 3218.63 | 424.29 | 427.30 | 433.75 | 578.34 | 722.92 | 1735.01 | 3017.14 |
| 3,000 | 4827.94 | 636.43 | 640.95 | 650.63 | 867.50 | 1084.38 | 2602.51 | 4525.71 |
| 4,000 | 6437.26 | 848.58 | 854.60 | 867.50 | 1156.67 | 1445.84 | 3470.02 | 6034.29 |
| 5,000 | 5046.57 | 1060.72 | 1068.25 | 1084.38 | 1445.84 | 1807.30 | 4337.52 | 7542.86 |
| 6,000 | 9655.89 | 1272.87 | 1281.90 | 1301.26 | 1735.01 | 2168.76 | 5205.02 | 9051.43 |
| 7,000 | 11265.20 | 1485.01 | 1495.55 | 1518.13 | 2024.18 | 2530.22 | 6072.53 | 10560.00 |
| 8,000 | 12874.52 | 1697.16 | 1709.20 | 1735.01 | 2313.34 | 2891.68 | 6940.03 | 12068.57 |
| 9,000 | 14483.83 | 1909.30 | 1922.85 | 1951.88 | 2602.51 | 32.53 .14 | 7807.54 | 13577.14 |
| 10,000 | 16093.15 | 2121.45 | 2136.50 | 2168.76 | 2891.68 | 3614.60 | 8675.04 | 15085.71 |
| 100 | 160.93 | 21.21 | 21.36 | 21.69 | 28.92 | 36.15 | 86.75 | 150.86 |
| 200 | 321. 56 | 42.43 | 42.73 | 43.38 | 57.83 | 72.29 | 173.50 | 301.71 |
| 300 | 482.79 | 63.64 | 64.09 | 65.06 | 86.75 | 108.44 | 260.95 | 452.57 |
| 400 | 64.3 .73 | 84.86 | 85.46 | 86.75 | 115.67 | 144.58 | 347.00 | 603.43 |
| 500 | 804.66 | 106.07 | 106.82 | 108.44 | 14.58 | 180.73 | 433.75 | 754.29 |
| 600 | 965.59 | 127.29 | 128.19 | 130.13 | 173.50 | 216.88 | 520.50 | 905.14 |
| 700 | 1126.52 | 148.50 | 149.55 | 151.81 | 202.4: | 253.112 | 607.25 | 1056.00 |
| 800 | 1247.45 | 169.72 | 170.92 | 173.50 | 231.33 | 289.17 | 694.00 | 1206.86 |
| 900 | 1448.38 | 190.93 | 192.28 | 195.19 | 260.25 | 325.31 | 780.75 | 1357.71 |
| 1000 | 1609.31 | 212.14 | 213.65 | 216.88 | 289.17 | 361.46 | 867.50 | 1508.57 |
| 1 | 1.61 | 0.21 | 0.21 | 0.22 | 0.29 | 0.36 | 0.87 | 1.51 |
| 2 | 3.22 | 0.42 | 0.43 | 0.43 | 0.58 | 0.72 | 1.74 | 3.02 |
| 3 | 4.83 | 0.64 | 0.64 | 0.65 | 0.87 | 1.08 | 2.60 | 4.53 |
| 4 | 6.44 | 0.85 | 0.85 | 0.87 | $1.16^{\circ}$ | 1.45 | 3.47 | 6.03 |
| 5 | 8.05 | 1.06 | 1.07 | 1.08 | 1.45 | 1.81 | 4.34 | 7.54 |
| 6 | 9.66 | 1.27 | 1.28 | 1.30 | 1.74 | 2.17 | 5.21 | 9.05 |
| 7 | 11.27 | 1.49 | 1.50 | 1.52 | 2.02 | 2.53 | 6.07 | 10.56 |
| 8 | 12.57 | 1.70 | 1.71 | 1.74 | 2.31 | 2.89 | 6.94 | 12.07 |
| 9 | 14.48 | 1.91 | 1.92 | 1.95 | 2.60 | 3.25 | 7.81 | 13.58 |
| 10 | 16.09 | 2.12 | 2.14 | 2.17 | 2.89 | 3.61 | 8.68 | 15.09 |
| 11 | 17.70 | 2.33 | 2.35 | 2.39 | 3.18 | 3.98 | 9.54 | 16.59 |
| 12 | 19.31 | 2.55 | 2.56 | 2.60 | 3.47 | 4.34 | 10.41 | 18.10 |
| 13 | 20.92 | 2.76 | 2.78 | 2.82 | 3.76 | 4.70 | 11.28 | 19.61 |
| 14 | 22.53 | 2.97 | 2.99 | 3.04 | 4.05 | 5.06 | 12.15 | 21.12 |
| 15 | 24.14 | 3.18 | 3.20 | 3.25 | 4.34 | 5.42 | 13.01 | 22.63 |
| 16 | 25.75 | 3.39 | 3.42 | 3.47 | 4.63 | 5.78 | 13.88 | 24.14 |
| 17 | 27.36 | 3.61 | 3.63 | 3.69 | 4.92 | 6.14 | 14.75 | 25.65 |
| 18 | 28.97 | 3.82 | 3.85 | 3.90 | 5.21 | 6.51 | 15.62 | 27.15 |
| 19 | 30.57 | 4.03 | 4.06 | 4.12 | 5.49 | 6.87 | 16.48 | 28.66 |
| 20 | 32.19 | 4.24 | 4.27 | 4.34 | 5.78 | 7.23 | 17.35 | 30.17 |

ENGLISH STATU'TE MILES INTO DIFFERENT GEOGRAPHICAL MEASURES OF DISTANCE.

| English Statute Miles. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \text { Eq. } \end{gathered}$ | $\begin{gathered} \text { Nautical } \\ \text { Learoes. } \\ 20=1^{\circ} \mathrm{Eq} . \end{gathered}$ | $\begin{gathered} \text { French } \\ \text { Leatarues. } \\ 25=1 \cup \mathrm{E}_{4} . \end{gathered}$ | Gengrapt'l or Nautical Miles. $60=1^{\circ} \mathrm{Eq}$. | $\begin{aligned} & \text { Russian } \\ & \text { Wersts. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 33.80 | 4.46 | 4.49 | 4.55 | 6.07 | 7.59 | 18.22 | 31.68 |
| 22 | 35.40 | 4.67 | 4.70 | 4.77 | 6.36 | 7.95 | 19.09 | 33.19 |
| 23 | 37.01 | 4.88 | 4.91 | 4.99 | 6.65 | 8.31 | 19.95 | 34.70 |
| 24 | 38.62 | 5.09 | 5.13 | 5.21 | 6.94 | 8.68 | 20.82 | 36.21 |
| 25 | 40.83 | 5.30 | 5.34 | 5.42 | 7.23 | 9.04 | 21.69 | 37.71 |
| 26 | 41.84 | 5.52 | 5.55 | 5.64 | 7.52 | 9.40 | 22.56 | 39.22 |
| 27 | 43.45 | 5.73 | 5.77 | 5.86 | 7.81 | 9.76 | 23.42 | 40.73 |
| 28 | 45.06 | 5.94 | 5.98 | 6.07 | 8.10 | 10.12 | 24.29 | 42.24 |
| 29 | 46.67 | 6.15 | 6.20 | 6.29 | 8.39 | 10.48 | 25.16 | 43.75 |
| 30 | 48.28 | 6.36 | 6.41 | 6.51 | 8.68 | 10.84 | 26.03 | 45.26 |
| 31 | 49.89 | 6.58 | 6.62 | 6.72 | 8.96 | 11.21 | 26.89 | 46.77 |
| 32 | 51.50 | 6.79 | 6.84 | 6.94 | 9.25 | 11.57 | 27.76 | 48.27 |
| 33 | 53.11 | 7.00 | 7.05 | 7.16 | 9.54 | 11.92 | 28.63 | 49.78 |
| 34 | 54.72 | 7.21 | 7.26 | 7.37 | 9.83 | 12.29 | 29.50 | 51.29 |
| 35 | 56.33 | 7.43 | 7.48 | 7.59 | 10.12 | 12.65 | 30.36 | 52.80 |
| 36 | 57.94 | 7.64 | 7.69 | 7.81 | 10.41 | 13.01 | 31.23 | 54.31 |
| 37 | 59.54 | 7.85 | 7.91 | 8.02 | 10.70 | 13.37 | 32.10 | 55.82 |
| 38 | 61.15 | 8.06 | 8.12 | 8.24 | 10.99 | 13.74 | 32.97 | 57.33 |
| 39 | 62.76 | 8.27 | 8.33 | 8.46 | 11.28 | 14.10 | 33.83 | 58.83 |
| 40 | 64.37 | 8.49 | 8.55 | 8.68 | 11.57 | 14.46 | 34.70 | 60.34 |
| 41 | 65.98 | 8.70 | 8.76 | 8.89 | 11.86 | 14.82 | 35.57 | 61.85 |
| 42 | 67.59 | 8.91 | 8.97 | 9.11 | 12.15 | 15.18 | 36.44 | 63.36 |
| 43 | 69.20 | 9.12 | 9.19 | 9.33 | 12.43 | 15.54 | 37.30 | 64.87 |
| 44 | 70.81 | 9.33 | 9.40 | 9.54 | 12.72 | 15.90 | 38.17 | 66.38 |
| 45 | 72.42 | 9.55 | 9.61 | 9.76 | 13.01 | 16.27 | 39.04 | 67.89 |
| 46 | 74.03 | 9.76 | 9.83 | 9.98 | 13.30 | 16.63 | 39.91 | 69.39 |
| 47 | 75.64 | 9.97 | 10.04 | 10.19 | 13.59 | 16.99 | 40.77 | 70.90 |
| 48 | 77.25 | 10.18 | 10.26 | 10.41 | 13.88 | 17.35 | 41.64 | 72.41 |
| 49 | 78.86 | 10.40 | 10.47 | 10.63 | 14.17 | 17.71 | 42.51 | 73.92 |
| 50 | 80.47 | 10.61 | 10.68 | 10.84 | 14.46 | 18.07 | 43.38 | 75.43 |
| 51 | 82.08 | 10.82 | 10.90 | 11.06 | 14.75 | 18.43 | 44.24 | 76.94 |
| 52 | 83.68 | 11.03 | 11.11 | 11.28 | 15.04 | 18.80 | 45.11 | 78.45 |
| 53 | 85.29 | 11.24 | 11.32 | 11.49 | 15.33 | 19.16 | 45.98 | 79.95 |
| 54 | 86.90 | 11.46 | 11.54 | 11.71 | 15.62 | 19.52 | 46.85 | 81.46 |
| 55 | 88.51 | 11.67 | 11.75 | 11.93 | 15.90 | 19.88 | 47.71 | 82.97 |
| 56 | 90.12 | 11.88 | 11.96 | 12.15 | 16.19 | 20.24 | 48.58 | 84.48 |
| 57 | 91.73 | 12.09 | 12.18 | 12.36 | 16.48 | 20.60 | 49.45 | 85.99 |
| 58 | 93.34 | 12.30 | 12.39 | 12.58 | 16.77 | 20.96 | 50.32 | 87.50 |
| 59 | 94.95 | 12.52 | 12.61 | 12.80 | 17.06 | 21.33 | 51.18 | 89.01 |
| 60 | 96.56 | 12.73 | 12.82 | 13.01 | 17.35 | 21.69 | 52.05 | 90.51 |

ENGLISII STATUTE MLES INTO DIFFERENT GEGGRAPHICAL MEASURES OF DISTANCE.

| English Statute Miles. | $\begin{gathered} \text { Kilo- } \\ \text { metres. } \end{gathered}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Myles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} E_{4} . \end{gathered}$ | $\begin{aligned} & \text { Nantical } \\ & \text { Learanes. } \\ & 20=10 \mathrm{Eq.} \end{aligned}$ | $\begin{gathered} \text { Frencl } \\ \text { Lastaes. } \\ 2 \overline{5}=1^{\circ} \mathrm{Eq}_{\mathrm{f}} . \end{gathered}$ |  | $\begin{aligned} & \text { Russian } \\ & \text { Wersts. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 98.17 | 12.94 | 13.03 | 13.23 | 17.64 | 22.45 | 52.92 | 92.12 |
| 62 | 99.78 | 13.15 | 13.25 | 13.45 | 17.93 | 22.41 | 53.79 | 93.53 |
| 63 | 101.39 | 13.37 | 13.46 | 13.66 | 18.22 | 22.77 | 54.65 | 95.04 |
| 64 | 102.00 | 13.58 | 13.67 | 13.88 | 18.51 | 23.13 | 55.52 | 96.55 |
| (6) | 104.61 | 13.79 | 13.69 | 14.10 | 18.80 | 23.49 | 56.39 | 98.06 |
| 66 | 106.21 | 14.00 | 14.10 | 14.31 | 19.09 | 23.86 | 57.26 | 99.57 |
| 67 | 107.82 | 14.21 | 14.31 | 14.53 | 19.37 | 24.22 | 58.12 | 101.07 |
| 68 | 104.43 | 14.43 | 14.53 | 14.75 | 19.66 | 24.58 | 58.99 | 102.58 |
| 69 | 111.04 | 14.64 | 14.74 | 14.96 | 19.95 | 24.94 | 59.86 | 104.09 |
| 70 | 112.65 | 14.85 | 14.96 | 15.18 | 20.24 | 25.30 | 60.73 | 105.60 |
| 71 | 114.26 | 15.06 | 15.17 | 15.40 | 20.53 | 25.66 | 61.59 | 107.11 |
| 72 | 115.57 | 15.27 | 15.38 | 15.62 | 20.82 | 26.03 | 62.46 | 108.62 |
| 73 | 117.48 | 15.49 | 15.60 | 15.83 | 21.11 | 26.39 | 63.33 | 110.13 |
| 74 | 119.09 | 15.70 | 15.81 | 16.05 | 21.40 | 26.75 | 64.20 | 111.63 |
| 75 | 120.70 | 15.91 | 16.02 | 16.27 | 21.69 | 27.11 | 65.06 | 113.14 |
| 76 | 12.31 | 16.12 | 16.24 | 16.48 | 21.98 | 27.47 | 65.93 | 114.65 |
| 77 | 123.92 | 16.34 | 16.45 | 16.70 | 22.27 | 27.83 | 66.80 | 116.16 |
| 78 | 125.53 | 16.55 | 16.66 | 16.92 | 22.56 | 29.19 | 67.67 | 117.67 |
| 79 | 127.14 | 16.76 | 16.88 | 17.13 | 22.84 | 28.56 | 68.53 | 119.18 |
| 80 | 128.75 | 16.97 | 17.09 | 17.35 | 23.13 | 28.92 | 69.40 | 120.69 |
| 81 | 130.35 | 17.18 | 17.31 | 17.57 | 23.42 | 29.28 | 70.27 | 122.19 |
| 82 | 131.96 | 17.40 | 17.52 | 17.78 | 23.71 | 29.64 | 71.14 | 123.70 |
| 83 | 133.57 | 17.61 | 17.73 | 18.00 | 24.00 | 30.00 | 72.00 | 125.21 |
| 84 | 135.18 | 17.82 | 17.95 | 18.22 | 24.29 | 30.36 | 72.87 | 126.72 |
| 85 | 136.79 | 18.03 | 18.16 | 18.43 | 24.58 | 30.72 | 73.74 | 128.23 |
| 86 | 138.40 | 18.24 | 18.37 | 18.65 | 24.87 | 31.09 | 74.61 | 129.74 |
| 87 | 140.01 | 15.46 | 18.59 | 18.87 | 25.16 | 31.46 | 75.47 | 131.25 |
| 88 | 141.62 | 18.67 | 18.80 | 19.09 | 25.45 | 31.82 | 76.34 | 132.75 |
| 89 | 143.23 | 18.88 | 19.01 | 19.30 | 25.74 | 32.18 | 77.21 | 184.26 |
| 90 | 144.84 | 19.09 | 19.23 | 19.52 | 26.03 | 32.53 | 78.08 | 135.77 |
| 91 | 146.45 | 19.31 | 19.44 | 19.74 | 26.31 | 32.59 | 78.94 | 137.28 |
| 92 | 148.06 | 19.52 | 19.66 | 19.95 | 26.60 | 33.25 | 79.81 | 138.79 |
| 93 | 149.67 | 19.73 | 19.87 | 20.17 | 26.59 | 33.82 | 80.68 | 140.30 |
| 94 | 151.28 | 19.94 | 20.08 | 20.39 | 27.18 | 34.18 | 81.55 | 141.81 |
| 95 | 152.88 | 20.15 | 20.30 | 20.60 | 27.47 | 34.54 | 82.41 | 143.31 |
| 96 | 154.49 | 20.37 | 21.51 | 20.82 | 27.76 | 34.90 | 83.28 | 144.82 |
| 97 | 156.10 | 20.58 | 21.72 | 21.04 | 28.05 | 35.26 | 84.15 | 146.33 |
| 98 | 157.71 | 20.79 | 20.94 | 21.25 | 28.34 | 35.62 | 85.02 | 147.84 |
| 99 | 159.32 | 21.00 | 21.15 | 21.47 | 28.63 | 35.98 | 85.88 | 149.35 |
| 100 | 160.93 | 21.21 | 21.36 | 21.69 | 28.12 | 36.15 | 86.75 | 150.86 |

IX. russian wersts into different geographical measures of distance.

| Russian Wersts. | Kilo- | Austrian Miles. | Prussian Miles. | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=I^{\circ} \mathbf{E q} . \end{aligned}$ | Nautical <br> Learues. <br> $20=1^{\circ}$ Eq. | $\begin{gathered} \text { French } \\ \text { Leayues. } \\ 2=1^{0} \text { Eq. } \end{gathered}$ | Geograph'1 <br> or Nautical Miles. $60=1^{\circ} \mathrm{Eq}$. | English Statute Miles. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 1066.78 | 140.63 | 141.62 | 143.76 | 191.68 | 239.60 | 575.05 | 662.88 |
| 2,000 | 2133.56 | 281.25 | 283.25 | 287.53 | 383.37 | 479.21 | 1150.10 | 1325.76 |
| 3,000 | 3200.34 | 421.88 | 424.87 | 431.29 | 575.05 | 718.81 | 1725.15 | 1988.64 |
| 4,000 | 4267.12 | 562.50 | 566.50 | 575.05 | 766.73 | 958.42 | 2300.20 | 2651.52 |
| 5,000 | 5333.90 | 703.13 | 708.12 | 718.81 | 958.42 | 1198.02 | 2875.25 | 3314.39 |
| 6,000 | 6400.68 | 843.76 | 849.74 | 862.58 | 1150.10 | 1437.62 | 3450.30 | 3977.27 |
| 7,000 | 7467.47 | 984.38 | 991.37 | 1006.3 4 | 1341.78 | 1677.23 | 4025.35 | 4640.15 |
| 8,000 | 8534.25 | 1125.01 | 1132.99 | 1150.10 | 1533.47 | 1916.83 | 4600.40 | 5303.03 |
| 9,000 | 9601.03 | 1265.63 | 1274.62 | 1293.86 | 1725.15 | 2156.44 | 5175.45 | 5965.91 |
| 10,000 | 10667.81 | 1406.26 | 1416.24 | 1437.62 | 1916.83 | 2396.04 | 5750.50 | 6628.79 |
| 100 | 106.68 | 14.06 | 14.16 | 14.38 | 19.17 | 23.96 | 57.50 | 66.29 |
| 200 | 213.36 | 28.13 | 28.32 | 28.75 | 38.34 | 47.92 | 115.01 | 132.58 |
| 300 | 320.03 | 42.19 | 42.49 | 43.13 | 57.50 | 71.88 | 172.51 | 198.86 |
| 400 | 426.71 | 56.25 | 56.65 | 57.51 | 76.67 | 95.84 | 230.02 | 265.15 |
| 500 | 533.39 | 70.31 | 70.81 | 71.88 | 95.84 | 119.80 | 287.52 | 331.44 |
| 600 | 640.07 | 84.38 | 84.97 | 86.26 | 115.01 | 143.76 | 345.03 | 397.73 |
| 700 | 746.75 | 98.44 | 99.14 | 100.63 | 134.18 | 167.72 | 402.53 | 464.02 |
| 800 | 853.42 | 112.50 | 113.30 | 115.01 | 153.35 | 191.68 | 460.04 | 530.30 |
| 900 | 960.10 | 126.56 | 127.46 | 129.39 | 172.51 | 215.64 | 517.54 | 596.59 |
| 1000 | 1066.78 | 140.63 | 141.62 | 143.76 | 191.68 | 239.60 | 575.05 | 662.88 |
| 1 | 1.07 | 0.14 | 0.14 | 0.14 | 0.19 | 0.24 | 0.58 | 0.66 |
| 2 | 2.13 | 0.28 | 0.28 | 0.29 | 0.38 | 0.48 | 1.15 | 1.33 |
| 3 | 3.20 | 0.42 | 0.42 | 0.43 | 0.58 | 0.72 | 1.73 | 1.99 |
| 4 | 4.27 | 0.56 | 0.57 | 0.58 | 0.77 | 0.96 | 2.30 | 2.65 |
| 5 | 5.33 | 0.70 | 0.71 | 0.72 | 0.96 | 1.20 | 2.88 | 3.31 |
| 6 | 6.40 | 0.84 | 0.85 | 0.86 | 1.15 | 1.44 | 3.45 | 3.98 |
| 7 | 7.47 | 0.98 | 0.99 | 1.01 | 1.34 | 1.68 | 4.03 | 4.64 |
| 8 | 8.53 | 1.13 | 1.13 | 1.15 | 1.53 | 1.92 | 4.60 | 5.30 |
| 9 | 9.60 | 1.27 | 1.27 | 1.29 | 1.73 | 2.16 | 5.18 | 5.97 |
| 10 | 10.67 | 1.41 | 1.42 | 1.44 | 1.92 | 2.40 | 5.75 | 6.63 |
| 11 | 11.73 | 1.55 | 1.56 | 1.58 | 2.11 | 2.64 | 6.33 | 7.29 |
| 12 | 12.80 | 1.69 | 1.70 | 1.73 | 2.30 | 2.88 | 6.90 | 7.95 |
| 13 | 13.87 | 1.83 | 1.84 | 1.87 | 2.49 | 3.11 | 7.48 | 8.62 |
| 14 | 14.93 | 1.97 | 1.98 | 2.01 | 2.68 | 3.35 | 8.05 | 9.28 |
| 15 | 16.00 | 2.11 | 2.12 | 2.16 | 2.88 | 3.59 | 8.63 | 9.94 |
| 16 | 17.07 | 2.25 | 2.27 | 2.30 | 3.07 | 3.83 | 9.20 | 10.61 |
| 17 | 18.14 | 2.39 | 2.41 | 2.44 | 3.26 | 4.07 | 9.78 | 11.27 |
| 18 | 19.20 | 2.53 | 2.55 | 2.59 | 3.45 | 4.31 | 10.35 | 11.93 |
| 19 | 20.27 | 2.67 | 2.69 | 2.73 | 3.64 | 4.55 | 10.93 | 12.59 |
| 20 | 21.34 | 2.81 | 2.83 | 2.88 | 3.83 | 4.79 | 11.50 | 13.26 |

RUSSIAN WERSTS INTO DIFFERENT GEOGRAPHICAL MEASURES OF DISTANCE.

| Russian Wersts. | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | Prussian Miles. | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical Leagues. $20=10 \mathrm{Eq}$. $20=1^{\circ} \mathrm{Eq}$. | $\begin{gathered} \text { Freuch } \\ \text { Leagues. } \\ 20=1^{\circ} \text { Eq. } \end{gathered}$ | Geograph'l or Niantical Miles. $60=1^{\circ} \mathrm{Eq}$. | English <br> Statute <br> Miles. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 22.40 | 2.95 | 2.97 | 3.02 | 4.03 | 5.03 | 12.08 | 13.92 |
| 22 | 23.47 | 3.09 | 3.12 | 3.16 | 4.22 | 5.27 | 12.65 | 14.58 |
| 23 | 24.54 | 3.23 | 3.26 | 3.31 | 4.41 | 5.51 | 13.23 | 15.25 |
| 24 | 25.60 | 3.38 | 3.40 | 3.45 | 4.60 | 5.75 | 13.80 | 15.91 |
| 25 | 26.67 | 3.52 | 3.54 | 3.59 | 4.79 | 5.99 | 14.38 | 16.57 |
| 26 | 27.74 | 3.66 | 3.68 | 3.74 | 4.98 | 6.23 | 14.95 | 17.23 |
| 27 | 28.80 | 3.80 | 3.82 | 3.88 | 5.18 | 6.47 | 15.53 | 17.90 |
| 28 | 29.87 | 3.94 | 3.97 | 4.03 | 5.37 | 6.71 | 16.10 | 18.56 |
| 29 | 30.94 | 4.08 | 4.11 | 4.17 | 5.56 | 6.95 | 16.68 | 19.22 |
| 30 | 32.00 | 4.22 | 4.25 | 4.31 | 5.75 | 7.19 | 17.25 | 19.89 |
| 31 | 33.07 | 4.36 | 4.39 | 4.46 | 5.94 | 7.43 | 17.83 | 20.55 |
| 32 | 34.14 | 4.50 | 4.53 | 4.60 | 6.13 | 7.67 | 18.40 | 21.21 |
| 33 | 35.20 | 4.64 | 4.67 | 4.74 | 6.33 | 7.91 | 18.98 | 21.88 |
| 34 | 36.27 | 4.78 | 4.82 | 4.89 | 6.52 | 8.15 | 19.55 | 22.54 |
| 35 | 37.34 | 4.92 | 4.90 | 5.03 | 6.71 | 8.39 | 20.13 | 23.20 |
| 36 | 38.40 | 5.06 | 5.10 | 5.18 | 6.90 | 8.63 | 20.70 | 23.86 |
| 37 | 39.47 | 5.20 | 5.24 | 5.32 | 7.09 | 8.87 | 21.28 | 24.53 |
| 38 | 40.54 | 5.34 | 5.38 | 5.46 | 7.28 | 9.10 | 21.85 | 25.19 |
| 39 | 41.60 | 5.48 | 5.52 | 5.61 | 7.48 | 9.34 | 22.43 | 25.85 |
| 40 | 42.67 | 5.63 | 5.66 | 5.75 | 7.67 | 9.58 | 23.00 | 26.52 |
| 41 | 43.74 | 5.77 | 5.81 | 5.89 | 7.86 | 9.82 | 23.58 | 27.18 |
| 42 | 44.80 | 5.91 | 5.95 | 6.04 | 8.05 | 10.06 | 24.15 | 27.84 |
| 43 | 45.87 | 6.05 | 6.09 | 6.18 | 8.24 | 10.30 | 24.73 | 28.50 |
| 44 | 46.94 | 6.19 | 6.23 | 6.33 | 8.43 | 10.54 | 25.30 | 29.17 |
| 45 | 48.01 | 6.33 | 6.37 | 6.47 | 8.63 | 10.78 | 25.88 | 29.83 |
| 46 | 49.07 | 6.47 | 6.51 | 6.61 | 8.52 | 11.02 | 26.45 | 30.49 |
| 47 | 50.14 | 6.61 | 6.66 | 6.76 | 9.01 | 11.26 | 27.03 | 31.16 |
| 48 | 51.21 | 6.75 | 6.80 | 6.90 | 9.20 | 11.50 | 27.60 | 31.82 |
| 49 | 52.27 | 6.89 | 6.94 | 7.04 | 9.39 | 11.74 | 28.18 | 32.48 |
| 50 | 53.34 | 7.03 | 7.08 | 7.19 | 9.58 | 11.98 | 28.75 | 33.14 |
| 51 | 54.41 | 7.17 | 7.22 | 7.33 | 9.78 | 12.22 | 29.33 | 33.81 |
| 52 | 55.47 | 7.31 | 7.36 | 7.45 | 9.97 | 12.46 | 29.90 | 34.47 |
| 53 | 56.54 | 7.45 | 7.51 | 7.62 | 10.16 | 12.70 | 30.48 | 35.13 |
| 54 | 57.61 | 7.59 | 7.65 | 7.76 | 10.35 | 12.94 | 31.05 | 35.80 |
| 55 | 58.67 | 7.73 | 7.79 | 7.91 | 10.54 | 13.18 | 31.63 | 36.46 |
| 56 | 59.74 | 7.88 | 7.93 | 8.05 | 10.73 | 13.42 | 32.20 | 37.12 |
| 57 | 60.81 | 8.02 | 8.07 | 8.19 | 10.93 | 13.66 | 32.78 | 37.78 |
| 58 | 61.87 | 8.16 | 8.21 | 8.34 | 11.12 | 13.90 | 33.35 | 38.45 |
| 59 | 62.94 | 830 | 8.36 | 8.48 | 11.31 | 14.14 | 33.93 | 39.11 |
| 60 | 64.01 | 8.44 | 8.50 | 8.63 | 11.50 | 14.38 | 34.50 | 39.77 |

RUSSIAN Wersts into different geographical measures of distance.

| $\begin{aligned} & \text { Russiau } \\ & \text { Wersts. } \end{aligned}$ | $\begin{aligned} & \text { Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Miles. } \end{aligned}$ | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nantical Leagues. $20=1^{\circ} \mathrm{Eq}$. | French <br> Leasues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical Miles. $60=1^{\circ}$ Eq. | English statute Miles. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 65.07 | 8.58 | 8.64 | 8.77 | 11.69 | 14.62 | 35.08 | 40.44 |
| 62 | 66.14 | 8.72 | 8.78 | 8.91 | 11.88 | 14.86 | 35.65 | 41.10 |
| 63 | 67.21 | 8.86 | 8.92 | 9.06 | 12.08 | 15.10 | 36.23 | 41.76 |
| 64 | 68.27 | 9.00 | 9.06 | 9.20 | 12.27 | 15.33 | 36.80 | 42.42 |
| 65 | 69.34 | 9.14 | 9.21 | 9.34 | 12.46 | 15.57 | 37.38 | 43.09 |
| 66 | 70.41 | 9.28 | 9.35 | 9.49 | 12.65 | 15.81 | 37.95 | 43.75 |
| 67 | 71.47 | 9.42 | 9.49 | 9.63 | 12.84 | 16.05 | 38.53 | 44.41 |
| 68 | 72.54 | 9.56 | 9.63 | 9.78 | 13.03 | 16.29 | 39.10 | 45.08 |
| 69 | 73.61 | 9.70 | 9.77 | 9.92 | 13.23 | 16.53 | 39.68 | 45.74 |
| 70 | 74.67 | 9.84 | 9.91 | 10.06 | 13.42 | 16.77 | 40.25 | 46.40 |
| 71 | 75.74 | 9.98 | 10.06 | 10.21 | 13.61 | 17.01 | 40.83 | 47.06 |
| 72 | 76.81 | 10.12 | 10.20 | 10.35 | 13.80 | 17.25 | 41.40 | 47.73 |
| 73 | 77.87 | 10.27 | 10.34 | 10.49 | 13.99 | 17.49 | 41.98 | 48.39 |
| 74 | 78.94 | 10.41 | 10.48 | 10.64 | 14.18 | 17.73 | 42.55 | 49.05 |
| 75 | 80.01 | 10.55 | 10.62 | 10.78 | 14.38 | 17.97 | 43.13 | 49.72 |
| 76 | 81.08 | 10.69 | 10.76 | 10.93 | 14.57 | 18.21 | 43.70 | 50.38 |
| 77 | 82.14 | 10.83 | 10.91 | 11.07 | 14.76 | 18.45 | 44.28 | 51.04 |
| 78 | 83.21 | 10.97 | 11.05 | 11.21 | 14.95 | 18.69 | 44.85 | 51.70 |
| 79 | 84.28 | 11.11 | 11.19 | 11.36 | 15.14 | 1893 | 45.43 | 52.37 |
| 80 | 85.34 | 11.25 | 11.33 | 11.50 | 15.33 | 19.17 | 46.00 | 53.03 |
| 81 | 86.41 | 11.39 | 11.47 | 11.64 | 15.53 | 19.41 | 46.58 | 53.69 |
| 82 | 87.48 | 11.53 | 11.61 | 11.79 | 15.72 | 19.65 | 47.15 | 54.36 |
| 83 | 88.54 | 11.67 | 11.75 | 11.93 | 15.91 | 19.89 | 47.73 | 55.02 |
| 84 | 89.61 | 11.81 | 11.90 | 12.08 | 16.10 | 20.13 | 48.30 | 55.68 |
| 85 | 90.68 | 11.95 | 12.04 | 12.22 | 16.29 | 20.37 | 48.88 | 56.34 |
| 86 | 91.74 | 12.09 | 12.18 | 12.36 | 16.48 | 20.61 | 49.45 | 57.01 |
| 87 | 92.81 | 12.23 | 12.32 | 12.51 | 16.68 | 20.85 | 50.03 | 57.67 |
| 88 | 93.88 | 12.38 | 12.46 | 12.65 | 16.87 | 21.09 | 50.60 | 58.33 |
| 89 | 94.94 | 12.52 | 12.60 | 12.79 | 17.06 | 21.32 | 51.18 | 59.00 |
| 90 | 96.01 | 12.66 | 12.75 | 12.94 | 17.25 | 21.56 | 51.75 | 59.66 |
| 91 | 97.08 | 12.80 | 12.89 | 13.08 | 17.44 | 21.80 | 52.33 | 60.32 |
| 92 | 98.14 | 12.94 | 13.03 | 13.23 | 17.63 | 22.04 | 52.90 | 60.98 |
| 93 | 99.21 | 13.08 | 13.17 | 13.37 | 17.83 | 22.28 | 53.48 | 61.65 |
| 94 | 100.28 | 13.22 | 13.31 | 13.51 | 18.02 | 22.52 | 54.05 | 62.31 |
| 95 | 101.34 | 13.36 | 13.45 | 13.66 | 18.21 | 22.76 | 54.63 | 62.97 |
| 96 | 102.41 | 13.50 | 13.60 | 13.80 | 18.40 | 23.00 | 55.20 | 63.64 |
| 97 | 103.48 | 13.64 | 13.74 | 13.94 | 18.59 | 23.24 | 55.78 | 64.30 |
| 98 | 104.55 | 13.78 | 13.88 | 14.09 | 18.78 | 23.48 | 56.35 | 64.96 |
| 99 | 105.61 | 13.92 | 14.02 | 14.23 | 18.98 | 23.72 | 56.93 | 65.63 |
| 100 | 106.68 | 14.06 | 14.16 | 14.38 | 19.17 | 23.96 | 57.50 | 66.29 |

X. comparative table of the most important itinerary or linear measures of distances.


## c) TABLES

FOR

COMPARING THE MOST IMPORTANT MEASURES OF GEOGRAPHICAL SURFACES.

## CONTENTS.

(The figures refer to the folio at the bottom of the page.)

TABLES FOR COMPARING TIE MOST IMPORTANT MEASURES OF GEOGRAPIIICAL SURFACES.

Conversion of the different Surface Measures into each other.
Table I. Conversion of Square Kilometres into Austrian Square Miles-
Prussian Square Miles—German Square Miles_Natieal Square
Leagues_French Square Leagues—Geographical Square Miles
" II. Conversion of Austrian Square Miles into Square KilometresPrussian Square Miles_German Square Miles_Nautical Square Leagues_French Square Leagues_Geographical Square Miles —English Square Statute Miles_Russian Square Wersts . 94
" III. Conversion of Prussian Square Miles into Square KilometresAustrian Square Miles-German Square Miles_Nautical Square Leagues_French Square Leagues_Geographical Square Miles -English Square Statute Miles-Russian Square Wersts97
" IV. Conversion of German Square Miles into Square KilometresAustrian Square Miles - Prussian Square Miles - Nautical Square Leagues_French Square Leagues_Geographical Square Miles_English Square Statute Miles_Russian Square Wersts 100
" V. Conversion of Nautical Square Leagues into Square KilometresAustrian Square Miles_Prussian Square Miles_German Square Miles_Freneh Square Leagues_Geographical Square Miles_English Square Statute Miles_Russian Square Wersts 103
" VL. Conversion of French Square Leagues into Square KilometresAustrian Square Miles-Prussian Square Miles_German Square Miles_Nautical Square Leagues-Geographical Square MilesEnglish Square Statute Miles_Russian Square Wersts
" VII. Conversion of Geographical Square Miles into Square Kilometres -Austrian Square Miles_Prussian Square Miles_German Square Miles - Nautical Square Leagnes _ French Square Leagues_-English Square Statute Miles—Russian Square Wersts 109
PAGE
Table VIII. Conversion of English Square Statute Miles into Square Kilo- metres-Austrian Square Miles_Prussian Square Miles_ German Square Miles_Nautical Square Leagues_French Square Leagues - Geographical Square Miles - Russian Square Wersts ..... 112
" IX. Conversion of Russian Square Wersts into Square Kilo-metres_Austrian Square Miles_-Prussian Square Miles-German Square Miles_Nautical Square Leagues_FrenchSquare Leagues - Geographical Square Miles - EnglishSquare Statute Miles115
" X. Table for comparing the most important Measures of Surface . ..... 118
E ..... 90
I. Square kilometres into different geographical square measures.

| Sq. Kilometres. | Austrian Sq. Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Sq. Miles. } \end{aligned}$ | German Sq. Miles. $15=1^{\circ}$ Eq. | $\begin{aligned} & \text { Nautical } \\ & \text { square } \\ & \text { Leagues. } \\ & 20=1^{\circ} \mathrm{Eq} . \end{aligned}$ | $\begin{gathered} \text { French } \\ \text { square } \\ \text { Leagues. } \\ 2 \overline{5}=1^{\circ} \text { Eq. } \end{gathered}$ | Geograph'1 or Nautical Sq. Miles. $60=1^{\circ} \mathrm{E} 4$ | English square Miles. | Russian square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 17.37727 | 17.62477 | 18.16105 | 32.28630 | 50.4473 | 290.5767 | 386.1161 | 878.7183 |
| 2,000 | 34.75454 | 35.24955 | 36.32209 | 64.57261 | 100.8947 | 581.1534 | 772.2323 | 1757.437 |
| 3,000 | 52.13181 | 52.87432 | 54.48314 | 96.85891 | 151.3420 | 871.7302 | 1158.348 | 2636.155 |
| 4,000 | 69.50907 | 70.49910 | 72.64415 | 129.1452 | 201.7894 | 1162.307 | 1544.464 | 3514.873 |
| 5,000 | 86.88634 | 88.12387 | 90.80523 | 161.4315 | 252.2367 | 1452.884 | 1930.581 | 4393.592 |
| 6,000 | 104.2636 | 105.7486 | 108.9663 | 193.7178 | 302.6841 | 1743.460 | 2316.697 | 5272.310 |
| 7,000 | 121.6409 | 123.3734 | 127.1273 | 226.0041 | 353.1314 | 2034.037 | 2702.813 | 6151.028 |
| 8,000 | 139.0181 | 140.9982 | 145.2884 | 258.2904 | 403.5788 | 2324.614 | 3088.929 | 7029.747 |
| 9,000 | 156.3954 | 158.6230 | 163.4494 | 290.5767 | 454.0261 | 2615.191 | 3475.045 | 7908.465 |
| 10,000 | 173.7727 | 176.2477 | 181.6105 | 322.8630 | 504.4735 | 2905.767 | 3861.161 | 5787.183 |
| 100 | 1.74 | 1.76 | 1.82 | 3.23 | 5.04 | 29.06 | 38.61 | 87.87 |
| 200 | 3.48 | 3.52 | 3.63 | 6.46 | 10.09 | 58.12 | 77.22 | 175.74 |
| 300 | 5.21 | 5.29 | 5.45 | 9.69 | 15.13 | 87.17 | 115.83 | 263.62 |
| 400 | 6.95 | 7.05 | 7.26 | 12.91 | 20.18 | 110.23 | 154.45 | 351.49 |
| 500 | 8.69 | 8.81 | 9.08 | 16.14 | 25.22 | 145.29 | 193.06 | 439.36 |
| 600 | 10.43 | 10.57 | 10.90 | 19.37 | 30.27 | 174.35 | 231.67 | 527.23 |
| 700 | 12.16 | 12.34 | 12.71 | 22.60 | 35.31 | 203.40 | 270.28 | 615.10 |
| 800 | 13.90 | 14.10 | 14.53 | 25.83 | 40.36 | 232.46 | 308.89 | 702.97 |
| 900 | 15.64 | 15.86 | 16.34 | 29.06 | 45.40 | 261.52 | 347.50 | 790.85 |
| 1000 | 17.38 | 17.62 | 18.16 | 32.29 | 50.45 | 290.58 | 386.12 | 878.72 |
| 1 | 0.02 | 0.02 | 0.02 | 0.03 | 0.05 | 0.29 | 0.39 | 0.88 |
| 2 | 0.03 | 0.04 | 0.04 | 0.06 | 0.10 | 0.58 | 0.77 | 1.76 |
| 3 | 0.05 | 0.05 | 0.05 | 0.10 | 0.15 | 0.87 | 1.16 | 2.64 |
| 4 | 0.07 | 0.07 | 0.07 | 0.13 | 0.20 | 1.16 | 1.54 | 3.51 |
| 5 | 0.09 | 0.09 | 0.09 | 0.16 | 0.25 | 1.45 | 1.93 | 4.39 |
| 6 | 0.10 | 0.11 | 0.11 | 0.19 | 0.30 | 1.74 | 2.32 | 5.27 |
| 7 | 0.12 | 0.12 | 0.13 | 0.23 | 0.35 | 2.03 | 2.70 | 6.15 |
| 8 | 0.14 | 0.14 | 0.15 | 0.26 | 0.40 | 2.32 | 3.09 | 7.03 |
| 9 | 0.16 | 0.16 | 0.16 | 0.29 | 0.45 | 2.62 | 3.48 | 7.91 |
| 10 | 0.17 | 0.18 | 0.18 | 0.32 | 0.50 | 2.91 | 3.86 | 8.79 |
| 11 | 0.19 | 0.19 | 0.20 | 0.36 | 0.55 | 3.20 | 4.25 | 9.67 |
| 12 | 0.21 | 0.21 | 0.22 | 0.39 | 0.61 | 3.49 | 4.63 | 10.54 |
| 13 | 0.23 | 0.23 | 0.24 | 0.42 | 0.66 | 3.78 | 5.02 | 11.42 |
| 14 | 0.24 | 0.25 | 0.25 | 0.45 | 0.71 | 4.07 | 5.41 | 12.30 |
| 15 | 0.26 | 0.26 | 0.27 | 0.48 | 0.76 | 4.36 | 5.79 | 13.18 |
| 16 | 0.28 | 0.28 | 0.29 | 0.52 | 0.81 | 4.65 | 6.18 | 14.06 |
| 17 | 0.30 | 0.30 | 0.31 | 0.55 | 0.86 | 4.94 | 6.56 | 14.94 |
| 18 | 0.31 | 0.32 | 0.33 | 0.58 | 0.91 | 5.23 | 6.95 | 15.82 |
| 19 | 0.33 | 0.33 | 0.35 | 0.61 | 0.96 | 5.52 | 7.34 | 16.70 |
| 20 | 0.35 | 0.35 | 0.36 | 0.65 | 1.01 | 5.81 | 7.72 | 17.57 |

SQUARE KILOMETRES INTO DIFFEREN'I GEOGRAPIICAL SQUARE MEASURES.

| Sq. Kilometres. | Austrian sy Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { sq. Miles. } \end{aligned}$ | German sq Miles. $15=10 \mathrm{Eq}$. $15=1^{\circ} \mathrm{Eq}$. | Naulical square Leagues. $20=1^{\circ} \mathrm{Eq}$. | French Square Leagues. $25=1^{\circ} \mathrm{E}_{4}$. | Geograph'l <br> or Nautical <br> Sq. Miles. <br> $60=1^{\circ} \mathrm{Eq}$. | Eoglish sycare Miles. | Russian <br> square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 0.36 | 0.37 | 0.38 | 0.68 | 1.06 | 6.10 | 8.11 | 18.45 |
| 22 | 0.38 | 0.39 | 0.40 | 0.71 | 1.11 | 6.39 | 8.49 | 19.33 |
| 23 | 0.40 | 0.41 | 0.42 | 0.74 | 1.16 | 6.68 | 8.88 | 20.21 |
| 24 | 0.42 | 0.42 | 0.44 | 0.77 | 1.21 | 6.97 | 9.27 | 21.09 |
| 25 | 0.43 | 0.44 | 0.45 | 0.81 | 1.26 | 7.26 | 9.65 | 21.97 |
| 26 | 0.45 | 0.46 | 0.47 | 0.84 | - 1.31 | 7.55 | 10.04 | 22.85 |
| 27 | 0.47 | 0.48 | 0.49 | 0.87 | 1.36 | 7.85 | 10.43 | 23.73 |
| 28 | 0.49 | 0.49 | 0.51 | 0.91 | 1.41 | 8.14 | 10.81 | 24.60 |
| 29 | 0.50 | 0.51 | 0.53 | 0.94 | 1.46 | 8.43 | 11.20 | 25.48 |
| 30 | 0.52 | 0.53 | 0.54 | 0.97 | 1.51 | 8.72 | 11.58 | 26.36 |
| 31 | 0.54 | 0.55 | 0.56 | 1.00 | 1.56 | 9.01 | 11.97 | 27.24 |
| 32 | 0.56 | 0.56 | 0.58 | 1.03 | 1.61 | 9.30 | 12.36 | 28.12 |
| 33 | 0.57 | 0.58 | 0.60 | 1.07 | 1.66 | 9.59 | 12.74 | 29.00 |
| 34 | 0.59 | 0.60 | 0.62 | 1.10 | 1.72 | 9.88 | 13.13 | 29.88 |
| 35 | 0.60 | 0.62 | 0.64 | 1.13 | 1.77 | 10.17 | 13.51 | 30.76 |
| 36 | 0.63 | 0.63 | 0.65 | 1.16 | 1.82 | 10.46 | 13.90 | 31.63 |
| 37 | 0.64 | 0.65 | 0.67 | 1.19 | 1.87 | 10.75 | 14.29 | 32.51 |
| 38 | 0.66 | 0.67 | 0.69 | 1.23 | 1.92 | 11.04 | 14.67 | 33.39 |
| 39 | 0.68 | 0.69 | 0.71 | 1.26 | 1.97 | 11.33 | 15.06 | 34.27 |
| 40 | 0.70 | 0.70 | 0.73 | 1.29 | 2.02 | 11.62 | 15.44 | 35.15 |
| 41 | 0.71 | 0.72 | 0.74 | 1.32 | 2.07 | 11.91 | 15.83 | 36.03 |
| 42 | 0.73 | 0.74 | 0.76 | 1.36 | 2.12 | 12.20 | 16.22 | 36.91 |
| 43 | 0.75 | 0.76 | 0.78 | 1.39 | 2.17 | 12.49 | 16.60 | 37.78 |
| 44 | 0.76 | 0.78 | 0.80 | 1.42 | 2.22 | 12.79 | 16.99 | 38.66 |
| 45 | 0.78 | 0.79 | 0.82 | 1.45 | 2.27 | 13.08 | 17.38 | 39.54 |
| 46 | 0.80 | 0.81 | 0.84 | 1.49 | 2.32 | 13.37 | 17.76 | 40.42 |
| 47 | 0.82 | 0.83 | 0.85 | 1.52 | 2.37 | 13.66 | 18.15 | 41.30 |
| 48 | 0.83 | 0.85 | 0.87 | 1.55 | 2.42 | 13.95 | 18.53 | 42.18 |
| 49 | 0.85 | 0.86 | 0.89 | 1.58 | 2.47 | 14.24 | 18.92 | 43.06 |
| 50 | 0.87 | 0.88 | 0.91 | 1.61 | 2.52 | 14.53 | 19.31 | 43.94 |
| 51 | 0.89 | 0.90 | 0.93 | 1.65 | 2.57 | 14.82 | 19.69 | 44.81 |
| 52 | 0.90 | 0.92 | 0.94 | 1.68 | 2.62 | 15.11 | 20.08 | 45.69 |
| 53 | 0.92 | 0.93 | 0.96 | 1.71 | 2.67 | 15.40 | 20.46 | 46.57 |
| 54 | 0.94 | 0.95 | 0.98 | 1.74 | 2.72 | 15.69 | 20.85 | 47.45 |
| 55 | 0.96 | 0.97 | 1.00 | 1.78 | 2.77 | 15.98 | <1.24 | 48.33 |
| 56 | 0.97 | 0.99 | 1.02 | 1.81 | 283 | 16.27 | 21.62 | 49.21 |
| 57 | 0.99 | 1.00 | 1.04 | 1.84 | 2.88 | 16.56 | 22.01 | 50.09 |
| 58 | 1.01 | 1.02 | 1.05 | 1.87 | 2.93 | 16.85 | 22.39 | 50.97 |
| 59 | 1.03 | 1.04 | 1.07 | 1.90 | 2.98 | 17.14 | 22.78 | 51.84 |
| 60 | 1.04 | 1.06 | 1.09 | 1.94 | 3.03 | 17.43 | 23.17 | 52.72 |

539
SQUARE KILOMETRES INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| Sq. Kilo metres. | Austrian Sq. Miles. | Prussian Sq. Miles. | German Sq. Miles. $15=1^{\circ} \mathrm{Eq}$. | Nautical square Leacues. $20=1^{\circ} \mathrm{Eq}$. | French Square Leagues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical Sq. Miles. $60=1^{\circ} \mathrm{E}_{4}$. | Euglish Square Miles. | Russian Square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 1.06 | 1.08 | 1.11 | 1.97 | 3.08 | 17.72 | 23.55 | 53.60 |
| 62 | 1.08 | 1.09 | 1.13 | 2.00 | 3.13 | 18.02 | 23.94 | 54.48 |
| 63 | 1.09 | 1.11 | 1.14 | 2.03 | 3.18 | 18.31 | 24.33 | 55.36 |
| 64 | 1.11 | 1.13 | 1.16 | 2.07 | 3.23 | 18.60 | 24.71 | 56.24 |
| 65 | 1.13 | 1.15 | 1.18 | 2.10 | 3.28 | 18.89 | 25.10 | 57.12 |
| 66 | 1.15 | 1.16 | 1.20 | 2.13 | 3.33 | 19.18 | 25.48 | 58.00 |
| 67 | 1.16 | 1.18 | 1.22 | 2.16 | 3.38 | 19.47 | 25.87 | 58.87 |
| 68 | 1.18 | 1.20 | 1.23 | 2.20 | 3.43 | 19.76 | 26.26 | 59.75 |
| 69 | 1.20 | 1.22 | 1.25 | 2.83 | 3.48 | 20.05 | 26.64 | 60.63 |
| 70 | 1.22 | 1.23 | 1.27 | 2.26 | 3.53 | 20.34 | 27.03 | 61.51 |
| 71 | 1.23 | 1.25 | 1.29 | 2.29 | 3.58 | 20.63 | 27.41 | 62.39 |
| 72 | 1.25 | 1.27 | 1.31 | 2.32 | 3.63 | 20.92 | 27.80 | 63.27 |
| 73 | 1.27 | 1.29 | 1.33 | 2.36 | 3.68 | 21.21 | 28.19 | 64.15 |
| 74 | 1.29 | 1.30 | 1.34 | 2.39 | 3.73 | 21.50 | 28.57 | 65.03 |
| 75 | 1.30 | 1.32 | 1.36 | 2.42 | 3.78 | 21.79 | 28.96 | 65.90 |
| 76 | 1.32 | 1.34 | 1.38 | 2.45 | 3.83 | 22.08 | 29.34 | 66.78 |
| 77 | 1.34 | 1.36 | 1.40 | 2.49 | 3.88 | 22.37 | 29.73 | 67.66 |
| 78 | 1.36 | 1.37 | 1.42 | 2.52 | 3.93 | 22.66 | 30.12 | 68.54 |
| 79 | 1.37 | 1.39 | 1.43 | 2.55 | 3.99 | 22.96 | 30.50 | 69.42 |
| 80 | 1.39 | 1.41 | 1.45 | 2.58 | 4.04 | 23.25 | 30.89 | 70.30 |
| 81 | 1.41 | 1.43 | 1.47 | 2.62 | 4.09 | 23.54 | 31.28 | 71.18 |
| 82 | 1.42 | 1.45 | 1.49 | 2.65 | 4.14 | 23.53 | 31.66 | 72.05 |
| 83 | 1.44 | 1.46 | 1.51 | 2.68 | 4.19 | 24.12 | 32.05 | 72.93 |
| 84 | 1.46 | 1.48 | 1.53 | 2.71 | 4.24 | 24.41 | 32.43 | 73.81 |
| 85 | 1.48 | 1.50 | 1.54 | 2.74 | 4.29 | 24.70 | 32.82 | 74.69 |
| 86 | 1.49 | 1.52 | 1.56 | 2.78 | 4.34 | 24.99 | 33.21 | 75.57 |
| 87 | 1.51 | 1.53 | 1.58 | 2.81 | 4.39 | 25.28 | 33.59 | 76.45 |
| 88 | 1.53 | 1.55 | 1.60 | 2.84 | 4.44 | 25.57 | 33.98 | 77.33 |
| 89 | 1.55 | 1.57 | 1.62 | 2.87 | 4.49 | 25.86 | 34.36 | 78.21 |
| 90 | 1.56 | 1.59 | 1.63 | 2.91 | 4.54 | 26.15 | 34.75 | 79.08 |
| 91 | 1.58 | 1.60 | 1.65 | 2.94 | 4.59 | 26.44 | 35.14 | 79.96 |
| 92 | 1.60 | 1.62 | 1.67 | 2.97 | 4.64 | 26.73 | 35.52 | 80.84 |
| 93 | 1.61 | 1.64 | 1.69 | 3.00 | 4.69 | 27.02 | 35.91 | 81.72 |
| 94 | 1.63 | 1.66 | 1.71 | 3.03 | 4.74 | 27.31 | 36.29 | 82.60 |
| 95 | 1.65 | 1.67 | 1.73 | 3.07 | 4.79 | 27.60 | 36.68 | 83.48 |
| 96 | 1.67 | 1.69 | 1.74 | 3.10 | 4.84 | 27.90 | 37.07 | 84.36 |
| 97 | 1.69 | 1.71 | 1.76 | 3.13 | 4.89 | 28.19 | 37.45 | 85.24 |
| 98 | 1.70 | 1.73 | 1.78 | 3.16 | 4.94 | 28.48 | 37.84 | 86.11 |
| 99 | 1.72 | 1.74 | 1.80 | 3.20 | 4.99 | 28.77 | 38.23 | 86.99 |
| 100 | 1.74 | 1.76 | 1.82 | 3.23 | 5.04 | 29.06 | 38.61 | 88.87 |

## II. austrian square miles into different geographical square measures.

| Anstrian Sq. Miles. | Sq. Kilometres. | $\begin{aligned} & \text { Prussian } \\ & \text { Sq. Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { si. Miles. } \\ 15=10 \text { EiI. } \end{gathered}$ | $\begin{aligned} & \text { Nautical } \\ & \text { Square } \\ & \text { Leagues. } \\ & 20=10 \mathrm{Eq} . \end{aligned}$ | French Square Leagnes. $2.5=1^{\circ} \mathrm{Eq}$. | Geograph'l or Natutical Sq. Miles. $60=1^{\circ} \mathrm{Eq}$. | Eoglish square Miles. | Russian square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 57546.44 | 1014.243 | 1045.104 | 1857.962 | 2903.066 | 16721.66 | 22219.61 | 50567.11 |
| 2,000 | 115092.9 | 2028.486 | 2090.207 | 3715.924 | 5806.131 | 33443.31 | 44439.22 | 101134.2 |
| 3,000 | 172639.3 | 3142.729 | 3135.311 | 5573.886 | 8709.197 | 50164.97 | 66658.83 | 151701.3 |
| 4,000 | 230185.8 | $4056.97 \because$ | 4180.414 | 7431.848 | 11612.26 | 66886.63 | 88878.44 | 202268.5 |
| 5,000 | 287732.2 | 5071.216 | 5225.518 | 9289.810 | 14515.33 | 83608.29 | 111098.0 | 252835.6 |
| 6,000 | 345278.7 | 6085.459 | 6270.622 | 11147.77 | 17418.39 | 100329.9 | 133317.7 | 303402.7 |
| 7,000 | 402825.1 | 7099.702 | 7315.725 | 13005.73 | 20321.46 | 117051.6 | 155537.3 | 353969.8 |
| 8,000 | 460371.5 | 8113.945 | 8360.829 | 14563.70 | 23224.52 | 133773.3 | 177756.9 | 404536.9 |
| 9,000 | 517918.0 | 9128.188 | 9405.932 | 16721.66 | 26127.59 | 150494.9 | 199976.5 | 455104.0 |
| 10,000 | 575464.4 | 10142.43 | 10451.04 | 18579.62 | 29030.66 | 167216.6 | 222196.1 | 505671.1 |
| 100 | 5754.64 | 101.42 | 104.51 | 185.80 | 290.31 | 1672.17 | 2221.96 | 5056.72 |
| 200 | 11509.29 | 202.85 | 209.02 | 371.59 | 580.61 | 3344.33 | 4443.92 | 10113.42 |
| 300 | 17263.93 | 304.27 | 313.53 | 557.39 | 870.92 | 5016.50 | 6665.88 | 15170.13 |
| 400 | 23018.58 | 405.70 | 418.04 | 743.18 | 1161.23 | 6688.66 | 8887.84 | 20226.85 |
| 500 | 28773.22 | 507.12 | 522.55 | 928.98 | 1451.53 | 8360.83 | 11109.80 | 25283.56 |
| 600 | 34527.87 | 608.55 | 627.06 | 1114.78 | 1741.84 | 10032.99 | 13331.77 | 30340.27 |
| 700 | 40282.51 | 709.97 | 731.57 | 1300.57 | 2032.15 | 11705.16 | 15553.73 | 35396.98 |
| 800 | 46037.15 | 811.39 | 836.08 | 1486.37 | 2322.45 | 13377.33 | 17775.69 | 40453.69 |
| 900 | 51791.24 | 912.82 | 940.59 | 1672.17 | 2612.76 | 15049.49 | 19997.65 | 45510.40 |
| 1000 | 57546.44 | 1014.24 | 1045.10 | 1857.96 | 2903.07 | 16721.66 | 22219.61 | 50567.11 |
| 1 | 57.55 | 1.01 | 1.05 | 1.86 | 2.90 | 16.72 | 22.22 | 50.57 |
| 2 | 115.09 | 2.03 | 2.09 | 3.72 | 5.81 | 33.44 | $44.4{ }^{4}$ | 101.13 |
| 3 | 172.64 | 3.04 | 3.14 | 5.57 | 8.71 | 50.16 | 66.66 | 151.70 |
| 4 | 230.19 | 4.06 | 4.18 | 7.43 | 11.61 | 66.89 | 88.88 | 202.27 |
| 5 | 287.73 | 5.07 | 5.23 | 9.29 | 14.52 | 83.61 | 111.10 | 252.84 |
| 6 | 345.28 | 6.09 | 6.27 | 11.15 | 17.42 | 100.33 | 133.32 | 303.40 |
| 7 | 402.83 | 7.10 | 7.32 | 13.01 | 20.32 | 117.05 | 155.54 | 353.97 |
| 8 | 460.37 | 8.11 | 8.36 | 14.86 | 23.22 | 133.77 | 177.76 | 404.54 |
| 9 | 517.92 | 9.13 | 9.41 | 16.72 | 26.13 | 150.49 | 199.98 | 455.10 |
| 10 | 575.46 | 10.14 | 10.45 | 18.58 | 29.03 | 167.22 | 222.20 | 505.67 |
| 11 | 633.01 | 11.16 | 11.50 | 20.44 | 31.93 | 183.94 | 244.42 | 556.24 |
| 12 | 690.56 | 12.17 | 12.54 | 22.30 | 34.84 | 200.66 | 266.64 | 606.81 |
| 13 | 748.10 | 13.19 | 13.59 | 24.15 | 37.74 | 217.38 | 288.85 | 657.37 |
| 14 | 805.65 | 14.20 | 14.63 | 26.01 | 40.64 | 234.10 | 311.07 | 707.94 |
| 15 | 863.20 | 15.21 | 15.68 | 27.87 | 43.55 | 250.8 | 333.29 | 758.51 |
| 16 | 920.74 | 16.23 | 16.72 | 29.73 | 46.45 | 267.55 | 355.51 | 809.07 |
| 17 | 978.29 | 17.24 | 17.77 | 31.59 | 49.35 | 284.27 | 377.7: | 859.64 |
| 18 | 1035.83 | 18.26 | 18.81 | 33.44 | 52.26 | 300.99 | 399.95 | 910.21 |
| 19 | 1093.38 | 19.27 | 19.86 | 35.30 | 55.16 | 317.71 | 422.17 | 960.78 |
| 20 | 1150.93 | 20.28 | 20.90 | 37.16 | 58.06 | 334.45 | 444.38 | 1011.34 |

541
AUSTRIAN SQUARE MILES INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| Austrian Sq. Miles. | Sq. Kilometres. | Prussian Sq. Miles. | German <br>  $15=10 \mathrm{Eq} .$ | Nautical Square Leagues. $20=1^{\circ} \mathrm{Eq}$. | French Square Leagues. $25=1^{\circ} \mathrm{E}_{1}$. | Geograph'l or Nautical sq. Miles. $60=1^{\circ} \mathrm{E}_{4}$. | English <br> Square <br> Miles. | Russian Square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 1208.48 | 21.30 | 21.95 | 39.02 | 60.96 | 351.15 | 466.61 | 1061.91 |
| 22 | 1266.02 | 22.31 | 22.99 | 40.88 | 63.87 | 367.88 | 488.83 | 1112.48 |
| 23 | 1323.57 | 23.33 | 24.04 | 42.73 | 66.77 | 384.60 | 511.05 | 1163.04 |
| 24 | 1381.11 | 24.34 | 25.08 | 44.59 | 69.67 | 401.32 | 533.27 | 1213.61 |
| 35 | 1438.66 | 25.36 | 26.13 | 46.45 | 72.58 | 418.04 | 555.49 | 1264.18 |
| 26 | 1496.21 | 26.37 | 27.17 | 48.31 | 75.48 | 434.76 | 577.71 | 1314.74 |
| 27 | 1553.75 | 27.38 | 28.22 | 50.16 | 78.38 | 451.48 | 599.93 | 1365.31 |
| 28 | 1611.30 | 28.40 | 29.26 | 52.02 | 81.29 | 468.21 | 622.15 | 1415.88 |
| 29 | 1668.85 | 29.41 | 30.31 | 53.88 | 84.19 | 484.93 | 644.37 | 1466.45 |
| 30 | 1726.39 | 30.43 | 31.35 | 55.74 | 87.09 | 501.65 | 666.59 | 1517.01 |
| 31 | 1783.94 | 31.44 | 32.40 | 57.60 | 90.00 | 518.37 | 688.81 | 1567.58 |
| 32 | 1841.49 | 32.46 | 33.44 | 59.45 | 92.90 | 535.09 | 711.03 | 1618.15 |
| 33 | 1899.03 | 33.47 | 34.49 | 61.31 | 95.80 | 551.81 | 733.25 | 1668.71 |
| 34 | 1956.58 | 34.48 | 35.53 | 63.17 | 98.70 | 568.54 | 755.47 | 1719.28 |
| 35 | 2014.13 | 35.50 | 36.58 | 65.03 | 101.61 | 585.26 | 777.69 | 1769.85 |
| 36 | 2071.67 | 36.51 | 37.62 | 66.89 | 104.51 | 601.98 | 799.91 | 1820.42 |
| 37 | 2129.22 | 37.53 | 38.67 | 68.74 | 107.41 | 618.70 | 822.13 | 1870.98 |
| 38 | 2186.76 | 38.54 | 39.71 | 70.60 | 110.32 | 635.42 | 84.35 | 1921.55 |
| 39 | 2244.31 | 39.56 | 40.76 | 72.46 | 113.22 | 652.14 | 866.56 | 1972.12 |
| 40 | 2301.86 | 40.57 | 41.80 | 74.32 | 116.12 | 668.87 | 888.78 | 2022.68 |
| 41 | 2359.40 | 41.58 | 42.85 | 76.18 | 119.03 | 685.59 | 911.00 | 2073.25 |
| 42 | 2416.95 | 42.60 | 43.89 | 78.03 | 121.93 | 702.31 | 933.22 | 2123.82 |
| 43 | 2474.50 | 43.61 | 44.94 | 79.89 | 124.83 | 719.03 | 955.44 | 2174.39 |
| 44 | 2532.04 | 44.63 | 45.98 | 81.75 | 127.73 | 735.75 | 977.66 | 2224.95 |
| 45 | 2589.59 | 45.64 | 47.03 | 83.61 | 130.64 | 752.47 | 999.88 | 2275.52 |
| 46 | 26.47 .14 | 46.66 | 48.07 | 85.47 | 133.54 | 769.20 | 1022.10 | 2326.09 |
| 47 | 2704.68 | 47.67 | 49.12 | 87.32 | 136.44 | 785.92 | 1044.32 | 2376.65 |
| 48 | 2762.23 | 48.68 | 50.16 | 89.18 | 139.35 | 802.64 | 1066.54 | 2427.22 |
| 49 | 2819.78 | 49.70 | 51.21 | 91.04 | 142.25 | 819.36 | 1088.76 | 2477.79 |
| 50 | 2877.32 | 50.71 | 52.25 | 92.90 | 145.15 | 836.08 | 1110.98 | 2528.36 |
| 51 | 2934.87 | 51.73 | 53.30 | 94.76 | 148.06 | 852.80 | 1133.20 | 2578.92 |
| 52 | 2992.42 | 52.74 | 54.34 | 96.61 | 150.96 | 869.53 | 1155.42 | 2629.49 |
| 53 | 3049.96 | 53.75 | 55.39 | 98.47 | 153.86 | 886.25 | 1177.64 | 2680.06 |
| 54 | 3107.51 | 54.77 | 56.44 | 100.33 | 156.77 | 902.97 | 1199.86 | 2730.62 |
| 55 | 3165.05 | 55.78 | 57.48 | 102.19 | 159.67 | 919.69 | 1222.08 | 2781.19 |
| 56 | 3222.60 | 56.80 | 58.53 | 104.05 | 162.57 | 936.41 | 1244.30 | 2831.76 |
| 57 | 3280.15 | 57.81 | 59.57 | 105.90 | 165.47 | 953.13 | 1266.52 | 2882.33 |
| 58 | 3337.69 | 58.83 | 60.62 | 107.76 | 168.38 | 969.86 | 1288.74 | 2932.89 |
| 59 | 3395.24 | 59.84 | 61.66 | 109.62 | 171.28 | 986.58 | 1310.96 | $\underline{9} 983.46$ |
| 60 | 3452.79 | 60.85 | 62.71 | 111.48 | 174.18 | 1003.30 | 1333.18 | 3034.03 |

## E

AUSTRIAN SQUARE MLLES INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| Austrian Sq. Miles. | Sq. Kilometres. | Prussian Sq. Miles. | $\begin{aligned} & \text { German } \\ & \mathrm{Sq} . \text { Miles. } \\ & 15=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical Square Leagues. $20=1^{\circ} \mathrm{Eq}$ | French Square Leagues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l <br> or Nautical <br> Sq. Miles. <br> $60=1^{\circ} \mathrm{Eq}$ | English Square Miles. | Russian <br> Square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 3510.33 | 61.87 | 63.75 | 113.34 | 177.09 | 1020.02 | 1355.40 | 3084.59 |
| 62 | 3567.88 | 62.88 | 64.80 | 115.19 | 180.00 | 1036.74 | 1377.62 | 3135.16 |
| 63 | 3625.43 | 63.90 | 65.84 | 117.05 | 182.89 | 1053.46 | 1399.84 | 3185.73 |
| 64 | 3682.97 | 64.91 | 66.89 | 118.91 | 185.80 | 1070.19 | 1422.05 | 3236.30 |
| 65 | 3740.52 | 65.93 | 67.93 | 120.77 | 188.70 | 1086.91 | 1444.27 | 3286.86 |
| 66 | 3798.07 | 66.94 | 68.98 | 122.63 | 191.60 | 1103.63 | 1466.49 | 3337.43 |
| 67 | 3855.61 | 67.95 | 70.02 | 124.48 | 194.51 | 1120.35 | 1488.71 | 3388.00 |
| 68 | 3913.16 | 68.97 | 71.07 | 126.34 | 197.41 | 1137.07 | 1510.93 | 3438.56 |
| 69 | 3970.70 | 69.98 | 72.11 | 128.20 | 200.31 | 1153.79 | 1533.15 | 3489.13 |
| 70 | 4028.25 | 71.00 | 73.16 | 130.06 | 203.21 | 1170.52 | 1555.37 | 3539.70 |
| 71 | 4085.80 | 72.01 | 74.20 | 131.91 | 206.12 | 1187.24 | 1577.59 | 3590.27 |
| 72 | 4143.34 | 73.03 | 75.25 | 133.77 | 209.02 | 1203.96 | 1599.81 | 3640.83 |
| 73 | 4200.89 | 74.04 | 76.29 | 135.63 | 211.92 | 1220.68 | 1622.03 | 3691.40 |
| 74 | 4258.44 | 75.05 | 77.34 | 137.49 | 214.83 | 1237.40 | 1644.25 | 3741.97 |
| 75 | 4315.98 | 76.07 | 78.38 | 139.35 | 217.73 | 1254.12 | 1666.47 | 3792.53 |
| 76 | 4373.53 | 77.08 | 79.43 | 141.20 | 220.63 | 1270.85 | 1688.69 | 3843.10 |
| 77 | 4431.08 | 78.10 | 80.47 | 143.06 | 223.54 | 1287.57 | 1710.91 | 3593.67 |
| 78 | 4488.62 | 79.11 | 81.52 | 144.92 | 226.44 | 1304.29 | 1733.13 | 3944.23 |
| 79 | 4546.17 | 80.13 | 82.56 | 146.78 | 229.34 | 1321.01 | 1755.35 | 3994.80 |
| 80 | 4603.72 | 81.14 | 83.61 | 148.64 | 232.25 | 1337.73 | 1777.57 | 4045.37 |
| 81 | 4661.26 | 82.15 | 84.65 | 150.49 | 235.15 | 1354.45 | 1799.79 | 4095.94 |
| 82 | 4718.81 | 83.17 | 85.70 | 152.35 | 238.05 | 1371.18 | 1822.01 | 4146.50 |
| 83 | 4776.35 | 84.18 | 86.74 | 154.21 | 240.95 | 1387.90 | 1844.23 | 4197.07 |
| 84 | 4833.90 | 85.20 | 87.79 | 156.07 | 243.86 | 1404.62 | 1866.45 | 4247.64 |
| 85 | 4891.45 | 86.21 | S8.83 | 157.93 | 246.76 | 1421.34 | 1888.67 | 4298.20 |
| 86 | 4948.99 | 87.22 | 89.88 | 159.78 | 249.66 | 1438.06 | 1910.89 | 4348.77 |
| 87 | 5006.54 | 88.24 | 90.92 | 161.64 | 252.57 | 1454.78 | 1933.11 | 4399.34 |
| 88 | 5064.09 | 89.25 | 91.97 | 163.50 | 255.47 | 1471.51 | 1955.33 | 4449.91 |
| 59 | 5121.64 | 90.27 | 93.01 | 165.36 | 258.37 | 1488.23 | 1977.55 | 4500.47 |
| 90 | 5179.18 | 91.28 | 94.06 | 167.22 | 261.28 | 1504.95 | 1999.76 | 4551.04 |
| 91 | 5236.73 | 92.30 | 95.10 | 169.07 | 264.18 | 1521.67 | 2021.98 | 4601.61 |
| 92 | 5294.27 | 93.31 | 96.15 | 170.93 | 267.08 | 1538.39 | 2044.20 | 4652.17 |
| 93 | 5351.82 | 94.32 | 97.19 | 172.79 | 269.99 | 1555.11 | 2066.42 | 4702.74 |
| 94 | 5409.37 | 95.34 | 98.24 | 174.65 | 272.89 | 1571.84 | 2088.64 | 4753.31 |
| 95 | 5466.91 | 96.35 | 99.28 | 176.51 | 275.79 | 1588.56 | 2110.86 | 4803.88 |
| 96 | 5524.46 | 97.37 | 100.33 | 178.36 | 278.69 | 1605.2 S | 2133.08 | 4854.44 |
| 97 | 5582.00 | 98.38 | 101.38 | 180.22 | 281.60 | 1622.00 | 2155.30 | 4905.01 |
| 98 | 5639.55 | 89.40 | 102.42 | 182.09 | 284.50 | 1638.72 | 2177.52 | 4955.58 |
| 99 | 5697.10 | 100.41 | 103.47 | 183.94 | 287.40 | 1655.44 | 2199.74 | 5006.14 |
| 100 | 5754.64 | 101.42 | 104.51 | 185.80 | 290.31 | 1672.17 | 2221.96 | 5056.72 |

543
III. prussian square miles into different geographical square measures.

| Prussian Sq. Miles. | Sq. Kilometres. | $\begin{aligned} & \text { Austrian } \\ & \text { Sq. Miles. } \end{aligned}$ | $\begin{aligned} & \text { German } \\ & \text { Sq. Miles. } \\ & 1 \delta=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical Square Learues $20=1^{\circ} \mathrm{Eq}$. | $\begin{gathered} \text { French } \\ \text { Square } \\ \text { Learues. } \\ 25=1^{\circ} \text { Eq. } \end{gathered}$ | Geograph'l <br> or Nautical <br> Sq. Miles. <br> $60=1^{\circ} \mathrm{E}_{1}$ | English Square miles. | Russian Square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 56738.31 | 985.957 | 1030.427 | 1831.870 | 2862.297 | 16486.33 | 21907.58 | 49857.01 |
| 2,000 | 113476.6 | 1971.914 | 2060.854 | 3663.741 | 5724.595 | 32973.66 | 43815.16 | 99714.19 |
| 3,000 | 170214.9 | 2957.871 | 3091.281 | 5495.611 | 8586.892 | 49460.50 | 65722.73 | 149571.3 |
| 4,000 | 226953.3 | 3943.828 | 4121.709 | 7327.482 | 11449.19 | 65947.34 | 87630.31 | 199428.4 |
| 5,000 | 283691.6 | 4929.785 | 5152.136 | 9159.353 | 14311.49 | 82434.17 | 109537.9 | 249285.5 |
| 6,000 | 340429.9 | 5915.742 | 6182.563 | 10991.22 | 17173.78 | 98921.00 | 131445.5 | 299142.6 |
| 7,000 | 397168.2 | 6901.698 | 7212.990 | 12823.09 | 20036.08 | 115407.8 | 153353.0 | 348999.7 |
| 8,000 | 453906.5 | 7887.655 | 8243.417 | 14654.96 | 22898.38 | 131894.7 | 175260.6 | 398856.8 |
| 9,000 | 510644.8 | 8873.612 | 9273.844 | 16486.83 | 25760.68 | 148381.5 | 197168.2 | 448713.9 |
| 10,000 | 567383.1 | 9859.569 | 10304.271 | 18318.70 | 28622.97 | 164868.3 | 219075.8 | 498571.0 |
| 100 | 5673.83 | 98.60 | 103.04 | 183.19 | 286.23 | 1648.68 | 2190.76 | 4985.70 |
| 200 | 11347.66 | 197.19 | 206.09 | 366.37 | 572.46 | 3297.37 | 4381.52 | 9971.42 |
| 300 | 17021.49 | 295.79 | 309.13 | 549.56 | 858.69 | 4946.05 | 6573.27 | 14957.1: |
| 400 | 22695.33 | 394.38 | 412.17 | 732.75 | 1144.92 | 6594.73 | 8763.03 | 19942.84 |
| 500 | 28369.16 | 492.98 | 515.21 | 915.94 | 1431.15 | 8243.41 | 10953.79 | 24928.55 |
| 600 | 34042.99 | 591.57 | 618.26 | 1099.12 | 1717.38 | 9892.10 | 13144.55 | 29914.26 |
| 700 | 39716.82 | 690.17 | 721.30 | 1282.31 | 2003.61 | 11540.78 | 15335.30 | 34899.97 |
| 800 | 45390.65 | 788.77 | 824.34 | 1465.50 | 2289.84 | 13189.47 | 17526.06 | 39885.6 |
| 900 | 51064.48 | 887.36 | 927.38 | 1648.68 | 2576.07 | 14838.15 | 19716.82 | 44871.39 |
| 1000 | 56738.31 | 985.96 | 1030.43 | 1831.87 | 2862.30 | 16486.83 | 21907.58 | 49857.01 |
| 1 | 56.74 | 0.99 | 1.03 | 1.83 | 2.86 | 16.49 | 21.91 | 49.86 |
| 2 | 113.48 | 1.97 | 2.06 | 3.66 | 5.72 | 32.97 | 43.82 | 99.71 |
| 3 | 170.21 | 2.96 | 3.09 | 5.50 | 8.59 | 49.46 | 65.72 | 149.57 |
| 4 | 226.95 | 3.94 | 4.12 | 7.33 | 11.45 | 65.95 | 87.63 | 199.48 |
| 5 | 283.69 | 4.93 | 5.15 | 9.16 | 14.31 | 82.43 | 109.54 | 249.28 |
| 6 | 340.43 | 5.92 | 6.18 | 10.99 | 17.17 | 98.92 | 131.45 | 299.14 |
| 7 | 397.17 | 6.90 | 7.21 | 12.82 | 20.04 | 115.41 | 153.35 | 349.00 |
| 8 | 453.91 | 7.89 | 8.24 | 14.65 | 22.90 | 131.89 | 175.26 | 398.86 |
| 9 | 510.64 | 8.87 | 9.27 | 16.49 | 25.76 | 148.38 | 197.17 | 448.71 |
| 10 | 567.38 | 9.86 | 10.30 | 18.32 | 28.62 | 164.87 | 219.08 | 498.57 |
| 11 | 624.12 | 10.85 | 11.33 | 20.15 | 31.49 | 181.36 | 240.98 | 548.43 |
| 12 | 680.86 | 11.83 | 12.37 | 21.98 | 34.35 | 197.84 | 262.89 | 598.29 |
| 13 | 737.60 | 12.82 | 13.40 | 23.81 | 37.21 | 214.33 | 284.80 | 648.14 |
| 14 | 794.34 | 13.80 | 14.43 | 25.65 | 40.07 | 231.82 | 306.71 | 698.00 |
| 15 | 851.07 | 14.79 | 15.46 | 27.48 | 42.93 | 247.30 | 328.61 | 747.86 |
| 16 | 907.81 | 15.78 | 16.49 | 29.31 | 45.80 | 263.79 | 350.52 | 797.71 |
| 17 | 964.55 | 16.76 | 17.52 | 31.14 | 48.66 | 280.28 | 372.43 | 847.57 |
| 18 | 1021.29 | 17.75 | 18.55 | 32.97 | 51.52 | 296.76 | 394.34 | 897.43 |
| 19 | 1078.03 | 18.73 | 19.58 | 34.81 | 54.38 | 313.25 | 416.24 | 947.28 |
| 20 | 1134.77 | 19.72 | 20.61 | 36.64 | 57.25 | 329.74 | 438.15 | 997.14 |

544
PrUSSIAN SQUARE MILES INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| Prussian Sq. Miles. | Sq. Kilo. metres. | Austrian Sq. Miles. | $\begin{aligned} & \text { German } \\ & \text { Sq. Milies. } \\ & 15=1^{\circ} \text { Eq. } \end{aligned}$ | $\begin{gathered} \text { Nautical } \\ \text { square } \\ \text { Lerayues. } \\ 20=1^{\circ} \mathrm{Eq} . \end{gathered}$ | French Square Leagues. $25=1^{\circ} \mathrm{E} 4$. | Geograph'l or Nautical sq. Miles. $60=1^{\circ}$ Eq. | English square Miles. | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 1191.50 | 20.71 | 21.64 | 38.47 | 60.11 | 346.22 | 460.06 | 1047.00 |
| 22 | 1248.24 | 21.69 | 22.67 | 40.30 | 62.97 | 362.71 | 481.97 | 1096.86 |
| 23 | 1304.98 | 22.68 | 23.70 | 42.13 | 65.83 | 379.20 | 503.87 | 1146.71 |
| 24 | 1361.72 | 23.66 | 24.73 | 43.96 | 68.70 | 395.68 | 525.78 | 1196.57 |
| 25 | 1418.46 | 24.65 | 25.76 | 45.80 | 71.56 | 412.17 | 547.69 | 1246.43 |
| 26 | 1475.20 | 25.63 | 26.79 | 47.63 | 74.42 | 428.66 | 569.60 | 1296.28 |
| 27 | 1531.93 | 26.62 | 27.82 | 49.46 | 77.28 | 445.14 | 591.50 | 1346.14 |
| 28 | 1588.67 | 27.61 | 28.85 | 51.29 | 80.14 | 461.63 | 613.41 | 1396.00 |
| 29 | 1645.41 | 28.59 | 29.88 | 53.12 | 83.01 | 478.12 | 635.32 | 1445.85 |
| 30 | 1702.15 | 29.58 | 30.91 | 54.96 | 85.87 | 494.61 | 657.23 | 1495.71 |
| 31 | 1758.89 | 30.56 | 31.94 | 56.79 | 88.73 | 511.09 | 679.13 | 1545.57 |
| 32 | 1815.63 | 31.55 | 32.97 | 58.62 | 91.59 | 527.58 | 701.04 | 1595.43 |
| 33 | 1872.36 | 32.54 | 34.00 | 60.45 | 94.46 | 544.07 | 722.95 | 1645.28 |
| 34 | 1929.10 | 33.52 | 35.03 | 62.28 | 97.32 | 560.55 | 74.86 | 1695.14 |
| 35 | 1985.84 | 34.51 | 36.06 | 64.12 | 100.18 | 577.04 | 766.77 | 1745.00 |
| 36 | 2042.58 | 35.49 | 37.10 | 65.95 | 103.04 | 593.53 | 788.67 | 1794.85 |
| 37 | 2099.32 | 36.48 | 38.13 | 67.78 | 105.91 | 610.01 | 810.58 | 1844.71 |
| 38 | 2156.06 | 37.47 | 39.16 | 69.61 | 108.77 | 626.50 | 832.49 | 1894.57 |
| 39 | 2212.79 | 38.45 | 40.19 | 71.44 | 111.63 | 642.99 | 854.40 | 1944.42 |
| 40 | 2269.53 | 39.44 | 41.22 | 73.27 | 114.49 | 659.47 | 876.30 | 1994.28 |
| 41 | 2326.27 | 40.42 | 42.25 | 75.11 | 117.35 | 675.96 | 898.21 | 20.44 .14 |
| 42 | 2383.01 | 41.41 | 43.28 | 76.94 | 120.22 | 692.45 | 920.12 | 2094.00 |
| 43 | 2439.75 | 42.40 | 44.31 | 78.77 | 123.08 | 708.93 | 942.03 | 2143.85 |
| 44 | 2496.49 | 43.38 | 45.34 | 80.60 | 125.94 | 725.42 | 963.93 | 2193.71 |
| 45 | 2553.22 | 44.37 | 46.37 | 82.43 | 128.80 | 741.91 | 985.84 | 2243.57 |
| 46 | 2609.96 | 45.35 | 47.40 | 84.27 | 131.67 | 758.39 | 1007.75 | 2293.42 |
| 47 | 2666.70 | 46.34 | 48.43 | 86.10 | 134.53 | 774.88 | 1029.66 | 2343.28 |
| 48 | 2723.44 | 47.33 | 49.46 | 87.93 | 137.39 | 791.37 | 1051.56 | 2393.14 |
| 49 | 2780.18 | 48.31 | 50.49 | 89.76 | 140.25 | 807.85 | 1073.47 | 2443.00 |
| 50 | 2836.92 | 49.30 | 51.52 | 91.59 | 143.11 | 824.34 | 1095.38 | 2492.85 |
| 51 | 2893.65 | 50.28 | 52.55 | 93.43 | 145.98 | 840.83 | 1117.29 | 2542.71 |
| 52 | 2950.39 | 51.27 | 53.58 | 95.26 | 148.84 | 857.32 | 1139.19 | 2592.57 |
| 53 | 3007.13 | 52.26 | 54.61 | 97.09 | 151.70 | 873.80 | 1161.10 | 2642.42 |
| 54 | 3163.87 | 53.24 | 55.64 | 98.92 | 154.56 | 890.29 | 1183.01 | 2692.28 |
| 55 | 3120.61 | 54.23 | 56.67 | 100.75 | 157.43 | 906.78 | 1204.92 | 2742.14 |
| 56 | 3177.35 | 55.21 | 57.70 | 102.58 | 160.29 | 923.26 | 1226.82 | 2791.99 |
| 57 | 3234.0S | 56.20 | 58.73 | 104.42 | 163.15 | 939.75 | 1248.73 | 2841.85 |
| 58 | 3290.82 | 57.19 | 59.76 | 106.25 | 166.01 | 956.24 | 1270.64 | 2891.71 |
| 59 | 3347.56 | 58.17 | 60.80 | 108.08 | 168.88 | 972.72 | 1292.55 | 2941.56 |
| 60 | 3404.30 | 59.16 | 61.83 | 109.91 | 171.74 | 989.21 | 1314.45 | 2991.42 |

prussian square miles into different geograplical square measures.

| Prussian <br> Sq. Miles. | Sq. Kilo- metres. | Austrian <br> Sq. Miles. | German Su. Miles. $15=1^{\circ} \mathrm{Eq}$. | Nautical Square Lengues. $20=1^{\circ} \mathrm{E} 4$ | French square Leagues. $2 \overline{0}=1^{\circ} \mathrm{Eq}$. | Geograph'1 or Nauticai sq. Miles. $60=1^{\circ}$ Eq. | English <br> square <br> Miles. | Russian <br> square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 3461.04 | 60.14 | 62.86 | 111.74 | 174.60 | 1005.70 | 1336.36 | 3041.28 |
| 62 | 3517.78 | 61.13 | 63.89 | 113.58 | 177.46 | 1022.18 | 1358.27 | 3091.13 |
| 63 | 3574.51 | 62.12 | 64.92 | 115.41 | 180.32 | 1035.67 | 1380.18 | 3140.99 |
| 64 | 3631.25 | 63.10 | 65.95 | 117.24 | 183.19 | 1055.16 | 1402.08 | 3190.85 |
| 65 | 3687.99 | 64.09 | 66.98 | 119.07 | 186.05 | 1071.64 | 1423.99 | 3240.71 |
| 66 | 3744.73 | 65.07 | 68.01 | 120.90 | 188.91 | 1088.13 | 1445.90 | 3290.56 |
| 67 | 3801.47 | 66.06 | 69.04 | 122.74 | 191.77 | 1104.62 | 1467.81 | 3340.42 |
| 68 | $3858.21{ }^{\circ}$ | 67.05 | 70.07 | 124.57 | 194.64 | 1121.10 | 1489.72 | 3390.28 |
| 69 | 3914.94 | 68.03 | 71.10 | 126.40 | 197.50 | 1137.59 | 1511.62 | 3440.13 |
| 70 | 3971.68 | 69.02 | 72.13 | 128.23 | 200.36 | 1154.08 | 1533.53 | 3489.99 |
| 71 | 4028.42 | 70.00 | 73.16 | 130.06 | 203.22 | 1170.57 | 1555.44 | 3539.85 |
| 72 | 4085.16 | 70.99 | 74.19 | 131.89 | 206.09 | 1187.05 | 1577.35 | 3589.71 |
| 73 | 4141.90 | 71.97 | 75.22 | 133.73 | 208.95 | 1203.54 | 1599.25 | 3639.56 |
| 74 | 4195.64 | 72.96 | 76.25 | 135.56 | 211.81 | 1220.03 | 1621.16 | 3689.42 |
| 75 | 4255.37 | 73.95 | 77.28 | 137.39 | 214.67 | 1236.51 | 1643.07 | 3739.28 |
| 76 | 4312.11 | 74.93 | 78.31 | 139.22 | 217.53 | 1253.00 | 1664.98 | 3789.13 |
| 77 | 4368.85 | 75.92 | 79.34 | 141.05 | 220.40 | 1269.49 | 1686.58 | 3838.99 |
| 78 | 4425.59 | 76.90 | 80.37 | 142.89 | 223.26 | 1285.97 | 1708.79 | 3888.85 |
| 79 | 4482.33 | 77.89 | 81.40 | 14.72 | 226.12 | 1302.46 | 1730.80 | 3938.70 |
| S0 | 4539.07 | 78.88 | 82.43 | 146.55 | 228.98 | 1318.95 | 1752.61 | 3988.56 |
| 81 | 4595.80 | 79.86 | 83.46 | 148.38 | 231.85 | 1335.43 | 1774.51 | 4038.42 |
| 82 | 4652.54 | 80.85 | 84.50 | 150.21 | 234.71 | 1351.92 | 1796.42 | 4088.28 |
| 83 | 4709.28 | 81.83 | 85.53 | 152.05 | 237.57 | 1368.41 | 1818.33 | 4138.13 |
| 84 | 4766.02 | 82.82 | 86.56 | 153.88 | 240.43 | 1384.89 | 1840.24 | 4187.99 |
| 85. | 4822.76 | 83.81 | 87.59 | 155.71 | 243.30 | 1401.38 | 1862.14 | 4237.85 |
| 86 | 4879.49 | 84.79 | 88.62 | 157.54 | 246.16 | 1417.87 | 1884.05 | 4287.70 |
| 87 | 4936.23 | 55.78 | 89.65 | 159.37 | 249.02 | 1434.35 | 1905.96 | 4337.56 |
| 88 | 4992.97 | 86.76 | 90.68 | 161.20 | 251.88 | 1450.84 | 1927.87 | 4357.42 |
| 89 | 5049.71 | 87.75 | 91.71 | 163.04 | 254.74 | 1467.33 | 1949.77 | 4437.27 |
| 90 | 5106.45 | 88.74 | 92.74 | 164.87 | 257.61 | 1483.81 | 1971.68 | 4487.13 |
| 91 | 5163.19 | 89.72 | 93.77 | 166.70 | 260.47 | 1500.30 | 1993.59 | 4536.99 |
| 92 | 5219.92 | 90.71 | 94.80 | 168.53 | 263.33 | 1516.79 | 2015.50 | 4586.85 |
| 93 | 5276.66 | 91.69 | 95.83 | 170.36 | 266.19 | 153:3.28 | 2037.40 | 4636.70 |
| 94 | 5333.40 | 92.68 | 96.86 | 172.20 | 269.06 | 1549.76 | 2059.31 | 4686.56 |
| 95 | 5390.14 | 93.67 | 97.89 | 174.03 | 271.92 | 1566.25 | 2081.22 | 4736.42 |
| 96 | 5446.88 | 94.65 | 98.92 | 175.86 | 274.78 | 1582.74 | 2103.13 | 4786.27 |
| 97 | 5503.62 | 95.64 | 99.95 | 177.69 | 277.64 | 1599.22 | 2125.04 | 4836.13 |
| 98 | 5560.35 | 96.62 | 100.98 | 179.52 | 280.51 | 1615.71 | 2146.94 | 4885.99 |
| 99 | 5617.09 | 97.61 | 102.01 | 181.36 | 283.37 | 1632.20 | 2168.85 | 4935.84 |
| 100 | 5673.83 | 98.60 | 103.04 | 183.19 | 286.23 | 1648.68 | 2190.76 | 4985.71 |

546
IV. german square miles into different geographical square measures.

| $\begin{gathered} \text { German } \\ \text { sq. Miles. } \\ 10=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Sq. Kilometres. | Austrian Sq. Miles. | Prussian Sq. Miles. | Nantical Square Leagues. $20=1^{\circ} \mathrm{Eq}$. | French Square Leagues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical sq. Miles. $60=1^{\circ} \mathrm{E} 4$. | English square Miles. | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 55062.91 | 956.8429 | 970.4713 | 1777.778 | 2777.778 | 16000.00 | 21260.68 | 48384.79 |
| 2,000 | 110125.8 | 1913.686 | 1940.943 | 3555.556 | 5555.556 | 32000.00 | 42521.35 | 96769.57 |
| 3,000 | 165188.7 | 2870.529 | 2911.414 | 5333.333 | 8333.333 | 48000.00 | 63782.03 | 145154.4 |
| 4,000 | 220251.6 | 3827.372 | 3881.885 | 7111.111 | 11111.111 | 64000.00 | 85042.71 | 193539.1 |
| 5,000 | 275314.5 | 4784.215 | 4852.357 | 8888.889 | 13888.89 | 80000.00 | 106303.4 | 241923.9 |
| 6,000 | 330377.4 | 5741.058 | 5822.828 | 10666.67 | 16666.67 | 96000.00 | 127564.1 | 290308.7 |
| 7,000 | 385440.4 | 6697.901 | 6793.299 | 12444.44 | 19444.44 | 112000.0 | 148824.7 | 338693.5 |
| 8,000 | 440503.3 | 7654.744 | 7763.771 | 14222.22 | 22222.22 | 128000.0 | 170085.4 | 387078.3 |
| 9,000 | 495566.2 | 8611.586 | 8734.242 | 16000.00 | 25000.00 | 144000.0 | 191346.1 | 435463.1 |
| 10,000 | 550629.1 | 9568.429 | 9704.713 | 17777.78 | 27777.78 | 160000.0 | 212606.8 | 483847.9 |
| 100 | 5506.29 | 95.68 | 97.05 | 177.78 | 277.78 | 1600.00 | 2126.07 | 4838.48 |
| 200 | 11012.55 | 191.37 | 194.09 | 355.56 | 555.56 | 3200.00 | 4252.14 | 9676.96 |
| 300 | 16518.87 | 287.06 | 291.14 | 533.33 | 833.33 | 4800.00 | 6378.20 | 14515.44 |
| 400 | 22025.16 | 382.74 | 388.19 | 711.11 | 1111.11 | 640000 | 8504.27 | 19353.91 |
| 500 | 27531.45 | 478.42 | 485.24 | 888.89 | 1388.89 | 8000.00 | 10630.34 | 24192.39 |
| 600 | 33037.74 | 574.11 | 582.28 | 1066.67 | 1666.67 | 9600.00 | 12756.41 | 29030.87 |
| 700 | 38544.04 | 669.79 | 679.33 | 1244.44 | 1944.44 | 11200.00 | 14882.47 | 33869.35 |
| 800 | 44050.33 | 765.47 | 776.38 | 1422.22 | 2292.22 | 12800.00 | 17008.54 | 38707.83 |
| 900 | 49556.62 | S61.16 | 873.42 | 1600.00 | 2500.00 | 14400.00 | 19134.61 | 43546.31 |
| 1000 | 55062.91 | 956.84 | 970.47 | 1777.78 | 2777.78 | 16000.00 | 21260.68 | 48384.79 |
| 1 | 55.06 | 0.96 | 0.97 | 1.78 | 2.78 | 16.00 | 21.26 | 48.38 |
| 2 | 110.13 | 1.91 | 1.94 | 3.56 | 5.56 | 32.00 | 42.52 | 96.77 |
| 3 | 165.19 | 2.87 | 2.91 | 5.33 | 8.33 | 48.00 | 63.78 | 145.15 |
| 4 | 220.25 | 3.83 | 3.88 | 7.11 | 11.11 | 64.00 | 85.04 | 193.54 |
| 5 | 275.31 | 4.78 | 4.85 | 8.89 | 13.89 | 80.00 | 106.30 | 241.92 |
| 6 | 330.38 | 5.74 | 5.82 | 10.67 | 16.67 | 96.00 | 127.56 | 290.31 |
| 7 | 385.44 | 6.70 | 6.79 | 12.44 | 19.44 | 112.00 | 148.82 | 338.69 |
| 8 | 440.50 | 7.65 | 7.76 | 14.22 | 22.22 | 128.00 | 170.09 | 387.08 |
| 9 | 495.57 | 8.61 | 8.73 | 16.00 | 25.00 | 144.00 | 191.35 | 435.46 |
| 10 | 550.63 | 9.57 | 9.70 | 17.78 | 27.78 | 160.00 | 212.61 | 483.85 |
| 11 | 605.69 | 10.53 | 10.68 | 19.56 | 30.56 | 176.00 | 233.87 | 532.23 |
| 12 | 660.75 | 11.48 | 11.65 | 21.33 | 33.33 | 192.00 | 255.13 | 580.62 |
| 13 | 715.82 | 12.44 | 12.62 | 23.11 | 36.11 | 208.00 | 276.39 | 629.00 |
| 14 | 770.88 | 13.40 | 13.59 | 24.89 | 38.89 | 224.00 | 297.65 | 677.39 |
| 15 | 825.94 | 14.35 | 14.56 | 26.67 | 41.67 | 240.00 | 318.91 | 725.77 |
| 16 | 881.01 | 15.31 | 15.52 | 28.44 | 44.44 | 256.00 | 340.17 | 774.16 |
| 17 | 936.07 | 16.27 | 16.50 | 30.22 | 47.22 | 272.00 | 361.43 | 822.54 |
| 18 | 991.13 | 17.22 | 17.47 | 32.00 | 50.00 | 288.00 | 382.69 | 870.93 |
| 19 | 1046.20 | 18.18 | 18.44 | 33.78 | 52.78 | 304.00 | 403.95 | 919.31 |
| 20 | 1101.26 | 19.14 | 19.41 | 35.56 | 55.56 | 320.00 | 425.21 | 967.70 |

547
GERMAN SQUARE MILES INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| $\begin{aligned} & \text { German } \\ & \text { Sq. Miles. } \\ & 10=1^{\circ} \text { Eq. } \end{aligned}$ | Sq. Kilometres. | Austrian sq. Miles. | Prussian Sq Miles. | $\begin{aligned} & \text { Nautical } \\ & \text { fquare } \\ & \text { Leagues. } \\ & 20=10 \mathrm{Eq} . \end{aligned}$ | French Square Leagues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical -q Miles. $60=1^{\circ} \mathrm{E} 4$. | English Equare Miles. | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 1156.32 | 20.09 | 20.38 | 37.33 | 58.33 | 336.00 | 446.47 | 1016.08 |
| 22 | 1211.38 | 21.05 | 21.35 | 39.11 | 61.11 | 352.00 | 467.73 | 1064.47 |
| 23 | 1266.45 | 22.01 | 22.32 | 40.89 | 63.89 | 368.00 | 489.00 | 1112.85 |
| 24 | 1321.51 | 22.96 | 23.29 | 42.67 | 66.67 | 384.00 | 510.26 | 1161.23 |
| 25 | 1376.57 | 23.92 | 24.26 | 44.44 | 69.44 | 400.00 | 531.52 | 1209.62 |
| 26 | 1431.64 | 24.88 | 25.23 | 46.22 | 72.22 | 416.00 | 552.78 | 1258.00 |
| 27 | 1485.70 | 25.83 | 26.20 | 48.00 | 75.00 | 432.00 | 574.04 | 1306.39 |
| 28 | 1541.76 | 26.79 | 27.17 | 49.78 | 77.78 | 448.00 | 595.30 | 1354.77 |
| 29 | 1596.82 | 27.75 | 28.14 | 51.56 | 80.56 | 464.00 | 616.56 | 1403.16 |
| 30 | 1651.89 | 28.71 | 29.11 | 53.33 | 83.33 | 480.00 | 637.82 | 1451.54 |
| 31 | 1706.95 | 29.66 | 30.08 | 55.11 | 86.11 | 496.00 | 659.08 | 1499.93 |
| 32 | 1762.01 | 30.62 | 31.06 | 56.89 | 88.89 | 512.00 | 680.34 | 1548.31 |
| 33 | 1817.08 | 31.58 | 32.03 | 38.67 | 91.67 | 528.00 | 701.60 | 1596.70 |
| 34 | 1872.14 | 32.53 | 33.00 | 60.44 | 94.44 | 544.00 | 722.86 | 1645.08 |
| 35 | 1927.20 | 33.49 | 34.00 | 62.22 | 97.22 | 560.00 | 744.12 | 1693.47 |
| 36 | 1982.26 | 34.45 | 34.94 | 64.00 | 100.00 | 576.00 | 765.38 | 1741.85 |
| 37 | 2037.33 | 35.40 | 35.91 | 65.78 | 102.78 | 592.00 | 786.65 | 1790.24 |
| 38 | 2092.39 | 36.36 | 36.88 | 67.56 | 105.56 | 608.00 | 807.91 | 1838.62 |
| 39 | 2147.45 | 37.32 | 37.85 | 69.33 | 108.33 | 624.00 | 829.17 | 1857.01 |
| 40 | 2202.52 | 38.27 | 38.82 | 71.11 | 111.11 | 640.00 | 850.43 | 1935.39 |
| 41 | 2257.58 | 39.23 | 39.79 | 72.59 | 113.89 | 656.00 | 871.69 | 1983.78 |
| 42 | 2312.64 | 40.19 | 40.76 | 74.67 | 116.67 | 672.00 | 892.95 | 2032.16 |
| 43 | 2367.70 | 41.14 | 41.73 | 76.44 | 119.44 | 688.00 | 914.21 | 2080.55 |
| 44 | 2422.76 | 42.10 | 42.70 | 78.22 | 122.22 | 704.00 | 935.47 | 2128.93 |
| 45 | 2477.83 | 43.06 | 43.67 | 80.00 | 125.00 | 720.00 | 956.73 | 2177.32 |
| 46 | 2532.89 | 44.01 | 44.64 | 81.78 | 127.78 | 736.00 | 977.99 | 2225.70 |
| 47 | 2587.96 | 44.97 | 45.61 | 83.56 | 130.56 | 752.00 | 999.25 | 2274.09 |
| 48 | 2642.02 | 45.93 | 46.58 | 85.33 | 133.33 | 768.00 | 1020.51 | 2322.47 |
| 49 | 2698.08 | 46.89 | 47.55 | 87.11 | 136.11 | 784.00 | 1041.77 | 2370.85 |
| 50 | 2753.14 | 47.84 | 48.52 | 88.89 | 138.89 | 800.00 | 1063.03 | 24.19 .24 |
| 51 | 2808.21 | 48.80 | 49.49 | 90.67 | 141.67 | 816.00 | 1084.29 | 2467.62 |
| 52 | 2863.27 | 49.76 | 50.46 | 92.44 | 144.44 | 832.00 | 1105.56 | 2516.01 |
| 53 | 2918.33 | 50.71 | 51.43 | 94.22 | 147.22 | 848.00 | 1126.82 | 2564.39 |
| 54 | 2973.40 | 51.67 | 52.41 | 96.00 | 150.00 | 864.00 | 1148.08 | 2612.78 |
| 55 | 3029.46 | 52.63 | 53.36 | 97.78 | 152.78 | 880.00 | 1169.34 | 2661.16 |
| 56 | 3083.52 | 53.58 | 54.35 | 99.56 | 155.56 | 896.00 | 1190.60 | 2709.55 |
| 57 | 3138.59 | 54.54 | 55.32 | 101.33 | 158.33 | 912.00 | 1211.86 | 2757.93 |
| 58 | 3193.65 | 55.50 | 56.29 | 103.11 | 161.11 | 928.00 | 1233.12 | 2806.32 |
| 59 | 3248.71 | 56.45 | 57.26 | 104.89 | 164.89 | 944.00 | 1254.38 | 2854.70 |
| 60 | 3303.77 | 57.41 | 58.23 | 106.67 | 166.67 | 960.00 | 1275.64 | 2903.09 |

german square miles into different geographical square measures.

| $\begin{gathered} \text { German } \\ \text { Sq. Miles. } \\ 15=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Sq. Kilometres. | $\begin{aligned} & \text { Austrian } \\ & \text { Sq. Miles. } \end{aligned}$ | Prussian Sq. Miles. | Nautical square Leagues. $20=1^{\circ} \mathrm{Eq}$. | $\begin{gathered} \text { French } \\ \text { square } \\ \text { Leayues. } \\ 25=1^{\circ} \text { Eq. } \end{gathered}$ | Geograph'l or Nautical Eq Miles. $60=1^{\circ}$ Eq. | English Square Miles. | Russian square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 3358.84 | 58.37 | 59.20 | 108.44 | 169.44 | 976.00 | 1296.90 | 2951.47 |
| 62 | 3413.90 | 59.32 | 60.17 | 110.22 | 172.22 | 992.00 | 1318.16 | 2999.86 |
| 63 | 3468.96 | 60.28 | 61.14 | 112.00 | 175.00 | 1008.00 | 1339.42 | 3048.24 |
| 64 | 3524.03 | 61.24 | 62.11 | 113.78 | 177.78 | 1024.00 | 1360.68 | 3096.63 |
| 65 | 3579.09 | 62.19 | 63.08 | 115.56 | 180.56 | 1040.00 | 1381.94 | 3145.01 |
| 66 | 3634.15 | 63.15 | 64.05 | 117.33 | 183.33 | 1056.00 | 1403.20 | 3193.40 |
| 67 | 3689.21 | 64.11 | 65.02 | 119.11 | 186.11 | 1072.00 | 1424.47 | 3241.78 |
| 68 | 3744.28 | 65.07 | 65.99 | 120.89 | 188.69 | 1088.00 | 1445.73 | 3290.17 |
| 69 | 3799.34 | 66.02 | 66.96 | 122.67 | 191.67 | 1104.00 | 1466.99 | 3338.55 |
| 70 | 3854.40 | 66.98 | 67.93 | 124.44 | 194.44 | 1120.00 | 1488.25 | 3386.94 |
| 71 | 3909.47 | 67.94 | 68.90 | 126.22 | 197.22 | 1136.00 | 1509.51 | 3435.32 |
| 72 | 3964.53 | 68.89 | 69.87 | 128.00 | 200.00 | 1152.00 | 1530.77 | 3483.71 |
| 73 | 4019.59 | 69.85 | 70.84 | 129.78 | 202.78 | 1168.00 | 1552.03 | 3532.09 |
| 74 | 4074.66 | 70.81 | 71.81 | 131.56 | 205.56 | 1184.00 | 1573.29 | 3580.47 |
| 75 | 4129.72 | 71.76 | 72.79 | 133.33 | 208.33 | 1200.00 | 1594.55 | 3628.86 |
| 76 | 4184.78 | 72.72 | 73.76 | 135.11 | 211.11 | 1216.00 | 1615.81 | 3677.24 |
| 77 | 4239.84 | 73.68 | 74.73 | 136.89 | 213.89 | 1232.00 | 1637.07 | 3725.63 |
| 78 | 4294.91 | 74.63 | 75.70 | 138.67 | 216.67 | 1248.00 | 1658.33 | 3774.01 |
| 79 | 4349.97 | 75.59 | 76.67 | 140.44 | 219.44 | 1264.00 | 1679.59 | 3822.40 |
| 80 | 4405.03 | 76.55 | 77.63 | 142.22 | 222.22 | 1280.00 | 1700.85 | 3870.78 |
| 81 | 4460.10 | 77.50 | 78.61 | 144.00 | 225.00 | 1296.00 | 1722.11 | 3919.17 |
| 82 | 4515.16 | 78.46 | 79.58 | 145.78 | 227.78 | 1312.00 | 1743.38 | 3967.55 |
| 83 | 4570.22 | 79.42 | 80.55 | 147.56 | 230.56 | 1328.00 | 1764.64 | 4015.94 |
| 84 | 4625.28 | 80.37 | 81.52 | 149.33 | 233.33 | 1344.00 | 1785.90 | 4064.32 |
| 85 | 4680.35 | 81.33 | 82.49 | 151.11 | 236.11 | 1360.00 | 1807.16 | 4112.71 |
| 86 | 4735.41 | 82.28 | 83.46 | 152.89 | 235.89 | 1376.00 | 1828.42 | 4161.09 |
| 87 | 4790.47 | 83.25 | 84.43 | 154.67 | 241.67 | 1392.00 | 1849.68 | 4209.48 |
| 88 | 4845.54 | 84.20 | 85.40 | 156.44 | 244.44 | 1408.00 | 1870.94 | 4257.86 |
| 89 | 4900.60 | 85.16 | 86.37 | 158.22 | 247.22 | 1424.00 | 1892.20 | 4306.25 |
| 90 | 4955.66 | 86.12 | 87.34 . | 160.00 | 250.00 | 1440.00 | 1913.46 | 4354.63 |
| 91 | 5010.73 | 87.07 | 88.31 | 161.78 | 252.78 | 1456.00 | 1934.72 | 4403.02 |
| 92 | 5065.79 | 88.03 | 89.28 | 163.56 | 255.56 | 1472.00 | 1955.98 | 4451.40 |
| 93 | 5120.85 | 88.99 | 90.25 | 165.33 | 258.33 | 1488.00 | 1977.24 | 4499.79 |
| 94 | 5175.91 | 89.94 | 91.22 | 167.11 | 261.11 | 1504.00 | 1998.50 | 4548.17 |
| 95 | 5230.98 | 90.90 | 92.19 | 168.89 | 263.89 | 1520.00 | 2019.76 | 4596.56 |
| 96 | 5286.04 | 91.86 | 93.17 | 170.67 | 266.67 | 1536.00 | 2041.03 | 4644.94 |
| 97 | 5341.10 | 92.81 | 94.14 | 172.44 | 269.44 | 1552.00 | 2062.29 | 4693.32 |
| 98 | 5396.17 | 93.77 | 95.11 | 174.22 | 272.22 | 1568.00 | 2083.55 | 4741.71 |
| 99 | 5451.23 | 94.73 | 96.08 | 176.00 | 275.00 | 1584.00 | 2104.81 | 4790.09 |
| 100 | 5506.29 | 95.68 | 97.05 | 177.78 | 277.78 | 1600.00 | 2126.07 | 4838.48 |


| Nautical Square Leagues. $20=1^{\circ}$ Eq. | Sq. Kilometres. | Austrian Sq. Miles. | Prussian Sq. Miles. | $\begin{aligned} & \text { German } \\ & \text { sq. Miles. } \\ & 1 s=1^{\circ} \text { Eq. } \end{aligned}$ | French Square Leagues. $25=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical aq Miles. $60=10 \mathrm{Eq}$. | English <br> square <br> Miles. | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 30972.89 | 538.2242 | 545.8901 | 562.5000 | 1562.500 | 9000.000 | 11959.13 | 27216.44 |
| 2,000 | 61945.77 | 1076.448 | 1091.780 | 1125.000 | 3125.000 | 18000.00 | 23918.26 | 54432.87 |
| 3,000 | 92918.66 | 1614.672 | 1637.670 | 1687.500 | 4687.500 | 27000.00 | 35877.39 | 81649.31 |
| 4,000 | 123891.5 | 2152.897 | 2183.561 | 2250.000 | 6250.000 | 36000.00 | 47836.52 | 108865.7 |
| 5,000 | 154864.4 | 2691.121 | 2799.451 | 2812.500 | 7812.500 | 45000.00 | 59795.65 | 136082.2 |
| 6,000 | 185837.3 | 3239.345 | 3275.341 | 3375.000 | 9375.000 | 54000.00 | 71754.78 | 163298.6 |
| 7,000 | 216810.2 | 3767.569 | 3821.231 | 3937.500 | 10937.50 | 53000.00 | 83713.91 | 190515.1 |
| 8,000 | 247783.1 | 4305.793 | 4367.121 | 4500.000 | 12500.00 | 72000.00 | 95673.04 | 217731.5 |
| 9,000 | 278756.0 | 4844.017 | 4913.011 | 5062.500 | 14062.50 | 81000.00 | 107632.2 | 244947.9 |
| 10,000 | 30972S.9 | 5382.242 | 5458.901 | 5625.000 | 15625.00 | 90000.00 | 119591.3 | 272164.4 |
| 100 | 3097.29 | 53.82 | 54.59 | 56.25 | 156.25 | 900.00 | 1195.91 | 2721.64 |
| 200 | 6194.58 | 107.64 | 109.18 | 112.50 | 312.50 | 1800.00 | 2391.83 | 5443.29 |
| 300 | 9291.87 | 161.47 | 163.77 | 168.75 | 468.75 | 2700.00 | 3557.74 | S164.93 |
| 400 | 12389.15 | 215.29 | 218.36 | 225.00 | 625.00 | 3600.00 | 4753.65 | 10886.57 |
| 500 | 15486.44 | 269.11 | 272.95 | 281.25 | 781.25 | 4500.00 | 5979.57 | 13608.22 |
| 600 | 18583.73 | 322.93 | 327.53 | 337.50 | 937.50 | 5400.00 | 7175.48 | 16329.86 |
| 700 | 21681.02 | 376.76 | 382.12 | 393.75 | 1093.75 | 6300.00 | 8371.39 | 19051.51 |
| 800 | 24778.31 | 430.58 | 436.71 | 450.00 | 1250.00 | 7200.00 | 9567.30 | 21773.15 |
| 900 | 27875.60 | 484.40 | 491.30 | 506.25 | 1406.25 | 8100.00 | 10763.22 | 24494.79 |
| 1000 | 30972.89 | 538.22 | 545.89 | 562.50 | 1562.50 | 9000.00 | 11959.13 | 27216.44 |
| 1 | 30.97 | 0.54 | 0.55 | 0.56 | 1.56 | 9.00 | 11.96 | 27.22 |
| 2 | 61.95 | 1.08 | 1.09 | 1.12 | 3.12 | 18.00 | 23.92 | 54.43 |
| 3 | 92.92 | 1.61 | 1.64 | 1.69 | 4.69 | 27.00 | 35.88 | 81.65 |
| 4 | 123.89 | 2.15 | 2.18 | 2.25 | 6.25 | 36.00 | 47.84 | 108.87 |
| 5 | 154.86 | 2.69 | 2.73 | 2.81 | 7.81 | 45.00 | 59.80 | 136.08 |
| 6 | 185.84 | 3.23 | 3.28 | 3.37 | 9.37 | 54.00 | 71.75 | 163.30 |
| 7 | 216.81 | 3.77 | 3.82 | 3.94 | 10.94 | 63.00 | 83.71 | 190.51 |
| 8 | 247.78 | 4.31 | 4.37 | 4.50 | 12.50 | 72.00 | 95.67 | 217.73 |
| 9 | 278.76 | 4.84 | 4.91 | 5.06 | 14.06 | 81.00 | 107.63 | 244.95 |
| 10 | 309.73 | 5.38 | 5.46 | 5.62 | 15.62 | 90.00 | 119.59 | 272.16 |
| 11 | 340.70 | 5.92 | 6.00 | 6.19 | 17.19 | 99.00 | 131.55 | 299.38 |
| 12 | 371.67 | 6.46 | 6.55 | 6.75 | 18.75 | 108.00 | 143.51 | 326.60 |
| 13 | 402.65 | 7.00 | 7.10 | 7.31 | 20.31 | 117.00 | 155.47 | 353.81 |
| 14 | 433.62 | 7.54 | 7.64 | 7.87 | 21.87 | 126.00 | 167.43 | 381.03 |
| 15 | 464.59 | 8.07 | 8.19 | 8.44 | 23.44 | 135.00 | 179.39 | 408.25 |
| 16 | 495.57 | 8.61 | 8.73 | 9.00 | 25.00 | 144.00 | 191.35 | 435.46 |
| 17. | 526.54 | 9.15 | 9.28 | 9.56 | 26.56 | 153.00 | 203.31 | 462.68 |
| 18 | 557.51 | 9.69 | 9.83 | 10.12 | 28.12 | 162.00 | 215.26 | 499.90 |
| 19 | 588.48 | 10.23 | 10.37 | 10.69 | 29.69 | 171.00 | 227.22 | 517.11 |
| 20 | 619.46 | 10.76 | 10.92 | 11.25 | 31.25 | 180.00 | 239.18 | 544.33 |

NAUTICAL SQUARE LEAGUES INTO DIFFERENT GEOGRAPIICAL SQUARE MEASURES.

| $\begin{gathered} \text { Nautical } \\ \text { square } \\ \text { Leayues. } \\ 20=10 \text { Eq. } \end{gathered}$ | Sq. Kilometres. | $\begin{aligned} & \text { Austrian } \\ & \text { Sq. Miles. } \end{aligned}$ | $\begin{aligned} & \text { Prussian } \\ & \text { Sq. Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { Sq. Miles. } \\ \mathbf{1 5}=1^{\circ} \text { Eq. } \end{gathered}$ | $\begin{gathered} \text { French } \\ \text { Square } \\ \text { Leagues. } \\ \text { 2. }=10 \text { Eq. } \end{gathered}$ | Geograph'l or Nautical Sq Miles. $60=1^{\circ} \mathrm{E} q$. | English Square Miles. | Russian <br> square <br> Wersto |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 650.43 | 11.30 | 11.46 | 11.81 | 32.81 | 189.00 | 251.14 | 571.55 |
| 22 | 681.40 | 11.84 | 12.01 | 12.37 | 34.37 | 198.00 | 263.10 | 598.76 |
| 23 | 712.37 | 12.38 | 12.56 | 12.94 | 35.94 | 207.00 | 275.06 | 625.98 |
| 24 | 743.35 | 12.92 | 13.10 | 13.50 | 37.50 | 216.00 | 287.02 | 653.19 |
| 25 | 774.32 | 13.46 | 13.65 | 14.06 | 39.06 | 225.00 | 298.98 | 680.41 |
| 26 | 805.29 | 13.99 | 14.19 | 14.62 | 40.62 | 234.00 | 310.94 | 707.63 |
| 27 | 836.27 | 14.53 . | 14.74 | 15.19 | 42.19 | 243.00 | 322.90 | 734.84 |
| 28 | 867.24 | 15.07 | 15.28 | 15.75 | 43.75 | 252.00 | 334.86 | 762.06 |
| 29 | - 898.21 | 15.61 | 15.83 | 16.31 | 45.31 | 261.00 | 346.81 | 789.28 |
| 30 | 929.19 | 16.15 | 16.38 | 16.87 | 46.87 | 270.00 | 358.77 | 816.49 |
| 31 | 960.16 | 16.68 | 16.92 | 17.44 | 48.44 | 279.00 | 370.73 | 843.71 |
| 32 | . 991.13 | 17.22 | 17.47 | 18.00 | 50.00 | 288.00 | 382.69 | 870.93 |
| 33 | 102.2 .11 | 17.76 | 18.01 | 18.515 | 51.56 | 297.00 | 394.65 | 898.14 |
| 34 | 1053.08 | 18.30 | 18.56 | 19.12 | 53.12 | 306.00 | 406.61 | 925.36 |
| 35 | 1084.05 | 18.84 | 19.11 | 19.69 | 54.69 | 315.00 | 418.57 | 952.58 |
| 36 | 1115.02 | 19.38 | 19.65 | 20.25 | 56.25 | 324.00 | 430.53 | 979.79 |
| 37 | 1146.00 | 19.91 | 20.20 | 20.81 | 57.81 | 333.00 | 442.49 | 1007.01 |
| 38 | 1176.97 | 20.45 | 20.74 | 21.37 | 59.37 | 342.00 | 454.45 | 1034.22 |
| 39 | 1207.94 | 20.99 | 21.29 | 21.94 | 60.94 | 351.00 | 466.41 | 1061.44 |
| 40 | 1238.92 | 21.53 | 21.84 | 22.50 | 62.50 | 360.00 | 478.37 | 1088.66 |
| 41 | 1269.89 | 22.07 | 22.38 | 23.06 | 64.06 | 369.00 | 490.32 | 1115.87 |
| 42 | 1300.86 | 22.61 | 22.98 | 23.62 | 65.62 | 378.00 | 502.28 | 1143.09 |
| 43 | 1331.83 | 23.14 | 23.47 | 24.19 | 67.19 | 387.00 | 514.24 | 1170.31 |
| 44 | 1362.81 | 23.68 | 24.02 | 24.75 | 68.75 | 396.00 | 526.20 | 1197.52 |
| 45 | 1393.78 | 24.22 | 24.57 | 25.31 | 70.31 | 405.00 | 538.16 | 1224.74 |
| 46 | 1424.75 | 24.76 | 25.11 | 25.87 | 71.87 | 414.00 | 550.12 | 1251.96 |
| 47 | 1455.73 | 25.30 | 25.66 | 26.44 | 73.44 | 423.00 | 562.08 | 1279.17 |
| 48 | 1486.70 | 25.83 | 26.20 | 27.00 | 75.00 | 432.00 | 574.04 | 1306.39 |
| 49 | 1517.67 | 26.37 | 26.75 | 27.56 | 76.56 | 441.00 | 586.00 | 1333.61 |
| 50 | 1548.64 | 26.91 | 27.29 | 28.12 | 78.12 | 450.00 | 597.96 | 1360.82 |
| 51 | 1579.69 | 27.45 | 27.84 | 28.69 | 79.69 | 459.00 | 609.92 | 1388.04 |
| 52 | 1610.59 | 27.99 | 28.39 | 29.25 | 81.25 | 468.00 | 621.87 | 1415.26 |
| 53 | 16.41 .56 | 28.53 | 28.93 | 29.81 | 82.81 . | 477.00 | 633.83 | 1442.47 |
| 54 | 1672.54 | 29.06 | 29.48 | 30.37 | 84.37 | 486.00 | 645.79 | 1469.69 |
| 55 | 1703.51 | 29.60 | 30.02 | 30.94 | 85.94 | 495.00 | 657.75 | 1496.90 |
| 56 | 1734.48 | 30.14 | 30.57 | 31.50 | 87.50 | 504.00 | 669.71 | 1524.12 |
| 57 | 1765.45 | 30.68 | 31.12 | 32.06 | 89.06 | 513.00 | 681.67 | 1551.34 |
| 58 | 1896.43 | 31.21 | 31.66 | 32.62 | 90.62 | 522.00 | 693.63 | 1578.55 |
| 59 | 1821.40 | 31.76 | 32.21 | 33.19 | 92.19 | 531.00 | 705.59 | 1605.77 |
| 60 | 1858.37 | 32.29 | 32.75 | 33.75 | 93.75 | 540.00 | 717.55 | 1632.99 |

nautical square leagues into different geographical square measures.

| Nautical Square Leagues. $20=1^{\circ} \mathrm{E}$. | Sq. Kilometres. | Austrian <br> Sq. Miles. | Prussian Sq. Miles. | German Sq. Miles. $15=1^{\circ}$ Eq. | French Square Leagues. $25=1^{\circ}$ Eq. | Geograph'l or Nautical Sq. Miles. $60=1^{\circ} \mathrm{E}_{\mathrm{T}}$. | English <br> square <br> Miles. | Russian Square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 1889.35 | 32.83 | 33.30 | 34.31 | 95.31 | 549.00 | 729.51 | 1660.20 |
| 62 | 1920.32 | 33.37 | 33.85 | 34.87 | 96.87 | 558.00 | 741.47 | 1687.42 |
| 63 | 1951.29 | 33.91 | 34.39 | 35.44 | 98.44 | 567.00 | 753.43 | 1714.64 |
| 64 | 1982.26 | 34.45 | 34.94 | 36.00 | 100.00 | 576.00 | 765.38 | 1741.85 |
| 65 | 2013.24 | 34.98 | 35.48 | 36.56 | 101.56 | 585.00 | 777.34 | 1769.07 |
| 66 | 2044.21 | 35.52 | 36.03 | 37.12 | 103.12 | 594.00 | 789.30 | 1796.39 |
| 67 | 2075.18 | 36.06 | 36.57 | 37.69 | 104.69 | 603.00 | 801.26 | 1823.50 |
| 68 | 2106.16 | 36.60 | 37.12 | 38.25 | 106.25 | 612.00 | 813.22 | 1850.72 |
| 69 | 2137.13 | 37.14 | 37.67 | 38.81 | 107.81 | 621.00 | ع25.18 | 1877.93 |
| 70 | 2168.10 | 37.68 | 38.21 | 39.37 | 109.37 | 630.00 | 837.74 | 1905.15 |
| 71 | 2199.08 | 38.21 | 38.76 | 39.94 | 110.94 | 639.00 | 849.10 | 1932.37 |
| 72 | 2230.05 | 38.75 | 39.30 | 40.50 | 112.50 | 648.00 | 861.06 | 1959.58 |
| 73 | 2261.02 | 39.29 | 39.85 | 41.06 | 114.06 | 657.00 | 873.02 | 1986.80 |
| 74 | 2291.99 | 39.83 | 40.40 | 41.62 | 115.62 | 666.00 | 884.98 | 2014.02 |
| 75 | 2322.97 | 40.37 | 40.94 | 42.19 | 117.19 | 675.00 | 896.93 | 2041.23 |
| 76 | 2353.94 | 40.91 | 41.49 | 42.75 | 118.75 | 684.00 | 908.89 | 2068.45 |
| 77 | 2384.91 | 41.44 | 42.03 | 43.31 | 120.31 | 693.00 | 920.85 | 2095.67 |
| 78 | 2415.89 | 41.98 | 42.58 | 43.87 | 121.87 | 702.00 | 932.81 | 2122.88 |
| 79 | 2446.86 | 42.52 | 43.13 | 44.44 | 123.44 | 711.00 | 944.77 | 2150.10 |
| 80 | 2477.83 | 43.06 | 43.67 | 45.00 | 125.00 | 720.00 | 956.73 | 2177.32 |
| 81 | 2508.81 | 43.60 | 44.22 | 45.56 | 126.56 | 729.00 | 968.69 | 2204.53 |
| 82 | 2539.78 | 44.13 | 44.76 | 46.12 | 128.12 | 738.00 | 980.65 | 2231.75 |
| 83 | 2570.75 | 44.67 | 45.31 | 40.69 | 129.69 | 747.00 | 992.61 | 2258.97 |
| 84 | 2601.72 | 45.21 | 45.85 | 47.25 | 131.25 | 756.00 | 1004.57 | 2286.18 |
| 85 | 2632.70 | 45.75 | 46.40 | 47.81 | 132.81 | 765.00 | 1016.53 | 2313.40 |
| 86 | 2663.67 | 46.29 | 46.95 | 48.37 | 134.37 | 774.00 | 1028.49 | 2340.61 |
| 87 | 2694.64 | 46.83 | 47.49 | 48.94 | 135.94 | 783.00 | 1040.44 | 2367.83 |
| 88 | 2725.62 | 47.36 | 48.04 | 49.50 | 137.50 | 792.00 | 1052.40 | 2395.05 |
| 89 | 2756.59 | 47.90 | 48.58 | 50.06 | 139.06 | 801.00 | 1064.36 | 2422.26 |
| 90 | 2787.56 | 48.44 | 49.13 | 50.62 | 140.62 | 810.00 | 1076.32 | 2449.48 |
| 91 | 2818.53 | 48.98 | 49.68 | 51.19 | 142.19 | 819.00 | 1088.28 | 2476.70 |
| 92 | 2849.51 | 49.52 | 50.22 | 51.75 | 143.75 | 828.00 | 1100.24 | 2503.91 |
| 93 | 2880.48 | 50.05 | 50.77 | 52.31 | 145.31 | 837.00 | 1112.20 | 2531.13 |
| 94 | 2911.45 | 50.59 | 51.31 | 52.87 | 146.87 | 846.00 | 1124.16 | 2558.35 |
| 95 | 2942.43 | 51.13 | 51.86 | 53.44 | 148.44 | 855.00 | 1136.12 | 2585.56 |
| 96 | 2973.40 | 51.67 | 52.41 | 54.00 | 150.00 | 864.00 | 1148.08 | 2612.78 |
| 97 | 3004.37 | 52.21 | 52.95 | 54.56 | 151.5 ; | 873.00 | 1160.04 | 2640.00 |
| 98 | 3035.34 | 52.75 | 53.50 | 55.12 | 153.12 | 882.00 | 1171.99 | 2667.21 |
| 99 | 3066.32 | 53.28 | 54.04 | 55.69 | 154.69 | 891.00 | 1183.95 | 2694.43 |
| 100 | 3097.29 | 53.82 | 54.59 | 56.25 | 156.25 | 900.00 | 1195.91 | 2721.64 |

## VI. french square leagues into different geggraphical square measures

| $\begin{aligned} & \text { French } \\ & \text { square. } \\ & \text { Leaves. } \\ & 25=1^{\circ} \text { Eq. } \end{aligned}$ | sq. Kilometres. | Austrian sq. Miles. | Prussian Sq. Miles. | $\begin{aligned} & \text { German } \\ & \text { Sq. Miles. } \\ & 1 b=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical square Leagues. $20=1^{\circ} \mathrm{Eq}$ | Geograph'l <br> or Natulucal <br> Sy Miles. $60=1^{\circ} \mathrm{Eq}$ | English square Miles. | Russian Square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 19822.63 | 344.463 | 349.370 | 360.000 | 640.000 | 5760.00 | 7653.844 | 17418.52 |
| 2,000 | 39645.27 | 688.927 | 698.739 | 720.000 | 1280.000 | 11520.00 | 15307.69 | 34837.05 |
| 3,000 | 59467.90 | 1033.390 | 1048.109 | 1080.000 | 1920.000 | 17250.00 | 22961.53 | 52255.57 |
| 4,000 | 79290.54 | 1377.853 | 1397.479 | $1+40.000$ | 2560.000 | 23040.00 | 30615.37 | 69674.09 |
| 5,000 | 99113.15 | 1722.317 | 1746.848 | 1800.000 | 3200.000 | 28800.00 | 38269.22 | 87092.61 |
| 6,000 | 118935.8 | 2066.781 | 2096.218 | 2160.000 | 3840.000 | 34560.00 | 45923.06 | 104511.1 |
| 7,000 | 138758.4 | 2411.244 | 2445.588 | 2520.000 | 4480.000 | 40320.00 | 53576.90 | 121929.7 |
| 8,000 | 158581.1 | 2755.708 | 2794.957 | 2880.000 | 5120.000 | 46080.00 | 61230.75 | 139348.2 |
| 9,000 | 178403.7 | 3100.171 | 3144.307 | 3240.000 | 5760.000 | 51840.00 | 68884.59 | 156766.7 |
| 10,000 | 198226.3 | 344.635 | 34.93697 | 3600.000 | 6400.000 | 57600.00 | 76538.43 | 174185.2 |
| 100 | 1982.26 | 34.45 | 34.94 | 36.00 | 64.00 | 576.00 | 765.38 | 1741.85 |
| 200 | 3964.53 | 68.89 | 69.87 | 72.00 | 128.00 | 1152.00 | 1530.77 | 3483.71 |
| 300 | 5946.79 | 103.34 | 104.81 | 108.00 | 192.00 | 1728.00 | 2296.15 | 5225.56 |
| 400 | 7929.05 | 137.79 | 139.75 | 144.00 | 256.00 | 2304.00 | 3061.54 | 6967.41 |
| 500 | 9911.32 | 172.23 | 174.68 | 180.00 | 320.00 | 2880.00 | 3826.92 | 8709.26 |
| 600 | 11893.58 | 206.68 | 209.62 | 216.00 | 384.00 | 3456.00 | 4592.31 | 10451.11 |
| 700 | 13875.84 | 241.12 | 24.56 | 252.00 | 448.00 | 4032.00 | 5357.69 | 12192.97 |
| 800 | 1:858.11 | 275.57 | 279.50 | 288.00 | 512.00 | 4608.00 | 6123.08 | 13934.82 |
| 900 | 17840.37 | 310.02 | 314.43 | 324.00 | 576.00 | 5184.00 | 6888.46 | 15676.67 |
| 1000 | 19822.63 | 344.46 | 349.37 | 360.00 | 640.00 | 5760.00 | 7653.84 | 17418.52 |
| 1 | 19.82 | 0.34 | - 0.35 | 0.36 | 0.64 | 5.76 | 7.65 | 17.42 |
| 2 | 39.65 | 0.69 | 0.70 | 0.72 | 1.28 | 11.52 | 15.31 | 34.84 |
| 3 | 59.47 | 1.03 | 1.05 | 1.08 | 1.92 | 17.28 | 22.96 | 52.26 |
| 4 | 79.29 | 1.38 | 1.40 | 1.44 | 2.56 | 23.04 | 30.62 | 69.67 |
| 5 | 99.11 | 1.72 | 1.75 | 1.80 | 3.20 | 28.80 | 38.27 | 87.09 |
| 6 | 118.94 | 2.07 | 2.10 | 2.16 | 3.84 | 34.56 | 45.92 | 104.51 |
| 7 | 138.76 | 2.41 | 2.45 | 2.52 | 4.48 | 40.32 | 53.58 . | 121.93 |
| 8 | 158.58 | 2.76 | 2.79 | 2.88 | 5.12 | 46.08 | 61.23 | 139.35 |
| 9 | 178.40 | 3.10 | 3.14 | 3.24 | 5.76 | 51.84 | 68.88 | 156.77 |
| 10 | 198.23 | 3.44 | 3.49 | 3.60 | 6.40 | 57.60 | 76.54 | 174.18 |
| 11 | 218.05 | 3.79 | 3.84 | 3.96 | 7.04 | 63.36 | 84.19 | 191.60 |
| 12 | 237.87 | 4.13 | 4.19 | 4.32 | 7.68 | 69.12 | 91.85 | 209.02 |
| 13 | 257.69 | 4.48 | 4.54 | 4.68 | 8.32 | 74.85 | 99.50 | 226.44 |
| 14 | 277.52 | 4.82 | 4.59 | 5.04 | 8.96 | 80.64 | 107.15 | 243.86 |
| 15 | 297.34 | 5.17 | 5.24 | 5.40 | 9.60 | 86.40 | 114.81 | 261.28 |
| 16 | 317.16 | 5.51 | 5.59 | 5.76 | 10.24 | 92.16 | 122.46 | 278.70 |
| 17 | 336.98 | 5.86 | 5.94 | 6.12 | 10.88 | 97.92 | 130.12 | 296.11 |
| 18 | 356.81 | 6.20 | 6.29 | 6.48 | 11.52 | 103.68 | 137.77 | 313.53 |
| 19 | 376.63 | 6.54 | 6.64 | 6.84 | 12.16 | 109.44 | 145.42 | 330.95 |
| 20 | 396.45 | 6.89 | 6.99 | 7.20 | 12.80 | 115.20 | 153.08 | 348.37 |

French square leagues into different geographlcal square measures.

| French Square Leagues. $25=1^{\circ} \mathrm{Eq}$. | Sq. Kilometres. | Austrian Sq. Miles. | Prussian <br> Sq. Miles. | Germian <br> Sq. Miles. <br> $15=1^{\circ} \mathrm{Eq}$. | Nautical square Leagues. $20=1^{\circ}$ Eq. | $\left\lvert\, \begin{gathered} \text { Geograph's } \\ \text { or Nautica } \\ \text { Sq. Miles. } \\ 60=1^{\circ} \text { Eq. } \end{gathered}\right.$ | English <br> Square <br> Miles. | Russian <br> square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 416.28 | 7.23 | 7.34 | 7.56 | 13.44 | 120.96 | 160.73 | 365.79 |
| 22 | 436.10 | 7.58 | 7.69 | 7.92 | 14.08 | 126.72 | 168.38 | 383.21 |
| 23 | 455.92 | 7.92 | 8.04 | 8.28 | 14.72 | 132.48 | 176.04 | 400.63 |
| 24 | 475.74 | 8.27 | 8.38 | 8.64 | 15.36 | 13824 | 183.69 | 418.04 |
| 25 | 495.57 | 8.61 | 8.73 | 9.00 | 16.00 | 144.00 | 191.35 | 435.46 |
| 26 | 515.39 | 8.96 | 9.08 | 0.36 | 16.64 | 149.76 | 199.00 | 452.88 |
| 27 | 535.21 | 9.30 | 9.43 | 9.72 | 17.28 | 155.52 | 206.65 | 470.30 |
| 28 | 555.03 | 9.65 | 9.78 | 10.08 | 17.92 | 161.28 | 214.31 | 487.72 |
| 29 | 574.86 | 9.99 | 10.13 | 10.44 | 18.56 | 167.04 | 221.96 | 505.14 |
| 30 | 594.68 | 10.33 | 10.48 | 10.80 | 19.20 | 172.80 | 229.62 | 522.56 |
| 31 | 614.50 | 10.68 | 10.83 | 11.16 | 19.84 | 178.56 | 237.27 | 539.97 |
| 32 | 634.32 | 11.02 | 11.18 | 11.52 | 20.48 | 184.32 | 244.92 | 557.39 |
| 33 | 654.15 | 11.37 | 11.53 | 11.88 | 21.12 | 190.08 | 252.58 | 574.81 |
| 34 | 673.97 | 11.71 | 11.88 | 12.24 | 21.76 | 195.84 | 260.23 | 592.23 |
| 35 | 693.79 | 12.06 | 12.23 | 12.60 | 22.40 | 201.60 | 267.88 | 609.65 |
| 36 | 713.61 | 12.40 | 12.58 | 12.96 | 23.04 | 207.36 | 275.54 | 627.07 |
| 37 | 733.44 | 12.75 | 12.93 | 13.32 | 23.68 | 213.12 | 283.19 | 644.49 |
| 38 | 753.26 | 13.09 | 13.28 | 13.68 | 24.32 | 218.88 | 290.85 | 661.90 |
| 39 | 773.08 | 13.43 | 13.63 | 14.04 | 24.96 | 224.64 | 298.50 | 679.32 |
| 40 | 792.91 | 13.78 . | 13.97 | 14.40 | 25.60 | 230.40 | 306.15 | 696.74 |
| 41 | 812.73 | 14.12 | 14.32 | 14.76 | 26.24 | 236.16 | 313.81 | 714.16 |
| 42 | 832.55 | 14.47 | 14.67 | 15.12 | 26.88 | 241.92 | 321.46 | 731.58 |
| 43 | 852.37 | 14.81 | 15.02 | 15.48 | 27.52 | 247.68 | 329.12 | 749.00 |
| 44 | 872.20 | 15.16 | 15.37 | 15.84 | 28.16 | 253.44 | 336.77 | 766.41 |
| 45 | 892.02 | 15.50 | 15.72 | 16.20 | 28.80 | 259.20 | 344.42 | 783.83 |
| 46 | 901.84 | 15.85 | 16.07 | 16.56 | 29.44 | 264.96 | 352.08 | 801.25 |
| 47 | 931.66 | 16.19 | 16.42 | 16.92 | 30.08 | 270.72 | 359.73 | 818.67 |
| 48 | 951.49 | 16.53 | 16.77 | 17.28 | 30.72 | 276.48 | 367.38 | 836.09 |
| 49 | 971.31 | 16.88 | 17.12 | 17.64 | 31.36 | 282.24 | 375.04 | 853.51 |
| 50 | 991.13 | 17.22 | 17.47 | 18.00 | 32.00 | 288.00 | 382.69 | 870.93 |
| 51 | 1010.95 | 17.57 | 17.82 | 18.36 | 32.64 | 293.76 | 390.35 | 888.34 |
| 52 | 1030.78 | 17.91 | 18.17 | 18.72 | 33.28 | 299.52 | 398.00 | 905.76 |
| 53 | 1050.60 | 18.26 | 18.52 | 19.08 | 33.92 | 305.28 | 405.65 | 923.18 |
| 54 | 1070.42 | 18.60 | 18.87 | 19.44 | 34.56 | 311.04 | 413.31 | 940.60 |
| 55 | 1090.24 | 18.95 | 19.22 | 19.80 | 35.20 | 316.80 | 420.96 | 958.02 |
| 56 | 1110.07 | 19.29 | 19.56 | 20.16 | 35.84 | 322.56 | 428.62 | 975.44 |
| 57 | 1129.89 | 19.63 | 19.91 | 20.52 | 36.48 | 328.32 | 436.27 | 992.86 |
| 58 | 1149.71 | 19.98 | 20.26 | 20.88 | 37.12 | 334.08 | 443.92 | 1010.27 |
| 59 | 1169.54 | 20.32 | 20.61 | 21.24 | 37.76 | 339.84 | 451.58 | 1027.69 |
| 60 | 1189.36 | 20.67 | 20.96 | 21.60 | 38.40 | 345.60 | 459.23 | 1045.11 |

554
FRENCH SQUARE LEAGUES INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| French Square Leagues. $25=1^{\circ} \mathrm{Eq}$ | Sq. Kilometres. | Austrian Sq. Miles. | Prussian <br> Sq. Miles. | $\begin{aligned} & \text { German } \\ & \text { Sq. Miles. } \\ & 15=1^{\circ} \text { Eq. } \end{aligned}$ | Nautical square Leagues. $20=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical Sq. Miles. $60=1^{\circ}$ Eq. | English Square Miles. | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 1209.18 | 21.01 | 21.31 | 21.96 | 39.04 | 351.36 | 466.88 | 1062.53 |
| 62 | 1229.00 | 21.36 | 21.66 | 22.32 | 39.68 | 357.12 | 474.54 | 1079.95 |
| 63 | 1248.83 | 21.70 | 22.01 | 22.68 | 40.32 | 362.88 | 482.19 | 1097.37 |
| 64 | 1268.65 | 22.05 | 22.36 | 23.04 | 40.96 | 368.64 . | 489.85 | 1114.79 |
| 65 | 1288.47 | 22.39 | 22.71 | 23.40 | 41.60 | 374.40 | 497.50 | 1132.20 |
| 66 | 1308.29 | 22.73 | 23.06 | 23.76 | 42.24 | 380.16 | 505.15 | 1149.62 |
| 67 | 1328.12 | 23.08 | 23.41 | 24.12 | 42.88 | 385.92 | 512.81 | 1167.0.4 |
| 68 | 1347.94 | 23.42 | 23.76 | 24.48 | 43.52 | 391.68 | 520.46 | 1184.46 |
| 69 | 1367.76 | 23.77 | 24.11 | 24.84 | 44.16 | 397.4 | 528.12 | 1201.88 |
| 70 | 1387.58 | 24.11 | 24.46 | 25.20 | 44.80 | 403.20 | 535.77 | 1219.30 |
| 71 | 1407.41 | 24.46 | 24.81 | 25.56 | 45.44 | 408.96 | 543.42 | 1236.72 |
| 72 | $14 \cdot 27.23$ | 24.80 | 25.15 | 25.92 | 46.08 | 414.72 | 551.08 | 1254.13 |
| 73 | 1447.05 | 25.15 | 25.50 | 26.28 | 46.72 | 420.48 | 558.73 | 1271.55 |
| 74 | 1466.87 | 25.49 | 25.85 | 26.64 | 47.36 | 426.24 | 566.38 | 1288.97 |
| 75 | 1486.70 | 25.83 | 26.20 | 27.00 | 48.00 | 432.00 | 574.04 | 1306.39 |
| 76 | 1506.52 | 26.18 | 26.55 | 27.36 | 48.64 | 437.76 | 581.69 | 1323.81 |
| 77 | 1526.34 | 26.52 | 26.90 | 27.72 | 49.28 | 443.52 | 589.35 | 1341.23 |
| 78 | 1546.17 | 26.87 | 27.25 | 28.08 | 49.92 | 449.28 | 597.00 | 1358.64 |
| 79 | 1565.99 | 27.21 | 27.60 | 28.44 | 50.56 | +45.04 | 604.65 | 1376.06 |
| 80 | 1585.81 | 27.56 | 27.95 | 28.80 | 51.20 | 460.80 | 612.31 | 1393.48 |
| 81 | 1605.63 | 27.90 | 28.30 | 29.16 | 51.84 | 466.56 | 619.96 | 1410.90 |
| 82 | 1625.46 | 28.25 | 28.65 | 29.52 | 52.48 | 472.32 | 627.62 | 1428.32 |
| 83 | 1645.28 | 25.59 | 29.00 | 29.88 | 53.12 | 478.08 | 635.27 | $1+45.74$ |
| 84 | 1665.16 | 28.93 | 29.35 | 30.24 | 53.76 | 483.84 | 642.92 | 1463.16 |
| 85 | 1684.92 | 29.28 | 29.70 | 30.60 | 54.40 | 489.60 | 650.58 | 1480.57 |
| 86 | 1704.75 | 29.62 | 30.05 | 30.96 | 55.04 | 495.36 | 658.23 | 1497.99 |
| 87 | 1724.57 | 29.97 | 30.40 | 31.32 | 55.78 | 501.12 | 665.88 | 1515.41 |
| 88 | 1744.39 | 30.31 | 30.74 | 31.68 | 56.32 | 506.88 | 673.54 | 1532.83 |
| 89 | 1764.21 | 30.66 | 31.09 | 32.04 | 56.96 | 512.64 | 681.19 | 1550.25 |
| 90 | 1784.04 | 31.00 | 31.44 | 33.40 | 57.60 | 518.40 | 688.85 | 1567.67 |
| 91 | 1803.86 | 31.35 | 31.79 | 32.76 | 58.24 | 524.16 | 696.50 | 1585.09 |
| 92 | 1833.65 | 31.69 | 32.14 | 33.12 | 58.88 | 529.92 | 704.15 | 1602.50 |
| 93 | 1843.51 | 32.04 | 32.49 | 33.48 | 59.52 | 535.68 | 711.81 | 1619.92 |
| 94 | 1863.33 | 32.38 | 32.84 | 33.84 | 60.16 | 541.44 | 719.46 | 1637.3.4 |
| 95 | 1883.15 | 32.72 | 33.19 | 34.20 | 60.80 | 547.20 | 727.12 | 1654.76 |
| 96 | 1902.97 | 33.07 | 33.54 | 34.56 | 61.44 | 552.96 | 734.77 | 1672.18 |
| 97 | 1922.80 | 33.41 | 33.89 | 34.92 | 62.08 | 558.72 | 742.42 | 1689.60 |
| 98 | 1942.62 | 33.76 | 34.24 | 35.28 | 62.72 | 564.48 | 750.08 | 1707.02 |
| 99 | 1962.44 | 34.10 | 34.59 | 35.64 | 63.36 | 570.24 | 757.73 | 1724.43 |
| 100 | 1982.26 | 34.45 | 34.94 | 36.00 | 64.00 | 576.00 | 765.38 | 1741.85 |
|  |  |  |  |  |  |  |  |  |

JI. geographical or nautical square miles into different geographical square measures.

| Geograph <br> or Naut. <br> Sq . Miles. <br> $60=1^{\circ} \mathrm{Eq}$ 。 | Sq. Kilometres. | Austrian Sq. Miles. | Prussian Sq. Miles. | German Sq. Miles. $15=1^{\circ} \mathrm{Eq}$. | Nautical Square Leagues. $20=1^{\circ} \mathrm{Eq}$. | French Square Leagues. $25=1^{\circ} \mathrm{Eq}$ | English Square Miles. | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 3441.43 | 59.80268 | 60.65446 | 62.5000 | 111.1111 | 173.6111 | 1328.792 | 3024.049 |
| 2,000 | 6882.86 | 119.6054 | 121.3089 | 125.000 | 222.2222 | 347.2222 | 2657.555 | 6048.098 |
| 3,000 | 10324.30 | 179.4081 | 181.9634 | 187.500 | 333.3333 | 520.8333 | 3986.377 | 9072.147 |
| 4,000 | 13765.73 | 239.2107 | 242.6178 | 250.000 | 444.4444 | 694.4444 | 5315.169 | 12096.20 |
| 5,000 | 17207.16 | 299.0134 | 303.2723 | 312.500 | 555.5556 | 868.0556 | 6643.964 | 15120.25 |
| 6,000 | 20648.59 | 358.8161 | 363.9268 | 375.000 | 666.6667 | 1041.667 | 7972.754 | 18144.29 |
| 7,000 | 24090.02 | 418.6188 | 424.5812 | 437.500 | 777.7778 | 1215.278 | 9301.546 | 21168.34 |
| 8,000 | 27531.45 | 478.4215 | 485.2357 | 500.000 | 888.8889 | 1388.889 | 10630.34 | 24192.39 |
| 9,000 | 30972.89 | 538.2242 | 545.8901 | 562.500 | 1000.000 | 1562.500 | 11959.13 | 27216.44 |
| 10,000 | 34414.32 | 598.0268 | 606.5446 | 625.000 | 1111.111 | 1736.111 | 13287.92 | 30240.49 |
| 100 | 344.14 | 5.98 | 6.07 | 6.25 | 11.11 | 17.36 | 132.88 | 302.40 |
| 200 | 688.29 | 11.96 | 12.13 | 12.50 | 22.22 | 34.72 | 265.76 | 604.81 |
| 300 | 1032.43 | 17.94 | 18.20 | 18.75 | 33.33 | 52.08 | 398.64 | 907.21 |
| 400 | 1376.57 | 23.92 | 24.26 | 25.00 | 44.44 | 69.44 | 531.52 | 1209.62 |
| 500 | 1720.72 | 29.90 | 30.33 | 31.25 | 55.56 | 86.81 | 664.40 | 1512.02 |
| 600 | 2064.86 | 35.88 | 36.39 | 37.50 | 66.67 | 104.17 | 797.28 | 1814.43 |
| 700 | 2409.00 | 41.86 | 42.46 | 43.75 | 77.78 | 121.53 | 930.15 | 2116.83 |
| 800 | 2753.15 | 47.84 | 48.52 | 50.00 | 88.89 | 138.89 | 1063.03 | 2419.24 |
| 900 | 3097.29 | 53.82 | 54.59 | 56.25 | 100.00 | 156.25 | 1195.91 | 2721.64 |
| 1000 | 3441.43 | 59.80 | 60.65 | 62.50 | 111.11 | 173.61 | 1328.79 | 3024.05 |
| 1 | 3.44 | 0.06 | 0.06 | 0.06 | 0.11 | 0.17 | 1.33 | 3.02 |
| 2 | 6.88 | 0.12 | 0.12 | 0.12 | 0.22 | 0.35 | 2.66 | 6.05 |
| 3 | 10.32 | 0.18 | 0.18 | 0.19 | 0.33 | 0.52 | 3.99 | 9.07 |
| 4 | 13.77 | 0.24 | 0.24 | 0.25 | 0.44 | 0.69 | 5.32 | 12.10 |
| 5 | 17.21 | 0.30 | 0.30 | 0.31 | 0.56 | 0.87 | 6.64 | 15.12 |
| 6 | 20.65 | 0.36 | 0.36 | 0.37 | 0.67 | 1.04 | 7.97 | 18.14 |
| 7 | 24.09 | 0.42 | 0.42 | 0.44 | 0.78 | 1.22 | 9.30 | 21.17 |
| 8 | 27.53 | 0.48 | 0.49 | 0.50 | 0.89 | 1.39 | 10.63 | 24.19 |
| 9 | 30.97 | 0.54 | 0.55 | 0.56 | 1.00 | 1.56 | 11.96 | 27.22 |
| 10 | 34.41 | 0.60 | 0.61 | 0.62 | 1.11 | 1.74 | 13.29 | 30.24 |
| 11 | 37.86 | 0.66 | 0.67 | 0.69 | 1.22 | 1.91 | 14.62 | 33.26 |
| 12 | 41.30 | 0.72 | 0.73 | 0.75 | 1.33 | 2.08 | 15.95 | 36.29 |
| 13 | 44.74 | 0.78 | 0.79 | 0.81 | 1.44 | 2.26 | 17.27 | 39.31 |
| 14 | 48.18 | 0.84 | 0.85 | 0.87 | 1.56 | 2.43 | 18.60 | 42.34 |
| 15 | 51.62 | 0.90 | 0.91 | 0.94 | 1.67 | 2.60 | 19.93 | 45.36 |
| 16 | 55.06 | 0.96 | 0.97 | 1.00 | 1.78 | 2.78 | 21.26 | 48.38 |
| 17 | 58.50 | 1.02 | 1.03 | 1.06 | 1.89 | 2.95 | 22.59 | 51.41 |
| 18 | 61.95 | 1.08 | 1.09 | 1.12 | 2.00 | 3.12 | 23.92 | 54.43 |
| 19 | 65.39 | 1.14 | 1.15 | 1.19 | 2.11 | 3.30 | 25.25 | 57.46 |
| 20 | 68.83 | 1.20 | 1.21 | 1.25 | 2.22 | 3.47 | 26.58 | 60.48 |

geographical or nautical square miles into different geographical square measures.

| Geograph. or Naut. Sy. Miles. $60=1^{\circ} \mathrm{Eq}$ | Sq. Kilometres. | Austrian sq. Miles. | Prussiau Sq. Miles. | $\begin{aligned} & \text { Gernian } \\ & \text { sq. Miles. } \\ & 10=1^{\circ} \mathrm{Eq} . \end{aligned}$ | $\begin{gathered} \text { Natical } \\ \text { square } \\ \text { Leaunes. } \\ 20=1^{\circ} \mathbf{E q} . \end{gathered}$ | French Square Leagues. $25=1^{\circ} \mathrm{E} 4$. | Euglish <br> Square <br> Miles. | Russiau <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 72.27 | 1.26 | 1.27 | 1.31 | 2.33 | 3.65 | 27.90 | 63.51 |
| 22 | 75.71 | 1.32 | 1.33 | 1.37 | 2.44 | 3.82 | 29.23 | 66.53 |
| 23 | 79.15 | 1.38 | 1.40 | 1.44 | 2.56 | 3.99 | 30.56 | 69.55 |
| 24 | 82.59 | 1.44 | 1.46 | 1.50 | 2.67 | 4.17 | 31.89 | 72.58 |
| 25 | 86.04 | 1.50 | 1.52 | 1.56 | 2.78 | 4.34 | 33.28 | 75.60 |
| 26 | 89.48 | 1.55 | 1.58 | 1.62 | 2.89 | 4.51 | 34.55 | 78.63 |
| 27 | 92.92 | 1.61 | 1.64 | 1.69 | 3.00 | 4.69 | 35.88 | 81.65 |
| 28 | 96.36 | 1.67 | 1.70 | 1.75 | 3.11 | 4.86 | 37.21 | 84.67 |
| 29 | 99.80 | 1.73 | 1.76 | 1.81 | 3.22 | 5.03 | 38.53 | 87.70 |
| 30 | 103.24 | 1.79 | 1.82 | 1.87 | 3.33 | 5.21 | 39.86 | 90.72 |
| 31 | 106.68 | 1.85 | 1.88 | 1.94 | 3.44 | 5.38 | 41.19 | 93.75 |
| 32 | 110.13 | 1.91 | 1.94 | 2.00 | 3.56 | 5.56 | 42.52 | 96.77 |
| 33 | 113.57 | 1.97 | 2.00 | 2.06 | 3.67 | 5.72 | 43.85 | 99.79 |
| 34 | 117.01 | 2.03 | 2.06 | 2.12 | 3.78 | 5.90 | 45.18 | 102.82 |
| 35 | 120.45 | 2.09 | 2.12 | 2.19 | 3.89 | 6.08 | 46.51 | 105.84 |
| 36 | 123.89 | 2.15 | 2.18 | 2.25 | 4.00 | 6.25 | 47.84 | 108.87 |
| 37 | 127.33 | 2.21 | 2.24 | 2.31 | 4.11 | 6.42 | 49.17 | 111.89 |
| 38 | 130.77 | 2.27 | 2.30 | 2.37 | 4.22 | 6.60 | 50.49 | 114.91 |
| 39 | 134.22 | 2.33 | 2.37 | 2.44 | 4.33 | 6.77 | 51.82 | 117.94 |
| 40 | 137.66 | 2.39 | 2.43 | 2.50 | 4.44 | 6.94 | 53.15 | 120.96 |
| 41 | 141.10 | 2.45 | 2.49 | 2.56 | 4.56 | 7.12 | 54.48 | 123.99 |
| 42 | 144.54 | 2.51 | 2.55 | 2.62 | 4.67 | 7.29 | 55.81 | 127.01 |
| 43 | 147.98 | 2.57 | 2.61 | 2.69 | 4.78 | 7.47 | 57.14 | 13003 |
| 44 | 151.42 | 2.63 | 2.67 | 2.75 | 4.89 | 7.64 | 58.47 | 133.06 |
| 45 | 154.86 | 2.69 | 2.73 | 2.81 | 5.00 | 7.81 | 59.80 | 136.08 |
| 46 | 158.31 | 2.75 | 2.79 | 2.87 | 5.11 | 7.99 | 61.12 | 139.11 |
| 47 | 161.75 | 2.81 | 2.85 | 2.94 | 5.22 | 8.16 | 62.45 | 142.13 |
| 48 | 165.19 | 2.87 | 2.91 | 3.00 | 5.33 | 8.33 | 63.78 | 145.15 |
| 49 | 168.63 | 2.93 | 2.97 | 3.06 | 5.44 | 8.51 | 65.11 | 148.18 |
| 50 | 172.07 | 2.99 | 3.03 | 3.12 | 5.56 | 8.68 | 66.44 | 151.20 |
| 51 | 175.51 | 3.05 | 3.09 | 3.19 | 5.67 | 8.85 | 67.77 | 154.23 |
| 52 | 178.96 | 3.11 | 3.15 | 3.25 | 5.78 | 9.03 | 69.10 | 157.95 |
| 53 | 182.40 | 3.17 | 3.21 | 3.31 | 5.89 | 9.20 | 70.43 | 160.27 |
| 54 | 185.84 | 3.23 | 3.28 | 3.37 | 6.00 | 9.37 | 71.75 | 163.30 |
| 55 | 189.28 | 3.29 | 3.34 | 3.44 | 6.11 | 9.55 | 73.08 | 166.32 |
| 56 | 192.72 | 3.35 | 3.40 | 3.50 | 6.22 | 9.72 | 74.41 | 169.35 |
| 57 | 196.16 | 3.41 | 3.46 | 3.56 | 6.33 | 9.90 | 75.74 | 172.37 |
| 58 | 199.60 | 3.47 | 3.52 | 3.62 | 6.44 | 10.67 | 77.07 | 175.39 |
| 59 | 203.04 | 3.53 | 3.58 | 3.69 | 6.56 | 10.24 | 78.40 | 178.42 |
| 60 | 206.49 | 3.59 | 3.64 | 3.75 | 6.67 | 10.42 | 79.73 | 181.44 |

geographical or nautical square mlles into different geographical SQUARE MEASURES.

| Geograph. or Naut. Sq. Miles. $60=1^{\circ} \mathrm{Eq}$. | Sq. Kilometres. | Austrian Sq. Miles. | Prussian Sq. Miles. | $\begin{aligned} & \text { German } \\ & \mathrm{Sq} . \mathrm{Milites} . \\ & 10=1^{\circ} \mathrm{Eq} . \end{aligned}$ | Nautical Square Leagues. $20=1^{\circ} \mathrm{Eq}$. | $\begin{gathered} \text { French } \\ \text { Square } \\ \text { Leagues. } \\ 25=1^{0} \text { Eq. } \end{gathered}$ | English Square Miles. | Russian square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 209.93 | 3.65 | 3.70 | 3.81 | 6.78 | 10.59 | 81.06 | 184.47 |
| 62 | 213.37 | 3.71 | 3.76 | 3.87 | 6.89 | 10.76 | 82.39 | 187.49 |
| 63 | 216.81 | 3.77 | 3.82 | 3.94 | 7.00 | 10.94 | 83.71 | 190.52 |
| 64 | 220.25 | 3.83 | 3.88 | 4.00 | 7.11 | 11.11 | 85.04 | 193.54 |
| 65 | 223.69 | 3.89 | 3.94 | 4.06 | 7.22 | 11.28 | 86.37 | 196.56 |
| 66 | 227.13 | 3.95 | 4.00 | 4.12 | 7.33 | 11.46 | 87.70 | 199.59 |
| 67 | 230.58 | 4.01 | 4.06 | 4.19 | 7.44 | 11.63 | 89.03 | 202.61 |
| 68 | 234.02 | 4.07 | 4.12 | 4.25 | $7.56{ }^{\circ}$ | 11.81 | 90.36 | 205.64 |
| 69 | 237.46 | 4.13 | 4.19 | 4.31 | 7.67 | 11.98 | 91.69 | 208.66 |
| 70 | 240.90 | 4.19 | 4.25 | 4.37 | 7.78 | 12.15 | 93.02 | 211.68 |
| 71 | 244.34 | 4.25 | 4.31 | 4.44 | 7.89 | 12.33 | 94.34 | 214.71 |
| 72 | 247.78 | 4.31 | 4.37 | 4.50 | 8.00 | 12.50 | 95.67 | 217.73 |
| 73 | 251.22 | 4.37 | 4.43 | 4.56 | 8.11 | 12.67 | 97.00 | 220.76 |
| 74 | 254.67 | 4.43 | 4.49 | 4.62 | 8.22 | 12.85 | 98.33 | 223.78 |
| 75 | 258.11 | 4.49 | 4.55 | 4.69 | 8.33 | 13.07 | 99.66 | 226.80 |
| 76 | 261.55 | 4.55 | 4.61 | 4.75 | 8.44 | 13.19 | 100.99 | 229.83 |
| 77 | 264.99 | 4.60 | 4.67 | 4.81 | 8.56 | 13.37 | 102.32 | 232.85 |
| 78 | 268.43 | 4.66 | 4.73 | 4.87 | 8.67 | 13.54 | 103.65 | 235.88 |
| 79 | 271.87 | 4.72 | 4.79 | 4.94 | 8.78 | 13.72 | 104.97 | 238.90 |
| 80 | 275.31 | 4.78 | 4.85 | 5.00 | 8.89 | 13.89 | 106.30 | 241.92 |
| 81 | 278.76 | 4.84 | 4.91 | 5.06 | 9.00 | 14.06 | 107.63 | 244.95 |
| 82 | 282.20 | 4.90 | 4.97 | 5.12 | 9.11 | 14.24 | 108.96 | 247.97 |
| 83 | 285.64 | 4.96 | 5.03 | 5.19 | 9.22 | 14.41 | 110.29 | 251.00 |
| 84 | 289.08 | 5.0 ? | 5.09 | 5.25 | 9.33 | 14.58 | 111.62 | 254.02 |
| 85 | 292.52 | 5.08 | 5.16 | 5.31 | 9.44 | 14.76 | 112.95 | 257.04 |
| 86 | 295.96 | 5.14 | 5.22 | 5.37 | 9.56 | 14.93 | 114.28 | 260.07 |
| 87 | 299.40 | 5.20 | 5.28 | 5.44 | 9.67 | 15.10 | 115.60 | 263.09 |
| 88 | 302.85 | 5.26 | 5.34 | 5.50 | 9.78 | 15.28 | 116.93 | 266.12 |
| 89 | 306.29 | 5.32 | 5.40 | 5.56 | 9.89 | 15.45 | 118.26 | 269.14 |
| 90 | 309.73 | 5.38 | 5.46 | 5.62 | 10.00 | 15.62 | 119.59 | 272.16 |
| 91 | 313.17 | 5.44 | 5.52 | 5.69 | 10.11 | 15.80 | 120.92 | 275.19 |
| 92 | 316.61 | 5.50 | 5.58 | 5.75 | 10.22 | 15.97 | 122.25 | 278.21 |
| 93 | 320.05 | 5.56 | 5.64 | 5.81 | 10.33 | 16.15 | 123.58 | 281.24 |
| 94 | 323.49 | 5.62 | 5.70 | 5.87 | 10.44 | 16.32 | 124.91 | 284.26 |
| 95 | 326.94 | 5.68 | 5.76 | 5.94 | 10.56 | 16.49 | 126.24 | 287.28 |
| 96 | 330.38 | 5.74 | 5.82 | 6.00 | 10.67 | 16.67 | 127.56 | 290.31 |
| 97 | 333.82 | 5.80 | 5.88 | 6.06 | 10.78 | 16.84 | 128.89 | 293.33 |
| 98 | 337.26 | 5.86 | 5.94 | 6.12 | 10.89 | 17.01 | 130.22 | 296.36 |
| 99 | 340.70 | 5.92 | 6.00 | 6.19 | 11.00 | 17.19 | 131.55 | 299.38 |
| 100 | 344.14 | 5.98 | 6.07 | 6.25 | 11.11 | 17.36 | 132.88 | 302.40 |

VlII. englisil square miles into different geographical square measnres.

| $\begin{aligned} & \text { English } \\ & \text { Square } \\ & \text { Miles. } \end{aligned}$ | Sq. Kilometres. | Austrian Sq. Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Sq. Miles. } \end{aligned}$ | $\begin{gathered} \text { German } \\ \text { sq. Milees. } \\ 1 \delta=1^{\circ} \mathbf{E q} . \end{gathered}$ | $\begin{gathered} \text { Nautical } \\ \text { Square } \\ \text { Learues. } \\ 20=1^{\circ} \text { Eq. } \end{gathered}$ | $\begin{gathered} \text { Freuch } \\ \text { Square } \\ \text { Leagues. } \\ 25=10 \text { Eq. } \end{gathered}$ | Geograph'l or Nautical Sq. Miles. $60=1^{\circ} \mathrm{E}_{1}$. | Russian Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000 | 2589.894 | 45.00529 | 45.64631 | 47.03519 | 83.61812 | 130.6534 | 752.5631 | 2275.788 |
| 2,000 | 5179.789 | 90.01058 | 91.29261 | 94.07038 | 167.2362 | 261.3068 | 1505.126 | 4551.575 |
| 3,000 | 7769.683 | 135.0159 | 136.9389 | 141.1056 | 250.8544 | 391.9602 | 2257.689 | 6827.363 |
| 4,000 | 10359.58 | 180.0117 | 182.5852 | 188.1408 | 334.4725 | 522.6136 | 3010.252 | 9103.151 |
| 5,000 | 12949.47 | 225.0265 | 228.2315 | 235.1760 | 418.0906 | 653.2671 | 3762.815 | 11378.94 |
| 6,000 | 15539.37 | 270.0318 | 273.8778 | 282.2112 | 501.7087 | 783.9205 | 4515.379 | 13654.73 |
| 7,000 | 18129.26 | 315.0470 | 319.5241 | 329.2463 | 585.3268 | 914.5739 | 5267.942 | 15930.51 |
| 8,000 | 20719.16 | 360.0423 | 365.1704 | 376.2815 | 668.9450 | 1045.227 | 6020.505 | 18206.30 |
| 9,000 | 23309.05 | 405.0476 | 410.8168 | 423.3167 | 752.5631 | 1175.881 | 6773.068 | 20482.09 |
| 10,000 | 25898.94 | 450.0529 | 456.4631 | 470.3519 | 836.1812 | 1306.534 | 7525.631 | 22757.88 |
| 100 | 258.99 | 4.50 | 4.56 | 4.70 | 8.36 | 13.07 | 75.26 | 227.58 |
| 200 | 517.98 | 9.00 | 9.13 | 9.41 | 16.72 | 26.13 | 150.51 | 455.16 |
| 300 | 776.97 | 13.50 | 13.69 | 14.11 | 25.09 | 39.20 | 225.77 | 682.74 |
| 400 | 1035.96 | 18.00 | 18.26 | 18.81 | 33.45 | 52.26 | 301.03 | 910.32 |
| 500 | 1294.95 | 22.50 | 22.82 | 23.52 | 41.81 | 65.33 | 376.28 | 1137.89 |
| 600 | 1555.39 | 27.00 | 27.39 | 28.22 | 50.17 | 78.39 | 451.54 | 1365.47 |
| 700 | 1812.93 | 31.50 | 31.95 | 32.92 | 58.53 | 91.46 | $5 \geq 6.79$ | 1593.05 |
| 800 | 2071.92 | 36.00 | 36.52 | 37.63 | 66.89 | 104.52 | 602.05 | 1820.63 |
| 900 | 2330.91, | 40.50 | 41.08 | 42.33 | 75.26 | 117.59 | 677.31 | 2048.21 |
| 1000 | 2589.89 | 45.01 | 45.65 | 47.04 | 83.62 | 130.65 | 752.56 | 2275.79 |
| 1 | 2.59 | 0.05 | 0.05 | 0.05 | 0.08 | 0.13 | 0.75 | 2.28 |
| 2 | 5.18 | 0.09 | 0.09 | 0.09 | 0.17 | 0.26 | 1.51 | 4.55 |
| 3 | 7.77 | 0.14 | 0.14 | 0.14 | 0.25 | 0.39 | 2.26 | 6.83 |
| 4 | 10.36 | 0.18 | 0.18 | 0.19 | 0.33 | 0.52 | 3.01 | 9.10 |
| 5 | 12.95 | 0.23 | 0.23 | 0.24 | 0.42 | 0.65 | 3.76 | 11.38 |
| 6 | 15.54 | 0.27 | 0.27 | 0.28 | 0.50 | 0.78 | 4.52 | 13.65 |
| 7 | 18.13 | 0.32 | 0.32 | 0.33 | 0.59 | 0.91 | 5.27 | 15.93 |
| 8 | 20.72 | 0.36 | 0.37 | 0.38 | 0.67 | 1.05 | 6.02 | 18.20 |
| 9 | 23.31 | 0.41 | 0.41 | 0.43 | 075 | 1.18 | 6.77 | 20.48 |
| 10 | 25.90 | 0.45 | 0.46 | 0.47 | 0.84 | 1.31 | 7.53 | 22.76 |
| 11 | 28.49 | 0.50 | 0.50 | 0.52 | 0.92 | 1.44 | 8.28 | 25.03 |
| 12 | 31.08 | 0.54 | 0.55 | 0.56 | 1.00 | 1.57 | 9.03 | 27.31 |
| 13 | 33.67 | 0.59 | 0.59 | 0.61 | 1.09 | 1.70 | 9.78 | 29.59 |
| 14 | 36.26 | 0.63 | 0.64 | 0.66 | 1.17 | 1.83 | 10.54 | 31.86 |
| 15 | 38.85 | 0.68 | 0.68 | 0.71 | 1.25 | 1.96 | 11.29 | 34.14 |
| 16 | 41.44 | 0.72 | 0.73 | 0.75 | 1.34 | 2.09 | 12.04 | 36.41 |
| 17 | 44.03 | 0.77 | 0.78 | 0.80 | 1.42 | 2.22 | 12.79 | 38.69 |
| 18 | 46.62 | 0.81 | 0.82 | 0.85 | 1.51 | 2.35 | 13.55 | 40.96 |
| 19 | 49.21 | 0.86 | 0.87 | 0.89 | 1.59 | 2.48 | 14.30 | 43.23 |
| 20 | 51.80 | 0.90 | 0.91 | 0.94 | 1.67 | 2.61 | 15.05 | 45.52 |

english square miles into different geographical square measures.

| English Square Miles. | Sq. Kilometres. | Austrian sq. Miles. | Prussian Sq. Miles. | $\begin{aligned} & \text { German } \\ & \text { Sq. Miles. } \\ & 15=1^{\circ} \mathrm{Eq} . \end{aligned}$ | $\begin{gathered} \text { Nautical } \\ \text { Square } \\ \text { Leayues. } \\ 20=1^{\circ} \mathrm{Eq} . \end{gathered}$ | French <br> Square Leagues. $25=1^{\circ}$ E 1. | Geograph'l or Nautical Sq. Miles. $60=1^{\circ} \mathrm{Eq}$ | Russian <br> Square <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 54.39 | 0.95 | 0.96 | 0.99 | 1.76 | 2.74 | 15.80 | 47.79 |
| 22 | 56.98 | 0.99 | 1.00 | 1.03 | 1.84 | 2.87 | 16.56 | 50.07 |
| 23 | 59.57 | 1.04 | 1.05 | 1.08 | 1.92 | 3.01 | 17.31 | 52.34 |
| 24 | 62.16 | 1.08 | 1.10 | 1.13 | 2.01 | 3.14 | 18.06 | 54.62 |
| 25 | 64.75 | 1.13 | 1.14 | 1.18 | 2.09 | 3.27 | 18.81 | 56.89 |
| 26 | 67.34 | 1.17 | 1.19 | 1.22 | 2.17 | 3.40 | 19.57 | 59.17 |
| 27 | 69.93 | 1.22 | 1.23 | 1.27 | 2.26 | 3.53 | 20.32 | 61.45 |
| 28 | 72.52 | 1.26 | 1.28 | 1.32 | 2.34 | 3.66 | 21.07 | 63.72 |
| 29 | 75.11 | 1.31 | 1.32 | 1.36 | 2.42 | 3.79 | 21.82 | 66.00 |
| 30 | 77.70 | 1.35 | 1.37 | 1.41 | 2.51 | 3.92 | 22.58 | 68.27 |
| 31 | 80.29 | 1.40 | 1.42 | 1.46 | 2.59 | 4.05 | 23.33 | 70.55 |
| 32 | 82.88 | 1.44 | 1.46 | 1.51 | 2.68 | 4.18 | 24.08 | 72.83 |
| 33 | 85.47 | 1.49 | 1.51 | 1.55 | 2.76 | 4.31 | 24.83 | 75.10 |
| 34 | 88.06 | 1.53 | 1.55 | 1.60 | 2.84 | 4.44 | 25.59 | 77.38 |
| 35 | 90.65 | 1.58 | 1.60 | 1.65 | 2.93 | 4.57 | 26.34 | 79.65 |
| 36 | 93.24 | 1.62 | 1.64 | 1.69 | 3.01 | 4.70 | 27.09 | 81.93 |
| 37 | 95.83 | 1.67 | 1.69 | 1.74 | 3.09 | 4.83 | 27.84 | 84.20 |
| 38 | 98.42 | 1.71 | 1.73 | 1.78 | 3.18 | 4.96 | 28.60 | 86.48 |
| 39 | 101.01 | 1.76 | 1.78 | 1.83 | 3.26 | 5.00 | 29.35 | 88.76 |
| 40 | 103.60 | 1.80 | 1.83 | 1.88 | 3.34 | 5.23 | 30.10 | 91.03 |
| 41 | 106.19 | 1.85 | 1.87 | 1.93 | 3.43 | 5.36 | 30.86 | 93.31 |
| 42 | 108.78 | 1.89 | 1.92 | 1.98 | 3.51 | 5.49 | 31.61 | 95.58 |
| 43 | 111.37 | 1.94 | 1.96 | 2.02 | 3.60 | 5.62 | 32.36 | 97.86 |
| 44 | 113.96 | 1.98 | 2.01 | 2.07 | 3.68 | 5.75 | 33.11 | 100.13 |
| 45 | 116.55 | 2.03 | 2.05 | 2.12 | 3.76 | 5.88 | 33.87 | 102.41 |
| 46 | 119.14 | 2.07 | 2.10 | 2.16 | 3.85 | 6.01 | 34.62 | 104.69 |
| 47 | 121.73 | 2.12 | 2.15 | 2.21 | 3.93 | 6.14 | 35.37 | 106.96 |
| 48 | 124.31 | 2.16 | 2.19 | 2.26 | 4.01 | 6.27 | 36.12 | 109.24 |
| 49 | 126.90 | 2.21 | 2.24 | 2.30 | 4.10 | 6.40 | 36.88 | 111.51 |
| 50 | 129.49 | 2.25 | 2.98 | 2.35 | 4.18 | 6.53 | 37.63 | 113.79 |
| 51 | 132.08 | 2.30 | 2.33 | 2.40 | 4.26 | 6.66 | 38.38 | 116.07 |
| 52 | 134.67 | 2.34 | 2.37 | 2.45 | 4.34 | 6.79 | 39.13 | 118.34 |
| 53 | 137.26 | 2.39 | 2.42 | 2.49 | 4.43 | 6.92 | 39.89 | 120.62 |
| 54 | 139.85 | 2.43 | 2.46 | 2.54 | 4.52 | 7.06 | 40.64 | 122.89 |
| 55 | 142.44 | 2.48 | 2.51 | 2.59 | 4.60 | 7.19 | 41.39 | 125.17 |
| 56 | 145.03 | 2.52 | 2.56 | 2.63 | 4.68 | 7.32 | 42.14 | 127.44 |
| 57 | 147.62 | 2.57 | 2.60 | 2.68 | 4.77 | 7.45 | 42.90 | 129.72 |
| 58 | 150.21 | 2.61 | 2.65 | 2.73 | 4.85 | 7.58 | 43.65 | 132.00 |
| 59 | 152.80 | 2.66 | 2.69 | 2.78 | 4.93 | 7.71 | 44.40 | 134.27 |
| 60 | 155.39 | 2.70 | 2.74 | 2.82 | 5.02 | 7.84 | 45.15 | 136.55 |

560
english square miles into different geographical square measures.

| English Square Miles. Miles. | Sq. Kilometres. | $\begin{aligned} & \text { Austrian } \\ & \text { sq. Miles. } \end{aligned}$ | Prussian Sq. Miles. | $\begin{gathered} \text { German } \\ \text { Sq. Miles. } \\ 15=1^{\circ} \mathbf{E}, \end{gathered}$ | Nautical square Leagues. $20=1^{\circ} \mathrm{Eq}$. | $\begin{gathered} \text { French } \\ \text { Square } \\ \text { Leatues. } \\ 25=1^{\circ} \text { E } 4 . \end{gathered}$ | $\begin{aligned} & \text { Geograph'l } \\ & \text { or Nautical } \\ & \text { sq. Miles. } \\ & 60=1^{\circ} \text { Eq. } \end{aligned}$ | Russian square Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 157.98 | 2.75 | 2.78 | 2.87 | 5.10 | 7.97 | 45.91 | 138.82 |
| 62 | 160.57 | 2.79 | 2.83 | 2.92 | 5.18 | 8.10 | 46.66 | 141.10 |
| 63 | 163.16 | 2.84 | 2.88 | 2.96 | 5.27 | 8.23 | 47.41 | 143.37 |
| 64 | 165.75 | 2.88 | 2.92 | 3.01 | 5.35 | 8.36 | 48.16 | 145.65 |
| 65 | 168.34 | 2.93 | 2.97 | 3.06 | 5.44 | 8.49 | 48.92 | 147.93 |
| 66 | 170.93 | 2.97 | 3.01 | 3.10 | 5.52 | 8.62 | 49.67 | 150.20 |
| 67 | 173.52 | 3.02 | 3.06 | 3.15 | 5.60 | 8.75 | 50.42 | 152.48 |
| 68 | 176.11 | 3.06 | 3.10 | 3.20 | 5.69 | 8.88 | 51.17 | 154.75 |
| 69 | 178.70 | 3.11 | 3.15 | 3.25 | 5.77 | 9.02 | 51.93 | 157.03 |
| 70 | 181.29 | 3.15 | 3.20 | 3.29 | 5.85 | 9.15 | 52.68 | 159.31 |
| 71 | 183.83 | 3.20 | 3.24 | 3.34 | 5.94 | 9.28 | 53.43 | 161.58 |
| 72 | 186.47 | 3.24 | 3.29 | 3.39 | 6.02 | 9.41 | 54.18 | 163.86 |
| 73 | 189.06 | 3.29 | 3.33 | 3.44 | 6.10 | 9.54 | 54.94 | 166.13 |
| 74 | 191.65 | 3.33 | 3.38 | 3.48 | 6.19 | 9.67 | 55.69 | 168.41 |
| 75 | 194.24 | 3.35 | 3.42 | 3.53 | 6.27 | 9.80 | 56.44 | 170.68 |
| 76 | 196.83 | 3.42 | 3.47 | 3.57 | 6.35 | 9.93 | 57.19 | 172.96 |
| 77 | 199.42 | 3.47 | 3.51 | 3.62 | 6.44 | 10.05 | 57.95 | 175.24 |
| 78 | 202.01 | 3.51 | 3.56 | 3.67 | 6.52 | 10.19 | 58.70 | 177.51 |
| 79 | 204.60 | 3.56 | 3.61 | 3.72 | 6.61 | 10.32 | 59.45 | 179.79 |
| 80 | 207.19 | 3.60 | 3.65 | 3.76 | 6.69 | 10.45 | 60.20 | 182.06 |
| 81 | 209.78 | 3.65 | 3.70 | 3.81 | 6.77 | 10.58 | 60.96 | 184.34 |
| 82 | 212.37 | 3.69 | 3.74 | 3.86 | 6.86 | 10.71 | 61.71 | 186.61 |
| 83 | 214.96 | 3.74 | 3.79 | 3.90 | $6.9 \pm$ | 10.84 | 62.46 | 188.89 |
| 84 | 217.55 | 3.78 | 3.83 | 3.95 | 7.02 | 10.97 | 63.22 | 191.17 |
| 85 | 220.14 | 3.83 | 3.88 | 4.00 | 7.11 | 11.11 | 63.97 | 193.44 |
| 86 | 222.73 | 3.87 | 3.93 | 4.05 | 7.19 | 11.24 | 64.72 | 195.72 |
| 87 | 225.32 | 3.92 | 3.97 | 4.09 | 7.27 | 11.37 | 65.47 | 197.99 |
| 88 | 237.91 | 3.96 | 4.02 | 4.14 | 7.36 | 11.50 | 66.23 | 200.27 |
| 89 | 230.50 | 4.01 | 4.06 | 4.19 | 7.44 | 11.63 | 66.98 | 202.55 |
| 90 | 233.09 | 4.05 | 4.11 | 4.23 | 7.53 | 11.76 | 67.73 | 204.82 |
| 91 | 235.68 | 4.10 | 4.15 | 4.28 | 7.61 | 11.99 | 68.48 | 207.10 |
| 92 | 238.27 | 4.14 | 4.20 | 4.33 | 7.69 | 12.02 | 69.24 | 209.37 |
| 93 | 240.86 | 4.19 | 4.25 | 4.37 | 7.78 | 12.15 | 69.99 | 211.65 |
| 94 | 243.45 | 4.23 | 4.29 | 4.42 | 7.86 | 12.28 | 70.74 | 213.92 |
| 95 | 246.04 | 4.28 | 4.34 | 4.47 | 7.94 | 12.41 | 71.49 | 216.20 |
| 96 | 248.63 | 4.32 | 4.38 | 4.52 | 8.03 | 12.54 | 72.25 | 218.48 |
| 97 | 251.22 | 4.37 | 4.43 | 4.56 | 8.11 | 12.67 | 73.00 | 220.75 |
| 98 | 253.81 | 4.41 | 4.47 | 4.61 | 8.19 | 12.80 | 73.75 | 223.03 |
| 99 | 256.40 | 4.46 | 4.52 | 4.66 | 8.28 | 12.93 | 74.50 | 225.30 |
| 100 | 258.99 | 4.50 | 4.56 | 4.70 | 8.36 | 13.07 | 75.26 | 227.58 |

IX. square wersts into different geographical square measures. 561

| Russian Square Wersts. | Sq. Kilometres. | Austrian sq. Miles. | Prussian Sq. Miles. | German Sq. Miles. $15=1^{\circ} \mathrm{Eq}$. | Nautical square Leagues. $20=1^{\circ} \mathrm{Eq}$. | French <br> square <br> Leagues. $20=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical Sq. Miles. $60=1^{\circ} \mathrm{Eq}$. | English Square Mijes. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1,000. | 1138.021 | 19.77570 | 20.05737 | 20.66765 | 36.74250 | 57.41015 | 330.6825 | 439.4083 |
| 2,000 | 2976.042 | 39.55140 | 40.11473 | 41.33531 | 73.48499 | 114.8203 | 661.3649 | 878.8166 |
| 3,000 | 3414.062 | $59.3: 710$ | 60.17210 | 62.00296 | 110.2275 | 172.2304 | 992.0474 | 1318.225 |
| 4,000 | 4552.083 | 79.10279 | 81.22946 | 82.67061 | 146.9700 | 229.6406 | 1322.730 | 1757.633 |
| 5,000 | 5690.104 | 98.87849 | 100.2868 | 103.3383 | 183.7125 | 287.0507 | 1653.412 | 2197.041 |
| 6,000 | 6828.125 | 118.6542 | 120.3442 | 124.0059 | 220.4550 | 344.4609 | 1984.095 | 2636.450 |
| 7,000 | 7966.146 | 138.4299 | 140.4116 | 144.6736 | 257.1975 | 401.8710 | 2314.757 | 3075.858 |
| 8,000 | $9104.166^{\circ}$ | 158.2056 | 160.4589 | 165.3412 | 293.9460 | 459.2812 | 2645.460 | 3515.266 |
| 9,000 | 10242.19 | 177.9813 | 180.5163 | 186.0189 | 330.6825 | 516.6913 | 2976.142 | 3954.675 |
| 10,000 | 11380.21 | 197.7570 | 200.5737 | 206.6765 | 367.4250 | 574.1015 | 3306.825 | 4394.083 |
| 100 | 113.80 | 1.98 | 2.01 | 2.07 | 3.67 | 5.74 | 33.07 | 43.94 |
| 200 | 237.60 | 3.96 | 4.01 | 4.13 | 7.35 | 11.48 | 66.14 | 87.88 |
| 300 | 341.41 | 5.93 | 6.02 | 6.20 | 11.02 | 17.22 | 99.21 | 131.82 |
| 400 | 455.21 | 7.91 | 8.02 | 8.27 | 14.70 | 22.96 | 132.27 | 175.76 |
| 500 | 569.01 | 9.89 | 10.03 | 10.33 | 18.37 | 28.71 | 165.34 | 219.70 |
| 600 | 682.81 | 11.87 | 12.03 | 12.40 | 22.05 | 34.45 | 198.41 | 263.64 |
| 700 | 796.61 | 13.84 | 14.04 | 14.47 | 25.72 | 40.19 | 231.48 | 307.59 |
| 800 | $910.4 *$ | 15.82 | 16.04 | 16.53 | 29.39 | 45.93 | 264.55 | 351.53 |
| 900 | 1024.21 | 17.80 | 18.15 | 18.60 | 33.07 | 51.67 | 297.61 | 395.47 |
| 1000 | $1138.0{ }^{\circ}$ | 19.78 | 20.06 | 20.67 | 36.74 | 57.41 | 330.68 | 439.41 |
| 1 | 1.14 | 0.02 | 0.02 | 0.02 | 0.04 | 0.06 | 0.33 | 0.44 |
| 2 | 2.28 | 0.04 | 0.04 | 0.04 | 0.07 | 0.11 | 0.66 | 0.88 |
| 3 | 3.41 | 0.06 | 0.06 | 0.06 | 0.11 | 0.17 | 0.99 | 1.32 |
| 4 | 4.55 | 0.08 | 0.08 | 0.08 | 0.15 | 0.23 | 1.32 | 1.76 |
| 5 | 5.69 | 0.10 | 0.10 | 0.10 | 0.18 | 0.29 | 1.65 | 2.20 |
| 6 | 6.83 | 0.12 | 0.12 | 0.12 | 0.24 | 0.34 | 1.98 | 2.64 |
| 7 | 7.97 | 0.14 | 0.14 | 0.14 | 0.26 | 0.40 | 2.31 | 3.08 |
| 8 | 9.10 | 0.16 | 0.16 | 0.17 | 0.29 | 0.46 | 2.65 | 3.52 |
| 9 | 10.24 | 0.18 | 0.18 | 0.19 | 0.33 | 0.52 | 2.98 | 3.95 |
| 10 | 11.38 | 0.20 | 0.20 | 0.21 | 0.36 | 0.57 | 3.31 | 4.39 |
| 11 | 12.52 | 0.22 | 0.22 | 0.23 | 0.40 | 0.63 | 3.64 | 4.83 |
| 12 | 13.66 | 0.24 | 0.24 | 0.25 | 0.44 | 0.69 | 3.97 | 5.27 |
| 13 | 14.79 | 0.26 | 0.26 | 0.27 | 0.48 | 0.75 | 4.30 | 5.71 |
| 14 | 15.93 | 0.28 | 0.28 | 0.29 | 0.51 | 0.80 | 4.63 | 6.15 |
| 15 | 17.07 | 0.30 | 0.30 | 0.31 | 0.55 | 0.86 | 4.96 | 6.59 |
| 16 | 18.21 | 0.32 | 0.32 | 0.33 | 0.59 | 0.92 | 5.29 | 7.03 |
| 17 | 19.35 | 0.34 | 0.34 | 0.35 | 0.62 | 0.98 | 5.62 | 7.47 |
| 18 | 20.48 | 0.36 | 0.36 | 0.37 | 0.66 | 1.03 | 5.95 | 7.91 |
| 19 | 21.62 | 0.38 | 0.38 | 0.39 | 0.70 | 1.09 | 6.28 | 8.35 |
| 20 | 22.76 | 0.40 | 0.40 | 0.41 | 0.73 | 1.15 | 6.61 | 8.79 |

SQUARE WERSTS INTO DIFFERENT GEOGRAPHICAL SQUARE MEASURES.

| $\begin{aligned} & \text { Russian } \\ & \text { square } \\ & \text { Wersts } \end{aligned}$ Wersts. | Sq. Kilo- metres. | $\begin{aligned} & \text { Austrian } \\ & \text { Sq. Miles. } \end{aligned}$ | Prussian Sq. Miles. | German <br> Sq. Miles. $15=1^{\circ} \mathrm{Eq} .$ | Nautical square Leagues. $20=1^{\circ} \mathrm{Eq}$. $20=1^{\circ} \mathrm{Eq}$. | French Square Leagnes. $2 j=1^{\circ} \mathrm{Eq}$. | Geograph'l or Nautical Sq. Miles. $60=1^{\circ} \mathrm{Eq}$. | English <br> Square <br> Miles. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 23.90 | 0.42 | 0.42 | 0.43 | 0.77 | 1.21 | 6.94 | 9.23 |
| 22 | 25.04 | 0.44 | 0.44 | 0.45 | 0.81 | 1.26 | 7.28 | 9.67 |
| 23 | 26.17 | 0.45 | 0.46 | 0.48 | 0.85 | 1.32 | 7.61 | 10.11 |
| 24 | 27.31 | 0.47 | 0.48 | 0.50 | 0.88 | 1.38 | 7.94 | 10.55 |
| 25 | 28.45 | 0.49 | 0.50 | 0.52 | 0.92 | 1.44 | 8.27 | 10.99 |
| 26 | 29.59 | 0.51 | 0.52 | 0.54 | 0.96 | 1.49 | 8.60 | 11.42 |
| 27 | 30.73 | 0.53 | 0.54 | 0.56 | 0.99 | 1.55 | 8.93 | 11.86 |
| 28 | 31.86 | 0.55 | 0.56 | 0.58 | 1.03 | 1.61 | 9.26 | 12.30 |
| 29 | 33.00 | 0.57 | 0.58 | 0.60 | 1.07 | 1.66 | 9.59 | 12.74 |
| 30 | 34.14 | 0.59 | 0.60 | 0.62 | 1.10 | 1.72 | 9.92 | 13.18 |
| 31 | 35.28 | 0.61 | 0.62 | 0.64 | 1.14 | 1.78 | 10.25 | 13.62 |
| 32 | 36.42 | 0.63 | 0.64 | 0.66 | 1.18 | 1.84 | 10.58 | 14.06 |
| 33 | 37.55 | 0.65 | 0.66 | 0.68 | 1.21 | 1.89 | 10.91 | 14.50 |
| 34 | 38.69 | 0.67 | 0.68 | 0.70 | 1.25 | 1.95 | 11.24 | 14.94 |
| 35 | 39.83 | 0.69 | 0.70 | 0.72 | 1.29 | 2.01 | 11.57 | 15.38 |
| 36 | 40.97 | 0.71 | 0.72 | 0.74 | 1.32 | 2.07 | 11.90 | 15.82 |
| 37 | 42.11 | 0.73 | 0.74 | 0.76 | 1.36 | 2.12 | 12.24 | 16.26 |
| 38 | 43.24 | 0.75 | 0.76 | 0.79 | 1.40 | 2.18 | 12.57 | 16.70 |
| 39 | 44.38 | 0.77 | 0.78 | 0.81 | 1.43 | 2.24 | 12.90 | 17.16 |
| 40 | 45.52 | 0.79 | 0.80 | 0.83 | 1.47 | 2.30 | 13.23 | 17.58 |
| 41 | 46.66 | 0.81 | 0.82 | 0.85 | 1.51 | 2.35 | 13.56 | 18.02 |
| 42 | 47.80 | 0.83 | 0.84 | 0.87 | 1.54 | 2.41 | 13.89 | 18.46 |
| 43 | 48.93 | 0.85 | 0.86 | 0.89 | 1.58 | 2.47 | 14.22 | 18.89 |
| 44 | 50.07 | 0.87 | 0.88 | 0.91 | 1.62 | 2.53 | 14.55 | 19.33 |
| 45 | 51.21 | 0.89 | 0.90 | 0.93 | 1.65 | 2.58 | 14.88 | 19.77 |
| 46 | 52.35 | 0.91 | 0.92 | 0.95 | 1.69 | 2.64 | 15.21 | 20.21 |
| 47 | 53.49 | 0.93 | 0.94 | 0.97 | 1.73 | 2.70 | 15.54 | 20.65 |
| 48 | 54.62 | 0.95 | 0.96 | 0.99 | 1.76 | 2.76 | 15.87 | 21.09 |
| 49 | 55.76 | 0.97 | 0.98 | 1.01 | 1.80 | 2.81 | 16.20 | 21.53 |
| 50 | 56.90 | 0.99 | 1.00 | 1.03 | 1.84 | 2.87 | 16.53 | 21.97 |
| 51 | 58.04 | 1.01 | 1.02 | 1.05 | 1.87 | 2.93 | 16.86 | 22.41 |
| 52 | 59.18 | 1.03 | 1.04 | 1.07 | 1.91 | 2.99 | 17.20 | 22.85 |
| 53 | 60.32 | 1.05 | 1.06 | 1.10 | 1.95 | 3.04 | 17.53 | 23.29 |
| 54 | 61.45 | 1.07 | 1.08 | 1.12 | 1.98 | 3.10 | 17.86 | 23.73 |
| 55 | 62.59 | 1.09 | 1.10 | 1.14 | 2.02 | 3.16 | 18.19 | 24.17 |
| 56 | 63.73 | 1.11 | 1.12 | 1.16 | 2.06 | 3.21 | 18.52 | 24.61 |
| 57 | 64.87 | 1.13 | 1.14 | 1.18 | 2.09 | 3.27 | 18.85 | 25.05 |
| 58 | 66.01 | 1.15 | 1.16 | 1.20 | 2.13 | 3.33 | 19.18 | 25.49 |
| 59 | 67.14 | 1.17 | 1.18 | 1.22 | 2.17 | 3.39 | 19.51 | 25.93 |
| 60 | 68.28 | 1.19 | 1.20 | 1.24 | 2.20 | 3.44 | 19.84 | 26.36 |

square wersts into different geographical square measures.

| Russian square Wersts. | $\begin{aligned} & \text { Sq. Kilo- } \\ & \text { metres. } \end{aligned}$ | Austrian Sq. Miles. | $\begin{aligned} & \text { Prussian } \\ & \text { Sq. Niles. } \end{aligned}$ | German <br> sq. Miles. <br> $15=1^{\circ} \mathrm{Eq}$. | Nautical square Leagues. $20=1^{\circ}$ Eq. | French Square Leagues. $2 \overline{0}=1^{\circ} \mathrm{Eq}$. | Geograph'l or Aautical Sq. Mijes. $60=1^{\circ} \mathrm{E} q$. | English <br> square <br> Miles. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 61 | 69.42 | 1.21 | 1.22 | 1.26 | 2.24 | 3.50 | 20.17 | 26.80 |
| 62 | 70.56 | 1.23 | 1.24 | 1.28 | 2.28 | 3.56 | 20.50 | 27.24 |
| 63 | 71.70 | 1.25 | 1.26 | 1.30 | 2.31 | 3.62 | 20.83 | 27.68 |
| 64 | 72.83 | 1.27 | 1.28 | 1.32 | 2.35 | 3.67 | 21.16 | 28.12 |
| 65 | 73.97 | 1.89 | 1.30 | 1.34 | 2.39 | 3.73 | 21.49 | 28.56 |
| 66 | 75.11 | 1.31 | 1.32 | 1.36 | 2.43 | 3.79 | 21.83 | 29.00 |
| 67 | 76.25 | 1.32 | 1.34 | 1.38 | 2.46 | 3.85 | 22.16 | 29.44 |
| 68 | 77.39 | 1.34 | 1.36 | 1.41 | 2.50 | 3.90 | 22.49 | 30.88 |
| 69 | 78.52 | 1.36 | 1.38 | 1.43 | 2.54 | 3.96 | 22.82 | 30.32 |
| 70 | 79.66 | 1.38 | 1.40 | 1.45 | 2.57 | 4.02 | 23.15 | 30.76 |
| 71 | 80.80 | 1.40 | 1.42 | 1.47 | 2.61 | 4.08 | 23.48 | 31.20 |
| 72 | 81.94 | 1.42 | 1.44 | 1.49 | 2.65 | 4.13 | 23.81 | 31.64 |
| 73 | 83.08 | 1.44 | 1.46 | 1.51 | 2.68 | 4.19 | 24.14 | 32.08 |
| 74 | 84.21 | 1.46 | 1.48 | 1.53 | 2.72 | 4.25 | 24.47 | 32.52 |
| 75 | 85.35 | 1.48 | 1.50 | 1.55 | 2.76 | 4.31 | 24.80 | 32.96 |
| 76 | 86.49 | 1.50 | 1.52 | 1.57 | 2.79 | 4.36 | 25.13 | 33.40 |
| 77 | 87.63 | 1.52 | 1.54 | 1.59 | 2.83 | 4.42 | 25.46 | 33.83 |
| 78 | 88.77 | 1.54 | 1.56 | 1.61 | 2.87 | 4.47 | 25.79 | 34.27 |
| 79 | 89.90 | 1.56 | 1.58 | 1.63 | 2.90 | 4.54 | 26.12 | 34.71 |
| 80 | 91.04 | 1.58 | 1.60 | 1.65 | 2.94 | 4.59 | 26.45 | 35.15 |
| 81 | 92.18 | 1.60 | 1.62 | 1.67 | 2.98 | 4.65 | 26.79 | 35.59 |
| 82 | 93.32 | 1.62 | 1.64 | 1.69 | 3.01 | 4.71 | 27.12 | 36.03 |
| 83 | 94.46 | 1.64 | 1.66 | 1.72 | 3.05 | 4.77 | 27.45 | 36.47 |
| 84 | 95.59 | 1.66 | 1.68 | 1.74 | 3.09 | 4.82 | 27.78 | 36.91 |
| 85 | 96.73 | 1.68 | 1.70 | 1.76 | 3.12 | 4.88 | 28.11 | 37.35 |
| 86 | 97.87 | 1.70 | 1.72 | 1.78 | 3.16 | 4.94 | 28.44 | 37.79 |
| 87 | 99.01 | 1.72 | 1.74 | 1.80 | 3.20 | 4.99 | 28.77 | 38.23 |
| 88 | 100.15 | 1.74 | 1.76 | 1.82 | 3.23 | 5.05 | 29.10 | 38.67 |
| 89 | 101.28 | 1.76 | 1.78 | 1.84 | 3.27 | 5.11 | 29.43 | 39.11 |
| 90 | 102.42 | 1.78 | 1.80 | : 1.86 | 3.31 | 5.17 | 29.76 | 39.55 |
| 91 | 103.56 | 1.80 | 1.83 | 1.88 | 3.34 | 5.22 | 30.09 | 39.99 |
| 92 | 104.70 | 1.82 | 1.85 | 1.90 | 3.38 | 5.28 | 30.42 | 40.43 |
| 93 | 105.84 | 1.84 | 1.87 | 1.92 | 3.42 | 5.34 | 30.75 | 40.86 |
| 94 | 106.97 | 1.86 | 1.89 | 1.94 | 3.45 | 5.40 | 31.08 | 41.30 |
| 95 | 108.11 | 1.88 | 1.91 | 1.96 | 3.49 | 5.45 | 31.41 | 41.74 |
| 96 | 109.25 | 1.90 | 1.93 | 1.98 | 3.53 | 5.51 | 31.75 | 42.18 |
| 97 | 110.39 | 1.92 | 1.95 | 2.00 | 3.56 | 5.57 | 32.08 | 42.62 |
| 98 | 111.53 | 1.94 | 1.97 | 2.03 | 3.60 | 5.63 | 32.41 | 43.06 |
| 99 | 112.66 | 1.96 | 1.99 | 2.05 | 3.64 | 5.68 | 32.74 | 43.50 |
| 100 | 113.80 | 1.98 | 2.01 | 2.07 | 3.67 | 5.74 | 33.07 | 43.94 |

X. COMPARATIVE TABLE OF THE MOST IMPORTANT MEASURES OF SURFACE.

| Square Kilometre. | $\begin{gathered} \text { Austrian } \\ \text { Square Mile. } \end{gathered}$ | Prussian Square Mile. | German Square Mile. $15=1^{\circ}$ Equator | Nautical Square League. $20=1^{\circ}$ Equator. | French Square League. $25=1^{\circ}$ Equator $25=1^{\circ}$ Equator. | Geographical or Nautical Square Mile. $60=1^{\circ}$ Equator. | $\begin{aligned} & \text { English } \\ & \text { Square Mile. } \end{aligned}$ | $\begin{gathered} \text { Russlan } \\ \text { Square Werst. } \end{gathered}$ | Swedish Square Mile. | Spanish Square legua antigua. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.017377 | 0.017625 | 0.018161 | 0.032286 | 0.050447 | 0.290577 | 0.386116 | 0.878718 | 0.008753 | 0.032201 |
| 0 | 8.239982 | 8.246124 | 8.259141 | 8.509018 | 8.702 38 | 9.463261 | 9.586718 | 9.943850 | 7.942172 | 8.507869 |
| 57.5464 | 1 | 1.01424 | 1.04510 | 1.85796 | 2.90307 | 16.72166 | 22.2196 | 50.5671 | 0.503721 | 1.85305 |
| 1.760018 | 0 | 0.006142 | 0.019159 | 0.269037 | 0.4628 .57 | 1.223279 | 1.346736 | 1.703868 | 9.702190 | 0.267887 |
| 56.7383 | 0.985957 | 1 | 1.03043 | 1.83187 | 2.86230 | 16.48683 | 21.9076 | 49.8570 | 0.496647 | 1.82703 |
| 1.753876 | 9.993858 | 0 | c.013017 | 0.262595 | 0.456715 | 1.217137 | $1.3+0594$ | 1.697726 | 9.696048 | 0.261745 |
| 55.0629 | 0.956843 | 0.970471 | 1 | 1.77778 | 2.77778 | 16.000000 | 21.2607 | 48.3848 | 0.481982 | 1.77308 |
| 1.740859 | 9.9503 .41 | 9.956983 | 0 | 0.249577 | 0.443697 | 1.204120 | 1.327577 | 1.684709 | 9.683031 | 0.248728 |
| 30.9729 | 0.538224 | 0.545890 | 0.562500 | 1 | 1.56250 | 9.000000 | 11.9591 | 27.2164 | 0.271115 | 0.997357 |
| 1.490982 | 9.73963 | 9.737105 | 9.750123 | 0 | 0.193820 | 0.954243 | 1.077700 | 1.434831 | 9.433153 | 9.998850 |
| 19.8226 | 0.344463 | 0.349370 | 0.360000 | 0.640000 | 1 | 5.760000 | 7.65384 | 17.4185 | 0.173513 | 0.638308 |
| 1.297162 | 9.537143 | 9.743285 | 9.556303 | 9.506180 | 0 | 0.760423 | 0.883850 | 1.241011 | 9.239333 | 9.505030 |
| 3.44143 | 0.059803 | 0.060654 | 0.062500 | 0.111111 | 0.173611 | 1 | 1.328792 | 3.024049 | 0.030124 | 0.110816 |
| 0.536739 | 8.776723 | 8.782859 | 8.795880 | 9.045757 | 9.239577 | 0 | 0.123457 | 0.480559 | 8.478913 | 9.044601 |
| 2.58989 | 0.045005 | 0.045646 | 0.047035 | 0.083618 | 0.130653 | 0.752563 | 1 | 2.27579 | 0.022670 | 0.083397 |
| 0.413282 | 8.653264 | 8.659406 | 8.672423 | 8.922300 | 9.116120 | 9.876.44 | 0 | 0.357132 | 8.355452 | 8.921151 |
| 1.13802 | 0.019776 | 0.020057 | 0.020668 | 0.036742 | 0.057410 | 0.330683 | 0.439408 | 1 | 0.009961 | 0.036645 |
| 0.056150 | 8.296132 | 8.302274 | 8315291 | 8.565169 | 8.755989 | 9.519412 | 9.642868 | 0 | 7.998322 | 8.564019 |
| 114.247 | 1.98523 | 2.01350 | 2.07477 | 3.68847 | 5.76324 | 33.19628 | 44.1109 | 100.387 | 1 | 3.67872 |
| 2.057845 | 0.297810 | 0.303952 | 0.316969 | 0.566847 | 0.760667 | 1.521059 | 1.644546 | 2.001678 | 0 | 0.565697 |
| 31.0550 | 0.539651 | 0.547337 | 0.563991 | 1.00265 | 1.56654 | 9.02400 | . 11.9908 | 27.2866 | 0.271833 | 1 |
| 1.492131 | 9.732113 | 9.738255 | 9.751272 | 0001150 | 0.194970 | 0.955399 | 1.078849 | 1.435981 | 9.434303 | 0 |

[^4]
# METEOROLOGICAL TABLES. 

## SERIES VI.

METEOROLOGICAL CORRECTIONS,

618

TABLES

for correcting series of observations for the periodic and non-periodic variations.

## CONTENTS.

[The figures refer to the folio at the bottom of the page. - The letters near them mean, $\mathrm{D} .=$ calculated by Dove ; Gl. = Glaisher ; G. $=$ Guyot $; L .=$ Lefroy. For the letters before the latitudes, see page 12.]

## Temperature.

Hourly Corrections for Periodic V'ariations.

## NORTH AMERICA.

Station. Latitude. Scale. Page.

Table I. Washington, District Columbia,
" II. Philadelphia, Girard College,
" III. Philadelphia, Girard College,
" IV. Frankfort Arsenal, Penn.,
". V. Frankfort Arsenal, Penn.,
" VI. Toronto, Canada West,
" VII. 'Toronto, Canada West,
" VIII. Toronto, Canada West,
" IX. Toronto, Canada West,
" X. Montreal, Canada East,
" XI. Sitka, Alaska,
" XII. Boothia Felix, Arctic America,
" XIII. Lake Athabasca, Arctic America,
"XIV. Melville Island, Arctic America,
" XV. Hecla Cove, Spitzbergen,
Appendix.
". V'. Amherst College, Mass.,

B 1. $\overbrace{8}^{8} 54 \mathrm{~N}$. Reau. D. 15
$\mathrm{A}^{\prime} 3$. 3958 N . Reau. D. 15
$\mathrm{A}^{\prime} 3.3958 \mathrm{~N}$. Fahr. G. 16
C. 3957 N. Reau. D. 17
C. 3957 N. Fahr. D. 18
B. 4340 N. Fahr. D. 19
B. 4340 N . Reau. D. 20

A'6. 4340 N. Fahr. L. 21
$A^{\prime}$ 6. 4340 N. Reau. D. 22
$\mathrm{A}^{\prime}{ }_{1} .4530 \mathrm{~N}$. Fahr. G. 22
A's. 573 N. Reau. D. 23
A. $\quad 6959 \mathrm{~N}$. Reau. D. 24
C. 59 N. Fahr. L. 25
C. 7447 N. Reau. D. 25
C. $\quad 7955$ N. Reau. D. 25
$\mathrm{A}^{\prime} 1.4222 \mathrm{~N}$. Fahr. D. 28

SOUTH AMERICA.

| " XVI. Rio Janeiro, Brazil, | C. | 2254 S. | Fiahr. | D. | 26 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| " XVII. Rio Janeiro, Brazil, | C. | 2254 S. | Reau. | D. | 27 |


|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Station. |  | Latitude. | Scale. | Page. |
| Table | XVIII. | Trevandrum, India, | A. | 831 N . | Fahr. | D. 31 |
| ، | NIX. | Trevandrum, India, | A. | 831 N . | Reau. | D. 32 |
| ' | XX. | Madras, India, | A. | 134 N. | Fahr. | D. 33 |
| " | XXI. | Madras, India, | A. | 134 N. | Reau. | D. 34 |
| " | XXII. | Bumbay, India, | A. | 1856 N. | Fahr. | D. 35 |
| " | XXII. | Bombay, India, | A. | 1856 N. | Reau. | D. 36 |
| '6 | SXIV. | Madras, India, | $\mathrm{A}^{\prime}{ }^{\text {a }}$. | 134 N . | Reau. | D. 37 |
| " | XXV. | Bombay, India, | $\mathrm{A}^{\prime}$. | 1856 N. | Reau. | D. 37 |
| " | XXV1. | Calcutta, India, | $\mathrm{A}^{\prime} 2$. | 2233 N . | Reau. | D. 38 |
| " | XXVII. | Tifis, Georgia, | $\mathrm{A}^{\prime}{ }^{\text {d }}$. | 4141 N. | Reau. | D. 39 |
| " | XSVIII. | Peking, China, | $\mathrm{A}^{\prime}{ }^{\text {d }}$. | 3954 N . | Reau. | D. 39 |
| " | SXIX. | Nertchinsk, Siberia, | $\mathrm{A}^{\prime} 6$. | 5118 N. | Reau. | D. 40 |
| " | XXX. | Nertchinsk, Siberia, | A. | 5118 N. | Reau. | D. 41 |
| " | XXXI. | Barnaul, Siberia, | A. | 5320 N . | Fahr. | D. 42 |
| '6 | SXXII. | Barnaul, Siberia, | A. | 5320 N. | Reau. | D. 43 |
| " | XXXIII. | Barnaul, Siberia, | $\mathrm{A}^{\prime} 6$. | 5320 N . | Reau. | D. 44 |

EUROPE.
" XXXIV. Rome, Italy,
" XXXV. Padua, Italy,
" XXXVI. Geneva, Switzerland,
" XXXVH. Geneva, Switzerland,
" XXXVIII. St. Bernard, Switzerland,
" XXXIX. St. Bernard, Switzerland,
" XL. Kremsmiinster, Austria,
" XLI. Salzburg, Austria,
" XLIl. Munich, Bavaria,
" XLIII. Prague, Bohemia,
" XLIV. Prague, Bohemia, XLV. Plymouth, England, XLVI. Plymonth, England, XLVII. Brussels, Belgium,
" XLVIII. Brussels, Belgium,
" XLIX. Schwerin, Germany,
" L. Miihhhausen, Prussia,
" LI. Utrecht, Holland,
" LII. Greenwich, England,
" LIII. Greenwich, England,
" LIV. Greenwich, England,
" LV. Halle, Prussia,
" LVI. Göttingen, Hanover,
C. 4154 N. Reau. D. 47
C. 4524 N. Reau. D. 48

C 10. 46 12 N. Reau. D. 49
$\mathrm{C}^{\prime}$ 4. 4612 N. Reau. D. 49
C 10. 4552 N. Reau. D. 50
$\mathrm{C}^{\prime}$ t. 4552 N. Reau. D. 50
C. 483 N. Reau. D. 51

A'6. 4748 N. Reau. D. 52
$\mathrm{A}^{\prime}$. 489 N . Reau. D. 52
A $^{\prime} 10.505 \mathrm{~N}$. Reau. D. 53
A. 505 N . Reau. D. 54
C. 5022 N. Fahr. D. 55
C. 5022 N. Reau. D. 56
B. 5051 N . Reau. D. 57

B'. 5051 N . Reau. D. 58
B's. 5336 N . Reau. D. 58
C. 5113 N. Reau. D. 59

A'2. 525 N . Reau. D. 60
B7. 5129 N. Reau. D. 60
B. $\quad 5129$ N. Reau. D. 61
B. $\quad 5129 \mathrm{~N} . \quad$ Fahr. Gl. 62
C. 5130 N . Reau. D. 63
C. 5132 N. Reau. D. 64


AFRICA AND AUSTRALIA.


Monthly Corrections for Non-periodic Variations.

|  | Station. | Latitude. | Scale. |  | Page. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Table LXXIX. | Madras, India, | $13{ }^{\circ} 4 \mathrm{~N}$. | Reau. | D. | 90 |
| LXXX. | Palermo, Sicily, | 387 N. | Reau. | D. | 91 |
| LXXXI. | Milan, Italy, | 4528 N. | Reau. | D. | 92 |
| LXXXII. | Geneva, Switzerland, | 4612 N. | Reau. | D. | 94 |
| " LXXXIII. | Vienna, Austria, | 4813 N. | Reau. | D. | 96 |
| " LXXXIV. | Ratisbon, Austria, | 491 N. | Reau. | D. | 97 |
| " LXXXV. | Stuttgart, South Germany, | 4846 N. | Rean. | D. | 99 |
| " LXXXVI. | Carlsruhe, South Germany, | 491 N. | Reau. | D. | 100 |
| " LXXXVII. | Berlin, Prussia, | 5230 N . | Reau. | D. | 102 |
| " LXXXVIII. | Copenhagen, Denmark, | 5541 N . | Reau. | D. | 105 |
| LXXXIX. | Paris, France, | 4850 N . | Reau. | D. | 107 |
| XC. | Zwanenburg, Holland, | 5223 N . | Reau. | D. | 108 |
| XCI. | London, England, | 5130 N . | Reau. | D. | 110 |

Station.
Table XCII. Kinfauns Castle, Scotland,
" XClII. Torneå, Finland,
" XCIV. Albany, N. Y., North America,
" XCV. Salem, Mass., North America,
" XCVI. Reikiavik, Iceland,
" XCVII. Godthaab, Greenland,

Latitude. Scale. Sage.
5624 N. Reau. D. 112
6550 N. Reau. D. 112
4239 N. Reau. D. 113
4231 N . Reau. D. 114
648 N. Reau. D. 115
6410 N. Reau. D. 115

Force of Vapor and Relative Humidity.
Hourly Corrections for Periodic Variations.
" XCVIII. Greenwich, England, Force of Vapor, by Glaisher, . . 119
" XCIX. Greenwich, England, Relative Humidity, by Glaisher, . 120

## METEOROLOGICAL CORRECTIONS.

One of the prominent objects of a prolonged series of meteorological observations is to determine the mean condition of the atmosphere, during a given interval of time, such as a day, a month, or a year, as to its temperature, moisture, and barometric pressure. In order to furnish the true means of these elements, free from the periodic changes which depend upon the daily course of the sun and upon the seasons, the observations ought to be made at equal intervals of time, and be so often repeated as actually to represent the sum of the variations which took place during the stated time. It is generally admitted that observations taken at every one of the twentyfour hours of the day give means which do not sensibly differ from the means which would be obtained from a still larger number of observations during the same time; so that means derived from hourly observations may be considered as the true daily, monthly, and annual means of the year in which the observations were taken.

However, as the means of a given month, or year, will generally be found somewhat to differ from those of another year, at the same place, from causes which are not of a periodic nature, it is obvious that the absolute means can only be derived from the means of a series of years, in which the differences arising from these nonperiodic variations may be considered as sufficiently balancing each other.

Hourly observations can be expected only from a very few stations, favored with peculiar arrangements for the purpose. By far the larger number of observers must necessarily confine themselves to three or four observations a day. The means, therefore, deduced from such a set of observations, generally differ from the true means which would be given by hourly observations, by a quantity which varies with the hours selected for the observations. If that quantity, however, is known by having been previously determined for every hour, or set of hours, by a long series
of hourly obscrvations taken at some station in a similar climatic situation, it is evident that, whatever be the hours at which observations are taken, the means derived from them can always be reduced to the true means by correcting them for that difference.

The following tables furnish such corrections, both for periodic and non-periodic variations of temperature, and for stations situated in various latitudes. They give the quantities which must be added to, or subtracted from, the hourly means, in order to obtain the true means of the day, of the month, and of the year.

Two tables of the same description, for moisture, which may be considered as specimens of the kind, close the set.

Two other tables, for correcting the mean barometric pressures, are found at the end of the Hypsometrical Tables, pp. 92, 93.

# CORRECTIONS FOR TEMPERATURE. 

HOURLY CORRECTIONS FOR PERIODIC VARIATIONS, or

## TABLES

for reducing the means of the observations taken at any hour of the day to the true mean temperature of the day, of the month, and of the year.

## HOURLY CORRECTIONS FOR PERIODIC VARIATIONS,

ов

## corrections to be applied to the means of the hours of observation, or sets of hours, in order to obtain the true mean temperatures of the respective days, months, and of the year.

The following set contains all the tables for correcting the means of observations on atmospheric temperature for the effect of diurnal variation which have been published by Dove, together with a few others of the same description. Dove's tables are found in two papers, published in the Memoirs of the Royal Academy of Berlin for 1846 and for 1856, and in the first Report on the Observations of the Meteorological Institute of Prussia, Berlin, 1851.
In the first paper are twenty-nine tables, in Reaumur's scale, nine of which have been republished, in Fahrenheit's scale, in the Proceedings of the British Association for 1847, and will also be found below. In that series the corrections have been formed by finding first the differences between the hourly and the true means, and then computing the observations by Bessel's formula, in order to eliminate the accidental irregularitics due to the shortness of the period during which the observations were taken. Calling $x$ the horary angle reckoned from noon, Bessel's formula is

$$
t x=u+u^{\prime} \sin \left(x+U^{\prime}\right)+u^{\prime \prime} \sin \left(2 x+U^{\prime \prime}\right)+u^{\prime \prime \prime} \sin \left(3 x+U^{\prime \prime \prime}\right) .
$$

The stations at which hourly observations were made are Trevandrum, Madras, Bombay, Salzuflen, Prague, St. Petersburg, Catharinenburg, Barnaul, Nertchinsk, Matosclikin-Schar, Strait of Kara, and Boothia Felix. Bi-hourly observations were taken at Brussels, Greenwich, and Toronto ; in all others the night observations are wanting, and were obtained by interpolation. Moreover, in several stations the number of observations was small, at Madras even only thirty-six days. The tables of that series may be readily distinguished from those belonging to the same stations in the second, by their containing the corrections for several sets of hours, which are not found in the tables of the other.

In Dove's second series, and in all other tables, the corrections given are simply the differences, with reverse signs, between the hourly and the true means, excepting, however, the stations of Toronto, in which the corrections were computed, by Bessel's formula, by Colonel Sabine ; of Prague, by Jelineck ; of Salzburg, and those of Geneva and St. Bernard, by Plantamour.
The observations from which these tables are derived were made hourly at Hobarton during 8 years; at the Cape of Good Hope, for $5 \frac{1}{4}$ years; St. Helena, 5 years; Madras, 5 years ; Bombay, 4 years ; Calcutta, $1 \frac{1}{2}$ years; Toronto, 6 years; Philadelphia, 3 years; Makerstoun, 3 years; Utrecht, $1 \frac{3}{2}$ years; Prague, $10 \frac{1}{2}$ years; Munich, 7 ycars; Salzburg, 6 years; St. Petersburg, 10 years; Catherinenburg, 6 years; Barnaul, $\mathbf{5}$ years; Tiffis, 4 years; Nertchinsk, 6 years; Peking, 4 years; Sitka, $\mathbf{5}$ years. In the following stations the observations were bi-hourly : - Washington, for $1 \frac{1}{2}$ years; Greenwich, 7 years; Dublin, 4 years; Brussels, 9 years; Geneva and St. Bernard, 4 years; Schwerin, $\mathbf{3}$ years.

The observations made in England, and in her colonies, are found in the various goverıment publications. Those of the Russian stations are taken from the Annuaire Météorologique et Magnétique des Ingénieurs des Mines, and in the Annales de
l'Observatoire Physique Central de Russie. The observations made at Pragne, Munich, Geneva, with those at St. Bernard, Makerstoun, Greenwich, Brussels, and Washington, were published by their respective Observatories; those of Utrecht, by BuysBallot; of Dublin, by Lloyd, in his Notes on the Meteorology of Ireland; those of Schwerin were communicated in manuscript by Dippe; the observations at Melville Island are published in No. 42 of the Parliamentary papers for 1854 ; and those at Bossekop, by Martins and Bravais, in the Voyage de la Commission Scientifique du Nord.

The tables of this second series being mostly deduced from longer serics of observations than those in the first, when the same station is found in both, the table in the second is generally to be preferred.

Glaisher's table for Greenwich has been taken from the Greenwich Obserrations. Captain Lefroy kindly furnished the tables for Toronto and Lake Athabasca. 'To him the author is also indebted for the observations made at Montreal by Mr. McCord, from which 'Table X. was computed. Table III., for Philadelphia, was deduced by the writer from the observations made at Girard College under the direction of Prof. A. D. Bache.

In order to facilitate the selection of the tables, they are marked in the table of contents with capitals, which have the following signification:-

A and B mean that the tables have been derived from hourly and bi-hourly observations, and have been computed by Bessel's formula; C, that the tables contain values obtained by interpolation.
$\mathrm{A}^{\prime}, \mathrm{B}^{\prime}$, and $\mathrm{C}^{\prime}$ indicate the tables based respectively on hourly and bi-hourly or partly interpolated observations, which give simply the differences between the hourly and the truc means.

The figures added to the letters indicate the number of years during which the observations used in forming the table were carried on. The stations are arranged, in each continent, in the order of their latitude.

## Use of the Tables.

In order to reduce meteorological means obtained from any set of hours to the true means, the table best suited to the purpose must first be selected. The diurnal variation changing with the seasons, the latitude, the altitude, and the distance from the sea-shore, the station which comes nearest, in all these respects, to the station the observations of which are to be corrected, must be adopted.

Suppose the thermometer has been observed at Baltimore, during the month of January, at 7 A. M., 1 P. M., and 7 P. M., and the monthly means of these hours to be respectively $27^{\circ}, 35^{\circ}$, and $31^{\circ}$ Fahrenbeit. We take Table III., Philadelphia, it being the nearest in latitude and climatic situation. We find the correction for the hours 7, 1, and 7, and we have

| Observ | red Means. | Corrections. |  | True Means. |
| :---: | :---: | :---: | :---: | :---: |
| For 7 A. M. | $27^{\circ}$ | $+3^{\circ} .63$ | $=$ | $30^{\circ} .63$ |
| For 1 P. M. | $35^{\circ}$ | - $3^{\circ} .87$ | $=$ | $31^{\circ} .13$ |
| For 7 P. M. | $31^{\circ}$ | $-1^{\circ} .13$ | $=$ | $29^{\circ} .87$ |
| Sums, | $93^{\circ}$ | $-\overline{10.37}$ | = | $91^{\circ} .63$ |
| Means, | $31^{\circ}$ | - $0^{\circ} .46$ | 二 | $30^{\circ} .54$ True Mean for January. |

It is obvious that the corrections can be applied, either separately to each hour, as is done above, or collectively, in taking the mean of the three bourly corrections and applying it to the mean of the three observations, as in the last line, which is the more convenient method. Therefore, in order to find the correction for any set of hours, it suffices to take the mean of the corrections given in the table for the hours composing the set. The true daily means can be found in the same way, and the true yearly means can be derived from the corrected monthly means, or by applying the corrections given in the last column.

# HoURLY C0RRECTIONS 

FOR

## PERIODIC VARIATIONS.

NORTH AMERICA. - SOUTH AMERICA.

North America. - Washington. Lat. $38^{\circ} 54^{\prime}$ N. Long. $77^{\circ} 3^{\prime}$ W. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the lear. - Dove.

Degrees of Reaumur.


## North America. - Philadelphia. Lat. $39^{\circ} 58^{\prime}$ N. Long. $75^{\circ} 11^{\prime}$ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Guxot.
Degrees of Fabrenheit.

| Hour. | Jan. | Feb. | March. | Aprit. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Miduight | 1.47 | 2.90 | 2.90 | 4.13 | 4.68 | 5.28 | 4.70 | 4.37 | 4.47 | 3.80 | 2.70 | 1.40 | 3.57 |
| 1 | 2.13 | 3.37 | 3.6:3 | 4.88 | 5.25 | 5.93 | 5.57 | 4.93 | 4.60 | 4.17 | 2.73 | 1.83 | 4.08 |
| 2 | 2.20 | 3.57 | 4.17 | 5.88 | 5.9 .5 | 6.45 | 6.10 | 5.43 | 5.00 | 4.87 | 3.20 | 2.20 | 4.59 |
| 3 | 2.57 | 4.43 | 4.50 | 6.28 | 6.68 | 7.23 | 6.53 | 5.50 | 5.47 | 5.27 | 3.37 | 2.53 | 503 |
| 4 | 2.80 | 4.67 | 4.70 | 6.75 | 7.38 | 7.68 | 6.90 | 6.17 | 5.77 | 5.77 | 3.90 | 2.87 | 5.45 |
| 5 | 3.07 | 4.83 | 5.63 | 6.95 | 7.15 | 7.10 | 7.033 | 6.50 | 6.03 | 6.23 | 4.10 | 3.10 | 5.70 |
| 6 | 3.10 | 5.10 | 5.50 | 6.4.) | 5.93 | 5.73 | 5.50 | 5.93 | 5.97 | 6.60 | 4.23 | 3.23 | 5.32 |
| 7 | 3.63 | 5.17 | 5.03 | 4.90 | 3.80 | 3.28 | 3.50 | 4.13 | 4.38 | 5.37 | 4.20 | 3.07 | 4.20 |
| 8 | 3.17 | 3.3:3 | 2.60 | 2.50 | 1.48 | 0.90 | 1.27 | 1.50 | 1.93 | 2.40 | 2.70 | 2.57 | 2.16 |
| 9 | 1.77 | 1.33 | $0 . \sim 0$ | 0.58 | -0.85 | $-1.15$ | $-0.77$ | $-0.43$ | $-0.10$ | -0.37 | 0.57 | 1.17 | 0.19 |
| 10 | $0.0 \%$ | -0.83 | -1.03 | -1.58 | 2.38 | -2.75 | $-2.20$ | $-2.37$ | -2.43 | $-2.67$ | -1.27 | -0.50 | -1.66 |
| 11 | -1. | 2.63 | -3.10 | -3.40 | 90 | -4.33 | $-3.87$ | -4.13 | $-4.27$ | $-4.43$ | -2. | 2.07 | -3.37 |
| Noon. | -2.70 | -3.93 | $-4.43$ | $-4.72$ | $-5.03$ | $-.5 .63$ | $-5.03$ | -5.27 | $-5.50$ | $-5.90$ | $-4.00$ | -2.87 | $-4.58$ |
| 1 | -3.87 | -5.27 | $-5.50$ | $-6.38$ | -6.0 | $-6.88$ | $-5.93$ | $-6.00$ | $-6.47$ | $-7.10$ | $-5.10$ | -3.67 | -5.69 |
| 2 | $-1.57$ | -.5.97 | $-6.17$ | $-7.12$ | $-6.98$ | $-7.15$ | $-6.63$ | -6.83 | $-7.20$ | $-7.80$ | $-5.67$ | $-4.13$ | -6.40 |
| 3 | $-1.70$ | $-6.30$ | $-6.90$ | $-7.63$ | -7.5.5 | $-7.63$ | 7.03 | $-7.00$ | $-7.33$ | 7.80 | $-5.60$ | 4. | -6.64 |
| 4 | -1.18 | -6.00 | -6.7. | $-7.6 .5$ | $-7.78$ | $-7.73$ | $-683$ | $-6.70$ | $-7.13$ | $-7.53$ | -5.07 |  | -6.44 |
| 5 | -2.90 | -4.N7 | -. 5.67 | -7.00 | $-7.33$ | -6.85 | -6.57 | -6.07 | -6.23 | -5.57 | -3.30 | $-2.47$ | -5.40 |
| 6 | -2.0: | -3.03 | -3.60 | $-5.55$ | -.5..53 | -5.55 | -5.13 | $-4.57$ | -3.97 | -3.03 | -1.87 | -1.43 | -3.77 |
| 7 | -1.13 | $-1.77$ | $-1.97$ | $-2.70$ | -2.58 | -3.10 | $-3.20$ | $-2.30$ | $-1.70$ | $-1.20$ | $-0.77$ | -0.70 | -1.95 |
| 8 | -0.4\% | $-0.43$ | $-0.13$ | -0.60 | -0.13 | 0.15 | 0.08 | 0.03 | 0.63 | 0.37 | 0.15 | $-0.10$ | $-0.11$ |
| 9 | 0.17 | $0.3)$ | 0.7 \% | 0.83 | 1.4 | 1.85 | 1.33 | 1.37 | 18.3 | 1.43 | 0.63 | 0.20 | 1.01 |
| 10 | 0.77 | 1.13 | 1.7 | 2.15 | 2.50 | 3.10 | 2.17 | 2.47 | 3.00 | 2.77 | 1.00 | 0.60 | 2.00 |
| 11 | 1.27 | 1.7. | 2.17 | 3.30 | 3.93 | 4.30 | 3.53 | 3.23 | 3.70 | 3.63 | 1.77 | 0.90 | 2.78 |
| 6, 6 | $0.6{ }^{-}$ | 1.01 | 0.9.) | 0.45 | 0.20 | 0.09 | 0.34 | 0.68 | 1.00 | 1.79 | 1.18 | 0.90 | 0.78 |
| 7, 7 | . 2 | 1.70 | 1.53 | 1.10 | 0.46 | 0.09 | 0.15 | 0.92 | 1.32 | 2.09 | 1.7 | 1.19 | 1.13 |
| 8, 8 | 1. ${ }^{\text {a }}$ | 1.15 | 1.18 | 0.8.) | 0.68 | 0.53 | 0.67 | 0.77 | 1.01 | 1.38 | 1.3 | 1.2 | 1.04 |
| 9,9 | 0.9 ; | 0.29 | 0.76 | 0.72 | 0.32 | 0.35 | 0.28 | 0.47 | 0.72 | 0.53 | 0.6 | 0.69 | 0.66 |
| 10, 10 | 0.42 | 0.15 | 0.35 | 0.81 | 0.21 | 0.18 | 0.14 | 0.0 .5 | 0.29 | 0.05 | -0.1 | 0.0 | 0.17 |
| $7,2,9$ | -0.22 | $-0.1$ | -0.15 | -0.53 | -0.57 | -0.77 | -0.61 | -0.44 | -0.3.5 | $-0.33$ | $-0.2$ | -0.29 | $-0.39$ |
| $6,2,8$ | -0.5\% | $-0.13$ | $-0.37$ | -0. 12 | -0.39 | -0.52 | -0.37 | -0.2: | -0.20 | -0.28 | $-0.4$ | -0.67 | $-0.41$ |
| $6,2,10$ | $-0.13$ | 0.0.) | 0.53 | 0.74 | 0.58 | 0.46 | 0.55 | 0.52 | 0.59 | 0. | -0.1 | $-0.10$ | 0.44 |
| 6, 2, 6 | $-1.0$ | -0.72 | $-1.42$ | $-2.07$ | -2.19 | $-2.42$ | $-1.43$ | -1.82 | $-1.7$ | -1. | $-1.1$ | $-0.78$ | -1.14 |
| 7, 2 | -0.47 | $-0.10$ | -0.57 | $-1.11$ | $-1.59$ | $-2.09$ | -1.57 | $-1.3 .5$ | $-1$. | -1.2 | -0.7 | -0.5 | -1.09 |
| 8,2 | -0.70 | -1.32 | -1.65 | $-2.31$ | $-2.7$ | $-3.28$ | $-2.65$ | -2.67 | -2.9 | -2.7 | -1. | $-0.7$ | $-2.10$ |
| 8, 1 | -0.35 | $-0.97$ | -1.3.5 | $-1.94$ | $-2.30$ | $-2.99$ | $-2.33$ | -2.25 | $-2.53$ | -2.35 | $-1.2$ | $-0.55$ | -1.76 |
| 7, 1 | -0.12 | $-0.07$ | -0.2i | -0.74 | -1.14 | -1.80 | -1.22 | -0.9 | -1.0 | -0.8 | -0. | -0.3 | -0.75 |
| $9,12,3,9$ | -1.37 | $-2.15$ | -2.4.5 | $-2.73$ | $-2.90$ | -3.14 | 1-2.88 | -2.83 | -9.8 | -3.16 | -2. | $-1.4$ | -2.53 |

N. America. - Frankfort Arsenal. Lat. $39^{\circ} 57^{\prime}$ N. Long. $75^{\circ} 8^{\prime}$ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 1.34 | 1.46 | 1.75 | 1.87 | 2.60 | 3.41 | 3.07 | 2.69 | 2.63 | 2.40 | 1.18 | 1.34 | 2.15 |
| 2 | 1.51 | 1.73 | 2.13 | 2.33) | 3.0 .5 | 3.73 | 3.51 | 3.04 | 3.05 | 2.67 | 1.27 | 1.50 | 2.46 |
| 3 | 1.82 | 1.98 | 2.56 | 2.88 | 3.43 | 3.92 | 3.83 | 3.32 | 3.49 | 2.94 | 1.41 | 1.66 | 2.77 |
| 4 | 2.13 | 2.23 | 2.90 | 3.29 | 3.57 | 3.84 | 3.84 | 3.36 | 3.73 | 3.13 | 1.51 | 1.80 | 2.94 |
| 5 | 231 | 2.46 | 2.95 | 3.31 | 3.32 | 3.36 | 3.40 | 2.99 | 3.54 | 3.12 | 1.73 | 1.87 | 2.86 |
| 6 | 2.25 | 2.35 | 2.62 | 2.83 | 2.65 | 2.46 | 2.52 | 2.21 | 2.84 | 2.82 | 1.38 | 1.80 | 2.39 |
| 7 | 1.88 | 2.01 | 1.91 | 1.94 | 1.66 | 1.26 | 1.34 | 1.15 | 1.71 | 2.19 | 1.06 | 1.52 | 1.64 |
| 8 | 1.22 | 1.33 | 0.94 | 0.85 | 0.57 | $-0.03$ | 0.08 | 0.01 | 0.36 | 1.26 | 0.58 | 0.97 | 0.68 |
| 9 | 0.34 | 0.30 | $-0.07$ | $-0.20$ | -0.45 | $-1.20$ | -1.06 | $-1.00$ | -0.96 | 0.12 | $-0.02$ | 0.18 | $-0.34$ |
| 10 | $-0.62$ | $-0.72$ | $-1.00$ | $-1.05$ | -1.29 | $-2.11$ | -1.96 | -1.78 | -2.06 | $-1.13$ | $-0.70$ | -0.76 | $-1.27$ |
| 11 | -1.54 | -1.77 | $-1.76$ | -1.69 | -1.97 | $-2.74$ | -2.64 | $-2.34$ | -2.89 | $-2.33$ | $-1.12$ | $-1.70$ | $-2.04$ |
| Noo | -2.30 | $-2.60$ | $-2.32$ | -2.22 | $-2.35$ | $-3.17$ | $-3.16$ | -2.78 | $-3.47$ | -3.35 | $-1.96$ | -2.45 | -2.65 |
| 1 | -2 | -30 | $-2.74$ | $-2.72$ | $-3.07$ | -3.51 | $-3.58$ | $-3.16$ | -3.86 | $-4.05$ | $-2.38$ | -2.87 | $-3.15$ |
| 2 | -3.02 | -3.18 | -3.01 | -3.19 | $-3.52$ | -3.77 | -3.87 | -3.48 | $-4.07$ | $-4.36$ | $-2.54$ | $-2.89$ | -3.41 |
| 3 | $-2.92$ | $-2.93$ | $-3.10$ | $-3.53$ | $-3.78$ | $-3.89$ | $-3.94$ | $-3.61$ | $-4.02$ | -4.22 | $-2.40$ | $-2.54$ | -3.41 |
| 4 | -2.53 | $-2.44$ | $-2.95$ | $-3.55$ | $-3.70$ | -3.75 | $-3.67$ | $-3.42$ | $-3.63$ | $-3.66$ | $-1.96$ | -1.94 | $-3.10$ |
| 5 | -1.90 | $-1.87$ | $-2.50$ | -3.11 | $-3.20$ | $-3.23$ | -3.00 | $-2.81$ | -2.84 | -2.75 | $-1.52$ | -1.23 | $-2.50$ |
| 6 | -1.1 | $-1.11$ | $-1.78$ | -2.23 | $-2.31$ | $-2.33$ | $-2.00$ | -1.83 | $-1.72$ | -1.65 | $-0.56$ | -0.5.5 | $-1.60$ |
| 7 | -0.0.37 | $-0.46$ | -0.92 | $-1.09$ | $-1.19$ | $-1.16$ | $-0.83$ | $-0.67$ | -0.48 | -0.54 | 0.14 | 0.01 | $-0.63$ |
| 8 | 0.29 | 0.12 | $-0.06$ | 0.02 | $-0.10$ | 0.07 | 0.28 | 0.43 | 0.66 | 0.43 | 0.69 | 0.42 | 0.27 |
| 9 | 0.76 | 0.66 | 0.61 | 0.85 | 0.50 | 1.17 | 1.17 | 1.29 | 1.49 | 1.17 | 1.02 | 0.71 | 0.98 |
| 10 | 1.02 | 0.93 | 1.0 | 1.32 | 1.43 | 2.02 | 1.79 | 1.81 | 1.96 | 1.66 | 1.15 | 090 | 1.42 |
| 11 | 1.13 | 1.18 | 1.3 | 1.5 | 1.85 | 2.61 | 2.24 | 2.15 | 2.18 | 1.96 | 0.91 | 1.06 | 1.67 |
| Midn. . | 1.19 | 1.36 | 1.48 | 1.62 | 2.01 | 3.04 | 2.63 | 2.40 | 2.35 | 2.18 | 1.15 | 1.20 | 1.88 |
| 6. 6 | 0.56 | 0.62 | 0.42 | 0.30 | 0.17 | 0.07 | 0.26 | 0.19 | 0.56 | 0.58 | 0.41 | 0.62 | 0.40 |
| 7. 7 | 0.76 | 0.78 | 0.5 | 0.4 | 0.24 | 0.05 | 0.26 | 0.24 | 0.62 | 0.83 | 0.60 | 0.76 | 0.51 |
| 8. 8 | 0.76 | 0.72 | 0.44 | 0.43 | 0.24 | 0.02 | 0.18 | 0.22 | 0.51 | 0.85 | 0.63 | 0.70 | 0.48 |
| 9. 9 | 0.5 | 0.4 | 0.27 | 0.33 | 0.18 | $-0.02$ | 0.06 | 0.14 | 0.26 | 0.64 | 0.50 | 0.44 | 0.32 |
| 10.10 | 0.20 | 0.11 | 0.03 | 0.13 | 0.07 | $-0.05$ | $-0.08$ | 0.03 | $-0.05$ | 0.26 | 0.23 | 0.07 | 0.08 |
| 7. 2. 9 | $-0.13$ | $-0.17$ | $-0.16$ | -0.13 | -0.35 | -0.45 | $-0.45$ | $-0.35$ | $-0.29$ | $-0.33$ | -0.15 | $-0.22$ | $-0.27$ |
| 6. 2. 8 | $-0.16$ | $-0.24$ | $-0.15$ | $-0.11$ | $-0.32$ | $-0.41$ | $-0.36$ | $-0.28$ | $-0.19$ | $-0.37$ | $-0.16$ | $-0.22$ | $-0.25$ |
| 6. 2.10 | 005 | 0.03 | 0.22 | 0.32 | 0.19 | 0.24 | 0.15 | 0.19 | 0.24 | 0.04 | 0.00 | $-0.06$ | 0.14 |
| 6. 2. 6 | $-0.64$ | $-0.65$ | $-0.72$ | $-0.86$ | -1.06 | $-1.21$ | $-1.12$ | $-1.03$ | $-0.98$ | $-1.06$ | $-0.57$ | $-0.55$ | $-0.57$ |
| 7. 2 | -0.57 | $-059$ | $-0.55$ | $-0.63$ | $-0.93$ | $-1.26$ | -1.27 | $-1.17$ | $-1.18$ | $-1.09$ | $-0.74$ | $-0.69$ | $-0.89$ |
| ช. 2 | $-0.90$ | $-0.93$ | $-1.04$ | $-1.17$ | $-1.43$ | $-1.90$ | $-1.90$ | $-1.74$ | $-1.86$ | -I.55 | $-0.98$ | $-0.96$ | $-1.37$ |
| 8. 1 | -0.82 | -0.84 | $-0.90$ | $-0.94$ | -1.25 | $-1.77$ | $-1.75$ | $-1.55$ | $-1.75$ | $-1.40$ | $-0.90$ | $-0.95$ | $-1.24$ |
| 7. 1 | $-0.49$ | $-0.50$ | $-0.42$ | $-0.39$ | $-0.71$ | -1.13 | $-1.12$ | $-1.10$ | -1.08 | $-0.93$ | $-0.66$ | $-0.68$ | $-0.76$ |
| 9.12.3.9 | $-1.03$ | $-1.14$ | $-1.22$ | $-1.28$ | $-1.45$ | $-1.77$ | $-1.75$ | -1.53 | -1.74 | -1.57 | $-0.84$ | $-1.03$ | $-1.36$ |
| 7.2.2(9) | 0.10 | 0.04 | $-0.03$ | 0.11 | $-0.07$ | $-0.04$ | $-0.05$ | 0.06 | 0.16 | 0.04 | 0.14 | 0.01 | 0.04 |
| Dail.ext. | -0.36 | $-0.36$ | -0.08 | $-0.12$ | -0. 11 | 0.02 | $-0.05$ | -0.13 | $-0.17$ | $-0.62$ | $-0.41$ | $-0.51$ | $-0.21$ |

The numbers without sign must be added ; those with the sign - must be subtracted.
N. America. - Frankfort Arsenal. Lat. $39^{\circ} 57^{\prime}$ N. Long. $75^{\circ} 8^{\prime}$ W. Greenw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Fahrenheit


The numbers without sign must be alded; those with the sign - must be subtracted.
N. America. - Toronto. Lat. $43^{\circ} 39^{\prime} 35^{\prime \prime}$ N. Long. $79^{\circ} 21^{\prime} 30^{\prime \prime}$ W. Greemw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Fahrenheit.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 1.87 | 0.92 | 3.04 | 4,43 | 5.90 | 5.94 | 6.30 | 5.06 | 5.74 | 4.16 | 1.91 | 1.04 | 3.87 |
| 2 | 2.16 | 1.33 | 3.56 | 5.11 | 6.64 | 6.62 | 7.13 | 5.68 | 6.68 | 1.68 | 2.14 | 1.13 | 4.41 |
| 3 | 2.39 | 1.91 | 4.19 | 5.76 | 7.36 | 7.29 | 8.01 | 6.82 | 7.63 | 5.04 | 2.39 | 1.40 | 5.02 |
| 4 | 2.68 | 2.66 | 4.75 | 6.17 | 7.65 | 7.56 | 8.44 | 7.61 | 8.19 | 5.20 | 2.61 | 1.78 | 5.45 |
| 5 | 3.02 | 3.40 | 4.95 | 5.94 | 7.07 | 6.98 | 7.88 | 7.49 | 7.94 | 5.02 | 2.68 | 2.16 | 5.38 |
| 6 | 3.29 | 3.92 | 4.61 | 4.97 | 5.49 | 5.38 | 6.14 | 6.14 | 6.71 | 4.45 | 2.52 | 2.39 | 4.68 |
| 7 | 3.26 | 3.98 | 3.65 | 3.35 | 3.17 | 3.04 | 3.49 | 3.67 | 4.52 | 3.44 | 2.0 .5 | 2.27 | 3.33 |
| 8 | 2.72 | 3.40 | 2.12 | 1.42 | 0.68 | 0.43 | 0.52 | 0.68 | 1.78 | 1.91 | 1.15 | 1.71 | 1.55 |
| 9 | 1.58 | 2.33 | 0.29 | $-0.50$ | -1.51 | $-1.85$ | $-2.12$ | -2.09 | $-1.06$ | $-0.05$ | $-0.07$ | 0.79 | $-0.36$ |
| 10 | 0.00 | 0.61 | $-1.60$ | $-2.07$ | -3.08 | -3.47 | $-4.01$ | $-4.14$ | $-3.62$ | $-2.25$ | $-1.46$ | $-0.34$ | $-2.12$ |
| 11 | -1.71 | $-1.15$ | -3.26 | $-3.26$ | $-4.14$ | $-4.16$ | $-5.15$ | $-5.33$ | $-5.72$ | $-4.39$ | $-2.79$ | $-1.44$ | $-3.55$ |
| N | -3.11 | $-2.66$ | $-4.55$ | $-4.19$ | $-5.00$ | $-5.18$ | $-5.90$ | $-5.96$ | $-7.25$ | $-6.12$ | $-3.78$ | $-2.30$ | $-4.66$ |
| 1 |  |  |  | -5 | -5.99 | $-5.94$ | $-6.59$ | $-6.50$ | -8.33 | $-7.11$ | $-4.28$ | $-2.77$ | -5 45 |
| 2 | - 9 9 | - | -5 | -5 | $-7.16$ | $-6.89$ | -7. | $-7.11$ | -8.89 | -7.25 | 4 | 6 | $-594$ |
| 2 | -0.95 | $\left.\right\|_{-4.07} ^{-3.9 .2}$ |  |  | -8.15 | $-7.74$ | $-8.28$ | $-7.70$ | -8.87 | $-6.53$ | -3.51 | -2.66 | -6.08 |
| 3 | -3.53 | -3.92 | -5.60 | -6.35 | -8.15 | -7.74 <br> -8.08 | -8.28 -8.55 | -7.70 -7.81 | -8.87 -8.12 | -6.33 -5.18 | --3.51 | -2.26 | $-5.72$ |
| 4 | $-2.84$ | $-3.33$ | -5.02 | $-6.18$ | -8.51 | -8.08 | -8.55 | $-7.81$ | -8.12 | $-5.18$ | $-2.52$ | $-2.23$ | $-5.72$ |
|  |  |  |  |  |  |  |  | $-6.95$ | $-6.59$ | -3.53 | $-1.44$ | $-1.71$ | $-4.84$ |
| 5 |  | -2 | - | - | - |  |  | -6.95 | -6.59 | -1.91 | -1.44 |  |  |
| 6 | $-1.62$ | $-1.89$ | $-2.75$ | $-4.66$ | $-5.83$ | -5.65 | $-5.94$ | $-5.00$ | $-4.43$ | -1.91 | $-0.45$ | $-1.13$ | -3.44 |
| 7 | $-1.24$ | $-1.24$ | $-1.31$ | -2.81 | $-3.08$ | $-3.04$ | $-3.17$ | $-2.25$ | $-1.94$ | $-0.50$ | 0.32 | $-0.54$ | $-1.73$ |
| 8 | $-0.85$ | $-0.68$ | 0.05 | $-0.77$ | $-0.16$ | -0.18 | $-0.18$ | 0.65 | 0.43 | 0.65 | 0.86 | 0.02 | $-0.02$ |
| 9 | $-0.43$ | $-0.25$ | 1.15 | 1.06 | 2.30 | 2.30 | 2.39 | 2.97 | 2.30 | 1.53 | 1.17 | 0.47 | 1.42 |
| 10 | 0.16 | 0.11 | 1.89 | 2.41 | 3.94 | 3.98 | 4.14 | 4.32 | 3.58 | 2.25 | 1.37 | 0.81 | 2.41 |
| 11 | 0.83 | 0.3 | 2.34 | 3.26 | 4.82 | 4.93 | 5.11 | 4.77 | 4.37 | 2.90 | 1.53 | 0.97 | 3.02 |
| Midn. | 1.42 | 0.63 | 2.66 | 3.85 | 5.33 | 5.45 | 5.64 | 4.8 .1 | 5.00 | 3.56 | 1.71 | 1.01 | 3.42 |
| 6. 6 | 0.83 | 1.01 | 0.95 | 0.16 | $-0.18$ | 0.14 | 0.11 | 0.56 | 1.13 | 1.28 | 1.04 | 0.63 | 0.61 |
| 7. 7 | 1.01 | 1.27 | 1.17 | 0.29 | $-0.0 .5$ | 0.00 | 0.16 | 0.72 | 1.28 | 1.49 | 1.19 | 0.86 | 0.81 |
| 8. 8 | 0.92 | 1.37 | 1.08 | 0.34 | 0.27 | 0.14 | 0.16 | 0.68 | 1.10 | 1.28 | 1.01 | 0.86 | 0.77 |
| 9. 9 | 0.59 | 0.99 | 0.72 | 0.29 | 0.41 | 0.23 | 0.14 | 0.45 | 0.63 | 0.74 | 0.56 | 0.63 | 0.54 |
| 10.10 | 0.07 | 0.36 | 0.14 | 0.16 | 0.43 | 0.27 | 0.07 | 0.09 | $-0.02$ | 0.00 | $-0.05$ | 0.23 | 0.14 |
| 7. 2. 9 | $-0.38$ | $-0.11$ | $-0.32$ | $-0.45$ | $-0.56$ | $-0.52$ | $-0.51$ | $-0.16$ | $-0.70$ | -077 | $-0.32$ | $-0.0 .5$ | $-0.41$ |
| 6. 2. 8 | -0.52 | $-0.27$ | $-0.36$ | $-0.52$ | $-0.61$ | $-0.56$ | $-0.50$ | $-0.11$ | $-0.59$ | $-0.70$ | -0.25 | -0.16 | $-0.43$ |
| 6. 2.10 | -0.18 | $-0.02$ | 0.27 | 0.54 | 0.77 | 0.83 | 0.95 | 1.13 | 0.47 | $-0.18$ | $-0.09$ | 0.11 | 0.38 |
| 6. 2. 6 | $-0.77$ | $-0.68$ | -1.28 | $-1.82$ | $-2.50$ | -2.39 | $-2.43$ | $-1.98$ | -2.21 | $-1.5 .5$ | $-0.70$ | -0.54 | $-1.58$ |
|  |  |  |  |  | -2.00 | $-1.94$ | $-2.00$ | $-1.73$ | -2.18 | $-1.91$ | $-1.06$ | -0.29 | $-1.31$ |
| 7. 2 | -0 | -0 | -1.04 | -1.19 | -2.00 | -1.94 | -2.00 | -1.73 |  | -1.91 |  | -0.59 | -2. 21 |
| 8. 2 | $-0.63$ | $-0.34$ | -1.80 | $-2.18$ | -3.24 | $-3.24$ | -3.49 | $-3.22$ | -3.56 | -2.68 | -1.51 | -0.59 | -2.21 |
| 8. 1 | $-0.59$ | $-0.14$ | -1.62 | $-1.80$ | $-2.66$ | -2.77 | $-3.04$ | -2.93 | $-3.29$ | -2.61 | $-1.58$ | $-0.54$ | -1.96 |
| \%. 1 | $-0.32$ | 0.16 | $-0.86$ | $-0.81$ | -1.42 | $-1.46$ | $-1.55$ | -1.42 | $-1.91$ | $-1.85$ | -1.13 | -0.25 | -1.06 |
| 9.12 .3 |  | -1.1 | -2.18 | $-2.50$ | $-3.03$ | -3.13 | $-3.19$ | $-3.20$ | -3.71 | $-2.79$ | $-1.55$ | $-0.92$ | $-2.43$ |
| 7. $2.2(9)$ | -0.41 | -0.16 | 0.07 | -0.07 | 0.16 | 0.18 | 0.20 | 0.63 | 0.07 | -0.18 | - 0.07 | 0.09 | 0.05 |

N. America. - Toronto. Lat. $43^{\circ} 39^{\prime} 35^{\prime \prime}$ N. Long. $79^{\circ} 21^{\prime} 30^{\prime \prime}$ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.83 | 0.41 | 1.35 | 1.97 | 2.62 | 2.64 | 2.80 | 2.25 | 2.55 | 1.85 | 0.85 | 0.46 | 1.72 |
| 2 | 0.96 | 0.59 | 1.58 | 2.27 | 2.95 | 2.94 | 3.17 | 2.57 | 2.97 | 2.08 | 0.95 | 0.50 | 1.96 |
| 3 | 1.06 | 0.85 | 1.86 | 2.56 | 3.27 | 3.24 | 3.56 | 3.03 | 3.39 | 2.24 | 1.06 | 0.62 | 2.23 |
| 4 | 1.19 | 1.18 | 2.11 | 2.74 | 3.40 | 3.36 | 3.75 | 3.38 | 3.64 | 2.31 | 1.16 | 0.79 | 2.42 |
| 5 | 1.34 | 1.51 | 2.20 | 2.64 | 3.14 | 3.10 | 3.50 | 3.33 | 3.53 | 2.23 | 1.19 | 0.96 | 2.39 |
| 6 | 1.46 | 1.74 | 2.05 | 2.21 | 2.44 | 2.39 | 2.73 | 2.73 | 2.98 | 1.99 | 1.12 | 1.06 | 2.08 |
| 7 | 1.45 | 1.77 | 1.62 | 1.50 | 1.41 | 1.35 | 1.55 | 1.63 | 2.01 | 1.53 | 0.91 | 1.01 | 1.48 |
| 8 | 1.21 | 1.51 | 0.94 | 0.63 | 0.30 | 0.19 | 0.23 | 0.30 | 0.79 | 0.85 | 0.51 | 0.76 | 0.69 |
| 9 | 0.70 | 0.99 | 0.13 | $-0.22$ | $-0.67$ | -0.82 | $-0.94$ | -0.93 | $-0.47$ | -0.02 | $-0.03$ | 0.35 | $-0.16$ |
| 10 | $-0.00$ | 0.27 | $-0.71$ | $-0.92$ | $-1.37$ | $-1.54$ | -1.78 | $-1.84$ | $-1.61$ | $-1.00$ | $-0.65$ | $-0.15$ | $-0.94$ |
| 11 | -0.76 | $-0.51$ | $-1.45$ | -1.45 | -1.84 | $-1.98$ | -2.29 | $-2.37$ | -2.54 | $-1.95$ | -1.24 | $-0.64$ | $-1.59$ |
| Noo | $-1.35$ | $-1.18$ | $-2.02$ | $-1.86$ | $-2.22$ | $-2.30$ | $-2.62$ | $-2.65$ | $-3.22$ | $-2.72$ | $-1.68$ | $-1.02$ | $-2.07$ |
| 1 | -1.73 | -1.63 | $-2.38$ | $-2.22$ | $-2.66$ | -2.64 | $-2.93$ | $-2.89$ | -3.70 | -3.16 | -1.90 | $-1.23$ | $-2.42$ |
| 2 | $-1.77$ | -1.81 | $-2.54$ | $-2.56$ | -3.18 | -3.06 | -3.32 | -3.16 | -3.95 | -3.22 | -1.84 | $-1.27$ | $-2.64$ |
| 3 | -1.57 | $-1.74$ | $-2.49$ | $-2.82$ | $-3.62$ | -3.44 | -3.68 | $-3.42$ | -3.94 | $-2.90$ | $-1.56$ | $-1.18$ | $-2.70$ |
| 4 | -1.26 | -1.50 | $-2.23$ | -2.85 | -3.78 | $-3.59$ | -3.80 | $-3.47$ | -3.61 | $-2.30$ | -1.12 | $-0.99$ | $-2.54$ |
| 5 | -0.95 | $-1.17$ | $-1.79$ | $-2.64$ | -3.45 | $-3.30$ | -3.48 | -3.09 | $-2.93$ | -1.57 | -0.64 | $-0.76$ | $-2.15$ |
| 6 | -0.72 | $-0.84$ | -1.22 | $-2.07$ | $-2.59$ | $-2.51$ | $-2.64$ | $-2.22$ | -1.97 | -0.85 | $-0.20$ | $-0.50$ | $-1.53$ |
| 7 | -0.55 | $-0.55$ | $-0.58$ | $-1.25$ | -1.37 | $-1.35$ | $-1.41$ | -1.00 | $-0.86$ | -0.22 | 0.14 | $-0.24$ | $-0.77$ |
| 8 | -0.39 | $-0.30$ | 0.02 | $-0.34$ | -0.07 | $-0.08$ | $-0.08$ | 0.29 | 0.19 | 0.29 | 0.36 | 0.01 | $-0.01$ |
| 9 | -0.19 | $-0.11$ | 0.51 | 0.47 | 1.02 | 1.02 | 1.06 | 1.32 | 1.02 | 0.68 | 0.52 | 0.21 | 0.63 |
| 10 | 0.07 | 0.05 | 0.84 | 1.07 | 1.75 | 1.77 | 1.84 | 1.92 | 1.59 | 1.00 | 0.61 | 0.36 | 1.07 |
| 11 | 0.37 | 0.17 | 1.04 | 1.45 | 2.14 | 2.19 | 2.27 | 2.12 | 1.94 | 1.29 | 0.68 | 0.43 | 1.34 |
| Midn. | 0.63 | 0.28 | 1.18 | 1.71 | 2.37 | 2.42 | 2.53 | 2.15 | 2.22 | 1.58 | 0.76 | 0.45 | 1.52 |
| 6. 6 | 0.37 | 0.45 | 0.42 | 0.07 | $-0.08$ | $-0.06$ | 0.05 | 0.25 | 0.50 | 0.57 | 0.46 | 0.28 | 0.27 |
| 7. 7 | 0.45 | 0.61 | 0.52 | 0.13 | 0.02 | 0.00 | 0.07 | 0.32 | 0.57 | 0.66 | 0.53 | 0.38 | 0.36 |
| 8. 8 | 0.41 | 0.61 | 0.48 | 0.15 | 0.12 | 0.06 | 0.07 | 0.30 | 0.49 | 0.57 | 0.45 | 0.38 | 0.34 |
| 9. 9 | 0.26 | 0.44 | 0.32 | 0.13 | 0.15 | 0.10 | 0.06 | 0.20 | 0.28 | 0.33 | 0.25 | 0.28 | 0.24 |
| 10.10 | 0.03 | 0.16 | 0.06 | 0.07 | 0.19 | 0.12 | 0.03 | 0.04 | $-0.01$ | 0.00 | -0.02 | 0.10 | 0.06 |
| 7. 2. 9 | -0.17 | -0.0.5 | $-0.14$ | -0.20 | -0.25 | -0.23 | $-0.24$ | $-0.07$ | -0.31 | -0.34 | $-0.14$ | $-0.02$ | -0.18 |
| 6.2. 8 | $-0.23$ | $-0.12$ | $-0.16$ | $-0.23$ | -0.2 | -0.25 | $-0.22$ | -0.05 | $-0.26$ | $-0.31$ | $-0.11$ | $-0.07$ | $-0.19$ |
| 6. 2.10 | -0.08 | $-0.01$ | 0.12 | 0.24 | 0.34 | 0.37 | 0.42 | 0.50 | 0.21 | -0.08 | $-0.04$ | 0.05 | 0.17 |
| 6. 2. 6 | $-0.34$ | $-0.30$ | $-0.57$ | -0.81 | -1.11 | $-1.06$ | -1.08 | $-0.88$ | -0.98 | -0.69 | $-0.31$ | $-0.24$ | $-0.70$ |
| 7. 2 | -0.16 | $-0.02$ | -0.46 | $-0.53$ | -0.89 | -0.86 | -0.89 | $-0.77$ | $-0.97$ | -0.8.5 | -0.47 | $-0.13$ | -0.58 |
| 8. 2 |  |  |  |  |  |  | -1.55 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 |  |  |  |  |  |  |  |  | -1.46 |  |  |  | -0.87 |
| 7. 1 | $-0.14$ | 0.07 | $-0.38$ | -0.36 | -0.63 | $-0.65$ | -0.69 | -0.63 | -0.85 | $-0.82$ | $-0.50$ | -0.11 | $-0.47$ |
| 9.12.3.9 | -0.61 | -0.51 | -0.97 | -1.11 | -1.37 | -1.39 | '-1.55 | -1.42 | -1.65 | $-1.24$ | -0.69 | -0.41 | -1.08 |
| 7. 2.2(9) | -0.18 | $-0.07$ | 0.03 | $-0.03$ | 0.07 | 0.08 | 0.09 | 0.28 | 0.03 | $-0.08$ | 0.03 | 0.04 | 0.02 |
| Dail ext | -0.16 | $-0.02$ | $-0.17$ | $-0.07$ | $-0.19$ | -0.12 | $-0.03$ | '0.05 | -0.16 | -0.16 | -0.36 | -0.11 | -0 |

The numbers without sign must be added; those with the sign - must be subtractea.

North America. - Toronto. Lat. $43^{\circ} 40^{\prime}$ N. Long. $79^{\circ} 21^{\prime}$ W. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Lefroy.

Degrees of Fahrenheit.

| Hour. | Jan. | Feb. | March. | Aprit. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midnight. | 1.47 | 1.73 | 2.63 | 3.22 | 5.02 | 5.15 | 6.37 | 5.33 | 5.96 | 3.22 | 1.80 | 0.90 | 3.57 |
| 1 | 1.95 | 2.09 | 3.11 | 3.79 | 5.93 | 6.00 | 7.13 | 6.06 | 4.57 | 3.80 | 2.10 | 1.50 | 4.00 |
| 2 | 2.05 | 2.46 | 3.47 | 4.48 | 6.77 | 6.70 | 7.63 | 6.69 | 5.17 | 4.13 | 2.36 | 1.85 | 4.48 |
| 3 | 2.20 | 2.82 | 3.76 | 5.08 | 7.45 | 7.50 | 8.41 | 7.29 | 5.59 | 4.31 | 2.66 | 1.96 | 4.92 |
| 4 | 2.28 | 3.20 | 4.07 | 5.38 | 7.93 | 8.06 | 9.03 | 7.63 | 6.18 | 4.64 | 2.85 | 2.01 | 5.27 |
| 5 | 2.46 | 3.62 | 4.35 | 5.75 | 7.53 | 7.88 | 9.02 | 7.89 | 6.77 | 4.77 | 2.76 | 2.07 | 5.43 |
| 6 | 1.83 | 4.23 | 4.75 | 5.48 | 5.40 | 5.21 | 5.92 | 6.57 | 6.17 | 4.71 | 2.52 | 2.39 | 4.60 |
| 7 | 1.94 | 4.34 | 3.93 | 3.22 | 2.43 | 2.41 | 2.38 | 3.28 | 3.68 | 3.94 | 2.52 | 2.55 | 3.05 |
| S | 1.66 | 3.29 | 1.89 | 1.09 | 0.06 | 0.10 | $-0.31$ | 0.21 | 1.02 | 1.66 | 1.53 | 2.12 | 1.25 |
| 9 | 0.63 | 1.02 | -0.25 | $-1.01$ | $-2.11$ | $-1.82$ | -2.39 | $-2.26$ | $-1.52$ | -1.01 | 0.01 | 0.92 | -0.52 |
| 10 | $-0.59$ | $-0.95$ | $-1.91$ | -2.4.) | -3.51 | $-3.49$ | $-3.98$ | $-4.18$ | $-3.47$ | $-2.93$ | $-1.41$ | $-0.53$ | $-2.47$ |
| 11 | $-1.70$ | 2.44 | $-3.1$ | -3.83 | $-4.92$ | $-4.77$ | $-5.49$ | $-5.57$ | $-4.85$ | $-4.33$ | $-2.44$ | $-1.72$ | $-3.77$ |
| Noon. | -2. | -3.56 | $-4.15$ | -4.86 | -5.87 | $-5.88$ | $-6.72$ | $-6.39$ | $-5.95$ | $-5.36$ | $-3.34$ | -2.52 | $-4.76$ |
| 1 | -2.92 | -4.49 | $-4.79$ | $-5.72$ | $-6.83$ | -6.59 | $-7.58$ | $-7.11$ | $-6.58$ | $-5.76$ | $-3.74$ | -3.06 | $-5.43$ |
| 2 | -3.20 | -4.88 | -5.31 | $-6.14$ | $-7.13$ | $-7.03$ | -8.26 | $-7.62$ | $-6.96$ | $-6.04$ | $-3.82$ | -3.31 | $-5.81$ |
| 3 | -3.16 | $-4.90$ | $-5.15$ | $-6.16$ | $-7.20$ | 7.37 | -8.34 | $-7.98$ | $-7.01$ | $-5.85$ | $-3.64$ | $-3.13$ | $-5.52$ |
| 4 | -2.63 | $-4.47$ | -4.65 | -5.8 1 | -7.17 | $-7.60$ | -8.25 | $-7.79$ | $-6.75$ | $-5.17$ | $-2.83$ | $-2.47$ | $-5.47$ |
| 5 | -1.68 | -3.30 | $-3.92$ | -5.12 | $-6.80$ | $-7.18$ | $-7.93$ | $-7.20$ | $-5.78$ | -3.40 | -1.58 | $-1.49$ | $-4.61$ |
| 6 | $-0.90$ | $-1.87$ | $-2.35$ | $-3.12$ | $-5.05$ | $-5.73$ | $-6.57$ | -5.39 | -3.16 | $-1.37$ | $-0.76$ | $-0.82$ | -3.12 |
| 7 | $-0.40$ | $-0.98$ | $-0.91$ | $-0.94$ | $-2.19$ | $-2.99$ | $-3.28$ | $-1.64$ | $-0.43$ | $-0.25$ | $-0.15$ | $-0.47$ | $-1.22$ |
| 8 | -0.12 | $-0.13$ | 0.03 | 0.66 | 0.43 | 0.33 | 0.68 | 1.23 | 0.81 | 0.48 | 0.19 | -0.12 | 0.38 |
| 9 | 0.07 | 0.52 | 1.00 | 1.78 | 2.31 | 2.44 | 2.99 | 2.70 | 1.90 | 1.25 | 0.44 | 0.18 | 1.46 |
| 10 | 0.44 | 1.06 | 1.63 | 2.59 | 3.29 | 3.80 | 4.24 | 3.73 | 2.94 | 1.97 | 0.78 | 0.47 | 2.24 |
| 11 | 0.77 | 1.60 | 2.01 | 3.07 | 1.20 | 4.76 | 5.21 | 4.54 | 3.61 | 2.65 | 1.13 | 0.59 | 2.85 |
| 6, 6 | 0.16 | 1.18 | 1.20 | 1.03 | 0.17 | -0.26 | $-0.32$ | 0.59 | 1.50 | 1.67 | 1.38 | 0.78 | 0.74 |
| 7, 7 | 0.77 | 1.67 | 1.51 | 1.14 | 0.12 | -0.29 | $-0.45$ | 0.82 | 1.62 | 1.84 | 1.18 | 1.04 | 0.91 |
| 8, 8 | 0.77 | 1.58 | 0.96 | 0.87 | 0.24 | 0.21 | 0.18 | 0.72 | 0.91 | 1.45 | 0.95 | 1.15 | 0.82 |
| 9,9 | 0.35 | 0.77 | 0.37 | 0.38 | 0.10 | 0.31 | 0.30 | 0.22 | 0.19 | 0.10 | 0.22 | 0.55 | 0.32 |
| 10, 10 | $-0.07$ | 0.05 | -0.14 | $-0.07$ | $-0.26$ | 0.25 | 0.13 | $-0.22$ | $-0.26$ | $-0.48$ | $-0.31$ | $-0.03$ | -0.11 |
| 6, 2, 10 | $-0.31$ | 0.14 | 0.36 | 0.64 | 0.52 | 0.66 | 0.63 | 0.89 | 0.72 | 0.21 | $-0.17$ | $-0.15$ | 0.34 |
| 7, 2, 9 | $-0.40$ | $-0.0$ | $-0.09$ | $-0.35$ | $-0.80$ | $-0.73$ | $-0.96$ | $-0.55$ | $-0.46$ | -0.28 | $-0.29$ | $-0.19$ | $-0.43$ |
| $9,12,3,9$ | -1.23 | $-1.73$ | -2.01 | $-2.56$ | -3.22 | $-3.16$ | -3.6I | -3.48 | $-3.14$ | $-2.74$ | $-1.63$ | $-1.14$ | $-2.18$ |
| Mean. | 25.82 | 23.70 | 29.79 | 41.99 | 52.92 | 60.67 | 66.39 | 65.86 | 57.55 | 44.14 | 36.18 | 27.40 | 44.37 |

The numbers without sign must be added ; those with the sign - must be subtracted.
F

## North America. - Toronto. Lat. $43^{\circ} 40^{\prime}$ N. Long. $79^{\circ} 21^{\prime}$ W. Gr.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour | Jan. | Feb | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Miln. | .6s | 0.51 | 1.10 | 1.45 | 2.24 | 2.36 | 2.91 | 2.43 | 1.76 | 1.44 | 0.51 | 0.40 | 1.53 |
| 1 | 0.88 | 0.98 | 1.31 | 0.75 | 2.62 | 2.67 | 3.29 | 2.72 | 2.03 | 1.71 | 0.94 | 0.66 | 1.80 |
| 2 | 0.92 | 1.13 | 1.48 | 2.08 | 2.99 | 2.98 | 3.54 | 3.02 | 2.29 | 1.85 | 1.06 | 0.83 | 2.01 |
| 3 | 0.99 | 1.82 | 1.61 | 2.17 | 3.31 | 3.32 | 3.56 | 3.32 | 2.49 | 1.92 | 1.20 | 0.88 | 2.20 |
| 4 | 1.03 | 1.45 | 1.78 | 2.36 | 3.52 | 3.58 | 4.14 | 3.18 | 2.76 | 2.06 | 1.25 | 0.90 | 2.36 |
| 5 | 1.11 | 1.61 | 2.01 | 2.52 | 3.49 | 3.49 | 4.16 | 3.57 | 3.04 | 2.13 | 1.23 | 0.91 | 2.44 |
| 6 | 0.79 | . 5 | 2.13 | 2.47 | 40 | 2.32 | 2.74 | 2.92 | 2.74 | 2.04 | 1.11 | 1.09 | 2.05 |
| 7 | 0.5 | 1.92 | 1.75 | 1.45 | 1.08 | 1.07 | 1.11 | 1.60 | 1.60 | 1.70 | 1.11 | 1.16 | 1.36 |
| S | 0.73 | 1.47 | 0.87 | 0.15 | 0.09 | 0.03 | -0.05 | 0.15 | 0.38 | 0.70 | 0.64 | 0.97 | 0.56 |
| 9 | 0.30 | 0.44 | -0.10 | -0.43 | -0.94 | -0.81 | -1.03 | -0.96 | -0.69 | -0.49 | -0.04 | 0.45 | -0.36 |
| 10 | -0.25' | - 0.45 | -0.87 | -1.11 | -1.69 | -1.55 | -1.78 | -1.84 | -1.57 | -1.35 | -0.68 | -0.20 | 1.11 |
| 11 | -0.77 | -1.16 | -1.41 | $-1.72$ | -2.20 | -2.12 | -2.47 | -2.48 | -2.20 | -1.96 | -1.13 | -0.75 | $-1.70$ |
| Noon. | -1.12 | -1.69 | -1.87 | -2.18 | -2.62 | -2.61 | -3.0.5 | -3.04 | -2.64 | -2.36 | -1. | -1. | -2.15 |
| 1 | -1.31 | $-2.07$ | -2.16 | -2.60 | -3.03 | -2.93 | -3.46 | -3.25 | -2.90 | -2.5.5 | -1.66 | -1.42 | -2.45 |
| 2 | -1.46 | -2.25 | 41 | $-2.76$ | -3.18 | -3.12 | -3.84 | -3.51 | -3.08 | $-2.70$ | -1.69 | -1.49 | $-2.62$ |
| 3 | -1.14 | -2.24 | -2.32 | -2.80 | -3.21 | -3.29 | -3.92 | -3.66 | -3.09 | -2.60 | $-1.62$ | -1.38 | -2.63 |
| 4 | $-1.21$ | -2.00 | -2.11 | -2.62 | -3.19 | -3.40 | -3.93 | -3.60 | $-3.00$ | $-2.28$ | -1.2 | 1.09 | $-2.47$ |
| 5 | -0.77 | -1.47 | . 78 | -2.30 | -3.02 | -3.13 | -3.72 | -3.35 | -2.57 | . 50 |  | . 67 | -2.08 |
| 6 | -0.40 | , | -1.03 | -1.50 | -2.2 4 | -2.55 | -3.05 | -2.51 | -1.38 | -0.59 | -0.32 | -0.36 | -1.40 |
| 7 | -0.17 | -0.38 | -0.39 | -0.37 | -0.96 | -1.33 | -1.54 | -0.74 | -0.18 | -0.10 | -0.06 | -0.21 | -0.53 |
| 8 | -0.03 | 0.00 | 0.05 | 0.33 | 0.21 | 0.13 | 0.33 | 0.56 | 0.39 | 0.23 | 0.08 | -0.0.t | 0.19 |
| 9 | 0.06 | 0.28 | 0.50 | 0.81 | 1.02 | 1.09 | 1.38 | 1.26 | 0.85 | 0.57 | 0.20 | 0.07 | 0.67 |
| 10 | 0.23 | 0.53 | 0.79 | 1.16 | 1.4.5 | 1.69 | 1.93 | 1.72 | 1.32 | 0.90 | 0.36 | 0.20 | 1.02 |
| 11 | 0.37 | 0.76 | 1.08 | 1.38 | 1.86 | 2.12 | 2.45 | 2.07 | 1.60 | 1.20 | 0.52 | 0.25 | 1.31 |
| Mean. | $-2.97$ | -3.59 | -0.99 | 4.72 | 9.29 | 12.75 | 15.11 | 15.00 | 11.37 | 5.42 | 1.58 | -2.03 |  |

## X.

Nortil America. - Montreal. Lat. $45^{\circ} 30^{\prime}$ N. Long. $73^{\circ}$ © $\mathfrak{P}^{\prime}$ E. Gr. Degrees of Fahrenheit.

| Hour. | Aur. | Sept. | Oct. | Tov. | Dee. | Jan. | Feb. | March. | April. | May. | June. | July. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Miln. | 4.00 | 8.89 | 2.83 | 1.36 | 1.65 | 1.10 | 1.28 | 1.31 | 2.52 | 4.55 | 5.2 .5 | 4.39 | 2.85 |
| 2 | 5.39 | 4.34 | 4.01 | 1.59 | 1.00 | 2.36 | 2.69 | 2.88 | 4.37 | 6.95 | 7.42 | 7.17 | 4.20 |
| 4 | 6.34 | 5.60 | 4.84 | 1.81 | 1.35 | 2.88 | 3.36 | 5.56 | 7.09 | 6.95 | 7.18 | 7.57 | 4.96 |
| 6 | 5.99 | 4.59 | 4.83 | 1.36 | 1.32 | 3.54 | 3.90 | 5.22 | 5.56 | 6.61 | 5.55 | 5.46 | 4.50 |
| 8 | 2.79 | 2.19 | 2.52 | 0.78 | 0.92 | 3.10 | 3.22 | 8.30 | 3.44 | 3.06 | 0.88 | 0.60 | 2.24 |
| 10 | -1.74 | -1.15 | -0.99 | -0.41 | 0.21 | -0.21 | -0.81 | -0.03 | -0.79 | -0.97 | -1.75 | -2.55 | -0.93 |
| Noon. | -5.63 | -5.43 | -4.22 | -1.87 | -1.22 | -2.52 | -3.50 | -4.23 | -5.01 | $-7.10$ | -5.17 | -5.46 | -4.30 |
| 2 | -7.93 | -6.60 | -6.96 | -2.37 | - 3.5 | -4.07 | $-5.43$ | -6 49 | -5.99 | -8.76 | -7.72 | -7.36 | -6.02 |
| 4 | -7.72 | -6.70 | -5.62 | -2.52 | -3.29 | -3.88 | -3.60 | -5.96 | -.5. 79 | -8.35 | -7.00 | -7.51 | -5.65 |
| 6 | -5.63 | -2.80 | $-2.79$ | -1.01 | $-1.30$ | -1.77 | -1.50 | -3.43 | -3.88 | -3.87 | $-5.02$ | $-5.40$ | -3.20 |
| 8 | -0.70 | 0.10 | -0.2.5 | 0.03 | 0.02 | -0.90 | -0.59 | -1.23 | -0.81 | -1.61 | $-1.10$ | -0.67 | -0.65 |
| 10 | 1.99 | 2.39 | 1.12 | 1.18 | 0.59 | 0.17 | 0.22 | -0 30 | 0.64 | -1.87 | 2.47 | 2.64 | 1.30 |
| Mean. | 66.40 | 57.70 | 48.31 | 30.39 | 23.42 | 8.10 | 20.84 | 27.31 | 4.2 .27 | 56.61 | 6438 | 70.39 | 43.01 |

The numbers without sign mast be added ; those with the sigu - must be subtracted.

## North America. - Montreal, Contimued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year.

Degrees of Fahrenheit.


The numbers without sign must be added : those with the sign - must be subtracted.

Arctic America. - Boothia Felix. Lat. $69^{\circ} 59^{\prime}$ N. Long. $9 \mathfrak{P}^{\circ} 1^{\prime}$ W. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.08 | 0.42 | 1.61 | 2.17 | 2.64 | 2.38 | 1.78 | 1.34 | 0.56 | 0.30 | 0.02 | 0.12 | 1.12 |
| 2 | 0.10 | 0.28 | 1.85 | 2.25 | 2.75 | 2.55 | 1.78 | 1.30 | 0.62 | 0.32 | 0.18 | 0.13 | 1.15 |
| 3 | 0.11 | 0.25 | 2.10 | 2.30 | 2.61 | 2.45 | 1.65 | 1.17 | 0.66 | 0.33 | 0.29 | 0.10 | 1.12 |
| 4 | 0.11 | 0.21 | 2.30 | 2.26 | 2.23 | 2.05 | 1.35 | 1.02 | 0.66 | 0.34 | 0.31 | 0.06 | 1.02 |
| 5 | 0.10 | 0.22 | 2.38 | 2.02 | 1.76 | 1.39 | 0.99 | 0.86 | 0.56 | 0.32 | 0.24 | 0.02 | 0.87 |
| 6 | 0.10 | 0.26 | 2.23 | 1.53 | 1.02 | 0.65 | 0.61 | 0.70 | 0.46 | 0.27 | 0.13 | $-0.04$ | 0.64 |
| 7 | 0.09 | 0.29 | 1.77 | 0.81 | 0.35 | $-0.04$ | 0.26 | 0.50 | 0.27 | 0.17 | 0.02 | $-0.07$ | 0.37 |
| 8 | 0.08 | 0.22 | 0.98 | -0.06 | $-0.32$ | $-0.58$ | $-0.03$ | 0.24 | 0.05 | 0.01 | 0.01 | $-0.10$ | 0.04 |
| 9 | 0.06 | 0.05 | -0.06 | $-0.98$ | $-0.95$ | -0.99 | -0.37 | -0.10 | $-0.12$ | $-0.20$ | $-0.04$ | $-0.10$ | $-0.32$ |
| 10 | 0.02 | -0.26 | $-1.22$ | $-1.81$ | $-1.54$ | -1.33 | $-0.70$ | $-0.49$ | $-0.43$ | $-0.41$ | $-0.14$ | $-0.10$ | $-0.70$ |
| 11 | $-0.02$ | $-0.58$ | $-2.28$ | -2.45 | $-2.06$ | -1.66 | $-1.05$ | $-0.86$ | $-0.65$ | -0.59 | -0.26 | $-0.11$ | $-1.05$ |
| N | -0.05 | $-0.87$ | $-3.05$ | $-2.86$ | $-2.46$ | $-2.02$ | $-1.13$ | -1.16 | -0.82 | $-0.69$ | $-0.32$ | $-0.12$ | $-1.32$ |
| 1 | -0. | -1.02 | $-3.38$ | -3.03 | $-2.66$ | -2.33 | $-1.70$ | -1.34 | -0.93 | $-0.68$ | $-0.30$ | -0.14 | -1.47 |
| 2 | $-0.1$ | -0.98 | -3.26 | -2.96 | $-2.65$ | -2.48 | -1.86 | -1.38 | $-0.94$ | -0.57 | -0.19 | -0.13 | -1.46 |
| 3 | $-0.1$ | $-0.78$ | $-2.7$ | -2.67 | -2.40 | -2.38 | -1.78 | $-1.32$ | -0.93 | -0.38 | $-0.04$ | -0.10 | -1.31 |
| 4 | $-0.14$ | $-0.46$ | $-2$ | -2.18 | $-1.98$ | $-1.98$ | $-1.56$ | -1.18 | -0.68 | $-0.18$ | 0.06 | $-0.05$ | -1.03 |
| 5 | -0. | $-0.14$ | $-1.29$ | $-1.50$ | $-1.45$ | $-1.36$ | $-1.18$ | $-1.01$ | $-0.44$ | 0.01 | 0.24 | 0.01 | -0.69 |
| 6 | $-0.09$ | 0.13 | -0.57 | $-0.74$ | $-0.55$ | $-0.66$ | $-0.7 \mathrm{~S}$ | $-0.78$ | -0.17 | 0.14 | 0.31 | 0.07 | $-0.34$ |
| 7 | -0. | 0.32 | 0.0 | 0.06 | $-0.34$ | $-0.01$ | $-0.34$ | $-0.50$ | 0.08 | 0.22 | 0.36 | 0.10 | -0.01 |
| 8 | -0.05 | 0.43 | 0.44 | 0.78 | 0.20 | 0.51 | 0.07 | $-0.16$ | 0.26 | 0.25 | 0.38 | 0.11 | 0.27 |
| 9 | $-0.03$ | 0.50 | 0.76 | 1.35 | 0.74 | 0.92 | 0.50 | 0.24 | 0.38 | 0.26 | 0.38 | 0.10 | 0.53 |
| 10 | $-0.02$ | 0.51 | 0.99 | 1.74 | 1.28 | 1.26 | 0.90 | 0.66 | 0.44 | 0.26 | 0.35 | 0.10 | 0.71 |
| 11 | 0.0 | 0.52 | 1.19 | 1.95 | 1. | 1.63 | 1.20 | 1.01 | 0.48 | 0.26 | 0.28 | 0.09 | 0.37 |
| Midn. . | 0.05 | 0.49 | 1.38 | 2.08 | 2.30 | 2.04 | 1.59 | 1.25 | 0.51 | 0.28 | 0.15 | 0.12 | 1.02 |
| 6. 6 | 0.01 | 0.20 | 0.83 | 0.40 | 0.07 | -0.01 | $-0.09$ | $-0.04$ | 0.15 | 0.21 | 0.09 | 0.02 | 0.15 |
| 7. | 0 | 0.3 | 0.89 | 0.44 | 0.01 | $-0.03$ | $-0.04$ | $-0.00$ | 0.18 | 0.20 | 0.17 | 0.02 | 0.18 |
| 8. 8 | 0 | 0.3 | 0.71 | 0.36 | $-0.06$ | $-0.04$ | 0.02 | 0.04 | 0.16 | 0.13 | 0.20 | 0.01 | 0.16 |
| 9. 9 | 0.02 | 0.2 | 0.35 | 0.19 | $-0.11$ | $-0.04$ | 0.07 | 0.07 | 0.13 | 0.03 | 0.17 | -0.00 | 0.10 |
| 10.10 | $-0.00$ | 0.13 | $-0.12$ | $-0.04$ | $-0.13$ | $-0.04$ | 0.10 | 0.09 | 0.01 | -0.08 | 0.11 | $-0.00$ | 0.00 |
| 7. 2. 9 | -0.03 | -0.06 | $-0.24$ | $-0.27$ | -0.52 | -0.53 | $-0.37$ | -0.21 | $-0.10$ | $-0.05$ | 0.06 | -0.03 | $-0.20$ |
| 6. 2. 8 | $-0.03$ | $-0.10$ | $-0.20$ | $-0.22$ | $-0.48$ | $-0.44$ | $-0.39$ | $-0.28$ | $-0.07$ | $-0.02$ | 0.02 | $-0.02$ | $-0.19$ |
| 6. 2.10 | -0.0 | $-0.07$ | $-0.01$ | 0.10 | $-0.12$ | $-0.19$ | $-0.12$ | $-0.01$ | $-0.01$ | $-0.01$ | 0.01 | $-0.02$ | $-0.04$ |
| 6. 2. 6 | $-0.04$ | $-0.20$ | $-0.53$ | $-0.72$ | $-0.84$ | $-0.83$ | $-0.68$ | $-0.49$ | $-0.22$ | -0.05 | $-0.00$ | $-0.03$ | $-0.39$ |
| 7. 2 | $-0.03$ | $-0.35$ | $-0.75$ | -1.08 | $-1.15$ | $-1.26$ | -0.80 | -0.44 | $-0.34$ | -0.20 | -0.11 | -0.10 |  |
| 8. 2 | $-0.03$ | -0.38 | $-1.14$ | $-1.51$ | -1.49 | $-1.53$ | $-0.95$ | $-0.57$ | -0.45 | -0.2S | $-0.09$ | $-0.12$ | $-0.71$ |
| 8. 1 | -0.02 | $-0.40$ | $-1.20$ | $-1.55$ | $-1.49$ | $-1.46$ | -0.87 | $-0.55$ | -0.44 | $-0.34$ | -0.15 | $-0.12$ | $-0.72$ |
| 7. 1 | -0.01 | $-0.37$ | $-0.81$ | $-1.11$ | $-1.16$ | $-1.19$ | $-0.72$ | $-0.42$ | $-0.33$ | $-0.26$ | $-0.16$ | $-0.11$ | $-0.55$ |
| 9.12.3.9 | -0.0.4 | $-0.25$ | $-1.25$ | $-1.29$ | $-1.27$ | $-1.12$ | $-0.77$ | -0.59 | $-0.37$ | $-0.25$ | $-0.01$ | -0.06 |  |
| 7.2.2(9) | $-0.03$ | 0.08 | 0.01 | 0.14 | $-0.21$ | $-0.17$ | -0.15 | $-0.10$ | 0.02 | 0.03 | 0.14 | -0.00 | $-0.02$ |
| Dail. ext. | -0.02 | $-0.25$ | -0.50 | $-0.37$ | 0.05 | 0.04 | $-0.04$ | $-0.02$ | $-0.14$ | -0.18 | 0.03 | -0.01 | $-0.16$ |

The numbers without sign must be added; those with the sign - must be subtracted.
N. America. - Lake Athabasca. Lat. $59^{\circ}$ N. Long. $111^{\circ}$ W. Greemw. Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Lefroy.

The corrections for April and May are derived from observations made at Fort Simpson, Lat. 620 N.
Degrees of Fahrenheit.

| Hour. | April. | May. | October. | November. | December. | January. | February. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| daily ext. | 1.58 | 1.71 | 0.33 | 0.25 | -0.17 | 0.77 | 1.19 |
| 6, 6 | 1.15 | 0.51 | 1.07 | 0.59 | 0.27 | 0.84 | 1.19 |
| 7,7 | 1.50 | 0.16 | 0.76 | 0.54 | 0.30 | 0.58 | 1.31 |
| 8, 8 | 1.72 | 0.18 | 0.69 | 0.55 | 0.62 | 0.95 | 1.27 |
| 9, 9 | 0.54 | 0.30 | 0.37 | 0.32 | 0.84 | 0.80 | 0.78 |
| 10, 10 | -0.43 | -0.03 | -0.32 | -0.06 | 0.34 | 0.12 | 0.31 |
| 11, 11 | -1.68 | -1.20 | -0.57 | -0.37 | 0.10 | -0.62 | -0.23 |
| 6, 2, 10 | 0.47 | 0.46 | -0.31 | -0.21 | -0.22 | -0.17 | -0.05 |
| 7, 3, 11 | 0.46 | 0.59 | -0.40 | -0.16 | 017 | 0.06 | -0.26 |
| Mean. | 32.48 | 44.56 | 21.44 | 9.76 | 0.40 | $-23.00$ | 4.79 |

## XIV.

Arctic America. - Melville Island. Lat. $74^{\circ} 47^{\prime}$ N. Long. $110^{\circ} 48^{\prime}$ W. Gr.Dove.
Degrees of Reaumur.

| Ifour. | January. | February. | March. | October. | Hour. | November. | December. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A.M. 1 | 0.12 | 0.10 | 1.01 | 0.04 | A.M. 2 | -0.12 | -0.09 |
| 3 | 0.18 | 0.05 | 1.22 | 0.12 | 4 | -0.02 | -0.06 |
| 5 | 0.07 | 0.25 | 090 | 0.24 | 6 | 0.00 | 0.11 |
| 7 | 0.11 | 0.29 | 0.57 | 0.20 | 8 | -0.22 | 0.07 |
| 9 | -0 13 | -0.24 | 0.29 | -0.15 | 10 | -0.38 | 0.11 |
| 11 | -0.3.5 | -0.43 | -1.33 | -0.46 | 12 | -0.41 | 0.24 |
| P.M. 1 | -0.22 | -0.6.5 | -1.72 | -0.43 | P.M. 2 | -0.27 | 0.14 |
| 3 | -0.2.5 | -0.52 | -1.00 | 0.22 | 4 | 0.16 | 0.00 |
| 5 | 0.04 | 0.04 | -0.43 | -0.24 | 6 | 0.27 | -0.12 |
| 7 | 0.04 | 0.24 | 0.06 | -0.10 | 5 | 0.38 | -0.26 |
| 9 | 0.11 | 0.35 | 0.33 | 0.11 | 10 | 0.36 | -0.12 |
| 11 | 0.40 | 0.49 | 0.66 | 0.43 | 12 | 0.2. | 0.00 |
| Mean. | -29.75 | $-27.58$ | -22.73 | -1432 | Mean. | -18.6.5 | -25.75 |

XV.

Spitzbergen. - Hecla Cove. Lat. $79^{\circ} 55^{\prime}$ N. Long. $16^{\circ} 49^{\prime}$ E. Gr.Dove.
Degrees of Reaumur.

| Hour | June. | July. | Augast. | Hour. | June. | July. | Angust. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A.M. I | 0.63 | 0.62 | 0.42 | P.M. 1 | -0.67 | -0.67 | $-0.63$ |
| 3 | 0.43 | 0.84 | 0.54 | 3 | -0.58 | -0.42 | $-0.58$ |
| 5 | 0.26 | $0 . .51$ | 0.53 | 5 | -0.27 | -0.14 | $-0.32$ |
| 7 | -0.12 | -0.02 | 0.25 | 7 | 0.26 | -0.17 | $-0.06$ |
| 9 | $-0.29$ | $-0.09$ | -0.09 | 9 | 0.21 | 0.06 | 0.14 |
| 11 | $-0.17$ | $-0.49$ | -0.45 | 11 | 0.61 | 0.26 | 0.24 |
|  |  |  |  | Mean. | 1.71 | 3.63 | 2.84 |

The numbers without sign must be added; those with the sigu - must be subtracted.

## XVI.

S. America. - Rio Janeiro. Lat. $22^{\circ} 54^{\prime}$ S. Long. $43^{\circ} 16^{\prime}$ W. Greemw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Fahrenheit.

| Hours. | Jan. | Feb, | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.74 | 1.51 | 1.80 | 0.90 | 1.13 | 0.56 | 1.85 | 1.31 | 1.04 | 0.97 | 1.76 | 1.31 | 1.24 |
| 2 | 1.64 | 2.41 | 2.45 | 1.64 | 2.12 | 1.53 | 2.75 | 2.00 | 1.69 | 1.64 | 2.32 | 2.05 | 2.03 |
| 3 | 2.50 | 3.11 | 3.02 | 2.32 | 2.93 | 243 | 3.47 | 2.66 | 2.27 | 2.21 | 2.75 | 266 | 2.70 |
| 4 | 3.08 | 3.90 | 3.24 | 2.79 | 3.38 | 3.04 | 3.87 | 3.04 | 2.59 | 2.50 | 2.93 | 2.99 | 3.06 |
| 5 | 3.22 | 3.29 | 3.15 | 2.90 | 3.40 | 3.29 | 3.83 | 3.08 | 2.66 | 2.52 | 279 | 2.99 | 3.08 |
| 6 | 2.93 | 2.84 | 2.75 | 2.75 | 3.06 | 3.20 | 3.47 | 2.79 | 2.41 | 2.27 | 2.32 | 2.68 | 2.79 |
| 7 | 2.30 | 2.21 | 2.14 | 2.30 | 2.48 | 2.84 | 2.70 | 2.25 | 2.00 | 1.82 | 1.67 | 2.12 | 2.23 |
| 8 | 1.49 | 1.49 | 1.40 | 1.71 | 1.55 | 2.39 | 1.96 | 1.60 | 1.46 | 1.23 | 0.90 | 1.40 | 1.58 |
| 9 | 0.63 | 0.72 | 0.59 | 1.04 | 1.15 | 1.82 | 1.15 | 0.90 | 0.86 | 0.65 | 0.14 | 0.59 | 0.86 |
| 10 | -0.07 | -0.05 | -0.23 | 0.32 | 0.50 | 1.13 | 0.32 | 0.23 | 0.18 | 0.05 | -0.56 | -0.23 | -0.14 |
| 11 | -0.75 | -0.66 | -1.01 | -0.45 | -0.23 | 0.32 | -0.50 | $-0.50$ | -0.54 | -0.59 | -1.22 | -1.04 | -0.61 |
| Noon. | -1.40 | -1.64 | -1.71 | -1.22 | -0.99 | -0.65 | -1.31 | -1.19 | -1.26 | -1.22 | -1.80 | -1.82 | -1.35 |
| 1 | -2.00 | -2.30 | -2.30 | -1.94 | -1.71 | -1.67 | -2.16 | -1.91 | -1.89 | -1.78 | -2.32 | -2.43 | -2.03 |
| 2 | -2.41 | -2.75 | -2.66 | -2. 11 | -2.30 | -2.48 | -2.88 | -2.48 | -2 34 | -2.16 | -2.66 | -2.81 | -2.52 |
| 3 | -2.59 | -2.85 | -2.84 | -2.66 | -2.66 | -2.99 | -3.40 | -2 84 | -2.50 | -2.27 | -2.79 | -2.86 | -2.77 |
| 4 | -2.45 | -2.70 | -2.77 | -2.57 | -2.75 | -3.04 | -3.60 | -2.93 | -2.36 | -2.12 | -2.66 | -2.59 | -2 70 |
| 5 | -2 05 | -2.30 | $-2.50$ | -2.21 | -2.54 | -2.75 | -3.47 | -2.68 | -2.00 | -1.75 | -2.25 | -2.09 | -2.39 |
| 6 | -1.51 | -1.82 | -2.12 | -1.76 | -2.21 | -2.23 | -3.04 | -2.23 | -1.55 | -1 37 | -1.67 | -1.49 | -1.91 |
| 7 | -1.04 | -1.40 | -1.67 | -1.25 | -1.89 | -1.76 | -2.39 | -1.67 | 1.13 | -1.04 | -1.08 | -0.99 | -1.44 |
| 8 | -0.72 | -1.13 | -1.22 | -0.95 | -1.67 | -1.42 | -1.85 | -1.13 | -0.83 | -0.77 | -0 59 | -0.61 | -1.08 |
| 9 | -0.59 | -0.92 | -0.77 | -0.72 | -1.44 | -1.26 | -1.22 | -0.70 | -0.61 | -0.61 | -0.14 | -0.38 | -0.79 |
| 0 | -0.56 | -0.63 | -0.25 | $-0.52$ | -1.13 | -1.13 | -0.59 | -0.32 | -0.41 | -0.45 | 0.23 | -0 16 | -0.50 |
| 11 | -0.41 | -0.14 | 0.36 | -0.25 | $-0.63$ | -0.86 | 0.09 | 0.09 | -0.09 | -0.16 | 0.65 | 0.14 | 0.09 |
| Midn. | 0.00 | 0.59 | 1.06 | 0.23 | 0.14 | -0.29 | 0.92 | 0.61 | 0.35 | 0.32 | 1.15 | 0.65 | 0.47 |
| 6. 6 | 0.72 | 0.52 | 0.32 | 0.50 | 0.43 | 0.50 | 0.30 | 0.29 | 0.43 | 0.45 | 0.34 | 0.61 | 0.45 |
| 7. 7 | 0.63 | 0.41 | 0.25 | 0.52 | 0.29 | 0.54 | 0.16 | 0.29 | 0.45 | 0.41 | 0.29 | 0.56 | 0.41 |
| 8. 8 | 35 | 018 | 0.09 | 0.38 | 0.09 | 0.50 | 0.07 | 0.25 | 0.32 | 0.27 | 0.16 | 0.41 | 0.25 |
| 9. 9 | 0.05 | -0.11 | -0.09 | -0.16 | -0.16 | 0.29 | -0.05 | 0.11 | 0.14 | 0.05 | 0.00 | 0.11 | 0.05 |
| 10.10 | -0.32 | -0.34 | -0.2.5 | -0.11 | -0.32 | 0.00 | -0.14 | -0.05 | -0.11 | -0.20 | -0.18 | -0.20 | -0.18 |
| 7. 2. 9 | -0.23 | -0.50 | -0.43 | -0.27 | -0.43 | -0.29 | -0.47 | -0.32 | -0.32 | $-0.32$ | -0.38 | -0.36 | -0.36 |
| 6. 2.8 | -007 | -0.34 | -0.38 | $-0.20$ | -0.29 | -0.23 | $-0.43$ | -0.27 | -0.25 | -0.23 | -0.32 | -0.25 | $-0.27$ |
| 6. 2.10 | $-0.02$ | -0.18 | -0.05 | -0.07 | -0.11 | -0.14 | 0.00 | 0.00 | -0.11 | -0.11 | -0.05 | -0.09 | -0.07 |
| 6. 2. 6 | -0.3 t | $-0.59$ | -0.68 | -0.47 | -0.47 | -0.50 | -0.81 | -0.63 | -0.50 | -0.43 | -0.68 | $-0.54$ | -0.56 |
| 7. 2 | -0.07 | $-0.27$ | $-0.27$ | -0.07 | 0.09 | 0.15 | -0.09 | -0.11 | -0.18 | -0.18 | -0.50 | $-0.36$ | -0.16 |
| 8. 2 | -0.47 | -0.63 | -0.63 | -0.36 | -0.23 | -0.05 | -0.47 | -0.45 | -0.45 | -0 45 | -0.88 | -0 72 | -0.47 |
| 8. 1 | -0.27 | -0.41 | -0.45 | -0.11 | 0.07 | 0.36 | -0.11 | -0.16 | -0.23 | -0.25 | $-0.72$ | -0.52 | -0.23 |
| 7. | 0.16 | -0.0.5 | -0.09 | 0.18 | 0.38 | 059 | -0.27 | 018 | 007 | 0.02 | -0.34 | -0.16 | -0.11 |
| 9.12.3.9 | -0.97 | -1.19 | -1.19 | -0.90 | -0.99 | -0 77 | -1.19 | -0.97 | -0 88 | -0.86 | -1.15 | -1.13 | -1.01 |
| 7. 2.2(9) | -0.32 | -0.61 | -0.52 | -0.38 | -0.68 | $-6.54$ | -0.65 | -0.41 | -0.38 | -0.38 | -0.32 | -0.36 | -0.47 |
| nail. ext. | 0.32 | 0.27 | 0.20 | 0.14 | 0.34 | 0.14 | 0.14 | 0.09 | 0.09 | 0.14 | 0.07 | 0.07 | 0.16 |

## XVII.

S. America. - Rio Janeiro. Lat. $22^{\circ} 54^{\prime}$ S. Long. $43^{\circ} 16^{\prime}$ W. Greemo.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.33 | 0.67 | 0.80 | 0.40 | 0.50 | 0.25 | 0.82 | 0.58 | 0.16 | 0.43 | 0.78 | 0.58 | 0.55 |
| 2 | 0.73 | 1.07 | 110 | 0.73 | 0.94 | 0.68 | 1.22 | 0.89 | 0.75 | 0.73 | 1.03 | 0.91 | 0.90 |
| 3 | 1.11 | 1.38 | 1.34 | 1.03 | 1.30 | 1.08 | 1.54 | 1.18 | 101 | 0.98 | 1.22 | 1.18 | 1.20 |
| 4 | 1.37 | 1.51 | 1.44 | 1.24 | 1.50 | 1.35 | 1.72 | 1.35 | 1.15 | 1.11 | 1.30 | 1.33 | 1.36 |
| 5 | 1.43 | 1.46 | 1.40 | 1.29 | 1.51 | 1.46 | 1.70 | 1.37 | 1.18 | 1.12 | 1.24 | 1.33 | 1.37 |
| 6 | 1.30 | 1.26 | 1.22 | 1.22 | 1.36 | 1.42 | 1.54 | 1.24 | 1.07 | 1.01 | 1.03 | 1.19 | 1.24 |
| 7 | 1.02 | 0.98 | 0.95 | 1.02 | 1.10 | 1.26 | 1.20 | 1.00 | 0.89 | 0.81 | 0.74 | 0.94 | 0.99 |
| 8 | 0.66 | 0.66 | 0.62 | 0.76 | 0.82 | 1.06 | 0.87 | 0.71 | 065 | 0.57 | 0.40 | 0.62 | 0.70 |
| 9 | 0.30 | 0.32 | 0.26 | 0.46 | 0.51 | 0.81 | 0.51 | 0.40 | 0.38 | 0.30 | 0.06 | 0.26 | 0.38 |
| 10 | -0.03 | -0.02 | -0.10 | 0.14 | 0.22 | 0.50 | 0.14 | 0.10 | 0.08 | 0.02 | -0.25 | $-0.10$ | 0.06 |
| 11 | -0.34 | -0.38 | -0.45 | -0.20 | -0.10 | 0.14 | -0.22 | -0.22 | -0.24 | -0.26 | -0.54 | -0.46 | -0.27 |
| Noon. | -0.62 | -0.73 | -0.76 | -0.54 | -0.4 | -0.29 | -0.53 | -0.53 | -0.56 | -0.54 | -0.80 | -0.81 | -0.60 |
| 1 | -0.89 | -1.02 | -1.02 | -0.86 | -0.76 | -0.74 | -0.96 | -0.85 | -0.84 | -0.79 | -1.03 | -1.0 | -0.90 |
| 2 | -1.07 | -1.22 | -1.18 | -1.07 | -1.02 | -1.10 | -1.28 | -1.10 | -1.01 | -0.96 | -1.18 | -1.2 | -1.12 |
| 3 | -1.15 | -1.28 | -1.26 | -1.18 | -1.18 | -1.33 | -1.31 | -1.26 | -1.11 | -1.01 | -1.24 | -1.27 | $-1.23$ |
| 4 | -1.09 | -1.20 | -1.23 | -1.14 | -1.22 | -1.35 | -1.60 | -1.30 | -1.05 | -0.94 | -1.1s | 1.1 | $-1.20$ |
| 5 | -0.91 | $-1.02$ | -1.11 | -0.98 | -1.13 | -1.22 | -1.54 | -1.19 | -0.89 | -0.79 | -1.00 | -0.93 | $-1.06$ |
| 6 | -0.67 | -0.81 | -0.94 | -0.78 | -0.98 | -0.99 | -1.3.5 | -0.99 | -0.69 | -0.61 | -0.74 | -0.66 | -0.85 |
| 7 | -0.46 | -0.62 | -0.74 | -0.57 | -0.54 | -0.78 | -1.06 | -0.74 | -0.50 | -0.46 | -0.48 | -0.4 | -0.64 |
| 8 | -0.32 | -0.50 | -0.54 | $-0.12$ | -0.74 | -0.63 | -0.82 | -0.50 | -0.37 | -0.34 | -0.26 | -0.27 | -0.48 |
| 9 | -0.26 | -0.41 | -0.34 | -0.32 | -0.64 | $-0.56$ | -0.54 | -0.31 | -0.27 | -0.27 | -0.06 | -0.17 | -0.35 |
| 10 | -0.2. | -0.28 | -0.11 | $-0.23$ | $-0.50$ | $-0.50$ | -0.26 | -0.14 | -0.18 | -0.20 | 0.10 | -0.07 | -0.22 |
| 11 | -0.18 | -0.06 | 16 | -0.11 | -0.28 | -0.38 | 0.04 | -0 04 | -0.04 | -0.07 | 0.29 | 0.06 | -0.04 |
| Midn. | 0.00 | 0.26 | 0.47 | 0.10 | 0.06 | -0.13 | 0.41 | 0.27 | 0.17 | 0.14 | 0.51 | 0.29 | 0.21 |
| 6. 6 | 0.32 | 0.23 | 0.14 | 0.22 | 0.19 | 0.22 | 0.10 | 013 | 0.19 | 0.20 | 0.15 | 027 | 0.20 |
| 7. 7 | 0.28 | 0.18 | 0.11 | 0.23 | 0.13 | 0.24 | 0.07 | 0.13 | 0.20 | 0.18 | 0.13 | 0.25 | 0.18 |
| 8. 8 | . 17 | 0.05 | 0.04 | 0.17 | 0.04 | 0.22 | 0.03 | 0.11 | 0.14 | 0.12 | 0.0 | 0.18 | 0.11 |
| 99 | 0.02 | -0.05 | -0.04 | 0.07 | -0.07 | 0.13 | -0.02 | 0.05 | 0.06 | 0.02 | -0.00 | 0.0 | 0.02 |
| 10.10 | -0.14 | -0.15 | -0.11 | -0.05 | -0.14 | -0.00 | -0.06 | $-0.02$ | -0.05 | -0. 19 | -0.08 | -0.09 | -0.08 |
| 7.2. 9 | -0.10 | -0.22 | -0.19 | -0.12 | -0.19 | -0.13 | -0.21 | 0.14 | -0.14 | -0.14 | -0.17 | -0.16 | -0.16 |
| 6. 2. s | -0.03 | $-0.15$ | -0.17 | -0.09 | -0.13 | $-0.10$ | -0.19 | -0.12 | -0.11 | $-0.10$ | $-0.14$ | -0.11 | -0.12 |
| 6. 2.10 | -0.01 | -0 08 | $-0.02$ | -0.03 | -0.05 | -0.06 | -0.00 | -0.00 | -0.05 | -0.05 | -0.02 | -0.04 | -0.03 |
| 6. 2. 6 | -0.15 | -0.26 | $-0.30$ | $-0.21$ | $-0.21$ | $-0.22$ | -0.36 | -0.23 | -0.22 | -0.19 | $-0.30$ | $-0.24$ | -0.25 |
| 7. 2 | -0.03 | -0.12 | $-0.12$ | $-0.03$ | 0.04 | 0.08 | -0.04 | -0 05 | -0.08 | -0.08 | -0.2 2 | -0.16 | -9.07 |
| 8. 2 | -0.21 | -0.28 | -0.28 | $-0.16$ | -0.10 | -0.02 | -0.21 | -0) 20 | -0.20 | -0.20 | -0.39 | $-0.32$ | -0.21 |
| 8. | -0.12 | -0.18 | $-0.20$ | -0.05 | 0.03 | 16 | -0.05 | - 0.07 | $-0.10$ | -0.11 | $-0.32$ | -0.23 | -0.10 |
| 7. | 0.07 | -0.02 | -0.04 | 008 | 0.17 | 0.26 | 0.12 | 0.08 | 0.03 | 0.01 | $-0.15$ | $-0.07$ | 0.05 |
| 9.12.3.9 | $-0.43$ | -0 33 | -0.53 | $-0.40$ | -0.44 | -0.34 | -0 53 | -0. 3 | -0.39 | $-0.38$ | -0.51 | -0.50 | -0.45 |
| 7. 2.2(9) | -0.14 | $-0.27$ | $-0.23$ | -0.17 | $-0.30$ | -0.24 | -0.29 | $-0.18$ | -0.17 | -0.17 | -0.14 | -0.16 | -0.21 |
| Dail.ext. | 0.14 | 0.12 | 0.09 | 0.06 | 0.15 | 0.06 | 0.06 | 0.04 | 0.04 | 0.06 | 0.03 | 0.03 | 0.07 |

The numbers without sign must be added ; those with the sign - must be subtracted.
N. America. - Amherst College. - Lat. $42^{\circ} 22^{\prime}$ N. Long. $72^{\circ} 30^{\prime}$ W. Greenw.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dewey.

Degrees of Fahrenheit.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 3.90 | 2.78 | 4.73 | . 23 | 5.51 | 6.64 | 6.39 | 5.14 | 5.36 | 4.87 | 2.34 | 1.63 | 4.63 |
| 2 | 4.24 | 3.03 | 4.81 | 6.69 | 6.48 | 7.28 | 6.83 | 5.66 | 6.12 | 5.65 | 2.99 | 2.20 | 5.16 |
| 3 | 4.13 | 3.20 | 5.36 | 7.42 | 7.41 | 7.92 | 7.28 | 6.03 | 6.92 | 6.46 | 3.49 | 2.55 | 5.68 |
| 4 | 4.50 | 3.94 | 5.69 | 7.85 | 7.58 | 8.04 | 7.42 | 6.29 | 6.56 | 7.09 | 3.72 | 2.70 | 6.06 |
| 5 | 4.72 | 4.20 | 6.04 | 8.12 | 8.18 | 7.80 | 7.54 | . 66 | 7.88 | 7.72 | 4.03 | 3.32 | 6.35 |
| 6 | 68 | 4.78 | 6.12 | 7.77 | 6.77 | 5.96 | 6.02 | 5.51 | 7.14 | 7.65 | 4.34 | 3.78 | 5.93 |
| 7 | 4.75 | 4.78 | 4.62 | 5.97 | 4.22 | 4.20 | 3.80 | 45 | 5.32 | 6.87 | 1.28 | 3.97 | 4.77 |
| 8 | 3.83 | 3.75 | 2.08 | 3.04 | 1.62 | 1.40 | 1.09 | 1.96 | 2.52 | 4.31 | 2.68 | 4.13 | 2.70 |
| 9 | 1.46 | 1.45 | -0.46 | 0.08 | -0.60 | -0.88 | $-0.57$ | -0.93 | -0.56 | 0.83 | 0.34 | 2.40 | 0.19 |
| 10 | 1.26 | -0 | -2.57 | - 2.69 | -1.12 | -3.12 | -3.80 | -3.0 | -3.32 | $-2.24$ | -1.43 | $-0.55$ | -2.34 |
| 11 | $-4.10$ |  | -4.77 | - 5.65 | -5.12 | -5.68 | $-6.43$ | -5 | . 04 | $-5.02$ | -3.01 | -2.76 | $-4.73$ |
| Noon. | 2 |  |  | - | 5 | -8.08 | -8.50 | $-6.86$ | -8.16 | -7.06 | -5.01 | $-4.30$ | -6.63 |
| 1 | -7.46 |  |  | - 9.46 | 5 | -9.36 | 83 | - |  | -8.24 | -6.12 | -6.14 | .84 |
| 2 | -7.80 | -6 | 3.1 | -10.42 | -8.75 | $-9.00$ | -9.50 | -7.86 | -9.50 | -9.28 | -5.97 | -6.30 | -8.26 |
| 3 | -7.32 | -5. 8 | 1 | $-9.81$ | -8.27 | -S.60 | -7.50 | -7.67 | -9.20 | -9.24 | -5.28 | -5.60 | $-7.70$ |
| 4 | -5.84 | -4 | 23 | -8.61 | . 86 | $-7.84$ | 17 | -6.23 | -8.40 | -8.24 | -3.85 | -3.76 | -6.66 |
| 5 | -3.32 | -3.10 | 65 | - 7.04 | -5.97 | -6.00 | -5.83 | -5.26 | -6.44 | -5.6. 5 | -2.28 | -2.03 | -4.88 |
| 6 | -2.06 | -1 | 16 | - 4.50 | -4.08 | -4.20 | $-4.17$ | -2.82 | . 52 | -3.50 | -0.85 | -0.68 | -2.92 |
| 7 | 0.24 | -1.0 | 7 | - 1.69 | -2.35 | -1.92 | -1.54 | -1 | -1.47 | -1.24 | -0.64 | -0.31 | -1.11 |
| 8 | 0.6-1 | -0.43 | 0.93 | 0.27 | -0.19 | 0.04 | 0.98 | 0.3 | 0.11 | 0.13 | 0.08 | 0.20 | 0.26 |
| 9 | 50 | 0.28 | 89 | 1.77 | . 6 | 96 | 5 | 1.59 | . 99 | 1.16 | 0.80 | 0.69 | 1.53 |
| 10 | 2.01 | 0.5 | 29 | 31 | 2.73 | 3.20 | 3.79 | 3.02 | 3.53 | 1.90 | 1.16 | 1.20 | 2.48 |
| 11 | 2.42 | 1.19 | 29 | 23 | 3.99 | 4.20 | 4.24 | 3.79 | 4.61 | 3.24 | 1.96 | 1.58 | 3.31 |
| Midnight. | 2.50 | 1.70 | 4.85 | 4.92 | 4.75 | 5.48 | 5.31 | 4.52 | 5.34 | 4.09 | 2.40 | 1.98 | 3.99 |
| 3, 9, 3, 9 | -0.05 | -0.22 | -0.08 | $-0.13$ | 0.05 | 0.10 | 0.49 | 0.26 | -0.21 | -0.20 | -0.16 | -0.01 | -0.01 |
| 9,9 | 8 | 0.8 | 72 | 93 | 53 | 0.54 | 9 | 0.33 | . 72 | 1.00 | 0.57 | 1.55 | . 86 |
| 10, 10 | 0.33 | -0 | 0.36 | 0.31 | . 81 | 0.04 | 0.00 | -0.51 | 0.11 | -0.17 | -0.13 | 0.33 | 0.12 |
| 7, 2, 9 | -0.48 | -0.33 | -0.61 | -0.89 | -0.96 | -0.95 | -0.58 | -0.60 | -0.83 | -0.42 | -0.29 | -0.55 | -0.65 |
| 6, 2, 10 | -0 | -0 |  | -0.24 | 0.25 | 0.0 | 0.10 | 0.32 | 0.39 | 0.09 | -0.16 | -0.44 | 0.01 |
| 7, 2, 10 | -0.3. | -0.04 | -0.14 | - 0.38 | -0 | . 53 | -0.64 | -0.12 | -0.32 | -0.17 | -0.18 | -0.38 | -0.32 |
| 7, 2, 11 | -0.21 | $-0.03$ | 0.19 | - 0.07 | -0.18 | -0.20 | -0.49 | 0.14 | 0.04 | 0.28 | 0.09 | -0.25 | -0.07 |
| $\left.\begin{array}{\|c}7,8,2,24 \\ 10,12\end{array}\right\}$ | -0.09 | 0.02 | 13 | 0.00 | -0.12 | -0.13 | -0.08 | 0.20 | 0.1 | . 07 | 3 | 0.17 | 0.03 |
| $7,2,2,(9)$ | -0.01 | -0.18 | 0.01 | $-0.23$ | -0.30 | -0.22 | 0.10 | -0.05 | -0.12 | -0.02 | -0.02 | -0.24 | -0.11 |
| Mean. | 22.94 | 28.57 | 34.81 | 43.54 | 56.92 | 61.60 | 71.61 | 67.44 | 59.80 | 50.46 | 34.80 | 29.28 | 47.23 |

The numbers without sign must be added. those with the sign - must be subtracted.
The above Table has heen derived from one year of hourly observations made at Amberst College, Massachusetts, in 1839, under the direction of Professor Snell, and communicated by Professor Chester Dewey. It gives the simple differences of the monthly means of each hour from the monthly means of the twenty-four hours which are found in the last line.

# II OURLY C0RRECTIONS 

FOR

PERIODIC VARIATIONS.

A SIA.

India. - Trevandrum. Lat. $8^{\circ} 31^{\prime}$ N. Long. $74^{\circ} 50^{\prime}$ E. Greenu.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Fahrenheit.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 4.41 | 4.03 | 3.50 | 3.85 | 3.26 | 2.66 | 2.41 | 2.88 | 2.99 | 3.06 | 3.33 | 4.25 | 3.42 |
| 2 | 5.13 | 4.95 | 4.64 | 4.46 | 3.80 | 3.02 | 2.75 | 3.24 | 3.44 | 3.44 | 3.83 | 4.86 | 3.96 |
| 3 | 6.03 | 6.12 | 5.67 | 5.15 | 4.39 | 3.47 | 3.17 | 3.74 | 3.98 | 3.92 | 4.46 | 5.67 | 4.66 |
| 4 | 6.95 | 7.31 | 6.64 | 5.74 | 4.82 | 3.80 | 3.58 | 4.21 | 4.48 | 4.34 | 5.04 | 6.50 | 5.29 |
| 5 | 7.56 | 8.15 | 7.13 | 5.81 | 4.52 | 3.53 | 3.76 | 4.41 | 4.61 | 4.46 | 5.22 | 6.93 | 5.56 |
| 6 | 7.34 | 8.01 | 6.73 | 5.11 | 4.14 | 3.35 | 3.49 | 4.07 | 4.14 | 4.01 | 4.73 | 6.57 | 5.15 |
| 7 | 6.01 | 6.59 | 5.20 | 3.53 | 2.81 | 2.34 | 2.68 | 3.06 | 3.02 | 2.85 | 3.40 | 5.11 | 3.59 |
| 8 | 3.56 | 3.92 I | 2.66 | 1.22 | 0.95 | 0.90 | 1.3 .5 | 1.49 | 1.26 | 1.13 | 1.40 | 2.70 | 1.87 |
| 9 | 0.41 | 0.50 | $-0.47$ | $-1.42$ | -1.13 | $-0.74$ | $-0.27$ | $-0.45$ | -0.81 | $-0.99$ | -0.92 | -0.29 | $-0.54$ |
| 10 | $-2.84$ | -2.97 | -3.53 | -3.89 | $-3.04$ | $-2.30$ | -1.91 | $-2.41$ | $-2.86$ | $-3.06$ | -3.11 | -3 24 | -2.93 |
| 11 | $-5.51$ | $-5.85$ | $-5.94$ | -5.76 | $-4.48$ | $-3.53$ | -3.33 | $-4.05$ | $-4.50$ | $-4.73$ | $-4.75$ | $-5.58$ | $-4.84$ |
| N | -7.25 | $-7.58$ | $-7.36$ | -6.82 | $-5.33$ | $-4.34$ | $-4.32$ | $-5.18$ | -5.54 | $-5.72$ | $-5.67$ | $-7.00$ | $-6.01$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | $-7.92$ | -8.17 | $-7.72$ | -7.04 | $-5.60$ | $-4.68$ | $-4.79$ | -5.69 | -5.87 | $-5.94$ | -5.90 | $-7.49$ | -6.41 |
| 2 | $-7.76$ | $-7.83$ | $-7.22$ | -6.59 | -5.38 | $-4.61$ | $-4.77$ | -5.60 | -5.60 | $-5.54$ | -5.60 | $-7.25$ | $-6.14$ |
| 3 | $-7.09$ | -6.98 | $-6.26$ | -5.65 | $-4.79$ | $-4.19$ | $-4.30$ | -5.04 | $-4.86$ | $-4.66$ | $-4.95$ | $-6.57$ | $-5.45$ |
| 4 | $-6.17$ | $-5.99$ | $-5.06$ | $-4.46$ | $-3.94$ | $-3.47$ | $-3.51$ | $-4.10$ | -3.80 | $-3.53$ | $-4.12$ | $-5.67$ | $-4.48$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | $-5.16$ | -4.88 | -3.83 | -3.11 | -2.88 | -2.52 | $-2.52$ | -2.90 | $-2.59$ | $-2.32$ | -315 | -4.61 | -8.38 |
| 6 | -3.92 | 3.74 | $-2.57$ | -1.71 | -1.69 | $-1.42$ | $-1.40$ | $-1.58$ | -1.31 | $-1.10$ | - 2.03 | -3.35 | $-2.16$ |
| 7 | -2.5 | $-2.45$ | $-1.31$ | $-0.34$ | $-0.50$ | $-0.32$ | $-0.29$ | $-0.27$ | $-0.11$ | 0.00 | -0.81 | -1.89 | $-0.90$ |
| 8 | $-0.92$ | -1.04 | $-0.07$ | 0.92 | 0.63 | 0.70 | 0.68 | 0.90 | 0.92 | 0.97 | 0.38 | $-0.32$ | 0.32 |
| 9 | 0.68 | 0.38 | 1.06 | 1.91 | 1.53 | 1.46 | 1.40 | 1.76 | 1.69 | 1.71 | 1.42 | 1.19 | 1.35 |
| 10 | 2.0 | 1.6 | 1.96 | 2.61 | 2.16 | 1.96 | 1.85 | 2.30 | 2.18 | 2.25 | 2.21 | 2.43 | 2.14 |
| 11 | 3 | 2 | 2.6 | 3.0 | 2. | 2.23 | 2.09 | 2.51 | 2.48 | 2.57 | 2.68 | 3.26 | 2.66 |
| Midn. | 3.83 | 3.31 | 3.17 | 3.42 | 2.88 | 2.41 | 2.23 | 2.68 | 2.70 | 2.81 | 2.99 | 3.80 | 3.02 |
| 6. 6 | 1.71 | 2.14 | 2.09 | 1.71 | 1.24 | 0.97 | 1.04 | 1.24 | 1.42 | 1.46 | 1.35 | 1.60 | 1.51 |
| 7. 7 | 1.76 | 2.07 | 1.96 | 1.60 | 1.17 | 1.01 | 1.19 | 1.40 | 1.44 | 1.44 | 1.28 | 1.62 | 1.49 |
| 8. 8 | 1.33 | 1.44 | 1.31 | 1.06 | 0.79 | 0.79 | 1.01 | 1.19 | 1.08 | 1.06 | 0.88 | 1.19 | 1.10 |
| 9. 9 | 0.54 | 0.43 | 0.29 | 0.2 .5 | 0.20 | 0.36 | 0.56 | 0.65 | 0.43 | 0.36 | 0.25 | 0.45 | 0.41 |
| 10.10 | $-0.41$ | $-0.65$ | $-0.79$ | $-0.63$ | $-0.45$ | $-0.18$ | $-0.02$ | $-0.07$ | $-0.34$ | $-0.41$ | $-0.45$ | $-0.40$ | -0.41 |
| 7. 2. 9 | -0..36 | $-0.29$ | $-0.32$ | -0.38 | - -0.34 | -0.27 | $-0.23$ | $-0.27$ | -0.29 | -0.32 | $-0.27$ | $-0.32$ | $-0.32$ |
| 6. 2. 8 | -0.45 | $-0.29$ | $-0.18$ | $-0.18$ | $-0.20$ | $-0.18$ | $-0.20$ | $-0.20$ | -0.18 | $-0.18$ | -0.16 | -0.34 | $-0.23$ |
| 6. 2.10 | 0.51 | 0.61 | 0.50 | 0.38 | 0.32 | 0.23 | 0.18 | 0.25 | 0.25 | 0.25 | 0.45 | 0.59 | 0.38 |
| 6. 2. 6 | -1.44 | $-1.19$ | $-1.01$ | $-1.06$ | $-0.97$ | $-0.90$ | $-0.90$ | $-1.04$ | $-0.92$ | $-0.88$ | $-0.97$ | $-1.35$ | -1.06 |
| 7. 2 | -0.88 | $-0.63$ | -1.01 | $-1.53$ | -1.28 | -1.15 | -1.06 | $-1.28$ | -1.31 | -1.33 | $-1.10$ | -1.08 | $-1.13$ |
| 8. 2 | -0.88 | -0.63 | -1.01 | $-1.53$ | $\left\lvert\, \begin{aligned} & -1.28 \\ & -2.23\end{aligned}\right.$ | -1.15 -1.57 | -1.06 -1.71 | $-2.07$ | $-1.31$ | $-2.21$ | $-2.12$ | -2.27 | -2.14 |
| 8. 1 |  |  | $-2.54$ |  | -2.23 | -1.87 | -1.71 -1.73 | $-2.12$ | -2.32 | $-2.41$ | $-2.25$ | -2.41 | $-2.27$ |
| 7. 1 | -0.18 |  | -2..94 | $-1.76$ | $\left\lvert\, \begin{aligned} & -2.34 \\ & -1.40\end{aligned}\right.$ | -1.89 | $\left(\begin{array}{l}-1.78 \\ -1.06\end{array}\right.$ | -2.12 -1.33 | -1.4.4 | $-1.53$ | $-1.26$ | -1.19 | -1.26 |
| 7. 1 | $-0.9$ | -0.79 | -1.26 | -1.86 | -1.40 | -1.17 | -1.06 | -1.33 | -1.44 | 1.53 |  |  |  |
| 9.12 .3 .9 | -3.31 | $-3.42$ | -3.26 | $-2.99$ | $-2.43$ | $-1.96$ | -1.87 | -2.23 | $-2.39$ | -2.41 | $-2.54$ | -3.17 | $-2.66$ |
| 7. $2.2(9)$ | $-0.11$ | $-0.11$ | 0.02 | 0.20 | 0.14 | 0.16 | 0.18 | 0.25 | 0.20 | 0.20 | 0.16 | 0.07 | 0.11 |

The numbers without sign must be added ; those with the sign - must be subtracted.
XIX.

India. - Trevandrum. Lat. $8^{\circ} 31^{\prime}$ N. Long. $74^{\circ} 50^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | Narch. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 1.96 | 1.79 | 1.69 | 1.7 | 1.45 | 1.18 | 1.07 | 1.28 | 1.33 | 1.36 | 1.4 | 1.8 | 1.52 |
| 2 | 2.28 | 2.20 | 2.06 | 1.95 | 1.69 | 1.34 | 1.22 | 1.44 | 1.53 | 1.53 | 1.70 | 2.16 | 1.76 |
| 3 | 2.68 | 2.72 | 2.52 | 2.29 | 1.95 | 1.54 | 1.41 | 1.66 | 1.77 | 1.74 | 1.98 | 2.52 | 2.07 |
| 4 | 3.09 | 3.25 | 2.95 | 2.55 | 2.14 | 1.69 | 1.59 | 1.87 | 1.90 | 1.93 | 2.2 | 2.89 | 2.35 |
| 5 | 3.36 | 3.62 | 3.17 | 2.58 | 2.1 | 1.70 | 1.67 | 1.96 | 2.05 | 1.98 | 2.32 | 3.08 | 2.47 |
| 6 | 3.26 | 3.56 | 2.99 | 2.27 | 1.85 | 1.49 | 1.55 | 1.51 | 1.84 | 1.75 | 2.1 | 2. | 2.29 |
| 7 | 2.67 | 2.93 | 2.31 | 1.57 | 1.2 .5 | 1.04 | 1.19 | 1.36 | 1.34 | 1.28 | 1.5 | 2. | 1.73 |
| 8 | 1.58 | 1.74 | 1.18 | 05 | 0.42 | 0.40 | 0.60 | 0.66 | 0.56 | 0.50 | 0.62 | 1. | 0.83 |
| 9 | 0.18 | 0.22 | -0.21 | -0.63 | -0.50 | -0.33 | -0.12 | -0.20 | -0.36 | -0.44 | -0.41 | -0 | -0.24 |
| 10 | -1.26 | $-1.32$ | -1.57 | -1.73 | -1.35 | -1.02 | -0.85 | -1.07 | -1.27 | -1.36 | -1.38 | -1.4 | -1.30 |
| 11 | $-2.45$ | -2.60 | -2.6. | -2.96 | -1.99 | -1.57 | -1.45 | -1.80 | -2.00 | -2.1 | -2.11 | -2.4 | -2.15 |
| Noon. | -3.22 | -3.37 | -3.27 | -3.03 | -2.37 | -1.93 | -1.92 | -2.30 | $-246$ | -2.54 | -2.52 | -3.1 | $-2.67$ |
| 1 | -3.52 | -3.63 | -3.43 | -3.13 | -2.49 | -2 08 | -2.13 | -2.53 | -2.61 | -2.6 | -2.62 | -3.3 | -2.85 |
| 2 | -3.45 | -3.48 | -3.21 | -2.93 | -2.39 | - - 0.05 | -2.12 | -2.49 | -2.49 | -2.46 | -2.49 | -3.22 | -2.73 |
| 3 | -3.15 | -3.10 | -2.75 | -2.31 | -2.13 | -1.86 | -1.91 | -2.24 | -2.16 | -2.07 | -2.20 | -2.92 | $-2.42$ |
| 4 | -2.74 | 2.66 | -2.25 | -1.98 | -1.7 | 1.54 | -156 | -1.82 | -1.69 | -1.57 | -1.83 | -2.52 | -1.99 |
| 5 | -2.28 | -2.17 | -1.70 | -1 | -1 | -1.12 | -1.12 | -1.29 | -1.15 | -1.03 | -1.40 | -2.05 | -1.50 |
| 6 | -1.74 | -1.66 | -1.14 | -0.76 | -0.75 | -0.4.3 | -0.62 | -0.70 | -0.58 | -0.49 | -0.90 | -1.49 | -0.96 |
| 7 | -1.11 | -1.09 | -0.58 | -0.15 | -0.22 | -0.14 | -0.13 | -0.12 | -0.05 | 0.00 | -0.36 | -0.84 | -0.40 |
| 8 | -0.41 | -0.46 | $-0.03$ | 0.41 | 028 | $0 . .1$ | 0.30 | 0.40 | 0.41 | 0.43 | 0.17 | -0.14 | 0.14 |
| 9 | 0.30 | 0.17 | 0.47 | 0.85 | 0.68 | 0.65 | 0.62 | 0.78 | 0.75 | 0.76 | 0.63 | 0.53 | 0.60 |
| 10 | 0.91 | 073 | 0.87 | 1.16 | 0.96 | 0.87 | 0.82 | 1.02 | 0.97 | 1.00 | 0.98 | 1.08 | 0.95 |
| 11 | 1.37 | 1.14 | 1.17 | 1.36 | 1.14 | 0.99 | 0.93 | 1.13 | 1.10 | 1.14 | 1.19 | 1.45 | 1.18 |
| Midn. | 1.70 | 1.47 | 1.41 | 1.52 | 1.28 | 1.07. | 0.99 | 1.19 | 120 | 1.25 | 1.33 | 1.69 | 1.34 |
| 6. 6 | 0.76 | 0.95 | 0.93 | 0.76 | 0.55 | 0.43 | 0.46 | 0.55 | 0.63 | 0.65 | 0.60 | 0.71 | 0.67 |
| 7. 7 | 0.78 | 092 | 0.87 | 0.71 | 0.52 | 0.45 | 0.53 | 0.62 | 064 | 0.64 | 0.57 | 0.72 | 0.66 |
| 8. 8 | 0.59 | 064 | 0.58 | 0.47 | 0.35 | 0.35 | 0.45 | 0.53 | 048 | 0.47 | 0.39 | 0.53 | 0.49 |
| 9. 9 | 0.24 | 0.19 | 0.13 | 0.11 | 0.09 | 0.16 | 0.25 | 0.29 | 6.19 | 0.16 | 0.11 | 0.20 | 0.18 |
| 10.10 | -0.18 | -0.29 | -0.35 | -0.28 | -0.20 | -0.08 | -0.01 | -0.03 | -0.15 | -0.18 | -0.20 | -0.18 | -0.18 |
| 7. 2. 9 | -0.16 | -0.13 | -0.14 | -0.17 | -0.15 | -0.12 | -0.10 | -0.12 | -0.13 | -0.14 | -0.12 | -0.14 | -0.14 |
| 6. 2. 8 | -0.20 | -0.13 | -0.08 | -0.08 | -0.09 | -0.08 | -0.09 | -0.09 | -0.08 | -0.08 | -0.0 | -0.15 | -0.10 |
| 6. 2.10 | 0.4 | 0.27 | 0.22 | 0.17 | 0.14 | 0.10 | 0.05 | 0.11 | 0.11 | 0.11 | 0.20 | 0.26 | 0.17 |
| 6. 2. 6 | -0.64 | -0.53 | -0.45 | -0.47 | -0.43 | -0.40 | -0.40 | -0.46 | -0.41 | -0.39 | -0.43 | -0.60 | -0.47 |
| 7. 2 | -0.39 | -0.28 | -0.45 | -0.68 | -0.57 | -0.51 | -0.47 | -0.57 | -0.58 | -0.59 | -0.49 | -0.48 | -0.50 |
| 8. 2 | -0.9.4 | -0.57 | $-1.02$ | $-1.20$ | -0.99 | -0.83 | -0.76 | -0.92 | -0.97 | -0.98 | -0.94 | -1.01 | -0.95 |
| 8. 1 | -0.97 | -0.95 | -1 13 | $-1.30$ | -1.04 | -0.84 | -0.77 | -0.94 | -1 03 | -1.07 | -1.00 | . 0 | -1.01 |
| 7. 1 | -0.43 | -0.85 | -0.56 | $-0.78$ | -0.62 | -0.52 | -0.47 | -0.59 | -0.64 | -0.68 | -0.56 | -0.53 | -0.56 |
| 9.12.3.9 | -1.47 | -1.52 | -1.45 | -1.33 | -1.08 | -0.87 | -0.83 | -0.99 | -1.06 | -1.07 | -1.1 | -1.41 | -1.18 |
| 7. $2.2(9)$ | -0.05 | -0.05 | 0.01 | 0.09 | 0.06 | 0.07 | 0.08 | 0.11 | 0.09 | 0.09 | 0.07 | 0.03 | 0.05 |
| Dail.ext. | -0.08 | -0.01 | -0.13 | -0.28 | -0.18 | -0.19 | -0.23 | -0.29 | -0.28 | -0.33 | -0.15 | -0.13 | -0.19 |

India. - Madras. Lat. $13^{\circ} 4^{\prime}$ N. Long. $80^{\circ} 19^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Fabrenheit.


The uumbers without sign must be added; those with the sigu - must be subtracted.

India. - Madras. Lat. $13^{\circ} 4^{\prime}$ N. Long. $80^{\circ} 19^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 1.41 | 1.22 | 1.32 | 1.06 | 1.26 | 1.15 | 0.93 | 0.83 | 1.26 | 1.18 | 1.0 | 1.38 | 1.17 |
| 2 | 1.79 | 1.64 | 1.42 | 1.36 | 1.59 | 1.42 | 1.09 | 1.40 | 1.52 | 1.46 | 1.32 | 1.50 | 1.46 |
| 3 | 2.14 | 2.10 | 1.50 | 1.76 | 1.94 | 1.70 | 1.26 | 1.66 | 1.67 | 1.70 | 1.70 | 1.68 | 1.73 |
| 4 | 2.38 | 2.42 | 1.53 | 2.10 | 2.17 | 1.90 | 1.42 | 1.66 | 1.70 | 1.58 | 1.90 | 1.93 | 1.92 |
| 5 | 2.42 | 2.43 | 1.61 | 2.20 | 2.18 | 1.95 | 1.42 | 1.45 | 1.62 | 1.88 | 2.02 | 2.17 | 1.95 |
| 6 | 2.22 | 2.05 | 1.48 | 1.91 | 1.86 | 1.77 | 1.33 | 1.10 | 1.39 | 1.64 | 1.81 | 2.25 | 1.73 |
| 7 | 1.76 | 1.30 | 1.14 | 1.24 | 1.19 | 1.30 | 1.12 | 0.75 | 1.02 | 1.14 | 1.27 | 2.00 | 1.27 |
| 8 | 1.05 | 0.36 | 0.54 | 0.30 | 0.27 | 0.70 | 0.78 | 0.46 | 0.47 | 0.10 | 0.50 | 1.32 | 0.60 |
| 9 | 0.15 | -0.39 | -0.23 | -0.71 | -0.75 | -0.06 | 0.35 | 0.16 | -0.23 | -0.46 | -0.3 | 0.27 | -0.20 |
| 10 | -0.8. | -1.38 | -1.04 | $-1.56$ | -1.67 | -0.82 | -0.21 | -0.18 | -1.02 | -1.26 | -1.10 | -0.94 | $-1.00$ |
| 11 | -1.74 | -1.94 | $-1.70$ | -2.12 | $-2.31$ | -1.46 | -0.86 | -0.62 | -1.75 | -1.83 | -1.75 | $-2.20$ | -1.69 |
| Noon. | -2.18 | $-2.23$ | -2.06 | -2.36 | -2.58 | -1.94 | -1.52 | -1.12 | $-2.29$ | -2.18 | $-2.12$ | -2.76 | -2.14 |
| 1 | -2.90 | -2.34 | -2.10 | -2.34 | -2.48 | -2.20 | -2.13 | -1.57 | -2.47 | -2.17 | -2.25 | -2.98 | -2.33 |
| 2 | -2.97 | -2.30 | -1.88 | -2.14 | -2.13 | -2.24 | -2.47 | -1.52 | -2.27 | -1.91 | -2.18 | -2.76 | -2.26 |
| 3 | -2.68 | -2.12 | $-1.52$ | -1.84 | -1.62 | -2.07 | -2.48 | -1.77 | -1.77 | -1.50 | -1.9 | -2.25 | -1.97 |
| 4 | -2.14 | -1.81 | -1.14 | -1.46 | -1.11 | $-1.74$ | -2.12 | -1.43 | -1.12 | -1.08 | -1.61 | -1.65 | -1.53 |
| 5 | -1.47 | -1.34 | $-0.83$ | -1.00 | -0.65 | -1.28 | -1.44 | -0.94 | -0.50 | -0.70 | $-1.10$ | $-1.13$ | -1.03 |
| 6 | -0.81 | -0.78 | $-0.58$ | -0.48 | -0.27 | -0.78 | -0.65 | -0.46 | -0.06 | $-0.38$ | -0.58 | -0.72 | -0.55 |
| 7 | -0.26 | -0.18 | -0.35 | 0.04 | 0.02 | -0.30 | 0.08 | -0.14 | 0.18 | -0.14 | -0.14 | -0.39 | -0.13 |
| 8 | 0.13 | 0.30 | -0.05 | 0.49 | 0.26 | 0.12 | 0.62 | -0.04 | 0.27 | 0.06 | 0.36 | -0.06 | 0.20 |
| 9 | 0.38 | 0.62 | 0.42 | 0.71 | 0.45 | 0.42 | 0.86 | -0.06 | 0.33 | 0.26 | 0.64 | 0.30 | 0.44 |
| 10 | 0.58 | 0.77 | 0.60 | 0.90 | 0.61 | 0.63 | 0.91 | -0.06 | 0.44 | 0.46 | 0.81 | 0.66 | 0.61 |
| 11 | 0.79 | 0.84 | 0.91 | 0.91 | 0.78 | 0.79 | 0.87 | 0.11 | 0.66 | 0.67 | 0.83 | 0.99 | 0.76 |
| Midn. | 1.06 | 0.96 | 1.16 | 0.92 | 0.98 | 0.94 | 0.84 | 0.47 | 0.95 | 0.91 | 0.59 | 1.22 | 0.94 |
| 6. 6 | 0.71 | 0.64 | 0.45 | 0.72 | 0.80 | 0.50 | 0.34 | 0.32 | 0.67 | 0.63 | 0.62 | 0.77 | 0.60 |
| 7. 7 | 0.75 | 0.56 | 0.40 | 0.64 | 0.61 | 0.50 | 0.60 | 0.31 | 0.60 | 0.50 | 0.57 | 0.81 | 0.57 |
| 8. 8 | 0.59 | 0.33 | 0.23 | 0.40 | 0.27 | 0.41 | 0.70 | 0.21 | 0.37 | 0.23 | 0.43 | 0.63 | 040 |
| 9. 9 | 0.27 | 0.02 | 0.10 | -0.00 | -0.15 | 0.18 | 0.61 | 0.05 | 0.05 | -0.10 | 0.15 | 0.29 | 0.12 |
| 10.10 | -0.12 | -0.31 | $-0.22$ | -0.33 | -0.53 | $-0.10$ | -0.35 | -0.12 | -0.29 | -0.40 | -0.15 | -0.14 | -0.20 |
| 7. 2. 9 | -0.28 | -0.13 | -0.11 | -0.06 | -0.16 | -0.17 | -0.16 | -0.38 | -0.31 | -0.17 | 0.09 | -0.15 | -0.18 |
| 6. 2.8 | -0.2 1 | 0.02 | -0.16 | 0.09 | -0.00 | 12 | -0.17 | -0.25 | -0.20 | -0.07 | 0.01 | -0.19 | -0.11 |
| 6. 2.10 | -0.06 | 0.17 | 0.07 | 0.22 | 0.11 | 0.05 | -0.08 | -0.26 | -0.15 | 0.06 | 0.15 | 0.0 .5 | 003 |
| 6. 2. 6 | $-0.52$ | -0.34 | -0.33 | -0.24 | -0.18 | -0.42 | -0.60 | -0.39 | -0.31 | -0.22 | -0.32 | -0.41 | -0.36 |
| 7. 2 | -0.61 | -0.50 | -0.37 | -0.45 | -0.47 | -0.47 | -0 6s | -0.54 | -0.63 | -0.32 | -0. 46 | 0.35 | -0.50 |
| 8. 2 | -0.96 | -0.97 | -0.67 | -0.92 | -0.93 | -0.77 | -0.55 | -0.68 | $-0.90$ | -0.76 | -0.8 | -0.72 | -0.83 |
| 8. | -0.93 | -0.99 | -0.78 | -1.02 | -1.11 | -0.75 | -0.68 | -0.56 | -1.00 | -0.89 | -0.8 | -0.8 | -0.87 |
| 7. 1 | -0.57 | -0.52 | -0.48 | -0.55 | -0.65 | -0.45 | -0.51 | -0.41 | $-0.73$ | -0.52 | -0.49 | -0.49 | -0 53 |
| 9.12.3.9 | -1.16 | -1.08 | -0.8.5 | -1.05 | -1.13 | -0.01 | -0.7) | -0.70 | -0.99 | -0.97 | -0.95 | -1.11 | -0.97 |
| 7. 2.2(9) | -0.11 | 0.06 | 0.03 | 0.13 | -0.01 | -0.03 | 009 | -0.30 | -0.15 | -0.06 | 0.09 | -0.04 | -0.03 |
| Dallext. | -0.2S | 0.05 | -0.25 | -0.08 | -0.20 | -0.15 | -0.53 | -0.08 | -0.39 | -0.15 | -0.12 | -0.37 | -0.19 |

India. - Bombay. Lat. $18^{\circ} 56^{\prime}$ N. Long. $72^{\circ} 54^{\prime}$ E. Greenv.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Fahrenheit.

| Hours. | Jan. | Feb. | March. | April. | Hay. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 1.49 | 1.40 | 0.99 | 1.13 | 1.42 | 1.15 | 0.79 | 0.97 | 0.56 | 1.49 | 2.03 | 1.55 | 1.26 |
| 2 | 1.80 | 1.69 | 1.33 | 1.51 | 178. | 1.40 | 0.88 | 1.13 | 0.97 | 1.57 | 2.18 | 1.87 | 1.53 |
| 3 | 2.27 | 2.21 | 1.91 | 2.05 | 2.14 | 1.69 | 0.90 | 1.24 | 1.24 | 2.32 | 2.45 | 2.41 | 1.91 |
| 4 | 2.86 | 2.84 | 2.59 | 2.48 | 2.32 | 1.91 | 0.90 | 1.31 | 1.53 | 2.75 | 2.81 | 3.11 | 2.27 |
| 5 | 3.47 | 3.40 | 3.04 | 2.61 | 2.23 | 1.96 | 0.86 | 1.31 | 1.71 | 2.95 | 3.11 | 3.78 | 2.54 |
| 4 | 3.83 | 3.62 | 3.06 | 2.34 | 1.80 | 1.50 | 0.79 | 1.24 | 1.67 | 2.79 | 3.15 | 4.16 | 2.52 |
| 7 | 3.69 | 3.33 | 2.54 | 1.67 | 1.15 | 1.42 | 0.65 | 1.04 | 1.22 | 2.21 | 2.79 | 4.01 | 2.14 |
| 8 | 2.97 | 2.48 | 1.58 | 0.77 | 036 | 0.88 | 0.38 | 0.74 | 0.79 | 1.28 | 1.91 | 3.24 | 1.44 |
| 9 | 1.69 | 1.22 | 0.38 | -0.14 | $-0.41$ | 0.23 | 0.00 | 0.32 | 0.09 | 0.16 | 0.63 | 1.87 | 0.50 |
| 10 | 0.07 | -0.23 | $-0.77$ | -0.90 | $-1.06$ | $-0.43$ | $-0.52$ | -0.20 | $-0.65$ | $-0.95$ | -0.83 | 0.16 | $-0.52$ |
| 11 | -1.55 | -1.55 | -1.67 | -1.49 | $-1.55$ | $-6.08$ | $-6.08$ | $-0.79$ | $-1.28$ | $-1.91$ | $-2.21$ | $-1.60$ | $-1.49$ |
| N | -2.86 | $-2.61$ | $-2.30$ | -1.91 | $-1.94$ | $-1.64$ | $-1.55$ | $-1.35$ | $-1.80$ | $-2.59$ | $-3.29$ | -3.08 | $-2.25$ |
| 1 | -3.69 | $-3.29$ | -2.66 | $-2.25$ | $-2.21$ | $-2.12$ | $-1.82$ | $-1.78$ | $-2.12$ | -2.99 | $-3.92$ | 4.10 | 2.75 |
| 2 | -3.98 | $-3.60$ | -2.84 | $-2.50$ | $-2.34$ | $-2.41$ | -1.78 | $-2.00$ | $-2.25$ | $-3.13$ | $-4.07$ | $-4.59$ | $-2.95$ |
| 3 | -3.85 | -3.65 | -2.86 | -2 | $-2.32$ | $-2.45$ | -1.44 | -1.98 | $-2.16$ | $-2.99$ | $-3.55$ | $-4.55$ | $-2.90$ |
| 4 | $-3.42$ | -3.42 | $-2.72$ | $-2.50$ | $-2.09$ | $-2.25$ | $-0.92$ | -1.69 | $-1.87$ | -2.66 | -3.33 | $-4.12$ | $-2.59$ |
| 5 | 4 |  | $-2.34$ |  |  |  |  | -1.24 |  | -2.14 | -2.61 | -3.38 | $-2.07$ |
| 5 |  |  |  |  |  |  |  |  |  |  | 8 |  |  |
| 6 |  |  |  | - |  |  |  |  |  |  |  | -2.45 | $-1.40$ |
| 7 | -1.49 | -1.44 | -0.88 | $-0.54$ | $-0.35$ | $-0.47$ | 0.38 | $-0.23$ | 0.05 | $-0.72$ | -0.88 | -1.46 | $-0.68$ |
| 8 | -0.79 | $-0.56$ | $-0.07$ | 0.23 | 0.18 | 0.14 | 0.50 | 0.16 | 0.47 | $-0.02$ | 0.00 | $-0.52$ | -0.02 |
| 9 | -0.1 | 0.23 | 0.56 | 0.72 | 059 | 0.54 | 0.54 | 1.43 | 0.86 | 0.52 | 0.77 | 0.29 | 0.50 |
| 10 | 0.47 | 0.81 | 0.90 | 0.92 | 0.53 | 0.79 | 0.54 | 0.59 | 0.99 | 0.88 | 1.35 | 0.86 | 0.83 |
| 11 | 0.92 | 1.10 | 0.97 | 0.92 | 0.99 | 096 | 0.61 | 0.72 | 0.97 | 1.08 | 1.71 | 1.19 | 1.01 |
| Midn. | 1.24 | 1.26 | 0.92 | 0.95 | 1.15 | 0.99 | 0.70 | 0.83 | 0.88 | 1.26 | 1.91 | 1.37 | 1.13 |
| 6. 6 | 0.81 | 0.68 | 0.68 | 0.50 | 0.38 | 0.34 | 0.43 | 0.25 | 0.45 | 0.68 | 0.70 | 0.86 | 0.56 |
| 7. 7 | 1.10 | 0.95 | 0.83 | 0.56 | 0.38 | 0.47 | 0.52 | 0.41 | 0.63 | 0.74 | 0.95 | 1.28 | 0.74 |
| 8. 8 | 1.08 | 0.97 | 0.77 | 0.50 | 0.27 | 0.50 | 0.45 | 0.45 | 0.63 | 0.63 | 0.95 | 1.35 | 0.72 |
| 9. 9 | 0.79 | 0.72 | 0.47 | 0.29 | 0.09 | 0.38 | 0.27 | 0.36 | 0.47 | 0.34 | 0.70 | 1.08 | 0.50 |
| 10.10 | 0.27 | 0.29 | 0.07 | 0.00 | -0.11 | 0.18 | 0.02 | 0.20 | 0.18 | $-0.05$ | 0.25 | 0.52 | 0.16 |
| 7. 2. 9 | -0.14 | $-0.02$ | 0.09 | $-0.0 .5$ | $-0.20$ | $-0.16$ | $-0.20$ | -0.18 | $-0.07$ | $-0.14$ | $-0.18$ | $-0.09$ | -0.11 |
| 6. 2. 8 | $-0.3$ | $-0.15$ | 0.03 | 0.02 | $-0.11$ | $-0.16$ | $-0.16$ | -0.20 | $-0.05$ | $-0.11$ | $-0.32$ | $-0.32$ | $-0.16$ |
| 6. 2.10 | 0.11 | 0.27 | 033 | 02.5 | 0.09 | 0.07 | $-0.16$ | $-0.07$ | 0.14 | 0.18 | 0.14 | 0.14 | 0.14 |
| 6. 2. 6 | $-0.79$ | -0.74 | $-0.50$ | $-0.52$ | $-0.52$ | $-0.59$ | $-0.29$ | $-0.50$ | $-0.45$ | -0.61 | $-0.90$ | $-0.97$ | -0.61 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | -0.16 | $-0.14$ | -0.16 | -0.43 | -0.61 | $-0.50$ | $-0.56$ | -0.50 | $-0.52$ | -0.47 | -0.65 | -0.29 | -0.41 |
| 8. 2 | $-0.52$ | $-0.56$ | -0.63 | $-0.88$ | -0.99 | $-0.7 \%$ | $-0.70$ | -0.63 | $-0.74$ | $-0.92$ | -1.08 | $-0.68$ | $-0.77$ |
| S. 1 | -0.36 | $-0.41$ | $-0.54$ | -0.79 | $-0.92$ | $-0.63$ | $-0.72$ | $-0.52$ | $-0.68$ | -0.86 | $-1.01$ | $-0.43$ | $-0.65$ |
| 7. 1 | 0.00 | 002 | $-0.07$ | $-029$ | $-0.54$ | $-0.36$ | $-0.59$ | $-0.38$ | $-0.45$ | $-0.41$ | $-0.56$ | $-0.05$ | $-0.32$ |
| 9.12.3.9 | -1.2s | -1.22 | -1.06 | $-0.99$ | -1.01 | $-0.83$ | -0.61 | $-0.65$ | $-0.77$ | $-1.24$ | $-1.44$ | -1.37 | $-1.04$ |
| 7. $2.2(9)$ | $-0.11$ | 0.05 | 0.20 | 0.16 | 0.00 | 0.02 | -0.02 | $-0.02$ | 0.18 | 0.02 | 0.07 | 0.00 | 0.05 |

India. - Bombay. Lat. $18^{\circ} 56^{\prime}$ N. Long. $72^{\circ} 54^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.66 | 0.62 | 0.44 | 0.50 | 0.63 | 0.51 | 0.35 | 0.43 | 038 | 0.66 | 0.90 | 0.69 | 0.56 |
| 2 | 0.80 | 0.75 | 0.59 | 0.67 | 0.79 | 0.62 | 0.39 | 0.50 | 0.43 | 0.83 | 0.97 | 0.83 | 0.68 |
| 3 | 1.01 | 0.98 | 0.85 | 0.91 | 0.95 | 0.75 | 0.40 | 0.55 | 0.55 | 103 | 1.09 | 1.07 | 0.85 |
| 4 | 1.27 | 1.26 | 1.15 | 1.10 | 1.03 | 0.85 | 0.40 | 0.58 | 0.68 | 1.22 | 1.25 | 1.38 | 1.01 |
| 5 | 1.54 | 1.51 | 1.35 | 1.16 | 0.99 | 0.87 | 0.38 | 0.58 | 0.76 | 1.31 | 1.38 | 1.68 | 1.13 |
| 6 | 70 | 1.61 | 1.36 | 1.04 | 0.80 | 0.80 | 0.35 | 0.55 | 0.74 | 1.24 | 1.40 | 1.85 | 1.12 |
| 7 | 1.64 | 1.48 | 1.13 | 0.74 | 0.51 | 0.63 | 0.29 | 0.46 | 0.54 | 0.98 | 1.24 | 1.78 | 0.95 |
| 8 | 1.32 | 1.10 | 0.70 | 0.34 | 0.16 | 0.39 | 0.17 | 0.33 | 0.35 | 0.57 | 0.85 | 1.44 | 0.64 |
| 9 | 75 | 0.54 | 0.17 | -0.06 | -0.18 | 0.10 | -0. | 0.1 | 0.04 | 0.07 | 0.28 | 0. | 0.22 |
| 10 | 0.03 | -0.10 | -0.34 | -0.40 | -0.47 | -0.19 | -0.23 | -0.09 | -0.29 | -0.42 | -0.37 | 0.07 | -0.23 |
| 11 | -0.69 | -0.69 | -0.74 | -0.66 | -0.69 | -0.48 | -0.48 | -0.35 | -0.57 | -0.85 | -0.98 | -0.7 | -0 66 |
| Noon | -1.27 | -1.16 | -1.02 | -0.85 | -0.86 | -0.73 | -0.69 | -0.60 | -0.80 | -1.15 | -1.46 | -1.37 | -1.00 |
| 1 | -1.64 | -1.46 | -1.18 | -1.00 | -0.98 | -0.9 | -0.81 | -0.7 | -0 | -133 | -1.74 | -1.82 | -1.22 |
| 2 | -1.77 | -1.60 | -1.26 | -1.11 | -1.04 | -1.07 | -0.79 | -0.89 | -1.00 | -1 39 | -1.81 | -2.0 | -1.31 |
| 3 | -1.71 | -1 | -1.27 | -1.16 | -1. 03 | -1.09 | -0.64 | -0.88 | -0.96 | -1 33 | -1.71 | -2.02 | -1.29 |
| 4 | -1.52 | -1.52 | -I. 21 | -1.11 | -0.93 | -1.00 | 41 | -0.75 | -0.83 | -1.18 | -1.48 | -1.83 | -1.15 |
| 5 | -1.26 | -1.31 | -1 | -0.92 | -0 | -0.79 | $-0.17$ | -0.55 | -0.61 | -0.95 | -1.16 | -1.50 | -0.92 |
| 6 | -0 | 1 | -0.76 | -0.61 | $-0.46$ | -0.51 | 0.04 | -0.32 | -0.33 | -0.65 | -0.79 | -1.09 | -0.62 |
| 7 | -0. | -0.64 | -0.39 | -0.24 | -0.1 | -0.21 | 0.17 | -0.10 | 0.02 | -0.32 | -0.39 | -0.65 | -0.30 |
| 8 | -0.35 | -0.25 | 0.03 | 0.10 | 0.08 | 0.06 | 0.22 | 0.07 | 0.21 | -0.01 | 0. | -0.23 | -0 01 |
| 9 | -0.05 | 10 | 0.25 | 0.32 | 0.26 | 0.24 | 0.24 | 0. | 0.38 | 0.23 | 0.34 | 0.13 | 0.22 |
| 10 | 21 | . 36 | 0.40 | 041 | 0.37 | 0.35 | 0.24 | 0.2 | 0.44 | 0.39 | 060 | 0.38 | 0.37 |
| 11 | 0.41 | 0.49 | 0.43 | 0.41 | 0.44 | 0.40 | 0.27 | 0.3 | 0.4 | 0.48 | 0.76 | 0.83 | 0.45 |
| Midn. | 0.55 | 0.56 | 0.41 | 0.42 | 0.51 | 0.44 | 0.31 | 0.37 | 0.39 | 0.56 | 0.85 | 0.61 | 0.50 |
| 6. 6 | 0.36 | 0.30 | 0.30 | 0.22 | 0.17 | 0.15 | 0.19 | 0.11 | 0.20 | 0.30 | 0.31 | 035 | 0.25 |
| 7. 7 | 49 | 0.42 | . 37 | 0.25 | 0.17 | 0.21 | 0.23 | 0.1 | 0.28 | 0.33 | 0.42 | 057 | 0.33 |
| 8. 8 | 0.48 | 0.43 | 34 | 0.22 | 0.12 | 0.22 | 0.20 | 0.20 | 028 | 0.28 | 042 | 0.60 | 0.32 |
| 9. 9 | 35 | 032 | 0.21 | 0.13 | 0.04 | 0.17 | 0.12 | 0.16 | 0.21 | 0.15 | 0.31 | 0.48 | 0.22 |
| 10.10 | 0.12 | 0.13 | 0.03 | 0.00 | -0.05 | 0.08 | 0.01 | 0.09 | 0.08 | -0.02 | 0.11 | 0.23 | 0.07 |
| 7. 2. 9 | -0.06 | -0.01 | 0.4 | -0.02 | -0.09 | -0.07 | 0.09 | -0.0s | -0.03 | -0.06 | -0.08 | -0.0.4 | -0.05 |
| 6. 2.8 | 14 | -0.08 | 0.02 | 01 | $-0.05$ | $-0.07$ | . 07 | $-0.09$ | -0.02 | -0.05 | -0.14 | -0.14 | -0.07 |
| 6. 2.10 | 005 | 0.12 | 0.17 | 0.11 | 0.04 | 0.03 | . 07 | -0.03 | 0.06 | 008 | 0.06 | 0.06 | 0.06 |
| 6. 2. 6 | -0.35 | -0.33 | -0.22 | $-0.23$ | -0.23 | -0.26 | . 13 | -0.22 | -0.20 | -0.27 | -0.40 | -0.43 | -0.27 |
| 7. 2 | -0.07 | -0.06 | $-0.07$ | -0.19 | -0.27 | . 22 | 25 | 0.22 | -0.23 | 0.21 | -0.29 | -0.13 | -0.18 |
| 8. 2 | -0.23 | -0.25 | -0.28 | -0.39 | -0.44 | -0.34 | 1 | -0.28 | 0.33 | 0.41 | -0.48 | -0.30 | -0.34 |
| 8. | -0.16 | -0.18 | -0.24 | -0.33 | -0.11 | -0.28 | 32 | -0 23 | -0.30 | 0.38 | 0.4 | 0.19 | -0.29 |
| 7. 1 | 0.00 | 0.01 | -0.03 | -0.13 | -0.2f | -0.16 | -0.26 | -0.17 | -0.20 | -0.18 | -0.25 | -0.02 | -0.14 |
| 9.12.2.9 | -0.57 | -0.54 | -0.47 | -0.44 | -0.45 | -0.37 |  | . 29 | -0.34 | -0.55 | -0.6. | -0.61 | -0.46 |
| 7. 2.2(9) | $-0.06$ | 0.02 | 0.09 | 0.07 | 0.00 | 0.01 | -0.01 | -0.01 | 0.08 | 0.01 | 0.03 | 000 | 0.02 |
| Dail.ext. | -0.04 | -0.01 | 0.05 | 0.01 | 0.00 | -0.11 | $1-0.21$ | -0.16 | -0.12 | -0.04 | -0.21 | -0.10 | -0.09 |

India. - Madras. Lat. $13^{\circ} 4^{\prime}$ N. Long. $80^{\circ} 19^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.91 | 1.13 | 1.00 | 1.62 | 1.22 | 1.35 | 1.19 | 1.27 | 1.04 | 0.82 | 0.91 | 0.84 | 1.11 |
| 1 | 1.13 | 1.45 | 1.29 | 1.37 | 1.47 | 1.56 | 1.38 | 1.34 | 1.20 | 1.01 | 1.13 | 1.00 | 1.28 |
| 2 | 1.32 | 1.76 | 1.60 | 1.59 | 1.65 | 1.72 | 1.58 | 1.51 | 1.38 | 1.24 | 1.35 | 1.17 | 1.49 |
| 3 | 1.48 | 2.01 | 1.88 | 1.81 | 1.81 | 1.90 | 1.75 | 1.64 | 1.58 | 1.39 | 1.56 | 1.32 | 1.68 |
| 4 | 1.61 | 2.25 | 2.13 | 1.96 | 1.98 | 2.08 | 1.92 | 1.77 | 1.76 | 1.54 | 1.74 | 1.42 | 1.55 |
| 5 | 1.74 | 2.44 | 2.33 | 1.98 | 2.08 | 2.20 | 2.07 | 1.93 | 1.88 | 1.65 | 1.88 | 1.60 | 1.98 |
| 6 | 1.80 | 2.51 | 2.27 | 1.68 | 1.72 | 1.87 | 1.92 | 1.81 | 1.70 | 1.46 | 1.80 | 1.66 | 1.85 |
| 7 | 1.08 | 1.48 | 1.13 | 0.79 | 0.92 | 1.12 | 1.30 | 1.24 | 1.08 | 0.50 | 1.89 | 1.06 | 1.07 |
| 8 | -0.02 | 0.13 | 0.07 | -0.08 | -0.05 | 0.17 | 0.47 | 0.44 | 0.32 | 0.06 | -0.25 | 0.00 | 0.10 |
| 9 | -0.90 | -0.86 | -0.84 | -1.07 | -1.08 | -0.77 | -0.34 | -0.40 | -0.50 | -0.56 | -1.11 | -0.77 | -0.77 |
| 10 | -1.45 | -1.60 | -1.63 | -1.84 | -2.08 | -1.63 | -1.19 | -1.22 | -1.32 | -1.04 | -1.57 | -1.36 | -1.49 |
| 11 | -1.79 | -2.14 | -2.14 | -2.15 | -2.56 | -2.23 | -1.89 | -1.85 | -2.02 | -1.41 | -1.82 | -1.61 | $-1.47$ |
| Noon. | -1.97 | -2.25 | -2.38 | -2.5 | -2.61 | -2.60 | -2.45 | -2.35 | -2.24 | -1.67 | -1.92 | -1.75 | -2.23 |
| 1 | -1.96 | -2.38 | -2.41 | $-2.46$ | -2.51 | -2.69 | -2.70 | -2.56 | -2.24 | -1.66 | -1.89 | -1.72 | -2.26 |
| 2 | -1.84 | -2.36 | -2.22 | $-2.20$ | -2.22 | -2.53 | -2.67 | -2.40 | -2.07 | -1.58 | -1.66 | $-1.60$ | -2.11 |
| 3 | -1.54 | -2.16 | -1.90 | -1.81 | -1.78 | -2.05 | -2.19 | -2.04 | -1.66 | -1.35 | -1.36 | -1.25 | -1.76 |
| 4 | -1.07 | -1.62 | -].38 | -1.18 | -1.09 | -1.59 | -1.66 | -1.53 | -1.14 | -1.06 | -0.88 | -0.91 | $-1.26$ |
| 5 | -0.53 | -1.01 | $-0.74$ | -0.46 | -0.45 | -0.55 | -0.97 | -0.82 | -0.64 | -0.56 | -0.39 | -0.45 | -0.66 |
| 6 | -0.17 | -0.49 | -0.23 | 0.09 | 0.05 | -0.26 | $-0.36$ | -0.31 | -0.23 | -0.28 | -0.11 | -0.17 | -0.21 |
| 7 | 0.04 | -0.16 | 0.07 | 0.37 | 0.31 | 0.16 | 0.07 | 0.06 | 0.03 | -0.08 | 0.0 .1 | 0.00 | 0.08 |
| 8 | 0.24 | 0.12 | 0.26 | 0.44 | 0.53 | 0.43 | 0.37 | 0.33 | 0.21 | 0.07 | 0.21 | 0.15 | 0.28 |
| 9 | 0.42 | 0.36 | 0.43 | 0.70 | 0.70 | 0.63 | 0.60 | 0.52 | 0.44 | 0.22 | 0.33 | 0.30 | 0.47 |
| 10 | 0.62 | 0.59 | 0.62 | 0.84 | 0.87 | 0.94 | 0.83 | 0.73 | 0.62 | 0.40 | 0.48 | 0.16 | 0.67 |
| 11 | 0.82 | 0.83 | 0.82 | 1.00 | 1.04 | 1.07 | 1.02 | 0.95 | 0.84 | 0.57 | 0.65 | 0.64 | 0.85 |
| Mean. | 19.90 | 20.76 | 22.83 | 23.83 | 24.49 | 24.45 | 24.10 | 23.34 | 22.89 | 21.86 | 20.68 | 19.89 |  |

## XXV.

India. - Bombay. Lat. $18^{\circ} 56^{\prime}$ N. Long. $72^{\circ} 54^{\prime}$ E. Greenw. - Dove.
Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 1.76 | 1.65 | 1.43 | 1.40 | 1.30 | 0.80 | 0.57 | 0.59 | 0.92 | 1.36 | 1.74 | 1.98 | 1.29 |
| 1 | 1.91 | 1.88 | 1.65 | 1.54 | 1.40 | 0.89 | 0.65 | 0.64 | 0.98 | 1.52 | 1.80 | 2.00 | 1.10 |
| 2 | 2.04 | 2.04 | 1.80 | 1.75 | 1.54 | 0.98 | 0.63 | 1.16 | 1.09 | 1.62 | 1.97 | 2.18 | 1.56 |
| 3 | 2.18 | 2.22 | 1.90 | 1.92 | 1.69 | 0.94 | 0.65 | 0.81 | 1.18 | 1.74 | 2.11 | 2.28 | 1.63 |
| 4 | 2.39 | 2.44 | 2.26 | 2.02 | 1.81 | 1.04 | 0.76 | 0.82 | 1.25 | 1.89 | 2.23 | 2.41 | 1.78 |
| 5 | 2.65 | 2.68 | 2.42 | 2.26 | 1.92 | 1.09 | 0.83 | 0.90 | 1.2.5 | 1.96 | 2.40 | 2.62 | 1.92 |
| 6 | 2.85 | 2.88 | 2.60 | 2.20 | 1.65 | 1.03 | 0.84 | 0.84 | 1.21 | 2.00 | 2.55 | 2.66 | 1.94 |
| 7 | 2.53 | 2.37 | 1.61 | 0.76 | 0.44 | 0.60 | 0.55 | 0.51 | 0.61 | 1.02 | 1.47 | 2.08 | 1.21 |
| 8 | 0.72 | 0.18 | -1.04 | $-0.62$ | $-0.51$ | -0.01 | 0.02 | 0.08 | $-0.20$ | $-0.31$ | $-0.12$ | 0.20 | $-0.11$ |
| 9 | -1.04 | $-1.05$ | $-1.49$ | $-1.53$ | $-1.30$ | $-0.46$ | $-0.46$ | -0.45 | $-0.84$ | $-1.53$ | $-1.40$ | $-1.00$ | $-1.05$ |
| 10 | -2.40 | $-2.29$ | $-2.28$ | $-2.00$ | -1.73 | $-0.79$ | $-0.74$ | $-0.76$ | $-1.32$ | $-2.17$ | -2.35 | -2.14 | $-1.75$ |
| 11 | -3.08 | $-2.98$ | $-2.54$ | $-2.20$ | $-2.08$ | $-1.18$ | $-1.07$ | -1.12 | -1.5] | -2.38 | $-3.15$ | $-3.94$ | $-2.19$ |

The numbers without sign must be added; those with the sign - must be subtracted.

India. - Bombay, Contimued.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | b. | Mar | April. | May. | June. | July. | Aug. | Scirt. | Oct. | Nov. | Dee | ar. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Noou. | -3.40 | -3.29 | -2.5 | 2.4 | -2.32 | -1.40 | -1.09 | -1.34 | -1.72 | $-2.39$ | -3.26 | -3.32 | -2.37 |
| 1 | -3. | -3.1 | -2.6 | -2 | -2.28 | -1.50 | -1.12 | -1.35 | -1.77 | -2.2 | -2.96 | -3.35 | -2.32 |
| 2 | -2.78 | -2.99 | -2.56 | -2.32 | -2.14 | -1.52 | -0.97 | -1.35 | -1.55 | -2.09 | -2.55 | -2.97 | $-2.14$ |
| 3 | -2.38 | -2.54 | -2.25 | -2.05 | -1.85 | -1.31 | -0.85 | -1.09 | -1.37 | -1.79 | -2.22 | -2.59 | $-1.86$ |
| 4 | -1.96 | -2.07 | -1.72 | -1.49 | $-1.36$ | -0.89 | -0.63 | -0.76 | -0.95 | -1.38 | -1.55 | -2.03 | $-1.40$ |
| 5 | -1.30 | -1.41 | -1.08 | -0.96 | -0.53 | -0.49 | -0.36 | -0.34 | -0.36 | -0.61 | -0.67 | -1.09 | $-0.79$ |
| 6 | -0.64 | -0.44 | -0.16 | . 00 | 0.09 | -0.02 | 0.03 | 0.13 | 0.14 | 0.01 | -0.14 | -0.52 | -0.13 |
| 7 | -0.2s | -0.07 | 0.19 | 0.43 | 0.63 | 0.22 | 0.21 | 0.26 | 0.28 | 0.30 | 0.09 | -0.23 | 0.17 |
| 8 | 0.00 | 23 | 18 | 0.66 | 0.87 | 0.39 | . 28 | 0.34 | 0.44 | 0.53 | 0.36 | 0.10 | 0.39 |
| 9 | 0.58 | 0.63 | 0.80 | 0.83 | 0.92 | 0.44 | 0.36 | 0.41 | 0.58 | 0.76 | 0.8 | 0.75 | 0.66 |
| 10 | 1.16 | 1.15 | 1.04 | 1.09 | 0.9.J | 0.52 | 0.41 | 0.52 | 0.78 | 0.96 | 1.32 | 1.35 | 0.94 |
| 11 | 1.47 | 1.48 | 1.20 | 1.24 | 1.17 | 0.71 | 0.48 | 0.56 | 0.89 | 1.15 | 1.58 | 1.65 | 1.13 |
| Mean. | 18.39 | 19.30 | 21.00 | 22.50 | 23.43 | 22.35 | 21.67 | 21.45 | 21.42 | 22.08 | 21.28 | 19.54 |  |

## XXVI.

India.-Chlcutta。Lat. $22^{\circ} 33^{\prime} 5^{\prime \prime}$ N. Long. $88^{\circ} 19^{\prime} 2^{\prime \prime}$ E. Greenw. - Dove. Degrees of Reaumur.

| Hlour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dee. | Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 1.86 | 1.69 | 2.06 | 1.60 | 1.90 | 1.12 | 0.69 | 0.69 | 0.71 | 1.00 | 1.24 | 1.51 | 1.34 |
| 1 | 2.24 | 2.00 | 2.37 | 1.96 | 2.06 | 1.12 | 0.50 | 0.78 | 0.76 | 1.17 | 1.47 | 1.77 | 1.54 |
| 2 | 2.3.3 | 2.22 | 2.62 | 2.18 | 2.21 | 1.16 | 0.91 | 0.85 | 0.84 | 1.26 | 1.69 | 2.00 | 1.71 |
| 3 | 2.80 | 2.44 | 2.84 | 2.27 | 2.32 | 1.29 | 1.02 | 0.92 | 0.93 | 1.26 | 1.82 | 2.31 | 1.85 |
| 4 | 3.06 | 2.71 | 3.05 | 2.10 | 2.41 | 1.29 | 1.11 | 0.96 | 1.04 | 1.46 | 2.00 | 2.40 | 1.99 |
| 5 | 3.33 | 2.89 | 3.25 | 2.47 | 2.50 | 1.34 | 1.24 | 1.07 | 1.16 | 1.53 | 2.22 | 2.66 | 2.14 |
| 6 | 53 | 3.11 | . 1 | . 53 | 4 | 1.34 | 1.24 | 1.12 | 1.1 | 1.62 | 2.36 | . 80 | 2.22 |
| 7 | 3.71 | 3.24 | 3.42 | 2.22 | 1.90 | 1.03 | 0.96 | 0.89 | 0.93 | 0.86 | 2.31 | 2.93 | 2.03 |
| 8 | 2.73 | 2.20 | 1.97 | . 18 | 0.81 | 0.45 | 0.42 | 0.32 | 0.27 | 0.31 | 0.93 | 1.68 | 1.11 |
| 9 | 0.91 | 0.71 | 0.46 | .11 | -0.34 | -0.13 | -0.16 | -0.22 | -0.24 | -0.47 | -0.13 | 0.35 | 0.07 |
| 10 | -0.78 | -0.62 | -0.95 | -0.44 | -1.39 | -0.66 | -0.69 | -0.33 | -0.73 | -0.58 | -1.02 | -0.76 | -0.75 |
| 11 | -2.09 | -1.64 | -2.14 | -1.82 | -2.14 | -1.15 | $-1.13$ | -1.08 | -1.16 | -1.60 | $-1.91$ | -1.87 | -1.64 |
| Noon. | -3.31 | - | -3.16 | -2.67 | -2.76 | -1.60 | -1.51 | -1.51 | -1.40 | -1.94 | -2.44 | -2.80 | -2.31 |
| 1 | $-4.14$ | -3.28 | -3.57 | -3.09 | -3.12 | -1.68 | -1.58 | -1.5.5 | -1.44 | -2.05 | -2.80 | -3.29 | -2.66 |
| 2 | -4.52 | -3.64 | -4.2.5 | -3.47 | -3.32 | -1.73 | -1.29 | -1.80 | -1.63 | -2.12 | -3.07 | -3.69 | -2.88 |
| 3 | -4.6.5 | -3.87 | -4.40 | -3.62 | $-3.43$ | -1.92 | -1.24 | -1.20 | -1.27 | -1.83 | -2.98 | -3.69 | -2.84 |
| 4 | -3.75 | -3.69 | 4.23 | 3.40 | -3.10 | $-1.53$ | -0 96 | -0.95 | -0.91 | 1.49 | -2.18 | -2.76 | -2.41 |
| 5 | -3.07 | -3.13 | 3.36 | -2.73 | -2.43 | $-1.20$ | -0.64 | -0.68 | -0.56 | 0.9 | -1.60 | -2.18 | -1.88 |
| 6 | -1.87 | -1.91 | -1.96 | $-1.42$ | -1.23 | -0.57 | -0.31 | $-0.31$ | -0.16 | -0.25 | -0.76 | -1.34 | -1.01 |
| 7 | -0.96 | -0.93 | -0.78 | -0.31 | -0.14 | -0.11 | -0.07 | $-0.09$ | 0.04 | 0.13 | -0.22 | -0.63 | -0.31 |
| 8 | -0.20 | -0.22 | 0.00 | 0.40 | 0.68 | 0.20 | 0.09 | 0.25 | 0.22 | 0.42 | 0.27 | -0.05 | 0.17 |
| 9 | 0.42 | 0.38 | 0.73 | 0.89 | 1.08 | 0.19 | 0.22 | 0.45 | 0.33 | 0.60 | 0.62 | 0.44 | 0.5 .5 |
| 10 | 0.9 .3 | 0.80 | 1.22 | 1.20 | 1.46 | 0.63 | 0.36 | 0.56 | 0.47 | 0.75 | 1.07 | 0.93 | 0.57 |
| 11 | 1.37 | 1.20 | 1.66 | 1.54 | 1.64 | 0.74 | 0.49 | 0.65 | 0.60 | 0.88 | 1.16 | 1.20 | 1.09 |
| Mam. | 15.49 | 17.57 | 21.19 | 23.51 | 24.01 | 23.29 | 22.68 | 22.86 | 22.42 | 21.73 | 18.88 | 16.36 |  |

Asia. - Tiflis. Lat. $41^{\circ} 41^{\prime}$ N. Long. $45^{\circ} 17^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.


The numbers without sign must be added; those with the sign - must be subtracted.

## China. - Peking, Continued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July | Aug | Sept. | Oct. | Nov. | Dec. | Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Noon. | -2.83 | -2.80 | -2.93 | -2.92 | -5.05 | -2.92 | -2.24 | -2.02 | -2.77 | -3.03 | -2.39 | -2.64 | -2.71 |
| 1 | -3.01 | -3.54 | -3.54 | -3.59 | -3.74 | -3.55 | -2.65 | -2.64 | -3.10 | -3.65 | -2.87 | -3.18 | -3.25 |
| 2 | -3.37 | -3.84 | -4.03 | -3.98 | $-4.08$ | -3.97 | -2.88 | -2.90 | -3.38 | -3.96 | -3.07 | -3.41 | -3.57 |
| 3 | -3.30 | -3.94 | $-4.12$ | -4.06 | -4.24 | -4.00 | -2.85 | -2.94 | -3.44 | -3.97 | -2.88 | -2.74 | -3.55 |
| 4 | -2.88 | -3.65 | -3.92 | -3.86 | -4.03 | -3.74 | -2.74 | -2.79 | -3.06 | -2.43 | -2.23 | -2.50 | -3.15 |
| 5 | -1.79 | -2.83 | -3.21 | -3.24 | -3.65 | -3.31 | -2.36 | -2.20 | -2.34 | -2.34 | -1.18 | -1.34 | -2.48 |
| 6 | -0.97 | -1.79 | -2.20 | -2.34 | -3.04 | -2.44 | -1.76 | -1.45 | -1.18 | $-1.12$ | -0.59 | -0.64 | -1.63 |
| 7 | -0.48 | -0.15 | -1.05 | -1.13 | -1.18 | -1.21 | $-0.72$ | -0.45 | -0.50 | -0.54 | -0.48 | -0.26 | -0.68 |
| 8 | -0.02 | -0.27 | -0.30 | -0.33 | -0.19 | -0.11 | 0.12 | 0.08 | 0.09 | -0.02 | 0.01 | 0.18 | -0.06 |
| 9 | 0.30 | 0.26 | 0.26 | 0.24 | 0.59 | 0.59 | 0.63 | 0.51 | 0.57 | 0.12 | 0.30 | 0.54 | 0.43 |
| 10 | 0.57 | 0.73 | 0.83 | 0.84 | 1.15 | 1.14 | 1.04 | 0.83 | 0.97 | 0.86 | 0.59 | 0.77 | 0.86 |
| 11 | 0.90 | 1.20 | 1.30 | 1.28 | 1.67 | 1.65 | 1.35 | 1.18 | 1.32 | 1.00 | 0.51 | 1.01 | 1.22 |
| Me:n. | -3.57 | -2.04 | 3.12 | 9.66 | 15.83 | 19.61 | 21.27 | 19.30 | 15.68 | 9.61 | 1.79 | -2.44 |  |

## XXIX.

Siberia. - Nertciminsk. Lat. $51^{\circ} 18^{\prime}$ N. Long. $117^{\circ} 20^{\prime}$ E. Gr. - Dove.
Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | Aprit. | May | June. | July | Aug. | Sept | Oct | Nov | Dee. | Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.78 | 1.38 | 1.92 | 2.53 | 3.10 | 3.13 | 2.63 | 2.51 | 2.12 | 1.66 | 0.96 | 0.75 | 1.96 |
| 1 | 1.06 | 1.61 | 2.25 | 2.95 | 3.71 | 3.55 | 3.00 | 2.87 | 2.58 | 1.93 | 1.22 | 0.94 | 2.31 |
| 2 | 1.24 | 1.91 | 2.65 | 3.36 | 4.20 | 3.98 | 3.34 | 3.25 | 2.93 | 2.27 | 1.42 | 1.16 | 2.64 |
| 3 | 1.45 | 2.15 | 3.02 | 3.75 | 4.78 | 4.32 | 3.64 | 3.57 | 3.28 | 2.57 | 1.70 | 1.33 | 2.96 |
| 4 | 1.70 | 2.40 | 3.38 | 4.09 | 5.04 | 4.29 | 3.86 | 3.79 | 3.62 | 2.80 | 1.91 | 1.45 | 3.19 |
| 5 | 1.93 | 2.72 | 3.70 | 4.15 | 3.97 | 3.27 | 3.17 | 3.68 | 3.97 | 3.80 | 2.06 | 1.63 | 3.10 |
| 6 | 2.03 | 2.94 | 3.89 | 2.96 | 2.3 | 2.03 | 1.99 | 2.61 | 3.63 | 3.16 | 2.15 | . 76 | 2.63 |
| 7 | 2.26 | 3.00 | 2.88 | 1.43 | 0.82 | 0.74 | 1.01 | 1.31 | 2.07 | 2.46 | 2.35 | 1.95 | 1.86 |
| 8 | 2.20 | 1.82 | 1.36 | 0.19 | -0.53 | -0.45 | -1.28 | 0.11 | 0.66 | 0.84 | 1.61 | 1.95 | 0.71 |
| 9 | 0.56 | -0.20 | -0.12 | $-1.32$ | $-1.77$ | -1.59 | -1.25 | -1.08 | -0.72 | -0.69 | -0.03 | 0.62 | -0.63 |
| 10 | -0.96 | -1.27 | -1.71 | -2.35 | $-2.73$ | -2.52 | $-2.13$ | -2.10 | -1.99 | $-1.52$ | -1.17 | -0.89 | $-1.80$ |
| 11 | -1.90 | $-2.34$ | $-2.61$ | -3.08 | -3.34 | -3.17 | -2.79 | -2.91 | -2.94 | -2.78 | -2.12 | -1.85 | -2.65 |
| Noon. | -2.70 | -3.16 | -3.43 | -3.70 | -3.82 | -3.62 | -3.28 | -3.49 | -3.71 | -3.41 | -2.84 | -2.58 | -3.31 |
| 1 | -3.06 | -3.75 | -396 | -4.01 | -4.08 | -3.80 | -3.58 | -3.76 | $-4.09$ | -3.75 | -3.09 | -2.55 | -3.65 |
| 2 | -3.00 | $-3.80$ | -4.23 | -4.05 | $-4.10$ | -3.73 | -3.66 | -3.92 | $-1.20$ | -3.66 | -2.97 | -2.52 | $-3.66$ |
| 3 | -2.50 | -3.47 | -4.03 | . 81 | -3.99 | -3.59 | -3.48 | -3.79 | -3.86 | -3.26 | -2.27 | -1.87 | -3.33 |
| 4 | -1.54 | $-2.73$ | -3.53 | -3.18 | -3.55 | -3.24 | -3.0 2 | -3.21 | -3.34 | -2.43 | -1.34 | -0.96 | -2.70 |
| 5 | -0.7 | -1.61 | -2.75 | 85 | -3.02 | -3.73 | -2.38 | -2.56 | -2.48 | $-1.42$ | -0.87 | -0.43 | $-1.98$ |
| 6 | -0.23 | -0.63 | $-1.71$ | -1.97 | -2.27 | -2.06 | -1.73 | -1.68 | -1.22 | -0.50 | -0.10 | -0.17 | -1.20 |
| 7 | 0.02 | 0.01 | $-0.31$ | -0.34 | -0.93 | -0.93 | -0.82 | -0.66 | -0.49 | -0.24 | $-0.17$ | -0.70 | -0.17 |
| 8 | 0.13 | 0.39 | 0.24 | 0.61 | 0.27 | 0.97 | 0.37 | 0.41 | 0.34 | 0.30 | 0.06 | 0.08 | 0.29 |
| 9 | 0.27 | 0.63 | 0.66 | 1.19 | 1.34 | 1.32 | 1.24 | 1.30 | 0.99 | 0.64 | 0.34 | 0.22 | 0.84 |
| 10 | 0.13 | 0.86 | 1.06 | 1.72 | 1.92 | 2.02 | 1.78 | 1.70 | 1.30 | 1.01 | 0.54 | 0.43 | 1.23 |
| 11 | 0.57 | 1.16 | 1.17 | 2.17 | 2.63 | 2.63 | 2.29 | 2.14 | 1.71 | 1.31 | 0.75 | 0.56 | 1.62 |
| Mcam. | -21.9 | -17.94 | -5.8.5 | 0.01 | 7.51 | 1.75 | 13.91 | 11.91 | 6.55 | $-1.50$ | -13.44 | -21.36 |  |

The nuubers without sign must be added ; those with the sign - must be subtracted.

Siberia. - Nertchinsk. Lat. $51^{\circ} 18^{\prime}$ N. Long. $119^{\circ} 21^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Mouths, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.91 | 1.42 | 2.07 | 2.69 | 4.07 | 4.29 | 3.07 | 3.00 | 2.16 | 2.31 | 0.76 | 0.66 | 2.28 |
| 2 | 1.00 | 1.68 | . 7 | 3.29 | 4.69 | 4.71 | 3.46 | 3.48 | 2.96 | 2.79 | 0.96 | 0.74 | 2.69 |
| 3 | 1.15 | 2.08 | 3.16 | 3.78 | 5.08 | 4.90 | 3.75 | 3.89 | 3.27 | 3.26 | 1.26 | 0.84 | 3.04 |
| 4 | 1.42 | 2.55 | 3.63 | 3.97 | 4.98 | 4.70 | 3.76 | 4.04 | 3.81 | 3.61 | 1.66 | 1.07 | 3.26 |
| 5 | 1.78 | 2.84 | 3.73 | 3.69 | 4.24 | 3.96 | 3.37 | 3.72 | 3.94 | 3.66 | 2.06 | 1.41 | 3.20 |
| 6 | 2.07 | 2.80 | 3.28 | 2.88 | 2.86 | 2.67 | 2.54 | 2.89 | 3.15 | 3.30 | 2.30 | 1.75 | 2.71 |
| 7 | 2.06 | 2.28 | 2.31 | 1.63 | 1.07 | 0.99 | 1.37 | 1.62 | 2.38 | 2.47 | 2.18 | 1.87 | 1.85 |
| 8 | 1.60 | 1.28 | 0.99 | 0.16 | -0.78 | -0.79 | 0.06 | 0.15 | 0.87 | 1.24 | 1.58 | 1.59 | 0.66 |
| 9 | 0.65 | -0.05 | -0.41 | -1.26 | -2.33 | -2.34 | -1.19 | -1.25 | -0.70 | -0.23 | 0.55 | 0.57 | -0.64 |
| 10 | -0.59 | -1.4: | -1.67 | -2.42 | -3.40 | -3.41 | -1.98 | -2.38 | -1.74 | -1.70 | -0.69 | -0.17 | -1.50 |
| 11 | -1.79 | -2.58 | -2.64 | -3.22 | -3.98 | -3.97 | -2.92 | -3.15 | -2.99 | -2.96 | -1.84 | -1.23 | -2.77 |
| Noon. | -2.61 | -3.29 | -3.25 | -3.64 | $-4.19$ | -4.12 | -3.38 | -3.61 | -3.49 | -3.84 | -2.60 | -2.01 | -3.34 |
| 1 | -2.87 | -3.49 | -3.61 | -3.76 | -4.22 | -4.05 | -3.64 | -3.83 | -3.69 | -4.25 | -2.81 | $-2.30$ | $-3.54$ |
| 2 | -2.56 | -3.27 | -3.74 | -3.65 | $-4.18$ | -3.92 | -3.72 | -3.85 | -4.00 | $-4.20$ | -2.50 | -2.08 | -3.48 |
| 3 | -1.89 | $-2.76$ | -3.65 | -3.33 | $-4.03$ | -3.77 | -3.62 | -3.75 | -3.54 | -3.77 | -1.87 | -1.54 | -3.13 |
| 4 | -1.14 | -2.12 | -3.31 | -2.84 | -3.69 | -3.54 | -3.29 | -3.40 | -3.24 | -3.08 | -1.17 | -0.92 | -2.65 |
| 5 | -0.56 | -1.45 | -2.65 | -2.17 | -3.04 | -3.07 | -2.68 | $-2.76$ | -2.68 | -2.24 | -0.61 | -0.47 | -2.03 |
| 6 | -0.23 | -0.81 | -1.78 | -1.39 | -2.08 | -2.30 | -1.82 | -1.86 | -1.54 | -1.36 | -0.27 | -0.25 | -1.31 |
| 7 | -0.11 | -0.21 | -0.77 | -0.56 | -0.92 | $-1.23$ | -0.81 | -0.80 | -0.86 | -0.54 | -0.12 | -0.23 | -0.60 |
| 8 | -0.04 | 0.31 | 0.18 | 0.20 | 0.26 | 0.00 | 0.20 | 0.24 | 0.17 | 0.17 | -0.25 | -0.24 | 0.12 |
| 9 | 0.09 | 0.74 | 0.90 | 0.82 | 1.29 | 1.21 | 1.06 | 1.11 | 0.97 | 0.74 | 0.05 | -0.17 | 0.73 |
| 10 | 0.31 | 1.02 | 1.34 | 1.29 | 2.11 | 2.25 | 1.51 | 1.74 | 1.17 | 1.18 | 0.20 | 0.02 | 1.18 |
| 11 | 0.57 | 1.19 | 1.56 | 1.71 | 2.78 | 3.09 | 2.23 | 2.19 | 1.73 | 1.54 | 0.39 | 0.28 | 1.61 |
| Midn. | 0.78 | 1.29 | 1.76 | 2.15 | 3.41 | 3.75 | 2.65 | 2.57 | 1.88 | 1.90 | 0.58 | 0.52 | 1.94 |
| 6. 6 | 0.92 | 1.00 | 0.75 | 0.75 | 0.39 | 0.19 | 0.36 | 0.52 | 080 | 0.97 | 1.01 | 0.75 | 0.70 |
| 7. 7 | 0.98 | 1.04 | . 77 | 0.53 | 0.07 | -0.12 | 0.28 | 0.41 | 0.76 | 0.97 | 1.03 | 0.82 | 0.63 |
| 8. 8 | 0.78 | 0.50 | 0.58 | 0.18 | -0.26 | -0.39 | 0.13 | 0.20 | 0.52 | 0.71 | 0.77 | 0.67 | 0.39 |
| 9.9 | 0.37 | 0.34 | 0.24 | -0.22 | -0.52 | -0.56 | -0.06 | -0.07 | 0.13 | 0.26 | 0.30 | 0.35 | 0.0 .5 |
| 10.10 | -0.14 | -0.20 | -0.16 | -0.57 | -0.65 | -0.58 | -0.24 | -0.32 | -0.29 | -0.26 | -0.25 | -0.07 | -0.31 |
| 7. 2. 9 | -0.14 | -0.08 | -0.18 | -0 40 | -0.61 | -0.57 | -0.43 | -0.38 | -0.22 | -0.33 | -0.09 | -0.13 | -0.30 |
| 6. 2. 8 | -0.18 | -0.0.5 | -0.09 | -0.19 | -0.35 | -0.42 | -0.33 | -0.25 | -0.23 | -0.24 | -0.08 | -0.19 | -0.22 |
| 6. 2.10 | -0.06 | 0.18 | 0.29 | 0.17 | 0.26 | 0.33 | 0.11 | 0.25 | 0.11 | 0.09 | 0.00 | -0.01 | 0.14 |
| 6. 2. 6 | -0.24 | -0.43 | -0.75 | 0.72 | -1.13 | -1.18 | -1.00 | -0.95 | -0.80 | -0.75 | -0.16 | -0.19 | -0.69 |
| 7. 2 | -0.41 | -0.61 | -0.65 |  |  | -1.53 | -1 | -1.11 | -0.66 | -0.89 | -0.32 | -0.22 | -0.8.5 |
| 8. 2 | -0 | 1.34 | -1.60 | -1.85 | -2.32 | -2.26 | -1.78 | -1.88 | -1.69 | -1.78 | -0.97 | -0.71 | -159 |
| 8. 1 | -0 | . 11 | -1.31 | -1.80 | -2.50 | -2.42 | -1.79 | -1.84 | -1.11 | -1.51 | $-0.62$ | -0.36 | -'.14 |
| 7. 1 | -0.25 | -0.50 | -0.72 | -1.01 | -1.56 | -1.47 | -1.18 | -1.13 | -0.81 | $-0.57$ | -0.16 | -0.11 | -0.81 |
| 9.12.3.9 | -0 48 | -1.00 | -1.38 | -1 |  | -2.36 | -1 | -1.87 | -1.57 | -1.48 | 9.46 | -0.25 | -1.41 |
| 7. 2.2(9) | -0.08 | 0.12 | 0.09 | -0.09 | -0.13 | -0.13 | -0.06 | $-0.01$ | 0.08 | $-0.04$ | -0.05 | $-0.14$ | $-0.04$ |
| Thail.ext. | -0.40 | -0.33 | -0.01 | -0.11 | 0.43 | 0.39 | 0.02 | 0.08 | -0.03 | -0.30 | -0.26 | -0.22 | -0.14 |

The numbers without sign must th: added: thase with the sign - must be subtracted.

## XXXI.

Siberia. - Barnaul. Lat. $53^{\circ} 20^{\prime}$ N. Long. $83^{\circ} 27^{\prime}$ E. Greenv.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Fahrenheit.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 2.54 | 1.85 | 4.70 | 5.49 | 8. 82 | 7.83 | 8.37 | 7.11 | 5.45 | 3.06 | 2.48 | 1.82 | 495 |
| 2 | 2.81 | 2.14 | 5.47 | 6.30 | 10.19 | 8.87 | 9.77 | 8.35 | 6.50 | 3.78 | 2.97 | 2.00 | 5.76 |
| 3 | 2.70 | 2.45 | 6.28 | 7.07 | 10.96 | 9.59 | 10.69 | 9.52 | 7.6.3 | 4.52 | 3.35 | 2.07 | 6.41 |
| 4 | 2.39 | 2.81 | 7.02 | 7.45 | 10.76 | 9.14 | 10.67 | 10.15 | 8.48 | 5.15 | 3.71 | 2.18 | 6.66 |
| 5 | 2.07 | 3.13 | 7.43 | 7.09 | 9.32 | 7.58 | 9.50 | 9.77 | 860 | 5.47 | 4.01 | 2.45 | 6.37 |
| 6 | 1.96 | 3.33 | 9.38 | 5.87 | 6.68 | 5.45 | 7.18 | 8.12 | 5.58 | 5.29 | 4.16 | 2.79 | 5.65 |
| 7 | 2.00 | 3.20 | 5.90 | 3.87 | 3.38 | 2.50 | 4.05 | 5.36 | 270 | 4.46 | 3.96 | 2.99 | 3.94 |
| 8 | 1.95 | 2.59 | 3.71 | 1.37 | -0.11 | -0.18 | 0.70 | 1.96 |  | 2.97 | 3.15 | 2.70 | 1.96 |
| 9 | 53 | 1.37 | 0.86 | -1.28 | $-3.02$ | -2.48 | -2.32 | -1.44 | -0 56 | 0.99 | 1.64 | 1.73 | -0.25 |
| 10 | 0.45 | -0.36 | -2.18 | -3.74 | -3.06 | $-4.61$ | $-4.68$ | -432 | $-367$ | -122 | -0.41 | 0.11 | $-2.48$ |
| 11 | -1.22 | -2.30 | -4.91 | $-5.78$ | -6.35 | -5.99 | -6.35 | -6.48 | $-621$ | -3 31 | $-2.61$ | -1.76 | -4.43 |
| Noo | -3.08 | $-403$ | $-6.89$ | -7.34 | $-7.20$ | -7.31 | $-7.52$ | -7.97 | -7.99 | $-5.00$ | -4.48 | -3.42 | -6.01 |
| 1 | -4.59 | -5.13 | -797 | -8.35 | -8.03 | -8.39 | -8 42 | -8.96 | -8.96 | -6.05 | $-558$ | -4.39 | $-7.07$ |
| 2 | -5.27 | -5.38 | -8.21 | -8.71 | -8.75 | -8.78 | $-9.16$ | -9.63 | -9.23 | -6.39 | -5.72 | -4.48 | $-7.47$ |
| 3 | -4.93 | -4.77 | $-7.76$ | -8 39 | -9.41 | -8 91 | -9.56 | -9.88 | -8.82 | -6.03 | $-502$ | -3.78 | $-7.27$ |
| 4 | -378 | -3.56 | -6.84 | -7.34 | $-9.50$ | -8.01 | $-9.36$ | -9.50 | -7.81 | -5.22 | -3.85 | -2 68 | $-6.46$ |
| 5 | -2. | -2.14 | -5.65 | $-5.58$ | -8.66 | -6.32 | -8.3.5 | -8.28 | -6.26 | -4.05 | -2.57 | -1.60 | --5.15 |
| 6 | -0.90 | -0.83 | $-6.46$ | -3.35 | -6.82 | -4.39 | -6.49 | -6.19 | -4.25 | -2.75 | -1.55 | -0 83 | -3.74 |
| 7 | 0.02 | 0.09 | -2.61 | -1.04 | -4.16 | -1.94 | $-4.01$ | -3.51 | -2 07 | -1.49 | -0.86 | -0.43 | -1.82 |
| 8 | 0.47 | 0.63 | -0.97 | 1.04 | -1.31 | 0.11 | -1.31 | -0.68 | 0.02 | -0.36 | -0.41 | -0 23 | -0.25 |
| 9 | 0.70 | 0.92 | 0.63 | 2.61 | 1.46 | 1.50 | 1.24 | 1.80 | 1.76 | 0.54 | 0.00 | 0.00 | 1.13 |
| 10 | 0.95 | 1.10 | 2.00 | 3.62 | 3.78 | 3.49 | 3.38 | 3.67 | 2.99 | 1.28 | 0.52 | 0.38 | 2.27 |
| 11 | 1.42 | 1.28 | 3.13 | 4.25 | 5.69 | 4.75 | 5.20 | 4.97 | 3.85 | 187 | 1.15 | 0.92 | 3.22 |
| Midn. | 2.03 | 1.55 | 3.98 | 4.82 | 7.36 | 6.26 | 6.82 | 6.03 | 4.59 | 2.45 | 1.85 | 1.44 | 4.10 |
| 6. 6 | 0.54 | 1.24 | 1.46 | 1.26 | -0.07 | 0.54 | 0.34 | 0.97 | 1.69 | 1.28 | 1.31 | 099 | 0.97 |
| 7. 7 | 1.01 | 1.64 | 1.64 | 1.42 | -0.41 | 0.27 | 0.02 | 0.92 | 1.76 | 1.49 | 1.55 | 128 | 1.06 |
| 8. 8 | 1.24 | 1.62 | 1.37 | 22 | -0.72 | -0 05 | $-0.29$ | 0.65 | 1.35 | 1.31 | 137 | 1.24 | 0.86 |
| 9.9 | 1.10 | 1.15 | 0.74 | 0.68 | $-0.79$ | -0.34 | -0.54 | 0.18 | 0.59 | 0.77 | 0.83 | 0.56 | 0.43 |
| 10.10 | 0.70 | 0.38 | -0.09 | -0.07 | -0.63 | -0.56 | -0.65 | $-0.34$ | $-0.34$ | 0.0.5 | 007 | 0.25 | -0.11 |
| 7. 2. 9 | -0.86 | -0.43 | $-0.56$ | -0 | . 31 | -1.49 | -1.28 | -0.83 | $-0.63$ | -0.47 | -0.59 | -0.50 | -0.81 |
| 6. 2. 8 | -0.95 | -0.47 | 0.07 | -0.61 | -1.13 | -1.08 | -1.10 | -0.72 | $-0.52$ | -0 50 | -0 65 | -0.63 | -0 70 |
| 6. 2.10 | -0.79 | $-0.32$ | 1.06 | 0.27 | 0.56 | 005 | 0.47 | 0.72 | 0.47 | 0.07 | -0.34 | -0.43 | 0.16 |
| 6. 2. 6 | -1.10 | -0.97 | $-1.76$ | -2.07 | -2.97 | -2.57 | -2.81 | -2.57 | -1.94 | -1.28 | -1.04 | 083 | -1.85 |
| 7. 2 | -1.64 | $-1.09$ | -1.16 | -2.42 | -2.70 | -3.14 | -2.56 | -2.11 | -1.83 | -0 97 | -0.88 | -0.75 | -1.77 |
| 8. 2 | -1.65 | -1.40 | -2 25 | -3.67 | $-4.45$ | $-4.48$ | -1.23 | -3.84 | -3.27 | $-171$ | -1.29 | -0.59 | -2 76 |
| 8. 1 | -1.31 | -1.27 | -2.13 | -3.49 | -4.07 | $-4.29$ | -3.86 | -3.50 | -3.13 | $-1.54$ | -1.22 | -0.85 | -2.56 |
| 7. 1 | -1.30 | $-0.97$ | -1.01 | $-2.24$ | -2 33 | -2.95 | -2.19 | -1.80 | $-1.69$ | -0.80 | -0.81 | -0.70 | -1.57 |
| 912.39 | -1.45 | -1.62 | -3.29 | -3.60 | $-4.55$ | $-4.23$ | -4.5) | -4.37 | -3 92 | . 39 | -1.96 | -1.37 | -3.11 |
| 7. $2.2(9)$ | $-0.47$ | -0.09 | -0.27 | 0.09 | -0.63 | -0.68 | -0.6.5 | -0.18 | -0.05 | $-0.23$ | -0.45 | $-0.38$ | -0.34 |
| Dail. ext. | -1.24 | -1.04 | 0.59 | -0.63 | 0.74 | 0.34 | 0.56 | 0.14 | -0 32 | -0.47 | -079 | -0.74 | -0.41 |

Siberia. - Barnaul. Lat. $53^{\circ} 20^{\prime}$ N. Long. $83^{\circ} 27^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Ocı. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 1.13 | 0.82 | 2.09 | 2.44 | 3.92 | 3.48 | 3.72 | 3.16 | 2.42 | 1.36 | 1.10 | 0.51 | 2.20 |
| 2 | 1.25 | 0.95 | 2.43 | 2.80 | 4.53 | 3.94 | 4.34 | 3.71 | 2.89 | 1.68 | 1.32 | 0.59 | 2.56 |
| 3 | 1.20 | 1.10 | 2.79 | 3.14 | 4.87 | 4.26 | 4.73 | 4.23 | 3.40 | 2.01 | 1.49 | 0.92 | 2.85 |
| 4 | 1.06 | 1.25 | 3.12 | 3.31 | 4.78 | 4.06 | 4.74 | 4.51 | 3.77 | 2.29 | 1.65 | 0.97 | 2.96 |
| 5 | 0.92 | 1.39 | 3.30 | 3.15 | 4.14 | ¢.37 | 4.22 | 4.34 | 3.82 | 2.43 | 1.78 | 1.09 | 2.83 |
| 6 | 0.87 | 1.48 | 4.17 | 2.61 | 2.97 | 2.42 | 3.19 | 3.61 | 3.40 | 2.35 | 1.55 | 1.24 | 2.51 |
| 7 | 0.89 | 1.42 | 2.62 | 1.72 | 1.50 | 1.11 | 1.80 | 2.38 | 2.48 | 1.98 | 1.76 | 1.33 | 1.75 |
| 8 | 0.88 | 1.15 | 1.65 | 0.61 | $-0.05$ | $-0.08$ | 0.31 | 0.57 | 1.20 | 1.32 | 1.40 | 1.20 | 0.87 |
| 9 | 0.65 | 0.61 | 0.38 | $-0.57$ | $-1.34$ | -1.10 | -1.03 | -0.64 | -0.25 | 0.44 | 0.73 | 0.77 | -0.11 |
| 10 | 0.20 | $-0.16$ | -0.97 | -1.66 | $-2.25$ | -2.05 | $-2.08$ | $-1.92$ | $-1.63$ | $-0.54$ | -0.18 | 0.05 | $-1.10$ |
| 11 | -0.54 | $-1.02$ | -2.18 | $-2.57$ | -2.82 | $-2.66$ | $-2.82$ | -2.88 | $-2.76$ | $-1.47$ | $-1.16$ | -0.78 | -1.97 |
| Noo | -1.37 | $-1.79$ | -3.06 | -3.26 | $-3.20$ | -3.25 | $-3.34$ | -3.54 | -3.55 | $-2.22$ | -1.99 | $-1.52$ | $-2.67$ |
| 1 | -2.04 | -2.28 | -3.54 | -3.71 | -3.57 | $-3.73$ | $-3.74$ | -3.98 | -3.98 | $-2.69$ | $-2.48$ | -1.95 | --3.14 |
| 2 | $-2.34$ | $-2.39$ | -3.65 | $-3.87$ | -3.90 | -3.90 | $-4.07$ | $-4.28$ | $-4.10$ | $-2.84$ | -2.54 | -1.99 | $-3.32$ |
| 3 | -2.19 | $-2.12$ | -3.45 | -3.73 | $-4.18$ | -3.96 | $-4.25$ | $-4.39$ | $-3.92$ | -2.69 | -2.23 | -1.68 | $-3.23$ |
| 4 | -1.68 | $-1.58$ | -3.04 | -3.26 | $-4.22$ | -3.56 | $-4.16$ | $-4.22$ | -3.47 | -2.32 | -1.71 | -1.19 | $-2.87$ |
| 5 | $-1.00$ | $-0.95$ | $-2.51$ | -2.48 | -3.85 | -2.81 | -3.71 | -3.68 | $-2.78$ | -1.80 | -1.14 | -0.71 | -2.29 |
| 6 | $-0.40$ | $-0.37$ | $-2.87$ | -1.49 | -3.08 | -1.95 | $-2.85$ | --9.75 | $-1.89$ | $-1.22$ | $-0.69$ | -0.37 | -1.66 |
| 7 | 0.01 | 0.04 | -1.16 | -0.46 | $-1.85$ | -0.86 | -1.78 | $-1.56$ | $-0.92$ | -0.66 | -0.38 | $-0.19$ | -0.81 |
| 8 | 0.21 | 0.28 | $-0.43$ | 0.46 | $-0.58$ | 0.05 | -0.58 | -0.30 | 0.01 | $-0.16$ | -0.18 | $-0.10$ | $-0.11$ |
| 9 | 0.31 | 0.41 | 0.28 | 1.16 | 0.6.) | 0.80 | 0.55 | 0.80 | 0.78 | 0.24 | 0.00 | 0.00 | 0.50 |
| 10 | 0.42 | 0.49 | 0.89 | 1.61 | 1.68 | 1.55 | 1.50 | 1.63 | 1.33 | 0.57 | 0.23 | 0.17 | 1.01 |
| 11 | 0.63 | 0.57 | 1.39 | 1.89 | 2.53 | 2.11 | 2.31 | 2.21 | 1.71 | 0.83 | 0.51 | 0.41 | 1.43 |
| Midn. | 0.90 | 0.69 | 1.77 | 2.14 | 3.27 | 2.78 | 3.03 | 2.68 | 2.04 | 1.09 | 0.82 | 0.64 | 1.82 |
| 6. 6 | 0.24 | 0.55 | 0.65 | 0.56 | $-0.03$ | 0.24 | 0.15 | 0.43 | 0.75 | 0.57 | 0.58 | 0.44 | 0.43 |
| 7. 7 | 0.45 | 0.73 | 0.73 | 0.63 | -0.15 | 0.12 | 0.01 | 0.41 | 0.78 | 0.66 | 0.69 | 0.57 | 0.47 |
| 8. 8 | 0.5 .5 | 0.72 | 0.61 | 0.54 | $-0.32$ | $-0.02$ | $-0.13$ | 0.29 | 0.60 | 0.58 | 0.61 | 0.55 | 0.38 |
| 9. 9 | 0.49 | 0.51 | 0.33 | 0.30 | -0.3.) | -0.15 | -0.24 | 0.08 | 0.26 | 0.34 | 0.37 | 0.38 | 0.19 |
| 10.10 | 0.31 | 0.17 | -0.04 | $-0.03$ | $-0.2 \mathrm{~S}$ | $-0.25$ | -0.29 | $-0.15$ | $-0.15$ | 0.02 | 0.03 | 0.11 | -0.05 |
| 7.2. 9 | -0.38 | -0.19 | -0.25 | $-0.33$ | $-0.58$ | -n. + it | $-0.57$ | -0.37 | $-0.28$ | $-0.21$ | -0.26 | $-0.22$ | -0.36 |
| 6.2. 8 | $-0.42$ | $-0.21$ | 0.03 | -0.27 | -0.50 | - - 43 | -0.49 | $-0.32$ | $-0.23$ | -0.22 | -0.29 | -0.28 | $-0.31$ |
| 6. 2.10 | -0.3. | $-0.14$ | 0.47 | 0.12 | 0.2 .5 | 0.02 | 0.21 | 0.32 | 0.21 | 0.03 | -0.15 | $-0.19$ | 0.07 |
| 6. 2. 6 | -0.62 | $-0.43$ | -0.78 | $-0.92$ | $-1.32$ | $-1.14$ | -1.25 | $-1.14$ | -0.86 | -0.57 | $-0.46$ | -0.37 | $-0.82$ |
| 7. 2 | -0.73 | $-0.49$ | $-0.52$ | -1.80 | $-1.20$ | $-1.40$ | $-1.14$ | -0.95 | -0.81 | $-0.43$ | -0.39 | -0.33 | -0.79 |
| S. 2 | $-0.73$ | $-0.62$ | $-1.0$ | -1.63 | $-1.98$ | $-1.99$ | $-1.88$ | -1.71 | -1.45 | $-0.76$ | $-0.57$ | $-0.40$ | $-1.23$ |
| S. 1 | -0.58 | -0.57 | -0.9.) | $-1.55$ | -1.81 | $-1.91$ | $-1.72$ | $-1.56$ | -1.39 | $-0.69$ | $-0.54$ | -0.38 | $-1.14$ |
| 7. 1 | -0.58 | $-0.43$ | -0.46 | $-1.00$ | -1.04 | -1.31 | $-0.97$ | -0.80 | $-0.75$ | -0.36 | $-0.36$ | -0.31 | $-0.70$ |
| 9.12.3.9 | -0.64 | -0.72 | $-1.46$ | $-1.60$ | -2.02 | -1.58 | $-2.02$ | $-1.94$ | $-1.74$ | -1.06 | $-0.87$ | -0.61 | -1.38 |
| 7. $2.2(9)$ | -0.21 | -0.04 | -0.12 | 0.04 | $-0.23$ | $-0.30$ | $-0.29$ | -0.08 | $-0.02$ | $-0.10$ | $-0.20$ | -0.17 | -0.15 |
| Dail.ext. | -0.5.5 | -0.46 | 0.26 | $-0.28$ | 0.33 | 0.15 | 0.25 | 0.06 | -0.14 | -0.21 | -0.35 | $-0.33$ | $-0.18$ |

Siberia. - Barnaul. Lat. $53^{\circ} 20^{\prime}$ N. Long. $83^{\circ} 27^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of lieaumur.

| Hour. | Jan. | Feb. | Mareh. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dee. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.99 | 1.98 | 2.43 | 2.65 | 3.70 | 3.75 | 3.18 | 3.10 | 2.50 | 1.99 | 1.06 | 0.77 | 2.39 |
| 1 | 1.15 | 2.21 | 2.78 | 3.03 | 4.11 | 4.30 | 4.07 | 3.50 | 3.20 | 2.24 | 1.22 | 0.86 | 2.72 |
| 2 | 1.26 | 2.36 | 3.13 | 3.24 | 4.47 | 4.83 | 4.49 | 3.90 | 3.63 | 2.50 | 1.89 | 0.95 | 3.00 |
| 3 | 1.41 | 2.47 | 3.34 | 3.49 | 4.72 | 4.95 | 4.77 | 4.29 | 3.92 | 2.69 | 1.46 | 1.01 , | 3.21 |
| 4 | 1.56 | 2.56 | 3.61 | 3.59 | 4.20 | 4.11 | 4.10 | 4.23 | 4.11 | 2.89 | 1.51 | 1.07 | 3.18 |
| 5 | 1.55 | 2.65 | 3.70 | 2.73 | 2.85 | 3.12 | 3.34 | 3.60 | 3.90 | 2.91 | 1.57 | 1.10 | 2.76 |
| 6 | 1.61 | 2.69 | 2.90 | 1.58 | 1.44 | 1.75 | 1.88 | 2.29 | 3.06 | 2.68 | 1.59 | 1.09 | 2.05 |
| 7 | 1.53 | 2.30 | 1.63 | 0.46 | 0.23 | 0.49 | 0.50 | 0.85 | 1.54 | 1.54 | 1.50 | 1.18 | 1.17 |
| 8 | 0.94 | 1.15 | 0.13 | -0.69 | $-0.80$ | $-0.65$ | $-0.54$ | $-0.51$ | $-0.08$ | 0.57 | 0.9 .5 | 0.93 | 0.14 |
| 9 | 0.27 | $-0.47$ | -1.3 | -1.80 | $-1.91$ | -1.78 | $-1.51$ | $-1.79$ | $-1.62$ | $-0.73$ | $-0.03$ | 0.11 | $-1.08$ |
| 10 | $-0.79$ | $-1.90$ | $-2.36$ | $-2.68$ | -2.71 | $-2.75$ | $-2.70$ | $-2.80$ | $-2.84$ | $-1.96$ | $-1.12$ | $-0.8{ }^{\prime}$ | $-2.12$ |
| 11 | -1.69 | $-2.95$ | $-3.31$ | $-3.27$ | -3.39 | $-3.39$ | -3.44 | $-3.41$ | $-3.75$ | $-2.81$ | $-1.93$ | $-1.62$ | -2.91 |
| Noon | $-2.35$ | -3.89 | $-3.75$ | -3.66 | $-3.73$ | $-3.98$ | $-3.90$ | -3.81 | $-4.19$ | $-3.48$ | $-2.42$ | -2.04 | -3.44 |
| 1 | -2.61 | $-1.25$ | $-4.11$ | $-3.65$ | $-4.04$ | $-1.19$ | $-4.09$ | $-4.11$ | $-1.41$ | $-3.72$ | $-2.57$ | -2.12 | -3.66 |
| 2 | -2.39 | $-4.23$ | $-4.07$ | -3.65 | $-4.13$ | $-4.34$ | $-4.21$ | $-4.10$ | $-4.34$ | -3.64 | $-2.39$ | -1.70 | -3.60 |
| 3 | $-1.88$ | -3.62 | $-3.69$ | -3.89 | $-4.09$ | $-4.19$ | -3.89 | -3.91 | $-4.11$ | -3.17 | -1.66 | $-1.09$ | -3.22 |
| 4 | -1.19 | $-2.30$ | $-2.67$ | $-2.62$ | -3.51 | -3.57 | -3.6.5 | -3.68 | $-3.21$ | $-2.58$ | $-1.05$ | $-0.76$ | $-2.56$ |
| 5 | -0.8I | $-1.30$ | $-1.69$ | -1.82 | -3.09 | -3.04 | $-3.07$ | -2.78 | -2.29 | $-1.49$ | $-0.71$ | $-0.53$ | $-1.59$ |
| 6 | $-0.41$ | $-0.56$ | $-0.81$ | -0.62 | $-1.92$ | -2.19 | $-2.09$ | $-1.54$ | $-1.0 .3$ | $-0.72$ | $-0.33$ | $-0.28$ | -1.05 |
| 7 | $-0.20$ | 0.09 | 0.35 | 0.27 | $-0.46$ | $-0.84$ | $-0.69$ | $-0.20$ | $-0.17$ | $-0.08$ | $-0.03$ | $-0.02$ | $-0.17$ |
| 8 | 0.12 | 0.69 | 0.39 | 0.99 | 0.77 | 0.51 | 0.52 | 0.67 | 0.60 | 0.81 | 0.23 | 0.19 | 0.50 |
| 9 | 0.32 | 1.08 | 0.88 | 1.50 | 1.64 | 1.48 | 1.12 | 1.46 | 1.26 | 0.52 | 0.42 | 0.39 | 1.06 |
| 10 | 0.73 | 1.47 | 1.16 | 2.02 | 2.42 | 2.31 | 2.22 | 2.04 | 1.85 | 1.29 | 0.59 | 0.58 | 1.58 |
| 11 | 0.78 | 1.76 | 1.92 | 2.35 | 3.11 | 3.0.) | 2.88 | 2.58 | 2.36 | 1.68 | 0.83 | 0.75 | 2.00 |
| Mean. | -14.71 | $-13.47$ | $-5.47$ | 1.77 | 7.78 | 13.62 | 14.98 | 12.76 | 7.53 | 1.58 | -8.36 | -13.07 | 1.94 |

The numbers without sign must be added; those with the sign - must be subtracted.

## IIOURLYCORRECTIONS

FOR

## PERIODIC VARIATIONS.

EUROPE.

## XxxIV.


Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.90 | 1.08 | 1.22 | 1.55 | 1.85 | 2.44 | 2.17 | 2.20 | 1.63 | 1.5 | 1.15 | 0.93 | 1.55 |
| 2 | 0.99 | 1.26 | 1.50 | 1.S4 | 2.10 | 2.59 | 2.41 | 2.49 | 1.91 | 1.75 | 1.29 | 1.02 | 176 |
| 3 | 1.14 | 1.58 | 1.96 | 2.31 | 256 | 3.02 | 2.99 | 3.00 | 2.38 | 2.12 | 1.53 | 1.19 | 2.15 |
| 4 | 1.36 | 1.99 | 2.46 | 2.80 | 3.06 | 3.51 | 3.68 | 3.54 | 2.91 | 2.58 | 1.87 | 1.43 | 2.60 |
| 5 | 1.60 | 2.36 | 2.80 | 3.07 | 330 | 3.71 | 4.06 | 3.79 | 3.25 | 2.9 | 2.22 | 1.70 | 2.90 |
| 6 | 1.77 | 2.52 | 2.76 | 2.92 | 3.04 | 3.36 | 3.81 | 3.53 | 3.17 | 3.10 | 2.42 | 1.87 | 2.86 |
| 7 | 1.74 | 2.33 | 2.24 | 2.25 | 2.19 | 2.38 | 2.82 | 2.62 | 2.58 | 2.82 | 2.33 | 1.83 | 2.34 |
| 8 | 1.40 | 1.73 | 1.29 | 1.15 | 0.93 | 0.98 | 1.27 | 1.22 | 1.51 | 2.05 | 1.82 | 1.47 | 1.40 |
| 9 | 0.72 | 0.78 | 0.10 | -0.15 | $-0.47$ | -0.51 | $-0.44$ | -0.35 | 0.15 | 0.8 | 0.93 | 0.78 | 020 |
| 10 | -0.24 | -0.3S | -1.08 | -1.39 | -1.68 | -1.75 | -1.89 | -1.78 | -1.23 | -0.58 | -0.22 | $-0.15$ | -1.03 |
| 11 | -1.27 | $-1.54$ | -2.06 | -2.36 | $-2.53$ | -2.59 | $-2.57$ | -2.84 | $-2.41$ | -2.00 | $-1.41$ | -1.14 | -2.09 |
| Noo | $-2.15$ | $-2.49$ | -2.71 | -2.98 | -3.01 | -3.08 | -3.38 | -3.49 | -3.24 | -3.14 | -2.39 | -1.99 | -2.84 |
| 1 | -2.69 | $-3.07$ | -3.02 | -3.27 | $-3.23$ | $-3.40$ | $-3.61$ | -3.51 | $-3.70$ | -3.82 | $-3.00$ | $-2.52$ | $-3.26$ |
| 2 | -2.78 | -3.2 | -3.04 | $-3.23$ | -3.31 | $-3.70$ | $-3.76$ | $-3.92$ | $-3.80$ | -3.99 | $-3.16$ | $-2.66$ | $-3.39$ |
| 3 | -2.44 | $-3.0$ | -2.8 | -3.10 | -3.31 | -3.97 | -3.89 | -3.87 | $-3.59$ | $-3.69$ | $-2.93$ | $-2.44$ | $-3.26$ |
| 4 | -1.83 | -2.5 | $-2.45$ | $-2.72$ | -3.14 | $-4.05$ | -3.88 | -3.62 | -3.11 | -3.04 | $-2.41$ | -1.95 | $-2.89$ |
| 5 | -1.11 | -1.81 | -1.89 | $-2.15$ | -2.70 | $-3.70$ | $-3.53$ | -3.05 | $-2.38$ | -2.21 | -1.76 | -1.35 | $-2.30$ |
| 6 | $-0.45$ | $-1.05$ | -1.20 | -1.39 | -1.9 I | $-2.79$ | $-2.67$ | -2.18 | $-1.48$ | $-1.3$ | - . 09 | -0.75 | -1.52 |
| 7 | 0.0 .5 | $-0.34$ | -0.44 | $-0.53$ | $-0.84$ | $-1.42$ | $-1.38$ | -1.01 | -0.51 | -0.50 | -11.48 | $-0.24$ | $-0.64$ |
| 8 | 0.39 | 0.25 | 0.26 | 0.30 | 0.29 | 0.13 | 0.08 | 0.21 | 0.38 | 0.19 | 0.05 | 0.17 | 0.23 |
| 9 | 0.59 | 0.67 | 0.75 | 0.94 | 1.22 | 1.46 | 1.33 | 1.22 | 1.0.) | 0.71 | 0.46 | 0.46 | 0.91 |
| 10 | 071 | 0.90 | 1.07 | 1.31 | 1.76 | 229 | 2.10 | 1.86 | 1.43 | 1.05 | 0.76 | 0.66 | 1.33 |
| 11 | 0.78 | 0.99 | 1.1 .5 | 1.44 | 1.93 | 2.57 | 2.33 | 2.11 | 1.54 | 1.24 | 0.95 | 0.79 | 1.49 |
| Midn. | 0.84 | 1.02 | 1.15 | 1.46 | 1.88 | 2.51 | 224 | 2.14 | 1.55 | 1.36 | 1.06 | 0.86 | 1.51 |
| 6. 6 | 0.66 | 0.74 | 0.78 | 0.76 | 0.57 | 0.28 | 0.57 | 0.68 | 0.85 | 0.89 | 0.67 | 0.56 | 0.67 |
| 7. 7 | 0.90 | 1.00 | 0.90 | 0.86 | 0.68 | 0.48 | 0.72 | 0.80 | 1.03 | 1.16 | 0.92 | 0.50 | 0.85 |
| 8. 8 | 0.89 | 0.99 | 0.77 | 0.72 | 0.61 | 0.55 | 0.67 | 0.71 | 095 | 1.12 | 0.94 | 0.52 | 0.81 |
| 9. 9 | 0.6.) | 0 72 | 0.44 | 0.40 | 0.37 | 0.45 | 0.45 | 043 | 0.60 | 0.78 | 0.70 | 0.62 | 0.55 |
| 10.10 | 0.24 | 0.26 | -0.01 | $-0.04$ | 0.04 | 0.27 | 0.10 | 0.04 | 0.10 | 0.23 | 0.27 | 0.26 | 0.15 |
| 7. 2, 9 | -0.15 | -0.08 | $-0.01$ | $-0.03$ | 0.03 | 0.05 | 0.13 | -0.03 | -0.06 | $-0.15$ | -0.12 | -0.12 | $-0.05$ |
| 6. 2. 8 | -0 21 | -0.16 | -0.01 | $-0.02$ | 0.01 | -0.07 | 0.04 | -0.06 | -0.08 | $-0.23$ | $-0.23$ | -0.21 | $-0.10$ |
| 6. 2.10 | -0.10 | 0.06 | 0.26 | 0.32 | 0.50 | 0.65 | 0.72 | 0.49 | 0.27 | 0.05 | 0.01 | $-0.04$ | 0.27 |
| 6. 2. 6 | $-0.49$ | $-0.59$ | $-0.49$ | -0.58 | $-0.73$ | $-1.04$ | $-0.57$ | -0.86 | $-0.70$ | -0.74 | -0.61 | -0.51 | -0 65 |
| 7. 2 | -0.52 | -0.46 | -0.40 | $-0.52$ | -0.56 | -0.66 | -0.47 | -0.6. | -0.61 | - 0.59 | -0.42 | $-0.42$ | -0.52 |
| 8. 2 | -0.69 | $-0.76$ | $-0.88$ | $-1.07$ | $-1.19$ | -1.36 | -1.25 | -1.35 | $-1.15$ | - 97 | -0.67 | $-0.60$ | -1.00 |
| 8. 1 | $-0.65$ | $-0.67$ | -0.8 | $-1.06$ | $-1.15$ | $-1.21$ | -1.17 | $-1.30$ | $-1.10$ | $-0.89$ | $-0.5$ | $-0.53$ | -0.93 |
| 7. 1 | $-0.48$ | -0.37 | -0.39 | $-0.51$ | $-0.52$ | $-0.51$ | $-0.40$ | $-0.60$ | -056 | $-9.50$ | $-0.34$ | -0.50 | -0.46 |
| 9.12.3.9 | -0.82 | -102 | -1.17 | -1.32 | -139 | $-1.53$ | -1.60 | -1.62 | $-1.41$ | $-1.32$ | -0 98 | $-0.50$ | -1.25 |
| 7. 2.2(9) | 0.04 | 0.11 | 0.19 | 0.21 | 0.33 | 0.40 | 0.43 | 0.29 | 0.22 | 0.06 | 0.02 | 0.02 | 0.19 |
| Dail.ext. | -0.51 | -0.37 | -0.12 | -0.11 | -0.01 | -0.17 | 0.09 | -0.07 | $-0.28$ | -0.45 | $-0.37$ | -0.40 | -0.25 |

The numbers without sign must be added : those with the sign - must be subtracted.

Italy. - Padua. Lat. $45^{\circ} 24^{\prime}$ N. Long. $11^{\circ} 52^{\prime}$ E. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mom. 1 | 058 | 0.57 | 0.89 | 1.23 | 2.43 | 2.21 | 2.86 | 2.27 | 159 | 0.86 | 1.04 | 0.83 | 1.45 |
| 2 | 0.58 | 0 sl | 1.20 | 1.49 | 2.70 | 2.40 | 3.20 | 2.70 | 1.85 | 1.03 | 1.16 | 0.96 | 1.67 |
| 3 | 0.76 | 097 | 1.42 | 166 | 3.00 | 2.68 | 3.53 | 3.05 | 2.10 | 1.20 | 1.26 | 0.98 | 1.88 |
| 4 | 0.79 | 1.13 | 1.68 | 1.97 | 3.14 | 2.71 | 3.78 | 3.44 | 2.34 | 1.39 | 1.35 | 1.05 | 2.06 |
| 5 | 1.06 | 1.31 | 189 | 2.26 | 2.97 | 2.39 | 3.34 | 3.44 | 2.66 | 1.58 | 1:42 | 1.12 | 2.12 |
| 6 | 1.13 | 1.46 | 2.06 | 2.22 | 1.96 | 1.22 | 2.07 | 2.93 | 2.54 | 154 | 1.49 | 1.16 | 1.82 |
| 7 | 1.25 | 1.58 | 1.86 | 1.82 | 0.66 | 0.08 | 0.56 | 1.82 | 1.78 | 1.37 | 1.58 | 1.23 | 1.30 |
| 8 | 1.07 | 1.42 | 0.66 | 1.03 | -0.23 | -0.65 | -0.25 | 0.58 | 0.79 | 0.81 | 0.97 | 1.00 | 0.60 |
| 9 | 0.70 | 0.82 | 0.61 | 0.18 | -1.07 | -1.24 | $-163$ | -1.65 | -0.58 | 0.18 | 0.02 | 0.33 | -0.28 |
| 10 | 0.10 | -0.08 | -0.s3 | -0.42 | $-1.70$ | -1.66 | -2 29 | -1.90 | -1.03 | -0.51 | -0.81 | -0.26 | -0.95 |
| 11 | -0.58 | -0.62 | -0.87 | -0.85 | -2.: 0 | -2.23 | -2.77 | -2.38 | -1.56 | -0.99 | -1.51 | -1.05 | -1.48 |
| Noor | -0.98 | -1.24 | -1.32 | -1.27 | -2.74 | -2.52 | -3.16 | $-2.97$ | -2.14 | -1.41 | -2.02 | $-1.50$ | -1.94 |
| 1 | -1.3s | -1.45 | -1.54 | -1.68 | -2.88 | -2.61 | -3.53 | -3.34 | -2.54 | -1.74 | -2.42 | -1.90 | -2.25 |
| 2 | -1.51 | -1.62 | -1.74 | -1.92 | -2.94 | -2.62 | -3.74 | -3.73 | -2.84 | -2.01 | -2.53 | -2.06 | -2.44 |
| 3 | -1.45 | -1.65 | -1.90 | -2.14 | $-2.94$ | -2.59 | -3.54 | -3.81 | -2.87 | -2.04 | -2.22 | -1.68 | -2.40 |
| 4 | -1.18 | -1.34 | -1.71 | -2.10 | -2.67 | -2.20 | -2.82 | -3.23 | -2.38 | -1.94 | -1.53 | -1.14 | -2.02 |
| 5 | -0.87 | -0.98 | -1.39 | -1.98 | -2.08 | -1.60 | -2.44 | -2.49 | -1.60 | -1.05 | -0.73 | -0.74 | -1.50 |
| 6 | -0.59 | -0.79 | -1.02 | -1.51 | -1.20 | $-1.00$ | -1.41 | -1.34 | -0.83 | -0.54 | -0.15 | $-0.33$ | -0.89 |
| 7 | -0.32 | -0.62 | -0.73 | -1.12 | -0.26 | -0.12 | -0.46 | -0.32 | -0.18 | -0.14 | 0.12 | -0.15 | -0.36 |
| 8 | -0.07 | -0.42 | -0.43 | -0.47 | -0.14 | 0.38 | 1.01 | 0.50 | -0.10 | 0.05 | 0.33 | 0.04 | 0.06 |
| 9 | 0.05 | -0.14 | -0 | -0.11 | 1.11 | 1.38 | 1.54 | 1.01 | 0.23 | 0.26 | 0.49 | 026 | 0.50 |
| 10 | 0.18 | 0.09 | 0.24 | 0.27 | 1.44 | 1.72 | 1.67 | 1.36 | 0.58 | 0.52 | 0.72 | 0.46 | 0.77 |
| 11 | 0.29 | 0.31 | 0.48 | 0.60 | 1.75 | 1.86 | 2.14 | 1.78 | 0.84 | 0.68 | 0.86 | 0.59 | 1.02 |
| Midn. | 0.37 | 0.49 | 0.72 | 0.85 | 2.02 | 2.10 | 2.43 | 2.23 | 1.36 | 0.78 | 0.94 | 0.70 | 1.25 |
| 6. 6 | 0.27 | 0.34 | 0.52 | 0.36 | 0.38 | 0.11 | 0.33 | 0.80 | 0.86 | 050 | 0.67 | 0.42 | 0.46 |
| 7. 7 | 047 | 0.48 | 0.57 | 0.3 .5 | 0.20 | -0.02 | 0.05 | 0.75 | 0.50 | 0.62 | 0.55 | 0.54 | 0.47 |
| 8. 8 | 0.50 | 0.50 | 0.12 | 0.28 | -0.19 | -0.14 | 0.38 | 0.54 | 0.35 | 0.43 | 0.65 | 0.52 | 0.33 |
| 9. 9 | 0.38 | 0.34 | 0.26 | 0.04 | 0.02 | 0.07 | -0.05 | $-0.32$ | -0.18 | 0.22 | 0.26 | 0.30 | 0.11 |
| 10.10 | 0.14 | 0.01 | -0.30 | -0.08 | -0.13 | 0.03 | -0.31 | -0.27 | -0.23 | 0.01 | -0.05 | 0.10 | -0.09 |
| 7. 2. 9 | -0.07 | -0.06 | 0.01 | -0.07 | -0.39 | -0.39 | -0.5.5 | -0.30 | -0.28 | -0.13 | -0.16 | -0.19 | $-0.21$ |
| 6. 2. | -0.15 | 19 | -0.04 | -0.06 | -0.37 | $-0.34$ | -0.22 | -0.10 | -0.13 | -0.14 | -0.24 | -0.29 | -0.19 |
| 6. 2.10 | -0.0\% | . 22 | 19 | 0.19 | 0.15 | 0.11 | -0.00 | 0.19 | $0 . r 9$ | 002 | -0.11 | -0.15 | 0.05 |
| 6. 2. 6 | -0.32 | -0.32 | -0.23\| | -0.40 | $-0.73$ | -0.80 | $-1.03$ | -0.71 | $-0.38$ | $-0.34$ | -0.40 | -0.41 | -0.51 |
| 7. 2 | -0.13 | -0.02 | 0.06 | -0.05 | -1.14 | -1.27 | $-1.59$ | -0 96 | -0.53 | -0.32 | -049 | -0.42 | -0.57 |
| 8. 2 | -0.22 | -0.10 | -0.54 | -0.45 | -1.59 | -1.64 | -2.00 | -1.58 | -1.03 | -0.60 | -0.79 | -0.53 | $-0.92$ |
| 8. 1 | -0.16 | -0.02 | -0.14 | -0.33 | -1.56 | -1.63 | -1.89 | -1.38 | -0.88 | 0.4 | 0.73 | -0.45 | -0.83 |
| 7. 1 | -007 | 0.07 | 0.16 | 0.07 | -1.11 | -1.27 | -1.49 | $-0.76$ | -0.38 | -0.19 | -0.42 | -0.34 | -0.48 |
| 9.12.ア.9 | $-0.42$ | -0.55 | -0.68 | -0.84 | -1.41 | -1.24 | -1.70 | -1.86 | -1 34 | -0.75 | -0.93 | -0.65 | -1.03 |
| 7. 2.2(9) | -0.04 | -0.08 | -0.02 | -0 08 | -0.02 | 0.06 | -0.03 | 0.13 | -0.15 | -0.03 | -0.00 | -0.08 | -0.04 |
| Dail.ext. | -0. 3 | -0.04 | 0.08 | 0.06 | 0.10 | 0.05 | 002 | -0.19 | -0.11 | -0.23 | -0.49 | -0.42 | -0.16 |

Switzerland. - Geneva. Lat. $46^{\circ} 1 \mathbf{2}^{\prime}$ N. Long. $6^{\circ} 9^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hour. ${ }^{\prime \prime}$ | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.50 | 0.68 | 1.35 | 1.68 | 2.16 | 2.77 | 2.54 | 2.38 | 1.86 | 1.44 | 0.80 | 0.49 | 1.56 |
| 1 | 0.62 | 0.93 | 1.88 | 2.14 | 2.72 | 3.32 | 3.19 | 3.08 | 2.41 | 1.71 | 0.97 | 0.54 | 1.95 |
| 2 | 0.74 | 1.01 | 2.34 | 2.53 | 3.16 | 3.65 | 3.70 | 3.65 | 2.93 | 1.95 | 1.14 | 0.61 | 2.29 |
| 3 | 0.53 | 1.22 | 2.70 | 2.76 | 3.40 | 3.74 | 3.59 | 4.03 | 3.34 | 2.14 | 1.30 | 0.70 | 2.50 |
| 4 | 0.92 | 1.46 | 2.59 | 2.78 | 3.34 | 3.50 | 3.80 | 4.00 | 3.49 | 2.22 | 1.43 | 0.81 | 2.55 |
| 5 | 0.98 | 1.66 | 2.63 | 2.54 | 2.93 | 2.58 | 3.26 | 3.52 | 3.30 | 2.14 | 1.51 | 0.91 | 2.37 |
| 6 | 1.02 | 1.75 | 2.49 | 2.03 | 2.22 | 2.03 | 2.39 | 2.65 | 2.72 | 1.85 | 1.48 | 0.97 | 1.97 |
| 7 | 0.97 | 1.66 | 1.90 | 1.33 | 1.28 | 1.05 | 1.38 | 1.54 | 1.84 | 1.34 | 1.26 | 0.92 | 1.37 |
| S | 0.78 | 1.33 | 1.09 | 0.50 | 0.27 | 0.08 | 0.26 | 0.37 | 0.78 | 0.65 | 0.84 | 0.70 | 0.64 |
| 9 | 0.46 | 0.74 | 0.17 | -0.34 | $-0.69$ | -0.82 | $-0.71$ | $-0.70$ | $-0.30$ | $-0.15$ | 0.23 | 0.34 | $-0.16$ |
| 10 | -0.02 | $-0.01$ | $-0.75$ | $-1.10$ | -1.51 | $-1.57$ | $-1.53$ | -1.53 | $-1.26$ | $-0.98$ | $-0.47$ | $-0.16$ | -0.91 |
| 11 | $-0.57$ | $-0.80$ | -1.61 | $-1.75$ | $-2.17$ | $-2.18$ | $-2.24$ | -2.29 | $-2.06$ | $-1.70$ | -1.14 | $-0.67$ | -1.60 |
| Noon. | $-1.06$ | $-1.49$ | $-2.26$ | $-2.23$ | $-2.66$ | $-2.70$ | $-2.74$ | -2.85 | $-2.66$ | $-2.29$ | $-1.66$ | $-1.10$ | $-2.14$ |
| 1 | $-1.40$ | $-1.95$ | $-2.70$ | $-2.55$ | $-2.95$ | $-3.10$ | -3.18 | $-3.29$ | -3.08 | $-2.53$ | -1.94 | $-1.37$ | -2.51 |
| 2 | $-1.50$ | $-2.18$ | $-2.87$ | $-2.67$ | -3.12 | $-3.35$ | $-3.48$ | $-3.55$ | -3.29 | $-2.55$ | -1.94 | $-1.41$ | -2.66 |
| 3 | $-1.41$ | $-2.10$ | $-2.51$ | $-2.61$ | $-3.07$ | -3.42 | -3.51 | -3.65 | -3.28 | $-2.41$ | $-1.74$ | $-1.26$ | -2.61 |
| 4 | $-1.14$ | -1.82 | -2.54 | -2.37 | $-2.80$ | -3.25 | -3.37 | $-3.43$ | -3.04 | -2.06 | $-1.38$ | $-0.97$ | -2.35 |
| 5 | $-0.79$ | $-1.37$ | $-2.10$ | $-1.9$ | -2.32 | $-2.78$ | $-2.90$ | $-2.92$ | $-2.57$ | $-1.59$ | -0.99 | $-0.64$ | -1.91 |
| 6 | $-0.46$ | $-0.9 .4$ | $-1.59$ | $-1.46$ | -1.70 | -2.11 | $-2.22$ | $-2.15$ | -1.9 | $-1.06$ | $-0.62$ | $-0.32$ | -1.38 |
| 7 | $-0.20$ | -0.51 | $-1.06$ | $-0.90$ | $-1.00$ | -1.29 | $-1.40$ | -1.31 | -1.16 | $-0.53$ | -0.30 | -0.07 | -0.51 |
| 8 | $-0.01$ | $-0.14$ | $-0.54$ | $-0.34$ | $-0.29$ | $-0.12$ | $-0.49$ | -0.46 | $-0.42$ | $-0.02$ | $-0.03$ | 0.11 | $-0.26$ |
| 9 | 0.12 | 0.14 | 0.0.) | 0.20 | 0.38 | 0.47 | 0.34 | 0.32 | 0.26 | 0.42 | 0.20 | 0.24 | 0.26 |
| 10 | 0.2 .5 | 0.37 | 0.42 | 0.70 | 0.91 | 1.30 | 1.10 | 1.02 | 0.83 | 0.82 | 0.42 | 0.34 | 0.71 |
| 11 | 0.37 | 0.54 | 0.90 | 1.20 | 1.51 | 2.07 | 1.57 | 1.70 | 1.35 | 1.15 | 0.62 | 0.41 | 1.14 |
| Mean | $-0.53$ | 1.24 | 3.11 | 6.77 | 10.37 | 13.31 | 14.30 | 13.58 | 11.46 | 7.48 | 3.76 | 0.55 |  |

## Xxxvir.

Switzerland.-Geneva. Lat. $46^{\circ} 12^{\prime}$ N. Long. $6^{\circ} 9^{\prime}$ E. Gr.-Dove.
Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.4 .5 | 0.69 | 1.26 | 1.44 | 1.54 | 1.98 | 2.12 | 1.63 | 1.44 | 0.94 | 0.50 | 0.59 | 1.21 |
| 2 | 0.70 | 0.96 | 2.21 | $2.62{ }^{1}$ | 2.60 | 8.20 | 3.15 | 2.83 | 2.72 | 1.46 | 0.73 | 0.66 | 1.99 |
| 4 | 1.01 | 1.8:3 | 2.91 | 3.36 | 3.11 | 3.55 | 3.82 | 3.51 | $3.26{ }^{\prime}$ | 1.90 | 1.02 | 0.80 | 2.46 |
| 6 | 1.19 | 1.49 | 2.70 | 2.87 | 2.26 | 2.38 | 2.47 | 2.82 | 2.79 | 1.74 | 1.13 | 0.97 | 2.07 |
| S | 1.22 | 1.22 | 1.42 | 0.74 | 0.27 | 0.13 | 0.29 | 0.19 | 0.72 | 0.94 | 0.90 | 0.9 .5 | 0.77 |
| 10 | $-0.02$ | $-0.25$ | $-0.65$ | -1.70 | -1.30 | -1.34 | $-1.25$ | -1.01 | $-1.10$ | $-0.73$ | $-0.26$ | $-0.14$ | $-0.73$ |
| Noon. | $-0.18$ | -1.30 | -1.97 | -2.14 | $-2.42$ | $-2.54$ | $-2.50$ | $-2.34$ | -2.38 | $-1.86$ | $-1.18$ | $-1.22$ | -1.91 |
| 2 | $-1.69$ | $-1.70$ | $-2.82$ | $-2.94$ | -2.97 | -3.09 | -3.11 | -3.17 | -3.03 | -2.3. | -1.5.) | $-1.46$ | $-2.49$ |
| 4 | $-1.30$ | $-1.61$ | $-2.70$ | $-2.94$ | -2. 16 | $-2.87$ | -2.59 | $-3.04$ | -2.86 | $-1.53$ | $-1.19$ | -1.0.5 | $-2.20$ |
| 6 | $-0.54$ | $-0.90$ | $-1.79$ | $-2.06$ | $-1.40$ | $-1.59$ | $-2.24$ | $-2.04$ | -1.74 | -0.88 | $-0.45$ | $-0.43$ | $-1.36$ |
| 8 | -0.09 | $-0.21$ | $-0.89$ | -0.70 | -0.10 | $-0.2 .5$ | $-0.58$ | -0.35 | -0.38 | -0.08 | 0.03 | 0.10 | $-0.29$ |
| 10 | 0.20 | 0.29 | 0.34 | 0.40 | 0.86 | 0.75 | 0.78 | 0.69 | 0.57 | 0.47 | 0.29 | 0.18 | 0.49 |
| Mean | 1.20 | 0.17 | 2.28 | 6.81 | 9.48 | 12.82 | 14.43 | 13.74 | 10.66 | 7.73 | 3.30 | 0.12 |  |

The numbers without sion must be added ; those with the sign - must be subtracted.

Switzerland. - St. Bernard. Lat. $45^{\circ} 52^{\prime}$ N. Long. $9^{\circ} 22^{\prime}$ E. Gr.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Iieaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dee. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.48 | 0.81 | 1.34 | 1.96 | 2.10 | 1.72 | 1.62 | 1.30 | 0.76 | 1.02 | 0.59 | 0.31 | 1.17 |
| 1 | 0.63 | 0.91 | 1.58 | 2.22 | 2.45 | 1.99 | 1.93 | 1.53 | 0.97 | 1.17 | 0.66 | 0.33 | 1.36 |
| 2 | 0.81 | 1.09 | 1.82 | 2.40 | 2.73 | 2.15 | 2.14 | 1.52 | 1.17 | 1.30 | 0.78 | 0.40 | 1.55 |
| 3 | 0.99 | 1.26 | 1.98 | 2.46 | 2.81 | 2.24 | 2.24 | 1.94 | 1.34 | 1.36 | 0.89 | 0.50 | 1.67 |
| 4 | 1.05 | 1.38 | 2.02 | 2.34 | 2.67 | 2.14 | 2.17 | 1.91 | 1.41 | 1.34 | 0.98 | 0.52 | 1.66 |
| 5 | 1.08 | 1.34 | 1.84 | 2.00 | 2.28 | 1.88 | 1.90 | 1.70 | 1.3.5 | 1.19 | 0.98 | 0.66 | 1.52 |
| 6 | 0.91 | 1.14 | 1.42 | 1.45 | 1.72 | 1.42 | 1.44 | 1.34 | 1.14 | 0.92 | 0.86 | 0.62 | 1.20 |
| 7 | 0.60 | 0.74 | 0.79 | 0.70 | 0.51 | 0.81 | 0.82 | 0.76 | 0.77 | 0.5:3 | 0.61 | 0.50 | 0.73 |
| 8 | 0.1 | 0.18 | 0.00 | -0.16 | -0.03 | 0.09 | 0.10 | 0.12 | 0.29 | 0.06 | 0.26 | 0.26 | 0.11 |
| 9 | -0.31 | -0.48 | -0.55 | -1.06 | -1.10 | -0.66 | -0.66 | -0.53 | -0.26 | -0.46 | -0.22 | -0.06 | -0.55 |
| 10 | -0.75 | -1.13 | -1.63 | -1.86 | -1.94 | -1.36 | -1.34 | -1.13 | -0.78 | -0.94 | -0.68 | -0.41 | -1.16 |
| 11 | -1.14 | -1.66 | $-2.23$ | -2.50 | -2.58 | -1.95 | -1.90 | -1.60 | -1.22 | -1.33 | -1.09 | -0.71 | -1.66 |
| Noon. | -1.34 | -1.98 | -2.58 | -2.87 | -2.96 | -2.34 | -2.26 | -1.90 | -1.51 | -1.58 | -1.36 | -0.94 | -1.97 |
| 1 | -1.38 | -2.04 | -2.62 | -2.98 | -3.06 | -2.51 | -2.40 | -2.02 | -1.62 | -1.66 | -1.47 | -1.03 | -2.07 |
| 2 | -1.24 | -1.86 | -2.33 | -2.78 | -2.89 | -2.44 | -2.33 | -1.94 | -1.56 | -1.59 | -1.89 | -0.99 | -1.95 |
| 3 | -0.98 | -1.47 | -1.92 | -2.36 | -2.51 | -2.21 | -2.08 | -1.74 | -1.35 | -1.35 | -1.16 | -0.82 | -1.66 |
| 4 | -0.6.5 | -0.97 | -1.34 | -1.79 | -1.98 | -1.80 | -1.70 | -1.42 | -1.05 | -1.07 | -0.83 | -0.57 | -1.26 |
| 5 | -0.32 | -0.43 | -0.73 | -1.17 | -1.40 | -1.32 | -1.26 | -1.06 | -0.70 | -0.72 | $-0.46$ | -0.27 | -0.82 |
| 6 | -0.0.3 | 0.04 | -0.19 | -0.54 | -0.81 | -0.80 | -0.30 | -0.70 | -0.38 | -0.36 | -0.10 | 0.00 | -0.39 |
| 7 | 0.14 | 0.39 | 0.25 | 0.04 | -0.25 | -0.2s | -0.34 | $-0.34$ | -0.11 | -0.03 | 0.19 | 0.21 | -0.01 |
| 8 | 0.25 | 0.60 | 0.56 | 0.54 | 0.27 | 0.20 | 0.09 | 0.00 | 0.10 | 0.24 | 0.38 | 0.3 .1 | 0.30 |
| 9 | 0.30 | 0.69 | 0.78 | 0.96 | 0.76 | 0.63 | 0.50 | 0.32 | 0.27 | 0.47 | 0.19 | 0.38 | 0.55 |
| 10 | 0.34 | 0.72 | 0.96 | 1.33 | 1.22 | 1.02 | 0.59 | 0.64 | 0.42 | 0.67 | 0.53 | 0.38 | 0.76 |
| 11 | 0.38 | 0.74 | 1.14 | 1.66 | 1.68 | 1.40 | 1.26 | 0.97 | 0.58 | 0.85 | 0.55 | 0.33 | 0.96 |
| Mean. | -8.26 | $-6.62$ | -5.72\| | -2.97 | 0.74 | 3.55 | 4.82 | 4.32 | 2.40 | -0.91 | -3.95 | -5.86 |  |

## SXXIX.

Switzerland. -St. Bernard. Lat. $45^{\circ} 5 \mathfrak{2}^{\prime}$ N. Long. $9^{\circ} \underset{2}{ } \mathfrak{Z}^{\prime}$ E. Gr. - Dove.
Degrees of Reaumur.

| Hour. | Jan. | Fet. | Ma | Alril. | May. | June. | July | Aug. | pt. |  | Nor. |  | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.34 | 0.55 | 0.75 | 1.19 | 1.26 | 1.39 | 1.02 | 1.08 | 0.81 | 0.66 | 0.33 | 0.25 | 0.80 |
| 2 | 0.52 | 0.75 | 1.14 | 1.64 | 1.75 | 1.88 | 1.62 | 1.53 | 1.16 | 0.94 | 0.12 | 0.27 | 1.14 |
| 4 | 0.82 | 06 | 50 | St | 1.91 | 1.98 | 1.52 | 1.71 | 1.34 | . 1 | 0.65 | 0.4 | 1.35 |
| 6 | 6. | . 6 | 20 | 1.50 | 1.53 | 1.46 | 1.46 | 1.27 | 0.98 | 0.88 | 0.50 | . 32 | 1.05 |
| 8 | 0.48 | 0.26 | 0.14 | -0.03 | -0.25 | 0.01 | 0.22 | 0.16 | 0.05 | 0.29 | 0.27 | 0.15 | 0.14 |
| 10 | -0.35 | -0.91 | -1.06 | -1.26 | -1.39 | -1.18 | -1.11 | -0.9 | O. 8 | 0.6 | -0.54 | -0.23 | -0.88 |
| Nuon | -1 | -1.66 | -1.74 | -2 | -2.15 | -1.92 | -1.81 | -1.77 | -1.58 | 1.45 | -1.26 | -0.91 | 1.65 |
| 2 | -1.37 | -1.5.5 | -1.89 | -2.12 | -2.12 | -2.23 | -2.01 | -1 97 | -1.54 | -1.52 | -1.23 | -1.22 | $-1.73$ |
| 4 | -0. | -0.71 | -1.14 | -1.5.) | -1.47 | -1.65 | -1.49 | -1.30 | -0.8 | -0.86 | -0.37 | -0.02 | $-0.99$ |
| 6 | 09 | 0.17 | 09 | -0.26 | -0.3.5 | -0.71 | -0.57 | -0.46 | -0.26 | -0.07 | 0.0 | 0.22 | -0.17 |
| 8 | 0.25 | 0.44 | 0.49 | . 49 | . 50 | . 35 | . 30 | . 2 | 0.26 | 0.2 | 0.70 | 0.30 | 0.35 |
| 10 | 37 | 0.55 | 0.55 | 0.71 | 0.76 | 0.64 | 0.56 | 0.43 | 0.46 | 0.43 | 0.40 | 0.40 | 0.52 |
| Mea | -6.0 | -8.83 | -6 | -3. | -0. | 2.71 | 4.82 | 1.70 | 2.07 | -0.36 | -5.46 | -6.18 |  |

The numbers without sign must be added; those with the sigu - must be subtracted.

Austria. - Kremsmünster. Lat. $48^{\circ} 3^{\prime}$ N. Long. $14^{\circ} 7^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Ang. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.58 | 0.90 | 1.05 | 1.14 | 2.30 | 2.77 | 1.86 | 1.94 | 1.52 | 1.26 | 0.61 | 0.40 | 1.36 |
| 2 | 0.66 | 1.03 | 1.30 | 1.36 | 2.66 | 3.08 | 2.16 | 2.26 | 1.94 | 1.58 | 0.72 | 0.42 | 1.60 |
| 3 | 0.71 | 1.07 | 1.57 | 1.63 | 2.84 | 3.14 | 2.35 | 2.50 | 2.32 | 1.82 | 0.78 | 0.42 | 1.76 |
| 4 | 0.78 | 1.12 | 1.50 | 1.88 | 2.78 | 2.90 | 2.34 | 2.54 | 2.58 | 1.97 | 0.83 | 0.42 | 1.83 |
| 5 | 0.84 | 1.19 | 1.90 | 1.99 | 2.44 | 2.32 | 2.08 | 2.30 | 2.60 | 1.98 | 0.88 | 0.46 | 1.75 |
| 6 | 0.88 | 1.24 | 1.82 | 1.88 | 1.86 | 1.54 | 1.54 | 1.80 | 2.34 | 1.91 | 0.93 | 0.54 | 1.52 |
| 7 | 0.84 | 1.26 | 1.50 | 1.41 | 1.11 | 0.68 | 0.94 | 1.11 | 1.81 | 1.63 | 0.92 | 0.59 | 1.15 |
| 8 | 0.67 | 1.07 | 0.96 | 0.87 | 0.31 | $-0.15$ | 0.23 | 0.35 | 1.09 | 1.21 | 0.80 | 0.56 | 0.66 |
| 9 | 0.35 | 0.67 | 0.30 | 0.14 | -0.45 | $-0.86$ | $-0.42$ | -0.37 | 0.28 | 0.62 | 0.51 | 0.38 | 0.10 |
| 10 | $-0.10$ | 0.01 | $-0.41$ | $-0.58$ | -1.10 | $-1.42$ | -0.9. | $-0.98$ | $-0.52$ | $-0.13$ | 0.06 | 0.05 | $-0.56$ |
| 11 | -0.58 | $-0.72$ | $-1.06$ | $-1.20$ | -1.65 | -1.84 | -1.39 | $-1.47$ | $-1.23$ | $-0.92$ | $-0.47$ | $-0.38$ | $-1.08$ |
| No | -0.98 | $-1.37$ | $-1.56$ | $-1.65$ | -2.09 | -2.17 | -1.75 | -1.86 | $-1.81$ | $-1.68$ | $-0.97$ | $-0.78$ | $-1.36$ |
| 1 | $-1.22$ | -1.78 | -1. 89 | -1.93 | $-2.42$ | $-2.42$ | -2.05 | -2.21 | $-2.28$ | $-2.25$ | $-1.30$ | -1.03 | $-1.90$ |
| 2 | -1.26 | $-1.90$ | $-2.02$ | $-2.06$ | $-2.62$ | -2.58 | $-2.26$ | $-2.38$ | $-2.56$ | $-2.53$ | $-1.40$ | -1.09 | $-2.05$ |
| 3 | -1.12 | -1.69 | $-1.99$ | $-2.04$ | $-2.67$ | $-2.62$ | $-2.33$ | $-2.46$ | $-2.65$ | -2.49 | $-1.28$ | $-0.94$ | $-2.02$ |
| 4 | $-0.86$ | -1.32 | $-1.79$ | $-1.89$ | $-2.51$ | $-2.49$ | $-2.22$ | $-2.34$ | $-2.52$ | $-2.17$ | $-1.01$ | -0.66 | $-1.98$ |
| 5 | $-0.59$ | $-0.92$ | $-1.48$ | $-1.60$ | -2.15 | -2.16 | -1.88 | $-2.00$ | -2.18 | -1.69 | $-0.68$ | $-0.35$ | $-1.47$ |
| 6 | -0.35 | $-0.57$ | -1.08 | $-1.18$ | $-1.62$ | $-1.66$ | $-1.38$ | $-1.49$ | $-1.66$ | -1.14 | $-0.41$ | $-0.11$ | $-1.05$ |
| 7 | $-0.18$ | $-0.36$ | -0.65 | -0.68 | $-0.98$ | $-1.03$ | $-0.76$ | $-0.86$ | -1.05 | $-0.66$ | $-0.22$ | 0.02 | $-0.62$ |
| 8 | -0.04 | $-0.19$ | $-0.23$ | -0.17 | $-0.34$ | $-0.35$ | -0.15 | -0.24 | $-0.46$ | $-0.26$ | $-0.11$ | 0.09 | $-0.20$ |
| 9 | 0.07 | $-0.02$ | 0.13 | 0.28 | 0.28 | 0.34 | 0.38 | 0.30 | 0.05 | 0.06 | $-0.02$ | 0.12 | 0.16 |
| 10 | 0.20 | 0.18 | 0.42 | 0.61 | 0.84 | 1.02 | 0.82 | 0.76 | 0.46 | 0.34 | 0.11 | 0.18 | 0.49 |
| 11 | 0.34 | 0.46 | 0.63 | 0.82 | 1.36 | 1.65 | 1.19 | 1.15 | 0.80 | 0.63 | 0.27 | 0.25 | 0.50 |
| Midn. | 0.47 | 0.70 | 0.83 | 0.97 | 1.8 | 2.27 | 1.52 | 1.53 | 1.14 | 0.94 | 0.46 | 0.34 | 1.08 |
| 6. 6 | 0.27 | 0.34 | 0.37 | 0.35 | 0.12 | -0.06 | 0.08 | 0.16 | 0.34 | 0.39 | 0.26 | 0.22 | 0.24 |
| 7. 7 | 0.33 | 0.45 | 0.43 | 0.37 | 0.07 | -0.18 | 0.09 | 0.13 | 0.38 | 0.48 | 0.35 | 0.29 | 0.27 |
| 8. 8 | 0.32 | 0.44 | 0.37 | 0.35 | -0.02 | $-0.10$ | 0.04 | $0.1) 6$ | 0.32 | 0.48 | 0.35 | 0.24 | 0.24 |
| 9. 9 | 0.21 | 0.33 | 0.22 | 0.21 | -0.09 | $-0.26$ | -0.02 | - f .04 | 0.17 | 0.34 | 0.25 | 0.2 .5 | 0.13 |
| 10.10 | 0.05 | 0.10 | 0.01 | 0.02 | $-0.13$ | $-0.20$ | $-0.07$ | 1.11 | $-0.03$ | 0.11 | 0.09 | 0.12 | 0.00 |
| 7. 2. 9 | -0.12 | -0.22 | $-0.13$ | $-0.12$ | -0.41 | $-0.52$ | $-0.31$ | -0.32 | -0.23 | -0.28 | -0.17 | -0.16 | $-0.25$ |
| 6. 2. 8 | -0.14 | -0.28 | $-0.14$ | $-0.12$ | $-0.37$ | $-0.46$ | -0.29 | $-0.27$ | $-0.23$ | $-0.29$ | -0.19 | $-0.15$ | -0.24 |
| 6. 2.10 | -0.06 | -0.16 | 0.07 | 0.14 | 0.03 | $-0.01$ | 0.03 | 0.06 | 0.08 | $-0.09$ | $-0.12$ | $-0.12$ | $-0.01$ |
| 6. 2. 6 | -0.24 | $-0.41$ | $-0.43$ | -0.45 | -0.79 | $-0.90$ | -0.70 | -0.69 | $-0.63$ | -0.94 | $-0.36$ | -0.15 | $-0.56$ |
| 7. 2 | -0.21 | $-0.32$ | $-0.26$ | $-0.33$ | $-0.76$ | -0.95 | $-0.66$ | $-0.63$ | -0.3S | -0.45 | $-0.24$ | -0.25 | $-0.45$ |
| 8. 2 | -0.30 | $-0.42$ | $-0.53$ | $-0.60$ | -1.16 | -1.22 | $-1.02$ | -1.02 | $-0.74$ | $-0.66$ | $-0.30$ | $-0.27$ | -0.69 |
| 8. 1 | -0.28 | -0.36 | $-0.47$ | $-0.53$ | -1.06 | -1.14 | -0.91 | -0.93 | $-0.60$ | $-0.52$ | $-0.25$ | $-0.24$ | -0.61 |
| 7. 1 | $-0.19$ | -0.26 | $-0.20$ | $-0.26$ | $-0.66$ | $-0.87$ | $-0.56$ | $-0.55$ | $-0.24$ | $-0.31$ | $-0.19$ | -0.22 | -0.38 |
| 9.12.3.9 | $-0.42$ | $-0.60$ | $-0.78$ | -0.82 | -1.2 | -1. | -1.03 | $-1.10$ | -1.03 | -0.87 | $-0.44$ | -0.31 | $-0.83$ |
| 7. $2.2(9)$ | $-0.07$ | $-0.17$ | -0.07 | $-0.02$ | -0.24 | -0.31 | -0.15 | -0.17 | $-0.14$ | $-0.19$ | -0.13 | $-0.07$ | -0.14 |
| Dail.ext. | -0.19 | $-0.32$ | -0.06 | -0.04 | 0.09 | 0.36 | 0.01 | 0.04 | $-0.03$ | -0.28 | -0.24 | $-0.25$ | -0.08 |

The numbers without sign must be added : those with the sign - must be subtracted.

Austria.- Salzburg. Lat. $47^{\circ} 48^{\prime}$ N. Long. $13^{\circ} 1^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Ifour. | Jan. | Feb. | March. | Aprit. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.54 | 0.70 | 1.06 | 1.31 | 2.03 | 2.07 | 1.87 | 1.57 | 1.21 | 1.02 | 0.48 | ct 2 | 1.19 |
| 1 | 0.59 | 0.79 | 1.29 | 1.58 | 2.37 | 2.27 | 2.13 | 1.81 | 1.45 | 1.15 | 0.65 | 0.50 | . 38 |
| 2 | 0.72 | 0.97 | 0.51 | 1.79 | 2.64 | 2.56 | 2.36 | 2.05 | 1.61 | 1.27 | 0.81 | 0.59 | 1.49 |
| 3 | 0.82 | 1.08 | 1.75 | 2.04 | 2.90 | 2.73 | , 2.64 | 2.24 | 1.87 | 1.41 | 0.88 | 0.70 | 1.75 |
| 4 | 0.96 | 1.09 | 1.89 | 2.21 | 3.10 | 2.82 | 2.62 | 2.23 | 2.04 | 1.52 | 0.91 | 0.69 | 1.84 |
| 5 | 1.03 | 1.25 | 2.01 | 2.37 | 3.10 | 2.75 | 2.59 | 2.24 | 2.14 | 1.72 | 1.03 | 0.81 | 1.92 |
| 6 | 1.06 | 1.3 | 2.14 | 2.28 | 2.76 | 2. | 2.31 | 2.26 | 2.18 | 1.77 | 1.03 | 0.87 | 1.57 |
| 7 | 1.09 | 1.36 | 2.06 | 1.86 | 1.8 | 1.53 | 1.61 | 1.74 | 1.94 | 1.74 | 1.06 | 0.94 | 1.57 |
| 8 | 1.12 | 1.24 | 1.58 | 1.06 | 0.84 | 0.63 | 0.67 | 0.89 | 1.15 | 1.26 | 1.07 | 1.00 | 1.04 |
| 9 | 0.91 | 0.75 | 0.76 | 0.14 | -0.10 | -0.25 | 0.20 | 0.04 | 0.33 | 0.48 | 0.64 | 0.74 | 0.39 |
| 10 | 0.38 | 0.04 | -0.06 | -0.67 | -0.92 | -1.10 | -0.97 | -0.76 | -0.53 | -0.35 | 0.06 | 0.21 | -0.39 |
| 11 | -0.26 | -0.62 | -0.96 | -1.39 | -1.80 | $-1.87$ | -1.63 | -1.40 | -1.25 | -1.17 | -0.62 | -0.35 | -1.11 |
| Noon | -0.90 | -1.19 | -1.75 | -1.99 | -2.36 | -2.90 | -2.1 | -2.13 | -2.00 | -1.54 | -1.25 | -0.93 | -1.78 |
| 1 | -1.47 | -1.68 | -2.26 | -2.48 | -2.82 | -2.8 | -2.59 | -2.59 | -1.48 | -2.39 | -1.68 | -1.47 | -2.15 |
| 2 | -1.70 | -1.96 | -2.55 | -2.74 | -3.08 | -3.03 | -2.77 | -2.73 | -2.71 | -2.55 | -1.85 | -1.64 | -2.44 |
| 3 | -1.65 | -2.04 | -2.61 | -2.74 | -3.21 | -3.04 | -2.90 | -2.75 | -2.67 | -2.51 | -1.75 | -1.55 | -2.45 |
| 4 | -1.40 | -1.80 | -2.55 | -2.60 | -3.27 | -3.00 | -2.90 | -2.85 | -2.56 | -2.21 | -1.37 | -1.19 | -2.31 |
| 5 | -1.00 | $-1.46$ | -2.26 | -2.10 | -2.97 | -2.64 | -2.64 | -2.46 | -2.09 | -1.63 | -0.85 | -0.72 | $-1.90$ |
| 6 | -0.60 | -0.76 | -1.51 | -1.52 | -2.27 | -2.10 | -2.05 | -1.78 | -1.31 | -0.83 | -0.35 | -0.42 | -1.29 |
| 7 | -0.31 | -0.27 | -0.76 | -0.75 | -1.43 | -1.21 | -1.24 | -0.55 | -0.48 | -0.29 | -0.10 | -0.15 | -0.65 |
| 8 | -0.25 | -0.02 | $-0.16$ | -0.07 | -0.43 | -0.13 | -0.24 | 0.06 | 0.15 | 0.16 | 0.11 | 0.04 | -0.06 |
| 9 | -0.04 | 0.20 | 0.17 | 0.51 | 0.48 | 0.71 | 0.67 | 0.70 | 0.50 | 0.48 | 0.24 | 0.17 | 0.40 |
| 10 | 0.12 | 0.43 | 0.46 | 0.81 | 1.03 | 1.41 | 1.22 | 1.09 | 0.78 | 0.76 | 0.34 | 0.33 | 0.73 |
| 11 | 0.28 | 0.53 | 0.76 | 1.08 | 1.50 | 1.70 | 1.56 | 1.38 | 0.76 | 1.03 | 0.52 | 0.41 | 0.96 |
| Mean. | -2 71 | 1.14 | 2.49 | 6.90 | 10.42 | 13.22 | 13.93 | 13.66 | 10.30 | 7.37 | 1.52 | 1.63 |  |

## XLII.

Germany. - Munich. Lat, $48^{\circ} 9^{\prime}$ N. Long. $11^{\circ} 37^{\prime}$ E. Greenw. - Dove.
Degrees of Reaumur.

| Hour | Jan. | Feb. | March. | April. | M y. | June | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Midn. | 0.71 | 0.92 | 1.54 | 2.27 | 2.68 | 2.49 | 2.84 | 2.37 | 2.17 | 1.53 | 0.91 | 0.46 | 1.73 |
| 1 | 0.90 | 1.04 | 1.83 | 2.37 | 3.02 | 3.06 | 3.27 | 2.64 | 2.33 | 1.59 | 0.87 | 0.58 | 1.96 |
| 2 | 0.97 | 1.18 | 2.04 | 2.62 | 3.30 | 3.39 | 3.56 | 2.94 | 2.61 | 1.67 | 0.94 | 0.67 | 2.16 |
| 3 | 1.04 | 1.30 | 2.16 | 2.89 | 3.61 | 3.66 | 3.80 | 3.19 | 2.81 | 1.78 | 1.00 | 0.77 | 2.33 |
| 4 | 1.03 | 1.33 | 2.25 | 3.12 | 3.85 | 3.82 | 4.05 | 3.41 | 2.98 | 1.91 | 1.04 | 0.85 | 2.47 |
| 5 | 1.07 | 1.43 | 2.37 | 3.29 | 3.69 | 3.25 | 3.71 | 3.50 | 3.16 | 2.01 | 1.12 | 0.92 | 2.46 |
| 6 | 1.14 | 1.52 | 2.56 | 2.93 | 2.61 | 211 | 2.41 | 2.79 | 3.08 | 2.14 | 113 | 0.99 | 2.12 |
| 7 | 1.17 | 1.55 | 2.17 | 1.50 | 1.21 | 0.77 | 0.93 | 1.48 | 2.22 | 1.84 | 1.13 | 0.97 | 1.44 |
| 8 | 1.10 | 1.14 | 1.14 | 0.36 | -0.07 | -0.35 | -0.28 | 0.18 | 0.59 | 0.99 | 0.75 | 0.88 | 0.54 |
| 9 | 0.46 | 0.36 | -0.11 | -0.79 | -1.00 | -1.21 | -1.25 | -1.05 | -0.74 | -0.24 | 0.06 | 0.41 | -0.42 |
| 10 | -0.72 | -0.61 | -1.18 | -1.80 | -1.99 | -1.96 | -2.12 | -1.88 | -1.70 | -1.34 | -0.79 | -0.42 | -1.38 |
| 11 | -1.06 | -1.46 | -2.04 | -2.39 | -2.59 | -2.69 | -2.66 | -2.58 | -2.61 | -2.19 | -1.49 | -0.97 | -2.06 |

The numbers without sigu must be added ; those with the sign - must be subtracted.

## Germany. - Munich, Contimued.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Itour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Noon | -1.70 | -1.93 | -2.67 | -2.99 | -3.28 | -2.98 | -3.14 | -3.09 | -3.18 | -2.69 | -1.94 | -1.02 | -2.55 |
| 1 | -2.03 | -2.31 | -3.01 | -3.27 | -3.59 | -3.41 | -3.48 | -3.55 | -3.58 | -3.08 | -2.23 | -1.83 | $-2.95$ |
| 2 | -2.15 | -2.40 | -3.24 | -3.60 | -3.77 | -3.79 | -3.75 | -3.72 | -3.74 | -3.15 | -2.05 | -1.85 | -3.10 |
| 3 | -1.83 | -2.15 | -3.17 | -3.45 | -3.77 | -3.54 | -3.83 | -3.58 | -3.56 | -2.87 | -1.75 | -1.43 | -2.91 |
| 4 | -1.08 | -1.67 | -2.64 | -3.15 | $-3.41$ | -3.34 | -3.49 | -3.30 | -3.24 | -2.27 | -1.02 | -0.76 | -2.45 |
| 5 | -0.46 | -0.95 | -1.98 | $-2.51$ | -2.87 | -2.80 | -3.07 | -2.76 | -2.56 | -1.27 | -0.43 | -0.34 | 83 |
| 6 | -0.1 | -0.37 | -0.94 | -1.53 | -2.05 | -1.94 | -2.32 | $-1.81$ | -1.29 | -0.44 | -0.12 | -0.13 | -1.09 |
| 7 | 0.04 | -0.07 | -0.20 | -0.36 | -0.74 | -0.84 | -2.99 | -0.47 | -0.30 | 0.08 | 0.20 | 0.06 | -0.47 |
| 8 | 0.23 | 0.22 | 0.28 | 0.40 | 0.41 | 0.61 | 0.40 | 0.55 | 0.37 | 0.56 | 0.44 | 0.14 | 0.38 |
| 9 | 0.39 | 0.45 | 0.55 | 0.91 | 1.13 | 1.35 | 1.20 | 1.15 | 0.93 | 0.88 | 0.57 | 0.23 | 0.81 |
| 10 | 0.49 | 0.59 | 1.02 | 1.31 | 1.65 | 1.86 | 1.87 | 1.60 | 1.40 | 1.14 | 0.74 | 0.33 | 1.17 |
| 11 | 0.61 | 0.77 | 1.33 | 1.69 | 2.18 | 2.28 | 2.41 | 2.06 | 1.80 | 1.34 | 0.85 | 0.40 | 1.48 |
| Mean. | -2.15 | -0.12 | 0.75 | 5.57 | 9.29 | 12.74 | 13.65 | 12.93 | 9.45 | 6.25 | 1.55 | -1.28 |  |

## XLIII.

Bohemia.-Prague. Lat. $50^{\circ} 5^{\prime}$ N. Long. $14^{\circ} 25^{\prime}$ E. Greenu.-Dove. Degrees of Reaumur.

| Itour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug | Sept | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn | 0.30 | . 52 | 1.03 | 1.47 | 1.70 | 1.68 | 1.72 | 1.17 | 1.23 | 0.84 | 0.36 | 0.25 | 1.02 |
| 1 | 0.40 | 0.60 | 1.14 | 1.68 | 1.97 | 1.97 | 2.05 | 1.78 | 1.49 | 1.02 | 0.45 | 0.32 | 1.24 |
| 2 | 0.50 | 0.71 | 1.29 | 1.95 | 2.25 | 2.23 | 2.34 | 2.10 | 1.72 | 1.19 | 0.54 | 0.39 | . 43 |
| 3 | 0.55 | 0.63 | 44 | 2.17 | 2.46 | 2.17 | 2.60 | 2.35 | . 96 | 1.81 | 0.61 | 0.50 | . 61 |
| 4 | 0.65 | . 89 | 1.60 | 2.39 | 2.75 | 2.71 | 2.91 | 2.63 | 2.19 | 1.49 | 0.70 | 0.56 | 1.79 |
| 5 | 0.71 | 0.99 | 1.72 | 2.64 | 2.96 | 2.86 | 3.07 | 2.88 | 2.43 | 1.65 | 0.77 | 0.65 | 1.94 |
| 6 | 0.77 | 1.00 | 1.81 | 2.75 | 2.96 | .71 | 2.92 | 2.93 | 2.61 | 1.73 | 2 | 2 | 8 |
| 7 | 0.68 | 0.99 | 1.53 | 2.32 | 2.11 | 1.88 | 2.13 | 2.34 | 2.29 | 1.65 | 0.79 | 0.73 | 1.62 |
| 8 | 0.73 | . 58 | 1.28 | 1.29 | 0.98 | 0.82 | 1.02 | 1.30 | 1.62 | 1.29 | 0.66 | 0.70 | 1.05 |
| 9 | 0.62 | 0.57 | 0.63 | 0.32 | 0.06 | -0.14 | 0.17 | 0.21 | 0.60 | 0.70 | 0.41 | 0.54 | 0.39 |
| 10 | 0.26 | 0.15 | -0.11 | -0.53 | -0.91 | -0.93 | -0.95 | -0.77 | -0.51 | -0.10 | -0.12 | 0.17 | -0.36 |
| 11 | -0.16 | -0.45 | -0.77 | -1.51 | -1.60 | -1.58 | -1.62 | -1.50 | -1.46 | -0.86 | -0.46 | -0.22 | -1.02 |
| Noon | -0 | -0 | -1.37 | - | - | - | - | -2.18 | -2.02 | -1. | -0. | -0.65 | -1.55 |
| 1 | -0.93 | -1.27 | -1.83 | -2.4 | -2.56 | -2.15 | -2.59 | -2.61 | -2.56 | -2.0 | -1.13 | -0.95 | -1.95 |
| 2 | -1.10 | $-1.50$ | -2.20 | $-2.74$ | -2.80 | -2.73 | -2.83 | -2.69 | -2.84 | . 3 | 1.2.) | 1.07 | -2.19 |
| 3 | -1.11 | $-1.51$ | -2.29 | -2.85 | -2.90 | -2.79 | -2.93 | -3.01 | -2.96 | 2.8 | 1.28 | 0.99 | $-2.25$ |
| 4 | -0.93 | -1.35 | -2.20 | -2.76 | -2.92 | -2.71 | -2.92 | -2.55 | -2.78 | -2.10 | -0.87 | -0.79 | -2.09 |
| 5 | -0.63 | -0.97 | -1.83 | -2.46 | -2.53 | -2.56 | -2.83 | -2.66 | -2.35 | -1.58 | -0.62 | 0.55 | ¢ |
| 6 | -0.44 | -0.61 | -1.26 | -1.9 | -2.17 | -2.10 | -2.36 | -2.11 | -1.64 | -1.01 | -0.36 | -0.37 | -1.36 |
| 7 | -0.31 | -0.32 | -0.70 | -1.12 | -1.49 | -1.37 | -1.59 | -1.23 | -0.87 | -0.5 4 | -0.19 | -0.21 | -0.83 |
| 8 | -0.23 | $-0.06$ | -0.24 | -0.33 | -0.51 | -0.39 | -0.58 | -0.34 | -0.24 | -0.10 | 0.01 | -0.19 | -0.25 |
| 9 | 0.01 | 0.12 | 0.09 | 0.20 | 0.27 | 0.30 | 0.22 | 0.20 | 0.27 | 0.23 | 0.16 | 0.06 | 0.18 |
| 10 | 0.10 | 0.26 | 0.40 | 0.72 | 0.50 | 0.91 | 0.90 | 0.81 | 0.74 | 0.51 | 0.29 | 0.16 | 0.55 |
| 11 | 0.19 | 0.39 | 0.66 | 1.12 | 1.24 | 1.28 | 1.32 | 1.20 | 1.08 | 0.85 | 0.4:3 | 0.25 | 0.83 |
| Mean. | -1.69 | 0.61 | 2.20 | 7.27 | 11.27 | 14.47 | 15.66 | 15.01 | 11.52 | 7.91 | 3.82 | -0.12 |  |

The numbers without sign must be added ; those with the sign - must be subtracted.

Bohemia. - Prague. Lat. $50^{\circ} 5^{\prime}$ N. Long. $14^{\circ} 24^{\prime}$ E. Greenv.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | Juty. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.45 | 0.76 | 0.86 | 1.73 | 1.47 | 1.90 | 1.93 | 1.59 | 1.46 | 1.06 | 0.73 | 0.45 | 1.20 |
| 2 | 0.52 | 0.85 | 1.05 | 2.06 | 1.77 | 2.22 | 2.24 | 1.8.) | 1.69 | 1.18 | 0.79 | 0.52 | 1.40 |
| 3 | 0.54 | 0.98 | 1.24 | 245 | 2.08 | 2.62 | 2.36 | 2.04 | 1.85 | 1.23 | 0.82 | 0.54 | 1.56 |
| 4 | 0.53 | 1.06 | 1.42 | 2.82 | 2.31 | 3.02 | 2.27 | 2.10 | 1.95 | 1.24 | 0.78 | 0.55 | 1.67 |
| 5 | 0.50 | 1.14 | 1.55 | 3.02 | 2.35 | 3.22 | 2.01 | 2.01 | 1.97 | 1.22 | 0.78 | 0.60 | 1.70 |
| 6 | 0.49 | 1.15 | 1.60 | 2.92 | 2.12 | 3.03 | 1.62 | 1.76 | 1.90 | 1.19 | 0.50 | 0.70 | 1.61 |
| 7 | 0.47 | 1.09 | 1.51 | 2.43 | 1.62 | 2.40 | 1.16 | 1.36 | 1.69 | 1.10 | 0.77 | 0.80 | 1.37 |
| 8 | 0.42 | 0.91 | 1.24 | 1.59 | 0.92 | 1.40 | 0.66 | 0.83 | 1.28 | 0.90 | 0.69 | 0.82 | 0.97 |
| 9 | 0.29 | 0.55 | 0.77 | 0.53 | 0.15 | 0.24 | 0.10 | 0.19 | 0.64 | 0.51 | 0.42 | 0.67 | 0.42 |
| 10 | 0.08 | -1.01 | 0.16 | -0.56 | -0.57 | -0.85 | -0.52 | -0.51 | -0.20 | -0.07 | -0.02 | 0.31 | -0.31 |
| 11 | -0.2 | 1.19 | -0.52 | -1.52 | -1.16 | -1.68 | -1.19 | -1.23 | -1.14 | -0.78 | -0.55 | -1.18 | -0.95 |
| Noon. | -0.52 | 1.10 | -1.16 | -2.25 | -1.60 | -2.23 | -1.84 | -1.86 | -2.00 | -1.47 | $-1.10$ | -0.70 | -1.49 |
| 1 | -0 | -1.51 |  |  |  | -2.55 | -2.37 | - |  | 99 | -1.47 | 1.08 | -1.91 |
| 2 | -0. | 0 | 9 | -3.00 | -2.14 | -2.76 | -2.66 | -2.57 | 9 | -2.21 | -1.58 | 1.23 | -2.13 |
| 3 | -0.85 | 64 | -1.92 | -3.08 | -2.26 | -2.92 | -2.65 | -2.53 | -2.76 | -2.08 | -1.44 | . 13 | -2.11 |
| 4 | -0.71 |  | 5 | -2.97 | -2.26 | -2.98 | -2.36 | -2.23 | . 31 | . 68 | -1.08 | -0.87 | -1.88 |
| 5 | -0.5 | -1.0.5 | -1.45 | 5 | $-2.05$ | - | 6 | . 75 | 70 | 14 | -0.67 | -0.56 | -1.52 |
| 6 | -0.31 | 66 | 10 | -2.13 | 1 | -2.45 | -1.28 | -1.18 | 1.07 | . 60 | -0.31 | -0.31 | -1.09 |
| 7 | -0.16 | 34 | -0.73 | - | -1.17 | -1.75 | -0.73 | -0.62 | -0.52 | -0.17 | -0.04 | -0.17 | -0.65 |
| 8 | -0.06 | -0.09 | -0.40 | -0.64 | -0.56 | -0.85 | -0.24 | -0.12 | -0.08 | 0.13 | 0.10 | -0.11 | -0.24 |
| 9 | 0.02 | 0.11 | 10 | 0.11 | 0.03 | 0.06 | 0.19 | 0.30 | 0.26 | 0.34 | 0.20 | 0.07 | 0.12 |
| 10 | 0.11 | 5 | 18 | 0.71 | 0.52 | 0.81 | 0.61 | 0.65 | 0.57 | 0.51 | 0.32 | 0.01 | 0.53 |
| 11 | 0.22 |  | 0. | . 15 | 0.89 | 1.32 | 1.05 | 0.97 | 0.87 | 0.70 | 0.44 | 0.14 | 0.77 |
| Midn. | 0.34 | 061 | 0.65 | 1.46 | 1.18 | 1.64 | 1.51 | 1.28 | 1.17 | 0.89 | 0.61 | 0.31 | 0.97 |
| 6. 6 | 0.09 | 0.24 | 0.25 | 0.40 | 0.21 | 0.29 | 0.17 | 0.29 | 0.42 | 0.29 | 0.25 | 0.19 | 0.26 |
| 7. 7 | 0.15 | 0.35 | 0.39 | 0.50 | 0.22 | 0.33 | 0.22 | 0.37 | 0.59 | 0.47 | 0.37 | 0.32 | 0.36 |
| 8. 8 | 0.18 | 0.41 | 0.42 | . 47 | . 18 | 0.27 | 0.21 | 0.36 | 0.60 | 0.51 | 0.39 | 0.35 | 0.36 |
| 9. 9 | 0.16 | 3 | 0.34 | 0.32 | 0.90 | 0.15 | 0.15 | 0.25 | 0.45 | 0.42 | 0.31 | 0.30 | 0.27 |
| 10.10 | 0.09 | 0.17 | 0.17 | 0.08 | -0.03 | -0.02 | 0.04 | 0.07 | 0.18 | 0.22 | 0.15 | 0.16 | 0.11 |
| 7. 2. 9 | -0.13 | -0.17 | -0.16 | -0.15 | -0.16 | -0.10 | -0.44 | -0.30 | . 31 | -0.26 | -0.2 | 0.17 | -0.21 |
| 6. 2.8 | -0.15 | -0.21 | -0.23 | -0.24 | -0.19 | -0.19 | -0. | -0.31 | $-0.36$ | -0.30 | -0.23 | -0.21 | -0.25 |
| 6. 2.10 | -0.09 | 0.27 | -0.04 | 0.21 | 0.17 | 0.36 | -0.14 | -0.05 | -0.1 | -0.17 | 0.15 | -0.17 | 0.01 |
| 6. 2. 6 | $-0.23$ | -0.40 | -0 46 |  | -0.58 | -0.73 | -0.77 | -0.66 | -0.69 | -0.54 | -0.36 | -0.28 | $-0.54$ |
| 7. 2 | -0.2 | 31 | -0.19 | -0.29 | -0.26 | -0.18 | -0.75 | . 61 | . 60 | 0.56 | -0.41 | -0.22 | -0.38 |
| 8. | -0 |  | . 33 | - | -0.61 | -0 68 | -1.00 | 0.87 | . 81 | -0.66 | -0.45 | -0. | -0.58 |
| 8. |  | 30 | -0.20 | $-0.58$ | -0.50 | -0.58 | -0 86 | 0.75 | . 68 | 0.55 | -0.39 | 0. | -0.97 |
| 7. 1 | -0.15 | -0.21 | -0.06 | -0.16 | -0.15 | -0.08 | -0.61 | -0.49 | -0.47 | -0.45 | 0.35 | -0.14 | -0.28 |
| 9.12.3.9 | -0.27 | -0.52 | -0.60 | -1.17 | -0.92 | -1.21 | -1.05 | -0.98 | -0.97 | 0.68 | 0.48 | -0.31 | -0.76 |
| 7. $2.2(9)$ | -0.09 | -0.10 | 5 | -0.09 | -0.12 | -0.06 | -0.28 | -0.15 | -0.17 | -0.11 | -0.10 | -0.14 | -0.13 |
| Dail.ext. | -0.17 | -0.18 | -0.16 | -0.03 | 0.05 | 0.12 | -0.15 | -0.24 | -0.46 | -0.49 | -0.38 | -0.21 | -0.22 |

The r.umbers without sign must be added: those with the sign - must be subtracted.

## XLV.

England. - Plymouth. Lat. $50^{\circ} 22^{\prime}$ N. Long. $4^{\circ} 7^{\prime}$ W. Greemb.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.


England. - Plynouth. Lat. $50^{\circ} 22^{\prime}$ N. Long. $4^{\circ} 7^{\prime}$ W. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.38 | 0.65 | 1.03 | 1.78 | 2.28 | 1.93 | 2.11 | 1.85 | 1.44 | 1.18 | 0.70 | 0.42 | 1.31 |
| 2 | 0.40 | 0.74 | 1.17 | 1.97 | 2.64 | 2.14 | 2.39 | 2.13 | 1.60 | 1.24 | 0.75 | 0.38 | 1.46 |
| 3 | 0.44 | 0.83 | 1.34 | 2.18 | 2.94 | 2.28 | 2.53 | 2.42 | 1.79 | 1.34 | 0.50 | 0.33 | 1.60 |
| 4 | 0.51 | 0.94 | 1.47 | 2.28 | 3.00 | 2.22 | 2.48 | $2 . .56$ | 1.93 | 1.47 | 0.87 | 0.36 | 1.67 |
| 5 | 0.61 | 1.05 | 1.51 | 2.18 | 2.68 | 2.03 | 2.14 | 2.41 | 1.89 | 1.56 | 0.93 | 0.46 | 1.62 |
| 6 | 0.68 | 1.10 | 1.37 | 1.77 | 1.94 | 1.24 | 1.49 | 1.87 | 1.61 | 1.50 | 0.95 | 0.58 | 1.34 |
| 7 | 0.65 | 1.02 | 1.00 | 1.06 | 0.89 | 0.42 | 0.63 | 1.00 | 1.03 | 1.18 | 0.84 | 0.62 | 0.86 |
| 8 | 0.49 | 0.74 | 0.43 | 0.13 | $-0.24$ | $-0.45$ | -0.29 | $-0.05$ | 0.22 | 0.56 | 0.55 | 0.50 | 0.22 |
| 9 | 0.16 | 0.26 | 0.28 | -0.86 | -1.28 | $-1.20$ | $-1.14$ | -1.06 | $-0.68$ | $-0.29$ | 0.07 | 0.18 | -0.51 |
| 10 | -0.27 | $-0.37$ | $-0.99$ | -1.75 | -2.03 | -1.72 | -1.79 | -1.57 | $-1.53$ | $-1.20$ | -0.52 | $-0.27$ | -1.19 |
| 11 | -0.70 | $-1.00$ | $-1.58$ | $-2.40$ | -2.50 | $-2.06$ | -2.23 | $-2.35$ | $-2.19$ | -1.96 | $-1.08$ | $-0.74$ | $-1.74$ |
| Noon | -1.03 | -1.48 | -1.97 | $-2.74$ | $-2.72$ | -2.19 | $-2.48$ | -2.61 | $-2.55$ | $-2.40$ | $-1.46$ | -1.08 | $-2.06$ |
| 1 | -1.17 | -1.71 | $-2.09$ | $-2.83$ | -2.83 | -2.23 | -2.58 | $-2.65$ | $-2.63$ | $-2.45$ | $-1.58$ | $-1.20$ | $-2.16$ |
| 2 | -1.11 | -1.64 | $-1.97$ | $-2.66$ | $-2.53$ | -2.18 | $-2.56$ | $-2.54$ | $-2.44$ | -2.15 | $-1.43$ | $-1: 09$ | -2.05 |
| 3 | $-0.87$ | -1.34 | $-1.66$ | $-2.32$ | $-2.72$ | $-2.06$ | $-2.40$ | $-2.34$ | -2.06 | -1.65 | -1.09 | $-0.82$ | $-1.78$ |
| 4 | -0.56 | $-0.92$ | $-1.25$ | $-1.84$ | $-2.43$ | -1.79 | $-2.06$ | -2.01 | $-1.55$ | -1.09 | $-0.69$ | $-0.49$ | $-1.39$ |
| 5 | -0.26 | $-0.49$ | $-0.78$ | -1.27 | $-1.92$ | -1.35 | $-1.54$ | $-1.53$ | -0.97 | $-0.59$ | $-0.34$ | -0.18 | 0.94 |
| 6 | -0.03 | -0.17 | -0.33 | -0.63 | $-1.1$ | -0.77 | -0.89 | -0.99 | $-0.39$ | $-0.20$ | $-0.10$ | 0.02 | 7 |
| 7 | 0.13 | 0.04 | 0.06 | $-0.00$ | -0.36 | -0.12 | -0.17 | -0.21 | 0.16 | 0.10 | 0.03 | 0 | 2 |
| 8 | 0.22 | 0.16 | 0.38 | 0.56 | 0.44 | 0.33 | 0.49 | 0.47 | 0.61 | 0.35 | 0.11 | 0.23 | 0.36 |
| 9 | 0.28 | 0.25 | 0.60 | 1.00 | 1.05 | 0.98 | 1.01 | 0.99 | 0.94 | 0.59 | 0.21 | 0.32 | 0.69 |
| 10 | 0.32 | 0.34 | 0.75 | 1.30 | 1.46 | 1.30 | 1.38 | 1.32 | 1.15 | 0.82 | 0.34 | 0.39 | 0.91 |
| 11 | 0.3 | 0.44 | 0.8 | 1.49 | 1.7 | 1.53 | 1.63 | 1.51 | 1.26 | 0.99 | 0.48 | 0.45 | 1.06 |
| Milln | 0.37 | 0.56 | 0.92 | 1.63 | 1.9 | 1.72 | 1.87 | 1.65 | 1.33 | 1.10 | 0.61 | 0.46 | 1.18 |
| 6. 6 | 0.33 | 0.47 | 0.59 | 0.57 | 0.38 | 0.24 | 0.30 | 0.44 | 0.61 | 0.65 | 0.43 | 0.30 | 0.44 |
| 7. 7 | 0.39 | 0.53 | 0.53 | 0.53 | 0.27 | 0.15 | 0.23 | 0.40 | 0.60 | 0.64 | 0.44 | 0.39 | 0.42 |
| 8. 8 | 0.36 | 0.45 | 0.41 | 0.35 | 0.10 | $-0.06$ | 0.10 | 0.21 | 0.42 | 0.46 | 0.33 | 0.37 | 0.29 |
| 9. 9 | 0.2 | 0.26 | 0.16 | 0.07 | $-0.12$ | $-0.11$ | $-0.07$ | $-0.04$ | 0.13 | 0.15 | 0.14 | 0.25 | 0.09 |
| 10.10 | 0.03 | -0.0 2 | $-0.12$ | -0.2: | $-0.29$ | $-0.21$ | $-0.21$ | $-0.28$ | $-0.19$ | $-0.19$ | $-0.09$ | 0.06 | $-0.14$ |
| 7.2. 9 | $-0.0$ | -0.12 | $-0.12$ | $-0.20$ | $-0.30$ | -0.26 | -0.31 | -0.18 | $-0.16$ | -0.13 | -0.13 | -0.05 | -0.17 |
| 6. 2. 8 | $-0.07$ | $-0.13$ | $-0.07$ | -0.11 | $-0.15$ | $-0.20$ | -0.19 | $-0.07$ | $-0.07$ | -0.10 | $-0.12$ | $-0.0$ | $-0.11$ |
| 6. 2.10 | -0.04 | $-0.07$ | 0.05 | 0.14 | 0.19 | 0.12 | 0.10 | 0.22 | 0.11 | 0.06 | $-0.05$ | $-0.04$ | 0.07 |
| 6. 2. 6 | -0.15 | -0.2 | -0.31 | $-0.51$ | $-0.69$ | $-0.57$ | -0.6 | -0.55 | -0.41 | $-0.28$ | $-0.19$ | $-0.1$ | -0.39 |
| 7. 2 | $-0.23$ | -0.31 | -0.42 | $-0.80$ | $-0.97$ | -0.85 | -0.97 | $-0.77$ | -0.71 | -0.4 | -0.3 | -0. | 0 |
| 8. 2 | -0.31 | $-0.45$ | $-0.77$ | -1.27 | $-1.54$ | $-1.32$ | -1.43 | $-1.30$ | -1.11 | -0.8 | $-0.44$ | -0.30 | 0.92 |
| 8. 1 | -0.34 | $-0.49$ | -0.s3 | -1.35 | $-1.54$ | $-1.34$ | $-1.44$ | -1.3 | -1.21 | -0.95 | 0.52 | -0.30 | 8 |
| 7. 1 | -0.26 | $-0.35$ | $-0.55$ | $-0.89$ | $-0.97$ | $-0.91$ | $-0.98$ | $-0.83$ | -0.80 | $-0.64$ | $-0.37$ | $-0.2$ | -0.65 |
| 9.12 .3 .9 | -0.37 | -0.58 | -0.83 | -1.23 | $-1.42$ | -1.12 | $-1.2$ | $-1.2$ | $-1.09$ | $-0.94$ | $-0.57$ | -0.3 | -0.92 |
| 7. 2.2(9) | 0.03 | $-0.03$ | 0.06 | 0.10 | 0.04 | 0.05 | 0.02 | 0.11 | 0.12 | 0.05 | $-0.04$ | 0.04 | 0.05 |
| Dail.ext. | -0.2.5 | $-0.31$ | $-0.99$ | -0.9? | 0.09 | 0.0 .3 | $-0.03$ | -0.05 | -0.35 | $-0.45$ | $-0.3$ | $-0.2$ | $-0.25$ |

[^5]
## XLVII.

Belgium. - Brussels. Lat. $50^{\circ} 51^{\prime}$ N. Long. $4^{\circ} 2 \mathfrak{P}^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.58 | 0.67 | 1.19 | 2.23 | 2.57 | 2.83 | 2.34 | 2.49 | 1.71 | 0.85 | 0.49 | 0.73 | 1.56 |
| 2 | 0.60 | 0.73 | 1.36 | 2.59 | 2.59 | 3.12 | 2.57 | 2.84 | 2.00 | 0.99 | 0.49 | 0.39 | 1.71 |
| 3 | 0.60 | 0.79 | 1.54 | 2.99 | 3.17 | 3.18 | 2.74 | 3.20 | 2.33 | 1.15 | 0.54 | 0.08 | 1.86 |
| 4 | 0.60 | 0.86 | 1.70 | 3.29 | 3.28 | 3.14 | 2.74 | 3.42 | 2.57 | 1.31 | 0.65 | 0.02 | 1.97 |
| 5 | 0.62 | 0.92 | 1.79 | 3.29 | 3.06 | 2.71 | 2.47 | 3.32 | 2.58 | 1.40 | 0.77 | 0.25 | 1.93 |
| 6 | 0.64 | 0.97 | 1.74 | 2.86 | 2.45 | 2.00 | 1.58 | 2.82 | 2.28 | 1.35 | 0.85 | 0.65 | 1.71 |
| 7 | 0.61 | 0.93 | 1.50 | 2.01 | 1.52 | 1.10 | 1.06 | 1.94 | 1.67 | 1.11 | 0.81 | 0.97 | 1.27 |
| 8 | 0.46 | 0.75 | 1.03 | 0.86 | 0.44 | 0.16 | 0.15 | 0.82 | 0.82 | 0.68 | 0.58 | 0.97 | 0.64 |
| 9 | 0.18 | 0.39 | 0.39 | -0.35 | -0.59 | -0.61 | -0.69 | -0.34 | $-0.14$ | 0.05 | 0.19 | 0.56 | $-0.08$ |
| 10 | $-0.22$ | $-0.13$ | $-0.36$ | $-1.42$ | -1.43 | -1.35 | $-1.33$ | -1.37 | $-1.06$ | $-0.60$ | -0.31 | $-0.13$ | $-0.81$ |
| 11 | -0.65 | -0.71 | -1.11 | -2.23 | -2.06 | -1.86 | $-1.77$ | -2.19 | -1.86 | -1.23 | -0.80 | -0.84 | $-1.44$ |
| N | -1.01 | $-1.23$ | $-1.72$ | $-2.77$ | -2.52 | -2.27 | -2.06 | -2.81 | -2.48 | -1.71 | $-1.16$ | $-1.29$ | -1.92 |
| 1 | $-1.20$ | $-1.57$ | $-2.13$ | -3.11 | -2.59 | -2.65 | -2.29 | -3.27 | -2.88 | $-1.96$ | -1.32 | -1.33 | -2.22 |
| 2 | -1.19 | $-1.65$ | $-2.29$ | $-3.29$ | -3.21 | $-2.97$ | -2.51 | -3.55 | -3.05 | $-1.95$ | -1.27 | -1.03 | $-2.33$ |
| 3 | $-0.99$ | -I. 49 | $-2.21$ | -3.33 | $-3.40$ | -3.25 | $-2.69$ | $-3.69$ | $-2.98$ | -1.71 | -1.05 | -0.59 | -2.28 |
| 4 | $-0.70$ | -1.14 | $-1.93$ | $-3.18$ | -3.36 | $-3.16$ | $-2.71$ | $-3.53$ | $-2.63$ | -1.31 | -0.75 | $-0.26$ | -2.06 |
| 5 | -0.39 | $-0.72$ | -1.51 | $-2.76$ | $-2.97$ | $-2.83$ | -2.47 | -3.02 | -2.05 | $-0.84$ | $-0.45$ | -0.16 | $-1.6 \mathrm{~S}$ |
| 6 | -0.15 | $-0.33$ | -1.03 | $-2.05$ | -2.21 | $-2.17$ | -1.91 | --2.19 | $-1.30$ | $-0.39$ | -0.18 | -0.25 | -1.18 |
| 7 | 0.02 | $-0.03$ | $-0.55$ | -1.13 | -1.20 | -1.28 | $-1.11$ | $-1.15$ | $-0.49$ | -0.01 | 0.03 | -0.37 | -0.61 |
| 8 | 0.12 | 0.17 | $-0.10$ | -0.16 | -0.12 | -0.31 | $-0.20$ | $-0.09$ | 0.23 | 0.28 | 0.19 | -0.33 | $-0.03$ |
| 9 | 0.21 | 0.31 | 0.28 | 0.69 | 0.82 | 0.68 | 0.64 | 0.82 | 0.78 | 0.48 | 0.32 | 0.05 | 0.50 |
| 10 | 0.31 | 0.41 | 0.59 | 1.31 | 1.51 | 1.37 | 1.31 | 1.48 | 1.13 | 0.60 | 0.41 | 0.37 | 0.90 |
| 11 | 0.42 | 0.50 | 0.83 | 1.70 | 1.96 | 1.97 | 1.77 | 1.89 | 1.33 | 0.68 | 0.47 | 0.75 | 1.19 |
| Miln. | 0.52 | 0.59 | 1.02 | 1.96 | 2.28 | 2.44 | 2.08 | 2.19 | 1.49 | 0.75 | 0.49 | 0.89 | 1.39 |
| 6. 6 | 0.25 | 0.32 | 0.35 | 0.41 | 0.12 | -0.09 | $-0.01$ | 0.31 | 0.49 | 0.48 | 0.33 | 0.20 | 0.26 |
| 7. 7 | 0.31 | 0.4 .5 | 0.47 | 0.44 | 0.16 | -0.09 | $-0.02$ | 0.39 | 0.59 | 0.55 | 0.42 | 0.30 | 0.33 |
| 8. 8 | 0.29 | 0.46 | 0.47 | 0.35 | 0.16 | $-0.07$ | $-0.03$ | 0.37 | 0.53 | 0.48 | 0.39 | 0.32 | 0.31 |
| 9. 9 | 0.20 | 0.3 .5 | 0.34 | 0.1 | 0.12 | 0.04 | $-0.02$ | 0.24 | 0.32 | 0.28 | 0.25 | 0.25 | 0.21 |
| 10.10 | 0.05 | 0.14 | 0.11 | 0.05 | 0.04 | 0.01 | $-0.01$ | 0.05 | 0.03 | 0.00 | 0.05 | 0.12 | 0.05 |
| 7. 2. 9 | $-0.12$ | $-0.14$ | -0.17 | -0.20 | $-0.29$ | -0.40 | -0.27 | -0.27 | $-0.20$ | $-0.12$ | -0.05 | $-0.04$ | -0.19 |
| 6. 2. 8 | -0.14 | $-0.17$ | -0.22 | $-0.20$ | $-0.29$ | $-0.43$ | $-0.28$ | -0.28 | -0.18 | $-0.11$ | -0.08 | $-0.24$ | $-0.22$ |
| 6. 2.10 | -0.08 | -0.09 | 0.01 | 0.29 | 0.25 | 0.13 | 0.23 | 0.24 | 0.12 | 0.00 | -0.00 | $-0.00$ | 0.09 |
| 6. 2. 6 | -0.23 | $-0.34$ | $-0.53$ | -0.83 | $-0.99$ | -1.05 | -0.85 | -0.98 | $-0.69$ | $-0.33$ | -0.20 | $-0.21$ | $-0.60$ |
| 7. 2 | -0.29 | -0.36 | $-0.40$ | $-0.64$ | -0.85 | -0.94 | $-0.73$ | -0.8 | -0 69 | $-0.42$ | -0.23 | -0.03 | $-0.53$ |
| 8. 2 | -0.37 | -0.45 | -0.63 | -1.22 | -1.39 | -1.41 | -1.18 | -1.38 | -1.12 | -0.6 | -0.35 | -0.03 | -0.85 |
| 8. 1 | -0.37 | $-0.41$ | $-0.55$ | $-1.13$ | -1.23 | $-1.25$ | -1.07 | -1.23 | -1.03 | $-0.6$ | -0.37 | $-0.18$ | -0.79 |
| 7. 1 | -0.30 | $-0.32$ | -0.32 | $-0.55$ | -0.69 | $-0.78$ | $-0.62$ | -0.67 | -0.61 | -0.43 | -0.26 | -0.18 | $-0.48$ |
| 9.12.2.9 | -0.40 | $-0.51$ | -0.82 | $-1.44$ | $-1.42$ | -1.36 | $-1.20$ | -1.51 | -1.21 | -0.72 | 0.43 | -0.34 | -0.95 |
| $72.2(9)$ | -0.04 | $-0.03$ | $-0.06$ | 0.03 | -0.01 | -0.13 | $-0.04$ | $-0.00$ | 0.05 | 0.03 | 0.05 | $-0.04$ | -0.02 |
| Dail.ext. | -0.28 | -0.34 | -0.25 | -0.02 | $-0.06$ | -0.04 | 0.02 | $-0.14$ | -0.24 | -0.28 | -0.24 | -0.18 | -0.18 |

The numbers without sign must be added ; those with the sign - must be subtracted

## XLVIII.

Belgium. - Brussels. Lat. $50^{\circ} 51^{\prime}$ N. Long. $4^{\circ} 22^{\prime}$ E. Greenv.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respeetive Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hfour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Miln. | 0.30 | 0.60 | 1.09 | 1.72 | 2.27 | 2.46 | 2.20 | 1.88 | 1.52 | 0.92 | 0.51 | 0.30 | 1.31 |
| 2 | 0.56 | 0.82 | 1.39 | 2.19 | 3.00 | 2.82 | 2.77 | 2.44 | 2.03 | 1.20 | 0.77 | 0.47 | 1.70 |
| 4 | 0.64 | 0.97 | 1.66 | 2.64 | 3.32 | 3.53 | 3.14 | 2.76 | 2.38 | 1.44 | 0.83 | 0.62 | 1.99 |
| 6 | 0.66 | 1.03 | 1.83 | 2.43 | 2.44 | 2.27 | 2.30 | 2.44 | 2.47 | 1.56 | 0.93 | 0.63 | 1.75 |
| 8 | 0.67 | 0.84 | 1.02 | 0.76 | 0.49 | 0.41 | 0.32 | 0.68 | 1.03 | 0.96 | 0.79 | 0.63 | 0.72 |
| 9 | 0.36 | 0.33 | 0.21 | -0.35 | 0.61 | -0.61 | -0.63 | -0.39 | -0.14 | 0.07 | 0.21 | 0.34 | 0.00 |
| 10 | 0.07 | -0.09 | -0.54 | -1.18 | -1.43 | -1.32 | -1.36 | -1.26 | -1.19 | -0.78 | -0.36 | -0.08 | $-0.79$ |
| Noon. | -0.92 | -1.27 | -178 | -2.42 | -2.61 | -2.47 | -2.35 | -2.47 | -2.46 | -1.87 | -1.27 | -0.83 | -1.89 |
| 2 | $-1.15$ | $-1.65$ | -2.30 | -2.95 | -3.22 | -3.21 | -2.92 | -3.08 | -3.04 | -2.17 | -1.42 | -1.04 | -2.35 |
| 4 | -0.72 | -1.19 | -2.04 | -2.63 | -3.15 | -3.18 | -2.90 | -2.93 | -2.70 | -1.61 | -0.90 | -0.65 | -2.05 |
| 6 | -0.21 | -0.49 | -0.94 | -1.71 | -2.44 | -2.57 | -2.38 | -1.57 | -1.21 | -0.37 | -0.28 | -0.18 | -1.22 |
| 8 | -0.03 | -0.0.5 | -0.00 | 0.13 | 0.0 .5 | -0.16 | -0.15 | 0.17 | 0.21 | 0.23 | 0.07 | -0.03 | 0.03 |
| 9 | 0.13 | 0.17 | 0.31 | 0.63 | 0.76 | 0.80 | 0.79 | 0.76 | 0.64 | 0.43 | 0.24 | 0.07 | 0.48 |
| 10 | 0.20 | 0.30 | 0.58 | 1.04 | 1.25 | 1.45 | 1.39 | 1.27 | 1.01 | 0.54 | 0.38 | 0.14 | 0.80 |
| Mean. | 0.52 | 2.45 | 3.56 | 7.27 | 10.37 | 13.10 | 13.69 | 13.58 | 11.22 | 7.69 | 4.72 | 1.89 |  |

## XLIX.

Germany. - Schwerin. Lat. $53^{\circ} 36^{\prime}$ N. Long. $11^{\circ} 30^{\prime}$ E. Gr.-Dove.
Degrees of Reaumur.

| Hour. | Jan. | Feh. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.0 .5 | 0.49 | 0.92 | 1.66 | 1.97 | 2.10 | 2.12 | 1.92 | 1.70 | 0.87 | 0.21 | 0.16 | 1.18 |
| 2 | 0.08 | 0.69 | 1.20 | 2.17 | 2.44 | 2.69 | 2.72 | 2.41 | 2.19 | 1.14 | 0.24 | 0.34 | 1.53 |
| 4 | 0.27 | 083 | 1.43 | 2.53 | 2.96 | 2.97 | 2.96 | 2.62 | 2.54 | 1.51 | 0.42 | 0.48 | 1.79 |
| 6 | 0.35 | 0.86 | 1.62 | 2.67 | 2.07 | 1.80 | 1.94 | 2.13 | 2.70 | 1.67 | 0.62 | 0.48 | 1.55 |
| 8 | 0.59 | 1.19 | 1.24 | 0.98 | 0.56 | 0.25 | 0.12 | 0.32 | 0.95 | 1.21 | 0.70 | 0.63 | 0.73 |
| 10 | 0.17 | 0.18 | -0.11 | -0.97 | -1.15 | $-1.20$ | -1.26 | -1.17 | -1.12 | -0.34 | 0.01 | 0.13 | -0.57 |
| Noon. | -0.42 | -0.97 | -1.32 | -2.34 | -2.47 | -2.36 | -2.20 | -2.29 | -2.42 | -1.50 | -0.77 | -0.43 | -1.65 |
| 2 | -0.61 | -0.72 | -2.21 | -3.50 | -3.38 | -3.23 | -3.26 | -3.45 | -3.58 | -2.54 | -0.91 | -0.68 | -2.42 |
| 4 | -0.43 | -1.22 | -2.13 | -2.86 | -2.70 | -2.62 | -2.76 | -2.76 | -3.03 | -1.85 | -0.62 | -0.62 | -1.97 |
| 6 | -0.02 | -0.42 | -0.95 | -1.54 | -1.62 | -1.71 | -1.70 | -1.37 | -1.32 | -0.55 | -0.23 | -0.2 | -0.98 |
| 8 | -0.07 | -0.07 | -0.11 | 0.13 | 0.11 | -0.02 | 0.08 | 0.34 | 0.26 | 0.16 | 0.02 | -0.14 | 0.06 |
| 10 | 0.06 | 0.21 | 0.45 | 1.01 | 1.15 | 1.28 | 1.29 | 1.30 | 1.19 | 0.57 | 0.24 | -0.02 | 0.73 |
| Mean. | -1.05 | -2.00 | 1.18 | 5.26 | 8.45 | 12.19 | 13.50 | 13.02 | 10.42 | 7.48 | 1.42 | -1.38 |  |

The numbers without sign must be added ; those with the sign - must be subtracted.

Prussia. - Mühlhausen. Lat. $51^{\circ} 13^{\prime}$ N. Long. $10^{\circ} 27^{\prime}$ E. Greemu.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.71 | 1.28 | 1.10 | 1.84 | 2.40 | 3.56 | 2.91 | 2.49 | 1.95 | 1.39 | 0.47 | 0.58 | 1.72 |
| 2 | 0.75 | 1.30 | 1.28 | 2.19 | 2.80 | 3.97 | 3.30 | 2.80 | 2.20 | 1.65 | 0.53 | 0.59 | 1.95 |
| 3 | 0.77 | 1.33 | 1.46 | 2.40 | 3.06 | 4.16 | 3.50 | 3.06 | 3.29 | 1.85 | 0.60 | 0.60 | 2.17 |
| 4 | 0.52 | 1.40 | 1.60 | 2.74 | 3.06 | 3.98 | 3.42 | 3.14 | 2.70 | 1.99 | 0.66 | 0.62 | 2.18 |
| 5 | 0.86 | 1.47 | 1.62 | 2.61 | 2.67 | 3.40 | 3.00 | 2.98 | 2.73 | 2.05 | 0.68 | 0.66 | 2.06 |
| 6 | 0.91 | 1.50 | 1.46 | 2.25 | 2.06 | 2.49 | 2.22 | 2.51 | 2.46 | 1.93 | 0.63 | 0.67 | 1.76 |
| 7 | 0.86 | 1.36 | 1.11 | 1.41 | 1.15 | 1.32 | 1.20 | 1.73 | 1.03 | 1.50 | 0.46 | 0.59 | 1.14 |
| 8 | 0.62 | 0.98 | 0.55 | 0.58 | 0.16 | 0.11 | 0.09 | 0.86 | 0.87 | 0.84 | 0.16 | 0.46 | 0.52 |
| 9 | 0.21 | 0.33 | -0.02 | -0.38 | $-0.75$ | $-1.02$ | $-0.97$ | -0.36 | $-0.26$ | $-0.03$ | -0.22 | 0.03 | $-0.29$ |
| 10 | -0.38 | $-0.50$ | $-0.70$ | $-1.16$ | $-1.50$ | -1.98 | $-1.82$ | $-1.38$ | $-1.40$ | $-0.99$ | -0.62 | $-0.54$ | -1.08 |
| 11 | -0.93 | $-1.35$ | $-1.30$ | $-1.97$ | -2.06 | $-2.77$ | $-2.46$ | -2.24 | $-2.42$ | -1.88 | $-0.92$ | $-0.77$ | -1.76 |
| Noon. | $-1.38$ | -2.02 | $-1.76$ | $-2.42$ | -2.44 | $-3.39$ | $-2.94$ | $-2.89$ | -3.14 | -2.53 | -1.09 | $-1.06$ | $-2.26$ |
| 1 | -1.58 | -2.38 | $-2.02$ | $-2.50$ | -2.71 | -3.86 | -3.26 | -3.29 | -3.52 | $-2.82$ | -1.08 | $-1.15$ | $-2.54$ |
| 2 | $-1.52$ | $-2.38$ | -2.07 | $-2.94$ | $-2.87$ | $-4.14$ | $-3.42$ | $-3.46$ | -3.54 | -2.99 | -0.89 | $-1.10$ | $-2.61$ |
| 3 | $-1.24$ | $-2.07$ | $-1.90$ | $-2.85$ | $-2.89$ | $-4.13$ | $-3.36$ | $-3.39$ | -3.23 | $-2.48$ | $-0.66$ | -0.81 | -2.42 |
| 4 | -0.84 | $-1.56$ | -1.58 | -2.39 | $-2.69$ | $-3.78$ | $-3.06$ | -3.07 | $-2.65$ | -1.89 | $-0.39$ | $-0.50$ | $-2.03$ |
| 5 | $-0.44$ | $-1.02$ | $-1.11$ | -1.95 | $-2.19$ | -3.06 | $-2.52$ | -2.51 | $-1.89$ | -1.21 | $-0.14$ | $-0.23$ | $-1.52$ |
| 6 | $-0.20$ | $-0.54$ | -0.62 | -1. 20 | $-1.59$ | $-2.10$ | $-1.76$ | $-1.76$ | -1.06 | $-0.58$ | 0.02 | $-0.02$ | -0.95 |
| 7 | $-0.04$ | $-0.17$ | -0.18 | $-0.47$ | -0. 03 | $-1.02$ | -0.85 | $-0.90$ | $-0.24$ | -0.03 | 0.06 | 0.12 | $-0.38$ |
| 8 | 0.18 | 0.13 | 0.16 | 0.09 | $-0.08$ | 0.05 | 0.03 | $-0.05$ | 0.50 | 0.38 | 0.22 | 0.26 | 0.16 |
| 9 | 0.27 | 0.41 | 0.45 | 0.53 | 0.58 | 1.01 | 0.81 | 0.71 | 0.99 | 0.70 | 0.26 | 0.32 | 0.59 |
| 10 | 0.37 | 0.66 | 0.64 | 0.59 | 1.10 | 1.76 | 1.46 | 1.24 | 1.35 | 0.91 | 0.34 | 0.40 | 0.93 |
| 11 | 0.53 | 0.89 | 0.78 | 1.14 | 1.56 | 2.42 | 2.01 | 1.78 | 1.58 | 1.10 | 0.38 | 0.47 | 1.22 |
| Midn. . | 0.64 | 1.08 | 0.94 | 1.58 | 1.98 | 3.05 | 3.29 | 2.16 | 1.75 | 1.26 | 0.42 | 0.54 | 1.56 |
| 6. 6 | 0.36 | 0.48 | 0.42 | 0.53 | 0.24 | 0.20 | 0.23 | 0.38 | 0.70 | 0.68 | 0.33 | 0.33 | 0.41 |
| 7. 7 | 0.41 | 0.60 | 0.47 | 0.47 | 0.16 | 0.15 | 0.18 | 0.42 | 0.40 | 0.74 | 0.26 | 0.36 | 0.35 |
| 8. 8 | 0.40 | 0.56 | 0.36 | 0.34 | 0.04 | 0.08 | 0.06 | 0.41 | 0.69 | 0.61 | 0.19 | 0.36 | 0.34 |
| 9. 9 | 0.24 | 0.37 | 0.22 | 0.08 | -0.09 | $-0.01$ | -0.08 | 0.18 | 0.37 | 0.34 | 0.02 | 0.18 | 0.15 |
| 10.10 | $-0.01$ | 0.08 | $-0.03$ | $-0.14$ | $-0.20$ | $-0.11$ | -0.18 | $-0.07$ | -0.03 | $-0.04$ | $-0.14$ | -0.07 | -0.0S |
| 7. 2. 9 | -0.13 | $-0.20$ | $-0.17$ | -0.23 | -0.38 | -0.60 | $-0.47$ | -0.34 | -0.51 | $-0.26$ | -0.06 | -0.06 | -0.29 |
| 6. 2. 8 | $-0.14$ | $-0.25$ | $-0.15$ | $-0.20$ | $-0.30$ | $-0.53$ | $-0.39$ | -0.33 | -0.19 | $-0.23$ | -0.01 | -0.06 | $-0.23$ |
| 6. 2.10 | -0.08 | $-0.07$ | 0.01 | 0.07 | 0.10 | 0.04 | 0.09 | 0.10 | 0.09 | -0.05 | 0.03 | $-0.01$ | 0.03 |
| 6. 2. 6 | $-0.27$ | $-0.47$ | $-0.41$ | $-0.63$ | $-0.80$ | $-1.25$ | $-0.99$ | $-0.90$ | $-0.71$ | -0.55 | -0.08 | $-0.15$ | $-0.60$ |
| 7. 2 | -0.33 | $-0.51$ | $-0.48$ | $-0.77$ | $-0.86$ | -1.41 | $-1.11$ | -0.87 | -1.26 | $-0.75$ | $-0.22$ | -0.26 | $-0.74$ |
| 8. 2 | -0.45 | $-0.70$ | $-0.76$ | -1.18 | -1.36 | -2.02 | -1.67 | $-1.30$ | -1.34 | -1.08 | -0.37 | -0.32 | -1.05 |
| 8. 1 | -0.48 | $-0.70$ | $-0.74$ | -1.11 | -1.28 | $-1.85$ | $-1.59$ | -1.22 | -1.33 | $-0.99$ | $-0.46$ | $-0.35$ | $-1.01$ |
| 7. 1 | $-0.36$ | $-0.51$ | $-0.46$ | $-0.70$ | $-0.78$ | $-1.27$ | $-1.03$ | $-0.78$ | -1.25 | $-0.66$ | $-0.31$ | $-0.25$ | $-0.70$ |
| 9.12 .3 .9 | $-0.54$ | -0.84 | -0.81 | $-1.28$ | $-1.38$ | -1.88 | -1.62 | -1.48 | -1.41 | $-1.09$ | $-0.43$ | -0.38 | $-1.10$ |
| 7. $2.2(9)$ | $-0.03$ | $-0.05$ | $-0.02$ | $-0.12$ | $-0.14$ | $-0.20$ | $-0.15$ | -0.08 | -0.13 | $-0.02$ | 0.02 | 0.03 | -0.07 |
| Dail.ext. | -0.34 | -0.44 | -0.23 | -0.10 | 0.09 | 0.01 | 0.04 | $-0.16$ | $-0.13$ | $-0.17$ | -0.21 | -0.2 | -0.22 |

Holland. - Utrecht. Lat. $52^{\circ} 5^{\prime}$ N. Long. $5^{\circ} 8^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year.- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.36 | 0.62 | 1.13 | 1.71 | 2.56 | 2.74 | 2.64 | 1.57 | 1.91 | 1.07 | 0.76 | 0.11 | 1.44 |
| 1 | 0.37 | 0.74 | 1.18 | 1.87 | 2.86 | 3.29 | 2.67 | 1.91 | 2.10 | 1.11 | 0.70 | 0.19 | 1.58 |
| 2 | 0.46 | 0.82 | 1.21 | 2.00 | 3.00 | 3.21 | 2.82 | 2.02 | 2.21 | 1.18 | 0.78 | 0.32 | 1.67 |
| 3 | 0.51 | 0.87 | 1.27 | 2.10 | 3.02 | 3.25 | 2.97 | 2.07 | 2.34 | 1.25 | 0.82 | 0.42 | 1.74 |
| 4 | 0.57 | 0.90 | 1.31 | 2.16 | 2.70 | 2.84 | 2.76 | 2.06 | 2.45 | 1.31 | 0.82 | 0.44 | 1.69 |
| 5 | 0.61 | 0.97 | 1.26 | 1.92 | 1.50 | 1.82 | 1.86 | 1.80 | 2.42 | 1.42 | 0.90 | 0.50 | 1.44 |
| 6 | 0.66 | 0.98 | 1.02 | 1.30 | 0.67 | 0.44 | 0.33 | 1.05 | 1.87 | 1.22 | 0.91 | 0.46 | 0.91 |
| 7 | 0.64 | 0.84 | 0.62 | 0.37 | -0.38 | -0.70 | -0.77 | 0.04 | 0.72 | 0.39 | 0.78 | 0.38 | 0.24 |
| S | 0.50 | 0.56 | -0.01 | -0.40 | -1.17 | -1.50 | $-1.28$ | -0.68 | -0.39 | 0.12 | 0.29 | 0.31 | -0.30 |
| 9 | 0.13 | -0.07 | -0.5.3 | $-1.20$ | -1.68 | -2.02 | -1.69 | -1.33 | -1.12 | -0.50 | -0.22 | 0.14 | -0.84 |
| 10 | -0.26 | -0.49 | -1.0.5 | -1.71 | -2.06 | $-2.42$ | -2.02 | -1.65 | -1.79 | -1.12 | -0.71 | -0.14 | $-1.29$ |
| 11 | -0.62 | -0.97 | -1.50 | -2.16 | -2.46 | -2.78 | -2.27 | -1.57 | -2.34 | -1.68 | -1.15 | -0.33 | $-1.68$ |
| Noon. | -0.8.5 | -1.34 | -1.77 | -2.41 | -2.78 | -2.94 | -2.53 | -2.16 | -2.83 | -1.98 | -1.49 | -0.62 | $-1.97$ |
| 1 | -0.98 | $-1.58$ | -1.88 | -2.42 | -2.94 | -3.00 | -2.61 | -2.40 | -3.07 | -2.11 | $-1.62$ | -0.75 | -2.11 |
| 2 | -1.02 | -1.54 | -1.82 | $-2.12$ | -2.83 | -2.94 | -2.60 | -2.30 | -2.99 | -1.99 | -1.43 | -0.66 | -2.05 |
| 3 | -0.81 | -1.21 | -1.54 | -2.24 | -2.55 | -2.64 | -1.58 | -2.13 | -2.68 | -1.64 | -1.08 | -0.47 | -1.72 |
| 4 | -0.60 | -0.89 | -1.25 | -1.52 | -2.06 | -2.20 | -2.00 | -1.79 | -2.06 | -1.10 | -0.70 | -0.23 | -1.39 |
| 5 | -0.3. | -0.48 | -0.75 | $-1.23$ | -1.42 | $-1.53$ | -1.62 | -1.30 | -1.34 | -0.52 | -0.42 | -0.17 | -0.93 |
| 6 | -0.19 | -0.21 | -0.24 | -0.47 | -0.76 | -0.74 | -0.76 | -0.61 | -0.52 | -0.11 | -0.18 | -0.10 | $-0.41$ |
| 7 | -0.0.5 | -0.03 | 0.14 | 020 | 0.07 | 0.17 | 0.02 | 0.14 | 0.10 | 0.22 | -0.02 | -0.03 | 0.06 |
| 8 | 0.0 .5 | 0.12 | 0.45 | 0.72 | 0.55 | 1.01 | 0.82 | 0.86 | 0.62 | 0.53 | 0.18 | 0.02 | 0.52 |
| 9 | 0.22 | 0.23 | 0.74 | 1.13 | 1.51 | 1.77 | 1.50 | 1.24 | 1.17 | 0.84 | 0.40 | 0.06 | 0.90 |
| 10 | 0.36 | 0.40 | 0.94 | 1.41 | 1.92 | 2.25 | 1.96 | 1.52 | 1.51 | 1.01 | 0.58 | 0.04 | 1.16 |
| 11 | 0.36 | 0.67 | 1.02 | 1.58 | 2.16 | 2.53 | 2.17 | 1.70 | 1.76 | 1.14 | 1.06 | 0.02 | 1.35 |
| Mean | -2.83 | 4.18 | 3.20 | 7.14 | 10.55 | 12.95 | 13.75 | 12.90 | 10.87 | 6.58 | 4.65 | 0.76 |  |

## LII.

England. - Greenwich. Lat. $51^{\circ} 28^{\prime} 38^{\prime \prime}$ N. Long. $0^{\circ} 0^{\prime}$. -Dove.
Degrees of Reaumur.

| IIour | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor. | Dee. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A.M. 1 | 0.44 | 0.75 | 1.44 | 2.32 | 2.72 | 3.24 | 2.73 | 2.49 | 2.05 | 1.34 | 0.67 | 0.47 | 1.72 |
| 3 | 0.62 | 0.94 | 1.66 | 2.66 | 3.04 | 3.70 | 3.11 | 2.82 | 2.40 | 1.42 | 0.80 | 0.56 | 1.98 |
| 5 | 0.75 | 1.06 | 1.92 | 2.84 | 2.84 | 3.25 | 2.91 | 2.89 | 2.58 | 1.54 | 0.57 | 0.56 | 2.00 |
| 7 | 0.86 | 1.05 | 1.60 | 1.31 | 0.75 | 0.80 | 0.88 | 1.22 | 1.65 | 1.26 | 0.88 | 0.60 | 1.07 |
| 9 | 0.41 | 0.24 | -0.22 | -0.82 | $-1.30$ | $-1.52$ | -1.14 | -1.14 | -0.76 | -0.30 | 0.11 | 0.24 | $-0.50$ |
| 11 | -0.74 | -1.03 | -1.90 | -2.48 | -2.60 | $-2.91$ | -2.67 | -2.64 | -2.57 | -1.88 | -1.06 | $-0.73$ | -1.93 |
| P.M. 1 | -1.2. | -1.73 | -2.62 | -3.31 | -3.36 | -3.75 | -3.17 | -3.40 | -3.28 | -2.40 | -1.64 | -1.20 | -2.59 |
| 3 | -1.10 | -1.59 | -2.43 | -3.08 | -3.02 | -3.60 | -3.09 | -3.20 | -2.94 | -2.04 | -1.26 | -0.85 | -2.35 |
| 5 | -0.36 | -0.63 | -1.33 | -2.04 | -2.05 | -2.51 | -2.2 4 | -2.11 | -1.65 | -0.73 | -0.38 | -0.24 | -1.37 |
| 7 | 0.03 | 0.0 .5 | 0.09 | -0.16 | -0.29 | -0.58 | $-0.50$ | -0.11 | 0.04 | 0.11 | 0.09 | 0.00 | -0.10 |
| 9 | 0.10 | 0.32 | 0.71 | 0.99 | 1.20 | 1.40 | 1.13 | 1.22 | 0.89 | 0.63 | 0.40 | 0.21 | 0.77 |
| 11 | 0.23 | 0.54 | 1.11 | 1.77 | 2.06 | 2.52 | 2.08 | 1.96 | 1.60 | 1.07 | 0.53 | 0.37 | 1.33 |
| Mean | 2.48 | 2.53 | 4.53 | 6.71 | 9.62 | 12.47 | 13.08 | 12.98 | 11.12 | 7.71 | 5.47 | 309 |  |

The numbers without sign must be added; those with the sign - must be subtracted.

England. - Greenwich. Lat. $51^{\circ} 29^{\prime}$ N. Long. $0^{\circ} 0^{\prime}$.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.38 | 0.68 | 1.29 | 2.21 | 2.72 | 3.13 | 2.61 | 2.61 | 1.89 | 1.28 | 0.60 | 0.40 | 1.65 |
| 2 | 0.63 | 0.82 | 1.44 | 2.31 | 2.85 | 3.30 | 2.71 | 2.68 | 2.06 | 1.45 | 0.75 | 0.52 | 1.79 |
| 3 | 0.53 | 0.95 | 1.62 | 2.14 | 2.91 | 3.41 | 2.71 | 2.78 | 2.92 | 1.56 | 0.88 | 0.59 | 1.91 |
| 4 | 0.93 | 1.02 | 1.82 | 2.54 | 2.85 | 3.40 | 2.71 | 2.86 | 2.34 | 1.60 | 0.95 | 0.62 | 1.97 |
| 5 | 0.93 | 1.03 | 1.95 | 2.46 | 2.60 | 3.14 | 2.53 | 2.81 | 2.35 | 1.56 | 0.95 | 0.62 | 1.91 |
| 6 | 0.84 | 0.97 | 1.93 | 2.17 | 2.08 | 2.52 | 2.11 | 2.48 | 2.15 | 1.42 | 0.89 | 0.60 | 1.68 |
| 7 | 0.71 | 0.54 | 1.66 | 1.56 | 1.2.) | 1.53 | 1.38 | 1.77 | 1.67 | 1.15 | 0.75 | 0.57 | 1.24 |
| 8 | 0.53 | 0.61 | 1.11 | 0.66 | 0.20 | 0.28 | 0.40 | 0.72 | 0.88 | 0.71 | 0.52 | 0.48 | 0.59 |
| 9 | 0.30 | 0.26 | 0.30 | $-0.37$ | $-0.92$ | $-1.02$ | -0.71 | -0.55 | $-0.13$ | 0.09 | 0.19 | 0.28 | $-0.19$ |
| 10 | $-0.01$ | $-0.20$ | $-0.63$ | -1.13 | -1.94 | -2.12 | $-1.73$ | $-1.78$ | $-1.23$ | $-0.66$ | $-0.26$ | -0.0.4 | $-1.01$ |
| 11 | $-0.39$ | $-0.7 .5$ | $-1.60$ | $-2.30$ | $-2.70$ | -2.89 | -2.51 | $-2.79$ | $-2.22$ | $-1.43$ | -0.77 | -0.16 | $-1.73$ |
| Noon. | $-0.79$ | $-1.27$ | $-2.35$ | -2.87 | $-3.13$ | -3.28 | $-2.94$ | $-3.43$ | $-2.94$ | $-2.07$ | $-1.25$ | $-0.87$ | $-2.27$ |
| 1 | -1.12 | $-1.66$ | $-2.79$ | $-3.17$ | $-3.26$ | -3.39 | $-3.04$ | $-3.69$ | $-3.28$ | $-2.45$ | -1.59 | $-1.17$ | -2.5.5 |
| 2 | -1.28 | $-1.81$ | $-2.85$ | $-3.14$ | -3.16 | -3.34 | $-2.91$ | $-3.63$ | -3.23 | $-2.18$ | -1.69 | $-1.25$ | $-2.56$ |
| 3 | -1.21 | $-1.67$ | $-2.57$ | $-2.92$ | $-2.90$ | $-3.21$ | $-2.67$ | $-3.34$ | $-2.56$ | $-2.17$ | $-1.51$ | $-1.10$ | $-2.31$ |
| 4 | -0.95 | $-1.29$ | $-2.05$ | $-2.54$ | -2.54 | -3.01 | $-2.38$ | -2.89 | -2.28 | $-1.63$ | $-1.10$ | $-0.76$ | $-1.95$ |
| 5 | $-0.58$ | $-0.78$ | $-1.40$ | $-1.97$ | -2.06 | -2.67 | $-2.30$ | -2.30 | -1.60 | -1.01 | $-0.59$ | $-0.36$ | 1.45 |
| 6 | $-0.22$ | $-0.26$ | $-0.75$ | $-1.34$ | $-1.45$ | $-2.10$ | $-1.57$ | $-1.56$ | -0.91 | $-0.43$ | $-0.10$ | $-0.01$ | $-0.89$ |
| 7 | 0.03 | 0.14 | $-0.17$ | -0.60 | -0.71 | $-1.26$ | -0.96 | $-0.69$ | $-0.27$ | 0.02 | 0.24 | 0.20 | $-0.34$ |
| 8 | 0.11 | 0.37 | 0.30 | 0.17 | 0.11 | -0.24 | -0.19 | 0.24 | 0.29 | 0.32 | 0.41 | 0.26 | 0.18 |
| 9 | 0.08 | 0.46 | 0.65 | 0.84 | 0.92 | 0.81 | 0.64 | 1.11 | 0.77 | 0.52 | 0.44 | 0.23 | 0.62 |
| 10 | 0.03 | 0.18 | 0.59 | 1.42 | 1.62 | 1.74 | 1.41 | 1.81 | 1.17 | 0.69 | 0.41 | 0.19 | 0.99 |
| 11 | 0.04 | 0.49 | 1.05 | 1.81 | 2.16 | 2.42 | 2.01 | 2.27 | 1.47 | 0.87 | 0.40 | 0.20 | 1.27 |
| Midn. | 0.16 | 0.56 | 1.17 | 2.03 | 2.51 | 2.86 | 2.40 | 2.51 | 1.70 | 1.08 | 0.16 | 0.28 | 1.48 |
| 6. 6 | 0.31 | 0.36 | $0 . .59$ | 0.42 | 0.31 | 0.21 | 0.27 | 0.46 | 0.62 | 0.50 | 0.39 | 0.30 | 0.40 |
| 7.7 | 0.37 | 0.49 | 0.75 | 0.45 | 0.27 | 0.13 | 0.21 | 0.54 | 0.70 | 0.59 | 0.50 | 0.38 | 0.45 |
| 8. 8 | 0.32 | 0.49 | 0.71 | 0.42 | 0.16 | 0.02 | 0.10 | 0.48 | 0.59 | 0.52 | 0.17 | 0.37 | 0.39 |
| 9. 9 | 0.19 | 0.36 | 0.48 | 0.24 | 0.00 | $-0.10$ | $-0.01$ | 0.28 | 0.32 | 0.31 | 0.91 | 0.2 .5 | 0.22 |
| 10.10 | 0.01 | 0.14 | 0.1 | $-0.00$ | $-0.16$ | $-0.19$ | $-0.16$ | 0.01 | $-0.03$ | 0.02 | 0.08 | 0.07 | $-0.01$ |
| 7.2. 9 | $-0.16$ | $-0.17$ | $-0.18$ | -0.2.) | $-0.33$ | $-0.33$ | $-0.30$ | $-0.25$ | -0.26 | $-0.27$ | $-0.17$ | -0.15 | -0.24 |
| 6. 2. 8 | -0.11 | $-0.16$ | $-0.21$ | -0.97 | $-0.32$ | $-0.35$ | $-0.33$ | -0.30 | $-0.26$ | $-0.25$ | $-0.13$ | $-0.13$ | -0.2 t |
| 6. 2.10 | $-0.14$ | $-0.12$ | $-0.01$ | 0.15 | 0.18 | 0.31 | $-0.20$ | 0.22 | 0.03 | $-0.12$ | $-0.13$ | $-0.15$ | 0.04 |
| 6. 2. 6 | $-0.22$ | $-0.37$ | $-0.56$ | $-0.77$ | -0.91 | -0.97 | -0.79 | $-0.90$ | $-0.66$ | -0.50 | $-0.30$ | $-0.22$ | $-0.59$ |
| 7. 2 | $-0.29$ | $-0.49$ | $-0.60$ | $-0.79$ | $-0.96$ | $-0.91$ | $-0.7 \%$ | $-0.93$ | $-0.78$ | $-0.67$ | $-0.47$ | $-0.31$ | $-0.67$ |
| 8. 2 | $-0.38$ | $-0.60$ | $-0.97$ | $-1.24$ | -1.48 | $-1.53$ | $-1.26$ | -1.46 | -1.18 | -0.89 | $-0.5$ | -0.39 | -0.99 |
| 8. 1 | -0.30 | $-0.53$ | -0.34 | -1.26 | $-1.53$ | -1.56 | -1.31 | -1.49 | $-1.20$ | -0.87 | -0.5 | -0.35 | -0.98 |
| 7. 1 | -0.21 | $-0.41$ | -0.57 | -0.81 | -1.01 | $-0.93$ | $-0.83$ | -0.96 | -0.81 | -0.65 | -0.42 | -0.30 | -0.66 |
| 9.12.3.9 | -0.41 | $-0.56$ | -0.99 | $-1.33$ | -1.51 | -1.68 | -1.42 | $-1.55$ | $-1.29$ | -0.91 | -0.53 | $-0.37$ | $-1.05$ |
| 7. $2.2(9)$ | $-0.10$ | $-0.01$ | 0.03 | 0.03 | $-0.02$ | $-0.05$ | $-0.06$ | 0.09 | $-0.01$ | $-0.07$ | $-0.02$ | $-0.06$ | -0.02 |
| Dail.ext. | -0.18 | $-0.39$ | $-0.45$ | $-0.32$ | -0.18 | 0.01 | $-0.15$ | -0.42 | $-0.47$ | -0. | $-0.37$ | -0.39 | 30 |

The numbers without sign must be added; those with the sign - must be subtracted.

England. - Greenwich. Lat. $51^{\circ} 29^{\prime}$ N. Long. $0^{\circ} 0^{\prime}$.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean ' Cemperatures of the respective Days, Months, and of the Year. - Glaisher.

Degrees of Fahrenheit.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn | 1.0 | 1.6 | 2.9 | 4.8 | 5.4 | 6.2 | 5.0 | 5.1 | 4.0 | 2.9 | 1.7 | 0.9 | 3.5 |
| 1 | 0.9 | 1.8 | 3.0 | 5.2 | 6.0 | 7.1 | 5.5 | 5.5 | 4.5 | 3.0 | 1.8 | 1.0 | 3.8 |
| 2 | 1.2 | 2.0 | 3.3 | 5.7 | 6.1 | 8.0 | 6.0 | 6.0 | 5.5 | 3.4 | 2.0 | 1.2 | 4.2 |
| 3 | 1.3 | 2.1 | 3.6 | 6.2 | 6.7 | 8.7 | 6.4 | 6.3 | 6.4 | 3.6 | 2.0 | 1.3 | 4.5 |
| 4 | 1.6 | 2.3 | 3.9 | 6.6 | 6.7 | 9.3 | 6.6 | 6.5 | 6.6 | 3.8 | 2.1 | 1.4 | 4.6 |
| 5 | 1.8 | 2.2 | 4.0 | 6.7 | 6.3 | 8.8 | 6.2 | 6.5 | 6.2 | 3.8 | 2.0 | 1.4 | 4.7 |
| 6 | 1.9 | 2.3 | 3.9 | 6.0 | 4.8 | 6.4 | 4.5 | 5.5 | 5.3 | 3.5 | 1.9 | 1.4 | 3.9 |
| 7 | 1.9 | 2.1 | 3.6 | 4.3 | 2.6 | 3.0 | 2.5 | 3.3 | 4.0 | 2.8 | 1.7 | 1.5 | 2.8 |
| 8 | 1.5 | 1.6 | 2.5 | 2.0 | 0.5 | 0.0 | 0.0 | 0.9 | 2.1 | 1.6 | 1.0 | 1.3 | 1.2 |
| 9 | 1.0 | 0.7 | 0.2 | -0.9 | $-2.0$ | $-2.5$ | $-2.0$ | $-1.6$ | $-0.4$ | 0.0 | 0.4 | 0.9 | $-0.5$ |
| 10 | 0.2 | $-0.5$ | -1.9 | $-3.2$ | $-4.0$ | $-4.5$ | $-4.0$ | -3.5 | $-3.0$ | $-2.0$ | -0.6 | 0.0 | $-2.2$ |
| 11 | -1.3 | -2.1 | $-3.5$ | $-5.3$ | -5.5 | $-5.8$ | $-5.4$ | $-5.4$ | $-5.0$ | -3.8 | $-2.0$ | $-1.3$ | -3.9 |
| Noon. | $-2.3$ | -3.2 | $-5.0$ | $-6.8$ | $-6.7$ | $-7.3$ | -6.4 | $-6.5$ | -6.4 | $-5.1$ | -3.1 | -2.1 | -5.1 |
| 1 | $-2.9$ | $-3.9$ | $-5.8$ | $-7.9$ | $-7.5$ | -8.1 | $-6.7$ | $-7.5$ | $-7.1$ | $-5.5$ | -8.5 | $-2.4$ | -5.7 |
| 2 | -3.0 | $-3.9$ | $-5.8$ | $-8.2$ | $-7.7$ | -8.6 | $-6.7$ | $-7.7$ | $-7.1$ | $-4.9$ | $-3.6$ | -2.3 | -5.8 |
| 3 | $-2.5$ | $-3.6$ | $-5.5$ | $-7.7$ | $-7.8$ | -8.4 | $-6.5$ | $-7.0$ | $-6.6$ | $-3.7$ | $-3.0$ | -1.9 | $-5.3$ |
| 4 | $-1.9$ | -2.8 | $-4.5$ | $-6.7$ | $-6.1$ | $-7.4$ | $-5.8$ | $-5.5$ | $-5.5$ | $-2.8$ | -2.1 | $-1.3$ | -4.4 |
| 5 | -1.1 | $-1.6$ | $-3.3$ | $-5.4$ | $-4.8$ | $-6.1$ | $-4.9$ | $-3.6$ | $-4.2$ | $-1.7$ | $-1.2$ | $-0.8$ | -3.2 |
| 6 | -0.6 | $-0.6$ | $-1.8$ | $-3.5$ | $-3.0$ | $-4.5$ | -3.5 | $-2.0$ | -2.5 | $-0.8$ | $-0.4$ | $-0.4$ | -2.0 |
| 7 | $-0.3$ | 0.3 | $-0.4$ | $-1.1$ | $-1.0$ | -2.4 | $-1.5$ | $-0.5$ | $-0.6$ | 0.0 | 0.1 | $-0.1$ | $-0.6$ |
| 8 | 0.1 | 0.6 | 0.9 | 0.7 | 0.9 | 0.0 | 0.3 | 1.0 | 1.0 | 0.7 | 0.6 | 0.2 | 0.6 |
| 9 | 0.4 | 1.0 | 1.7 | 2.0 | 2.3 | 1.8 | 1.9 | 2.4 | 1.8 | 1.3 | 1.0 | 0.4 | 1.5 |
| 10 | 0.6 | 1.3 | 2.3 | 3.2 | 3.5 | 3.6 | 3.3 | 3.3 | 2.7 | 1.9 | 1.3 | 0.5 | 2.3 |
| 11 | 0.7 | 1.5 | 2.6 | 4.1 | 4.5 | 5.0 | 4.2 | 4.3 | 3.4 | 2.4 | 1.5 | 0.8 | 2.9 |
| 6. 6 | 0.6 | 0.9 | 1.0 | 1.2 | 0.9 | 0.9 | 0.5 | 1.7 | 1.4 | 1.3 | 0.8 | 0.5 | 0.9 |
| 7. 7 | 0.8 | 1.2 | 1.6 | 1.6 | 0.8 | 0.3 | 0.5 | 1.4 | 1.7 | 1.4 | 0.9 | 0.7 | 1.1 |
| 8. 8 | 0.8 | 1.1 | 1.7 | 1.3 | 0.7 | 0.0 | 0.1 | 0.9 | 1.5 | 1.1 | 0.8 | 0.8 | 0.9 |
| 9. 9 | 0.7 | 0.8 | 0.9 | 0.5 | 0.1 | -0.3 | $-0.0$ | 0.4 | 0.7 | 0.6 | 0.7 | 0.6 | 0.5 |
| 10.10 | 0.4 | 0.4 | 0.2 | 0.0 | $-0.2$ | $-0.4$ | $-0.4$ | $-0.1$ | $-0.1$ | -0.0 | 0.4 | 0.2 | 0.0 |
| 7.2.9 | -0.2 | $-0.3$ | $-0.2$ | -0.6 | $-0.9$ | -1.2 | $-0.8$ | $-0.7$ | $-0.4$ | $-0.2$ | -0.3 | $-0.1$ | $-0.5$ |
| 6. 2. 8 | $-0.3$ | $-0.8$ | $-0.3$ | $-0.5$ | $-0.7$ | -0.7 | -0.6 | $-0.4$ | $-0.3$ | -0.2 | -0.4 | $-0.2$ | $-0.4$ |
| 6. 2.10 | $-0.2$ | $-0.1$ | 0.1 | 0.3 | 0.2 | 0.5 | 0.4 | 0.3 | 0.3 | 0.2 | $-0.1$ | $-0.1$ | 0.1 |
| 6. 2. 6 | -0.6 | $-0.7$ | $-1.2$ | $-1.9$ | -1.9 | $-2.2$ | $-1.9$ | $-1.4$ | -1.4 | $-0.7$ | $-0.7$ | $-0.4$ | -1.3 |
| 7. 2 | -0.5 | -0.9 | -1.1 | -1.9 | -2.5 | -2.8 | -2.1 | -2.2 | $-1.5$ | $-1.0$ | -0.9 | $-0.4$ | -1.5 |
| 8. 2 | -0.7 | $-1.1$ | -1.6 | -3.1 | $-3.6$ | $-4.3$ | -3.3 | -3.4 | -2.5 | $-1.7$ | -1.3 | $-0.5$ | -2.3 |
| 8. 1 | -0.7 | $-1.1$ | -1.6 | $-2.9$ | $-3.5$ | $-4.0$ | -3.4 | -3.3 | -2.5 | $-1.9$ | -1.3 | $-0.5$ | $-2.2$ |
| 7. 1 | $-0.5$ | $-0.9$ | $-1.1$ | -1.8 | $-2.4$ | -2.6 | $-2.1$ | -2.1 | $-1.5$ | -1.4 | $-0.9$ | $-0.4$ | -1.5 |
| 9.12.3.9 | -0.8 | -1.3 | -2.1 | $-3.3$ | -3.4 | -4.1 | -3.2 | -3.2 | $-2.9$ | -1.9 | -1.2 | -0.7 | -2.4 |

Prussia. - Halle. Lat. $51^{\circ} 30^{\prime}$ N. Long. $11^{\circ} 57^{\prime}$ E. Greenu.
Corrections to be applied to the Means of the Hours of Olservation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb | March | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.53 | 1.00 | 1.36 | 2.52 | 3.98 | 3.91 | 3.72 | 3.32 | 2.70 | 2.01 | 0.95 | 0.46 | 2.21 |
| 2 | 0.56 | 1.14 | 1.58 | 2.86 | 4.10 | 3.94 | 3.82 | 3.57 | 2.99 | 2.22 | 0.97 | 0.48 | 2.35 |
| 3 | 0.60 | 1.26 | 1.74 | 3.00 | 3.78 | 3.62 | 3.56 | 3.56 | 3.12 | 2.37 | 1.01 | 0.50 | 2.34 |
| 4 | 0.66 | 1.34 | 1.82 | 2.94 | 43.10 | 2.95 | 2.97 | 3.27 | 3.02 | 2.41 | 1.03 | 0.54 | 2.17 |
| 5 | 0.72 | 1.36 | 1.72 | 2.62 | 2.18 | 2.09 | 2.14 | 2.64 | 2.62 | 2.25 | 1.00 | 0.55 | 1.82 |
| 6 | 0.72 | 1.30 | 1.42 | 1.98 | 1.30 | 1.18 | 1.24 | 1.90 | 1.97 | 1.90 | 0.92 | 0.55 | 1.37 |
| 7 | 0.65 | 1.10 | 0.94 | 1.07 | 0.32 | 0.25 | 0.23 | 0.84 | 0.98 | 1.32 | 0.74 | 0.55 | 0.75 |
| 8 | 0.36 | 0.53 | 0.20 | 0.03 | $-0.56$ | $-0.58$ | -0.6 | -0 | 0.12 | 0.33 | 0.30 | 0.25 | 0.02 |
| 9 | 0.05 | 0.08 | -0.66 | -0.9 | -1.34 | -1.34 | $-1.30$ | $-1.20$ | -1.14 | $-0.71$ | -0.31 | -0.09 | $-0.76$ |
| 10 | $-0.45$ | -0.7 | -1.1 | -1. | -2.09 | $-2.01$ | $-1.99$ | -2.10 | $-2.03$ | -1.66 | $-0.87$ | $-0.54$ | $-1.46$ |
| 11 | -0.82 | $-1.29$ | -1.7 | 2. | -2.66 | $-2.68$ | -2.65 | $-2.90$ | $-2.72$ | $-2.44$ | $-1.35$ | $-0.90$ | $-2.06$ |
| Noon | $-1.09$ | -1.7\% | $-2.0$ | -3.08 | $-3.14$ | 7 | -3.16 | -3.35 | $-3.11$ | $-2.86$ | -1.66 | -1.08 | $-2.45$ |
| 1 | $-1.17$ | -2.02 | $-2.22$ | -3.32 | -3.33 | $-3.35$ | $-3.46$ | $-3.53$ | -3.30 | $-3.01$ | $-1.73$ | -1.09 | $-2.63$ |
| 2 | -1.06 | -1.86 | $-2.10$ | -3.26 | -3.37 | $-3.46$ | -3.54 | $-3.57$ | -3.27 | $-2.76$ | $-1.52$ | $-0.9$ | $-2.56$ |
| 3 | -0.8 | -1.49 | -1.86 | $-2.90$ | -3.13 | -3.23 | -3.29 | $-3.30$ | -2.98 | $-2.32$ | -1.14 | -0.74 | $-2.27$ |
| 4 | $-0.53$ | $-1.01$ | $-1.42$ | $-2.39$ | . 74 | 74 | -2.76 | -2.84 | -2.50 | $-1.81$ | $-0.75$ | $-0.42$ | -1.83 |
| 5 | -0.30 | -0.59 | -0.91 | -1.78 | -2.24 | -2.22 | $-2.1$ | -1.97 | - | -1.20 | -0.40 | $-0.20$ | 1.82 |
| 6 | -0.13 | -0.29 | $-0.52$ | -0.9 | -1.55 | -1.50 | -1.39 | -1.38 | -1.12 | -0.69 | -0.14 | -0.03 | -0.51 |
| 7 | -0. | 0.0 | $-0.0$ |  | 86 | -0.73 | -0.55 | -0.59 | $-0.38$ | $-0.21$ | 0.04 | 0.09 | $-0.31$ |
| 8 | 0.11 | 0.13 | 0.26 | 0.32 | $-0.10$ | 0.07 | 0.26 | 0.15 | 0.29 | 0.25 | 0.21 | 0.22 | -0.18 |
| 9 | 0.21 | 0.30 | 0.59 | 0.58 | 0.68 | 0.90 | 1.09 | 0.90 | 0.87 | 0.68 | 0.39 | 0.34 | 0.65 |
| 10 | 0.31 | 0.46 | 0.79 | 1.33 | 1.64 | 1.s] | 1.87 | 1.61 | 1.42 | 1.12 | 0.59 | 0.37 | 1.11 |
| 11 | 0.41 | 0.6 | 0.98 | 1.78 | 2.61 | 2.69 | 2.64 | 2.30 | 1.90 | 1.47 | 0.76 | 0.40 | 1.55 |
| Midn. . | 0.48 | 0.83 | 1.16 | 2.17 | 3.43 | 3.42 | 3.29 | 2.86 | 2.33 | 1.77 | 0.89 | 0.43 | .92 |
| 6. | 0.21 | 0.39 | 0.41 | 0.42 | $-0.03$ | $-0.07$ | $-0.01$ | 0.34 | 0.40 | 0.53 | 0.30 | 0.18 | 0.26 |
| 7. 7 | 0.30 | 0.51 | 0.45 | 0.51 | -0.14 | $-0.16$ | $-0.08$ | 0.26 | 0.43 | 0.61 | 0.39 | 0.28 | 0.28 |
| 8. 8 | 0.33 | 0.51 | 0.44 | 0.3 | -0.27 | $-0.24$ | $-0.16$ | 0.13 | 0.30 | 0.56 | 0.39 | 0.32 | 0.22 |
| 9. 9 | 0.24 | 0.33 | 0.23 | 0.18 | $-0.33$ | $-0.26$ | $-0.16$ | $-0.03$ | 0.21 | 0.29 | 0.26 | 0.25 | 0.10 |
| 10.10 | 0.13 | 0.11 | $-0.04$ | -0.05 | -0.33 | -0.22 | -0.11 | -0.15 | $-0.14$ | $-0.02$ | 0.04 | 0.13 | $-0.05$ |
| 7.2. 9 | -0.11 | $-0.20$ | $-0.18$ | $-0.34$ | $-0.71$ | $-0.70$ | -0.65 | $-0.49$ | $-0.35$ | $-0.29$ | $-0.20$ | $-0.10$ | $-0.36$ |
| 6. 2. 8 | $-0.15$ | $-0.25$ | $-0.19$ | $-0.3 .5$ | $-0.67$ | $-0.66$ | $-0.62$ | $-0.19$ | $-0.35$ | $-0.32$ | -0.2: | -0.15 | $-0.37$ |
| 6. 2.10 | $-0.08$ | $-0.12$ | 0.03 | 0.06 | -0.16 | -0.12 | -0.08 | $-0.00$ | 0.06 | -0.03 | $-0.11$ | -0.0 | -0.05 |
| 6.2. 6 | -0.25 | $-0.12$ | -0.47 | -0.83 | $-1.13$ | -1.16 | $-1.16$ | $-0.95$ | -0.84 | -0. | -0.38 | 0.2 | $-0.71$ |
| 7. 2 | $-0.23$ | $-0.36$ | $-0.40$ | $-0.67$ | -1.02 | -1.09 | -1.1 | -0.82 | -0. | -0. | -0.41 | $-0.2$ | $-0.69$ |
| 8. 2 | $-0.26$ | $-0.46$ | $-0.64$ | $-1.13$ | -1.51 | $-1.55$ | $-1.62$ | -1.3. | -1.1 | -0. 5 | 0.5 | -0.2 | -0.94 |
| 8. 1 | $-0.22$ | $-0.34$ | $-0.56$ | -1.01 | $-1.41$ | -1.41 | $-1.47$ | -1.2 | -1.0 | $-0.77$ | . 4 | -0. | -0.85 |
| 7. 1 | -0.19 | $-0.24$ | -0.32 | -0.55 | $-0.92$ | -0.95 | $-0.96$ | $-0.73$ | -0.57 | -0.43 | $-0.37$ | -0.25 | $-0.54$ |
| 9.12.3.9 | -0.35 | $-0.62$ | -0.8 | -1.37 | -1.67 | -1.66 | -1.6 | -1 | -1.4 | -1.16 | $-0.59$ | $-0.34$ | -1. 10 |
| 7. $2.2(9)$ | -0.06 | $-0.12$ | $-0.07$ | $-0.18$ | $-0.56$ | -0.51 | $-0.4$ | $-0.3$ | -0.19 | $-0.1$ | 0.10 | -0.0 | $-0.23$ |
| Dail.ext. | $-0.23$ | $-1.38$ | $-0.20$ | $-0.16$ | 0.37 | 0.24 | 0.14 | 0.00 | $-0.09$ | $-0.30$ | -0.35 | -0.26 | -0.14 |

IIanover. - Göttingen. Lat. $51^{\circ} 32^{\prime} \mathrm{N}$. Long. $9^{\circ} 56^{\prime}$ E. Greemu.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.90 | 1.13 | 1.58 | 2.24 | 3.31 | 3.43 | 3.56 | 3.35 | 2.31 | 1.58 | 0.69 | 0.60 | 2.06 |
| 2 | 0.92 | 1.14 | 1.77 | 2.49 | 3.70 | 3.71 | 3.82 | 3.70 | 2.68 | 1.75 | 0.74 | 0.59 | 2.25 |
| 3 | 0.94 | 1.16 | 2.01 | 2.79 | 3.93 | 3.73 | 3.92 | 3.92 | 3.23 | 1.94 | 0.52 | 0.58 | 2.41 |
| 4 | 0.99 | 1.20 | 2.22 | 3.04 | 3.91 | 3.57 | 3.79 | 3.89 | 3.63 | 2.10 | 0.92 | 0.58 | 2.49 |
| 5 | 1.15 | 1.26 | 2.29 | 3.08 | 3.55 | 3.10 | 3.36 | 3.52 | 3.62 | 2.15 | 1.00 | 0.62 | 2.39 |
| 6 | 1.12 | 1.20 | 2.10 | 2.73 | 2.62 | 2.22 | 2.59 | 2.79 | 3.50 | 1.99 | 1.08 | 0.66 | 2.05 |
| 7 | 1.13 | 1.14 | 1.77 | 2.24 | 1.75 | 1.21 | 1.40 | 1.69 | 2.62 | 1.58 | 0.94 | 0.65 | 1.51 |
| 8 | 1.12 | 0.80 | 1.02 | 0.89 | 0.75 | 0.49 | 0.48 | 0.56 | 1.36 | 1.08 | 0.53 | 0.54 | 0.80 |
| 9 | 0.50 | -0.0s | -0.14 | -0.16 | -0.47 | -0.55 | -0.65 | -0.68 | -0.22 | -0.21 | 0.10 | 0.30 | -0.19 |
| 10 | -0.37 | -0.88 | -1.09 | -1.32 | -1.53 | -1.60 | -2.22 | -1.84 | -1.45 | -0.82 | -0.42 | -0.02 | -1.13 |
| 11 | -1.26 | -1.78 | -1.57 | -2.30 | -2.59 | -2.53 | -2.74 | -2.83 | -2.45 | -1.74 | -0.99 | -0.74 | -1.99 |
| Noon. | -1.83 | -2.17 | -2.43 | -2.98 | -3.30 | -3.19 | -3.48 | -3.52 | -3.37 | -2.50 | -1.46 | -1.12 | -2.61 |
| 1 | -2.02 | -2.32 | -2.81 | -3.37 | -3.82 | -3.72 | -3.78 | -3.82 | -3.80 | -2.89 | -1.58 | $-1.42$ | 2.95 |
| 2 | -2.03 | -2.23 | -3.05 | -3.56 | -3.98 | -4.03 | -4.09 | -4.15 | -4.00 | -2.98 | -1.60 | -1.28 | -3.08 |
| 3 | -1.74 | -1.98 | -2.88 | -3.48 | -3 95 | -3.91 | -4.00 | $-4.03$ | -4.03 | -2.84 | -1.32 | 1.02 | 2.93 |
| 4 | -1.23 | -1.35 | -2.48 | -3.24 | -3.67 | -3.65 | -3.82 | -3.71 | -3.62 | -2.40 | -0.90 | -0.66 | 2.56 |
| 5 | -0.79 | -0.59 | -1.79 | -2.64 | -3.13 | -3.09 | -3.18 | -3.15 | -2.94 | -1.74 | -0.54 | -0.36 | 2.00 |
| 6 | -0.33 | -0.04 | -1.06 | -1.86 | -2.40 | -2.20 | -2.40 | -2.32 | -1.97 | -0.94 | -0.23 | -0.14 | $-1.32$ |
| 7 | -0.05 | 0.31 | -0.26 | -0.50 | -1.44 | -1.16 | -1.30 | -1.09 | -0.87 | $-0.30$ | 0.01 | 0.06 | -0.57 |
| 8 | 0.24 | 0.58 | 0.34 | 0.04 | 0.22 | -0.15 | 0.03 | 0.13 | 0.05 | 0.24 | 0.17 | 0.20 | 0.14 |
| 9 | 0.40 | 0.82 | 0.78 | 0.77 | 0.88 | 0.79 | 1.09 | 1.05 | 0.78 | 0.71 | 0.30 | 0.30 | 0.72 |
| 10 | 0.57 | 0.94 | 1.05 | 1.30 | 1.59 | 1.73 | 1.87 | 1.62 | 1.28 | 1.02 | 0.42 | 0.10 | 1.15 |
| 11 | 0.71 | 1.01 | 1.30 | 1.75 | 2.29 | 2.69 | 2.62 | 2.26 | 1.71 | 1.35 | 0.56 | 0.44 | 1.56 |
| Midn. | 0.58 | 1.07 | 1.54 | 2.11 | 2.52 | 3.01 | 3.18 | 2.93 | 2.00 | 1.44 | 0.62 | 0.56 | 1.22 |
| 6. 6 | 0.40 | 0.58 | 0.52 | 0.44 | 0.11 | 0.01 | 0.10 | 0.24 | 0.77 | 0.53 | 0.43 | 0.26 | 0.37 |
| 7. 7 | 0.54 | 0.73 | 0.76 | 0.72 | 0.17 | 0.03 | 0.05 | 0.30 | 0.88 | 0.64 | 0.48 | 0.36 | 0.47 |
| 8. 8 | 0.68 | 0.69 | 0.68 | 0.47 | 0.27 | 0.17 | 0.26 | 0.35 | 0.71 | 0.66 | 0.35 | 0.37 | 0.47 |
| 9. 9 | 0.45 | 0.37 | 0.32 | 0.31 | 0.21 | 0.12 | 0.22 | 0.19 | 0.28 | 0.25 | 0.20 | 0.30 | 0.27 |
| 10.10 | 0.10 | 0.03 | -0.02 | -0.01 | 0.03 | . 07 | -0.19 | -0.11 | -0.09 | 0.10 | -0.00 | 0.19 | 0.01 |
| 7. 2. 9 | -0.17 | -0.09 | -0.17 | -0.18 | -0.44 | -0.68 | -0.53 | $-0.47$ | -0.20 | -0.23 | -0.12 | -0.11 | -0.28 |
| 6. 2.8 | -0.22 | -0.15 | $-0.20$ | -0.26 | $-0.53$ | -0.65 | -0.49 | -0.41 | -0.15 | -0.25 | -0.12 | -0.14 | -0.30 |
| 6. 2.10 | -0.11 | -0.03 | 0.03 | 0.16 | 0.05 | -0.03 | 0.12 | 0.09 | 0.26 | 0.01 | -0.03 | -0.07 | 0.04 |
| 6. 2.6 | -0.41 | -0.36 | -0.67 | -0.90 | -1.25 | -1.34 | $-1.30$ | -1.23 | -0.82 | -0.64 | -0.25 | -0.25 | -0.79 |
| 7. 2 | -0.45 | -0.5.5 | -0.64 | -0.66 | -1.10 | -1.41 | -1.35 | -1.23 | $-0.69$ | -0.70 | $-0.33$ | $-0.32$ | -0.79 |
| 8. 2 | $-0.46$ | -0.72 | -1.02 | -1.34 | -1.62 | -1.77 | -1.81 | -1.80 | -1.32 | -0.95 | -0.54 | -0. | -1.14 |
| 8. 1 | -0.45 | -0.76 | $-0.90$ | -1.24 | $-1.54$ | -1.62 | -1.65 | -1.63 | -1.22 | -0.91 | -0.53 | -0. | 1.07 |
| 7. 1 | -0.45 | -0.59 | -0.5 | 0.57 | -1.02 | -1.26 | -1.19 | -1.07 | -0.59 | -0.66 | -0.32 | -0.39 | -0.72 |
| 9.12.3.9 | -0.67 | -0.85 | -1.17 | . | -1.71 | . | -1.76 | -1.80 | -1.71 | -1.21 | 0.60 | 0.39 | 1.25 |
| 7. $2.2(9)$ | -0.03 | 0.14 | 0.07 | 0.06 | -0.11 | -0.31 | -0.13 | -0.09 | 0.05 | 0.01 | -0.02 | -0.01 | -0.03 |
| Dail. ext. | -0.44 | -0.53 | -0.38 | -0.24 | -0 | -0.15 | -0.09 | -0.12 | -0.20 | -0.42 | -0.26 | -0.38 | -0.30 |

The numbers without sign must be added; those with the sign - must be subtracted.

## LVII.

Prussia. - Berlin. Lat. $52^{\circ} 30^{\prime}$ N. Long. $13^{\circ} 24^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.


## LVIII.

Germany. - Salzuflen. Lat. $52^{\circ} 5^{\prime} \mathrm{N}$. Long. $8^{\circ} 40^{\prime}$ E. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Lec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.00 | 1.10 | 1.0.5 | 2.11 | 2.41 | 2.57 | 2.0 .5 | 1.71 | 2.12 | 1.24 | 0.90 | 0.31 | 1.46 |
| 2 | 0.5 .5 | 1.22 | 1.20 | 2.44 | 2.93 | 2.85 | 2.27 | 2.01 | 2.44 | 1.55 | 1.26 | 0.48 | 1.77 |
| 3 | 0.60 | 1.27 | 1.34 | 2.64 | 3.29 | 2.98 | 2.39 | 2.23 | 2.74 | 1.82 | 1.53 | 0.65 | - 1.96 |
| 4 | 0.62 | 1.26 | 1.38 | 2.62 | 3.37 | 2.86 | 2.32 | 2.26 | 2.87 | 1.98 | 1.64 | 0.78 | 2.00 |
| 5 | 0.72 | 1.18 | 1.29 | 2.35 | 3.08 | 2.47 | 1.99 | 2.00 | 2.71 | 1.97 | 1.58 | 0.83 | 1.85 |
| 6 | 0.62 | 1.01 | 1.06 | 1.80 | 2.41 | 1.53 | 1.42 | 1.45 | 2.18 | 1.75 | 1.37 | 0.79 | 1.48 |
| 7 | 0.51 | 0.75 | 0.70 | 1.05 | 1.45 | 1.02 | 0.70 | 0.79 | 1.34 | 1.34 | 1.04 | 0.64 | 0.94 |
| 8 | 0.31 | 0.41 | 0.25 | 0.20 | 0.38 | 0.15 | -0.06 | 0.08 | 0.30 | 0.75 | 0.62 | 0.38 | 0.31 |
| 9 | 0.08 | -0.03 | -0.22 | -0.63 | -0.59 | -0.67 | $-0.74$ | -0.54 | -0.65 | 0.09 | 0.14 | 0.06 | -0.31 |
| 10 | -0.33 | $-0.53$ | -0.68 | $-1.36$ | -1.42 | -1.35 | -1.15 | $-1.02$ | -1.47 | -0.63 | -0.35 | -0.2 4 | -0.88 |
| 11 | -0.74 | $-1.02$ | -1.06 | -1.93 | -1.96 | -1.94 | -1.62 | -1.38 | -2.08 | -1.27 | -0.02 | -0.48 | -1.29 |
| Noon. | -0.91 | -1.42 | -1.39 | -2.32 | -2.31 | -2.39 | -1.90 | $-1.72$ | -2.41 | -1.78 | -1.18 | -0.62 | -1.70 |
| 1 | -1.01 | $-1.65$ | -1.59 | -2.54 | -2.53 | -2.72 | -2.13 | -2.03 | -2.75 | -2.09 | -1.48 | -0.64 | -1.93 |
| 2 | -0.94 | $-1.74$ | -1.65 | -2.60 | -2.66 | -2.91 | -2.30 | -2.30 | -2.90 | -2.18 | -1.56 | -0.58 | -2.03 |
| 3 | -0.79 | $-1.58$ | -1.56 | -2.49 | $-2.72$ | -2.92 | -2.36 | -2.12 | -2.90 | -2.06 | -1.46 | -0.50 | -1.98 |
| 4 | -0.50 | $-1.29$ | -1.33 | -2.21 | -2.65 | -2.71 | $-2.24$ | -2.30 | -2.70 | -1.76 | -1.22 | -0.41 | -1.78 |
| 5 | -0.20 | -0.90 | -0.98 | -1.77 | -2.39 | -2.26 | -1.89 | -1.87 | -2.25 | -1.34 | -0.92 | -0.35 | -1.43 |
| 6 | -0.10 | $-0.51$ | $-0.56$ | $-1.22$ | -1.94 | -1.62 | $-1.32$ | -1.22 | -1.55 | -0.90 | -0.6. | -0.32 | -0.99 |
| 7 | 0.01 | -0.17 | -0.15 | -0.62 | -1.34 | -0.56 | -0.62 | 0.47 | -0.71 | -0.47 | -0.44 | -0.30 | -0.51 |
| 8 | 0.08 | 0.11 | 0.19 | -0.04 | -0.65 | -0.09 | 0.09 | 0.21 | 0.12 | -0.11 | -0.31 | -0.27 | -0.06 |
| 9 | 0.14 | 0.34 | 0.45 | 0.48 | 0.04 | 0.62 | 0.70 | 0.71 | 0.81 | 0.18 | -0.20 | -0.21 | 0.34 |
| 10 | 0.21 | 0.55 | 0.63 | 0.94 | 0.68 | 1.22 | 1.26 | 1.03 | 1.30 | 0.42 | -0.06 | -0.12 | 0.67 |
| 11 | 0.22 | 0.74 | 0.77 | 1.34 | 1.27 | 1.74 | 1.52 | 1.25 | 1.61 | 0.66 | 0.18 | 0.01 | 0.94 |
| Midn. | 0.40 | 0.93 | 0.90 | 1.74 | 1.84 | 2.18 | 1.50 | 1.45 | 1.86 | 0.94 | 0.50 | 0.15 | 1.22 |
| 6. 6 | 0.26 | 0.25 | 0.25 | 0.29 | 0.24 | 0.11 | 0.0 .5 | 0.13 | 0.32 | 0.43 | 036 | 0.24 | 0.24 |
| 7. 7 | 0.26 | 0.29 | 0.29 | 0.22 | 0.06 | 0.08 | 0.04 | 0.16 | 0.32 | 0.44 | 0.30 | 0.17 | 0.22 |
| 8. 8 | 020 | 0.26 | 0.22 | 0.08 | -0.14 | 0.03 | 0.02 | 0.15 | 0.21 | 0.32 | 0.16 | 0.06 | 0.13 |
| 9. 9 | 0.11 | 0.16 | 0.12 | -0.08 | -0.2s | -0.03 | -0.02 | 0.09 | 0.08 | 0.14 | -0.03 | -0.08 | 0.02 |
| 10.10 | -0.06 | 0.01 | $-0.03$ | -0.21 | -0.37 | -0.08 | 0.06 | 0.01 | -0.09 | -0.11 | -0.21 | -0.18 | -0.11 |
| 7. 2. 9 | -0.10 | -0.22 | -0.17 | -0.36 | -0.39 | -0.42 | -0 30 | -0.27 | -0.25 | -0.22 | -0.24 | -0.0.5 | -0.25 |
| 6. 2. 8 | -0.08 | -0.21 | -0.13 | -0.28 | -0.30 | $-0.39$ | -0.26 | $-0.20$ | -0.20 | -0.1s | -0.17 | -0.02 | -0 20 |
| 6. 2.10 | -0.0. 4 | -0.06 | 0.01 | 0.05 | 0.14 | 0.05 | 0.13 | 007 | 0.19 | -0.00 | -0.08 | 0.03 | 0.04 |
| 6. 2. 6 | -0.14 | -0.41 | -0.38 | -0.67 | -0.73 | -0.90 | -0.73 | -0.68 | -0.76 | -0.44 | -0.28 | -0.04 | -0.51 |
| 7. 2 | -0.22 | -0.50 | $-0.48$ | -0.78 | -0.61 | -0.9.) | -0.80 | $-0.76$ | -0.7s | -0.42 | -0.26 | 0.03 | -0.54 |
| 8. 2 | -0.32 | -0.67 | -0.70 | -1.20 | -1.14 | -1.38 | -1.18 | -1.11 | -1.30 | $-0.72$ | -0.47 | -0.10 | -0.86 |
| 8. 1 | -0.3.5 | -0.64 | -0.67 | -1.17 | -1.08 | -1.29 | -1.10 | -0.98 | -1.23 | -0.67 | -0.43 | -0.13 | -0.81 |
| 7. 1 | -0.25 | -0.47 | -0.45 | -0.75 | -0.54 | -0.85 | -0.72 | -0.62 | -0.71 | -0.38 | -0.22 | -0.00 | -0.50 |
| 9.12.3.9 | -0.37 | -0.67 | -0.68 | -1.24 | -1.40 | -1.34 | -1.08 | -0.99 | -1.29 | -0.89 | -0.68 | -0.32 | -0.91 |
| 7. $2.2(9)$ | -0.04 | -0.08 | -0.01 | -0.15 | $-0.28$ | -0.16 | -0.05 | -0.02 | 0.02 | -0.12 | -0.23 | -0.09 | -0.10 |
| Dail.ext. | -0.15 | -0.24 | -0.14 | 0.02 | 0.33 | 0.03 | 0.02 | -0.08 | -0.02 | -0.10 | 0.04 | 0.10 | -0.02 |

Prussia. - Stettin. Lat. $53^{\circ} 25$ N. Long. $14^{\circ} 34^{\prime}$ E. Greemb.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | Feb | Mareb. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Noy. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midnight. | 0.26 | 0.54 | 0.98 | 1.66 | 2.21 | 2.21 | 1.83 | 1.93 | 1.53 | 0.95 | 0.50 | 0.39 | 1.24 |
| 1 | 0.35 | 0.59 | 1.17 | 1.91 | 2.66 | 2.46 | 2.25 | 2.24 | 1.61 | 1.01 | 0.44 | 0.46 | 1.43 |
| 2 | 0.4.3 | 0.70 | 1.30 | 2.15 | 3.03 | 2.84 | 2.62 | 2.54 | 1.87 | 1.13 | 0.47 | 0.50 | 163 |
| 3 | 0.49 | 0.85 | 1.41 | 2.39 | 3.39 | 3.10 | 2.95 | 2.83 | 2.11 | 1.24 | 0.51 | 0.56 | 1.99 |
| 4 | 0.53 | 0.89 | 1.51 | 2.60 | 3.55 | 3.08 | 3.07 | 3.05 | 2.33 | 1.33 | 0.55 | 0.61 | 1.92 |
| 5 | 0.57 | 0.97 | 1.63 | 2.67 | 3.45 | 2.75 | 2.55 | 3.10 | 2.46 | 1.40 | 0.55 | 0.64 | 1.92 |
| 6 | 0.55 | 0.94 | 1.62 | 2.10 | 2.78 | 2.12 | 2.21 | 2.78 | 2.45 | 1.42 | 0.60 | 0.56 | 1.70 |
| 7 | 0.46 | 0.83 | 1.37 | 1.70 | 1.63 | 1.17 | 1.31 | 2.02 | 1.95 | 1.25 | 0.52 | 0.46 | 1.23 |
| S | 0.36 | 0.66 | 0.90 | 0.69 | 0.33 | 0.20 | 0.35 | 0.96 | 1.11 | 0.79 | 0.4 \% | 0.38 | 0.59 |
| 9 | 0.22 | 0.36 | 0.23 | -0.4 | -0.58 | -0.72 | -0.53 | -0.26 | -0.05 | 0.16 | 0.13 | 0.23 | -0.13 |
| 10 | -0.04 | -0.02 | -0.44 | -1.36 | -1.87 | -1.54 | -1.33 | -1.40 | -1.1] | -0.5.j | -0.22 | -0.03 | -0 83 |
| 11 | -0.36 | $-0.53$ | $-1.06$ | -2.07 | $-2.62$ | 2.18 | $-1.96$ | -2.23 | -1.96 | -1.2; | -0.60 | -0.3.5 | $-1.43$ |
| Noon. | -0.63 | -0.93 | -1.59 | -2.50 | -3.09 | -2.59 | -2.46 | -2.93 | -2.58 | -1.68 | -0.90 | -0.64 | -1.ss |
| 1 | -0.81 | -1.26 | $-1.92$ | -2.80 | -3.36 | -2.90 | -2.81 | -3.88 | -2.88 | $-1.9 \bigcirc$ | -1.06 | -0.86 | -2.17 |
| 2 | -0.90 | 1.33 | -2.08 | -2.9 | -3.50 | -2.99 | -2.99 | -3.50 | -2.99 | -2.06 | -1.06 | -0.94 | -2.28 |
| 3 | -0.75 | -1.34 | $-2.06$ | -2.94 | -3.35 | $-2.90$ | -2.80 | -3.38 | -2.52 | . 68 | -0.9 | -0.56 | -2.16 |
| 4 | -0.63 | 1.15 | 1.8 | -2.54 | -2.99 | -2.99 | -2.60 | -3.03 | -2.44 | -i. 43 | -0.65 | -0.70 | -1.92 |
| 5 | -0.41 | -0.83 | -1.43 | -2.02 | $-2.46$ | -2.46 | $-2.15$ | $-2.40$ | -1.55 | -0.99 | -0.39 | -0.48 | -1.49 |
| 6 | -0.25 | -0.46 | -0.90 | $-1.32$ | 1.74 | -1.74 | -1.62 | -1.68 | -1.14 | -0.46 | -0.19 | -0.30 | -0.98 |
| 7 | -0.11 | -0.23 | -0.40 | -0.55 | -0.s9 | -0.69 | $-0.93$ | -0.75 | -0.52 | -0.10 | $-0.00$ | -0.15 | -0.46 |
| 8 | 0.01 | -0.01 | -0.02 | 0.10 | -0.14 | -0.14 | -0.17 | 0.02 | 0.06 | 0.17 | 0.15 | -0.06 | -0.00 |
| 9 | 0.08 | 0.16 | 0.32 | 0.65 | 0.73 | 0.73 | 0.65 | 0.74 | 0.60 | 0.39 | $0 .: 0$ | 0.07 | 0.31 |
| 10 | 0.20 | 0.30 | 0.61 | 1.10 | 1.30 | 1.30 | 1.03 | 1.20 | 1.00 | 0.58 | 0.43 | 0.22 | 0.77 |
| 11 | 0.25 | 0.42 | 0.79 | 1.42 | 1.76 | 1.76 | 1.47 | 1.60 | 1.31 | 0.74 | 0.50 | 0.32 | 1.03 |
| 6, 6 | 0.15 | 0.24 | 0.36 | 0.54 | 0.52 | 0.19 | 0.29 | 0.55 | 0.6 .5 | 0.48 | 0.21 | 0.13 | 0.36 |
| 7, 7 | 0.17 | 0.30 | 0.18 | 0.57 | 0.37 | 0.14 | 0.19 | 0.62 | 0.73 | 0.57 | 0.26 | 0.14 | 0.35 |
| s, s | 0.19 | 0.31 | 0.44 | 0.38 | 0.10 | 0.03 | 0.09 | 0.19 | 0.59 | 0.45 | 0.31 | 0.16 | 0.30 |
| 9, 9 | 0.15 | 0.26 | 0.25 | 0.13 | -0.05 | 0.01 | -0.03 | 0.24 | 0.28 | 0.25 | 0.22 | 0.15 | 0.16 |
| 10, 10 | 0.08 | 0.14 | 0.09 | -0.13 | -0.29 | -0.12 | -0.15 | -0.10 | -0.06 | 0.02 | 0.11 | 0.10 | -0.03 |
| 7, 1 | -0.17 | -0.21 | -0.67 | -0.55 | -0.86 | -0.86 | -0.75 | -0.65 | -0.45 |  | -0.27 | -0.20 | -0.50 |
| 7, 2, 9 | -0.13 | -0.13 | -0.13 | -0.19 | -0.38 | -0.36 | -0.10 | -0.25 | -0.1 | -0.11 | -0.08 | -0.14 | -0.21 |
| 6, 2, 10 | -0.05 | -0.05 | 0.38 | 0.19 | 0.19 | 0.14 | 0.08 | 0.16 | 0.15 | -0.02 | -0.01 | -0.05 | 0.09 |
| Daily ext. | $-0.16$ | -0.21 | -0.23 | -0.14 | 0.04 | 0.06 |  | -0.20 | -0.27 | -0.32 | -0.23 | -0.15 | -0.15 |

The numbers without sign must be added : those with the sigu - must be subtracted.

Sleswick. - Apenrade. Lat. $55^{\circ} 3^{\prime}$ N. Lomg. $9^{\circ} 25^{\prime}$ E. Greenw.
Corrections to be applied to the Mcans of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of licaumur.

| Hours. | $J_{\text {dan }}$ | Feb. | Ma, | April. | May. | June. | July. | Ang. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.26 | 0.69 | 0.98 | 1.73 | 3.18 | 3.82 | 2.50 | 2.61 | 2.16 | 1.06 | 0.54 | 0.31 | 1.65 |
| 2 | 0.31 | 0.78 | 1.14 | 1.83 | 317 | 3.90 | 2.38 | 2.66 | 2.29 | 1.19 | 0.59 | 0.35 | 1.72 |
| 3 | 0.38 | 0.79 | 1.26 | 1.98 | 3.02 | 3.82 | 2.13 | 2.66 | 2.54 | 1.30 | 0.61 | 0.37 | 1.74 |
| 4 | 0.42 | 0.75 | 1.34 | 2.10 | 2.71 | 3.50 | 1.78 | 2.64 | 2.62 | 1.37 | 0.66 | 0.38 | 1.69 |
| 5 | 0.44 | 0.69 | 1.31 | 2.02 | 2.22 | 2.89 | 1.35 | 2.18 | 2.13 | 1.36 | 0.69 | 0.40 | 1.50 |
| 6 | 0.50 | 0.62 | 1.18 | 1.63 | 1.54 | 1.94 | 0.86 | 1.56 | 2.02 | 1.25 | 0.69 | 0.40 | 1.18 |
| 7 | 0.17 | 0.54 | 0.90 | 1.15 | 0.70 | 0.83 | 0.30 | 0.77 | 1.15 | 0.97 | 0.61 | 0.37 | 0.73 |
| 8 | 0.39 | 0.38 | 0.50 | 0.41 | -0.23 | -0.34 | -0.29 | -0.15 | 0.18 | 0.52 | 0.42 | 0.27 | 0.17 |
| 9 | 0.23 | 0.10 | -0 | -0.12 | -1.14 | -1.38 | -0.87 | $-1.10$ | -0.88 | -0.10 | 0.10 | 0.10 | -0.44 |
| 10 | -0.06 | -0.32 | -0.66 | -1.22 | -1.90 | -2.16 | $-1.10$ | -1.98 | -1.71 | -0.79 | -0.30 | -0.15 | -1.00 |
| 11 | -0.36 | -0.75 | -1.15 | -1.90 | $-2.19$ | $-2.66$ | -1.80 | $-2.42$ | -2.38 | -1.35 | -0.68 | -0.43 | -1.41 |
| Noon. | -0.62 | -1.19 | -1.62 | $-2.42$ | $-2.86$ | -2.98 | -2.09 | -2.74 | $-2.79$ | -1.94 | -0.98 | -0.66 | -1.91 |
| 1 | -0.78 | -1.40 | -1.90 | -2.75 | -3.08 | -3.24 | -2.23 | -2.89 | -3.03 | -2.15 | -1.10 | -0.78 | $-2.11$ |
| 2 | -0.69 | -1.34 | $-1.96$ | -2.59 | -3.16 | -3.19 | -2.27 | -2.90 | -3.08 | $-2.07$ | -1.02 | -0.75 | -2.14 |
| 3 | -0.61 | -1.06 | -1.78 | -2.79 | -3.10 | -3 68 | -2.21 | -2.78 | -2.93 | -1.74 | -0.82 | -0.59 | -2.01 |
| 4 | -0.38 | -0.64 | -1.41 | -2.43 | -2.56 | $-3.62$ | -2.02 | -2.39 | -2.54 | -1.23 | -0.59 | -0.38 | -1.71 |
| 5 | -0.16 | -0.23 | -0.92 | -1.80 | -2.40 | -3.34 | -1.70 |  | 93 | -0.71 | -0.29 | -0.15 | -1.30 |
| 6 | -0.03 | 0.0 .5 | -0.42 | $-0.99$ | -1.70 | -2.57 | -1.18 | -1. | -1.13 | -0.25 | -0.12 | 0.02 | -0.80 |
| 7 | 0.01 | 0.18 | 0.02 | -0.12 | -0.79 | -1.12 | -0.57 | -0.47 | -0.26 | 0.10 | 0.02 | 0.10 | $-0.27$ |
| 8 | 0.03 | 0.18 | 0.33 | 0.66 | 0.22 | -0.07 | 0.18 | 0.40 | 0.56 | 0.34 | 0.03 | 0.14 | 0.25 |
| 9 | 0.01 | 0.17 | 0.54 | 1.2.) | 1.22 | 1.25 | 0.97 | 1.21 | 1.21 | 0.51 | 0.09 | 0.15 | 0.71 |
| 10 | 0.02 | 0.22 | 0.66 | 1.57 | 2.05 | 2.33 | 1.63 | 1.72 | 1.61 | 0.65 | 0.18 | 0.18 | 1.07 |
| 11 | 0.07 | 0.33 | 0.76 | 1.69 | 2.66 | 3.10 | 2.14 | 2.25 | 1.83 | 0.5 .5 | 0.30 | 0.21 | 1.35 |
| Midn. | 0.15 | 0.52 | 0.86 | 1.70 | 3.02 | 3.57 | 2.43 | 1.68 | 1.97 | 0.92 | 0.42 | 0.26 | 1.46 |
| 6. 6 | 0.24 | 0.34 | 0.38 | 0.32 | -0.05 | -0.32 | -0.16 | 0.17 | 0.15 | 0.50 | 0.29 | 0.21 | 0.19 |
| 7. 7 | 0.24 | 0.36 | 0.16 | .52 | -0 0.5 | -0.30 | -0 14 | 0.15 | 0.16 | 0.54 | 0.30 | 0.24 | 0.23 |
| 8. 8 | 0.21 | 0.28 | 0.12 | 0.54 | -0.0.1 | -0.21 | -0.06 | 0.11 | 0.37 | 0.43 | 0.2 | 0.21 | 0.21 |
| 9. 9 | 0.11 | 0.14 | 0.26 | $0 .+2$ | 0.04 | -0.07 | 0.0 .5 | 0.06 | 0.19 | 0.21 | 0.10 | 0.13 | 0.14 |
| 10.10 | -0.02 | -0.05 | -0.00 | 0.18 | 0.08 | 0.09 | 0.12 | -0.13 | -0.05 | -0.07 | -0.06 | 0.02 | 0.01 |
| 7. 2. 9 | -0.08 | -0.21 | -0.17 | -0.16 | -0.41 | -0.47 | -0.33 | $-0.31$ | -0.23 | -0.20 | -0.11 | -0.08 | -0.23 |
| 6. 2.8 | -0.0.5 | -0.15 | -0.15 | -0.20 | $-0.47$ | $-0.54$ | -0.41 | $-0.31$ | -0.17 | $-0.16$ | -0.10 | -0.07 | -0.23 |
| 6. 2.10 | -0.06 | -0.17 | -0.04 | 0.10 | 0.14 | 0.26 | 0.07 | 0.13 | 0.18 | -0.06 | -0.05 | -0.06 | 0.04 |
| 6. 2. 6 | $-0.07$ | $-0.22$ | -0.40 | $-0.75$ | -1.11 | -1.37 | -0 86 | -0.86 | $-0.73$ | -0.36 | -0.15 | -0.11 | -0.5s |
| 7. 2 | -0.11 | -0.40 | -0.53 | -0.87 | -1. 23 | -1.33 | -0.99 | -1.07 | -0.9.) | -0.55 | -0.21 | -0.19 | -0.70 |
| 8. 2 | -0.1.5 | -0.48 | $-0.73$ | -1.24 | -1.70 | -1.92 | -1.28 | -1.54 | -1.45 | -0.78 | -0.30 | -0.21 | -0.98 |
| 8. 1 | $-0.20$ | -0.51 | -0.70 | $-1.17$ | -1.66 | -1.79 | -1.26 | -1.54 | -1.43 | -0.82 | -0.34 | -0.26 | -0.97 |
| 71 | -0.16 | -0.43 | $-0.50$ | -0.50 | -1.19 | $-1.21$ | -0.97 | -1.06 | -0.93 | -0.59 | -0.25 | -0.21 | -0.69 |
| 9.12.3.7 | -0.2.5 | -0.50 | -0.72 | -1.10 | -1.47 | $-1.70$ | -1.0.) | -1.35 | -1.34 | -0.82 | -0.40 | -0.25 | -0.91 |
| 7. 2.2(9) | -0.06 | -0.12 | 0.01 | 0.19 | 0.01 | $-0.04$ | -0.01 | 0.07 | 0.13 | -0.02 | -0.06 | -0.02 | 0.01 |
| Dail.ext. | -0.14 | -0.31 | -0.31 | -0.40 | 0.01 | 0.11 | 0.12 | -0.12 | -0.23 | -0.39 | -0.21 | -0.19 | -0.20 |

The numbers without sign must be added; those with the sign - must be subtracted.

Scotland. - Leith. Lat. $55^{\circ} 59^{\prime}$ N. Long. $3^{\circ} 10^{\prime}$ E. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Fahrenheit.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.38 | 0.56 | 1.76 | 3.02 | 3.04 | 3.29 | 4.10 | 2.95 | 2.54 | 1.10 | 1.26 | 0.72 | 2.09 |
| 2 | 0.61 | 0.77 | 1.98 | 3.92 | 3.47 | 3.62 | 4.28 | 3.20 | 2.77 | 1.19 | 1.53 | 0.65 | 2.33 |
| 3 | 0.6 S | 0.77 | 2.41 | 4.57 | 3.96 | 3.74 | 4.66 | 3.49 | 3.29 | 1.31 | 1.40 | 0.61 | 2.57 |
| 4 | 0.95 | 0.95 | 2.59 | 5.31 | 4.41 | 3.98 | 5.11 | 3.71 | 3.65 | 1.33 | 1.46 | 0.70 | 2.84 |
| 5 | 1.06 | 1.17 | 2.75 | 5.49 | 4.28 | 3.94 | 4.59 | 3.65 | 3.78 | 1.62 | 1.37 | 0.77 | 2.87 |
| 6 | 1.06 | 1.31 | 2.75 | 5.36 | 3.51 | 3.04 | 3.56 | 3.26 | 3.51 | 2.03 | 1.28 | 0.59 | 2.61 |
| 7 | 0.97 | 1.24 | 2.48 | 3.47 | 2.66 | 2.25 | 2.39 | 2.25 | 2.75 | 1.62 | 1.06 | 0.68 | 1.98 |
| 8 | 0.88 | 1.26 | 1.80 | 2.18 | 1.40 | 1.10 | 1.15 | 1.08 | 1.46 | 0.97 | 1.04 | 0.54 | 1.24 |
| 9 | 0.61 | 0.77 | 0.81 | $-0.27$ | 0.11 | -0.18 | $-0.23$ | $-0.50$ | $-0.14$ | 0.32 | 0.56 | 0.32 | 0.18 |
| 10 | 0.16 | $-0.07$ | 0.18 | -2.00 | -1.06 | -1.31 | $-1.37$ | $-1.26$ | $-1.10$ | $-0.83$ | -0.34 | $-0.02$ | -0.75 |
| 11 | $-0.34$ | $-0.97$ | $-1.22$ | $-3.02$ | $-2.00$ | $-2.30$ | $-2.25$ | $-2.03$ | -2.21 | $-1.71$ | $-1.33$ | $-0.56$ | -1.69 |
| Noo | -1.04 | -1.69 | $-2.61$ | -3.92 | -2.75 | -2.79 | -3.58 | -2.99 | $-3.13$ | -2.36 | -1.96 | $-1.3$ | 2.51 |
| 1 | $-1.42$ | -2.25 | $-2.97$ | $-4.37$ | $-3.35$ | $-3.15$ | $-3.67$ | -3.44 | -3.92 | $-2.79$ | -2.30 | -1.51 | -2.93 |
| 2 | $-1.55$ | -2.23 | -3.29 | $-4.73$ | $-3.78$ | -3.83 | $-4.07$ | $-3.65$ | -4.28 | $-2.84$ | -2.57 | -1.55 | $-3.20$ |
| 3 | $-1.60$ | $-2.27$ | $-3.35$ | $-5.09$ | $-3.85$ | $-4.37$ | $-4.37$ | -3.65 | $-4.16$ | $-2.57$ | $-2.63$ | $-1.13$ | $-3.26$ |
| 4 | -1.19 | $-1.73$ | -3.33 | $-4.79$ | $-4.19$ | $-3.94$ | $-4.46$ | -3.87 | -3.56 | $-1.96$ | -1.69 | $-0.83$ | -2.96 |
| 5 | -0.68 | -0.9.) | $-2.84$ | $-4.25$ | $-4.03$ | -3.71 | $-4.57$ | -3.76 | -3.56 | $-1.31$ | $-1.04$ | $-0.50$ | -2.60 |
| 6 | $-0.45$ | -0.47 | -2.14 | $-3.83$ | $-3.51$ | $-3.29$ | $-4.41$ | $-3.47$ | $-2.30$ | $-0.59$ | $-0.65$ | -0.27 | $-2.12$ |
| 7 | -0.09 | $-0.09$ | $-1.17$ | -2.45 | $-2.61$ | $-2.52$ | $-3.58$ | -1.69 | $-0.97$ | 0.05 | $-0.25$ | 0.18 | $-1.27$ |
| 8 | 0.14 | 0.32 | $-0.45$ | -0.81 | $-1.17$ | -0.79 | $-1.31$ | $-0.41$ | $-0.16$ | 0.59 | 0.05 | 0.29 | -0.31 |
| 9 | 0.23 | 0.61 | 0.25 | 0.38 | 0.32 | 0.50 | 0.43 | 0.59 | 0.59 | 0.72 | 0.32 | 0.36 | 0.44 |
| 10 | 0.1 | 0.8 | 0.77 | 1.08 | 0.86 | 1.8 | 1.71 | 1.58 | 1.24 | 1.15 | 0.79 | 0.41 | 1.04 |
| 11 | 0.32 | 0.9 | 1.31 | 2.1 | 1.69 | 2.1 | 2.52 | 2.23 | 1.67 | 1.60 | 1.19 | 0.54 | 1.53 |
| Midn. | 0.38 | 1.01 | 1.44 | 2.68 | 2.32 | 2.6 S | 3.44 | 2.77 | 2.27 | 1.49 | 1.42 | 0.59 | 1.87 |
| 6. 6 | 0.32 | 0.43 | 0.34 | 0.77 | 0.00 | -0.14 | $-0.43$ | $-0.11$ | 0.61 | 0.72 | 0.32 | 0.16 | 0.25 |
| 7. 7 | 0.45 | 0.59 | 0.65 | 0.52 | 0.02 | $-0.14$ | -0.61 | 0.29 | 0.90 | 0.83 | 0.41 | 0.43 | 0.36 |
| 8. 8 | 0.52 | 0.79 | 0.68 | 0.70 | 0.11 | 0.16 | -0.09 | 0.34 | 0.65 | 0.79 | 0.54 | 0.43 | 0.47 |
| 9. 9 | 0.43 | 0.70 | 0.54 | 0.07 | 0.23 | 0.16 | 0.11 | 0.05 | 0.23 | 0.52 | 0.45 | 0.34 | 0.32 |
| 10.10 | 0.18 | 0.41 | 0.47 | $-0.47$ | $-0.11$ | 0.29 | 0.18 | 0.16 | 0.07 | 0.16 | 0.23 | 0.20 | 0.15 |
| 7. 2. 9 | $-0.14$ | $-0.14$ | -0.18 | $-0.29$ | $-0.27$ | -0.36 | $-0.43$ | $-0.27$ | $-0.32$ | $-0.16$ | -0.41 | -0.18 | $-0.26$ |
| 6. 2. 8 | $-0.14$ | $-0.20$ | $-0.32$ | $-007$ | $-0.47$ | $-0.52$ | $-0.61$ | $-0.27$ | $-0.32$ | $-0.07$ | -0.41 | $-0.23$ | $-0.30$ |
| 6. 2.10 | -0.11 | $-0.02$ | 0.09 | 0.56 | 0.20 | 0.36 | 0.11 | 0.41 | 0.16 | 0.11 | -0.16 | $-0.18$ | 0.15 |
| 6. 2. 6 | $-0.32$ | $-0.47$ | $-0.88$ | $-1.06$ | $-1.26$ | $-1.35$ | $-1.64$ | $-1.28$ | $-1.01$ | $-0.47$ | -0.65 | $-0.41$ | -0.90 |
| 7. 2 | -0.32 | $-0.50$ | $-0.41$ | $-0.63$ | $-0.56$ | $-0.79$ | $-0.86$ | $-0.70$ | $-0.77$ | -0.61 | $-0.77$ | $-0.15$ | -0.61 |
| 8. 2 | -0.36 | $-0.50$ | $-0.74$ | $-1.28$ | -1.19 | $-1.37$ | -1.46 | -1.28 | $-1.42$ | -0.95 | -0.77 | $-0.5$ | -0.99 |
| 8. 1 | -0.27 | $-0.50$ | $-0.59$ | $-1.10$ | $-0.99$ | $-1.04$ | -1.26 | $-1.19$ | -1.24 | $-0.92$ | $-0.63$ | $-0.50$ | -0.85 |
| 7. 1 | $-0.23$ | -0.52 | $-0.25$ | $-0.45$ | $-0.36$ | $-0.45$ | -0.65 | $-0.61$ | $-0.59$ | $-0.59$ | $-0.63$ | 0.41 | -0.47 |
| \%.12.3.9 | $-0.45$ | $-0.65$ | $-1.24$ | -2.23 | -1.55 | -1.71 | $-1.94$ | $-1.64$ | -1.71 | $-0.97$ | -0.92 | $-0.45$ | -1.29 |
| 7. $2.2(9)$ | $-0.05$ | 0.07 | $-0.09$ | $-0.14$ | $-0.14$ | $-0.16$ | $-0.20$ | $-0.07$ | $-0.09$ | 0.07 | -0.23 | $-0.05$ | -0.09 |
| Dail. ext. | $-0.27$ | -0.49 | $-0.29$ | 0.20 | -0.11 | -0.20 | 0.27 | -0.09 | $-0.25$ | $-0.40$ | -0.56 | $-0.40$ | -0: 0 |

## LXII.

Scotland. - Leith. Lat. $55^{\circ} 59^{\prime}$ N. Long. $3^{\circ} 10^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of lieaumur.

| Hours. | Jan. | Feb. | Narch. | April. | Nay. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.17 | 0.38 | 0.78 | 1.34 | 1.35 | 1. 16 | 1.82 | 1.31 | 1.13 | 0.49 | 0.56 | 0.32 | 0.93 |
| 2 | 0.27 | 0.34 | 0.68 | 1.74 | 1.54 | 161 | 1.90 | 1.42 | 1.23 | 0.53 | 0.68 | 0.29 | 1.04 |
| 3 | 0.30 | 0.34 | 1.07 | 2.033 | 1.76 | 1.66 | 2.07 | 15.5 | 1.46 | 0.58 | 0.62 | 0.97 | 1.14 |
| 4 | 0.42 | 0.42 | 1.15 | 2.36 | 1.96 | 1.77 | 2.27 | 1.65 | 1.62 | 0.59 | 0.65 | 0.31 | 1.26 |
| 5 | 0.47 | 0.52 | 1.22 | 2.44 | 1.90 | 1.75 | 2.04 | 1.62 | 1.68 | 0.72 | 0.61 | 0.34 | 1.28 |
| 6 | 0.47 | 0.58 | 1.24 | 2.38 | 1.56 | 1.35 | 1.55 | 1.45 | 1.56 | 0.90 | 0.57 | 0.26 | 1.16 |
| 7 | 0.43 | 0.55 | 1.10 | 1.54 | 1.18 | 1.00 | 1.06 | 1.00 | 1.22 | 0.72 | 0.47 | 0.30 | 0.58 |
| 8 | 0.39 | 0.56 | 0.80 | 0.97 | 0.62 | 0.19 | 0.51 | 0.48 | 0.65 | 0.43 | 0.46 | 0.24 | 0.55 |
| 9 | 0.27 | 0.34 | 0.86 | $-0.12$ | 0.05 | -0.0s | -0 | $-0.22$ | -0.06 | 0.14 | 0.25 | 0.14 | 0.08 |
| 10 | 0.07 | $-0.03$ | 0.08 | $-0.89$ | -0.47 | $-0.58$ | -0.61 | $-0.56$ | $-0.49$ | $-0.37$ | -0.15 | $-0.01$ | $-0.33$ |
| 11 | -0.15 | $-0.43$ | $-0.54$ | $-1.34$ | -0.89 | $-1.02$ | $-1.00$ | $-0.90$ | $-0.98$ | $-0.76$ | -0.59 | -0.38 | $-0.75$ |
| No | $-0.46$ | $-0.75$ | $-1.16$ | $-1.74$ | $-1.22$ | $-1.24$ | $-1.59$ | -1.83 | $-1.39$ | $-1.05$ | -0.87 | $-0.59$ | -1.12 |
| 1 | -0.63 | $-1.00$ | -1.32 | -1.94 | $-1.49$ | -1 | -1.63 | -1.53 | -1 | -1.24 | -1.02 | -0.67 | $-1.30$ |
| 2 | -0.70 | -0.99 | $-1.16$ | $-2.10$ | -1.68 | -1.70 | -1.81 | $-1.62$ | -1.90 | -1.26 | -1.14 | -0.69 | $-1.42$ |
| 3 | -0.71 | -1.01 | $-1.50$ | $-2.26$ | -1.71 | -1.94 | -1.94 | -1.62 | -1.85 | $-1.14$ | $-1.17$ | $-0.50$ | 5 |
| 4 | $-0.53$ | -0.77 | $-1.18$ | -2.13 | -1.86 | $-1.75$ | -1.98 | $-1.72$ | -1.58 | -0.87 | -0.75 | $-0.37$ | $-1.32$ |
| 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | -0 |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | $-0.20$ | $-0.21$ | $-0.95$ | -1.70 | $-1.56$ | -1. 46 | -1.96 | $-1.54$ | -1.02 | -0.26 | $-0.30$ | $-0.12$ | -0.94 |
| 7 | -0.04 | -0.0.4 | $-0.52$ | -1.09 | $-1.16$ | $-1.12$ | $-1.59$ | $-0.75$ | $-0.43$ | 0.02 | $-0.11$ | 0.08 | $-0.56$ |
| 8 | 0.06 | 0.14 | $-0.20$ | $-0.36$ | $-0.52$ | $-0.3$ | -0.5s | -0.18 | $-0.07$ | 0.26 | 0.02 | 0.13 | $-0.14$ |
| 9 | 0.10 | 0.27 | 0.11 | 0.17 | 0.14 | 0.22 | 0.19 | 0.26 | 0.26 | 0.32 | 0.14 | 0.16 | 0.20 |
| 10 | 0.08 | 0.39 | 0.34 | 0.45 | 0.38 | 0.84 | 0.76 | 0.70 | 0.5.5 | 0.51 | 0.35 | 0.18 | 0.46 |
| 11 | 0.14 | 0.44 | 0.58 | 0.97 | 0.75 | 0.96 | 1.12 | 0.99 | 0.74 | 0.71 | 0.53 | 0.24 | 0.68 |
| Midn. . | 0.17 | 0.45 | 0.64 | 1.19 | 1.03 | 1.19 | 1.53 | 1.23 | 1.01 | 0.66 | 0.63 | 0.26 | 0.83 |
| 6. 6 | 0.14 | 0.19 | 0.15 | 0.34 | 0.00 | $-0.06$ | -0.19 | -0.05 | 0.27 | 0.32 | 0.14 | 0.07 | 0.11 |
| 7. 7 | 0.2 | 0.2 | 0.29 | 0.23 | 0.01 | -0.06 | $-0.27$ | 0.13 | 0.40 | 0.37 | 0.18 | 0.19 | 0.16 |
| S. 8 | 0.2 | 0.3 | 0.30 | 0.31 | 0.05 | 0.07 | -0.04 | 0.15 | 0.29 | 0.35 | 0.24 | 0.19 | 0.21 |
| 9. 9 | 0.19 | 0.31 | 0.24 | 0.03 | 0.10 | 0.07 | 0.05 | 0.02 | 0.10 | 0.23 | 0.20 | 0.15 | 0.14 |
| 10.10 | 0.08 | 0.18 | 21 | $-0.21$ | $-0.05$ | 0.13 | 0.08 | 0.07 | 0.03 | 0.07 | 0.10 | 0.09 | 0.06 |
| 7. 2. 9 | -0.06 | -0.0 | -0.08 | $-0.13$ | $-0.1$ | -0.16 | $-0.19$ | $-0.12$ | -0.14 | $-0.07$ | -0.18 | $-0.08$ | $-0.12$ |
| 6. 2. S | -0.0 | O.0 | -0.14 | -0. | -0.2] | $-0.23$ | -0.27 | $-0.12$ | $-0.14$ | -0.03 | $-0.18$ | $-0.10$ | $-0.13$ |
| 6. 2.10 | -0 | -0.01 | 0.04 | 0.25 | 0.09 | 0.16 | 0.15 | 0.18 | 0.07 | 0.05 | $-0.07$ | -0.08 | 0.07 |
| 6.2. 6 | $-0.14$ | -0.21 | -0.39 | -0.47 | $-0.56$ | $-0.60$ | $-0.73$ | $-0.57$ | $-0.45$ | $-0.21$ | $-0.29$ | -0.18 | -0.10 |
| 7. | -0. | 0.2 | -0. | -0.28 | -0.25 | -0.35 | -0.38 | -0.31 | $-0.34$ | -0.27 | -0.34 | $-0.20$ | -0. 27 |
| 8. 2 | $-0.16$ | $-0.22$ | -0.33 | -0.57 | -0.53 | -0.61 | -0.65 | -0.57 | -0.63 | $-0.12$ | $-0.34$ | -0.23 | -0.44 |
| 8. 1 | -0.12 | -0.22 | -0.26 | -0.49 | $-0.44$ | $-0.46$ | -0.56 | $-0.53$ | -0.55 | -0.41 | -0.28 | -0.22 | -0.38 |
| 7. 1 | -0.10 | $-0.23$ | -0.11 | $-0.20$ | -0.16 | $-0.20$ | -0.29 | -0.27 | $-0.26$ | $-0.26$ | -0.28 | -0.18 | -0.21 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9.12.3.9 | -0.20 | $-0.29$ | -0.55 | -0.99 | -0.69 | $-0.76$ | -0.86 | $-0.73$ | $-0.76$ | -0.43 | -0.41 | 0.20 | 0.57 |
| 7. $2.2(9)$ | $-0.02$ | 0.03 | $-0.04$ | $-0.06$ | $-0.06$ | $-0.07$ | -0.09 | -0.03 | $-0.04$ | 0.03 | -0.10 | -0.02 | -0.04 |
| Dail.ext. | -0.12 | -0.22 | $-013$ | 0.09 | 0.05 | $-0.09$ | 0.12 | -0.04 | -0.11 | -0.18 | -0.25 | $-0.18$ | -0.09 |

The numbers without sign must be added; those with the sign - must be subtracted.

Scotland. - Makerstoun. Lat. $55^{\circ} 36^{\prime}$ N. Long. $2^{\circ} 31^{\prime}$ W. Gr.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.67 | 0.88 | 1.24 | 2.30 | 2.00 | 2.25 | 2.10 | 1.98 | 1.95 | 0.88 | 0.46 | 0.24 | 1.41 |
| 1 | 0.76 | 0.92 | 1.37 | 2.52 | 2.04 | 2.43 | 2.44 | 2.24 | 2.15 | 0.88 | 0.46 | 0.16 | 1.53 |
| 2 | 0.78 | 1.08 | 1.37 | 2.70 | 2.33 | 2.54 | 2.57 | 2.38 | 2.26 | 1.06 | 0.60 | 0.18 | 1.65 |
| 3 | 0.76 | 1.06 | 1.48 | 2.79 | 2.55 | 2.65 | 2.79 | 2.56 | 2.35 | 1.57 | 0.60 | 0.29 | 1.79 |
| 4 | 0.67 | 1.01 | 1.66 + | 2.96 | 2.51 | 2.43 | 2.70 | 2.56 | 2.48 | 1.20 | 0.68 | 0.40 | 1.77 |
| 5 | 0.75 | 0.92 | 1.77 | 2.88 | 2.06 | 1.96 | 2.21 | 2.44 | 2.46 | 1.40 | 0.60 | 0.44 | 1.66 |
| 6 | 0.60 | 0.85 | 1.73 | 2.25 | 1.31 | 1.12 | 1.35 | 1.78 | 2.22 | 1.31 | 0.66 | 0.51 | 1.31 |
| 7 | 0.31 | 0.99 | 1.26 | 1.43 | 0.48 | 0.32 | 0.46 | 0.91 | 1.24 | 1.26 | 0.66 | 0.44 | 0.83 |
| 8 | 0.53 | 0.79 | 0.46 | 0.36 | -0.25 | -0.51 | -0.39 | -0.09 | 0.00 | 0.62 | 0.66 | 0.40 | 0.22 |
| 9 | 0.33 . | 0.08 | -0.33 | -0.79 | -0.94 | -1.11 | -0.96 | $-1.02$ | -1.00 | -0.16 | 0.08 | 0.22 | -0.47 |
| 10 | -0.22 | -0.72 | -1.12 | -1.86 | -1.52 | -1.68 | -1.59 | -1.78 | -1.92 | -0.96 | -0.47 | -0.20 | $-1.17$ |
| 11 | -0.84 | -1.21 | -1.67 | -2.55 | -2.09 | -2.26 | -2.14 | -2.33 | -2.45 | -1.63 | -0.94 | -0.62 | $-1.73$ |
| Noon. | -1.36 | -1.61 | -2.09 | -3.06 | -2.31 | -2.48 | -2.45 | -2.73 | -2.67 | -2.03 | -1.34 | -0.93 | -2.09 |
| 1 | -1.71 | -2.03 | -2 27 | -3.44 | -2.69 | -2.75 | -2.48 | -2.87 | -3.03 | -2.25 | -1.56 | $-1.13$ | -2.35 |
| 2 | -1.67 | -2.05 | -2.36 | -3.57 | -2.65 | $-2.57$ | -2.52 | -2.93 | -3.12 | -2.20 | -1.47 | $-0.96$ | -2.34 |
| 3 | -1.29 | -1.68 | -2.32 | -3.52 | -2.65 | -2.28 | -2.54 | -2.73 | -2.55 | -1.83 | -0.96 | -0.60 | -2.10 |
| 4 | -0.71 | -1.30 | -1.80 | -3.0.5 | -2.27 | -1.95 | -2.23 | -2.47 | -2.29 | -1.23 | -0.45 | -0.16 | $-1.66$ |
| 5 | -0.13 | -0.50 | $-1.20$ | -2.30 | -1.76 | -1.64 | -1.81 | -1.78 | -1.49 | -0.49 | -0.07 | -0.11 | -1.11 |
| 6 | 0.18 | -0.08 | -0 40 | -1.39 | -0.98 | -0.9.5 | -1.34 | -1.07 | -0.60 | -0.09 | 0.13 | 0.18 | -0.53 |
| 7 | 0.29 | 0.15 | 0.08 | -0.19 | -0.18 | -0.40 | -0.59 | -0.18 | 0.06 | 0.17 | 0.17 | 0.18 | -0.04 |
| 8 | 0.31 | 0.37 | 0.16 | 0.52 | 0.62 | 0.36 | 0.35 | 0.56 | 0.46 | 0.40 | 0.25 | 0.15 | 0.41 |
| 9 | 0.29 | 0.52 | 0.73 | 1.21 | 1.15 | 1.00 | 0.95 | 1.09 | 0.95 | 0.64 | 0.37 | 0.24 | 0.76 |
| 10 | 0.27 | 0.64 | 0.95 | 1.74 | 1.46 | 1.56 | 1.48 | 1.58 | 1.33 | 0.73 | 0.46 | 0.31 | 1.04 |
| 11 | 0.22 | 0.79 | 1.06 | 2.08 | 1.77 | 1.94 | 1.70 | 1.89 | 1.51 | 0.73 | 0.40 | 0.36 | 1.20 |
| Mean. | 1.53 | 0.35 | 206 | 5.96 | 6.56 | 10.25 | 10.12 | 10.00 | 8.51 | 6.64 | 4.60 | 1.16 |  |

## LXIV.


Degrees of Reanmur.

| Hour. | Jan. | Fel. | Mareh. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A.M. 1 | 0.53 | 0.53 | 1.56 | 2.18 | 2.53 | 2.76 | 2.18 | 2.22 | 1.64 | 1.16 | 0.53 | 0.36 | 1.52 |
| 3 | 0.80 | 0.71 | 1.64 | 2.40 | 2.89 | 3.11 | 2.53 | 2.10 | 1.87 | 1.42 | 0.67 | 0.49 | 1.74 |
| 5 | 0.93 | 0.98 | 1.64 | 2.49 | 2.31 | 2.18 | 2.18 | 2.53 | 1.57 | 1.73 | 0.76 | 0.55 | 1.68 |
| 7 | 0.81 | 0.93 | 1.35 | 0.58 | -0.22 | -0.59 | -0.36 | 0.40 | 1.07 | 1.56 | 0.20 | 0.53 | 0.56 |
| 9 | 0.36 | 0.18 | -0.31 | -1.11 | -1.24 | -1.38 | -1.10 | -1.16 | -0.76 | -0.09 | 0.27 | 0.36 | -0.50 |
| 11 | -0.98 | -0.07 | -1.82 | $-2.40$ | -2.18 | -2.09 | -2.04 | -2.27 | -2.13 | -1.91 | -0.98 | -0.71 | -1.71 |
| P.M. 1 | -1.60 | -1.78 | -2.67 | -2.93 | -2.62 | -2.40 | -2.27 | -2.62 | -2.67 | -2.44 | -1.56 | -1.16 | -2.23 |
| 3 | $-1.33$ | -1.47 | -2.44 | -2.84 | -2.71 | -2.31 | -2.27 | -2 49 | -2.22 | -2.04 | -1.11 | -0.67 | -1.99 |
| 5 | -0.44 | 0.14 | -1.29 | -1.82 | -1.82 | -1.57 | -1.64 | -1.73 | -1.29 | -0.84 | -0.27 | -0.18 | -1.14 |
| 7 | 0.09 | 0.18 | 0.18 | 0.04 | -0.27 | -0.44 | -0.27 | -0.09 | 0.27 | 0.04 | 0.04 | 0.09 | -0.01 |
| 9 | 0.22 | 0.31 | 0.76 | 1.20 | 1.29 | 1.24 | 1.20 | 1.16 | 0.93 | 0.58 | 0.36 | 0.18 | 0.79 |
| 11 | 0.36 | 0.40 | 1.07 | 1.73 | 1.96 | 2.04 | 1.87 | 1.64 | 1.42 | 084 | 0.44 | 0.22 | 1.17 |
| Mean. | 4.09 | 4.75 | 5.10 | 6.66 | 9.51 | 11.86 | 12.48 | 12.31 | 10.79 | 7.73 | 599 | 4.88 |  |

The numbers without sign must be added; those with the sign - must be subtracted.

Russia. - Catharinenburg. Lat. $56^{\circ} 50^{\prime}$ N. Long. $60^{\circ} 34^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.59 | 0.91 | 1.54 | 1.97 | 3.09 | 3.69 | 3.51 | 2.49 | 1.99 | 0.68 | 0.47 | 0.65 | 1.82 |
| 2 | 0.58 | 0.59 | 2.09 | 2.41 | 3.52 | 4.15 | 3.76 | 2.93 | 2.27 | 0.54 | 0.42 | 0.67 | 2.04 |
| 3 | 0.53 | 0.87 | 2.42 | 2.87 | 3.80 | 4.35 | 3.96 | 3.42 | 2.60 | 1.04 | 0.36 | 0.64 | 2.24 |
| 4 | 0.48 | 0.89 | 2.80 | 3.21 | 3.82 | 1.17 | 4.01 | 3.78 | 2.89 | 1.23 | 0.35 | 0.61 | 2.35 |
| 5 | 0.58 | 0.95 | 3.11 | 3.23 | 3.45 | 3.54 | 3.78 | 3.79 | 2.98 | 1.36 | 0.43 | 0.63 | 2.32 |
| 6 | 0.54 | 1.00 | 3.15 | 2.83 | 2.67 | 2.49 | 3.18 | 3.30 | 2.74 | 1.36 | 0.55 | 0.72 | 2.04 |
| 7 | 0.60 | 0.94 | 2.76 | 1.99 | 1.57 | 1.18 | 2.21 | 2.29 | 2.11 | 1.17 | 0.64 | 0.81 | 1.52 |
| 8 | 0.56 | 0.71 | 1.90 | 0.84 | 0.31 | 0.17 | 0.98 | 0.94 | 1.16 | 0.80 | 0.60 | 0.80 | 0.79 |
| 9 | 0.37 | 0.27 | 0.65 | -0.41 | -0.88 | -1.35 | -0.34 | -0.48 | 0.05 | 0.28 | 0.37 | 0.61 | -0.07 |
| 10 | -0.0. | -0.33 | -0.75 | -1.52 | -1.85 | -2.23 | -1.61 | -1.70 | -1.03 | -0.32 | $-0.02$ | 0.21 | -0.93 |
| 11 | -0.60 | -0.97 | -2.03 | -2.34 | -2.53 | -2.79 | -2.72 | -2.55 | -1.93 | -0.89 | -0.49 | -0.34 | -1.68 |
| Noon. | -0.98 | -1.17 | -3.00 | 2.83 | 2.98 | -3.13 | -3.64 | -3.03 | $-2.58$ | -1.34 | -0. 59 | -0.90 | $-2.23$ |
| 1 | $-1.30$ | -1.75 | -3.52 | -3.04 | -3.25 | -3.35 | -4.33 | -3.25 | -2.98 | -1.62 | -1.12 | -1.32 | -2.57 |
| 2 | -1.37 | -1.77 | -3.62 | -3.03 | -3.41 | -3.50 | -4.78 | -3.34 | -3.16 | -1.69 | -1.13 | -1.50 | -2.69 |
| 3 | -1.19 | -1.55 | -3.39 | -2.58 | -3.46 | -3.56 | $-4.90$ | -3.36 | -3.17 | -1.58 | -0.95 | -1.40 | -2.62 |
| 4 | -0.84 | -1.19 | -2.96 | -2.60 | -3.33 | -3.46 | $-4.62$ | -3.27 | -2.98 | $-1.31$ | -0.66 | $-1.10$ | -2.36 |
| 5 | -0.3 4 | -0.79 | -2.40 | -2.18 | -2.93 | -3.09 | $-3.90$ | -2.98 | -2.57 | -0.96 | -0.37 | -0.73 | $-1.94$ |
| 6 | -0.11 | -0.42 | -1.77 | -1.61 | -2.29 | -2.43 | -2.77 | -2.39 | -1.93 | -0.58 | -0.14 | -0.39 | -1.40 |
| 7 | 0.11 | -0.10 | -1.08 | -0.92 | -1.41 | -1.52 | -1.39 | -1.53 | -1.12 | -0.23 | 0.01 | -0.14 | -0.78 |
| 8 | 0.22 | 0.17 | 0.36 | -0.22 | -0.42 | -0.48 | 0.03 | -0.53 | -0.26 | 0.06 | 0.12 | 0.03 | 0.14 |
| 9 | 0.30 | 0.42 | 0.32 | 0.42 | 0.53 | 0.56 | 1.28 | 0.43 | 0.52 | 0.26 | 0.22 | 0.15 | 0.45 |
| 10 | 0.37 | 0.63 | 0.90 | 0.91 | 1.35 | 1.51 | 2.22 | 1.20 | 1.13 | 0.40 | 0.33 | 0.28 | 0.95 |
| 11 | 0.36 | 0.80 | 1.32 | 1.29 | 2.03 | 2.35 | 2.84 | 1.74 | 1.52 | 0.48 | 0.42 | 0.43 | 1.30 |
| Midn. | 0.55 | 0.89 | 1.62 | 1.61 | 2.59 | 3.07 | 3.23 | 2.12 | 1.77 | 0.56 | 0.48 | 0.57 | 1.59 |
| 6. 6 | 0.21 | 0.27 | 0.69 | 0.61 | 0.19 | 0.03 | 0.20 | 0.45 | 0.40 | 0.39 | 0.21 | 0.17 | 0.32 |
| 7. 7 | 0.35 | 0.42 | 0.84 | 0.53 | 0.08 | -0.17 | 0.41 | 0.38 | 0.49 | 0.47 | 0.33 | 0.33 | 0.37 |
| 8. 8 | 0.39 | 0.44 | 0.75 | 0.31 | -0.03 | -0.33 | 0.51 | 0.20 | 0.45 | 0.43 | 0.36 | 0.41 | 0.32 |
| 9. 9 | 0.33 | 0.84 | 0.49 | 0.01 | -0.17 | -0.39 | 0.17 | -0.03 | 0.29 | 0.27 | 0.29 | 0.38 | 0.19 |
| 10.10 | 0.18 | 0.15 | 0.08 | -0.30 | -0.25 | -0.36 | 0.31 | -0.25 | 0.05 | 0.01 | 0.15 | 0.25 | 0.00 |
| 7. 2. 9 | -0.16 | -0.14 | -0.18 | -0.21 | -0.44 | -0.59 | -0.43 | -0.21 | -0.18 | -0.09 | -0.09 | -0.18 | -0.20 |
| 6.2. 8 | -0.20 | -0.20 | -0.28 | -0.14 | -0.39 | -0.50 | $-0.52$ | -0.19 | $-0.23$ | -0.09 | -0.15 | $-0.25$ | -0.26 |
| 6. 2.10 | -0.15 | -0.05 | 0.14 | 0.24 | 0.20 | 0.17 | 0.21 | 0.39 | 0.24 | 0.02 | 0.08 | -0.17 | 0.10 |
| 6. 2. 6 | -0.31 | -0.40 | -0.75 | -0.60 | -0.01 | -1.15 | $-1.46$ | -0.81 | -0.78 | $-0.30$ | -0.24 | -0.39 | -0.68 |
| 7. 2 | -0.3.3 | -0.42 | -0.43 | -0.52 | -0.92 | -1.16 | $-1.29$ | $-0.53$ | -0.53 | $-0.26$ | -0.25 | -0.35 | -0.59 |
| 8. 2 | -0.41 | -0.54 | -0.86 | $-1.10$ | $-1.55$ | -1.84 | -1.90 | $-1.20$ | -1.00 | -0.45 | -0.27 | -0.35 | -0.96 |
| 8. 1 | $-0.37$ | -0.52 | -0.81 | $-1.10$ | -1.47 | -1.76 | -1.68 | -1.16 | -0.91 | -0.41 | -0.26 | -0.26 | -0.89 |
| 7. 1 | -0.35 | -0.41 | -0.38 | $-0.53$ | -0.84 | -1.09 | -1.06 | -0.18 | -0.44 | -0.23 | -0.24 | -0.26 | -0.53 |
| 9.12.3.9 | -0.38 | -0.58 | -1.36 | -1.43 | $-1.70$ | -1.87 | -1.90 | -1.61 | $-1.30$ | $-0.60$ | -0.31 | -0.39 | -1.12 |
| 7. $2.2(9)$ | -0.04 | -0.00 | -0.06 | -0.0.5 | -0.20 | -0.30 | -0.00 | -0.05 | 0.00 | 0.00 | -0.01 | -0.10 | 0.06 |
| Dail.ext. | - 0.39 | -0.39 | -0.24 | 0.10 | 0.18 | 0.40 | -0.45 | 0.22 | 0.17 | -0.17 | -0.25 | -0.35 | -0.17 |

Russia. - Catharinenburg. Lat. $56^{\circ} 50^{\prime}$ N. Long. $60^{\circ} 34^{\prime}$ E. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reammur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.42 | 1.07 | 1.70 | 2.12 | 2.64 | 3.06 | 2.93 | 2.16 | 1.96 | 0.59 | 0.47 | 0.47 | 1.66 |
| 1 | 0.52 | 1.19 | 2.00 | 2.40 | 3.11 | 3.51 | 3.41 | 2.49 | 2.31 | 1.08 | 0.51 | 0.50 | 1.92 |
| 2 | 0.52 | 1.25 | 2.23 | 2.82 | 3.49 | 3.90 | 3.86 | 2.76 | 2.58 | 0.99 | 0.54 | 0.52 | 2.12 |
| 3 | 0.55 | 1.41 | 2.53 | 3.05 | 3.73 | 4.15 | 4.11 | 3.03 | 2.83 | 1.47 | 0.58 | 0.54 | 2.33 |
| 4 | 0.63 | 1.52 | 2.75 | 3.26 | 3.74 | 3.92 | 4.28 | 3.22 | 3.06 | 1.61 | 0.68 | 0.58 | 2.44 |
| 5 | 0.68 | 1.67 | 2.85 | 3.24 | 3.27 | 3.35 | 3.66 | 3.14 | 3.22 | 1.67 | 0.71 | 0.61 | 2.34 |
| 6 | 0.73 | 1.76 | 3.06 | 2.24 | 2.27 | 1.99 | 2.47 | 2.45 | 3.04 | 1. 69 | 0.82 | 0.64 | 1.93 |
| 7 | 0.81 | 1.76 | 2.59 | 1.61 | 0.59 | 0.61 | 1.02 | 1.37 | 2.27 | 1.53 | 0.85 | 0.65 | 1.33 |
| S | 0.83 | 1.51 | 1.46 | 0.34 | $-0.24$ | -0.53 | -0.28 | 0.15 | 0.85 | 0.91 | 0.77 | 0.58 | $0 . .34$ |
| 9 | 0.67 | 0.73 | $-0.06$ | -0.81 | $-1.09$ | -1.46 | -1.45 | $-0.97$ | $-0.57$ | $-0.03$ | 0.33 | 0.39 | $-0.36$ |
| 10 | 0.13 | $-0.45$ | $-1.45$ | -1.99 | $-1.94$ | -2.23 | -2.35 | $-1.72$ | $-1.68$ | $-0.78$ | $-0.22$ | -0.08 | $-1.23$ |
| 11 | $-0.57$ | -1.44 | -2.39 | $-2.62$ | $-2.72$ | -2.93 | -3.10 | $-2.54$ | $-2.50$ | $-1.46$ | $-0.72$ | $-0.71$ | -1.95 |
| Noon. | -1.04 | $-2.13$ | $-2.95$ | -3.09 | -3.19 | -3.33 | $-3.58$ | $-2.99$ | $-3.09$ | $-1.73$ | --1.0:3 | $-1.19$ | $-2.45$ |
| 1 | -1.39 | $-2.58$ | $-3.27$ | -3.22 | -3.23 | $-3.48$ | -3.57 | -3.04 | $-3.32$ | -1.99 | $-1.25$ | -1.4. | -2.65 |
| 2 | -1.50 | $-2.74$ | $-3.38$ | $-3.26$ | $-3.41$ | $-3.59$ | -3.55 | $-3.02$ | $-3.36$ | $-2.02$ | $-1.23$ | $-1.29$ | $-2.70$ |
| 3 | -1.28 | $-2.37$ | -3.18 | $-2.86$ | $-3.14$ | -3.37 | $-3.40$ | $-3.03$ | $-3.48$ | $-2.23$ | $-1.11$ | -1.00 | $-2.54$ |
| 4 | -0.85 | $-1.97$ | $-2.82$ | -2.6.5 | $-2.99$ | $-3.05$ | $-3.15$ | $-2.83$ | $-3.18$ | $-1.61$ | $-0.79$ | -0.6 | $-2.21$ |
| 5 | -0.50 | $-1.28$ | $-2.20$ | $-2.14$ | $-2.60$ | -2.49 | $-2.67$ | $-2.37$ | $-2.48$ | $-0.95$ | -0.47 | $-0.33$ | $-1.71$ |
| 6 | $-0.22$ | $-0.74$ | $-1.37$ | -]. 46 | $-1.98$ | -1.98 | $-2.14$ | -1.66 | $-1.56$ | $-0.56$ | $-0.26$ | -0.1 | -1.17 |
| 7 | 0.00 | $-0.25$ | $-0.67$ | $-0.59$ | $-0.95$ | $-1.17$ | $-1.29$ | $-0.79$ | $-0.65$ | $-0.22$ | $-0.07$ | 0.02 | -0.55 |
| 8 | 0.10 | 0.05 | $-0.12$ | 0.13 | $-0.04$ | $-0.12$ | $-0.16$ | 0.11 | 0.07 | 0.06 | 0.06 | 0.11 | 0.02 |
| 9 | 0.17 | 0.40 | 0.44 | 0.65 | 0.85 | 0.96 | 0.83 | 0.84 | 0.67 | 0.36 | 0.16 | 0.26 | 0.55 |
| 10 | 0.24 | 0.65 | 0.94 | 1.13 | 1.53 | 1.88 | 1.67 | 1.39 | 1.25 | 0.53 | 0.27 | 0.39 | 0.99 |
| 11 | 0.34 | 0.86 | 1.34 | 1.58 | 2.13 | 2.51 | 2.36 | 1.81 | 1.65 | 0.74 | 0.40 | 0.56 | 1.36 |
| Mean. | -10.76 | -9.50 | -5.83 | 0.47 | 6.31 | 12.08 | 14.53 | 10.61 | 6.32 | 1.41 | $-6.11$ | 11.68 |  |
| R | IA. | St. P | Peter | URC |  | LX <br> t. $59^{\circ}$ grees of | VII. <br> $56^{\prime}$ <br> Reaum |  | . 30 | $18^{\prime} \mathrm{F}$ | Gr. | - D |  |
| Hour. | Jan. | Feb. | March. | April. | Nay. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| Midn. | 0.14 | 0.38 | 0.73 | 1.44 | 2.08 | 1.99 | 1.77 | 1.68 | 1.17 | 0.52 | 0.15 | 0.17 | 1.02 |
| 1 | 0.21 | 0.44 | 0.99 | 1.68 | 2.43 | 2.29 | 2.05 | 2.02 | 1.38 | 0.60 | 0.17 | 0.21 | 1.21 |
| 2 | 0.25 | 0.46 | 1.22 | 1.91 | 2.70 | 2.56 | 2.24 | 2.24 | 1.58 | 0.65 | 0.15 | 0.27 | 1.3 .5 |
| 3 | 0.30 | 0.52 | 1.33 | 2.11 | 2.91 | 2.73 | 2.43 | 2.48 | 1.75 | 0.73 | 0.25 | 0.34 | 1.49 |
| 4 | 0.38 | 0.63 | 1.56 | 2.24 | 2.56 | 2.44 | 2.32 | 2.59 | 1.87 | 0.78 | 0.30 | 0.36 | 1.53 |
| 5 | 0.43 | 0.72 | 1.71 | 2.28 | 2.38 | 1.97 | 1.92 | 2.40 | 1.96 | 0.84 | 0.34 | 0.34 | 1.44 |
| 6 | 0.45 | 0.76 | 1.75 | 1.95 | 1.72 | 1.33 | 1.33 | 1.96 | 1.90 | 0.90 | 037 | 0.30 | 1.23 |
| 7 | 0.41 | 0.78 | 1.57 | 1.32 | 0.93 | 0.63 | 0.64 | 1.19 | 1.47 | 0.82 | 0.37 | 0.29 | 0.87 |
| 8 | 0.42 | 0.60 | 1.07 | 0.65 | 0.14 | $-0.04$ | 0.05 | 0.42 | 0.81 | 0.57 | 0.32 | 0.2.5 | 0.44 |
| 9 | 0.35 | 0.40 | 0.40 | -0.05 | $-0.59$ | $-0.69$ | $-0.56$ | $-0.40$ | 0.00 | 0.20 | 0.17 | 0.17 | 0.05 |
| 10 | 0.13 | -0.0. | $-0.19$ | -0.78 | $-1.30$ | $-1.21$ | -1.12 | $-1.07$ | -0.71 | -0.22 | 0.00 | 0.04 | $-0.54$ |
| 11 | $-0.20$ | $-0.48$ | $-0.86$ | -1.42 | -1.92 | -1.71 | -1.58 | -1.64 | -1.27 | $-0.61$ | $-0.20$ | $-0.14$ | -1.00 |

The numbers without sigu must be added ; those with the sign - must be subtracted.

Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | b. | March. | Aprit. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Noon. | -0.38 | -0.90 | -1.31 | -1.93 | -2.30 | -1.99 | -1.89 | -2.10 | $-1.72$ | -0.94 | -0.37 | -0.30 | -1.34 |
| 1 | -0.63 | -0.97 | -1.62 | -2.10 | -2.41 | -2.17 | -2.03 | -2.47 | -2.26 | -1.75 | -0.64 | -0.48 | -1.63 |
| 2 | -0.66 | -1.04 | -1.88 | -2.36 | $-2.65$ | -2.32 | -2.15 | -2.60 | -2.34 | -1.29 | -0.63 | -0.58 | -1.71 |
| 3 | -0.5.5 | -0.99 | -1.94 | -2.49 | -2.90 | -2.45 | -2.29 | -2.64 | $-2.31$ | -1.06 | -0.46 | -0.40 | -1.71 |
| 1 | -0.33 | -0.53 | -1.92 | -2.65 | $-2.92$ | -2.60 | -2.41 | -2.80 | -2.27 | -0.86 | -0.20 | -0.31 | -1.68 |
| 5 | -0.2.5 | -0.45 | -1.53 | -2.31 | -2.4S | -2.23 | -2.06 | -2.45 | $-1.76$ | -0.50 | -0.16 | -0.22 | -1.37 |
| 6 | -0.19 | -0.26 | -1.02 | -1.43 | -1.65 | -1.41 | -1.30 | -1.41 | -0.9 | -0.2.) | -0.11 | -0.14 | -0.84 |
| 7 | -0.15 | -0.16 | $-0.55$ | -0.61 | -0.74 | -0.71 | -0.63 | -062 | -0.35 | -0.09 | $-0.05$ | -0.10 | $-0.10$ |
| 8 | -0.14 | -0.03 | -0.25 | -0.03 | 0.06 | -0.03 | 0.02 | 0.09 | 0.07 | 0.07 | 0.01 | 0.08 | -0.01 |
| 9 | -0.11 | 0.08 | 0.03 | 0.47 | 0.79 | 0.67 | 0.64 | 0.65 | 0.40 | 0.18 | 0.08 | 0.03 | 0.33 |
| 10 | -0.03 | 0.17 | 0.24 | 0.54 | 1.22 | 1.2.) | 1.18 | 1.05 | 0.66 | 0.33 | 0.08 | 0.02 | 0.58 |
| 11 | 0.06 | 0.30 | 0.50 | 1.17 | 1.76 | 1.65 | 1.45 | 1.40 | 0.91 | 0.45 | 0.11 | 0.11 | 0.82 |
| Mean. | -7.41 | $-6.73$ | -3.36 | 1.10 | 7.01 | 11.3 | 13.39 | 13.55 | 8.43 | 3.61 | -0.n0 | $-3.75$ |  |

LXVIII.

Russia. - Helsingfors. Lat. $60^{\circ} 10^{\prime}$ N. Long. $24^{\circ} 57^{\prime}$ E. Gr. - Dòve. Degrees of Reaumur.

| Hour. | Jan. | Fet, | March. | April. | May. | June. | July | Aug. | Sept. | Oct. | Nor. | Sec. | Year |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.06 | 0.47 | 1.28 | 1.61 | 1.61 | 2.01 | 1.6 .5 | 1.36 | 0.83 | 0.37 | 0.18 | 0.20 | 0.97 |
| 1 | 0.13 | 0.49 | 1.48 | 1.87 | 1.94 | 2.44 | 1.90 | 1.68 | 1.03 | 0.45 | 0.15 | 0.21 | 1.15 |
| 2 | 0.16 | 0.52 | 1.64 | 2.07 | 2.21 | 2.84 | 2.17 | 1.98 | 1.21 | 0.55 | 0.18 | 0.18 | 1.31 |
| 3 | 0.23 | 0.67 | 1.84 | 2.21 | 2.58 | 3.04 | 2.45 | 2.23 | 1.35 | 0.65 | 0.23 | 0.15 | 1.47 |
| 4 | 0.35 | 0.64 | 1.91 | 2.37 | 2.68 | 2.77 | 2.42 | 2.49 | 1.48 | 0.62 | 0.28 | 0.23 | 1.52 |
| 5 | 0.38 | 0.77 | 1.93 | 2.34 | 2.23 | 2.21 | 2.05 | 2.41 | 1.63 | 0.67 | 0.33 | 0.10 | 1.43 |
| 6 | 0.38 | 0.92 | 2.01 | 1.74 | 1.31 | 1.31 | 1.33 | 1.81 | 1.63 | 0.75 | 0.33 | 0.03 | 1.13 |
| 7 | 0.41 | 0.99 | 1.78 | 1.14 | 0.58 | 0.51 | 0.5.) | 1.11 | 1.28 | 0.73 | 0.86 | 0.01 | 0.79 |
| S | 0.43 | $0.99{ }^{1}$ | 1.04 | 0.17 | $-0.19$ | $-0.36$ | $-0.10$ | 0.26 | 0.58 | 0.57 | 0.35 | 0.00 | 0.31 |
| 9 | 0.35 | 0.55 | 0.04 | $-8.73$ | $-0.86$ | $-0.83$ | $-0.73$ | $-0.56$ | $-0.09$ | 0.83 | 0.25 | 0.06 | -0.18 |
| 10 | 0.05 | $-0.20$ | $-0.89$ | $-1.49$ | $-1.39$ | $-1.29$ | $-1.23$ | $-1.12$ | $-0.6 .5$ | -0.15 | 0.13 | $-0.07$ | $-0.69$ |
| 11 | $-0.19$ | $-0.93$ | $-1.19$ | $-1.93$ | $-1.76$ | $-1.83$ | $-1.65$ | $-1.59$ | $-1.05$ | $-0.47$ | $-0.19$ | $-0.32$ | -1.09 |
| Noon. | $-0.72$ | -1.25 | $-2.36$ | -2.26 | $-1.82$ | $-1.76$ | $-1.80$ | -2.02 | $-1.67$ | $-0.90$ | $-0.59$ | $-0.42$ | $-1.46$ |
| 1 | $-0.79$ | $-1.50$ | $-2.62$ | $-2.46$ | $-2.12$ | -2.06 | $-2.13$ | $-2.26$ | $-1.82$ | $-1.08$ | $-0.70$ | $-0.45$ | $-1.67$ |
| 2 | $-0.74$ | $-1.60$ | $-2.62$ | $-2.56$ | $-2.19$ | $-2.36$ | $-2.25$ | $-2.31$ | -1.8.5 | $-1.10$ | -0.64 | $-0.12$ | $-1.72$ |
| 3 | $-0.49$ | $-1.33$ | -2.46 | $-2.37$ | -2.16 | $-2.49$ | -2.13 | $-2.17$ | $-1.7 .5$ | $-0.95$ | $-0.50$ | $-0.22$ | $-1.58$ |
| 4 | $-9.21$ | $-0.90$ | $-2.12$ | $-1.89$ | $-1.82$ | $-2.16$ | $-1.75$ | -1.81 | $-1.52$ | $-0.77$ | $-0.29$ | $-0.02$ | $-1.28$ |
| 5 | $-0.12$ | $-0.43$ | $-1.56$ | $-1.59$ | -1 | $-1.89$ | $-1.48$ | $-1.64$ | $-1.20$ | $-0.43$ | $-0.17$ | 0.03 | $-1.00$ |
| 6 | $-0.04$ | $-0.21$ | $-0.79$ | $-1.09$ | $-1.09$ | $-1.53$ | $-1.15$ | $-1.19$ | $-0.72$ | -0.25 | $-0.09$ | $-0.02$ | $-0.68$ |
| 7 | 0.03 | 0.07 | $-0.29$ | $-0.49$ | $-0.86$ | $-0.96$ | -0.65 | $-0.64$ | -0.27 | -0.13 | -0.04 | 0.01 | $-0.35$ |
| 8 | 0.03 | 0.20 | 0.01 | 0.14 | $-0.16$ | $-0.36$ | -0.10 | $-0.14$ | 0.05 | -0.03 | 0.00 | 0.11 | -0.02 |
| 9 | 0.10 | 0.25 | 0.41 | 0.64 | 0.44 | 0.37 | 0.5 .5 | 0.28 | 0.23 | 0.0 .5 | 0.06 | 0.13 | 0.29 |
| 10 | 0.0 s | 0.3 .5 | 0.74 | 1.04 | 0.94 | 1.04 | 1.02 | 0.71 | 0.43 | 0.13 | 0.10 | 0.18 | 0.56 |
| 11 | 0.01 | 0.42 | 1.01 | 1.37 | 1.34 | 1.54 | 1.37 | 1.06 | 0.63 | 0.27 | 0.18 | 0.15 | 0.78 |
| Mean. | $-.5 .02$ | $-7.43$ | -3.89 | $-0.06$ | 5.11 | 10.84 | 12.75 | 14.11 | 9.23 | 4.55 | 1.13 | -3.42 |  |

The numbers without sign must be added; those with the sigu - must be subtracted.

Russia. - Petersburg. Lat. $59^{\circ} 56^{\prime}$ N. Long. $30^{\circ} 18^{\prime}$ E. Greemv.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Ang. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.20 | 0.38 | 0.92 | 1.52 | 2.59 | 2.10 | 1.98 | 2.08 | 1.39 | 0.72 | 0.14 | 0.17 | 1.21 |
| 2 | 0.23 | 0.37 | 1.10 | 1.75 | 2.84 | 2.69 | 2.26 | 2.43 | 1.67 | 0.77 | 0.13 | 0.27 | 1.38 |
| 3 | 0.22 | 0.39 | 1.30 | 2.01 | 3.03 | 2.90 | 2.49 | 2.79 | 1.97 | 0.82 | 0.14 | 0.33 | 1.53 |
| 4 | 0.21 | 0.43 | 1.49 | 2.19 | 3.05 | 2.91 | 2.57 | 3.01 | 2.20 | 0.88 | 0.16 | 0.35 | 1.62 |
| 5 | 0.26 | 0.50 | 1.59 | 2.17 | 2.79 | 2.60 | 2.37 | 2.92 | 2.25 | 0.95 | 0.20 | 0.35 | 1.58 |
| 6 | 0.37 | 0.57 | 1.56 | 1.58 | 2.20 | 1.98 | 1.88 | 2.16 | 2.06 | 0.95 | 0.23 | 0.34 | 1.38 |
| 7 | 0.51 | 0.56 | 1.36 | 1.35 | 1.27 | 1.13 | 1.15 | 1.70 | 1.62 | 0.92 | 0.23 | 0.33 | 1.01 |
| 8 | 0.59 | 0.46 | 0.99 | 0.68 | 0.41 | 0.24 | 0.34 | 0.79 | 1.01 | 0.72 | 0.16 | 0.31 | 0.56 |
| 9 | 0.53 | 0.23 | 0.47 | -0.02 | -0.47 | -0.53 | -0.40 | -0.10 | 1 | . 36 | 0.03 | 0.27 | 0.06 |
| 10 | 0.33 | -0.09 | -0.13 | -0.65 | -1.16 | -1.09 | -0.97 | -0.86 | -0.42 | -0.09 | -0.16 | 0.18 | -0.43 |
| 11 | 0.01 | $-0.43$ | $-0.74$ | -1.18 | $-1.65$ | -1. 49 | -1.37 | -1.17 | $-1.12$ | -0.58 | -0.35 | 0.03 | -0.86 |
| Noon. | -0.34 | $-0.73$ | -1.28 | $-1.62$ | -2.09 | -1.83 | -1.67 | -2.01 | $-1.75$ | -0.99 | -0.49 | -0.15 | -1.25 |
| 1 | -0.59 | -0.92 | -1.68 | -2.01 | $-2.50$ | -2.20 | -1.98 | -2.53 | -2.29 | -1.27 | -0.54 | -0.32 | -1.57 |
| 2 | -0.68 | -0.9.5 | -1.89 | -2.33 | -2.91 | $-2.62$ | -2.31 | -3.01 | -2.67 | -1.36 | -0.49 | -0.4.4 | -1.81 |
| 3 | -0.61 | -0.86 | -1.92 | -2.52 | -3.2.) | -2.98 | -2.58 | -3.35 | -2.81 | -1.30 | -0.35 | $-0.48$ | -1.92 |
| 4 | -0.45 | -0.67 | -1.75 | -2.50 | -3.36 | -3.12 | . 68 | -3.39 | -2.6.) | -1.12 | -0.18 | -0.44 | -1.86 |
| 5 | -0.27 | -0.44 | -1. | -2.10 | -3.1 | -2.89 | -2.46 | -3.02 | -2.19 | -0.88 | -0.02 | -0.36 | -1.61 |
| 6 | -0.15 | -0.22 | -1.04 | -1.01 | -2.44 | -2.26 | -1.94 | -2.26 | $-1.50$ | -0.62 | 0.10 | -0.26 | -1.18 |
| 7 | -0.12 | -0.02 | -0.60 | -0.86 | -1.37 | -1.33 | -1.15 | -1.25 | -0.72 | $-0.37$ | 0.17 | -0.19 | $\rightarrow 0.65$ |
| 8 | -0.13 | 0.13 | $-0.20$ | -0.10 | $-0.34$ | -0.31 | $-0.29$ | -0.20 | $-0.01$ | -0.12 | 0.19 | -0.14 | -0.13 |
| 9 | -0.14 | 0.24 | 0.14 | 0.54 | 0.69 | 0.61 | 0.49 | 0.66 | 0.53 | 0.11 | 0.19 | -0.12 | 0.33 |
| 10 | -0.09 | 0.32 | 0.40 | 0.96 | 1.47 | 1.30 | 1.07 | 1.24 | 0.37 | 0.33 | 0.18 | -0.09 | 0.66 |
| 11 | 0.02 | 0.37 | 0.59 | 1.20 | 2.00 | 1.77 | 1.45 | 1.58 | 1.05 | 0.50 | 0.17 | $-0.02$ | 0.89 |
| Miãn. | 0.12 | 0.38 | 0.75 | 1.35 | 2.33 | 2.11 | 1.73 | 1.81 | 1.20 | 0.63 | 0.16 | 0.07 | 1.05 |
| 6. 6 | 0.11 | 0.18 | 0.26 | 0.14 | -0.12 | -0.14 | -0.03 | 0.10 | 0.28 | 0.18 | 0.17 | 0.04 | 0.10 |
| 7. 7 | 0.20 | 0.27 | 0.38 | 0.25 | $-0.05$ | -0.10 | -0.00 | 0.23 | 0.45 | 0.28 | 0.20 | 0.07 | 0.15 |
| 8. 8 | 0.23 | 0.29 | 0.40 | 0.29 | 0.01 | -0.04 | 0.03 | 0.29 | 0.50 | 0.30 | 0.18 | 0.09 | 0.22 |
| 9. 9 | 0.20 | 0.21 | 0.31 | 0.26 | 0.11 | 0.04 | 0.04 | 0.28 | 0.42 | 0.24 | 0.11 | 0.08 | 0.19 |
| 10.10 | 0.12 | 0.12 | 0.13 | 0.15 | 0.16 | 0.11 | 0.05 | 0.19 | 0.22 | 0.12 | 0.01 | 0.05 | 0.12 |
| 7. 2. 9 | -0.10 | -0.05 | -0.13 | -0.15 | -0.32 | -0.29 | -0.22 | -0.22 | -0.17 | -0.11 | $-0.02$ | -0.08 | -0.16 |
| 6. 2. 8 | -0.15 | -0.03 | -0.18 | -0.18 | -0.3.5 | -0.32 | -0.24 | -0.25 | -0.21 | -0.17 | -0.02 | -0.08 | -0.19 |
| 6. 2.10 | -0.13 | -0.02 | 0.02 | 0.17 | 0.25 | 0.22 | 0.21 | 0.23 | 0.09 | -0.02 | -0.03 | $-0.06$ | 0.08 |
| 6. 2. 6 | -0.15 | -0.20 | $-0.46$ | -0.69 | -1.05 | -0.97 | $-0.79$ | -0.94 | -0.70 | -0.33 | -0.05 | -0.12 | -0.54 |
| 7. 2 | -0.09 | -0.20 | -0.27 | -0.49 | -0.82 | -0.75 | -0.58 | -0.66 | -0.53 | -0.22 | -0.13 | -0.06 | -0.40 |
| 8. 2 | -0.05 | -0.25 | -0.45 | -0.83 | -1.25 | -1.19 | -0.99 | -1.11 | -0.83 | -0.32 | -0.17 | -0.07 | -0.63 |
| 8. 1 | 0.00 | -0.23 | -0.35 | $-0.67$ | -1.05 | -0.98 | -0.82 | -0.87 | -0.64 | -0.29 | -0.19 | $-0.01$ | -0.51 |
| 7. 1 | -0.04 | -0.18 | $-0.16$ | -0.33 | -0.62 | -0.54 | -0.42 | -0.42 | -0.34 | -0.18 | -0.16 | 0.01 | -0.28 |
| 9.12.3.9 | -0.14 | -0.28 | -0.65 | -0.91 | -1.28 | -1.18 | -1.04 | -1.20 | -0.93 | -0.46 | -0.16 | -0.12 | -0.70 |
| 7. $2.2(9)$ | -0.11 | 0.02 | -0.06 | 0.03 | -0.07 | -0.07 | -0.05 | 0.00 | 0.00 | -0.06 | 0.03 | $-0.09$ | -0.04 |
| Dail.cxt. | -0.0.5 | -0.19 | -0.17 | -0.17 | -0.16 | -0.11 | -0.06 | -0.19 | -0.28 | -0.19 | -0.16 | -0.07 | -0.15 |

The numbers without sign must be added ; those with the sign - must be subtracted.

Russia. - Helsingfors. Lat. $60^{\circ} 10^{\prime}$ N. Long. $24^{\circ} 57^{\prime}$ E. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean 'Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | Juty. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.47 | 0.85 | 1.40 | 2.10 | 2.49 | 3.37 | 3.16 | 2.58 | 1.6 | 1.06 | 0.64 | 0.34 | 1.67 |
| 2 | 0.79 | 1.25 | 1.86 | 3.18 | 2.82 | 3.78 | 3.48 | 2.96 | 2.0 | 1.45 | 0.99 | 0.68 | 2.11 |
| 3 | 0.99 | 1.55 | 2.28 | 2.79 | 2.59 | 3.74 | 3.45 | 3.11 | 2.45 | 1.70 | 1.22 | 0.91 | 2.26 |
| 4 | 1.13 | 1.71 | 2.52 | 2.75 | 2.62 | 3.22 | 3.02 | 2.92 | 2.61 | 1.74 | 1.26 | 0.97 | 2.21 |
| 5 | 1.06 | 1.66 | 2.49 | 2.41 | 2.06 | 2.32 | 2.25 | 2.39 | 2.40 | 1.51 | 1.09 | 0.84 | 1.57 |
| 6 | 0.86 | 1.43 | 2.16 | 1.76 | 1.30 | 1.24 | 1.23 | 1..59 | 1.84 | 1.10 | 0.76 | 0.59 | 1.32 |
| 7 | 0.58 | 1.07 | 1.54 | 0.92 | 0.49 | 0.20 | 0.17 | 0.64 | 1.06 | 0.59 | 0.38 | 0.31 | 0.67 |
| 8 | 0.28 | 0.60 | 0.79 | 0.05 | -0.26 | -0.65 | -0.78 | -0.28 | 0.21 | 0.08 | 0.02 | 0.07 | 0.01 |
| 9 | 0.01 | 0.10 | -0.05 | -0.74 | -0.87 | -1.26 | $-1.51$ | -1.07 | -0.58 | -0.38 | -0.27 | -0.10 | -0.56 |
| 10 | -0.25 | -0.42 | -0.87 | -1.35 | -1.34 | -1.65 | -2.02 | $-1.68$ | -1.23 | $-0.77$ | -0.48 | -0.22 | -1.02 |
| 11 | -0.48 | -0.91 | -1.56 | -1.50 | -1.70 | -1.93 | -2.35 | -2.12 | $-1.71$ | $-1.07$ | -0.64 | -0.32 | -1.38 |
| Noon | -0.70 | -1.29 | -2.06 | -2.10 | -1.98 | -2.16 | $-2.54$ | -2.43 | -2.04 | -1.30 | -0.76 | -0.43 | -1.65 |
| 1 | -0.86 | -1.54 | -2 36 | -2.30 | -2.19 | -2.36 | -2 65 | -2.61 | -2.23 | -1.42 | -0.55 | -0.54 | -1.83 |
| 2 | -0.92 | -1.60 | -2.45 | -2.37 | -2.32 | -2.51 | -2.66 | -2.66 | -2.30 | -1.43 | -0.58 | -0.61 | -1.89 |
| 3 | -0.84 | -1.47 | -2.32 | $-2.31$ | -2.31 | -2.55 | -2.55 | -2.5.5 | -2.20 | -1.30 | -0.82 | -0.60 | -1.82 |
| 4 | -0.73 | -1.20 | -2.01 | -2.10 | $-2.11$ | -2.42 | -2.27 | -2.26 | $-1.92$ | -1.05 | -0.68 | -0.49 | -1.60 |
| 5 | -0.52 | -0.87 | -1.56 | -1.73 | -1.77 | -2.13 | -1.85 | -1.80 | -1.48 | -0.74 | -0.48 | -0.33 | -1.27 |
| 6 | $-0.32$ | -0.57 | -1.07 | -1.25 | -1.30 | -1.71 | -1.30 | $-1.24$ | -0.95 | -0.44 | -0.2s | -0.18 | -0.88 |
| 7 | -0.19 | -0.38 | -0.60 | -0.72 | -0.78 | -1.20 | -0.68 | $-0.62$ | -0.42 | -0.22 | -0.16 | -0.11 | -0.51 |
| 8 | -0.15 | -0.25 | -0.20 | -0.21 | -0.24 | -0.61 | -0.04 | -0.03 | -0.00 | -0.10 | $-0.12$ | -0.12 | -0.17 |
| 9 | -0.16 | -0.18 | 0.10 | 0.26 | 0.29 | 0.07 | 0.61 | 0.52 | 0.31 | -0.03 | -0.12 | -0.20 | 0.12 |
| 10 | -0.16 | -0.0s | 0.36 | 0.69 | 0.82 | 0.87 | 1.27 | 1.03 | 0.54 | 0.08 | $-0.10$ | -0.25 | 0.42 |
| 11 | -0.06 | 0.12 | 0.63 | 1.15 | 1.10 | 1.75 | 1.95 | 1.54 | 0.79 | 0.29 | 0.02 | -0 19 | 0.78 |
| Midn. | 0.16 | 0.44 | 0.96 | 1.60 | 1.97 | 2.63 | 2.61 | 2.08 | 1.14 | 0.63 | 0.28 | 0.02 | 1.21 |
| 6. 6 | 0.27 | 0.43 | 0.5 .5 | 0.26 | -0.00 | -0.24 | -0.04 | 0.18 | 0.45 | 0.33 | 0.24 | 0.21 | 0.22 |
| 7. 7 | 0.20 | 0.35 | 0.49 | 0.10 | -0.15 | -0.50 | -0.26 | 0.01 | 0.32 | 0.19 | 0.11 | 0.10 | 0.08 |
| 8. 8 | 0.07 | 0.18 | 0.30 | -0.08 | -0.25 | -0.63 | -0.41 | -0.16 | 0.11 | -0.01 | -0.05 | -0.03 | -0.08 |
| 9. 9 | -0.08 | -0.04 | 0.03 | -0.24 | -0.29 | -0.60 | $-0.45$ | -0.28 | -0.14 | -0.21 | -0.20 | -0.15 | -0.22 |
| 10.10 | -0.21 | -0.2.5 | -0.26 | -0.33 | -0.26 | -0.39 | -0.38 | -0.33 | -0.35 | -0.35 | -0.29 | -0.24 | -0.30 |
| 7. 2. 9 | -0.17 | -0.24 | -0.26 | -0.40 | -0.51 | -0.75 | -0.63 | -0.50 | -0.31 | -0.29 | -0.2] | -0.17 | -0.87 |
| 6.2. 8 | -0.07 | -0.14 | -0.16 | -0.27 | -0.12 | -0.63 | -0.49 | -0.37 | -0.15 | -0.14 | -0.08 | -0.05 | -0.25 |
| 6. 2.10 | $-0.07$ | -0.08 | 0.02 | 0.03 | -0.07 | -0.13 | -0.0: | -0.01 | 0.03 | -0.08 | -0.07 | -0.09 | -0.05 |
| 6. 2. 6 | -0.13 | -0.2.5 | -0.4. | -0.62 | -0.77 | -0.99 | -0.91 | -0.74 | -0.47 | -0.26 | -0.13 | -0.07 | -0.49 |
| 7. 2 | -0.17 | -0.27 | -0.44 | -0.73 | -0.92 | -1. | -1.25 |  | -0.62 | -0.42 | 0.25 | -0.15 | -0.62 |
| 8. 2 | -0.32 | -0.50 | -0.83 | -1.16 | -1.29 | -1.58 | -1.72 | -1.47 | -1.0. | -0.68 | -0.43 | -0.27 | -0.94 |
| 8. 1 | -0.29 | -0.47 | -0.79 | -1.13 | -1.23 | -1.51 | -1.72 | -1.4. | -1.01 | -0.67 | -0.42 | 0.24 | -0.91 |
| 7. 1 | -0.14 | -0.24 | -0.40 | -0.69 | -0.s5 | -1.08 | -1.24 | -0.99 | $-0.59$ | -0.42 | -0.24 | -0.12 | -0.58 |
| 9.12.3.9 | -0.42 | -0.71 | -1.05 | -1.22 | -1.22 | -1.48 | -1.50 | -1.38 | -1 13 | -0.75 | -0.49 | -0.33 | -0.98 |
| 7. 2.2(9) | -0.17 | -0.22 | $-0.17$ | $-0.23$ | -0.31 | -0.54 | -0.32 | $-0.25$ | -0.16 | -0.23 | -0.19 | -0.1s | -0.25 |
| Dail.ext. | 0.11 | 0.06 | 0.04 | 041 | 0.29 | 0.62 | 0.41 | 0.23 | 0.16 | 0.16 | 0.19 | 0.18 | 0.19 |

The numbers without sign must be added; those with the sign - must be subtracted.

Normay. - Ciristiania. Lat. $59^{\circ} 55^{\prime}$ N. Long. $10^{\circ} 43^{\prime}$ E. Greemw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Iear. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.16 | 0.89 | 1.07 | 1.56 | 2.55 | 2.58 | 2.21 | 2.04 | 1.64 | 0.74 | 0.52 | 0.22 | 1.35 |
| 2 | 0.21 | 0.94 | 1.30 | 1.88 | 2.85 | 3.15 | 2.53 | 2.23 | 1.88 | 0.82 | 0.50 | 0.21 | 1.54 |
| 3 | 0.27 | 1.17 | 1.51 | 2.03 | 3.23 | 3.28 | 2.64 | 2.41 | 2.03 | 0.94 | 0.49 | 0.28 | 1.69 |
| 4 | 0.32 | 1.49 | 1.67 | 2.12 | 3.21 | 3.05 | 2.62 | 2.60 | 2.07 | 1.06 | 0.55 | 0.30 | 1.84 |
| 5 | 0.38 | 1.60 | 1.82 | 2.23 | 2.55 | 2.39 | 2.09 | 2.44 | 2.14 | 1.16 | 0.51 | 0.22 | 1.63 |
| 6 | 0.47 | 1.54 | 1.69 | 1.81 | 1.63 | 1.31 | 1.37 | 1.98 | 2.10 | 1.16 | 0.60 | 0.11 | 1.31 |
| 7 | 0.51 | 1.67 | 1.71 | 1.28 | 0.71 | 0.43 | 0.58 | 1.00 | 1.50 | 1.13 | 0.46 | 0.19 | 0.93 |
| 8 | 0.54 | 1.42 | 1.29 | 0.56 | 0.07 | $-0.32$ | -0.22 | 0.10 | 0.62 | 0.75 | 0.38 | 0.15 | 0.44 |
| 9 | 0.48 | 1.11 | 0.36 | $-0.06$ | $-0.52$ | -0.86 | $-0.78$ | $-0.59$ | 0.01 | 0.15 | 0.17 | 0.16 | $-0.03$ |
| 10 | 0.24 | 0.27 | $-0.35$ | $-0.67$ | -1.19 | $-1.57$ | $-1.26$ | $-1.23$ | $-0.78$ | $-0.48$ | $-0.23$ | 0.11 | -0.59 |
| 11 | $-0.17$ | $-0.69$ | $-0.96$ | -1.38 | -1.66 | $-2.05$ | $-1.74$ | -1.67 | -1.44 | $-1.00$ | $-0.76$ | $-0.20$ | $-1.14$ |
| N | -0.67 | -1.32 | -1.48 | $-1.80$ | $-2.17$ | $-2.29$ | -2.02 | -2.11 | -2.02 | $-1.30$ | $-1.06$ | $-0.40$ | $-1.55$ |
| 1 | -0.87 | $-1.90$ | -1.74 | -2.22 | -2.46 | $-2.50$ | $-2.21$ | $-2.35$ | -2.41 | $-1.59$ | $-1.15$ | -0.42 | -1.82 |
| 2 | $-1.04$ | -2.22 | -1.95 | $-2.32$ | $-2.46$ | $-2.40$ | $-2.20$ | $-2.50$ | -2.54 | -1.67 | $-1.15$ | -0.35 | $-1.90$ |
| 3 | -0.91 | $-2.29$ | $-2.16$ | $-2.26$ | $-2.54$ | $-2.47$ | $-2.21$ | $-2.50$ | $-2.50$ | $-1.58$ | -0.88 | $-0.23$ | -1.88 |
| 4 | -0.62 | $-2.00$ | $-1.99$ | $-2.11$ | $-2.53$ | $-2.29$ | $-2.00$ | $-2.32$ | $-2.35$ | -1.33 | $-0.55$ | $-0.12$ | -1.68 |
| 5 | $-0.35$ | -1.42 | -1.58 | $-1.80$ | $-2.20$ | $-2.14$ | -1.87 | $-1.97$ | -1.80 | $-0.90$ | $-0.23$ | $-0.06$ | $-1.36$ |
| 6 | -0.12 | -1.10 | $-1.10$ | -1.27 | -1.82 | $-1.70$ | -1.48 | $-1.48$ | -1.21 | $-0.52$ | $-0.02$ | $-0.03$ | $-0.99$ |
| 7 | -0.01 | $-0.60$ | -0.6.5 | $-0.70$ | -1.35 | $-0.98$ | -0.89 | $-0.78$ | -0.57 | $-0.24$ | 0.11 | $-0.10$ | $-0.58$ |
| 8 | 0.12 | $-0.32$ | $-0.20$ | $-0.14$ | -0.44 | -0.31 | $-0.30$ | $-0.10$ | 0.02 | 0.18 | 0.23 | $-0.13$ | $-0.1 \%$ |
| 9 | 0.16 | 0.09 | 0.09 | 0.36 | 0.24 | 0.44 | 0.45 | 0.55 | 0.36 | 0.36 | 0.27 | -0.05 | 0.28 |
| 10 | 0.27 | 0.34 | 0.36 | 0.70 | 0.93 | 1.20 | 1.06 | 1.08 | 0.81 | 0.58 | 0.33 | $-0.04$ | 0.6:3 |
| 11 | 0.3 | 0.52 | 0.53 | 0.99 | 1.46 | 1.76 | 1.63 | 1.41 | 1.06 | 0.75 | 0.43 | 0.10 | 0.91 |
| Midn. | 0.33 | 0.86 | 0.77 | 1.20 | 1.90 | 2.31 | 2.00 | 1.75 | 1.38 | 0.95 | 0.48 | 0.09 | 1.17 |
| 6. 6 | 0.18 | 0.22 | 0.30 | 0.27 | -0.10 | -0.20 | -0.06 | 0.25 | 0.45 | 0.32 | 0.29 | 0.04 | 0.16 |
| 7. 7 | 0.25 | 0.54 | 0.53 | 0.29 | $-0.32$ | $-0.28$ | $-0.16$ | 0.11 | 0.47 | 0.45 | 0.29 | 0.05 | 0.18 |
| 8. 8 | 0.33 | 0.55 | 0.55 | 0.21 | $-0.19$ | $-0.32$ | $-0.26$ | 0.00 | 0.32 | 0.47 | 0.31 | 0.01 | 0.16 |
| 9. 9 | 0.32 | 0.60 | 0.23 | 0.15 | $-0.14$ | $-0.21$ | $-0.17$ | $-0.02$ | 0.19 | 0.26 | 0.22 | 0.06 | 0.12 |
| 10.10 | 0.26 | 0.31 | 0.01 | 0.05 | $-0.13$ | $-0.18$ | $-0.10$ | -0.08 | 0.02 | 0.0.5 | 0.05 | 0.04 | 0.02 |
| 7. 2. 9 | -0.12 | $-0.15$ | $-0.05$ | $-0.23$ | $-0.50$ | $-0.51$ | $-0.39$ | $-0.32$ | -0.23 | -0.06 | -0.14 | -0.07 | -0.23 |
| 6. 2. 8 | -0.15 | $-0.83$ | $-0.15$ | -0.22 | $-0.42$ | $-0.47$ | -0.38 | $-0.21$ | -0.14 | -0.11 | $-0.11$ | $-0.12$ | $-0.23$ |
| 6. 2.10 | -0.10 | $-0.11$ | 0.03 | 0.06 | 0.03 | 0.04 | 0.08 | 0.19 | 0.12 | 0.02 | -0.07 | -0.09 | 0.02 |
| 6. 2. 6 | -0.23 | $-0.59$ | $-0.45$ | $-0.59$ | $-0.76$ | $-0.67$ | $-0.70$ | $-0.67$ | $-0.55$ | $-0.34$ | $-0.19$ | $-0.11$ | $-0.49$ |
| 7. 2 | -0.27 | $-0.28$ | $-0.12$ | $-0.52$ | -0.88 | -0.99 | $-0.81$ |  |  |  | -0.35 |  |  |
| 8. 2 | -0.25 | $-0.40$ | -0.33 | -0.88 | -1.20 | -1.04 | -0.99 |  |  |  | -0. |  |  |
| 8. 1 | $-0.17$ |  | -0.23 |  |  | 09 |  |  |  |  | -0.39 |  |  |
| 7. 1 | -0.18 | -0.12 | $-0.02$ |  | -0.88 | -1.04 | -0.82 |  | -0.46 | $-0.23$ | -0.35 | -0.12 | -0.50 |
|  | - 18 |  |  |  | -0.88 | 1.04 | -0.82 |  | -0.46 | $-0.23$ | -0..35 | -0.12 | $-0.50$ |
| 9.12.3.9 | $-0.56$ | $-0.60$ | -0.80 | $-0.94$ | $-1.25$ | $-1.29$ | -1.14 | -1.16 | -1.04 | $-0.59$ | $-0.38$ | -0.13 | $-0.82$ |
| 7. $2.2(9)$ | -0.05 | $-0.09$ | $-0.02$ | -0.08 | $-0.32$ | -0.27 | -0.18 | $-0.10$ | -0.08 | 0.05 | -0.04 | $-0.07$ | $-0.11$ |
| Dail.ext. | -0.25 | -0.31 | $-0.17$ | -0.05 | 0.35 | 0.39 | 0.22 | 0.05 | $-0.20$ | $-0.26$ | -0.28 | -0.06 | -0.05 |

The numbers without sign must be added; those with the sign - must be subtracted.

## LXXII.

Norway. - Dronthem. Lat. $63^{\circ} 26^{\prime}$ N. Long. $10^{\circ} 25^{\prime}$ E. Greemv.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.29 | 0.41 | 0.77 | 1.94 | 2.63 | 2.64 | 2.53 | 2.51 | 1.37 | 0.89 | 0.27 | 0.33 | 1.38 |
| 2 | 0.25 | 0.50 | 0.95 | 2.09 | 2.97 | 2.76 | 2.75 | 2.65 | 1.48 | 0.91 | 0.31 | 0.31 | 1.50 |
| 3 | 0.22 | 0.64 | 1.11 | 2.19 | 3.13 | 2.82 | 2.77 | 2.91 | 1.59 | 0.97 | 0.23 | 0.42 | 1.58 |
| 4 | 0.20 | 0.71 | 1.27 | 2.32 | 3.03 | 2.82 | 2.65 | 2.77 | 1.55 | 1.07 | 0.28 | 0.34 | 1.58 |
| 5 | 0.13 | 0.75 | 1.37 | 2.05 | 2.76 | 2.52 | 2.35 | 2.58 | 1.59 | 0.86 | 0.30 | 0.42 | 1.47 |
| 6 | 0.11 | 0.82 | 1.42 | 1.67 | 2.30 | 1.96 | 1.86 | 2.13 | 1.49 | 0.71 | 0.14 | 0.43 | 1.25 |
| 7 | 0.04 | 0.58 | 1.35 | 1.36 | 1.68 | 1.39 | 1.17 | 1.58 | 1.07 | 0.42 | 0.00 | 0.36 | 0.92 |
| 8 | 0.08 | 0.23 | 1.17 | 0.94 | 0.83 | 0.61 | 0.40 | 1.02 | 0.57 | 0.06 | $-0.02$ | 0.36 | 0.52 |
| 9 | 0.00 | -0.08 | 0.41 | $-0.02$ | $-0.28$ | -0.03 | $-0.14$ | 0.22 | $-0.07$ | $-0.29$ | $-0.14$ | 0.19 | $-0.02$ |
| 10 | -0.09 | $-0.48$ | $-0.13$ | $-0.85$ | -1.29 | $-0.92$ | -1.30 | -1.22 | $-0.89$ | -0.59 | $-0.16$ | 0.02 | $-0.65$ |
| 11 | -0.16 | $-0.78$ | $-0.65$ | $-1.90$ | $-2.09$ | $-2.01$ | -1.95 | $-2.63$ | $-1.34$ | -0.88 | $-0.33$ | $-0.12$ | -1.24 |
| Noo | $-0.59$ | -1.08 | -1.35 | $-2.57$ | $-2.81$ | $-2.43$ | $-2.77$ | -3.21 | $-2.05$ | $-1.20$ | -0.38 | $-0.42$ | -1.75 |
| 1 | -0.80 | -1.22 | -1.70 | $-2.66$ | -3.28 | $-3.25$ | -3.20 | -3.39 | $-2.12$ | -1.14 | -0.44 | $-0.42$ | -1.97 |
| 2 | -0.68 | $-1.15$ | $-1.70$ | $-2.46$ | -3.27 | $-3.32$ | $-3.07$ | -3.36 | $-2.28$ | -1.09 | $-0.42$ | $-0.47$ | $-1.94$ |
| 3 | -0.48 | -0.80 | $-1.51$ | $-2.29$ | -3.25 | -3.05 | -3.06 | -3.21 | $-1.85$ | -1.07 | $-0.28$ | $-0.37$ | $-1.76$ |
| 4 | -0.36 | $-0.56$ | -1.37 | -1.83 | $-2.90$ | $-2.78$ | -2.41 | -2.81 | -1.43 | -0.86 | -0.16 | -0.29 | -1.48 |
| 5 | $-0.29$ | $-0.36$ | -1.07 | -1.30 | $-2.20$ | $-2.45$ | $-2.02$ | $-2.23$ | $-1.09$ | $-0.50$ | -0.06 | -0.22 | -1.15 |
| 6 | $-0.17$ | $-0.11$ | -0.75 | $-0.90$ | -1.70 | -1.84 | $-1.15$ | $-1.27$ | $-0.79$ | $-0.51$ | 0.08 | $-0.23$ | $-0.78$ |
| 7 | 0.09 | $-0.04$ | $-0.54$ | $-0.57$ | -1.03 | $-1.00$ | $-0.61$ | $-0.68$ | $-0.32$ | $-0.28$ | 0.09 | $-0.30$ | $-0.43$ |
| 8 | 0.27 | 0.17 | -0.27 | $-0.20$ | -0.37 | 0.04 | 0.01 | 0.11 | 0.03 | $-0.02$ | 0.17 | $-0.19$ | $-0.02$ |
| 9 | 0.45 | 0.37 | 0.00 | 0.16 | 0.50 | 0.41 | 0.66 | 0.51 | 0.43 | 0.22 | 0.05 | $-0.11$ | 0.30 |
| 10 | 0.52 | 0.53 | 0.23 | 0.61 | 1.10 | 1.08 | 1.17 | 1.18 | 0.75 | 0.55 | 0.13 | $-0.06$ | 0.65 |
| 11 | 0.47 | 0.50 | 0.43 | 0.90 | 1.61 | 1.63 | 1.48 | 1.67 | 1.02 | 0.74 | 0.11 | 0.02 | 0.88 |
| Midn. | 0.45 | 0.49 | 0.63 | 1.27 | 1.92 | 2.07 | 1.88 | 2.13 | 1.28 | 1.14 | 0.19 | 0.02 | 1.12 |
| 6. 6 | $-0.03$ | 0.36 | 0.34 | 0.39 | 0.30 | 0.06 | 0.36 | 0.43 | 0.35 | 0.10 | 0.11 | 0.10 | 0.24 |
| 7. 7 | 0.07 | 0.27 | 0.41 | 0.40 | 0.33 | 0.20 | 0.28 | 0.45 | 0.38 | 0.07 | 0.05 | 0.03 | 0.24 |
| 8. 8 | 0.18 | 0.20 | 0.45 | 0.37 | 0.23 | 0.33 | 0.21 | 0.57 | 0.30 | 0.02 | 0.08 | 0.09 | 0.25 |
| 9. 9 | 0.23 | 0.15 | 0.21 | 0.07 | 0.11 | 0.19 | 0.26 | 0.37 | 0.18 | -0.04 | -0.05 | 0.04 | 0.14 |
| 10.10 | 0.22 | 0.03 | 0.05 | -0.1 | $-0.10$ | 0.08 | $-0.07$ | $-0.02$ | $-0.07$ | $-0.02$ | -0.02 | $-0.02$ | 0.00 |
| 7. 2. 9 | -0.06 | $-0.07$ | $-0.12$ | -0.31 | $-0.36$ | -0.51 | $-0.41$ | $-0.42$ | $-0.26$ | -0.15 | $-0.12$ | -0.07 | -0.24 |
| 6. 2. 8 | -0.10 | -0.05 | $-0.18$ | -0.3:; | $-0.4$ | $-0.44$ | $-0.40$ | -0.37 | -0.25 | $-0.13$ | -0.04 | -0.08 | $-0.23$ |
| 6. 2.10 | $-0.02$ | 0.07 | $-0.02$ | $-0.06$ | 0.04 | $-0.09$ | -0.01 | $-0.02$ | $-0.01$ | 0.06 | -0.05 | -0.03 | $-0.01$ |
| 6. 2. 6 | -0.25 | -0.62 | -0.39 | $-0.56$ | -0.89 | -1.06 | $-0.79$ | $-0.83$ | $-0.53$ | $-0.30$ | -0.07 | -0.09 | -0.53 |
| 7. 2 | -0.32 | $-0.29$ | -0.18 | -0.55 | -0. 80 | $-0.97$ | -0.9 | -0.89 | -0.61 | -0.34 | -0.21 | -0.06 | -0.51 |
| 8. 2 | -0.30 | 0.46 | $-0.27$ | $-0.76$ | -1.22 | -1.36 | -1.3 | $-1.17$ | $-0.86$ | $-0.52$ | -0.22 | -0.06 | $-0.63$ |
| 8. 1 | -0.36 | $-0.50$ | $-0.27$ | -0. | $-1.23$ | $-1.32$ | $-1.40$ | -1.19 | -0.75 | $-0.54$ | -0.23 | -0.03 | -0.73 |
| 7. 1 | -0.38 | $-0.32$ | -0.1S | -0.65 | -0.80 | -0.93 | -1.02 | -0.91 | $-0.53$ | $-0.36$ | -0.22 | -0.03 | $-0.53$ |
| 9.12.3.9 | -0.16 | $-0.10$ | -0.62 | $-1.1$ | -1.46 | -1.28 | $-1.33$ | -1.42 | -0.89 | $-0.59$ | $-0.1$ | -0.18 | -0.87 |
| 7. $2.2(9)$ | 0.07 | 0.04 | $-0.09$ | -0.19 | -0.15 | -0.28 | $-0.15$ | -0.19 | -0.09 | $-0.16$ | $-0.02$ | -0.12 | $-0.11$ |
| Dail.ext. | -0.14 | $-0.20$ | $-0.14$ | -0.17 | -0.08 | -0.25 | -0.22 | -0.24 | -0.35 | -0.07 | -0. | -0.02 | -0.16 |

## LXXIII.

Strait of Kara. Lat. $70^{\circ} 37^{\prime}$ N. Long. $57^{\circ} 47^{\prime}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | 0.27 | 0.38 | 1.66 | 2.53 | 2.26 | 1.86 | 1.37 | 0.62 | 0.33 | 0.00 | 0.08 | 0.5 | 0.99 |
| 2 | 0.24 | 0.38 | 1.78 | 2.67 | 2.22 | 1.68 | 1.24 | 0.58 | 0.40 | 0.02 | 0.14 | 0.42 | 0.98 |
| 3 | 0.22 | 0.40 | 1.86 | 2.66 | 2.06 | 1.41 | 1.03 | 0.53 | 0.49 | 0.02 | 0.14 | 0.26 | 0.92 |
| 4 | 0.23 | 0.12 | 1.85 | 2.44 | 1.82 | 1.12 | 0.79 | 0.47 | 0.58 | 0.06 | 0.15 | 0.11 | 0.84 |
| 5 | 0.25 | 0.42 | 1.80 | 1.98 | 1.48 | 0.82 | 0.54 | 0.38 | 0.61 | 0.17 | 0.22 | -0.00 | 0.72 |
| 6 | 0.27 | 0.33 | 1.55 | 1.30 | 1.01 | 0.49 | 0.25 | 0.26 | 0.58 | 0.29 | 0.36 | $-0.15$ | 0.55 |
| 7 | 0.29 | 0.16 | 1.10 | 0.52 | 0.40 | 0.10 | -0.05 | 0.10 | 0.42 | 0.35 | 0.52 | $-0.29$ | 0.30 |
| 8 | 0.30 | 0.08 | 0.42 | -0.27 | $-0.30$ | -0.33 | -0.35 | -0.07 | 0.27 | 0.32 | 0.64 | -0.42 | 0.01 |
| 9 | 0.26 | 0.30 | $-0.43$ | -0.98 | $-1.01$ | $-0.78$ | $-0.66$ | $-0.23$ | 0.01 | 0.18 | 0.66 | -0.5. | $-0.32$ |
| 10 | 0.1 | $-0.50$ | $-1.32$ | $-1.55$ | $-1.63$ | -1.19 | -0.65 | $-0.36$ | -0.28 | 0.02 | 0.55 | -0.61 | $-0.63$ |
| 11 | 0.04 | -0.64 | $-2.07$ | $-2.13$ | -2.06 | $-1.45$ | -0.98 | $-0.16$ | $-0.54$ | $-0.25$ | 0.33 | -0.62 | $-0.91$ |
| N | $-0.1$ | -0.70 | $-2.56$ | -2.41 | -2.27 | $-1.62$ | -1.04 | -0.55 | $-0.72$ | -0.37 | 0.18 | -0.5. | $-1.07$ |
| 1 | -0.31 | $-0.70$ | $-2.70$ | -2.67 | -2 | $-1.62$ | -1.03 | $-0.63$ | $-0.81$ | $-0.43$ | $-0.13$ | -0.44 | $-1.14$ |
| 2 | $-0.49$ | -0.64 | $-2.52$ | $-2.81$ | -2.11 | $-1.54$ | $-1.00$ | -0.71 | $-0.78$ | -0.36 | -0.25 | -0.31 | $-1.13$ |
| 3 | -0.6 | $-0.53$ | $-2.10$ | -2.75 | -1.88 | $-1.40$ | -0.95 | $-0.76$ | -0.66 | -0.23 | -0.30 | $-0.21$ | $-1.03$ |
| 4 | -0.63 | $-0.38$ | -1.54 | -2.46 | -1.61 | $-1.25$ | $-0.90$ | $-0.69$ | $-0.49$ | $-0.10$ | -0.32 | -0.11 | -0.87 |
| 5 | $-0.58$ | $-0.21$ | -0.98 | -1.91 | $-1.30$ | $-1.05$ | $-0.78$ | $-0.59$ | -0.30 | 0.02 | -0.35 | -0.04 | $-0.67$ |
| 6 | -0.46 | $-0.02$ | $-0.47$ | -1.18 | -0.90 | -0.76 | -0.59 | $-0.38$ | $-0.13$ | 0.07 | -0.41 | 0.06 | $-0.43$ |
| 7 | $-0.26$ | 0.14 | $-0.04$ | -0.37 | -0.40 | -0.35 | $-0.29$ | $-0.09$ | 0.06 | 0.08 | -0.18 | 0.18 | -0.15 |
| 8 | -0.06 | 0.32 | 0.3 | 0.42 | 0.20 | 0.18 | 0.11 | 0.22 | 0.11 | 0.07 | $-0.52$ | 0.33 | 0.14 |
| 9 | 0.11 | 0.42 | 0.67 | 1.08 | 0.53 | 0.78 | 0.54 | 0.46 | 0.17 | 0.06 | $-0.49$ | 0.18 | 0.43 |
| 10 | 0.2 | 0.4 | 0.98 | 1.59 | 1.42 | 1.31 | 0.9 .4 | 0.62 | 0.20 | 0.06 | $-0.38$ | 0.61 | 0.67 |
| 11 | 0.28 | 0.44 | 1.25 | 1.98 | 1.8 | 1.7 | 1.23 | 0.68 | 0.23 | 0.06 | $-0.20$ | 0.66 | 0.85 |
| Midn. | 0.29 | 0.40 | 1.48 | 2.29 | 2.16 | 1.90 | 1.3 | 0.66 | 0.27 | 0.01 | $-0.03$ | 0.64 | 0.95 |
| 6. 6 | 0.10 | 0.16 | 0.54 | 0.06 | 0.06 | $-0.14$ | -0.17 | -0.06 | 0.23 | 0.18 | -0.03 | $-0.05$ | 0.06 |
| 7. 7 | 0.0 | 0.1 | 0.53 | 0.08 | $-0.00$ | $-0.13$ | -0.17 | 0.01 | 0.24 | 0.22 | 0.02 | $-0.06$ | 0.08 |
| 8. S | 0.1 | 0.12 | 0.38 | 0.08 | $-0.05$ | $-0.05$ | -0.12 | 0.08 | 0.19 | 0.20 | 0.06 | $-0.05$ | 0.08 |
| 9. 9 | 0.19 | 0.06 | 0.12 | 0.05 | -0.09 | $-0.00$ | $-0.06$ | 0.12 | 0.09 | 0.12 | 0.09 | $-0.03$ | 0.05 |
| 10.10 | 0.20 | $-0.02$ | -0.17 | 0.01 | $-0.11$ | 0.06 | 0.05 | 0.13 | -0.0. | 0.04 | 0.09 | $-0.00$ | 0.02 |
| 7. 2. 9 | -0.03 | $-0.02$ | $-0.25$ | $-0.40$ | -0.29 | $-0.22$ | -0.17 | $-0.05$ | -0.06 | 0.02 | $-0.07$ | -0.0.4 | $-0.12$ |
| 6. 2. 8 | $-0.09$ | $-0.00$ | $-0.21$ | $-0.36$ | $-0.30$ | -0.29 | $-0.21$ | -0.08 | -0.03 | $-0.00$ | $-0.14$ | $-0.04$ | $-0.15$ |
| 6. 2.10 | -0.00 | 0.05 | $-0.00$ | 0.03 | 0.11 | 0.09 | 0.06 | 0.06 | -0.00 | $-0.00$ | $-0.09$ | 0.05 | 0.03 |
| 6. 2. 6 | -0.23 | -0.11 | $-0.48$ | $-0.90$ | $-0.67$ | -0.60 | -0.45 | $-0.28$ | -0.11 | -0.00 | $-0.10$ | $-0.13$ | 0.34 |
| 7. 2 | -0.10 | $-0.24$ | $-0.71$ | $-1.15$ | -0.86 | $-0.72$ | $-0.53$ | $-0.31$ | -0.18 | $-0.01$ | 0.14 | 30 |  |
| 8. 2 | -0.10 | $-0.36$ | -1.05 | -1.54 | -1.21 | $-0.94$ | -0.68 | $-0.39$ | $-0.26$ | $-0.02$ | 0.20 | 37 |  |
| 8. 1 | -0.01 | $-0.39$ | $-1.14$ | -1.4 | -1.28 | $-0.9 \mathrm{~S}$ | $-0.69$ | $-0.35$ | $-0.27$ | $-0.06$ | 0.26 | -0. 13 |  |
| 7. 1 | $-0.01$ | $-0.27$ | $-0.80$ | -1.08 | -0.93 | -0.76 | $-0.54$ | $-0.27$ | $-0.20$ | $-0.04$ | 0.20 | -0.37 | $-0.42$ |
| 9.12.3.9 | $-0.09$ | $-0.28$ | -1.11 | -1.27 | -1.08 | $-0.76$ | $-0.53$ | $-0.27$ | -0.30 | -0.09 | -0.01 | $-0.20$ | $-0.50$ |
| $72.2(9)$ | 0.01 | 0.09 | $-0.02$ | $-0.03$ | $-0.01$ | 0.03 | 0.01 | 0.08 | $-0.01$ | 0.03 | $-0.18$ | 0.09 | 0.01 |
| Dail. ext. | -0.17 | -0.12 | $-0.41$ | -0.07 | -0.01 | 0.14 | 0.17 | $-0.04$ | $-0.10$ | $-0.04$ | 0.07 | 0.02 | $-9.08$ |

## LXXIV.

Novaia Zemlia. - Matoschkin Schar. Lat. $73^{\circ}$ - ' N. Long. $57^{\circ} 20^{\prime}$ E. Gr.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Morn. 1 | -0.22 | 0.16 | 0.46 | 1.63 | 2.42 | 1.70 | 1.18 | 0.73 | 1.08 | -0.49 | -0.14 | -0.11 | 0.70 |
| 2 | -0.30 | 0.09 | 0.70 | 1.34 | 2.28 | 1.54 | 1.20 | 0.79 | 0.88 | -0.47 | -0.14 | 0.05 | 0.66 |
| 3 | -0.31 | 0.01 | 0.91 | 1.15 | 1.89 | 1.26 | 1.11 | 0.80 | 0.62 | -0.22 | -0.10 | 0.17 | 0.61 |
| 4 | -0.26 | -0.06 | 1.02 | 1.09 | 1.41 | 0.93 | 0.94 | 0.72 | 0.46 | 0.02 | -0.00 | 0.26 | 0.54 |
| 5 | -0.14 | -0.09 | 0.99 | 0.81 | 0.85 | 0.61 | 0.73 | 0.55 | 0.46 | 0.20 | 0.10 | 0.34 | 0.45 |
| 6 | -0.03 | -0.09 | 0.86 | 0.63 | 0.26 | 0.30 | 0.47 | 0.30 | 0.56 | 0.26 | 0.20 | 0.41 | 0.34 |
| 7 | 0.06 | -0.07 | 0.62 | 0.09 | -0.38 | -0.02 | 0.18 | 0.01 | 0.58 | 0.18 | 0.26 | 0.45 | 0.16 |
| 8 | 0.10 | -0.05 | 0.34 | -0.50 | -1.03 | -0.38 | -0.13 | $-0.30$ | 0.38 | 0.06 | 0.26 | 0.46 | -0.07 |
| 9 | 0.10 | - 0.05 | 0.02 | -1.14 | -1.65 | -0.78 | -0.46 | $-0.58$ | -0.00 | -0.06 | 0.24 | 0.43 | -0.33 |
| 10 | 0.07 | -0.06 | -0.25 | -1.78 | -2.17 | -1.16 | -0.75 | -0.79 | -0.71 | -0.19 | 0.18 | 0.37 | -0.61 |
| 11 | 0.05 | -0.10 | -0.58 | -2.02 | -2.53 | -1.45 | -0.97 | -0.91 | -1.24 | -0.14 | 0.15 | 0.28 | -0.79 |
| Noo | 0.05 | -0.13 | -0.78 | -2.09 | -2.67 | -1.58 | -1.08 | $-0.93$ | -1.46 | -0.12 | 0.11 | 0.18 | -0.88 |
| 1 | 0.06 | -0.14 | -0.93 | -1.93 | -2.58 | -1.52 | -1.06 | -0.85 | -1.32 | -0.10 | 0.08 | 0.10 | -0.85 |
| 2 | 0.09 | -0.14 | -0.96 | -1.62 | -2.28 | -1.32 | -0.96 | -0.70 | -0.59 | -0.09 | 0.02 | -0.0.2 | -0.74 |
| 3 | 0.10 | $-0.11$ | -0.88 | -1.26 | -1.83 | -1.05 | -0.81 | $-0.52$ | -0.40 | -0.07 | -0.04 | -0.11 | -0.58 |
| 4 | 0.10 | $-0.07$ | -0.71 | -0.80 | -1.30 | -0.75 | -0.66 | -0.32 | -0.07 | -0.02 | -0.10 | -0.20 | -0.41 |
| 5 | 10 | -0.03 | -0.50 | -0.54 | $-0.72$ | -0.57 | -0.54 | -0.14 | -0.02 | 0.10 | -0.15 | -0.26 | -0.28 |
| 6 | 0.10 | 0.02 | -0.30 | $-0.26$ | -0.14 | -0.38 | -0.43 | $-0.00$ | $-0.17$ | 0.26 | -0.20 | -0.36 | -0.16 |
| 7 | 0.10 | 0.06 | -0.16 | 0.30 | 0.46 | -0.16 | -0.30 | 0.12 | -0.35 | 0.40 | -0.15 | -0.43 | -0.01 |
| 8 | 0.12 | 0.10 | -0.09 | 0.70 | 1.04 | 0.15 | -0.11 | 0.21 | -0.36 | 0.46 | -0.14 | -0.48 | 0.13 |
| 9 | 0.12 | 0.15 | -0.06 | 1.24 | 1.59 | 0.56 | 0.14 | 0.30 | -0.12 | 0.36 | -0.10 | -0.49 | 0.31 |
| 10 | 0.08 | 0.19 | $-0.02$ | 1.50 | 2.06 | 1.02 | 0.46 | 0.39 | 0.33 | 0.18 | -0.08 | -0.44 | 0.47 |
| 11 | $\bigcirc 0.00$ | 0.21 | 0.09 | 1.75 | 2.40 | 1.42 | 0.78 | 0.50 | 0.79 | -0.15 | -0.08 | -0.34 | 0.61 |
| Midn. | -0.11 | 0.20 | 0.23 | 1.72 | 2.55 | 1.66 | 1.03 | 0.62 | 1.06 | $-0.39$ | -0.11 | -0.22 | 0.69 |
| 6. 6 | 0.04 | 0.04 | 0.28 | 0.19 | 0.06 | -0.04 | 0.02 | 0.15 | 0.20 | 0.26 | 0.00 | 0.03 | 0.10 |
| 7. 7 | 0.08 | 0.01 | 0.23 | 0.20 | 0.04 | -0.09 | -0.06 | 0.07 | 0.12 | 0.29 | 0.04 | 0.01 | 0.08 |
| 8. 8 | 0.11 | 0.03 | 0.13 | 0.10 | 0.01 | -0.12 | -0.12 | -0.05 | 0.01 | 0.26 | 0.06 | -0.01 | 0.03 |
| 9. 9 | 0.11 | 0.05 | -0.02 | 0.05 | $-0.03$ | -0.11 | -0.16 | $-0.14$ | -0.06 | 0.15 | 0.07 | -0.03 | -0.01 |
| 10.10 | 0.08 | 0.07 | -0.15 | -0.14 | -0.06 | -0.07 | -0.15 | $-0.20$ | -0.19 | -0.01 | 0.05 | -0.04 | -0.07 |
| 7. 2. 9 | 0.09 | -0.02 | -0.13 | -0.10 | -0.36 | -0.26 | -0.21 | -0.13 | -0.14 | 0.15 | 0.06 | -0.02 | -0.09 |
| 6. 2. 8 | 0.06 | $-0.04$ | -0.06 | -0.10 | -0.33 | -0.29 | $-0.20$ | $-0.06$ | $-0.23$ | 0.21 | 0.03 | -0.03 | -0.09 |
| 6. 2.10 | 0.0 .5 | -0.01 | -0.04 | 0.17 | 0.01 | -0.00 | -0.01 | -0.00 | -0.00 | 0.12 | 0.05 | -0.02 | 0.03 |
| 6. 2. 6 | 0.05 | -0.07 | -0.13 | -0.42 | $-0.72$ | -0.47 | -0.31 | $-0.13$ | -0.17 | 0.14 | 0.01 | 0.01 | -0.18 |
| 7. 2 | 0.08 | -0.11 | $-0.17$ | -0.77 | -1.33 | $-0.67$ | -0.39 | $-0.35$ | -0.16 | 0.05 | 0.14 | 0.22 | -0.29 |
| 8. 2 | 0.10 | -0.10 | -0.31 | -1.06 | -1.66 | -0.85 | -0.55 | -0.50 | $-0.26$ | $-0.02$ | 0.14 | 0.22 | -0.40 |
| 8. 1 | 0.08 | -0.10 | -0.30 | -1.22 | -1.81 | -0.95 | $-0.60$ | $-0.58$ | -0.47 | -0.02 | 0.17 | 0.28 | $-0.46$ |
| 7. 1 | 0.06 | -0.11 | $-0.16$ | -0.92 | -1.48 | -0.77 | -0.44 | $-0.42$ | -0.37 | 0.04 | 0.17 | 0.28 | -0.34 |
| 9.12.3.9 | 0.09 | -0.04 | $-0.43$ | -0.81 | -1.14 | -0.71 | $-0.55$ | $-0.43$ | -0.50 | 0.03 | 0.05 | -0.00 | -0.37 |
| 7. 2.2(9) | 0.10 | 0.02 | $-0.12$ | 0.24 | 0.13 | -0.06 | $-0.13$ | -0.02 | -0.14 | 0.20 | 0.02 | -0.14 | 0.01 |
| Dail.ext. | -0.10 | 0.04 | 0.03 | -0.17 | -0.06 | 0.06 | 0.06 | -0.07 | -0.19 | -0.02 | 0.03 | -0.02 | -0.09 |

The numbers without sign must be added; those with the sign - must be subtracted.

Norway. - Bossekop. Lat. $69^{\circ} 58^{\prime}$ N. Long. $22^{\circ}$ E. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true
Mean Temperatures of the respective Days, Months, and of the Year. - Dove.
Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | Sept. | Oct. | Nov. | Dec. | 80 Days without Sun. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A.M. 2 | -0.26 | 0.36 | 1.37 | -•• | 1.20 | 0.66 | 0.04 | 0.35 | 0.04 |
| 4 | -0.11 | 0.30 | 1.78 |  | 1.01 | 0.53 | -0.03 | 0.12 | 0.10 |
| 6 | 0.00 | 0.50 | 1.90 |  | 1.22 | 0.73 | 0.04 | 0.28 | 0.08 |
| 8 | 0.09 | 0.26 | 1.18 | 0.36 | 0.62 | 0.41 | 0.07 | 0.10 | 0.02 |
| 10 | $-0.13$ | $-0.19$ | -1.09 | -0.83 | -1.01 | -0.29 | -0.15 | -0.14 | -0.19 |
| Noon. | 0.18 | -0.79 | -2.39 | -1.29 | -1.66 | -1.05 | -0.13 | -0.09 | -0.03 |
| 2 | 0.20 | -1.02 | -2.55 | -1.22 | -1.69 | $-1.02$ | -0.09 | -0.34 | -0.10 |
| 4 | 0.30 | -0.11 | -2.38 | -0.82 | -1.54 | -0.50 | 0.09 | -0.38 | 0.06 |
| 6 | 0.18 | 0.06 | -0.57 | -0.10 | -0.27 | -0.17 | 0.18 | -0.23 | 0.09 |
| 8 | 0.12 | 0.16 | 0.46 | 0.70 | 0.39 | 0.09 | 0.14 | -0.26 | 0.02 |
| 10 | -0.31 | 0.21 | 1.19 | 1.44 | 0.79 | 0.13 | -0.03 | 0.14 | -0.10 |
| 12 | -0.27 | 0.22 | 1.39 | 1.83 | 0.89 | 0.49 | -0.13 | 0.17 | -0.10 |
| Mean. | -7.67 | -6.39 | -7.55 | -0.77 | 5.91 | -1.62 | -6.55 | -5.66 | -7.66 |

## LXXV'.

Norway. - Bossekop. Lat. $69^{\circ} 58^{\prime} \mathrm{N}$. Long. $22^{\circ}$ E. Greenw.
Centigrade Degrees.

| Hour. | Jan. | Feb. | March. | April. | Sept. | Oct. | Nov. | Dee. | 80 Days without Sun. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A.M. 2 | -0.32 | 0.45 | 1.71 |  | 1.50 | 0.62 | 0.0.5 | 0.44 | 0.05 |
| 4 | -0.14 | 0.37 | 2.22 |  | 1.26 | 0.66 | -0.04 | 0.52 | 0.12 |
| 6 | 0.00 | 0.62 | 2.37 |  | 1.52 | 0.91 | 0.05 | 0.35 | 0.10 |
| 8 | 0.11 | 0.32 | 1.47 | 0.45 | 0.77 | 0.51 | 0.09 | 0.12 | 0.02 |
| 10 | -0.16 | -0.24 | -1.36 | -1.06 | $-1.26$ | -0.36 | -0.19 | -0.17 | -0.24 |
| Noon. | 0.22 | -0.99 | -2.98 | -1.62 | -2.07 | -1.31 | -0.16 | -0.11 | -0.04 |
| 2 | 0.25 | -1.27 | -3.56 | -1.52 | -2.11 | -1.27 | -0.11 | -0.42 | -0.12 |
| 4 | 0.37 | -0.14 | -2.97 | -1.02 | -1.92 | -0.62 | 0.11 | -0.47 | 0.07 |
| 6 | 0.22 | 0.07 | -0.71 | -0.12 | -0.34 | -0.21 | 0.22 | -0.29 | 0.11 |
| 8 | 0.15 | 0.20 | 0.57 | 0.87 | 0.49 | 0.11 | 0.17 | -0.32 | 0.02 |
| 10 | -0.42 | 0.26 | 1.48 | 1.80 | 0.99 | 0.16 | -0.04 | 0.17 | -0.12 |
| 12 | -0.34 | 0.27 | 1.73 | 2.29 | 1.11 | 0.61 | -0.16 | 0.21 | -0.12 |
| Mean. | -9.59 | -7.99 | -9.44 | -0.96 | 7.39 | -2.02 | -8.19 | -7.07 | -9.57 |

# H0URLY CORRECTIONS 

FOR

## PERIODIC VARIATIONS.

AFRICA.-AUSTRALIA.

## LXXVI.

Africa. - St. Helena. Lat. $155^{\circ} 55^{\prime}$ S. Long. $5^{\circ} 43^{\prime}$ W. Greenw.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 0.76 | 0.70 | 0.63 | 0.58 | 0.52 | 0.43 | 0.48 | 0.43 | 0.52 | 0.62 | 0.71 | 0.73 | 0.59 |
| 1 | 0.55 | 0.76 | 0.71 | 0.66 | 0.61 | 0.48 | 0.53 | 0.48 | 0.56 | 0.71 | 0.78 | 0.81 | 0.66 |
| 2 | 0.93 | 0.54 | 0.77 | 0.70 | 0.66 | 0.54 | 0.56 | 0.53 | 0.62 | 0.78 | 0.56 | 0.90 | 0.72 |
| 3 | 1.03 | 0.92 | 0.86 | 0.76 | 0.73 | 0.59 | 0.62 | 0.63 | 0.69 | 0.86 | 0.95 | 0.98 | 0.80 |
| 4 | 1.06 | 1.00 | 0.92 | 0.81 | 0.80 | 0.65 | 0.66 | 0.66 | 0.76 | 0.91 | 0.99 | 1.02 | 0.55 |
| 5 | 1.11 | 1.04 | 0.93 | 0.86 | 0.83 | 0.67 | 0.69 | 0.73 | 0.79 | 0.94 | 1.02 | 1.08 | 0.89 |
| 6 | 1.15 | 1.07 | 0.98 | 0.93 | 0.83 | 0.68 | 0.72 | 0.74 | 0.83 | 0.99 | 1.07 | 1.09 | 0.92 |
| 7 | 1.16 | 1.08 | 0.97 | 0.94 | 0.59 | 0.71 | 0.75 | 0.79 | 0.81 | 0.96 | 1.03 | 1.06 | 0.93 |
| 8 | 0.95 | 0.99 | 0.78 | 0.85 | 0.88 | 0.69 | 0.72 | 0.72 | 0.72 | 0.77 | 0.50 | 0.98 | 0.52 |
| 9 | 0.53 | 0.63 | 0.52 | 0.49 | 0.46 | 0.42 | 0.41 | 0.13 | 0.42 | 0.38 | 0.40 | 0.48 | 0.46 |
| 10 | -0.05 | 0.06 | -0.07 | -0.04 | -0.0s | -0.04 | -0.0.4 | -0.02 | -0.0. | -0.17 | -0.16 | -0.09 | -0.06 |
| 11 | -0.62 | -0.55 | -0.49 | -0.51 | -0.47 | -0.40 | $-0.40$ | -0.40 | $-0.55$ | -0.66 | -0.67 | $-0.56$ | -0.52 |
| Noon. | -1 | -1.06 | -0.95 | -1.00 | -0.96 | -0.73 | -0.76 | -0.50 | -0.92 | -1.11 | -1.12 | -1.08 | -0.97 |
| 1 | -1.64 | -1.46 | -1.28 | -1.31 | $-1.20$ | $-1.04$ | $-1.06$ | -1.12 | -1.25 | -1.45 | -1.60 | -1.52 | -1.33 |
| 2 | -1.81 | -1.67 | $-1.48$ | $-1.46$ | -1.32 | $-1.20$ | -1.26 | -1.2. | -1.42 | -1.67 | -1.80 | -1.80 | -1.51 |
| 3 | -1.76 | -1.78 | -1.62 | -1.50 | -1.35 | -1.18 | -1.24 | -1.31 | -1.38 | -1.64 | -1.84 | -1.82 | -1.54 |
| 4 | -1.69 | -1.66 | -1.54 | -1.35 | -1.2 4 | -1.03 | -1.12 | -1.13 | -1.20 | -1.37 | -1.64 | -1.76 | -1.39 |
| 5 | -1.48 | -1.38 | -1.27 | -1.06 | -0.94 | -0.78 | -0.34 | -0.86 | -0.91 | -0.99 | -1.24 | -1.38 | -1.09 |
| 6 | -0 | -0. | -0.83 | -0.61 | -0.47 | -0.40 | -0.44 | -0.42 | -0.43 | -0.48 | -0.66 | -0.92 | -0.62 |
| 7 | -0.27 | $-0.33$ | -0.23 | -0.11 | -0.23 | -0.03 | -0.07 | -0.03 | 0.01 | 0.02 | -0.04 | -0.18 | -0.13 |
| 8 | 0.26 | 0.21 | 0.18 | 0.20 | -0.12 | 0.17 | 0.13 | 0.15 | 0.23 | 0.29 | 0.32 | 0.30 | 0.19 |
| 9 | 0.47 | 0.44 | 0.34 | 0.34 | 0.14 | 0.26 | 0.23 | 0.25 | 0.32 | 0.26 | 0.48 | 0.48 | 0.33 |
| 10 | 0.60 | 0.55 | 0.48 | 0.44 | 0.11 | 0.32 | 0.33 | 0.32 | 0.38 | 0.49 | 0.56 | 0.58 | 0.46 |
| 11 | 0.69 | 0.64 | 0.55 | 0.51 | 0.45 | 0.39 | 0.38 | 0.38 | 0.46 | 0.55 | 0.64 | 0.67 | 0.53 |
| Mean. | 14.21 | 15.04 | 15.22 | 14.93 | 13.80 | 12.48 | 11.55 | 11.19 | 11.14 | 11.66 | 12.37 | 13.23 |  |
|  |  |  |  |  |  | LX | II. |  |  |  |  |  |  |
| Africa.-Cape of Good Hore. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Hour | Ja | Feb | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor |  | ear. |
| Midn. | 1.69 | 1.50 | 1.51 | 1.37 | 1.00 | 0.88 | 1.04 | 0.85 | 1.07 | 1.45 | 1.62 | 5 | 1.32 |
| 1 | 2.80 | 1.64 | 1.64 | 1.49 | 1.07 | 1.01 | 1.20 | 1.03 | 1.2.) | 1.62 | 1.79 | 2.01 | 1.55 |
| 2 | 1.89 | 1.74 | 1.81 | 1.61 | 1.14 | 1.09 | 1.33 | 1.14 | 1.39 | 1.72 | 1.98 | 2.16 | 1.58 |
| 3 | 2.01 | 1.92 | 1.92 | 1.70 | 1.24 | 1.16 | 1.43 | 1.23 | 1.54 | 1.82 | 2.12 | 2.30 | 1.70 |
| 4 | 2.10 | 2.00 | 2.05 | 1.88 | 1.34 | 1.30 | 1.53 | 1.37 | 1.63 | 1.92 | 2.21 | 2.42 | 1.81 |
| 5 | 1.96 | 2.13 | 2.13 | 1.93 | 1.46 | 1.42 | 1.59 | 1.53 | 1.59 | 1.93 | 1.92 | 2.01 | 1.50 |
| 6 | 1.06 | 1.53 | 1.97 | 1.98 | 1.59 | 1.48 | 1.73 | 1.55 | 1.62 | 1.26 | 0.85 | 0.86 | 1.46 |
| 7 | 0.15 | 0.70 | 1.21 | 1.39 | 1.41 | 1.47 | 1.57 | 1.22 | 0.81 | 0.39 | -0.02 | -0.20 | 0.84 |
| 8 | -0.53 | -0.01 | 0.16 | - 0.36 | 0.53 | 0.86 | 0.77 | 0.64 | -0.06 | -0.46 | -0.67 | -0.81 | 0.06 |
| 9 | -1.10 | $-0.80$ | -0.76 | -0.68 | $-0.39$ | -0.12 | -0.24 | -0.42 | -0.82 | -1.24 | -1.25 | -1.36 | $-0.77$ |
| 10 | -1.72 | -1.65 | -1.66 | -1.48 | -1.10 | -0.90 | $-1.09$ | $-1.08$ | -1.41 | -1.82 | $-1.80$ | -1.90 | $-1.47$ |
| 11 | -2.23 | -2.31 | -2.37 | $-2.10$ | -1.64 | -1.46 | -1.72 | -1.63 | -1.9.5 | -2.25 | -2.24 | -2.2.) | -2.00 |

The numbers without sigu must be added ; those with the sign - must be subtracted.

Africa. - Cape of Good Hope, Continued.
Corrections to be applied to the Means of the Hours of Observation to obtain the true Mean Temperatures of the respective Days, Months, and of the Year. - Dove.

Degrees of Reaumur.

| Hour. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dee. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Noon. | -2.48 | -2.72 | -2.66 | -2.56 | -2.09 | -1.92 | -2.11 | -1.88 | -2.15 | -2.45 | -2.46 | -2.52 | -2.33 |
| 1 | -2.54 | -2.74 | -2.95 | -2.81 | -2.20 | -2.07 | -2.33 | -2.04 | -2.23 | -2.55 | -2.48 | -2.61 | -2.46 |
| 2 | $-2.42$ | -2.54 | -2.86 | -2.79 | -2.14 | -2.06 | -2.33 | -1.97 | -2.18 | -2.44 | -2.30 | -2.44 | -2.37 |
| 3 | -2.16 | -2.20 | -2.51 | -2.42 | -1.84 | -1.86 | -2.13 | -1.77 | -1.82 | -2.08 | -2.01 | -2.16 | -2.08 |
| 4 | -1.75 | -1.70 | -1.78 | -1.75 | -1.28 | -1.23 | $-1.49$ | -1.32 | -1.28 | -1.52 | -1.66 | -1.90 | -1.56 |
| 5 | -1.21 | -1.09 | -1.03 | $-0.71$ | -0.6 I | -0.64 | -0.76 | -0.57 | -0.56 | -0.71 | -1.05 | -1.28 | -0.85 |
| 6 | -0.16 | -0.13 | -0.10 | -0.03 | -0.21 | -0.29 | -0.33 | -0.17 | 0.00 | 0.20 | -0.01 | -0.15 | -0.12 |
| 7 | 0.65 | 0.54 | 0.35 | 0.22 | 0.09 | -0.05 | -0.03 | 012 | 0.30 | 0.57 | 0.60 | 0.63 | 0.33 |
| 8 | 0.95 | 0.79 | 0.61 | 0.48 | 0.36 | 0.19 | 0.26 | 0.32 | 0.51 | 0.36 | 0.92 | 0.96 | 0.60 |
| 9 | 1.14 | 1.00 | 0.92 | 0.73 | 0.54 | 0.40 | 0.45 | 0.46 | 0.69 | 1.09 | 1.10 | 1.20 | 0.81 |
| 10 | 1.30 | 1.14 | 1.14 | 1.00 | 0.78 | 0.61 | 0.69 | 0.65 | 0.97 | 1.26 | 1.31 | 1.46 | 1.03 |
| 11 | 1.55 | 1.32 | 1.29 | 1.22 | 0.95 | 0.81 | 0.91 | 0.76 | 1.02 | 1.44 | 1.48 | 1.67 | 1.20 |
| Mean. | 15.81 | 15.96 | 15.00 | 13.61 | 11.38 | 9.81 | 9.96 | 10.06 | 11.01 | 12.43 | 13.54 | 14.82 |  |

## LXXVIII.

Australia. - Hobarton. Lat. $42^{\circ} 53^{\prime}$ S. Long. $147^{\circ} 21^{\prime}$ E. Gr. - Dove.
Degrees of Reaumur.

| Hour | Jan | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | De | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | 2.31 | 1.95 | 78 | 1.31 | 0.88 | . 66 | 0.72 | 1.10 | 1.51 | 1.99 | 2.44 | 2.45 | 1.59 |
| 1 | 2.59 | 2.17 | 99 | 1.41 | 1.03 | 0.76 | 0.86 | 1.36 | 1.71 | 2.19 | 2.67 | 2.76 | 79 |
| 2 | 2.59 | 2.32 | 2.19 | 1.62 | 1.11 | 0.88 | 1.01 | 1.43 | 1.93 | 2.45 | 2.77 | 2.95 | . 96 |
| 3 | 3.09 | 2.53 | 2.39 | 1.75 | 1.23 | 0.97 | 1.16 | 1.58 | 2.06 | 2.68 | 2.98 | 3.24 | . 14 |
| 4 | 3.20 | 2.68 | 2.49 | 1.85 | 1.31 | 1.15 | 1.23 | 1.69 | 2.20 | 2.80 | 3.11 | 3.38 | 2.26 |
| 5 | 3.33 | 2.82 | 2.54 | 1.99 | 1.44 | 1.15 | 1.40 | 1.82 | 2.32 | 2.85 | 2.99 | 3.13 | 2.31 |
| 6 | 2.62 | 2.59 | 2.64 | 2.11 | 1.5 | 1.29 | 1.5 | 1.91 | 2.34 | 2.60 | 2.24 | 2.24 | 2.14 |
| 7 | 18 | 1.73 | 2.10 | 2.00 | 1.60 | 1.37 | 1.50 | 1.90 | 1.84 | 1.61 | 1.16 | 1.03 | 1.61 |
| 8 | 0.27 | 0.68 | 1.05 | 1.30 | 1.27 | 1.26 | 1.31 | 1.32 | 0.93 | 0.41 | 0.01 | -0.24 | 0.80 |
| 9 | -0.88 | -0.56 | -0.17 | 0.21 | 0.45 | 0.60 | 0.60 | 0.44 | -0.21 | -0.70 | -1.13 | -1.27 | -0.22 |
| 10 | -1.92 | -1.61 | -1.28 | -0.85 | $-0.46$ | -0.18 | $-0.21$ | -0.52 | -1.21 | -1.68 | -2.10 | -2.16 | -1.18 |
| 11 | -2.75 | -2.34 | -2.24 | -1.78 | -1.29 | -0.96 | -1.01 | -1.53 | -2.09 | -2.54 | -2.89 | -2.85 | -2.02 |
| Noon. | -3 | -3.22 | -3 | -2.58 | -2.0 | -1.67 | -1.67 | -2.28 | -2.70 | -3.10 | -3.43 | -3.36 | -2.71 |
| 1 | -3.82 | -3.52 | -3 18 | -2.95 | -2.42 | -2.08 | -2.17 | -2.73 | -3.14 | -3.48 | -3.72 | -3.67 | -3.10 |
| 2 | -3.91 | -3.54 | -3.63 | -3.11 | -2.53 | -2.22 | -2.38 | -2.91 | -3.25 | -3.18 | -3.67 | -3.56 | -3.18 |
| 3 | -3.60 | -3.36 | $-3+3$ | -2.87 | -2.3 | -2.02 | -2.23 | -2.71 | -3.10 | -3.32 | -3.33 | -3.45 | -2.98 |
| 4 | -3.20 | -2.94 | -2.92 | -2.23 | -1.69 | -1.43 | -1.73 | $-2.20$ | -2.53 | -3.04 | -3.12 | -3.12 | -2.51 |
| 5 | -2.57 | -2.22 | -2.02 | -1.35 | $-0.92$ | -0.73 | -1.01 | -1.37 | -1.59 | -2.02 | -2.30 | -2.56 | -1.72 |
| 6 | -1.38 | -1.04 | -0 84 | -0.56 | -0.36 | -0.25 | -0.48 | -0.64 | -0.65 | -0.80 | -1.01 | -1.38 | -1.78 |
| 7 | -0.13 | -0.20 | -0.04 | -0.05 | 0.01 | 0.00 | 0.12 | -0.13 | 0.01 | 0.05 | 0.20 | -0.09 | -0.02 |
| 8 | 0.82 | 0.68 | 0.45 | 0.32 | 0.27 | 0.24 | 0.14 | 0.21 | 0.46 | 0.55 | 0.90 | 0.89 | 0.49 |
| 9 | 1.31 | 1.13 | 0.82 | 0.57 | 0.42 | 0.24 | 0.34 | 0.57 | 0.79 | 1.00 | 1.41 | 1.51 | 0.84 |
| 10 | 1.71 | 1.47 | 1.19 | 0.84 | 0.62 | 0.40 | 0.50 | 0.79 | 1.08 | 1.34 | 1.75 | 1.91 | 1.13 |
| 11 | 2.05 | 1.77 | 1.47 | 1.06 | 0.77 | 0.54 | 0.64 | 0.93 | 1.31 | 1.63 | 2.05 | 2.25 | 1.37 |
| Mean. | 3.35 | 13.96 | 11.96 | 9.41 | 7.69 | 5.93 | 5.21 | 6.24 | 7.97 | 9.39 | 11.38 | 12.95 |  |

The numbers without sign must be added; those with the sign - must be subtracted.

# CORRECTIONS FOR TEMPERATURE. 

MONTHLY AND YEARLY<br>CORRECTIONS FOR NON-PERIODIC VARIATIONS,<br>OR<br>\section*{TABLES}<br>FOR REDUCING THE MONTULY AND YEARLY MEANS OF SINGLE yEARS TO THE MEANS DERIVED FROB A SERIES OF Years.

## TABLES

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FOR REDUCING THE MONTHLY AND YEARLY MEANS OF SINGLE YEARS TO THE
    MEANS DERIVED FROM A SERIES OF YEARS.
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Observation shows that the monthly and annual mean temperature of a place somewhat varies from year to year. No law, however, has been as yet discovered as to the course of these oscillations. It follows that the means derived from observations carried on during a single year are but approximations to the true means. These last must be obtained from observations made for a series of years, during which these irregular variations become insensible by compensating cach other ; and it is obvious that their accuracy increases with the number of years which compose the series.

Professor Dove, having proved by his researches that these abnormal temperatures above and below the average of a whole month, or of a year, are apt to be felt simultaneously on extensive tracts of country, concluded that the means of a single year could be made available for obtaining the true means of the place, by being corrected for the non-periodic variations by means of normal stations in the same meteorological region, in which those elements had been more accurately determined by the observations of a long series of years. Comparing, namely, the means of a given year with the means derived from the whole series, we find a difference in + or - , which, applied, with reverse signs, to the means of the same year in the neighboring station to be corrected, will reduce, with a good degree of probability, the means of that particular year to the means which would have been obtamed from a long series of years similar to that of the normal station.

The following tables, LXXIX. to XCVII., have been selected from those given by Dove in his five papers on the non-periodic variations of the atmospheric temperature, to be found in the Memoirs of the Academy of Sciences of Berlin for the years $1838,1839,1842,1848$, and 1853 , to which we must refer for further details. 'They furnish normal stations for various latitudes; the columns contain the corrections for every month, viz. the differences, with reverse signs, between the monthly means in the year indicated in the first and last columns, and the means derived from the whole series, which are contained in the line at the bottom.

Region of the Monsoons. - Madras.
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  | $\bigcirc$ |  |  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |  |
| 1796 | 0.00 | 0.24 | 0.00 | 0.36 | -0.10 | -1.48 | -1.16 | -1.15 | -0.31 | -0.28 | -0.47 | -0.51 | 1796 |
| 1797 |  |  | 0.66 | 0.53 | 0.39 | 0.56 | 0.09 | 0.85 | -0.09 | -0.33 | 0.16 | -0.02 | 1797 |
| 1798 | -0.13 | 1.12 | 0.40 |  |  | 0.39 | 0.53 | -0.31 | 0.27 | 0.56 | -0.16 | 0.20 | 1798 |
| 1799 | -0.13 | -0.08 | 0.62 | 0.36 | 0.26 | -0.06 | -1.20 | 0.00 | -0.36 | 0.38 | -1.44 | 0.25 | 1799 |
| 1800 | 0.40 | 0.41 | 0.57 | 1.20 | -0.23 | -0.50 | -1.02 | -0.40 | -0.58 | 0.20 | 0.47 | -0.60 | 1800 |
| 1801 | 0.44 | 0.01 | 1.77 |  |  | -0.59 | -0.67 | 0.63 | -0.49 | -0.02 | -0.20 | 0.25 | 1801 |
| 1802 | 0.44 | 0.86 | 1.77 | 1.02 | -0.36 | 0.65 | 0.58 | -0.04 | 1.60 | 0.43 | -0.02 | -0.28 | 1802 |
| 1503 | 0.22 | 0.21 | 0.80 | 0.53 | -0 32 | 0.08 | 0.18 | 0.80 | 0.80 | 0.38 | 0.33 | 0.65 | 1803 |
| 1804 | 1.64 | 1.18 | 0.75 | 1.38 | 0.70 | 0.70 | 1.24 | 0.00 | 0.58 | 0.38 | 0.91 | 0.29 | 1904 |
| 1805 | 0.27 | 0.41 | 0.66 | -0.36 | 0.61 | 0.52 | $-0.76$ | -0.22 | -0.27 | -0.33 | 0.69 | 0.65 | 1805 |
| 1806 | 0.00 | -0.39 | -0 09 | 0.09 | -0.41 | -1.61 | 0.00 | $-0.13$ | 1.07 | 0.47 | 0.96 | 0.12 | 1806 |
| 1807 | 0.22 | -1.54 | -3.20 | -5.47 | -1.79 | 0.48 | 1.20 | -0.17 | -0.09 | -0.64 | -0.20 | 0.78 | 1807 |
| 1813 | 0.80 | 0.37 | 0.13 | 0.96 | 1.12 | -0.32 | 0.44 | -0.22 | -0.18 | 0.25 | $-0.38$ | -1.04 | 1813 |
| 1814 | -0.36 | -0.39 | -0.58 | 0.04 | -2.99 | 1.10 | 1.38 | 0.29 | -0.22 | 0.07 | $-0.20$ | $-0.37$ | 1814 |
| 1515 | -0.98 | 0.32 | -0.67 | 2.00 | 1.55 | $-1.39$ | -0.98 | 0.27 | 0.31 | $-0.73$ | -0.91 | $-0.82$ | 1815 |
| 1816 | -1.09 | -1.76 | -1.56 | -0.93 | 0.44 | 0.39 | -0.44 | -0.71 | -0.67 | -0.20 | 0.33 | -0.51 | 1816 |
| 1817 | -0.58 | -0.70 | -0.67 | -0.62 | 0.12 | -0.19 | 0.67 | 0.29 | $-0.71$ | -0.55 | -0.96 | 0.52 | 1817 |
| 1818 | 0.22 | 0.32 | -0.s0 | -0.04 | 1.41 | 0.65 | -1.33 | -2.00 | -0.15 | -0.55 | -0.56 | -0.37 | 1818 |
| 1819 | -1.78 | -1.28 | -0.76 | -0.13 | 0.45 | 0.88 | 0.44 | 0.98 | $-0.31$ | 0.03 | 0.78 | 0.16 | 1819 |
| 1820 | -0.67 | -0.30 | -0.55 | 0.5 | -1.16 | -0.32 | 0.18 | 0.23 | -0.09 | 0.47 | 0.69 | 0.47 | 1820 |
| 1821 | 1.02 | 0.64 | 1.06 | -1.51 | 0.26 | 0.05 | 0.58 | 0.94 | -0.04 | -0.02 | 0.20 | 0.20 | 1821 |
| Means. | 19.19 | 20.07 | 21.30 | 22.41 | 24.41 | 24.96 | 23.84 | 23.43 | 23.03 | 22.16 | 20.74 | 19.45 | Mea |
| 1822 | -0.36 | 0.37 | 0.41 | -0.28 | 0.07 | -0.95 | $-0.76$ | 0.72 | -0.37 | -0.70 | -0.35 | -0.19 | 1822 |
| 1523 | 0.31 | 0.37 | -0.21 | 0.30 | 0.15 | 0.29 | 0.22 | 0.17 | -0.60 | 0.72 | 0.27 | 0.97 | 1823 |
| 18.4 | 0.71 | 0.59 | 0.27 | 0.52 | -0.02 | 0.60 | 1.55 | 0.88 | 1.36 | -0.93 | 0.14 | 0.26 | 1824 |
| 18.5 | -0.09 | 0.37 | -0.21 | 0.12 | 0.24 | -0.29 | 0.04 | -0.36 | 0.03 | 0.32 | 0.59 | $-0.59$ | 1825 |
| 1826 | 0.80 | 0.24 | 0.45 | 0.92 | 0.78 | -1.17 | 0.04 | -0.36 | 0.25 | 0.81 | 0.36 | 0.30 | 1826 |
| 1827 | -0.09 | -0.29 | -0.17 | 0.17 | -1.27 | -0.46 | -0.01 | -0.09 | -0.15 | -0.13 | 0.54 | 0.08 | 1827 |
| 1828 | 07 | 0.51 | -0.57 | -0.59 | -0.42 | 0.34 | -0.23 | 0.04 | -0.60 | -0.17 | 0.81 | 0.21 | 1828 |
| 1529 | 0.09 | -0.69 | -0.35 | 0.08 | -0.11 | 0.16 | -0.89 | -0.01 | 0.16 | 0.54 | 0.23 | 0.12 | 1829 |
| 1830 | -0.27 | -0.74 | 0.01 | -0.32 | $-2.73$ | -0.15 | -0.36 | -0.23 | 0.25 | 1.12 | 0.68 | 0.53 | 1830 |
| 1831 | 0.31 | 1.49 | 1.66 | 0.48 | 1.59 | 1.36 | 0.04 | 0.67 | 0.70 | 0.41 | 0.41 | 0.53 | 1831 |
| 1832 | -0.49 | -0.29 | 1.26 | 1.73 | 2.51 | 2.65 | 1.64 | 2.40 | 0.34 | -0.25 | 0.46 |  | 1832 |
| 1533 | 0.36 | 0.91 | -0.19 | 0.97 | 0.83 | 0.83 | 1.33 | 0.40 | 0.16 | 0.41 | 0.19 | 1.06 | 1833 |
| 1834 | 0.18 | 0.60 | . 3.5 | -0.58 | 1.31 | 0.12 | -0.98 | -0.18 | -0.15 | -0.03 | 0.01 | -0.01 | 1834 |
| 183.5 | -0.66 | -0.73 | -0.5 | -1.07 | -0.24 | -0.96 | -0.67 | -0.45 | -0.46 | -0.7 | -0.48 | -0.94 | 1835 |
| 18:36 | -0.75 | -0.73 | -1.41 | -0.72 | 0.60 | 0.12 | -0.58 | -1.29 | -0.24 | 0.15 | -0.92 | -1.03 | 1236 |
| 1837 | -0.31 | -0.02 | 0.06 | -0.63 | -1.17 | -0.41 | -0.40 | -0.05 | 0.03 | -0.34 | -0.17 | -0.85 | 1837 |
| 1858 | -1.24 | -0.69 | -0.30 | . 04 | -0.33 | -0.24 | 0.75 | -0.05 | 0.65 | -0.12 | -0.57 | -0.41 | 1838 |
| 1839 | 0.36 | -0.11 | $-0.12$ | -0.4.5 | -0.15 | -0.41 | -0.49 | -0.93 | -0.68 | 0.68 | -0.53 | 0.71 | 1839 |
| 1840 | -0.13 | -0.42 | $-0.70$ | 0.17 | 0.29 | 0.2 .5 | -0.45 | 0.27 | -0.75 | 0.19 | -1.14 | -0.32 | 18.10 |
| 1541 | 0.05 | -0.16 | -0.17 | -0.58 | -1.17 | -0.81 | 0.35 | -0.71 | 0.74 | -1.28 | -0.34 | -0.27 | 1841 |
| 1842 | -0.09 | -0.51 | -0.08 | -0.49 | 0.47 | 0.07 | 0.00 | 0.09 | -0.86 | -0.30 | -0.30 | -0.23 | 1842 |
| 1843 | 0.23 | -0.02 | -0.03 | 0.22 | -1.53 | -1.0.1 | - 2.22 | 0.44 | 0.16 | -0.52 | 0.23 | -0.32 | 184.3 |
| Means. | 29.53 | 21.31 | 22.92 | 24.27 | 25.62 | 25.35 | 24.31 | 23.73 | 23.70 | 22.92 | 21.32 | 20.67 | Means. |

The numbers without sign must be subtracted; those with the sign - must be added.

Sicily. - Palermo.
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 791 | - | $\bigcirc$ | - | $\bigcirc$ | -0.44 | $-0.32 \mid$ | -0.52 | $\stackrel{\circ}{\circ} \mathrm{O} .95$ | $\stackrel{\circ}{-0.67}$ | $\begin{gathered} \circ \\ -0.36 \end{gathered}$ | $\stackrel{\circ}{1.73}$ | $\begin{aligned} & \circ \\ & 0.00 \end{aligned}$ | 1791 |
| 1792 | 1.18 | 0.51 | 0.09 | 0.12 | -0.48 | 1.12 | -1.01 | -1.65 | -0.63 | 0.22 | -0.53 | $-0.96$ | 1792 |
| 1793 | -1.68 | -0.38 | -0.33 | -1.63 | $-2.04$ | -1.83 | -1.28 | -1.14 | 0.86 | -0.54 | -0.25 | 0.44 | 1793 |
| 1794 | -0.04 | -0.69 | -0.51 | 0.59 | -0.79 | -1.92 | -0.81 | -0.48 | -0.14 | -0.69 | -0.29 | -0.47 | 1794 |
| 1795 | -1.62 | 1.27 | 0.78 | -0.10 | 0.12 | -0.59 | -1.12 | -0.34 | -0.72 |  | -0.23 | 0.18 | 1795 |
| 1796 | 0.78 | 0.58 | -0.84 | -1.56 | -0.19 | -0.59 | -0.39 | -0.01 | 0.40 | 1.11 | 0.00 | 0.98 | 1796 |
| 1797 | -0.24 | -0.29 | -1.15 | -0.19 | -0.24 | -0.70 | -0.56 | 0.39 | 0.15 | 0.13 | -0.12 | 0.16 | 1797 |
| 1798 | 0.03 | 0.20 | 0.78 | -0.90 | -0.99 | -0.45 | 0.72 | -0.41 | 0.00 | -1.00 | 1.97 | 0.31 | 1798 |
| 1799 | -1.75 | 1.38 | 0.52 | 0.64 | -0.35 | 0.08 | 0.37 | 0.75 | 0.48 | 1.40 | -0.32 | 0.40 | 1799 |
| 1800 | 2.27 | 2.96 | 0.69 | 2.46 | 0.63 | -0.14 | 0.26 | -0.41 | -0.58 | 0.02 | -0.18 | 0.09 | 1500 |
| 1801 | -0.11 | 0.76 | 1.45 | 0.24 | -0.10 | -0.16 | 1.26 | -0.56 | -0.07 | 1.04 | 1.04 | 1.64 | 1801 |
| 1802 | 0.09 | -0.16 | 0.47 | -1.01 | -0.30 | 2.50 | 0.17 | 0.72 | 0.42 | 0.77 | 1.51 | 1.40 | 1802 |
| 1803 | 67 | $-1.69$ |  | 2.08 | -1.08 | 0.66 | 0.04 | 0.52 | 0.31 | -0.65 | 1.42 | 0.42 | 1803 |
| 1804 | . 3 | -0.82 | 0.16 | 0.21 | 0.14 | 1.30 | 1.12 | 0.12 | -0.14 | 0.31 | 1.22 | 1.40 | 1804 |
| 1505 | 0.80 | 0.69 | -0.68 | -1.59 | -1.59 | 1.21 | -0.65 | -0.34 | $-1.52$ | 0.06 | -1.55 | -1.02 | 1805 |
| 1806 | -1.15 | 0.64 | -0.04 | -0.50 | 0.41 | 0.10 | -0.14 | -0.85 | -1.16 | -0.43 | -0.14 | 0.40 | 1806 |
| 1807 | -1.06 | 0.16 | 0.34 | -1.21 | 0.74 | 0.90 | 1.37 | 0.92 | 2.80 | 1.26 | 1.95 | -0.07 | 1807 |
| 1808 | -0.24 | -1.22 | -0.86 | -1.36 | -0.48 | -0.43 | 0.88 | 0.04 | 2.42 | -1.92 | -0.29 | -2.31 | 1808 |
| 1809 | 0.57 | -0.31 | 0.23 | $-0.50$ | -0.48 | 0.86 | 1.46 | -0.23 | -0.67 | -1.67 | -1.36 | -0.9s | 1809 |
| 1510 | 0.01 | $-0.27$ | 2.49 | 0.28 | 0.50 | -0.63 | -0.54 | -0.19 | -0.29 | -0.67 | 0.06 | -0.91 | 1810 |
| 1811 | -0.15 | 0.69 | -0.91 | 0.24 | 0.43 | 1.46 | 0.97 | 0.26 | 0.04 | 0.95 | 0.00 | -0.76 | 1811 |
| 1812 | -1.51 | 0.40 | 0.00 | $-0.39$ | -0.61 | 0.15 | -1.32 | -0.21 | -0.69 | -0.16 | 0.35 | -0.18 | 1812 |
| 1813 | -1.51 | -1.02 | -0.80 | -0.52 | 0.79 | 0.32 | -0.92 | -1.25 | -1.00 | 1.31 | 0.04 | -1.18 | 1813 |
| 1814 | 0.54 | -3.04 | -0.88 | 0.04 | -1.46 | -0.59 | -0.96 | -0.56 | -2.03 | -0.49 | -0.52 | -0.42 | 1814 |
| 1815 | -0.46 | 0.07 | 0.29 | 0.90 | 0.61 | -0.63 | -1.12 | -2.01 | -0.78 | 0.22 | 0.08 | -0.78 | 1815 |
| 1816 | -0.40 | -0.31 | $-0.71$ | $-0.54$ | 0.05 | -1.94 | -0.65 | -0.48 | -0.50 | -1.09 | -0.63 | -1.24 | 1816 |
| 1817 | -0.11 | -0.09 | -0.15 |  |  | 0.32 | -0.39 | 0.46 | -0.34 | 0.11 | -0.47 | -0.02 | 1817 |
| 1818 | -0.66 | 0.87 |  | 1.21 | 0.19 | -1.10 | -0.25 | -0.45 | 0.24 | -0.78 | 0.33 | 0.62 | 1818 |
| 1819 | -1.02 | 0.18 | 0.72 | 0.97 | -0.12 | $-0.21$ | -0.28 | -0.34 | -0.32 | 0.82 | 1.11 | 0.82 | 1819 |
| 1820 | 1.89 | -0.11 | -0.97 | 0.37 | 2.03 | 0.68 | 0.48 |  |  |  | -0.65 | 0.29 | 1820 |
| 1821 | 1.92 | -0.76 | 0.49 | 0.50 | 0.55 | -0.74 | -0.30 | -0.21 | 0.51 | -0.74 | -0.72 | 0.69 | 1821 |
| 1822 | -1.28 | -1.11 | $-0.53$ |  | 0.68 | 2.97 | 1.48 | 1.46 | 1.88 | 1.51 | 0.06 | 0.18 | 1822 |
| 1823 | 0.52 | 1.78 | -0.80 | 0.28 | 0.99 | 0.30 | -0.36 | 0.35 | -0.34 | $-0.76$ | -1.63 | -0.53 | 1823 |
| 1824 | -0.91 | 0.42 | -1.04 | -1.01 | 1.25 | -0.25 | -0.70 | 1.86 | 0.13 | 1.51 | 0.64 | 0.51 | 1824 |
| 1825 | -1.04 | -1.02 | $-0.17$ | 0.12 | 0.30 | $-0.45$ | -0.10 | 0.46 | 0.55 | $-1.00$ | -0.05 | 1.67 | 1825 |
| 1826 | -0.s8 | 0.56 | -0.29 | $-0.59$ | -1.08 | -0.74 | 0.39 | 0.52 | 1.35 | 0.46 | -0.87 | -0.24 | 1826 |
| 1827 | 0.07 | 0.83 | 0.82 | -0.51 | 0.18 | $-1.30$ | 0.80 | 1.33 | $-0.73$ | 0.50 | -1.76 | -0.04 | 1827 |
| 1828 | -0.16 | 0.20 | 0.23 | 0.29 | 1.99 | 1.28 | 2.48 | 1.10 | 0.74 | -0.34 | 0.06 | -0.37 | 1828 |
| 1829 | 0.79 | -1.90 | 1.12 | 2.49 | -0.09 | $-0.47$ | 0.16 | -0.12 | 0.41 | -0.38 | -0.35 | -0.16 | 1829 |
| Means. | 8.35 | 8.27 | 9.40 | 11.52 | 14.35 | 17.12 | 19.25 | 19.48 | 17.60 | 14.78 | 11.69 | 9.44 | Means |

The numbers without sign must be subtracted; those with the sign - must be added

North Italy. - Milan.
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | - | - | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ |  | - | - | $\bigcirc$ | $\bigcirc$ |  |
| 1763 | -1.32 | 1.58 | $-0.60$ | 0.27 | -2.28 | $-0.79$ | 0.68 | 1.11 | -1.11 | $-1.69$ | $-0.56$ | 1.02 | 1763 |
| 1761 | 1.68 | 1.98 | $-0.70$ | $-0.63$ | 1.32 | 0.91 | $-0.12$ | $-1.29$ | $-1.21$ | -1.19 | $-0.26$ | 1.52 | 1764 |
| 1765 | 3.83 | $-0.92$ | 0.60 | 0.47 | $-1.08$ | 0.11 | $-2.62$ | $-1.69$ | $-0.11$ | 0.11 | 0.24 | -0.98 | 1765 |
| 1766 | -3.42 | -1.52 | $-0.10$ | $0 . .57$ | 0.02 | 1.31 | $-1.32$ | $-0.19$ | -1.21 | $-0.49$ | 2.14 | $-0.68$ | 1766 |
| 1767 | $-4.22$ | 0.38 | 0.10 | $-0.93$ | $-1.08$ | $-1.19$ | 0.78 | $-0.69$ |  | - • |  | -0.88 | 1767 |
| 1768 | -0.82 | -1.22 | $-1.50$ | 0.37 | $-0.58$ | $-2.19$ | 0.68 | 0.51 | -• | - • | 0.64 | -0.78 | 1768 |
| 1769 | 1.85 | $-0.42$ | $-0.50$ | -1.63 | $-0.18$ | 1.01 | $-0.52$ | 1.51 |  | -2.19 | 1.24 | 0.62 | 1769 |
| 1770 | -0.52 | 0.98 | $-0.60$ | -0.33 | $-0.38$ | 0.81 | $-0.72$ | 0.01 | 1.99 | 0.51 | 1.04 | -0.68 | 1770 |
| 1771 | 1.78 | $-0.52$ | $-0.60$ | $-1.43$ | 1.02 | $-0.19$ | 0.68 | 1.51 | 0.49 | $-0.69$ | -1.06 | 2.32 | 1771 |
| 1772 | 1.58 | $2,4 *$ | 2.50 | 0.57 | $-0.58$ | 1.61 | 1.38 | 0.41 | 0.29 | 2.01 | 1.94 | 2.02 | 1772 |
| 1773 | 1.58 | -0.42 | $-0.80$ | $-0.03$ | $-0.18$ | - | -1.72 | $-1.29$ | 0.69 | 1.61 | 0.34 | 1.82 | 1773 |
| 1774 | 0.48 | 0.08 | 0.70 | 0.77 | $-0.28$ | 0.51 | $-0.12$ | 1.31 | -0.31 | $-1.09$ | -0.96 | $-2.68$ | 1774 |
| 1775 | 0.38 | 2.08 | 1.60 | 0.47 | $-0.58$ | 0.71 | 0.78 | $-0.09$ | $-0.31$ | -1.79 | -0.16 | $-0.88$ | 1775 |
| 1776 | $-0.32$ | $-0.02$ | 1.30 | 0.97 | -1.28 | 0.11 | 0.48 | 0.41 | $-0.71$ | 0.11 | -0.36 | -1.18 | 1776 |
| 1777 | $-1.52$ | $-1.42$ | 1.30 | $-0.23$ | -1.08 | $-0.79$ | $-1.22$ | 0.51 | 0.19 | 0.41 | 1.24 | $-1.98$ | 1777 |
| 1778 | 0.38 | 0.08 | $-1.90$ | 1.47 | 0.62 | $-0.29$ | 0.98 | 0.81 | $-0.81$ | $-0.09$ | 0.64 | 1.72 | 1778 |
| 1779 | -3.52 | 1.98 | 0.00 | 1.07 | 1.72 | -1.39 | 0.18 | $-0.19$ | 1.59 | 1.51 | $-0.16$ | 1.82 | 1779 |
| 1780 | $-0.62$ | -1.92 | 2.70 | $-0.43$ | 1.72 | 1.51 | 0.78 | 0.11 | $-0.51$ | 1.81 | -0.16 | $-1.05$ | 1780 |
| 1781 | -0.12 | 0.35 | 1.90 | 1.4 | 0.22 | 0.01 | 1.78 | 0.41 | 0.59 | -0.89 | 0.04 | 1.42 | 1781 |
| 1752 | 2.18 | -2. 12 | $-0.70$ | $-1.03$ | -1.08 | 1.21 | 2.08 | 0.91 | -0.31 | -1.79 | $-2.16$ | -0.58 | 1782 |
| 1783 | 0.98 | 1.15 | -0.60 | 0.97 | 0. | -0.99 | 1.08 | -0.29 | -0.31 | 1.51 | 0.24 | $-1.88$ | 1783 |
| 1784 | 0.18 | $-2.02$ | 0.50 | $-2.03$ | 2.62 | 2.11 | 1.38 | 0.61 | 1.49 | $-1.49$ | $-0.16$ | -1.18 | 1784 |
| 1785 | 0.58 | $-1.12$ | $-3.80$ | -1.23 | 0.72 | 1.21 | 0.68 | 0.61 | 2.69 | 0.41 | 0.74 | 2.02 | 1785 |
| 1756 | 0.18 | 0.68 | -0.90 | 0.87 | 0.72 | 0.81 | $-0.52$ | $-0.89$ | 1.09 | -1.89 | -0.3i | -0.45 | 1786 |
| 1787 | $-0.32$ | 0.08 | 0.90 | $-0.03$ | -1.98 | 1.71 | $-0.02$ | 1.61 | 0.09 | 0.81 | 0.84 | 1.72 | 1787 |
| 1788 | 2.78 | 1.08 | 2.30 | 1.37 | -0.18 | 1.51 | 2.78 | -0.39 | 0.99 | 0.21 | -0.86 | $-2.88$ | 1788 |
| 1759 | $-1.72$ | 0.93 | -1.70 | 1.37 | 2.22 | $-0.79$ | 0.28 | 0.11 | 0.29 | 0.31 | $-1.26$ | -2.35 | 1789 |
| 1790 | -0.12 | 1.48 | $-0.20$ | $-1.73$ | 1.62 | 0.71 | $-0.72$ | 1.21 | 0.19 | 2.21 | 1.21 | 0.02 | 1790 |
| 1791 | 2.48 | 1.08 | 1.20 | 1.57 | -0.18 | $-0.49$ | 0.58 | 1.51 | 009 | -0.29 | $-0.46$ | 1.92 | 1791 |
| 1792 | 0.98 | $-0.12$ | 1.30 | 1.87 | $-0.15$ | 0.21 | 0.08 | 0.11 | -0.11 | 0.71 | 0.54 | $-0.0 \mathrm{~s}$ | 1792 |
| 1793 | -1.22 | $-0.02$ | 0 | $-1.43$ | $-0.38$ | 0.01 | 1.78 | -0.29 | 2.49 | 1.31 | 1.44 | 2.22 | 1793 |
| 1791 | 2.28 | 3.08 | 2.00 | 2.37 | -0.08 | 0.81 | 1.78 | 0.21 | -1.11 | -0.49 | 1.84 | -0.38 | 1794 |
| 1795 | -3.72 | -3.12 | $-0.20$ | 1.37 | 1.52 | $-0.79$ | $-1.42$ | 0.91 | 0.49 | 1.71 | -0.16 | 1.52 | 1795 |
| 1796 | 2.48 | 1.18 | $-1.70$ | $-0.13$ | $-0.28$ | $-0.29$ | -0.12 | 0.71 | 1.39 | 0.41 | 1.24 | $-1.38$ | 1796 |
| 1797 | 0.75 | 0.18 | $-1.40$ | 0.67 | 1.22 | -1.59 | 1.18 | $2 . .71$ | 1.09 | $-0.59$ | 0.94 | 1.32 | 1797 |
| 1798 | 1.78 | 2.08 | 0.20 | 0.27 | 0.72 | $-0.09$ | 0.48 | 0.51 | 0.29 | -0.39 | -0.86 | -2.05 | 1798 |
| 1799 | $-3.23$ | 0.88 | 0.60 | $-1.23$ | -0.98 | -1.49 | $-0.62$ | 0.41 | 1.39 | 0.51 | -0.96 | $-1.18$ | 1799 |
| 1800 | 1.75 | 4.55 | -1.10 | 2.67 | 1.32 | -1.59 | 0.38 | $-0.09$ | 0.49 | 0.01 | 1.24 | -0.08 | 1800 |
| 1801 | 1.38 | 1.08 | 1.50 | 0.77 | 0.39 | $-0.39$ | $-0.62$ | $-0.79$ | 0.49 | 0.61 | 0.04 | 0.02 | 1801 |
| 1802 | 0.18 | 1.18 | 8 0.70 | 0.87 | -0.08 | 1.71 | 0.28 | 2.21 | 1.09 | 2.81 | 1.04 | 1.52 | 1802 |
| 1803 | 2.35 | -3.82 | 0.30 | 1.47 | -0.85 | 1.11 | 0.78 | 1.11 | -0.91 | $-0.49$ | 0.31 | 0.22 | 1803 |

The numbers without sign must be subtracted; those with the sign - must be added.
LXXXI.

## North Italy. - Milan (contimued).

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | ○ ${ }^{\circ}$ | ) 0 | $\bigcirc$ |  |
| 1804 | 3.98 | $-1.82$ | -0.60 | $-0.03$ | 1.32 | 2.11 |  | -0.39 | 0.49 | 0.71 | $-0.36$ | $-0.18$ | 1804 |
| 1ऽ05 | $-0.12$ | $-0.02$ | $-0.10$ | $-2.03$ | $-0.75$ | 0.21 | -0.42 | -0.29 | 0.79 | $-1.19$ | $-2.36$ | $-1.55$ | 1805 |
| 1806 | 0.18 | 1.68 | 0.10 | $-1.53$ | 0.32 | 1.01 | $-0.52$ | -1.19 | $-0.41$ | $-0.19$ | 1.34 | 1.92 | 1506 |
| 1807 | 0.58 | 0.28 | $-2.40$ | -1.33 | 1.32 | 0.21 | 1.18 | 1.71 | 0.19 | 1.71 | 1.34 | $-0.0 \mathrm{~s}$ | 1807 |
| 1808 | -1.02 | $-1.62$ | $-3.80$ | -1.23 | 1.62 | $-0.49$ | 1.98 | $-0.69$ |  | -2.39 | 0.24 | -2.08 | 1808 |
| 1509 | 0.48 | 1.98 | -1.40 | -2.63 | 1.02 | 0.51 | $-0.52$ | 0.21 | -0.51 | $-0.19$ | $-0.96$ | 0.22 | 1809 |
| 1810 | 0.08 | $-0.72$ | 1.90 | $-0.23$ | 0.22 | $-1.49$ | -2.12 | $-0.79$ | 0.59 | 1.11 | 0.34 | 1.83 | 1810 |
| 1811 | $-0.72$ | 1.48 | 1.70 | 1.47 | 1.82 | -0 29 | 1.18 | $-0.49$ | 0.39 | 2.21 | 2.24 | $-0.38$ | 1811 |
| 1812 | -3.32 | $-0.32$ | $-0.40$ | -1.73 | 0.92 | 1.01 | -0.82 | $-0.59$ | -1.41 | 0.11 | $-2.96$ | -2.38 | 1812 |
| 1813 | $-0.12$ | 1.08 | 0.50 | 1.07 | 1.52 | $-0.99$ | $-3.12$ | -1.09 | -1.11 | 0.21 | $-0.56$ | 1.32 | 1813 |
| 1514 | $-0.12$ | $-4.42$ | $-1.40$ | 0.77 | -1.98 | -1.09 | $-0.12$ | $-1.09$ | -1.91 | $-0.69$ | 1.04 | 1.82 | 1814 |
| 1815 | -2.02 | $-0.32$ | 1.90 | 0.77 | 1.22 | -0.49 | $-1.22$ | -1.39 | 0.29 | 0.81 | $-1.26$ | -1.75 | 1815 |
| 1816 | $-0.52$ | -2.92 | $-1.20$ | $-0.93$ | -0.58 | -1.49 | $-2.22$ | -3.69 | $-0.51$ | 0.41 | $-1.46$ | -1.88 | 1816 |
| 1817 | $-2.52$ | 2.08 | 0.30 | $-2.83$ | -1.28 | 0.21 | -3.52 | $-0.59$ | 0.89 | $-1.89$ | 0.44 | -0.18 | 1817 |
| 1818 | 0.48 | 3.34 | 0.70 | 0.37 | $-3.80$ | 0.26 | 0.53 | $-0.79$ | $-0.23$ | 0.48 | 1.13 | $-0.39$ | 1818 |
| 1819 | 0.00 | 0.73 | 1.48 | 1.35 | -0.02 | $-0.53$ | 0.32 | $-0.50$ | 0.48 | 0.46 | 0.98 | 0.30 | 1819 |
| 1820 | $-0.79$ | 0.58 | -0.56 | 1.60 | 1.03 | $-0.45$ | $-0.48$ | 1.76 | -0.09 | $-0.30$ | $-0.72$ | -0.03 | 1820 |
| 1521 | 0.80 | $-0.15$ | $-0.52$ | 0.59 | 0.10 | $-2.20$ | $-1.46$ | 0.43 | 1.01 | -0.29 | 0.78 | 0.35 | 1821 |
| 1822 | 1.81 | 1.28 | 2.10 | 0.99 | 1.05 | 3.31 | 0.53 | 0.26 | 0.78 | 0.66 | 1.38 | $-0.48$ | 1822 |
| 1823 | $-1.92$ | -0.25 | $-0.37$ | -0.5. | 0.93 | $-0.78$ | $-0.60$ | 0.53 | 1.18 | 0.11 | -1.37 | 0.01 | 1823 |
| 1824 | 1.01 | 1.49 | $-0.40$ | -0.85 | $-0.16$ | $-1.57$ | 1.33 | 0.90 | 0.71 | 0.23 | 1.25 | 2.07 | 1824 |
| 1525 | 1.39 | 0.62 | $-2.38$ | 1.21 | $-0.17$ | 0.32 | 0.05 | 0.53 | 0.86 | $-0.81$ | 0.82 | 3.92 | 1825 |
| 1826 | -2.18 | 0.44 | 0.76 | $-0.72$ | $-1.23$ | $-0.09$ | 0.18 | 1.55 | 0.71 | 1.48 | $-0.56$ | 1.16 | 1826 |
| 1827 | 0.36 | $-1.72$ | 1.12 | 0.73 | 0.46 | $-1.26$ | 1.20 | $-0.60$ | $-1.06$ | 1.37 | $-1.46$ | 0.25 | 1527 |
| 1828 | 1.38 | $-0.36$ | 1.49 | 0.64 | 0.45 | 1.27 | 1.38 | 0.19 | 0.47 | 0.38 | $-0.81$ | 0.60 | 1528 |
| 1829 | $-0.04$ | $-2.79$ | 0.05 | 0.05 | $-0.03$ | 0.23 | 0.22 | -1.15 | -0.89 | $-0.40$ | -1.68 | -1.90 | 1829 |
| 1830 | $-3.72$ | $-3.45$ | 1.66 | 2.66 | 0.66 | $-0.33$ | 1.71 | 1.02 | $-0.79$ | $-0.81$ | 0.99 | 0.60 | 1830 |
| 1831 | 0.38 | -0.51 | 0.73 | 0.19 | -1.12 | $-0.56$ | 0.12 | $-1.0 .5$ | $-1.08$ | 1.77 | 0.2.4 | 1.34 | 1831 |
| 1832 | 0.41 | 0.52 | $-0.21$ | -0.68 | $-2.07$ | -1.27 | 0.03 | 0.49 | -1.15 | $-0.47$ | $-0.41$ | $-1.71$ | 1832 |
| 1833 | $-0.17$ | 1.18 | $-0.59$ | -1.23 | 2.00 | 0.37 | -2.28 | -2.77 | $-3.20$ | -1.36 | 0.14 | 1.37 | 1833 |
| 1834 | 0.17 | -0.80 | $-0.19$ | $-1.97$ | 0.53 | $-0.31$ | -0.23 | -1.16 | 0.41 | -0.79 | -0.23 | -0.94 | 1834 |
| 1835 | 1.03 | 0.76 | $-0.44$ | -0.88 | $-1.01$ | $-1.47$ | -2.59 | -2.35 | -2.01 | $-2.24$ | -3.27 | -2.69 | 1835 |
| 1836 | -2..51 | -2.08 | $-0.05$ | -1.07 | $-3.41$ | $-0.49$ | $-0.97$ | -1.09 | $-2.48$ | -0.65 | $-2.16$ | $-0.02$ | 1836 |
| 1837 | $-0.83$ | -4.75 | $-3.12$ | -2.41 | -3.58 | 0.64 | $-1.29$ | 0.37 | $-2.40$ | -1.93 | -1.76 | $-0.36$ | 1837 |
| 1538 | -2.16 | $-2.39$ | $-0.72$ | -2.7 | -0.98 | $-0.75$ | $-0.78$ | -1.55 | -1.5s | -1.74 | 0.08 | $-0.80$ | 18:38 |
| Means. | 0.52 | 2.82 | 6.40 | 10.03 | 14.08 | 17.09 | 18.92 | 18.39 | 15.31 | 10.79 | 5.76 | 2.08 | Means. |

The numbers without sign must be subtracted; those with the sign - must be added.

Switzerland. - Geneva.
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | - |  |
| 1765 | $-1.86$ | $-0.01$ | $-2.35$ | $-0.11$ | -0.6 | -1.71 | -0.92 | $-1.25$ | $-1.42$ | 0.99 | 0.77 | 0.08 | 1768 |
| 1769 | 0.92 | 0.16 | $-1.05$ | 0.13 | $-0.71$ | $-1.57$ | -1.11 | $-1.43$ | -0.89 | $-3.00$ | 1.62 | 0.61 | 1769 |
| 1770 | -1.25 | -1.3 | -1.72 | $-2.40$ | $-1.20$ | -1.3 | -2.97 | $-1.24$ | 0.49 | $-0.81$ | 0.35 | 0.42 | 1770 |
| 1771 | 0.53 | $-0.67$ | 0.17 | -2.6s | 0.34 | -1.84 | 0.07 | $-1.45$ | $-0.57$ | -0.17 | -1.80 | 1.66 | 1771 |
| 1772 | 0.61 | 2.57 | 1.76 | $-0.41$ | $-2.23$ | 0.35 | $-0.72$ | $-0.47$ | 0.52 | 1.34 | 1.29 | 1.16 | 1772 |
| 1773 | 1 | -1.84 | $-1.18$ |  | -1.64 | -0.87 | $-2.03$ | $-1.70$ | $-0.12$ | $-0.35$ | $-0.12$ | 1.01 | 1773 |
| 1774 | 1.22 | 0.91 | 2.38 | 0.73 | $-0.94$ | $-0.47$ | -1.27 | 0.42 | $-1.0 \mathrm{~s}$ | $-1.45$ | $-1.18$ | $-2.03$ | 1774 |
| 1775 | 0.89 | 1.89 | 0.99 | $-1.60$ | $-1.90$ | 0.54 | -0.84 | $-0.82$ | $-0.02$ | -0.24 | 0.33 | -0.68 | 1775 |
| 1776 | -1.78 | 1.92 | 1.55 | 0.18 | $-1.96$ | 0.09 | 0.20 | 0.28 | $-1.50$ | 0.26 | -0.26 | $-0.09$ | 1776 |
| 1777 | -0.41 | $-0.76$ | 2.46 | $-1.23$ | -1.51 | $-0.38$ | $-1.12$ | 0.45 | $-0.41$ | 1.27 | 0.21 | $-1.72$ | 1777 |
| 1778 | 0.03 | $-0.93$ | 0.86 | 0.78 | $-0.09$ | $-0.76$ | 1.59 | 0.6 S | $-1.85$ | 0.32 | 0.76 | 1.85 | 1778 |
| 1779 | $-3.43$ | -0.28 | $-0.14$ | 1.70 | 0.97 | $-1.22$ | -0.61 | $-0.45$ | 0.48 | 1.77 | 0.57 | 2.70 | 1779 |
| 1780 | -1 | $-1.63$ | 2.35 | $-0.86$ | 09 | 1.1 | 0.95 | 1.16 | 0.14 | 0.51 | -1.02 | $-1.25$ | 1780 |
| 1781 | 0.9 | 1.09 | 0.37 | 2.15 | 1.7 | 0. | $-1.17$ | 0.30 | 0.76 | $-0.47$ | 1.69 | 2.97 | 1781 |
| 1782 | 2.22 | $-3.74$ | $-0.53$ | -0.9.5 | $-1.76$ | 0.15 | $-1.10$ | $-0.72$ | -0.97 | $-1.06$ | -1.83 | $-2.04$ | 1782 |
| 1783 | 2.01 | 1.68 | $-0.27$ | $-0.71$ | -0 | -1 | 1.75 | $-0.94$ | 0.17 | 0.93 | 0.81 | 1.03 | 1783 |
| 1784 | -1.06 | $-2.0$ | $-0.13$ | $-2.51$ | 1.73 | 1.69 | 0.84 | $-1.62$ | 1.40 | -1.67 | $-0.76$ | $-3.35$ | 1784 |
| 1785 | 0.58 | -3.26 | $-6.75$ | $-5.48$ | $-0.19$ | 0.30 | $-0.33$ | $-1.75$ | 0.94 | $-0.40$ | 0.11 | 0.42 | 1785 |
| 1786 | 0.41 | 0.08 | $-1.62$ | 0.69 | $-0.25$ | 1.92 | $-0.99$ | $-1.22$ | $-0.59$ | -1.71 | -0.69 | 0.19 | 1786 |
| 1787 | $-1.99$ | $-1.15$ | 1.76 | $-0.30$ | $-1.98$ | 0.79 | $-0.70$ | 0.21 | $-0.27$ | 0.41 | 0.72 | 2.83 | 1787 |
| 1788 | 1.01 | 2.06 | 2.19 | 1.04 | 113 | 1.04 | 1.61 | $-0.45$ | 0.71 | -0.83 | $-2.15$ | $-4.48$ | 788 |
| 1789 | -1.17 | 1.12 | $-1.97$ | 1.19 | 1.71 | -1.25 | -0.80 | -0.19 | $-0.57$ | -0.59 | -1.59 | $-0.17$ | 1789 |
| 1790 | 0.3 | 0.75 | 0.99 | $-0.73$ | 1.52 | 0.94 | $-1.10$ | 0.63 | $-0.84$ | 1.95 | 1.13 | 0.78 | 1790 |
| 1791 | 2.40 | 0. | $-0.02$ | 2.86 | 0. | 1.04 | 0.98 | 2.30 | 0.98 | 0.72 | $-1.37$ | 1.30 | 1791 |
| 1792 | 1.22 | -0.2 | 2.11 | 1.81 | $-0.12$ | 1.14 | 1.03 | 0.83 | $-0.09$ | 1.37 | 0.86 | 0.45 | 1792 |
| 1793 | $-0.52$ | 1.05 | 1.77 | 0.0 S | $-0.0$ | 0.2 | 3.12 | 2.49 | $-0.12$ | 1.24 | 0.61 | 1.19 | 1793 |
| 1794 | 0.1 | 2.2 | 1.9 | 3.26 | 0.7 | 1.10 | 2.11 | 0.39 | $-0.74$ | -0.28 | 0. | -1.75 | 1794 |
| 1795 | -4.85 | 0.3 | 0.26 | 1.76 | 1.32 | 1 | $-0.73$ | 1.34 | 1.51 | 1.92 | $-0.96$ | 1.11 | 1795 |
| 1796 | 1.25 | 0.72 | $-2.15$ | $-0.06$ | 0.60 | 0.60 | 0.37 | 0.80 | 1.61 | 0.41 | $-0.1$ | $-1.92$ | 1796 |
| 1797 | 0.11 | $-1.41$ | -1.05 | 1.49 | 2.14 | -1.2s | 2.21 | 1.28 | 0.71 | $-0.0 \mathrm{~s}$ | 0.71 | 1.61 | 1797 |
| 1798 | 0.53 | $-1.17$ | $-1.02$ | 0.83 | 1.00 | 1.29 | 0.45 | 0.81 | 0.18 | $-0.29$ | 0.44 | -0.96 | 1795 |
| 1799 | -1.57 | 1.71 | $-0.16$ | -1. | -1. | $-1.16$ | $-0.13$ | 0.67 | 0.21 | -0 | -0.7 4 | $-2.59$ | 1799 |
| 1800 | 1.64 | 0.06 | $-1.66$ | 2.43 | 2.40 | -0.8:3 | 1.48 | 0.82 | 0.96 | $-1.5 .5$ | 0.63 | -0.27 | 1800 |
| Means. | $-0.43$ | 0.75 | 3.08 | 7.19 | 11.21 | 14.03 | 15.44 | 14.85 | 11.49 | 7.32 | 3.34 | 0.57 | Means. |
| 1796 | 2.27 | 0.07 | $-2.14$ | $-0.25$ | -0.91 | -0.64 | -1.10 | 0.16 | 0.70 | $0.0 \mathrm{~S}^{1}$ | -0.68 | -1.70 | 1796 |
| 1797 | 0.45 | -0.8. | $-0.66$ | 0.97 | 0.67 | $-2.03$ | 1.27 | 0.71 | $-0.18$ | $-0.26$ | 0.47 | 1.58 | 1797 |
| 1798 | 0.68 | $-0.25$ | $-0.40$ | 0.96 | $-0.23$ | 0.32 | $-0.64$ | $-0.14$ | 0.12 | $-0.02$ | -0.76 | -1.36 | 1798 |
| 1799 | --1.44 | 1.93 | $-0.26$ | $-1.60$ | $-1.50$ | $-0.49$ | $-0.46$ | 0.33 | 0.19 | -0.26 | -1.24 | $-3.30$ | 1799 |
| 1800 | 2.06 | 0.03 | $-1.53$ | 2.85 | 1.66 | -0.97 | 1.62 | 0.70 | 0.41 | $-1.16$ | 0.67 | -0.32 | 1800 |
| 1801 | 1.81 | 0.13 | 1.43 | 0.74 | 0.43 | $-0.26$ | 0.42 | 0.15 | 0.90 | 0.84 | 0.67 | 0.95 | 1801 |
| 1802 | -3.98 | $-0.35$ | 0.94 | 1.18 | 0.53 | 1.66 | $-0.12$ | 2.68 | 1.72 | 2.51 | 0.63 | 0.58 | 1802 |
| 1803 | -0.26 | $-2.58$ | 0.24 | 2.05 | $-1.42$ | 0.89 | 2.20 | 2.25 | $-0.79$ | $-0.57$ | 1.0 | 1.58 | 1803 |
| 1804 | 4.58 | -1.55 | -0.19 | 0.30 | 1.50 | 2.02 | 0.04 | 0.47 | 0.59 | 0.22 | 1.36 | -0.59 | 1801 |

Switzerland. - Geneva (continued).
For Keducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ |  |  |  |  |  | $\bigcirc$ | 0.73 | 0.18 |  | 2, 19 | $\begin{gathered} \circ \\ -1.64 \end{gathered}$ | 1805 |
| 1805 | -0.41 | -0. | -0 | -1.35 | -1.22 | -0.49 |  |  | 0.15 |  |  |  | 1806 |
| 1806 | 3.23 | 1.83 | 0.12 | -1.80 | 1.33 | 1.66 | 0.08 | -0.39 | 0.11 | 1.10 | 1.34 | 2.42 | 1806 |
| 1807 | $-1.10$ | 0.24 | -2.65 | -1.47 | 1.42 | 0.43 | 2.66 | 3.03 | -0.5s | 1.42 | 0.39 | $-2.48$ | 1807 |
| 1808 | -0.49 | -3.14 | -2.58 | -1.87 | 1.14 | -1.33 | 0.70 | 0.59 | -0.14 | -2.40 | -0.28 | -2.99 | 1808 |
| 1809 | 2.23 | 1.95 | 0.19 | -3.68 | -0.06 | 0.12 | -0.43 | -0.32 | - 1.00 | -1.05 | -1.76 | 0.70 | 1809 |
| 1810 | -3.14 | -3.34 | 3.08 | -0.28 | 0.29 | -0.45 | -1.01 | -0.70 | 1.37 | 1.26 | 1.05 | 1.19 | 1810 |
| 1811 | -2 | 98 | 1.46 | 1.34 | 1.23 | 1.52 | 1.53 | -0.11 | 0.70 | 2.21 | 0.71 | -0.8.5 | 1811 |
| 1812 | -3.92 | 10 | -0 | -1.54 | 0.27 | 0.02 | -0.37 | -0.69 | -0.43 | 0.13 | -1.80 | -2.74 | 1812 |
| 1813 | -1.74 | 1.51 | -0.69 | 0.53 | 0.54 | -0.84 | -2.10 | -1.02 | -1.14 | 0.78 | -0.49 | 0.32 | 1813 |
| 1814 | -1.32 | $-3.92$ | -1.44 | 0.96 | -1.74 | -0.26 | 0.37 | -0.66 | -1.74 | -0.87 | 0.95 | 2.34 | 1814 |
| 1815 | -2.24 | 1.43 | 2.17 | 1.06 | 0.82 | 0.08 | 0.20 | -0.59 | 0.54 | 1.43 | -1.57 | -0.39 | 1815 |
| 1816 | -0.13 | -1.33 | 2.5 | -0.48 | -0.54 | -1.41 | -2.40 | -2.14 | -0.47 | 0.59 | -1.05 | -0.02 | 1816 |
| 1817 | 2.50 | 2.35 | 0.29 | -2.11 | -1.34 | 1.35 | -0.25 | -0.71 | 2.16 | -1.58 | 0.85 | -0.45 | 1817 |
| 1818 | 0.54 | 0.69 | 0.13 | -0.08 | -1.26 | 0.66 | 1.41 | -0.41 | -0.89 | $-0.29$ | 1.60 | -0.26 | 1818 |
| 1819 | 1.86 | 0.98 | 0.82 | 00 | -0.21 | -0.19 | 0.07 | -0.34 | 0.42 | 0.07 | -0.40 | 0.95 | 1819 |
| 1820 | 10 | . 54 | -1.24 | 2.07 | 0.39 | -0.59 | -0.65 | . 84 | -1.93 | -0.31 | -2.16 | 0.02 | 1820 |
| 1821 |  | -1.31 | 0.94 | . 71 | -1.19 | -1.54 | $-1.17$ | 0.62 | 0.26 | 0.27 | 2.34 | 3.36 | 1821 |
| 1822 | 0.20 | 27 | 3.06 | 0.47 | 1.32 | 3.85 | 0.27 | -0.85 | -0.07 | 0.69 | 1.60 | $-2.32$ | 1822 |
| 1823 | -1 |  | -0.29 | -0.42 | 0.17 | -1.62 | -1.54 | -1.04 | -0.42 | -2.10 | -1.97 | 1.04 | 1823 |
| 1824 | -0 | -0.30 | -1.84 | $-2.05$ | -1.50 | -2.0.) | 0.17 | -1.49 | -1.23 | -1.58 | 0.03 | 1.30 | 1824 |
| 1825 | -0.07 | -0.55 | -1.09 | 1.69 | $-0.63$ | 0.26 | -0.40 | -0.11 | 0.88 | 0.30 | 0.54 | 2.76 | 1825 |
| Means. | $-0.42$ | 1.87 | 4.70 | 8.79 | 13.45 | 15.81 | 17.67 | 17.66 | 14.70 | 9.73 | 5.23 | 1.27 | Means. |
| 1826 | -3.23 | 1.12 | 47 | 0.34 | -1.04 | $-0.06$ | 0.90 | 2.57 | 1.22 | 0.95 | -1.19 | 0.03 | 1826 |
| 1827 | 1.49 | -2.15 | 02 | 1.29 | 0.90 | -0.07 | 1.95 | 0.66 | 0.24 | 0.99 | -2.02 | 2.56 | 1827 |
| 1828 | 2.82 | 1.06 | 0.70 | 0.81 | 1.22 | 0.89 | 0.59 | -0.80 | 0.86 | 0.96 | 0.62 | 0.91 | 1828 |
| 1829 | -0.8 | -0.6.3 | 0.10 | 0.25 | $-0.06$ | $-0.83$ | 0.15 | -0.59 | $-0.71$ | -1.52 | -1.28 | -3.87 | 1829 |
| 1830 | -4 | -1.74 | 1.20 | 2.70 | 0.57 | -0.49 | 0.53 | -0.01 | -0.94 | -0.86 | 0.46 | -0.90 | 1830 |
| 1831 | -1.10 | 0.46 | 67 | 1.54 | 0.53 | -0.11 | -0.02 | -0.02 | -0.29 | 2.16 | 0.58 | 0.90 | 1831 |
| 1832 | 0 | 0.36 | -0.25 | 0.45 | -0.40 | -0.83 | 0.81 | 2.29 | $-0.39$ | 0.07 | -0.02 | 0.62 | 1832 |
| 1833 | -0.06 |  | -0 | -0 | 2.67 | 3 | -1.29 | -1.17 | -0.17 | 0.59 | 0.39 | 3.28 | 1833 |
| 1834 | 5.06 |  | 0 | -0.70 | 2.28 | 1.53 | 1.94 | 1.07 | 2.74 | 0.68 | 0.71 | -1.18 | 1834 |
| 1835 | 1.15 | 40 | $-0.44$ | $-0.06$ | 0.56 | 0.15 | 1.69 | 0.40 | 22 | -1.34 | -2.27 | $-2.66$ | 1835 |
| 1836 |  | -0.04 | 82 | -0.95 | -2.14 | 0.17 | 0.57 | 0.28 | -0.62 | 0.14 | -0.02 | 0.50 | 1836 |
| 1837 | 0.37 | 52 | -2.94 | -1 | -2.18 | 1.21 | -0.58 | 1.41 | -1.16 | -0.39 | -1.06 | -0.46 | 1837 |
| 1838 | -3.64 | -0.91 | 0.25 | -1.75 | -0.11 | -0.71 | $-0.56$ | -1.23 | -0.58 | -0.61 | 1.18 | $-0.57$ | 1838 |
| 1839 | 0.55 | -0.07 | -0.42 | $-1.55$ | -0.97 | 1.14 | 0.24 | -1.73 | -0.58 | 1.11 | 1. | 2.81 | 1839 |
| 1840 | 2.60 | 02 | -3.22 | 71 | -0.10 | -0.37 | -2.32 | -0.01 | $-0.56$ | 6-1.74 | 1.43 | -3.14 | 1840 |
| 1841 | 0.45 | -0.25 | - 0.77 | -0.69 | 2 | 2-1.71 | -1.98 | -1.37 | 0.09 | 0.90 | 0.2 | 0.89 | 1841 |
| 1842 | -5.18 | -2.84 | 10.56 | -0.58 | 0.02 | 21.00 | -0.19 | 0.78 | -1.08 | -2.18 | -1.03 | -0.71 | 1842 |
| 1843 | 1.50 | ) 2.22 | -0.34 | 0.27 | -1.60 | -2.56 | -2.35 | -0.73 | 0.60 | -0.2 | 0.25 | -0.83 | 1843 |
| 1844 |  |  |  |  |  |  |  |  |  |  |  |  | 1844 |
| 1845 | 1.70 | -3.33 | -1.77 | 70.49 | -1.98 | 80.47 | 0.06 | -1,53 | 1.10 | 0.40 | 1.54 | 1.74 | 1845 |
| Means | -0.72 | 20.98 | \% 4.16 | ( 7.03 | 10.77 | 713.61 | 14.96 | 14.59 | 11.84 | 47.98 | 3.98 | 1.30 | Means |

The numbers without sign must be subtracted; those with the sign - aust be added

South Germany. - Vienna.
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | - | - | - | $\bigcirc$ | $\bigcirc$ | c | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| 1775 | $-1.43$ | 1.86 | 1.21 | -2.35 | $-2.77$ | 1.32 | -0.4I | 1.29 | 0.84 | 0.26 | 0.29 | -1.09 | 1775 |
| 1776 | $-4.30$ | 0.57 | 0.70 | -1.11 | $-2.30$ | $-0.42$ | $-0.24$ | 0.25 | $-1.42$ | $-1.53$ | $-1.32$ | $-2.19$ | 1776 |
| 1777 | -1.79 | $-1.24$ | 0.32 | $-2.93$ | -0.22 | $-0.10$ | -1.17 | 0.57 | -1.38 | $-0.53$ | 0.35 | $-1.00$ | 1777 |
| 1778 | 1.92 | -1.04 | 0.18 | 1.89 | 0.04 | $-0.43$ | 1.18 | 0.95 | -0.89 | $-0.54$ | 0.87 | 3.61 | 1778 |
| 1779 | -1.75 | 3.15 | 2.27 | 3.05 | 1.24 | -1.32 | $-1.35$ | -0.07 | 0.65 | 1.00 | 0.43 | 3.01 | 1779 |
| 1780 | -1.68 | 3.04 | 2.73 | -1.38 | -0.18 | -0.92 | $-0.70$ | $-0.48$ | -1.08 | 0.51 | 0.19 | $-1.99$ | 1780 |
| 1781 | -0.87 | 0.05 | 0.77 | 0.86 | 0.25 | 1.44 | $-0.06$ | 2.31 | I. 40 | -0.4. | 1.84 | 0.34 | 1781 |
| 1782 | 2.72 | $-2.63$ | 0.60 | $-0.06$ | 0.54 | 1.82 | 2.74 | 0.85 | 0.86 | $-0.76$ | $-1.50$ | 0.62 | 1782 |
| 1783 | 3.59 | 4.12 | -0.08 | 0.65 | 1.51 | 1.94 | 1.66 | 1.81 | 2.12 | 1.59 | 0.58 | $-2.56$ | 1783 |
| 1784 | -3.51 | $-1.87$ | $-0.42$ | -1.36 | 1.69 | 0.86 | 0.47 | 0.49 | 1.93 | $-2.56$ | 0.70 | 0.03 | 1784 |
| 1785 | $-0.73$ | $-0.93$ | $-5.63$ | $-3.04$ | $-0.67$ | $-1.47$ | $-0.83$ | -0.86 | 2.11 | -0.55 | 0.41 | 0.17 | 1785 |
| 1786 | 0.52 | 0.16 | $-0.04$ | 1.84 | $-1.12$ | 0.2 .5 | $-1.54$ | -1.85 | $-0.92$ | -2.11 | $-2.12$ | 0.60 | 1786 |
| 1757 | -0.39 | 1.47 | 0.65 | -1.46 | $-2.11$ | 1.11 | $-0.40$ | 0.35 | $-0.78$ | 1.10 | 0.93 | 2.52 | 1787 |
| 1785 | 2.22 | 0.17 | 0.81 | 0.05 | $-0.36$ | 1.18 | 2.28 | $-1.72$ | 1.00 | $-0.29$ | $-1.39$ | $-6.79$ | 1788 |
| 1789 | $-0.49$ | 2.00 | $-2.43$ | 1.19 | 2.15 | $-0.49$ | 0.40 | $-0.60$ | 0.37 | 0.77 | 0.73 | 0.21 | 1789 |
| 1790 | 0.86 | 2.87 | 0.31 | $-1.11$ | 1.20 | 1.56 | $-1.10$ | 0.31 | $-0.93$ | $-0.76$ | $-0.43$ | 2.09 | 1790 |
| 1791 | 4.29 | 1.01 | 1.63 | 1.33 | -0.44 | $-0.33$ | $-0.37$ | 0.67 | -0.84 | $-0.40$ | $-0.46$ | 0.89 | 1791 |
| 1792 | 0.56 | $-1.24$ | 0.47 | 0.35 | -0.96 | 0.62 | 0.38 | 0.26 | -0.93 | $-1.11$ | -0.24 | 0.56 | 1792 |
| 1793 | -1.55 | 1.27 | $-1.00$ | $-2.40$ | -1.23 | -1.05 | 1.81 | 1.86 | $-0.07$ | 1.13 | 0.64 | 1.99 | 1793 |
| 1794 | 2.24 | 2.99 | 1.9.) | 3.74 | 1.35 | 1.55 | 2.92 | $-0.75$ | -1.38 | $-0.19$ | 0.33 | -0.95 | 1794 |
| 1795 | $-4.94$ | $-1.29$ | 0.23 | 1.81 | -0.0.7 | 1.44 | $-1.95$ | 0.31 | $-0.17$ | 2.75 | $-1.00$ | 2.28 | 1795 |
| 1796 | 5.23 | 1.32 | $-2.73$ | $-1.52$ | 0.48 | $-0.04$ | 0.14 | 0.58 | 1.96 | 0.84 | $-0.14$ | $-1.48$ | 1796 |
| 1797 | 1.58 | 1.02 | $-0.71$ | 2.10 | 294 | 0.65 | 1.95 | 2.17 | 2.01 | 1.23 | 0.54 | 1.11 | 1797 |
| 1798 | 1.96 | 2.83 | 1.40 | 0.65 | 0.26 | 0.84 | 0.14 | 1.29 | 1.62 | $-0.17$ | $-0.68$ | $-3.68$ | 1798 |
| 1799 | $-5.34$ | -2.08 | $-0.83$ | $-0.13$ | $-0.45$ | -1.16 | $-0.58$ | 1.00 | $-0.50$ | 0.4.) | 0.58 | $-2.94$ | 1799 |
| 1800 | 0.74 | $-0.19$ | -3.31 | 5.57 | 1.90 | $-1.45$ | -0.44 | 1.49 | 0.27 | $-0.40$ | 1.57 | 0.10 | 1800 |
| 1801 | 1.85 | -0.21 | 2.47 | 0.80 | 1.83 | -0. | -1.18 | $-1.32$ | 1.37 | 1.94 | 1.71 | 0.99 | 1801 |
| 1802 | $-0.43$ | $-1.34$ | 0.89 | 0.73 | -1.14 | 1.33 | 1.02 | 1.6 .5 | 0.35 | 2.10 | 1.94 | 1.40 | 1802 |
| 1803 | $-2.68$ | -3.46 | $-0.50$ | 2.49 | -1.59 | -0.75 | 0.23 | 0.08 | $-2.12$ | $-0.45$ | 1.24 | 0.27 | 1503 |
| 1804 | 3.12 | $-0.59$ | -2.44 | 0.05 | 0.29 | $-0.10$ | 0.25 | -0.5] | 0.80 | 0.48 | $-2.47$ | $-2.40$ | 180.1 |
| 1805 | $-0.48$ | $-1.18$ | -1.28 | $-2.16$ | -1.85 | -0.79 | $-1.26$ | $-1.61$ | $-0.04$ | $-2.89$ | $-2.19$ | 0.24 | 1805 |
| 1806 | 4.04 | 2.12 | 1.07 | $-2.07$ | 1.84 | -0.02 | $-0.16$ | $-0.62$ | 0.56 | -0.80 | 1.60 | 3.45 | 1806 |
| 1807 | 1.08 | 1.96 | -1.54 | $-1.18$ | 1.23 | -0.34 | 1.25 | 4.74 | 0.17 | $1 .: 37$ | 1.96 | 0.46 | 1807 |
| 1808 | I.20 | $-0.51$ | $-4.99$ | $-1.20$ | 1.42 | 0.15 | 1.30 | 1.80 | 1.13 | $-0.97$ | -0.32 | $-3.65$ | 1808 |
| 1509 | -0.08 | 1.54 | $-1.13$ | $-2.51$ | 0.89 | 0.27 | 0.23 | 0.79 | 0.11 | $-1.31$ | -0.75 | 1.67 | 1809 |
| 1810 | $-0.71$ | $-0.03$ | 2.03 | $-0.74$ | 0.50 | $-1.6 .5$ | 0.52 | 0.15 | 2.26 | -0.1s | -0.09 | 2.01 | 1810 |
| 1811 | -3.58 | -0.91 | 2.03 | 0.75 | 3.12 | 4.62 | 2.56 | 0.99 | 0.42 | 3.63 | 1.20 | 0.19 | 1811 |
| 1812 | -2.13 | 0.53 | 0.67 | $-2.67$ | 0.65 | 0.35 | -0.87 | $-0.52$ | $-1.32$ | 2.04 | -0.3t | $-3.96$ | 1812 |
| 1813 | -1.84 | 3.07 | $-0.76$ | I. 56 | 0.36 | -1.82 | $-1.34$ | -I. 80 | $-1.34$ | $-0.37$ | -0.24 | 0.65 | 1813 |
| 1814 | -0.34 | 4-4.37 | -0.55 | 1.54 | $-2.19$ | $-1.76$ | 0.66 | -0.21 | $-2.45$ | -0.73 | 0.32 | 2.19 | 1814 |
| 1815 | -1.03 | 2.39 | 2.06 | 0.10 | 0.52 | 0.28 | -1.51 | $-1.29$ | -1.20 | 0.06 | $-1.07$ | $-2.37$ | 1815 |
| 1816 | 1.8 | -0.80 | $-0.19$ | 0.09 | $-0.95$ | -0.73 | -1.58 | $-1.39$ | $-0.9 .5$ | -0.73 | $-0.39$ | $-1.45$ | 1816 |
| 1817 | 3.24 | 3.75 | 0.51 | $-4.08$ | 0.53 | 2.18 | -0.03 | -0.25 | 0.56 | -2.29 | 1.0 ) | 0.16 | 1817 |
| 1818 | 2.77 | 0.78 | 1.84 | 2.01 | $-0.11$ | 0.55 | 0.13 | -0.71 | 0.41 | 0.84 | 0.60 | $-1.31$ | 1818 |
| 1819 | 1.22 | 2.04 | 1.94 | 1.17 | $-0.75$ | 51.01 | 0.66 | -0.35 | 0.71 | -0.12 | 0.51 | -1.21 | 1819 |

South Germany. - Vienna (continued).
F،r Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | - | - |  | 0 | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | , | - |  |
| 1820 | $-2.47$ | 0.36 | $-0.86$ | 1.78 | 1.97 | -1.18 | $-0.96$ | 2.36 | -0.71 | 0.16 | $-0.36$ | $-1.49$ | 1820 |
| 1821 | 2.22 | $-1.56$ | $-0.72$ | 1.57 | -0.81 | -3.08 | -1.83 | $-0.76$ | 0.51 | $-0.12$ | 1.93 | 2.90 | 1821 |
| 1522 | 2.85 | 1.63 | 3.44 | 1.05 | 1.21 | 1.50 | 1.16 | -0.27 | 0.06 | 2.12 | 0.44 | -0.27 | 1822 |
| 1523 | $-4.55$ | 0.68 | 0.80 | $-0.29$ | 0.42 | $-0.68$ | $-1.35$ | 0.15 | 0.36 | 1.13 | 0.29 | 1.35 | 1523 |
| 1324 | 1.77 | 2.31 | 0.09 | $-0.72$ | $-0.74$ | -0.60 | $-0.22$ | $-0.53$ | 1.36 | 0.60 | 1.56 | 4.00 | 1824 |
| 1825 | 3.15 | 0.50 | -1.59 | 1.02 | $-0.14$ | -0.31 | $-0.72$ | $-0.17$ | $-0.62$ | -1.71 | 1.74 | 3.11 | 1825 |
| 1826 | -3.65 | -2.12 | 0.91 | $-0.12$ | $-2.42$ | -0.38 | 1.34 | 2.06 | 0.69 | 0.89 | $-0.32$ | 1.78 | 1826 |
| 1827 | 0.69 | $-2.92$ | 1.61 | 1.65 | 1.33 | 1.19 | 1.67 | $-1.06$ | $-0.57$ | 0.82 | $-3.48$ | 0.83 | 1827 |
| 1828 | 0.19 | $-2.22$ | 0.88 | 1.30 | $-0.16$ | 0.21 | 0.63 | -1.49 | $-0.70$ | -0.82 | 0.48 | 1.57 | 1828 |
| 1829 | $-1.66$ | -3.79 | $-1.87$ | $-0.23$ | -2.26 | -2 | -0.32 | $-2.62$ | $-0.31$ | $-2.12$ | -3.62 | $-6.11$ | 1529 |
| 1830 | -5.31 | $-3.23$ | $-0.44$ | 0.94 | $-0.39$ | 0.33 | 0.02 | $-0.04$ | -1.81 | -1.68 | 0.76 | 1.13 | 1830 |
| 1831 | $-1.42$ | 0.26 | 0.43 | 2.23 | $-0.90$ | -1.86 | 0.33 | $-1.01$ | $-1.96$ | 2.02 | $-0.16$ | $-0.04$ | 1831 |
| 1832 | 0.55 | 0.61 | 0.04 | $-0.16$ | $-1.90$ | $-1.46$ | $-1.29$ | 0.32 | $-0.86$ | 0.04 | -1.57 | -1.86 | 1832 |
| 1833 | $-3.35$ | 2.33 | 0.24 | $-1.40$ | 2.57 | 1.20 | $-2.26$ | $-2.80$ | -1.22 | $-0.55$ | 0.23 | 4.03 | 1833 |
| 1834 | 4.67 | 0.32 | -0.29 | $-1.17$ | 2.24 | . 1.65 | 2.61 | 1.26 | 2.85 | -0.08 | $-0.89$ | 1.2.) | 1834 |
| 1835 | 1.71 | 1.46 |  | $-1.10$ | 0.27 | $-0.07$ | 0.92 | 0.19 | 0.09 | -0.76 | -3.77 | -1.39 | 1835 |
| 1836 | -0.08 | 0.29 | 3.84 | 0.00 | $-2.95$ | 0.30 | $-0.18$ | $-0.78$ | $-0.89$ | 0.91 | $-1.00$ | 2.44 | 1536 |
| 1837 | 0.20 | $-2.39$ | $-1.96$ | -1.18 | $-2.57$ | -1.38 | -2.96 | 0.84 | $-2.22$ | $-0.82$ | $-0.74$ | $-0.95$ | 1837 |
| 1838 | -5.10 | $-4.14$ | $-0.50$ | $-2.44$ | $-0.76$ | -0.74 | -1.39 | $-2.29$ | $-0.03$ | $-1.75$ | $-0.65$ | -0.54 | 1838 |
| 1839 | 1.12 | 0.73 | $-2.31$ | -3.85 | -2.04 | 1.06 | 0.36 | -2.23 | 0.23 | 1.05 | 1.55 | 0.70 | 1839 |
| 1840 | 1.03 | $-0.85$ | $-3.76$ | $-0.55$ | $-1.59$ | $-1.0 .5$ | $-1.56$ | $-1.94$ | $-0.11$ | -2.03 | 2.09 | $-7.72$ | 1840 |
| 1841 | 0.33 | $-3.24$ | 0.65 | 0.93 | 2.19 | -1.02 | 0.5.5 | $-1.10$ | 0.24 | 2.04 | 0.28 | 2.27 | 1841 |
| Means. | $-1.22$ | 0.63 | 3.85 | 8.66 | 13.31 | 15.72 | 17.14 | 16.77 | 13.25 | 8.51 | 3.67 | 0.39 | Means. |

LXXXIV. South Germany. - Ratisbon.


The numbers without sign must be subtracted ; those with the sign - must be added
LXXXIV.

South Germany. - Ratisbon (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derivod from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ${ }^{\circ}$ |  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | c | - | $\bigcirc$ |  |
| 1792 | $-0.57$ | $-0.21$ | 1.41 | 1.17 | $-1.12$ | 0.87 | 0.66 | 0.88 | -1.01 | 0.0 .5 | 0.17 | 0.89 | 1792 |
| 1793 | $-1.17$ | 1.26 | 0.53 | $-1.81$ | -1.23 | $-0.76$ | 1.56 | 1.09 | $-0.47$ | 1.87 | 0.95 | 1.26 | 1793 |
| 1794 | 2.30 | 3.01 | 3.0 .5 | 3.04 | 1. 19 | 1.69 | 2.5. | -0.80 | $-1.00$ | 1.24 | 0.67 | $-0.78$ | 1794 |
| 1795 | -5.0.5 | -0.89 | $-0.10$ | 1.96 | $-0.82$ | 1.39 | $-2.22$ | 0.29 | 1.08 | 3.11 | -0.98 | 2.26 | 1795 |
| 1796 | 4.26 | . 59 | -1.6\% | -0.77 | $-0.85$ | 0.05 | 0.47 | 0.93 | 2.24 | 0.28 | -0.38 | $-2.04$ | 1796 |
| 1797 | 1.46 | 1.52 | $-0.17$ | 2.09 | 2.60 | $-0.72$ | 2.14 | 1.73 | 0.75 | 0.06 | 1.00 | 1.59 | 1797 |
| 1798 | 1.85 | 1.94 | 0.18 | 1.02 | 0.66 | 1.65 | 0.50 | 1.26 | 1.08 | $-0.73$ | -0.68 | -2.69 | 1798 |
| 1799 | -5.61 | 0.14 | $-0.29$ | $-1.87$ | -1.37 | -0.53 | -0.91 | $-2.86$ | -0.60 | -0.23 | -0.35 | -3.81 | 1799 |
| 1800 | 15 | 0.63 | $-2.63$ | 4.66 | 1.80 | $-1.12$ | 0.32 | 1.53 | 0.43 | $-0.69$ | 1.30 | 0.63 | 1800 |
| 1801 | 2.72 | 0.1 | 1.82 | 0.76 | 2.45 | $-0.75$ | $-0.30$ | 0.13 | 1.15 | 1.60 | 1.45 | 0.81 | 1801 |
| 1802 | -3.20 | $-0.90$ | 0.29 | 0.62 | 0.16 | 1.66 | $-0.04$ | 2.80 | 0.73 | 2.40 | 0.63 | 0.71 | 1802 |
| 1803 | -1.24 | -2.05 | -0.06 | 2.70 | $-1.78$ | $-0.31$ | 1.70 | 1.31 | $-0.96$ | -0.33 | 0.29 | 0.93 | 1803 |
| 1804 | 3.34 | -0.86 | $-1.18$ | $-0.49$ | 1.17 | 0.88 | 0.29 | $-0.14$ | 1.27 | 1.09 | $-0.71$ | $-1.68$ | 1804 |
| 1805 | $-1.41$ | -1.00 | $-0.34$ | $-1.27$ | $-1.76$ | -0.88 | -0.8s | $-1.60$ | 0.71 | $-2.03$ | -1.91 | -0.21 | 1805 |
| 1806 | 4.22 | 2.45 | 0.40 | $-2.24$ | 2.47 | 0.16 | $-0.49$ | 0.15 | 0.86 | 0.04 | 1.94 | 3.58 | 1806 |
| 1807 | 1.19 | 18 | $-1.17$ | $-1.32$ | 1.24 | 0.16 | 2.87 | 4.63 | $-0.94$ | 1.58 | 1.03 | 1.54 | 1807 |
| 1508 | , | -0.73 | -2.7 | -1.93 | 2.02 | $-0.45$ | 1.61 | 1.19 | 0.33 | -1.97 | $-0.23$ | $-5.46$ | 1808 |
| 1809 | 0.38 | 2.19 | $-0.40$ | -2.9 | 0.71 | $-0.25$ | 0.02 | 0.23 | $-0.31$ | $-0.76$ | -0.86 | 0.93 | 1809 |
| 1810 | $-1.72$ | $-2.39$ | 0.86 | -0.63 | -0.0.5 | -1.00 | $-0.41$ | 0.17 | 2.72 | 0.52 | 0.04 | 1.89 | 1810 |
| 1811 | $-2.93$ | $-0.16$ | 2.09 | 1.48 | 2.23 | 2.85 | 1.75 | 0.24 | 0.43 | 2.24 | 1.43 | $-0.25$ | 1811 |
| 1812 | $-1.383$ | 1.05 | 0.28 | $-2.87$ | 0.13 | -1.15 | $-2.18$ | -1.41 | $-1.39$ | 0.60 | $-1.99$ | $-4.72$ | 1812 |
| 1813 | -3.03 | 0.99 | $-1.15$ | 0.46 | -0.60 | -1.86 | -1.73 | $-2.10$ | -1.47 | -0.50 | $-0.75$ | $-0.33$ | 1813 |
| 1814 | -1.37 | $-4.71$ | $-2.93$ | 0.49 | $-2.79$ | $-2.39$ | $-0.12$ | $-1.12$ | $-2.45$ | $-1.50$ | 0.65 | 1.77 | 1814 |
| 1515 | $-1.30$ | 1.05 | 1.15 | $-0.37$ | $-0.16$ | $-0.74$ | --2.23 | -2.07 | -1.35 | $-0.70$ | $-1.37$ | $-2.26$ | 1815 |
| 1816 | 1.36 | $-1.83$ | -1.23 | -0.93 | $-2.69$ | $-2.21$ | $-2.42$ | $-2.56$ | $-2.04$ | $-0.93$ | $-1.49$ | $-0.75$ | 1816 |
| 1817 | 2.51 | 2.12 | -1.1. | $-5.01$ | $-1.93$ | 0.61 | $-1.79$ | $-1.89$ | 0.56 | $-3.22$ | 0.63 | $-0.70$ | 1817 |
| 1818 | $2.0 \times$ | 0.29 | -0.16 | 0.27 | $-1.72$ | $-0.02$ | -0. | -2.27 | -1.09 | $-0.71$ | 0.41 | $-2.08$ | 1818 |
| 1819 | 1.19 | 0.60 | 0.64 | $-0.09$ | $-0.76$ | 0.15 | -0.0.) | -0.33 | -0.28 | $-0.75$ | $-0.99$ | -1.34 | 1819 |
| 18.20 | -2.13 | -0.3.5 | $-2.26$ | 0.3 s | $-0.17$ | $-2.89$ | -1.66 | 0.93 | $-2.25$ | $-1.22$ | $-1.63$ | -1.66 | 1820 |
| 1521 | 1.1 | -3.06 | $-1.51$ | 0.99 | -2.18 | -3.01 | $-2.77$ | -1.15 | -0.06 | -0.99 | 1.51 | 2.53 | 1521 |
| 1823 | 2.21 | 0.6 .3 | 1.92 | 0.26 | 0.53 | 2.43 | 0.49 | -0.87 | $-0.56$ | $0.7 \%$ | 0.45 | $-2.29$ | 1822 |
| 1833 | $-4.17$ | 0.86 | 0.11 | $-1.72$ | 0.20 | $-0.97$ | -1.0.5 | 0.13 | 0.38 | 0.02 | -0.61 | 1.05 | 1823 |
| 1824 | 0.92 | 0.35 | $-1.0$ | -2.10 | -1.74 | -1.07 | $-0.11$ | $-0.51$ | 0.97 | $-0.26$ | 1.14 | 3.93 | 1824 |
| 1825 | 2.80 | 0.39 | $-1.0 .5$ | 2.12 | 0.93 | 0.56 | 0.51 | 0.32 | 1.31 | 0.21 | 3.06 | 4.15 | 1825 |
| 1826 | $-3.57$ | $-0.34$ | 1.39 | 0.17 | -1.04 | 1.05 | 1.99 | 3.61 | 1.61 | 1.38 | -0.28 | 0.92 | 1826 |
| 1527 | 0.09 | -4.95 | 1.00 | 1.31 | 1.20 | 1.05 | 2.06 | $-0.57$ | 0.93 | 1.35 | -1.30 | 2.93 | 1827 |
| 1828 | 2.12 | 0.27 | 0.51 | 0.31 | $-0.77$ | 0.39 | 0.35 | $-2.47$ | -1.9. | $-0.20$ | 0.61 | 2.28 | 1829 |
| 1829 | --0.85 | -3.13 | $-1.38$ | 0.30 | $-1.14$ | -1.11 | $-0.20$ | -2.37 | -1.3 | -1.41 | $-3.79$ | $-5.79$ | 1829 |
| 1830 | -5.98 | $-3.61$ | 1.17 | 0.77 | $-0.12$ | $-0.94$ | 0.50 | $-1.28$ | $-1.05$ | -0.88 | 1.14 | $-0.58$ | 1830 |
| 1831 | -2.09 | $-082$ | 0.70 | 3.60 | $-0.15$ | -1.36 | -0.09 | $-0.12$ | $-1.57$ | 2.40 | 2.27 | 0.26 | 1831 |
| 1832 | 0.77 | 1.28 | 0.09 | 0.21 | $-2.45$ | $-0.57$ | $-1.18$ | 0.59 | $-0.98$ | 0.16 | $-0.71$ | 0.25 | 1832 |
| 1833 | $-3.05$ | 3.32 | 0.21 | $-1.45$ | 2.29 | 1.06 | $-1.70$ | $-3.06$ | $-2.01$ | $-0.90$ | 2.78 | 3.95 | 1833 |
| 1534 | 5.52 | $-0.43$ | $-0.2 .5$ | -1.69 | 0.99 | 0.44 | 4.59 | 2.48 | 1.21 | 10.50 | 0.74 | 1.36 | 1834 |
| Means. | $-2.42$ | ' -0.09 | 3.09 | 7.55 | 11.94 | 13.72 | 14.85 | 14.62 | 11.69 | ) 7.11 | 2.22 | -0.71 | Means |

The numbers without sign must be subtracted ; those with the sigu - must be added.

## South Germany. - Stuttgard.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | Aprit. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ |  | $\bigcirc$ |  |  |  | , | $\bigcirc$ |  | $\bigcirc$ |  | $\bigcirc$ |  |
| 1792 | 0.64 | -1.23 | 1.78 |  | -1.12 | -0.30 | 1.04 | 1.70 | -0.70 | 1.30 | -0.73 | 0.44 | 1792 |
| 1793 | -1.41 | 1.64 | 0.37 | -1.36 | -1.24 | -0.31 | 2.52 | 1.84 | -0.84 | 1.71 | 0.66 | 2.10 | 1793 |
| 1794 | 2.02 | 3.72 | 2.76 | 3.26 | 0.41 | 1.30 | 2.75 | 0.12 | -1.34 | 0.32 | 0.85 | -1.72 | 1794 |
| 1795 | -4.88 | 0.36 | 0.65 | 2.51 | 0.64 | 1.43 | -1.01 | 1.33 | 1.93 |  | -0.49 | 3.76 | 1795 |
| 1796 | 6.17 | 1.90 | -2.51 | -0.67 | -0.32 | 0.10 | $-0.36$ | 0.23 | 2.34 | 0.13 | -0.87 | -2.18 | 1796 |
| 1797 | 2.46 | 0.08 | -0.27 | 1.88 |  | -1.30 | 2.86 | 1.01 | 1.04 | 0.36 | 1.82 | 3.02 | 1797 |
| 1798 | 0.65 | 1.44 | 0.69 | 1.16 | 0.66 | 1.21 | 0.14 | 0.66 | 1.36 | 0.53 | 0.33 | -2.05 | 1798 |
| 1799 | -3.46 | 1.77 | -0.78 | -1.30 | -0.89 | -0.75 | -0.99 | 0.32 | -0.04 | -0.15 | 0.42 | $-4.70$ | 1799 |
| 1800 | 3.03 | -0.92 | $-2.04$ | 4.56 | 2.03 | -1.81 | 0.00 | 0.79 | 0.84 | -0.37 | 1.61 | -0.15 | 1800 |
| 1801 | 3.95 | 0.97 | 1.98 | 0.24 | 0.94 | $-0.54$ | 0.91 | 1.42 | 2.32 | 2.89 | 1.30 | 1.46 | 1801 |
| 1802 | -2.55 | -0.02 | 0.80 | 2.13 | 0.23 | 1.53 | -0.24 | 2.22 | 0.62 | 2.08 | 0.81 | 1.41 | 1802 |
| 1803 | -0.81 | -1.90 | -1.31 | 1.49 | -2.28 | 0.05 | 1.21 | 1.28 | -1.78 | -0.90 | 0.46 | 1.36 | 1803 |
| 1804 | 4.61 | -0.98 | -1.05 | -0.22 | 0.78 | 0.92 | -0.35 | -0.66 | 2.88 | 0.74 | 0.56 | -1.56 | 1804 |
| 1505 | -1.03 | -0.28 | -0.60 | -1.38 | -2.16 | -1.35 | -1.28 | -1.44 | 0.38 | -2.73 | -2.17 | 0.06 | 1805 |
| 1806 | -2.78 | 2.77 | 1.10 | -1.99 | 1.37 | -0.27 | -0.62 | -0.59 | -0.27 | 0.03 | 1.67 | 4.55 | 1806 |
| 1807 | 0.76 | 1.58 | -2.43 | 1.14 | -1.02 | -0.21 | 2.15 | 3.23 | -0.74 | 1.71 | 1.37 | $-0.94$ | 1807 |
| 1805 | 95 | -1.23 | -3.55 | 1.35 | 1.96 | -0.98 | 0.54 | 0.77 | -0.34 | $-1.49$ | -0.17 | -4.02 | 1808 |
| 1809 | 1.56 | 3.64 | 0.69 | -2.58 | 0.84 | -0.65 | -0.36 | 0.16 | 0.30 | -1.05 | -1.65 | 2.12 | 1809 |
| 1810 | -1.56 | -2.45 | 2.11 | -4.12 | -0.25 | -0.95 | -0.26 | -0.48 | 2.08 | 0.09 | 1.44 | 0.97 | 1810 |
| 1811 | -3.01 | 0.49 | 2.31 | 0.97 | 1.41 | 1.41 | 0.75 | -0.38 | -0.04 | 3.02 | 1.28 | -0.04 | 1811 |
| 1812 | -2.36 | 26 | -0.23 | -3.17 | 0.64 | 0.37 | -1.85 | 17 | -0.49 | 0.01 | -2.28 | -4.81 | 1812 |
| 1813 | -2.25 | 0.28 | -0.42 | 0.53 | 0.13 | -1.45 | -1.96 | -3.00 | $-1.63$ | -0.34 | -1.15 | -0.70 | 1813 |
| 1814 | -1.96 | -3.96 | -3.67 | 9 | -2.14 | -1.52 | 0.26 | 76 | -1.56 | -1.3.4 | 0.69 | 2.13 | 1814 |
| 1815 | -1.92 | 1.26 | 2.15 | 0.39 | 0.71 | -0.42 | -1.95 | -1.4 | -0.48 | 0.03 | $-2.30$ | -1.44 | 1815 |
| 1816 | 0.69 | -2.37 | $-0.60$ | -0.68 | -2.22 | -2.63 | -2.45 | -2.34 | -0.85 | -0.17 | -2.45 | -0.82 | 1816 |
| 1817 | 3.31 | 1.47 | -0.71 | -3.71 | -1.78 | 0.92 | -1.5.4 | -0 97 | 1.08 | -3.25 | 1.01 | -0.49 | 1817 |
| 1818 | 2.67 | 0.40 | 0.41 | 1.33 | -0.82 | 1.06 | 0.15 | -0.91 | -0.70 | -0.91 | 1.62 | -2.04 | 1818 |
| 1819 | -0.61 | 1.54 | 0.89 | . 21 | 0.29 | 0.36 | 1.02 | 0.36 | -0.92 | -0.02 | -0.95 | 1.16 | 1819 |
| 1520 | -1.64 | -0.06 | $-2.16$ | 1 | -0.0.5 | -1.91 | $-1.37$ | 1.10 | 1. | -1.11 | -2.51 | -0.66 | 1820 |
| 1821 | 13 | $-2.72$ | 0.19 | 1.52 | 98 | -2.26 | -1.97 | 0.15 | 0.77 | -0.62 | 2.42 | 3.25 | 1821 |
| 1822 | 2.11 | 1.58 | 2.61 | 0.51 | 1.43 | 2.90 | 0.08 | -0.85 | -0.48 | 1.33 | 1.82 | -3.09 | 1822 |
| 1823 | -2.76 | 1.25 | -0.05 | -0.77 | 0.92 | -1. 12 | -1.19 | 0.25 | -0.38 | -1.03 | -1.37 | 1.70 | 1823 |
| 1824 | 0.79 | 0.79 | -0.89 | -1.61 | -1.0.5 | -0.98 | 0.30 | -0.39 | 0.65 | 0.44 | 2.52 | 3.81 | 1824 |
| 1825 | 1.92 | -0.37 | -1.36 | 1.85 | 0.27 | 0.26 | 0.19 | 0.02 | -0.61 | -0.64 | 1.27 | 2.74 | 1825 |
| 1826 | $-4.81$ | 1.06 | 1.16 | 0.19 | $-0.93$ | 0.54 | 1.70 | 1.78 | 1.51 | 1.43 | -1.07 | 0.54 | 1826 |
| 1827 | -0.49 | $-5.36$ | 1.47 | 1.22 | 1.60 | 0.23 | 1.10 | -0.45 | 0.08 | 0.67 | -2.41 | 2.98 | 1827 |
| 1828 | 3.10 | -0.35 | 0.61 | 0.54 | 0.43 | 0.97 | 1.02 | $-1.10$ | 0.07 | -0.61 | -0.17 | 1.19 | 1828 |
| 1829 | -2.45 | -3.10 | -0.58 | 0.46 | $-0.36$ | -0.61 | 0.45 | $-1.13$ | -1.50 | -1.66 | -2.s | -5.91 | 1829 |

[^6]
## LXXXV.

South Germany. - Stuttgard (contimued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived
from Series of Years.
Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | , | $\bigcirc$ | , | $\bigcirc$ | , | $\bigcirc$ | - |  |
| 1830 | $-6.40$ | $-3.47$ | 1.62 | 2.06 | 0.90 | $-0.38$ | 1.05 | 0.00 | $-1.43$ | $-0.89$ | 0.90 | $-0.74$ | 1530 |
| 1831 | $-0.73$ | 1.25 | 1.68 | 1.44 | -0.11 | -0.09 | 1.22 | $-0.10$ | -1.15 | 2.92 | 0.15 | 1.26 | 1831 |
| 1832 | 0.10 | $-0.76$ | $-0.64$ | 0.13 | -0.93 | $-0.59$ | $-0.22$ | 0.75 | $-1.05$ | $-0.78$ | $-1.41$ | 0.05 | 1832 |
| 1833 | $-2.56$ | 2.99 | $-0.99$ | $-1.31$ | 3.38 | 2.06 | -1.46 | $-2.81$ | -1.35 | -1.03 | $-0.13$ | 3.18 | 1833 |
| 1834 | 5.05 | 0.14 | -0.60 | -1.87 | 2.16 | 1.33 | 2.74 | 0.90 | 1.73 | -0.06 | 0.12 | -0.27 | 1834 |
| 1835 | 1.53 | 1.20 | -0.15 | $-0.90$ | -0.53 | 0.28 | 1.62 | -0.21 | 0.60 | $-1.20$ | $-3.22$ | $-2.85$ | 1835 |
| 18.36 | 0.45 | $-1.27$ | 3.18 | -0.90 | $-2.14$ | 0.64 | 0.22 | 0.46 | $-1.21$ | 0.47 | -0.01 | 1.04 | 1836 |
| 1837 | 0.90 | 0.24 | -2.68 | $-2.54$ | $-2.23$ | 1.16 | -1.19 | 1.17 | -1.94 | $-0.60$ | $-0.40$ | 0.04 | 1837 |
| 1838 | $-4.43$ | -2.08 | 0.21 | $-2.32$ | $-0.45$ | $-0.03$ | $-0.36$ | -0.90 | 0.64 | $-0.36$ | 1.03 | -1.34 | 1838 |
| 1839 | 0.78 | $-0.63$ | $-1.31$ | $-2.71$ | $-1.07$ | 2.30 | 0.58 | $-1.55$ | 0.64 | 0.84 | 1.07 | 1.95 | 1839 |
| 1940 | 1.82 | 0.15 | $-2.90$ | 1.36 | 0.29 | 0.16 | -1.42 | $-0.23$ | $-0.26$ | -2.39 | 1.10 | $-5.61$ | 1840 |
| 18.4 | 0.89 | -1.98 | 2.09 | 0.53 | 3.42 | -1.55 | -1.93 | -0.69 | 1.6 .3 | 1.24 | 1.22 | 2.85 | 1841 |
| 1842 | $-1.50$ | $-1.05$ | 1.36 | $-0.47$ | 1.35 | 1.74 | 0.35 | 2.64 | 0.07 | $-2.47$ | $-1.82$ | $-0.20$ | 1842 |
| 1843 | 2.07 | 1.54 | 0.15 | 0.60 | $-1.06$ | $-1.48$ | $-0.68$ | 0.20 | $-0.15$ | 0.02 . | 0.67 | 0.23 | 1843 |
| 18.44 | 0.31 | $-0.91$ | $-0.30$ | 1.42 | -1.01 | 1.39 | -1.99 | $-2.17$ | 0.56 | 0.39 | 0.91 | -3.18 | 1844 |
| Means. | -0.80 | 1.64 | 3.97 | 7.80 | 11.87 | 14.03 | 15.18 | 15.02 | 12.05 | 8.05 | 4.11 | 1.25 | Means. |

LXXXYI. South Germany - Carlsruhe.


South Germany. - Cirlsrume (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | - | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  |
| 1507 | 0.02 | 1.11 | -2.83 | -1.34 | 1.19 | -0.28 | 2.34 | 3.15 | -1.57 | 1.30 | 1.21 | $-0.53$ | 1807 |
| 1805 | 1.38 | $-1.25$ | $-3.54$ | $-1.63$ | 2.40 | -0.41 | 1.94 | 0.96 | $-0.54$ | $-1.2 \mathrm{~S}$ | $-0.24$ | -3.75 | 1808 |
| 1809 | 1.24 | 3.25 | 0.52 | $-3.16$ | 0.41 | -1.22 | -0.61 | $-0.33$ | -0.80 | -1.36 | $-1.90$ | 1.60 | 1809 |
| 1810 | -3.19 | $-2.78$ | 1.26 | $-0.17$ | $-0.60$ | -0.62 | -0.65 | -0.46 | 1.58 | $-0.05$ | 0.84 | 1.69 | 1810 |
| 1811 | $-2.40$ | 1.17 | 2.79 | 1.65 | 2.32 | 1.55 | 0.78 | $-0.29$ | 0.53 | 2.92 | 1.21 | 0.48 | 1511 |
| 1812 | -2.09 | 1.47 | $-0.16$ | $-2.96$ | 0.83 | $-0.50$ | $-1.53$ | -0.27 | -0.24 | 1.33 | $-1.42$ | -3.80 | 1812 |
| 1813 | -0.84 | 2.15 | 0.57 | 1.50 | 0.12 | -1.01 | -1.75 | -1.78 | $-1.15$ | 0.27 | -0.11 | -0.89 | 1813 |
| 1814 | -1.51 | $-3.24$ | $-1.56$ | 1.82 | -1.65 | $-1.66$ | 0.07 | -1.12 | $-1.07$ | $-0.68$ | 0.82 | 2.67 | 1814 |
| 1815 | -2.35 | 2.31 | 2.67 | 0.75 | 1.10 | $-0.57$ | $-1.75$ | -1.03 | 0.09 | 0.62 | $-1.99$ | $-1.02$ | 1815 |
| 1816 | 1.38 | $-2.00$ | $-0.27$ | 0.27 | $-2.23$ | $-2.48$ | $-2.61$ | $-2.16$ | $-0.89$ | $-0.33$ | $-2.14$ | 0.17 | 1816 |
| 1817 | 3.56 | 2.16 | $-0.36$ | -3.14 | -1.63 | 0.87 | -1.47 | $-1.40$ | 1.60 | $-2.82$ | 1.75 | 0.13 | 1817 |
| 1818 | 2.91 | 1.12 | 0.59 | 1.53 | -1.44 | 1.00 | 0.34 | -1.01 | $-0.50$ | -0.63 | 1.49 | $-2.11$ | 1818 |
| 1819 | 1.85 | 1.30 | 0.75 | 1.42 | 0.49 | 0.15 | 0.42 | 0.64 | 0.49 | $-0.15$ | $-0.75$ | 0.31 | 1819 |
| 1820 | -1.09 | 0.55 | -1.3. | 2.19 | 0.22 | -2.16 | $-0.96$ | 0.66 | -1.20 | $-0.61$ | -1.80 | 0.00 | 18.20 |
| 1521 | 2.31 | $-1.59$ | 0.73 | 1.75 | -1.87 | $-2.01$ | $-2.03$ | 0.14 | 0.17 | -0.68 | 2.72 | 3.52 | 1821 |
| 1822 | 2.52 | 2.96 | 4.0 .4 | 1.75 | 2.11 | 3.77 | 0.56 | $-0.14$ | 0.46 | 1.19 | 2.66 | -1.31 | 1822 |
| 1823 | $-2.23$ | 2.20 | 1.05 | $-0.09$ | 1.23 | $-1.02$ | -1.14 | 0.87 | 0.24 | $-0.27$ | $-0.11$ | 2.95 | 1823 |
| 1824 | 1.39 | 1.95 | $-0.10$ | -0.89 | $-1.13$ | -0.65 | 0.32 | $-0.22$ | 1.04 | 0.66 | 2.65 | 4.09 | 1824 |
| 1825 | 1.92 | 0.28 | $-0.76$ | 1.43 | -0.15 | $-0.41$ | 0.85 | 5.49 | 1.15 | 0.15 | 1.51 | 3.05 | 1825 |
| 1826 | -3.4 | 1.35 | 1.13 | 0.20 | -1.25 | 1.06 | 2.12 | 2.86 | 1.75 | 1.94 | $-0.21$ | 0.93 | 1826 |
| 1827 | -0.55 | $-5.10$ | 1.19 | 1.50 | 1.25 | 1.01 | 2.06 | 0.00 | 1.15 | 1.34 | $-2.01$ | 2.85 | 1827 |
| 1828 | 3.18 | 0.41 | 1.17 | 0.82 | 0.74 | 1.19 | 0.91 | $-1.22$ | 0.48 | 0.28 | $-0.33$ | 1.85 | 1823 |
| 1529 | $-2.12$ | $-2.33$ | $-0.05$ | 0.72 | $-0.04$ | 0.21 | 0.50 | $-1.17$ | -0.85 | $-0.60$ | -1.8S | $-4.97$ | 1829 |
| 1830 | -5.83 | -2.98 | 2.14 | 2.21 | 0.81 | -0.22 | 0.86 | -0.13 | -1.01 | $-0.17$ | 1.31 | $-0.32$ | 1830 |
| 1831 | -0.98 | 0.96 | 1.65 | 1.83 | $-0.50$ | -0.61 | 0.38 | 0.40 | -0.81 | 3.26 | 0.30 | 1.64 | 1831 |
| 1832 | 0.10 | -0.27 | 0.23 | 0.96 | -0.85 | $-0.49$ | $-0.01$ | 1.02 | -0.59 | 0.18 | $-0.68$ | 0.9.3 | 1832 |
| 1833 | $-2.63$ | 3.41 | $-0.71$ | $-0.78$ | 2.9 .4 | 1.45 | $-1.24$ | $-2.23$ | -1.05 | $-0.17$ | 0.51 | 4.43 | 1833 |
| 1834 | 5.74 | 0.29 | 0.76 | -1.12 | 1.87 | 1.12 | 2.76 | 1.35 | 1.82 | 0.53 | 0.79 | 0.29 | 1834 |
| 1835 | 1.77 | 1.74 | 0.11 | $-0.90$ | $-0.68$ | 0.13 | 1.46 | -0.17 | $-0.03$ | -0.83 | $-2.92$ | $-2.23$ | 1835 |
| 1836 | 0.43 | $-0.55$ | 3.27 | $-0.66$ | -1.99 | 0.47 | 0.21 | 0.47 | 1.67 | 0.82 | 0.66 | 1.56 | 1836 |
| 1837 | 1.30 | 0.80 | -1.86 | -2.33 | -2.05 | 1.26 | $-0.86$ | 1.24 | -1.66 | 0.28 | 0.46 | 0.72 | 1837 |
| 1838 | $-4.35$ | $-2.13$ | 0.21 | $-2.36$ | $-0.33$ | -0.21 | $-0.36$ | -1.20 | 0.44 | $-0.02$ | 1.10 | $-0.52$ | 1838 |
| 1539 | 0.88 | 0.67 | $-0.73$ | --2.24 | $-0.54$ | 2.28 | 0.16 | -0.47 | 0.09 | 1.20 | 1.49 | 2.20 | 1839 |
| 1840 | 1.37 | -0.69 | $-2.82$ | 1.28 | $-0.51$ | 0.23 | -1.39 | 0.34 | -0.22 | $-2.04$ | 1.81 | -5.32 | 1840 |
| Means. | -0.17 | 1.93 | 4.39 | 8.31 | 12.40 | 14.43 | 15.80 | 15.41 | 12.60 | 8.30 | 4.16 | 1.35 | Means. |

## LXXXVII.

## North Germany. - Berlin.

For Keducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reatrmur.

| Yeas. | Jan. | Feb. | March | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | $\bigcirc$ | $\bigcirc$ |  | - | - | - | $\bigcirc$ | - | c | - | $\bigcirc$ |  |
| 1719 | 2.44 | 0.21 | 1.50 | 0.69 | 1.45 | 2.38 | 3.13 | 1.86 | 0.08 | 0.66 | 2.09 | $-1.02$ | 1719 |
| 1720 | 2.27 | 0.40 | $-0.14$ | 0.70 | 1.34 | 0.94 | 2.01 | 0.31 | 0.10 | 1.62 | -0.03 | 1.47 | 1720 |
| 1721 | 2.35 | $-1.80$ | $-1.53$ | 2.23 | -0.9 I | 1.21 | $-0.67$ | $-0.17$ | 0.54 | 0.40 | 1.69 | 0.07 | 1721 |
| 1728 | 1.50 | $-2.28$ | 2.39 | 0.65 | 1.24 | 0.26 | $-0.38$ | $-1.36$ | $-0.10$ | 0.66 | $-0.58$ | $-1.51$ | 1728 |
| 1729 | -3.18 | $-1.46$ | -3.57 | -2.11 |  | - • | - | -• |  | - • |  | -• | 1729 |
| 1730 | 1.64 | 0.20 | 0.29 | 0.70 | 0.00 | 0.12 | $-0.62$ | $-0.03$ | -0.69 | -2.55 | 1.99 | $-0.48$ | 1730 |
| 1731 | $-2.00$ | -1.75 | $-0.67$ | $-1.67$ | $-1.33$ | $-0.89$ | $-1.44$ | $-0.62$ | -0.25 | 1.85 | 0.67 | 0.26 | 1731 |
| 1732 | $-1.50$ | 1.34 | 1.05 | 1.34 | 0.29 | -1.54 | $-1.95$ | $-0.98$ | -0.84 | 1.14 | -0.78 | -3.99 | 1732 |
| 1733 | 2.69 | 2.54 | 0.86 | 1.59 | $-1.77$ | $-2.71$ | -0.38 | $-0.97$ | $-2.02$ | $-0.33$ | 0.21 | 2.46 | 1733 |
| 1734 | 0.40 | 2.51 | 1.86 | 0.55 | $-0.54$ | $-1.26$ | $-0.62$ | -0.93 | $-0.54$ | 0.65 | -2.85 | $-1.03$ | 1734 |
| 1735 | 1.79 | 0.30 | 1.81 | 1.49 | $-0.87$ | -0.33 | -1.38 | -0.64 | 0.91 | -1.01 | $-1.07$ | -0.17 | 1735 |
| 1736 | -0.08 | $-0.92$ | $-0.73$ | 0.55 | $-0.68$ | -0.87 | $-0.24$ | 0.64 | -0.98 | 0.23 | $-0.09$ | 1.18 | 1736 |
| 1737 | 1.83 | 0.55 | 1.57 | -1.36 | 0.77 | 0.11 | -0.77 | -1.65 | $-0.10$ | $-0.39$ | $-0.83$ | $-0.05$ | 1737 |
| 1738 | -0.55 | 0.55 | 1.11 | 1.54 | -0.08 | -0.42 | $-0.79$ | $-0.38$ | -0.03 | 0.88 | -2.21 | 0.90 | 1738 |
| 1739 | $-0.17$ | 2.06 | 1.11 | $-1.65$ | 0.64 | $-0.96$ | 0.99 | -123 | 0.91 | $-2.62$ | $-5.35$ | $-0.01$ | 1739 |
| 1740 | -6. | $-6.54$ | $-3.28$ | -3.15 | $-3.49$ | -1.70 | -0.96 | -0.62 | 1.62 | -3.12 | $-2.35$ | $-0.18$ | 1740 |
| 1741 | $-0.93$ | 1.88 | $-0.71$ | -1.38 | -1.90 | -1.59 | 0.17 | -0.54 | $-0.20$ | 1.22 | 1.77 | -0.16 | 1741 |
| 1742 | -1.23 | 1.08 | $-0.99$ | -2.16 | $-1.83$ | $-0.72$ | $-0.66$ | -1.26 | -1.78 | 0.19 | 0.70 | -3.22 | 1742 |
| 1743 | 1.32 | 0.99 | $-0.58$ | $-1.94$ | 0.28 | 1.05 | -1.46 | 0.32 | $-0.50$ | $-1.44$ | 2.77 | 0.84 | 1743 |
| 1744 | $-1.95$ | -2.42 | $-0.09$ | 2.3 | 0.10 | $-1.47$ | 0.25 | $-0.60$ | 0.94 | 2.10 | 1.25 | $-0.39$ | 1644 |
| 1745 | -1.92 | $-1.26$ | $-0.10$ | 0.20 | 0.73 | 1.01 | 0.01 | 0.17 | 0.10 | 1.15 | 2.17 | $-2.36$ | 1745 |
| 1746 | 0.1 | 0.0 .3 | $-1.88$ | $-0.39$ | 0.43 | $-0.72$ | 1.11 | $-0.43$ | 0.44 | -1.06 | $-0.53$ | 1.69 | 1746 |
| 1747 | $-0.17$ | 3.49 | $-2.09$ | 0.70 | $-0.67$ | 2.34 | $-0.33$ | 0.18 | 1.43 | 0.43 | 0.21 | 1.04 | 1747 |
| 1748 | -1.17 | $-1.70$ | -2.29 | 0.22 | 1.53 | 2.11 | 0.56 | 2.85 | $-0.14$ | 0.00 | 1.79 | 3.19 | 1745 |
| 1749 | 2.28 | 0.47 | $-1.52$ | $-0.14$ | 1.58 | 0.21 | 0.39 | 1.64 | 0.3:3 | 0.05 | $-0.63$ | 1.28 | 1749 |
| 1750 | 1.19 | 3.22 | 3.57 | 1.26 | 0.30 | 1.06 | 1.97 | 1.56 | 0.26 | $-0.55$ |  | $-0.06$ | 1750 |
| 1751 | -0.45 | $-1.70$ | 2.79 | $-0.86$ | 3.59 | 2.39 | 1.78 | 3.12 | 0.42 | $-0.04$ |  |  | 1751 |
| Means. | $-0.19$ | 0.69 | 2.65 | 6.51 | 10.63 | 12.82 | 14.02 | 13.14 | 11.06 | 6.53 | 3.15 | 1.24 | Means. |
| 1755 | $-4.56$ | $-6.47$ |  | 0.54 |  |  |  | -0.25 |  |  |  | 2.14 | 1755 |
| 1756 | 4.13 | 2.63 | 1.85 | 1.77 | 0.37 | 2.55 | 1.50 | -0.35 | 1.61 | 1.62 | $-0.38$ | -1.43 | 1756 |
| 1757 | 1.17 | 2.37 | 1.71 |  | -0.39 | 1.47 | 3.25 | 0.22 | $-1.70$ | $-2.88$ | 1.21 | -1.25 | 1757 |
| 1758 | -2.57 | $-0.17$ | 0.13 | -0.21 | 1.08 | 0.18 | $-0.86$ | 0.55 | $-1.11$ | $-0.97$ | 0.16 | 0.38 | 1758 |
| 1759 | 3.26 | 1.79 | 1.18 | -0.01 | $-1.45$ | 0.87 | 1.15 | 0.60 | $-0.45$ | 1.09 | -2.21 | -3.85 | 1759 |
| 1760 | $-0.56$ | -1.48 | -0.81 | 0.34 | 0.33 | 0.57 | -0.29 | 0.03 | 0.87 | 0.98 | 0.12 | 2.05 | 1760 |
| 1761 | 0.97 | 1.65 | 2.51 | -0.01 | 1.55 | 1.9 .7 | $-0.62$ | 1.88 | 2.30 | -1.02 | $-0.12$ | -3.08 | 1761 |
| 1762 | 2.11 | -0.01 | $-1.88$ | 1.88 | 0.42 | 0.27 | $-0.19$ | $-1.45$ | 0.23 | -1.34 | $-0.32$ | $-1.82$ | 1762 |
| 1763 | -2.25 | 3.02 | $-0.40$ | -0.55 | $-0.34$ | 0.17 | 0.92 | 1.32 | $-0.86$ | $-0.57$ | $-0.25$ | 2.67 | 1763 |
| 1764 | 2.91 | 2.58 | $-0.10$ | $-0.30$ | 1.71 | -1.94 | 1.43 | $-0.60$ | -1.70 | $-0.63$ | -1.32 | $-1.54$ | 1764 |
| 1765 | 1.64 | -2.90 | 1.70 | 0.78 | $-2.50$ | -0.88 | $-1.92$ | 1.12 | -1.16 | 1.20 | 0.15 | 0.03 | 1765 |
| 1766 | $-0.10$ | -0.12 | 1.01 | 2.07 | 1.17 | 0.30 | -0.: | -0.25 | 0.73 | $-0.43$ | 0.48 | $-0.26$ | 1766 |
| 1767 | $-5.54$ | 1.74 | 0.01 | -1.58 | -1.03 | -1.65 | $-0.23$ | 0.98 | 0.42 | 0.95 | 2.03 | $-1.75$ | 1767 |

The numbers without sign must be subtracted; those with he sign - must be added.

North Germany. - Berlin (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | c | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - |  |
| 1768 | -3.52 | $-0.98$ | -1.25 | $-0.11$ | -0.68 | -0.06 | 0.28 | -0.08 | $-1.03$ | $-0.48$ | 0.54 | 0.47 | 1768 |
| 1769 | 1.22 | $-0.74$ | 0.75 | 0.11 | -1.01 | -1.01 | $-0.71$ | $-1.07$ | 0.58 | -2.26 | 0.26 | 0.84 | 1769 |
| 1770 | $-0.20$ | $-0.21$ | -3.16 | -1.09 | $-0.11$ | -1.20 | $-0.35$ | -0.08 | 0.62 | 0.81 | 0.16 | 1.92 | 1770 |
| 1771 | -1.24 | $-3.28$ | -8. 10 | -3.27 | 2.04 | -0.21 | $-0.82$ | $-2.12$ | $-0.46$ | 0.76 | $-1.47$ | 0.95 | 1771 |
| 1772 | 0.66 | 1.20 | 0.86 | -0.86 | $-2.50$ | $-0.10$ | $-1.40$ | -0.4] | 0.60 | 1.62 | 1.89 | 1.38 | 1772 |
| 1773 | 2.50 | $-1.00$ | $-0.61$ | 0.49 | 1.37 | $-1.22$ | -0.85 | 0.06 | 0.57 | 1.89 | $-0.92$ | 2.21 | 1773 |
| Means. | -0.13 | 1.64 | 3.87 | 7.71 | 11.94 | 15.23 | 16.18 | 15.34 | 12.12 | 7.73 | 4.38 | 1.85 | Means. |
| 1774 | 1.50 | 2.26 | 2.29 | 1.56 | $-0.05$ | 0.69 | $-1.56$ | $-1.92$ | $-1.61$ | 0.71 | $-3.70$ | $-0.75$ | 1774 |
| 1775 | 0.95 | 3.20 | 2.53 | $-0.65$ | $-0.72$ | 3.26 | 1.88 | 1.61 | 2.00 | 1.23 | -0.8! | 2.16 | 1775 |
| 1776 | $-5.55$ | 2.42 | 2.10 | $-0.13$ | -2.11 | 1.19 | 1.21 | 0.32 | 0.12 | $-0.47$ | 0.70 | 0.54 | 1776 |
| 1777 | 0.04 | $-1.67$ | 0.67 | $-1.12$ | 0.52 | 0.04 | $-0.60$ | -0.01 | $-1.71$ | 0.23 | 2.23 | 0.75 | 1777 |
| 1778 | -0.58 | -1.72 | 1.09 | 1.98 | 0.67 | 0.30 | 1.02 | 0.66 | $-0.67$ | -1.69 | 1.44 | 3.84 | 1778 |
| 1779 | 0.33 | 3.82 | 2.99 | 2.39 | 0.61 | -0.30 | 0.74 | 1.71 | 1.59 | 1.95 | 0.90 | 2.26 | 1779 |
| 1780 | -1.06 | $-2.02$ | 3.37 | $-1.27$ | 0.72 | 0.24 | 0.45 | 0.99 | $-0.03$ | 1.46 | $-0.34$ | $-0.70$ | 1780 |
| 1781 | $-0.44$ | 0.53 | 2.05 | 1.85 | 1.19 | 1.97 | 2.02 | 2.56 | 1.60 | $-0.39$ | 0.80 | 0.01 | 1781 |
| 1782 | 3.15 | -2.86 | $-0.39$ | -0.87 | 0.33 | 1.78 | 1.52 | 0.21 | 1.75 | -0.30 | -1.13 | 0.78 | 1782 |
| 1783 | 3.19 | 3.67 | -0.58 | 0.86 | 1.38 | 2.71 | 1.45 | 0.71 | 0.36 | 0.34 | 0.50 | $-1.51$ | 1783 |
| 1784 | -3.97 | -3.54 | -1.68 | $-2.30$ | 0.58 | 0.20 | $-0.75$ | -1.35 | 0.02 | $-2.21$ | 1.29 | $-0.94$ | 1784 |
| 1785 | 0.47 | $-3.28$ | $-5.74$ | $-2.54$ | $-1.48$ | -0.84 | $-0.70$ | $-1.12$ | 0.61 | $-0.31$ | 1.09 | $-1.42$ | 178.5 |
| 1786 | 1. 81 | $-0.93$ | -2.32 | 1.60 | $-1.25$ | 0.54 | $-1.71$ | -1. 26 | -1.86 | -1.97 | -3.64 | $-0.16$ | 1786 |
| 1787 | $-0.29$ | 1.35 | 2.0 .5 | -1.31 | $-0.77$ | 0.99 | -0.6.) | $-0.59$ | $-0.17$ | 1.32 | 0.69 | 2.07 | 1787 |
| 1788 | 2.46 | $-1.26$ | $-1.47$ | 0.10 | 0.45 | 1.64 | 1.64 | -1.21 | 1.20 | $-0.35$ | $-0.79$ | $-8.64$ | 1788 |
| 1789 | -1.93 | 1.46 | $-4.45$ | 0.01 | 1.85 | 0.14 | 0.11 | 0.36 | 1.85 | 0.64 | 0.89 | 3.5.5 | 1789 |
| 1790 | 3.05 | 2.82 | 2.19 | -1.67 | 1.70 | 0.58 | -1.13 | -0.54 | $-0.48$ | -0.14 | -0.30 | 1.92 | 1790 |
| 1791 | 3.9 | 1.52 | 1.47 | 1.74 | $-1.16$ | 0.19 | 0.78 | 1.08 | $-0.78$ | 0.22 | -0.89 | 1.35 | 1791 |
| 1792 |  | $-1.89$ | 0.80 | 1.45 | $-0.81$ | 0.83 | 1.59 | 0.46 | $-0.98$ | $-0.30$ | -0.01 | 1.14 | 1792 |
| 1793 | $-0.70$ | 2.14 | 0.61 | $-0.68$ | $-0.58$ | $-1.34$ | 1.68 | 0.22 | $-0.83$ | 1.99 | 0.99 | 2.05 | 1793 |
| 1794 | 1.18 | 2.56 | 3.66 | 3.12 | 0.18 | 1.77 | 2.79 | $-0.59$ | $-1.62$ | 0.37 | 1.53 | $-2.14$ | 1794 |
| 1795 | -5.23 | $-0.36$ | $-0.84$ | 2.88 | $-1.78$ | 2.10 | $-0.92$ | $-0.37$ | 1.27 | 3.36 | 0.10 | 3.14 | 1795 |
| 1796 | 6.51 | 0.68 | $-1.70$ | $-0.34$ | -0.46 | 0.38 | 0.48 | 1.33 | 1.74 | 0.07 | $-0.60$ | $-1.92$ | 1796 |
| 1797 | 1.60 | 1.89 | 0.66 | 1.09 | 1.41 | $-0.23$ | 1.55 | 1.26 | 2.02 | 0.55 | -0.80 | 1.81 | 1797 |
| 1798 | 1.79 | 1.57 | $-0.07$ | 1.29 | 0.76 | 1.20 | 0.38 | 0.92 | 1.24 | $-0.17$ | -0.45 | $-3.54$ | 1798 |
| 1799 | $-2.97$ | $-4.47$ | -1.65 | -2.12 | -2 27 | -1.53 | -1.05 | -0.32 | -0.65 | $-0.70$ | 0.48 | $-4.41$ | 1799 |
| 1800 | -1.12 | -3.61 | $-4.09$ | 4.43 | 2.33 | -3.06 | $-1.99$ | 0.22 | 0.67 | $-0.41$ | 1.47 | 0.00 | 1800 |
| 1801 | 1.88 | $-1.02$ | 1.84 | 0.0 .5 | 3.00 | -1.37 | $-0.61$ | $-0.68$ | 1.01 | 1.40 | 0.93 | 0.84 | 1801 |
| 1802 | $-1.00$ | 0.50 | 1.65 | 0.45 | $-2.37$ | -1.01 | $-1.54$ | 1.54 | $-0.08$ | 3.04 | 0.78 | 1.51 | 1802 |
| 1803 | $-5.33$ | 2.02 | $-0.16$ | 2.81 | $-1.36$ | $-1.46$ | 2.03 | 1.80 | $-1.82$ | $-0.45$ | 0.65 | $-0.39$ | 1803 |
| 1804 | 1.51 | -1.48 | -3.11 | -1.06 | 1.04 | -0.54 | 0.10 | $-0.73$ | 1.17 | $-0.02$ | -2.40 | $-3.92$ | 180.4 |
| 1805 | $-3.90$ | $-1.94$ | -0.48 | -1.58 | 1.36 | $-1.53$ | -1.18 | $-1.83$ | 0.55 | -3.53 | -2.58 | 1.24 | 1805 |
| 1806 | 3.02 | 0.94 | 0.19 | -2.82 | 0.99 | $-2.26$ | -1.35 | -0.98 | 0.41 | $-0.12$ | 1.47 | 4.14 | 1806 |
| 1807 | 1.62 | 0.18 | -1.97 | -1.43 | $-0.42$ | -1.50 | 0.42 | 3.72 | -2.15 | 0.02 | 1.11 | 1.53 | 1807 |

North Germany. - Berlin (contimued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derivea from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  | - |  | , | $\bigcirc$ | $\bigcirc$ | 1 |  |
| 1805 | 0.83 | -1.07 | -3.39 | -2.80 | 0.80 | $-0.42$ | 1.19 | 0.69 | -0.54 | $-1.56$ | -1. | $-4.40$ | 1808 |
| 1809 | -3.31 | 1.64 | -1.09 | $-3.3 .1$ | 0.99 | -0.89 | $-0.48$ | 0.36 | 0.29 | $-0.99$ | 0.02 | 2.23 | 1809 |
| 1810 | -0.99 | $-1.66$ | 0.40 | -1.41 | -1.88 | $-1.93$ | -0.05 | $-0.47$ | 1.16 | $-1.33$ | 0.09 | 1.22 | 1510 |
| 1511 | $-2.93$ | $-0.72$ | 2.01 | $-0.15$ | 3.07 | 2.67 | 0.94 | $-0.59$ | $-0.72$ | 2.21 | 0.35 | 1.50 | 1811 |
| 1512 | -1.14 | -0.2 | -1. | -3.9 | -1.20 |  | $-2.37$ | $-0.78$ | -1.81 | 1.14 | $-1.57$ | $-5.52$ | 1812 |
| 1813 | -1.20 | 2.38 | 0.21 | 1. | -0.73 | 1.38 | -1.27 | $-2.07$ | -0.62 | -1.30 | 0.05 | 1.02 | 1813 |
| 1814 | $-2.12$ | $-5.52$ | $-2.78$ | 1. | $-2.92$ | -1.99 | 1.02 | $-1.34$ | -2.23 | $-1.21$ | 0.53 | 1.26 | 1814 |
| 1815 | -2.81 | 1.14 | 1.56 | -0.45 | -0.15 | 0.61 | $-2.98$ | $-1.57$ | -1.95 | 0.42 | -0.69 | $-1.37$ | 1815 |
| 1816 | 0.95 | -2.27 | -0.65 | -0.21 | -2.68 | -1.54 | -1.32 | $-2.59$ | $-1.64$ | $-1.23$ | -1.96 | $-0.39$ | 1816 |
| 1817 | 2.55 | 1.79 | $-0.19$ | -3.86 | $-0.49$ | 1.0 .1 | -1.57 | $-0.55$ | 1.43 | $-2.57$ | 2.37 | $-0.14$ | 1817 |
| 1818 | 2.54 | 0.19 | 1.56 | 0.53 | 0.22 | 0.95 | . 72 | -1.41 | 0.14 | $-0.58$ | -0.60 | $-0.89$ | 1818 |
| 1819 | 2.51 | 1.57 | 1.59 | 0.85 | 1.00 | 2.28 | 1.42 | 1.60 | 0.81 | $-0.41$ | $-0.66$ | $-2.61$ | 1819 |
| 1520 | -3.0s | 0.34 | $-0.02$ | 1.52 | 1 | $-2.38$ | -2.08 | 1.23 | $-0.75$ | 0.99 | $-1.57$ | $-1.88$ | 1820 |
| 1821 | 1.52 | $-1.05$ | 0.14 | 3.28 | -0.45 | -2.17 | -1.51 | $-0.78$ | 0.91 | 1.33 | 3.27 | 3.44 | 1821 |
| Means. | -1.59 | 0.3 | 2.2 | 6.89 | 11.36 | 13.73 | 15.16 | 15.00 | 11.83 | 7.16 | 2.61 | -0.32 | Means. |
| 1822 | 3.39 | 3.67 | 3.22 | 1.55 | 0.59 | 0.58 | 0.77 | -0. | $-1.24$ | 1.36 | 1.55 | $-3.18$ | 1822 |
| 1823 | $-7.56$ | $-0.25$ | 0.41 | $-1.82$ | -0.26 | $-0.78$ | -1.76 | 1.03 | $-0.34$ | 0.66 | 1.01 | 1.12 | 1823 |
| 18.4 | 3.67 | 2.45 | 0.29 | $-0.52$ | -1.04 | $-0.75$ | $-0.56$ | $-0.58$ | 1.27 | 0.56 | 1.96 | 2.69 | 18.24 |
| 182.5 | 3.92 | 0.92 | -2.26 | 0.86 | -0.15 | -1.10 | $-0.47$ | 0.05 | 0.54 | $-0.12$ | 1.30 | 2.03 | 182.5 |
| 1826 | -3.44 | 1.98 |  | -0.19 | $-0.24$ | 1.20 | 3.03 | 3.00 | 0.35 | 0.71 | $-0.33$ | 0.49 | 1826 |
| 1827 |  | 90 | 1.25 | 2.29 | 1.95 | 1.33 | 0.80 | -0.04 | 1.09 | 0.83 | $-2.24$ | 1.16 | 1827 |
| 1828 | -0.2 | $-0.5 .5$ | 0.6 | 1.22 | 0.33 | 0.30 | 1.17 | $-0.71$ | $-0.15$ | $-0.28$ | 0.17 | 0.47 | 1828 |
| 1529 | -2.8 | -2 | -1.23 | 0.41 | -0.29 | 0.12 | 0.41 | $-0.5$ | -0.16 | -1.6 | $-2.54$ | $-8.25$ | 1829 |
| 1830 | -4.21 | $-2.70$ | 1.09 | 1.53 | 0.30 | 0.07 | 0.35 | -0. | $-0.57$ | $-0.69$ | 1.47 | $-1.79$ | 1830 |
| 1831 | -1.8 | 0.75 | 0.40 | 2.21 | $-0.94$ | -1.34 | 0.36 | 0. | -1.2.2 | 1.77 | -0.54 | 0.11 | 1831 |
| 1832 | 0.76 | 1.12 | 0.42 | 0.32 | -1.43 | $-0.33$ | $-2.40$ | 0. | -1.22 | -0. | $-0.63$ | $-0.24$ | 1832 |
| 1833 | -0.56 | 3.16 | $-0.1$ | -1.82 | 3.46 | 1.33 | -0.45 | -3.12 | $-0.48$ | $-0.93$ | 0.14 | 2.48 | $18: 33$ |
| 1834 | 4.73 | 1.31 | 1.00 | $-0.68$ | 1.82 | 1.23 | 3.65 | 2.34 | 0.74 | -0.2 | 0.56 | 0.36 | 1834 |
| 183.5 | 2.81 | 2.37 | 0.57 | -0.91 | -0.86 | 0.13 | 0.21 | $-0.59$ | 1. | -0.9 | -2.7 | $-1.77$ | 1835 |
| 1836 | 1.37 | 1.11 | 3.42 | 0.07 | $-2.55$ | 0.20 | -1.0s | $-1.49$ | $-1.06$ | 1.00 | -1.10 | 0.26 | 1836 |
| 1837 | 1.91 | 0.38 | $-1.98$ | -1.68 | -1.42 | -0.69 | -1.11 | 1.20 | -0.92 | 0.37 | 0.72 | $-0.57$ | 1887 |
| $18: 38$ | $-6.30$ | $-3.63$ | 0.1 | -1.42 | $-0.24$ | 035 | -0.22 | $-1.78$ | 1.27 | $-0.59$ | -1.14 | -0.33 | 1838 |
| 1839 | 0.79 | 1.50 | $-1.9$ | $-2.54$ | 0.58 | 0.95 | 0.77 | -0.44 | 1.10 | 0.15 | 1.10 | $-1.49$ | 1839 |
| 1840 | -0.09 | 0.6 .3 | 0.23 | $-0.07$ | $-0.03$ | 0.16 | 0.27 | -0.07 | -0.05 | 0.09 | -0.05 | $-0.33$ | 1840 |
| 1841 | -0.01 | -4.0.3 | 0.91 | 1.01 | 2.51 | -0.88 | -1.10 | $-0.01$ | 0.58 | 1.29 | 0.75 | 1.62 | 1841 |
| 1842 | $-1.34$ | 0.39 | 0.93 | $-1.52$ | 0.75 | $-0.54$ | $-0.84$ | 3.13 | 0.42 | -1.55 | -2.82 | 0.71 | 1842 |
| 1843 | 2.40 | 2.45 | $-1.09$ | 0.44 | -2.01 | $-1.00$ | $-0.41$ | 1.17 | -0.64 | $-0.66$ | 1.42 | 1.96 | 1843 |
| 1844 | 1.00 | $-0.96$ | $-1.50$ | 0.48 | 0.56 | $-1.00$ | -2.: | $-1.6$ | 0.36 | $-0.2$ | 0.56 | 2.41 | 1844 |
| 1845 | 1.65 | $-4.55$ | $-6.24$ | 0.28 | -1.48 | 0.49 | 0.90 | $-0.9$ | -0.93 | $-0.18$ | 1.26 | 0.33 | 1845 |
| Means. | -1.90 | -0.15 | 2.74 | 6.58 | 10.92 | 13.94 | 15.04 | 14.13 | 11.75 | 797 | 3.25 | 1.32 | Means |

The numbers without sign must be subtracted; those with the sign - must be added.

Denmark. - Copenhagen.
For Reducing the Monthly and Yearly Means of Single Years to the Means deriven from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | , |  | , |  | $\bigcirc$ | , | , | , | $\bigcirc$ |  | 10 |  |
| 1767 | -3.89 | 0.34 | 0.52 | -1.49 | -1.83 | -1.99 | $-1.40$ | -0.47 | 0.22 | $-0.75$ | 1.58 | $-0.29$ | 1767 |
| 1768 | -0.67 | -0.14 | $-\mathrm{I} .01$ | 0.11 | -0.82 | $-0.50$ | $-0.18$ | $-0.59$ | -1.37 | -0.49 | 0.57 | 1.66 | 1768 |
| 1769 | 1.74 | 0.79 | 1.44 | 0.30 | $-0.70$ | $-0.50$ | $-0.42$ | $-1.21$ | $-0.17$ | -1.92 | 0.03 | 0.37 | 1769 |
| 17\%0 | 0.19 | 1.64 | -2.57 | $-0.77$ | $-0.32$ | $-0.88$ | 0.21 | 0.36 | 1.11 | 1.38 | $-0.18$ | 0.69 | 1770 |
| 1771 | $-1.20$ | $-2.18$ | -3.96 | -3.14 | 0.27 | 1.50 | $-0.33$ | $-2.04$ | -0.90 | 0.03 | -1.11 | 1.10 | 1771 |
| 1772 | -0.88 | -1.71 | -2.53 | $-1.72$ | -1.94 | -0.51 | $-0.56$ | $-0.59$ | 0.83 | 1.49 | 2.39 | 1.33 | 1772 |
| 1773 | 1.78 | $-0.46$ | 0.35 | 0.33 | 0.83 | $-0.54$ | 0.50 | 0.81 | 0.45 | 1.73 | 0.81 | 0.94 | 1773 |
| 1774 | $-2.37$ | 0.34 | 0.87 | 0.83 | $-0.09$ | 0.37 | 0.0.1 | -0.65 | $-1.07$ | $-0.3$ | $-5.39$ | $-2.55$ | 1774 |
| 1775 | -0.51 | 1.79 | 1.72 | 0.21 | $-0.09$ | 2.13 | 1.39 | 1.72 | 2.60 | 0.78 | $-1.97$ | 0.71 | 1775 |
| 1776 | -5.22 | 1.18 | 1.49 | 0.73 | -0.87 | 1.61 | 2.30 | 1.35 | 0.59 | 0.6 | 0.77 | 0.69 | 1776 |
| 1782 | 2.38 | $-0.61$ | $-0.99$ | $-0.62$ | $-0.63$ | 3.43 | 0.12 | 0.32 | 0.99 | -1.09 | $-1.42$ | 0.07 | 1782 |
| 1783 | 0.81 | 2.57 | $-0.38$ | 2.01 | 1.97 | 2.36 | 3.05 | 1.56 | 1.67 | 1.91 | $-0.06$ | $-0.87$ | 1783 |
| 1784 | -2.02 | $-0.59$ | $-2.41$ | $-1.51$ | 0.24 | 0.07 | $-0.31$ | $-0.21$ | 0.18 | $-0.78$ | 1.16 | $-0.76$ | 1784 |
| 1785 | 0.53 | -2.27 | $-2.96$ | -1.04 | $-1.52$ | 0.78 | -0.33 | $-0.46$ | 0.10 | -0.03 | 1.55 | $-0.20$ | 1785 |
| 1786 | 0.13 | 0.06 | -2.69 | 0.83 | -1.08 | 1.45 | -0.35 | $-0.41$ | $-0.74$ | -1.2 | -2.91 | $-0.04$ | 1786 |
| 1787 | 0.94 | 2.21 | 2.09 | $-0.20$ | 0.07 | 0.01 | 0.06 | $-0.31$ | 0.58 | 1.81 | $-0.40$ | 0.26 | 1787 |
| 1785 | 2.02 | 0.63 | -1.14 | 0.95 | 1.00 | 1.28 | $-0.93$ | 0.38 | 1.71 | $-0.31$ | $-0.19$ | $-6.92$ | 1788 |
| 1798 | 1.15 | 2.27 | 1.31 | 2.48 | 2.71 | 2.06 | 2.00 | 2.15 | 1.09 | 1.01 | 0.01 | $-2.29$ | 1798 |
| 1799 | $-0.71$ | $-4.50$ | $-1.94$ | -1.59 | $-2.12$ | $-0.44$ | $-0.18$ | $-0.43$ | 0.21 | 0.56 | 1.27 | $-2.55$ | 1799 |
| 1800 | -0.96 | $-2.07$ | $-3.57$ | 2.60 | 1.77 | -1.69 | -0.89 | 0.42 | 0.21 | 1.19 | 1.78 | 1.20 | 1800 |
| 1801 | 1.28 | 0.75 | 2.92 | 1.44 | 2.93 | $-0.10$ | 1.30 | 0.58 | 0.69 | 2.17 | 1.97 | 0.46 | 1801 |
| 1802 | $-0.56$ | 1.04 | 1.90 |  | -1.78 | $-2.26$ | $-3.12$ | $-0.56$ | -0.87 | 0.98 | 0.45 | 0.32 | 1802 |
| 1803 | -3.02 | $-1.58$ | -0.39 | 1.86 | -1.69 | $-2.02$ | $-0.21$ | $-0.14$ | -1.76 | $-0.90$ | $-0.31$ | $-1.36$ | 1803 |
| 1804 | 2.01 | $-1.47$ | $-1.92$ | $-0.58$ | 0.25 | $-0.57$ | $-0.30$ | 0.12 | 1.23 | 0.77 | $-1.74$ | -2.85 | 1804 |
| 1805 | -1.79 | $-2.02$ | 0.26 | -1.03 | $-2.14$ | $-3.46$ | $-1.48$ | $-1.03$ | 0.77 | $-2.53$ | $-0.56$ | 0.77 | 1805 |
| 1806 | 1.90 | 1.64 | $-0.49$ | -1.59 | 0.03 | $-2.28$ | $-1.79$ | $-0.08$ | 1.32 | 0.35 | 1.27 | 2.54 | 1806 |
| 1507 | 1.75 | 1.46 | $-0.55$ | $-0.56$ | $-0.37$ | -1.60 | $-0.17$ | 2.54 | -2.22 | 0.02 | 0.19 | 0.77 | 1807 |
| 1803 | 1.04 | $-0.77$ | $-1.30$ | -1.40 | 0.19 | 0.02 | 1.26 | 1.34 | 1.10 | -0.14 | $-0.85$ | $-2.12$ | 1808 |
| 1809 | -2.64 | 0.30 | $-0.42$ | -2.52 | 0.60 | $-0.91$ | $-0.59$ | 0.47 | 0.30 | $-0.14$ | -0.23 | 1.65 | 1809 |
| 1810 | 0.60 | -0.28 | 0.05 | -1.19 | $-2.69$ | $-1.01$ | -0.07 | $-0.29$ | 0.51 | $-0.79$ | $-0.22$ | 0.10 | 1810 |
| 1811 | -0.65 | 0.23 | 2.16 | $-0.71$ | 1.75 | 0.96 | 2.07 | -0.32 | -0.26 | 1.28 | 1.12 | 1.07 | 1811 |
| 1812 | 0.40 | 1.21 | $-1.55$ | $-2.62$ | $-1.63$ | $-0.97$ | -2.38 | $-0.61$ | -1.67 | 1.36 | -1.14 | $-3.56$ | 1812 |
| 1813 | 0.23 | 2.66 | 1.50 | 0.55 | $-1.01$ | $-1.00$ | 0.44 | -0.89 | $-0.53$ | $-2.01$ | 0.20 | 0.97 | 1813 |
| 1814 | -3.81 | $-4.01$ | $-2.15$ | 0.28 | $-2.99$ | -1.97 | 0.13 | -0.87 | -1.05 | $-0.58$ | 1.22 | 0.85 | 1814 |
| 1515 | $-0.67$ | 1.47 | 1.82 | 0.30 | $-0.26$ | $-1.26$ | $-1.95$ | $-0.81$ | -1.11 | 0.59 | 0.20 | -0.66 | 1815 |
| 1816 | 0.72 | -1.56 | -0.05 | $-0.49$ | $-2.69$ | -1.87 | $-0.19$ | -1.86 | $-0.89$ | $-10.7$ | -0.95 | $-0.31$ | 1816 |

The numbers without sign must be subtracted; those with the sign - must be added.

Denmark. - Copenhagen (contimued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derivea from Series of Years.

| Year. | Jan. | Feb. | March | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | 5 | $\bigcirc$ | 0. | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - |  | $\bigcirc$ | 0 | 0 |  |
| 1817 | 2.79 | 2.98 | 1.13 | -1.10 | $-0.01$ | -1.04 | -1.53 | $-1.38$ | 0.62 | $-2.24$ | 1.41 | $-1.71$ | 1817 |
| 1818 | 1.99 | 1.73 | 2.40 | $-1.05$ | $-0.05$ | 0.97 | 1.29 | $-0.24$ | 0.69 | 0.87 | 1.48 | 0.20 | 1818 |
| 1519 | 3.46 | 2.30 | 2.39 | 1.56 | 1.25 | 1.69 | 1.58 | 3.28 |  | $-0.79$ | -1.03 | $-1.26$ | 1819 |
| 1820 | -1.67 | 0.51 | 0.52 | 1.55 | 0.25 | -1.16 | $-0.36$ | $-0.33$ | -0.60 | $-0.64$ | $-0.56$ | -0.87 | 1820 |
| 1821 | 0.36 | 0.16 | 0.24 | 2.24 | $-0.43$ | -1.77 | -1.81 | $-0.86$ | 0.67 | 1.62 | 1.65 | 2.47 | 1821 |
| 1822 | 2.56 | 3.82 | 3.64 | 2.28 | 1.59 | 0.87 | 0.24 | $-0.17$ | -0.64 | 1.52 | 2.63 | 0.56 | 1822 |
| 1523 | $-2.60$ | $-0.08$ | 0.70 | -0.04 | 0.51 | 0.15 | -0.94 | 0.41 | 0.47 | 1.02 | 1.88 | 1.74 | 1523 |
| 1824 | 3.65 | 2.36 | 0.97 | 0.91 | 0.14 | 1.22 | $-0.61$ | $-0.48$ | 1.62 | 0.09 | 1.20 | 2.15 | 1824 |
| 1826 |  | -• | -• | -• | 4.30 | 5.91 | 7.76 | , 6.63 | -• |  | -• | 2.04 | 1826 |
| 1527 | 0.16 | $-2.30$ | 0.59 | 2.14 | 1.44 | 1.93 | 0.09 | -0.29 | 1.48 | 1.16 | $-1.20$ | 2.30 | 1827 |
| 1828 | -0.07 | 0.43 | 1.37 | 0.58 | 1.31 | 1.34 | 1.36 | 0.26 | 0.41 | 0.46 | 0.61 | 0.50 | 1828 |
| 1829 | -1.14 | $-3.06$ | $-0.95$ | $-1.00$ | 1.84 | 1.50 | -0.23 | $-1.01$ | 0.03 | $-1.43$ | -2.91 | $-3.60$ | 1529 |
| 1830 | $-2.26$ | $-2.85$ | 1.39 | 0.69 | $-0.18$ | $-0.86$ | 0.30 | $-0.81$ | -0.95 | 0.15 | 1.75 | $-0.22$ | 1830 |
| 1831 | -1.60 | 0.61 | $-0.16$ | 1.87 | 0.31 | 0.85 | 2.52 | 1.55 | $-0.59$ | 2.71 | -0.65 | 1.91 | 1831 |
| 1832 | 1.52 | 1.73 | 1.55 | 1.84 | -0.23 | 1.29 | $-0.94$ | $-0.06$ | $-0.98$ | 0.60 | -0.47 | 0.58 | 1832 |
| 1833 | 0.05 | 1.50 | -0.45 | -0.72 | 2.32 | 0.72 | 0.79 | $-2.27$ | 0.05 | 0.63 | 0.77 | 1.32 | 1833 |
| 1534 | 2.26 | 1.71 | 2.23 | 0.90 | 1.98 | 0.72 | 3.60 | 3.26 | 0.11 | $-0.05$ | 0.22 | 0.59 | 1834 |
| 1835 | 1.87 | 2.16 | 1.66 | $-0.02$ | $-0.92$ | 1.17 | 1.03 | $-0.57$ | 0.09 | $-0.5 .5$ | -1.44 | $-0.88$ | 1835 |
| 1836 | 0.29 | 0.63 | 2.71 | 0.14 | $-0.17$ | 0.21 | $-0.89$ | $-1.86$ | -1.62 | $-0.15$ | -1.34 | 0.09 | 1836 |
| 1837 | 0.17 | 0.54 | -1.08 | $-1.50$ | $-1.10$ | 0.05 | -0.21 | 0.60 | $-0.80$ | $-0.06$ | $-0.91$ | $-0.75$ | 1837 |
| 1838 | -2.8.3 | 4.8 .5 | $-0.56$ | -2.63 | -0.97 | $-0.70$ | -0.09 | $-2.25$ | -0.44 | -1.82 | -2.01 | -0.25 | 1838 |
| 1839 | $-0.17$ | -0.38 | $-2.06$ | $-2.80$ | 0.49 | 0.13 | 0.23 | -1.2 t | $-0.10$ | 0.11 | -0.19 | $-2.12$ | 1839 |
| 1840 | -0.63 | -0.39 | $-0.64$ | 0.35 | -2.64 | $-2.17$ | -8.2. | $-1.79$ | -1.9.7 | $-3.75$ | $-0.51$ | $-2.6 .5$ | 1840 |
| 1841 | $-1.14$ | -2.52 | 0.97 | 0.62 | 2.21 | $-1.37$ | $-2.56$ | -0.97 | $-0.71$ | $-0.38$ | $-0.36$ | 2.37 | 1841 |
| 1842 | $-0.26$ | 1.43 | 2.05 | 0.61 | 1.75 | $-0.11$ | $-0.99$ | 2.73 | 0.31 | -0.85 | $-1.57$ | 2.36 | 1842 |
| 184.3 | 1.82 | 0.79 | -0.33 | 0.46 | $-0.96$ | -0.25 | -0.67 | 1.03 | -0.20 | $-1.23$ | 3 0.86 | 2.99 | 1843 |
| 1844 | 0.07 | -2.48 | $-1.50$ | 0.74 | 1.49 | $-1.12$ | $-2.17$ | -1.12 | $-0.62$ | $-0.29$ | ) 0.46 | -1.43 | 1844 |
| 184.5 | 1.24 | -4.16 | $-4.45$ | 0.54 | -1.01 | 0.20 | 0.22 | $-0.86$ | -1.26 | -1.04 | 11.28 | 0.59 | 1845 |
| Means. | -1.16 | -0.80 | 0.5 .5 | 4.45 | 8.98 | 12.45 | 13.81 | 13.50 | 10.36 | 7.05 | 3 3.12 | 0.68 | Means. |

## France. - Paris.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ |  | , | , | $\bigcirc$ |  | $\bigcirc$ | $\bigcirc$ | - | 0 | - |  |
| 1806 | 3.35 | 1.38 | 0.28 | -1.54 | 2.07 | 0.77 | 0.64 | -0.38 | 0.53 | -0. | 1.6 | 4.00 | 1806 |
| 1807 | 0.34 | 1.39 | $-2.74$ | $-0.63$ | 1.28 | $-0.52$ | 1.94 | 2.34 | -2.08 | 1.1 | -0.7 | -1.7.3 | 1807 |
| 1808 | 0.42 | $-1.42$ | $-2.19$ | $-2.23$ | 2.55 | $-0.30$ | 2.14 | 0.66 | $-0.78$ | -1.7 | 0.58 | $-1.87$ | 1808 |
| 1809 | 2.95 | 2.91 | 0.42 | $-2.72$ | 0.54 | -1.38 | -1.08 | $-0.36$ | $-0.81$ | -1.0 | -1.54 | 1.04 | 1809 |
| 1810 | $-2.90$ | $-1.11$ | 1.16 | $-0.42$ | $-0.62$ | -0.06 | $-0.74$ | $-0.70$ | 1.75 | 0.25 | 0.80 | 1.30 | 1810 |
| 1811 | -1.83 | 2.31 | 1.90 | 1.58 | 2.14 | 0.25 | 0.44 | -0.66 | 0.95 | 2.55 | 1.38 | 0.72 | 1811 |
| 1812 | $-0.32$ | 1.63 | -0.82 | $-1.92$ | 0.88 | $-0.75$ | -0.96 | -0.46 | $-0.17$ | 0.5 | $-1.95$ | $-3.71$ | 1812 |
| 1813 | $-1.18$ | 1.33 | $-0.23$ | 0.71 | 0.48 | $-1.26$ | -1.12 | $-1.42$ | $-1.35$ | 0.2 | -0.6 | $-0.17$ | 1813 |
| 1814 | -1.70 | -3.37 | $-2.30$ | 1.30 | $-1.67$ | -1.17 | 0.46 | -0.91 | $-0.26$ | $-1.22$ | $-0.51$ | 2.02 | 1814 |
| 1815 | -1.98 | 2.39 | 2.29 | 0.36 | 0.18 | $-0.89$ | $-0.93$ | -0.54 | -0.11 | 0.77 | -2.70 | $-1.34$ | 1815 |
| 1816 | 0.54 | -1.69 | $-0.71$ | 0.10 | $-1.40$ | $-1.83$ | $-2.53$ | $-2.37$ | $-1.26$ | 0.2 | $-2.24$ | 0.07 | 1816 |
| 1817 | 2.48 | 2.2 | $-0.20$ | $-2.02$ | -1.70 | 0.61 | -1.34 | $-1.66$ | 0.99 | $-3.16$ | 1.80 | $-1.12$ | 1817 |
| 1818 | 1.94 | -0.21 | $-0.15$ | 1.20 | $-0.65$ | 1.75 | 1.14 | -0.18 | 0.0 .5 | 0.38 | 1.98 | $-1.23$ | 1818 |
| 1819 | 2.43 | 0.95 | 0.16 | 1.31 | 0.02 | -0.85 | 0.30 | 0.78 | 0.55 | $-0.12$ | -1.66 | $-0.30$ | 1819 |
| 1820 | -2.02 | -0.93 | $-1.42$ | 1.20 | $-0.30$ | -1.37 | $-0.35$ | 0.11 | -1.19 | -0.9 | -1.30 | -0.22 | 1820 |
| 1821 | 1.02 | $-2.5$ | 0.54 | 1.34 | -1.95 | -2.05 | $-1.39$ | 1.20 | 0.55 | -0.14 | 2.70 | 3.10 | 1521 |
| 1822 | 1.96 | 1.52 | 2.6 | 1.0 | 1.72 | 3.26 | 0.09 | 0.42 | 0.15 | 1.72 | 1.82 | -3.42 | 1522 |
| 1823 | -1.79 | 0.88 | $-0.14$ | $-0.62$ | 0.50 | -1.69 | -1.23 | 0.46 | 0.00 | $-0.58$ | -0.5 4 | 1.58 | 1823 |
| 1824 | 0.61 | 0.63 | $-1.00$ | -0.54 | $-1.52$ | $-0.61$ | -0.02 | -0.17 | 0.89 | 0.54 | 2.30 | 2.74 | 1894 |
| 1825 | 1.23 | 0.06 | $-0.94$ | 1.54 | -0.22 | $-0.05$ | 1.24 | 0.70 | 1.77 | 0.75 | 0.40 | 2.18 | 1823 |
| 1826 | -2.77 | 1.73 | 0.56 | 0.27 | -1.48 | 1.35 | 1.59 | 2.10 | 1.11 | 1.7 | -1.08 | 1.72 | 1826 |
| 1827 | -1.63 | -4.14 | 1.14 | 1.14 | 0.18 | -0.09 | 0.85 | $-0.43$ | 0.46 | 1. | -0.77 | 2.58 | 1827 |
| 1828 | 3.23 | 0.50 | 0.29 | 0.50 | 0.46 | 0.34 | 0.34 | $-0.74$ | 0.74 | $-0.30$ | 0.51 | 0.89 | $18: 8$ |
| 1829 | -3.16 | $-0.97$ | $-0.75$ | -0.08 | 0.32 | 0.05 | $-0.10$ | -1.30 | $-1.53$ | -1.01 | -1.64 | $-5.70$ | 18.9 |
| 1830 | -3.42 | $-2.59$ | 2.51 | 1.68 | 0.11 | -0.82 | 0.16 | -1.23 | $-1.50$ | $-0.44$ | 0.83 | $-0.82$ | 1830 |
| 1831 | 0.13 | 1.53 | 1.85 | 1.30 | $-0.20$ | $-0.12$ | 0.86 | 0.12 | -0.3.5 | 2.83 | $-0.10$ | 1.50 | 1831 |
| 1832 | -0.36 | -0.59 | $-0.93$ | 0.65 | -1.05 | 0.22 | 0.68 | 1.87 | $-0.10$ | 0.06 | $-0.10$ | 0.53 | 1832 |
| 1833 | -1.73 | 2 | -1.82 | $-0.38$ | 2.54 | 1.06 | $-0.24$ | -1.65 | $-1.53$ | 0.57 | $-0.61$ | 3.46 | 18:33 |
| 1834 | 4.34 | -0.42 | 0.67 | $-0.70$ | 1.59 | 0.70 | 1.25 | 0.69 | 1.24 | 0.29 | $-0.05$ | $-0.02$ | 1834 |
| 1835 | 1.35 | 1.69 | $-0.14$ | -0.38 | $-0.55$ | 0.18 | 1.92 | 1.42 | 0.36 | -0.92 | $-1.10$ | $-2.84$ | 1835 |
| 1836 | 0.55 | -1.0.3 | 1.62 | $-1.02$ | $-1.67$ | 1.06 | 0.56 | 0.30 | $-1.24$ | 4-0.04 | 0.66 | 0.36 | 1836 |
| 1837 | 0.39 | 0.97 | $-3.26$ | $-3.34$ | $-2.79$ | 1.14 | $-0.32$ | 1.26 | $-0.84$ | 40.04 | $-0.62$ | 0.60 | 1837 |
| 1838 | $-5.21$ | $-5.03$ | 0.26 | $-2.52$ | -0.23 | -0.68 | $-0.32$ | -0.42 | $-0.12$ | -0.04 | 0.74 | -1.48 | 1833 |
| 1839 | 0.75 | 0.73 | -0.62 | $-1.70$ | -0.71 | 1.62 | $-0.04$ | -0.86 | 0.00 | -0.56 | 1.10 | 1.60 | 1839 |
| 1840 | 1.23 | $-0.47$ | $-2.58$ | 2.26 | 0.49 | 1.02 | $-1.08$ | 0.98 | $-0.64$ | 4-1.40 | 0.99 | $-4.76$ | 1840 |
| 1841 | 0.47 | -1.35 | 1.94 | 0.42 | 2.25 | -1.26 | -1.68 | $-0.50$ | 2.28 | 0.12 | 2.02 | 1.48 | 1841 |
| 1842 | -2.6.5 | 0.33 | 1.30 | 0.26 | 0.05 | 2.66 | 0.52 | 3.18 | $-0.12$ | -2.25 | $-1.10$ | 0.36 | 1842 |
| 1843 | 2.07 | -0.39 | 1.06 | 0.50 | -0.31 | -0.86 | $-0.48$ | 0.70 | 0.96 | 60.12 | 2. 0.54 | 0.60 | 1843 |
| 1844 | 0.83 | -1.31 | 0.15 | 2.22 | -1.35 | 0.54 | -1.12 | -2.34 | 0.24 | $4-0.36$ | ) 0.26 | $-3.40$ | 1844 |
| Means. | 1.53 | 3.35 | 5.33 | 7.90 | 11.59 | 13.66 | 14.96 | 14.82 | 12.52 | 29.00 | 0 5.41 | 2.92 | Means |

The numbers witnout sign must be subtracted; those with the sign - must be added.

## Holland. - Zwanenburg.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | - | - | - | - | $\bigcirc$ | - | - | $\bigcirc$ | - | $\bigcirc$ |  |
| 1743 | 0.60 | 1.40 | -0.15 | $-2.69$ | -0. 40 | 0.59 | -1.15 | 0.0.) | $-0.22$ | $-2.27$ | 1.83 | -0.23 | 1743 |
| 1744 | -0.91 | $-2.36$ | -0.74 | -0.80 | -0.89 | $-0.26$ | $-1.02$ | -1.23 | $-0.71$ | 0.39 | 0.66 | 0.21 | 1744 |
| 1745 | 0.15 | -1.64 | $-0.70$ | $-0.43$ | $-0.04$ | -0.69 | $-0.92$ | -1.20 | 0.02 | $-0.27$ | $-0.50$ | $-2.16$ | 1745 |
| 1746 | -0.82 | $-1.70$ | $-2.19$ | $-1.20$ | 1.36 | -0.62 | 0.04 | $-1.28$ | $-0.65$ | -2.09 | $-2.80$ | 1.02 | 1746 |
| 1747 | $-0.47$ | 2.16 | -2.29 | $-0.15$ | -0.52 | 0.92 | $-0.65$ | $-0.21$ | 0.34 | $-0.49$ | 1.62 | 1.60 | 1747 |
| 1748 | -0.24 | -2.63 | $-4.14$ | -2.12 | -0.31 | 1.45 | 0.08 | 0.39 | $-0.03$ | 0.28 | 1.65 | 3.46 | 1748 |
| 1749 | 2.68 | 0.11 | -1.09 | -0.52 | 1.11 | $-2.30$ | $-0.10$ | 0.23 | $-0.11$ | -0.35 | -0.4. | 1.6.) | 1749 |
| 1750 | -0.34 | 2.60 | 2.88 | $-0.06$ | 0.14 | $-0.10$ | 0.97 | $-0.45$ | 0.75 | -1.2.5 | -1.63 | -0.3 I | 1750 |
| 1751 | 1.09 | $-2.29$ | 1.33 | -0.60 | $-1.21$ | $-0.10$ | $-0.7 \mathrm{~S}$ | -0.52 | $-1.19$ | $-0.48$ | -1.31 | 0.33 | 1751 |
| 1752 | 1.71 | $-0.56$ | . 7 | 3 | -1.10 | 0.95 | $-0.18$ | -0.09 | 0.39 | 0.07 | 0.90 | 1.37 | 1752 |
| 1753 | -1.80 | -0.11 | 1.34 | 0.01 | -0.30 | 1.19 | $-0.34$ | $-1.00$ | 0.30 | 0.59 | -0.88 | 0.67 | 1753 |
| 1754 | 0.64 | $-1.14$ | $-2.23$ | $-1.40$ | 0.41 | $-0.49$ | -1.33 | $-0.16$ | -0.44 | 0.61 | 0.05 | -0.36 | 1754 |
| 17.55 | -1.95 | $-3.19$ | -1.24 | 1.72 | -1.37 | 1.59 | -0.31 | $-1.33$ | $-1.12$ | -0.08 | -0.03 | 1.22 | 1755 |
| 1756 | 3.20 | 1.32 | 0.38 | -1.37 | $-1.53$ | 0.97 | 0.80 | -0.50 | 0.74 | -0.31 | $-1.13$ | $-2.60$ | 1756 |
| 1757 | -2.22 | $-0.59$ | 0.00 | 1.00 | -1.01 | $-0.11$ | 2.37 | 0.36 | $-0.21$ | $-1.09$ | 1.43 | $-0.09$ | 1757 |
| 1758 | -1.28 | 0.37 | 0.41 | $-0.39$ | 1.95 | 0.29 | -1.41 | - . 99 | $-0.17$ | 0.21 | 0.05 | 0.36 | 1758 |
| 1759 | 2.86 | 2.13 | 1.49 | 0.86 | -0.58 | 0.99 | 1.66 | 0.71 | $-0.07$ | 1.05 | $-1.54$ | -2.68 | 1759 |
| 1760 | -1.64 | -0.69 | 0.15 | 0.77 | $-0.22$ | 1.31 | $-0.15$ | $-0.40$ | 1.14 | 0.28 | 1.08 | 2.67 | 1760 |
| 176 I | 1.78 | 1.90 | 2.37 | 0.17 | 0.92 | 0.56 | -0.61 | 1.16 | 0.67 | -1.75 | 0.34 | $-1.59$ | 1761 |
| 1762 | 2.10 | 0.09 | $-1.2 .3$ | 2.37 | 0.93 | 0.67 | 0.30 | -1.31 | $-0.04$ | -1.98 | -1.37 | -2.02 | 1762 |
| 1763 | $-4.88$ |  | -0.34 | -0.24 | -1.04 | 0.28 | -0.08 | 0.2 | -0.56 | -0.99 | 0.56 | 1.52 | 1763 |
| 1764 | 3.37 | 2.52 | 0.17 | 0.52 | 1.71 | 0.02 | 1.43 | $-0.32$ | $-1.14$ | $-0.74$ | -0.45 | $-1.01$ | 1764 |
| 1765 | 2.24 | $-2.13$ | 2.30 | 1.62 | 0.27 | 1.22 | $-0.84$ | 0.85 | $-0.05$ | 1.24 | 0.08 | -0.82 | 1765 |
| 1766 | -0.22 | $-0.78$ | 0.72 | 1.67 | 0.37 | 0.35 | 0.20 | 0.45 | 0.49 | 0.32 | 0.46 | -0.68 | 1766 |
| 1767 | -3.34 | 2.34 | 1.05 | -0.63 | $-1.36$ | $-0.94$ | $-0.80$ | 0.36 | 0.98 | 0.71 | 2.15 | $-1.33$ | 1767 |
| 1768 | -1.94 | 0.9 | $-0.07$ | -0.09 | $-0.02$ | 0.54 | 0.65 | 0.33 | -1.27 | -0.37 | 0.70 | 0.72 | 1768 |
| 1769 | 1.19 | 0.09 | 0.85 | 0.99 | -0.2I | $-0.53$ | 0.53 | $-0.06$ | 0.48 | $-1.71$ | 0.58 | 1.43 | 1769 |
| 1770 | 1.45 | 0.92 | $-1.12$ | $-1.04$ | $-0.15$ | $-0.34$ | 0.02 | 1.20 | 1.59 | 0.19 | 0.06 | 2.01 | 1770 |
| 1771 | $-0.50$ | -1.4 | -2.33 | $-2.59$ | 1.72 | 0.26 | $-0.29$ | -1.01 | 0.04 | 0.59 | 0.69 | 1.68 | 1771 |
| 1772 | 0.11 | 0.21 | 0.6 | $-0.50$ | $-1.11$ | 1.19 | 0.57 | 0.36 | 0.83 | 2.68 | 2.36 | 1.16 | 1772 |
| 1773 | 3.38 | -0.57 | 1.36 | 0.81 | 0.35 | 0.31 | $-0.16$ | 1.17 | 0.66 | 1.79 | 1.51 | 1.76 | 1773 |
| 1774 | 0.58 | 1.62 | 2.18 | 1.30 | 0.08 | 0.96 | 1.12 | 0.51 | -0.30 | 1.23 | -1.84 | -0.45 | 1774 |
| 1775 | 1.31 | 3.40 | 2.12 | 1.04 | $-0.12$ | 2.19 | 0.75 | 0.88 | 1.84 | 1.25 | -1.53 | 1.65 | 1775 |
| 1776 | -4.40 | 1.20 | 1.99 | 1.45 | $-0.85$ | 1.11 | 1.56 | 0.47 | -0.0 I | 1.31 | 0.46 | 0.05 | 1776 |
| 1777 | -0.23 | $-1.57$ | 1.14 | $-0.56$ | 0.15 | $-0.19$ | $-0.07$ | 0.88 | 0.60 | 0.73 | 1.97 | $-0.60$ | 1777 |
| 1778 | -1.26 | -1.70 | $-0.55$ | 0.36 | 0.71 | 0.43 | 1.43 | 0.51 | $-1.58$ | -2.02 | 1.08 | 2.90 | 1778 |
| 1779 | $-0.28$ | 2.55 | 1.79 | 1.21 | 0.61 | $-0.77$ | 0.60 | 1.51 | 1.27 | 1.6 I | 0.19 | 0.53 | 1779 |
| 17~0 | $-1.54$ | $-0.56$ | 2.65 | -0.78 | 1.07 | $-0.51$ | $-0.25$ | 2.04 | 1.08 | 1.03 | -0.07 | -1.09 | 1780 |

The numbers without sigo must be subtracted ; those with the sign - must be added.

Holland. - Zwanenburg (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | A pril. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | - | - | , | $\bigcirc$ | , | , | $\bigcirc$ | $\bigcirc$ |  | $\bigcirc$ |  |
| 1781 | -0.97 | 1.18 | 1.18 | 1.23 | 0.37 | 2.47 | 1.04 | 1.56 | 0.91 | 0.75 | 0.36 | 0.39 | 1781 |
| 1782 | 2.88 | -1.88 | -0.56 | -1.11 | -1.09 | 0.77 | 0.34 | -0.54 | 0.50 | -0.93 | -2.43 | -0.89 | 1782 |
| 1783 | 2.39 | 2.13 | -1.31 | 1.24 | -0.05 | 0.92 | 2.75 | 0.93 | 0.44 | 0.73 | 0.48 | -2.74 | 1783 |
| 1784 | -3.26 | -3.01 | -2.04 | -2.16 | 1.23 | 0.15 | -0.37 | -0.80 | 0.94 | -2.30 | 0.80 | -1.60 | 1784 |
| 1785 | -0.06 | -2.34 | -3.32 | -1.54 | -0.96 | -0.46 | -0.01 | -0.59 | 1.14 | 0.40 | 0.41 | -1.70 | 1785 |
| 1786 | 0.35 | -0.08 | -3.19 | 0.44 | -0.59 | 0.72 | -1.80 | -0.75 | -1.55 | -1.49 | -3.59 | -0.23 | 1786 |
| 1787 | -0.23 | 1.24 | 1.52 | -0.90 | -1.11 | -0.11 | -0.82 | -0.56 |  |  |  |  | 1787 |
| 1788 | 2.20 | -0.42 | -1.15 | 0.24 | 0.58 | 1.05 | 0.57 | -0.66 | 0.30 | 0.33 | -0.73 | -6.23 | 1788 |
| 1789 | -2.66 | 0.98 | -3.65 | -1.64 | 0.56 | -0.65 | -0.58 | -0.07 | -0.40 | -1.13 | -1.10 | 1.84 | 1789 |
| 1790 | 2.20 | 2.51 | 1.53 | -2.00 | 0.89 | -0.72 | -1.76 | -1.25 | -1.73 | -0.86 | -1.71 | 0.89 | 1790 |
| 1791 | 2.74 | 1.29 | 1.23 | 1.34 | -1.21 | -1.25 | -1.20 | -0.1. | -0.74 | -0.60 | -0.79 | -0.53 | 1791 |
| 1792 | 1.06 | -0.38 | 0.03 | 1.70 | -1.11 | -0.93 | -0.07 | 0.27 | -1.53 | -1.13 | -0.14 | 1.05 | 1792 |
| 1793 | 0.52 | 1.59 | 0.03 | -1.40 | -1.61 | -1.70 | 0.67 | -0.65 | -1.65 | 0.98 | -0.17 | 1.60 | 1793 |
| 1794 | -0.21 | 2.09 | 2.58 | 2.59 | -0.76 | -0.43 | 1.52 | -0.87 | -1.14 | -0.54 | 0.41 | -2.08 | 1794 |
| 1795 | -4.52 | -1.53 | -0.92 | 0.85 | -1.88 | -0.18 | -2.29 | -0.08 | 1.51 | 2.39 | 0.37 | 2.87 | 1795 |
| 1796 | 4.72 | 1.76 | -0.99 | 1.00 | -0.63 | -0.50 | -0.91 | 0.02 | 0.64 | -0.80 | -0.46 | -2.07 | 1796 |
| 1797 | 0.84 | 0.52 | -0.18 | 0.81 | 0.52 | -1.18 | 1.38 | 0.01 | -0.78 | -0.60 | 0.32 | 1.59 | 1797 |
| 1798 | 1.45 | 1.73 | 0.31 | 1.22 | 0.11 | 0.77 | -0.05 | 0.36 | 0.19 | 0.68 | -0.17 | -3.49 | 1798 |
| 1799 | -2.11 | -2.00 | -1.77 | -2.19 | -1.68 | -1.83 | -1.47 | -1.08 | -0.72 | -0.63 | 0.59 | -3.54 | 1799 |
| 1800 | -0.65 | -1.76 | -1.97 | 2.08 | 1.85 | -2.10 | $-1.32$ | 0.04 | 0.50 | 0.02 | 1.12 | -0.46 | 1800 |
| 1801 | 1.97 | -0.59 | 1.61 | 0.26 | 0.68 | -1.43 | -0.76 | 0.32 | 0.45 | 1.16 | 0.53 | 0.47 | 1801 |
| 1802 | -0.75 | 0.24 | 0.56 | 0.55 | -1.10 | -0.28 | -1.69 | 1.08 | 0.03 | 1.15 | 0.54 | 1.19 | 1802 |
| 1803 | -3.04 | -2.29 | 0.00 | 2.06 | -1.55 | -0.92 | 1.43 | 0.75 | -1.11 | 0.06 | 0.29 | 0.43 | 1803 |
| 1804 | 3.30 | 0.13 | -0.92 | -0.84 | 1.35 | 0.26 | 0.03 | -0.20 | 1.57 | 0.62 | -1.79 | -2.84 | 1804 |
| 1805 | -1.22 | -0.36 | -0.07 | -0.56 | -2.16 | -1.97 | -1.18 | 0.05 | 1.47 | -2.00 | -1.69 | 0.94 | 1805 |
| 1806 | 3.14 | 1.58 | 0.2. | -1.95 | 1.79 | -0.52 | 0.13 | 0.67 | 1.41 | 0.23 | 2.52 | 4.12 | 1806 |
| 1807 | 2.36 | 1.74 | -1.32 | -0.37 | 1.09 | $-0.17$ | 1.64 | 2.53 | $-1.40$ | 1.63 | $-0.15$ | 0.84 | 1807 |
| 1808 | 1.19 | 0.07 | -1.71 | -2.02 | 2.07 | $-0.46$ | 2.62 | 1.64 | 0.24 | -1.35 | $-0.05$ | -1.50 | 1808 |
| 1809 |  |  |  | -2.53 | 1.30 | -1.03 | -0.47 | 0.09 | -0.27 | -1.32 | $-0.99$ | 0.68 | 1809 |
| 1810 | -1.94 | -1.39 | -0.36 | -0.41 | -1.76 | $-0.96$ | 0.05 | $-0.07$ | 0.99 | -0.63 | -0.03 | 1.06 | 1810 |
| 1811 | -2.75 | 0.55 | 1.41 | 1.16 | 2.75 | 1.53 | 0.47 | -0.30 | -0.49 | 2.40 | 1.80 | 1.05 | 1811 |
| 1812 | 0.81 | 1.20 | -1.21 | -2.48 | 0.16 | -0.68 | -1.28 | -0.56 | -0.62 | 0.46 | -2.11 | $-4.00$ | 1812 |
| 1813 | -0.84 | 1.53 | 0.16 | 0.04 | 0.85 | -0.32 | -0.12 | -0.91 | -0.75 | -1.32 | -0.76 | -1.31 | 1813 |
| 1814 | -3.33 | $-4.20$ | -2.89 | 1.27 | -2.01 | -1.86 | 0.44 | -0.66 | -0.72 | -1.44 | -0.17 | 0.17 | 1814 |
| 1815 | -2.69 | 0.96 | 2.23 | 0.59 | 0.59 | $-0.03$ | -1.63 | -0.77 | $-0.54$ | 0.07 | -0.97 | $-1.90$ | 1815 |
| 1816 | 0.52 | -1.64 | -0.78 | -0.28 | -1.48 | -2.28 | -1.31 | -1.85 | -1.14 | -0.12 | -2.06 | -0.45 | 1816 |
| 1817 | 2.36 | 2.31 | 0.19 | -2.12 | -1.38 | 0.84 | $-0.83$ | -1.30 | 0.69 | -3.16 | 1.83 | -0.67 | 1817 |
| 1818 | 1.96 | -0.40 | 0.40 | -0.21 | -0.56 | 1.69 | 0.99 | -0.64 | -0.36 | -0.34 | 0.7 | -1.22 | 1818 |

The numbers without sign must be subtracted; those with the sign - must be added.

Holland. - Zwanenburg (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reanmur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | , |  | - | 0.81 | 091 | 0.50 |  |  | 0.55 | -0.79 | ${ }_{-1}{ }^{\circ} 18$ | - ${ }_{-2.18}$ |  |
| 1819 | 1.47 | 1.04 | 0.68 | 0.84 | 0.91 | 0.50 | 0.56 | 1.12 | 0.55 | -0.79 |  |  | 1819 |
| 1820 | -2.89 | -1.49 | -1.21 | 0.72 | 0.12 | -1.71 | -1.06 | -0.11 | -0.93 | -0.81 | -1.84 | -1.59 | 1820 |
| 1821 | -0.67 | -1.32 | -0.16 | 1.66 | -1.24 | -1.91 | -1.81 | -0.14 | 0.72 | 0.20 | 1.72 | 2.08 | 1821 |
| 1822 | 2.64 | 1.93 | 2.26 | 0.40 | 1.53 | 1.65 | 0.24 | -0.19 | -0.88 | 0.74 | 1.99 | -2.95 | 1822 |
| 1823 | -6.29 | -0.94 | 0.11 | -1.19 | 0.44 | -1.88 | -0.99 | 0.12 | -0.37 | -0.66 | 0.90 | 1.65 | 1823 |
| 1824 | 2.30 | 0.20 | -0.22 | -0.78 | -0.47 | -0.40 | -0.19 | 0.00 | 1.03 | 0.36 | 1.52 | 2.59 | 1824 |
| 1825 | 2.63 | 0.60 | $-1.42$ | 0.43 | 0.12 | 0.00 | -0.04 | -0.36 | 1.20 | 1.04 | 1.03 | 1.70 | 1825 |
| 1826 | -2.57 | 0.97 | 0.87 | 0.17 | -0.59 | 1.52 | 2.12 | 2.01 | 0.30 | 1.95 | 0.16 | 1.99 | 1826 |
| 1827 | -0.65 | -3.83 | 0.58 | 0.93 | 0.40 | -0.24 | 0.14 | -0.55 | -0.14 | 0.88 | -0.91 | 2.79 | 1827 |
| 1828 | 0.75 | -0.75 | 1.05 | 0.43 | 0.49 | 0.70 | 0.79 | -0.6. | 0.43 | 0.24 | -0.18 | 1.96 | 1828 |
| 1829 | -3.35 | -2.47 | -1.43 | -0.45 | 0.10 | $-0.37$ | -0.42 | -1.35 | -1.52 | -0.43 | -1.61 | -5.77 | 1829 |
| 1830 | -2.70 | -4.01 | 0.50 | 0.75 | 0.13 | -1.45 | 0.59 | -1.17 | -1.45 | 0.34 | 1.00 | -1.80 | 1830 |
| 1831 | -1.07 | 0.04 | 1.24 | 1.61 | -0.10 | -0.09 | 0.90 | 0.66 | -0.14 | 3.16 | 6 0.66 | 1.72 | 1831 |
| 1832 | -0.77 | -1.34 | -0.43 | 0.55 | -1.49 | -0.07 | -1.74 | -0.12 | -0.64 | 0.48 | -1.37 | 0.72 | 1832 |
| 1833 | -2.12 | 1.33 | -1.62 | -0.68 | 2.22 | 0.92 | -0.48 | -2.08 | -0.99 | 0.11 | 1 0.44 | 3.07 | 1833 |
| 1834 | 4.21 | 0.40 | 1.15 | -0.87 | 1.31 | 0.57 | 1.80 | 1.00 | 0.86 | 0.68 | $-0.31$ | 1.42 | 1834 |
| 1835 | 1.21 | 1.81 | 0.47 | -0.76 | -1.09 | 0.92 | 0.47 | 0.07 | -0.22 | -0.77 | -1.44 | -0.44 | 1835 |
| Means. | 0.99 | 3.14 | 3.86 | 6.50 | 10.12 | 12.45 | 13.97 | 14.13 | 12.30 | 8.61 | 1.84 | 2.16 | Means. |

## XCl. England. - London.

Degrees of Reaumur.

| 1794 | -0.96 | 2.72 | 1.23 | 1.64 | -0.99 | -0.43 | 1.53 | -0.38 | -1.35 | -0.61 | 0.36 | -1.10 | 1794 |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1795 | -5.04 | -2.08 | -1.26 | -0.23 | -0.46 | -1.98 | -0.04 | 0.11 | 1.76 | 1.61 | -0.88 | 2.46 | 1795 |
| 1796 | 4.42 | 0.50 | -1.00 | 1.10 | -1.26 | -1.00 | -1.28 | -0.51 | 1.23 | -1.45 | -0.97 | -3.76 | 1796 |
| 1797 | -0.01 | -1.44 | -1.51 | -0.45 | -0.70 | -1.56 | 0.62 | -0.82 | -0.97 | -1.34 | -0.44 | 0.93 | 1797 |
| 1798 | -3.44 | -0.28 | -0.12 | 1.41 | 0.44 | 1.31 | -0.10 | 0.88 | -0.11 | 0.09 | -1.24 | -2.39 | 1798 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1799 | -1.00 | -1.05 | -1.74 | -1.94 | -1.39 | -1.34 | -0.79 | -1.40 | -1.19 | -1.02 | 0.13 | -2.79 | 1799 |
| 1800 | 0.59 | -2.04 | -1.70 | 1.14 | 0.66 | -1.37 | 0.66 | 1.23 | 0.42 | -0.66 | -0.15 | -0.24 | 1800 |
| 1801 | 1.64 | -0.08 | 1.26 | -0.35 | -0.10 | -0.09 | -0.48 | 0.76 | 0.88 | 0.33 | -1.08 | -1.37 | 1801 |
| 1802 | -1.21 | 0.11 | -0.04 | 1.14 | -1.50 | -0.66 | -2.20 | 1.74 | 0.49 | 0.23 | -0.89 | -0.56 | 1802 |
| 1803 | -0.92 | -1.03 | 0.51 | 0.88 | -1.12 | -0.89 | 0.97 | 0.41 | -1.77 | -0.40 | -0.31 | 0.98 | 1803 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1804 | 3.39 | -0.73 | 0.00 | -0.95 | 1.80 | 1.07 | -0.57 | -0.20 | 1.16 | 0.66 | 0.68 | -1.52 | 1804 |
| 1805 | -0.52 | 0.04 | 0.34 | -0.20 | -1.38 | -1.49 | -0.89 | 0.60 | 1.15 | -1.06 | -1.17 | 0.08 | 1805 |
| 1806 | 2.27 | 1.27 | -0.23 | -1.21 | 1.00 | 0.64 | -0.06 | 0.38 | 0.16 | 0.54 | 2.11 | 3.64 | 1806 |
| 1807 | 0.64 | 0.54 | -1.80 | -0.14 | 1.05 | -0.34 | 1.07 | 1.36 | -1.61 | 1.44 | -1.60 | -1.19 | 1807 |
| 1805 | 0.64 | -1.01 | -1.80 | -1.43 | 1.99 | 0.02 | 1.87 | 0.82 | -0.55 | -1.76 | 0.58 | -1.32 | 1808 |
| 1809 | -0.11 | 2.36 | 0.6 .5 | -2.05 | 1.23 | -0.38 | -0.75 | -1.09 | -0.24 | -0.08 | -1.33 | 0.72 | 1809 |

The numbers without sign must be subtracted; those with the sign - must be added

England. - London (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | $\bigcirc$ | , | 0 | , | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 | 0 |  |
| 1810 | -0.47 | 0.01 | 0.38 | 0.12 | -1.44 | 0.20 | $-0.44$ | $-0.16$ | 1.32 | 0.95 | 0.32 | -0.03 | 1810 |
| 1811 | -1.09 | 0.85 | 1.54 | 1.64 | 2.03 | 0.51 | 0.36 | $-0.51$ | 0.83 | 2.50 | 1.29 | $-0.16$ | 1811 |
| 1812 | 0.42 | 1.43 | $-0.68$ | $-1.56$ | $-0.19$ | -1.09 | $-1.24$ | $-1.89$ | $-0.64$ | $-1.10$ | $-0.75$ | 0.90 | 1812 |
| 1813 | -0.51 | 1.34 | 0.87 | -0.81 | 0.12 | $-0.96$ | -0.97 | -1.00 | -0.99 | -1.05 | $-0.84$ | $-1.01$ | 1813 |
| 1814 | $-3.80$ | -2.21 | -2.55 | 1.06 | $-1.66$ | -2.03 | -0.04 | $-0.91$ | $-0.72$ | $-1.10$ | $-0.75$ | 0.90 | 1814 |
| 1815 | -1.49 | 1.34 | 1.94 | 0.44 | 1.19 | 0.24 | -0.53 | -0.07 | 2.48 | 0.55 | -1.42 | $-0.83$ | 1815 |
| 1816 | 0.64 | $-0.70$ | -0.64 | $-0.50$ | $-0.99$ | $-1.27$ | $-2.35$ | -1.18 | 0.96 | 0.28 | -1.24 | $-0.48$ | 1816 |
| 1517 | 1.84 | 2.05 | 0.25 | $-0.63$ | $-1.75$ | 0.77 | -1.46 | $-2.60$ | $-0.81$ | $-1.76$ | 2.14 | $-0.70$ | 1817 |
| 1818 | 1.67 | $-1.32$ | 0.03 | 0.04 | $-0.06$ | 2.24 | 2.40 | 1.98 | 2.30 | 2.06 | 3.20 | $-0.08$ | 1818 |
| 1819 | 2.29 | 0.85 | 1.36 | 1.37 | 0.88 | $-0.69$ | 0.36 | 1.58 | 0.70 | 3.08 | $-0.75$ | $-0.74$ | 1819 |
| 1820 | -1.44 | -0.66 | 0.25 | 1.68 | -0.01 | $-0.74$ | -0.71 | -1.18 | -0.99 | $-0.96$ | -0.22 | 0.59 | 1820 |
| 1821 | 1.04 | -0.97 | 0.87 | 2.08 | $-1.26$ | $-1.80$ | $-1.55$ | 0.47 | 1.28 | 0.32 | 2.32 | 2.32 | 1821 |
| 1822 | 2.16 | 2.19 | 2.78 | 0.48 | 1.45 | 1.57 | 0.36 | 0.29 | $-0.24$ | 1.04 | 2.36 | $-1.14$ | 1822 |
| 1823 | -1.40 | 0.19 | 0.16 | $-0.10$ | 2.16 | 0.33 | 0.14 | 0.78 | 0.39 | $-0.56$ | 0.54 | 0.55 | 1823 |
| 1824 | 0.78 | 2.41 | $-0.73$ | -0.94 | $-1.48$ | $-1.40$ | 0.00 | $-0.29$ | 0.48 | $-0.03$ | 1.38 | 1.08 | 1824 |
| 1825 | 1.31 | -0.21 | $-1.17$ | 1.28 | 0.08 | $-0.03$ | 1.47 | 0.38 | 1.63 | 0.32 | -0.84 | 0.59 | 1825 |
| 1826 | -1.49 | 1.61 |  | 1.46 | 1.16 | 1.97 | 1.69 | 1.67 | 0.30 | 1.28 | -1.11 | 1.19 | 1826 |
| 1827 | -0.96 | $-3.19$ | 0.74 | 0.39 | $-0.08$ | $-0.40$ | 0.74 | $-0.73$ | 0.21 | 0.84 | $-0.28$ | 1.99 | 1827 |
| 1828 | 1.73 | 0.54 | 1.00 | 0.28 | 0.70 | 0.88 | 0.36 | $-0.62$ | 0.52 | $-0.16$ | 0.65 | 2.37 | 1828 |
| 1829 | -1.76 | -0.24 | -1.08 | $-0.85$ | 0.50 | 0.35 | $-0.48$ | $-1.22$ | $-1.41$ | $-1.16$ | $-1.60$ | $-3.14$ | 1829 |
| 1830 | -2.31 | -2.17 | 1.98 | 1.15 | -1.39 | -1.09 | 0.65 | $-1.09$ | $-1.37$ | 0.32 | 0.63 | -2.12 | 1830 |
| 1831 | -0.73 | 1.01 | 1.16 | 1.21 | $-0.21$ | 0.55 | 1.49 | 1.29 | $-0.04$ | 2.39 | -0.08 | 1.21 | 1831 |
| 1832 | 0.13 | -0.56 | $-0.42$ | 0.35 | $-0.70$ | 0.57 | $-0.20$ | 0.18 | $-0.06$ | 0.52 | 0.47 | 1.08 | 1832 |
| 1833 | -0.64 | 1.45 | $-1.68$ | $-0.10$ | 2.72 | 0.66 | $-0.13$ | -1.31 | $-1.41$ | 0.24 | 0.16 | 2.21 | 1833 |
| 1834 | 3.73 | 0.48 | 1.16 | -0.48 | 1.59 | 1.20 | 1.29 | 0.76 | 0.70 | 0.10 | 0.45 | 0.35 | 1834 |
| 1835 | 0.82 | 0.81 | -0.22 | 0.30 | $-0.12$ | 0.71 | 0.87 | 1.09 | 0.21 | $-0.90$ | 0.05 | $-1.76$ | 1835 |
| 1836 | 0.80 | -0.99 | 0.94 | -1.12 | -1.28 | 0.48 | 0.18 | -1.11 | -1.50 | -1.14 | $-0.55$ | 0.28 | 1836 |
| 1837 | 0.73 | 0.74 | -2.22 | $-2.79$ | -2.01 | 0.04 | 0.05 | $-0.16$ | $-0.75$ | 0.21 | -0.57 | 1.17 | 1837 |
| 1838 | -2.93 | $-2.57$ | 0.18 | -1.50 | -0.88 | 0.02 | $-0.31$ | $-0.42$ | $-0.92$ | 0.10 | $-0.68$ | -0.03 | 1838 |
| 1839 | 0.73 | 0.14 | -1.08 | -2.48 | $-1.24$ | 0.66 | $-0.35$ | $-0.73$ | -1.06 | $-0.52$ | 0.67 | -0.21 | 1839 |
| 1840 | 1.27 | $-0.50$ | $-1.97$ | -0.01 | 0.14 | 1.02 | $-0.77$ | 0.73 | -1.10 | -1.32 | 0. | -2.41 | 1840 |
| 1841 | -0.38 | -1.41 | 2.58 | 0.61 | 2.08 | 2.17 | -1.02 | $-0.02$ | 0.16 | -0.01 | 0.40 | 1.06 | 1841 |
| 1842 | -1.02 | 0.81 | 1.47 | $-0.43$ | 0.59 | 2.84 | 0.18 | 2.11 | 0.19 | -1.70 | 0.36 | 62.50 | 1842 |
| Means. | 2.38 | 3.81 | 5.00 | 7.30 | 10.46 | 12.92 | 14.26 | 14.07 | 12.06 | 8.88 | 5.51 | 3.81 | Means |

The numbers without sign must be subtracted ; those with the sign - must be added.

## Scotland. - Kinfauns Castle.

For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  | $\bigcirc$ |  |
| 1814 | -4.71 | -1.63 | -1.73 | 0.56 | -2.46 | -2.36 | -0.60 | -1.12 | -0.34 | -1.16 | -1.61 | -1.46 | 1814 |
| 1815 | -1.69 | 1.13 | 0.16 | -0.03 | 0.95 | 0.24 | -0.12 | 0.23 | 0.27 | 0.74 | -1.68 | -2.47 | 1815 |
| 1816 | -0.24 | -1.60 | -1.49 | -1.58 | -0.74 | -0.60 | -0.96 | -0.53 | -0.99 | -0.24 | -1.12 | -1.84 | 1816 |
| 1817 | 1.60 | 1.29 | -0.44 | 0.33 | -1.12 | 0.50 | -0.43 | -1.11 | 0.18 | -2.22 | 1.78 | -1.38 | 1817 |
| 1818 | 0.51 | -1.03 | -1.41 | -1.59 | 1.03 | 1.43 | 0.85 | -0.22 | -0.15 | 2.34 | 2.54 | 0.25 | 1818 |
| 1819 | 0.85 | -0.88 | 0.67 | $-0.20$ | -0.36 | -0.85 | 0.07 | 2.00 | 0.30 | -0.32 | -2.35 | -2.60 | 1819 |
| 1820 | -2.43 | 0.95 | 0.33 | 1.10 | 0.20 | -0.12 | 0.39 | -0.26 | -0.36 | -1.20 | 0.15 | 0.36 | 1820 |
| 1821 | 0.55 | 0.97 | 0.26 | 1.12 | -1.09 | -0.45 | -0.01 | 0.84 | 1.44 | 0.83 | 0.38 | 0.73 | 1821 |
| 1822 | 1.85 | 1.25 | 1.08 | 0.79 | 0.97 | 2.04 | 0.50 | 0.26 | -0.81 | 0.48 | 1.38 | -0.61 | 1822 |
| 1823 | -0.91 | -1.69 | $-0.16$ | -0.60 | 0.63 | -1.01 | -0.92 | -0.55 | -0.15 | -0.56 | 2.02 | -0.04 | 1823 |
| 1824 | 2.64 | 1.29 | -0.56 | 0.39 | 0.18 | 0.26 | 0.43 | 0.03 | 0.24 | -2.16 | -0.16 | 0.35 | 1824 |
| 1825 | 1.94 | 0.84 | 0.45 | 0.82 | -0.09 | 0.31 | 1.59 | 1.53 | 1.85 | 1.79 | -0.32 | 0.80 | 1825 |
| 1827 | 0.68 | -0.77 | 0.02 | 0.73 | 0.51 | 0.38 | 0.16 | 0.37 | 1.48 | 2.48 | -0.99 | 2.23 | 1827 |
| 1828 | 2.50 | 1.44 | 1.63 | 0.69 | 1.20 | 1.23 | 0.93 | 1.03 | 1.23 | 1.10 | 2.05 | 2.73 | 1828 |
| 1829 | -0.38 | 0.96 | 0.42 | -0.48 | 0.87 | 1.00 | -0.12 | -0.44 | -1.02 | 0.34 | -0.19 | 0.02 | 1829 |
| 1830 | 0.40 | -0.22 | 2.07 | 0.97 | 0.60 | -0.63 | 0.50 | -1.13 | 0.11 | 1.33 | 0.92 | -0.89 | 1830 |
| 1832 | 1.91 | 1.27 | 0.92 | 1.22 | -0.19 | 0.50 | 0.24 | 0.93 | 1.35 | 1.53 | -0.56 | 0.40 | 1832 |
| 1833 | -1.40 | 0.51 | -0.41 | 0.32 | 2.79 | 0.59 | 0.67 | -0.98 | -0.24 | 0.53 | 0.12 | 0.57 | 1833 |
| 1834 | 2.23 | 0.97 | 1.05 | 0.51 | 1.01 | 0.53 | 0.93 | 0.34 | 0.28 | 0.49 | 0.14 | 0.57 | 1834 |
| 1835 | -0.27 | 0.72 | -0.08 | 0.23 | -0.58 | 0.20 | -0.17 | 1.09 | -0.10 | -1.10 | -0.31 | -0.34 | 1835 |
| 1836 | 0.59 | -0.67 | -0.70 | -0.81 | 0.10 | -0.54 | -1.16 | -1.09 | -1.67 | -0.86 | -0.94 | -0.05 | 1836 |
| 1837 | -0.07 | 0.20 | -2.26 | -2.35 | -1.70 | -0.05 | 0.52 | -1.13 | -1.32 | 0.23 | -1.18 | 1.74 | 1837 |
| 1838 | -2.58 | -4.61 | -0.83 | -1.44 | -1.75 | -1.03 | -0.04 | -0.24 | -0.53 | -0.55 | 2.73 | 0.48 | 1838 |
| 1839 | -0.90 | -0.79 | $-1.56$ | -1.24 | -1.18 | -0.45 | $-0.34$ | -0.79 | -0.64 | -0.17 | 0.11 | -0.35 | 1839 |
| 1840 | 0.65 | -0.26 | -0.07 | 1.00 | -0.72 | -0.40 | -1.30 | 0.21 | -1.29 | -0.63 | -0.17 | -0.58 | 1840 |
| 1841 | -2.19 | -0.09 | 2.25 | -0.25 | 0.51 | -1.07 | -0.83 | -0.20 | 0.51 | -1.52 | -1.94 | -0.49 | 1841 |
| 1842 | -1.17 | 0.49 | 0.35 | -0.07 | 0.48 | 0.02 | -0.83 | 1.24 | 0.32 | $-1.52$ | -0.81 | 1.81 | 1842 |
| Means. | 1.77 | 2.74 | 3.87 | 5.71 | 8.13 | 10.58 | 11.76 | 11.28 | 9.52 | 6.72 | 4.35 | 2.96 | Means. |

## XCIII. Finland. - Tornea.

| 1801 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1502 | -0.57 | -0.17 | -0.15 | 0.10 | -2.88 | -0.66 | -2.03 | -1.60 | -1.60 | 1.30 | -2.10 | -4.06 | 1801 |
| 1803 | -3.50 | -0.90 | -0.13 | 1.57 | 1.69 | -0.44 | -0.58 | 0.93 | -0.90 | 1.18 | 0.71 | -3.67 | 1803 |
| 1804 | -2.50 | -4.82 | -2.34 | 1.99 | 1.50 | -0.97 | 0.78 | -0.70 | -0.21 | 1.19 | 1.46 | -4.01 | 180.4 |
| 1805 | 3.36 | -2.94 | -1.15 | -0.79 | -1.56 | -2.90 | -1.03 | 0.62 | -1.34 | -4.62 | -2.83 | -2.98 | 1805 |
| 1806 | 2.91 | 1.91 | -0.03 | 2.02 | 1.00 | -1.18 | -1.90 | 2.00 | 1.20 | 0.13 | -0.97 | 0.74 | 1806 |
| 1807 | -3.40 | 1.94 | -1.25 | -2.57 | -1.93 | -0.61 | 0.34 | 0.89 | -1.41 | -2.30 | -0.20 | -0.92 | 1807 |
| 1808 | 1.80 | -1.50 | 0.19 | -2.31 | 1.14 | 2.65 | 0.53 | -0.11 | -0.51 | 3.53 | 2.24 | -3.74 | 1808 |
| 1809 | -7.19 | -3.99 | -2.74 | -3.78 | -1.91 | 0.62 | -0.50 | 1.16 | -0.34 | -0.25 | -1.67 | 8.07 | 1809 |
| 1810 | -2.18 | -2.36 | -2.41 | -2.45 | -6.45 | -0.68 | -2.13 | -0.68 | -1.34 | -1.23 | -4.13 | -2.20 | 1810 |
| 1811 | 2.98 | -2.74 | 3.64 | -2.04 | -0.69 | 0.42 | -0.91 | -2.66 | -1.05 | -1.90 | -0.10 | -2.06 | 1811 |
| 1812 | 1.18 | 1.85 | -3.37 | -1.39 | 0.55 | -2.94 | -2.53 | -1.20 | -2.85 | -0.78 | -4.18 | -1.15 | 1812 |
| 1813 | 1.32 | 1.15 | 1.70 | 1.88 | -0.71 | -1.58 | 1.87 | 0.08 | 1.58 | -2.89 | 3.65 | -1.43 | 1813 |

The numbers without sign must be subtracted; those with the sign - must be added.

Finland. - Tornea (continued).
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nor. | nec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1814 | $\stackrel{\bigcirc}{-7.01}$ | 2. | -1.85 | 0.92 | -0.59 |  | $\stackrel{\circ}{4.65}$ | 4.46 | $\stackrel{\circ}{2.60}$ | $0.44$ | ${ }_{-0.15}$ | $-4.50$ | 1814 |
| 1815 | 22 | 3.16 | 0.66 | .27 | 3.22 | 5.58 | 4.70 | 5.03 | 4.02 | 3.38 | 4.30 | 4.82 | 1815 |
| 1816 | 27 | -8.23 | -4.25 | 50 | -3.05 | -0.12 | 0.18 | -0.41 | 1.97 | 0.16 | 1.17 | 2.29 | 1816 |
| 1:17 | 3.54 | -2.13 | -2.78 | 0.19 | 2.42 | -1.14 | 0.65 | -1.34 | -0.36 | -1.14 | -0.07 | -2.8.5 | 1817 |
| ${ }_{1} 18$ | 3.46 | $-3.34$ | -1.07 | -2.61 | -3.48 | -0.92 | 2.98 | -2.55 | 0.09 | 1.08 | 2.89 | 5.83 | 1818 |
| 1819 | 4.47 | -0.15 | -0.50 | -2.07 | 23 | 1.46 | . 90 | 2.22 | 1.04 | -4.58 | -3.62 | -2.15 | 181 |
| 1820 | -5.74 | -0.22 | -0 | -1.32 | -0.73 | 1.62 | . 13 | -0.17 | 0.18 | -2.17 | -1.94 | -2.67 | 1820 |
| 1821 | -2.18 | 1.12 | 0.50 | 83 | 2 | -3.70 | -2.44 | -1.32 | -0.58 | . 58 | -1.52 | -4.13 | 1821 |
| 1822 | 0.13 | 6.44 | 5.68 | 4.22 | 1.67 | -1.39 | -0.89 | 1.75 | -0.14 | 0.47 | -2.05 | 4.46 | 1822 |
| 1823 | -4.01 | -1.08 | 15 | 0.66 | 0.87 | -0.43 | -0.09 | -0.73 | -0.86 | 2.06 | -1.38 | 1.26 | 1823 |
| 1824 | 0.71 | 4.20 | 1.75 | -0.22 | -0.40 | 0.29 | -0.89 | -0 | 5 | -2.18 | -1.01 | -0.96 | 1824 |
| 1825 | 3.99 | 12 | 1.83 | 78 | $-0.29$ | -0.43 | -1.53 | -0.17 | 6.34 | 2.14 | 2.35 | 3.2 | 1825 |
| 1826 | 1.99 | . 70 | 99 | 0.50 | 2.65 | 1.56 | 2.28 | 1.70 | -0.70 | 2.67 | 3.23 | 3.74 | 6 |
| 1827 | 0.03 | 0.00 | 0.59 | -2.13 | 2.39 | 79 | -2.00 | -1.64 | 1.21 | -1.53 | -0.56 | 5.68 | 1827 |
| 1828 | -0.50 | -0.84 | -1.77 | -0.66 | 2.84 | 0.18 | -1.73 | -0.73 | -2.86 | 1.1 | 0.50 | 1.69 | 1828 |
| 1829 | 1.26 | -4.27 | -2.69 | -2.53 | 1.26 | -0.31 | 0.30 | -1.82 | 38 | -1.78 | -0.33 | 2.86 | 1829 |
| 1830 | 0.99 | 0.80 | 2.08 | $-0.54$ | -1.10 | $-0.66$ | -0.89 | -1.73 | -0.88 | -0.03 | 3.44 | -1.22 | 1830 |
| 1831 | -3.98 | -0.07 | -2.31 | 2.01 | 0.98 | 1.98 | 0.81 | 0.79 | -0.54 | 0.01 | 2.99 |  | 1831 |
| 1832 | 5.26 | 8.25 | 3.64 | 2.92 | 0.10 | 0.51 | -1.11 | -1.22 | -3.67 | 2.86 |  |  | 1832 |
| Means. | -12.5 | -10.76 | -7.19 | -1.62 | 4.01 | 10.59 | 13.05 | 10.81 | 6.22 | 0.26 | -6.27 | -10.32 | Means. |

XCIV. North America. - Albany, N. Y.

Degrees of Reaumur.

| 1826 | 1.92 | 2.44 | 1.65 | -1.02 | 3.23 | 1.07 | 0.72 | 1.09 | 1.57 | 1.46 | 0.81 | 0.35 | 1826 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1827 | -2.91 | 1.07 | 1.15 | 1.62 | -0.02 | 0.05 | 0.55 | 0.08 | 0.43 | 1.14 | -1.72 | 0.77 | 1827 |
| 1828 | 2.80 | 4.52 | $2.10-$ | -0.83 | 0.76 | 2.66 | -0.41 | 1.33 | 0.35 | -0.31 | 0.76 | 3.17 | 1828 |
| 1829 | -0.21 | -2.27 | -0.87 | 0.12 | 2.09 | 0.03 | -1.54 | -0.42 | -1.93 | 0.92 | 0.50 | 3.63 | 1829 |
| 1830 | 0.28 | -0.11 | 1.41 | 3.64 | $-0.21$ | -0.92 | 0.81 | 0.27 | 0.19 | 1.42 | 3.83 | 4.71 | 1830 |
| 1831 | -1.3 | -1 | 2.77 | 1.89 | 1.07 | 2.11 | 0.32 | 1.01 | 1.00 | 1.52 | 0.63 | $-4.94$ | 1831 |
| 1832 | 0.18 | -0.57 | 0.16 | -1.29 - | -1.35 | 0.19 | -0.31 | -0.31 | 0.53 | 0.67 | 1.15 | 0.76 | 1832 |
| 1833 | 2.34- | -1.34- | -1.15 | 1.75 | 1.53 | -2.35 | -1.06 | -1.47 | -0.55 | -0.55 | -0.61 | 0.18 | 1833 |
| 1834 | -1.18 | 3.73 | 0.67 | 0.65 | -0 05 | -1.12 | 1.59 | -0.03 | 0.27 | -1.31 | -0.36 | -1.13 | 1834 |
| 1835 | -1.06 | -1.50 | -0.98- | -1.59 - | $-0.57$ | -0.34 | -0.43 | -0.90 | -2.14 | 1.45 | 0.31 | $-3.06$ | 1835 |
| 1836 | -0.35 | -3.59 | -3.18 - | -2.27 | -0.95 | -1.30 | 0.20 | -2.39 | -0.39 | -3.06 | -0.62 | $-0.92$ | 1836 |
| 1837 | -3.40 | -0.72 | -1.94 | -2.02 | -1.23 | 0.07 | -0.95 | -0.9> | -0.60 | -0.89 | 0.33 | -0.49 | 1837 |
| 1838 | 3.34 | $-4.01$ | 0.97 - | -3.07 | -1.26 | 1.78 | 0.31 | 0.27 | 0.36 | -0.68 | -1.47 | -2.11 | 1838 |
| 1839 | -0.2. | 1.62 | 0.14 | 0.79 | -0.79 | -1.79 | 0.15 | -0.14 | 0.41 | 0.99 | -0.94 | -0.19 | 1839 |
| 1840 | -3.32 | 3.14 | 0.60 | 1.32 | 0.96 | -0.14 | 0.94 | 0.81 | -0.91 | 0.28 | 0.28 | -1.26 | 1840 |
| 1841 | 1.95 | -0.72 | -1.19- | -2.58 | -1.13 | 1.90 | 0. | 1.23 | 0.88 | -1.72 | -0.49 | 0.86 | 1841 |
| 1842 | 2.03 | 3.15 | 2.06 | 0.62 | -1.96 | -0.95 | 0.28 | 0.13 | -1.09 | -0.12 | $-1.00$ | -1.69 | 1842 |
| 1843 | 2.65 | -3.06 | -4.26- | -0.62 | -0.62 | -0.64 | -0.55 | 0.64 | 0.85 | -1.24 | -1.11 | 0.93 | 1843 |
| 1844 | -3.74 | -0.15 | 0.27 | 2.97 | 0.47 | $-0.29$ | -0.60 | -0.19 | 0.72 | 0.02 | -0.20 | 0.17 | 1844 |
| Means. | -3.58 | -3.08 | 1.28 | 7.04 | 12.33 | 16.02 | 17.80 | 16.96 | 13.06 | 7.64 | 2.70 | $\mid-165$ | Means |

The numbers without sign must be subtracted; those with the sign - must be added.

North America. - Salem, Mass.
For Reducing the Monthly and Yearly Means of Single Years to the Means derivad from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1787 | $0.40$ | $-1.37$ | 0.2 | $-0.24$ | $\stackrel{0}{-0.61}$ | $-0.84$ | $\begin{gathered} 0 \\ -1.53 \end{gathered}$ | $-0.28$ | $-1.13$ | $-1.00$ | $\begin{aligned} & 0 \\ & 0.58 \end{aligned}$ | $\begin{aligned} & \circ \\ & 0.07 \end{aligned}$ | 1757 |
| 1787 | -1.38 |  |  | -0.24 |  | -0.84 -1.39 | -1.5 .3 0.14 | -0.2.17 | -1.13 | -1.00 -1.00 | 0.58 2.03 | 0.07 -1.60 | 1787 |
| 1788 1789 | -1.88 |  |  | $-0.47$ | $-1.94$ | -1.89 | -0. | -0.17 0.05 | -0.87 | -1.00 | 2.03 | -1.60 1.18 | 1788 |
|  | 17 | , |  | -0.47 | $-1.94$ | 0.61 | -0. | 0.05 | -0.47 | -2. | 0.47 | 1.15 | 789 |
| 1790 | 1.17 | $-1.04$ | $-1.32$ | -1.47 | -0.50 | -0.50 | -0.75 | $-1.50$ | -1.02 | -0.56 | -0.97 | -2.82 | 1790 |
| 1791 | 0.17 | -1.48 | 0.90 | 0.64 | 1.50 | 1.16 | -0.08 | 0.16 | $-0.69$ | -2.23 | $-0.42$ | 0.07 | 1791 |
| 1792 | -2.94 | -0.37 | 1.79 | 0.87 | 1.61 | $-0.84$ | -0.64 | -0.28 | $-1.80$ | 0.77 | 0.92 | $-1.15$ | 1792 |
| 1793 | 1.03 | 0.70 | 1.42 | 1.51 | 2.55 | 2.07 | 0.59 | 0.75 | 0.37 | -0.09 | 0.07 | $-0.10$ | 1793 |
| 1794 | 0.95 | -0.25 | 1.91 | 1.19 | 1.16 | 0.11 | 0.52 | 0.58 | 0.75 | -1.26 | $-0.16$ | 4.35 | 1794 |
| 1795 | 0.20 | -0.50 | 0.54 | 0.21 | 0.39 | 0.12 | -0.31 | 1.85 | 1.04 | 1.24 | 0.36 | 1.51 | 1795 |
| 1796 | 1.18 | 0.12 | $-0.37$ | 1.1 | -0.11 | 0.40 | 0.39 | 0.80 | $-0.06$ | $-0.55$ | -1.26 | $-3.02$ | 1796 |
| 1797 | -1.15 | 2.24 | 0.55 | -0.26 | -1.2. | 0.41 | 1.40 | -0.45 | -0.64 | $-0.83$ | -1.72 | -2.52 | 1797 |
| 1798 | 0.68 | -0.89 | 0.54 | 0.76 | 1.4 | 0.60 | 0.46 | 2.29 | 0.53 | 0.81 | -1.57 | $-3.03$ | 1798 |
| 1799 | 0.28 | 0.08 | 0.31 | 0.51 | 0.6 | 0.58 | 0.15 | 0.99 | 0.27 | -0.16 | -0.53 | $-0.53$ | 1799 |
| 1800 | 0.31 | 0.24 | $-0.31$ | 1.92 | $-0.12$ | 1.22 | 1.15 | 0.11 | 0.04 | 0.43 | $-0.93$ | 1.63 | 1800 |
| 1801 | 0.40 | 0.46 | 1.51 | 0.21 | 1.69 | 0.08 | 0.35 | 0.49 | 1.41 | 0.96 | 0.17 | 0.30 | 1801 |
| 1802 | 3.79 | $-0.16$ | 0.76 | 0.31 | -1.34 | 0.13 | 0.13 | 0.85 | 1.19 | 1.87 | 1.23 | 1.19 | 1802 |
| 1803 | 1.12 | 2.15 | 0.67 | 0.38 | $-0.81$ | 0.53 | -0.03 | 1.09 | $-0.24$ | 0.96 | $-0.71$ | 1.99 | 1803 |
| 1804 | -0.48 | 0.08 | -0.48 | $-0.98$ | 1.55 | 0.20 | $-0.25$ | -0.44 | 0.28 | -1.05 | 0.16 | -1.76 | 1804 |
| 180.5 | -1.46 | 1.02 | 1.92 | 1.45 | 0.91 | 0.11 | 1.40 | 052 | 1.23 | -0.82 | 0.13 | 3.24 | 1805 |
| 1806 | 0.48 | 1.60 | -1.83 | -2.28 | $-0.44$ | $-0.19$ | $-1.12$ | $-0.77$ | $-0.52$ | $-0.04$ | 0.15 | $-0.06$ | 1806 |
| 1807 | -1.0.5 | -1.13 | -1.30 | -0.31 | -0.80 | $-0.62$ | 0.05 | 0.00 | -1.08 | 0.22 | -0.65 | 2.45 | 1807 |
| 1508 | 0.13 | 1.41 | 1.55 | 0.37 | -0.74 | 0.04 | $-0.15$ | $-0.86$ | 0.54 | $-0.72$ | 0.69 | 0.72 | 1808 |
| 1809 | -1.15 | $-1.73$ | -1.36 | 0.31 | -0.24 | $-0.42$ | -1.90 | $-0.76$ | -0.95 | 3.00 | -2.19 | 2.04 | 1809 |
| 1510 | 0.11 | 0.9 .5 | $-0.68$ | 0.70 | 0.84 | 0.04 | -0.93 | -0.39 | 0.46 | -0.12 | -0.24 | -0.34 | 1810 |
| 1511 | 0.30 | 0.11 | 1.69 | $-0.01$ | 0.65 | 0.43 | 0.16 | 0.14 | 0.58 | 1.74 | 0.67 | -0.34 | 1811 |
| 1812 | $-1.51$ | -1 | -2.68 | -1.05 | -3.22 | $-2.04$ | $-2.13$ | -1.64 | $-2.07$ | $-0.30$ | $-0.90$ | $-0.73$ | 1812 |
| 1813 | -1.09 | $-0.34$ | $-2.55$ | 0.03 | $-1.46$ | -0.95 | -1.17 | 0.44 | 1.02 | $-0.62$ | 0.83 | -0.70 | 1813 |
| 1814 | -0.73 | 0.80 | $-0.51$ | 1.08 | 0.76 | $-1.58$ | -0.30 | -0.94 | -0.57 | $-0.07$ | 0.39 | $-1.78$ | 1814 |
| 1815 | -0.93 | $-1.98$ | 0.2 | -1.47 | -1.49 | $-0.16$ | 1.12 | $-1.82$ | $-0.50$ | -0.69 | 1.07 | -0.45 | 1815 |
| 1816 | -0.16 | 0.07 | $-2.14$ | -0.44 | -1.36 | -2.36 | $-2.49$ | -1.31 | $-1.77$ | 0.17 | 1.79 | 0.31 | 1816 |
| 1817 | -0.71 | -3.48 | $-1.43$ | -0.73 | -0.44 | -1.65 | -0.52 | -0.76 | 0.18 | $-0.70$ | 0.78 | 0.68 | 1817 |
| 1818 | -0.51 | $-3.56$ | 0.14 | -2.31 | $-0.42$ | 1.17 | 0.85 | -0.01 | -0.84 | 0.61 | 1.92 | -1.94 | 1818 |
| 1819 | 2.45 | 4.91 | $-2.30$ | -1.06 | $-0.23$ | 1.33 | 0.64 | 0.59 | 1.63 | 0.64 | 1.26 | $-0.43$ | 1819 |
| 1820 | -1.5] | 1.00 | $-0.22$ | -0.07 | $-0.93$ | 0.51 | 1.95 | 0.26 | 1.52 | $-0.17$ | -0.98 | $-2.49$ | 1820 |
| 1821 | $-2.75$ | 1.50 | -0.80 | -0.97 | -0.37 | 0.36 | -1.05 | 0.83 | -0.11 | $-0.05$ | 0.42 | -1.31 | 1821 |
| 1822 | -1.60 | $-0.50$ | 1.64 | -0.87 | 1.77 | 0.09 | 0.44 | 0.06 | 1.54 | 0.75 | 0.96 | 0.12 | 1822 |
| 1823 | 0.37 | $-1.99$ | $-0.99$ | 0.20 | -1.19 | $-0.42$ | $-0.19$ | 0.35 | $-1.63$ | $-0.58$ | -1.72 | 0.52 | 1823 |
| 1824 | 2.28 | 0.47 | -0.11 | 0.62 | -0.84 | $-0.59$ | $-0.14$ | -1.08 | 0.12 | 0.21 | -0.61 | 1.43 | 1824 |
| 1825 | 1.30 | 1.27 | 2.16 | 1.49 | 0.69 | 1.74 | 2.36 | -0.12 | $-1.05$ | 0.70 | $-0.14$ | 0.62 | 1825 |
| 1826 | 0.96 | 1.11 | 0.10 | $-1.05$ | 2.95 | 0.04 | 1.56 | $-0.13$ | 0.75 | 0.23 | 0.19 | 0.55 | 1826 |
| 1827 | $-1.49$ | 0.52 | 0.64 | 1.56 | -0.03 | -0.60 | $-0.35$ | $-0.82$ | -0.28 | 1.13 | -2.74 | 0.01 | 1827 |
| 1828 | 2.42 | 4.05 | 1.10 | $-0.97$ | -0.68 | 1.06 | 0.36 | 0.96 | 0.37 | $-0.19$ | 1.17 | 2.04 | 1828 |
| Means. | -2.8 | -1.85 | 1.54 | 6.36 | 11.0.5 | 15.61 | 17.97 | 17.17 | 13.80 | 8.56 | 3.53 | $-0.63$ | Means |

The numbers without sign must be subtracted; those with the sign - must be added.
XCVI.

Iceland. - Reikiavik.
For Reducing the Monthly and Yearly Means of Single Years to the Means derived from Series of Years.

Degrees of Reaumur.

| Year. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\bigcirc$ | - |  | - | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - |  |
| 1823 | 1.80 | $-0.56$ | 0.10 | 2.09 | $-0.60$ | 0.06 | 2.44 | 1.76 | 0.84 | $-1.50$ | 0.18 | $-0.86$ | 1823 |
| 1824 | -0.32 | 0.61 | $-0.05$ | 2.16 | 2.95 | 4.63 | 3.12 | 1.53 | $-0.73$ | $-2.37$ | -3.64 | $-3.99$ | 1824 |
| . 825 | -1.07 | $-0.40$ | 3.04 | 0.98 | 0.50 | 0.33 | 1.70 | 0.66 | 2.34 | 1.68 | -0.81 | $-0.92$ | 1825 |
| 1826 | $-0.19$ | 2.84 | 2.15 | $-0.79$ | 1.58 | $-1.10$ | $-0.75$ | $-0.18$ | 1.24 | 1.12 | 0.36 | 1.17 | 1826 |
| 1827 | $-0.72$ | 1.93 | $-3.80$ | -0.86 | 0.67 | 0.86 | 0.14 | 1.73 | 0.64 | 2.29 | 2.26 | 0.88 | 1827 |
| 1828 | 1.98 | 2.48 | 1.54 | 1.29 | 2.37 | 0.53 | 3.15 | 3.98 | 3.07 | 3.26 | 0.94 | 2.77 | 1828 |
| 1829 | 1.02 | $-0.09$ | 0.20 | 0.56 | 0.79 | 0.26 | 1.21 | 2.21 | $-0.20$ | -1.16 | 0.03 | 1.86 | 1829 |
| 1830 | 1.59 | $-0.58$ | $-1.22$ | $-0.72$ | 2.44 | 0.52 | $-0.80$ | 0.68 | 0.85 | 2.09 | $-0.35$ | $-2.60$ | 1830 |
| 1831 | 0.28 | $-0.95$ | 2.58 | 1.39 | $-1.76$ | 1.44 | -1.89 | $-1.85$ | $-0.37$ | 0.95 | $-0.76$ | 1.45 | 1831 |
| 1832 | 0.71 | $-0.48$ | $-1.77$ | 0.17 | $-2.20$ | $-1.87$ | $-2.80$ | $-2.94$ | $-2.59$ | $-0.12$ | 1.22 | $-0.29$ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 1832 |
| 1833 | 1.41 | -0.13 | 1.93 | -0.21 | $-0.57$ | $-0.40$ | -1.96 | $-2.14$ | $-1.22$ | $-0.79$ | 0.31 | -1.64 | 1833 |
| 1834 | -0.43 | 0.10 | 0.73 | 0.14 | $-1.35$ | $-1.99$ | $-1.81$ | $-2.41$ | -1.44 | $-1.13$ | 0.22 | 2.76 | 1834 |
| 1835 | $-4.08$ | -1.92 | -1.55 | -1.32 | $-2.35$ | $-1.97$ | $-1.62$ | $-0.38$ | $-0.64$ | $-2.41$ | 1.55 | 1.30 | 1835 |
| 1836 | -1.56 | $-3.24$ | $-2.00$ | $-3.01$ | $-0.37$ | $-0.94$ | $-0.59$ | $-2.6 \mathrm{~S}$ | $-1.80$ | $-1.67$ | -1.52 | $-1.95$ | 1836 |
| 1837 | $-0.42$ | 0.43 | -2.23 | -1.91 | $-2.07$ | $-0.32$ | 0.40 |  |  |  |  |  | 1837 |
| Means. | -1.00 | -1.60 | -1.07 | 1.84 | 5.54 | 8.67 | 10.78 | 9.27 | 6.42 | 2.19 | -0.60 | -1.15 | Means. |

## XCVII. Greenland. - Godthaab.

Degrees of Reaumur.

| 1796 |  |  |  |  |  |  |  | -• | . . | -2.52\| | 1.51 | 2.19 | 1796 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1797 | 0.91 | -2.08 | -0.73 | -1.96 | 1.14 | 0.27 | 1.40 | 1.31 | 0.77 | 1.02 | 2.22 | 0.87 | 1797 |
| 1798 | -1.30 | 0.53 | 3.98 | 0.08 | 0.37 | -0.39 | 0.39 | 0.07 | -0.37 | -0.67 | 0.83 | -0.08 | 1798 |
| 1799 | -0.40 | 3.08 | -1.87 | 0.47 | 0.37 | -0.71 | -0.47 | -0.72 | 0.62 | -0.43 | -0.91 | 4.72 | 1799 |
| 1800 | 2.75 | 0.22 | 2.32 | -0.68 | 1.52 | 1.05 | 0.35 | 0.88 | -0.42 | 0.48 | 0.05 | 0.07 | 1800 |
| 1801 | -0.86 | 2.63 | 0.00 | -1.00 | -2.86 | -1.61 | 0.89 | 0.92 | -0.39 | 0.19 | 0.22 | 1.94 | 1801 |
| 1802 | 1.85 | -2.99 | -3.76 | -2.68 | -0.44 |  | . . |  |  |  |  |  | 1802 |
| 1816 |  |  |  |  |  |  | 0.09 | -0.98 | -0.12 | -0.15 | -0.01 | -6.91 | 1816 |
| 1817 | -1.55 | -2.46 | -4.17 | 0.37 | -1.32 | -0.79 | -1.63 | -0.28 | -0.41 | -1.65 | -0.52 | -1.73 | 1817 |
| 1818 | -5.58 | $-5.13$ | $-4.00$ | 2.56 | -0.90 | -0.84 | 0.52 | 0.15 | -0.71 | -1.97 | -1.82 | -0.42 | 1818 |
| 1819 | -2.74 | , | -0.35 | 0.98 | -0.91 | $-0.97$ | -3.78 | -2.29 | -2.30 | 1.78 | 1.38 | 3.15 | 1819 |
| 1820 | 4.16 | 0.14 | 0.35 | -2.15 | 0.97 | 0.66 | -0.96 | -1.57 | -0.72 | -0.06 | 1.60 | 1.19 | 1820 |
| 1821 | 0.04 | 0.42 | 1.30 | 1.00 | -0.07 | 0.63 |  |  |  |  |  |  | 182\% |
| 1841 |  |  |  |  |  |  |  |  | 0.45 | 0.14 | -0.27 | 0.23 | 1841 |
| 1842 | 1.13 | -1.15 | -1.12 | 1.56 | 2.03 | 0.37 | 0.89 | 0.34 | 1.39 | 1.95 | -0.37 | -1.37 | 1842 |
| 1843 | 0.11 | 4.74 | 4.65 | 2.18 | 1.18 | 1.16 | 1.52 | 0.72 | 1.57 | 1.66 | -2.89 | -3.93 | 1843 |
| 1844 | -0.13 | 0.40 | -0.51 | -3.10 | -1.29 | 0.79 | 0.78 | 1.39 | 0.66 | 0.19 | -1.08 | 0.01 | 1844 |
| 1845 | 1.54 | 0.76 | 3.98 | 2.34 | 0.24 | 0.32 |  |  |  |  |  |  | 1845 |
| Means. | -8.72 | 8.64 | -7.29 | -4.44 | 0.07 | 3.15 | 4.41 | 3.93 | 1.62 | -0.96 | -4.47 | -6.45 | Means. |

The numbers without sign must be subtracted; those with the sign - must be added.

## CORRECTIONS

FOR

# FORCE OF VAPOR AND RELATIVE HUMIDITY. 

HOURLY CORRECTIONS FOR PERIODIC VARLATIONS,
or

TABLES

FOR REDUCING THE MEANS OF THE OBSERVATIONS TAKEN AT ANY HOUR OF THE DAY TO THE TRUE MEAN FORCE OF VAPOR AND RELATIVE HUMIDITY OF THE DAY, OF THE MONTH, AND OF THE YEAR.

England.-Greenwich. Lat. $51^{\circ} 29^{\prime} \mathrm{N} . ;$ Long. $0^{\circ} 0^{\prime}$.
Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours, to obtain the true Mean Force of Vapor for the respective Months. (Glaisher.)

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inc | In |  |  | Inch. |  |  | Inch. |  |  |  | Inch. | Inch. |
| Midn. . | . 006 | . 006 | . 008 | . 017 | . 026 | . 031 | . 028 | . 025 | . 024 | . 018 | . 010 | . 009 | . 017 |
| 1 | . 011 | . 008 | . 010 | . 021 | . 028 | . 037 | . 031 | . 031 | . 030 | . 020 | . 012 | . 010 | . 021 |
| 2 | . 015 | . 010 | . 011 | . 024 | . 031 | . 043 | . 036 | . 035 | . 035 | . 021 | . 015 | . 010 | . 024 |
| 3 | . 015 | . 011 | . 013 | . 027 | . 032 | . 0.48 | . 038 | . 039 | . 037 | . 023 | . 017 | . 011 | . 026 |
| 4 | . 015 | . 013 | . 015 | . 029 | .031 | . 047 | . 037 | . 040 | . 040 | . 025 | . 019 | . 011 | . 027 |
| 5 | . 015 | . 014 | . 016 | . 029 | . 027 | . 037 | . 031 | . 038 | . 040 | . 023 | . 021 | . 011 | . 025 |
| 6 | . 014 | . 015 | . 016 | . 025 | . 019 | . 022 | . 019 | . 029 | . 033 | . 021 | . 021 | . 010 | . 020 |
| 7 | . 013 | . 014 | . 014 | . 016 | . 007 | . 008 | . 007 | . 014 | . 022 | . 018 | . 018 | . 009 | . 013 |
| 8 | . 010 | . 010 | . 010 | . 005 | -. 005 | -. 004 | $-.004$ | . 000 | . 010 | . 011 | . 012 | . 007 | . 005 |
| 9 | . 007 | . 006 | . 005 | . 005 | -. 016 | -. 015 | -. 014 | -. 012 | -. 005 | . 005 | . 005 | . 005 | -. 002 |
| 10 | . 002 | . 000 | -. 003 | -. 013 | -.024 | -. 027 | -. 019 | -. 021 | -. 019 | -. 005 | -. 004 | . 001 | -. 010 |
| 11 | -. 004 | -. 005 | -. 007 | $-.020$ | -. 028 | -. 036 | -.025 | -. 027 | -. 027 | -. 009 | -. 010 | -. 004 | -. 017 |
| Noon. | -. 00 | -. 0 | -. 012 | -. 026 | -. 030 | -. 042 | -. 029 | -. 030 | -. 030 | -. 015 | -. 017 | -. 007 | -. 021 |
| 1 | -. 008 | -.013 | -. 013 | -. 027 | -. 030 | -. 045 | -. 033 | -. 032 | -. 030 | -. 018 | -. 019 | -. 008 | $-.023$ |
| 2 | -. 007 | -. 015 | -. 013 | -. 027 | -.028 | -. 043 | -.034 | -. 034 | -. 029 | -. 017 | -. 020 | -. 008 | $-.023$ |
| 3 | . 007 | . 012 | -. 012 | -. 025 | -. 026 | -. 039 | -. 033 | -. 031 | -. 027 | -.014 | -. 016 | -. 008 | -. 021 |
| 4 | -. 007 | . 010 | -. 010 | $-.020$ | -. 021 | -. 035 | -. 028 | -. 027 | -. 021 | $-.009$ | $-.010$ | -. 007 | -. 017 |
| 5 | -. 004 | -. 006 | -. 006 | -.014 | -. 015 | -. 025 | -. 021 | -. 020 | -. 017 | -.006 | -. 005 | -. 005 | -. 012 |
| 6 | -. 002 | -. 004 | -. 002 | -. 006 | -. 010 | -. 017 | -. 016 | -. 015 | -. 010 | -.004 | . 000 | -. 003 | -. 007 |
| 7 | -. 001 | -.001 | . 002 | . 001 | $-.004$ | -. 007 | -. 007 | -.006 | -. 003 | . 003 | . 004 | $-.001$ | -. 002 |
| 8 | . 000 | . 001 | . 004 | . 005 | . 005 | . 005 | . 004 | . 004 | . 004 | . 005 | . 006 | . 001 | . 004 |
| 9 | . 000 | . 003 | . 005 | . 007 | . 013 | . 015 | . 010 | . 010 | . 008 | . 008 | . 008 | . 004 | . 007 |
| 10 | . 001 | . 004 | . 007 | . 010 | . 017 | . 023 | . 017 | . 015 | . 013 | . 011 | . 009 | . 005 | . 011 |
| 11 | . 002 | . 005 | . 008 | . 014 | . 022 | . 029 | . 024 | . 020 | . 018 | . 014 | . 010 | . 006 | . 014 |
| 6. 6 | . 006 | . 005 | . 007 | . 009 | . 005 | . 003 | . 001 | . 007 | . 012 | . 008 | . 010 | . 004 | . 006 |
| 7. 7 | . 006 | . 006 | . 008 | . 009 | . 001 | . 000 | . 000 | . 004 | . 009 | . 011 | . 011 | . 00.4 | . 005 |
| 8. 8 | . 005 | . 005 | . 007 | . 005 | . 000 | . 000 | . 000 | . 002 | .007 | . 008 | . 009 | . 004 | . 005 |
| 9. 9 | . 003 | . 004 | . 005 | . 006 | -. 002 | . 000 | -. 002 | -. 001 | . 002 | . 006 | . 007 | . 004 | . 003 |
| 10.10 | . 001 | . 002 | . 002 | -. 002 | -. 003 | -. 002 | -. 001 | -. 003 | -. 003 | . 003 | . 002 | . 003 | . 000 |
| 7. 2. 9 | . 002 | . 001 | . 002 | -. 001 | $-.003$ | $-.007$ | $-.006$ | $-.003$ | . 000 | . 003 | . 002 | . 002 | $-.001$ |
| 6.2. 8 | . 002 | . 000 | . 002 | . 001 | -. 001 | $-.005$ | $-.004$ | -. 000 | . 003 | . 003 | . 002 | . 001 | . 000 |
| 6. 2.10 | . 003 | . 001 | . 003 | . 003 | . 002 | . 001 | . 001 | . 003 | . 006 | . 005 | . 003 | . 002 | . 003 |
| 6. 2.6 | . 002 | -. 001 | . 000 | $-.003$ | $-.006$ | $-.013$ | -. 010 | -. 007 | -. 002 | . 000 | . 000 | $-.000$ | $-.065$ |
| 7. 2 | . 003 | -. 000 | . 000 | -. 005 | -. 011 | -. 017 | -. 014 | -. 010 | -. 003 | . 000 | -. 001 | . 000 | -. 005 |
| 8. 2 | . 001 | -. 002 | -. 001 | -. 011 | -. 017 | -. 023 | -. 019 | -. 017 | -. 009 | -. 003 | $-.004$ | $-.000$ | $-.009$ |
| 8. 1 | . 001 | -. 001 | -. 001 | -. 011 | -. 017 | -. 025 | -. 018 | -. 016 | -. 010 | -. 004 | -.004 | -. 000 | -. 009 |
| 7. 1 | . 002 | . 001 | . 000 | -. 005 | -. 012 | -. 018 | -. 013 | -. 009 | -. 004 | $-.000$ | $-.000$ | . 000 | $-.005$ |
| 9.12.3.9 | -. 002 | $-.003$ | -. 003 | -. 010 | -. 015 | -.020 | -. 016 | -. 016 | -. 013 | -. 004 | -. 005 | -. 001 | -. 009 |

The numbers without sign must be added; those with the sign - must be subtracted.

England.-Greenwich. Lat. $51^{\circ} 29^{\prime}$ N.; Long. $0^{\circ} 0^{\prime}$.
Corrections to be applied to the Means of the Hours of Observation, or Sets of Hours to obtain the true Mean Humidity for the respective Months. (Glaisher.)

Thousandths.

| Hours. | Jan. | Feb. | March. | April. | May. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Mean. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Midn. | -. 013 | -. 021 | -. 063 | -. 095 | -.087 | -. 105 | -. 091 | $-.096$ | -. 080 | -. 053 | -. 018 | -. 011 | -. 061 |
| 1 | . 002 | -. 021 | -. 065 | -. 106 | -. 100 | -. 114 | -.095 | -. 104 | $-.080$ | -. 059 | -. 009 | -. 012 | -.064 |
| 2 | . 004 | -.026 | -.066 | -. 116 | -. 108 | -. 125 | -. 107 | -. 113 | -. 085 | -. 066 | -.011 | -. 017 | -. 069 |
| 3 | -. 003 | -. 033 | -. 067 | -. 123 | -. 113 | -. 132 | 116 | -. 117 | -. 091 | -.070 | -020 | -. 019 | -.075 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | -. 013 | -. 036 | -. 068 | -. 126 | -. 114 | -. 138 | -. 120 | -. 123 | -. 097 | -.075 | -.030 | -. 024 | $-.080$ |
| 5 | -. 019 | -. 035 | -. 066 | -. 125 | -. 106 | -. 139 | -. 120 | $-.123$ | -.098 | -. 077 | -.030 | -.024 | -. 080 |
| 6 | -. 021 | -. 034 | -. 063 | -. 112 | -. 085 | -. 107 | -. 097 | -. 107 | -.097 | -. 071 | -.033 | -.026 | -. 071 |
| 7 | -. 020 | -. 030 | $-.055$ | -. 080 | -.059 | $-.065$ | -. 055 | -. 061 | -.080 | $-.058$ | -.031 | -. 025 | -. 052 |
| 8 |  |  | -. 035 | -. 065 | -.024 | -. 015 | -. 005 | -. 020 | -. 047 | -. 037 | -. 021 | -. 018 | -. 027 |
| 9 | -. 017 | -. 007 | -. 003 | -.034 | . 018 | . 035 | 41 | . 030 | .000 | -. 009 | -. 008 | -. 007 | . 003 |
| 10 | -. 004 | . 009 | . 031 | -. 015 | . 051 | 78 | . 080 | 070 | . 042 | . 025 | .008 | .008 | . 032 |
| 11 | . 011 | . 028 | . 060 | . 022 | . 083 | . 100 | . 104 | . 102 | . 082 | . 060 | . 027 | . 022 | . 058 |
| No | . 031 | . 045 | . 084 | . 070 | . 110 | . 123 | . 114 | . 127 | . 115 | . 088 | . 040 | . 033 | . 082 |
| 1 | . 054 | . 058 | . 100 | . 132 | . 126 | . 137 | . 119 | . 142 | .131 | . 109 | . 050 | . 046 | . 100 |
| 2 | . 059 | . 065 | . 106 | . 151 | . 125 | . 135 | . 123 | . 145 | . 132 | . 113 | . 054 | . 048 | . 105 |
| 3 | . 048 | . 065 | . 104 | . 147 | . 118 | . 123 | . 121 | . 138 | . 126 | . 108 | . 047 | . 036 | . 098 |
| 4 | . 036 | . 053 | . 087 | 28 | . 108 | 13 | . 111 | . 120 | . 103 | . 089 | . 032 | . 024 | . 084 |
| 5 | . 021 | . 032 | . 063 | 10 | . 091 | . 099 | . 095 | . 100 | . 071 | . 055 | . 018 | . 013 | . 064 |
| 6 | . 007 | . 009 | . 035 | . 088 | . 074 | . 078 | . 062 | . 071 | . 044 | . 030 | . 005 | . 004 | . 042 |
| 7 | -. 005 | -. 010 | . 010 | . 059 | . 052 | . 049 | . 025 | . 036 | . 009 | . 007 | $-.005$ | $-.003$ | . 019 |
| 8 | -. 01 | 3 | -. 010 | . 020 | . 022 | . 010 | $-.015$ | . 000 | -. 015 | -. 011 | -. 012 | -. 005 | -. 004 |
| 9 | -. 01 | -. 029 | -.032 | -. 030 | -.018 | -. 025 | $-.040$ | -. 038 | -. 040 | $-.025$ | -. 017 | 00 | $-.026$ |
| 10 | -. 019 | -. 030 | -. 048 | -. 058 | -. 050 | -. 060 | -. 068 | $-.067$ | -.058 | -. 039 | -. 020 | -. 008 | $-.044$ |
| 11 | -. 018 | -. 036 | - | -. 080 | -. 075 | $-.085$ | $-.080$ | -.08.) | $-.071$ | -. 048 | $-.020$ | $-.009$ | -. 055 |
| 6. 6 | -. 007 | -. 012 | -. 012 | -. 012 | -. 005 | -. 015 | -. 017 | -. 018 | -. 027 | -. 020 | -. 014 | -. 011 | -. 015 |
| 7. 7 | -. 012 | -. 020 | -. 023 | -. 010 | -.004 | -. 008 | -. 015 | -. 012 | -.035 | -. 026 | -. 018 | -. 014 | -. 017 |
| 8. 8 | -. 017 | -. 021 | -. 023 | -. 022 | -.001 | -. 003 | $-.010$ | $-.010$ | -. 031 | -. 024 | -. 016 | -. 011 | $-.016$ |
| 9. 9 | -.016 | -. 018 | -. 018 | -. 032 | . 000 | . 005 | 00 | -. 004 | -.026 | -. 017 | -. 012 | -. 007 | -.012 |
| 10.10 | -.011 | -. 010 | -. 009 | -. 037 | . 000 | . 009 | . 006 | . 001 | -. 008 | -. 007 | -. 006 | . 000 | $-.006$ |
| 7. 2. 9 | . 008 | . 002 | . 006 | . 014 | . 016 | . 015 | . 009 | . 015 | . 004 | . 010 | . 002 | . 005 | . 009 |
| 6. 2. 8 | . 008 |  | . 01 | . 019 | . 021 | $) 13$ | . 004 | . 013 | . 016 | . 010 | . 003 | 006 | . 010 |
| 6. 2.10 | -. 006 | . 000 | -. 0 | -. 0 | -. 0 | -. 010 | . 014 | -. 009 | -. 008 | . 001 | . 000 | . 005 | $-.00{ }^{-2}$ |
| 6. 2. 6 | . 015 | . 013 | . 027 | . 042 | . 038 | . 035 | . 029 | . 036 | . 026 | . 024 | . 009 | . 009 | .028 |
| 7. 2 | . 019 | . 017 | . 026 | . 036 | . 033 | . 035 | . 034 | . 042 | . 026 | . 027 | . 012 | . 011 | . 026 |
| 8. 2 | . 019 | . 022 | . 036 | . 043 | . 050 | . 060 | . 059 | . 062 | . 042 | . 038 | . 016 | . 015 | . 039 |
| 8. 1 | . 017 | . 019 | . 032 | . 034 | . 051 | . 061 | . 057 | . 061 | . 042 | . 036 | . 014 | . 014 | . 037 |
| 7. 1 | .017 | . 014 | . 023 | . 026 | . 033 | . 036 | . 032 | . 041 | . 025 | . 026 | . 009 | . 010 | . 024 |
| 9.12.3.9 | . 011 | -. 018 | . 038 | . 038 | . 032 | . 064 | . ${ }^{5} 9$ | . 064 | . 050 | . 040 | . 016 | . 014 | . 037 |

# METEOROLOGICAL TABLES. 

SERIES VII.

## MISCELLANEOUS TABLES,

USEFUL IN

TERRESTRIAL PHYSICS AND METEOROLOGY.

## CONTENTS.

Table I. Positions of the Principal Observatories. From the American, English, and German Nantical Almanacs ..... 5
". II. To convert Parts of the Equator in Are into Sidereal Time, or to convert Terrestrial Longitude in Are into Time. From Downes, U. S. Almanac for 1845, as given in Lee's Tables and Formula, $2 d$ edition, p. 146 et seq. ..... 9
" III. To convert Sidereal Time into D'arts of the Equator in Are, or toconvert time into Terrestrial Longitude in Are. From Downes,U. S. Almanac for 1845, p. 150, and Lee's Tables and Formula11
" IV. For converting Sidereal Time into Mean Solar Time, and Mean Solar Time into Sidereal Time. From Lee's Tables and Formule ..... 12
" V. Correction of the Time obtained by Observation of the Sun, in order to have the True Time of the Clock. Communicated by Prof. B. Peirce, of Harvard University ..... 13
" VI. Tables giving the length of a Degree of the Meridian and of the Parallel, calculated according to the formula of Clarke ..... 14
6. VII. For computing Terrestrial Surfaces, based on the preceding Tables ..... 19

1) Quadrilateral surfaces of 1 degree ..... 20
2) 6 6 6 2 degrees ..... 22
3) 6 6 ، 6 ..... 23
4) " 6 ، 10 ..... 23
5) 6 " " $6,10,20$, and 30 minutes ..... 24
" VIII. Comparison of the Standards of Length of England, France, Belgium, Prussia, Russia, India, and Australia ..... 25
". IX. Table giving the length of Insolation for any given Latitude ..... 27

## POSITIONS OF THE PRINCIPAL OBSERVATORIES.

(North Latitudes and West Longitudes are considered as positive.)




if. to convert parts of the equator in arc into sidireal time, oa to Convert terrestrial longitude in arc into time.


694 to convert parts of the equator in arc into sidereal time, or to convert terrestrial longitude in arc into time.

| Degrees. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. |
| 0 | h. m. | - | h m . | $\bigcirc$ | h. m. | 0 | h. m. | $\bigcirc$ | h. m. | - | h. m. |
| 241 | 164 | 261 | 1724 | 281 | 1844 | 301 | $20 \quad 4$ | 321 | 2124 | 341 | 2244 |
| 242 | 16 S | 262 | 1728 | 282 | 1848 | 302 | $20 \quad 8$ | 322 | 2128 | 342 | 2248 |
| 243 | 1612 | 263 | 1732 | 283 | 1852 | 303 | 2012 | 323 | 2132 | 343 | 2252 |
| 244 | 1616 | 264 | 1736 | 284 | 1856 | 304 | 2016 | 324 | 2136 | 344 | 2256 |
| 245 | 1620 | 265 | 1740 | 285 | $19 \quad 0$ | 305 | 2020 | 325 | 2140 | 345 | 230 |
| 246 | 1624 | 266 | 1744 | $\stackrel{286}{ }$ | 194 | 306 | 2024 | 326 | 2144 | 346 | $23 \quad 4$ |
| 247 | 1628 | 267 | 1748 | 287 | 198 | 307 | 2028 | 327 | 2148 | 347 | 23 8 |
| 248 | 1632 | 268 | 1752 | 288 | 1912 | 308 | 2032 | 328 | 2152 | 348 | 2312 |
| 249 | 1636 | 269 | 1756 | 289 | 1916 | 309 | 2036 | 329 | 2156 | 349 | 2316 |
| 250 | 1640 | 276 | 180 | 290 | 1920 | 310 | 2040 | 330 | 220 | 350 | 2320 |
| 251 | 1644 | 271 | 184. | 291 | 1924 | 311 | 2044 | 331 | 224 | 351 | 2324 |
| 252 | 1648 | 272 | $15 \quad 8$ | 292 | 19 | 312 | 2048 | 332 | 228 | 352 | $23 \quad 28$ |
| 253 | 1652 | 273 | 1812 | 293 | 1932 | 313 | 2052 | 338 | 2212 | 353 | 2332 |
| 254 | 1656 | 274 | 1516 | 294 | 1936 | 314 | 2056 | 334 | 2216 | 354 | 2336 |
| 255 | 170 | 275 | 1820 | 295 | 1940 | 315 | 210 | 335 | 2220 | 355 | 2340 |
| 256 | 174 | 276 | 1824 | 296 | 1944 | 316 | 214 | 336 | 2224 | 356 | 2344 |
| 257 | 178 | 277 | 1828 | 297 | 1948 | 317 | 218 | 337 | 2228 | 357 | 2348 |
| 258 | 1712 | 278 | 1832 | 298 | 1952 | 318 | 2112 | 338 | 2232 | 358 | 2352 |
| 259 | 1716 | 279 | 1836 | 299 | 1956 | 319 | 2116 | 339 | 2236 | 359 | 2356 |
| 260 | 1720 | 280 | 1840 | 300 | $20 \quad 0$ | 320 | 2120 | 340 | 2240 | 360 | $24 \quad 0$ |
| Minutes. |  |  |  |  |  |  |  |  |  |  |  |
|  | m. s. | , | m. s. |  | m. s. |  | m. ${ }^{8}$ |  | m. s. |  | m. s. |
| 1 | 04 | 11 | 044 | 21 | 124 | 31 | 24 | 41 | 244 | 51 | 324 |
| 2 | 08 | 12 | 048 | 22 | 128 | 32 | 28 | 42 | 248 | 52 | 328 |
| 3 | $\begin{array}{ll}0 & 12\end{array}$ | 13 | 052 | 23 | 132 | 33 | 212 | 43 | 252 | 53 | 332 |
| 4 | 016 | 14 | 056 | 24 | 136 | 34 | 216 | 44 | 256 | 54 | 336 |
| 5 | 020 | 15 | 10 | 25 | 140 | 35 | 220 | 45 | 30 | 55 | 340 |
| 6 | 024 | 16 | 14 | 26 | 144 | 36 | 224 | 46 | 34 | 56 | 344 |
| 7 | 028 | 17 | 18 | 27 | 148 | 37 | 228 | 47 | 38 | 57 | 348 |
| 8 | $0 \quad 32$ | 18 | 112 | 28 | 152 | 38 | 232 | 48 | 312 | 58 | 352 |
| 9 | 036 | 19 | 116 | 29 | 156 | 39 | 236 | 49 | 316 | 59 | 356 |
| 10 | $0 \quad 40$ | 20 | 120 | 30 | 20 | 40 | 240 | 50 | 320 | 60 | 40 |
| Seconds |  |  |  |  |  |  |  |  |  |  |  |
|  | s. | " | s. | I | s. | , | s. | " | s. | , | s. |
| 1 | 0.067 | 11 | 0.733 | 21 | 1.400 | 31 | 2.067 | 41 | 2.733 | 51 | 3.400 |
| 2 | 0.133 | 12 | 0.500 | 22 | 1.467 | 32 | 2.138 | 42 | 2.800 | 52 | 3.467 |
| 3 | 0.200 | 13 | 0.867 | 23 | 1.533 | 33 | 2.200 | 43 | 2.867 | 53 | 3.533 |
| 4 | 0.267 | 14 | 0.933 | 24 | 1.600 | 34 | 2.267 | 44 | 2.933 | 54 | 3.600 |
| 5 | 0.333 | 15 | 1.000 | 25 | 1.667 | 35 | 2.333 | 45 | 3.000 | 55 | 3.667 |
| 6 | 0.400 | 16 | 1.067 | 26 | 1.733 | 36 | 2.400 | 46 | 3.067 | 56 | 3.733 |
| 7 | 0.467 | 17 | 1.133 | 27 | 1.800 | 37 | 2.467 | 47 | 3.133 | 57 | 3.800 |
| 8 | 0.533 | 18 | 1.200 | 28 | 1.867 | 38 | 2.533 | 48 | 3.200 | 58 | 3.867 |
| 9 | 0.600 | 19 | 1.267 | 29 | 1.933 | 39 | 2.600 | 49 | 3.267 | 59 | 3.933 |
| 10 | 0.667 | 20 | 1.333 | 30 | 2.000 | 40 | 2.667 | 50 | 3.333 | 60 | 4.000 |

III. TO CONVERT SIDEREAL TIME INTO PARTS OF THF EQUATOR IN ARC, OR TO CONVERT TIME INTO TERRESTRIAL LONGITUDE IN ARC.

| Hours. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time. | Arc. | Time | Arc | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. |
| h. | ${ }^{\circ}$ | h | $\bigcirc$ | $h$. | $\bigcirc$ | h. | $\bigcirc$ | h. | $\bigcirc$ | h. | $\bigcirc$ |
| 1 | 15 | 5 | 75 | 9 | 135 | 13 | 195 | 17 | 25.5 | 21 | 315 |
| 2 | 30 | 6 | 90 | 10 | 150 | 14 | 210 | 18 | 270 | 22 | 330 |
| 3 | 45 | 7 | 105 | 11 | 165 | 15 | 225 | 19 | 285 | 23 | 345 |
| 4 | 60 | 8 | 120 | 12 | 180 | 16 | 240 | 20 | 300 | 24 | 360 |
| Minvies |  |  |  |  |  |  |  |  |  |  |  |
| m | - | m. | - | m . | $\bigcirc$, | m . | $\bigcirc$ | m. | $\bigcirc$ | m. |  |
| 1 | 015 | 11 | 245 | 21 | 515 | 31 | 745 | 41 | 1015 | 51 | 1245 |
| 2 | 030 | 12 | 30 | 22 | 530 | 32 | 80 | 42 | 1030 | 52 | 130 |
| 3 | 045 | 13 | 315 | 23 | $\bigcirc 45$ | 33 | 815 | 43 | 1045 | 53 | 1315 |
| 4 | 10 | 14 | 330 | 24 | 60 | 34 | 830 | 44 | 110 | 54 | 1330 |
| 5 | 115 | 15 | 345 | 25 | 615 | 35 | 845 | 45 | 1115 | 55 | 1345 |
| 6 | 130 | 16 | 40 | 26 | 630 | 36 | $9 \quad 0$ | 46 | 1130 | 56 | 140 |
| 7 | 145 | 17 | 415 | 27 | 645 | 37 | 915 | 47 | 1145 | 57 | 1415 |
| 8 | 20 | 18 | 430 | 28 | 70 | 38 | 930 | 48 | 120 | 58 | 1430 |
| 9 | 215 | 19 | 445 | 29 | 715 | 39 | 945 | 49 | 1215 | 59 | 1445 |
| 10 | 230 | 20 | 50 | 30 | 730 | 40 | 100 | 50 | 1230 | 60 | 150 |
| Seconds |  |  |  |  |  |  |  |  |  |  |  |
| s. | $\begin{array}{ll}1 & \prime \prime \\ 0 & 15\end{array}$ | s. | 1 <br> 2 <br> 15 | 21 | ${ }^{\prime} 5115$ | s. | $1 / 15$ 7 | s. | 10 15 | s. | 19 ${ }^{\prime \prime}$ |
| 2 | 030 | 12 | 30 | 22 | 530 | 32 | 80 | 42 | 1030 | 52 | 130 |
| 3 | 045 | 13 | 315 | 23 | 545 | 33 | 815 | 43 | 1045 | 53 | 13 15 |
| 4 | 10 | 14 | 330 | 24 | 60 | 34 | 830 | 44 | 110 | 54 | 1330 |
| 5 | 115 | 15 | 345 | 25 | 615 | 35 | 845 | 45 | 1115 | 55 | 1345 |
| 6 | 130 | 16 | 40 | 26 | 630 | 36 | 90 | 46 | 1130 | 56 | 140 |
| 7 | 145 | 17 | 415 | 27 | 645 | 37 | 915 | 47 | 1145 | 57 | 1415 |
| 8 | 20 | 18 | 430 | 23 | 70 | 38 | 930 | 48 | 120 | 58 | 1430 |
| 9 | 215 | 19 | 445 | 29 | 715 | 39 | 945 | 49 | 1215 | 59 | 1145 |
| 10 | 230 | 20 | 50 | 30 | 730 | 40 | $10 \quad 0$ | 50 | 1230 | 60 | 150 |
| Tenths of Seconds. |  |  |  |  |  |  |  |  |  |  |  |
| s. |  | , | " | s. |  | s |  | ${ }^{\text {s }}$ |  | s. | " |
| 0.01 | 0.15 | 0.18 | 2.70 | 0.35 | 5.25 | 0.52 | 7.80 | 0.69 | 10.35 | 0.86 | 12.90 |
| 0.02 | 0.30 | 0.19 | 2.85 | 0.36 | 5.40 | 0.53 | 7.95 | 0.70 | 10.50 | 0.87 | 13.05 |
| 0.03 | 0.45 | 0.20 | 3.00 | 0.37 | 5.55 | 0.54 | 8.10 | 0.71 | 10.65 | 0.88 | 13.20 |
| 0.04 | 0.60 | 0.21 | 3.15 | 0.38 | 5.70 | 0.55 | 8.25 | 0.72 | 10.80 | 0.89 | 13.35 |
| 0.05 | 0.75 | 0.22 | 3.30 | 0.39 | 5.85 | 0.96 | 8.40 | 0.73 | 10.95 | 0.90 | 13.50 |
| 0.06 | 0.90 | 0.23 | 3.45 | 0.40 | 6.00 | 0.57 | 8.55 | 0.74 | 11.10 | 0.91 | 13.65 |
| 0.07 | 1.05 | 0.24 | 3.60 | 0.41 | 6.15 | 0.58 | 8.70 | 0.75 | - 11.25 | 0.92 | 13.80 |
| 0.08 | 1.20 | 0.25 | 3.75 | 0.12 | 6.30 | 0.59 | 8.85 | 0.76 | 11.40 | 0.93 | 13.9.5 |
| 0.09 | 1.35 | 0.26 | 3.90 | 0.43 | 6.45 | 0.60 | 9.00 | 0.77 | 11.55 | 0.94 | 14.10 |
| 0.10 | 1.50 | 0.27 | 4.05 | 0.44 | 6.60 | 0.61 | 9.15 | 0.78 | 11.70 | 0.95 | 14.25 |
| 0.11 | 1.65 | 0.28 | 4.20 . | 0.45 | 6.75 | 0.62 | 9.30 | 0.79 | 11.85 | 0.96 | 14.40 |
| 0.12 | 1.80 | 0.29 | 4.35 | 0.46 | 6.90 | 0.63 | 9.45 | 0.80 | 12.00 | 0.97 | 14.55 |
| 0.13 | 1.95 | 0.30 | 4.50 | 0.47 | 7.05 | 0.64 | 9.60 | 0.81 | 12.15 | 0.98 | 14.70 |
| 0.14 | 2.10 | 0.31 | 4.65 | 0.48 | 7.20 | 0.65 | 9.75 | 0.82 | 12.30 | 0.99 | 14.85 |
| 0.15 | 2.25 | 0.32 | 480 | 0.49 | 7.35 | 0.66 | 9.90 | 0.83 | 12.45 | 1.00 | 15.00 |
| 0.16 | 2.40 | 0.38 | 4.95 | 0.50 | 7.50 | 0.67 | 10.05 | 0.94 | 12.60 |  |  |
| 0.17 | 2.55 | 0.34 | 5.10 | 0.51 | 7.65 | 0.68 | 10.20 | 0.85 | 12.75 |  |  |

IV. FOR CONVERTING SIDEREAL TIME INTO MEAN SOLAR TIME, AND MEAN TIME INTO SIDEREAL TIME.

| hochs. |  |  | minctes. |  |  |  |  |  | SECONDS. |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hours | Mean 'line. | Sidereal 'lime. | Minutes. | Mean Time | sidereal Time. | Minutes. | $\begin{aligned} & \text { Mean } \\ & \text { Time. } \end{aligned}$ | Silereal 'lime | Sec- onds. |  | Seconds. | $\begin{gathered} \text { Mehn } \\ \text { or } \\ \text { Silereal } \\ \text { Témee } \end{gathered}$ |
|  | 11 s . | m E . |  | s. | 8. |  | $\varepsilon$. | 8 |  | 8. |  | 8. |
| 1 | 0 O.8.83 | 0 9.86 | 1 | 0.16 | 0.16 | 31 | 5.08 | 5.09 | 1 | 0.00 | 31 | 0.09 |
| 2 | 01966 | 019.71 | 2 | 0.33 | 0.33 | 32 | 5.24 | 5.26 | 2 | 0.01 | 32 | 0.09 |
| 3 | 029.49 | 029.57 | 3 | 0.49 | 0.49 | 33 | 5.41 | 5.42 | 3 | 0.01 | 33 | 0.09 |
| 4 | 039.32 | 039.43 | 4 | 0.66 | 0.66 | 34 | 5.57 | 5.59 | 4 | 0.01 | 34 | 0.09 |
| 5 | 049.15 | 049.28 | 5 | 0.82 | 0.82 | 35 | 5.75 | 5.75 | 5 | 0.01 | 35 | 0.10 |
| 6 | 058.95 | 059.14 | 6 | 0.98 | 0.99 | 36 | 5.90 | 5.91 | 6 | 0.02 | 36 | 0.10 |
| 7 | 18.51 | 19.00 | 7 | 1.15 | 1.15 | 37 | 6.06 | 6.08 | 7 | 0.02 | 37 | 0.10 |
| 8 | 115.64 | 118.85 | 8 | 1.31 | 1.31 | 38 | 6.23 | 6.24 | 8 | 0.02 | 38 | 0.10 |
| 9 | 125.47 | 128.71 | 9 | 1.47 | 1.48 | 39 | 6.39 | 6.41 | 9 | 0.03 | 39 | 0.11 |
| 10 | 135.30 | 138.57 | 10 | 1.64 | 1.64 | 40 | 6.55 | 6.57 | 10 | 0.03 | 40 | 0.11 |
| 11 | 148.13 | 148.42 | 11 | 1.80 | 1.81 | 41 | 6.72 | 6.74 | 11 | 0.03 | 41 | 0.11 |
| 12 | 157.96 | 158.25 | 12 | 1.97 | 1.97 | 12 | 6.88 | 6.90 | 12 | 0.03 | 42 | 012 |
| 13 | 27.75 | 28.13 | 13 | 213 | 2.14 | 43 | 7.05 | 706 | 13 | 0.04 | 43 | 0.12 |
| 14 | 217.61 | 217.99 | 14 | 2.29 | 2.30 | 4 | 7.21 | 7.23 | 14 | 0.04 | 4 | 0.12 |
| 15 | 227.44 | 227.85 | 15 | 2.16 | 2.46 | 45 | 7.37 | 7.39 | 15 | 0.04 | 45 | 0.12 |
| 16 | 237.27 | 237.70 | 16 | 2.62 | 2.63 | 46 | 7.54 | 7.56 | 16 | 0.04 | 46 | 013 |
| 17 | 247.10 | 247.56 | 17 | 2.79 | 2.79 | 47 | 7.70 | 772 | 17 | 005 | 47 | 0.13 |
| 13 | 256.93 | 257.42 | 18 | 2.95 | 2.96 | 45 | 7.86 | 7.89 | 18 | 0.05 | 48 | 0.13 |
| 19 | 36.76 | $\begin{array}{lll}3 & 7.27\end{array}$ | 19 | 3.11 | 312 | 49 | 8.03 | 805 | 19 | 0.05 | 49 | 0.13 |
| 20 | 316.59 | 317.13 | 20 | 3.28 | 3.29 | 50 | 8.19 | 8.21 | 20 | 0.06 | 50 | 0.14 |
| 21 | 326.42 | 326.99 | 21 | 3.44 | 3.45 | 51 | 8.36 | 8.35 | 21 | 0.06 | 51 | 0.14 |
| $\because 2$ | 3 36.25 | 336.84 | 22 | 3.60 | 3.61 | 52 | 8.52 | 8.54 | 22 | 0.06 | 52 | 0.14 |
| 23 | $3+6.03$ | 3 46.70 | 23 | 3.77 | 3.79 | 53 | 8.68 | 8.71 | 23 | 0.06 | 53 | 015 |
| 24 | 35.5 .91 | 356.56 | 24 | 3.93 | 3.94 | 54 | 8.55 | 8.87 | 24 | 0.07 | 54 | 0.15 |
| 25 | $\pm 5.74$ | 46.41 | 25 | 4.10 | 4.11 | 55 | 9.01 | 9.04 | 25 | 0.07 | 55 | 0.15 |
| 26 | 415.57 | 416.27 | 26 | 4.26 | 4.27 | 56 | 9.17 | 9.20 | 26 | 0.07 | 56 | 0.15 |
| 27 | 425.40 | $+26.13$ | 27 | 4.42 | 4.43 | 57 | 9.34 | 9.36 | 27 | 0.07 | 57 | 0.16 |
| $2 \cdot$ | 43.5 .23 | 435.95 | 28 | 4.59 | 4.60 | 58 | 9.50 | 9.53 | 28 | 0.08 | 58 | 0.16 |
| 29 | 445.06 | 4 4.5.84 | 29 | 4.75 | 4.76 | 59 | 9.67 | 9.69 | 29 | 0.08 | 59 | 0.16 |
| 30 | 454.89 | $+5.5 .69$ | 30 | 4.92 | 4.93 | 60 | 9.83 | 9.86 | 30 | 0.08 | 60 | 0.16 |

G
V. CORRECTION OF TIIE TME obtained by obsERYATION OF THE SUN, in ORDER TO HAVE THE TRUE TIME OF THE ClOCK.

|  | Jan. | Feb. | Mar. | Apr. | Apr. | May. | June. | June. | July. | Aug. | Sept. | Oct. | Nov. | Dec. | Dec. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Add. | Add. | Add. | Add. | Subt. | Subt. | Subt. | Add. | Add. | Add. | Subt. | Subt. | Subt. | Subt. | Add. |  |
|  | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. | Min. |  |
| 1 | 4 | 14 | 13 | 4 | -• | 3 | 3 | -• | 3 | 6 | 0 | 10 | 16 | 11 | . . | 1 |
| 2 | 4 | 14 | 12 | 4 | -• | 3 | 2 | . - | 4 | 6 | 0 | 11 | 16 | 10 | -• | 2 |
| 3 | 5 | 14 | 12 | 3 | -• | 3 | 2 | , • | 4 | 6 | 1 | 11 | 16 | 10 | -• | 3 |
| 4 | 5 | 14 | 12 | 3 | -• | 3 | 2 | -• | 4 | 6 | 1 | 11 | 16 | 10 | -• | 4 |
| 5 | 6 | 14 | 12 | 3 | -• | 4 | 2 | -• | 4 | 6 | 1 | 12 | 16 | 9 | - . | 5 |
| 6 | 6 | 14 | 12 | 2 | -• | 4 | 2 | -• | 4 | 6 | 2 | 12 | 16 | 9 | - . | 6 |
| 7 | 7 | 14 | 11 | 2 | -• | 4 | 2 | -• | 4 | 5 | 2 | 12 | 16 | 8 | - • | 7 |
| 8 | 7 | 15 | 11 | 2 | -• | 4 | 1 | -• | 5 | 5 | 2 | 12 | 16 | 8 | -• | 8 |
| 9 | 8 | 15 | 11 | 2 | - . | 4 | 1 | -• | 5 | 5 | 3 | 13 | 16 | 7 | - . | 9 |
| 10 | 8 | 15 | 11 | 1 | . | 4 | 1 | -• | 5 | 5 | 3 | 13 | 16 | 7 | . $\cdot$ | 10 |
| 11 | 9 | 15 | 10 | 1 | -• | 4 | 1 | -• | 5 | 5 | 3 | 13 | 16 | 6 | -• | 11 |
| 12 | 9 | 15 | 10 | 1 | - | 4 | 1 | -• | 5 | 5 | 4 | 13 | 16 | 6 | - - | 12 |
| 13 | 9 | 15 | 10 | 1 | -• | 4 | 0 | -• | 5 | 5 | 4 | 14 | 16 | 5 | - . | 13 |
| 14 | 10 | 14 | 9 | 0 | - . | 4 | 0 | -• | 5 | 4 | 5 | 14 | 15 | 5 | - - | 1.4 |
| 15 | 10 | 14 | 9 | 0 | -• | 4 | 0 | -• | 6 | 4 | 5 | 14 | 15 | 4 | - - | 15 |
| 16 | 10 | 14 | 9 | 0 | -• | 4 | 0 | -• | 6 | 4 | 5 | 14 | 15 | 4 | . | 16 |
| 17 | 11 | 14 | 9 | 0 | -• | 4 | 0 | -• | 6 | 4 | 6 | 15 | 15 | 3 | . - | 17 |
| 18 | 11 | 14 | 8 | -• | 1 | 4 | -• | 1 | 6 | 4 | 6 | 15 | 15 | 3 |  | 18 |
| 19 | 11 | 14 | 8 |  | 1 | 4 | -• | 1 | 6 | 3 | 6 | 15 | 14 | 2 |  | 19 |
| 20 | 11 | 14 | 8 |  | 1 | 4 |  | 1 | 6 | 3 | 7 | 15 | 14 | 2 | -• | 20 |
| 21 | 12 | 14 | 7 |  | 1 | 4 |  | 1 | 6 | 3 | 7 | 15 | 14 | 1 | - | 21 |
| 22 | 12 | 14 | 7 |  | 2 | 4 | - . | 2 | 6 | 3 | 7 | 15 | 14 | 1 | -• | 22 |
| 23 | 12 | 14 | 7 | - | 2 | 4 | - . | 2 | 6 | 2 | 8 | 16 | 13 | 0 | - . | 23 |
| 24 | 12 | 13 | 6 | -• | 2 | 3 | -• | 2 | 6 | 2 | 8 | 16 | 13 | 0 |  | 24 |
| 25 | 13 | 13 | 6 | - . | 2 | 3 | - • | 2 | 6 | 2 | 8 | 16 | 13 | 0 |  | 25 |
| 26 | 13 | 13 | 6 | - . | 2 | 3 | -• | 2 | 6 | 2 | 9 | 16 | 12 |  | 1 | 26 |
| 27 | 13 | 13 | 5 |  | 2 | 3 | - . | 3 | 6 | 1 | 9 | 16 | 12 |  | 1 | 27 |
| 28 | 13 | 13 | 5 | . | 3 | 3 | -• | 3 | 6 | 1 | 9 | 16 | 12 |  | 2 | 28 |
| 29 | 14 | 13 | 5 | - . | 3 | 3 | -• | 3 | 6 | 1 | 10 | 16 | 11 |  | 2 | 29 |
| 30 | 14 | . . | 4 | -• | 3 | 3 | -• | 3 | 6 | 0 | 10 | 16 | 11 |  | 3 | 30 |
| 31 | 14 | -• | 4 | -• | - . | 3 | -• | -• | 6 | 0 | - . | 16 | - . |  | 3 | 31 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## VI. the lengtil of a degree of thif mebidian and of the parallel.

The formule from which the following tables have been computed are as follows:1 degree of the meridian $=111,132.09^{\mathrm{m}}-566.05^{\mathrm{m}} \cos 2 \phi+1.20^{\mathrm{m}} \cos 4 \phi-$ $0.003^{\mathrm{m}} \cos 6 \phi$, etc., in which $\phi$ is the latitute. 1 degree of the parallel $=111,415.10^{\mathrm{m}}$ $\cos \phi-94.54^{\mathrm{m}} \cos 3 \phi+0.12^{\mathrm{m}} \cos 5 \phi$, in which $\phi$ is the middle latitude. For example, the number given for $40^{\circ}$ in the meridian table gives the length from $39.30^{\circ}$ to $40.30^{\circ}$. The dimensions of the earth used in the formula are those of Clarke's spheroid of revolution of 1866 , and are the same as those now (1884) used in the U. S. Coast and Geoletic Survey: They are ats follows :-

$$
\begin{array}{rlrl}
a, \text { semi-axis major }=6.378 .206 .4 \text { metres, } \log a & =6.80469857 . \\
b, \text { semi axis minor }=6,3.56,583.8 \text { metres, } \log b & =6.80322378 . \\
e^{2}=\frac{a^{2}-b^{2}}{a^{2}}=0.0064686 .580 & \log e^{2} & =7.83050257 . \\
\frac{a-b}{a}=0.003390075 & \log \frac{a-b}{a} & =7.53020934 . \\
\log \frac{a-b}{a+b} & =7.22991612 .
\end{array}
$$

The numbers used in reduction to the different measures are as follows:-
German mite $\quad=\frac{1}{15}$ equatorial degree $=7421.3802$ metres, $\log 3.87048468$
Nantical league $=\frac{1}{2}$ equatorial degree $=5.56 .03 .01$ metres, $\log 3.745 .54594$
French league $=\frac{1}{2}$ equatorial degree $=4452.8281$ metres, $\log 3.64863593$
Naut. or geog. mile $=\frac{1}{6} \overline{0}$ equatorial degree $=1855.3450$ metres, $\log 3.26842469$
Statute mile $\quad=1609.3296$ metres, $\log 3.20664499$
Russian werst $\quad=1066.781$ metres, $\log 3.0280752$
1.) Length of one degree of the meridian in different measures. 699

| Degrees. | Metres. | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \mathrm{Eq.} . \end{aligned}$ | Nautical <br> Leagues. $20=1^{\circ}$ Eq. | $\begin{gathered} \text { French } \\ \text { Leatrues. } \\ 25=i^{\circ} \mathrm{E} . \end{gathered}$ | Nautical or Geog. Miles. $60)=1^{\circ} \mathrm{E4}$. | Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 110567.2 | 14.898 | 19.865 | 24.831 | 59.594 | 68.704 | 103.646 |
| 1 | 110567.6 | 14.899 | 19.865 | 24.831 | 59.594 | 68.704 | 103.646 |
| 2 | 110568.6 | 14.899 | 19.865 | 24.831 | 59.595 | 68.705 | 103.647 |
| 3 | 110570.3 | 14.899 | 19.865 | 24.832 | 59.596 | 68.706 | 103.649 |
| 4 | 110572.7 | 14.899 | 19.866 | 24.832 | 59.597 | 68.707 | 103.651 |
| 5 | 110575.8 | 14.900 | 19.866 | 24.833 | 59.598 | 68.709 | 103.654 |
| 6 | 110579.5 | 14.900 | 19.867 | 24.834 | 59.600 | 68.711 | 103.657 |
| 7 | 110583.9 | 14.901 | 19.868 | 24.835 | 59.603 | 68.714 | 103.661 |
| 8 | 110589.0 | 14.901 | 19.869 | 24.836 | 59.606 | 68.717 | 103.666 |
| 9 | 110594.7 | 14.902 | 19.870 | 24.837 | 59.609 | 68.721 | 103.671 |
| 10 | 110601.1 | 14.903 | 19.871 | 24.838 | 59.612 | 68.725 | 103.677 |
| 11 | 110608.1 | 14.904 | 19.872 | 24.840 | 59.616 | 68.729 | 103.684 |
| 12 | 110615.8 | 14.905 | 19.573 | 24.842 | 59.620 | 68.734 | 103.691 |
| 13 | 110624.1 | 14.906 | 19.875 | 24.844 | 59.625 | 68.739 | 103.699 |
| 14 | 110633.0 | 14.907 | 19.876 | 24.846 | 59.629 | 68.745 | 103.707 |
| 15 | 110642.5 | 14.909 | 19.878 | 24.848 | 59.634 | 68.751 | 103.716 |
| 16 | 110652.6 | 14.910 | 19.880 | 24.850 | 59.640 | 68.757 | 103.726 |
| 17 | 110663.3 | 14.911 | 19.882 | 24.852 | 59.646 | 68.763 | 103.736 |
| 18 | 110674.5 | 14.913 | 19.884 | 24.855 | 59.652 | 68.770 | 103.746 |
| 19 | 110686.3 | 14.914 | 19.886 | 24.857 | 59.658 | 68.778 | 103.757 |
| 20 | 110698.7 | 14.916 | 19.888 | 24.860 | 59.665 | 68.786 | 103.769 |
| 21 | 110711.6 | 14.918 | 19.891 | 24.863 | 59.672 | 68.794 | 103.781 |
| 22 | 110725.0 | 14.920 | 19.893 | 24.866 | 59.679 | 68.802 | 103.793 |
| 23 | 110738.8 | 14.922 | 19.895 | 24.869 | 59.686 | 68.810 | 103.806 |
| 24 | 110753.2 | 14.924 | 19.898 | 24.872 | 59.694 | 68.819 | 103.820 |
| 25 | 110768.0 | 14.926 | 19.901 | 24.876 | 59.702 | 68.829 | 103.834 |
| 26 | 110783.3 | 14.928 | 19.903 | 24.879 | 59.710 | 68.838 | 103.848 |
| 27 | 110799.0 | 14.930 | 19.906 | 24.883 | 59.719 | 68.848 | 103.863 |
| 28 | 110815.1 | 14.932 | 19.909 | 24.886 | 59.727 | 68.858 | 103.878 |
| 29 | 110831.6 | 14.934 | 19.912 | 24.890 | 59.736 | 68.868 | 103.893 |
| 30 | 110848.5 | 14.936 | 19.915 | 24.894 | 59.745 | 68.879 | 103.909 |
| 31 | 110865.7 | 14.939 | 19.918 | 24.898 | 59.755 | 68.889 | 103.925 |
| 32 | 110883.2 | 14.941 | 19.921 | 24.902 | 59.764 | 68.900 | 103.942 |
| 33 | 110901.1 | 14.943 | 19.925 | 24.906 | 59.774 | 68.911 | 103.959 |
| 34 | 110919.2 | 14.946 | 19.928 | 24.910 | 59.784 | 68.923 | 103.976 |
| 35 | 110937.6 | 14.948 | 19.931 | 24.914 | 59.794 | 68.934 | 103.993 |
| 36 | 110956.2 | 14.951 | 19.935 | 24.918 | 59.804 | 68.946 | 104.010 |
| 37 | 110975.0 | 14.953 | 19.938 | 24.922 | 59.814 | 68.957 | 104.028 |
| 38 | 110994.1 | 14.956 | 19.941 | 24.927 | 59.824 | 68.969 | 104.046 |
| 39 | 111013.3 | 14.959 | 19.945 | 24.931 | 59.834 | 68.981 | 104.064 |
| 40 | 111032.7 | 14.961 | 19.948 | 24.935 | 59.845 | 68.993 | 104.082 |
| 41 | 111052.2 | 14.964 | 19.952 | 24.940 | 59.855 | 69.005 | 104.100 |
| 42 | 111071.7 | 14.966 | 19.955 | 24.944 | 59.866 | 69.017 | 104.119 |
| 43 | 111091.4 | 14.969 | 19.959 | 24.948 | 59.876 | 69.029 | 104.137 |
| 44 | 111111.1 | 14.972 | 19.962 | 24.953 | 59.887 | 69.042 | 104.156 |
| 45 | 111130.9 | 14.974 | 19.966 | 24.957 | 59.898 | 69.054 | 104.174 |

1.) LENGTH OF ONE DEGREE OF THE MERIDIAN IN DIfFERENT MEASURES.

| Degrees. | Metres. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=1^{\circ} \text { Eq. } \end{gathered}$ | $\begin{aligned} & \text { Nautical } \\ & \text { Leagues. } \\ & 20=1 \text { Eq. } \end{aligned}$ | $\begin{gathered} \text { French } \\ \text { Leagues. } \\ 25=1^{\circ} \text { Eq. } \end{gathered}$ | Nautical or Geog. Miles. $60=1^{\circ} \mathrm{Eq}$. | Statute Miles. | Russian <br> Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 46 | 111150.7 | 14.977 | 19.969 | 24.962 | 59.908 | 69.067 | 104.193 |
| 47 | 111170.4 | 14.980 | 19.973 | 24.966 | 59.919 | 69.079 | 104.211 |
| 48 | 111190.1 | 14.982 | 19.976 | 24.971 | 59.929 | 69.091 | 104.230 |
| 49 | 111909.7 | 14.985 | 19.980 | 24.975 | 59.940 | 69.103 | 104.248 |
| 50 | 111229.3 | 14.988 | 19.984 | 24.979 | 59.951 | 69.115 | 104.266 |
| 51 | 111248.7 | 14.990 | 19.987 | 24.984 | 59.961 | 69.127 | 104.285 |
| 52 | 111268.0 | 14.993 | 19.991 | 24.988 | 59.972 | 69.139 | 104.303 |
| 53 | 111287.1 | 14.995 | 19.994 | 24.992 | 59.982 | 69.151 | 104.321 |
| 54 | 111306.0 | 14.998 | 19.997 | 24.997 | 59.992 | 69.163 | 104.338 |
| 55 | 111324.8 | 15.000 | 20.001 | 25.001 | 60.002 | 69.175 | 104.356 |
| 56 | 111343.3 | 15.003 | 20.004 | 25.005 | 60.012 | 69.186 | 104.373 |
| 57 | 111361.5 | 15.005 | 30.007 | 25.909 | 60.022 | 69.198 | 104.390 |
| 58 | 111379.5 | 15.008 | 20.011 | 25.013 | 60.032 | 69.209 | 104.407 |
| 59 | 1113!7.2 | 15.010 | 20.014 | 25.017 | 60.041 | 69.220 | 104.424 |
| 60 | 111414.5 | 15.013 | 20.017 | 25.021 | 60.051 | 69.230 | 104.440 |
| ${ }_{61}$ | 111431.5 | 15.015 | 20.020 | 25.025 | 60.060 | 69.241 | 104.456 |
| 62 | 111448.2 | 15.017 | 20.023 | 25.029 | 60.069 | 69.251 | 104.472 |
| 63 | 111464.4 | 15.019 | 20.026 | 25.032 | 60.077 | 69.261 | 104.487 |
| 64 | 111480.3 | 15.022 | 20.029 | 25.036 | 60.086 | 69.271 | 104.502 |
| 65 | $1114!5.7$ | 15.024 | 20.031 | 25.039 | 60.094 | 69.281 | 104.516 |
| 66 | 111510.7 | 15.026 | 20.034 | 25.043 | 60.102 | 69.290 | 104.530 |
| 67 | 111525.3 | 15.028 | 20.037 | 25.046 | 60.110 | 69.299 | 104.544 |
| 68 | 111539.3 | 15.029 | 20.039 | 25.049 | 60.118 | 69.308 | 104.557 |
| 69 | 111552.9 | 15.031 | 20.042 | 25.052 | 60.125 | 69.316 | 104.570 |
| 70 | 111565.9 | 15.033 | 20.044 | 25.055 | 60.132 | 69.324 | 104.582 |
| 71 | 111578.4 | 15.035 | 20.046 | 25.058 | 60.139 | 69.332 | 104.594 |
| 72 | 111590.4 | 15.036 | 20.048 | 25.061 | 60.145 | 69.340 | 104.605 |
| 73 | 111601.8 | 15.038 | 20.050 | 25.063 | 60.151 | 69.347 | 104.616 |
| 74 | 111612.6 | 15.039 | 20.052 | 25.066 | 60.157 | 69.354 | 104.626 |
| 75 | 111622.9 | 15.041 | 20.054 | 25.068 | 60.163 | 69.360 | 104.635 |
| 76 | 111632.6 | 15.042 | 20.056 | 25.070 | 60.168 | 69.366 | 104.644 |
| 77 | 111641.6 | 15.043 | 20.058 | 25.072 | 60.173 | 69.372 | 104.653 |
| 78 | 111650.0 | 15.044 | 20.059 | 25.074 | 60.177 | 69.377 | 104.661 |
| 79 | 111657.8 | 15.045 | 20.061 | 25.076 | 60.182 | 69.382 | 104.668 |
| 80 | 111664.9 | 15.046 | 20.063 | 25.077 | 60.186 | 69.386 | 104.675 |
| 81 | 111671.4 | 15.047 | 20.063 | 25.079 | 60.189 | 69.390 | 104.681 |
| 82 | 111677.2 | 15.048 | 20.064 | 25.080 | 60.192 | 69.394 | 104.686 |
| 83 | 111682.4 | 15.149 | 20.065 | 25.081 | 60.195 | 69.397 | 104.691 |
| 84 | 111686.9 | 15.049 | 20.066 | 25.082 | 60.197 | 69.400 | 104.695 |
| 85 | 111690.7 | 15.050 | 20.066 | 25.083 | 60.199 | 69.402 | 104.699 |
| 86 | 111693.8 | 15.050 | 20.067 | 25.084 | 60.201 | 69.404 | 104.702 |
| 87 | 111696.2 | 15.051 | 20.067 | 25.084 | 60.202 | 69.405 | 104.704 |
| 88 | 111698.0 | 15.051 | 20.068 | 25.084 | 60.203 | 69.407 | 104.706 |
| 89 | 111699.0 | 15.051 | 20.068 | 25.085 | 60.204 | 69.407 | 104.707 |
| 90 | 111699.3 | 15.051 | 20.068 | 25.085 | 60.204 | 69.407 | 104.707 |

2.) Length of one degree of the parallel in different measures.

| Degrees. | Metres. | $\begin{gathered} \text { German } \\ \text { Miles. } \\ 15=-1^{\circ} \mathrm{E}_{1} . \end{gathered}$ | Nautical Leagues. $20=1^{\circ} \mathrm{E}!$. | French Leagues. $25=10 \mathrm{E} 1$. | Nautical or Geog. Mnles. $60=1^{\circ} \mathrm{Eq}$. | Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 111320.7 | 15.000 | 20.000 | 25.000 | 60.000 | 69.17 | 104.352 |
| 1 | 111303.9 | 14.998 | 19.997 | 24.996 | 59.991 | 69.162 | 104.336 |
| 2 | 111953.4 | 14.991 | 19.988 | $\simeq 4.985$ | 59.964 | 69.130 | 104.289 |
| 3 | 111169.2 | 14.980 | 19.973 | 24.966 | 59.918 | 69.078 | 104.210 |
| 4 | 111051.3 | 14.964 | 19.952 | 24.940 | 59.855 | 69.005 | 104.100 |
| 5 | 110599.9 | 14.943 | 19.924 | 24.905 | 59.773 | 68.911 | 103.958 |
| 6 | 110714.9 | 14.918 | 19.891 | 24.864 | 59.673 | 68.796 | 103.784 |
| 7 | 110496.5 | 14.889 | 19.852 | 24.815 | 59.556 | 68.660 | 103.579 |
| 8 | 114244.6 | 14.855 | 19.807 | 24.758 | 59.420 | 68.503 | 103.343 |
| 9 | 109959.3 | 14.817 | 19.755 | $24.69 \pm$ | 59.266 | 68.320 | 103.076 |
| 10 | 109640.7 | 14.774 | 19.698 | 24.623 | 59.095 | 68.128 | $10 \cdot 3.777$ |
| 11 | 109288.9 | 14.726 | 19.635 | $\boxed{24.544}$ | 58.905 | 67.909 | 102.447 |
| 12 | 108904.0 | 14.674 | 19.566 | 24.457 | 58.697 | 67.670 | 102.087 |
| 13 | 108486.1 | 14.618 | 19.491 | 24.363 | 58.472 | 67.411 | 101.695 |
| 14 | 108035.4 | 14.557 | 19.410 | 24.262 | 58.239 | 67.131 | 101.272 |
| 15 | 107551.9 | 14.492 | 19.323 | $\bigcirc 4.154$ | 57.969 | 66.830 | 100.819 |
| 16 | 107035.8 | 14.433 | 19.230 | 24.038 | 57.690 | 66.510 | 100.335 |
| 17 | 106487.3 | 14.349 | 19.132 | 23.915 | 57.395 | 66.169 | 99.821 |
| 18 | 105906.5 | 14.270 | 19.027 | 93.784 | $57.08{ }^{\text {a }}$ | 65.808 | 99.976 |
| 19 | 105293.6 | 14.188 | 18.917 | 23.646 | 56.751 | 65.427 | 98.702 |
| 20 | 104648.7 | 14.101 | 18.801 | 23.502 | 56.404 | 65.026 | 98.098 |
| 21 | 103972.0 | 14.010 | 18.680 | 23.350 | 56.039 | 64.606 | 97.463 |
| 2.2 | $103: 63.8$ | 13.914 | 18.553 | 23.191 | 55.657 | 64.166 | 96.799 |
| 23 | 102524.2 | 13.815 | 18.420 | 23.025 | 55.259 | 63.706 | $96.106^{2}$ |
| 24 | 101753.5 | 13.711 | 18.281 | 22.851 | 54.843 | 63.297 | 95.384 |
| 25 | 100951.8 | 13.603 | 18.137 | 92. 971 | 54.411 | 62.729 | 94.630 |
|  | 100119.5 | 13.491 | 17.988 | 22.485 | 53.963 | 62.21: | 93.852 |
| 27 | 99.56 .7 | 13.374 | 17.833 | 22.391 | 53.498 | 61.676 | 93.043 |
| 28 | 98363.7 | 13.254 | 17.672 | 22.090 | 53.016 | 61.121 | 92.206 |
| 99 | 97440.8 | 13.130 | 17.506 | 21.883 | 52.519 | 60.548 | 91.341 |
| 30 | 96458.2 | 13.001 | 17.335 | 21.669 | 52.006 | 59.956 | 90.448 |
|  | 95506.2 | 12.869 | 17.159 | 21.448 | 51.476 | 59.345 | 89.508 |
| 32 | 94495.1 | 12.733 | 16.977 | 21.221 | 50.931 | 58.717 | 88.580 |
| 33 | 93455.2 | 12.593 | 16.790 | 20.988 | 50.371 | 58.071 | 87.605 |
|  | 92386.9 | 12.449 | 16.598 | 20.748 | 49.795 | 57.407 | 86.603 |
|  | 91290.3 | 12.301 | 16.401 | 20.502 | 49.204 | 56.726 | 85.575 |
|  | 90165.8 | 12.149 | 16.199 | 20.249 | 48.598 | 56.027 | 84.521 |
| 36 37 | 89013.8 | 11.994 | 15.992 | 19.990 | 47.977 | 55.311 | 83.442 |
|  | 87834.6 | 11.835 | 15.780 | 19.726 | 47.341 | 54.578 | 82.3:36 |
| 39 | 86628.6 | 11.673 | 15.564 | 19.455 | 46.691 | 53.939 | 81.306 |
| 40 | 85396.1 | 11.507 | 15.342 | 19.178 | 46.027 | 53.0693 | 80.050 |
|  | 84137.4 | 11.337 | 15.116 | 18.895 | 45.349 | 52.281 | 78.870 |
|  | 82853.0 | 11.164 | 14.885 | 18.607 | 44.656 | 51.483 | 77.668 |
|  | 81543.3 | 10.988 | 14.650 | 18.313 | 43.950 | 50.669 | 76.439 |
|  | $80 \geq 08.5$ | 10.808 | 14.410 | 18.013 | 43.231 | 49.840 | 75.187 |
| 44 45 | 78849.1 | 10.625 | 14.166 | 17.708 | 42.498 | 48.995 | 73.913 |

## 702

2.) Lengtif of one degree of the parallel in different measures.

| Degrees. | Metres. | $\begin{aligned} & \text { German } \\ & \text { Miles. } \\ & 15=1^{\circ} \text { Eq. } \end{aligned}$ | $\begin{aligned} & \text { Nautical } \\ & \text { 10:10nes. } \\ & 20=10 \mathrm{Ey} . \end{aligned}$ | $\begin{gathered} \text { French } \\ \text { League. } \\ 20=1^{\circ} \mathrm{Eq} . \end{gathered}$ | Nautical or Geng. Miles. $60=1^{\circ} \mathbf{E}_{1}$ | Statute Miles. | Russian Wersts. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 46 | 77465.6 | 10.438 | 13.918 | 17.397 | 41.753 | 48.135 | 72.616 |
| 47 | 76058.3 | 10.249 | 13.665 | 17.081 | 40.994 | 47.261 | 71.297 |
| 48 | 74627.7 | 10.056 | 13.408 | 16.760 | 40.223 | 46.372 | 69.956 |
| 49 | 73174.1 | 9.860 | 13.147 | 16.433 | 39.440 | 45.469 | 68.593 |
| 50 | 71698.1 | 9.661 | 12.881 | 16.102 | 38.644 |  | 67.210 |
| 51 | 70200.0 | 9.459 | 12.612 | 15.765 | 37.837 | 43.621 | 65.805 |
| 52 | 68680.3 | 9.254 | 12.339 | 15.424 | 37.018 | 42.676 | 64.381 |
| 53 | 67139.5 | 9.047 | 12.062 | 15.078 | 36.187 | 41.719 | 62.937 |
| 54 | 45.578 .1 | 8.836 | 11.782 | 14.727 | 35.346 | 41.749 | 61.473 |
| 55 | 63996.4 | 8.623 | 11.498 | 14.372 | 34.493 | 39.766 | 59.990 |
| 56 | 1523:5.0 | 8.407 | 11.210 | 14.013 | 33.630 | 38.771 | 58.489 |
| 57 | 60\%74.4 | 8.189 | 10.919 | 13.649 | 32.757 | 37.764 | 56.970 |
| 58 | 59185.1 | 7.968 | 10.624 | 13.280 | 31.673 | 36.745 | 55.433 |
| 59 | 57478.5 | 7.745 | 10.326 | 12.908 | 30.979 | 35.715 | 53.679 |
| 60 | 55502.2 | 7.519 | 10.025 | 12.532 | 30.076 | 34.674 | 52.309 |
| 61 | 54109.4 | 7.291 | 9.721 | 12.152 | 29.164 | 33.622 | 50.722 |
| 62 | 52400.3 | 7.061 | 9.414 | 11.768 | 28.243 | 32.560 | 49.120 |
| 63 | 50674.9 | 6.828 | 9.104 | 11.380 | 27.313 | 31.488 | 47.503 |
| 64 | 48.338 .7 | 6.594 | 8.791 | 10.989 | 26.374 | 30.406 | 45.870 |
| 65 | 47177.5 | 6.357 | 8.476 | 10.595 | 25.428 | 29.315 | 44.224 |
| 66 | 45406.6 | 6.118 | 8.158 | 10.197 | 24.473 | 28.215 | 42.564 |
| 67 | 43621.7 | 5.878 | 7.837 | 9.796 | 23.511 | 27.106 | 40.691 |
| 68 | 41823.3 | 5.636 | 7.514 | 9.392 | 22.542 | 25.988 | 39.205 |
| 69 | 40012.0 | 5.391 | 7.189 | 8.986 | 21.566 | 24.862 | 37.507 |
| 70 | 38158.2 | 5.146 | 6.861 | 8.576 | 20.583 | 23.729 | 35.780 |
| 71 | 36352.6 | 4.898 | 6.531 | 8.164 | 19.593 | 22.589 | 34.077 |
| 72 | 34505.8 | 4.649 | 6.199 | 7.749 | 18.598 | 21.441 | 32.346 |
| 73 | 32445.2 | 4.399 | 5.866 | 7.332 | 17.597 | 20.287 | 30.604 |
| 74 | 30780.5 | 4.148 | 5.530 | 6.913 | 16.590 | 19.126 | 28.854 |
| 75 | 28903.3 | 3.595 | 5.193 | 6.491 | 15.578 | 17.960 | 27.094 |
| 76 | 27017.1 | 3.640 | 4.854 | 6.067 | 14.542 | 16.788 | 25.326 |
| 77 | 25122.5 | 3.385 | 4.514 | 5.642 | 13.541 | 15.611 | 23.550 |
| 78 | 23200.2 | 3.129 | 4.172 | 5.215 | 12.515 | 14.428 | 21.767 |
| 79 | 21310.6 | 2.872 | 3.829 | 4.786 | 11.486 | 13.242 | 19.977 |
| 80 | 19394.4 | 2.613 | 3.484 | 4.356 | 10.453 | 12.051 | 18.1 と0 |
| 81 | 17472.2 | 2.354 | 3.139 | 3.924 | 9.417 | 10.857 | 16.378 |
| 82 | 15544.5 | 2.095 | 2.793 | 3.491 | 8.378 | 9.659 | 14.571 |
| 83 | 13612.0 | 1.834 | 2.446 | 3.057 | 7.337 | 8.458 | 12.760 |
| 84 | 11675.3 | 1.573 | 2.098 | 2.622 | 6.293 | 7.255 | 10.944 |
| 85 | 9735.0 | 1.312 | 1.749 | 2.186 | 5.247 | 6.049 | 9.126 |
| 86 | 7791.6 | 1.0511 | 1.400 | 1.750 | 4.200 | 4.841 | 7.304 |
| 87 | 5845.8 | 0.788 | 1.050 | 1.313 | 3.151 | 3.632 | 5.480 |
| 88 | 3898.2 | 0.525 | 0.700 | 0.875 | 2.101 | 2.422 | 3.654 |
| 89 | 1949.4 | 0.263 | 0.350 | 0.438 | 1.051 | 1.211 | 1.827 |
| 90 | 0. | 0. | 0. | 0. | 0 . | 0. | 0. |
|  |  |  |  |  |  |  |  |

## VII. tables for computing terrestrial surfaces.

These tables replace a similar set in the earlier edition, which were published first by Delcros in the Anmuaire Météorologique de la France pour 1850, p. 6is et seq. In the following tables the dimensions assumed for the earth are those of Clarke's spheroid of revolution of 1866 (see table, p. G 14 et sec.)

The formula from which the tables have been computed reads as follows :-

$$
\mathrm{S}=\frac{a b \pi}{90}\left\{\begin{array}{l}
\sin \frac{1}{2} \phi \cos \left(\mathrm{~L}+\frac{1}{2} \phi\right) \\
-\frac{1}{3}\left[2\left(\frac{a-b}{a+b}\right)+\left(\frac{a-b}{a+b}\right)^{2}\right] \sin \left(\phi+\frac{1}{2} \phi\right) \cos \left[3 \mathrm{~L}+\left(\phi+\frac{1}{2} \phi\right)\right] \\
+\frac{1}{5}\left[3\left(\frac{a-b}{a+b}\right)^{2}+\left(\frac{a-b}{a+b}\right)^{3}\right] \sin \left(2 \phi+\frac{1}{2} \phi\right) \cos \left[5 \mathrm{~L}+\left(2 \phi+\frac{1}{2} \phi\right)\right] \\
- \text { elc: }
\end{array}\right.
$$

in which $a$ and $b$ are the semi-axes, L and $\mathrm{L}^{\prime}$ the latitudes of the upper and lower limits of the quadrilateral surface respectively, $\phi=\mathrm{L}^{\prime}-\mathrm{L}$. Substituting numerical values, we have for surface of one degree

$$
\mathrm{S}=\left\{\begin{array}{l}
224.996175 \cos \left(\mathrm{~L}+0^{\circ} 30^{\prime}\right) \\
-0.764620 \cos \left(3 \mathrm{~L}+1^{\circ} 30^{\prime}\right) \\
+0.001946 \cos \left(5 \mathrm{~L}+2^{\circ} 30^{\prime}\right) \\
+ \text { etc. }
\end{array}\right.
$$

As in the tables in the earlier edition the numbers are given in square miles the linear base of which is a mile equal to $\frac{1}{1}$ a of the mean degree of the meridian. That mile is thus $\frac{10001888.2}{90 \times 15}=7408.806$ metres, log. 3.86974822 . In order to convert these results into geographical miles, $60=1^{\circ}$ equator, multiply by 15.9458 .27 , log. 1.20264706 ; into French leagues, $25=1^{\circ}$ equator, multiply by 2.768371 , log. 0.44222458 ; into nautical leagues, $20 \doteq 1^{\circ}$ equator, multiply by 1.771759 , log. 0.24840456 ; into German miles, $15=1^{\circ}$ equator, multiply by 0.996614 , log. 9.99852708 ; into English statute miles, multiply by 21.193684 , $\log .1 .32620646$.

## Use of the Tables.

Table I., which gives the number of square miles contained in the quadrilateral surfaces of one degree in latitnde and longitude, successively from the equator to the pole, will be more frequently used. Table II. has been computed for maps on a smaller scale; and Tables III. and IV. for maps of very small scale, covering large areas, in which surfaces of one degree could not be estimated with sufficient accuracy. If the scale is large enough to have the minntes traced on, then Table V. is to be used. For computing a surface by Table I., which may serve as an example for all the others, find first the lowest parallel circle which crosses, on the map, the surface to be estimated; suppose it is $40^{\circ}$ lat. N., and the zone within $40^{\circ}$ and $41^{\circ}$ lat. N. contains four integral degrees of longitude, that is, four surfaces of one degree each way; then in the tirst column of the table, on the line beginning with latitude $40^{\circ}$, and in the vertical column headed 4 , take the value of these fonr surfaces, viz. 685.94. Then take likewise the valne of the number of surfaces between $41^{\circ}$ and 420 lat. N., and so on. The fractional parts left outside of the integral degrees are best estimated, with the compass, in decimals, the values of which can be fonnd in the columns of the multiples, by properly moving the decimal point to the left. Having taken them in that way, and summing them up with all the integral surfaces, we obtain the total surface required.

Table 1,) Quaphlateral Surfaces of 1 Deghee ix Latitude and in Longltude on the Terrestrial Ellipsehd.

| $\begin{aligned} & \text { Limiting } \\ & \text { Latitudes. } \end{aligned}$ |  | Multiples of these Qudrilateral surfaces from $\mathbf{1}$ to $\mathbf{9}$. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\operatorname{lnf}$. | Sup. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | s. | 9. |
| 0 | 1 | 224.225 | 448.45 | 672.68 | 896.90 | 1121.13 | 1345.35 | 1569.58 | 1793.81 | 2018.03 |
| 1 | 2 | 224.154 | 448.32 | 672.45 | 896.63 | 1120.79 | 1344.95 | 1569.11 | 1793.27 | 2017.43 |
| $\because$ | 3 | 224.026 | 448.05 | 67.2 .08 | 896.10 | 1120.13 | 1344.15 | 1568.18 | 1792.21 | 2016.23 |
| 3 | 4 | 233.827 | 447.65 | 671.45 | 895.31 | 1119.13 | 1342.96 | 1566.79 | 1790.61 | 2014.44 |
| 4 | 5 | 223.561 | 447.12 | 670.68 | 894.24 | 1117.80 | 1341.36 | 1564.93 | 17 -8.49 | 2012.05 |
| 5 | 6 | 223.229 | 446.46 | 669.69 | 8.92 .92 | 111614 | 133:.37 | 1542.60 | 1785.83 | 2009.06 |
| 6 | 7 | 22.831 | 445.66 | 668.49 | 631.32 | 1114.15 | 1336.98 | 1559.*1 | 1782.6.4 | 2005.48 |
| 7 | $\checkmark$ | 222.36 | 44.73 | 667.10 | 859.47 | 1111.83 | 1334.20 | 1556.59 | 1775.13 | 2001.30 |
| 8 | 9 | 221.836 | 443.67 | 665.51 | 887.34 | 1109.18 | 1331.02 | 1552.05 | 1774.69 | 1996.52 |
| 9 | 10 | 221.240 | 442.48 | 663.72 | 884.96 | 1106.20 | 1327.44 | 1548.68 | 1769.92 | 1991.16 |
| 10 | 11 | 220.575 | 441.16 | 661.73 | 882.31 | 1102.89 | 1323.47 | 1544.04 | 1764.62 | 1985.20 |
| 11 | 12 | 219.650 | 439.70 | (0.9.55) | 879.40 | 1099.25 | 1319.1 | 1535.95 | 1758.80 | 1978.65 |
| 12 | 13 | 219.05 | 438.11 | 637.17 | 876.33 | 1095.29 | 1314.34 | 1533.40 | 1752.46 | 1971.51 |
| 13 | 14 | 215.199 | 436.40 | 65.460 | 872.80 | 1090.49 | 1304.19 | 1527.39 | 1745.59 | 1963.79 |
| 14 | 15 | 21 | 434.55 | . 6.51 .83 | 869.10 | 10868.38 | 1303.65 | 1500.93 | 1738.20 | 1955.46 |
| 15 | 16 | 21 | 432.57 | 649.86 | 865.15 | 10.1 .44 | 1297.72 | 1514.01 | 1730.30 | 1946.58 |
| 16 | 17 | 215.204 | 430.17 | 645.70 | 860.94 | 1076.17 | 1291.41 | 1506.64 | 1721.88 | 1983.11 |
| 17 | 13 | 214.117 | 428.23 | 642.35 | 856.47 | 1070.5! | 1284.70 | 1498.82 | 1712.94 | . 06 |
| 18 | 19 | $\because 12.936$ | 425.87 | 638.81 | 851.74 | 10164.68 | 1277.62 | 1490.55 | 1763.49 | 1315.42 |
| 19 | 20 | 211.61 | 423.38 | 1855.07 | 846.7 | 1058.45 | 1270.15 | 1481.E4 | $16: 33.53$ | 1905.22 |
| 20 | 21 | 210.382 | 420.76 | 631.15 | 8 | 10.51 .91 | 1212.29 | 1472.68 | 1683.06 | 1893.44 |
| 21 | $\therefore 2$ | 209.01 J | 415.02 | 627.03 | 836.04 | 1045.05 | 1254.06 | 1463.17 | 1672.48 | 1881.10 |
| 22 | $\because 3$ | 207.576 | 415.15 | 622.73 | 830.30 | 1037.85 | 1245.46 | 1453.03 | 1660.61 | 1868.18 |
| 23 | $\because 4$ | 206.079 | +12.16 | 618.24 | 1.3 | 1030.39 | 12365.47 | 1443.55 | 1648.63 | 1854.71 |
| 24 | 25 | 204.519 | 400. 0.4 | 613.56 | 818.08 | 1022.60 | 1227.12 | 1431.64 | 1636.16 | 7 |
| 25 | 21 | 202 | 4 | 608.70 | 59 | 1014.49 | 1217.39 | 1420.29 | 1623.19 | . 09 |
| $2 ;$ | 27 | 211.216 | 40.2 .3 | 603.65 | $804.86^{\circ}$ | 1006.08 | 1207.30 | 1408.51 | 1609.73 | 810.95 |
| 27 | 28 | 199.473 | $3!心 .9 \%$ | 548.42 | 797.ヶ9 | 097.36 | 1196.84 | 1396.31 | 1595.78 | 1795.26 |
| $\because 8$ | $2!$ | 197.469 | 395.34 | 593.01 | 790.65 | 988.34 | 1186.01 | 1383.68 | 16 b 1.35 | 1779.02 |
| $\because 9$ | 30 | 195.805 | 391.6] | 587.42 | 783.22 | 979.03 | 1174.83 | 1370.64 | 15664.44 | 5 |
| 30 | 31 | 193.852 | 35 | 4 | 775.53 | 969.41 | 1163.29 | 1357.17 |  | 93 |
| 31 | 32 | 191.599 | 383.60 | 575.70 | 767.60 | 959.49 | 1151.39 | 1343.29 | 15:5. 19 | 1727.09 |
| 32 | 33 | 159.55 | 379.72 | 569.57 | 759.43 | 949.29 | $113!5$ | 1329.00 | 1518.86 | 1708.72 |
| 33 | 34 | 187.759 | 375.52 | 563.25 | 751.03 | 938.79 | 1106.55 | 1314.31 | 1509.07 | 1689.83 |
| 34 | 35 | 185.602 | 371.20 | 556.81 | 742.41 | 92.2 .01 | 1113.61 | 1299.21 | 1404.80 | 670.42 |
| 35 | 36 | 183.388 | 366.78 | 550.16 | 733.55 | 916.94 | $1100.3: 3$ | 1283.72 | 1467.11 | 1650.49 |
| 36 | 37 | 181.118 | 362.24 | 543.35 | 724.47 | 905.59 | 1086.71 | 1267.83 | 1445.94 | 1630.06 |
| 37 | 38 | 178.792 | 357.58 | 536.35 | 715.17 | 893.96 | 1072.75 | 123.5\% | 14:0.34 | 1609.13 |
| 38 | 39 | 176.411 | 352.82 | 529.23 | 705.64 | 88.005 | 10.54 .46 | 129458 | 1411.20 | 1587.70 |
| 39 | 40 | 173.976 | 347.95 | 521.93 | 095.90 | 869.88 | 1043. 5 | 1217.83 | 1391.80 | 1565.78 |
| 40 | 41 | 171.456 | $3 \pm 2.97$ | 514.46 | 685.94 | 857.43 | 1025.92 | 1200.49 | 1371.89 | 1543.37 |
| 41 | 42 | 168.943 | 337.89 | 506.83 | 675.77 | 84.72 | 1013.66 | 1152.60 | 1351.55 | 1520.49 |
| 42 | 43 | 166.34 | 33:2.70 | 499.05 | 665.39 | 831.74 | 998.09 | 11ti4.44 | 1330.79 | 1497.14 |
| 43 | 44 | 163.701 | 327.40 | 491.10 | 654.81 | 818.51 | 98.21 | 1145.91 | 1309.61 | 1473.31 |
| 4 | 4.) | 161.003 | 322.01 | 483.01 | 644.01 | 0.05 .02 | 966.02 | 1107.02 | 1288.03 | 1449.03 |

TABLE 1.) (Concluded) Quadrifateral Surfaces of 1 Degree in Latitude and in Longitude un the 'Terrestrial Ehhisulib.

| Limiting <br> Latitudes. |  | Multiples of these Quadrilateral Surfaces from 1 to 9. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inf. | Sup. | 1. | 2. | 3. | 4. | 5. | 6. | 7. | S. | 9. |
| 45 | 46 | 158.255 | 316.51 | 474.77 | 633.02 | 791.28 | 949.53 | 1107.79 | 1266.04 | 1424.30 |
| 46 | 47 | 155.457 | 310.91 | 466.37 | 621.83 | 777.29 | 932.74 | 1088.20 | 1243.66 | 1399.12 |
| 47 | 48 | 152.611 | 305.22 | 457.83 | 610.44 | 763.05 | 915.66 | 1068.27 | 1220. 89 | 1373.50 |
| 48 | 49 | 149.716 | 299.43 | 449.15 | 598.86 | 748.58 | 898.30 | 1048.01 | 1197.73 | 1347.45 |
| 49 | 50 | 146.775 | 293.55 | 440.32 | 587.10 | 733.87 | 880.65 | 1027.42 | 1174.20 | 1320.97 |
| 50 | 51 | 143.787 | 287.57 | 431.36 | 575.15 | 718.93 | 862.72 | 1006.51 | 1150.29 | 1294.08 |
| 51 | 52 | 140.753 | 281.51 | 422.26 | 563.01 | 703.77 | 844.52 | 985.27 | 1126.02 | 1266.78 |
| 52 | 53 | 137.675 | 275.35 | 413.03 | 550.70 | 688.38 | 826.05 | 963.73 | 1101.40 | 1239.08 |
| 53 | 54 | 134.554 | 269.11 | 403.66 | 538.21 | 67.37 | 807.32 | 941.88 | 1076.43 | 1210.98 |
| 54 | 55 | 131.389 | 262.78 | 394.17 | 525.56 | 656.95 | 788.33 | 919.72 | 1051.11 | 1182.50 |
| 55 | 56 | 128.183 | 256.37 | 384.55 | 512.73 | 640.91 | 769.10 | 897.28 | 1025.46 | 1153.65 |
| 56 | 57 | 124.936 | 249.87 | 374.81 | 499.74 | 624.68 | 749.62 | 874.55 | 999.49 | 1124.42 |
| 57 | 58 | 121.649 | 243.30 | 364.95 | 486.60 | 608.24 | 729.89 | 851.54 | 973.19 | 1094.84 |
| 58 | 59 | 118.323 | 236.65 | 354.97 | 473.29 | 591.62 | 709.94 | 828.26 | 946.59 | 1064.91 |
| 59 | 60 | 114.959 | 229.92 | 344.88 | 459.84 | 574.80 | 689.76 | 804.72 | 919.68 | 1034.63 |
| 60 | 61 | 111.559 | 223.12 | 334.68 | 446.24 | 557.79 | 669.35 | 780.91 | 892.47 | 1004.03 |
| 61 | 62 | 108.122 | 216.24 | 324.37 | 432.49 | 540.61 | 648.73 | 756.86 | 864.98 | 973.10 |
| 62 | 63 | 104.651 | 209.30 | 313.95 | 418.60 | 523.26 | 627.91 | 732.56 | 837.21 | 941.86 |
| 63 | 64 | 101.146 | 202.29 | 303.44 | 40.4 .58 | 505.73 | 606.88 | 70.02 | 809.17 | 910.31 |
| 64 | 65 | 97.608 | 195.22 | 292.83 | 390.43 | 488.04 | 585.65 | 683.26 | 780.87 | 878.48 |
| 65 | 66 | 94.039 | 188.08 | 282.12 | 376.16 | 470.20 | 564.23 | 658.27 | 752.31 | 846.35 |
| 66 | 67 | 90.440 | 180.88 | 271.32 | 361.76 | 452.20 | 542.64 | 633.08 | 723.52 | 813.96 |
| 67 | 68 | 86.811 | 173.62 | 260.43 | 347.24 | 434.05 | 520.86 | 607.67 | 694.48 | 781.30 |
| 68 | 69 | 83.153 | 166.31 | 249.46 | 332.61 | 415.77 | 498.92 | 582.07 | 665.23 | 748.38 |
| 69 | 70 | 79.469 | 158.94 | 238.41 | 317.88 | 397.35 | 476.82 | 556.28 | 635.75 | 715.28 |
| 70 | 71 | 75.759 | 151.52 | 227.28 | 303.04 | 378.80 | 454.56 | 530.31 | 606.07 | 681.83 |
| 71 | 72 | 72.024 | 14.05 | 216.07 | 288.10 | 360.12 | 432.15 | 504.17 | 576.19 | 648.22 |
| 72 | 73 | 68.266 | 136.53 | 204.80 | 273.06 | 341.33 | 409.60 | 477.86 | 546.13 | 614.40 |
| 73 | 74 | 64.486 | 128.97 | 193.46 | 257.94 | 322.43 | 386.91 | 451.40 | 515.89 | 580.37 |
| 74 | 75 | 60.684 | 121.37 | 182.05 | 242.74 | 303.42 | 364.10 | 424.79 | 485.47 | 546.16 |
| 75 | 76 | 56.863 | 113.73 | 170.59 | 227.45 | 284.31 | 341.18 | 398.04 | 454.90 | 511.76 |
| 76 | 77 | 53.023 | 106.05 | 159.07 | 212.09 | 265.11 | 318.14 | 371.16 | 424.18 | 477.20 |
| 77 | 78 | 49.165 | 98.33 | 147.50 | 196.66 | 245.83 | 294.99 | 344.16 | 393.32 | 442.49 |
| 78 | 79 | 45.292 | 90.58 | 135.88 | 181.17 | 226.46 | 271.75 | 317.04 | 362.33 | 407.63 |
| 79 | 80 | 41.403 | 82.81 | 124.21 | 165.61 | 207.02 | 248.42 | 289.82 | 331.23 | 372.63 |
| 80 | 81 | 37.501 | 75.00 | 112.50 | 150.01 | 187.51 | 225.01 | 262.51 | 300.01 | 337.51 |
| 81 | 82 | 33.587 | 67.17 | 100.76 | 134.35 | 167.94 | 201.52 | 235.11 | 268.70 | 302.28 |
| 82 | 83 | 29.662 | 59.32 | 88.99 | 118.65 | 148.31 | 177.97 | 207.63 | 237.29 | 266.95 |
| 83 | 84 | 25.727 | 51.45 | 77.18 | 102.91 | 128.63 | 154.36 | 180.09 | 205.81 | 231.54 |
| 84 | 85 | 21.783 | 43.57 | 65.35 | 87.13 | 108.91 | 130.70 | 152.48 | 174.26 | 196.05 |
| 85 | 86 | 17.832 | 35.66 | 53.50 | 71.33 | 89.16 | 106.99 | 124.83 | 142.66 | 160.49 |
| 86 | 87 | 13.876 | 27.75 | 41.63 | 55.50 | 69.38 | 83.25 | 97.13 | 111.00 | 124.88 |
| 87 | 88 | 9.914 | 19.83 | 29.74 | 39.66 | 49.57 | 59.49 | 69.40 | 79.32 | 89.23 |
| 88 | 89 | 5.950 | 11.90 | 17.85 | 23.80 | 29.75 | 35.70 | 41.65 | 47.60 | 53.55 |
| 89 | 90 | 1.984 | 3.97 | 5.95 | 7.93 | 9.92 | 11.90 | 13.89 | 15.87 | 17.85 |

G

TABLE 2.) Quadrilateral Surfaces of 2 Degrees in Latitude and in Lungitude on the Terrestrial kllifsuid.

| Limiting Latitudes. |  | Multiples of these Quadrilateral Surfaces from 1 to 9. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inf. | Sup. | 1. | 2. | 3. | . | 5. | 6. | 7. | S. | 9. |
| 0 | 2 | 896.7 | 1793.54 | 2690.30 | 35 | 4483.84 | 5380.61 | 6277.37 | 7174.14 |  |
| 2 | 4 | 895.705 | 1791.41 | 2687.11 | 3582.82 | 4478.52 | 5374.23 | 6269.93 | 7165.64 | 8061.34 |
| 4 | 6 | 893.579 | 1787.16 | 2680.74 | 3574.32 | 4467.90 | 5361.48 | 6255.06 | 7148.64 | 8042.21 |
| 6 | 8 | 890.394 | 1780.79 | 2671.18 | 3561.58 | 4451.97 | 5342.36 | 6232.76 | 7123.15 | 8013.55 |
| 8 | 10 | 886.1 | 1772.30 | 2658.46 | 3544.61 | 4430.76 | 5316.91 | 6203.06 | 7089.21 | 7975.37 |
| 10 | 12 | 880 | 1761.71 | 2642.57 | 3523.42 | 4404.28 | 5285.14 | 6165.99 | 7046.85 | 7927.71 |
| 12 | 14 | 574.512 | 1749.02 | 2623.54 | 3498.05 | 4372. | 5247.07 | 6121.58 | 6996.09 | 7870.61 |
| 14 | 16 | 867.10. | 1734.25 | 2601.38 | 3468.50 | 4335.63 | 5202.75 | 6069.88 | 6937.00 | 7804.13 |
| 16 | 18 | 855.70 | 1717.41 | 2576.11 | 3434.81 | 4293.52 | 5152.22 | 6010.92 | 6869.63 | 7728.33 |
| 18 | 20 | 849.254 | 1698.51 | 2547.76 | 3397.02 | 4246.27 | 5095.52 | 5944.78 | 6794.03 | 7643.28 |
| 20 | 22 | 838.7 | 1677.57 | 2516.36 | 3355.14 | 4193.93 | 5032.72 | 5871.50 | 6710.29 | 7549.07 |
| 22 | 24 | 8.27 .3 | 1654.62 | 2481.93 | 3309.24 | 4136.55 | 4963.86 | 5791.17 | 6618.48 | 7445.79 |
| 24 | 26 | 814.83 | 1629.67 | 2444.51 | 3259.34 | 4074.18 | 4889.01 | 5703.85 | 6518.68 | 7333.52 |
| 26 | $\pm 8$ | 801.37 | 1602.76 | 2404.13 | 3205.51 | 4006.89 | 4808.27 | 5 | 6411.02 | 7212.40 |
| 28 | 30 | 78 | 1573.90 | 2360.84 | 3147.76 | 3934.74 | 4721.69 | 5508.64 | 6295.59 | 7082.53 |
| 30 | 32 | 771 | 1 | 2314.68 | 3086.24 | 3557.81 | 4629.37 | 5400.93 |  | 6944.05 |
| 32 | 34 | 75... | 15 | 2265.70 | 3021.93 | 3776.16 | 4531.40 | 5286.63 | 6041.86 | 6797.09 |
| 34 | 36 | 73 | 1 | 2213.94 | 29 | 3689.90 | $4 \pm 27$. | 5165.86 | 5903.84 | 6641.82 |
| 36 | 38 | 719.8 | 1439.64 | 21 |  | 3599.10 | 4318.92 | 5038.74 | 6 |  |
| 38 | 40 | 700. | 14 | 21 | 2 | 3503.87 | 4204.64 | 4905.41 | 5606.19 | 96 |
| 40 | 42 | 68 |  |  |  | 3404.30 | 4085.15 | 4766.01 | 5446.57 | 73 |
| 42 | 4 | 660.100 | 1320. | 1980.30 | 2640. | 3300.50 | 3960.60 | 4620.70 | 5280.80 | 5940.90 |
| 44 | 46 | 638.517 | 1277.03 | 1915.55 | 2554.07 | 3192.59 | 3831.10 | 4469.62 | 5108.14 | 5746.65 |
| 46 | 48 | 616.136 | 1232.27 | 1848.41 | 2464 | 3080.68 | 3696.82 | 4312.95 | 4929.09 | 5545.22 |
| 48 | 50 | 592.982 | 1185.96 | 1778.94 | 2371.93 | 2964.91 | 3557.89 | 4150.87 | 4743.85 | 336.83 |
| 50 | 52 | 569.07 | 1138.16 | 1707.24 | 2276.32 | 2845.40 | 3414.48 | 3983.56 | 4552.64 | 11 |
| 52 | 54 | 544.457 | 1088.91 | 1633.37 | 2177.83 | 2722.29 | 3266.74 | 3811.20 | 4355.66 | 4900.12 |
| 54 | 56 | 519.144 | 1038.39 | 1557.43 | 20 | 2595.72 | 3114.87 | 3634.01 | 4153.15 | 4672.30 |
| 56 | 58 | 493.17 | . 3 | 1 | ¢ | 2465.85 | 2959.02 | 3452.19 | 3945.36 | 4438.53 |
| 58 | 60 | 466.565 | 933.13 | 13 | 1 | $233 \pm .83$ | 2799.39 | 3265.96 | 3732.52 | 9 |
| 60 | 62 | 439.363 | 8.73 | 1318.09 | 1757.45 | 2196.81 | 2636.18 | 3075.54 | 3514.90 |  |
| 62 | 64 | 411.594 | 823.19 | 1234.78 | 1646.38 | 2057.97 | 2469.57 | 2881.16 | 3292.75 | 3704.35 |
| 64 | 66 | 35 | 766.59 | 1149.88 | 15 | 1916.47 | 2299.77 | 2683.06 | 3066.36 | 3449.65 |
| 66 | 68 | 354.500 | 709.00 | 1063.50 | 1418.00 | 1772.50 | 2127.00 | 2481.50 | 2836.00 | 3190.50 |
| 68 | 70 | 32.5 .245 | 650.49 | 975.74 | 1300.98 | 1626.23 | 1951.47 | 2276.72 | 2601.96 |  |
| 70 | 72 | 295.567 | 591.13 | 886.70 | 1182.27 | 1477.83 | 1773.40 | 2068.97 | 2364.54 | 2660.10 |
| 72 | 74 | 265.504 | 531.01 | 796.51 | 1062.02 | 1327.53 | 1593.02 | 1858.53 | 2124.03 | 2359.53 |
| 74 | 76 | 235.09 | 470.19 | 705.28 | 940 | 1175. | 1410.56 | 1645.66 | 1880.75 | 2115.84 |
| 76 | 78 | 204.376 | 408.75 | 613.13 | 0 | 1021.68 | 1226.26 | 1430.63 | 1635.01 | 38 |
| 78 | 80 | 173.390 | 346.78 | 520.17 | 693.56 | 866.95 | 1040.34 | 1213.73 | 1387.12 | 1560.51 |
| 80 | 82 | 142.177 | 284.35 | 426.53 | 568.71 | 710.88 | 853.06 | 995.24 | 1137.41 | 1279.59 |
| 82 | 84 | 110.737 | 221.55 | 332.33 | 443.11 | 553.88 | 664.66 | 775.44 | 886.21 | 996.99 |
| 54 | 86 | 79.230 | 158.46 | 237.69 | 316. | 396.15 | 475.38 | 554.41 | 633.84 | 713.07 |
| 86 | 88 | 47.580 | 95.16 | 142.74 | 190.32 | 237.90 | 285.45 | 333.06 | 380.64 | 428.22 |
| 88 | 90 | 15.867 | 31.73 | 47.60 | 63.47 | 79.34 | 95.20 | 111.07 | 126.94 | 142.80 |

TABLE 3.) Quadrilateral Surfaces of 5 Degrees in Latitude and in Lungitude un the 'Terrestrial Ellipsuid.

| $\underset{\text { Latitit }}{\text { Limi }}$ | iting, | Multiples of these Quadrilaterai Surfaces from 1 to 9. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iuf. | Sup. | 1. | 2. | 3. | 4. | 5. | 6. | $\%$ | s. | 9. |
| 0 | 5 | 5598.9851 | 11197.97 | 16796.96 | 22395.94 | 27994.93 | 33593.91 | 39192.90 | 44791.88 | 50390.87 |
| 5 | 10 | 5557.5091 | 11115.021 | 16672.53 | 22230.04 | 27787.55 | 33345.06 | 38902.57 | 44460.07 | 50017.58 |
| 10 | 15 | 5474.7971 | 10949.591 | 16424.39 | 21899.19 | 27373.98 | 32848.78 | 38323.58 | 43798.38 | 49273.17 |
| 15 | 20 | 5351.3291 | 10702.661 | 16053.99 | 21405.32 | 26756.65 | 32107.98 | 37459.30 | 42810.63 | 48161.96 |
| 20 | 25 | 5187.8381 | 10375.681 | 15563.51 | 20751.35 | 25939.19 | 31127.02 | 36314.86 | 41502.70 | 46690.54 |
| 25 | 30 | 4985.307 | 9970.61 | 14955.98 | 19941.23 | 24926.54 | 29911.85 | 34897.15 | 39882.46 | 44867.77 |
| 30 | 35 | 4744.993 | 9489.99 | 14234.98 | 18979.97 | 23724.96 | 28469.96 | 33214.95 | 37959.94 | 42704.94 |
| 35 | 40 | 468.425 | 8936.85 | 13405.271 | 17873.70 | 22342.13 | 26810.55 | 31278.97 | 35747.40 | 40215.82 |
| 40 | 45 | 4157.414 | 8314.83 | 12472.24 | 16629.66 | 20787.07 | 24944.49 | 29101.90 | 33259.31 | 37416.73 |
| 45 | 50 | 3814.070 | '7628.14 | 11422.211 | 15256.28 | 19070.35 | 22884.42 | 26698.49 | 30512.56 | 34326.63 |
| 50 | 55 | 3440.788 | 6881.58 | 10322. 36 | 13763.15 | 17203.94 | 20644.73 | 24085.51 | 27526.30 | 30967.09 |
| 55 | 60 | 3040.252 | 6080.50 | 9120.76 | 12161.01 | 15201.26 | 18241.51 | 21281.78 | 24322.02 | 27362.27 |
| 60 | 65 | 2615.434 | 5230.87 | 7846.301 | 10461.74 | 13077.17 | 15692.60 | 18308.04 | 20923.47 | 23538.91 |
| 65 | 70 | 2169.559 | 4339.12 | 6503.68 | 8678.24 | 10847.79 | 13017.35 | 15186.91 | 17356.47 | 19526.03 |
| 70 | 75 | 1706.098 | 3412.20 | 5118.29 | 6824.39 | 8530.49 | 10236.59 | 11942.69 | 13648.78 | 15354.88 |
| 75 | 80 | 1228.729 | 2457.46 | 3686.19 | 4914.92 | 6143.65 | 7372.37 | 8601.10 | 9829.83 | 11058.56 |
| 80 | 85 | 741.298 | 1482.60 | 2223.89 | 2965.19 | 3706.49 | 4447.79 | 5189.09 | 5930.38 | 6671.68 |
| 85 | 90 | 247.779 | 495.56 | 743.34 | 991.12 | 1238.90 | 1486.67 | 1734.45 | 1982.23 | 2230.01 |

## TABLE 4.) Quadrilateral Surfaces of 10 Degrees in Latitude and in Longitule on the Terrestrial Ellipsoid.



TABLE 5.) Mean Quadrilateral Surfaces of 1, 10, 20, and 30 Minutes in Latitude ani, in Longitude deduced from each Quadrilateral of 1 Degree in T'able 1.)


## COMPARISON

of The

# STANDARDS OF LENGTH 

OF

ENGLAND, FRANCE, BELGIUM, PRUSSSLA, RUSSIA, INDIA, AND ALSTRALIA,

MADE AT

THE ORDNANCE SURVEY OFFICE, SOUTHAMPTON.

BY
Captain A. R. CLARKE, R.E., F.R.S.,

UNDER THE DIRECTION OF

Colonel Sir HENRY JAMES, R.E., F.R.S., etc., director of ordnance surver.


## IX. Tables for finding tie Length of Tine of Insolation for any Latitude, and for any Day of the Year.

The formula for computing the length of time of daily solar illumination are obtained as follows :-

Let $P^{\prime \prime}$ be the north pole (celestial), $S$ the true place of the sun's centre when that centre is bronght by refraction to the hori-
 zon of the place, and let $Z$ be the zenith of the place.
Let $\delta=$ the north declination of the sun (negative when south)

$$
\begin{aligned}
& =90^{\circ}-P S \\
& =90^{\circ}-P Z \\
& =Z S-90^{\circ}
\end{aligned}
$$

$l=$ the norti latitude of the place
(negative when south)
$r=$ the horizontal refraction
$h=$ the hour angle $Z P S$.
We have $\quad \cos Z S=\cos P Z \cos P S+\sin P Z \sin P S \cos Z P S$.
Or $\quad-\sin r \quad=\sin l \sin \delta+\cos l \cos \delta \cos h$
Also $\quad \cos (l-\delta)=\cos l \cos \delta+\sin l \sin \delta$
$\cos (l+\delta)=\cos l \cos \delta-\sin l \sin \delta$
Subtract [1] from [2], and add [1] to [8].

$$
\begin{aligned}
& \cos (l-\delta)+\sin r=\cos l \cos \delta(1-\cos h)=2 \cos l \cos \delta \sin ^{2} \frac{1}{2} h \\
& \cos (l+\delta)-\sin r=\cos l \cos \delta(1+\cos h)=2 \cos l \cos \delta \cos ^{2} \frac{1}{2} h
\end{aligned} \quad\left[\frac{4}{2}\right]
$$

Observing that $\sin x+\sin y=2 \sin \frac{1}{2}(x+y) \cos \frac{1}{2}(x-y)$ the two last equations give us

$$
\begin{align*}
& \sin ^{2} \frac{1}{2} h=\frac{\sin \left(45^{\circ}-\frac{1}{2} l+\frac{1}{2} \delta+\frac{1}{2} r\right) \cos \left(45^{\circ}-\frac{1}{2} l+\frac{1}{2} \delta-\frac{1}{2} r\right)}{\cos l \cos \delta}  \tag{6}\\
& \cos ^{2} \frac{1}{2} h=\frac{\sin \left(45^{\circ}-\frac{1}{2} l-\frac{1}{2} \delta-\frac{1}{2} r\right) \cos \left(45^{\circ}-\frac{1}{2} l-\frac{1}{2} \delta+\frac{1}{2} r\right)}{\cos l \cos \delta} \tag{7}
\end{align*}
$$

which are the formula used in computing the tables.
The refraction has been assumed to be $34^{\prime}$.
The declinations used are from the Nautical Almanac for 1862, for Greenwich mean noon; except in finding the limiting date when the sun's centre does not go below the horizon throughout the whole day, in which case the midnight declination hats been used.

A supplementary table is given by the aid of which the main table may be used for southern as well as northern latitudes.

The use of the main table may be illustrated by the following example:-
Find the time of insolation for May 13th, latitude $43^{\circ}-30 \mathrm{~N}$.

| May 11th, lat. $42^{\circ}$ | $=14^{\mathrm{h}} .37$ | May 11 th, lat. $44^{\circ}=14^{\mathrm{h}} .54$ |
| :--- | :--- | :--- |
| $\frac{2}{2}$ diff. to May 16 th, | $=+.07$ | $\frac{2}{5}$ 恀. to May $16 \mathrm{th}=+.07$ |
| May 13 th, lat. $42^{\circ}$ | $=14^{\mathrm{h}} .44$ | May 13 th, lat. $44^{\circ}=14^{\mathrm{h}} .61$ |
| $\frac{5}{4}$ diff. $42^{\circ}$ to $44^{\circ}$ | $=+.13$ | Diff. lat. 42 to $44^{\circ}=0^{\mathrm{h}} .17$ |

May 13th, lat. $43^{\circ}-30=14^{\mathrm{h}} .57 \mathrm{ans}$.
The use of the supplementary table is sufficiently plain. For example: To find the time of insolation for Jannary 6 th in any south latitude, add the tabular number 1 d .97 to the corresponding date of July; with the latter and the latitude of the place (regarding it as north instead of south) as arguments, the required time of insolation may at once be found.

| DATE. | Latitude North. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | $5^{\circ}$ | 80 | $\underline{120}$ | $16^{\circ}$ | $20^{\circ}$ | 210 | $28^{\circ}$ | $3{ }^{12}$ | $36^{\circ}$ | $10^{\circ}$ |
| January $\begin{aligned} & \text { J } \\ & 1 \\ & 1 \\ & 2 \\ & 2\end{aligned}$ | 12 hb .08 | $11^{\text {h. }} 86$ | $11^{\mathrm{h}} .63$ | $11^{\mathrm{h}} .39$ | $11^{\mathrm{h}} .15$ | $10^{\mathrm{h}} .90$ | $10^{\text {h }} .63$ | $10^{\mathrm{h}} .35$ | $10^{\text {b }} .04$ | $9^{\text {b }} .70$ | $9^{\text {b }} .32$ |
|  | 12.08 | 11.86 | 11.64 | 11.41 | 11.18 | 10.93 | 10.67 | 10.40 | 10.10 | 9.77 | 9.40 |
|  | 12.08 | 11.87 | 11.65 | 11.43 | 11.21 | 10.97 | 10.72 | 10.46 | 10.17 | 9.85 | 9.50 |
|  | 12.08 | 11.88 | 11.67 | 11.46 | 11.25 | 11.02 | 10.78 | 10.53 | 10.25 | 9.95 | 9.62 |
|  | 12.08 | 11.89 | 11.69 | 11.49 | 11.29 | 11.08 | 10.55 | 10.61 | 10.35 | 10.07 | 9.75 |
|  | 12.08 | 11.90 | 11.72 | 11.53 | 11.34 | 11.14 | 10.93 | 10.71 | 10.47 | 10.21 | 9.91 |
| February $\begin{array}{r}\text { r } \\ \\ 1 \\ 1 \\ 2 \\ 2\end{array}$ | 12.08 | 11.92 | 11.75 | 11.58 | 11.41 | 11.23 | 11.04 | 10.84 | 10.62 | 10.38 | 10.11 |
|  | 12.08 | 11.93 | 11.78 | 11.63 | 11.47 | 11.30 | 11.13 | 10.95 | 10.75 | 10.54 | 10.30 |
|  | 12.08 | 11.95 | 11.81 | 11.67 | 11.53 | 11.38 | 11.83 | 11.07 | 10.90 | 10.71 | 10.50 |
|  | 12.08 | 11.96 | 11.84 | 11.72 | 11.60 | 11.47 | 11.34 | 11.20 | 11.05 | 10.88 | 10.70 |
|  | 12.08 | 11.98 | 11.88 | 11.78 | 11.67 | 11.56 | 11.45 | 11.33 | 11.20 | 11.06 | 10.91 |
|  | 12.08 | 12.00 | 11.91 | 11.83 | 11.74 | 11.65 | 11.56 | 11.46 | 11.36 | 11.24 | 11.12 |
| March | 12.08 | 12.01 | 11.94 | 11.87 | 11.79 | 11.71 | 11.63 | 11.55 | 11.46 | 11.36 | 11.25 |
|  | 12.08 | 12.03 | 11.97 | 11.92 | 11.86 | 11.80 | 11.75 | 11.69 | 11.62 | 11.54 | 11.46 |
|  | 12.08 | 12.14 | 12.01 | 11.98 | 11.94 | 11.90 | 11.86 | 11.82 | 11.78 | 11.73 | 11.68 |
|  | 12.08 | 12.06 | 12.04 | 12.03 | 12.01 | 12.00 | 11.98 | 11.96 | 11.94 | 11.92 | 11.90 |
|  | 12.08 | 12.08 | 12.08 | 12.08 | 12.09 | 12.10 | 12.10 | 12.11 | 12.11 | 12.12 | 12.13 |
|  | 12.08 | 12.10 | 12.12 | 12.14 | 12.17 | 12.20 | 12.23 | 12.26 | 12.29 | 12.32 | 1235 |
| April | 12.08 | 12.12 | 12.16 | 12.20 | 12.25 | 12.30 | 12.35 | 12.41 | 12.47 | 12.53 | 12.61 |
|  | 12.08 | 12.13 | 12.19 | 12.26 | 12.33 | 12.40 | 12.47 | 12.55 | 12.63 | 12.72 | 12.53 |
|  | 12.05 | 12.15 | 12.23 | 12.31 | 12.40 | 12.49 | 12.58 | 12.68 | 12.79 | 12.91 | 13.04 |
|  | 12.08 | 12.17 | 12.27 | 12.37 | 12.47 | 12.58 | 12.69 | 12.81 | 12.95 | 13.09 | 13.25 |
|  | 12.08 | 12.19 | 12.30 | 12.42 | 12.54 | 12.67 | 12.80 | 12.94 | 13.10 | 13.27 | 13.46 |
|  | 12.08 | 12.21 | 12.34 | 12.48 | 12.62 | 12.76 | 12.90 | 13.07 | 13.25 | 13.44 | 13.66 |
| May | 12.08 | 12.22 | 12.37 | 12.52 | 12.67 | 12.83 | 13.00 | 13.19 | 13.39 | 13.61 | 13.85 |
|  | 12.08 | 12.24 | 12.40 | 12.56 | 12.73 | 12.91 | 13.10 | 13.30 | 13.52 | 13.76 | 14.03 |
|  | 12.08 | 12.25 | 12.43 | 12.61 | 12.79 | 12.9s | 13.19 | 13.41 | 13.65 | 13.91 | 14.20 |
|  | 12.08 | 12.27 | 12.46 | 12.65 | 12.84 | 13.05 | 13.27 | 13.51 | 13.77 | 14.05 | 14.36 |
|  | 12.08 | 12.28 | 12.48 | 12.68 | 12.89 | 13.11 | 13.35 | 13.60 | 13.87 | 14.17 | 14.51 |
|  | 12.08 | 12.29 | 12.50 | 12.71 | 12.93 | 13.17 | 13.42 | 13.68 | 13.96 | 14.28 | 14.64 |
| June $\begin{array}{cc} \\ & \\ & 1 \\ & 1 \\ & 2 \\ & 2\end{array}$ | 12.08 | 12.30 | 12.52 | 12.74 | 12.97 | 13.22 | 13.48 | 13.76 | 14.06 | 14.39 | 14.76 |
|  | 12.05 | 12.30 | 12.53 | 12.76 | 13.00 | 13.25 | 13.52 | 13.81 | 14.12 | 14.46 | 14.85 |
|  | 12.08 | 12.31 | 12.54 | 12.78 | 13.02 | 13.28 | 13.55 | 13.84 | 14.16 | 14.52 | 14.91 |
|  | 12.08 | 12.31 | 12.55 | 12.79 | 13.03 | 13.29 | 13.57 | 13.87 | 14.19 | 14.55 | 14.95 |
|  | 12.08 | 12.31 | 12.55 | 12.79 | 13.04 | 13.30 | 13.58 | 13.88 | 14.20 | 14.56 | 14.96 |
|  | 12.08 | 12.31 | 12.55 | 12.79 | 13.03 | 13.29 | 13.57 | 13.87 | 14.19 | 14.55 | 14.95 |
|  |  |  |  |  |  |  |  |  |  |  |  |


| Date. |  | Latitude North. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | $4^{\circ}$ | $\mathbf{s}^{\circ}$ | 120 | $16^{\circ}$ | $\mathbf{2 0}{ }^{\circ}$ | 24 | 28 | 320 | $36^{\circ}$ | $40^{\circ}$ |
| July | 1 | $12^{\mathrm{h}} .08$ | $12^{\text {h }} .31$ | 12 b .54 | $12^{\text {h. }} 78$ | $13^{\text {n }} .02$ | $13^{\text {b }} .28$ | $13^{\text {b }} .55$ | $13^{\text {h }} .84$ | $14^{\text {h }} .16$ | $14^{\text {b }} .52$ | $14^{\text {b }} .92$ |
|  | 6 | 12.08 | 12.30 | 12.53 | 12.76 | 13.00 | 13.25 | 13.52 | 13.81 | 14.12 | 14.46 | 14.86 |
|  | 11 | 12.08 | 12.30 | 12.52 | 12.74 | 12.98 | 13.2.2 | 13.48 | 13.76 | 14.06 | 14.39 | 14.77 |
|  | 16 | 12.08 | 12.29 | 12.50 | 12.72 | 12.94 | 13.18 | 13.43 | 13.70 | 13.99 | 14.31 | 14.67 |
|  | 21 | 12.08 | 12.28 | 12.48 | 12.68 | 12.90 | 13.13 | 13.37 | 13.63 | 13.90 | 14.20 | 14.55 |
|  | 26 | 12.08 | 12.27 | 12.46 | 12.65 | 12.86 | 13.07 | 13.30 | 13.54 | 13.79 | 14.08 | 14.41 |
| August | 1 | 12.08 | 12.25 | 12.43 | 12.61 | 12.80 | 12.99 | 13.20 | 13.42 | 13.66 | 13.93 | 14.22 |
|  | 6 | 12.08 | 12.24 | 12.40 | 12.57 | 12.74 | 12.92 | 13.11 | 13.32 | 13.54 | 13.79 | 14.05 |
|  | 11 | 12.08 | 12.22 | 12.37 | 12.52 | 12.68 | 12.85 | 13.02 | 13.20 | 13.41 | 13.63 | 13.87 |
|  | 16 | 12.08 | 12.21 | 12.34 | 12.48 | 12.62 | 12.77 | 12.92 | 13.08 | 13.26 | 13.46 | 13.68 |
|  | 21 | 12.05 | 12.19 | 12.31 | 12.43 | 12.55 | 12.68 | 12.82 | 12.96 | 13.12 | 13.29 | 13.49 |
|  | 26 | 12.08 | 12.17 | 12.27 | 12.37 | 12.48 | 12.59 | 12.71 | 12.83 | 12.97 | 13.12 | 13.29 |
| September |  | 12.08 | 12.15 | 12.23 | 12.31 | 12.40 | 12.49 | 12.58 | 12.68 | 12.79 | 12.91 | 13.04 |
|  | 6 | 12.08 | 12.14 | 12.20 | 12.26 | 12.33 | 12.40 | 12.47 | 12.55 | 12.63 | 12.72 | 12.83 |
|  | 11 | 12.08 | 12.12 | 12.16 | 12.20 | 12.25 | 12.30 | 12.35 | 12.41 | 12.47 | 12.54 | 12.61 |
|  | 16 | 12.08 | 12.10 | 12.13 | 12.15 | 12.18 | 12.21 | 12.24 | 12.27 | 12.31 | 12.35 | 12.40 |
|  | 21 | 12.08 | 12.09 | 12.09 | 12.10 | 12.10 | 12.11 | 12.12 | 12.13 | 12.15 | 12.17 | 12.18 |
|  | 26 | 12.08 | 12.07 | 12.05 | 12.04 | 12.03 | 12.02 | 12.01 | 12.00 | 11.99 | 11.98 | 11.96 |
| October | 1 | 12.08 | 12.05 | 12.02 | 11.99 | 11.96 | 11.93 | 11.89 | 11.86 | 11.82 | 11.78 | 11.74 |
|  | 6 | 12.08 | 12.03 | 11.98 | 11.93 | 11.58 | 11.83 | 11.78 | 11.72 | 11.66 | 11.59 | 11.52 |
|  | 11 | 12.08 | 12.01 | 11.94 | 11.88 | 11.81 | 11.74 | 11.67 | 11.59 | 11.50 | 11.40 | 11.31 |
|  | 16 | 12.08 | 12.00 | 11.91 | 11.83 | 11.74 | 11.65 | 11.55 | 11.45 | 11.34 | 11.22 | 11.09 |
|  | 21 | 12.08 | 11.95 | 11.87 | 11.77 | 11.66 | 11.56 | 11.44 | 11.31 | 11.18 | 11.04 | 10.88 |
|  | 26 | 12.08 | 11.96 | 11.84 | 11.72 | 11.59 | 11.46 | 11.33 | 11.18 | 11.03 | 10.86 | 10.68 |
| November |  | 12.08 | 11.94 | 11.80 | 11.66 | 11.52 | 11.37 | 11.21 | 11.04 | 10.86 | 10.66 | 10.44 |
|  | 6 | 12.08 | 11.93 | 11.77 | 11.61 | 11.45 | 11.25 | 11.11 | 10.92 | 10.71 | 10.49 | 10.25 |
|  | 11 | 12.08 | 11.91 | 11.74 | 11.57 | 11.39 | 11.21 | 11.01 | 10.80 | 10.58 | 10.34 | 10.07 |
|  | 16 | 12.08 | 11.90 | 11.71 | 11.53 | 11.34 | 11.14 | 10.92 | 10.70 | 10.46 | 10.20 | 9.90 |
|  | 21 | 12.08 | 11.69 | 11.69 | 11.49 | 11.29 | 11.08 | 10.85 | 10.61 | 10.35 | 10.07 | 9.75 |
|  | 26 | 12.08 | 11.88 | 11.67 | 11.46 | 11.25 | 11.02 | 10.78 | 10.52 | 10.25 | 9.95 | 9.61 |
| December |  | 12.08 | 11.87 | 11.65 | 11.43 | 11.21 | 10.97 | 10.72 | 10.45 | 10.17 | 9.85 | 9.49 |
|  | 6 | 12.08 | 11.86 | 11.64 | 11.41 | 11.18 | 10.93 | 10.67 | 10.40 | 10.10 | 9.77 | 9.40 |
|  | 11 | 12.08 | 11.86 | 11.63 | 11.39 | 11.15 | 10.90 | 10.64 | 10.36 | 10.05 | 9.71 | 9.33 |
|  | 16 | 12.08 | 11.85 | 11.62 | 11.38 | 11.13 | 10.88 | 10.62 | 10.33 | 10.01 | 9.67 | 9.29 |
|  | 21 | 12.08 | 11.85 | 11.62 | 11.38 | 11.13 | 10.88 | 10.61 | 10.32 | 10.00 | 9.65 | 9.27 |
|  | 26 | 12.08 | 11.85 | 11.62 | 11.38 | 11.13 | 10.88 | 10.61 | 10.32 | 10.01 | 9.66 | 9.28 |


| DATE. |  | Latitude North. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $40^{\circ}$ | 42 | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | 520 | $54{ }^{\circ}$ | $56^{\circ}$ | 58 | $60^{\circ}$ |
| Januar | 1 | 9 h .32 | 9 d .11 | $8^{\mathrm{n}} .89$ | $8^{\text {b }} .65$ | $8^{\text {b }} .39$ | $8{ }^{\text {b }} .10$ | 7h. 77 | 7 7 .40 | $6^{\text {L }} .99$ | $6^{\text {b. }} 51$ | $5^{4} .92$ |
|  | 6 | 9.40 | 9.19 | 8.98 | 8.74 | 8.48 | 8.20 | 7.89 | 7.53 | 7.13 | 6.67 | 6.12 |
|  | 11 | 9.50 | 9.30 | 9.09 | 8.86 | 8.62 | 8.35 | 8.05 | 7.71 | 7.33 | 6.89 | 6.38 |
|  | 16 | 9.62 | 9.43 | 9.23 | 9.01 | 8.78 | 8.52 | 8.24 | 7.93 | 7.57 | 7.16 | 6.68 |
|  | 21 | 9.75 | 9.58 | 9.39 | 9.19 | 8.97 | 8.73 | 8.47 | 8.17 | 7.84 | 7.47 | 7.03 |
|  | 26 | 9.91 | 9.75 | 9.58 | 9.39 | 9.18 | 8.96 | 8.72 | 8.45 | 8.15 | 7.81 | 7.41 |
| Februa | y 1 | 10.11 | 9.97 | 9.82 | 9.65 | 9.46 | 9.26 | 9.05 | 8.81 | 8.54 | 8.24 | 7.90 |
|  | 6 | 10.30 | 10.17 | 10.03 | 9.88 | 9.71 | 9.53 | 9.34 | 9.13 | 8.89 | 8.62 | 8.32 |
|  | 11 | 10.50 | 10.38 | 10.25 | 10.12 | 9.97 | 9.85 | 9.65 | 9.46 | 9.26 | 9.12 | 8.76 |
|  | 16 | 10.70 | 10.60 | 10.49 | 10.37 | 10.25 | 10.12 | 9.97 | 9.81 | 9.63 | 9.43 | 9.21 |
|  | 21 | 10.91 | 10.83 | 10.74 | 10.64 | 10.53 | 10.42 | 10.29 | 10.16 | 10.01 | 9.84 | 9.66 |
|  | 26 | 11.12 | 11.05 | 10.98 | 10.90 | 10.81 | 10.72 | 10.62 | 10.51 | 10.39 | 10.26 | 10.11 |
| March | 1 | 11.25 | 11.19 | 11.12 | 11.05 | 10.98 | 10.90 | 10.82 | 10.73 | 10.62 | 10.51 | 10.38 |
|  | 6 | 11.46 | 11.42 | 11.37 | 11.32 | 11.27 | 11.21 | 11.15 | 11.09 | 11.02 | 10.94 | 1084 |
|  | 11 | 11.68 | 11.65 | 11.62 | 11.59 | 11.56 | 11.53 | 11.49 | 11.45 | 11.41 | 11.36 | 11.29 |
|  | 16 | 11.90 | 11.69 | 11.88 | 11.87 | 11.86 | 11.85 | 11.83 | 11.81 | 11.80 | 11.78 | 11.75 |
|  | 21 | 12.13 | 12.13 | 12.14 | 12.14 | 12.15 | 12.16 | 12.17 | 12.18 | 12.19 | 12.20 | 12.21 |
|  | 26 | 12.35 | 12.37 | 12.39 | 12.41 | 12.44 | 12.47 | 12.50 | 12.54 | 12.58 | 12.62 | 12.66 |
| April | 1 | 12.61 | 12.65 | 12.69 | 12.74 | 12.79 | 12.84 | 12.90 | 12.97 | 13.04 | 13.12 | 13.21 |
|  | 6 | 12.83 | 12.88 | 12.94 | 13.01 | 13.08 | 13.16 | 13.24 | 13.33 | 13.43 | 13.54 | 13.66 |
|  | 11 | 13.04 | 13.11 | 13.19 | 13.27 | 13.36 | 13.46 | 13.57 | 13.58 | 13.81 | 13.96 | 14.12 |
|  | 16 | 13.25 | 13.34 | 13.43 | 13.53 | 13.64 | 13.76 | 13.89 | 14.03 | 14.19 | 14.37 | 14.57 |
|  | 21 | 13.46 | 13.56 | 13.67 | 13.79 | 13.92 | 14.06 | 14.21 | 14.38 | 14.57 | 14.78 | 15.01 |
|  | 26 | 13.66 | 13.78 | 13.90 | 14.03 | 14.18 | 14.34 | 14.52 | 14.71 | 14.93 | 15.18 | 15.45 |
| May | 1 | 13.85 | 13.98 | 14.12 | 14.27 | 14.44 | 14.63 | 14.83 | 15.05 | 15.29 | 15.57 | 15.89 |
|  | 6 | 14.03 | 14.18 | 14.34 | 14.51 | 14.69 | 14.89 | 15.12 | 15.37 | 15.64 | 15.96 | 16.32 |
|  | 11 | 14.20 | 14.37 | 14.54 | 14.73 | 14.93 | 15.15 | 15.39 | 15.66 | 15.97 | 16.32 | 16.72 |
|  | 16 | 14.36 | 14.54 | 14.72 | 14.93 | 15.15 | 15.39 | 15.65 | 15.95 | 16.29 | 16.67 | 17.11 |
|  | 21 | 14.51 | 14.69 | 14.89 | 15.11 | 15.35 | 15.61 | 15.89 | 16.21 | 16.58 | 17.00 | 17.48 |
|  | 26 | 14.64 | 14.83 | 15.04 | 15.27 | 15.52 | 15.80 | 16.11 | 16.45 | 16.84 | 17.29 | 17.82 |
| June | 1 | 14.76 | 14.97 | 15.20 | 15.44 | 15.70 | 15.99 | 16.32 | 16.69 | 17.11 | 17.60 | 18.18 |
|  | 6 | 14.85 | 15.07 | 15.30 | 15.55 | 15.82 | 16.12 | 16.46 | 16.85 | 17.29 | 17.80 | 18.42 |
|  | 11 | 14.91 | 15.13 | 15.37 | 15.63 | 15.91 | 16.22 | 16.57 | 16.97 | 17.43 | 17.95 | 18.60 |
|  | 16 | 14.95 | 15.17 | 15.41 | 15.67 | 15.96 | 16.28 | 16.64 | 17.04 | 17.50 | 18.05 | 18.71 |
|  | 21 | 14.96 | 15.19 | 15.43 | 15.69 | 15.98 | 16.30 | 16.66 | 17.06 | 17.53 | 18.08 | 18.75 |
|  | 26 | 14.95 | 15.18 | 15.42 | 15.68 | 15.97 | 16.29 | 16.64 | 17.04 | 17.51 | 18.05 | 18.72 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |


| Date. |  | Latitude North. |  |  |  |  |  |  |  |  |  |  |
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|  |  | $40^{\circ}$ | 420 | $4{ }^{\circ}$ | $46^{\circ}$ | 480 | $50^{\circ}$ | 5:10 | 540 | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
| July | 1 | $14^{4 .} 92$ | $15^{\text {h }} .14$ | $15^{\text {b }} .37$ | $15^{\text {b }} .63$ | $15^{\text {b }} .92$ | $16^{\text {b }} .24$ | $16^{\text {b }} .59$ | $16^{\text {b }} .98$ | $17^{\mathrm{h}} .43$ | $17^{\mathrm{h}} .97$ | $18^{\text {h }} .61$ |
|  | 6 | 14.86 | 15.07 | 15.30 | 15. 5 | 15.83 | 16.14 | 16.48 | 16.86 | 17.30 | 17.82 | 18.44 |
|  | 11 | 14.77 | 14.98 | 15.21 | 15.46 | 15.72 | 16.01 | 16.34 | 16.71 | 17.13 | 17.62 | 18.20 |
|  | 16 | 14.67 | 14.87 | 15.09 | 15.32 | 15.57 | 15.85 | 16.16 | 16.51 | 16.91 | 17.37 | 17.92 |
|  | 21 | 14.55 | 14.74 | 14.94 | 15.16 | 15.40 | 15.67 | 15.96 | 16.29 | 16.66 | 17.09 | 17.60 |
|  | 26 | 14.41 | 14.59 | 14.78 | 14.99 | 15.31 | 15.46 | 15.73 | 16.03 | 16.38 | 16.78 | 17.24 |
| August | 1 | 14.22 | 14.39 | 14.56 | 14.75 | 14.95 | 15.17 | 15.43 | 15.71 | 16.01 | 16.36 | 16.77 |
|  | 6 | 14.05 | 14.20 | 14.36 | 14.53 | 14.72 | 14.93 | 15.15 | 15.40 | 15.68 | 16.00 | 16.37 |
|  | 11 | 13.87 | 14.00 | 14.15 | 14.31 | 14.48 | 14.67 | 14.87 | 15.09 | 15.34 | 15.62 | 15.95 |
|  | 16 | 13.68 | 13.80 | 13.94 | 14.08 | 14.23 | 14.39 | 14.57 | 14.77 | 14.99 | 15.24 | 15.52 |
|  | 21 | 13.49 | 13.60 | 13.72 | 13.84 | 13.96 | 14.11 | 14.26 | 14.43 | 14.62 | 14.84 | 15.08 |
|  | 26 | 13.29 | 13.38 | 13.47 | 13.57 | 13.69 | 13.82 | 13.95 | 14.09 | 14.25 | 14.43 | 14.64 |
| September |  | 13.04 | 13.11 | 13.19 | 13.27 | 13.36 | 13.46 | 13.56 | 13.68 | 13.81 | 13.95 | 14.11 |
|  | 6 | 12.83 | 12.88 | 12.95 | 13.01 | 13.08 | 13.16 | 13.24 | 13.33 | 13.42 | 13.53 | 13.66 |
|  | 11 | 12.61 | 12.65 | 12.70 | 12.74 | 12.79 | 12.85 | 12.91 | 12.98 | 13.04 | 13.12 | 13.21 |
|  | 16 | 12.40 | 12.42 | 12.45 | 12.48 | 12.51 | 12.54 | 12.58 | 12.62 | 12.66 | 12.71 | 12.76 |
|  | 21 | 12.18 | 12.19 | 12.20 | 12.21 | 12.22 | 12.23 | 12.24 | 12.26 | 12.27 | 12.29 | 12.31 |
|  | 26 | 11.96 | 11.96 | 11.95 | 11.94 | 11.93 | 11.92 | 11.91 | 11.90 | 11.89 | 11.88 | 11.86 |
| October | 1 | 11.74 | 11.72 | 11.69 | 11.67 | 11.64 | 11.61 | 11.58 | 11.54 | 11.50 | 11.46 | 11.41 |
|  | 6 | 11.52 | 11.48 | 11.44 | 11.40 | 11.35 | 11.30 | 11.24 | 11.18 | 11.12 | 11.05 | 10.96 |
|  | 11 | 11.31 | 11.25 | 11.19 | 11.13 | 11.06 | 10.99 | 10.91 | 10.82 | 10.73 | 10.63 | 10.51 |
|  | 16 | 11.09 | 11.02 | 10.95 | 10.87 | 10.78 | 10.68 | 10.58 | 10.47 | 10.35 | 10.22 | 10.06 |
|  | 21 | 10.88 | 10.80 | 10.71 | 10.61 | 10.50 | 10.39 | 10.26 | 10.12 | 9.97 | 9.80 | 9.61 |
|  | 26 | 10.68 | 10.58 | 10.47 | 10.35 | 10.22 | 10.09 | 9.94 | 9.78 | 9.60 | 9.39 | 9.17 |
| November |  | 10.44 | 10.32 | 10.19 | 10.05 | 9.90 | 9.74 | 9.56 | 9.37 | 9.15 | 8.90 | 8.63 |
|  | 6 | 10.25 | 10.12 | 9.97 | 9.82 | 9.65 | 9.47 | 9.27 | 9.05 | 8.80 | 8.52 | 8.21 |
|  | 11 | 10.07 | 9.92 | 9.76 | 9.59 | 9.40 | 9.20 | 8.98 | 8.73 | 8.46 | 8.15 | 7.79 |
|  | 16 | 9.90 | 9.73 | 9.56 | 9.38 | 9.17 | 8.95 | 8.71 | 8.44 | 8.13 | 7.79 | 7.39 |
|  | 21 | 9.75 | 9.57 | 9.39 | 9.19 | 8.96 | 8.72 | 8.46 | 8.16 | 7.83 | 7.45 | 7.02 |
|  | 26 | 9.61 | 9.42 | 9.22 | 9.01 | 8.77 | 8.52 | 8.23 | 7.91 | 7.56 | 7.15 | 6.67 |
| December |  | 9.49 | 9.30 | 9.09 | 8.86 | 8.61 | 8.34 | 8.04 | 7.70 | 7.32 | 6.88 | 6.36 |
|  | 6 | 9.40 | 9.20 | 8.98 | 8.73 | 8.48 | 8.20 | 7.89 | 7.53 | 7.13 | 6.66 | 6.11 |
|  | 11 | 9.33 | 9.12 | 8.89 | 8.64 | 8.38 | 8.09 | 7.77 | 7.40 | 6.98 | 6.50 | 5.92 |
|  | 16 | 9.29 | 9.07 | 8.84 | 8.59 | 8.32 | 8.02 | 7.69 | 7.32 | 6.89 | 6.39 | 5.79 |
|  | 21 | 9.27 | 9.05 | 8.82 | 8.57 | 8.30 | 8.00 | 7.66 | 7.28 | 6.85 | 6.35 | 5.75 |
|  | 26 | 9.28 | 9.06 | 8.84 | 8.59 | 8.31 | 8.01 | 7.68 | 7.31 | 6.88 | 6.38 | 5.78 |


| DATE. |  | Latitude North. |  |  |  |  |  |  |  |  |  |  |
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|  |  | $60^{\circ}$ | $61{ }^{\circ}$ | $6: 2$ | $63{ }^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | 6\% | 6so | $69^{\circ}$ | $80^{\circ}$ |
| January | 1 | $5^{\text {h. }} 92$ | $5^{\text {h }} .59$ | 54.22 | $4^{\text {b }} .79$ | $4^{\text {b }} .30$ | $3^{\text {b }} .70$ | $2^{2 .} 91$ | $1^{4} .60$ | Appears <br> Jin. 6 , <br> A. $\mathbf{M}$. |  |  |
|  | 6 | 6.12 | 5.80 | 5.45 | 5.05 | 4.59 | 4.05 | 3.37 | 2.46 | $0 .{ }^{1} 63$ | Appears <br> Jan. 13, <br> $11 h .54$ |  |
|  | 11 | 6.38 | 6.05 | 5.75 | 5.39 | 4.97 | 4.48 | 3.91 | 3.17 | 213 |  |  |
|  | 16 | 6.68 | 6.41 | 6.11 | 5.7 | 6.40 | 4.97 | 4.48 | 3.57 | 3.10 | $1^{\text {b }} 97$ |  |
|  | 21 | 7.03 | 6.78 | 6.51 | 6.21 | 6.88 | 5.50 | 5.08 | 4.58 | 3.97 | 3.20 | $2{ }^{2} .06$ |
|  | 26 | 7.41 | 7.19 | 6.95 | 6.69 | 7.40 | 6.07 | 5.70 | 5.28 | 4.79 | 4.20 | 3.45 |
| February | 1 | 7.90 | 7.71 | 7.50 | 7.27 | 7.02 | 6.75 | 6.44 | 6.10 | 5.11 | 5.27 | 4.73 |
|  | 6 | 8.32 | 8.15 | 7.97 | 7.7 | 7.56 | 7.33 | 7.07 | 6.78 | 6.45 | 6.09 | 5.67 |
|  | 11 | 8.76 | 8.61 | 8.46 | 8.29 | 8.11 | 7.91 | 7.69 | 7.45 | 7.18 | 6.85 | 6.54 |
|  | 16 | 9.21 | 9.09 | 8.96 | 8.82 | S. 66 | 8.49 | 8.31 | 8.11 | 7.89 | 7.64 | 7.37 |
|  | 21 | 9.66 | $9 \cdot 56$ | 9.44 | 9.33 | 9.20 | 9.07 | 8.92 | 8.76 | 8.58 | ع.38 | 8.16 |
|  | 26 | 10.11 | 10.03 | 9.94 | 9.54 | 9.74 | 9.63 | 9.81 | 9.38 | 9.25 | 9.10 | 8.93 |
| March | 1 | 10.38 | 10.31 | 10.24 | 10.16 | 10.07 | 9.98 | 9.88 | 9.77 | 9.65 | 9.52 | 9.38 |
|  | ${ }^{6}$ | 10.84 | 10.79 | 10.74 | 10.68 | 10.62 | 10.55 | 10.45 | 10.40 | 10.32 | 10.23 | 10.13 |
|  | 11 | 11.29 | 11.26 | 11.23 | 11.20 | 11.16 | 11.12 | 11.08 | 11.03 | 10.95 | 10.92 | 10.86 |
|  | 16 | 11.75 | 11.74 | 11.73 | 11.72 | 11.70 | 11.69 | 11.67 | 11.65 | 11.63 | 11.61 | 11.58 |
|  | 21 | 12.21 | 12.21 | 12.22 | 12.23 | 12.24 | 12.25 | 12.26 | 12.27 | 12.29 | 12.30 | 12.31 |
|  | 26 | 12.66 | 12.69 | 12.72 | 12.75 | 12.78 | 12.82 | 12.c6 | 12.90 | 12.94 | 12.99 | 13.04 |
| A ${ }^{\text {pril }}$ | 1 | 13.21 | 13.26 | 13.31 | 13.37 | 13.43 | 13.49 | 13.56 | 13.64 | 13.72 | 13.81 | 13.92 . |
|  | 6 | 13.66 | 13.73 | 13.60 | 13.88 | 13.97 | 14.06 | 14.16 | 14.27 | 14.38 | 14.51 | 14.66 |
|  | 11 | 14.12 | 14.20 | 14.30 | 14.40 | 14.51 | 14.63 | 14.76 | 14.90 | 15.05 | 15.22 | 15.41 |
|  | 16 | 14.57 | 14.67 | 14.79 | 14.92 | 15.05 | 15.19 | 15.36 | 15.54 | 15.73 | 15.94 | 16.18 |
|  | 21 | 15.01 | 15.14 | 15.28 | 15.44 | 15.60 | 15.77 | 15.97 | 16.19 | 16.42 | 16.68 | 16.98 |
|  | 26 | 15.45 | 15.60 | 15.77 | 15.95 | 16.14 | 16.35 | 16.59 | 16.84 | 17.13 | 17.45 | 17.82 |
| May | 1 | \|15.89 | 16.07 | 16.26 | 16.47 | 16.69 | 16.94 | 17.21 | 17.51 | 17.86 | 18.26 | 18.72 |
|  | 6 | 16.32 | 16.52 | 16.74 | 16.98 | 17.23 | 17.52 | 17.85 | 18.21 | 18.63 | 19.12 | 19.71 |
|  | 11 | 16.72 | 16.95 | 17.20 | 17.47 | 17.77 | 18.10 | 18.48 | 18.92 | 19.43 | 20.05 | 20.86 |
|  | 16 | 17.11 | 17.37 | 17.65 | 17.95 | 18.30 | 18.68 | 19.13 | 19.66 | 20.30 | 21.15 | 22.55 |
|  | 21 | 17.48 | 17.7 | 18.15 | 18.42 | 18.81 | 19.26 | 19.79 | 20.45 | 21.31 | $\underline{2} 2.81$ |  |
|  | 26 | 17.82 | 18.13 | 18.47 | 18.86 | 19.30 | 19.82 | 20.46 | 21.89 | 22.68 |  | $\begin{gathered} \text { Mrom } \\ \text { May } 17, \end{gathered}$ |
| June | 1 | 18.18 | 18.52 | 18.90 | 19.33 | 19.84 | 20.46 | 21.27 | 22.56 | Above <br> horizon | May 22, <br> 0 . 4 | $\begin{aligned} & \text { A. } 3.59 \\ & \text { Jul to } \\ & \text { Jut } \end{aligned}$ |
|  | 6 | 18.42 | 18.78 | 19.19 | 19.66 | 20.23 | 20.94 | 21.95 | $\underset{\substack{\text { Above } \\ \text { borizulu } \\ \text { troni }}}{\text { a }}$ | $\begin{aligned} & \text { frum } \\ & \text { May }=8, \end{aligned}$ |  |  |
|  | 11 | 18.60 | 18.98 | 19.41 | 19.92 | 20.54 | 21.34 | 2.2 .65 | $\begin{aligned} & \text { trom } \\ & \text { June } \\ & \text { 5h i } \end{aligned}$ | $\begin{aligned} & \text { Ah. } 26 \\ & \text { A. } \end{aligned}$ |  | $70 d 23 \mathrm{~h} .0$ |
|  | 16 | 18.71 | 19.11 | 19.56 | 20.09 | 20.74 | 21.62 | 23.40 |  | to, Juls |  |  |
|  | 21 | 18.75 | 19.15 | 19.60 | 20.14 | 20.81 | $21.72$ |  | $\left\{\begin{array}{c} 11 h .56 \\ \mathrm{p} . \mathrm{I}_{6} \\ 35 d 23 h .31 \end{array}\right.$ | $\begin{gathered} 11 / 56 \\ p .3 . \\ \text { 43d } 33 . h 30 \end{gathered}$ |  |  |
|  | 26 | 18.72 | 19.11 | 19.56 | 20.09 | 20.75 | 21.64 | 23.45 |  |  |  |  |






Table from which may be taken for any given date the number of days to be added (algebraically, as the sigu directs) to its supplementary date so as to give the date with which to find from the table of insolations for the given date the insolation for the given date in a southern latitude.

| Given date. | Days to be added to supplementary date. | Given date. | Days to be added to supplementary date. | Given date. | Days to be added to supplementary date. | Given date. | Days to le added to supple. mentary date. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| January 6 | $+1^{\text {d }} .97$ | April 6 | $+3 \mathrm{~d} .51$ | July 6 | $-1^{\text {d }} .83$ | October 6 | $-3{ }^{\text {d }} .53$ |
| 16 | +2.66 | 16 | $+3.39$ | 16 | $-2.52$ | 16 | $-3.44$ |
| 26 | +3.31 | 26 | $+3.18$ | 26 | -3.18 | 26 | $-3.26$ |
| February 6 | + 3.95 | May 6 | $+1.86$ | August 6 | $-3.71$ | November 6 | $-1.92$ |
| 16 | $+4.46$ | $11 i$ | +1.45 | 16 | $-4.25$ | 16 | $-1.52$ |
| 26 | $+4.86$ | 26 | $+0.96$ | 26 | $-4.68$ | 26 | $-1.03$ |
| March 6 | $+2.14$ | June 6 | $+1.30$ | September 6 | $-2.08$ | December 6 | $-1.39$ |
| 16 | + 2.35 | $11 ;$ | + 0.64 | 16 | - 2.34 | 16 | -0.68 |
| 26 | $+2.50$ | 26 | -0.03 | 26 | -2.48 | 219 | $+0.03$ |

## ALPHABETICAL INDEX.

A.
Air, column corresponding to a Millimetre in Barometer ..... page ..... 427
" same at different Temperatures and Elevations ..... 429
" column corresponding to tenths of an inch in Barometer ..... 427
" same at different Temperatures and Elevations ..... 18
" cubic foot, Dry and Saturated, compared
Albany, Monthly corrections Non-periodic Variations of Temperature ..... 677
Altitudes, comparison of lengths used in measuring ..... 449 -500
Amherst, Hourly corrections Periodic Var. Temperature ..... 592
Apenrade, Hourly corrections Periodic Var. 'Temperature ..... 632
Apjohn, Factors for computing Force of Vapor ..... 176
Aqueous Vapor, comparison of Dry and Saturated Air ..... 180
" " Elastic force of, in French measures, Regnault ..... 46
" " " ، Greenwich constants ..... 137
" " ، 6 in Millimetres, August ..... 186
" ". " .. ." . Kacmtz ..... 188
" " . . . " Magnus ..... 188
" ، " . 6 Cubic Foot of Saturated Air ..... 130
.. ، " .، .. .. .. .. Greenwich constants ..... 179
" " Force of, and Relative Humidity corresponding to degrees of Saussure's Hygrometer, Gay Lissac ..... 198
" " " different values of different authorities ..... 190
" ." $\quad$ English measures, Regnault ..... 7
" " " Greenwich Homrly corrections, Glaisher ..... 65:3
" " ، Inches, Royal Soc. ..... $18!$
" " " weight of, in Cubic Metre of air . ..... 74" " " ." Factor for deducing from indications ofdew point instruments . . 17!in Grammes, in Cubic Metre of air,Kaemtz192
in Grammes. in Cubic Metre of air. Pouillet ..... 192
Arc, from Sidereal Time ..... 69.5
" into Sidereal Time ..... 693
Athabasca, Hourly corrections Periodic Var. Temperature ..... 589
PAGE
August, Elastic force of Vapor in Millimetres ..... 186
Australia, standards of Length compared with other nations ..... 709
Austrian Miles into Kilometres ..... 508
" " Prussian Miles," " German Miles," " Nautical Leagues," " French Leagues," " Geographical Miles," " English Statute Miles,
"، " Russian Wersts ..... 508
Austrian Square Miles into Square Kilometres ..... 540
" " " 3 Prussian Square Miles,
" ${ }^{6}$ " " German Square Miles,
" " " Nautical Square Leagues," " " Freuch Square Leagues," " " Geographical Square Miles," " " English Square Statute Miles," " " Russian Square Wersts . . . . 540
B.
Baily, depression of Barometric column, capillary ..... 340
". Hypsometric Tables, English measures ..... 407
Barometer, English and Metrical compared ..... 215
" "، " old French compared ..... 219
" " brass scale reduced to freezing point ..... 269
" " capillary correction ..... 337
" " from Metrical ..... 225
" " " old French . ..... 238
" " glass or wooden scale reduced to freezing point ..... 276
equivalents of millimetres, in metres ..... 427
same at different Temperatures and Elevations ..... 429
equivalents of Paris Lines, in French Feet ..... 427
" tenths of an inch, in English Feet ..... 427
same at different 'Temperatures and Elevations ..... 430
Metrical, capillary corrections (Meniscus) ..... 338
" 6 from English ..... 215
" " "، old French ..... 243
" "، " Russian ..... 247
" " into English ..... 225
" "، reduced to freezing point, Delcros ..... 281
" " " ، " Haeghens ..... 287
" old French, reduced to freezing point ..... 330
" " compared with English ..... 238
" " " " Metrical ..... 243
" " " "، Russian ..... 252
page
Barometer reduced to Sea Level ..... 426
Barometric column, capillary correction for English Barometers ..... 337
" " " " " French Barometers ..... 338
" " " depression, Baily ..... 340
" " 6 " Delcros ..... 340
" " ، Gehler ..... 339
" " " ." Pouillet ..... 339
" differences, comparison of ..... 257-261
" pressure, true mean, Hourly Corrections, Greenwich ..... 432
" " " " " $"$ Philatelphia ..... 431
" pressures, corresponding to Temperatures of boiling water, Metrical ..... 442
" " same, Metrical, Regnault ..... 438
" " same, English measures ..... 444
" scales, comparison of different ..... 209-252
Barometrical Tables ..... 209-340
Bavarian Feet, into Metres ..... 493
Belgium, standards of Length compared with other nations ..... 709
Berghaus, Horary correction ..... 418
Berlin, Hourly corrections Periodic Var. Temperature ..... 629
" Monthly corrections Non-periodic Var. Temperature ..... 666
Bernaul, Hourly corrections Periodic Var. Temperature ..... 606-608
Bessel, Plantamour's Hypisometric Tables ..... 410
Boiling water, Temperatures aud corresponding Barometric pressures, English measures ..... 444
" " same, Moritz, Metrical measures ..... 442
" "، same, Regnault, Metrical measures ..... 438
Bolivian Fect, into English Feet ..... 496
". Varas, into Metres ..... 496
Bombay, Hourly corrections Periodic Var. 'Temperature ..... 599, 602
Boothia Felix, Hourly corrections Periodic Var. Temperature ..... 588
Bossekop, Hourly corrections Periodic Var. Temperature ..... 645
Brussels, Hourly corrections Periodic Var. Temperature ..... 621, 622
C.
Calcutta, Hourly corrections Periodic Var. 'Temperature ..... 602
Cape of Good Hope, Hourly corrections Periodic Var. Temperature ..... 649
Capillary action, correction for English Barometers ..... 337
" " " " Metrical Barometers, Delcros ..... 338
" " depression of barometric column, Baily ..... 340
" " ." " $"$ Delcros ..... 340
" " " " " Geller ..... 339
" ، " ، Ponillet ..... 339
Carlsrulie, Monthly corrections Non-periodic Var. Temperature ..... 664
Castilian Varas, into Metres . ..... 494
PAGE
Catharinenburg, Hourly corrections Periodic Var. Temperature ..... 636, 637
Centigrade degrees, expressed in equal number of degrees of Fahrenbeit ..... 35
 ..... 34
" Scale, compared with Reaumur's and Fahrenheit's, full degrees from $+100^{\circ}$ to $+50^{\circ}$ ..... 10
" " converted into Fahrenheit, tenths of degrees from $+50^{\circ}$ to $-54^{\circ}$, and from $+100^{\circ}$ to $+89^{\circ}$ ..... 25
" " " " Reaumur, tenths of degrees from $+40^{\circ}$ to $-40^{\circ}$ ..... 28
Centimetres (rain measure), from English Inches ..... 201
" " " " French Inches and Lines ..... 202
" " " into English inches ..... 200
" " ، " French Inches and Lines ..... 200
Christiania, Hourly corrections Periodic Var. Temperature ..... 641
Cocfficients of Hourly Corrections, Berghaus ..... 418
Column of air, Height corresponding to a Millimetre, in Metres ..... 427
" ". same at different Temperatures and Elevations ..... 429
" " equivalents of Paris Lines, in French Feet . ..... 427
" ، " " tenths of an inch, in English Feet ..... 427
$66 \quad 66$ same at different Temperatures and Elevations ..... 430
Comparison of Barometrical differences ..... 257-261
.. "، different Barometric Scales ..... 209-252
". " measures of length used in measuring altitudes ..... 449-500
" " most important measures of Geographical Distances ..... 501-532
" " " " 6 Geographical Surfaces ..... 533-564
" " . " " Length (units) ..... 499
" " " " " Surface (units) ..... 564
" "Quantities of Rain-water, different measures . ..... 200-203
" " Standards of Lengtl of England, France, Belginm, Prussia, Russia. India, and Australia ..... 709
Constants of Greenwich observations, Iygrometric Tables based on them ..... 137-182
" " Laplace, Hypsometrical Tables based on them ..... 347-409
" ". Regnault, Hygrometric Tables based on them ..... 44-129
Copenhagen, Monthly eorrections Non-priodic Var. Temperature ..... 669
Correction of Barometrical observations for capillary action ..... 335-340
" Horary, coefficients of Berghaus ..... 418
"، "، old French Measures ..... 419
" hypsometric, for curvature and refraction ..... 434
" of Time from Solar observation, to obtain True time of Clocks ..... 697
Corrections, for Half-sums of Temperatures at Geneva and St, Bernard, Plan- tamour ..... 420
" Ilorary, to be applied to obtain True mean Barometric Pressure, Greenwich ..... 432
" to be applied to obtain True mean Barometric Pressure, Philadelphia ..... 431
Corrections, Hourly Periodic Var. Temperature ..... 579-650
" ." ." " Force of Vapor and Relative ILumidity ..... 683, 684
، Monthly, for Non-periodic Var. Temperature ..... $654-679$
Cubic foot of air, Weight of Vapor in English measures ..... 130
Greenwich Observations ..... 179
" " Dry and Saturated air compared in weight ..... 180
" metre of air, Weight of Vapor in French measures ..... 74
-. ." $\quad$. 6 Grammes, Kaemtz ..... 192
Curvature and Refiaction, Hypsometric correction ..... 192 ..... 434

## D.

Day, length of, at.different Latitudes ..... 711
Degrees, Centigrade, expressed in equal number of degrees of Fahrenheit ..... 3.5
34
" ". scale, compared with Fahrenheit and Reammur ..... 11
" ." ." converted into Fahrenheit ..... 2.9
Reammor . ..... 25
" Fahrenheit, expressed in equal number of degrees of Centigrade ..... 34
" " " " $"$. ..... 34
" " scale, compared with Centigrade and Reammur ..... r
" ". " converted into Centigrade ..... 13
" 6 . 6 Reaumur ..... 18
". from Time ..... 695
" into Time ..... 693
.- length of, on Meridian and Parallel ..... 695
.- Reaumur, expressed in equal number of digrees of C'rntigrade ..... 35

- " " " " 6 Fahrenheit ..... 35
" " scale, comipared with Centigrade and Fahrenheit ..... 10
". ." . converted into C'entigrade ..... 32
" . " 6 Fahrenheit ..... 30
" Squares of ..... 703
Delcros, correction for capillary action, metrical ..... 338
" depression from capillary action ..... 340
" Hypsometric Tables ..... 349
" normal height of meniscus, in Millimetres ..... 337
". Reduction of Metrical Barometer to freezing point ..... 281
Depression of Barometric colmmn, capillary, Baily ..... 340
" " " " " Deleros ..... 340
" " " " " Gehler . ..... 339
" " " " " Pouillet ..... 339
" " " " correction, English Barometers ..... 337
" " " Metrical Barometers ..... 338
Dew point, factors for deducing weight of Vapor ..... 179
PAGE
Dew point, from Psychrometer readings ..... 178, 182
"، Guyot's Tables, English measures ..... 111" Haeghens's Tables for reducing Relative Humidity, Frenchmeasures66
Dippe's modified Gauss's Tables, Hypsometric ..... 392
Tables, Hypsometric ..... 396
Distances, comparison of measures of Geographical ..... 501-532
Drontheim, Hourly corrections Periodic Viar. Temperature ..... 642
Dry air, cubic foot, compared with Saturated air ..... 180
Dublin, Hourly corrections Periodic Var. Temperature ..... 635
E.
Elastic force of Aqueous Vapor, English measures ..... 78
" "، ، ، French measures ..... 46
" " " " Greenwich constants ..... 137
" " Vapor, difference in Values ..... 190
" " " English Inches, Royal Soc. Report ..... 189
" " " in millimetres, by August ..... 186
" " ، 6 " Kaemtz ..... 188
" " " " " Magnus ..... 188
England, standards of Length compared with those of other nations ..... 709
English Baroneter and Metrical Barometers compared ..... 215
" . $\quad$ old Frenclı Barometers compared ..... 219
". ${ }^{\text {. }}$ brass scale, to freezing point ..... 269
" " capillary correction ..... 337
" "، from Metrical ..... 225
"، ، " old French ..... 238
"، " glass or wooden scale, to freezing point ..... 276
". Fathoms from Metres ..... 500
". $\quad$ into Metres ..... 500
". Feet, equivalents of, tenths of an inch in Barometer ..... 427
". ." equivalents of, tenths of an inch in Barometer at different Temperatures and Elevations ..... 430
" " from Bolivian Feet ..... 496
" ، " Feet of Viema ..... 489
.. ." ". French Toises ..... 461
". ." " Klatter of Vienna ..... 486
" ." ". Metres ..... 466
.. ". " Mexican Feet ..... 495
". " " Paris Feet ..... 477 •
.. "، " Rhine Feet ..... 492
". ". into Metres ..... 481
" " " Paris Feet ..... 482
" " " Rline Feet ..... 483
" " " Feet of Vienna ..... 484page
English Hypsometric Tables, Guyot ..... 371
". Inches, from Centimetres (rain measure) ..... 200
" " " French Inches and Lines (rain measure) ..... 203
" ". " French or Paris Lines . ..... 260
" ." " Millimetres ..... 258
" $\quad$ into Centimetres (rain measure) ..... 201
" " " French Inches and Lines (rain measure) ..... 201
" ." ". French or P'aris Lines ..... 257
.. .. ." Millimetres ..... 2.5
." Measures for Thermonetrical measurement of heights ..... 444
". Statute Miles into Kilometres ..... 526
" " " Austrian Miles,
" 6 ." Prussian Miles,
" ". ". German Miles,
" " ، Nautical Leagues,
" ، "، French Leagues,
" " " Geographical Miles,
" ". " Russian Wersts . . . . . 526
". Square Statute Miles into Square Kilometres . . . 258
" ". " " Austrian Square Miles,
" " " " Prussian Square Miles,
" " " " German Square Miles,
" " " ${ }^{6}$ Nautical Square Leagnes,
" " " " French Square Leagues,
" " " " Geographicai Square Miles,
" " " " Russian Square Wersts . . . 558
" Yards, into French Toises ..... 480
" " ، Metres ..... 450
F.
Factor $\frac{100}{\mathbf{F}}$ for computing relative Humidity, Regnault's constants, English measures ..... 126
" " " " Regnault's constants, French measures ..... 72
Factors for computing force of vapor, from Psychrometrical observations, Apjohn's formula ..... 176
" deducing the Weight of Vapor from the Indications of Dew Point Instruments ..... 179
" finding Temperature of the Dew Point from the Readings of the Psychrometer ..... 178
Fahrenheit degrees, expressed in equal number of degrees Centigrade ..... 34
. 6 6 6 6 6 of Reanmur ..... 34" scale, compared with Centigrade and Reaummr, full degrees (from$+212^{\circ}$ to $-39^{\circ}$ )8Fahrenheit scale, converted into Centigrade, tenths of degrees (from $+122^{\circ}$to -76 $6^{\circ}$ )13
" " converted into Reaumur, tenths of degrees (from $+122^{\circ}$ to $-38^{\circ}$ ) ..... 18
Fathoms, English, from Metres ..... 500
.. .. into Metres ..... 500
Feet and inches, from Decimals of a Toise ..... 497
.- Bavarian, into Metres ..... 493
.- Bolivian, into English Feet ..... 496
.. 6. ". Metres ..... 496
-. English, equisalents of tenths of an inch in Barometer ..... 427
". " equivalents of tenths of an inch in Barometer at different Tem- peratures and Elevations ..... 430
" ${ }^{\text {. }}$ from Bolivian Feet ..... $4!6$
". " " French Toises ..... 461
"، "، 6 Metres ..... 466
" ". " Mexican Feet ..... 49.
" " 6 Paris Feet ..... 477
، " ، Rhine Feet ..... 492
"، 6 V Vienna Feet ..... 489
". " ${ }^{6}$ Vienna Klafter ..... 486

6. Mexican, into English Feet ..... 49.
6 's " Metres ..... 495
" old Spamish, into Metres ..... 494
". Paris, from English Feet ..... 482
" " " French Toises ..... 4619
6 " " Metres ..... $46: 3$
" " " Rline Feet ..... 492
" "، " Vienna Feet ..... 485
7. "6 "، Vienna Klafter ..... 481;
" Prussian or Rhine, from Metres ..... 474
" Rhenish, from French Toises ..... 461
" Rhine, from English Feet ..... $48: 3$
" " " Paris Feet. ..... 48.
" " " Vienna Feet ..... 490
" " into English Feet ..... 492
"، ، " French Toises ..... 491
" ، " Metres ..... 491
" " " Paris Feet ..... 492
" ، " Vienna Feet ..... 493
"، Vienna, from English Feet ..... 484
" ، " Paris Feet ..... $47!$
". " " Rhine Feet ..... 493
" .. " Metres ..... 474
" ." into English Feet ..... 489
Feet, Vienna, into Metres ..... 4871AGE
.. " " Paris Fect ..... 488
" ، "6 Rhine Feet ..... 490
Foot, Decimals of, into Inches and Decimals ..... 498
" " from Inches and Duodecimal Lines ..... 498
" $6 \quad$ into Inches and Duodecimal Lines ..... 498
Force of Aqueous Vapor, Elastic, Greenwich constants ..... 137
" " " " Regnault's constants, English measures ..... 78
" " ، " " " French measures ..... 46
" " " inches, Royal Soc. Report . ..... 189
" Vapor, Elastic, in Millimetres, August ..... 186
" " ، " Kaemtz ..... 188
" 6 6 " Magnus ..... 188
" " " different values of different authorities ..... 190
" " and Relative Itumidity corresponding to the degrees ofSaussure's Ilair Hygrometer, Gay Lassac193
Force of Vapor, Greenwich, Glaisher ..... 683
France, Standards of Length compared with other nations ..... 769
Franktort Arsenal, Pa., Hourly corrections Periodic Var. Temperature ..... 581, 582
Freezing Point, English Barometer, brass scale ..... 269
" " " " glass or wooden scale ..... 276
". Metrical Barometer ..... 287
" old French Barometer ..... 330
French Barometer, reduction to Freezing point ..... 330
" old, compared with English ..... 238
"، "6 " Metrical ..... 243
" Russian ..... 252
Feet, equivatents of Paris Lines, in Barometer ..... 427
" Inches and Lines (rain measure), from Centimetres ..... 200
" " " " English Inches ..... 201
" " " into Centimetres ..... 20:2
" " " English Inches ..... 203
Leagaes into Kilometres ..... 520
" " Anstrian Miles,
" " Prussian Miles,
" " German Miles,
" " Nantical Miles,
" " Geographical Miles," "6 English Statute Miles," " Russian Wersts520
Lines, into English Inches ..... 260
" "، Millimetres ..... 260
measures, old, correction for hour of day ..... 419
" " Dippe's Hypsometric Tables ..... 398
" " " Gauss's Mypsometric Tobles ..... 396
PAGE
French Square Leagues into Square Kilometres ..... 552" ." ". ". Austrian Square Miles,

| "، | " | " | " | Prussian Square Miles, |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| " | " | " | " German Square Miles, |  |  |  |
| " | " | " | " | Nautical Square Leagues, |  |  |
| " | " | " | " | Geographical Square Miles, |  |  |
| " | " | " | " | English Square Statute Miles, |  |  |
| " | " | " | " | Russian Square Wersts | . . . 552 |  |

". Toises, from English Yards ..... 480
"، $\quad$ Rhine Feet ..... 491
" " into Metres ..... 460
" " " English Feet ..... 461
" " " Paris Feet ..... 460
" " " Rhine Feet ..... 461
G.
Gauss's Hypsometric Tables, modified by Dippe ..... 396
Gay Lussac, Force of Vapor and Relative Humidity corresponding to degrees of Saussure's Hygrometer ..... 193
Gehler's Worterbuch, capillary depression, Barometric column ..... 339
Geneva, correction for half-sums of Temperature, Geneva, St. Bernard ..... 420
" Hourly corrections Periodic Var. Temperature ..... 613
" Monthly corrections Non-periodic Var. Temperature ..... 658
Geographical Distances, Comparison of measures ..... 501-532
"، measures, comparison of ..... 447-565
" Miles into Kilometres . . . . . . 523
" 6 Austrian Miles," " Prussian Miles," " German Miles," "، Nautical Leagues," " French Leagues," ، English Statute Miles," " Russian Wersts . . . . . 523
" Square Miles into Siquare Kilometres . . . . 555" " " Austriiu Square Miles," " " Prussian Square Miles," " " German Square Miles," " " Nautical Square Leagues," "، " French Square Leagues," " " English Square Statute Miles," " " Russian Square Wersts . . . 555
" Surfaces, Comparison of' measures ..... 533-564
German Miles mto Kilometres ..... 514" Austrian Miles,
German Miles into Prussian Miles," Nautical Leagues," French Leagues," Geographical Miles," English Statute Miles,
" Russian Wersts . . . . . . 514
Square Miles into Square Kilometres . . . . j46
" Austrian Square Miles,
" Prussian Square Miles,
" Nautical Square Leagues,
" French Square Leagues,
" Geographical Square Miles,
" English Square Statute Miles,
" Russian Square Wersts . . . . 546
Glaisher, Force of Vapor, Greenwich ..... 683
" Psychrometer Tables ..... 140
" Relative Humidity, Greenwich ..... 684
Godthaab, Monthly corrections Non-periodic Var. Temperature ..... 679
Gottingen, Hourly corrections Periodic Var. Temperature ..... 628
Greenwich, Force of Vapor, Glaisher ..... 683
" Relative Humidity, Glaisher ..... 684
" Hourly correction to mean Barometric Pressure ..... 432
" " corrections Periodic Var. Temperature ..... $624-626$
" " " " " Force of Vapor and Relative
Humidity ..... 683, 684
" Hygrometric Constants ..... 137-182
Guyot's Hypsometric Tables . ..... 371
" Psychrometric Tables, English measures ..... 82
" Relative Humidity from dew point observations ..... 111
II.
Haeghens, Psychrometrical Tables, French measures ..... 48
" Relative Humidity and Force of Vapor from Saussure's Hygro- meter ..... 194
" Reduction to freezing point, Metrical Barometer ..... 287
Halle, Hourly correction Periodic Var. Temperature ..... 627
Hecla Cove, Hourly correction Periodic Var. Temperature ..... 589
Helsingfors, Hourly correction Periodic Var. Temperature ..... 638, 640
Hobarton, Hourly correction Periodic Var. Temperature ..... 650
Hourly corrections, Berghaus ..... 418
" " for mean Barometric Pressure, Greenwich ..... 432
" " " " " Philadel!hia ..... 431
" "، old French measures ..... 419
" " Periodic Var. Temperature ..... 579-650
Page
Humidity, Relative, and Force of Vapor, Haeghens ..... 194
Katemtz ..... 195
" ، Factor ${ }_{F}^{100}$, English measures ..... 126
، "، "، French measures ..... 72
" " from Dew point Instruments ..... 111
" " " Saussure's Hygrometer, Gay Lussac ..... 193
". " " ، " Hateghens ..... 194
". ." Greenwich, Glaisher ..... 140
Hygrometrical Tables ..... $37-205$
". ." based on Greenwich observations ..... 137
" " constants of Laplace ..... 349
"، "، 6 Regnault ..... 46
Hypsometric correction for curvature and refraction ..... 434
" Tables, Baily (English measures) ..... 407
" " Delcros ..... 349
" "، Dippe ..... 398
"، ". " modified Ganss's ..... 392
، ، Guyot ..... 371
" " Plantamour's, Besse! ..... 410
I.
Inches and Duodecimal Lines into Decimals of a Foot ..... 498
". English, from Centimetres ..... 200
"، "، French Inches and Lines ..... 203
، .، "، "t or Paris Lines ..... 260
" ." " Millimetres ..... 258
"، .، moto Centimetres ..... 201
، ". "، French Inches and Lines ..... 201
" ، ، " or Paris Lines ..... 257
" ، " Millimetres ..... 2.7
" French, from Centimetres (rain measures) ..... 200
" " " English Inches (rain measures) ..... 201
" into Centimetres (rain measures) ..... 202
" English Inches (rain measures) ..... 203
India, standard of Length compared with other nations ..... 709
Insolation, length of, for any given Latitude ..... 711
K.
Kaemtz, Elastic Force of Vapor, in Millimetres ..... 188
". Reduction of old French Barometer to freezing point ..... 330
" Relative Hmmidity, corresponding to degrees of Saussure's Hygro- meter ..... 195
" Weight of Vapor, in Grammes in Cubic Metre of Air ..... 192
Kara, Straits of, Hourly correction Periodic Var. Temperature ..... 643
Kilometres into Austrian Miles ..... 505
" " Prussian Miles, " " German Miles,
"6 " Nautieal Leagues, " " French Leagues,
" " Geographical Miles,
" " English Statute Miles, ..... " " Russian Wersts . . . . . . . 505
" Square, into Austrian Square Miles ..... 537
"، ". " Prussian Square Miles," " " German Square Miles," " " Nautical Square Leagroes," " " French Square Leagues," " " Geographical Sipuare Miles," " " English Square Statute Miles,"6 " " Russian Square Wersts . . . . 537
Kinfams Castle, Monthly correction Non-periorlic Viar. Temperature ..... (676
Klafter of Viemna, into English Feet ..... 486
" " ، Metres ..... 485
" " " Paris Feet ..... 486
Kremsmunster, Hourly correction Periodic Var. Temperature ..... 615
L.
Laplace, constants of Hypsometric Tables ..... 349-407
Latitude, length of Insolation for any given ..... 711
Latitudes, length of a degree at different ..... 698
" of Prineipal Observatories ..... 689
" surfaces at different ..... 703
Leagues, French, into Kilometres ..... 520
" ." " Austrian Miles,
" ." " Prussian Miles," 6 " German Miles," ${ }^{6}$ " Nantieal Leagnes," " " Geographical Miles,". ". ". English Statute Miles,
، " ، Russian Wersts ..... 520

* Nantical, into Kilometres ..... 517
"، .. .. Austrian Miles,
" ، $"$ " Prussian Miles,
" " " German Miles,
" "، " French Leagues,
" " " Geographical Miles,
" ". "، English Statute Miles,
" ، "، Russian Wersts ..... 517



## M.

Madras, Mourly corrections Periodic Var. Temperature . . 597, 601
${ }^{6}$ Monthly corrections Non-periodic Var. Temperature . © 4
Magnus, Elastic Force of Vapor in Millimetres . . . 188
Makerstoun, Hourly correetions, Periodic Yar. Temperature . 635
Matoschkin Schar, Hourly corrections, Periodic Var. Temperature . . 644
Measures of Geographical Distances ..... 501-531
"، ، " comparison of units ..... 532
". "، ${ }^{6}$ Surfaces ..... 533-563
" " Length, Comparison of units ..... 499
" " " used in measuring Altitudes, Comparison of ..... 449-500
" " Surface, Comparison of units ..... 564
Melville Island, Hourly corrections Periodic Var. Temperature ..... 589
Meniscus, normal Height of, in Millimetres ..... 337
Meridian, Lengths of Degree of ..... 695
Metres, from Bavarian Feet ..... 493
". " Bolivian Feet ..... 496
". " ، Varas ..... 496
." " English Fathoms ..... 500
" .. "، Feet ..... 181
" " " Yards ..... 480
" " Feet of Vienna ..... 487
" " French Toises ..... 460
، "، Klafter of Viemna ..... 48.5
" " Paris Feet ..... 476
" " Mexican Feet ..... 495
" "، " Varas ..... $4!5$
" ${ }^{6}$ old Spanish or Castillian Varas ..... $4!4$
". " ، " Feet ..... 494
". ، Rhine Feet ..... 491
." into English Fathoms ..... 500
" ، 6 Feet ..... 4196
، "، Feet of Vienna ..... 474
" " French Toises ..... 462
" "، Paris Feet ..... 463
" Rhine or Prussian Feet . ..... 474
" Height of Column of Air corresponding to Millimetre in Barometer ..... 427
" same at different Temperatures and Elevations ..... $4 \because 9$
Metrical Barometer, Capillary corrections, Deleros ..... 338
" ". from English ..... 215
" "، "، old French ..... 243
" " " Russian ..... 247
" " into English ..... 225
" ، " old French ..... 231
" " reduction to Freezing point, Delcros ..... 281
" " " " Haeghens ..... 287
" Measures, Deleros Hypsometrical Tables ..... 349
" " Plantamour's Hypsometrical Tables ..... 410" " Regnanlt's Barometric pressures, corresponding to Tem-peratures of boiling water, Moritz442
same, English measures ..... 444
Mexican Feet into English Feet . . . . . . 495
" 6 " Metres . . . . . . . 495
". Varas into Metres . . . . . . . 495
Milan, Monthly corrections Non-periodic Var. Temperature . 6506, 657 Miles, Austrian, into Kilometres . . . . . . 508
" ، " Prussian Miles,
" "6 " German Miles,
" ، " Nautical Leagues,
" " " French Leagues,
" ، " Geographical Miles,
" ، ، Engli-h Statute Miles,
" " " Russian Wersts . . . . . 508
" Prussian, into Kilometres . . . . . . 511
". ." ." Anstrian Miles,
-" 6 .. German Miles,
" " " Nautical Leagues,
" " ." French Leagues,
.. ". ". Geographical Miles,
" " " English Statute Miles,
.، ". " Rusition Wersts . . . . . . 511
.. German, into Kilometres . . . . . . 514
". ." ". Austrian Miles,
." ." " Prussitu Miles,
" " " Nantical Leagues,
" " " French Leagues,
" " . " Geographical Miles,
" " " English Statute Miles,
" " ". Rusian Wersts . . . . . . 514
" Greographical, into Kilometres . . . . . . 523
.. .. ". Austrism Miles,
." .. .. Prussian Miles,
.. ". $\quad$ Cerman Miles,
" " $"$ Nautical Leagues,
.. ،. ." French Leagues,
.. .. ." English Statute Miles,
.. " ، Russian Wersts . . . . . 523
" English Statute, into Kilometres . . . . . . 2 ;
" .. .. .. Anstrian Miles,
" ، ." "، Prussian Miles,
.. .. .. .. German Miles.
.. " . " Niatical Leagues,
.. .. .. ." French Leagues,
." " " " Geographical Miles,
.. " ، " Russian Wersts . . . . . 529
". Anstrian Sipuare, into Square Kilometres . . . . 540
.. ، .. " Prussian Square Miles.

" Prusian Square, into Square Kilometres ..... i43" .. .. " Anstrian Square Miles,
" " .. ". German Square Miles,
" 6 "، " Nautical Square Leagues,
" " " " French Square Leagues,
" " " " Geographical Square Miles,
" " " " English Square Statute Miles,
" 6 " " Russian Square Wersts . . . . 543
" German Square, into Square Kilometres . . . . i 44

" Geographical Square, into Square Kilometres . . . . ins
" " " " Austrian Square Miles,
" ، " " Prussian Square Miles,
" " " " German Square Miles,
". "، " Nautical Square Leagues,
" " " " French Square Leagues,

" English Square Statute, into Square Kilometres ..... 55s
" ". " " . A Austrian Square Miles,

." .. .. .. " Prussian Square Miles,

." ." ". " German Square Miles,

" .. " .. " Nautical Square Leagues,

.. .. ". " " French Square Leagues.

.. ". " " Geographical Square Miles, ..... i.s
Millimetre, Height of Colamn of Air corresponding to a ..... 127
" same at different Temperatures and Elevations ..... ! 9
Millimetres, Elastic force of Vapor expressed in, by August
". .. .. .. .. " Kaemitz ..... 1 1s
" 6 " 6 Magnus ..... 1 s
" from English inches ..... 
(، " French or Paris Lines ..... $\therefore 150$
Page
Millimetres, from Russian Half-Lanes ..... 261
" into English Inches ..... 258
" " French or Paris Lines ..... 259
" normal Height of Memiscus, Deleros ..... 337
Montreal, Hourly corrections Periodic Var. Temperature ..... 586
Moritz, Tables for Barometric pressures correspouding to Temperatures of Boiling water ..... 442
" same, in English measures ..... 444
Mithithausen, Hourly corrections Periolic Var. Temperature ..... 623
Munich, Hourly corrections Periodic Var. 'Temperature ..... 616, 617
N.
Nantical Leagues into Kilometres ..... 517
" " ." Austrian Miles,

" " " ${ }^{6}$ Prussian Miles,

" " " German Miles,
" " " Frenclı Leagues, ..... " " " Geographical Miles,
" " " English Statute Miles,

- "، Russian Wersts ..... 517
.. Miles into Kilometres ..... 523" ". .. Austrian Miles,
" ". " Prussian Miles,
." .. ." German Miles,
" .. " Nautical Leagues,
". ." ". French Leagues,
" .. ". English Statute Miles,
". ". " Russian Wersts ..... 523
-. Square Leagues into Square Kilometres ..... 549
" " ، " Austriau Square Miles, .. .. "، " Prussian Square Miles, ." .. " " German Square Miles, ." .. " " French Square Leagues, " ." ". " Geographical Square Miles, " .. "6 " English Square Statute Miles,
*.. $\quad$. ${ }^{6}$ Russian Square Wersts ..... 549
" ." Miles into Square Kilometres ..... 555
" " " " Austrian Square Miles,.. ." "، " Prussian Square Miles,". " " " German Square Miles,.. .. ". " French Square Leagues,." ." ." " Nantical Square Leagues,." .. ". " English Square Statute Miles," .. .. " Russian Square Wersts555
Non-periodic Variations of Temperature, Monthly Corrections

Nertchinsk, Hourly corrections Periodic Var. Temperature . . 604, 605

## O.

Observatories, Positions of Principal . . . . . $68!$

## P.

Padua, Hourly corrections Periodic Var. Temperature ..... 612
Palermo, Monthly corrections Non-periodic Var. "1emperature ..... 65.5
Parallel, length of degree of ..... 698
Paris Feet from English Feet ..... 482
". " . French Toises ..... 460
"، " " Metres ..... 463
" " ، Rhine Feet ..... 492
، ، .، Vienna Feet ..... 485
، ،6 6 Viemna Klafter ..... $4 \times 1$
" Lines from Russian Half-Lines ..... 261
" " into English Inches ..... 260
" " ، Millimetres ..... 260
" Monthly corrections Non-periodic Var. Temperature ..... (i71
Peking, Hourly corrections Periodic Var. Temperature ..... 603, 6,04
Periodic Variations of 'Temperature, Howrly Corrections ..... 579-650
" ، Force of Vapor and Relative Humidity, Hourly Cor-iections683, 684
Philadelphia, Hourly corrections Periodic Yar. 'Temperature ..... 579, 580
Plantamour, Corrections for Half-sums of 'Cemperatures at Geneva and St. Bernard ..... 420
Hypsometric Tables, Bessel ..... 110
Plymonth, England, Hourly corrections Periodic Var. 'Temperature ..... 619, 620
Pouillet, Depression of Barometric column due to terpillary action ..... 339

- Weight of Vapor in Grammes in Cubic Metre of Air ..... 192
Prague, Hourly corrections Periodic Var. 'Гemperature ..... 617, 618
Pressure, Barometric, corresponding to 'Temperatures of Boiling water ..... 438-445
Prussia, standards of Length compared with other nations ..... 709
Prussian Miles into Kilometres ..... 511

| " | " | " | Austrian Miles |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| " | " | " | German Miles, |  |  |
| " | " | " | Nautical Leagues, |  |  |
| " | " | " | French Leagues, |  |  |
| " | " | " | Geographical Miles, |  |  |
| " | " | . | English Statute Miles, |  |  |
| " | " | " | Russian Wersts . | . . . . . 511 |  |

Prussian Square Miles into Square Kilometres, . . . . 543
.. .. ". .. " Anstrian Square Miles,
.. .. " ." "6 German Square Miles,
.. .. " ." " Nantical Square Leagues,
" " " . " " French Square Leagnes,
.. .. . . . 6 Geographical Square Miles,
.. ." ، ، " English iquare Statute Miles,
.. .. ." ". " Rusian Square Wersts . . . 543
Psychrometer, Fators tor finding Dew point from readings, of ..... 178-182
Psyehrometrical observations, Factors for deducing Force of Vapor, Apjohn ..... 176
Tables, Glaisher, Greenwich constants ..... 140
". $،$ Guyot, English measures ..... 82
" " Hategens, Freuch measures ..... 48
R.
Rain measure, Centimetres, from English Inches ..... 201
". ." ". French Inclees and Lines ..... 212
." ". $\quad$ into English inches ..... 200
.. .. .. " French Inches and Lines ..... 200
.. ". English Inches, from Centimetres ..... 200
.. .. ". ". French Inches and Lines ..... 203
" .. " " into Centimetres ..... 201
". .. ". " " French Inches and Lines ..... 201
". . French Inches and Lines, from Centimetres ..... 200
" ." " ." "، " English Inches ..... 201
.، .. " " ${ }^{\text {. }}$ into Centimetres ..... 202
" ." ". .6 " " English Inches ..... 203
Ratisbon, Monthly corrections Non-periodic Variations of 'Temperature ..... 661, 662
Reammur degrees, expresed in equal number of degrees of Centigrade ..... 35
" ". " . " " Fahrenheit ..... 35
." Scale, compared with Fahrenheit and Centigrade, full degrees from $+80^{\circ}$ to $+40^{\circ}$ ..... 10
" " converted into Centigrade, tenths of degrees from $+40^{\circ}$ to $-40^{\circ}$ ..... 32
6 " Falirenheit, tenths of degrees from $+40^{\circ}$ to $-40^{\circ}$. ..... 30
Reducing Barometer to Sea Level ..... 426
Refraction and Curvature, Hypsometric correction ..... 434
Regnault's Barometric Pressure, equivalent to 'Temperature of Boiling water ..... 438
to Temperature of Boiling water English measure, Moritz ..... 444
" " " " to Temperature of Boiling water Metrical measures, Moritz ..... 442
،. Constants, Hygrometric Tables based on them ..... 44-129
Reikiarik, Monthly correction Non-periodic Var. Temperaturepage
Relative Humidity, corresponding to degrees of Saussure's Hair Hygrometer ..... 195
corresponding to degrees of Saussure's Hair Hygrometer, Gay Lussac ..... 193
" " deduced from Indications of Saussure? Hair Hygrometer, Haeghens ..... 194
 ..... 126 ..... 72
" $"$ from Dew point instruments ..... 111
". . . . . Haeghens ..... 66
Rhine Feet into English Feet ..... 492
.. .. Feet of Vienna ..... 493
.. .. French Feet ..... 492
،. 6 .. Toises ..... 491
". 6 Motres ..... 491
Rio Taneiro, Homly corrections Periodic Var. Temperature ..... 890, 591
Rome, Hourly corrections Perionlic Var. Temperature ..... 611
Russia, standards of Length compared with other mations ..... 709
Russian Barometer compared with Metrical ..... 247

- old French ..... 25:
.: Half-Lines converted into Millimetres ..... 261
.. .. .. .. Paris Lines ..... 261
Russian Wersts into Kilometres ..... 529.. .. .. Anstrian Miles,.. .. .. Prussian Miles, .. .. German Miles,
.. .. .. Nantical Leagues,
.. .. .. French Leagues,.. .. .. Geographical Miles,
.. .. .. English Statute Miles ..... 529
.- Square Wrats into Square Kilometres ..... 261
.. .. .. "A Anstrian Square Miles... .. .. " Prussian Square Miles,
.. .. .. .. German Square Miles.
.. .. .. .. Nantical Spuare Leagues,
.. .. .. .. French Square Leagues,
.. .. .. .. Geographical Square Miles,
.. .. .. .. English Square Statute Miles ..... 561


## s.

Salem, Monthly corrections Non-periodic Viar. Temperature ..... $1: 78$
Salzburg, Hourly corrections Periotic Var. Temperature ..... 1116
S:lzuflen, Hourly corrections Periodic Var. 'Temperature ..... 1330
page
Saturated Air, Cubic foot, compared with Dry Air ..... 180
Saussure's Hygrometer, for deducing Relative Humidity from indications of, Haeghens. ..... 194
" " Force of Vapor and Relative Humidity, correspond- ing to degrees of . ..... 193
" " Relative Humidity, corresponding to degree of, Kaemtz ..... 195
Schwerin, Hourly corrections Periodic Var. Temperature ..... 622
Sidereal Time, from parts of Equator in Are ..... 694
" " into mean Solar Time ..... 696
" ، " parts of Equator in Are ..... 695
Sitka, Hourly corrections Periodic Var. Temperature ..... 587
Solar observations, Correction of Time to obtain True Time of Clock ..... 697
". Time, mean, into Sidereal Time ..... 696
Spanish old or Castilian Varas, into Metres ..... 494
.، $\cdot$ Feet irto Metres ..... 494
Square Austrian Miles, see Miles, or ..... 540
". English Statute Miles, see Miles, or ..... 558
". French Leagues, see Leagues, or ..... 552
". Geographical Miles, see Miles, or ..... 555
" German Miles, see Miles, or ..... 546
". Nautical Leagnes, see Leagues, or ..... 549
" Prissian Miles, see Miles, or ..... 543
.. Russian Wersts, see Wersts, or ..... 561
Square Statute Miles, English, into Square Kilometres ..... 558
" . . . . . Austrian Square Miles, .. ". ." " Prussian Square Miles, ". .. ." ". " German Square Miles,
". . ." " " Nantical Square Leagnes,
." .. .. ". " French Square Leagues,
.. "، ". " Geographical Square Miles, ..... 558
Statute Miles, English, into Kilometres ..... 526
.. " ". " Anstrian Miles,
." .. " " Prussian Miles, ." .. .. ." German Miles,
" ، ". " French Leagues,
. " " " Geographical Miles,
.. .. ." ". Russian Wersts ..... 526
Stettin. Hourly corrections, Periodic Var. Temperature ..... 631
St. Bernard and Geneva, corrections for Half-sums of 'Temperatures, Planta- mour ..... 420
St. Bernard, Hourly corrections Periodic Var. Temperature . ..... 614
St. Helena, Hourly corrections Periodic Var. Temperature ..... 6.49
St. Petersburg, Hourly correction Periodic Var. Temperaturepage
Stuttgart, Monthly corrections Non-periodic Var. Temperature ..... 663
Sun, correction of 'Time by observation of, to obtain True Time of Clock ..... 697
Surfaces, comparison of measures of Geographical ..... 534-563
units of measures ..... 564
" Tables for computing Terrestrial ..... 703
T.
Temperature, corrections for Half-sums of, at Geneva and St. Bernard,
Plantamour ..... 420
" Hourly corrections Periodic Variations, Amherst ..... 592

". Apenrade ..... 632
.. Athabasca Lake ..... 589 .....
$\begin{array}{ll}\text {.. } & \text { Berm } \\ & \text { Bernanl }\end{array}$ ..... 629
.. Bombay ..... 599, 602
"، -. Bossekop ..... 645

"
.. Brussels ..... 621, 622
." Calcutta ..... 602
.. Cape of Good Hope ..... 649
" Catharinenburg ..... 636, 637
" Clnristiania ..... 641
.. Drontheim ..... 642
.- Dublin ..... 635
.. Frankfort Arsenal ..... 581, 582
.. Geneva ..... 613
.. Greenwich ..... 624, 626
.. Göttingen ..... 628
.. Halle ..... 627
.. Hecla Cove ..... 589
.. Helsingfors ..... 638, 64"

- Hobarton ..... - 650
". Kara, Straits of ..... - 643
". Kremsmunster ..... 615
" Leith . ..... 633, 634
، Madras ..... -997, 601
.. Makerstoun ..... -635
". Matoschkin Schar ..... 644
" Melville Island ..... 589
"، Montreal ..... 586
". Miihlhausen ..... 623
". Munich ..... 616, 617
" Nertchinsk 604, 605
PAGE
Temperature, Hourly corrections Periodic Variations, Padua ..... 612
". Peking ..... 603, 60.4
" Philadelphia ..... 579, 580
، Plymouth, England
17,
". Prague ..... 617, 618
". Rio Janeiro ..... 590, 591
.- Rome ..... 611
.. Salzhurg ..... 616
.. Salzuflen ..... 630
". Schwerin ..... 622
.. Sitka ..... 587
.. Stettin ..... 631
". St. Bernard ..... 614
.. St. Helena ..... 649
.- St. Petersburg ..... 637, 639
.. Tiflis ..... 603
.. Toronto ..... 583-586
-. Trevandrum ..... 595, 596
.. Uirecht ..... 624
W:ahington ..... 579
Monthly corrections Non-periotic Variations, Albany ..... 677
Berlin ..... 666-668
Carlsruhe ..... 664, 665
.. Copenhagen ..... 669
". Geneva ..... 658, 659
.. Godthaab ..... $67!$
-• Kinfanns Castle ..... 676
.. London ..... 674 . 675
.. Madras ..... 6.54
-. Milan ..... 656, 6.57
.. Palermo ..... 6.5.)
.. Paris ..... 671
.- Ratisbon ..... 661, $66 \div$
.. Reikiavik ..... 679
.. Salem ..... 67 x
.- Stuttgart ..... (663)
. Torneá ..... 686. 677
". Vienna ..... fo60, 1861
Zwanemburg ..... 67き-(674
of Boiling Waler. Barometric Pressures corresponding to, Moritz, English measures ..... 44
Barometric Pressures corresponding to, Moritz. Metrical measures ..... 442
Barometric Pressures corresponding to, Regnault ..... 438
Temperature of Dew point, from Psychrometrical readings ..... 178-182page
" Non-periodic Variations, Monthly corrections ..... 651-679
" Periodic Variations, Hourly corrections ..... 579-650
Terrestrial Longitule in Arc, from Time ..... 69.
" 6 .. into Time
" Surfaces, Tables for computing ..... $70:$
Thermometric mesturement of Heights ..... 435-445
Thermometrical Tables ..... 8-3.9
Tiflis, Hourly correction Periodic Var. Temperature ..... 603
Time correction of Solar observation to oltain True Time of clock ..... 697
-. mean Solar, into Siderial Tine ..... 696
". Silerial, from parts of Equator in Are ..... 693
". .. into mean Solar Time ..... 696
" ". " parts of Equator in Are ..... 695
Toise, Decimals of, into Feet and Inches ..... 497
" Frencli, from EnglishYards ..... 480
". ، .. Rhine Feet ..... 491
" .. ". Metres ..... $46{ }^{2}$
" ، ." Paris Feet ..... 47.5
". .. into English Feet ..... 461
". " 6 Metres ..... 460
". ." " Paris Feet ..... 460
" " " Rhine Feet ..... 461
Torneá, Monthly corrections Non-periodic Var. Temperature ..... 676, 677
Toronto, Hourly corrections Periodic Var. Temperature ..... 583-586
Trevandrum, Ilourly corrections Periodic Var. 'Temperature ..... 595, 596
Tropic hours of daty Variation at Halle ..... 425
True Time of clock correction for Solar observations ..... 697
U.
Utrecht, Hourly corrections Periodic Var. Temperature ..... 624
V.
Vapor, comparison of Mry and Saturated Air (Greenwich) ..... 180
" Elastic force of, in French measures, Reguatult ..... 46
" . " " Greenwich constants ..... 137
" ". ". " in Millimetres, August ..... 186
". ." .. ". ${ }^{\circ}$ Katemtz ..... 188
" " ." " Magnus ..... 188
" " ." " Cubic Foot of Saturated Air ..... 130
" " " " " " " Greenwich constants ..... 179
Force of, and Relative Ihmidity corresponding to degrees of Saussure'sHygrometer, Gay Lassac193
PAGE
Yapor, Force of, different values of different authorities ..... 190
" " Erglish measures, Regnault ..... 78
" " Greenwich, Glaisher, Hourly corrections Periodie Variations ..... 683
" Inches, Royal Society ..... 189
" Weight of, in Cubic Foot of air ..... 130
" ". " Metre of air ..... 74
" " Factor for deducing from indications of dew point instru- ments ..... 179
in Grammes, in Cubic Metre of air, Kaemtz ..... 192
" $،$ " 6 . $\quad$ Pouillet ..... 192
Vienna, Feet of, from English Feet ..... 484
" ، ، Paris Feet ..... 479
" ، .. Rhine Feet ..... 493
" " into English Feet ..... 489
، ، ، Metres ..... 487
" " " Paris Feet ..... 488
" ، " Rline Feet ..... 490
" Klafter of, into English Feet ..... 486
" " ، Metres ..... 485
، ". ، Paris Feet ..... 486
Vienna, Montlly corrections Non-periodic Var. Temperature ..... 660, 661
Varas, Bolivian, into Mptres ..... 496
" Mexican, into Metres. ..... 495
" old Spanish or Castilian, into Metres ..... 494
W.
Washington, Hourly corrections Periodic Var. Temperature ..... 579
Water, Temperatures of Boiling, and corresponding Barometric Pressures, Moritz, English measures ..... 444
and corresponding Barometric Pressures, Moritz, French measures ..... 442
and corresponding Barometric Pressures, Regnault ..... 438
Weight of Cubic Foot of Dry and Satmrated Air ..... 180
، Vapor, Factors for deducing, from Dew point indications ..... 179
، "، ، " " Greenwieh ..... 179
، "، in Cubic Foot of Air, Regnault ..... 130
.، ". . Metre of Air, Regnault ..... 74
.. ،6 in Grammes in Cubic Metre of Air, Kiamtz ..... 192
"، 6 Pouillet ..... $1!2$
Wersts, Russian, into Kilometres ..... 52!
" " " Austrian Miles,
." .. " Prussian Miles,
" ." "، German Miles,
ALPMABETICAL INDEX. ..... 747
Wersts, Russian, into Nautical Leagues,
". .. " French Leagues,
.. ." "6 English Statute Miles ..... 52!)
.. .. Square, into Square Kilometres ..... 561
.. ، ، ، Prussian Square Miles,
" 6 " " German Square Miles,
. ، ، ". English Square Statute Mile ..... 561
Y.
Yards, English, into French 'Toises ..... 480
" " ، Metres . ..... 480
Z.
Zwanenburg, Monthly corrections Non-periodic Var. Temperature ..... 672-674




[^0]:    A

[^1]:    * Etudes sur l'Hygrométrie, par M. V. Regnault. Annales de Chimie et de Physique, $3^{\text {me }}$ Série, Tom XV., 1845.

[^2]:    * While .his table was moing through the press, a similar one, prepared by Prof. J. H. Coffin for his private use, was published by the Smithsonian Institution, in order to meet an urgent demand from many quarters. Being based on the same formula, it gives the same results, except, perhaps, in degrees below $14^{\circ}$ Fahrenheit, where the tables show slight discrepancies. These mimportant differences arise from the fact that Prof. Coffin's table was computed from Regnault's tensions, as given in the first edition of this collection, while the anthor's table is based on the table of tensions as given in this second edition, in which the valnes below $14^{\circ}$ Fahrenheit have been somewhat modified, for reasons given above. The following table gives also the relative humidity with one more decimat, which makes the interpolations more easy ; and a column of differences for finding the values for fractions of $t^{\prime}$. A table for reducing the results to another barometric height is added at the end of the table.

[^3]:    Mean Horizontal Difference of Force of Fapor for each $0^{\circ} .1=0.0013$.

[^4]:    In this table each measure named at the head of its vertical column, occurs once as unit, and all the numbers, on the same horizontal line, express the equivalents of that unit in the other measures. The smaller figures, below the larger ones, are the logarithms of the same.

[^5]:    The mantera withum sign must be added : those with the sign - must be subracted.

[^6]:    The numbers without sign must be subtracted ; those with the sign - must be added.

