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METEOROLOGICAL TABLES

## $\varepsilon_{\text {uncer }}$ SMITHSONIAN

## Meteorological Tables

[BASED ON GUYOT'S METEOROLOGICAL AND PHYSICAL TABLES.]
(REVISED EDITION)


CITY OF WASHINGTON:

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## PREFACE TO REVISED EDITION.

The original edition of Smithsonian Meteorological Tables, issued in 1893, having become exhausted, necessitating a second edition, a careful examination of the original work has been made, at my request, by Mr. Alexander McAdie, of the United States Weather Bureau.

All errata thus far detected have been corrected upon the plates, and a few slight changes have been made. The International Meteorological Symbols and an Index have been added.
S. P. LANGLEY,

Secretary.
Smithsonian Institution, February 15, 1896.

## PREFACE

In connection with the system of meteorological observations established by the Smithsonian Institution about 1850, a collection of meteorological tables was compiled by Dr. Arnold Guyot, at the request of Secretary Henry, and published in 1852 as a volume of the Miscellaneous Collections.

Five years later, in 1857, a second edition was published after careful revision by the author, and the various series of tables were so enlarged as to extend the work from 212 to over 600 pages.

In 1859 a third edition was published, with further amendments.
Although designed primarily for the meteorological observers reporting to the Smithsonian Institution, the tables obtained a much wider circulation, and were extensively used by meteorologists and physicists in Europe and in the United States.

After twenty-five years of valuable service, the work was again revised by the author; and the fourth edition, containing over 700 pages, was published in 1884. Before finishing the last few tables, Dr. Guyot died, and the completion of the work was intrusted to his assistant, Prof. Wm. Libbey, Jr., who executed the duties of final editor.

In a few years the demand for the tables exhausted the edition, and thereupon it appeared desirable to recast entirely the work. After very careful consideration, I decided to publish the new tables in three parts: Meteorological Tables, Geographical Tables, and Physical Tables, each representative of the latest knowledge in its field, and independent of the others; but the three forming a homogeneous series.

Although thus historically related to Dr. Guyot's Tables, the present work is so substantially changed with respect to material, arrangement, and presentation that it is not a fifth edition of the older tables, but essentially a new publication.

## BAROMETRICAL TABLES.-Continued.

Determination of heights by the barometer - English measures.
Values of $60368[\mathrm{r}+0.0010195 \times 36] \log \frac{29.90}{B}$. ..... 100
20
Term for temperature ..... 104 ..... 21
Correction for latitude and weight of mercury ..... 106
22
108 ..... 23
Correction for an average degree of humidity
24 Correction for the variation of gravity with altitude ..... 109
Determination of heights by the barometer - Metric measures.
Values of $18400 \log ^{760} B$ ..... IIO
Term for temperature ..... III
Correction for humidity ..... II 2
Correction for latitude and weight of mercury ..... II4
Correction for the variation of gravity with altitude ..... II5
Difference of height corresponding to a change of o. I inch in the barometer - English measures ..... I 16
31 Difference of height corresponding to a change of 1 millimetre in the barometer - Metric measures ..... II 7
Determination of heights by the barometer.
Formula of Babinet ..... II8
Barometric pressures corresponding to the temperature of the boiling point of water -
33 English measures ..... II9
34Metric measuresII9
HYGROMETRICAL TABLES.
Pressure of aqueous vapor (Broch) -
35 English measures ..... 122
36
Metric measures ..... 128
37 Pressure of aqueous vapor at low temperatures (C. F. Marvin) - English and Metric measures ..... I 30
38 Weight of aqueous vapor in a cubic foot of saturated air- English measures ..... 132
39 Weight of aqueous vapor in a cubic metre of saturated air - Metric measures ..... 133
Reduction of psychrometric observations - English measures. ..... 134
Values of $0.000367 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{\mathrm{I} 57 \mathrm{I}}\right)$ ..... I36
41Relative humidity - Temperature Fahrenheit138
HYGROMETRICAL TABLES.-Continued.
Table page
Reduction of psychrometric observations - Metric measures.
43 Pressure of aqueous vapor ..... 142
Values of $0.000660 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{873}\right)$ ..... 143
45 Relative humidity-Temperature Centigrade ..... 144
Reduction of snowfall measurements.
46 Depth of water corresponding to the weight of snow (or rain) collected in an 8-inch gage ..... 146
47 Rate of decrease of vapor pressure with altitude ..... 146
WIND TABLES.
Mean direction of the wind by Lambert's formula-
Multiples of $\cos 45^{\circ}$; form and example of computation ..... 148
Values of the mean direction ( $\alpha$ ) or its complement (90-a) ..... 149
49 Values of the mean directio ..... 154
51 Miles per hour into feet per second ..... I 55
52 Feet per second into miles per hour ..... I 55
53 Metres per second into miles per hour ..... 156
54 Miles per hour into metres per second ..... 157
55 Metres per second into kilometres per hour ..... 158
56 Kilometres per hour into metres per second ..... 159
57 Beaufort wind scale and its conversion into velocity ..... 160
GEODETICAL TABLES.
58 Relative acceleration of gravity at different latitudes ..... 162
59 Length of one degree of the meridian at different latitudes ..... 164
60 Length of one degree of the parallel at different latitudes ..... 165
61 Duration of sunshine at different latitudes ..... 166
62 Declination of the sun for the year 1894 ..... 177
63 Relative intensity of solar radiation at different latitudes ..... 178
CONVERSION OF LINEAR MEASURES.
64 Inches into millimetres ..... 180
65 Millimetres into inches ..... 187
66 Feet into metres ..... 200
67 Metres into feet ..... 202
68 Miles into kilometres ..... 204
69 Kilometres into miles ..... 206
70 Interconversion of nautical and statute miles ..... 208
71 Continental measures of length with their metric and English equivalents ..... 208
CONVERSION OF MEASURES OF TIME AND ANGLE.
CONVERSION OF MEASURES OF TIME AND ANGLE.
Table Page
72 Arc into time ..... 210
73 Time into arc ..... 211
74 Days into decimals of a year and angle ..... 212
75 Hours, minutes and seconds into decimals of a day ..... 216
76 Decimals of a day into hours, minutes and seconds ..... 216
77 Minutes and seconds into decimals of an hour ..... 217
78 Mean time at apparent noon ..... 217
79 Sidereal time into mean solar time ..... 218
80 Mean solar time into sidereal time ..... 218
MISCELLANEOUS TABLES.
81 Density of air at different temperatures Fahrenheit ..... 220
Density of air at different humidities and pressures-English measures.
82 Term for humidity : auxiliary to Table 83 ..... 221
Values of $\frac{h}{29.921}=\frac{b-0.378 e}{29.921}$ ..... 222
83 ..... 
84 Density of air at different temperatures Centigrade ..... 224
Density of air at different humidities and pressures - Metric measures.
85 Term for humidity : auxiliary to Table 86 ..... 225
Values of $\frac{h}{760}=\frac{b-0.378 e}{760}$ ..... 226
86
87 Conversion of avoirdupois pounds and ounces into kilogrammes ..... 226
230
88 Conversion of kilogrammes into avoirdupois pounds and ounces
230
89 Conversion of grains into grammes
231
90 Conversion of grammes into grains
231
91 Conversion of units of magnetic intensity
232
92 Quantity of water corresponding to given depths of rainfall
232
93 Dates of Dove's pentades
94 Division by 28 of numbers from 28 to 867972 ..... 233
95 Division by 29 of numbers from 29 to 898971 ..... 234
96 Division by 31 of numbers from 3I to 960969 ..... 235
97 Natural sines and cosines ..... 236
98 Natural tangents and cotangents ..... 238
99 Logarithms of numbers ..... 240
100 LIST OF METEOROLOGICAL STATIONS ..... 243
APPENDIX.
Constants ..... 258
Synoptic conversion of English and metric units ..... 260
Dimensions of physical quantities ..... 262
International Meteorological Symbols ..... 263

## INTRODUCTION.

## DESCRIPTION AND USE OF THE TABLES.

THERMOMETRICAL TABLES.<br>COMPARISON OF THERMOMETRIC SCALES.

Conversion of readings of the Reaumur thermometer to readings of the Fahrenheit and Centigrade thermometers.

Table 1.
The argument is given for every Reaumur degree from $+80^{\circ}$ to $-40^{\circ}$ Reaumur, and the corresponding readings Fahrenheit and Centigrade are given to hundredths of a degree, permitting the exact values to be expressed. A column of proportional parts gives the values corresponding to tenths of a Reaumur degree. By the help of the column of proportional parts, the table is also conveniently used for converting Fahrenheit to Centigrade and Reaumur, and Centigrade to Fahrenheit and Reaumur throughout the thermometric scale from the boiling point of water to $-60^{\circ} F$. or $-51^{\circ} C$.

The formulæ expressing the relation between the different scales are given at the bottom of the table, where

$$
\begin{aligned}
& F^{\circ}=\text { Temperature Fahrenheit. } \\
& C^{\circ}=\text { Temperature Centigrade. } \\
& R^{\circ}=\text { Temperature Reaumur. }
\end{aligned}
$$

## Examples:

To convert 18.3 Reaumur to Fahrenheit and Centigrade.


To convert $147^{\circ} .7$ Fahrenheit to Centigrade and Reaumur.


To convert $16^{\circ} 9$ Centigrade to Fahrenheit and Reaumur.
From the table,

| $\begin{aligned} 16{ }^{\circ} 25 C & = \\ 0.65 & = \end{aligned}$ | $\begin{aligned} 61.25 F & = \\ 1.17 & = \end{aligned}$ | $\begin{aligned} & \text { ェ } 3 \text { ․o } R . \\ & 0.5 \end{aligned}$ |
| :---: | :---: | :---: |
| 9 C. | 2.4 F. | 13.5 |

TABLE 2. Conversion of readings of the Fahrenheit thermometer to readings Centigrade.

The conversion of Fahrenheit temperatures to Centigrade temperatures is given for every tenth of a degree from $+130.9 F$. to $-70.9 F$. The side argument is the whole number of degrees Fahrenheit, and the top argument, tenths of a degree Fahrenheit; interpolation to hundredths of a degree, when desired, is readily effected mentally. The tabular values are given to hundredths of a degree Centigrade.

The formula for conversion is

$$
C^{\circ}=\frac{5}{9}\left(F^{\circ}-32^{\circ}\right)
$$

where $F^{\circ}$ is a given temperature Fahrenheit, and $C^{\circ}$ the corresponding temperature Centigrade.

## Example:

To convert 79.7 Fahrenheit to Centigrade.
The table gives directly $26.5^{\circ} \mathrm{C}$.
For conversions of temperatures above $\mathbf{I} \mathrm{I}^{\circ} F$, use Table I .
table 3. Conversion of readings of the Centigrade thermometer to readings Fahrenheit.

The conversion of Centigrade temperatures to Fahrenheit temperatures is given for every tenth of a degree Centigrade from +50.9 to -50.9 C . The tabular values are expressed in hundredths of a degree Fahrenheit.

The formula for conversion is

$$
F^{\circ}=\frac{9}{5} C^{\circ}+32^{\circ}
$$

where $C^{\circ}$ is a given temperature Centigrade, and $F^{\circ}$ the corresponding temperature Fahrenheit.

For conversions of temperatures above the upper limit of the table, use Tables I and 4.
table 4. Conversion of readings of the Centigrade thermometer near the boiling point to readings Fahrenheit.

This is an extension of Table 3 from 90.0 to roo. 9 Centigrade.
Example:
To convert $95^{\circ} \cdot 74$ Centigrade to Fahreuheit.
From the table,

$$
\begin{aligned}
95^{\circ} 70 C & =204^{\circ} .26 F . \\
0.04 & =\frac{0.07}{95^{\circ} .74} C
\end{aligned}=\frac{204^{\circ} .33}{} F .
$$

By interpolation,

Conversion of differences Fahrenheit to differences Centigrade. table 5.
The table gives for every tenth of a degree from $0^{\circ}$ to $20.9 F$. the corresponding lengths of the Centigrade scale.

Conversion of differences Centigrade to differences Fahrenheit.
TAble 6.
The table gives for every tenth of a degree from $0^{\circ}$ to $9.9 C$. the corresponding lengths of the Fahrenheit scale.

## Example:

To find the equivalent difference in Fahrenheit degrees for a difference of $4.7^{\circ}$ Centigrade.
From the table,

$$
\begin{aligned}
4^{\circ} .70 C & =8.46 F . \\
0.02 & =0.04 \\
\frac{4.72}{0.0} C & =\overline{8.50} F .
\end{aligned}
$$

From the table by moving the decimal point for 0.2,

## REDUCTION OF TEMPERATURE TO SEA LEVEL.

English Measures.
Table 7.
Metric Measures.
Table 8.
These tables give for different altitudes and for different uniform rates of decrease of temperature with altitude, the amount in hundredths of a degree Fahrenheit and Centigrade, which must be added to observed temperatures in order to reduce them to sea level.

The rate of decrease of temperature with altitude varies from one region to another, and in the same region varies according to the season and the meteorological conditions; being in general greater in warm latitudes than in cold ones, greater in summer than in winter, and greater in cyclones than in anti-cyclones. For continental plateau regions, the reduction often becomes fictitious or illusory. The use of the tables theresore requires experience and judgment in selecting the rate of decrease of temperature to be used.

The tables are given in order to facilitate the reduction of temperature either upwards or downwards in special investigations, but the reduction is not ordinarily applied to meteorological observations.

The tables, 7 and 8, are computed for rates of temperature change ranging from $\mathrm{I}^{\circ}$ Fahrenheit in 200 feet to $\mathrm{I}^{\circ}$ Fahrenheit in 900 feet, and from $I^{\circ}$ Centigrade in 100 metres to $I^{\circ}$ Centigrade in 500 metres; and for altitudes up to 5,000 feet and 3,000 metres respectively.

## Example, Table 7:

Observed temperature at an elevation of 2,500 feet,
Reduction to sea level for an assumed decrease in temperature of $r^{\circ} F$. for every 300 feet,
$+8.3$
Temperature reduced to sea level,

Example, Table 8 :
Observed temperature at an elevation of 500 metres, $12{ }^{\circ}{ }_{5} C$.
Reduction to sea level for an assumed decrease in temperature of $I^{\circ} C$. for every 200 metres,

$$
+2^{\circ} .5
$$

Temperature reduced to sea level,
I5.ㅇ $C$.

## CORRECTION FOR THE TEMPERATURE OF THE MERCURY IN THE THERMOMETER STEM.

table 9. Fahrenheit thermometers; Centigrade thermometers.
When the temperature of the thermometer stem is materially different from that of the bulb, a correction needs to be applied to the observed reading in order to correct it for the difference in the length of the mercury column caused by this difference in its temperature. This correction frequently becomes necessary in physical experiments where the bulb only is immersed in a bath whose temperature is to be determined, and in meteorological observations it may become appreciable in wet-bulb, dew point, and solar radiation thermometers, when the temperature of the bulb is considerably above or below the air temperature.

If $t^{\prime}$ be the average temperature of the mercury column, $t$ the observed reading of the thermometer, $n$ the length of mercury in the stem in scale degrees, and $a$ the apparent expansion of mercury in glass for $I^{\circ}$, the correction is given by the expression

$$
-a n\left(t^{\prime}-t\right)
$$

in which, for Centigrade temperatures, $a=0.000154$ or 0.000155 .
The average temperature of the mercury column can not be directly observed and is difficult to determine, for it differs from the temperature of the glass stem by an amount depending on the conduction of heat between the bulb and the mercury column. Practically however it is possible to use the actually observed temperature of the glass stem as the value of $t^{\prime}$ by making a small compensating change in the value of $a$, and this appears to be the simplest method that has been proposed. Mr. T. E. Thorpe (Journal of the Chemical Society, vol. 37, 188o, p. 160) has determined by a series of experiments that the proper thermometric corrections will be obtained by this method if o.000I43 be used as a coefficient (for Centigrade temperatures) instead of the value of a given above, and this value has been adopted in the present tables.

The correction formulæ are, then,
$T=t-0.0000795 n\left(t^{\prime}-t\right)$ Temperature Fahrenheit.
$T=t-0.000143 n\left(t^{\prime}-t\right)$ Temperature Centigrade.
in which $T=$ Corrected temperature.
$t=$ Observed temperature.
$t^{\prime}=$ Mean temperature of the glass stem.
$n=$ Length of mercury in the stem in scale degrees.

When $t^{\prime}$ is $\left\{\begin{array}{c}\text { greater } \\ \text { less }\end{array}\right\}$ than $t$, the numerical correction is to be $\left\{\begin{array}{c}\text { subtracted. } \\ \text { added. }\end{array}\right\}$ Example :

The observed temperature of a black bulb thermometer is $120.4 F_{\text {. , the }}$ temperature of the glass stem is $55^{\circ} 2 \mathrm{~F}$. and the length of mercury in the stem is $130^{\circ} F$. To find the corrected temperature.

With $n=130^{\circ} F$. and $-t^{\prime} t=[-] 65^{\circ} F$., as arguments, the table gives the correction $0^{\circ} .7 F_{\text {. , which by }}$, above rule is to be added to the observed temperature. The corrected temperature is therefore $121.1 F$.

## BAROMETRICAL TABLES.

## REDUCTION TO A STANDARD TEMPERATURE OF OBSERVATIONS MADE WITH barometers having brass scales.

The indicated height of the mercurial column in a barometer varies not only with changes of atmospheric pressure, but also with variations of the temperature of the mercury and of the scale. It is evident therefore that if the height of the barometric column is to be a true relative measure of atmospheric pressure, the observed readings must be reduced to the values they would have if the mercury and scale were maintained at a constant standard temperature.

This reduction is known as the reduction for temperature, and combines both the correction for the expansion of the mercury and that for the expansion of the scale, on the assumption that the attached thermometer gives the temperature both of the mercury and of the scale.

The freezing point is universally adopted as the standard temperature of the mercury, to which all readings are to be reduced. The temperature to which the scale is reduced is che normal or standard temperature of the adopted standard of length. For English scales, which depend upon the English yard, this is $62^{\circ}$ Fahrenheit. For metric scales, which depend upon the metre, it is $o^{\circ}$ Centigrade.

As thus reduced, observations made with English and metric barometers become perfectly comparable when converted by the ordinary tables of linear conversion, viz.: millimetres to inches and inches to millimetres (see Tables 64,65 ), for these conversions refer to the metre at $0^{\circ}$ Centigrade and the English yard at $62^{\circ}$ Fahrenheit.

The general formula for reducing barometric readings to a standard temperature is

$$
C=-B \frac{m(t-T)-l(t-\theta)}{\mathrm{I}+m(t-T)}
$$

in which $C=$ Correction for temperature.
$B=$ Observed height of the barometric column.
$t=$ Temperature of the attached thermometer.
$T=$ Standard temperature of the mercury.
$m=$ Coefficient of expansion of mercury.
$l=$ Coefficient of linear expansion of brass.
$\theta=$ Standard temperature of the scale.
The accepted determination of the coefficient of expansion of mercury is that given by Broch's reduction of Regnault's experiments, viz :

$$
m\left(\text { for } \mathrm{r}^{\circ} C .\right)=10^{-9}\left(181792+0.175 t+0.035116 t^{2}\right) .
$$

As a sufficiently accurate approximation, the intermediate value

$$
m=0.00018 \mathrm{r} 8
$$

has been adopted uniformly for all temperatures in conformity with the usage of the International Meteorological Tables.

Various specimens of brass scales made of alloys of different composition show differences in their coefficients of expansion amounting to eight and sometimes ten per cent. of the total amount. The Smithsonian Tables prepared by Prof. Guyot were computed with the average value $l\left(\right.$ for $\left.\mathrm{I}^{\circ} \mathrm{C}\right)=0.0000188$; for the sake of uniformity with the International Meteorological Tables, the value

$$
l=0.0000184
$$

has been used in the present volume. For any individual scale, either value may easily be in error by four per cent.

A small portion of the tables has been independently computed, but the larger part of the values have been copied from the International Meteorological Tables, one inaccuracy having been found and corrected.

TABLE 10. Reduction of the barometer to standard temperature-Englis/h measures.

For the English barometer the formula for reducing observed readings to a standard temperature becomes

$$
C=-B \frac{m\left(t-32^{\circ}\right)-l\left(t-62^{\circ}\right)}{\mathrm{I}+m\left(t-32^{\circ}\right)}
$$

in which $B=$ Observed height of the barometer in English inches.
$t=$ Temperature of attached thermometer in degrees Fahrenheit.

$$
\begin{aligned}
m & =0.0001818 \times \frac{5}{9}=0.000101 \\
l & =0.0000184 \times \frac{5}{9}=0.0000102
\end{aligned}
$$

The combined reduction of the mercury to the freezing point and of the scale to $62^{\circ}$ Fahrenheit brings the point of no correction to approximately
28.5 Fahrenheit, and this is therefore the standard temperature to which all readings are reduced. For temperatures above 28.5 Fahrenheit, the correction is subtractive, and for temperatures below $28^{\circ} .5$ Fahrenheit, the correction is additive, as indicated by the signs ( + ) and ( - ) inserted throughout the table.

The table gives the corrections for every half degree Fahrenheit from $0^{\circ}$ to 100 . The limits of pressure are 19 and 31.6 inches, the corrections being computed for every half inch from 19 to 24 inches, and for every two tenths of an inch from 24 to 3 r. 6 inches.

## Example :

| Observed height of barometer | $=29.143$ |
| :--- | :--- |
| Attached thermometer, $54^{\circ} 5 \mathrm{~F}$. | $=-0.068$ |
| Reduction for temperature | $=\underline{29.075}$ |
| Barometric reading corrected for temperature | $=$ |

TABLE 11.
TABLE 11. Reduction of the barometer to standard temperature-Metric measures.

For the metric barometer the formula for reducing observed readings to the standard temperature, $\circ^{\circ} C$., becomes

$$
C=-B \frac{(m-l) t}{1+m t}
$$

in which $C$ and $B$ are expressed in millimetres and $t$ in Centigrade degrees.

$$
m=0.00018 \mathrm{I} 8 ; \quad l=0.0000184 .
$$

In the tables, the limits adopted for the pressure are 440 and 795 millimetres, the intervals being io millimetres between 440 and 600 millimetres, and 5 millimetres between 600 and 795 millimetres.

The limits adopted for the temperature are $0^{\circ}+$ and +35.8 , the intervals being 0.5 and 1.0 from 440 to 560 millimetres, and 0.2 from 560 to 795 millimetres.

For temperatures above $0^{\circ}$ Centigrade the correction is negative, and hence is to be subtracted from the observed readings.

For temperatures below $0^{\circ}$ Centigrade the correction is positive, and from $0^{\circ} \mathrm{C}$. down to $-20^{\circ} \mathrm{C}$. the numerical values thereof, for ordinary barometric work, do not materially differ from the values for the corresponding temperatures above $0^{\circ} \mathrm{C}$. Thus the correction for $-9^{\circ} \mathrm{C}$. is numerically the same as for $+9^{\circ} \mathrm{C}$. and is taken from the table. In physical work of extreme precision, the numerical values given for positive temperatures may be used for temperatures below $0^{\circ} \mathrm{C}$. by applying to them the following corrections :

Corrections to be applied to the tabular values of Table 11 in order to use them when the temperature of the attached thermometer is below $0^{\circ}$ Centigrade.

| Temperature. | PRESSURE IN MILITMETRES. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 450 | 500 | 550 | 600 | 650 | 700 | 750 | 800 |
| c. | mm. | mm . | mm. | mm. | mm. | mm. | mm . | mm. |
| $-\mathrm{I}^{\circ}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| - 9 | .oo | . 0 | .00 | .00 | . 0 | . 00 | . 00 | . 0 |
| - 10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | +0.01 | +0.01 | +0.01 |
| 11 | . 0 | . 00 | . 00 | . 00 | +0.01 | . 01 | . OI | . 01 |
| 12 | .oo | . 00 | . 00 | +0.01 | .or | .or | .or | .or |
| 13 | . 0 | . 00 | +0.01 | .oi | .or | .or | . OI | .or |
| - 14 | .00 | +0.01 | .or | .or | .or | . or | . OI | . or |
| $-15$ | +0.01 | +0.01 | +0.01 | +0.01 | + 0.01 | +0.01 | +0.01 | +o.01 |
| 16 | . 01 | . Or | .or | . OI | . 0 I | .or | . 01 | . OI |
| 17 | . OI | . OI | . OI | .or | .or | . Or | .or | . 02 |
| 18 | . 01 | . OI | .or | .or | . Or | . OI | .or | . 02 |
| $-19$ | .or | .or | .or | .or | .or | . OI | . 02 | . 02 |
| -20 | + 0.01 | +0.01 | + 0.01 | +0.01 | +0.01 | +0.02 | +0.02 | +0.02 |
| 21 | .or | . OI | . OI | . 02 | . 02 | . 02 | . 02 | . 02 |
| 22 | .or | .or | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 |
| 23 | .oI | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 |
| -24 | .or | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 03 |

## Example:

Observed height of barometer, $7^{6} 3 \cdot 17^{m m}$ : Temperature of the attached thermometer, $-12^{\circ} \mathrm{C}$.
Numerical value of the reduction for $+12^{\circ} \mathrm{C}$.


Correction for temperature below $0^{\circ} \mathrm{C}$.
Reduction for $-12^{\circ} \mathrm{C}$.
Observed height of barometer
Barometer corrected for temperature

## REDUCTION OF THE BAROMETER TO STANDARD GRAVITY AT LATITUDE $45^{\circ}$

The atmospheric pressure is measured by the weight of the mercurial column of the barometer, but by common usage the pressures are expressed in terms of the height of the barometric column instead of by its weight. The observed height however is not a true measure of the pressure, because it changes with the temperature of the mercury and with the variations in the value of gravity. Therefore to obtain a height that shall be a true relative measure of the atmospheric pressure, the observed height of the mercurial column must be reduced to that which would be measured at a standard temperature and under a uniform standard value of gravity.

The standard value of gravity adopted is that prevailing at latitude $45^{\circ}$ and sea level. The reduction, accordingly, consists of two parts - a correction for altitude and a correction for latitude. The gravity correction for altitude is usually combined with the reduction of the barometer to sea level ; the gravity correction for latitude, which is here given, is commonly called simply the "gravity correction," or the "reduction to standard gravity."

If $B_{\phi}$ and $B_{48}$ represent the barometric heights (corrected for temperature) at latitudes $\phi$ and $45^{\circ}$, and $g_{\phi}, g_{45}$ the acceleration of gravity at these latitudes, we have

$$
\frac{B_{\phi}}{B_{45}}=\frac{g_{45}}{g_{\phi}}
$$

and the correction to the observed height will be

$$
C=B_{45}-B_{\phi}=-B_{\phi}\left(\mathrm{I}-\frac{g_{\phi}}{g_{45}}\right)
$$

If the earth be an ellipsoid of revolution composed of homogeneous homofocal layers arranged according to any law of density,

$$
g_{\phi}=g_{45}(1-k \cos 2 \phi)
$$

in which $k$ is a constant depending on the ellipticity of the earth; and the correction becomes

$$
C=-k \cos 2 \phi B_{\phi} .
$$

The value of $k$ adopted here is that determined by Prof. Harkness,*

$$
k=0.002662
$$

The correction is the same numerically for $\phi=45^{\circ}+a$ and $\phi=45^{\circ}-a$. It is negative for latitudes below $45^{\circ}$ and positive for latitudes above $45^{\circ}$

TABLES 12, 13.
Table 12 (English measures) gives the correction in thousandths of an inch for every degree of latitude and for each inch of barometric pressure from 19 to 30 inches.
table 13 (Metric measures) gives the correction in hundredths of a millimetre for each 20 millimetres barometric pressure from 520 to 770 millimetres.

## Example:

Barometric reading (corrected for temperature) at Dodge City, latitude $37^{\circ} 45^{\prime}, \quad=27.434$
Gravity correction for latitude from Table 12,

$$
=-0.018
$$

Barometer reduced to latitude $45^{\circ}$, $=27.416$

[^0]
## REDUCTION OF THE BAROMETER TO SEA LEVEL.

The fundamental formula for reducing the barometer to sea level and for determining heights by the barometer is the original formula of Laplace, amplified into the following form-

$$
Z=K(\mathrm{I}+a \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-0.378 \frac{e}{b}}\right)(\mathrm{I}+k \cos 2 \phi)\left(\mathrm{I}+\frac{h+h_{\mathrm{o}}}{R}\right) \log \frac{p_{\mathrm{o}}}{\bar{p}}
$$

in which $h=$ Height of the upper station.
$h_{\mathrm{o}}=$ Height of the lower station.
$Z=h-h_{0}$.
$p=$ Atmospheric pressure at the upper station.
$p_{0}=$ Atmospheric pressure at the lower station.
$R=$ Mean radius of the earth.
$\theta=$ Mean temperature of the air column between the altitudes $h$ and $h_{0}$.
$e=$ Mean pressure of aqueous vapor in the air column.
$b=$ Mean barometric pressure of the air column.
$\phi=$ Latitude of the stations.
$K=$ Barometric constant.
$a=$ Coefficient of the expansion of air.
$k=$ Constant depending on the figure of the earth.
The pressures $p_{0}$ and $p$ are computed from the height of the column of mercury at the two stations; the ratio $\frac{B_{0}}{B}$ of the barometric heights may be substituted for the ratio $\frac{p_{0}}{p}$, if $B$ o and $B$ are reduced to the values that would be measured at the same temperature and under the same relative value of gravity.

The correction of the observed barometric heights for instrumental temperature is always separately made, but the correction for the variation of gravity with altitude is generally introduced into the formula itself.

If $B_{0}, B$ represent the barometric heights corrected for temperature only, we have the equation

$$
\frac{p_{\circ}}{\bar{p}}=\frac{B_{0}}{B}\left(\mathrm{I}+\mu \frac{Z}{R}\right)
$$

$\mu$ being a constant depending on the variation of gravity with altitude.

$$
\log \frac{p_{\circ}}{\not p}=\log \frac{B_{\mathrm{o}}}{B}+\log \left(\mathrm{r}+\mu \frac{Z}{R}\right)
$$

Since $\frac{\mu Z}{R}$ is a very small fraction, we may write

$$
\text { Nap. } \log \left(\mathrm{r}+\frac{\mu Z}{R}\right)=\frac{\mu Z}{R}, \text { and } \log \left(\mathrm{I}+\frac{\mu Z}{R}\right)=\frac{\mu Z}{R} M
$$

$M$ being the modulus of common logarithms.

By substituting for $Z$ its approximate value $Z=K \log \frac{B_{0}}{B}$, we have

$$
\log \left(\mathrm{I}+\frac{\mu Z}{R}\right)=\frac{\mu K}{R} M \log \frac{B_{\circ}}{B} .
$$

With these substitutions the barometric formula becomes

$$
\begin{gathered}
Z=K(\mathrm{I}+\alpha \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-\mathrm{o} .378 \frac{e}{b}}\right)(\mathrm{I}+k \cos 2 \phi)\left(\mathrm{I}+\frac{h+h_{\mathrm{o}}}{R}\right) \\
\left(\mathrm{I}+\frac{\mu K}{R} M\right) \log \frac{B_{\mathrm{o}}}{B} .
\end{gathered}
$$

As a further simplification we shall put

$$
\beta=0.378 \frac{e}{b}, \gamma=k \cos 2 \phi \text { and } \eta=\frac{\mu K}{R} M,
$$

and write the formula-

$$
Z=K(\mathrm{I}+a \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-\beta}\right)(\mathrm{r}+\gamma)\left(\mathrm{I}+\frac{h+h_{\mathrm{o}}}{R}\right)(\mathrm{r}+\eta) \log \frac{B_{0}}{B} .
$$

Values of the constants.-The barometric constant $K$ is a complex quantity defined by the equation

$$
K=\frac{\Delta \times B_{n}}{\delta \times M} .
$$

$B_{n}$ is the normal barometric height of Laplace, 760 mm .
$\Delta$ is the density of mercury at the temperature of melting ice. M. Marek (Travaux et Mémoires du Bureau international des Poids et Mesures, t. II, p. D 55) gives the value, $\Delta=13.5956$, and finds that different specimens of mercury purified by different processes differ from this by several units in the fourth decimal. The International Meteorological Committee have taken the value

$$
\Delta=13.5958,
$$

and for the sake of uniformity this value is here adopted.
$\delta$ is the density of dry air at $0^{\circ} C$. and under the pressure of a column of mercury $B_{n}$ at the sea level and at latitude $45^{\circ}$. The value adopted by the International Bureau of Weights and Measures (Travaux et Mémoires, t. $\mathrm{I}, \mathrm{p}, \mathrm{A} 54$ ) is

$$
\delta=0.001293052
$$

$M$ (the modulus of common logarithms) $=0.4342945$.
These numbers give for the value of the barometric constant

$$
K=18400 \text { metres. }
$$

For the remaining constants, the following values have been used :
$a=0.00367$ for $r^{\circ}$ Centigrade. (International Bureau of Weights and Measures : Travaux et Mémoires, t. I, p. A 54.)
$\gamma=k \cos 2 \phi=0.002662 \cos 2 \phi$. (Harkness : The solar parallax, etc., see p . xix.)
$R=6367324$ metres. (A. R. Clarke: Geodesy, $8^{\circ}$, Oxford, 1880.)
$\eta=\frac{\mu K M}{R}=0.002396$. (Ferrel : Report Chief Signal Officer, 1885, pt. 2, p. 393.)
In reducing the barometer to sea-level, $h_{\mathrm{o}}=0$, and the factor $\left(\mathrm{I}+\frac{h+h_{\mathrm{o}}}{R}\right)$ becomes $\left(\mathrm{r}+\frac{Z}{R}\right)$. Taking the product of this factor and $K(\mathrm{r}+a \theta)$ ( $\mathrm{I}+n$ ), and neglecting the term in $\theta Z$, the formula becomes in metric measures

$$
Z \text { (metres) }=(\mathrm{I} 8444+67.53 \theta c .+0.003 Z)\left(\frac{\mathrm{I}}{\mathrm{I}-\beta}\right)(\mathrm{I}+\gamma) \log \frac{B}{B},
$$ and in English measures

$$
Z(\text { feet })=\left(56573+123.1 \theta^{\circ} F+0.003 Z\right)\left(\frac{\mathrm{I}}{\mathrm{I}-\beta}\right)(\mathrm{I}+\gamma) \log \frac{B_{0}}{B} .
$$

The form adopted for the tables is that of M. Angot.*
Taking the formula in English measures, let

$$
m=\frac{Z}{56573+123.1 \theta+0.003 Z} \cdot \frac{1}{1-\beta} .
$$

Then disregarding the small correction for gravity, $m=\log \frac{B_{0}}{B}$ gives an approximate value of $B_{0}$, and the correction to be added to the observed pressure to obtain the sea-level pressure is

$$
C=B_{\circ}-B=B\left(\mathrm{ro}^{m}-\mathrm{r}\right) .
$$

If $m_{1}$ be the value of $m$ corrected for gravity, we have

$$
m_{1}=\frac{m}{\mathrm{I}+\gamma} \text { or, approximately, }=m-m \gamma .
$$

The correction for gravity is therefore made by applying to the approximate value $m$ the small correction $m \gamma$. With this corrected value of $m$, the reduction to sea-level is given by the expression

$$
B\left(\mathrm{ro}^{m}-\mathrm{r}\right) .
$$

The above fraction designated $m$ contains the altitude $Z$, the mean temperature $\theta$, and the humidity factor $\frac{\mathrm{I}}{\mathrm{I}-\beta}$. In the Smithsonian tables, meteorological and physical, by Dr. A. Guyot, the distinguished author

[^1]in treating of this humidity factor in connection with hypsometric tables took the following position :
"To introduce a separate correction for the expansion of aqueous vapor " is, in the writer's view, a doubtful improvement. The laws of the distri-
" bution and transmission of moisture through the atmosphere are too little
" known, and its amount, especially in mountain regions, is too variable, and
"depends too much upon local winds and local condensation, to allow a " reasonable hope of obtaining the mean humidity of the layer of air between " the two stations by means of hygrometrical observations made at each of "them. These doubts are confirmed by the experience of the author and " of many other observers, which shows that, on an average, Laplace's " method works not only as well as the other, but more uniformly well. At " any rate the gain, if there be any, is not clear enough to compensate for " the undesirable complication of the formula."

Since this position was taken by Dr. Guyot forty years ago, there has been no such advance in our knowledge as to impair the practical conclusion in conformity with which he constructed his hypsometric table. Accordingly in treating this portion of the formula in the construction of the present tables for the reduction of the barometer to sea level, it has been deemed advantageous to retain the method adopted by Guyot, and to incorporate the humidity factor in the temperature term, thereby assuming the air to contain the average degree of humidity corresponding to the actually prevailing condition of temperature.

In evaluating the humidity factor as a function of the air temperature, the tables given by Prof. Ferrel have been adopted (Meteorological researches. Part iii.-Barometric hypsometry and reduction of the barometer to sea level. Report, U. S. Coast Survey, 1881. Appendix io.) These tables by interpolation, and by extrapolation below $\circ^{\circ} F$., give the following values for $\beta$ :

For Fahrenheit temperatures,

| $\theta$ | $\beta$ | $\theta$ | $\beta$ | $\theta$ | $\beta$ | $\theta$ | $\beta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. |  | F. |  | F. |  | F. |  |
| $-20^{\circ}$ | 0.00008 | $10^{\circ}$ | 0.00104 | $36^{\circ}$ | 0.00267 | $62^{\circ}$ | 0.00724 |
| - 16 | . 00020 | 12 | .00111 | 38 | . 00293 | 64 | . 00762 |
| - 12 | .00032 | 14 | . 00118 | 40 | .00322 | 66 | .0080I |
| $-8$ | . 00044 | 16 | . 00126 | 42 | . 00353 | 68 | . 00839 |
|  |  | 18 | .00134 | 44 | . 00386 | 70 | . 00877 |
| $-6$ | 0.00050 | 20 | . 00143 | 46 | . 00421 | 72 | . 00914 |
| - 4 | . 00056 | 22 | .00153 | 48 | . 00458 |  |  |
| $-2$ | . 00062 | 24 | .00163 | 50 | . 00496 | 76 | 0.00990 |
| 0 | . 00068 | 26 | .00174 | 52 | . 00534 | 80 | . 01065 |
| $+2$ | . 00075 | 28 | .00187 | 54 | . 00572 | 84 | .OII4I |
|  | . 00082 | 30 | . 00203 | 56 | .00610 | 88 | .OI217 |
| 6 | .00089 | 32 | . 00222 | 58 | .00648 | 92 |  |
| 8 | 0.00096 | 34 | 0.0243 | 60 | . 00686 | 96 | . 01369 |

For Centigrade temperatures,

| $\theta$ | $\beta$ | $\theta$ | $\beta$ | $\theta$ | $\beta$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| c. |  | c. |  | c. |  |
| $-18^{\circ}$ | 0.0007 | $\circ^{\circ}$ | 0.0022 | $18^{\circ}$ | 0.0077 |
| -16 | .0008 | $+2$ | . 0026 | 20 | . 0084 |
| -14 -12 | .0009 | 4 6 | .0031 .0037 .0031 | 22 24 | .0091 |
| - 12 - 10 | . $01012+$ | 6 | .0037 | 24 26 | .00974 |
|  | . 0013 | ı |  | 28 | . 0111 |
| -6 -4 | . 0015 | 12 14 14 | . 0056 | 30 32 | . 0118 |
| - ${ }_{2}$ | . O . 019 | 14 16 | . 0070 | 34 3 | .0132 |
|  |  |  |  | 36 | .or39 |

The practical tables consist essentially of two mutually dependent parts:-the first gives values of 2000 m in a table of double entry of which the altitude of the station and the mean temperature of the air between the station and sea level are the arguments; the second gives the reduction to sea level in a table of double entry of which the arguments are 2000 m and the observed barometric height corrected for temperature. In addition, a subsidiary table gives the small correction for latitude to be applied to the values of 2000 m . This correction, while of theoretical interest, seldom becomes of practical importance, since its effect is in general overshadowed by the relatively large uncertainties incident to the determination of the true mean temperature.

The mean temperature of the air column is to be obtained from the observed temperature at the station by employing some assumption as to the rate of change of temperature with altitude. In the discussion of barometric observations made in the mountain and plateau regions of the United States, it has been found that this rate of change is a climatic factor which needs to be determined for every station for different seasons of the year, and for different atmospheric conditions. When the results of such investigations are embodied in tables for reduction to sea level, the tables and the method of their use may be simplified and the labor of obtaining the reduction greatly abridged; but in the nature of the case, these special methods can not be utilized in the construction of general tables which are to be applicable to all phases of topography and climate.

Whatever method be used for obtaining the mean temperature of the air column ( $\theta$ ) from the observed temperature at the station, the former and hence the latter is subject to the important condition that it shall not contain the diurnal fluctuation. Hence in reducing to sea level any indi--vidual observation of the barometer, the simultaneous observation of air temperature used in obtaining $\theta$ should be reduced to the daily mean by a correction, or, better, the actual mean temperature of the preceding twentyfour hours should be taken.

TABLES 14, 15, 16.
Tables 14,15,16. Reduction of the barometer to sea level-English measures.

Table 14 gives values of $2000 \times m$.

$$
m=\frac{Z}{56573+\mathrm{I} 23 . \mathrm{I} \theta+0.003 Z} \cdot \frac{\mathrm{I}}{\mathrm{I}-\beta}
$$

The temperature $\theta$ varies by intervals of $2^{\circ}$ from $-20^{\circ} F$. to $96^{\circ} F$, except near the extremities of the table where the interval is $4^{\circ}$ The altitude $Z$ varies by intervals of 100 feet from 100 to 9000 feet. The values of 2000 m are given to one decimal.

In order to facilitate interpolations for sractions of a 100 feet in altitude, the tabular differences for 100 feet have been added on each line.

Table 15 gives a small correction to $2000 m$ for latitude, computed from the expression

$$
2000 m \times 0.002662 \cos 2 \phi
$$

The arguments are 2000 m , which varies by tens from 10 to 350 , and the latitude, which varies by $5^{\circ}$ from $0^{\circ}$ to $90^{\circ}$. The correction is to be subtracted for latitudes below $45^{\circ}$ and added for latitudes above $45^{\circ}$ The tabular values are given to one decimal.

Table 16, with the value of $2000 m$ thus corrected, gives the correction which must be applied to the barometric reading $B$ (corrected for temperature) to reduce it to sea level. The arguments are $B$, which varies by 0.5 inch from 31.00 inches to 19.5 inches, and values of 2000 m , which are given for every unit from 1 to 334 .

The reduction values $B \circ-B$ are given to o.or inch.

## Example :

Let $B=26.24$ inches be the barometric reading (corrected for temperature) observed at a station whose altitude is 3572 feet, and latitude 32. Suppose the mean temperature of the air column $\theta=63^{\circ} \circ \mathrm{F}$.

Table 14 gives (p. 63) with $Z=3,500$ feet and $\theta=62.8 \mathrm{~F}$., $2000 \mathrm{~m}=108.0$
The difference for 72 feet is
The approximate value of 2000 m is
IIO. 2

Table 15 , with $2000 m=110$ and latitude $=32^{\circ}$, gives the subtractive correction O.I. Hence the corrected value of 2000 m is IIo.i.

With $2000 m=$ IIo. I and $B=26.24$, Table 16 (p. 72) gives the reduction to sea level, 3.55 inches. Accordingly the barometric pressure reduced to sea level is

$$
B_{.}=26.24+3.55=29.79 \text { inches. }
$$

tables 17, 18, 19. Reduction of the barometer to sea level-Metric measures.
For reducing to sea level readings of the metric barometer, the barometric formula in metric measures derived on page xxii is treated in the same manner as the formula in English measures just described in detail, and the method of construction of the tables is the same.

Table 17 gives values of 2000 m .

$$
m=\frac{Z}{18444+67.53 \theta+0.003 Z} \cdot \frac{\mathrm{I}}{\mathrm{I}-\beta} .
$$

The temperature $\theta$ varies by intervals of $2^{\circ}$ from $-16^{\circ} \mathrm{C}$. to $+36^{\circ} \mathrm{C}$. except near the extremities of the table where the interval is $4^{\circ}$. The altitude $Z$ varies by io metres from io to 3000 metres. The values of 2000 m are given to one decimal.

Table 18 gives the small correction to $2000 m$ for latitude. The arguments are 2000 m , which varies by tens from 10 to 350 , and the latitude which varies by $5^{\circ}$ from $0^{\circ}$ to $90^{\circ}$. The correction is to be subtracted for latitudes below $45^{\circ}$ and added for latitudes above $45^{\circ}$. The tabular values are given to one decimal. The value of 2000 m thus corrected is then used in entering Table 19.

Table 19 gives the correction which must be applied to the barometric reading $B$ (corrected for temperature) to reduce it to sea level. The arguments are $B$, which varies by 10 mm . from 790 mm . to 480 mm ., and values of $2000 m$ which vary by units from I to 345 . The tabular values $B_{0}-B$ are given to 0.1 mm .

## Example :

Let $B=648.7 \mathrm{~mm}$. be the barometric reading observed and corrected for temperature at a station whose altitude is I 353 metres and latitude $32^{\circ}$ Suppose the mean temperature of the air column $\theta=14.3 \mathrm{C}$.
Table 17 gives (p. 83) for $\theta=14^{\circ}$ and $Z=1353, \quad 2000 m=138.6$
The proportional part for 0.3 is
Hence the approximate value of 2000 m is
Table 18, with $2000 m={ }_{1} 88$ and latitude $32^{\circ}$, gives the subtractive correction c.15. Hence the corrected value of 2000 m is I 38.3 . With this value and $B=649 \mathrm{~mm}$. as arguments, Table ig gives $B_{0}-B=112.0 \mathrm{~mm}$.

Accordingly the barometric reading reduced to sea level is

$$
B_{\circ}=648.7+112.0=760.7 \mathrm{~mm} .
$$

THE DETERMINATION OF HEIGHTS BY THE BAROMETER.
tables 20, 21, 22, 23, 24. English Measures.
The barometric formula developed in the preceding section (see p. xxi) is arranged in the following form for determining heights by the barometer.

$$
Z=K\left(\log B_{0}-\log B\right)\left[\begin{array}{l}
(\mathrm{I}+\alpha \theta) \\
(\mathrm{I}+\beta) \\
(\mathrm{I}+k \cos 2 \phi)(\mathrm{I}+\eta) \\
\left(\mathrm{I}+\frac{Z+2 h_{\mathrm{o}}}{R}\right)
\end{array}\right]
$$

in which $K\left(\log B_{0}-\log B\right)$ is an approximate value of $Z$ and the factors in the brackets are correction factors depending respectively on the air temperature, the humidity, the variation of gravity with latitude, the variation of gravity with altitude in its effect on the weight of mercury in the barometer, and the variation of gravity with altitude in its effect on the weight of the air. With the constants already given, the formula becomes in English measures :

$$
Z(\text { feet })=60368\left(\log B_{0}-\log B\right)\left[\begin{array}{l}
{\left[\mathrm{I}+0.002039\left(\theta-32^{\circ}\right)\right]} \\
(\mathrm{I}+\beta) \\
(\mathrm{I}+0.002662 \cos 2 \phi)(\mathrm{I}+0.00239) \\
\left(\mathrm{I}+\left(\frac{Z+2 h_{\mathrm{o}}}{R}\right)\right.
\end{array}\right]
$$

In order to make the temperature correction as small as possible for average air temperatures, $50^{\circ} F$. will be taken as the temperature at which the correction factor is zero. This is accomplished by the following transformation :

$$
1+0.002039\left(\theta-32^{\circ}\right)=\left[\mathrm{I}+0.002039\left(\theta-50^{\circ}\right)\right]\left[\mathrm{I}+0.0010195 \times 36^{\circ}\right] .
$$

The second factor of this expresssion combines with the constant, and gives $60368\left(\mathrm{I}+\mathrm{o} .00\right.$ Io $\left.95 \times 36^{\circ}\right)=62583.6$.

The first approximate value of $Z$ is therefore

$$
62583.6\left(\log B_{\circ}-\log B\right)
$$

In order further to increase the utility of the tables, we shall make a further substitution for $\log B_{\circ}-\log B$, and write

$$
62583.6\left(\log B_{\circ}-\log B\right)=62583.6 \log \left(\frac{29.9}{B}-\log \frac{29.9}{B_{\circ}}\right)
$$

Table 20 contains values of the expression

$$
62583.6 \log \frac{29.9}{B}
$$

for values of $B$ varying by intervals of o.or inch from 12.00 inches to 30.90 inches.

The first approximate value of $Z$ is then obtained by subtracting the tabular value corresponding to $B_{0}$ from the tabular value corresponding to $B$ ( $B$ and $B_{0}$ obeing the barometric readings observed and corrected ior temperature at the upper and lower stations respectively).

Table 21 gives the temperature correction

$$
Z \times 0.002039\left(\theta-50^{\circ}\right) .
$$

The side argument is the mean temperature of the air column $(\theta)$ given for intervals of $\mathrm{I}^{\circ}$ from $0^{\circ}$ to $100^{\circ} \mathrm{F}$. The top argument is the approximate difference of altitude $Z$ obtained from Table 20.

For temperatures above $50^{\circ} \mathrm{F}$., the correction is to be added, and for temperatures below $50^{\circ} \mathrm{F}$., the correction is to be subtracted. It will be observed that the correction is a linear function of $Z$, and hence, for example, the value for $Z=1740$ is the sum of the corrections in the columns headed 1000, 700, and 40.

In general, accurate altitudes can not be obtained unless the temperature used is freed from diurnal variation.

Table 22 gives the correction for latitude, and for the variation of gravity with altitude in its effect on the weight of the mercury. When altitudes are determined with aneroid barometers the second factor does not enter the formula. In this case the effect of the latitude factor can be obtained by taking the difference between the tabular value for the given latitude and the tabular value for latitude $45^{\circ}$. The side argument is the latitude of the station given for intervals of $2^{\circ}$. The top argument is the approximate difference of height $Z$.

Table 23 gives the correction for the average humidity of the air at different tem peratures; the values of the factor $(1+\beta)$ adopted by Prof. Ferrel and given on page xxiii have been used. This correction could have been incorporated with the temperature factor in Table 21, but it is given separately in order that the magnitude of the correction may be apparent, and in order that, when the actual humidity is observed, the correction may be computed if desired, by the expression

$$
Z\left(0.378 \frac{e}{b}\right)
$$

where $e$ is the mean pressure of vapor in the air column, and $b$ the mean barometric pressure.

The side argument is the mean temperature of the air column, varying by intervals of $2^{\circ}$ from $-20^{\circ} F$. to $96^{\circ} F$., except near the extremities of the table where the interval is $4^{\circ}$ The top argument is the approximate difference of altitude $Z$.

Table 24 gives the correction for the variation of gravity with altitude in its effect on the weight of the air. The side argument is the approximate difference of altitude $Z$, and the top argument is the elevation of the lower station $h_{0}$.

The corrections given by Tables 22, 23 and 24 are all additive.

## Example:

Let the barometric pressure observed, and corrected for temperature, at the upper and lower stations be, respectively, $B=23.61$ and $B_{0}=29.97$. Let the mean temperature of the air column be $35^{\circ} \mathrm{F}$., and the latitude $44^{\circ} 16^{\prime}$. To determine the difference of height.

| Table 20, argument 23.61, gives | $\begin{aligned} & \text { Feet. } \\ & 6420 \end{aligned}$ |
| :---: | :---: |
| Table 20, " 29.97, " | 64 |
| Approximate difference of height ( $Z$ ) | $=6484$ |
| Table 21, with $Z=6484$ and $\theta=35^{\circ} \mathrm{F}$., gives | - 198 |
| Table 22, with $Z=6300$ and $\phi=44^{\circ}$, gives | + 16 |
| Table 23, with $Z=6300$ and $\theta=35^{\circ} F$., gives | 17 |
| Table 24, with $Z=6300$ and $h_{\circ}=0$, gives |  |
| Final difference of height ( $Z$ ) | $=632 \mathrm{I}$ |

If in this example the barometric readings be observed with aneroid barometers, the correction to be obtained from Table 22 will be simply the portion due to the latitude factor, and this will be obtained by subtracting the tabular value for $45^{\circ}$ from that for $44^{\circ}$, the top argument being $Z=6300$. This gives $16-15=1$.
tables 25, 26, 27, 28, 29. Metric Measures.
The barometric formula developed on page xxi is, in metric units,

$$
Z(\text { metres })=18400\left(\log B_{0}-\log B\right)\left[\begin{array}{l}
(\mathrm{I}+0.00367 \theta C .) \\
\left(\mathrm{I}+0.378 \frac{e}{b}\right) \\
(\mathrm{I}+0.00266 \cos 2 \phi)(\mathrm{I}+0.00239) \\
\mathrm{I}+\frac{\left(Z+2 h_{\mathrm{o}}\right)}{6367323}
\end{array}\right]
$$

The approximate value of $Z$ (the difference of height of the upper and lower station) is given by the factor $18400\left(\log B_{\mathrm{o}}-\log B\right)$. This expression is computed by means of two entries of a table whose argument is the barometric pressure. In order that the two entries may result at once in an approximate value of the elevation of the upper and lower stations, a transformation is made, which gives the following identity:

$$
18400\left(\log B_{\circ}-\log B\right)=18400\left(\log \frac{760}{B}-\log \frac{760}{B_{0}}\right) .
$$

TABLE 25
Table 25 gives values of the expression $18400 \log \frac{760}{B}$ for values of $B$ varying by intervals of I mm . from 300 mm . to 779 mm . The first approximate value of $Z$ is then obtained by subtracting the tabular value corresponding to $B_{0}$ from the tabular value corresponding to $B$ ( $B$ and $B$ 。 being the barometric readings observed and reduced to $o^{\circ} C$. at the upper and lower
stations respectively). The first entry of Table 25 with the argument $B$ gives an approximate value of the elevation of the upper station above sea level, and the second entry with the argument $B$ 。gives an approximate value of the elevation of the lower station.

Table 26 gives the temperature correction: $0.00367 \theta C . \times Z$.
The side argument is the approximate difference of elevation $Z$ and the top argument is the mean temperature of the air column. The values of $Z$ vary by intervals of 100 m . from 100 to 4000 metres and the temperature varies by intervals of $1^{\circ}$ from $1^{\circ} C$. to $10^{\circ} \mathrm{C}$. with additional columns for $20^{\circ}$, $30^{\circ}$, and $40^{\circ} \mathrm{C}$. Attention is called to the fact that the formula is linear with respect to $\theta$, and hence that the correction, for example, for $27^{\circ}$ equals the correction for $20^{\circ}$ plus the correction for $7^{\circ}$. When the table is used for temperatures below $\circ^{\circ} C$., the tabular correction must be subtracted from, instead of added to, the approximate value of $Z$.

Table 27 (pp. II2 and II3) gives the correction for humidity resulting from the factor $0.378 \frac{e}{b} \times Z=\beta Z$.

Page 112 gives the value of $0.378 \frac{e}{b}$ multiplied by 10000 . The side argument is the mean pressure of aqueous vapor, $e$, which serves to represent the mean state of humidity of the air between the two stations. $e=\frac{1}{2}\left(f+f_{0}\right)$ ( $f$ and $f_{0}$. being the vapor pressures observed at the two stations) has been written at the head of the table, but the value to be assigned to $e$ is in reality left to the observer, independently of all hypothesis. The top argument is the mean barometric pressure $\frac{1}{2}\left(B+B_{0}\right)$.

The vapor pressure varies by millimetres from $I$ to 40 , and the mean barometric pressure varies by intervals of 20 mm . from 500 mm . to 760 mm . The tabular values represent the humidity factor $\beta$ or $0.378 \frac{e}{b}$, multiplied by 10000.

Page II3 gives the correction for humidity, with $Z$ and $10000 \times 0.378 \frac{e}{b}$ (derived from page it2) as arguments.

The approximate difference of altitude is given by intervals of roo metres from 100 to 4000 metres, and the values of $10000 \beta$ vary by intervals of 25 from 25 to 300 . The tabular values are given in tenths of metres to facilitate and increase the accuracy of interpolation.

Table 28 gives the correction for latitude, and for the variation of gravity with altitude in its effect on the weight of the mercurial column. When altitudes are determined with aneroid barometers, the latter factor does not enter the formula. In this case the effect of the latitude factor can be obtained by subtracting the tabular value for latitude $45^{\circ}$ from the tabular value for the latitude in question.

The side argument is the approximate difference of elevation $Z$, varying by intervals of 100 metres from 100 to 4000 . The top argument is the latitude varying by intervals of $5^{\circ}$ from $0^{\circ}$ to $75^{\circ}$

## TABLE 29.

Table 29 gives the correction for the variation of gravity with altitude in its effect on the weight of the air.

The side argument is the same as in Table 28 ; the top argument is the height of the lower station varying by intervals of 200 metres from o to 2000, with additional columns for 2500,3000 and 4000 metres.

## Example:

Let the barometric reading (reduced to $0^{\circ} C$.) at the upper station be 655.7 mm .; at the lower station, 772.4 mm . Let the mean temperature of the air column be $\theta=12.3 C$., the mean vapor pressure $e=9 \mathrm{~mm}$. and the latitude $\phi=32^{\circ}$.
Table 25, with argument $655 \cdot 7$, gives
II79 metres.
Table 25, " " 772.4, "
Approximate value of $Z$
$=1308$
Table 26, with $Z=1300$ and $\theta=12 .{ }^{\circ} C$, gives
59
Table 27, with $e=9 \mathrm{~mm}$. and $Z=1370$, gives 7
Table 28, with $Z=1370$ and $\phi=32^{\circ}$, gives 5
Table 29, with $Z=1370$ and $h_{\circ}=0$, gives
Corrected value of $Z \quad=1379$ metres.
TABLE 30.
TABLE 30. Difference of height corresponding to a change of 0.1 inch in the barometer-English measures.
If we differentiate the barometric formula, page xxvii, we shall obtain, neglecting insensible quantities,

$$
d Z=-2628 \mathrm{I} \frac{d B}{B}\left(\mathrm{I}+0.002039\left(\theta-32^{\circ}\right)\right)(\mathrm{I}+\beta)
$$

in which $B$ represents the mean pressure of the air column $d Z$.
Putting $d B=0$. I inch,

$$
d Z=-\frac{2628.1}{B}\left(\mathrm{I}+0.002039\left(\theta-32^{\circ}\right)\right)(\mathrm{I}+\beta)
$$

The second member, taken positively, expresses the height of a column of air in feet corresponding to a tenth of an inch in the barometer on the parallel of $45^{\circ}$ latitude. Since the last factor $(I+\beta)$, as given on page xxiii, is a function of the temperature, the function has only two variables and admits of convenient tabulation.

Table 30 , containing values of $d Z$ for short intervals of the arguments $B$ and $\theta$, has been taken from the Report of the U. S. Coast Survey, 1881, Appendix 10,-Barometric hypsometry and reduction of the barometer to sea level, by Wm. Ferrel.*

[^2]The temperature argument is given for every $5^{\circ}$ from $30^{\circ} \mathrm{F}$. to $85^{\circ} \mathrm{F}$., and the pressure argument for every 0.2 inch from 22.0 to 30.8 inches.

This table may be used in computing small differences of altitude, and, up to a thousand feet or more, very approximate results may be obtained.

## Example:

Mean pressure at Augusta, October, 1891, 29.94 ; temperature, $\quad 60.8 \mathrm{~F}$.
Mean pressure at Atlanta, October, 1891, 28.97 ; temperature, 59.4
Mean pressure of air column, $\quad B=29.455$; $\quad \theta=60^{\circ}$.
Entering the table with 29.455 and $60^{\circ}$ I as arguments, we take out 94.95 as the difference of elevation corresponding to a tenth of an inch difference of pressure. Multiplying this value by the number of tenths of inches difference in the observed pressures, viz. 97, we obtain the difference of elevation 92 I feet.

TABLE 31. Difference of height of air corresponding to a change of I millimetre in the barometer-Metric measures.

This table has been computed by converting Table 18 into metric units. The temperature argument is given for every $2^{\circ}$ from $-2^{\circ} \mathrm{C}$. to $+36^{\circ} \mathrm{C}$.; the pressure argument is given for every millimetre from 760 to 560 mm .
table 32. Babinet's formula for determining heights by the barometer.
Babinet's formula for computing differences of altitude* represents the formula of Laplace quite accurately for differences of altitude up to 1000 metres, and within one per cent for much greater altitudes. As it has been quite widely disseminated among travellers and engineers, and is of convenient application, the formula is here given in English and metric measures. It might seem desirable to alter the figures given by Babinet so as to conform to the newer values of the barometrical constants now adopted; but this change would increase the resulting altitudes by less than one-half of one per cent without enhancing their reliability to a corresponding degree, on account of the outstanding uncertainty of the assumed mean temperature of the air.

The formula is, in English measures,

$$
Z(\text { feet })=52494\left[\mathrm{r}+\frac{t_{0}+t-64^{\circ}}{900}\right] \frac{B_{0}-B}{B_{0}+B} ;
$$

and in metric measures,

$$
Z \text { (metres })=16000\left[\mathrm{I}+\frac{2\left(t_{\mathrm{o}}+t\right)}{1000}\right] \frac{B_{\circ}-B}{B_{\circ}+B}
$$

in which $Z$ is the difference of elevation between a lower and upper station at which the barometric pressures corrected for all sources of instrumental error are $B_{\mathrm{o}}$ and $B$, and the observed air temperatures are $t_{\mathrm{o}}$ and $t$, respectively.

[^3]For ready computation the formula is written

$$
Z=C \times \frac{B_{0}-B}{B_{0}+B},
$$

and the factor $C$, computed both in English and metric measures, has been kindly furnished by Prof. Cleveland Abbe. The argument is $\frac{1}{2}\left(t_{0}+t\right)$ given for every $5^{\circ}$ Fahrenheit between $10^{\circ}$ and $100^{\circ} F$., and for every $2^{\circ}$ Centigrade between $10^{\circ}$ and $40^{\circ}$ Centigrade.

In using the table, it should be borne in mind that on account of the uncertainty in the assumed temperature, the last two figures in the value of $C$ are uncertain, and are here given only for the sake of convenience of interpolation. Consequently one should not attach to the resulting altitudes a greater degree of confidence than is warranted by the accuracy of the temperatures and the formula. The table shows that the numerical factor changes by about one per cent of its value for every change of five degrees Fahrenheit in the mean temperature of the stratum of air between the upper and lower stations; therefore the computed difference of altitude will have an uncertainty of one per cent if the assumed temperature of the air is in doubt by $5^{\circ} \mathrm{F}$. With these precautions the observer may properly estimate the reliability of his altitudes whether computed by Babinet's formula or by more elaborate tables.

## Example:

Let the barometric pressure observed and corrected for temperature at the upper and lower stations be, respectively, $B=635 \mathrm{~mm}$. and $B_{\circ}=730 \mathrm{~mm}$. Let the temperatures be, respectively, $t=15^{\circ} \mathrm{C}$., $t_{0}=20^{\circ} \mathrm{C}$. To find the approximate difference of height.
With $\frac{1}{2}\left(t_{0}+t\right)=\frac{20^{\circ}+15^{\circ}}{2}=17^{\circ} .5 C$., the table in metric measures gives $C=17120$ metres. $\quad \frac{B_{0}-B}{B_{0}+B}=\frac{95}{1365}$.
The approximate difference of height $=17120 \times \frac{95}{1365}=1191.5$ metres.

THERMOMETRICAL MEASUREMENT OF HEIGHTS BY OBSERVATION OF THE
TEMPERATURE OF THE BOILING POINT OF WATER.
When water is heated in the open air, the elastic force of its vapor gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles and the water boils. The temperature at which water boils in the open air thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the higher the
station where an observation is made, the lower will be the temperature of the boiling point.

The difference of elevation between two places therefore can be deduced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and, the atmospheric pressures at both places being known, to compute the difference of height by the tables given herein for computing heights from barometric observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometric observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water gives only indirectly the atmospheric pressure, which is given directly by the barometer. This method is thus liable to all the chances of error which may affect the measurements by means of the barometer, besides adding to them new ones peculiar to itself, the principal of which is the difficulty of ascertaining with the necessary accuracy the true temperature of boiling water. In the present state of thermometry it would hardly be safe, indeed, to rely, in the most favorable circumstances, upon quantities so small as hundredths of a degree, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and substance of the vessel containing the water, the purity of the water itself, the position at which the bulb of the thermometer is placed, whether in the current of the steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric pressure. Owing to these various causes, an observation of the boiling point, differing by one-tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one-tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimetres in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one-tenth of a millimetre, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer is of the greatest utility to travellers and explorers in rough countries, on account of its being more conveniently transported and much less liable to accidents than the mercurial barometer. A suitable form for it, designed by Regnault (Annales de Chimie et de Physique, Tome xiv, p. 202), consists of an accurate thermometer with long degrees, subdivided into tenths. For observation the bulb is placed, about 2 or 3 centimetres above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp.

Barometric pressures corresponding to the temperature of boiling water.
TABLE 33.
TABLE 34.
English Measures.
Metric Measures.

Table 33 is a conversion into English measures of Table 34. The argument is the temperature of boiling water for every tenth of a degree from $185^{\circ} \circ$ to 212.9 Fahrenheit. The tabular values are given to the nearest o.oI inch.

Table 34 is Regnault's table of barometric pressures corresponding to temperatures of boiling water, revised by A. Moritz (Acad. Sci. Bull., St. Petersburg, xiii., 1855 , col. $4 \mathrm{r}-44$ ). To the degree of precision here desired, these values do not differ from the more recent reduction by Broch. The argument is given for every tenth of a degree from 80.0 to 100.9 C . The tabular values are given to the nearest o. 1 mm .

## HYGROMETRICAL TABLES.

PRESSURE OF AQUEOUS VAPOR IN SATURATED AIR.
Tables 35, 36, and 43, giving the pressure of aqueous vapor in saturated air, are based upon Dr. Broch's reduction of the observations of Regnault (Travaux et Mémoires du Bureau international des Poids et Mesures, t. I, p. A 19-39). This reduction assumes that the observations may be represented by the empirical formula

$$
F=A \times 10 \frac{b t+c t^{2}+d t^{3}+e t^{4}+f t^{5}}{1+a t}
$$

in which $F$ is the pressure of aqueous vapor expressed in millimetres of standard mercury, that is at $0^{\circ} \mathrm{C}$. and at latitude $45^{\circ}$ and sea level, its density being 55.59593 .
$t$, the temperature expressed in normal Centigrade degrees.

$$
\alpha=0.003667458
$$

By using the simultaneous values of $F$ and $t$ given by Regnault's observations, Dr. Broch obtained a series of observation equations whose solution by the method of least squares gave the following values for the coefficients :

$$
\begin{aligned}
A & =4.5686859 \\
b & =10^{-2} \times 3 . \mathrm{I} 34366 \mathrm{I} 74 \\
c & =-10^{-5} \times \mathrm{I} .4 \mathrm{I} 6 \mathrm{I} 2423 \\
d & =10^{-7} \times 1.935338308 \\
e & =-10^{-9} \times 2.646535 \mathrm{IO} 3 \\
f & =10^{-11} \times 1.139377 \mathrm{I} 58
\end{aligned}
$$

From this formula Broch's tables of vapor pressure were computed.

## TABLE 35. Pressure of aqueous vapor-English measures.

This table is a conversion into English measures of Table 36. It gives the vapor pressure in saturated air for temperatures varying by $0^{\circ} .2$ from -20.0 to 214.0 Fahrenheit.

The tabular values are given in inches to four decimals.
A column of differences for $0 . r$ is added for convenience in interpolating.
tables 36, 43. Pressure of aqueous vapor.-Metric measures.
These tables, taken from Broch, give the pressure of aqueous vapor to hundredths of a millimetre for temperatures varying by 0.1 . $C$. from - $29^{\circ}$. to $100^{\circ} 9$ Centigrade. The values for temperatures between $0^{\circ} \mathrm{C}$. and $45^{\circ} \mathrm{C}$. are given in Table 43, the remainder in Table 36.
table 37. Pressure of aqueous vapor at low temperature.-(C. F. Marvin.)
Broch's vapor pressures at temperatures below $0^{\circ} C$. $\left(32^{\circ} F\right.$.) as given in Tables 35 and 36 , when compared with the actual observed values of Regnault are found to be systematically too large. This discrepancy signifies that the e-npirical formula adopted by Broch fails to represent accurately the law of variation of vapor pressure for temperatures both above and below the freezing point. Moreover, the failure in the application of the formula might be inferred from the laws of diffusion following from the kinetic theory of gases, for these give no reason to suppose that the function expressing the relation between vapor pressure and temperature is continuous between the two states of water and ice.

Under proper conditions water can be cooled far below $0^{\circ} C$. ( $32^{\circ} \mathrm{F}$.) before solidifying, so that at the same temperature we may have it either in the liquid or the solid state, and experiments confirm the theory of diffusion in showing that the pressure of the vapor is different according as it is in contact with its liquid or its solid at the same temperature. The method hitherto employed of combining vapor pressures above and below freezing, and attempting to represent them by a single continuous function: must therefore be considered as radically erroneous.

Recognizing the systematic errors of the vapor pressures given by Broch's formula for temperature below freezing, the Chief Signal Officet lately authorized a new determination by direct observation. This experimental investigation has been carried out by Prof. C. F. Marvin, from the results of which (Annual Report Chief Signal Officer, 1891; Appendix No. ro,) Table 37 is reproduced. The interpolation between the observed pressures which were noted at intervals of about $5^{\circ} \mathrm{F}$., was effected graphically and not by mathematical formula.

The vapor pressures were determined for the case of the vapor in contact with ice and not a water surface. For the temperature of melting ice ( $0^{\circ} \mathrm{C}$. or $32^{\circ} \mathrm{F}$.) all values agree. Below this temperature Marvin's vapor pressures are slightly smaller than Regnault's, but differ from the latter less than any other tabular values.

The argument of the table is given for every two-tenths of a degree Fahrenheit from -60.0 to 32.0 Fahrenheit. The tabular values are given in millimetres and inches to three and four decimals respectively.

TABLES 38, 39.
table 38. Weight of aqueous vapor in a cubic foot of saturated airEnglish measures.
table 39. Weight of aqueous vapor in a cubic metre of saturated airMetric measures.

The weight of aqueous vapor in a cubic metre of saturated air is given by the expression

$$
W=\frac{a \delta}{\mathrm{I}+a t} \cdot \frac{F}{760^{\prime}},
$$

$a$ is the weight of a cubic metre of dry air (free from carbonic acid) at temperature $0^{\circ} \mathrm{C}$., and pressure of 760 millimetres of standard mercury at $45^{\circ}$ latitude and sea-level : $a=\mathrm{r} .29278 \mathrm{~kg}$. (Bureau International des Poids et Mesures: Travaux et Mémoires, t. I, p. A 54.)
$\delta$ is the density of aqueous vapor: $\delta=0.622$ I
$F$ is the pressure of aqueous vapor in saturated air whose temperature is $t$; Broch's values are adopted, expressed in millimetres.
$a$ is the coefficient of expansion of air for $\mathrm{I}^{\circ}$ C.: $a=0.003667$
$t$ is the temperature in Centigrade degrees.
Whence we have

$$
W(\text { grammes })=1.05821 \times \frac{F}{1+0.003667 t} .
$$

Table 39 is computed from this formula and gives the weight of vapor in grammes in a cubic metre of saturated air for dew-points from $-29^{\circ}$ to $40^{\circ} \mathrm{C}$., the intervals from $6^{\circ}$ to $40^{\circ} \mathrm{C}$. being 0.1 C . The tabular values are given to three decimals.

The weight $W^{\prime}$ of aqueous vapor in a cubic foot of saturated air is obtained by converting the foregoing constants into English measures.

The weight of a cubic foot of dry air at temperature $32^{\circ} \mathrm{F}$. and at a pressure of 760 mm . or 29.92 I inches is

We have therefore,

$$
a^{\prime}(\text { grains })=\frac{1292.78 \times 15.43235}{(3.280833)^{3}}=564.94 .
$$

$$
\begin{aligned}
W^{\prime}(\text { grains })= & \frac{a^{\prime} \delta}{29.92 \mathrm{I}} \times \frac{F^{\prime}}{\mathrm{I}+a^{\prime}\left(t^{\prime}-32^{\circ}\right)} \\
& =11.7459 \frac{F^{\prime}}{\mathrm{I}+0.002037\left(t^{\prime}-32^{\circ}\right)}
\end{aligned}
$$

The temperature $t$ is expressed in degrees Fahrenheit; the vapor pressure $F^{\prime}$, expressed in inches, is obtained from Table 35.

Table 38* gives the weight of aqueous vapor in grains in a cubic foot of saturated air for dew-points given to every 0.5 from - 19.5 to $115^{\circ} \mathrm{F}$., the values being computed to the thousandth of a grain.

The computation of Tables 38 and 39 has been furnished by Prof. Wm. Libbey, jr.

## REDUCTION OF OBSERVATIONS WITH THE PSYCHROMETER AND DETERMINATION OF RELATIVE HUMIDITY.

The psychrometric formula derived by Maxwell, Stefan, August, Regnault and others is, in its simplest form,

$$
f=f_{1}-A B\left(t-t_{1}\right),
$$

in which $t=$ Air temperature.
$t_{1}=$ Temperature of the wet-bulb thermometer.
$f=$ Pressure of aqueous vapor in the air.
$f_{1}=$ Pressure of aqueous vapor in saturated air at temperature $t_{1}$.
$B=$ Barometric pressure.
$A=\mathrm{A}$ quantity which, for the same instrument and for certain conditions, is a constant, or a function depending in a small measure on $t_{1}$.
The important advance made since the time of Regnault consists in recognizing that the value of $A$ differs materially according to whether the wet-bulb is in quiet or moving air. This was experimentally demonstrated by the distinguished Italian physicist, Belli, in 1830, and was well known to Espy, who always used a whirled psychrometer. The latter describes his practice as follows: "When experimenting to ascertain the dew-point by means of the wet-bulb, I always swung both thermometers moderately in the air, having first ascertained that a moderate movement produced the same depression as a rapid one."

The principles and methods of these two pioneers in accurate psychrometry have now come to be adopted in the standard practice of meteorologists, and psychrometric tables are adapted to the use of a whirled or ventilated instrument.

The factor $A$ depends in theory upon the size and shape of the thermometer bulb, largeness of stem and velocity of ventilation, and different formulæ and tables would accordingly be required for different instruments. But by using a ventilating velocity of three metres or more per second, the differences in the results given by different instruments vanish, and the same tables can be adapted to any kind of a thermometer and to all changes of velocity above that which gives sensibly the greatest depression of the wetbulb temperature; and with this arrangement there is no necessity to measure or estimate the velocity in each case further than to be certain that it does not fall below the assigned limit.

[^4]The formula and tables here given for obtaining the vapor pressure and dew-point from observations of the whirled or ventilated psychrometer are those deduced by Prof. Wm. Ferrel (Annual Report Chief Signal Officer, 1886, Appendix 24) from a discussion of a large number of observations.

Taking the psychrometric formula in metric units, pressures being expressed in millimetres and temperatures in Centigrade degrees, Prof. Ferrel derived for $A$ the value

$$
A=0.000656\left(\mathrm{I}+0.0019 t_{1}\right)
$$

In this expression for $A$, the factor depending on $t_{1}$ arises from a similar term in the expression for the latent heat of water, and the theoretical value of the coefficient of $t_{1}$ is o.ooris. Since it would require a very small change in the method of observing to cause the difference between the theoretical value and that obtained from the experiments, Prof. Ferrel adopted the theoretical coefficient 0.00115 and then recomputed the observations, obtaining therefrom the final value

$$
A=0.000660\left(\mathrm{I}+0.00 \mathrm{I} \mathrm{I}_{5} t_{1}\right)
$$

With this value the psychrometric formula in metric measures becomes

$$
f=f_{1}-0.000660 B\left(t-t_{1}\right)\left(\mathrm{I}+0.001 \mathrm{I}_{5} t_{1}\right)
$$

In order to adapt the formula to convenient tabulation, Prof. Ferrel substituted $t-t_{1}$ for $t_{1}$ in the last factor, a modification which produces appreciable error only in extreme cases. The error in the computed vapor pressure will be

$$
E=0.00000076 B\left(t-t_{1}\right)\left(t-2 t_{1}\right) .
$$

Expressed in English measures, the formula is

$$
f=f_{\mathrm{r}}-0.000367 B\left(t-t_{\mathrm{r}}\right)\left[\mathrm{r}+0.00064\left(t_{\mathrm{r}}-32^{\circ}\right)\right]
$$

and with the same modification in order to render the formula more convenient for tabulation, we have

$$
f=f_{1}-0.000367 B\left(t-t_{1}\right)\left(\mathrm{I}+0.00064\left(t-t_{1}\right)\right),
$$

, n which $f=$ Vapor pressure in inches.
$f_{1}=$ Vapor pressure in saturated air at temperature $t_{1}$.
$t=$ Temperature of the air in Fahrenheit degrees.
$t_{1}=$ Temperature of the wet-bulb thermometer in Fahrenheit degrees.
$B=$ Barometric pressure in inches.
TABLES 40, 41.

## Reduction of Psychrometric Observations-English measures.

table 40. Pressure of aqueous vapor.
TABLE 41. Values of $0.000367 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{\mathrm{I} 57 \mathrm{I}}\right)$
These two tables provide for computing the vapor pressure and dewpoint from observations of ventilated wet- and dry-bulb Fahrenheit thermometers.

Table 40, with the wet-bulb temperature $t_{1}$ as an argument, gives the value of $f_{1}$, the first term of the formula for the vapor pressure $f$, given above. It is simply an abbreviation of Table 35 for temperatures above $32^{\circ} F$., and of Table 37 for temperatures below $32^{\circ} F$., reprinted for convenience.

Table 41, with $t-t_{1}$ and B as arguments, gives the value of the second term of the formula, viz:

$$
0.000367 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{\mathrm{I}_{57} \mathrm{I}}\right)
$$

The top argument is given for every half inch from 30.5 to 18.5 inches; the side argument, $t-t_{1}$, is given for every whole degree up to $40^{\circ} F$. Tabular values are given to thousandths of inches.

With the two tables we then have,

$$
f(\text { vapor pressure })=\text { Table } 40-\text { Table } 4 \mathrm{I} .
$$

The value of $t$ in Table 40, corresponding to the vapor pressure thus obtained, is the dew-point.
Examples :

1. Given $t=84^{\circ} 3 ; t_{1}=66^{\circ} 7$, and $B=30.00$ inches, to find the vapor pressure and dew-point.
Table 40, with $t_{1}=66^{\circ} 7$, gives $f_{1}=0.654$ inches.
Table 41, with $t-t_{1}=84.3-66^{\circ}{ }^{\circ}=17.6$ and $B=30.00$ inches as arguments, gives 0.196 inch as the value of the last term of the expression above. Hence we have the vapor pressure $f=0.654-0.196=0.458$ inch. The temperature (Table 40) corresponding to this value of $f$ is the dew-point, $d=56.6 \mathrm{~F}$.
2. Given $t=34.5 ; t_{1}=29^{\circ} .4$, and $B=22.3$ inches, to find the vapor pressure and dew-point.
Table 40, with $t_{1}=29^{\circ} 4$, gives $f_{1}=0.162$ inch.
Table 41, with $t-t_{1}=34^{\circ} 5-29^{\circ} 4=5 .{ }^{\circ}$ and $B=22.5$ inches (the nearest value in the table to 22.3 inches) as arguments, gives 0.042 inch as the value of the second term of the expression for $f$. Hence we have the vapor pressure $f=0.162-0.042=0.120$ inch.
The temperature in Table 40, corresponding to this value of $f$, is the dew-point, $d=22.0$.
Note-In using Table 40, the proportional part for tenths of the argument, $t-t_{1}$, may be easily obtained by taking one-tenth of the tabular value belonging to the same number of degrees; for instance, in the first example, the tabular value for $17^{\circ}$ is 0.189 , and the proportional part for 0.6 is one-tenth the tabular value for $6^{\circ} 0^{\circ}$, viz., one-tenth of .066 , or .007 . Hence we get $0.189+0.007=0.196$.
table 42. Relative humidity-Temperature Fahrenheit.
Table 42 gives the relative humidity of the air in hundredths, having given the air temperature $t$ and the dew-point $d$ in Fahrenheit degrees.

It is computed by the formula

$$
\text { Relative humidity }=\frac{f}{F} .
$$

$f$ and $F$ are the maximum pressures of vapor corresponding respectively to the temperatures $d$ and $t$ as given in Table 35 for temperatures above $32^{\circ} \mathrm{F}$. and in Table 37 for temperatures below $32^{\circ} \mathrm{F}$.

The top argument is $t-d$, extending by half degree intervals from $0^{\circ}$ to $15^{\circ} F_{\text {. }}$, and by increasing intervals from $15^{\circ}$ to $75^{\circ} \mathrm{F}$.

The side argument is the air temperature $t$, given for intervals of four degrees from $-32^{\circ}$ to $120^{\circ} \mathrm{F}$.

## Example:

Let the air temperature be $62^{\circ} F$. and the dew-point $5 I^{\circ} F$., to find the relative humidity.

With $t-d=1 I^{\circ}$ for the top argument, and $t=62^{\circ}$ for the side argument, the table gives 67.5 per cent as the relative humidity.

TABLES 43, 44.
Reduction of Psychrometric Observations-Metric measures.
table 43. Pressure of aqueous vapor.
TABLE 44. Values of $0.000660 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{873}\right)$.
These two tables provide for computing the vapor pressure and dewpoint from observations of ventilated wet and dry-bulb thermometers Centigrade.

Table 43, with the wet-bulb temperature $t_{1}$ as an argument, gives the value of $f_{1}$, the first term of the formula for the vapor pressure $f$, viz :

$$
f=f_{1}-0.000660 B\left(t-t_{1}\right)\left[\mathrm{r}+0.001 \mathrm{I} 5\left(t-t_{1}\right)\right]
$$

It gives the vapor pressure to hundredths of a millimetre from $-30^{\circ} .0$. to $45^{\circ} .9 \mathrm{C}$., the intervals being $\mathrm{I}^{\circ}$ for temperatures below $0^{\circ} \mathrm{C}$. and $0 .{ }^{\circ} \mathrm{I}$ for temperatures above $0^{\circ} \mathrm{C}$.

Table 44, with the depression of the wet-bulb $t-t_{1}$, and the barometric pressure $B$ as arguments, gives the value of the second term of the formula.

The top argument is given for every io millimetres from 770 to 460 mm ; the side argument $t-t_{1}$ is given for every whole degree up to 20. Tabular values are given to hundredths of a millimetre.

From the two parts of the table we then have
Vapor pressure, $f(\mathrm{~mm})=$ Table 43 - Table 44 .
The temperature in Table 43, corresponding to the vapor pressure thus. obtained, is the dew-point.

## Example:

Given $t=10.4 \mathrm{C} . ; t_{1} \equiv 8 .{ }_{3}^{\circ} \mathrm{C}$. and $B=74 \mathrm{~mm}$., to find the vapor pressure and dew-point.
Table 43, with the argument $t_{1}=8.3{ }_{3} C$., gives $f_{1}=8.15 \mathrm{~mm}$.
Table 44, with $t-t_{1}=2.1$ and $B=740$ as arguments, gives 1.03 mm . as the value of the last term of the expression for $f$. Hence we have the vapor pressure, $f=8.15-1.03=7.12 \mathrm{~mm}$. The value of the temperature in Table 40 , corresponding to this vapor pressure, is the dew-point $d=6 .{ }_{3} C$.
table 45. Relative humidity-Temperature Centigrade.
Table 45 gives the relative humidity of the air in hundredths, having given the air temperature $t$ and the dew-point $d$ in Centigrade degrees.

It is computed by the formula

$$
\text { Relative humidity }=\frac{f}{F},
$$

$f$ and $F$ being the maximum pressures of aqueous vapor corresponding to the temperatures $d$ and $t$ as given in Tables 36 and 43.

The top argument is the dew-point $d$, extending by $5^{\circ}$ intervals from $-15^{\circ}$ to $30^{\circ} \mathrm{C}$.

The side argument is the depression of the dew-point $t-d$, given for every $0.2 C$. from 0.0 to 10.0 ; for every 0.5 from ro.0 to 20.0 , and for every $r^{\circ}$ from 20.0 to 30.0 .

Example:
Given the air temperature $21^{\circ} C$. and the dew-point $17^{\circ} C$., to determine the relative humidity.
With $t-d=4^{\circ} C$. for the side argument, and $d=17^{\circ} C$. for the top argument, the table gives 78 per cent as the relative humidity.

TABLE 46. REDUCTION OF SNOWFALL MEASUREMENT.
The determination of the water equivalent of snowfall has usually been made by one of two methods: (a) by dividing the depth of snow by an arbitrary factor ranging from 8 to 16 for snow of different degrees of compactness; (b) by melting the snow and measuring the depth of the resulting water. The first of these methods has always been recognized as incapable of giving reliable results, and the second, although much more accurate, is still open to objection. After extended experience in the trial of both these methods, it has been found that the most accurate and most convenient measurement is that of weighing the collected snow, and then converting the weight into depth in inches. The method is equally applicable whether the snow as it falls is caught in the gage, or a section of the fallen snow is taken by collecting it in an inverted gage.

TABLE 46. Depth of water corresponding to the weight of snow (or rain) collected in an 8 -inch gagé.
The table gives the depth to hundredths of an inch, corresponding to the weight of snow or rain collected in a gage having a circular collecting mouth 8 inches in diameter - this being the standard size of gage used throughout the United States.

The argument is given in avoirdupois pounds, ounces and quarter ounces in order that it shall be adapted to the customary graduation of commercial scales.

## Example:

The weight of snow collected in an 8 -inch gage is $2 \mathrm{lbs} .21 / 4 \mathrm{oz}$. To find the corresponding depth of water.
The table gives directly 1.18 inches.
TABLE 47.
table 47. Rate of decrease of vapor pressure with altitude.
From hygrometric observations made at various mountain stations on the Himalayas, Mount Ararat, Teneriffe, the Alps, and also in balloon ascensions, Dr. J. Hann (Zeitschrift für Meteorologie, vol. ix, 1874, p. 193-200) has deduced the following empirical formula showing the average relation between the vapor pressure $f_{0}$ at a lower station and $f$ the vapor pressure at an altitude $h$ metres above it :

$$
\frac{f}{f_{0}}=10^{-\frac{h}{6557}} .
$$

This is of course an average relation for all times and places from which the actual rate of decrease of vapor pressure in any individual case may widely differ.

Table 47 gives the values of the ratio $\frac{f}{f_{0}}$ for values of $h$ from 200 to 6000 metres. An additional column gives the equivalent values of $h$ in feet.

## WIND TABLES.

CALCULATION OF THE MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.

Lambert's formula for the eight principal points of the compass is

$$
\tan a=\frac{E-W+(N E+S E-N W-S W) \cos 45^{\circ}}{N-S+(N E+N W-S E-S W) \cos 45^{\circ}}
$$

$a$ is the angle of the resultant wind direction with the meridian.
$E, N E, N$, etc., represent the wind movement from the corresponding directions East, Northeast, North, etc. In practice instead of taking the total wind movement, it is often considered sufficient to take as proportional
thereto the number of times the wind has blown from each direction, which is equivalent to considering the wind to have the same mean velocity for all directions.

If directions are observed to sixteen points, half the number belonging to each extra point, should be added to the two octant points between which it lies ; for example, $N N E=6$ should be separated into $N=3$ and $N E=3 ; E S E=4$ into $E=2$ and $S E=2$. The result will be approximately identical with that obtained by using the complete formula for sixteen points.

Table 48. Multiples of $\cos 45^{\circ}$; form for computing the numerator and denominator.
table 49. Values of the mean direction (a) or its complement ( $90^{\circ}-a$ ).
Table 48 gives products of $\cos 45^{\circ}$ by numbers up to 209 , together with a form for the computation of the numerator and denominator, illustrated by an example. The quadrant in which a lies is determined by the following rule :

When the numerator and denominator are positive, a lies between $N$ and $E$.

When the numerator is positive and the denominator negative, $a$ lies between $S$ and $E$.

When the numerator and denominator are negative, a lies between $S$ and $W$.

When the numerator is negative and the denominator positive, $\alpha$ lies between $N$ and $W$.

Table $49 *$ combines the use of a division table and a table of natural tangents. It enables the computer, with the numerator and denominator of Lambert's formula (computed from Table 48) as arguments, to take out directly the mean wind direction $a$ or its complement.

The top argument consists of every fifth number from to to 200 .
The side argument is given for every unit from I to 50 and for every two units from 50 to 150 . Tabular values are given to the nearest whole degree.

Rule for using the table:
Enter the table with the larger number (either numerator or denominator) as the top argument.
If the denominator be larger than the numerator, the table gives $\alpha$.
If the denominator be smaller than the numerator, the table gives $90^{\circ}-a$.
$a$ is measured from the meridian in the quadrant determined by the rule given with Table 48.

* From Hand-book of Meteorological Tables. By H. A. Hazen. Washington, 1888. A corrected copy of the table has been kindly furnished for the present volume by the author.


## Example :

$$
\begin{aligned}
\tan a & =\frac{-43}{-27} \\
90^{\circ}-a & =32^{\circ} \\
a & =S 58^{\circ} W
\end{aligned}
$$

Table 49 gives

NoTe.-If the numerator and denominator both exceed 150 or if either exceeds 200, the fraction must be divided by some number which will bring them within the limits of the table. The larger the values, provided they are within these limits, the easier and more accurate will be the computation. For example, let $\tan \alpha=\frac{-18}{14}$. The top argument is not given for 18 , but if we multiply by 5 or 10 and obtain $\frac{-90}{70}$ or $\frac{-180}{140}$, the table gives, without interpolation, $90^{\circ}-a=38^{\circ}$ and $a=N 52^{\circ} \mathrm{W}$.

## CONVERSION OF VELOCITIES.

TABLE 50.
Synoptic conversion of velocities.
This table*, contained on a single page, converts miles per hour into metres per second, feet per second and kilometres per hour. The argument, miles per hour, is given for every half unit from $o$ to 78 . Tabular values are given to one decimal. For the rapid interconversion of velocities, when extreme precision is not required, this table has proved of marked convenience and utility.

TABLE 51.
table 51. Conversion of miles per hour into feet per second.
The argument is given for every unit up to 149 and the tabular values are given to one decimal.

TABLE 62.
table 52. Conversion of feet per second into miles per hour.
The argument is given for every unit up to 199 and the tabular values are given to one decimal.

TABLE 53.
TABLE 53. Conversion of metres per second into miles per hour.
The argument is given for every tenth of a metre per second up to 60 metres per second, and the tabular values are given to one decimal.

TABLE 54.
table 54. Conversion of miles per hour into metres per second.
The argument is given for every unit up to 149 , and the tabular values are given to two decimals.

[^5]TABLE 55. Conversion of metres per second into kilometres per hour.
The argument is given for every tenth of a metre per second up to 60 metres per second, and the tabular values are given to one decimal.

TABLE 56. Conversion of kilometres per hour into metres per second.
The argument is given for every unit up to 200 , and the tabular values are given to two decimals.

TABLE 57. Beaufort wind scale and its conversion into velocity.
The personal observation of the estimated force of the wind on an arbitrary scale is a method that belongs to the simplest meteorological records and is widely practiced. Although anemometers are used at meteorological observatories the majority of observers are still dependent upon estimates based largely upon their own judgment, and so reliable can such estimates be made that for many purposes they abundantly answer the needs of meteorology as well as of climatology.

A great variety of such arbitrary scales have been adopted by different observers, but the one that has come into the most general use and received the greatest definiteness of application is the duodecimal scale introduced into the British navy by Admiral Beaufort about 1800.

The definitions of the successive grades of the Beaufort scale were made in terms of the effect of the wind on the sails of a full-rigged ship, so that navigators of all nations have generally acquired a very uniform and definite idea of their meaning and a very considerable expertness in the use of the scale. The Table gives the designations of the 12 grades together with several conversions of the scale into wind velocities as made by different meteorologists. A committee appointed by the Royal Meteorological Society to establish a conversion of the Beaufort scale into wind velocity made a preliminary report (Quart. Journal Roy. Meteorological Soc., vol. 13, 1887), but did not consider their work sufficiently complete to present a definite conversion table. $\dagger$

## GEODETICAL TABLES.

TABLE 58. Relative acceleration of gravity at sea-level at different latitudes.
The formula adopted for the variation of gravity with latitude is that of Prof. Harkness*

$$
g_{\phi}=g_{45}(\mathrm{I}-0.002662 \cos 2 \phi)
$$

in which $g_{\phi}$ is the acceleration of the gravity at latitude $\phi$, and $g_{45}$ the acceleration at latitude $45^{\circ}$.

The table gives the values of the ratio $\frac{g_{\phi}}{g_{45}}$ to six decimals for every $10^{\prime}$ of latitude from the equator to the pole.

* Wm. Harkness : The solar parallax and its related constants. Washington, i8gr.
$\dagger$ Modern steamships move with velocities sufficient to affect all wind observations aboard of them.


## LENGTH OF A DEGREE OF THE MERIDIAN AND OF ANY PARALLEL.

The dimensions of the earth used in computing lengths of the meridian and of parallels of latitude are those of Clarke's spheroid of 1866.* This spheroid undoubtedly represents very closely the true size and shape of the earth, and is the one to which nearly all geodetic work in the United States is now referred.

The values of the constants are as follows:

$$
\begin{array}{ll}
a \text {, semi-major axis }=20926062 \text { feet } ; & \log a=7.3206875 . \\
b, \text { semi-minor axis }=20855 \mathrm{I} 2 \mathrm{I} \text { feet } ; & \log b=7.3192127 . \\
e^{2}=\frac{a^{2}-b^{2}}{a^{2}}=0.00676866 ; & \log e^{2}=7.8305030-\text { го. }
\end{array}
$$

With these values for the figure of the earth, the formula for computing any portion of a quadrant of the meridian is

$$
\begin{aligned}
\text { Meridional distance in feet } & =[5.5618284] \Delta \phi \text { (in degrees) }, \\
& -[5.0269880] \cos 2 \phi \sin \Delta \phi, \\
& +[2.0528] \cos 4 \phi \sin 2 \Delta \phi,
\end{aligned}
$$

in which $2 \phi=\phi_{2}+\phi_{1}, \Delta \phi=\phi_{2}-\phi_{1}, \phi_{1}, \phi_{2}=$ end latitudes of arc.
For the length of I degree, the formula becomes:
I degree of the meridian, in feet $=364609.9-1857.1 \cos 2 \phi+3.94 \cos 4 \phi$.
The length of the parallel is given by the equation

$$
\begin{aligned}
& \text { I degree of the parallel at latitude } \phi \text {, in feet }= \\
& 365538.48 \cos \phi-310.17 \cos 3 \phi+0.39 \cos 5 \phi .
\end{aligned}
$$

TABLE 59.
Table 59. Length of one degree of the meridian at different latitudes.
This gives for every degree of latitude the length of one degree of the meridian in statute miles to three decimals, in metres to one decimal, and in geographic miles to three decimals-the geographic mile being here defined to be one minute of arc on the equator. The values in metres are computed from the relation : I metre $=39.3700$ inches. The tabular values represent the length of an arc of one degree, the middle of which is situated at the corresponding latitude. For example, the length of an arc of one degree of the meridian, whose end latitudes are $29^{\circ} 30^{\prime}$ and $30^{\circ} 30^{\prime}$, is 68.879 statute miles.

TABLE 60.
TABLE 60. Length of one degree of the parallel at different latitudes.
This table is similar to Table 59.

[^6]table 61. Duration of sunshine at different latitudes for different values of the sun's declination.


Let $Z$ be the zenith, and $N H$ the horizon of a place in the northern hemisphere.
$P$ the pole;
$Q E Q^{\prime}$ the celestial equator;
$R R^{\prime}$ the parallel described by the sun on any given day;
$S$ the position of the sun when its upper limit appears on the horizon;
$P N$ the latitude of the place, $\phi$.
$S T$ the sun's declination, $\delta$.
$P S$ the sun's polar distance, $90^{\circ}-\delta$.
$Z S$ the sun's zenith distance, $z$.
$Z P S$ the hour angle of the sun from meridian, $t$.
$r$ the mean horizontal refraction $=34^{\prime}$ approximately.
$s$ the mean solar semi-diameter $=16^{\prime}$

$$
z=90^{\circ}+r+s=90^{\circ} 50^{\prime}
$$

In the spherical triangle $Z P S$, the hour angle $Z P S$ may be computed from the values of the three known side by the formula
or

$$
\begin{gathered}
\sin \frac{1}{2} Z P S=\sqrt{\frac{\sin \frac{1}{2}(Z S+P Z-P S) \sin \frac{1}{2}(Z S+P S-P Z)}{\sin P Z \sin P S}} \\
\sin \frac{1}{2} t=\sqrt{\frac{\sin \frac{1}{2}(z+\delta-\phi) \sin \frac{1}{2}(z-\delta+\phi)}{\cos \phi \cos \delta}}
\end{gathered}
$$

The hour angle $t$, converted into mean solar time and multiplied by 2 is the duration of sunshine.

Table 6I has been computed for this volume by Prof. Wm. Libbey, jr. It is a table of double entry with arguments $\delta$ and $\phi$. For north latitudes northerly declination is considered positive and southerly declination as negative. The table may be used for south latitudes by considering southerly declination as positive and northerly declination as negative.

The top argument is the latitude, given for every $5^{\circ}$ from $0^{\circ}$ to $40^{\circ}$, for every $2^{\circ}$ from $40^{\circ}$ to $60^{\circ}$, and for every degree from $60^{\circ}$ to $80^{\circ}$.

The side argument is the sun's declination for every $20^{\prime}$ from $S 23^{\circ} 27^{\prime}$ to $N 23^{\circ} 27^{\prime}$.

The duration of sunshine is given in hours and minutes.
To find the duration of sunshine for a given day at a place whose latitude is known, find the declination of the sun at mean noon for that day in the Nautical Almanac, and enter the table with the latitude and declination as arguments.

## Example:

To find the duration of sunshine, May 18, 1892, in latitude $49^{\circ} 30^{\prime}$ North. From the Nautical Almanac, $\delta=19^{\circ} 43^{\prime} N$.
From the table, with $\delta=19^{\circ} 43^{\prime} N$ and $\phi=49^{\circ} 30^{\prime}$, the duration of sunshine is found to be $15^{h} 3 \mathrm{I}^{\mathrm{m}}$.
table 62. Declination of the sun for the year 1894.
This table is an auxiliary to Table 6I, and gives the declination of the sun for every third day of the year 1894 . These declinations may be used as approximate values for the corresponding dates of other years when the exact declination can not readily be obtained. Thus, in the preceding example, the declination for May 18 may be taken as approximately the same as that for the same date in 1894, viz. $19^{\circ} 37^{\prime}$.

RELATIVE INTENSITY OF SOLAR RADIATION AT DIFFERENT LATITUDES FOR DIFFERENT SEASONS OF THE YEAR.
rable 63. Mean vertical intensity for 24 hours of solar radiation $J$ and the solar constant $A$ in terms of the mean solar constant $A_{\text {。 }}$.
This table is that of Prof. Wm. Ferrel, published in the Annual Report of the Chief Signal Officer, 1885, Part 2, and in Professional Papers of the Signal Service, No. 14, p. 427, where the formulæ and constants will be found.

It gives the mean vertical intensity for 24 hours of solar radiation $J$ in terms of the mean solar constant $A_{0}$ for each tenth parallel of latitude of the northern hemisphere, and for the first and sixteenth day of each month; also the values of the solar constant $A$ in terms of $A_{\mathrm{o}}$, and the angular motion of the sun in longitude for the given dates.

## CONVERSION OF LINEAR MEASURES.

The relation here adopted between the metre and the English measures of length is that used and officially authorized by the U. S. Bureau of Weights and Measures, viz :

$$
\text { I metre }=39.3700 \text { inches }
$$

TABLE 64.

## TABLE 64.

 Inches into millimetres.The argument is given for every hundredth of an inch up to 32.00 inches, and the tabular values are given to hundredths of a millimetre. A table of proportional parts for thousandths of an inch is added on each page.

## Example:

To convert 24.362 inches to millimetres.
The table gives (p. 184)

$$
(24.36+0.02) \text { inches }=(618.75+0.05 \mathrm{~mm} .)=618.80 \mathrm{~mm} .
$$

TABLE 65.
Millimetres into inches.
From o to 400 mm . the argument is given to every millimetre, with subsidiary interpolation tables for tenths and hundredths of a millimetre. The tabular values are given to four decimals. From 400 to 1000 mm ., covering the numerical values which are of frequent use in meteorology for the conversion of barometric readings from the metric to the English barometer, the argument is given for every tenth of a millimetre, and the tabular values to three decimals.

## Example:

To convert 143.34 mm . to inches.
The table gives
$143+.3+.04 \mathrm{~mm} .=5.6299+0.0118+0.0016$ inches $=5.6433$ inches.

## TABLE $66 . \quad$ Feet into metres.

From the adopted value of the metre, 39.3700 inches-

$$
\text { I English foot }=0.3048006 \text { metre. }
$$

Table 66 gives the value in metres and thousandths (or millimetres) for every foot from o to 99 feet; the value to hundredths of a metre (or centimetres) of every 10 feet from 100 to 4000 feet ; and the value to tenths of a metre of every 10 feet from 4000 to 9090 feet. In using the latter part, the first line of the table serves to interpolate for single feet.

## Example :

To convert 47 feet 7 inches to metres. 47 feet 7 inches $=47.583$ feet.

The table gives
By moving the decimal point,

$$
\begin{aligned}
& 47 \quad \text { feet }=14.326 \text { metres. } \\
& 0.583 ،=0.178
\end{aligned}
$$

$$
47.583 \text { feet }=14.504 \text { metres. }
$$

TAble 67.
Metres into feet.

$$
\text { I metre }=39.3700 \text { inches }=3.280833+\text { feet }
$$

From o to 500 metres the argument is given for every unit, and the tabular values to two decimals; from 500 to 5000 the argument is given to every ro metres, and the tabular values to one decimal. The conversion for tenths of a metre is added for convenience of interpolation.

## Example :

Convert 4327 metres to feet.
The table gives

$$
(4320+7) \text { metres }=(14173.2+23.0) \text { feet }=14196.2 \text { feet. }
$$

TAble 68.
Miles into kilometres.
TABLE 68.

$$
\mathrm{I} \text { mile }=\mathrm{r} .609347 \text { kilometres } .
$$

The table extends from o to 1000 miles with argument to single miles, and from 1000 to 20000 miles for every 1000 miles. The tabular quantities are given to the nearest kilometre.
table 69.
Kilometres into miles.
TABLE 69.

$$
\text { I kilometre }=0.621370 \text { mile } .
$$

The table extends to rooo kilometres with argument to single kilometres, and from 1000 to 20000 kilometres for every rooo kilometres. Tabular values are given to tenths of a mile.
Example :
Convert 3957 kilometres into miles.
The table gives
$(3000+957)$ kilometres $=(1864.1+594.7)$ miles $=2458.8$ miles.
table 70. Interconversion of nautical and statute miles.
The definition of the nautical mile here used is that adopted by the U. S. Coast and Geodetic Survey.

A nautical mile is equal to the length of one minute of arc on the great circle of a sphere whose surface is equal to the surface of the earth.

Computed on Clarke's spheroid of 1866, the nautical mile thus defined equals 6080.27 feet. (Report, U. S. Coast Survey, 1881, page 354.)

The table gives, for nautical and statute miles from I to 9 , the equivalent in statute and nautical miles, respectively, to four decimals.

TABLE 71.
Table 71. Continental measures of length with their metric and English equivalents.
This table gives a miscellaneous list of continental measures of length alphabetically arranged, with the name of the country to which they belong and their metric and English equivalents.

## CONVERSION OF MEASURES OF TIME AND ANGLE.

TAble 72. Arc into time.

$$
\mathrm{I}^{\circ}=4^{\mathrm{m}} ; \quad \mathrm{r}^{\prime}=4^{\mathrm{s}} ; \quad \mathrm{I}^{\prime \prime}=\frac{\mathrm{x}}{15} \mathrm{~s}=0.067
$$

## Example :

Change $124^{\circ} 15^{\prime} 24^{\prime \prime} .7$ into time.
From the table,

| $124^{\circ}$ | $=$ | $8^{\mathrm{h}}$ | $16^{\mathrm{m}}$ | $0^{\mathrm{s}}$ |
| ---: | :--- | :--- | :--- | :--- |
| $15^{\prime}$ | $=$ |  | 1 | 0 |
| $24^{\prime \prime}$ | $=$ |  |  | 1.600 |
| $0^{\prime \prime} .7$ | $=$ |  |  | .047 |
|  |  |  | $8^{\mathrm{h}}$ | $17^{\mathrm{m}}$ |
|  | 1.5647 |  |  |  |

TAble 73.
Time into arc.

$$
\mathrm{I}^{\mathrm{h}}=\mathrm{I} 5^{\circ} ; \quad \mathrm{I}^{\mathrm{m}}=\mathrm{I} 5^{\prime} ; \quad \mathrm{I}^{\mathrm{s}}=\mathrm{I} 5^{\prime \prime}
$$

## Example :

Change $8^{\mathrm{h}} \mathrm{I}^{\mathrm{m}} \mathrm{I}^{\mathrm{s}} 647$ into arc.

| From the table, | $8^{\text {h }}$ |  | $120^{\circ}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $17^{\text {m }}$ |  | 4 | ${ }^{15}$ |  |
|  | $\mathrm{I}^{\text {s }}$ | = |  |  | $15^{\prime \prime}$ |
|  | 0.64 |  |  |  | 9.60 |
| By moving the | t, .007 |  |  |  | 0.10 |

table 74. Days into decimals of a year and angle.
The table gives for the beginning of each day the corresponding decimal of the year to five places. Thus, at the epoch represented by the beginning of the 15th day, the decimal of the year that has elapsed since January r.o is computed from the fraction $\frac{14}{365.25}$. The corresponding value in angle obtained by multiplying this fraction by $360^{\circ}$, is given to the nearest minute.

Two additional columns serve to enter the table with the day of the month either of the common or the bissextile year as the argument, and may be used also for converting the day of the month to the day of the year, and vice versa.

## Example:

To find the number of days and the decimal of a year between February 12 and August 27 in a bissextile year.
Aug. 27: Day of year $=240$; decimal of a year $\quad=0.65435$
Feb. 12: " " 43; " " " =0.11499
Interval in days $=197$; interval in decimal of a year $=0.53936$
The decimal of the year corresponding to the interval 197 days may also be taken from the table by entering with the argument 198.
table 75. Hours, minutes and seconds into decimals of a day.
The tabular values are given to six decimals.
Example:
Convert $5^{\mathrm{h}} 24^{\mathrm{m}} 23^{\mathrm{s}} .4$ to the decimal of a day :

$$
\begin{array}{rlr}
5^{\mathrm{h}} & =0.208333 \\
24^{\mathrm{m}} & = & 016667 \\
23^{\mathrm{s}} & = & 266
\end{array}
$$

By interpolation, or by moving the decimal for $4^{\text {s }} 0.4=\quad 5$
od. 22527 I
table 76. Decimals of a day into hours, minutes and seconds. Example:

Convert od ${ }^{2} 2527$ to hours, minutes and seconds :

$$
\begin{array}{ll}
0.22 & \text { day }=4^{\mathrm{h}} 4^{\mathrm{m}}+28^{\mathrm{m}} 48^{\mathrm{s}}=5^{\mathrm{h}} 16^{\mathrm{m}} 48^{\mathrm{s}} \\
0.0052 \text { day }=7^{\mathrm{m}} 12^{\mathrm{s}}+17^{\mathrm{s}} \mathrm{~S}_{2}= & 72^{29.28} \\
0.00007 \mathrm{I} \text { day }=6.05+0.09= & \frac{6.14}{5^{\mathrm{h}} 24^{\mathrm{m}} 23^{\mathrm{s}} .4}
\end{array}
$$

TABLE 76.

TABLE 77.
table 77. Minutes and seconds into decimals of an hour.
The tabular values are given to six decimals.
Example:
Convert $34^{\mathrm{m}}{ }^{285} 7$ to decimals of an hour.

$$
\begin{array}{rrr}
34^{\mathrm{m}} & = & 0^{\mathrm{h}} .566667 \\
28^{\mathrm{s}} & = & 7778 \\
0.7 & = & 194 \\
& \frac{0.574639}{}
\end{array}
$$

## TAble 78.

Mean time at apparent noon.
This table gives the time that should be shown by a clock when the sun crosses the meridian, on the 1st, 8th, 16th, and 24th days of each month. The table is useful in correcting a clock by means of a sun-dial or noon-mark.

## Example:

To find the correct mean time when the sun crosses the meridian on December 15, 1891.
The table gives for December $16, \mathrm{II}^{\mathrm{h}} 5^{6 \mathrm{~m}}$. By interpolating, it is seen that the change to December 15 would be less than one-half minute ; the correct clock time is therefore 4 minutes before 12 o'clock noon.

TABLE 79. Sidereal time into mean solar time.
table 80. Mean solar time into sidereal time.
According to Bessel, the length of the tropical year is 365.24222 mean solar days,* whence

$$
365.24222 \text { solar days }=366.24222 \text { sidereal days. }
$$

Any interval of mean time may therefore be changed into sidereal time by increasing it by its $\frac{1}{365.24222}$ part, and any interval of sidereal time may be changed into mean time by diminishing it by its $\frac{1}{366.24222}$ part.

[^7]Table 79 gives the quantities to be subtracted from the hours, minutes and seconds of a sidereal interval to obtain the corresponding mean time interval, and Table 80 gives the quantities to be added to the hours, minutes and seconds of a mean time interval to obtain the corresponding sidereal interval. The correction for seconds is sensibly the same for either a sidereal or a mean time interval and is therefore given but once, thus forming a part of each table.

Examples:
Change $14^{\mathrm{h}}{ }^{2} 5^{\mathrm{m}} 36^{5}{ }^{\mathrm{s}}$ sidereal time into mean solar time.

| Given sidereal time |  | $14^{\text {h }} \quad 25^{\text {m }}$ | $36{ }^{\text {s }} 2$ |
| :---: | :---: | :---: | :---: |
| Correction for $14{ }^{\text {h }}$ | $=-2^{m}{ }^{17}{ }^{\text {s }} 6 \mathrm{I}$ |  |  |
| $25^{\text {m }}$ | 4.10 |  |  |
| 36.2 | 10 |  |  |
|  | -2 21.8 I | -2 | 21.8 |
| Corresponding mean time | = | $14 \quad 23$ | 14. |

2. Change $13^{\mathrm{h}} 37^{\mathrm{m}} \quad 22^{5} .7$ mean solar time into sidereal time.


## MISCELLANEOUS TABLES.

DENSITY OF AIR AT DIFFERENT TEMPERATURES, HUMIDITIES AND PRESSURES.

The following tables ( 8 I to 86 ) give the factors for computing the density of air at different temperatures, humidities and pressures.

The formula from which they have been computed is, in metric measures,

$$
\delta=\frac{0.00129305[7.1116153]}{1+0.00367 t}\left(\frac{b-0.378 e}{760}\right)
$$

in which $\delta$ is the weight of a cubic centimetre of air expressed in grammes, under the standard value of gravity at latitude $45^{\circ}$ and sea level.
$b$ is the barometric pressure in millimetres.
$e$ is the pressure of aqueous vapor in millimetres.
$t$ is the temperature in Centigrade degrees.
For dry atmospheric air (containing 0.0004 of its weight of carbonic acid) at a pressure of 760 mm . and temperature $0^{\circ} C$., the absolute density,
or the weight of one cubic centimetre, is 0.00129305 gramme. (International Bureau of Weights and Measures: Travaux et Mémoires, t. I, p. A 54.)

In English measures, the formula becomes

$$
\delta=\frac{0.00129305}{1 \times 0.0020389\left(t-32^{\circ}\right)}\left(\frac{b-0.378 e}{29.92 \mathrm{I}}\right)
$$

where $\delta$ is defined as before, but $b$ and $e$ are expressed in inches and $t$ in Fahrenheit degrees. Thus by the use of tables based on these two formulæ, lines of equal atmospheric density may be drawn for the whole world (neglecting slight variations in gravity), whether the original observations are in English or metric measures. Prof. Cleveland Abbe has kindly furnished for the present volume the logarithms of the density given in the accompanying tables (8I to 86).

Table 81. Density of air at different temperatures Fahrenheit.
This table gives the values and logarithms of the expression

$$
\frac{0.00129305}{1+0.0020389\left(t-32^{\circ}\right)}
$$

for values of $t$ extending from $-45^{\circ} F$. to $140^{\circ} F$., the intervals between $0^{\circ} F$. and $10^{\circ} F$. being I .

The tabular values are given to five significant figures.
TABLES 82, 83.
Density of air at different humidities and pressures-English measures.
table 82. Term for humidity; auxiliary to Table 83.
table 83. Values of $\frac{b-0.378 e}{29.921}$.
Table 82 gives values of $0.378 e$ to three decimal places as an aid to the use of Table 83 .

The argument is the dew-point given for every degree from $-40^{\circ} \mathrm{F}$. to $140^{\circ} \mathrm{F}$. A second column gives the corresponding values of the vapor pressure (e) according to Broch.

Table 83 gives values and logarithms of $\frac{h}{29.92 \mathrm{I}}=\frac{b-0.378 e}{29.921}$ for values of $h$ extending from 10.0 to 31.7 inches. The logarithms are given to five significant figures and the corresponding numbers to four decimals.

## Example :

The air temperature is $68^{\circ} F$., the pressure is 29.36 inches and the dewpoint $51^{\circ} F$. Find the logarithm of the density.
Table 81, for $t=68^{\circ}{ }^{\circ} F$., gives 7.08085-10
Table 82, for dew-point $51^{\circ}$, gives $0.378 e=0.14 \mathrm{I}$ inch,
Table 83, for $h=b-0.378 e=29.36-0.14=29.22$, gives 9.98941 - 10
table 84. Density of air at different temperatures Centigrade.
This gives values and logarithms of the expression

$$
\delta_{t, 760}=\frac{0.00129305}{1+0.00367 t}
$$

for values of $t$ extending from $-34^{\circ} \mathrm{C}$. to $69^{\circ} \mathrm{C}$. The tabular values are given to five significant figures.

## Density of air at different humidities and pressures-Metric measures.

table 85. Term for humidity: values of $0.378 e$.
TABLE 86. Values of $\frac{h}{760}=\frac{b-0.378 e}{760}$.
Table 85 gives values of $0.378 e$ to hundredths of a millimetre for dewpoints extending by intervals of $\mathrm{I}^{\circ}$ from $-30^{\circ} \mathrm{C}$. to $50^{\circ} \mathrm{C}$. The values of Broch's vapor pressures (e) corresponding to these dew-points are given in a second column to hundredths of a millimetre. The table is thus conveniently used when either the vapor pressure or the dew-point is known.

Table 86 gives values and logarithms of $\frac{h}{760}=\frac{b-0.378 e}{760}$ for values of $h$ extending from 300 to 800 mm . The barometric pressure $b$ is the barometer reading corrected for temperature and $0.378 e$ is the term for humidity obtained from Table 85. The logarithms are given to five significant figures and the corresponding numbers to four decimal places.

TABLE 87. Conversion of avoirdupois pounds and ounces into kilogrammes.
The latest comparisons made by the International Bureau of Weights and Measures between the Imperial standard pound and the "kilogramme proto-type" result in the relation:

$$
\text { I pound avoirdupois }=453.5924277 \text { grammes. }
$$

This value has been adopted by the United States Bureau of Weights and Measures and is here used.

For the conversion of pounds, Table 87 gives the argument for every tenth of a pound up to 9.9 , and the tabular conversion values to ten-thousandths of a kilogramme.

For the conversion of ounces, the argument is given for every tenth of an ounce up to $\mathbf{1 5} .9$, and the tabular values to ten-thousandths of a kilogramme.

Table 88. Conversion of kilogrammes into avoirdupois pounds and ounces.
From the above relation between the pound and the kilogramme,

$$
\begin{aligned}
\text { r kilogramme } & =2.204622 \text { avoirdupois pounds. } \\
& =35.274 \quad \text { avoirdupois ounces. }
\end{aligned}
$$

The table gives the value to thousandths of a pound of every tenth of a kilogramme up to 9.9 ; the values of tenths of kilogrammes in ounces to four decimals ; and the values of hundredths of a kilogramme in pounds and ounces to three and two decimals respectively.

TABLE 89. Conversion of grains into grammes.
table 90. Conversion of grammes into grains.
TABLES 89, 90.

From the above relation between the pound and the kilogramme,
I gramme $=15.432356$ grains.
I grain $=0.06479892$ gramme.
Table 89 gives to ten-thousandths of a gramme the value of every grain from I to 99, and also the conversion of tenths and hundredths of a grain for convenience in interpolating.

Table 90 gives to hundredths of a grain the value of every tenth of a gramme from o. I to 9.9, and the value of every gramme from I to 99. The values of hundredths and thousandths of a gramme are added as an aid to interpolation.

The computation of these two tables has been furnished by Professor William Libbey, who has used the relation, I gramme $=15.432531$ grains. This value is practically identical with the relation above adopted, differing from it by about I part in 3,000,000.
table 91. Conversion of units of magnetic intensity.
TABle 91
This table gives the conversion factors from I to 9 for converting English measures of magnetic intensity into C. G. S. measures, and vice versa.

The English unit of magnetic intensity is the force which, acting for I second on a unit of magnetism associated with a mass of I grain, produces a velocity of I foot per second.

The C. G. S. unit of magnetic intensity is the dyne-the force which, acting upon one gramme for 1 second, generates a velocity of I centimetre per second. The Gaussian unit of magnetic intensity, which has been extensively used, is a force which, acting upon a mass of 1 milligramme for i second, generates a velocity of i millimetre per second.

By using the dimensions of magnetic intensity [ $\mathrm{M}^{\frac{1}{2}} / \mathrm{L}^{\frac{1}{2}} \mathrm{~T}$ ], the interconversion of these units is easily made.

I C. G. S. unit $=\sqrt{\frac{1000 \mathrm{M}}{10 \mathrm{~L}}}$ Gaussian units

$$
=\text { Io Gaussian units }
$$

I C. G. S. unit $=\sqrt{\frac{\mathrm{r} 5.432356 \mathrm{M}}{.03280833 \mathrm{~L}}}$ English units

$$
=21.6882 \quad \text { English units }
$$

TABLE 92. Quantity of water corresponding to given depths of rainfall.
This table gives for different depths of rainfall over an acre and a square mile the total quantity of water measured in imperial gallons and tons respectively.

## table 93. Dates of Dove's pentades.

For tabulating and averaging meteorological data, Dove divided the year into seventy-three intervals of five days each, which have been called Dove's pentades, and this system of averaging has been used in the publication of a very considerable amount of meteorological data. Table 93 gives the initial and terminal dates of each pentade throughout the year.

TABLE 94. Division by 28 of numbers from 28 to 867972.
TABLE 95. Division by 29 of numbers from 29 to 89897 I.
TABLE 96. Division by 3I of numbers from 31 to 960969.
The frequent occasion in meteorological work to divide by the numbers 28, 29 and 31 renders useful the division tables compiled by Mr. H. A. Hazen (Handbook of Meteorological Tables, Washington, D. C., 1888), the use of which has been kindly granted.

As here printed, the dividend is given in plain type and the quotient in heavy-face type, and in order that one shall never be mistaken for the other, a column is given containing the letters D and Q successively, which designates that all figures on a line with D are dividends, and all on a line with $Q$ are quotients. The four columns to the right of this $D-Q$ column give the last two figures of the dividend and of the quotient, namely, the units and tens. The ten columns to the left side of the $\mathrm{D}-\mathrm{Q}$ column give the preceeding figures of the dividend, namely, the hundreds, thousands, and tens of thousands. These two parts of the dividend-to the left and right of the D-Q column-are always to be taken on the same horizontal line.

Each dividend is an exact multiple of the divisor, hence each quotient is exact or without remainder.

For example, the dividend 17360 in Table 94 is found in two parts; ${ }^{1} 73$ is found in the column headed 600 on the left-hand side of the $\mathrm{D}-\mathrm{Q}$ column, and 60 in the same horizontal row in the third column on the righthand side.

The hundreds figure of the quotient is given in bold-face type at the top, middle and bottom of the page, and each one obtains for all the dividend figures in its own column. The units and tens figures of the quotient are found, as already stated, on the right side of the D-Q column directly under the last two figures of the dividend. Thus in the above example, for dividend 17360 the hundreds figure of the quotient is 6 and the units and tens will be 20 , or the quotient of 17360 divided by 28 is 620 . When any given dividend
is not an exact multiple of the divisor, the nearest even multiple as given in the table must be used.

For example, $23979 \div 28=856$; the 8 is in the 9th column above 239 and the 56 is under 68, the nearest figure to 79 in the right-hand part of the table.

The last column, which is separated from the rest of the table by a triple line, is to be used when the quotient exceeds three figures, or 999.

The bold-face figures in this column give the thousands and tens of thousands figures of the quotient, and the plain figures are the multiples thereof by the divisor. To use the column, find in it the number which, with three ciphers added, comes nearest to (but is less than) the dividend; the heavy-face figures beneath it will be the first figures of the quotient. Subtract this multiple number from the given dividend, and with the remainder enter the main body of the table to obtain the last three figures of the quotient as already described.

For example: Divide 833885 by 28. The nearest figure to 833000 in the last column is 812000 and the quotient 29000. $833885-812000=21885$. Under 218 we have 7 , and under 96 , the nearest figure to 85 on the right, we find 82. $833885 \div 28=29782$.
table 97. Natural sines and cosines.
table 98. Natural tangents and cotangents.
TABLE 97.

TABLE 98.
table 99. Logarithms of numbers.
table 100. List of meteorological stations.
This list of meteorological stations has been compiled for this volume from data furnished by the United States Weather Bureau.

A geographical arrangement has been adopted as being most serviceable for the purposes for which the table will most generally be used.

In making the selection of stations from the vast number available, the object has been to choose such of the higher order stations as will fairly represent the varied climatic conditions of each country. With few exceptions, the stations are active ; in all cases there are published observations, which may generally be found in the monthly and annual reports of the national meteorological services of the countries in which the stations are situated, or by which they are politically controlled.

So far as known, the list contains all first order stations, i.e., those at which the principal meteorological elements are either recorded continuously and automatically, or are observed at hourly or bi-hourly intervals; such stations are designated by an asterisk (*).

The names of the stations have been given in the native orthography, which is in all cases the form adopted by the national meteorological service in its official publications.

GEORGE E. CURTIS.

## THERMOMETRICAL TABLES.

Conversion of thermometric scales -
Reaumur scale to Fahrenheit and Centigrade . . . . Table I
Fahrenheit scale to Centigrade . . . . . . . . . Table 2
Centigrade scale to Fahrenheit . . . . . . . . . Table 3
Centigrade scale to Fahrenheit, near the boiling point of water . . . . . . . . . . . . . . . . . TabLE 4

Differences Fahrenheit to differences Centigrade . . . . Table 5
Differences Centigrade to differences Fahrenheit . . . . Table 6
Reduction of temperature to sea level-English measures . Table 7
Reduction of temperature to sea level-Metric measures . . Table 8
Correction for the temperature of the mercury in the thermometer stem. For Fahrenheit and Centigrade thermometers

REAUMUR SCALE TO FAHRENHEIT AND CENTIGRADE.

| $\begin{aligned} & \text { Reau- } \\ & \text { mur } \\ & \hline \end{aligned}$ | Fahrenheit | Centigrade | Reaumur | Fahrenheit | Centigrade | Reaumur | Fahrenheit | Centigrade | Pro | Parts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ¢180' | +-212000 | +100.00 | $+40^{\circ}$ | +122.00 | +50.00 | $\pm 0^{\circ}$ | +32.00 | $\pm 0.00$ |  |  |
| 79 | 209.75 | 98.75 | 39 | 119.75 | 48.75 | - I | 29.75 | - 1.25 |  |  |
| 78 | 207.50 | 97.50 | 38 | II7.50 | 47.50 | 2 | 27.50 | 2.50 |  |  |
| 77 | 205.25 | 96.25 | 37 | II5.25 | 46.25 | 3 | 25.25 | 3.75 | R. <br> O.I | F. |
| 76 | 203.00 | 95.00 | 36 | II3.00 | 45.00 | 4 | 23.00 | 5.00 | 0.1 | F. 225 .450 |
| $+75$ | +200.75 | $+93.75$ | +35 | +110.75 | +43.75 | $-5$ | +20.75 | -6.25 | . 4 | . 675 |
| 74 | 198.50 | 92.50 | 34 | 108.50 | 42.50 | 6 | 18.50 | 7.50 | . 5 | 1.125 |
| 73 | 196.25 | 91.25 | 33 | 106.25 | 41.25 | 7 | 16.25 | 8.75 | 6 | 1.350 |
| 72 | 194.00 | 90.00 | 32 | 104.00 | 40.00 | 8 | 14.00 | 10.00 | . 7 | 1.575 r.800 |
| 71 | 191.75 | 88.75 | 31 | 10r. 75 | 38.75 | 9 | 11.75 | 11.25 | 0.9 | 1.800 2.025 |
| $+70$ | +189.50 | $+87.50$ | $+30$ | $+99.50$ | $+37.50$ | $-10$ | $+9.50$ | -12.50 |  |  |
| 69 | 187.25 | 86.25 | 29 | 97.25 | 36.25 | II | 7.25 | 13.75 |  |  |
| 68 | 185.00 | 85.00 | 28 | 95.00 | 35.00 | 12 | 5.00 | 15.00 |  |  |
| 67 | 182.75 | 83.75 | 27 | 92.75 | 33.75 | 13 | 2.75 | 16.25 | R. | C. |
| 66 | 180.50 | 82.50 | 26 | 90.50 | 32.50 | 14 | + 0.50 | 17.50 | 2 | . 250 |
| $+65$ | +178.25 | $+8 \mathrm{r} .25$ | +25 | $+88.25$ | +31.25 | $-15$ | $-1.75$ | -18.75 | . 4 | . 375 |
| 64 | 176.00 | 80.00 | 24 | 86.00 | 30.00 | 16 | 4.00 | 20.00 | . 5 | . 625 |
| 63 | 173.75 | 78.75 | 23 | 83.75 | 28.75 | 17 | 6.25 | 21.25 | . 6 | . 750 |
| 62 | 171.50 | 77.50 | 22 | 81.50 | 27.50 | 18 | 8.50 | 22.50 | . 7 |  |
| 61 | 169.25 | 76.25 | 21 | 79.25 | 26.25 | 19 | 10.75 | 23.75 |  | 1.125 |
| $+60$ | +167.00 | $+75.00$ | +20 | + 77.00 | +25.00 | -20 | - 13.00 | -25.00 |  |  |
| 59 | 164.75 | 73.75 | 19 | 74.75 | 23.75 | 21 | 15.25 | 26.25 |  |  |
| 58 | 162.50 | 72.50 | 18 | 72.50 | 22.50 | 22 | 17.50 | 27.50 | F. | c. |
| 57 | 160.25 | 71.25 | 17 | 70.25 | 21.25 | 23 | 19.75 | 28.75 | 0.25 | 0.14 |
| 56 | 158.00 | 70.00 | 16 | 68.00 | 20.00 | 24 | 22.00 | 30.00 | . 50 | . 28 |
| +55 | + 155.75 | + 68.75 | $+15$ | + 65.75 | +r8.75 | -25 | -24.25 | -31.25 | .75 r. \% | .42 .56 |
| 54 | 153.50 | 67.50 | 14 | 63.50 | 17.50 | 26 | 26.50 | 32.50 | 1.25 | . 69 |
| 53 | 151.25 | 66.25 | 13 | 61.25 | 16.25 | 27 | 28.75 | 33.75 | 1.50 <br> I. 75 <br> 150 |  |
| 52 | 149.00 | 65.00 | 12 | 59.00 | 15.00 | 28 | 31.00 | 35.00 |  |  |
| 51 | 146.75 | 63.75 | II | 56.75 | 13.75 | 29 | 33.25 | 36.25 |  |  |
| $+50$ | +144.50 | $+62.50$ | $+10$ | $+54.50$ | +12.50 | -30 | $-35.50$ | -37.50 |  |  |
| 49 | 142.25 | 61.25 | 9 | 52.25 | 11.25 | 31 | 37.75 | 38.75 | c. | F. |
| 48 | 140.00 | 60.00 | 8 | 50.00 | 10.00 | 32 | 40.00 | 40.00 | 0.05 | 0.09 |
| 47 | 137.75 | 58.75 |  | 47.75 | 8.75 | 33 | 42.25 | 4 I .25 | .10 | . 18 |
| 46 | 135.50 | 57.50 | 6 | 45.50 | 7.50 | 34 | 44.50 | 42.50 | . 15 | .27 .36 |
| +45 | +I33.25 | + 56.25 | $+5$ | $+43.25$ | $+6.25$ | -35 | -46.75 | -43.75 | . 25 | . 45 |
| 44 | 131.00 | 55.00 | 4 | 41.00 | 5.00 | 36 | 49.00 | 45.00 | . 75 | .90 1.35 |
| 43 | 128.75 | 53.75 | 3 | 38.75 | 3.75 | 37 | 51.25 | 46.25 |  | 1.80 |
| 42 | 126.50 | 52.50 | 2 | 36.50 | 2.50 | 38 | 53.50 | 47.50 |  |  |
| 41 | 124.25 | 51.25 | $+\mathrm{I}$ | 34.25 | + 1.25 | 39 | 55.75 | 48.75 |  |  |
| $+40$ | +122.00 | $+50.00$ | $\pm 0$ | + 32.00 | $\pm 0.00$ | -40 | $-58.00$ | -50.00 |  |  |
|  | $\begin{aligned} \mathrm{F}^{\circ} & =\frac{9}{5} \mathrm{C}^{\circ}+32^{\circ} \\ & =\frac{9}{4} \mathrm{R}^{\circ}+32^{\circ} \end{aligned}$ |  |  | $\begin{aligned} \mathrm{C}^{\circ} & =\frac{5}{9}\left(\mathrm{~F}^{\circ}-32^{\circ}\right) \\ & =\frac{5}{4} \mathrm{R}^{\circ} \end{aligned}$ |  |  | $\begin{aligned} \mathrm{R}^{\circ} & =\frac{4}{9}\left(\mathrm{~F}^{\circ}-32^{\circ}\right) \\ & =\frac{4}{5} \mathrm{C}^{\circ} \end{aligned}$ |  |  |  |

TAble 2.
FAHRENHEIT SCALE TO CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | C. | c. | c. | c. | C. | C. | c. | c. | c. |
| $+130^{\circ}$ | $+54.44$ | $+54^{\circ} 50$ | $+54^{\circ} 56$ | $+54^{\circ} .61$ | $+54.67$ | $+54.72$ | $+54^{\circ} 78$ | $+54.83$ | +54.89 | $+54.94$ |
| 129 | 53.89 | 53.94 | 54.00 | 54.06 | 54.11 | 54.17 | 54.22 | 54.28 | 54.33 | 54.39 |
| 128 | 53.33 | 53.39 | 53.44 | 53.50 | 53.56 | 53.61 | 53.67 | 53.72 | 53.78 | 53.83 |
| 127 | 52.78 | 52.83 | 52.89 | 52.94 | 53.00 | 53.06 | 53.11 | 53.17 | 53.22 | 53.28 |
| 126 | 52.22 | 52.28 | 52.33 | 52.39 | 52.44 | 52.50 | 52.56 | 52.6 I | 52.67 | 52.72 |
| $+125$ | $+51.67$ | + 51.72 | $+51.78$ | $+51.83$ | +51.89 | +51.94 | +52.00 | +52.06 | +52.11 | +52.17 |
| 124 | 51.11 | 51.17 | 51.22 | 51.28 | 5 I .33 | 51.39 | 5 I .44 | 51.50 | 51.56 | 51.6I |
| 123 | 50.56 | 50.61 | 50.67 | 50.72 | 50.78 | 50.83 | 50.89 | 50.94 | 51.00 | 51.06 |
| 122 | 50.00 | 50.06 | 50.11 | 50.17 | 50.22 | 50.28 | 50.33 | 50.39 | 50.44 | 50.50 |
| 12 I | 49.44 | 49.50 | 49.56 | 49.61 | 49.67 | 49.72 | 49.78 | 49.83 | 49.89 | 49.94 |
| +120 | +48.89 | +49.94 | +49.00 | +49.06 | +49.11 | $+49.17$ | +49.22 | +49.28 | +49.33 | +49.39 |
| 119 | 48.33 | 48.39 | 48.44 | 48.50 | 48.56 | 48.6I | 48.67 | 48.72 | 48.78 | 48.83 |
| 118 | 47.78 | 47.83 | 47.89 | 47.94 | 48.00 | 48.06 | 48. I I | 48.17 | 48.22 | 48.28 |
| 117 | 47.22 | 47.28 | 47.33 | 47.39 | 47.44 | 47.50 | 47.56 | 47.6I | 47.67 | 47.72 |
| 116 | 46.67 | 46.72 | 46.78 | 46.83 | 46.89 | 46.94 | 47.00 | 47.06 | 47.11 | 47.17 |
| +115 | +46. 11 | $+46.17$ | +46.22 | +46.28 | +46.33 | +46.39 | $+46.44$ | $+46.50$ | +46.56 | +46.6I |
| 114 | 45.56 | 45.6 I | 45.67 | 45.72 | 45.78 | 45.83 | 45.89 | 45.94 | 46.00 | 46.06 |
| 113 | 45.00 | 45.06 | 45. II | 45.17 | 45.22 | 45.28 | 45.33 | 45.39 | 45.44 | 45.50 |
| I 12 | 44.44 | 44.50 | 44.56 | 44.61 | 44.67 | 44.72 | 44.78 | 44.83 | 44.89 | 44.94 |
| III | 43.89 | 43.94 | 44.00 | 44.06 | 44. I I | 44.17 | 44.22 | 44.28 | 44.33 | 44.39 |
| $+110$ | +43.33 | +43.39 | +43.44 | +43.50 | +43.56 | +43.6I | +43.67 | +43.72 | +43.78 | +43.83 |
| 109 | 42.78 | 42.83 | 42.89 | 42.94 | 43.00 | 43.06 | 43.11 | 43.17 | 43.22 | 43.28 |
| 108 | 42.22 | 42.28 | 42.33 | 42.39 | 42.44 | 42.50 | 42.56 | 42.61 | 42.67 | 42.72 |
| 107 | 41.67 | 41.72 | 41.78 | 41.83 | 4 I .89 | 41.94 | 42.00 | 42.06 | 42.11 | 42.17 |
| 106 | 41. II | 41.17 | 41.22 | 41.28 | 41.33 | 41.39 | 41.44 | 41.50 | 41.56 | 41.61 |
| $+105$ | $+40.56$ | +40.6r | +40.67 | +40.72 | +40.78 | +40.83 | +40.89 | +40.94 | $+41.00$ | +41.06 |
| 104 | 40.00 | 40.06 | 40.11 | 40.17 | 40.22 | 40.28 | 40.33 | 40.39 | 40.44 | 40.50 |
| 103 | 39.44 | 39.50 | 39.56 | 39.61 | 39.67 | 39.72 | 39.78 | 39.83 | 39.89 | 39.94 |
| 102 | 38.89 | 38.94 | 39.00 | 39.06 | 39. II | 39.17 | 39.22 | 39.28 | 39.33 | 39.39 |
| IOI | 38.33 | 38.39 | 38.44 | 38.50 | 38.56 | 38.61 | 38.67 | 38.72 | 38.78 | 38.83 |
| $+100$ | $+37.78$ | +37.83 | +37.89 | +37.94 | +38.00 | +38.06 | +38.11 | $+38.17$ | +38.22 | $+38.28$ |
| 99 | 37.22 | 37.28 | 37.33 | 37.39 | 37.44 | 37.50 | 37.56 | 37.61 | 37.67 | 37.72 |
| 98 | 36.67 | 36.72 | 36.78 | 36.83 | 36.89 | 36.94 | 37.00 | 37.06 | 37.11 | 37.17 |
| 97 | 36.11 | 36.17 | 36.22 | 36.28 | 36.33 | 36.39 | 36.44 | 36.50 | 36.56 | 36.61 |
| 96 | 35.56 | 35.6I | 35.67 | 35.72 | 35.78 | 35.83 | 35.89 | 35.94 | 36.00 | 36.06 |
| $+95$ | +35.00 | +35.06 | +35. I I | +35.17 | +35.22 | +35.28 | +35.33 | +35.39 | +35.44 | $+35.50$ |
| 94 | 34.44 | 34.50 | 34.56 | 34.61 | 34.67 | 34.72 | 34.78 | 34.83 | 34.89 | 34.94 |
| 93 | 33.89 | 33.94 | 34.00 | 34.06 | 34.11 | 34.17 | 34.22 | 34.28 | $34 \cdot 33$ | 34.39 |
| 92 | 33.33 | 33.39 | 33.44 | 33.50 | 33.56 | 33.61 | 33.67 | 33.72 | 33.78 | 33.83 |
| 91 | 32.78 | 32.83 | 32.89 | 32.94 | 33.00 | 33.06 | 33.11 | 33.17 | 33.22 | 33.28 |
| +90 | +32.22 | +32.28 | +32.33 | +32.39 | +32.44 | +32.50 | $+32.56$ | +32.6I | $+32.67$ | +32.72 |
| 89 | 31.67 | 3 I .72 | 31.78 | 3 I .83 | 31.89 | 31.94 | 32.00 | 32.06 | 32.11 | 33.17 |
| 88 | 3 I .11 | 3 I .17 | 31.22 | 3 I .28 | 31.33 | 31.39 | 31.44 | 3 I .50 | 31.56 | 31.61 |
| 87 86 | 30.56 | 30.61 | 30.67 | 30.72 | 30.78 | 30.83 | 30.89 | 30.94 | 31.00 | 31.06 |
| 86 | 30.00 | 30.06 | 30.11 | 30.17 | 30.22 | 30.28 | 30.33 | 30.39 | 30.44 | 30.50 |
| $+85$ | +29.44 | +29.50 | +29.56 | +29.6I | +29.67 | +29.72 | +29.78 | +29.83 | +29.89 | +29.94 |
| 84 | 28.89 | 28.94 | 29.00 | 29.06 | 29.11 | 29.17 | 29.22 | 29.28 | 29.33 | 29.39 |
| 83 | 28.33 | 28.39 | 28.44 | 28.50 | 28.56 | 28.61 | 28.67 | 28.72 | 28.78 | 28.83 |
| 82 81 | 27.78 | 27.83 | 27.89 | 27.94 | 28.00 | 28.06 | 28.11 | 28.17 | 28.22 | 28.28 |
|  | 27.22 +26.67 | 27.28 | 27.33 | 27.39 | 27.44 | 27.50 | 27.56 | 27.61 | 27.67 | 27.72 |
| +80 | +26.67 | +26.72 | +26.78 | +26.83 | +26.89 | +26.94 | +27.00 | $+27.06$ | +27.11 | $+27.17$ |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

Smithsonian Tables.

TABLE 2.
FAHRENHEIT SCALE TO CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $+80^{\circ}$ | $\begin{gathered} c . \\ +26.67 \end{gathered}$ | $\begin{gathered} c . \\ +26.72 \end{gathered}$ | $\begin{gathered} \text { c. } \\ +26^{\circ} .78 \end{gathered}$ | $\begin{gathered} c . \\ +26.83 \end{gathered}$ | $\begin{gathered} c . \\ +26^{\circ} .89 \end{gathered}$ | $\begin{gathered} c . \\ +26.94 \end{gathered}$ | $\begin{gathered} c . \\ +27.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ +27.06 \end{gathered}$ | $\begin{gathered} c . \\ +27^{\circ} . \mathrm{II} \end{gathered}$ | $\begin{gathered} c . \\ +27^{\circ} \cdot 17 \end{gathered}$ |
| 79 | 26.11 | 26.17 | 26.22 | 26.28 | 26.33 |  | 26.44 | 26.50 | 26.56 | 26.61 |
| 78 | 25.56 | 25.61 | 25.67 | 25.72 | 25.78 | 25.83 | 25.89 | 25.94 | 26.00 | 26.06 |
| 77 | 25.00 | 25.06 | 25.11 | 25.17 | 25.22 | 25.28 | 25.33 | 25.39 | 25.44 | 25.50 |
| 76 | 24.44 | 24.50 | 24.56 | 24.61 | 24.67 | 24.72 | 24.78 | 24.83 | 24.89 | 24.94 |
| +75 | +23.89 | +23.94 | +24.00 | +24.06 | +24.II | $+24.17$ | +24.22 | +24.28 | +24.33 | +24.39 |
| 74 | 23.33 | 23.39 | 23.44 | 23.50 | 23.56 | 23.61 | 23.67 | 23.72 | 23.78 | 23.83 |
| 73 | 22.78 | 22.83 | 22.89 | 22.94 | 23.00 | 23.06 | 23.11 | 23.17 | 23.22 | 23.28 |
| 72 | 22.22 | 22.28 | 22.33 | 22.39 | 22.44 | 22.50 | 22.56 | 22.61 | 22.67 | 22.72 |
| 71 | 21.67 | 21.72 | 21.78 | 21.83 | 21.89 | 21.94 | 22.00 | 22.06 | 22.11 | 22.i7 |
| +70 | +21.11 | +21.17 | +21.22 | +21.28 | +2I.33 | +21.39 | +21.44 | +21.50 | +21.56 | +21.61 |
| 69 | 20.56 | 20.61 | 20.67 | 20.72 | 20.78 | 20.83 | 20.89 | 20.94 | 21.00 | 21.06 |
| 68 | 20.00 | 20.06 | 20.11 | 20.17 | 20.22 | 20.28 | 20.33 | 20.39 | 20.44 | 20.50 |
| 67 | 19.44 | 19.50 | 19.56 | 19.61 | 19.67 | 19.72 | 19.78 | 19.83 | 19.89 | 19.94 |
| 66 | 18.89 | 18.94 | 19.00 | 19.06 | 19.11 | 19.17 | 19.22 | 19.28 | 19.33 | 19.39 |
| +65 | +18.33 | +18.39 | +18.44 | +18.50 | +18.56 | +r8.6I | +18.67 | +18.72 | +18.78 | +18.83 |
| 64 | 17.78 | 17.83 | 17.89 | 17.94 | 18.00 | 18.06 | 18.11 | 18.17 | 18.22 | 18.28 |
| 63 | 17.22 | 17.28 | 17.33 | 17.39 | 17.44 | 17.50 | 17.56 | 17.61 | 17.67 | 17.72 |
| 62 | 16.67 | 16.72 | 16.78 | 16.83 | 16.89 | 16.94 | 17.00 | 17.06 | 17.11 | 17.17 |
| 6 I | 16.II | 16.17 | 16.22 | 16.28 | 16.33 | 16.39 | 16.44 | 16.50 | 16.56 | 16.61 |
| $+60$ | + r 5.56 | +15.6I | +15.67 | +15.72 | +15.78 | +15.83 | +15.89 | +15.94 | $+16.00$ | +r6.06 |
| 59 | 15.00 | 15.06 | 15.11 | 15.17 | 15.22 | 15.28 | 15.33 | 15.39 | 15.44 | 15.50 |
| 58 | 14.44 | 14.50 | 14.56 | 14.61 | 14.67 | 14.72 | 14.78 | 14.83 | 14.89 | 14.94 |
| 57 | 13.89 | 13.94 | 14.00 | 14.06 | 14.11 | 14.17 | 14.22 | 14.28 | 14.33 | 14.39 |
| 56 | 13.33 | 13.39 | 13.44 | 13.50 | 13.56 | 13.61 | 13.67 | 13.72 | 13.78 | 13.83 |
| $+55$ | +12.78 | +12.83 | +12.89 | +12.94 | +13.00 | +13.06 | +13.11 | $+\mathrm{I} 3.17$ | +13.22 | +13.28 |
| 54 | 12.22 | 12.28 | 12.33 | 12.39 | 12.44 | 12.50 | 12.56 | 12.61 | 12.67 | 12.72 |
| 53 | 11.67 | 11.72 | 11.78 | 11.83 | 11.89 | 11.94 | 12.00 | 12.06 | 12.11 | 12.17 |
| 52 | II.11 | 11.17 | II. 22 | 11.28 | 11.33 | 11.39 | 11.44 | II. 50 | II. 56 | 11.61 |
| 51 | 10.56 | 10.61 | 10.67 | 10.72 | 10.78 | 10.83 | 10.89 | 10.94 | II.OO | $\pm 1.06$ |
| $+50$ | +10.00 | +10.06 | +10.11 | +10.17 | +10.22 | +10.28 | +10.33 | +10.39 | +10.44 | +10.50 |
| 49 | 9.44 | 9.50 | 9.56 | 9.6 I | 9.67 | 9.72 | 9.78 | 9.83 | 9.89 | 9.94 |
| 48 | 8.89 | 8.94 | 9.00 | 9.06 | 9.1I | 9.17 | 9.22 | 9.28 | 9.33 | 9.39 |
| 47 | 8.33 | 8.39 | 8.44 | 8.50 | 8.56 | 8.61 | 8.67 | 8.72 | 8.78 | 8.83 |
| 46 | 7.78 | 7.83 | 7.89 | 7.94 | 8.00 | 8.06 | 8.1I | 8.17 | 8.22 | 8.28 |
| +45 | + 7.22 | + 7.28 | $+7.33$ | + 7.39 | + 7.44 | $+7.50$ | $+7.56$ | $+7.61$ | $+7.67$ | + 7.72 |
| 44 | 6.67 | 6.72 | 6.78 | 6.83 | 6.89 | 6.94 | 7.00 | 7.06 | 7.11 | 7.17 |
| 43 | 6.11 | 6.17 | 6.22 | 6.28 | 6.33 | 6.39 | 6.44 | 6.50 | 6.56 | 6.61 |
| 42 | 5.56 | 5.61 | 5.67 | 5.72 | 5.78 | 5.83 | 5.89 | 5.94 | 6.00 | 6.06 |
| 41 | 5.00 | 5.06 | 5.11 | 5.17 | 5.22 | 5.28 | 5.33 | 5.39 | 5.44 | 5.50 |
| $+40$ | + 4.44 | $+4.50$ | $+4.56$ | $+4.61$ | + 4.67 | $+4.72$ | $+4.78$ | $+4.83$ | + 4.89 | + 4.94 |
| 39 | 3.89 | 3.94 | 4.00 | 4.06 | 4.11 | 4.17 | 4.22 | 4.28 | 4.33 | 4.39 |
| 38 | 3.33 | 3.39 | 3.44 | 3.50 | 3.56 | 3.61 | 3.67 | 3.72 | 3.78 | 3.83 |
| 37 | 2.78 | 2.83 | 2.89 | 2.94 | 3.00 | 3.06 | 3.11 | 3.17 | 3.22 | 3.28 |
| 36 | 2.22 | 2.28 | 2.33 | 2.39 | 2.44 | 2.50 | 2.56 | 2.61 | 2.67 | 2.72 |
| +35 | + 1.67 | + 1.72 | + 1.78 | + 1.83 | + 1.89 | + 1.94 | + 2.00 | +2.06 | +2.11 | $+2.17$ |
| 34 | +1.11 | +1.17 | + 1.22 | + 1.28 | + 1.33 | + 1.39 | + 1.44 | + 1.50 | + 1.56 | + 1.61 |
| 33 | $+0.56$ | +0.6I | + 0.67 | +0.72 | + 0.78 | + 0.83 | +o.89 | + 0.94 | + 1.00 | + 1.06 |
| 32 | 0.00 | + 0.06 | +0.II | +0.17 | + 0.22 | + 0.28 | +0.33 | +0.39 | + 0.44 | $+0.50$ |
| 3 I | $-0.56$ | $-0.50$ | -0.44 | $-0.39$ | $-0.33$ | $-0.28$ | $-0.22$ | $-0.17$ | -0.11 | - 0.06 |
| $+30$ | - I.II | - 1.06 | $-1.00$ | $-0.94$ | $-0.89$ | $-0.83$ | $-0.78$ | $-0.72$ | $-0.67$ | -0.6I |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

FAHRENHEIT SCALE TO CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | C. | c. | c. | C. | C. | c. | c. | c. | c. |
| $+30^{\circ}$ | - İII | - I.06 | $-\mathrm{I} .00$ | $-0.94$ | -0.89 | $-0.83$ | $-0.78$ | $-0.72$ | -0.67 | - 0.61 |
| 29 | 1.67 | 1.61 | I. 56 | 1.50 | I. 44 | I. 39 | 1.33 | I. 28 | I. 22 | I. 17 |
| 28 | 2.22 | 2.17 | 2.11 | 2.06 | 2.00 | 1.94 | 1.89 | r. 83 | 1.78 | 1.72 |
| 27 | 2.78 | 2.72 | 2.67 | 2.61 | 2.56 | 2.50 | 2.44 | 2.39 | 2.33 | 2.28 |
| 26 | 3.33 | 3.28 | 3.22 | 3.17 | 3.11 | 3.06 | 3.00 | 2.94 | 2.89 | 2.83 |
| $+25$ | $-3.89$ | $-3.83$ | $-3.78$ | - 3.72 | $-3.67$ | - 3.61 | $-3.56$ | - 3.50 | - 3.44 | $-3.39$ |
| 24 | 4.44 | 4.39 | 4.33 | 4.28 | 4.22 | 4.17 | 4.11 | 4.06 | 4.00 | 3.94 |
| 23 | 5.00 | 4.94 | 4.89 | 4.83 | 4.78 | 4.72 | 4.67 | 4.61 | 4.56 | 4.50 |
| 22 | 5.56 | 5.50 | 5.44 | $5 \cdot 39$ | $5 \cdot 33$ | 5.28 | 5.22 | 5.17 | 5.11 | 5.06 |
| 21 | 6.11 | 6.06 | 6.00 | 5.94 | 5.89 | 5.83 | 5.78 | 5.72 | 5.67 | 5.61 |
| +20 | $-6.67$ | - 6.6I | $-6.56$ | $-6.50$ | - 6.44 | -6.39 | $-6.33$ | $-6.28$ | $-6.22$ | $-6.17$ |
| 19 | 7.22 | 7.17 | 7.11 | 7.06 | 7.00 | 6.94 | 6.89 | 6.83 | 6.78 | 6.72 |
| 18 | 7.78 | 7.72 | 7.67 | 7.61 | 7.56 | 7.50 | 7.44 | 7.39 | 7.33 | 7.28 |
| 17 | 8.33 | 8.28 | 8.22 | 8.17 | 8.11 | 8.06 | 8.00 | 7.94 | 7.89 | 7.83 |
| 16 | 8.89 | 8.83 | 8.78 | 8.72 | 8.67 | 8.6 I | 8.56 | 8.50 | 8.44 | 8.39 |
| $+15$ | - 9.44 | - 9.39 | $-9.33$ | $-9.28$ | - 9.22 | -9.17 | $-9.11$ | $-9.06$ | -9.00 | - 8.94 |
| 14 | 10.00 | 9.94 | 9.89 | 9.83 | 9.78 | 9.72 | 9.67 | 9.61 | 9.56 | 9.50 |
| 13 | 10.56 | 10.50 | 10.44 | 10.39 | 10.33 | 10.28 | 10.22 | 10.17 | 10.11 | 10.06 |
| 12 | II.II | 11.06 | 11.00 | 10.94 | 10.89 | 10.83 | 10.78 | 10.72 | 10.67 | 10.61 |
| II | 11.67 | 11.61 | 11.56 | 11.50 | II. 44 | II. 39 | 11.33 | 11.28 | 11.22 | 11.17 |
| $+10$ | -12.22 | -12.17 | -12.11 | -12.06 | -12.00 | -II.94 | -11.89 | $-11.83$ | -11.78 | -11.72 |
| 9 | 12.78 | 12.72 | 12.67 | 12.61 | 12.56 | 12.50 | 12.44 | 12.39 | 12.33 | 12.28 |
| 8 | 13.33 | 13.28 | 13.22 | 13.17 | 13.11 | 13.06 | 13.00 | 12.94 | 12.89 | 12.83 |
| 7 | 13.89 | 13.83 | 13.78 | 13.72 | 13.67 | 13.61 | 13.56 | 13.50 | 13.44 | 13.39 |
| 6 | 14.44 | 14.39 | 14.33 | 14.28 | 14.22 | 14.17 | 14.11 | 14.06 | 14.00 | 13.94 |
| $+5$ | -15.00 | -14.94 | $-14.89$ | $-14.83$ | -14.78 | -14.72 | -14.67 | -14.61 | -14.56 | $-14.50$ |
| 4 | 15.56 | 15.50 | 15.44 | 15.39 | 15.33 | 15.28 | 15.22 | 15.17 | 15.11 | 15.06 |
| 3 | 16.11 | 16.06 | 16.00 | 15.94 | 15.89 | 15.83 | 15.78 | 15.72 | 15.67 | 15.61 |
| 2 | 16.67 | 16.61 | 16.56 | 16.50 | 16.44 | 16.39 | 16.33 | 16.28 | 16.22 | 16.17 |
|  | 17.22 | 17.17 | 17.11 | 17.06 | 17.00 | 16.94 | 16.89 | 16.83 | 16.78 | 16.72 |
| $+0$ | 17.78 | 17.72 | 17.67 | 17.61 | 17.56 | 17.50 | 17.44 | 17.39 | 17.33 | 17.28 |
| 0 | $-17$ | $-17.83$ | -17.89 | -17.94 | -18.00 | -18.06 | -18.11 | -18.17 | -18.22 | $-18.28$ |
| 1 | 18.33 | 18.39 | 18.44 | 18.50 | 18.56 | 18.61 | 18.67 | 18.72 | 18.78 | 18.83 |
| 2 | 18.89 | 18.94 | 19.00 | 19.06 | 19.11 | 19.17 | 19.22 | 19.28 | 19.33 | 19.39 |
|  | 19.44 | 19.50 | 19.56 | 19.61 | 19.67 | 19.72 | 19.78 | 19.83 | 19.89 | 19.94 |
| 4 | 20.00 | 20.06 | 20.11 | 20.17 | 20.22 | 20.28 | 20.33 | 20.39 | 20.44 | 20.50 |
| - | -20.56 | -20.6I | $-20.67$ | $-20.72$ | -20.78 | $-20.83$ | $-20.89$ | -20.94 | -21.00 | -21.06 |
| 6 | 21.1 | 21.17 | 21.22 | 21.28 | 21.33 | 21.39 | 21.44 | 21.50 | 21.56 | 21.6I |
| 7 | 21.67 | 21.72 | 21.78 | 21.83 | 21.89 | 21.94 | 22.00 | 22.06 | 22.11 | 22.17 |
| 8 | 22.22 | 22.28 | 22.33 | 22.39 | 22.44 | 22.50 | 22.56 | 22.61 | 22.67 | 22.72 |
| 9 | 22.78 | 22.83 | 22.89 | 22.94 | 23.00 | 23.06 | 23.11 | 23.17 | 23.22 | 23.28 |
| $-10$ | -23.33 | -23.39 | -23.44 | -23.50 | $-23.56$ | -23.6I | $-23.67$ | -23.72 | $-23.78$ | $-23.83$ |
| II | 23.89 | 23.94 | 24.00 | 24.06 | 24.11 | 24.17 | 24.22 | 24.28 | 24.33 | 24.39 |
| 12 | 24.44 | 24.50 | 24.56 | 24.6I | 24.67 | 24.72 | 24.78 | 24.83 | 24.89 | 24.94 |
| 13 | 25.00 | 25.06 | 25.11 | 25.17 | 25.22 | 25.28 | 25.33 | 25.39 | 25.44 | 25.50 |
| 14 | 25.56 | 25.61 | 25.67 | 25.72 | 25.78 | 25.83 | 25.89 | 25.94 | 26.00 | 26.06 |
| -15 -16 | -26.11 | -26.17 | -26.22 | -26.28 | -26.33 | -26.39 | -26.44 | -26.50 | -26.56 | -26.61 |
| 16 | 26.67 | 26.72 | 26.78 | 26.83 | 26.89 | 26.94 | 27.00 | 27.06 | 27.11 | 27.17 |
| 17 | 27.22 | 27.28 | 27.33 | 27.39 | 27.44 | 27.50 | 27.56 | 27.61 | 27.67 | 27.72 |
| 0 | 27.78 | 27.83 | 27.89 | 27.94 | 28.00 | 28.06 | 28. II | 28.17 | 28.22 | 28.28 |
| 19 | 28.33 | 28.39 | 28.44 | 28.50 | 28.56 | 28.61 | 28.67 | 28.72 | 28.78 | 28.83 |
| -20 | -28.89 | -28.94 | -29.00 | -29.06 | -29. 11 | -29.17 | -29.22 | -29.28 | -29.33 | -29.39 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

Smithaonian Tables.

FAHRENHEIT SCALE TO CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | c. | c. | c. | c. | c. | c. | c. | c. | c. |
| $-20^{\circ}$ | $-28.89$ | -28.94 | $-29.00$ | 29.06 | -29.11 | $-29^{\circ} 17$ | $-29^{\circ} .22$ | -29.28 | $-29^{\circ} 33$ | -29.39 |
| 21 | 29.44 | 29.50 | 29.56 | 29.61 | 29.67 | 29.72 | 29.78 | 29.83 | 29.89 | 29.94 |
| 22 | 30.00 | 30.06 | 30.11 | 30.17 | 30.22 | 30.28 | 30.33 | 30.39 | 30.44 | 30.50 |
| 23 | 30.56 | 30.61 | 30.67 | 30.72 | 30.78 | 30.83 | 30.89 | 30.94 | 31.00 | 3 T .06 |
| 24 | 31.11 | 31.17 | 31.22 | 31.28 | 31.33 | 31.39 | 31.44 | 3 I .50 | 31.56 | 3 I .61 |
| -25 | -31.67 | -31.72 | $-31.78$ | $-31.83$ | 31.89 | -31.94 | -32.00 | -32.06 | -32.11 | -32.17 |
| 26 | 32.22 | 32.28 | 32.33 | 32.39 | 32.44 | 32.50 | 32.56 | 32.61 | 32.67 | 32.72 |
| 27 | 32.78 | 32.83 | 32.89 | 32.94 | 33.00 | 33.06 | 33.11 | 33.17 | 33.22 | 33.28 |
| 28 | 33.33 | 33.39 | 33.44 | 33.50 | 33.56 | 33.61 | 33.67 | 33.72 | 33.78 | 33.83 |
| 29 | 33.89 | 33.94 | 34.00 | 34.06 | 34. II | 34.17 | 34.22 | 34.28 | 34.33 | 34.39 |
| -30 | -34.44 | -34.50 | -34.56 | -34.61 | -34.67 | -34.72 | -34.78 | -34.83 | -34.89 | -34.94 |
| 31 | 35.00 | 35.06 | 35.11 | 35.17 | 35.22 | 35.28 | 35.33 | 35.39 | 35.44 | 35.50 |
| 32 | 35.56 | 35.61 | 35.67 | 35.72 | 35.78 | 35.83 | 35.89 | 35.94 | 36.00 | 36.06 |
| 33 | 36.11 | 36.17 | 36.22 | 36.28 | 36.33 | 36.39 | 36.44 | 36.50 | 36.56 | 36.61 |
| 34 | 36.67 | 36.72 | 36.78 | 36.83 | 36.89 | 36.94 | 37.00 | 37.06 | 37.11 | 37.17 |
| -35 | -37.22 | $-37.28$ | $-37.33$ | -37.39 | -37.44 | $-37.50$ | -37.56 | $-37.61$ | $-37.67$ | $-37.72$ |
| 36 | 37.78 | 37.83 | 37.89 | 37.94 | 38.00 | 38.06 | 38.11 | 38.17 | 38.22 | 38.28 |
| 37 | 38.33 | 38.39 | 38.44 | 38.50 | 38.56 | 38.61 | 38.67 | 38.72 | 38.78 | 38.83 |
| 38 | 38.89 | 38.94 | 39.00 | 39.06 | 39.11 | 39.17 | 39.22 | 39.28 | 39.33 | 39.39 |
| 39 | 39.44 | 39.50 | 39.56 | 39.61 | 39.67 | 39.72 | 39.78 | 39.83 | 39.89 | 39.94 |
| -40 | -40.00 | -40.06 | -40.11 | -40.17 | -40.22 | -40.28 | -40.33 | -40.39 | -40.44 | -40.50 |
| 41 | 40.56 | 40.61 | 40.67 | 40.72 | 40.78 | 40.83 | 40.89 | 40.94 | 41.00 | 41.06 |
| 42 | 41.11 | 41.17 | 41.22 | 41.28 | 41.33 | 41.39 | 41.44 | 41.50 | 41.56 | 4 r .61 |
| 43 | 41.67 | 41.72 | 41.78 | 4 r .83 | 41.89 | 41.94 | 42.00 | 42.06 | 42.11 | 42.17 |
| 44 | 42.22 | 42.28 | 42.33 | 42.39 | 42.44 | 42.50 | 42.56 | 42.61 | 42.67 | 42.72 |
| -45 | $-42.78$ | $-42.83$ | $-42.89$ | -42.94 | -43.00 | -43.06 | -43.11 | -43.17 | -43.22 | -43.28 |
| 46 | 43.33 | 43.39 | 43.44 | 43.50 | 43.56 | 43.61 | 43.67 | 43.72 | 43.78 | 43.83 |
| 47 | 43.89 | 43.94 | 44.00 | 44.06 | 44.11 | 44.17 | 44.22 | 44.28 | 44.33 | 44.39 |
| 48 | 44.44 | 44.50 | 44.56 | 44.61 | 44.67 | 44.72 | 44.78 | 44.83 | 44.89 | 44.94 |
| 49 | 45.00 | 45.06 | 45.11 | 45.17 | 45.22 | 45.28 | 45.33 | 45.39 | 45.44 | 45.5) |
| -50 | -45.56 | -45.61 | $-45.67$ | -45.72 | -45.78 | $-45.83$ | $-45.89$ |  |  |  |
| 51 | 45.11 | 46.17 | 46.22 | 46.28 | 46.33 | 46.39 | 46.44 | 46.50 | 46.56 | 46.6r |
| 52 | 46.67 | 46.72 | 46.78 | 46.83 | 46.89 | 46.94 | 47.00 | 47.06 | 47.11 | 47.17 |
| 53 | 47.22 | 47.28 | 47.33 | 47.39 | 47.44 | 47.50 | 47.56 | 47.61 | 47.67 | 47.72 |
| 54 | 47.78 | 47.83 | 47.89 | 47.94 | 48.00 | 48.06 | 48.11 | 48.17 | 48.22 | 48.28 |
| -55 | -48.33 | -48.39 | $-48.44$ | $-48.50$ | -48.56 | -48.6I | $-48.67$ | -48.72 | $-48.78$ | -48.83 |
| 56 | 48.89 | 48.94 | 49.00 | 49.06 | 49.11 | 49.17 | 49.22 | 49.28 | 49.33 | 49.39 |
| 57 | 49.44 | 49.50 | 49.56 | 49.61 | 49.67 | 49.72 | 49.78 | 49.33 | 49.89 | 49.94 |
| 5 | 50.00 | 50.06 | 50.11 | 50.17 | 50.22 | 50.28 | 50.33 | 50.39 | 50.44 | 50.50 |
| 59 | 50.56 | 50.61 | 50.67 | 50.72 | 50.78 | 50.83 | 50.89 | 50.94 | 51.00 | 51.06 |
| -60 61 | -51.11 -51.67 5 | -51.17 | -51.22 | -51.28 | -51.33 | -51.39 | -51.44 | -51.50 | -51.56 | -51.61 |
| 61 62 | 51.67 52.22 | 51.72 52.28 | 51.7 | 51.83 52.39 | 51.89 52.44 | 51.94 52.50 | 52.00 52.56 | 52.06 52.61 | 52.11 52.67 | 52.17 52.72 |
| 63 | 52.78 | 52.83 | 52.89 | 52.94 | 53.00 | 53.06 | 53.11 | 53.17 | 53.22 | 53.28 |
| 64 | 53.33 | 53.39 | 53.44 | 53.50 | 53.56 | 53.61 | 53.67 | 53.72 | 53.78 | 53.83 |
| -65 | $-53.89$ | -53.94 | $-54.00$ | -54.06 | -54.11 | -54.17 | -54.22 | -54.28 | $-54.33$ | -54.39 |
| 66 | 54.44 | 54.50 | 54.56 | 54.61 | 54.67 | 54.72 | 54.78 | 54.83 | 54.89 | 54.94 |
| 67 | 55.00 | 55.06 | 55.11 | 55.17 | 55.22 | 55.28 | 55.33 | 55.39 | 55.44 | 55.50 |
| 68 | 55.56 | 55.61 | 55.67 | 55.72 | 55.78 | 55.83 | 55.89 | 55.94 | 56.00 | 56.06 |
| 69 | 56.11 | 56.17 | 56.22 | 56.28 | 56.33 | 56.39 | 56.44 | 56.50 | 56.56 | 56.61 |
| -70 | -56.67 | $-56.72$ | $-56.78$ | -56.83 | -56.89 | -56.94 | -57.00 | -57.06 | -57.11 | -57.17 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

CENTIGRADE SCALE TO FAHRENHEIT.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F |  | F. | F. | F. | F. | F. | F. | F. | F. |
| $+50^{\circ}$ | +122.00 | +122.18 | +122.36 | +I22.54 | +122.72 | +122.90 | +123.08 |  |  | 123.62 |
| 49 | 120.20 | 120.38 | 120.56 | 120.74 | 120.92 | 121.10 | 121.28 | 121.46 | 121.64 | 121.82 |
| 48 | 118.40 | 118.58 | 118.76 | 118.94 | 119.12 | 119.30 | 119.48 | 119.66 | 119.84 | 120.02 |
| 47 | 116.60 | 116.78 | II6.96 | 117.14 | 117.32 | 117.50 | 117.68 | 117.86 | 118.04 | 118.22 |
| 46 | 114.80 | 114.98 | 115.16 | II5.34 | II5.52 | 115.70 | 115.88 | 116.06 | 116.24 | 116.42 |
| +45 | +113.00 | -113.18 | +113.3 | 113 | +113.72 | 113.90 | 14.08 | +II4.26 |  | 114.62 |
| 44 | III. 20 | 111.38 | 111.56 | 111.74 | 111.92 | II2.10 | 112.28 | 112.46 | 112.64 | 112.82 |
| 43 | 109.40 | 109.58 | 109.76 | 109.94 | 110.12 | 110.30 | 110.48 | 110.66 | 110.84 | 111.02 |
| 42 | 107.60 | 107.78 | 107.96 | 108. 14 | 108.32 | 108.50 | 108.68 | 108.86 | 109.04 | 109.22 |
| 41 | $\underline{105.80}$ | 105.98 | 106.16 | 106.34 | 106.52 | 106.70 | 106.88 | 107.06 | 107.24 | 107.42 |
| $+40$ | +104. |  | 04. | 104. | -104.72 | +104.90 |  |  |  | 105.62 |
| 39 | 102.20 | 102.38 | 102.56 | 102.74 | 102.92 | 103.10 | 103.28 | 103.46 | 103.64 | 103.82 |
| 38 | 100.40 | 100.58 | 100.76 | 100.94 | IOI.12 | 101.30 | IOI. 48 | IOI. 66 | IOI. 84 | 102.02 |
| 37 | 98.60 | 98.78 | 98.96 | 99. 14 | 99.32 | 99.50 | 99.68 | 99.86 | 100.04 | 100.22 |
| 36 | 96.80 | 96.98 | 97.16 | 97.34 | 97.52 | 97.70 | 97.88 | 98.06 | 98.24 | 98.42 |
| +35 | +95.00 | + 95.18 | +95.3 | +95.54 | + 95.72 | +95.90 | +96.08 | +96.26 | +96.44 | + 96.62 |
| 34 | 93.20 | 93.38 | 93.56 | 93.74 | 93.92 | 94.10 | 94.28 | 94.46 | 94.64 | 94.82 |
| 33 | 91.40 | 91.58 | 91.76 | 91.94 | 92.12 | 92.30 | 92.48 | 92.66 | 92.84 | 93.02 |
| 32 | 89.60 | 89.78 | 89.96 | 90.14 | 90.32 | 90.50 | 90.68 | 90.86 | 91.04 | 91.22 |
| 3 I | 87.80 | 87.98 | 88.16 | 88.34 | 88.52 | 88.70 | 88.88 | 89.06 | 89.24 | 89.42 |
| +30 | +86.00 | +86.18 | +86.36 | +86.54 | +86.72 | +86.90 | $+87.08$ | +87.26 | $+87.44$ | $+87.62$ |
| 29 | 84.20 | 84.38 | 84.56 | 84.74 | 84.92 | 85. 10 | 85.28 | 85.46 | 85.64 | 85.82 |
| 28 | 82.40 | 82.58 | 82.76 | 82.94 | 83.12 | 83.30 | 83.48 | 83.66 | 83.84 | 84.02 |
| 27 | 80.60 | 80.78 | 80.96 | 81.14 | 8 I .32 | 8 I .50 | 81.68 | 8 s .86 | 82.04 | 82.22 |
| 26 | 78.80 | 78.98 | 79.16 | 79.34 | 79.52 | 79.70 | 79.88 | 80.06 | 80.24 | 80.42 |
| $+25$ | + 77.00 | + 77.18 | + 77.36 | + 77.54 | +77.72 | +77.90 | + 78.08 | + 78.26 | + 78.44 | + 78.62 |
| 24 | 75.20 | 75.38 | 75.56 | 75.74 | 75.92 | 76.10 | 76.28 | 76.46 | 76.64 | 76.82 |
| 23 | 73.40 | 73.58 | 73.76 | 73.94 | 74.12 | 74.30 | 74.48 | 74.66 | 74.84 | 75.02 |
| 22 | 71.60 | 71.78 | 71.96 | 72.14 | 72.32 | 72.50 | 72.68 | 72.86 | 73.04 | 73.22 |
| 21 | 69.80 | 69.98 | 70.16 | 70.34 | 70.52 | 70.70 | 70.88 | 71.06 | 7 I .24 | 71.42 |
| +20 | +68.00 | +68.18 | +68.36 | $+68.54$ | +68.72 | +68.90 | $+69.08$ | +69.26 | +69.44 | +69.62 |
| 19 | 66.20 | 66.38 | 66.56 | 66.74 | 66.92 | 67.10 | 67.28 | 67.46 | 67.64 | 67.82 |
| 18 | 64.40 | 64.58 | 64.76 | 64.94 | 65.12 | 65.30 | 65.48 | 65.66 | 65.84 | 66.02 |
| 17 | 62.60 | 62.78 | 62.96 | 63.14 | 63.32 | 63.50 | 63.68 | 63.86 | 64.04 | 64.22 |
| 16 | 60.80 | 60.98 | 61.16 | 61.34 | 6I. 52 | 61.70 | 61.88 | 62.06 | 62.24 | 62.42 |
| +15 | $+59.00$ | + 59.18 | $+59.36$ | $+59.54$ | +59.72 | $+59.90$ | $+60.08$ | $+60.26$ | $+60.44$ | +60.62 |
| 14 | 57.20 | 57.38 | 57.56 | 57.74 | 57.92 | 58. 10 | 58.28 | 58.46 | 58.64 | 58.82 |
| 13 | 55.40 | 55.58 | 55.76 | 55.94 | 56.12 | 56.30 | 56.48 | 56.66 | 56.84 | 57.02 |
| 12 | 53.60 | 53.78 | 53.96 | 54.14 | 54.32 | 54.50 | 54.68 | 54.86 | 55.04 | 55.22 |
| II | 5 I .80 | 51.98 | 52.16 | 52.34 | 52.52 | 52.70 | 52.88 | 53.06 | 53.24 | 53.42 |
| $+10$ | $+50.00$ | + 50.18 | $+50.36$ | $+50.54$ | $+50.72$ | $+50.90$ | $+51.08$ | +51.26 | +51.44 | $+51.62$ |
|  | 48.20 | 48.38 | 48.56 | 48.74 | 48.92 | 49.10 | 49.28 | 49.46 | 49.64 | 49.82 |
| 8 | 46.40 | 46.58 | 46.76 | 46.94 | 47.12 | 47.30 | 47.48 | 47.66 | 47.84 | 48.02 |
| 7 | 44.60 | 44.78 | 44.96 | 45.14 | 45.32 | 45.50 | 45.68 | 45.86 | 46.04 | 46.22 |
| 6 | 42.80 | 42.98 | 43.16 | 43.34 | 43.52 | 43.70 | 43.88 | 44.06 | 44.24 | 44.42 |
| $+5$ | +41.00 | $+41.18$ | +41.36 | +41.54 | + 41.72 | +41.90 | +42.08 | + 42.26 | + 42.44 | $+42.62$ |
| 4 | 39.20 | 39.38 | 39.56 | 39.74 | 39.92 | 40.10 | 40.28 | 40.46 | 40.64 | 40.82 |
| 3 | 37.4 | 37.58 | 37.76 | 37.94 | 38.12 | 38.30 | 38.48 | 38.66 | 3 S.84 | 39.02 |
| 2 | 35.60 | 35.78 | 35.96 | 36.14 | 36.32 | 36.50 | 36.68 | 36.86 | 37.04 | 37.22 |
|  | 33.80 | 33.98 | 34.16 | 34.34 | 34.52 | 34.70 | 34.88 | 35.06 | 35.24 | 35.42 |
| $+0$ | $+32.00$ | + 32.18 | $+32.36$ | +32.54 | + 32.72 | $+32.90$ | + 33.08 | $+33.26$ | $+33.44$ | +33.62 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

Smithsonian Tables.

TABLE 3.
CENTIGRADE SCALE TO FAHRENHEIT.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F. | $\stackrel{\mathrm{F}}{\text { F }}$ | ${ }_{\text {F. }}^{\text {F. }}$ | ${ }_{\text {F. }}{ }^{\text {c }}$ | ${ }_{\text {F. }}^{\text {F. }}$ | $\stackrel{\text { F. }}{\text { c }}$ | ${ }_{\text {F }}$ | ${ }^{\text {F. }}$ | ${ }_{\text {F. }}^{\text {F. }}$ | ${ }_{\text {F. }}$ |
| $0{ }^{\circ}$ | +32.00 | +31.822 | +31.64 | +31.46 | $+31.28$ | +31.10 | $+30.92$ | $+30^{\circ} 74$ | 30.56 | $+30^{\circ} 38$ |
| 1 | 30.20 | 30.02 | 29.84 | 29.66 | 29.48 | 29.30 | 29.12 | 28.94 | 28.76 | 28.58 |
| 2 | 28.40 | 28.22 | 28.04 | 27.86 | 27.68 | 27.50 | 27.32 | 27.14 | 26.96 | 26.78 |
| 3 | 26.60 | 26.42 | 26.24 | 26.06 | 25.88 | 25.70 | 25.52 | 25.34 | 25.16 | 24.98 |
| 4 | 24.80 | 24.62 | 24.44 | 24.26 | 24.08 | 23.90 | 23.72 | 23.54 | 23.36 | 23.18 |
| - 5 | +23.00 | +22.82 | +22.64 | +22.46 | +22.28 | +22.10 | +21.92 | +21.74 | +21.56 | +21.38 |
| 6 | 21.20 | 21.02 | 20.84 | 20.66 | 20.48 | 20.30 | 20.12 | 19.94 | 19.76 | 19.58 |
| 7 | 19.4 | 19.22 | 19.04 | 18.86 | 18.68 | 18.50 | 18.32 | 18.14 | 17.96 | 17.78 |
| 8 | 17.60 | 17.42 | 17.24 | 17.06 | 16.88 | 16.70 | 16.52 | 16.34 | 16.16 | 15.98 |
| 9 | 15.80 | 15.62 | 15.44 | 15.26 | 15.08 | 14.90 | 14.72 | 14.54 | 14.36 | 14.18 |
| -10 | +14.00 | +13.82 | +13.64 | + 3.46 | +13.28 | +13.10 | +12.92 | +12.74 | +12.56 | +12.38 |
| 11 | 12.20 | 12.02 | 11.84 | I1. 66 | 11.48 | I1. 30 | 11.12 | 10.94 | 10.76 | Io. 58 |
| 12 | 10.40 | 10.22 | 10.04 | 9.86 | 9.68 | 9.50 | 9.32 | 9.14 | 8.96 | 8.78 |
| 13 | 8.60 | 8.42 | 8.24 | 8.06 | 7.88 | 7.70 | 7.52 | 7.34 | 7.16 | 6.98 |
| 14 | 6.80 | 6.62 | 6.44 | 6.26 | 6.08 | 5.90 | 5.72 | 5.54 | 5.36 | 5.18 |
| -15 | + 5.00 | + 4.82 | + 4.64 | + 4.46 | + 4.28 | + 4.10 | + 3.92 | + 3.74 | +3.56 | + 3.38 |
| 16 | + 3.20 | +3.02 | +2.84 | + 2.66 | + 2.48 | +2.30 | + 2.12 | + 1.94 | + 1.76 | + 1.58 |
| 17 | + 1.40 | + 1.22 | + 1.04 | + 0.86 | + 0.68 | + 0.50 | +0.32 | + 0.14 | - o. 04 | - 0.22 |
| 18 | - 0.40 | - 0.58 | -0.76 | - 0.94 | - 1.12 | - 1.30 | - 1.48 | - 1.66 | - 1.84 | - 2.02 |
| 19 | - 2.20 | $-2.38$ | $-2.56$ | - 2.74 | $-2.92$ | - 3.10 | - 3.28 | - 3.46 | $-3.64$ | - 3.82 |
| -20 | -4.00 | -4.18 | $-4.36$ | - 4.54 | -4.72 | -4.90 | $-5.08$ | - 5.26 | - 5.44 | - 5.62 |
| 21 | . 80 | 5.98 | 6.16 | 6.34 | 6.52 | 6.70 | 6.88 | 7.06 | 7.24 | 7.42 |
| 22 | 7.60 | 7.78 | 7.96 | 8.14 | 8.32 | 8.50 | 8.68 | 8.86 | 9.04 | 9.22 |
| 23 | 9.40 | 9.58 | 9.76 | 9.94 | 10.12 | 10.30 | 10.48 | 10.66 | 10.84 | 11.02 |
| 24 | 11.20 | 11.38 | 11.56 | 11.74 | 11.92 | 12.10 | 12.28 | 12.46 | 12.64 | 12.82 |
| -25 | -13.00 | $-13.18$ | $-13.36$ | $-13.54$ | -13.72 | $-13.90$ | -14.08 | -14.26 |  |  |
| 26 | 14.80 | 14.98 | 15.16 | 15.34 | 15.52 | 15.70 | 15.88 | 16.06 | 16.24 | 16.42 |
| 27 | 16.60 | 16.78 | 16.96 | 17.14 | 17.32 | 17.50 | 17.68 | 17.86 | 18.04 | 18.22 |
| 28 | 18.40 | 18.58 | 18.76 | 18.94 | 19.12 | 19.30 | 19.48 | 19.66 | 19.84 | 20.02 |
| 29 | 20.20 | 20.38 | 20.56 | 20.74 | 20.92 | 21.10 | 21.28 | 21.46 | 21.64 | 21.82 |
| -30 | -22.00 | -22.18 | -22.36 | -22.54 | -22.72 | -22.90 | -23.08 | -23.26 | -23.44 | -23.62 |
| 31 | 23.80 | 23.98 | 24.16 | 24.34 | 24.52 | 24.70 | 24.88 | 25.06 | 25.24 | 25.42 |
| 32 | 25.60 | 25.78 | 25.96 | 26.14 | 26.32 | 26.50 | 26.68 | 26.86 | 27.04 | 27.22 |
| 33 | 27.40 | 27.58 | 27.76 | 27.94 | 28.12 | 28.30 | 28.48 | 28.66 | 28.84 | 29.02 |
| 34 | 29.20 | 29.38 | 29.56 | 29.74 | 29.92 | 30.10 | 30.28 | 30.46 | 30.64 | 30.82 |
| -35 | -31.00 | $-31.18$ | -31.36 | $-31.54$ | -31.72 | $-31.90$ | -32.08 | -32.26 | $-32.44$ | -32.62 |
| 36 | 32.80 | 32.98 | 33.16 | 33.34 | 33.52 | 33.70 | 33.88 | 34.06 | 34.24 | 34.42 |
| 37 | 34.60 | 34.78 | 34.96 | 35.14 | 35.32 | 35.50 | 35.68 | 35.86 | 36.04 | 36.22 |
| 38 | 36.40 | 36.58 | 36.76 | 36.94 | 37.12 | 37.30 | 37.48 | 37.66 | 37.84 | 38.02 |
| 39 | 38.20 | 38.38 | 38.56 | 38.74 | 38.92 | 39. Io | 39.28 | 39.46 | 39.64 | 39.82 |
| -40 | -40.00 | -40.18 | -40.36 | -40.54 | -40.72 | -40.90 | -41.08 | -41.26 | -41.44 | -41.62 |
| 4 I | 41.80 | 41.98 | 42.16 | 42.34 | 42.52 | 42.70 | 42.88 | 43.06 | 43.24 | 43.42 |
| 42 | 43.60 | 43.78 | 43.96 | 44.14 | 44.32 | 44.50 | 44.68 | 44.86 | 45.04 | 45.22 |
| 43 | 45.40 | 45.58 | 45.76 | 45.94 | 46.12 | 46.30 | 46.48 | 46.66 | 46.84 | 47.02 |
| 44 | 47.20 | 47.38 | 47.56 | 47.74 | 47.92 | 48.10 | 48.28 | 48.46 | 48.64 | 48.82 |
| -45 | -49.00 | -49.18 | $-49.36$ | $-49.54$ | -49.72 | -49.90 | $-50.08$ | -50.26 | $-50.44$ | $-50.62$ |
| 46 | 50.80 | 50.98 | 51.16 | 51.34 | 51.52 | 51.70 | 51.88 | 52.06 | 52.24 | 52.42 |
| 47 | 52.60 | 52.78 | 52.96 | 53.14 | 53.32 | 53.50 | 53.68 | 53.86 | 54.04 | 54.22 |
| 48 | 54.40 | 54.58 | 54.76 | 54.94 | 55.12 | 55.30 | 55.48 | 55.66 | 55.84 | 56.02 |
| 49 | 56.20 | 56.38 | 56.56 | 56.74 | 56.92 | 57.10 | 57.28 | 57.46 | 57.64 | 57.82 |
| -50 | -58.00 | $-58.18$ | $-58.36$ | -58.54 | -58.72 | $-58.90$ | $-59.08$ | -59.26 | $\underline{-59.44}$ | -59.62 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

table 4.
CENTIGRADE SCALE TO FAHRENHEIT - Near the Boiling Point.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $100^{\circ}$ | $\begin{gathered} \text { F. } \\ 212.00 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212 . \\ \hline \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.36 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.54 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 2 \mathrm{I} 2 \cdot \mathrm{P}_{2} \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.90 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 213.08 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 213.26 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 213.44 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 213.62 \end{gathered}$ |
| 99 | 210.20 | 210.38 | 210.56 | 210.74 | 210.92 | 211.10 | 211.28 | 211.46 | 211.64 | 211.82 |
| 98 | 208.40 | 208.58 | 208.76 | 208.94 | 209.12 | 209.30 | 209.48 | 209.66 | 209.84 | 210.02 |
| 97 | 206.60 | 206.78 | 206.96 | 207.14 | 207.32 | 207.50 | 207.68 | 207.86 | 208.04 | 208.22 |
| 96 | 204.80 | 204.98 | 205.16 | 205.34 | 205.52 | 205.70 | 205.88 | 206.06 | 206.24 | 206.42 |
| 95 | 203.00 | 203.18 | 203.36 | 203.54 | 203.72 | 203.90 | 204.08 | 204.26 | 204.44 | 204.62 |
| 94 | 201.20 | 201.38 | 201.56 | 201.74 | 201.92 | 202.10 | 202.28 | 202.46 | 202.64 | 202.82 |
| 93 | 199.40 | 199.58 | 199.76 | 199.94 | 200.12 | 200.30 | 200.48 | 200.66 | 200.84 | 201.02 |
| 92 | 197.60 | 197.78 | 197.96 | 198.14 | 198.32 | 198.50 | 198.68 | 198.86 | 199.04 | 199.22 |
| 91 | 195.80 | 195.98 | 196.16 | 196.34 | 196.52 | 196.70 | 196.88 | 197.06 | 197.24 | 197.42 |
| 90 | 194.00 | 194.18 | 194.36 | 194.54 | 194.72 | 194.90 | 195.08 | 195.26 | 195.44 | 195.62 |

TABLE 5.
DIFFERENCES FAHRENHEIT TO DIFFERENCES CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | c. | c. | c. | c. | c. | c. | c. | c. | c. |
| $0^{\circ}$ | 0.00 | 0.06 | 0.11 | -.17 | 0.22 | 0.28 | 0.33 | 0. 39 | 0.44 | 0.50 |
| 1 | 0.56 | 0.61 | 0.67 | 0.72 | 0.78 | 0.83 | 0.89 | 0.94 | 1.00 | 1.06 |
| 2 | I.II | I. 17 | 1.22 | 1.28 | 1.33 | 1.39 | I. 44 | I. 50 | 1.56 | 1.61 |
| 3 | 1.67 | 1.72 | 1.78 | 1.83 | 1.89 | 1.94 | 2.00 | 2.06 | 2.11 | 2.17 |
| 4 | 2.22 | 2.28 | 2.33 | 2.39 | 2.44 | 2.50 | 2.56 | 2.61 | 2.67 | 2.72 |
| 5 | 2.78 | 2.83 | 2.89 | 2.94 | 3.00 | 3.06 | 3.11 | 3.17 | 3.22 | 3.28 |
| 6 | 3.33 | $3 \cdot 39$ | 3.44 | 3.50 | 3.56 | 3.6I | 3.67 | 3.72 | 3.78 | 3.83 |
| 7 | 3.89 | 3.94 | 4.00 | 4.06 | 4.11 | 4.17 | 4.22 | 4.28 | 4.33 | 4.39 |
| 8 | 4.44 | 4.50 | 4.56 | 4.61 | 4.67 | 4.72 | 4.78 | 4.83 | 4.89 | 4.94 |
| 9 | 5.00 | 5.06 | 5.11 | 5.17 | 5.22 | 5.28 | $5 \cdot 33$ | 5.39 | 5.44 | 5.50 |
| 10 | 5.56 | 5.61 | 5.67 | 5.72 | 5.78 | 5.83 | 5.89 | 5.94 | 6.00 | 6.06 |
| II | 6.11 | 6.17 | 6.22 | 6.28 | 6.33 | 6.39 | 6.44 | 6.50 | 6.56 | 6.61 |
| 12 | 6.67 | 6.72 | 6.78 | 6.83 | 6.89 | 6.94 | 7.00 | 7.06 | 7.11 | 7.17 |
| 13 | 7.22 | 7.28 | 7.33 | 7.39 | 7.44 | 7.50 | 7.56 | 7.6I | 7.67 | 7.72 |
| 14 | 7.78 | 7.83 | 7.89 | $7 \cdot 94$ | 8.00 | 8.06 | 8.11 | 8.17 | 8.22 | 8.28 |
| 15 | 8.33 | 8.39 | 8.44 | 8.50 | 8.56 | 8.61 | 8.67 | 8.72 | 8.78 | 8.83 |
| 16 | 8.89 | 8.94 | 9.00 | 9.06 | 9.11 | 9.17 | 9.22 | 9.28 | 9.33 | 9.39 |
| 17 | 9.44 | 9.50 | 9.56 | 9.61 | 9.67 | 9.72 | 9.78 | 9.83 | 9.89 | 9.94 |
| 18 | 10.00 | 10.06 | 10.11 | 10.17 | 10.22 | 10. 28 | 10.33 | 10.39 | 10.44 | 10.50 |
| 19 | 10.56 | 10.61 | 10.67 | 10.72 | 10.78 | 10.83 | 10.89 | 10.94 | I 1.00 | 11.06 |
| 20 | II.II | 11.17 | II. 22 | II. 28 | II. 33 | II. 39 | II. 44 | 11.50 | I 1.56 | II.6I |

TABLE 6.
DIFFERENCES CENTIGRADE TO DIFFERENCES FAHRENHEIT.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | $\begin{gathered} \text { F. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.18 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.36 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.54 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.72 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.90 \end{gathered}$ | $\begin{aligned} & \text { F. } \\ & \text { I. } 08 \end{aligned}$ | $\begin{gathered} \text { F. } \\ \text { I. } 26 \end{gathered}$ | $\begin{gathered} \text { F. } \\ \text { r. } 44 \end{gathered}$ | $\begin{gathered} \text { F. } \\ \text { I: } 62 \end{gathered}$ |
| 0 | 1.80 | 1.98 | 2.16 | 2.34 | 2.52 | 2.70 | 2.88 | 3.06 | 3.24 | 3.42 |
| 2 | 3.60 | 3.78 | 3.96 | 4. 14 | 4.32 | 4.50 | 4.68 | 4.86 | 5.04 | 5.22 |
| 3 | 5.40 | 5.58 | 5.76 | 5.94 | 6.12 | 6.30 | 6.48 | 6.66 | 6.84 | 7.02 |
| 4 | 7.20 | 7.38 | 7.56 | 7.74 | 7.92 | 8.10 | 8.28 | 8.46 | 8.64 | 8.82 |
| 5 | 9.00 | 9.18 | 9.36 | 9.54 | 9.72 | 9.90 | 10.08 | 10.26 | 10.44 | 10.62 |
| 6 | 10.80 | 10.98 | II. 16 | III. 34 | 11.52 | 11.70 | I 1.88 | 12.06 | 12.24 | 12.42 |
| 7 | 12.60 | 12.78 | 12.96 | 13.14 | 13.32 | 13.50 | 13.68 | 13.86 | 14.04 | 14.22 |
| 8 | 14.40 | 14.58 | 14.76 | 14.94 | 15.12 | 15.30 | 15.48 | ${ }^{1} 5.66$ | 15.84 | 16.02 |
| 9 | 16.20 | 16.38 | 16.56 | 16.74 | 16.92 | 17.10 | 17.28 | 17.46 | 17.64 | 17.82 |

Smithbonian Tables.

## REDUCTION OF TEMPERATURE TO SEA LEVEL. ENGLISH MEASURES.



Table 8.
REDUCTION OF TEMPERATURE TO SEA LEVEL. METRIC MEASURES.

| Rate of decrea temperature. $1^{\circ} \mathrm{C}$. forevery | DIFFERENCES BETWEEN THE TEMPERATURE AT ANY ALTITUDEAND AT SEA LEVFL. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ALTITUDE IN METRES. |  |  |  |  |  |  |  |  |  |  |  |
|  | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 | 2000 | 3000 |
| $\begin{array}{r} \mathrm{m} . \\ 100 \end{array}$ | $\begin{gathered} \text { c. } \\ \text { r.oo } \end{gathered}$ | $\begin{gathered} \text { c. } \\ 2.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 3.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ \text { 4.00 } \end{gathered}$ | $\begin{gathered} \text { c. } \\ 5.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 6.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 7.09 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 8.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 9.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ \text { 10.00 } \end{gathered}$ | $\begin{gathered} \text { c. } \\ 20.00 \end{gathered}$ | c. $0.00$ |
| 102 | 0.98 | 1.96 | 2.94 | 3.92 | 4.90 | 5.88 | 6.86 | 7.84 | 8.82 | 9.80 | 19.61 | 29.41 |
| 104 | 0.96 | 1.92 | 2.88 | 3.85 | 4.81 | 5.77 | 6.73 | 7.69 | 8.65 | 9.62 | 19.23 | 28.85 |
| 106 | 0.94 | 1.89 | 2.83 | 3.77 | 4.72 | 5.66 | 6.60 | 7.55 | 8.49 | 9.43 | 18.87 | 28.30 |
| 108 | 0.93 | 1.85 | 2.78 | 3.70 | 4.63 | 5.56 | 6.48 | 7.41 | 8.33 | 9.26 | 18.52 | 27.78 |
| 110 | 0.91 | 1.82 | 2.73 | 3.64 | 4.55 | 5.45 | 6.36 | 7.27 | 8.18 | 9.09 | 18. 18 | 27.27 |
| 115 | 0.87 | 1.74 | 2.61 | 3.48 | 4.35 | 5.22 | 6.09 | 6.96 | 7.83 | 8.70 | 17.39 | 26.09 |
| 120 | 0.83 | 1.67 | 2.50 | 3.33 | 4.17 | 5.00 | 5.83 | 6.67 | 7.50 | 8.33 | 16.67 | 25.00 |
| 125 | 0.80 | 1.60 | 2.40 | 3.20 | 4.00 | 4.80 | 5.60 | 6.40 | 7.20 | 8.00 | 16.00 | 24.00 |
| 130 | 0.77 | 1.54 | 2.31 | 3.08 | 3.85 | 4.62 | $5 \cdot 38$ | 6.15 | 6.92 | 7.69 | 15.38 | 23.08 |
| 135 | 0.74 | 1. 48 | 2.22 | 2.96 | 3.70 | 4.44 | 5.19 | 5.93 | 6.66 | 7.41 | 14.81 | 22.22 |
| 140 | 0.71 | 1.43 | 2.14 | 2.86 | 3.57 | 4.29 | 5.00 | 5.71 | 6.43 | 7.14 | 14.29 | 21.43 |
| 145 | 0.69 | 1. 38 | 2.07 | 2.76 | 3.45 | 4.14 | 4.83 | 5.52 | 6.21 | 6.90 | 13.79 | 20.69 |
| 150 | 0.67 | 1.33 | 2.00 | 2.67 | 3.33 | 4.00 | 4.67 | 5.33 | 6.00 | 6.67 | 13.33 | 20.00 |
| 155 | 0.65 | 1.29 | 1.94 | 2.58 | 3.23 | 3.87 | 4.52 | 5.16 | 5.8I | 6.45 | 12.90 | 19.35 |
| 160 | 0.62 | 1.25 | 1.87 | 2.50 | 3.12 | 3.75 | $4 \cdot 37$ | 5.00 | 5.62 | 6.25 | 12.50 | 18.75 |
| 170 | 0.59 | I. 18 | 1.76 | 2.35 | 2.94 | 3.53 | 4.12 | 4.70 | 5.29 | 5.88 | 11.76 | 17.65 |
| 180 | 0.56 | I. 11 | 1.67 | 2.22 | 2.78 | 3.33 | 3.89 | 4.44 | 5.00 | 5.56 | II.II | 16.67 |
| 190 | 0.53 | 1.05 | 1.58 | 2.10 | 2.63 | 3.16 | 3.68 | 4.21 | 4.74 | 5.26 | 10.53 | 15.79 |
| 200 | 0.50 | 1.00 | 1.50 | 2.00 | 2.50 | 3.00 | 3.50 | 4.00 | 4.50 | 5.00 | 10.00 | 15.00 |
| 210 | 0.4 | 0.95 | 1.43 | 1.90 | 2.38 | 2.86 | 3.33 | 3.81 | 4.29 | 4.76 | 9.52 | 14.29 |
| 220 | 0.45 | 0.91 | 1. 36 | 1.82 | 2.27 | 2.73 | 3.18 | 3.64 | 4.09 | 4.55 | 9.09 | 13.64 |
| 230 | 0.43 | 0.87 | 1.30 | 1.74 | 2.17 | 2.61 | 3.04 | 3.48 | 3.91 | $4 \cdot 35$ | 8.70 | 13.04 |
| 240 | 0.42 | 0.83 | 1.25 | 1.67 | 2.08 | 2.50 | 2.92 | 3.33 | 3.75 | 4.17 | 8.33 | 12.50 |
| 250 | 0.40 | 0.80 | 1.20 | 1.60 | 2.00 | 2.40 | 2.80 | 3.20 | 3.60 | 4.00 | 8.00 | 12.00 |
| 260 | 0.38 | 0.77 | I. 15 | 1.54 | 1.92 | 2.31 | 2.69 | 3.08 | 3.46 | 3.85 | 7.69 | Ir. 54 |
| 270 | 0.37 | 0.74 | I.II | 1.48 | 1.85 | 2.22 | 2.59 | 2.96 | 3.33 | 3.70 | 7.41 | II.II |
| 280 | 0.36 | 0.71 | 1.07 | 1.43 | 1.79 | 2.14 | 2.50 | 2.86 | 3.21 | 3.57 | 7.14 | 10.71 |
| 290 | 0.34 | 0.69 | 1.03 | 1.38 | 1.72 | 2.07 | 2.41 | 2.76 | 3.10 | 3.45 | 6.90 | 10.34 |
| 300 | 0.33 | 0.67 | 1.00 | 1.33 | 1.67 | 2.00 | 2.33 | 2.67 | 3.00 | 3.33 | 6.67 | 10.00 |
| 320 | 0.31 | 0.62 | 0.94 | 1.25 | 1.56 | 1.87 | 2.19 | 2.50 | 2.81 | 3.12 | 6.25 | 9.37 |
| 340 | 0.29 | 0.59 | 0.88 | 1,18 | 1.47 | 1.76 | 2.06 | 2.35 | 2.65 | 2.94 | 5.88 | 8.82 |
| 360 | 0.28 | 0.56 | 0.83 | I.II | 1.39 | 1.67 | r. 94 | 2.22 | 2.50 | 2.78 | 5.56 | 8.33 |
| 380 | 0.26 | 0.53 | 0.79 | 1.05 | 1.32 | 1.58 | 1.84 | 2.10 | 2.37 | 2.63 | 5.26 | 7.89 |
| 400 | 0.25 | 0.50 | 0.75 | 1.00 | I. 25 | 1.50 | 1. 75 | 2.00 | 2.25 | 2.50 | 5.00 | 7.50 |
| 420 | 0.24 | 0.48 | 0.71 | 0.95 | I. 19 | 1. 43 | 土. 67 | 1.90 | 2.14 | 2.38 | 4.76 | 7.14 |
| 440 | 0.23 | 0.45 | 0.68 | 0.91 | 1.14 | 1.36 | 1.59 | 1.82 | 2.05 | 2.27 | 4.55 | 6.82 |
| 460 | 0.22 | 0.43 | 0.65 | 0.87 | 1.09 | 1.30 | 1.52 | 1.74 | 1.96 | 2.17 | 4.35 | 6.52 |
| 480 | 0.21 | 0.42 | 0.62 | 0.83 | 1.04 | 1.25 | 1.46 | 1.67 | r. 87 | 2.08 | 4.17 | 6.25 |
| 500 | 0.20 | 0.40 | 0.60 | 0.80 | 1.00 | I. 20 | 1. 40 | 1.60 | r.80 | 2.00 | 4.00 | 6.00 |

Tabular values are to be added to the observed temperature to obtain the temperature at sea level.

Smitheonian Tables.

TABLE 9.
CORRECTION FOR THE TEMPERATURE OF THE MERCURY IN THE THERMOMETER STEM.
$T=t-0.0000795 n\left(t^{\prime}-t\right)-$ Fahrenheit temperatures.
$T=t-0.000143 n\left(t^{\prime}-t\right)$ - Centigrade temperatures.
$T=$ Corrected temperature.
$t=$ Observed temperature.
$t^{\prime}=$ Mean temperature of the glass stem and mercury column.
$n=$ Length of mercury in the stem in scale degrees.

Correction for Fahrenheit Thermometers.
Values of $0.0000795 n\left(t^{\prime}-t\right)$

| $n$ | $t^{\prime}-t$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ | $90^{\circ}$ | $100^{\circ}$ |
| F. | F. | F. | F. | F. | F. | F. | F. | F. | F. | F. |
| $10^{\circ}$ | O.OI | 0.02 | 0.02 | 0.03 | 0.04 | 0.05 | 0.06 | 0.06 | 0.07 | 0.08 |
| 20 | 0.02 | 0.03 | 0.05 | 0.06 | 0.08 | 0. 10 | 0. 11 | o. 13 | o. 14 | 0. 16 |
| 30 | 0.02 | 0.05 | 0.07 | 0. 10 | 0.12 | 0.14 | 0. 17 | o. 19 | 0.21 | 0. 24 |
| 40 | 0.03 | 0.06 | O.IO | 0. 13 | 0.16 | 0. 19 | 0.22 | 0.25 | 0.29 | 0.32 |
| 50 | 0.04 | 0.08 | 0.12 | 0.16 | 0.20 | 0.24 | 0.28 | 0.32 | 0.36 | 0.40 |
| 60 | 0.05 | 0.10 | 0. 14 | 0.19 | 0.24 | 0.29 | 0.33 | 0.38 | 0.43 | 0.48 |
| 70 | 0.06 | O. 11 | o. 17 | 0.22 | 0.28 | 0.33 | 0.39 | 0.45 | 0.50 | 0. 56 |
| 80 | 0.06 | 0.13 | o. 19 | 0.25 | 0.32 | 0.38 | 0.45 | 0.51 | 0.57 | 0.64 |
| 90 | 0.07 | 0. 14 | 0.21 | 0.29 | 0.36 | 0.43 | 0.50 | 0.57 | 0.64 | 0.72 |
| 100 | 0.08 | 0.16 | 0.24 | 0.32 | 0.40 | 0.48 | 0.56 | 0.64 | 0.72 | 0.79 |
| 110 | 0.09 | O. 17 | 0.26 | 0.35 | 0.44 | 0.52 | 0.61 | 0.70 |  | 0.87 |
| 120 | 0.10 | 0.19 | 0.29 | o. 38 | 0.48 | 0.57 | 0.67 | 0.76 | 0.86 | 0.95 |
| 130 | 0. 10 | 0.21 | 0.31 | 0.41 | 0.52 | 0.62 | 0.72 | 0.83 | 0.93 | 1.03 |

Correction for Centigrade Thermometers.
Values of o.000I43 $n\left(t^{\prime}-t\right)$

| $n$ | $t^{\prime}-t$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ |
| $10^{c}$ | c. o. 1.1 | C. 0.03 | C. | c. 0.06 | c. O옥 | c. $0.09$ | c. | C. |
| 20 | 0.03 | 0.06 | 0.09 | 0.11 | O. 14 | 0. 17 | 0.20 | 0.23 |
| 30 | 0.04 | 0.09 | 0. 13 | 0.17 | 0.21 | 0.26 | 0.30 | 0.34 |
| 40 | 0.06 | O. 11 | 0. 17 | 0.23 | 0.29 | 0.34 | 0.40 | 0.46 |
| 50 | 0.07 | 0. 14 | 0.21 | 0.29 | 0.36 | 0.43 | 0.50 | 0.57 |
| 60 | 0.09 | 0.17 | 0.26 | 0.34 | 0.43 | 0.51 | 0.60 | 0.69 |
| 70 | 0. 10 | 0.20 | 0.30 | 0.40 | 0.50 | 0.60 | 0.70 | 0.80 |
| 80 | O. 11 | 0.23 | 0.34 | 0.46 | 0.57 | 0.69 | 0.80 | 0.92 |
| 90 | 0.13 | 0.26 | 0.39 | 0.51 | 0.64 | 0.77 | 0.90 | 1.03 |
| 100 | o. 14 | 0.29 | 0.43 | 0.57 | 0.72 | 0.86 | 1.00 | 1.14 |

When $t^{\prime}$ is $\left\{\begin{array}{l}\text { greater } \\ \text { less }\end{array}\right\}$ than $t$ the correction is to be $\left\{\begin{array}{l}\text { subtracted } \\ \text { added }\end{array}\right\}$

## BAROMETRICAL TABLES.

Reduction of the barometer to standard temperature - English measures Table 10
Metric measures ..... II
Reduction of the barometer to standard gravity at latitude $45^{\circ}$ - English measures ..... Table 12
Metric measures ..... 13
Reduction of the barometer to sea level - English measures.Values of 2000 mTABLE 14
Correction of 2000 m for latitude ..... 15
$B_{\circ}-B=B\left(\mathrm{Io}^{m}-\mathrm{r}\right)$ ..... 16
Reduction of the barometer to sea level - Metric measures.
Values of 2000 m ..... TAble 17
Correction of 2000 m for latitude ..... 18
$B_{\circ}-B=B\left(\mathrm{r}^{m}-\mathrm{r}\right)$ ..... 19Determination of heights by the barometer - English measures.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$ Table 20
Term for temperature ..... 21
Correction for latitude and weight of mercury ..... 22
Correction for an average degree of humidity ..... 23
Correction for the variation of gravity with altitude. ..... 24
Determination of heights by the barometer - Metric measures.
Values of $18400 \log \frac{760}{B}$ ..... TAble 25
Term for temperature ..... 26
Correction for humidity ..... 27
Correction for latitude and weight of mercury ..... 28
Correction for the variation of gravity with altitude ..... 29
Difference of height corresponding to a change of 0.1 inch in the barometer - English measures Table 30
Difference of height corresponding to a change of 1 millimetre in the barometer - Metric measures ..... TABLE 3I
Determination of heights by the barometer. Formula of Babinet ..... TAble 32
Barometric pressures corresponding to the temperature of the boiling point of water -
English measures ..... 33
Metric measures ..... 34

TABLE 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther. mometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| $\begin{array}{r} F \\ 0.0 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.050 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.05 \mathrm{I} \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.052 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.053 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.055 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.056 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.057 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.059 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.060 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.06 \mathrm{I} \end{gathered}$ |
| +0.5 I. | +0.049 .048 | +0.050 .049 | +0.051 .050 | $+\begin{array}{r}+0.053 \\ .052\end{array}$ | +0.054 | +0.055 | +0.056 | +0.058 | +0.059 | +0.060 |
| 1.0 | . 048 | . 049 | .050 | .052 | . 053 | . 054 | .055 | .057 | . 058 | .059 |
| 1.5 | . 047 | . 048 | . 049 | .051 | . 052 | . 053 | . 054 | . 056 | . 057 | . 058 |
| 2.0 | . 046 | . 047 | . 049 | .050 | .05I | . 052 | . 053 | . 055 | . 056 | . 057 |
| 2.5 | . 045 | . 046 | . 048 | . 049 | . 050 | .05I | .052 | . 054 | . 055 | . 056 |
| 3.0 | +0.044 | +0.046 | +0.047 | +0.048 | +0.049 | +0.050 | +0.051 | +0.053 | +0.054 | +0.055 |
| 3.5 | . 043 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | .05I | . 053 | . 054 |
| 4.0 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | . 052 | . 053 |
| 4.5 | . 042 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 051 | . 052 |
| 5.0 | .04I | . 042 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 051 |
| 5.5 | +0.040 | +0.04I | +0.042 | +0.043 | +0.044 | +0.045 | +0.046 | +0.047 | +0.048 | +0.049 |
| 6.0 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 |
| 6.5 | . 038 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | . 045 | . 046 | . 047 |
| 7.0 | . 037 | . 038 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | . 045 | . 046 |
| $7 \cdot 5$ | . 037 | . 038 | .038 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | . 045 |
| 8.0 | +0.036 | +0.037 | +0.038 | +0.038 | +0.039 | +0.040 | +0.04I | +0.042 | +0.043 | +0.044 |
| 8.5 | . 035 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 | .04I | . 042 | . 043 |
| 9.0 | . 034 | . 035 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 | .04I | . 042 |
| 9.5 | . 033 | . 034 | . 035 | . 036 | . 037 | . 037 | . 038 | . 039 | . 040 | . 041 |
| 10.0 | .032 | . 033 | . 034 | . 035 | . 036 | . 036 | . 037 | . 038 | . 039 | . 040 |
| 10.5 | +0.031 | +0.032 | +0.033 | +0.034 | +0.035 | +0.035 | +0.036 | +0.037 | $+0.038$ | +0.039 |
| 11.0 | . 030 | . 03 I | . 032 | . 033 | . 034 | . 034 | . 035 | . 036 | . 037 | . 338 |
| 11.5 | . 030 | . 030 | . 031 | . 032 | . 033 | . 034 | . 034 | . 035 | . 036 | . 037 |
| 12.0 | . 029 | . 030 | . 030 | .03I | . 032 | . 033 | . 033 | . 034 | . 035 | . 036 |
| 12.5 | . 028 | . 029 | . 029 | . 030 | . 03 I | . 032 | . 032 | . 033 | . 034 | . 034 |
| 13.0 | +0.027 | +0.028 | +0.028 | +0.029 | +0.030 | +0.03I | +0.031 | +0.032 | +0.033 | +0.033 |
| 13.5 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 | . 030 | . 031 | . 032 | . 032 |
| 14.0 | . 025 | . 026 | . 027 | . 027 | . 028 | . 029 | . 029 | . 030 | . 31 | . 31 |
| 14.5 | . 024 | . 025 | . 026 | . 026 | . 027 | . 028 | . 028 | . 029 | . 330 | . 030 |
| 15.0 | . 024 | . 024 | . 025 | . 025 | . 026 | . 027 | . 027 | . 028 | . 029 | . 029 |
| 15.5 | +0.023 | +0.023 | +0.024 | +0.024 | +0.025 | +0.026 | +0.026 | +0.027 | +0.027 | +0.028 |
| 16.0 | . 022 | . 023 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 | . 026 | . 027 |
| 16.5 | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 |
| 17.0 | . 020 | .021 | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 | . 024 | . 025 |
| 17.5 | . 019 | . 020 | . 020 | . 02 I | .02I | . 022 | . 022 | . 023 | . 023 | . 024 |
| 18.0 | +0.018 | +0.019 | +0.019 | $+0.020$ | +0.020 | +0.02I | +0.021 | +0.022 | +0.022 | +0.023 |
| 18.5 | . 017 | . 018 | . 018 | . 019 | . 019 | . 020 | . 020 | . 02 I | . 02 I | . 022 |
| 19.0 | . 017 | . 017 | . 018 | . 018 | . 018 | . 019 | . 019 | . 020 | . 020 | . $\mathrm{O2I}$ |
| 19.5 | .O16 | . 016 | . 017 | . 017 | . 017 | . 018 | . 018 | . 019 | . 019 | .02C |
| 20.0 | . 015 | . 015 | . 016 | . 016 | . 016 | . 017 | . 017 | .or8 | . 018 | . 018 |
| 20.5 | +0.014 | +0.014 | +0.015 | +0.015 | +0.016 | +0.016 | +0.016 | +0.017 | +0.017 | +0.017 |
| 21.0 | . 013 | . 014 | . 014 | . 014 | . O 5 | . 015 | . 015 | . 016 | . 016 | . 016 |
| 21.5 | .OI2 | .or3 | . 013 | . 013 | . 014 | . 014 | .OI4 | . OI 5 | . 015 | . OI 5 |
| 22.0 | . OII | . 012 | . 012 | . 012 | . OI 3 | .OI3 | .OI3 | .OI4 | . OI 4 | .OI4 |
| 22.5 | .OII | .OII | . OrI | .OII | . OI 2 | . 012 | . OI 2 | . OI3 | . OI 3 | . OI 3 |
| 23.0 | +0.010 | +0.010 | +0.010 | +o.010 | +0.011 | +0.011 | +o.011 | +0.012 | +0.012 | +0.012 |
| 23.5 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 | . 010 | . OII | . OII | . OI |
| 24.0 | . 008 | . 008 | . 008 | . 009 | . 009 | . 009 | . 009 | .OIO | . 010 | . 010 |
| 24.5 | . 007 | . 007 | . 008 | . 008 | . 008 | . 008 | . 008 | . 009 | . 009 | . 009 |
| 25.0 | . 006 | .006 | . 007 | . 007 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 |

table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| $\begin{array}{r} \text { F. } \\ 25^{\circ} .5 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.005 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +\mathbf{o . 0 0 7} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ |
| 26.0 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 006 |
| 26.5 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 005 |
| 27.0 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | .003 | . 003 | . 003 | . 003 |
| 27.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 28.0 | +0.001 | +0.001 | +0.001 | +0.001 | +0.00I | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | 0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 002 | . 002 | . 002 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 30.5 | 0.003 | -0.003 | -0.003 | -0.003 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 |
| 31.0 | . 004 | . 004 | . 004 | . 004 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 31.5 | . 005 | . 005 | . 005 | . 005 | . 005 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 32.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 32.5 | . 007 | . 007 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 008 | . 008 |
| 33.0 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.009 | -0.009 | -0.009 | -0.009 | -0.009 |
| 33.5 | . 008 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | .010 | . 010 | . 010 |
| 34.0 | . 009 | . 010 | . 010 | . 010 | . 010 | . 010 | . OI I | . OII | . OII | . OII |
| 34.5 | . 010 | . 010 | .OII | .OII | . 011 | . OII | . 012 | . OI 2 | . OI 2 | . 013 |
| 35.0 | . 011 | . 011 | . OI 2 | . 012 | . 012 | . 012 | . 013 | . 013 | . 013 | . 014 |
| 35.5 | -0.012 | -0.012 | -0.012 | -0.013 | -0.013 | -0.013 | -0.014 | -0.014 | -0.014 | -0.015 |
| - 36.0 | . 013 | . 013 | .OI3 | . 014 | . 014 | . O 4 | . 015 | .or5 | . 015 | . 016 |
| 36.5 | . 014 | . 014 | . 014 | . 015 | . 015 | . OI 5 | . 016 | . 016 | . 016 | . 017 |
| 37.0 | . 014 | . 015 | . 015 | . 016 | . 016 | . 016 | . 017 | . 017 | .OI7 | . 018 |
| 37.5 | . 015 | . 016 | . 016 | . 017 | . 017 | . 017 | . 018 | . 018 | . 019 | . 019 |
| 38.0 | -0.016 | -0.017 | -0.017 | -0.017 | -0.018 | -0.018 | -0.019 | -0.019 | -0.020 | -0.020 |
| 38.5 | . 017 | . 017 | . 018 | . 018 | .OI9 | . 019 | . 020 | . 020 | . 02 I | . 021 |
| 39.0 | . 018 | . 018 | .OI9 | .O19 | . 020 | . 020 | . 021 | .02I | . 022 | . 022 |
| 39.5 | . 019 | .019 | . 020 | . 020 | .02I | . 02 I | . 022 | . 022 | . 023 | . 023 |
| 40.0 | . 020 | . 020 | . 021 | . 02 I | . 022 | . 022 | . 023 | . 023 | . 024 | . 024 |
| 40.5 | 0.020 | -0.02I | -0.022 | -0.022 | -0.023 | -0.023 | -0.024 | -0.024 | -0.025 | -0.025 |
| 41.0 | . 021 | . 02 | . 0 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 | . 026 |
| 41.5 | . 022 | . 023 | . 023 | . 024 | . 025 | . 025 | . 026 | . 026 | . 027 | . 027 |
| 42.0 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 | . 027 | . 027 | . 028 | . 029 |
| 42.5 | . 024 | . 025 | . 025 | . 026 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 |
| 43.0 | -0.025 | -0.025 | -0.026 | -0.027 | -0.027 | -0.028 | -0.029 | -0.029 | -0.030 | -0.03I |
| 43.5 | . 026 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 | . 030 | . 031 | . 032 |
| 44.0 | . 026 | . 027 | . 028 | . 029 | . 029 | . 030 | . 031 | . 031 | . 032 | . 033 |
| 44.5 | . 027 | . 028 | . 029 | . 030 | . 030 | . 031 | . 032 | . 032 | . 033 | . 034 |
| 45.0 | . 028 | . 029 | . 030 | . 030 | . 031 | . 032 | . 033 | . 033 | . 034 | . 035 |
| 45.5 | -0.029 | -0.030 | -0.031 | -0.031 | -0.032 | -0.033 | -0.034 | -0.034 | -0.035 | -0.036 |
| 46.0 | . 030 | .03I | . 031 | . 032 | . 033 | . 034 | . 035 | . 035 | . 036 | . 037 |
| 46.5 | . 031 | . 032 | . 032 | . 033 | . 034 | . 035 | . 036 | . 036 | . 037 | . 038 |
| 47.0 | . 032 | .032 | . 033 | . 034 | . 035 | . 036 | . 037 | . 037 | . 038 | . 039 |
| 47.5 | . 033 | . 033 | . 034 | . 035 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 |
| 48.0 | -0.033 | -0.034 | -0.035 | -0.036 | -0.037 | -0.038 | -0.039 | -0.040 | -0.040 | -0.04I |
| 48.5 | . 034 | . 035 | . 036 | . 037 | . 038 | . 039 | . 040 | .04I | .04I | . 042 |
| 49.0 | . 035 | . 036 | . 037 | . 038 | . 039 | . 040 | .041 | . 042 | . 042 | . 043 |
| 49.5 | . 036 | . 037 | . 038 | . 039 | . 040 | . 041 | . 042 | . 043 | . 044 | . 044 |
| 50.0 | . 037 | . 038 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | 0.45 | . 046 |

Smithsonian Tables.

T'able 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE,
ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |  | Inch. | Inch. | Inch. |
| 50.5 | -0.038 | -0.039 | -0.040 | -0.04I | $-0.042$ | $-0.043$ | -0.044 | -0.045 | $-0.046$ | 0.047 |
| 51.0 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | . 045 | . 046 | 0.47 | . 048 |
| 51.5 | . 039 | . 040 | .04I | . 042 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 |
| 52.0 | . 040 | . 041 | . 042 | . 043 | . 044 | . 046 | . 047 | . 048 | . 049 | . 050 |
| 52.5 | . 041 | . 042 | . 043 | . 044 | . 045 | . 047 | . 048 | . 049 | . 050 | .051 |
| 53.0 | -0.042 | -0.043 | -0.044 | -0.045 | -0.046 | -0.047 | -0.049 | -0.050 | -0.05I | -0.052 |
| 53.5 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 | . 050 | .051 | . 052 | . 053 |
| 54.0 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | .051 | .052 | . 053 | . 054 |
| 54.5 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | . 052 | . 053 | . 054 | . 055 |
| 55.0 | . 045 | . 047 | . 048 | . 049 | . 050 | .05I | . 053 | . 054 | . 055 | . 056 |
| 55.5 | -0.046 | -0.047 | -0.049 | -0.050 | -0.05I | -0.052 | -0.054 | -0.055 | -0.056 | -0.057 |
| 56.0 | . 047 | . 048 | . 050 | .05I | . 052 | . 053 | . 055 | . 056 | . 057 | . 058 |
| 56.5 | . 048 | . 049 | . 050 | . 052 | . 053 | . 054 | . 056 | . 057 | . 058 | . 059 |
| 57.0 | . 049 | . 050 | .05I | . 053 | . 054 | . 055 | .057 | . 058 | . 059 | . 060 |
| 57.5 | . 050 | .05I | . 052 | . 054 | . 055 | . 056 | . 058 | . 059 | . 060 | .06I |
| 58.0 | -0.051 | -0.052 | -0.053 | -0.055 | -0.056 | -0.057 | -0.059 | -0.060 | -0.06I | -0.063 |
| 58.5 | . 051 | . 053 | . 054 | . 055 | . 057 | . 058 | . 060 | . 061 | . 062 | . 064 |
| 59.0 | . 052 | . 054 | . 055 | . 056 | . 058 | . 059 | . 061 | . 062 | . 063 | . 065 |
| 59.5 | . 053 | . 055 | . 056 | . 057 | . 059 | .060 | .06I | . 063 | . 064 | . 066 |
| 60.0 | . 054 | . 055 | . 057 | . 058 | . 060 | .06I | . 062 | . 064 | . 065 | . 067 |
| 60.5 | -0.055 | -0.056 | -0.058 | -0.059 | -0.061 | -0.062 | -0.063 | -0.065 | -0.066 | -0.068 |
| 6 I .0 | . 056 | . 057 | . 059 | . 060 | . 062 | . 063 | . 064 | . 066 | . 067 | . 069 |
| 61.5 | . 057 | . 058 | . 060 | .061 | . 062 | . 064 | . 065 | . 067 | . 068 | . 070 |
| 62.0 | . 057 | . 059 | . 060 | . 062 | . 063 | . 065 | . 066 | . 068 | . 069 | .071 |
| 62.5 | . 058 | . 060 | .061 | . 063 | . 064 | . 066 | . 067 | . 069 | . 07 I | . 072 |
| 63.0 | -0.059 | -0.06I | -0.062 | -0.064 | -0.065 | -0.067 | -0.068 | -0.070 | -0.072 | -0.073 |
| 63.5 | . 060 | . 062 | . 063 | . 065 | . 066 | 0.68 | . 069 | . 071 | . 073 | . 074 |
| 64.0 | .06I | . 062 | . 064 | . 066 | . 067 | . 069 | . 070 | . 072 | . 074 | . 075 |
| 64.5 | . 062 | . 063 | . 065 | . 067 | . 068 | . 070 | . 071 | . 073 | . 075 | . 076 |
| 65.0 | . 063 | . 064 | . 066 | . 067 | . 069 | . 071 | . 072 | . 074 | . 076 | . 077 |
| 65.5 | $-0.063$ | -0.065 | -0.067 | -0.068 | -0.070 | -0.072 | -0.073 | -0.075 | -0.077 | -0.078 |
| 66.0 | . 064 | . 066 | . 068 | . 069 | .071 | . 073 | . 074 | . 076 | . 078 | . 079 |
| 66.5 | . 065 | . 067 | . 069 | . 070 | . 072 | . 074 | . 075 | . 077 | . 079 | .08I |
| 67.0 | . 066 | . 068 | . 069 | . 071 | . 073 | . 075 | . 076 | . 078 | .080 | . 082 |
| 67.5 | . 067 | . 069 | . 070 | . 072 | . 074 | . 076 | . 077 | . 079 | .08I | . 083 |
| 68.0 | -0.068 | -0.069 | -0.071 | -0.073 | -0.075 | -0.077 | -0.078 | -0.08o | -0.082 | -0.084 |
| 68.5 | . 069 | . 070 | . 072 | . 074 | . 076 | .078 | . 079 | .08I | . 083 | . 085 |
| 69.0 | . 069 | . 071 | . 073 | . 075 | . 077 | . 079 | .080 | . 082 | . 084 | . 086 |
| 69.5 | . 070 | . 072 | . 074 | . 076 | . 078 | . 079 | .081 | . 083 | .085 | . 087 |
| 70.0 | . 07 I | . 073 | . 075 | . 077 | . 079 | . 080 | . 082 | . 084 | . 086 | . 088 |
| 70.5 | -0.072 | -0.074 | -0.076 | -0.078 | -0.080 | -0.08I | $-0.083$ | -0.085 | -0.087 | -0.089 |
| 71.0 | . 073 | . 075 | . 077 | . 079 | . 080 | . 082 | . 084 | . 086 | . 088 | . 090 |
| 71.5 | . 074 | . 076 | . 078 | . 079 | .08I | .083 | .085 | . 087 | . 089 | .091 |
| 72.0 72.5 | . 075 | . 076 | . 078 | .080 | . 082 | . 088 | . 086 | . 088 | . 090 | . 092 |
| 72.5 | . 075 | . 077 | . 079 | .08I | . 083 | . 085 | . 087 | . 089 | .09I | . 093 |
| 73.0 | -0.076 | -0.078 | -0.080 | -0.082 | -0.084 | -0.086 | -0.088 | -0.090 | -0.092 | -0.094 |
| 73.5 | . 077 | . 079 | .08I | . 083 | . 085 | . 087 | . 089 | .091 | . 093 | . 095 |
| 74.0 | . 078 | .080 | . 082 | . 084 | . 086 | . 088 | . 090 | . 092 | . 094 | . 096 |
| 74.5 | . 079 | .08I | . 083 | . 085 | . 087 | . 089 | .091 | . 093 | . 095 | . 097 |
| 75.0 | . 080 | . 082 | . 084 | . 086 | . 088 | . 090 | . 092 | . 094 | . 096 | . 099 |

table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| F. | Inch. | Inch. | Inch | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch |
| 75.5 | -0.08I | -0.083 | -0.085 | -0.087 | -0.089 | -0.091 | -0.093 | -0.095 | -0.097 | -0.100 |
| 76.0 | .08I | . 084 | . 086 | . 088 | . 090 | . 092 | . 094 | . 096 | . 098 | . IOI |
| 76.5 | . 082 | . 084 | .087 | .089 | .091 | . 093 | . 095 | . 097 | . 100 | . 102 |
| 77.0 | . 083 | . 085 | . 087 | . 090 | . 092 | . 094 | . 096 | . 098 | . IOI | . 103 |
| 77.5 | . 084 | . 086 | . 088 | .091 | . 093 | . 095 | . 097 | . 099 | . 102 | . 104 |
| 78.0 | -0.085 | -0.087 | -0.089 | -0.091 | -0.094 | -0.096 | -0.098 | -0.100 | -0.103 | -0.105 |
| 78.5 | . 086 | . 088 | . 090 | . 092 | . 095 | . 097 | . 099 | . 101 | . 104 | . 106 |
| 79.0 | . 086 | . 089 | .09I | . 093 | . 096 | . 098 | . 100 | . 102 | . 105 | . 107 |
| 79.5 | . 087 | . 090 | .092 | . 094 | . 097 | . 099 | . IOI | . 103 | . 106 | . 108 |
| 80.0 | . 088 | .091 | . 093 | . 095 | . 097 | . 100 | . 102 | . 104 | . 107 | . 109 |
| 80.5 | -0.089 | -0.091 | -0.094 | -0.096 | -0.098 | -0.101 | -0.103 | -0.105 | -0.108 | -0.110 |
| 81.0 | . 090 | . 092 | . 095 | . 097 | . 099 | . 102 | . 104 | . 106 | . 109 | . 111 |
| 81.5 | .09I | . 093 | . 096 | . 098 | . 100 | . 103 | . 105 | .107 | . 110 | . 112 |
| 82.0 | . 092 | . 094 | .096 | . 099 | . 101 | . 104 | . 106 | . 108 | . III | . 113 |
| 82.5 | . 092 | . 095 | . 097 | . 100 | . 102 | . 105 | . 107 | .109 | . 112 | . 114 |
| 83.0 | -0.093 | -0.096 | -0.098 | -0.101 | -0.103 | -0.106 | -0.108 | -0.111 | -0.113 | -0.115 |
| 83.5 | . 094 | . 097 | . 099 | . 102 | . 104 | . 107 | . 109 | . 112 | . 114 | . 117 |
| 84.0 | . 095 | . 098 | .100 | . 103 | . 105 | . 108 | . 110 | . 113 | . 115 | . 118 |
| 84.5 | . 096 | . 098 | . 101 | . 103 | . 106 | .108 | . III | . 114 | . 116 | . 119 |
| 85.0 | . 097 | . 099 | . 102 | . 104 | . 107 | . 109 | . 112 | . 115 | . 117 | . 120 |
| 85.5 | -0.098 | -0.100 | -0.103 | -0. 105 | -0.108 | -0.110 | -0.113 | -0.116 | -0.118 | -0.121 |
| 86.0 | . 098 | . 101 | . 104 | . 106 | . 109 | . 111 | . 114 | . 117 | . 119 | . 122 |
| 86.5 | . 099 | . 102 | . 105 | . 107 | . 110 | . 112 | . 115 | . 118 | . 120 | . 123 |
| 87.0 | . 100 | . 103 | . 105 | . 108 | . III | . II 3 | . 116 | . 119 | . 121 | . 124 |
| 87.5 | . 101 | . 104 | . 106 | . 109 | . 112 | . 114 | . 117 | . 120 | . 122 | . 125 |
| 88.0 | -0.102 | -0.105 | -0.107 | -0.110 | -0.113 | -0.115 | -0.118 | -0.12I | -0.123 | -0.126 |
| 88.5 | . 103 | . 105 | . 108 | . 111 | . 114 | . 116 | . 119 | . 122 | . 124 | . 127 |
| 89.0 | . 104 | . 106 | . 109 | . 112 | . 114 | . 117 | . 120 | . 123 | . 125 | . 128 |
| 89.5 | . 104 | . 107 | . 110 | . 113 | . 115 | . 118 | . 121 | . 124 | . 126 | . 129 |
| 90.0 | . 105 | . 108 | . 111 | . 114 | . 116 | . 119 | . 122 | . 125 | . 127 | . 130 |
| 90.5 | -0.106 | -0.109 | -0.112 | -0.114 | -0.117 | -0.120 | -0.123 | -0.126 | -0.128 | -0.131 |
| 91.0 | . 107 | . 110 | . II3 | . 115 | . 118 | . 121 | . 124 | . 127 | . 129 | . 132 |
| 91.5 | . 108 | . III | . II3 | . 116 | . 119 | . 122 | .125 | . 128 | . 131 | . 133 |
| 92.0 | .109 | . 112 | . 114 | . 117 | . 120 | . 123 | . 126 | . 129 | . 132 | . 134 |
| 92.5 | . 110 | . 112 | . 115 | . 118 | . 121 | . 124 | . 127 | . 130 | . 133 | . 135 |
| 93.0 | O. I 10 | -0.113 | -0.116 | -0.119 | -0. 122 | -0.125 | -0. 128 | -0.131 | -0.134 | -0. 137 |
| 93.5 | . III | . 114 | . 117 | . 120 | . 123 | . 126 | . 129 | . 132 | . 135 | . 138 |
| 94.0 | . 12 | . 115 | . 118 | . 121 | . 124 | . 127 | . 130 | . 133 | . 136 | . 139 |
| 94.5 | . 113 | . 116 | . 119 | . 122 | . 125 | .128 | .131 | . 134 | . 137 | . 140 |
| 95.0 | . 114 | . 117 | . 120 | .123 | . 126 | .129 | . 132 | . 135 | . 138 | .141 |
| 95.5 | -O.115 | -0.118 | -0.121 | -0.124 | -0.127 | -0.130 | -0.133 | -0.136 | -0.139 | -0.142 |
| 96.0 | . 115 | . 119 | . 122 | . 125 | . 128 | . 131 | . 134 | . 137 | . 140 | . 143 |
| 96.5 | . 116 | . 119 | . 122 | . 126 | . 129 | . 132 | . 135 | . 138 | . 141 | . 144 |
| 97.0 | . I17 | . 120 | .123 | . 126 | .130 | . 133 | . 136 | . 139 | . 142 | . 145 |
| 97.5 | . 118 | . 121 | . 124 | . 127 | . 130 | . 134 | . 137 | . 140 | . 143 | . 146 |
| 98.0 | -0.119 | O. 122 | -0.125 | -0.128 | -0.131 | -0.135 | -0.138 | -0.141 | -0.144 | -0.147 |
| 98.5 | . 120 | . 123 | . 126 | . 129 | . 132 | . 135 | . 139 | . 142 | . 145 | . 148 |
| 99.0 | . 121 | . 124 | . 127 | . 130 | . 133 | . 136 | . 140 | . 143 | . 146 | . 149 |
| 99.5 | . 121 | . 125 | . 128 | . 131 | . 134 | . 137 | .141 | .144 | . 147 | . 150 |
| 100.0 | . 122 | . 126 | . 129 | . 132 | . 135 | . 138 | . 142 | . 145 | . 148 | . 151 |

table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\begin{gathered} \text { F. } \\ 0.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.063 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.063 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.064 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.064 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.065 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.065 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.066 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.066 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.067 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.067 \end{gathered}$ |
| +0.5 | +0.06I | +0.062 | +0.063 | +0.063 | +0.064 | +0.064 | +0.065 | +0.065 | +0.066 | +0.066 |
| 1.0 | . 060 | .06I | .061 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 065 |
| 1.5 | . 059 | . 060 | . 060 | .06I | . 061 | . 062 | . 062 | . 063 | . 063 | . 064 |
| 2.0 | . 058 | . 059 | . 059 | . 060 | . 060 | .06I | .06I | . 062 | . 062 | . 063 |
| 2.5 | . 057 | .058 | . 058 | . 059 | . 059 | . 059 | . 060 | . 060 | .06I | .061 |
| 3.0 | +0.056 | +0.056 | +0.057 | +0.057 | +0.058 | +0.058 | +0.059 | +0.059 | +0.060 | +0.060 |
| 3.5 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 | . 059 | . 059 |
| 4.0 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 |
| 4.5 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 057 |
| 5.0 | . 052 | .052 | . 052 | . 053 | . 053 | . 054 | . 054 | . 055 | . 055 | . 056 |
| 5.5 | +0.05I | +0.05I | +0.05I | +0.052 | +0.052 | +0.053 | +0.053 | +0.053 | +0.054 | +0.054 |
| 6.0 | . 049 | . 050 | . 050 | . 051 | .05I | . 052 | . 052 | . 052 | . 053 | . 053 |
| 6.5 | . 048 | . 049 | . 049 | . 050 | . 050 | . 050 | . 051 | .05I | . 052 | . 052 |
| 7.0 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 050 | . 050 | . 050 | .05I |
| 7.5 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 050 |
| 8.0 | +0.045 | +0.045 | +0.046 | +0.046 | +0.047 | +0.047 | +0.047 | +0.048 | +0.048 | +0.048 |
| 8.5 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 047 | . 047 | . 047 |
| 9.0 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 |
| 9.5 | . 042 | . 042 | . 042 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 |
| 10.0 | .04I | .04I | .04I | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 |
| 10.5 | +0.040 | +0.040 | +0.040 | +0.041 | +0.04I | +0.041 | +0.042 | +0.042 | +0.042 | +0.043 |
| 11.0 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | .04I | . 041 | . 041 |
| 11.5 | . 037 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 |
| 12.0 | . 036 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 | . 039 |
| 12.5 | . 035 | . 036 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 038 | . 038 |
| 13.0 | +0.034 | +0.034 | +0.035 | +0.035 | +0.035 | +0.036 | $+0.036$ | +0.036 | +0.036 |  |
| 13.5 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 036 |
| 14.0 | . 032 | . 032 | . 032 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 |
| 14.5 | . 031 | .03I | .03I | . 032 | . 032 | .032 | . 032 | . 033 | . 033 | . 033 |
| 15.0 | . 030 | . 330 | . 030 | . 030 | .031 | .03I | . 031 | .03I | . 032 | . 032 |
| 15.5 | +0.029 | +0.029 | +0.029 | +0.029 | +0.030 | +0.030 | +0.030 | +0.030 | +0.03I | +0.031 |
| 16.0 | . 028 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 030 |
| 16.5 | . 026 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 028 |
| 17.0 | . 025 | . 026 | . 026 | . 026 | . 026 | . 026 | . 027 | . 027 | . 027 | . 027 |
| 17.5 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 |
| 18.0 | +0.023 | +0.023 | +0.024 | +0.024 | +0.024 | +0.024 | +0.024 | +0.025 | +0.025 | +0.025 |
| 18.5 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 |
| 19.0 | . 021 | .02I | .021 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 |
| 19.5 | . 020 | . 020 | . 020 | . 020 | .021 | .021 | .02I | . 021 | . $\mathrm{O2I}$ | . 021 |
| 20.0 | . 019 | . 019 | . 019 | . 019 | . 019 | . 020 | . 020 | . 020 | . 020 | . 020 |
| 20.5 | +0.018 | +0.018 | +0.018 | +0.018 | +0.018 | +0.018 | +0.019 | +0.019 | +0.019 | +0.019 |
| 21.0 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 018 | . 018 | . 018 |
| 21.5 | .016 | . 016 | .or6 | .or6 | . 016 | . 016 | . 016 | .or6 | . 017 | . 017 |
| 22.0 | . 014 | . 15 | .or5 | . 015 | . 015 | . 015 | . Or 5 | . 015 | . OI 5 | . 016 |
| 22.5 | . O 3 | . 1013 | .or4 | . 014 | . 014 | . 014 | . 014 | . 014 | . 014 | . 014 |
| 23.0 | +0.012 | +0.012 | +0.012 | +0.013 | +0.013 | +0.013 | +0.013 | +0.013 | +0.013 | +0.013 |
| 23.5 | . 011 | . 011 | .or 1 | .ori | . 012 | . 012 | . O 2 | . 012 | . O 2 | . OI 2 |
| 24.0 | . 010 | . 010 | . 010 | . 010 | . 010 | .OII | .OII | . Or 1 | . Or I | .OII |
| 24.5 | . 009 | . 009 | . 009 | . 009 | .009 | . 009 | . 009 | . 010 | .oro | . 010 |
| 25.0 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 009 |

Table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther. mometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\begin{gathered} \text { F. } \\ 25.5 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.007 \end{array}$ |
| 26.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 26.5 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 27.0 | . 004 | . 004 | . 004 | .004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 27.5 | . 002 | . 002 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 28.0 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | 0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 30.5 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 | -0.004 |
| 31.0 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 006 | . 006 |
| 31.5 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 32.0 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 |
| 32.5 | . 008 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 |
| 33.0 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 |
| 33.5 | .OII | . Or 1 | . OI I | . OII | . OII | . 011 | . OI 1 | . OII | . OI I | . 017 |
| 34.0 | . 012 | . Or 2 | .OI2 | . 012 | . 012 | . 012 | . 012 | . OI 2 | . 012 | .OI3 |
| 34.5 | .013 | . OI 3 | .OI3 | . Or 3 | . 013 | . .oI3 | . 013 | . 014 | . 014 | . 014 |
| 35.0 | . 014 | . 014 | . 014 | . 014 | . 014 | . 014 | . 015 | . 015 | . 015 | . 015 |
| 35.5 | 0.015 | -0.015 | -0.015 | -0.015 | -0.015 | -0.016 | -0.016 | -0.016 | -0.016 | 0.016 |
| 36.0 | . 016 | . 016 | . 016 | . 016 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 |
| 36.5 | . 017 | . 017 | . OI 7 | . 018 | . 018 | .or8 | .or8 | . 018 | . 18 | . 18 |
| 37.0 | . 018 | . 018 | . 019 | . 019 | . 019 | . 019 | . 019 | .OI9 | . 019 | . 019 |
| 37.5 | . 019 | . 019 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 02 I | .02I |
| 38.0 | -0.020 | -0.021 | -0.021 | -0.021 | -0.021 | -0.021 | -0.021 | -0.022 | -0.022 | -0.022 |
| 38.5 | . 02 I | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 |
| 39.0 | . 023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 |
| 39.5 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 |
| 40.0 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 | . 026 | . 027 |
| 40.5 | -0.026 | -0.026 | -0.026 | -0.026 | -0.027 | -0.027 | -0.027 | -0.027 | -0.028 | -0.028 |
| 41.0 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 |
| 41.5 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 | .030 |
| 42.0 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | .03I | .03I | . 31 | .03I |
| 42.5 | . 030 | .030 | .03I | . 031 | . 031 | .03I | . 032 | . 032 | . 032 | . 032 |
| 43.0 | -0.031 | -0.032 | -0.032 | -0.032 | -0.032 | -0.033 | -0.033 | -0.033 | -0.033 | --0.034 |
| 43.5 | . 032 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 035 | . 035 |
| 44.0 | . 033 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 |
| 44.5 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 |
| 45.0 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 |
| 45.5 | -0.037 | -0.037 | -0.037 | -0.038 | -0.038 | -0.038 | -0.039 | -0.039 | -0.039 | -0.039 |
| 46.0 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | .04I |
| 46.5 | . 039 | . 039 | . 040 | . 040 | . 040 | .04I | .041 | .041 | . 041 | . 042 |
| 47.0 | . 040 | . 040 | .041 | . 041 | .04I | . 042 | . 042 | . 042 | . 043 | . 043 |
| 47.5 | .04I | . 041 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 | . 044 |
| 48.0 | -0.042 | -0.042 | -0.043 | -0.043 | -0.044 | -0.044 | -0.044 | -0.045 | -0.045 | -0.045 |
| 48.5 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 |
| 49.0 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 |
| 49.5 | . 045 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 |
| 50.0 | . 046 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 050 | . 050 |

table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\stackrel{\text { F. }}{5}$ | Inch. | Inch. | Inch. | Inch. | Inch. |  | Inch. |  | Inch. |  |
| 50.5 | -0.048 | -0.048 | -0.048 | -0.049 | -0.049 | -0.050 | -0.050 | -0.050 | -0.05I | -0.051 |
| 51.0 | . 049 | . 049 | . 049 | . 050 | . 050 | .05I | .05I | . 051 | . 052 | . 052 |
| 51.5 | . 050 | . 050 | . 051 | . 051 | . 051 | . 052 | . 052 | . 053 | . 053 | . 053 |
| 52.0 | .05I | .05I | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 | . 055 |
| 52.5 | . 052 | . 052 | . 053 | . 053 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 |
| 53.0 | -0.053 | -0.053 | -0.054 | -0.054 | -0.055 | $\bigcirc 0.055$ | -0.056 | -0.056 | -0.057 | -0.057 |
| 53.5 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 |
| 54.0 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 | . 058 | . 059 | . 059 |
| 54.5 | . 056 | . 057 | . 057 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 060 |
| 55.0 | . 057 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | .06I | .06I | . 062 |
| 55.5 | -0.058 | -0.059 | -0.059 | -0.060 | -0.060 | -0.061 | -0.06I | -0.062 | -0.062 | $-0.063$ |
| 56.0 | . 060 | . 060 | . 060 | .06I | . 061 | . 062 | . 062 | . 063 | . 063 | . 064 |
| 56.5 | . 061 | .06I | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 |
| 57.0 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 |
| 57.5 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 |
| 58.0 | -0.064 | -0.064 | -0.065 | -0.065 | -0.066 | -0.066 | -0.067 | -0.068 | -0.068 | -0.069 |
| 58.5 | . 065 | . 065 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 |
| 59.0 | . 066 | . 067 | . 067 | . 068 | . 068 | .069 | .069 | . 070 | . 070 | . 071 |
| 59.5 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | . 072 | . 072 |
| 60.0 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | . 072 | . 072 | . 073 | . 073 |
| 60.5 | -0.069 | -0.070 | -0.070 | -0.071 | -0.072 | -0.072 | -0.073 | -0.073 | -0.074 | -0.074 |
| 61.0 | . 070 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 076 |
| 61.5 | . 071 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 076 | . 076 | . 077 |
| 62.0 | . 073 | . 073 | . 074 | . 074 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 |
| 62.5 | . 074 | . 074 | . 075 | . 075 | . 076 | . 077 | . 077 | . 078 | . 078 | . 079 |
| 63.0 | -0.075 | -0.075 | -0.076 | -0.077 | -0.077 | -0.078 | -0.078 | -0.079 | -0.08o | -0.080 |
| 63.5 | . 076 | . 076 | . 077 | . 078 | . 078 | . 079 | . 080 | . 080 | .081 | .081 |
| 64.0 | . 077 | . 077 | . 078 | . 079 | . 079 | . 080 | .08I | .081 | . 082 | . 082 |
| 64.5 | . 078 | . 079 | . 079 | . 080 | .08I | .08I | . 082 | . 082 | . 083 | . 084 |
| 65.0 | . 079 | . 080 | . 080 | .08I | . 082 | . 082 | . 083 | . 084 | . 084 | . 085 |
| 65.5 | -0.080 | -0.08I | -0.08I | -0.082 | -0.083 | -0.083 | -0.084 | -0.085 | -0.085 | -0.086 |
| 66.0 | . 081 | . 082 | . 083 | . 083 | . 084 | . 085 | . 085 | . 086 | . 087 | . 087 |
| 66.5 | . 082 | . 083 | . 084 | . 084 | . 085 | . 086 | . 086 | . 087 | . 088 | . 088 |
| 67.0 | . 083 | . 084 | . 085 | . 085 | . 086 | . 087 | . 087 | . 088 | .089 | . 090 |
| 67.5 | . 084 | . 085 | . 086 | . 087 | . 087 | . 088 | .089 | . 089 | . 090 | .09I |
| 68.0 | -0.085 | -0.086 | -0.087 | -0.088 | -0.088 | -0.089 | -0.090 | -0.090 | -0.091 | -0.092 |
| 68.5 | . 087 | . 087 | . 088 | . 089 | . 089 | . 090 | . 091 | . 092 | . 092 | . 093 |
| 69.0 | . 088 | . 088 | .089 | . 090 | .091 | .091 | . 092 | . 093 | . 093 | . 094 |
| 69.5 | .089 | . 089 | . 090 | .091 | . 092 | . 092 | . 093 | . 094 | . 095 | . 095 |
| 70.0 | . 090 | .09I | .091 | . 092 | . 093 | . 094 | . 094 | . 095 | . 096 | . 097 |
| 70.5 | -0.091 | -0.092 | -0.092 | -0.093 | -0.094 | -0.095 | -0.095 | -0.096 | -0.097 | -0.098 |
| 71.0 | . 092 | . 093 | . 094 | . 094 | . 095 | . 096 | . 097 | . 097 | . 098 | . 099 |
| 71.5 | . 093 | . 094 | . 095 | . 095 | . 096 | . 097 | . 098 | . 098 | . 099 | . 100 |
| 72.0 | . 094 | . 095 | . 096 | . 096 | . 097 | . 098 | . 099 | . 100 | . 100 | . 101 |
| 72.5 | . 095 | . 096 | . 097 | . 098 | . 098 | . 099 | . 100 | . IOI | . 102 | . 102 |
| 73.0 | -0.096 | -0.097 | -0.098 | -0.099 | -0.100 | -0.100 | -0.101 | -0.102 | -0.103 | -0.104 |
| 73.5 | . 097 | . 098 | . 099 | . 100 | . IOI | . 101 | . 102 | . 103 | . 104 | . 105 |
| 74.0 | . 098 | . 099 | . 100 | . IOI | . 102 | . 103 | . 103 | . 104 | . 105 | . 106 |
| 74.5 | . 100 | .100 | . 101 | . 102 | . 103 | .104 | .105 | .105 | . 106 | . 107 |
| 75.0 | . 101 | . IOI | . 102 | . 103 | . 104 | .105 | . 106 | . 106 | . 107 | . 108 |

TAble 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\begin{array}{r} \text { F. } \\ 75.5 \end{array}$ | $\begin{gathered} \text { Inch. } \\ -0.102 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{o.} \mathrm{103} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{o.} \mathrm{IO} \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & \text {-o. } 104 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} .105 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ - \text { o. } 106 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -0.107 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ - \text { o. } 108 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{o.} 108 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ \text {-0. } 109 \end{gathered}$ |
| 76.0 | . 103 | . 104 | . 104 | . 105 | . 106 | . 107 | . 108 | . 109 | . 110 | . 110 |
| 76.5 | . 104 | . 105 | . 106 | . 106 | . 107 | . 108 | . 109 | . 110 | . III | . 112 |
| 77.0 | . 105 | . 106 | . 107 | . 108 | . 108 | . 109 | . 110 | . 111 | . 112 | . 113 |
| 77.5 | . 106 | . 107 | . 108 | . 109 | . 110 | . 110 | . II I | . 112 | . 113 | . 114 |
| 78.0 | -0.107 | -0. 108 | -0.109 | -0.110 | -O. 111 | -0.112 | -0.112 | -0.113 | -0.114 | -0. 115 |
| 78.5 | . 108 | . 109 | . 110 | . 111 | . 112 | . 113 | . 114 | . 114 | . 115 | . 116 |
| 79.0 | . 109 | . 110 | . 111 | . 112 | . 113 | .114 | , .115 | . 116 | . 117 | . 117 |
| 79.5 | . 110 | . III | . 112 | . 113 | . 114 | . II5 | . 116 | . 117 | . 118 | . 119 |
| 80.0 | . 111 | . 112 | . 113 | . 114 | . 115 | . 116 | . 117 | . 118 | . 119 | . 120 |
| 80.5 | -0.112 | -0.113 | -O. 114 | -0.115 | -0.116 | -0.117 | -0.118 | -0.119 | -0.120 | -0.121 |
| 8 I .0 | . 114 | . 115 | . 115 | . 116 | . 117 | . 118 | . 119 | . 120 | . 121 | . 122 |
| 81. 5 | . 115 | . 116 | . 117 | .118 | . 118 | . 119 | . 120 | . 121 | . 122 | . 123 |
| 82.0 | . 116 | . 117 | . 118 | . 119 | . 120 | . 12 I | . 122 | . 122 | . 123 | . 124 |
| 82.5 | . 117 | . 118 | . 119 | . 120 | . 121 | . 122 | . 123 | . 124 | . 125 | . 126 |
| 83.0 | -0.118 | -0.119 | -0.120 | -0.12I | -0.122 | -0.123 | -0.124 | -0.125 | -0.126 | -0.127 |
| 83.5 | . 119 | . 120 | . 121 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 |
| 84.0 | . 120 | . 121 | . 122 | .123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 |
| 84.5 | . 121 | . 122 | .123 | . 124 | . 125 | . 126 | .127 | . 128 | . 129 | . 130 |
| 85.0 | . 122 | .123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | . 31 |
| 85.5 | -0.123 | -0. 124 | -0. 125 | -0. 126 | -0. 127 | -0.128 | -0.129 | -0.130 | -0.13I | -0.133 |
| 86.0 | . 124 | . 125 | . 126 | . 127 | . 128 | . 130 | . 13 I | . 132 | . 133 | . 134 |
| 86.5 | . 125 | . 126 | . 128 | . 129 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 |
| 87.0 | . 126 | .128 | .129 | . 130 | . 131 | . 132 | . 133 | . 134 | . 35 | . 136 |
| 87.5 | . 128 | .129 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 |
| 88.0 | -0. 129 | -0.130 | -0.131 | -0.132 | -0.133 | -0.134 | -0. I35 | -0.136 | -0. 137 | -0.138 |
| 88.5 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 |
| 89.0 | . 131 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 140 | . 141 |
| 89.5 | .132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 |
| 90.0 | . 133 | .134 | . 135 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 | . 143 |
| 90.5 | -0.134 | -0.135 | -0.136 | -0. I37 | -OI. 39 | -0.140 | -0.141 | -0.142 | -0.143 | -0.144 |
| 91.0 | . 135 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 |
| 91.5 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 |
| 92.0 | . 137 | . 138 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 148 |
| 92.5 | . 138 | . 139 | .141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 148 | . 149 |
| 93.0 | -0. 139 | -0.14I | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 | -0.148 | -0.149 | -0.150 |
| 93.5 | . 140 | . 142 | . 143 | . 144 | . 145 | . 146 | . 148 | . 149 | . 150 | . 151 |
| 94.0 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 149 | .150 | . 151 | . 152 |
| 94.5 | .143 | . 144 | . 145 | . 146 | . 147 | . 149 | .150 | .151 | . 152 | . 153 |
| 95.0 | . 144 | . 145 | . 146 | . 147 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 |
| 95.5 | -0. 145 | -0.146 | -0.147 | -0.148 | -0.150 | -0.151 | -0.152 | -0.153 | -0.154 | -0.156 |
| 96.0 | . 146 | . 147 | . 148 | . 150 | . 151 | . 152 | . 153 | . 154 | . 156 | . 57 |
| 96.5 | . 147 | . 148 | . 149 | -. 151 | . 152 | . 153 | . 154 | . 156 | . 157 | . 158 |
| 97.0 97.5 | .148 .149 | .149 .150 | . 150 | 152 .153 | . 153 | . 154 | . 155 | $\begin{array}{r}157 \\ . \\ \hline 58\end{array}$ | . 158 | . 159 |
| 97.5 | . 149 | . 150 | . 152 | . 153 | . 154 | . 155 | . 157 | . 158 | . 159 | . 160 |
| 98.0 | -0.150 | -0.15I | -0.153 | -0.154 | -0. 155 | -0.156 | -0.158 | -0.159 | $-0.160$ | $-0.161$ |
| 98.5 | . 151 | . 53 | . 54 | . 155 | . 156 | . 158 | .159 | . 160 | .16I | . 163 |
| 99.0 | .152 | . 154 | .155 | . 156 | . 157 | . 159 | . 160 | .161 | . 162 | . 164 |
| 99.5 100.0 | .153 .154 | .155 .156 | .156 .157 | .157 .158 | .159 .160 | .160 .161 | .161 | .162 .163 | .164 .165 | . 165 |
|  | . 54 | . 5 | - 57 |  |  |  |  |  | .165 |  |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| $\begin{gathered} \text { F. } \\ 0.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.068 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.068 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.069 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.069 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.070 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.070 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.07 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.07 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.072 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.072 \end{gathered}$ |
| +0.5 | +0.067 | +0.067 | +0.068 | +0.068 | +0.069 | +0.069 | +0.070 | +0.070 | +0.071 | +0.071 |
| 1.0 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 |
| 1.5 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 |
| 2.0 | . 063 | . 064 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 |
| 2.5 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 |
| 3.0 | +0.06I | +0.06I | +0.062 | +0.062 | +0.063 | +0.063 | +0.063 | +0.064 | +0.064 | +0.065 |
| 3.5 | . 059 | . 060 | . 060 | . 061 | . 061 | . 062 | . 062 | . 063 | . 063 | . 064 |
| 4.0 | . 058 | . 059 | . 059 | . 060 | . 060 | .06I | .06I | . 061 | . 062 | . 062 |
| 4.5 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | .06I | .06I |
| 5.0 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 | . 059 | . 059 | . 059 | . 060 |
| 5.5 | +0.055 | +0.055 | +0.056 | +0.056 | +0.056 | +0.057 | +0.057 | +0.058 | +0.058 | +0.059 |
| 6.0 | . 054 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 056 | . 057 | . 057 |
| 6.5 | . 052 | . 053 | .053 | . 054 | . 054 | . 054 | . 055 | .055 | .056 | . 056 |
| 7.0 | .05I | . 052 | . 052 | . 052 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 |
| $7 \cdot 5$ | . 050 | . 050 | .05I | .05I | .052 | .052 | .052 | . 053 | . 053 | . 053 |
| 8.0 | +0.049 | +0.049 | +0.050 | +0.050 | +0.050 | +0.05I | +0.051 | +0.051 | +0.052 | +0.052 |
| 8.5 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | .05I | .051 |
| 9.0 | . 046 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 |
| 9.5 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 |
| 10.0 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 |
| 10.5 | +0.043 | +0.043 | +0.044 | +0.044 | +0.044 | +0.045 | +0.045 | +0.045 | +0.046 | +0.046 |
| 11.0 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 |
| 11.5 | .04I | .041 | .041 | .041 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 |
| 12.0 | . 039 | . 040 | . 040 | . 040 | . 041 | . 041 | . 041 | .04I | . 042 | . 042 |
| 12.5 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | . 040 | . 041 |
| 13.0 | +0.037 | +0.037 | +0.038 | +0.038 | +0.038 | +0.038 | +0.039 | +0.039 | +0.039 | +0.040 |
| 13.5 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 |
| 14.0 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 | . 037 | . 037 |
| 14.5 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 036 |
| 15.0 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 |
| 15.5 | +0.03I | +0.031 | +0.032 | +0.032 | +0.032 | +0.032 | +0.032 | +0.033 | +0.033 | +0.033 |
| 16.0 | . 030 | . 030 | . 030 | . 031 | . 031 | . 031 | . 031 | . 031 | . 032 | . 032 |
| 16.5 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | . 030 | . 031 |
| 17.0 | . 027 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 |
| 17.5 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 |
| 18.0 | +0.025 | +0.025 | +0.026 | +0.026 | +0.026 | +0.026 | +0.026 | +0.026 | +0.027 | +0.027 |
| 18.5 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 |
| 19.0 | . 023 | . 023 | . 023 | . 023 | .023 | . 024 | . 024 | . 024 | . 024 | . 024 |
| 19.5 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 |
| 20.0 | . 020 | . 021 | . 021 | . 021 | . 021 | . 021 | . 021 | .02I | . 022 | . 022 |
| 20.5 | +0.019 | +0.019 | +0.020 | +0.020 | +0.020 | +0.020 | +0.020 | +0.020 | +0.020 | +0.021 |
| 21.0 | . 018 | . 018 | . 018 | . 018 | . 019 | . 019 | . 019 | . 019 | . 019 | . 019 |
| 21.5 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 018 | . 018 | . 018 | . 018 |
| 22.0 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 017 | .OI7 | . 017 |
| 22.5 | . 014 | . 1215 | . 015 | . 015 | . 015 | . 015 | . 015 | . 015 | . 015 | . 015 |
| 23.0 | +0.013 | +0.013 | +0.014 | +0.014 | +0.014 | +0.014 | +0.014 | +0.014 | +0.014 | +o.014 |
| 23.5 | . 012 | . 012 | . 012 | . 012 | . 012 | .oI3 | .013 | . 013 | . 013 | . 013 |
| 24.0 | . OII | .OII | .OII | . 011 | . 011 | . Ol 1 | . 011 | . 012 | . 012 | . Ol 2 |
| 24.5 | . 010 | . 010 | .OIO | . 010 | . 010 | . 010 | . 010 | . 010 | . 010 | . 110 |
| 25.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 |

table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| $\begin{gathered} \text { F. } \\ 25^{\circ} .5 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ |
| 26.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 |
| 26.5 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 27.0 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | .004 | . 004 | . 004 | . 004 |
| 27.5 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 28.0 | +.0.00I | +0.001 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | 0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 30.5 | -0.004 | -0.004 | -0.004 | -0 005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 |
| 31.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 31.5 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 32.0 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 009 |
| 32.5 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 | . 010 |
| 33.0 | -0.010 | -0.010 | -0.010 | -0.01I | -0.01I | -0.011 | -0.011 | -0.011 | -0.011 | -0.011 |
| 33.5 | . OII | . 012 | . OI 2 | . 012 | . 012 | . 012 | . 012 | . OI 2 | . 012 | . 012 |
| 34.0 | .or3 | . 013 | .OI3 | . OI 3 | . 013 | . 013 | .or3 | . OI 3 | . OI 3 | .OI4 |
| 34.5 | . 014 | . 014 | . 014 | . 014 | . 014 | .014 | . 014 | . OI 5 | . OI 5 | . 015 |
| 35.0 | . 015 | .015 | . OI 5 | . 015 | . 015 | . 016 | . 016 | . 016 | . 016 | . 016 |
| 35.5 | -0.016 | -0.016 | -0.016 | -0.017 | -0.017 | -0.017 | -0.017 | -0.017 | -0.017 | -0.017 |
| 36.0 | . 017 | . 018 | . 018 | . 018 | . or 8 | .oI8 | . 018 | . 018 | . 018 | . 019 |
| 36.5 | . 019 | . 019 | . 019 | . 019 | . 019 | .OI9 | . 019 | . 020 | . 020 | . 020 |
| 37.0 | . 020 | . 020 | . 020 | . 020 | . 020 | .02I | .021 | . 02 I | . 021 | .02I |
| 37.5 | . 021 | .02I | . 021 | . 021 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 |
| 38.0 | 0.022 | -0.022 | -0.022 | -0.023 | -0.023 | -0.023 | -0.023 | -0.023 | -0.023 | -0.024 |
| 38.5 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 |
| 39.0 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 |
| 39.5 | . 026 | . 026 | . 026 | . 026 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 |
| 40.0 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 028 | . 029 |
| 40.5 | -0.028 | -0.028 | -0.028 | -0.029 | -0.029 | -0.029 | -0.029 | -0.030 | -0.030 | -0.030 |
| 41.0 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | . 031 | . 031 | . 031 | . 031 |
| 41.5 | .030 | .03I | . 031 | . 031 | . 031 | . 032 | . 032 | . 032 | . 032 | . 032 |
| 42.0 | . 032 | . 032 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 033 | . 034 |
| 42.5 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 |
| 43.0 | -0.034 | -0.034 | -0.034 | -0.035 | -0.035 | -0.035 | -0.035 | -0.036 | -0.036 | -0.036 |
| 43.5 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 |
| 44.0 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 |
| 44.5 | . 037 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 |
| 45.0 | . 039 | . 039 | - . 039 | . 039 | . 040 | . 040 | . 040 | . 041 | .04I | .04I |
| 45.5 | -0.040 | -0.040 | -0.040 | -0.04I | -0.04I | -0.041 | -0.042 | -0.042 | -0.042 | -0.043 |
| 46.0 | .041 | .04I | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 | . 044 |
| 46.5 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 |
| 47.0 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 |
| 47.5 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 |
| 48.0 | -0.046 | -0.046 | -0.046 | -0.047 | -0.047 | -0.047 | -0.048 | -0.048 | -0.048 | -0.049 |
| 48.5 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 |
| 49.0 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | .05I | . 051 | .051 |
| 49.5 | . 049 | . 050 | .050 | . 050 | .051 | .051 | .051 | . 052 | . 052 | . 053 |
| 50.0 | . 050 | .05I | .05I | . 052 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 |

TABLE 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 50.5 | -0.052 | -0.052 | -0.052 | -0.053 | -0.053 | -0.054 | -0.054 | -0.054 | -0.055 | -0.055 |
| 51.0 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 056 |
| 51.5 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 056 | . 057 | . 057 | . 058 |
| 52.0 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 | . 058 | . 059 |
| 52.5 | . 056 | . 057 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 |
| 53.0 | -0.057 | -0.058 | -0.058 | -0.059 | -0.059 | -0.060 | -0.060 | -0.06I | -0.06I | -0.06r |
| 53.5 | . 059 | . 059 | . 059 | . 060 | . 060 | .06I | . 061 | . 062 | . 062 | . 063 |
| 54.0 | . 060 | . 060 | .06I | .06I | . 062 | . 062 | . 063 | . 063 | . 063 | . 064 |
| 54.5 | .06I | .06I | . 062 | . 062 | . 063 | . 063 | . 664 | . 064 | . 065 | . 065 |
| 55.0 | . 062 | . 063 | . 063 | . 064 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 |
| 55.5 | -0.063 | -0.064 | -0.064 | -0.065 | $-0.065$ | -0.066 | -0.066 | -0.067 | $-0.067$ | -0.068 |
| 56.0 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 |
| 56.5 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 |
| 57.0 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | .070 | . 070 | .071 | .071 |
| 57.5 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | .071 | . 072 | . 072 | . 073 |
| 58.0 | -0.069 | -0.070 | -0.070 | -0.071 | -0.07I | -0.072 | -0.072 | -0.073 | -0.073 | -0.074 |
| 58.5 | . 070 | . 07 I | . 071 | . 072 | . 072 | . 073 | . 074 | . 074 | . 075 | . 075 |
| 59.0 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | .076 | . 076 |
| 59.5 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | . 076 | . 077 | . 077 | . 078 |
| 60.0 | . 074 | . 074 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 | . 079 |
| 60.5 | -0.075 | $-0.076$ | -0.076 | -0.077 | -0.077 | -0.078 | -0.078 | -0.079 | -0.080 | -0.08o |
| 6 I .0 | . 076 | . 077 | . 077 | . 078 | . 079 | . 079 | .080 | . 080 | .081 | .081 |
| 61.5 | . 077 | . 078 | . 079 | . 079 | .080 | .080 | .08I | . 082 | .082 | . 083 |
| 62.0 | . 079 | . 079 | .080 | .080 | .08I | . 082 | . 082 | . 083 | . 083 | .084 |
| 62.5 | . 080 | . 080 | .08I | .082 | . 082 | . 083 | . 083 | . 084 | . 085 | . 085 |
| 63.0 | -0.081 | -0.082 | -0.082 | -0.083 | -0.083 | -0.084 | -0.085 | -0.085 | -0.086 | -0.086 |
| 63.5 | . 082 | . 083 | . 083 | . 084 | . 085 | . 085 | . 086 | . 086 | . 087 | .088 |
| 64.0 | .083 | . 084 | . 085 | . 085 | . 086 | . 086 | . 087 | . 088 | . 088 | .089 |
| 64.5 | . 084 | . 085 | . 086 | . 086 | . 087 | . 088 | . 088 | . 089 | . 090 | . 090 |
| 65.0 | . 086 | . 086 | . 087 | . 088 | . 088 | . 089 | . 090 | . 090 | .091 | . 092 |
| 65.5 | -0.087 | -0.087 | 0.088 | -0.089 | -0.089 | -0.090 | -0.091 | -0.091 | -0.092 | -0.093 |
| 66.0 | . 088 | .089 | .089 | . 090 | .091 | .091 | . 092 | . 093 | . 093 | . 094 |
| 66.5 | .089 | . 090 | . 090 | .09I | . 092 | . 093 | . 093 | . 094 | . 095 | . 095 |
| 67.0 | . 090 | .091 | . 092 | . 092 | . 093 | . 094 | . 094 | . 095 | . 096 | . 097 |
| 67.5 | . 092 | . 092 | . 093 | . 094 | . 094 | . 095 | . 096 | . 096 | . 097 | . 098 |
| 68.0 | -0.093 | -0.093 | -0.094 |  | -0.095 | -0.096 | -0.097 | -0.098 | -0.098 | -0.099 |
| 68.5 | . 094 | . 095 | . 095 | . 096 | . 097 | . 097 | .098 | . 099 | . 100 | . 100 |
| 69.0 | . 095 | . 096 | . 096 | . 097 | . 098 | . 099 | . 099 | . 100 | . 101 | . 102 |
| 69.5 | . 096 | . 097 | . 098 | . 098 | . 099 | . 100 | . 101 | . IOI | . 102 | . 103 |
| 70.0 | . 097 | . 098 | . 099 | . 100 | . 100 | . 101 | . 102 | . 103 | . 103 | . 104 |
| 70.5 | -0.098 | -0.099 | -0.100 | -0.101 | -0. IOI | -0.102 | -0.103 | -0.104 | -0.105 | -0. 105 |
| 71.0 | . 100 | . 100 | . 101 | . 102 | . 103 | . 103 | . 104 | . 105 | . 106 | . 107 |
| 71.5 | . 101 | . 102 | . 102 | . 103 | . 104 | . 105 | .105 | . 106 | . 107 | . 108 |
| 72.0 | . 102 | . 103 | . 104 | . 104 | . 105 | . 106 | . 107 | . 107 | .108 | .109 |
| 72.5 | . 103 | . 104 | . 105 | . 106 | . 106 | . 107 | . 108 | . 109 | .109 | . 110 |
| 73.0 | -0.104 | -0. 105 | -0. 106 | -0.107 | -0. 108 | -0.108 | -0.109 | -0. 110 | -O. III | -0.112 |
| 73.5 | . 105 | . 106 | . 107 | . 108 | . 109 | . 110 | . 110 | . III | . 112 | . II 3 |
| 74.0 | . 107 | . 107 | . 108 | . 109 | . 110 | . III | . 112 | . 112 | . 113 | . 114 |
| 74.5 | . 108 | . 109 | . 109 | . 110 | . III | . II2 | .113 | . II4 | 114 | . II5 |
| 75.0 | .109 | . 110 | . III | . 112 | . 112 | .113 | .114 | . 115 | 116 | . 117 |

Table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- heit. | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 75.5 | -o.110 | -0.1 | -0.112 | -0.113 | -0.114 | . 114 | -0.115 | -0.116 | -0.117 | -0. II8 |
| 76.0 | . 111 | . 112 | . 113 | . 114 | . 115 | . 116 | . 116 | . 117 | .118 | . 119 |
| 76.5 | .113 | .113 | . 114 | .115 | .ri6 | . 117 | . 118 | . 119 | . 119 | . 120 |
| 77.0 | . 114 | .115 | . 115 | . 116 | . 117 | . 118 | . 119 | . 120 | . 12 I | . 122 |
| 77.5 | . 115 | . 116 | . 117 | . 117 | . 118 | . 119 | . 120 | . 121 | . 122 | . 123 |
| 78.0 | -0.116 | -0.117 | -0.118 | -0.119 | -0.120 | -0.120 | -0.121 | -0.122 | -0.123 | -O. 124 |
| 78.5 | . 117 | . 118 | .119 | . 120 | . 121 | . 122 | . 123 | .123 | . 124 | . 125 |
| 79.0 | . 118 | . 119 | . 120 | . 12 I | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 |
| 79.5 | . 120 | . 120 | . 121 | . 122 | .123 | . 124 | . 125 | . 126 | . 127 | . 128 |
| 80.0 | . 121 | . 122 | . 123 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 |
| 80.5 | -0.122 | -0.123 | -0.124 | -0.125 | -0.126 | -0.127 | -0.127 | -0.128 | -0.129 | -0.130 |
| 81.0 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | .13I | .r 32 |
| 81.5 | . 124 | .125 | . 126 | .127 | . 128 | . 129 | . 130 | . 131 | . 132 | . 133 |
| 82.0 | .125 | . 126 | . 127 | . 128 | . 129 | .130 | .13I | . 132 | . 133 | . 134 |
| 82.5 | . 127 | . 128 | . 128 | .129 | . 130 | .131 | . 132 | . 133 | . 134 | . 135 |
| 83.0 | -0.128 | -0.129 | -0.130 | -0.13I | -0.132 | -0.133 | -0.134 | -0.135 | -0.136 | -0.137 |
| 83.5 | . 129 | .130 | .13I | . 132 | . 133 | . 134 | . 135 | .136 | .137 | .138 |
| 84.0 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 |
| 84.5 | . 131 | .132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 | . 140 |
| 85.0 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 339 | . 141 | . 142 |
| 85.5 | -0.134 | -0.135 | -0.136 | -0.137 | -0.138 | -0.139 | -0.140 | -0.14I | $\bigcirc .142$ | -0.143 |
| 86.0 | . 135 | . 36 | . 137 | . 138 | . 139 | . 140 | . 141 | . 142 | . 143 | . 144 |
| 86.5 | . 136 | . 137 | . 138 | . 139 | .140 | .141 | . 142 | . 143 | . 144 | . 145 |
| 87.0 | . 137 | . 138 | . 139 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 147 |
| 87.5 | . 138 | . 139 | . 140 | .14I | . 142 | . 144 | . 145 | . 146 | . 147 | . 148 |
| 88.0 | -0.139 | -0.140 | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 | -0.147 | -0.148 | -0.149 |
| 88.5 | .14I | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 |
| 89.0 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 152 |
| 89.5 | .143 | .144 | . 145 | .146 | . 147 | .148 | . 149 | . 151 | . 152 | . 153 |
| 90.0 | . 144 | . 145 | .146 | . 147 | . 148 | . 150 | . 151 | . 152 | . 153 | . 154 |
| 90.5 | -0.145 | -0.146 | -0.147 | -0.149 | -0.150 | -0.15I | -0.152 | -0.153 | -0.154 | -0.155 |
| 91.0 | . 146 | . 147 | . 149 | .150 | .15I | . 152 | . 153 | . 154 | . 155 | . 157 |
| 91.5 | . 148 | . 149 | .150 | . 151 | . 152 | . 153 | . 154 | .155 | .157 | . 158 |
| 92.0 | . 149 | . 150 | . 515 | . 152 | . 153 | . 154 | . 156 | . 157 | . 158 | . 159 |
| 92.5 | . 150 | . 151 | . 152 | . 153 | . 154 | . 156 | . 157 | . 158 | . 159 | . 160 |
| 93.0 | -0.15I | -0.152 | -0.153 | -0.155 | -0.156 | -0.157 | -0.158 | -0.159 | -0.160 | -0.16I |
| 93.5 | . 152 | .153 | . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | . 162 | . 163 |
| 94.0 | . 153 | . 155 | .156 | . 157 | . 158 | . 159 | . 160 | . 162 | .163 | . 164 |
| 94.5 | . . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | . 162 | .163 | . 164 | . 165 |
| 95.0 | . 156 | . 157 | . 158 | . 159 | . 160 | . 162 | . 163 | . 164 | . 165 | . 166 |
| 95.5 | -0.157 | -0.158 | -0.159 | -0.160 | -0.162 | $-0.163$ | -0.164 | -0.165 | -0.167 | -0.168 |
| 96.0 | . 158 | . 159 | . 160 | . 162 | .163 | . 164 | .165 | . 167 | . 168 | .169 |
| 96.5 | . 159 | . 160 | .162 | .163 | .164 | . 165 | . 167 | . 168 | . 169 | . 170 |
| 97.0 | .160 | .162 | .163 | .164 | .165 | .167 | . 168 | . 169 | -. 170 | . 171 |
| 97.5 | . 162 | . 163 | . 164 | .165 | . 166 | . 168 | . 169 | . 170 | . 171 | . 173 |
| 98.0 | -0.163 | -0. 164 | -0.165 | -0. 166 | -0. 168 | -0.169 | -0.170 | -0.17I | -0.173 | -0.174 |
| 98.5 | .164 | . 165 | . 166 | . 168 | . 169 | . 170 | . 171 | . 173 | . 174 | . 175 |
| 99.0 | .165 | . 166 | .168 | .169 | .170 | .171 | . 173 | . 174 | . 175 | . 176 |
| 99.5 100.0 | . 166 | .167 | .169 | .170 | .171 | . 173 | .174 | . 175 | .176 | . 178 |
| 100.0 | . 167 | . 169 | . 170 | .171 | . 172 | . 174 | . 175 | .176 | .178 | . 179 |

TABLE 10.

## REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28.0 | 28.2 | 28.4 | 28.6 | 28.8 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| $\begin{gathered} F . \\ 0.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.073 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.074 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.074 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.075 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.075 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.076 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.076 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.077 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.077 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.078 \end{array}$ |
| +0.5 | +0.072 | $+0.072$ | +0.073 | +0.073 | +0.074 | $+0.074$ | $+0.075$ | +0.075 | +0.076 | +0.076 |
| 1.0 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 |
| 1.5 | .069 | . 070 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 |
| 2.0 | . 068 | . 068 | .069 | . 069 | . 070 | . 070 | . 071 | . 07 I | . 072 | . 072 |
| 2.5 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 069 | . 070 | . 070 | . 071 |
| 3.0 | +0.065 | +0.066 | +0.066 | +0.067 | +0.067 | +0.068 | $\pm 0.068$ | +0.069 | +0.069 | +0.070 |
| 3.5 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 |
| 4.0 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 |
| 4.5 | . 062 | . 062 | . 062 | .063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 065 |
| 5.0 | . 060 | .061 | .06I | . 062 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 |
| 5.5 | +0.059 | +0.059 | +0.060 | +0.060 | +0.06I | +0.06I | +0.062 | +0.062 | +0.062 | +0.063 |
| 6.0 | . 058 | . 058 | . 059 | . 059 | . 059 | . 060 | . 060 | .06I | .06r | .06I |
| 6.5 | . 056 | . 057 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 |
| 7.0 | . 055 | . 056 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 | . 058 | . 059 |
| 7.5 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 |
| 8.0 | +0.053 | +0.053 | +0.053 | +0.054 | +0.054 | +0.054 | +0.055 | +0.055 | +0.056 | +0.056 |
| 8.5 | .051 | . 052 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 | . 055 |
| 9.0 | . 050 | . 050 | .051 | .05I | .05I | . 052 | . 052 | . 053 | . 053 | . 053 |
| 9.5 | . 049 | . 049 | . 049 | . 050 | . 050 | . 050 | .051 | .05I | . 052 | . 052 |
| 10.0 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 050 | . 050 | . 050 | . 051 |
| 10.5 | +0.046 | +0.047 | +0.047 | +0.047 | +0.048 | +0.048 | +0.048 | +0.049 | +0.049 | +0.049 |
| 11.0 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 047 | . 048 |
| 11.5 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | . 046 |
| 12.0 | . 042 | . 043 | . 043 | . 043 | . 044 | . 044 | . 044 | . 044 | . 045 | . 045 |
| 12.5 | .04I | . 041 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 | . 044 |
| 13.0 | +0.040 | +0.040 | +0.040 | +0.041 | +0.041 | +0.04I | +0.042 | +0.042 | +0.042 | +0.042 |
| 13.5 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | . 040 | . 041 | .04I |
| 14.0 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 039 | . 040 |
| 14.5 | . 036 | . 336 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 |
| 15.0 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 | . 037 | . 037 |
| 15.5 | +0.033 | +0.034 | +0.034 | +0.034 | +0.034 | +0.035 | +0.035 | +0.035 | +0.035 | +0.036 |
| 16.0 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 |
| 16.5 | .03I | . 331 | . 03 I | . 032 | . 032 | . 032 | . 032 | . 032 | . 033 | . 033 |
| 17.0 | . 030 | . 330 | . 030 | . 030 | . 030 | . 031 | .03I | .031 | . 031 | . 032 |
| 17.5 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 |
| 18.0 | +0.027 | +0.027 | +0.027 | +0.028 | +0.028 | +0.028 | +0.028 | +0.028 | +0.029 | $+0.029$ |
| 18.5 | . 026 | . 026 | . 026 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 027 |
| 19.0 | . 025 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 |
| 19.5 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 |
| 20.0 | . 022 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 | . 023 | . 023 |
| 20.5 | +0.021 | +0.021 | +0.02I | +0.021 | +0.02I | +0.02I | +0.022 | +0.022 | +0.022 | +0.022 |
| 21.0 | . 019 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 021 | . 021 |
| 21.5 | . 018 | . or 8 | . 018 | . 019 | . 019 | .OI9 | .019 | . 019 | . 019 | . 019 |
| 22.0 | . 017 | . 017 | .017 | . 017 | . 017 | .O17 | . 018 | . 018 | .o18 | .o18 |
| 22.5 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 017 |
| 23.0 | +0.014 | +0.014 | +0.015 | +0.015 | +0.015 | +0.015 | +o.015 | +0.015 | +0.015 | +0.015 |
| 23.5 | .OI3 | . Or 3 | . 013 | . O13 | . 013 | . 014 | . 014 | . 014 | .OI 4 | . 014 |
| 24.0 | . 012 | . Ol 2 | . 012 | . 012 | . 012 | . 012 | . 012 | . 012 | . 012 | . 013 |
| 24.5 | . OII | . OII | .OII | . OI I | . 011 | . OII | . OII | . OII | .OII | . OII |
| 25.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 | . 010 | . 010 |

TABLE 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28.0 | 28.2 | 28.4 | 28.6 | 28.8 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| $\begin{array}{r} F \\ 25^{\circ} .5 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.008 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ |
| 26.0 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 26.5 | . 005 | . 005 | . 005 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 27.0 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 27.5 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 28.0 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | $+0.002$ | +0.002 | +0.002 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 003 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 30.5 | 0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 |
| 31.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 31.5 | . 007 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 |
| 32.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | 009 | . 009 | . 009 |
| 32.5 | . 010 | . 010 | . 010 | . 010 | . 010 | . 010 | . 010 | . OIO | . OIO | . 010 |
| 33.0 | O.OII | -0.011 | -O.OII | -0.01 1 | -O.OII | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 |
| 33.5 | .OI2 | . 012 | .OI3 | .OI3 | . OI 3 | .OI 3 | .OI3 | .OI3 | .OI 3 | .OI3 |
| 34.0 | . 014 | .OI4 | .OI4 | .OI4 | .OI4 | .OI4 | . O14 | .OI4 | .OI4 | . OI5 |
| 34.5 | .OI5 | .OI5 | .OI5 | .OI5 | .OI5 | . OI 5 | .or6 | .OI6 | .OI6 | . 016 |
| 35.0 | . 016 | .OI6 | .OI6 | .OI7 | .OI7 | . OI 7 | . 017 | . OI 7 | . OI 7 | . 017 |
| 35.5 | -0.017 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.018 | -0.019 |
| 36.0 | .OI9 | .OI9 | . 019 | . 019 | . 019 | . 019 | . 020 | . 020 | . 020 | . 020 |
| 36.5 | . 020 | . 020 | .020 | . 020 | . 021 | . 021 | . 021 | . 021 | . $\mathrm{O2}$ I | . 021 |
| 37.0 | . 021 | . 021 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 |
| $37 \cdot 5$ | .023 | .023 | .023 | .023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 |
| 38.0 | 0.024 | -0.024 | -0.024 | -0.024 | -0.024 | -0.025 | -0.025 | -0.025 | -0.025 | -0.025 |
| 38.5 | . 025 | .025 | .025 | . 026 | . 026 | . 026 | . 026 | . 026 | . 027 | . 027 |
| 39.0 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 |
| 39.5 | . 028 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 |
| 40.0 | .029 | . 029 | .029 | . 030 | . 030 | . 030 | . 030 | . 030 | .O3I | . O 31 |
| 40.5 | -0.030 | -0.030 | -0.031 | -0.031 | -0.031 | -0.03I | -0.03I | -0.032 | -0.032 | -0.032 |
| 41.0 | . 031 | . 032 | . 032 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 033 |
| 41.5 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 |
| 42.0 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 |
| 42.5 | .035 | .035 | .036 | . 036 | . 036 | .036 | .037 | . 037 | .037 | . 037 |
| 43.0 | -0.036 | -0.037 | -0.037 | -0.037 | -0.038 | -0.038 | -0.038 | -0.038 | -0.039 | -0.039 |
| 43.5 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 |
| 44.0 | . 039 | . 039 | . 040 | . 040 | . 040 | . 040 | . 041 | .04I | .04I | . 042 |
| $44 \cdot 5$ | . 040 | .04I | .04I | . 041 | . 041 | . 042 | . 042 | . 042 | . 043 | . 043 |
| 45.0 | . 042 | . 042 | .042 | . 042 | . 043 | . 043 | .043 | . 044 | . 044 | . 044 |
| 45.5 | -0.043 | -0.043 | -0.043 | -0.044 | -0.044 | -0.044 | -0.045 | -0.045 | -0.045 | -0.046 |
| 46.0 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 |
| 46.5 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 |
| 47.0 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 |
| 47.5 | . 048 | . 048 | .049 | . 049 | . 049 | .050 | .050 | .050 | .051 | . 051 |
| 48.0 | -0.049 | -0.050 | -0.050 | -0.050 | -0.051 | -0.051 | -0.05I | -0.052 | -0.052 | -0.052 |
| 48.5 | . 050 | . 051 | . 051 | . 052 | . 052 | .052 | . 053 | . 053 | . 053 | . 054 |
| 49.0 | . 052 | .052 | .052 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 |
| 49.5 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 056 |
| 50.0 | . 054 | . 055 | .055 | . 055 | . 056 | . 056 | .057 | . 057 | . 057 | . 058 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

|  | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28.0 | 28.2 | 28.4 | 28.6 | 28.8 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| F. | Inch. | ch. | uch. | Inch | ch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 50.5 | -0.055 | -0.056 | -0.056 | -0.057 | -0.057 | -0.057 | -0.058 | -0.058 | -0.059 | -0.059 |
| 51.0 | . 057 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 060 |
| 51.5 | . 058 | . 558 | . 059 | . 059 | . 060 | . 060 | .061 | . 061 | . 061 | . 662 |
| 52.0 | . 059 | . 060 | . 060 | . 061 | .061 | . 061 | . 062 | . 062 | . 063 | . 663 |
| 52.5 | . 061 | .06I | . 061 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 064 |
| 53.0 | -0.062 | -0.062 | -0.063 | -0.063 | -0.064 | -0.064 | -0.064 | -0.065 | -0.065 | -0.066 |
| 53.5 | . 063 | . 064 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 |
| 54.0 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 068 |
| 54.5 | . 066 | . 066 | . 067 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 |
| 55.0 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | . 071 |
| 55.5 | -0.068 | -0.069 | -0.069 | -0.070 | -0.070 | -0.071 | -0.071 | --0.072 | -0.072 | -0.073 |
| 56.0 | . 069 | . 070 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 |
| 56.5 | . 071 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 |
| 57.0 | . 072 | . 072 | . 073 | . 073 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 |
| 57.5 | . 073 | . 074 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 |
| 58.0 | 0.074 | -0.075 | -0.076 | -0.076 | -0.077 | 0.077 | -0.078 | -0.078 | -0.079 | -0.079 |
| 58.5 | . 076 | . 076 | . 077 | . 077 | . 078 | . 78 | . 079 | . 080 | . 080 | .081 |
| 59.0 | . 077 | . 078 | . 078 | . 079 | . 079 | . 080 | . 080 | .081 | .081 | . 082 |
| 59.5 | . 078 | . 079 | . 079 | . 080 | .081 | .08I | . 082 | . 082 | . 083 | . 083 |
| 60.0 | . 080 | . 080 | .08I | .08I | . 082 | . 082 | . 083 | . 084 | . 084 | . 085 |
| 60.5 | . 081 | -0.081 | -0.082 | -0.083 | -0.083 | -0.084 | -0.084 | -0.085 | -0.085 | -0.086 |
| 6 I .0 | . 082 | . 083 | . 083 | . 084 | . 084 | . 085 | . 086 | . 086 | . 087 | . 087 |
| 61.5 | . 083 | . 084 | . 085 | . 085 | . 086 | . 086 | . 087 | . 087 | . 088 | . 089 |
| 62.0 | . 085 | . 085 | . 886 | . 086 | . 087 | . 088 | . 888 | . 089 | . 089 | . 090 |
| 62.5 | . 886 | . 086 | . 087 | . 088 | . 088 | .089 | . 990 | . 090 | . 091 | . 091 |
| 63.0 | -0.087 | -0.088 | -0.088 | -0.089 | -0.090 | -0.090 | -0.091 | -0.091 | -0.092 | -0.093 |
| 63.5 | . 888 | . 089 | . 090 | . 090 | . 091 | . 092 | . 092 | . 093 | . 093 | . 094 |
| 64.0 | . 090 | . 090 | . 091 | . 092 | . 092 | . 093 | . 993 | . 094 | . 095 | . 095 |
| 64.5 | . 091 | . 092 | . 092 | . 093 | . 093 | . 094 | . 995 | . 095 | . 096 | . 097 |
| 65.0 | . 092 | . 093 | . 993 | . 094 | . 095 | . 095 | . 996 | . 097 | . 097 | . 098 |
| 65.5 | 0.093 | -0.094 | -0.095 | -0.095 | -0.096 | -0.097 | -0.097 | -0.098 | -0.099 | -0.099 |
| 66.0 | . 995 | . 095 | . 096 | . 097 | . 097 | . 098 | . 999 | . 099 | . 100 | .101) |
| 66.5 | . 096 | . 097 | . 097 | . 098 | . 099 | . 099 | . 100 | .ror | . 101 | . 102 |
| 67.0 | . 097 | . 098 | . 099 | . 099 | . 100 | . 101 | . 101 | . 102 | . 103 | . 103 |
| 67.5 | . 098 | . 099 | . 100 | . 101 | . 101 | . 102 | .103 | . 103 | . 104 | . 105 |
| 68.0 | -0.100 | -0.100 | -0.101 | -0.102 | -0.103 | -0.103 | -0.104 | -0.105 | -0.105 | -0.106 |
| 68.5 | . 101 | . 102 | . 102 | . 103 | . 104 | . 105 | . 105 | . 106 | . 107 | . 107 |
| 69.0 | . 102 | . 103 | . 104 | . 104 | . 105 | . 106 | . 107 | . 107 | . 108 | . 109 |
| 69.5 | . 104 | . 104 | . 105 | . 106 | . 106 | . 107 | . 108 | . 109 | . 109 | . 110 |
| 70.0 | . 105 | . 106 | . 106 | . 107 | . 108 | . 109 | . 109 | . 110 | .III | .112 |
| 70.5 | -0.106 | -0.107 | -0.108 | -0.108 | -0.109 | -0.110 | -0.1II | -0.1II | -0.112 | -0.113 |
| 71.0 | .107 | .108 | . 109 | . 110 | . 110 | . 111 | . 112 | .113 | .113 | . 114 |
| 71.5 | . 109 | . 109 | . 110 | . 111 | . 112 | . 112 | . 113 | . 114 | .115 | . 116 |
| 72.0 | . 110 | . 111 | .III | . 112 | .113 | . 114 | .115 | .115 | .116 | . 117 |
| 72.5 | II | . 112 | .113 | .113 | . 114 | . 115 | . 116 | . 117 | . 117 | .118 |
| 73.0 | -0.112 | -0.113 | -0.114 | -0.115 | -0.116 | -0.116 | -0.117 | -0.118 | 0.119 | . 120 |
| 73.5 | . 114 | . 114 | .115 | . 116 | . 117 | .118 | .118 | . 119 | . 120 | . 121 |
| 74.0 | .115 | .116 | . 117 | .117 | . 118 | .119 | . 120 | . 121 | . 121 | . 122 |
| 74.5 | . 116 | . 117 | .ri8 | .119 | .119 | . 120 | .121 | .122 | .123 | . 124 |
| 75.0 | . 117 | . 118 | . 119 | . 120 | . 121 | . 122 | . 122 | . 123 | . 124 | . 125 |

TABLE 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- heit. | 28.0 | 28.2 | 28.4 | 286 | 288 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 75.5 | -0.119 | -0.119 | -0.120 | -0.12I | -0.122 | -0.123 | -0.124 | -0. 125 | -0.125 | -0. 126 |
| 76.0 | . 120 | . 121 | . 122 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 |
| 76.5 | . 121 | . 122 | . 123 | . 124 | . 125 | . 125 | . 126 | .127 | . 128 | . 129 |
| 77.0 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 129 | .130 |
| 77.5 | . 124 | . 125 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | . . 13 I | . 132 |
| 78.0 | -0.125 | -0.126 | -0.127 | -0.128 | -0.129 | -0. 129 | -0.130 | -0.13I | -0.132 | -0.133 |
| 78.5 | . 126 | . 127 | . 128 | . 129 | . 130 | . 13 I | . 132 | . 133 | . 133 | . 134 |
| 79.0 | . 127 | . 128 | . 129 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 | . 136 |
| 79.5 | . 129 | . 130 | .13I | .13I | .132 | . I33 | . 134 | . 135 | . 136 | . 137 |
| 80.0 | . 130 | .13I | . 132 | . 133 | . 134 | . 135 | -136 | . 136 | . 137 | . 138 |
| 80.5 | -0.13I | -0.132 | -0.133 | -0.134 | -0.135 | -0.136 | -0.137 | -0.138 | -0.139 | -0.140 |
| 81.0 | . 132 | .133 | .134 | . 135 | . 136 | . 137 | . 138 | . 339 | . 140 | . 141 |
| 8 r .5 | . 134 | . 135 | .136 | . 137 | . 138 | . 139 | .139 | .140 | .14I | . 142 |
| 82.0 | . 135 | . 136 | .137 | . 138 | . 139 | . 140 | . I4I | . 142 | . 143 | . 144 |
| 82.5 | . 136 | . 137 | .I38 | . 139 | . 140 | .141 | . 142 | . 143 | . 144 | . 145 |
| 83.0 | -0.138 | -0.139 | -0.139 | -0.140 | -0.14I | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 |
| 83.5 | . 139 | . 140 | .14I | . 142 | . 143 | . 144 | . 145 | . .146 | . 147 | . 148 |
| 84.0 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 |
| 84.5 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | .147 | . 148 | . 149 | . 150 |
| 85.0 | . 143 | . 144 | . 145 | .146 | . 147 | . 148 | . 149 | . 150 | . 151 | . 152 |
| 85.5 | -0.144 | -0.145 | -0.146 | -0. 147 | -0.148 | -0.149 | -0.150 | -0.15I | -0.152 | -0. 153 |
| 86.0 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | .15I | . 152 | . 53 | . 154 |
| 86.5 | . 146 | . 147 | . 148 | . 149 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 |
| 87.0 | . 148 | . 149 | . 150 | .15I | . 152 | . 153 | . 54 | . 155 | . 156 | . 157 |
| 87.5 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 | . 158 |
| 88.0 | -0.150 | -0.151 | -0.152 | -0.153 | -0.154 | -0.155 | -0. 157 | -0.158 | -0.159 | $-0.160$ |
| 88.5 | . 151 | . 152 | . 154 | . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | .161 |
| 89.0 | . 153 | . 154 | . 155 | . 156 | . 157 | .158 | . 159 | .160 | .161 | . 162 |
| 89.5 | . 154 | . 155 | . 156 | . 157 | .158 | . 159 | . 160 | .162 | .163 | . 164 |
| 90.0 | . 155 | . 156 | . 157 | . 158 | . 160 | . 161 | . 162 | . 163 | . 164 | . 165 |
| 90.5 | -0.156 | -0.157 | -0.159 | -0.160 | -0.161 | -0.162 | $-0.163$ | -0.164 | -0.165 | -0.166 |
| 91.0 | . 158 | . 159 | . 160 | .16I | . 162 | .163 | . 164 | . 166 | . 167 | . 168 |
| 91.5 | . 159 | . 160 | .16I | . 162 | . 163 | . 165 | . 166 | . 167 | . 168 | . 169 |
| 92.0 | . 160 | . 161 | . 162 | . 164 | . 165 | . 166 | . 167 | .168 | .169 | . 170 |
| 92.5 | .161 | . 163 | . 164 | . 165 | .166 | . 167 | . 168 | . 169 | .171 | . 172 |
| 93.0 | -0.163 | -0.164 | -0.165 | -0.166 | -0.167 | -0.168 | -0.170 | -0.171 | -0.172 | -0.173 |
| 93.5 | .164 | . 165 | . 166 | . 167 | . 169 | . 170 | .171 | . 172 | .173 | . 174 |
| 94.0 | . 165 | .166 | . 168 | . 169 | . 170 | . 171 | . 172 | . 173 | . 175 | . 176 |
| 94.5 | .166 | . 168 | . 169 | . 170 | .171 | . 172 | . 174 | . 175 | .176 | .177 |
| 95.0 | . 168 | . 169 | . 170 | .171 | . 172 | . 174 | . 175 | . 176 | . 177 | .178 |
| 95.5 | -0.169 | -0.170 | -0.171 | -0.173 | -0.174 | -0.175 | -0.176 | -0.177 | -0.179 | -0.18o |
| 96.0 | .170 | . 171 | . 173 | . 174 | . 175 | . 176 | . 177 | . 179 | . 180 | .18I |
| 96.5 | . 171 | . 173 | . 174 | . 175 | . 176 | . 178 | . 179 | . 180 | . 181 | . 182 |
| 97.0 | . 173 | . 174 | . 175 | .176 | . 178 | . 179 | . 180 | .18I | . 183 | . 184 |
| 97.5 | . 174 | . 175 | . 176 | . 178 | . 179 | . 180 | . 181 | . 183 | . 184 | . 185 |
| 98.0 | -0.175 | -0.176 | -0.178 | -0.179 | -0.180 | -0.18I | -0.183 | -0.184 | -0.185 | -0.186 |
| 98.5 | . 176 | . 178 | . 179 | . 180 | . 181 | . 183 | . 184 | . 185 | . 187 | . 188 |
| 99.0 | .178 | . 179 | . 180 | . 182 | . 183 | . 184 | . 185 | . 187 | . 188 | . 189 |
| 99.5 | .179 | . 180 | . 182 | . 183 | . 184 | . 185 | . 187 | . 188 | . 189 | . 190 |
| 100.0 | . 180 | . 182 | . 183 | . 184 | . 185 | . 187 | . 188 | . 189 | .19I | . 192 |

Table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached <br> Thernometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| $\begin{gathered} \text { F. } \\ 0.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.078 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.078 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.079 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.079 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.080 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.080 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.08 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.08 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.082 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.082 \end{gathered}$ |
| 0.5 | +0.076 | +0.077 | +0.077 | +0.078 | +0.078 | +0.079 | +0.079 | +0.080 | +0.080 | +0.081 |
| 1.0 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 | . 079 | . 079 | .080 |
| 1.5 | . 074 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 |
| 2.0 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 |
| 2.5 | . 07 I | . 07 I | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 |
| 3.0 | +0.070 | +0.070 | +0.070 | +0.071 | +0.071 | +0.072 | +0.072 | +0.073 | +0.073 | +0.074 |
| 3.5 | . 068 | . 069 | . 069 | . 070 | . 070 | . 070 | . 071 | . 07 I | . 072 | . 072 |
| 4.0 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | . 070 | . 071 |
| 4.5 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 069 |
| 5.0 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 |
| 5.5 | +0.063 | +0.063 | +0.064 | +0.064 | +0.064 | +0.065 | +0.065 | +0.066 | +0.066 | +0.067 |
| 6.0 | . 06 I | . 062 | . 062 | . 063 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 |
| 6.5 | . 060 | . 060 | .06I | .06r | . 062 | . 062 | . 062 | . 063 | . 063 | . 064 |
| 7.0 | . 059 | .059 | . 059 | . 060 | . 060 | .06I | .06I | . 061 | . 062 | . 062 |
| 7.5 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 060 | .06I |
| 8.0 | +0.056 | +0.056 | +0.057 | +0.057 | +0.057 | +0.058 | +0.058 | +0.059 | +0.059 | +0.059 |
| 8.5 | . 055 | . 055 | . 055 | . 056 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 |
| 9.0 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 056 |
| 9.5 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 |
| 10.0 | .05I | .05I | .051 | . 052 | . 052 | .052 | . 053 | . 053 | . 053 | . 054 |
| 10.5 | +0.049 | +0.049 | +0.050 | +0.050 | +0.050 | +0.051 | +0.051 | +0.05I | +0.052 | +0.052 |
| 11.0 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | . 050 | .05I |
| 11.5 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 |
| 12.0 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 |
| 12.5 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 |
| 13.0 | +0.042 | +0.043 | +0.043 | +0.043 | +0.044 | +0.044 | +0.044 | +0.044 | +0.045 | +0.045 |
| 13.5 | .041 | .04I | . 042 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 |
| 14.0 | . 040 | . 040 | . 040 | . 040 | .04I | .041 | .04I | . 042 | . 042 | . 042 |
| 14.5 | . 038 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | . 040 | . 041 |
| 15.0 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 |
| 15.5 | +0.036 | +0.036 | +0.036 | +0.036 | +0.037 | +0.037 | +0.037 | +0.037 | +0.037 | +0.038 |
| 16.0 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 |
| 16.5 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 |
| 17.0 | . 032 | .032 | . 032 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 033 |
| 17.5 | . 030 | . 030 | .03I | . 031 | . 031 | .03I | .03I | . 032 | . 032 | . 032 |
| 18.0 | +0.029 | +0.029 | +0.029 | +0.029 | +0.030 | +0.030 | +0.030 | +0.030 | +0.030 | +0.03I |
| 18.5 | . 027 | . 028 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 |
| 19.0 | . 026 | . 026 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 |
| 19.5 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 | . 026 |
| 20.0 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 |
| 20.5 | +0.022 | +0.022 | +0.022 | +0.022 | +0.023 | +0.023 | +0.023 | +0.023 | +0.023 | +0.023 |
| 21.0 | . 021 | . 021 | . 02 I | . 021 | . 021 | . 021 | . 022 | . 022 | . 022 | . 022 |
| 21.5 | .or9 | . 019 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 |
| 22.0 | .or8 | . 018 | . 018 | . 018 | . 018 | . 019 | . 019 | .o19 | .oi9 | .019 |
| 22.5 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 018 |
| 23.0 | +0.015 | +0.015 | +0.015 | +0.016 | +0.016 | +0.016 | +0.016 | +0.016 | +0.016 | +0.016 |
| 23.5 | . 014 | . 014 | . 014 | . 014 | . 014 | . 014 | . OI 4 | . OI 5 | . OI 5 | . 015 |
| 24.0 | . 013 | . 013 | . OI 3 | . OI 3 | .OI3 | . OI 3 | . 013 | . 013 | . 013 | .or3 |
| 24.5 | . OII | . OII | . OII | . OI I | . OII | . 012 | . O 2 | . 012 | . Ol 2 | . O 2 |
| 25.0 | . 010 | . 010 | . 010 | . 010 | .oro | . 010 | . 010 | . 010 | 0.10 | . 010 |

Table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

## ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| $\begin{array}{r} \text { F. } \\ 25.5 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.009 \end{gathered}$ | Inch. <br> $+0.009$ |
| 26.0 | +0.008 .007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 008 | . 008 |
| 26.5 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 27.0 | . 004 | . 004 | . 004 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 27.5 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 28.0 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | 0.001 | 0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 30.5 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 |
| 31.0 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 31.5 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 |
| 32.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 |
| 32.5 | . 010 | . 011 | . 011 | . 011 | . OI I | . OII | . OII | . OII | . OII | . 011 |
| 33.0 | -0.012 | -0.012 | -0.012 | -0.012 | 0.012 | 0.012 | 0.012 | 0.012 | -0.012 | -0.013 |
| 33.5 | . 013 | . 013 | . 013 | .OI3 | . 014 | . 014 | . 014 | . 014 | . 014 | . 014 |
| 34.0 | . 015 | . 015 | . 015 | . 015 | . 015 | . 015 | .015 | . 015 | . 015 | . 015 |
| 34.5 | .or6 | .oI6 | . 016 | .or6 | . 016 | .or6 | . 017 | . 017 | . 017 | . 017 |
| 35.0 | .OI7 | . 017 | .or7 | .or8 | . 018 | . 018 | . 018 | . 018 | . 018 | . 18 |
| 35.5 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.020 | -0.020 |
| 36.0 | . 020 | . 020 | . 020 | . 020 | . 020 | .021 | .021 | . 021 | . 021 | . 021 |
| 36.5 | . 021 | .021 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 |
| 37.0 | . 023 | . 023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 |
| $37 \cdot 5$ | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 | . 025 |
| 38.0 | -0.025 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.027 | -0.027 | -0.027 |
| 38.5 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 028 |
| 39.0 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 |
| 39.5 | . 029 | . 030 | . 030 | . 030 | . 030 | . 030 | .031 | . 031 | .03I | .031 |
| 40.0 | .03I | . 031 | .03I | . 031 | . 032 | .032 | .032 | .032 | . 032 | . 033 |
| 40.5 | -0.032 | -0.032 | -0.033 | -0.033 | -0.033 | -0.033 | -0.033 | -0.034 | -0.034 | -0.034 |
| 41.0 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 035 |
| 41.5 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 | . 037 | . 037 |
| 42.0 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 |
| 42.5 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 |
| 43.0 | -0.039 | -0.039 | -0.039 | -0.040 | -0.040 | -0.040 | -0.040 | -0.04I | -0.04I | -0.041 |
| 43.5 | . 040 | . 040 | .04I | . 041 | .04I | . 042 | . 042 | . 042 | . 042 | . 043 |
| 44.0 | . 042 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 | . 044 | . 044 |
| 44.5 | . 043 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 045 |
| 45.0 | . 044 | . 045 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 |
| 45.5 | -0.046 | -0.046 | -0.046 | -0.047 | -0.047 | -0.047 | -0.047 | -0.048 | -0.048 | -0.048 |
| 46.0 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 049 | . 050 |
| 46.5 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | . 050 | .051 | .05I | .051 |
| 47.0 | . 050 | . 050 | . 050 | .051 | .051 | .05I | . 052 | . 052 | . 052 | . 053 |
| 47.5 | .05I | . 051 | . 052 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 |
| 48.0 | -0.052 | -0.053 | $\bigcirc 0.053$ | -0.053 | -0.054 | -0.054 | -0.054 | -0.055 | -0.055 | -0.055 |
| 48.5 | . 054 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 |
| 49.0 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 | . 058 | . 058 |
| 49.5 | . 056 | . 057 | . 057 | . 058 | .058 | . 058 | . 059 | . 059 | . 059 | . 060 |
| 50.0 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 060 | .06I | . 061 |

## Table 10

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 50.5 | -0.059 | -0.059 | -0.060 | -0.060 | -0.06I | -0.06I | -0.061 | -0.062 | -0.062 | $-0.063$ |
| 51.0 | . 060 | .06I | .06I | . 062 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 |
| 51.5 | . 062 | . 062 | .063 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 065 |
| 52.0 | . 063 | . 064 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 | . 066 | . 067 |
| 52.5 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 067 | . 068 | . 068 |
| 53.0 | -0.066 | -0.066 | -0.067 | -0.067 | -0.068 | -0.068 | -0.068 | -0.069 | -0.069 | -0.070 |
| 5.35 | . 067 | . 068 | . 068 | . 069 | . 069 | . 069 | . 070 | . 070 | . 071 | . 071 |
| 54.0 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 |
| 54.5 | . 070 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 |
| 55.0 | . 07 I | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | . 075 |
| 55.5 | -0.073 | -0.073 | -0.074 | -0.074 | -0.074 | -0.075 | -0.075 | -0.076 | -0.076 | -0.077 |
| 56.0 | . 074 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 |
| 56.5 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 | . 079 | . 079 | . 080 |
| 57.0 | . 077 | . 077 | . 078 | . 078 | . 079 | . 079 | .08o | . 080 | .081 | .081 |
| 57.5 | . 078 | . 078 | . 079 | . 079 | . 080 | .08I | .08I | . 082 | . 082 | .083 |
| 58.0 | -0.079 | -0.08o | -0.080 | -0.081 | -0.08I | -0.082 | $-0.082$ | -0.083 | -0.084 | -0.084 |
| 58.5 | .081 | .081 | . 082 | . 082 | . 083 | . 083 | . 084 | . 084 | . 085 | . 085 |
| 59.0 | . 082 | . 083 | . 083 | . 084 | . 084 | . 085 | . 085 | . 086 | . 086 | . 087 |
| 59.5 | . 083 | . 084 | .084 | . 085 | . 086 | . 086 | . 087 | . 087 | . 088 | . 088 |
| 60.0 | . 085 | . 085 | .086 | . 086 | . 087 | . 087 | . 088 | . 089 | .089 | . 090 |
| 60.5 | -0.086 | -0.087 | -0.087 | -0.088 | -0.088 | -0.089 | -0.089 | -0.090 | -0.091 | -0.091 |
| 61.0 | . 087 | . 088 | .089 | . 089 | . 090 | . 090 | .091 | . 091 | . 092 | . 093 |
| 61.5 | .089 | .089 | . 090 | . 090 | .09I | . 092 | . 092 | . 093 | . 093 | . 094 |
| 62.0 | . 090 | .091 | .091 | . 092 | . 092 | . 093 | . 094 | . 094 | . 095 | . 095 |
| 62.5 | .091 | . 092 | . 093 | . 093 | . 094 | . 094 | . 095 | . 096 | . 096 | . 097 |
| 63.0 | -0.093 | -0.093 | -0.094 | -0.095 | -0.095 | -0.096 | -0.096 | -0.097 | -0.098 | -0.098 |
| 63.5 | . 094 | . 095 | . 095 | . 096 | . 097 | . 097 | .098 | . 098 | . 099 | . 100 |
| 64.0 | . 095 | . 096 | . 097 | . 097 | . 098 | . 099 | . 099 | . 100 | . IOI | . 101 |
| 64.5 | . 097 | . 097 | . 098 | . 099 | . 099 | . 100 | . 101 | . IOI | . 102 | . 103 |
| 65.0 | . 098 | . 099 | . 099 | . 100 | . 101 | . IOI | . 102 | . 103 | . 103 | . 104 |
| 65.5 | -0.099 | -0.100 | -0.101 | -0.101 | -0. 102 | -0.103 | -0.103 | -0.104 | -0.105 | -0. 105 |
| 66.0 | . 101 | . 101 | . 102 | . 103 | . 103 | . 104 | . 105 | . 106 | . 106 | . 107 |
| 66.5 | . 102 | . 103 | . 103 | . 104 | . 105 | . 106 | . 106 | . 107 | . 108 | . 108 |
| 67.0 | . 103 | . 104 | . 105 | . 106 | . 106 | .107 | . 108 | . 108 | . 109 | . 110 |
| 67.5 | . 105 | . 106 | . 106 | . 107 | . 108 | . 108 | . 109 | . 110 | . 110 | . III |
| 68.0 | -0.106 | -0.107 | -0.108 | -0.108 | -0.109 | -0.110 | -0.110 | -0.111 | -0.112 | -0.113 |
| 68.5 | . 107 | . 108 | . 109 | . 1 Io | . 110 | . 111 | . 112 | . 113 | . 113 | . 114 |
| 69.0 | . 109 | . 110 | . 110 | .III | . 112 | . 112 | .113 | . 114 | . 115 | . 115 |
| 69.5 | . IIO | . III | . 112 | . 112 | . 113 | . II4 | . 115 | . II5 | . 116 | . 117 |
| 70.0 | . 112 | . 112 | . 113 | . 114 | . 115 | . 115 | . 116 | . 117 | . 117 | . 118 |
| 70.5 | -0.113 | -0.114 | -0.114 | -0. 115 | -0.116 | -0.117 | -0.117 | -0.118 | -0.119 | -0. 120 |
| 71.0 | . II4 | . 115 | . 116 | . 116 | . I17 | . 118 | . 119 | . 120 | . 120 | . 121 |
| 71.5 | . 116 | . 116 | . 117 | . 118 | . 19 | . 119 | . 120 | . 121 | . 122 | . 123 |
| 72.0 | . 117 | . 118 | . 118 | . 119 | . 120 | . 121 | .122 | . 122 | .123 | . 124 |
| 72.5 | . 118 | . II9 | . 120 | . 12 I | :121 | . 122 | . 123 | . 124 | . 125 | . 125 |
| 73.0 | -0.120 | -0.120 | -0.121 | -0.122 | -0.123 | -0.124 | -0.124 | -0.125 | -0.126 | -0.127 |
| 73.5 | . 121 | . 122 | . 123 | . 123 | . 124 | . 125 | . 126 | . 127 | . 127 | . 128 |
| 74.0 | . 122 | . 123 | . 124 | . 125 | . 126 | . 126 | . 127 | . 128 | . 129 | . 130 |
| 74.5 | .124 | .124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 129 | . 130 | .131 |
| 75.0 | . 125 | . 126 | . 127 | . 127 | . 128 | . 129 | . 130 | .13I | . 132 | . 132 |

Table 10.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thepmometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| ${ }_{7}^{\mathrm{F} .}$ | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| $75.5$ | $-0.126$ | $-0.127$ | $-0.128$ | $\text { -0. } 129$ | $-0.130$ | $-0.13 I$ | $-0.131$ | $-0.132$ | $\text { -0. I } 33$ | -0. 134 |
| 76.0 | . 128 | . 128 | .129 | . 130 | . 131 | . 132 | . 133 | . 134 | . 134 | . 135 |
| 76.5 | . 129 | . 130 | .13I | . 132 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 |
| 77.0 | . 130 | . 31 | . 132 | . 133 | . 134 | . 135 | . 136 | . 136 | . 137 | . 138 |
| 77.5 | . 132 | . 133 | . 133 | . 134 | . 135 | .136 | . 137 | . 138 | . 139 | . 140 |
| 78.0 | -0.133 | -0.134 | -0.135 | -0.136 | -0.137 | -0.137 | -0.138 | -0.139 | -0.140 | -0.141 |
| 78.5 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 | . 140 | .141 | . 142 | . 142 |
| 79.0 | . 136 | . 137 | . 137 | . 138 | . 139 | . 140 | .141 | . 142 | . 143 | . 144 |
| 79.5 | . 137 | . 138 | . 139 | . 140 | . 141 | . 142 | . 143 | . 143 | . 144 | . 145 |
| 80.0 | . 138 | . 139 | . 140 | .14I | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 |
| 80.5 | 0.140 | -0.141 | -0.142 | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 | -0.147 | -0.148 |
| 81.0 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 |
| 81.5 | . 142 | . 143 | . 144 | . 145 | . 146 | .147 | . 148 | . 149 | . 150 | . 151 |
| 82.0 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 149 | . 150 | .15I | . 152 |
| 82.5 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 |
| 83.0 | -0.146 | -0.147 | -0.148 | -0.149 | -0.150 | -0.15I | -0.152 | -0.153 | -0.154 | -0.155 |
| 83.5 | . 148 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 |
| 84.0 | . 149 | . 150 | . 151 | . 152 | . 53 | . 154 | . 155 | . 156 | . 157 | . 158 |
| 84.5 | . 150 | . 151 | .152 | . 55 | . 154 | . 155 | . 156 | . 157 | . 158 | . 159 |
| 85.0 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | .16I |
| 85.5 | -0.153 | -0.154 | -0.155 | -0.156 | -0.157 | -0.158 | -0.159 | $-0.160$ | -0.161 | -0.162 |
| 86.0 | . 154 | . 155 | . 156 | . 158 | . 159 | .160 | .161 | . 162 | . 163 | . 164 |
| 86.5 | . 156 | . 157 | . 158 | . 159 | . 160 | .16I | . 16.2 | .163 | .164 | . 165 |
| 87.0 | . 157 | . 158 | . 159 | .160 | .16I | .162 | .163 | . 164 | . 166 | . 167 |
| 87.5 | . 158 | . 159 | . 16 I | . 162 | . 163 | . 164 | . 165 | . 166 | . 167 | . 168 |
| 88.0 | -0.160 | -0.161 | -0.162 | $-0.163$ | -0.164 | -0.165 | -0.166 | -0.167 | -0.168 | -0.169 |
| 88.5 | .161 | . 162 | . 163 | . 164 | . 165 | . 166 | . 168 | . 169 | . 170 | . 171 |
| 89.0 | . 162 | . 164 | . 165 | . 166 | . 167 | . 168 | . 169 | . 170 | . 171 | . 172 |
| 89.5 | . 164 | .165 | . 166 | . 167 | . 168 | .169 | . 170 | . 171 | . 173 | . 174 |
| 90.0 | . 165 | . 166 | . 167 | . 168 | . 170 | .171 | . 172 | . 173 | . 174 | . 175 |
| 90.5 | -0.166 | -0.168 | -0.169 | $-0.170$ | -0.171 | -0.172 | -0.173 | -0.174 | -0.175 | -0.176 |
| 91.0 | . 168 | .169 | . 170 | . 171 | . 172 | .173 | . 175 | .176 | . 177 | . 178 |
| 91.5 | . 169 | . 170 | .171 | . 173 | . 174 | . 175 | .176 | .177 | . 178 | . 179 |
| 92.0 | . 170 | .172 | . 173 | . 174 | . 175 | .176 | . 177 | . 178 | . 180 | .18I |
| 92.5 | . 172 | . 173 | . 174 | . 175 | . 176 | . 178 | . 179 | . 180 | .181 | . 182 |
| 93.0 | -0.173 | -0.174 | -0.175 | -0.177 | -0.178 | -0.179 | -0.180 | -0.181 | -0.182 | -0.184 |
| 93.5 | . 174 | .176 | . 177 | . 178 | . 179 | . 180 | .181 | . 183 | . 184 | . 185 |
| 94.0 | . 176 | . 177 | . 178 | . 179 | . 180 | . 182 | .183 | . 184 | . 185 | . 186 |
| 94.5 | . 177 | .178 | . 179 | .181 | . 182 | .183 | . 184 | .185 | . 187 | . 188 |
| 95.0 | . 178 | . 180 | .18I | . 182 | . 183 | . 184 | . 186 | . 187 | . 188 | . 189 |
| 95.5 | -0.180 | -0.181 | -0.182 | -0.183 | -0.185 | -0.186 | -0.187 | -0.188 | -0.189 | -0.191 |
| 96.0 | . 181 | . 182 | . 184 | . 185 | . 186 | . 187 | . 188 | . 190 | .191 | . 192 |
| 96.5 | .182 | . 184 | . 185 | . 186 | . 187 | . 189 | . 190 | . 191 | . 192 | . 193 |
| 97.0 | .184 | .185 | . 186 | . 187 | .189 | . 190 | .191 | . 192 | . 194 | . 195 |
| 97.5 | . 185 | . 186 | . 188 | . 189 | . 190 | .191 | . 193 | . 194 | . 195 | . 196 |
| 98.0 | -0.186 | -0.188 | -0.189 | -0.190 | -0. I9I | -0.193 | -0.194 | -0.195 | -0.196 | -0.198 |
| 98.5 | . 188 | . 189 | . 190 | . 192 | . 193 | . 194 | . 195 | . 197 | . 198 | . 199 |
| 99.0 | . 189 | . 190 | . 192 | . 93 | . 194 | . 195 | . 197 | . 198 | . 199 | . 201 |
| 99.5 | . 190 | .192 | . 193 | . 194 | . 196 | . 197 | . 198 | . 199 | . 201 | . 202 |
| 100.0 | . 192 | . 193 | . 194 | . 196 | . 197 | . 198 | . 200 | . 201 | . 202 | . 203 |

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION TO BE SUBTRACTED.

| Attached Thermometer Centigrade. | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 440 | 450 | 460 | 470 | 480 | 490 | 500 | 510 | 520 | 530 | 540 | 550 | 560 |
| c. | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm . | mm . | mm. | mm . | mm. | mm. |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.5 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 05 |
| 1.0 | . 07 | . 07 | . 08 | . 08 | . 08 | . 08 | . 08 | . 08 | . 08 | . 09 | . 09 | . 09 | . 09 |
| 1.5 | . 11 | . 11 | . II | . 12 | . 12 | . 12 | . 12 | . 12 | . 13 | . 13 | . 13 | . 13 | . 14 |
| 2.0 | . 14 | . 15 | . 15 | . 15 | . 16 | . 16 | . 16 | . 17 | . 17 | . 17 | . 18 | . 18 | . 18 |
| 2.5 | 0.18 | 0.18 | 0.19 | 0. 19 | 0.20 | 0.20 | 0.20 | 0.21 | 0.21 | 0.22 | 0.22 | 0.22 | 0.23 |
| 3.0 | . 22 | . 22 | . 23 | . 23 | . 24 | . 24 | . 24 | . 25 | . 25 | . 26 | . 26 | . 27 | . 27 |
| 3.5 | . 25 | . 26 | . 26 | . 27 | . 27 | . 28 | . 29 | . 29 | . 30 | . 30 | . 31 | . 31 | . 32 |
| 4.0 | . 29 | . 29 | . 30 | . 31 | . 31 | . 32 | . 33 | . 33 | . 34 | . 35 | . 35 | . 36 | . 37 |
| 4.5 | . 32 | . 33 | . 34 | . 35 | . 35 | . 36 | . 37 | . 37 | . 38 | . 39 | . 40 | . 40 | . 41 |
| 5.0 | 0.36 | 0.37 | 0.38 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 |
| $5 \cdot 5$ | . 40 | . 40 | . 41 | . 42 | . 43 | . 44 | . 45 | . 46 | . 47 | . 48 | . 48 | . 49 | . 50 |
| 6.0 | . 43 | . 44 | . 45 | . 46 | . 47 | . 48 | . 49 | . 50 | . 51 | . 52 | . 53 | . 54 | . 55 |
| 6.5 | . 47 | . 48 | . 49 | . 50 | . 51 | . 52 | . 53 | . 54 | . 55 | . 56 | . 57 | . 58 | . 59 |
| 7.0 | . 50 | . 51 | . 53 | . 54 | . 55 | . 56 | . 57 | . 58 | . 59 | . 61 | . 62 | . 63 | . 64 |
| 7.5 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.60 | 0.61 | 0.62 | 0.64 | 0.65 | 0.66 | 0.67 | 0.69 |
| 8 o | . 57 | . 59 | . 60 | .61 | . 63 | . 64 | . 65 | . 67 | . 68 | . 69 | . 70 | . 72 | . 73 |
| 8.5 | .6I | . 62 | . 64 | . 65 | . 67 | . 68 | . 69 | . 71 | . 72 | . 73 | . 75 | . 76 | . 78 |
| 9.0 | . 65 | . 66 | . 68 | . 69 | . 70 | . 72 | . 73 | . 75 | .76 | . 78 | . 79 | .81 | . 82 |
| 9.5 | . 68 | . 70 | . 71 | . 73 | . 74 | . 76 | .77 | . 79 | .8I | . 82 | . 84 | . 85 | . 87 |
| 10.0 | 0.72 | 0.73 | 0.75 | 0.77 | 0.78 | 0.80 | 0.82 | 0.83 | 0.85 | 0.86 | 0.88 | 0.90 | 0.91 |
| 10.5 | . 75 | . 77 | . 79 | . 80 | . 82 | . 84 | . 86 | . 87 | . 89 | . 91 | . 92 | . 94 | . 96 |
| 11.0 | . 79 | .81 | . 83 | . 84 | . 86 | . 88 | . 90 | . 91 | . 93 | . 95 | . 97 | . 99 | 1.00 |
| 11.5 | . 83 | . 84 | . 86 | . 88 | . 90 | . 92 | . 94 | . 96 | . 98 | . 99 | 1.01 | 1.03 | 1.05 |
| 12.0 | . 86 | . 88 | . 90 | . 92 | . 94 | . 96 | . 98 | 1.00 | 1.02 | 1.04 | 1.06 | 1.08 | I. 10 |
| 13.0 | 0.93 | 0.95 | 0.97 | 1.00 | 1.02 | 1.04 | 1.06 | 1.08 | I. 10 | 1.12 | 1. 14 | 1.17 | 1. 19 |
| 14.0 | 1.00 | 1.03 | 1.05 | 1.07 | I. 10 | I. 12 | 1. 14 | 1.16 | I. 19 | 1.21 | 1.23 | 1.25 | 1.28 |
| 15.0 | 1.08 | 110 | I. 12 | 1.15 | I. 17 | 1.20 | 1.22 | 1.25 | 1.27 | I. 30 | 1.32 | I. 34 | I. 37 |
| 16.0 | 1.15 | 1.17 | 1.20 | 1.23 | 1.25 | I. 28 | 1.30 | 1.33 | I. 36 | I. 38 | 1.41 | I. 43 | 1. 46 |
| 17.0 | 1.22 | 1.25 | 1.27 | 1.30 | I. 33 | I. 36 | 1.38 | 1.41 | 1. 44 | 1.47 | 1.50 | 1.52 | 1.55 |
| 18.0 | 1.29 | I. 32 | 1.35 | 1.38 | I.4I | 1.44 | 1.47 | 1.50 | I. 52 | I. 55 | 1.58 | 1.6I | 1.64 |
| 19.0 | 1.36 | I. 39 | 1.42 | 1.45 | I. 49 | 1.52 | 1.55 | 1.58 | 1.61 | 1.64 | 1.67 | 1.70 | 1.73 |
| 20.0 | 1.43 | 1. 47 | 1.50 | 1.53 | 1.56 | 1.60 | 1.63 | 1.66 | I. 69 | 1.73 | 1.76 | 1.79 | 1.82 |
| 21.0 | 1.50 | I. 54 | 1.57 | 1.61 | 1.64 | 1.67 | 1.71 | 1.74 | I. 78 | I. 81 | I. 85 | 1.88 | 1.91 |
| 22.0 | 1.58 | 1.61 | 1.65 | 1.68 | 1.72 | 1.75 | 1.79 | 1.83 | 1.86 | 1.90 | I. 93 | 1.97 | 2.01 |
| 23.0 | 1.65 | 1.68 | I. 72 | 1.76 | 1.80 | 1.83 | 1.87 | 1.91 | 1.95 | 1.98 | 2.02 | 2.06 | 2.10 |
| 24.0 | 1.72 | 1.76 | 1.80 | 1.84 | 1.87 | 1.91 | 1.95 | 1.99 | 2.03 | 2.07 | 2.11 | 2.15 | 2.19 |
| 25.0 | 1.79 | 1.83 | 1.87 | 1.91 | 1.95 | 1.99 | 2.03 | 2.07 | 2.11 | 2.16 | 2.20 | 2.24 | 2.28 |
| 26.0 | 1.86 | 1.90 | 1.95 | 1.99 | 2.03 | 2.07 | 2.11 | 2.16 | 2.20 | 2.24 | 2.28 | 2.33 | 2.37 |
| 27.0 | 1.93 | 1.98 | 2.02 | 2.06 | 2.11 | 2.15 | 2.20 | 2.24 | 2.28 | 2.33 | 2.37 | 2.41 | 2.46 |
| 28.0 | 2.00 | 2.05 | 2.09 | 2.14 | 2.18 | 2.23 | 2.28 | 2.32 | 2.37 | 2.41 | 2.46 | 2.50 | 2.55 |
| 29.0 | 2.07 | 2.12 | 2.17 | 2.22 | 2.26 | 2.31 | 2.36 | 2.40 | 2.45 | 2.50 | 2.55 | 2.59 | 2.64 |
| 30.0 | 2.15 | 2.19 | 2.24 | 2.29 | 2.34 | 2.39 | 2.44 | 2.49 | 2.54 | 2.58 | 2.63 | 2.68 | 2.73 |
| 31.0 | 2.22 | 2.27 | 2.32 | 2.37 | 2.42 | 2.47 | 2.52 | 2.57 | 2.62 | 2.67 | 2.72 | 2.77 | 2.82 |
| 32.0 | 2.29 | 2.34 | 2.39 | 2.44 | 2.50 | 2.55 | 2.60 | 2.65 | 2.70 | 2.76 | 2.81 | 2.86 | 2.91 |
| 33.0 | 2.36 | 2.41 | 2.47 | 2.52 | 2.57 | 2.63 | 2.68 | 2.73 | 2.79 | 2.84 | 2.89 | 2.95 | 3.00 |
| 34.0 | 2.43 | 2.48 | 2.54 | 2.60 | 2.65 | 2.71 | 2.76 | 2.82 | 2.87 | 2.93 | 2.98 | 3.04 | 3.09 |
| . 35.0 | 2.50 | 2.55 | 2.61 | 2.67 | 2.73 | 2.78 | 2.84 | 2.90 | 2.96 | 3.01 | 3.07 | 3.13 | 3.18 |

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 560 mm. |  |  |  |  | HEIGHT OF THE BAROMETER 570 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm. | mm . | mm. | mm. | mm. | mm . | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.05 | 0.07 | 0.00 | 0.02 | 0.04 | 0.06 | 0.07 |
| I | . 09 | . II | . 13 | . 15 | . 16 | . 09 | . II | 13 | . 5 | . 17 |
| 2 | . 18 | . 20 | . 22 | . 24 | . 26 | .19 | . 20 | 22 | . 24 | . 26 |
| 3 | . 27 | . 29 | . 31 | . 33 | . 35 | . 28 | . 30 | . 32 | . 34 | . 35 |
| 4 | . 37 | .38 | . 40 | .42 | . 44 | - 37 | - 39 | . 41 | . 43 | . 45 |
| 5 | 0.46 | 0.48 | 0.49 | 0.51 | 0.53 | 0.47 | 0.48 | 0.50 | 0.52 | 0.54 |
| 6 | . 55 | . 57 | . 58 | . 60 | . 62 | . 56 | . 58 | . 60 | . 61 | . 63 |
| 7 | . 64 | . 66 | . 68 | . 69 | . 71 | . 65 | . 67 | . 69 | . 71 | . 73 |
| 8 | . 73 | . 75 | . 77 | . 79 | . 80 | .74 | . 76 | . 78 | . 80 | . 82 |
| 9 | . 82 | . 84 | . 86 | . 88 | . 90 | . 84 | . 86 | . 87 | . 89 | . 91 |
| 10 | 0.91 | 0.93 | 0.95 | 0.97 | 0.99 | 0.93 | 0.95 | 0.97 | 0.99 | 1.00 |
| 11 | 1.00 | 1.02 | 1,04 | 1.06 | 1.08 | I. 02 | 1.04 | 1.06 | 1.08 | 1.10 |
| 12 | 1.10 | I. II | I. 13 | 1.15 | 1.17 | 1.12 | 1.13 | 1. 15 | 1.17 | 1.19 |
| 13 | 1.19 | 1.20 | 1.22 | 1.24 | 1.26 | I. 21 | 1.23 | 1.25 | 1.26 | 1.28 |
| 14 | 1.28 | 1.30 | 1.31 | 1.33 | I. 35 | 1.30 | 1.32 | 1.34 | 1. 36 | 1.37 |
| 15 | 1.37 | 1.39 | I. 41 | 1.42 | 1.44 | 1.39 | 1.41 | 1.43 | 1.45 | 1.47 |
| 16 | 1.46 | 1.48 | 1.50 | 1.51 | 1.53 | I. 49 | 1.50 | 1.52 | I. 54 | 1.56 |
| 17 | I. 55 | 1.57 | 1.59 | 1.61 | 1.62 | I. 58 | 1.60 | 1.62 | 1.63 | 1.65 |
| 18 | 1.64 | 1.66 | 1.68 | 1.70 | 1.71 | 1.67 | 1.69 | 1.71 | 1.73. | I. 75 |
| 19 | 1.73 | 1.75 | 1.77 | 1.79 | 1.81 | 1.76 | 1.78 | 1.80 | I. 82 | 1.84 |
| 20 | 1.82 | 1.84 | 1.86 | 1.88 | 1.90 | 1.86 | 1.87 | 1.89 | 1.91 | 1.93 |
| 21 | 1.91 | 1.93 | 1.95 | 1.97 | 1.99 | 1.95 | 1.97 | 1.99 | 2.00 | 2.02 |
| 22 | 2.01 | 2.02 | 2.04 | 2.06 | 2.08 | 2.04 | 2.06 | 2.08 | 2. 10 | 2.11 |
| 23 | 2.10 | 2.11 | 2.13 | 2.15 | 2.17 | 2.13 | 2.15 | 2.17 | 2.19 | 2.21 |
| 24 | 2.19 | 2.20 | 2.22 | 2.24 | 2.26 | 2.23 | 2.24 | 2.26 | 2.28 | 2.30 |
| 25 | 2.28 | 2.30 | 2.31 | 2.33 | 2.35 | 2.32 | 2.34 | 2.35 | 2.37 | 2.39 |
| 26 | 2.37 | 2.39 | 2.40 | 2.42 | 2.44 | 2.41 | 2.43 | 2.45 | 247 | 2.48 |
| 27 | 2.46 | 2.48 | 2.49 | 2.51 | 2.53 | 2.50 | 2.52 | 2.54 | 2.56 | 2.58 |
| 28 | 2.55 | 2.57 | 2.59 | 2.60 | 2.62 | 2.59 | 2.61 | 2.63 | 2.65 | 2.67 |
| 29 | 2.64 | 2.66 | 2.68 | 2.69 | 2.71 | 2.69 | 2.71 | 2.72 | 2.74 | 2.76 |
| 30 | 2.73 | 2.75 | 2.77 | 2.78 | 2.80 | 2.78 | 2.80 | 2.82 | 2.83 | 2.85 |
| 31 | 2.82 | 2.84 | 2.86 | 2.87 | 2.89 | 2.87 | 2.89 | 2.91 | 2.93 | 2.94 |
| 32 | 2.91 | 2.93 | 2.95 | 2.97 | 2.98 | 2.96 | 2.98 | 3.00 | 3.02 | 3.04 |
| 33 | 3.00 | 3.02 | 3.04 | 3.06 | 3.07 | 3.06 | 3.07 | 3.09 | 3.11 | 3.13 |
| 34 | 3.09 | 3.11 | 3.13 | 3.15 | 3.16 | 3.15 | 3.17 | 3.18 | 3.20 | 3.22 |
| 35 | 3.18 | 3.20 | 3.22 | 3.24 | 3.25 | 3.24 | 3.26 | 3.28 | 3.29 | $3 \cdot 31$ |

Smithbonian Tables.

Table 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
for temperatures above $0^{\circ}$ centigrade, the correction is to be subtracted.

| Attached Thermometer. | height of the barometer 580 mm . |  |  |  |  | height of the barometer 590 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm . |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 09 | . 11 | .13 | .15 | . 17 | . 10 | . 12 | . 13 | . 15 | .17 |
| 2 | . 19 | . 21 | . 23 | . 25 | . 27 | . 19 | . 21 | . 23 | . 25 | . 27 |
| 3 | . 28 | . 30 | . 32 | . 34 | .36 | . 29 | . 31 | . 33 | $\cdot 35$ | . 37 |
| 4 | . 38 | . 40 | . 42 | . 44 | . 45 | . 39 | . 40 | . 42 | . 44 | . 46 |
| 5 | 0.47 | 0.49 | 0.51 | 0.53 | 0.55 | 0.48 | 0.50 | 0.52 | 0. 54 | 0.56 |
| 6 | . 57 | . 59 | . 61 | . 62 | . 64 | . 58 | . 60 | . 62 | . 64 | . 65 |
| 7 | . 66 | . 68 | . 70 | . 72 | . 74 | . 67 | . 69 | .71 | . 73 | . 75 |
| 8 | . 76 | . 78 | . 79 | .81 | . 83 | . 77 | . 79 | .81 | . 83 | . 85 |
| 9 | . 85 | . 87 | . 89 | .91 | . 93 | . 87 | . 89 | . 90 | . 92 | . 94 |
| 10 | 0.95 | 0.96 | 0.98 | 1.00 | 1.02 | 0.96 | 0.98 | 1.00 | 1.02 | 1.04 |
| 11 | 1.04 | 1.06 | 1.08 | 1.10 | 1.12 | 1.06 | 1.08 | I.10 | 1.12 | 1.14 |
| 12 | I.I3 | 1.15 | 1.17 | 1.19 | 1.21 | 1.15 | 1.17 | I. 19 | I. 21 | 1.23 |
| 13 | 1.23 | 1.25 | 1. 27 | 1.29 | 1. 30 | 1. 25 | I. 27 | I. 29 | 1.31 | I. 33 |
| 14 | 1.32 | I. 34 | I. 36 | 1. 38 | 1.40 | I. 35 | I. 37 | I. 38 | I. 40 | 1.42 |
| 15 | 1.42 | 1.44 | 1.46 | 1. 47 | 1. 49 | I. 44 | 1. 46 | 1. 48 | I. 50 | 1.52 |
| 16 | 1.51 | 1. 53 | 1. 55 | 1. 57 | 1. 59 | I. 54 | I. 56 | 1.58 | 1.60 | ${ }^{1} .61$ |
| 17 | 1.61 | 1.62 | 1. 64 | 1.66 | I. 68 | I. 63 | 1. 65 | 1.67 | I. 69 | 1.71 |
| 18 | 1.70 | 1.72 | 1. 74 | 1.76 | 1.78 | 1. 73 | 1.75 | 1.77 | 1.79 | 1.81 |
| 19 | 1.79 | 1.81 | I. 83 | I. 85 | I. 87 | 1.83 | I. 84 | 1.86 | I. 88 | 1.90 |
| 20 | 1.89 | 1.91 | I. 93 | 1.95 | 1.96 | 1.92 | 1.94 | 1.96 | 1. 98 | 2.00 |
| 21 | 1.98 | 2.00 | 2.02 | 2.04 | 2.06 | 2.02 | 2.04 | 2.06 | 2.07 | 2.09 |
| 22 | 2.08 | 2.10 | 2.11 | 2.13 | 2.15 | 2.11 | 2.13 | 2.15 | 2.17 | 2.19 |
| 23 | 2.17 | 2.19 | 2.21 | 2.23 | 2.25 | 2.21 | 2.23 | 2.25 | 2.27 | 2.28 |
| 24 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 | 2.30 | 2.32 | 2.34 | 2.36 | 2.38 |
| 25 | 2.36 | 2.38 | 2.40 | 2.41 | 2.43 | 2.40 | 2.42 | 2.44 | 2.46 | 2.48 |
| 26 | 2.45 | 2.47 | 2.49 | 2.51 | 2.53 | 2.49 | 2.51 | 2.53 | 2.55 | 2.57 |
| 27 | 2.55 | 2.57 | 2.58 | 2.60 | 2.62 | 2.59 | 2.61 | 2.63 | 2.65 | 2.67 |
| 28 | 2.64 | 2.66 | 2.68 | 2.70 | 2.72 | 2.69 | 2.70 | 2.72 | 2.74 | 2.76 |
| 29 | 2.73 | 2.75 | 2.77 | 2.79 | 2.81 | 2.78 | 2.80 | 2.82 | 2.84 | 2.86 |
| 30 | 2.83 | 2.85 | 2.87 | 2.88 | 2.90 | 2.88 | 2.90 | 2.91 | 2.93 | 2.95 |
| 3 I | 2.92 | 2.94 | 2.96 | 2.98 | 3.00 | 2.97 | 2.99 | 3.01 | 3.03 | 3.05 |
| 32 | 3.02 | 3.03 | 3.05 | 3.07 | 3.09 | 3.07 | 3.09 | 3.11 | 3.12 | 3.14 |
| 33 | 3.11 | 3.13 | 3.15 | 3.16 | 3.18 | 3.16 | 3.18 | 3.20 | 3.22 | 3.24 |
| 34 | 3.20 | 3.22 | 3.24 | 3.26 | 3.28 | 3.26 | 3.28 | 3.30 | 3.31 | 3.33 |
| 35 | 3.30 | 3.31 | 3.33 | 3.35 | 3.37 | 3.35 | 3.37 | 3.39 | 3.41 | 3.43 |

Smithsonian Tables.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
for temperatures above $0^{\circ}$ Centigrade, the correction is to be subtracted.

|  | HEIGHT OF THE BAROMETER 600 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 605 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 12 | . 14 | . 16 | . 18 | 10 | . 12 | . 14 | . 16 | . 18 |
| 2 | . 20 | . 22 | . 24 | . 25 | . 27 | . 20 | . 22 | . 24 | . 26 | . 28 |
| 3 | . 29 | . 31 | . 33 | . 35 | . 37 | . 30 | - 32 | - 34 | . 36 | . 38 |
| 4 | - 39 | .4I | . 43 | . 45 | . 47 | . 40 | . 41 | . 43 | . 45 | . 47 |
| 5 | 0.49 | 0.51 | 0.53 | 0.55 | 0.57 | 0.49 | 0.51 | 0.53 | 0.55 | 0.57 |
| 6 | . 59 | .6I | . 63 | . 65 | . 67 | . 59 | .6I | . 63 | . 65 | . 67 |
| 7 | . 69 | . 70 | . 72 | . 74 | . 76 | . 69 | . 71 | . 73 | . 75 | . 77 |
| 8 | . 78 | . 80 | . 82 | . 84 | . 86 | . 79 | .81 | . 83 | . 85 | . 87 |
| 9 | . 88 | . 90 | . 92 | . 94 | .96 | . 89 | .91 | . 93 | . 95 | . 97 |
| 10 | 0.98 | 1.00 | 1.02 | 1.04 | 1.06 | 0.99 | 1.01 | 1.03 | 1.05 | 1.07 |
| II | 1.08 | I. 10 | 1.12 | I. 13 | I. 15 | 1.09 | 1.10 | 1.12 | 1.14 | 1.16 |
| 12 | I. 17 | I. 19 | 1.21 | 1.23 | I. 25 | 1.18 | 1.20 | 1.22 | 1.24 | 1.26 |
| 13 | 1.27 | I. 29 | 1.31 | 1.33 | I. 35 | 1.28 | 1.30 | 1.32 | 1.34 | 1.36 |
| 14 | I. 37 | I. 39 | 1.41 | 1.43 | I. 45 | 1.38 | 1.40 | I. 42 | 1.44 | I. 46 |
| 15 | 1.47 | 1.49 | 1.51 | 1.53 | 1.54 | 1.48 | 1.50 | 1.52 | 1.54 | 1.56 |
| 16 | 1.56 | 1.58 | 1.60 | 1.62 | 1.64 | I. 58 | 1.60 | 1.62 | 1.64 | 1.66 |
| 17 | 1.66 | 1.68 | 1.70 | 1.72 | 1.74 | 1.68 | 1.70 | 1.71 | 1.73 | 1.75 |
| 18 | 1.76 | 1.78 | 1.80 | 1.82 | 1.84 | 1.77 | 1.79 | 1.81 | 1.83 | 1.85 |
| 19 | r. 86 | 1.88 | 1.90 | 1.91 | 1.93 | 1.87 | I. 89 | 1.91 | 1.93 | 1.95 |
| 20 | 1.95 | 1.97 | 1.99 | 2.01 | 2.03 | 1.97 | 1.99 | 2.01 | 2.03 | 2.05 |
| 21 | 2.05 | 2.07 | 2.09 | 2.11 | 2.13 | 2.07 | 2.09 | 2.11 | 2.13 | 2.15 |
| 22 | 2.15 | 2.17 | 2.19 | 2.21 | 2.23 | 2.17 | 2.19 | 2.21 | 2.23 | 2.24 |
| 23 | 2.25 | 2.26 | 2.28 | 2.30 | 2.32 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 |
| 24 | 2.34 | 2.36 | 2.38 | 2.40 | 2.42 | 2.36 | 2.38 | 2.40 | 2.42 | 2.44 |
| 25 | 2.44 | 2.46 | 2.48 | 2.50 | 2.52 | 2.46 | 2.48 | 2.50 | 2.52 | 2.54 |
| 26 | 2.54 | 2.56 | 2.58 | 2.60 | 2.61 | 2.56 | 2.58 | 2.60 | 2.62 | 2.64 |
| 27 | 2.63 | 2.65 | 2.67 | 2.69 | 2.71 | 2.66 | 2.68 | 2.70 | 2.71 | 2.73 |
| 28 | 2.73 | 2.75 | 2.77 | 2.79 | 2.81 | 2.75 | 2.77 | 2.79 | 2.8 I | 2.83 |
| 29 | 2.83 | 2.85 | 2.87 | 2.89 | 2.91 | 2.85 | 2.87 | 2.89 | 2.91 | 2.93 |
| 30 | 2.93 | 2.94 | 2.96 | 2.98 | 3.00 | 2.95 | 2.97 | 2.99 | 3.01 | 3.03 |
| 31 | 3.02 | 3.04 | 3.06 | 3.08 | 3.10 | 3.05 | 3.07 | 3.09 | 3.11 | 3.13 |
| 32 | 3.12 | 3.14 | 3.16 | 3.18 | 3.20 | 3.15 | 3.16 | 3.18 | 3.20 | 3.22 |
| 33 | 3.22 | 3.24 | 3.25 | 3.27 | 3.29 | 3.24 | 3.26 | 3.28 | 3.30 | 3.32 |
| 34 | 3.31 | 3.33 | 3.35 | 3.37 | 3.39 | 3.34 | 3.36 | 3.38 | 3.40 | 3.42 |
| 35 | 3.4 I | 3.43 | 3.45 | 3.47 | 3.49 | 3.44 | 3.46 | 3.48 | 3.50 | 3.52 |

Smithbonian Tables.

TAble 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
for temperatures above $0^{\circ}$ Centigrade, the correction is to be subtracted.

|  | height of the barometer 610 mm. |  |  |  |  | HEIGHT OF THE BAROMETER 615 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm. | mm. | mm . | mm . | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | 12 | . 14 | . 16 | . 18 | . 10 | . 12 | . 14 | . 16 | . 18 |
| 2 | . 20 | . 22 | . 24 | . 26 | . 28 | . 20 | . 22 | . 24 | . 26 | . 28 |
| 3 | . 30 | . 32 | . 34 | . 36 | .38 | . 30 | . 32 | . 34 | .36 | . 38 • |
| 4 | . 40 | . 42 | . 44 | .46 | .48 | . 40 | .42 | . 44 | .46 | . 48 |
| 5 | 0.50 | 0.52 | 0.54 | 0.56 | 0.58 | 0.50 | 0.52 | 0.54 | 0.56 | 0.58 |
| 6 | . 60 | . 62 | . 64 | . 66 | . 68 | . 60 | . 62 | . 64 | . 66 | . 68 |
| 7 | . 70 | .72 | .74 | .76 | . 78 | . 70 | .72 | . 74 | .76 | . 78 |
| 8 | . 80 | . 82 | . 84 | . 86 | . 88 | . 80 | . 82 | . 84 | . 86 | . 88 |
| 9 | .90 | .92 | . 94 | .96 | . 98 | . 90 | .92 | . 94 | . 96 | .98 |
| 10 | 0.99 | I.OI | 1.03 | 1.05 | 1.07 | 1.00 | 1.02 | 1.04 | 1.06 | 1. 08 |
| II | 1.09 | I.II | I. 13 | I. 15 | 1.17 | 1.10 | 1.12 | 1. 14 | 1.16 | I. 18 |
| 12 | I. 19 | 1.21 | 1.23 | 1.25 | 1.27 | 1.20 | 1.22 | 1.24 | I. 26 | 1.28 |
| 13 | I. 29 | 1.31 | 1.33 | I. 35 | 1.37 | 1.30 | 1.32 | I. 34 | I. 36 | I. 38 |
| 14 | I. 39 | 1.4I | r. 43 | 1.45 | 1.47 | I. 40 | I. 42 | 1.44 | I. 46 | 1.48 |
| 15 | I. 49 | 1.5I | 1.53 | I. 55 | 1.57 | 1.50 | 1.52 | 1. 54 | 1. 56 | 1.58 |
| 16 | I. 59 | I.6I | 1.63 | 1.65 | 1.67 | I. 60 | 1.62 | 1.64 | 1.66 | 1.68 |
| 17 | I. 69 | 1.71 | 1.73 | 1.75 | 1.77 | 1.70 | 1. 72 | 1.74 | I. 76 | 1.78 |
| 18 | 1.79 | 1.81 | 1.83 | 1.85 | 1.87 | 1.80 | 1.82 | I. 84 | I. 86 | I. 88 |
| 19 | 1.89 | 1.91 | 1.93 | 1.95 | 1. 97 | 1.90 | 1.92 | I. 94 | 1. 96 | I. 98 |
| 20 | 1.99 | 2.01 | 2.03 | 2.05 | 2.07 | 2.00 | 2.02 | 2.04 | 2.06 | 2.08 |
| 21 | 2.09 | 2.10 | 2.12 | 2.14 | 2.16 | 2.10 | 2.12 | 2.14 | 2.16 | 2.18 |
| 22 | 2.18 | 2.20 | 2.22 | 2.24 | 2.26 | 2.20 | 2.22 | 2.24 | 2.26 | 2.28 |
| 23 | 2.28 | 2.30 | 2.32 | 2.34 | 2.36 | 2.30 | 2.32 | 2.34 | 2.36 | 2.38 |
| 24 | 2.38 | 2.40 | 2.42 | 2.44 | 2.46 | 2.40 | 2.42 | 2.44 | 2.46 | 2.48 |
| 25 | 2.48 | 2.50 | 2.52 | 2.54 | 2.56 | 2.50 | 2.52 | 2.54 | 2.56 | 2.58 |
| 26 | 2.58 | 2.60 | 2.62 | 2.64 | 2.66 | 2.60 | 2.62 | 2.64 | 2.66 | 2.68 |
| 27 | 2.68 | 2.70 | 2.72 | 2.74 | 2.76 | 2.70 | 2.72 | 2.74 | 2.76 | 2.78 |
| 28 | 2.78 | 2.80 | 2.82 | 2.84 | 2.86 | 2.80 | 2.82 | 2.84 | 2.86 | 2.88 |
| 29 | 2.88 | 2.90 | 2.91 | 2.93 | 2.95 | 2.90 | 2.92 | 2.94 | 2.96 | 2.98 |
| 30 | 2.97 | 2.99 | 3.01 | 3.03 | 3.05 | 3.00 | 3.02 | 3.04 | 3.06 | 3.08 |
| 3 I | 3.07 | 3.09 | 3.11 | 3.13 | 3.15 | 3.10 | 3.12 | 3.14 | 3.16 | 3.18 |
| 32 | 3.17 | 3.19 | 3.21 | 3.23 | 3.25 | 3.20 | 3.22 | 3.24 | 3.26 | 3.28 |
| 33 | 3.27 | 3.29 | 3.3 I | 3.33 | 3.35 | 3.30 | $3 \cdot 32$ | 3.34 | $3 \cdot 36$ | 3.38 |
| 34 | 3.37 | 3.39 | 3.41 | 3.43 | 3.45 | 3.40 | 3.42 | 3.44 | 3.46 | 3.46 |
| 35 | 3.47 | 3.49 | 3.51 | 3.53 | 3.55 | 3.49 | 3.51 | 3.53 | 3.55 | 3.57 |

Smitheonian Tableg.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | heigirt of tie barometer 620 mm . |  |  |  |  | heigit of the barometer 625 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | min. | mm . | mm . | mm. | mm . | mm. | mm. | mm . |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 12 | . 14 | . 16 | . 18 | . 10 | . 12 | . 14 | . 16 | . 18 |
| 2 | . 20 | . 22 | . 24 | . 26 | . 28 | . 20 | . 22 | . 24 | . 27 | . 29 |
| 3 | . 30 | . 32 | - 34 | . 36 | . 3 S | . 31 | . 33 | . 35 | - 37 | - 39 |
| 4 | . 40 | . 43 | . 45 | . 47 | . 49 | . 41 | . 43 | . 45 | . 47 | . 49 |
| 5 | 0.51 | 0.53 | 0.55 | 0.57 | 0.59 | 0.51 | 0.53 | 0.55 | 0.57 | 0.59 |
| 6 | .61 | . 63 | . 65 | . 67 | . 69 | .61 | . 63 | . 65 | . 67 | . 69 |
| 7 | . 71 | . 73 | . 75 | - 77 | . 79 | .71 | . 73 | . 75 | . 78 | . 80 |
| 8 | .8r | . 83 | . 85 | . 87 | . 89 | . 82 | . 84 | . 86 | . 88 | . 90 |
| 9 | .91 | . 93 | . 95 | . 97 | . 99 | . 92 | . 94 | . 96 | . 98 | 1.00 |
| 10 | 1.OI | 1.03 | 1.05 | 1.07 | 1.09 | 1.02 | 1.04 | 1.06 | 1.08 | I. 10 |
| II | I.II | I. 13 | I. 15 | I. 17 | I. 19 | I. 12 | I. 14 | I. 16 | I. 18 | 1.20 |
| 12 | I. 21 | 1.23 | 1.25 | 1.27 | 1.29 | 1.22 | I. 24 | 1.26 | I. 28 | I. 30 |
| 13 | 1.31 | 1.33 | I. 35 | 1.37 | I. 39 | 1.32 | 1.34 | I. 37 | 1.39 | I. 41 |
| 14 | I.4I | 1.43 | 1.46 | 1.48 | 1.50 | 1.43 | 1.45 | 1.47 | 1.49 | 1.51 |
| 15 | 1.52 | 1.54 | 1.56 | 1.58 | 1.60 | 1.53 | 1.55 | 1.57 | 1.59 | 1.61 |
| 16 | t. 62 | 1.64 | 1.65 | 1.63 | 1.70 | 1.63 | I. 65 | 1.67 | 1.69 | 1.71 |
| 17 | 1.72 | 1.74 | 1.76 | 1.78 | 1.80 | 1.73 | 1.75 | 1.77 | 1.79 | 1.81 |
| 18 | 1.82 | 1.84 | 1.86 | 1.88 | 1.90 | 1.83 | 1.85 | 1.87 | 1.89 | 1.91 |
| 19 | 1.92 | 1.94 | I. 96 | 1.98 | 2.00 | 1.93 | I. 95 | 1.97 | 1.99 | 2.01 |
| 20 | 2.02 | 2.04 | 2.06 | 2.08 | 2. 10 | 2.04 | 2.06 | 2.08 | 2.10 | 2.12 |
| 21 | 2. 12 | 2.14 | 2.16 | 2.18 | 2.20 | 2.14 | 2.16 | 2. 18 | 2.20 | 2.22 |
| 22 | 2.22 | 2.24 | 2.26 | 2.28 | 2.30 | 2.24 | 2.26 | 2.28 | 2.30 | 2.32 |
| 23 | 2.32 | 2.34 | 2.36 | 2.38 | 2.40 | 2.34 | 2.36 | 2.38 | 2.40 | 2.42 |
| 24 | 2.42 | 2.44 | 2.45 | 2.48 | 2.50 | 2.44 | 2.46 | 2.48 | 2.50 | 2.52 |
| 25 | 2.52 | 2.54 | 2.56 | 2.58 | 2.60 | 2.54 | 2.56 | 2.58 | 2.60 | 2.62 |
| 26 | 2.62 | 2.64 | 2.66 | 2.68 | 2.70 | 2.64 | 2.66 | 2.68 | 2.70 | 2.72 |
| 27 | 2.72 | 2.74 | 2.76 | 2.78 | 2.80 | 2.74 | 2.76 | 2.78 | 2.80 | 2.82 |
| 28 | 2.82 | 2.84 | 2.86 | 2.88 | 2.90 | 2.85 | 2.87 | 2.89 | 2.91 | 2.93 |
| 29 | 2.92 | 2.94 | 2.96 | 2.98 | 3.00 | 2.95 | 2.97 | 2.99 | 3.01 | 3.03 |
| 30 | 3.02 | 3.04 | 3.06 | 3.08 | 3.10 | 3.05 | 3.07 | 3.09 | 3.11 | 3.13 |
| 3 I | 3.12 | 3.14 | 3.16 | 3.18 | 3.20 | 3.15 | 3.17 | 3.19 | 3.21 | 3.23 |
| 32 | 3.22 | 3.24 | 3.26 | 3.28 | 3.30 | 3.25 | 3.27 | 3.29 | $3 \cdot 3 \mathrm{I}$ | 3.33 |
| 33 | 3.32 | $3 \cdot 34$ | 3.36 | 3.38 | 3.40 | 3.35 | 3.37 | 3.39 | 3.4 I | 3.43 |
| 34 | 3.42 | 3.44 | 3.46 | 3.48 | 3.50 | 3.45 | 3.47 | 3.49 | 3.51 | 3.53 |
| 35 | $3 \cdot 52$ | 3.54 | 3.56 | 3.58 | 3.60 | 3.55 | 3.57 | 3.59 | 3.61 | 3.63 |

Smithsonian Tables.

TAble 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 630 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 635 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 12 | . 14 | . 16 | . 19 | . 10 | . 12 | . 15 | . 17 | . 19 |
| 2 | . 21 | . 23 | . 25 | . 27 | . 29 | . 21 | . 23 | . 25 | . 27 | . 29 |
| 3 | . 31 | - 33 | . 35 | $\cdot 37$ | . 39 | . 31 | . 33 | . 35 | . 37 | . 39 |
| 4 | . 41 | . 43 | . 45 | . 47 | . 49 | . 41 | . 44 | .46 | . 48 | . 50 |
| 5 | 0.51 | 0.53 | 0.56 | 0.58 | 0.60 | 0.52 | 0.54 | 0.56 | 0.58 | 0.60 |
| 6 | . 62 | . 64 | . 66 | . 68 | . 70 | . 62 | . 64 | . 66 | . 68 | . 70 |
| 7 | . 72 | . 74 | .76 | .78 | . 80 | . 73 | . 75 | . 77 | .79 | .81 |
| 8 | . 82 | . 84 | . 86 | . 88 | . 90 | . 83 | . 85 | . 87 | . 89 | .91 |
| 9 | . 92 | . 95 | . 97 | . 99 | I. OI | -93 | . 95 | . 97 | . 99 | 1.02 |
| 10 | 1.03 | 1.05 | 1.07 | 1.09 | I.II | 1.04 | 1.06 | 1.08 | 1.10 | I. 12 |
| II | I. 13 | 1.15 | 1.17 | 1. 19 | 1.21 | 1.14 | 1.16 | 1. 18 | 1.20 | 1.22 |
| 12 | 1.23 | 1.25 | 1.27 | 1.29 | I. 3 I | 1.24 | I. 26 | 1.28 | 1.30 | 1.33 |
| 13 | 1.34 | 1.36 | 1.38 | 1.40 | 1.42 | 1.35 | 1.37 | 1.39 | I. 41 | 1.43 |
| 14 | 1.44 | I. 46 | 1.48 | 1. 50 | 1.52 | 1.45 | 1.47 | 1.49 | 1.51 | 1.53 |
| 15 | 1.54 | 1.56 | 1.58 | 1.60 | 1.62 | 1.55 | 1.57 | 1.59 | 1.6r | 1.63 |
| 16 | I. 64 | 1.66 | 1.68 | 1.70 | 1.72 | 1.66 | 1.68 | 1.70 | 1.72 | 1.74 |
| 17 | 1.74 | 1.77 | 1.79 | 1.81 | 1.83 | 1.76 | 1.78 | 1.80 | 1.82 | 1.84 |
| 18 | 1.85 | 1.87 | I. 89 | 1.91 | 1.93 | 1.86 | 1.88 | 1.90 | 1.92 | 1.94 |
| 19 | 1.95 | 1.97 | 1.99 | 2.01 | 2.03 | 1.96 | 1.99 | 2.01 | 2.03 | 2.05 |
| 20 | 2.05 | 2.07 | 2.09 | 2.11 | 2.13 | 2.07 | 2.09 | 2.11 | 2.13 | 2.15 |
| 21 | 2.15 | 2.17 | 2.19 | 2.21 | 2.24 | 2.17 | 2.19 | 2.21 | 2.23 | 2.25 |
| 22 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 | 2.27 | 2.29 | 2.31 | 2.34 | 2.36 |
| 23 | 2.36 | 2.38 | 2.40 | 2.42 | 2.44 | 2.38 | 2.40 | 2.42 | 2.44 | 2.46 |
| 24 | 2.46 | 2.48 | 2.50 | 2.52 | 2.54 | 2.48 | 2.50 | 2.52 | 2.54 | 2.56 |
| 25 | 2.56 |  | 2.60 | 2.62 | 2.64 | 2.58 | 2.60 | 2.62 | 2.64 | 2.66 |
| 26 | 2.66 | 2.68 | 2.70 | 2.73 | 2.75 | 2.69 | 2.71 | 2.73 | 2.75 | 2.77 |
| 27 | 2.77 | 2.79 | 2.81 | 2.83 | 2.85 | 2.79 | 2.81 | 2.83 | 2.85 | 2.87 |
| 28 | 2.87 | 2.89 | 2.91 | 2.93 | 2.95 | 2.89 | 2.91 | 2.93 | 2.95 | 2.97 |
| 29 | 2.97 | 2.99 | 3.01 | 3.03 | 3.05 | 2.99 | 3.01 | 3.03 | 3.05 | 3.08 |
| 30 | 3.07 | 3.09 | 3.11 | 3.13 | 3.15 | 3.10 | 3.12 | 3.14 | 3.16 | 3.18 |
| 3 I | 3.17 | 3.19 | 3.21 | 3.23 | 3.25 | 3.20 | 3.22 | 3.24 | 3.26 | 3.28 |
| 32 | 3.28 | 3.30 | 3.32 | 3.34 | 3.36 | 3.30 | 3.32 | 3.34 | 3.36 | 3.38 |
| 33 | 3.38 | 3.40 | 3.42 | 3.44 | 3.46 | 3.40 | 3.42 3.53 | 3.44 | 3.47 | 3.49 |
| 34 | 3.48 | 3.50 | 3.52 | 3.54 | 3.56 | 3.51 | 3.53 | 3.55 | 3.57 | 3.59 |
| 35 | 3.58 | 3.60 | 3.62 | 3.64 | 3.66 | 3.6 I | 3.63 | 3.65 | 3.67 | 3.69 |

Smithoonian Tables.

Table 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
for temperatures above $0^{\circ}$ centigrade, the correction is to be subtracted.

|  | height of the barometer 640 mm . |  |  |  |  | height of the barometer 645 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm . | mm. | mm. | mm. | mm . | mm . | mm. | mm . |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 13 | . 15 | . 17 | . 19 | . II | . 13 | . 15 | . 17 | . 19 |
| 2 | . 21 | . 23 | . 25 | . 27 | . 29 | . 21 | . 23 | . 25 | . 27 | . 29 |
| 3 | . 31 | . 33 | . 36 | . 38 | . 40 | . 32 | . 34 | . 36 | . 38 | . 40 |
| 4 | . 42 | . 44 | . 46 | . 48 | . 50 | . 42 | . 44 | .46 | .48 | . 51 |
| 5 | 0.52 | 0.54 | 0.56 | 0.59 | 0.6I | 0.53 | 0.55 | 0.57 | 0.59 | 0.61 |
| 6 | . 63 | . 65 | . 67 | . 69 | . 71 | . 63 | . 65 | . 67 | . 69 | . 72 |
| 7 | . 73 | . 75 | . 77 | . 79 | . 81 | . 74 | . 76 | . 78 | . 80 | . 82 |
| 8 | . 84 | . 86 | . 88 | . 90 | . 92 | . 84 | . 86 | . 88 | . 90 | . 93 |
| 9 | . 94 | .96 | .98 | 1.00 | 1.02 | . 95 | . 97 | . 99 | I.OI | 1. 03 |
| 10 | 1.04 | r. 06 | 1.09 | I.II | 1.13 | 1.05 | 1.07 | 1.09 | 1.12 | I. 14 |
| II | I. 15 | 1.17 | I. 19 | 1.21 | 1.23 | 1. 16 | I. 18 | 1.20 | 1.22 | 1.24 |
| 12 | 1.25 | 1.27 | 1.29 | 1.31 | 1.34 | 1.26 | I. 28 | 1.30 | 1.32 | 1.35 |
| 13 | I. 36 | 1.38 | 1.40 | 1.42 | I. 44 | I. 37 | I. 39 | I. 41 | 1.43 | 1.45 |
| 14 | I. 46 | r. 48 | 1.50 | 1.52 | 1.54 | r. 47 | I. 49 | 1.5I | 1.53 | I. 56 |
| 15 | 1.56 | 1.59 | 1.6I | 1.63 | 1. 65 | 1.58 | 1. 60 | 1.62 | 1. 64 | 1.66 |
| 16 | 1.67 | 1.69 | 1.71 | 1.73 | 1.75 | 1. 68 | 1.70 | 1.72 | 1.74 | 1.77 |
| 17 | 1.77 | 1.79 | I.8I | 1.83 | 1.86 | 1.79 | I.8I | 1.83 | 1.85 | 1. 87 |
| 18 | 1.88 | 1.90 | 1.92 | 1.94 | 1.96 | 1.89 | I. 91 | 1.93 | 1.95 | 1.97 |
| 19 | 1.98 | 2.00 | 2.02 | 2.04 | 2.06 | 2.00 | 2.02 | 2.04 | 2.06 | 2.08 |
| 20 | 2.08 | 2.10 | 2.13 | 2. 15 | 2.17 | 2.10 | 2.12 | 2.14 | 2.16 | 2.18 |
| 21 | 2.19 | 2.21 | 2.23 | 2.25 | 2.27 | 2.20 | 2.23 | 2.25 | 2.27 | 2.29 |
| 22 | 2.29 | 2.31 | 2.33 | 2.35 | 2.37 | 2.31 | 2.33 | 2.35 | 2.37 | 2.39 |
| 23 | 2.40 | 2.42 | 2.44 | 2.46 | 2.48 | 2.41 | 2.43 | 2.46 | 2.48 | 2.50 |
| 24 | 2.50 | 2.52 | 2.54 | 2.56 | 2.58 | 2.52 | 2.54 | 2.56 | 2.58 | 2.60 |
| 25 | 2.60 | 2.62 | 2.64 | 2.66 | 2.69 | 2.62 | 2.64 | 2.66 | 2.69 | 2.71 |
| 26 | 2.71 | 2.73 | 2.75 | 2.77 | 2.79 | 2.73 | 2.75 | 2.77 | 2.79 | 2.81 |
| 27 | 2.8 I | 2.83 | 2.85 | 2.87 | 2.89 | 2.83 | 2.85 | 2.87 | 2.89 | 2.92 |
| 28 | 2.91 | 2.93 | 2.95 | 2.98 | 3.00 | 2.94 | 2.96 | 2.98 | 3.00 | 3.02 |
| 29 | 3.02 | 3.04 | 3.06 | 3.08 | 3.10 | 3.04 | 3.06 | 3.08 | 3.10 | 3.12 |
| 30 | 3.12 | 3.14 | 3.16 | 3.18 | 3.20 | 3.14 | 3.17 | 3.19 | 3.21 | 3.23 |
| 3 I | 3.22 | 3.24 | 3.27 | 3.29 | 3.31 | 3.25 | 3.27 | 3.29 | 3.31 | 3.33 |
| 32 | 3.33 | 3.35 | $3 \cdot 37$ | $3 \cdot 39$ | 3.41 | 3.35 | 3.37 | 3.39 | 3.42 | 3.44 |
| 33 | 3.43 | 3.45 | 3.47 3.58 | 3.49 | 3.51 | 3.46 | 3.48 | 3.50 | 3.52 | 3.54 |
| 34 | 3.53 | 3.55 | 3.58 | 3.60 | 3.62 | 3.56 | 3.58 | 3.60 | 3.62 | 3.64 |
| 35 | 3.64 | 3.66 | 3.68 | 3.70 | 3.72 | 3.67 | 3.69 | 3.71 | 3.73 | 3.75 |

Smithbonian Tables.

TAble 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

## METRIC MEASURES.

for temperatures above $0^{\circ}$ centigrade, the correction is to be subtracted.

|  | height of the barometer 650 mm . |  |  |  |  | height of the barometer 655 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.09 |
| 1 | .II | . 13 | . 15 | . 17 | . 19 | . 11 | .13 | . 15 | . 17 | . 19 |
| 2 | . 21 | . 23 | . 25 | . 28 | . 30 | . 21 | . 24 | . 26 | . 28 | . 30 |
| 3 | . 32 | . 34 | . 36 | .38 | . 40 | . 32 | . 34 | . 36 | . 39 | . 41 |
| 4 | . 42 | . 45 | . 47 | . 49 | .51 | . 43 | . 45 | . 47 | . 49 | . 51 |
| 5 | 0.53 | 0.55 | 0.57 | 0.59 | 0.62 | 0.53 | 0.56 | 0. 58 | 0.60 | 0.62 |
| 6 | . 64 | . 66 | . 68 | . 70 | . 72 | . 64 | . 66 | . 68 | .71 | . 73 |
| 7 | . 74 | . 76 | . 78 | .81 | . 83 | . 75 | . 77 | . 79 | . 81 | . 83 |
| 8 | . 85 | . 87 | . 89 | . 91 | . 93 | . 85 | . 88 | . 90 | . 92 | . 94 |
| 9 | . 95 | . 98 | 1.00 | 1.02 | I. 04 | . 96 | . 98 | 1.00 | 1.03 | 1.05 |
| 10 | 1. 06 | 1.08 | 1.10 | 1.12 | I. 14 | 1.07 | 1.09 | 1.11 | I. 13 | I. 15 |
| 11 | 1.17 | I. 19 | 1.21 | 1.23 | I. 25 | 1.17 | 1.20 | 1.22 | 1.24 | 1. 26 |
| 12 | 1.27 | I. 29 | 1.31 | I. 34 | I. 36 | 1.28 | 1.30 | 1.32 | 1. 35 | I. 37 |
| 13 | I. 38 | 1.40 | 1.42 | I. 44 | I. 46 | 1. 39 | I.41 | 1.43 | I. 45 | 1.47 |
| 14 | I. 48 | 1.50 | 1.53 | I. 55 | 1. 57 | I. 49 | I. 52 | 1.54 | 1. 56 | I. 58 |
| 15 | 1. 59 | 1.61 | 1. 63 | 1. 65 | І. 67 | ı.60 | 1. 62 | 1.64 | 1. 66 | 1.69 |
| 16 | I. 69 | 1.72 | 1.74 | 1.76 | 1. 78 | 1.71 | 1.73 | 1.75 | 1.77 | 1.79 |
| 17 | 1.80 | 1.82 | 1.84 | I. 86 | 1.88 | I.81 | 1.84 | 1.86 | 1.88 | I. 90 |
| 18 | 1.91 | 1.93 | 1.95 | 1.97 | 1.99 | 1.92 | I. 94 | 1.96 | 1.98 | 2.01 |
| 19 | 2.01 | 2.03 | 2.05 | 2.07 | 2.10 | 2.03 | 2.05 | 2.07 | 2.09 | 2.11 |
| 20 | 2.12 | 2.14 | 2.16 | 2.18 | 2.20 | 2.13 | 2.15 | 2.18 | 2.20 | 2.22 |
| 21 | 2.22 | 2.24 | 2.26 | 2.29 | 2.31 | 2.24 | 2.26 | 2.28 | 2.30 | 2.32 |
| 22 | 2.33 | 2.35 | 2.37 | 2.39 | 2.41 | 2.35 | 2.37 | 2.39 | 2.41 | 2.43 |
| 23 | 2.43 | 2.45 | 2.47 | 2.50 | 2.52 | 2.45 | 2.47 | 2.49 | 2.52 | 2.54 |
| 24 | 2.54 | 2.56 | 2.58 | 2.60 | 2.62 | 2.56 | 2.58 | 2.60 | 2.62 | 2.64 |
| 25 | 2.64 | 2.66 | 2.69 | 2.71 | 2.73 | 2.66 | 2.68 | 2.71 | 2.73 | 2.75 |
| 26 | 2.75 | 2.77 | 2.79 | 2.81 | 2.83 | 2.77 | 2.79 | 2.81 | 2.83 | 2.85 |
| 27 | 2.85 | 2.87 | 2.90 | 2.92 | 2.94 | 2.88 | 2.90 | 2.92 | 2.94 | 2.96 |
| 28 | 2.96 | 2.98 | 3.00 | 3.02 | 3.04 | 2.98 | 3.00 | 3.02 | 3.05 | 3.07 |
| 29 | 3.06 | 3.08 | 3.11 | 3.13 | 3.15 | 3.09 | 3.11 | 3.13 | 3.15 | 3.17 |
| 30 | 3.17 | 3.19 | 3.21 | 3.23 | 3.25 | 3.19 | 3.21 | 3.24 | 3.26 | 3.28 |
| 31 | 3.27 | 3.30 | 3.32 | 3.34 | 3.36 | 3.30 | 3.32 | 3.34 | 3.36 | 3.38 |
| 32 | 3.38 | 3.40 | 3.42 | 3.44 | 3.46 | 3.41 | 3.43 | 3.45 | 3.47 | 3.49 |
| 33 | 3.48 | 3.51 | 3.53 | 3.55 | - 3.57 | 3.51 | 3.53 | 3.55 | 3.57 | 3.60 |
| 34 | 3.59 | 3.61 | 3.63 | 3.65 | 3.67 | 3.62 | 3.64 | 3.66 | 3.68 | 3.70 |
| 35 | 3.69 | 3.71 | 3.74 | 3.76 | 3.78 | 3.72 | 3.74 | 3.76 | 3.79 | 3.81 |

Smithsonian Tables.

## METRIC MEASURES.

for temperatures above $0^{\circ}$ Centigrade, the correction is to be subtracted.

|  | HEIGHT OF THE BAROMETER 660 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 665 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.09 | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 |
| 1 | . II | . 13 | . 15 | . 17 | . 19 | . II | . 13 | . 15 | . 17 | . 20 |
| 2 | . 22 | . 24 | . 26 | . 28 | . 30 | . 22 | . 24 | . 26 | . 28 | . 30 |
| 3 | . 32 | . 34 | . 37 | . 39 | . 41 | . 33 | . 35 | - 37 | - 39 | . 41 |
| 4 | . 43 | . 45 | . 47 | . 50 | . 52 | . 43 | . 46 | . 48 | . 50 | . 52 |
| 5 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.54 | 0.56 | 0.59 | 0.6I | 0.63 |
| 6 | . 65 | . 67 | . 69 | . 71 | . 73 | . 65 | . 67 | . 69 | . 72 | . 74 |
| 7 | . 75 | . 78 | . 80 | . 82 | . 84 | .76 | . 78 | . 80 | . 82 | . 85 |
| 8 | . 86 | . 88 | . 90 | . 93 | . 95 | . 87 | . 89 | .91 | . 93 | . 95 |
| 9 | . 97 | . 99 | I. OI | I. 03 | 1.05 | . 98 | 1.00 | 1.02 | 1.04 | 1.06 |
| 10 | 1. 08 | I. 10 | 1.12 | I. 14 | I. 16 | 1.08 | I. II | 1. 13 | 1.15 | 1. 17 |
| II | I. 18 | 1.21 | 1.23 | 1.25 | 1.27 | I. 19 | 1.21 | 1.24 | 1.26 | 1.28 |
| 12 | I. 29 | 1.31 | 1.33 | I. 36 | I. 38 | 1.30 | 1.32 | 1.34 | 1.37 | 1.39 |
| 13 | 1.40 | 1.42 | 1.44 | 1.46 | 1.48 | I.4I | 1. 43 | 1.45 | 1.47 | 1.50 |
| 14 | 1.5I | I. 53 | L. 55 | 1.57 | I. 59 | 1.52 | I. 54 | I. 56 | 1.58 | 1.60 |
| 15 | 1.61 | 1.63 | 1.66 | 1. 68 | 1.70 | 1.63 | 1.65 | 1.67 | 1.69 | 1.71 |
| 16 | 1.72 | 1.74 | 1.76 | 1.78 | I.8I | 1.73 | 1.76 | 1.78 | 1.80 | 1.82 |
| 17 | 1.83 | 1.85 | 1.87 | 1.89 | 1.91 | I. 84 | I. 86 | 1.88 | 1.91 | 1.93 |
| I8 | 1.93 | 1.96 | 1.98 | 2.00 | 2.02 | 1.95 | 1.97 | 1.99 | 2.01 | 2.04 |
| 19 | 2.04 | 2.06 | 2.08 | 2.11 | 2.13 | 2.06 | 2.08 | 2. 10 | 2.12 | 2.14 |
| 20 | 2.15 | 2.17 | 2. 19 | 2.21 | 2.23 | 2. I7 | 2.19 | 2.21 | 2.23 | 2.25 |
| 21 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 | 2.27 | 2.29 | 2.32 | 2.34 | 2.36 |
| 22 | 2.36 | 2.38 | 2.41 | 2.43 | 2.45 | 2.38 | 2.40 | 2.42 | 2.45 | 2.47 |
| 23 | 2.47 | 2.49 | 2.51 | 2.53 | 2.56 | 2.49 | 2.51 | 2.53 | 2.55 | 2.57 |
| 24 | 2.58 | 2.60 | 2.62 | 2.64 | 2.66 | 2.60 | 2.62 | 2.64 | 2.66 | 2.68 |
| 25 | 2.68 | 2.71 | 2.73 | 2.75 | 2.77 | 2.70 | 2.73 | 2.75 | 2.77 | 2.79 |
| 26 | 2.79 | 2.81 | 2.83 | 2.85 | 2.88 | 2.81 | 2.83 | 2.85 | 2.88 | 2.90 |
| 27 | 2.90 | 2.92 | 2.94 | 2.96 | 2.98 | 2.92 | 2.94 | 2.96 | 2.98 | 3.01 |
| 28 | 3.00 | 3.03 | 3.05 | 3.07 | 3.09 | 3.03 | 3.05 | 3.07 | 3.09 | 3.11 |
| 29 | 3.11 | 3.13 | 3.15 | 3.18 | 3.20 | 3.13 | 3.16 | 3.18 | 3.20 | 3.22 |
| 30 | 3.22 | 3.24 | 3.26 | 3.28 | 3.30 | 3.24 | 3.26 | 3.29 | 3.3 I | 3.33 |
| 3 I | 2.32 | 3.35 | 3.37 | $3 \cdot 39$ | 3.41 | 3.35 | 3.37 | 3.39 | 3.41 | 3.44 |
| 32 | 3.43 | 3.45 | 3.47 | 3.49 | 3.52 | 3.46 | 3.48 | 3.50 | 3.52 | 3.54 |
| 33 | 3.54 | 3.56 | 3.58 | 3.60 | 3.62 | 3.56 | 3.59 | 3.6 I | 3.63 | 3.65 |
| 34 | 3.64 | 3.67 | 3.69 | 3.71 | 3.73 | 3.67 | 3.69 | 3.7 I | 3.74 | 3.76 |
| 35 | 3.75 | 3.77 | 3.79 | 3.8 I | 3.84 | 3.78 | 3.80 | 3.82 | 3.84 | 3.86 |

Smitheonian Tables.

TAble 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 670 mm. |  |  |  |  | HEIGHT OF THE BAROMETER 675 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm . | mm. | mm . | mm . | mm. | mm. | mm . | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 |
| 1 | . II | . 13 | . 15 | . 18 | . 20 | . II | . 13 | . 15 | . 18 | . 20 |
| 2 | . 22 | . 24 | . 26 | . 28 | . 31 | . 22 | . 24 | . 26 | . 29 | . 31 |
| 3 | . 33 | . 35 | - 37 | . 39 | . 42 | . 33 | - 35 | . 37 | . 40 | . 42 |
| 4 | . 44 | . 46 | . 48 | . 50 | . 53 | . 44 | . 46 | . 48 | . 51 | . 53 |
| 5 | 0.55 | 0.57 | 0.59 | 0.61 | 0.63 | 0.55 | 0.57 | 0.60 | 0.62 | 0.64 |
| 6 | . 66 | . 68 | . 70 | . 72 | . 74 | . 66 | . 68 | . 71 | . 73 | . 75 |
| 7 | . 77 | - . 79 | .81 | . 83 | . 85 | . 77 | . 79 | . 82 | . 84 | . 86 |
| 8 | . 87 | . 90 | . 92 | . 94 | . 96 | . 88 | . 90 | . 93 | . 95 | . 97 |
| 9 | . 98 | I.OI | 1.03 | 1.05 | 1.07 | . 99 | I.OI | 1.04 | 1.06 | 1.08 |
| 10 | 1.09 | I. II | I. 14 | I. 16 | I. 18 | 1.10 | 1.12 | I. 14 | 1.17 | I. 19 |
| 11 | 1.20 | 1.22 | 1.25 | 1.27 | 1.29 | I.2I | 1.23 | 1.25 | 1.28 | 1.30 |
| 12 | 1.31 | 1.33 | 1.35 | r. 38 | 1.40 | 1.32 | 1.34 | I. 36 | 1.39 | 1.41 |
| 13 | 1.42 | I. 44 | I. 46 | 1.49 | 1.51 | 1.43 | 1.45 | 1.47 | 1.50 | 1.52 |
| 14 | 1.53 | 1.55 | 1.57 | 1.59 | 1.62 | 1.54 | 1.56 | 1.58 | 1.6I | 1.63 |
| 15 | 1.64 | 1.66 | 1.68 | 1.70 | 1.72 | r. 65 | 1.67 | 1.69 | 1.72 | 1.74 |
| 16 | 1.75 | 1.77 | 1.79 | I.81 | 1.83 | 1.76 | 1.78 | 1.80 | 1.83 | 1.85 |
| 17 | 1.86 | 1.88 | 1.90 | 1.92 | 1.94 | 1.87 | I. 89 | 1.91 | 1.94 | 1.96 |
| 18 | 1.96 | 1.99 | 2.01 | 2.03 | 2.05 | 1.98 | 2.00 | 2.02 | 2.04 | 2.07 |
| 19 | 2.07 | 2.09 | 2.12 | 2.14 | 2.16 | 2.09 | 2.11 | 2.13 | 2.15 | 2.18 |
| 20 | 2.18 | 2.20 | 2.23 | 2.25 | 2.27 | 2.20 | 2.22 | 2.24 | 2.26 | 2.29 |
| 21 | 2.29 | 2.31 | 2.33 | 2.36 | 2.38 | 2.31 | 2.33 | 2.35 | 2.37 | 2.39 |
| 22 | 2.40 | 2.42 | 2.44 | 2.46 | 2.49 | 2.42 | 2.44 | 2.46 | 2.48 | 2.50 |
| 23 | 2.51 | 2.53 | 2.55 | 2.57 | 2.59 | 2.53 | 2.55 | 2.57 | 2.59 | 2.61 |
| 24 | 2.62 | 2.64 | 2.66 | 2.68 | 2.70 | 2.64 | 2.66 | 2.68 | 2.70 | 2.72 |
| 25 | 2.72 | 2.75 | 2.77 | 2.79 | 2.81 | 2.74 | 2.77 | 2.79 | 2.81 | 2.83 |
| 26 | 2.83 | 2.85 | 2.88 | 2.90 | 2.92 | 2.85 | 2.88 | 2.90 | 2.92 | 2.94 |
| 27 | 2.94 | 2.96 | 2.98 | 3.01 | 3.03 | 2.96 | 2.99 | 3.01 | 3.03 | 3.05 |
| 28 | 3.05 | 3.07 | 3.09 | 3.11 | 3.14 | 3.07 | 3.09 | 3.12 | 3.14 | 3.16 |
| 29 | 3.16 | 3.18 | 3.20 | 3.22 | 3.24 | 3.18 | 3.20 | 3.23 | 3.25 | 3.27 |
| 30 | 3.27 | 3.29 | 3.31 | 3.33 | 3.35 | 3.29 | 3.3 I | 3.33 | 3.36 | 3.38 |
| 3 I | 3.37 | 3.40 | 3.42 | $3 \cdot 44$ | 3.46 | 3.40 | $3 \cdot 42$ | 3.44 | 3.47 | 3.49 |
| 33 | 3.48 | 3.50 | 3.53 | 3.55 | 3.57 | 3.51 | 3.53 | 3.55 | 3.57 | 3.60 |
| 33 | 3.59 | 3.61 | 3.63 | 3.66 | 3.68 | 3.62 | 3.64 | 3.66 | 3.68 | 3.71 |
| 34 | 3.70 | 3.72 | 3.74 | 3.76 | 3.79 | 3.73 | 3.75 | 3.77 | 3.79 | 3.81 |
| 35 | 3.8 I | 3.83 | 3.85 | 3.87 | 3.89 | 3.84 | 3.86 | 3.88 | 3.90 | 3.92 |

Emithsonian Tables.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

| - | HEIGHT OF THE BAROMETER 680 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 685 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 |
| 1 | . II | . 13 | . 16 | . 18 | . 20 | . 11 | . 13 | . 16 | . 18 | . 20 |
| 2 | . 22 | . 24 | . 27 | . 29 | -31 | . 22 | . 25 | . 27 | . 29 | -3I |
| 3 | . 33 | . 36 | - 38 | . 40 | . 42 | . 34 | . 36 | . 38 | . 40 | . 43 |
| 4 | . 44 | . 47 | . 49 | . 51 | . 53 | . 45 | . 47 | . 49 | . 51 | . 54 |
| 5 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.56 | 0.58 | 0.60 | 0.63 | 0.65 |
| 6 | . 67 | . 69 | . 71 | . 73 | . 75 | . 67 | . 69 | . 72 | . 74 | . 76 |
| 7 | . 78 | . 80 | . 82 | . 84 | . 87 | . 78 | . 80 | . 83 | . 85 | . 87 |
| 8 | . 89 | .91 | . 93 | . 95 | . 98 | . 89 | . 92 | . 94 | . 96 | . 98 |
| 9 | 1.00 | 1.02 | 1.04 | 1.06 | 1.09 | I. 12 | 1.03 | 1.05 | 1.07 | 1.09 |
| 10 | I. II | 1.13 | 1. 15 | 1.18 | 1.20 | I. 12 | 1.14 | 1.16 | 1. 18 | I. 21 |
| 11 | 1.22 | I. 24 | I. 26 | 1.29 | I. 31 | 1.23 | 1.25 | 1.27 | I. 30 | 1.32 |
| 12 | 1.33 | 1.35 | 1.37 | 1.40 | 1.42 | 1.34 | 1. 36 | 1.38 | I.4I | 1.43 |
| 13 | 1. 44 | I. 46 | I. 49 | I.51 | 1.53 | 1.45 | 1.47 | 1.50 | 1.52 | I. 54 |
| 14 | I. 55 | 1.57 | 1.60 | 1.62 | 1.64 | I. 56 | 1.59 | 1.6I | 1.63 | 1.65 |
| 15 | 1.66 | 1.68 | 1.71 | 1.73 | 1.75 | 1.6'7 | 1.70 | 1.72 | 1.74 | 1.76 |
| 16 | 1.77 | 1.79 | 1.82 | 1.84 | 1.86 | 1.79 | 1.81 | 1.83 | 1.85 | 1.87 |
| 17 | 1.88 | 1.91 | 1.93 | 1.95 | 1.97 | 1.90 | 1.92 | 1.94 | 1.96 | 1.99 |
| 18 | 1.99 | 2.02 | 2.04 | 2.06 | 2.08 | 2.01 | 2.03 | 2.05 | 2.07 | 2.10 |
| 19 | 2.10 | 2.13 | 2. 15 | 2.17 | 2.19 | 2.12 | 2.14 | 2.16 | 2.19 | 2.21 |
| 20 | 2.21 | 2.24 | 2.26 | 2.28 | 2.30 | 2.23 | 2.25 | 2.27 | 2.30 | 2.32 |
| 21 | 2.32 | 2.35 | 2.37 | 2.39 | 2.41 | 2.34 | 2.36 | 2.39 | 2.41 | 2.43 |
| 22 | 2.43 | 2.46 | 2.48 | 2.50 | 2.52 | 2.45 | 2.47 | 2.50 | 2.52 | 2.54 |
| 23 | 2.54 | 2.57 | 2.59 | 2.61 | 2.63 | 2.56 | 2.59 | 2.61 | 2.63 | 2.65 |
| 24 | 2.66 | 2.68 | 2.70 | 2.72 | 2.74 | 2.67 | 2.70 | 2.72 | 2.74 | 2.76 |
| 25 | 2.77 | 2.79 | 2.81 | 2.83 | 2.85 | 2.79 | 2.81 | 2.83 | 2.85 | 2.87 |
| 26 | 2.88 | 2.90 | 2.92 | 2.94 | 2.96 | 2.90 | 2.92 | 2.94 | 2.96 | 2.99 |
| 27 | 2.99 | 3.01 | 3.03 | 3.05 | 3.07 | 3.01 | 3.03 | 3.05 | 3.07 | 3.10 |
| 28 | 3.10 | 3.12 | 3.14 | 3.16 | 3.18 | 3.12 | 3.14 | 3.16 | 3.18 | 3.21 |
| 29 | 3.21 | 3.23 | 3.25 | 3.27 | 3.29 | 3.23 | 3.25 | 3.27 | 3.30 | 3.32 |
| 30 | $3 \cdot 32$ | $3 \cdot 34$ | 3.36 | 3.38 | 3.40 | $3 \cdot 34$ | 3.36 | 3.38 | 3.41 | 3.43 |
| 31 | 3.43 | 3.45 | 3.47 | 3.49 | 3.51 | 3.45 | 3.47 | 3.49 | 3.52 | 3.54 |
| 32 | 3.54 | 3.56 | 3.58 | 3.60 | 3.62 | 3.56 | 3.58 | 3.61 | 3.63 | 3.65 |
| 33 | 3.64 | 3.67 | 3.69 | 3.71 | 3.73 | 3.67 | 3.69 | 3.72 | 3.74 | 3.76 |
| 34 | 3.75 | 3.78 | 3.80 | 3.82 | 3.84 | 3.78 | 3.80 | 3.83 | 3.85 | 3.87 |
| 35 | 3.86 | 3.89 | 3.91 | 3.93 | 3.95 | 3.89 | 3.91 | 3.94 | 3.96 | 3.98 |

Smitheonian Tables.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 690 mm. |  |  |  |  | HEIGHT OF THE BAROMETER 695 mm. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm . | mm. | mm . | mm. | mm. | mm . | mm. |
| $0{ }^{5}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
| 1 | . II | . 14 | . 16 | . 18 | . 20 | . II | . 14 | . 16 | . 18 | . 20 |
| 2 | . 23 | . 25 | . 27 | . 29 | . 32 | . 23 | . 25 | . 27 | . 30 | . 32 |
| 3 | . 34 | . 36 | . 38 | .4I | . 43 | - 34 | . 36 | . 39 | . 41 | . 43 |
| 4 | . 45 | . 47 | . 50 | . 52 | . 54 | . 45 | .48 | . 50 | . 52 | . 54 |
| 5 | 0.56 | 0.59 | 0.6I | 0.63 | 0.65 | 0.57 | 0.59 | 0.61 | 0.64 | 0.66 |
| 6 | . 68 | . 70 | . 72 | . 74 | . 77 | . 68 | . 70 | . 73 | . 75 | . 77 |
| 7 | . 79 | .81 | . 83 | . 86 | . 88 | . 79 | . 82 | . 84 | . 86 | . 88 |
| 8 | . 90 | . 92 | . 95 | . 97 | . 99 | . 91 | . 93 | . 95 | . 98 | 1.00 |
| 9 | I.OI | 1.04 | 1.06 | 1.08 | I. 10 | 1.02 | 1.04 | 1.07 | 1.09 | I. II |
| 10 | I. 13 | I. 15 | 1.17 | 1.19 | 1.22 | I. 13 | I. 16 | I. 18 | 1.20 | 1.22 |
| II | 1.24 | 1.26 | 1.28 | 1.31 | 1.33 | 1.25 | 1.27 | 1.29 | 1. 31 | 1.34 |
| 12 | 1.35 | 1.37 | 1.39 | 1.42 | 1.44 | 1.36 | 1.38 | 1.41 | 1.43 | 1.45 |
| 13 | 1.46 | 1.48 | 1.51 | 1.53 | I. 55 | 1.47 | 1.50 | 1.52 | I. 54 | 1.56 |
| 14 | 1. 57 | 1.60 | 1.62 | 1.64 | 1.66 | 1.59 | 1.6I | 1.63 | 1. 65 | 1.68 |
| 15 | 1.69 | 1.71 | 1.73 | 1.75 | 1.78 | 1.70 | 1.72 | 1.74 | 1.77 | 1.79 |
| 16 | 1.80 | 1.82 | 1.84 | 1.87 | 1.89 | I.8I | 1.83 | I. 86 | 1.88 | 1.90 |
| 17 | 1.91 | 1.93 | 1.96 | 1.98 | 2.00 | 1.92 | 1.95 | 1.97 | 1.99 | 2.01 |
| 18 | 2.02 | 2.05 | 2.07 | 2.09 | 2.11 | 2.04 | 2.06 | 2.08 | 2.11 | 2.13 |
| 19 | 2.13 | 2.16 | 2.18 | 2.20 | 2.22 | 2. 15 | 2.17 | 2.20 | 2.22 | 2.24 |
| 20 | 2.25 | 2.27 | 2.29 | 2.31 | 2.34 | 2.26 | 2.29 | 2.31 | 2.33 | 2.35 |
| 21 | 2.36 | 2.38 | 2.40 | 2.43 | 2.45 | 2.38 | 2.40 | 2.42 | 2.44 | 2.47 |
| 22 | 2.47 | 2.49 | 2.52 | 2.54 | 2.56 | 2.49 | 2.51 | 2.53 | 2.56 | 2.58 |
| 23 | 2.58 | 2.60 | 2.63 | 2.65 | 2.67 | 2.60 | 2.62 | 2.65 | 2.67 | 2.69 |
| 24 | 2.69 | 2.72 | 2.74 | 2.76 | 2.78 | 2.71 | 2.74 | 2.76 | 2.78 | 2.80 |
|  | 2.81 | 2.83 | 2.85 | 2.87 | 2.90 | 2.83 | 2.85 | 2.87 | 2.89 | 2.92 |
| 26 | 2.92 | 2.94 | 2.96 | 2.99 | 3.01 | 2.94 | 2.96 | 2.98 | 3.01 | 3.03 |
| 27 | 3.03 | 3.05 | 3.07 | 3.10 | 3.12 | 3.05 | 3.07 | 3.10 | 3.12 | 3.14 |
| 28 | 3.14 | 3.16 | 3.19 | 3.21 | 3.23 | 3.16 | 3.19 | 3.21 | 3.23 | 3.25 |
| 29 | 3.25 | 3.27 | 3.30 | 3.32 | 3.34 | 3.28 | 3.30 | 3.32 | 3.34 | 3.37 |
| 30 | 3.36 | 3.39 | 3.41 | 3.43 | 3.45 | 3.39 | 3.41 | 3.43 | 3.46 | 3.48 |
| 31 | 3.48 | 3.50 | 3.52 | 3.54 | 3.56 | 3.50 | 3.52 | 3.55 | 3.57 | 3.59 |
| 32 | 3.59 | 3.61 | 3.63 | 3.65 | 3.68 | 3.61 | 3.64 | 3.66 | 3.68 | 3.70 |
| 33 | 3.70 | 3.72 | 3.74 | 3.77 | 3.79 | 3.73 | 3.75 | 3.77 | 3.79 | 3.81 |
| 34 | 3.81 | 3.83 | 3.85 | 3.88 | 3.90 | 3.84 | 3.86 | 3.88 | 3.90 | 3.93 |
| 35 | 3.92 | 3.94 | 3.97 | 3.99 | 4.01 | 3.95 | 3.97 | 3.99 | 4.02 | 4.04 |

Syithsonian Tables.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

## METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 700 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 705 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm . | mm . | mm. | mm. | mm . | mm. | mm . | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
|  | . 11 | . 14 | . 16 | . 18 | . 21 | . 12 | . 14 | . 16 | . 18 | . 21 |
| 2 | . 23 | . 25 | . 27 | . 30 | . 32 | . 23 | . 25 | . 28 | . 30 | . 32 |
| 3 | - 34 | - 37 | . 39 | . 41 | . 43 | - 35 | - 37 | - 39 | . 41 | . 44 |
| 4 | . 46 | . 48 | . 50 | . 53 | . 55 | . 46 | . 48 | . 51 | . 53 | . 55 |
| 5 | 0.57 | 0.59 | 0.62 | 0.64 | 0.66 | 0.58 | 0.60 | 0.62 | 0.64 | 0.67 |
| 6 | . 69 | . 71 | . 73 | . 75 | . 78 | . 69 | . 71 | . 74 | . 76 | . 78 |
| 7 | . 80 | . 82 | . 85 | . 87 | . 89 | .81 | . 83 | . 85 | . 87 | . 90 |
| 8 | .91 | . 94 | . 96 | . 98 | 1.00 | . 92 | . 94 | . 97 | . 99 | I.OI |
| 9 | 1.03 | 1.05 | 1.07 | I. 10 | 1.12 | 1.04 | 1.06 | 1.08 | 1.10 | 1.13 |
| 10 | I. 14 | I. 16 | 1.19 | I.2I | 1.23 | 1.15 | 1.17 | 1.20 | 1.22 | 1.24 |
| 11 | 1.26 | 1.28 | 1.30 | 1.32 | 1.35 | 1.26 | 1.29 | 1.31 | 1.33 | 1.36 |
| 12 | 1.37 | 1.39 | 1.42 | 1.44 | 1.46 | I. 38 | I. 40 | 1.43 | 1.45 | 1.47 |
| 13 | 1.48 | 1.51 | 1.53 | 1.55 | 1.57 | I. 49 | 1.52 | 1.54 | 1.56 | 1.59 |
| 14 | 1.60 | 1.62 | 1.64 | 1.67 | 1.69 | 1.6I | 1.63 | 1.65 | 1.68 | 1.70 |
| 15 | 1.71 | 1.73 | 1.76 | 1.78 | 1.80 | 1.72 | 1.75 | 1.77 | 1.79 | 1.81 |
| 16 | 1.82 | 1.85 | 1.87 | 1.89 | 1.92 | 1.84 | 1.86 | 1.88 | 1.91 | 1.93 |
| 17 | 1.94 | 1.96 | 1.98 | 2.01 | 2.03 | 1.95 | 1.98 | 2.00 | 2.02 | 2.04 |
| 18 | 2.05 | 2.07 | 2.10 | 2.12 | 2.14 | 2.07 | 2.09 | 2.11 | 2.14 | 2.16 |
| 19 | 2.17 | 2.19 | 2.21 | 2.23 | 2.26 | 2.18 | 2.20 | 2.23 | 2.25 | 2.27 |
| 20 | 2.28 | 2.30 | 2.32 | 2.35 | 2.37 | 2.30 | 2.32 | 2.34 | 2.36 | 2.39 |
| 21 | 2.39 | 2.42 | 2.44 | 2.46 | 2.48 | 2.41 | 2.43 | 2.46 | 2.48 | 2.50 |
| 22 | 2.51 | 2.53 | 2.55 | 2.57 | 2.60 | 2.52 | 2.55 | 2.57 | 2.59 | 2.62 |
| 23 | 2.62 | 2.64 | 2.67 | 2.69 | 2.71 | 2.64 | 2.66 | 2.68 | 2.71 | 2.73 |
| 24 | 2.73 | 2.76 | 2.78 | 2.80 | 2.82 | 2.75 | 2.78 | 2.80 | 2.82 | 2.84 |
| 25 | 2.85 | 2.87 | 2.89 | 2.91 | 2.94 | 2.87 | 2.89 | 2.91 | 2.94 | 2.96 |
| 26 | 2.96 | 2.98 | 3.01 | 3.03 | 3.05 | 2.98 | 3.00 | 3.03 | 3.05 | 3.07 |
| 27 | 3.07 | 3.10 | 3.12 | 3.14 | 3.16 | 3.10 | 3.12 | 3.14 | 3.16 | 3.19 |
| 28 | 3.19 | 3.21 | 3.23 | 3.25 | 3.28 | 3.21 | 3.23 | 3.25 | 3.28 | 3.30 |
| 29 | 3.30 | 332 | 3.34 | 3.37 | 3.39 | 3.32 | 3.35 | 3.37 | 3.39 | $3 \cdot 4 \mathrm{I}$ |
| 30 | 3.41 | 3.44 | 3.46 | 3.48 | 3.50 | 3.44 | 3.46 | 3.48 | 3.51 | 3.53 |
| 3 I | 3.53 | 3.55 | 3.57 | 3.59 | 3.62 | 3.55 | 3.57 | 3.60 | 3.62 | 3.64 |
| 32 | 3.64 | 3.66 | 3.68 | 3.71 | 3.73 | 3.66 | 3.69 | 3.71 | 3.73 | 3.76 |
| 33 | 3.75 | 3.77 | 3.80 | 3.82 | 3.84 | 3.78 | 3.80 | 3.82 | 3.85 | 3.87 |
| 34 | 3.87 | 3.89 | 3.91 | 3.93 | 3.96 | 3.89 | 3.92 | 3.94 | 3.96 | 3.98 |
| 35 | 3.98 | 4.00 | 4.02 | 4.05 | 4.07 | 4.01 | 4.03 | 4.05 | 4.07 | 4.10 |

Smithsonian Tables.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 710 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 715 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
| 1 | . 12 | . 14 | . 16 | . 19 | . 21 | . 12 | . 14 | . 16 | . 19 | . 21 |
| 2 | . 23 | . 26 | . 28 | - 30 | - 32 | . 23 | . 26 | . 28 | . 30 | - 33 |
| 3 | - 35 | . 37 | . 39 | . 42 | . 44 | . 35 | - 37 | . 40 | . 42 | . 44 |
| 4 | .46 | . 49 | . 51 | . 53 | .56 | . 47 | . 49 | .51 | . 54 | . 56 |
| 5 | 0.58 | 0.60 | 0.63 | 0.65 | 0.67 | 0.58 | 0.61 | 0.63 | 0.65 | 0.68 |
| 6 | . 70 | . 72 | . 74 | . 76 | . 79 | . 70 | . 72 | . 75 | . 77 | . 79 |
| 7 | .81 | . 83 | . 86 | . 88 | . 90 | . 82 | . 84 | . 86 | . 89 | . 91 |
| 8 | . 93 | . 95 | . 97 | 1.00 | 1.02 | . 93 | .96 | . 98 | 1.00 | 1.03 |
| 9 | 1. 04 | 1.07 | 1.09 | I.II | I. 13 | 1.05 | 1.07 | I. 10 | I. 12 | 1.14 |
| 10 | I. 16 | 1. 18 | 1.20 | 1.23 | 1.25 | I. 17 | I. 19 | I. 21 | I. 24 | 1.26 |
| II | 1.27 | 1.30 | 1.32 | I. 34 | 1.37 | 1.28 | 1.3I | 1.33 | 1. 35 | 1. 38 |
| 12 | 1.39 | 1.41 | 1.44 | 1.46 | I. 48 | I. 40 | 1.42 | r. 45 | r. 47 | I. 49 |
| 13 | 1.50 | 1. 53 | I. 55 | 1.57 | 1.60 | 1.52 | I. 54 | I. 56 | r. 58 | 1.6I |
| 14 | 1. 62 | 1.64 | 1. 67 | I. 69 | 1.71 | 1.63 | 1.65 | I. 68 | 1.70 | 1.72 |
| 15 | 1. 74 | 1.76 | 1.78 | 1.80 | 1.83 | 1.75 | 1.77 | 1.79 | 1.82 | 1. 84 |
| 16 | 1.85 | 1.87 | 1.90 | 1.92 | 1.94 | 1.86 | 1.89 | 1.91 | 1.93 | 1.96 |
| 17 | 1.97 | 1.99 | 2.01 | 2.04 | 2.06 | 1.98 | 2.00 | 2.03 | 2.05 | 2.07 |
| 18 | 2.08 | 2. 10 | 2.13 | 2.15 | 2.17 | 2.10 | 2.12 | 2.14 | 2.17 | 2.19 |
| 19 | 2.20 | 2.22 | 2.24 | 2.27 | 2.29 | 2.21 | 2.24 | 2.26 | 2.28 | 2.30 |
| 20 | 2.31 | 2.33 | 2.36 | 2.38 | 2.40 | 2.33 | 2.35 | 2.37 | 2.40 | 2.42 |
| 21 | 2.43 | 2.45 | 2.47 | 2.50 | 2.52 | 2.44 | 2.47 | 2.49 | 2.51 | 2.54 |
| 22 | 2.54 | 2.57 | 2.59 | 2.61 | 2.63 | 2.56 | 2.58 | 2.61 | 2.63 | 2.65 |
| 23 | 2.66 | 2.68 | 2.70 | 2.73 | 2.75 | 2.68 | 2.70 | 2.72 | 2.75 | 2.77 |
| 24 | 2.77 | 2.80 | 2.82 | 2.84 | 2.86 | 2.79 | 2.81 | 2.84 | 2.86 | 2.88 |
| 25 | 2.89 | 2.91 | 2.93 | 2.96 | 2.98 | 2.91 | 2.93 | 2.95 | 2.98 | 3.00 |
| 26 | 3.00 | 3.03 | 3.05 | 3.07 | 3.09 | 3.02 | 3.05 | 3.07 | 3.09 | 3.12 |
| 27 | 3.12 | 3.14 | 3.16 | 3.19 | 3.21 | 3.14 | 3.16 | 3.19 | 3.21 | 3.23 |
| 28 | 3.23 | 3.25 | 3.28 | 3.30 | 3.32 | 3.25 | 3.28 | $3 \cdot 30$ | 3.32 | 3.35 |
| 29 | 3.35 | 3.37 | 3.39 | 3.42 | 3.44 | 3.37 | 3.39 | 3.42 | 3.44 | 3.46 |
| 30 | 3.46 | 3.48 | 3.51 | 3.53 | 3.55 | 3.49 | 3.51 | 3.53 | 3.56 | 3.58 |
| 31 | 3.58 | 3.60 | 3.62 | 3.65 | 3.67 | 3.60 | 3.62 | 3.65 | 3.67 | 3.69 |
| 32 | 3.69 | 3.71 | 3.74 | 3.76 | 3.78 | 3.72 | 3.74 | 3.76 | 3.79 | 3.81 |
| 33 | 3.81 | 3.83 | 3.85 | 3.87 | 3.90 | 3.83 | 3.86 | 3.88 | 3.90 | 3.92 |
| 34 | 3.92 | 3.94 | 3.97 | 3.99 | 4.01 | 3.95 | 3.97 | 3.99 | 4.02 | 4.04 |
| 35 | 4.03 | 4.06 | 4.08 | 4.10 | 4.13 | 4.06 | 4.09 | 4.II | 4.13 | 4.16 |

Smitheonian Tableg.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 720 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 725 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thernometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
| 1 | . 12 | . 14 | . 16 | . 19 | . 21 | . 12 | . 14 | . 17 | . 19 | . 21 |
| 2 | . 24 | . 26 | . 28 | . 31 | . 33 | . 24 | . 26 | . 28 | . 31 | . 33 |
| 3 | . 35 | .38 | . 40 | . 42 | . 45 | . 36 | . 38 | . 40 | . 43 | . 45 |
| 4 | 47 | . 49 | . 52 | . 54 | . 56 | . 47 | . 50 | . 52 | . 54 | . 57 |
| 5 | 0.59 | 0.61 | 0.63 | 0.66 | 0.68 | 0.59 | 0.62 | 0.64 | 0.66 | 0.69 |
| 6 | . 71 | . 73 | . 75 | . 78 | . 80 | . 71 | . 73 | . 76 | . 78 | . 80 |
| 7 | . 82 | . 85 | . 87 | . 89 | . 92 | . 83 | . 85 | . 88 | . 90 | . 92 |
| 8 | . 94 | . 96 | . 99 | 1.OI | 1.03 | . 95 | . 97 | . 99 | 1.02 | 1.04 |
| 9 | 1.06 | 1.08 | 1.10' | 1.13 | 1.15 | 1.06 | 1.09 | I.II | I. 14 | I. 16 |
| 10 | 1.17 | 1.20 | 1.22 | 1.24 | 1.27 | 1. 18 | 1.21 | . 1.23 | 1.25 | 1.28 |
| II | I. 29 | 1.31 | 1.34 | 1.36 | 1.39 | 1.30 | 1.32 | 1.35 | 1.37 | 1.39 |
| 12 | 1.41 | 1.43 | 1.46 | 1.48 | 1.50 | 1.42 | 1.44 | 1.47 | 1.49 | 1.51 |
| 13 | 1.53 | 1.55 | 1.57 | 1.60 | 1.62 | I. 54 | 1.56 | 1.58 | 1.61 | 1.63 |
| 14 | I. 64 | 1.67 | 1.69 | 1.71 | 1.74 | 1.65 | 1.68 | 1.70 | 1.73 | 1.75 |
| 15 | 1.76 | 1.78 | 1.81 | 1.83 | 1.85 | 1.77 | 1.80 | 1.82 | 1.84 | 1.87 |
| 16 | 1.88 | 1.90 | 1.92 | 1.95 | 1.97 | 1.89 | 1.91 | 1.94 | 1.96 | 1.98 |
| 17 | 1.99 | 2.02 | 2.04 | 2.06 | 2.09 | 2.01 | 2.03 | 2.05 | 2.08 | 2.10 |
| 18 | 2. II | 2.13 | 2.16 | 2.18 | 2.20 | 2. 13 | 2.15 | 2.17 | 2.20 | 2.22 |
| 19 | 2.23 | 2.25 | 2.27 | 2.30 | 2.32 | 2.24 | 2.27 | 2.29 | 2.3 I | 2.34 |
| 20 | 2.34 | 2.37 | 2.39 | 2.41 | 2.44 | 2.36 | 2.38 | 2.41 | 2.43 | 2.45 |
| 21 | 2.46 | 2.48 | 2.51 | 2.53 | 2.55 | 2.48 | 2.50 | 2.53 | 2.55 | 2.57 |
| 22 | 2.58 | 2.60 | 2.62 | 2.65 | 2.67 | 2.60 | 2.62 | 2.64 | 2.67 | 2.69 |
| 23 | 2.69 | 2.72 | 2.74 | 2.76 | 2.79 | 2.71 | 2.74 | 2.76 | 2.78 | 2.81 |
| 24 | 2.81 | 2.83 | 2.86 | 2.88 | 2.90 | 2.83 | 2.85 | 2.88 | 2.90 | 2.92 |
| 25 | 2.93 | 2.95 | 2.97 | 3.00 | 3.02 | 2.95 | 2.97 | 3.00 | 3.02 | 3.04 |
| 26 | 3.04 | 3.07 | 3.09 | 3.11 | 3.14 | 3.07 | 3.09 | 3.11 | 3.14 | 3.16 |
| 27 | 3.16 | 3.18 | 3.21 | 3.23 | 3.25 | 3.18 | 3.21 | 3.23 | 3.25 | 3.28 |
| 28 | 3.28 | 3.30 | 3.32 | 3.35 | 3.37 | 3.30 | 3.32 | 3.35 | 3.37 | 3.39 |
| 29 | 3.39 | 3.42 | 3.44 | 3.46 | 3.49 | 3.42 | 3.44 | 3.46 | 3.49 | 3.51 |
| 30 | 3.51 | 3.53 | 3.56 | 3.58 | 3.60 | 3.53 | 3.56 | 3.58 | 3.60 | 3.63 |
| 31 | 3.63 | 3.65 | 3.67 | 3.70 | 3.72 | 3.65 | 3.68 | 3.70 | 3.72 | 3.75 |
| 32 | 3.74 | 3.77 | 3.79 | 3.81 | 3.84 | 3.77 | 3.79 | 3.82 | 3.84 | 3.86 |
| 33 | 3.86 | 3.88 | 3.91 | 3.93 | 3.95 | 3.89 | 3.91 | 3.93 | 3.96 | 3.98 |
| 24 | 3.98 | 4.00 | 4.02 | 4.05 | 4.07 | 4.00 | 4.03 | 4.05 | 4.07 | 4.10 |
| 35 | 4.09 | 4.1I | 4.14 | 4.16 | 4.18 | 4.12 | 4.14 | 4.17 | 4.19 | 4.21 |

Smitheonian Tables.

Table 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 730 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 735 mm. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0\% | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | O. 10 | 0.00 | 0.02 | 0.05 | 0.07 | 0.10 |
| I | . 12 | . 14 | . 17 | . 19 | . 21 | . 12 | . 14 | . 17 | . 19 | . 22 |
| 2 | . 24 | . 26 | . 29 | -31 | . 33 | . 24 | . 26 | . 29 | . 31 | - 34 |
| 3 | . 36 | - 38 | . 41 | . 43 | . 45 | . 36 | . 38 | . 41 | . 43 | . 46 |
| 4 | . 48 | . 50 | . 52 | . 55 | . 57 | . 48 | . 50 | . 53 | . 55 | . 58 |
| 5 | 0.60 | 0.62 | 0.64 | 0.67 | 0.69 | 0.60 | 0.62 | 0.65 | 0.67 | 0.70 |
| 6 | . 71 | . 74 | . 76 | . 79 | .81 | . 72 | . 74 | . 77 | . 79 | . 82 |
| 7 | . 83 | . 86 | . 88 | .91 | . 93 | . 84 | . 86 | . 89 | .91 | . 94 |
| 8 | . 95 | . 98 | 1.00 | 1.02 | 1.05 | . 96 | . 98 | I. OI | 1.03 | 1.06 |
| 9 | 1.07 | 1.10 | 1.12 | 1.14 | 1.17 | 1.08 | I. 10 | I. 13 | I. 15 | 1.17 |
| 10 | I. 19 | I.2I | 1.24 | 1.26 | 1.29 | I. 20 | 1.22 | 1.25 | 1.27 | 1.29 |
| II | 1.31 | 1.33 | 1.36 | 1.38 | 1.40 | I. 32 | 1.34 | I. 37 | I. 39 | I.4I |
| 12 | 1.43 | I. 45 | 1.48 | 1.50 | 1.52 | I. 44 | 1.46 | I. 49 | I. 51 | 1.53 |
| 13 | I. 55 | 1.57 | 1.59 | 1.62 | 1.64 | I. 56 | 1.58 | 1.6I | 1.63 | I. 65 |
| 14 | 1.67 | 1.69 | 1.71 | 1.74 | 1.76 | 1.68 | 1.70 | 1.72 | I. 75 | 1.77 |
| 15 | r. 78 | r.81 | 1.83 | 1.86 | 1.88 | 1.80 | 1. 82 | r. 84 | 1.87 | 1.89 |
| 16 | 1.90 | 1.93 | 1.95 | 1.97 | 2.00 | 1.92 | 1.94 | 1.96 | 1.99 | 2.01 |
| 17 | 2.02 | 2.05 | 2.07 | 2.09 | 2.12 | 2.04 | 2.06 | 2.08 | 2.11 | 2.13 |
| 18 | 2.14 | 2.16 | 2.19 | 2.21 | 2.23 | 2.15 | 2.18 | 2.20 | 2.23 | 2.25 |
| 19 | 2.26 | 2.28 | 2.3 I | 2.33 | 2.35 | 2.27 | 2.30 | 2.32 | 2.35 | 2.37 |
| 20 | 2.38 | 2.40 | 2.42 | 2.45 | 2.47 | 2.39 | 2.42 | 2.44 | 2.46 | 2.49 |
| 21 | 2.50 | 2.52 | 2.54 | 2.57 | 2.59 | 2.51 | 2.54 | 2.56 | 2.58 | 2.61 |
| 22 | 2.61 | 2.64 | 2.66 | 2.68 | 2.71 | 2.63 | 2.66 | 2.68 | 2.70 | 2.73 |
| 23 | 2.73 | 2.76 | 2.78 | 2.80 | 2.83 | 2.75 | 2.77 | 2.80 | 2.82 | 2.85 |
| 24 | 2.85 | 2.87 | 2.90 | 2.92 | 2.94 | 2.87 | 2.89 | 2.92 | 2.94 | 2.97 |
| 25 | 2.97 | 2.99 | 3.02 | 3.04 | 3.06 | 2.99 | 3.01 | 3.04 | 3.06 | 3.08 |
| 26 | 3.09 | 3.11 | 3.13 | 3.16 | 3.18 | 3.11 | 3.13 | 3.16 | 3.18 | 3.20 |
| 27 | 3.20 | 3.23 | 3.25 | 3.28 | 3.30 | 3.23 | 3.25 | 3.27 | 3.30 | 3.32 |
| 28 | 3.32 | 3.35 | 3.37 | 3.39 | 3.42 | 3.35 | 3.37 | 3.39 | 3.42 | 3.44 |
| 29 | 3.44 | 3.46 | 3.49 | 3.51 | 3.54 | 3.46 | 3.49 | 3.51 | 3.54 | 3.56 |
| 30 | 3.56 | 3.58 | 3.61 | 3.63 | 3.65 | 3.58 | 3.61 | 3.63 | 3.65 | 3.68 |
| 3 I | 3.68 | 3.70 | 3.72 | 3.75 | 3.77 | 3.70 | 3.73 | 3.75 | 3.77 | 3.80 |
| 32 | 3.79 | 3.82 | 3.84 | 3.87 | 3.89 | 3.82 | 3.84 | 3.87 | 3.89 | 3.92 |
| 33 | 3.91 | 3.94 | 3.96 | 3.98 | 4.01 | 3.94 | 3.96 | 3.99 | 4.01 | 4.03 |
| 34 | 4.03 | 4.05 | 4.08 | 4.10 | 4.12 | 4.06 | 4.08 | 4.11 | 4.13 | 4.15 |
| 35 | 4.15 | 4.17 | 4.20 | 4.22 | 4.24 | 4.18 | 4.20 | 4.22 | 4.25 | 4.27 |

Smitheonian Tables.

TABle 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 740 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 745 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm. | mm. | mm . | mm . | mm . | mm. | mm . | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0. 10 | 0.00 | 0.02 | 0.05 | 0.07 | O. 10 |
| I | . 12 | . 15 | . 17 | . 19 | . 22 | 12 | . 15 | . 17 | . 19 | . 22 |
| 2 | . 24 | . 27 | . 29 | . 31 | . 34 | . 24 | . 27 | . 29 | . 32 | . 34 |
| 3 | . 36 | . 39 | . 41 | . 44 | . 46 | - 37 | . 39 | . 41 | . 44 | . 46 |
| 4 | . 48 | .5I | - 53 | . 56 | . 58 | . 49 | .5I | . 54 | . 56 | . 58 |
| 5 | 0.60 | 0.63 | 0.65 | 0.68 | 0.70 | 0.6I | 0.63 | 0.66 | 0.68 | 0.71 |
| 6 | . 72 | . 75 | . 77 | . 80 | . 82 | . 73 | . 75 | . 78 | . 80 | . 83 |
| 7 | . 85 | . 87 | . 89 | . 92 | . 94 | . 85 | . 88 | . 90 | . 92 | . 95 |
| 8 | . 97 | . 99 | I. 01 | 1.04 | 1.06 | . 97 | 1.00 | 1.02 | 1.05 | 1.07 |
| 9 | 1.09 | I. II | I. 13 | 1.16 | I. 18 | 1.09 | 1. 12 | 1.14 | 1. 17 | 1. 19 |
| 10 | I.2I | 1.23 | I. 26 | 1.28 | I. 30 | 1.22 | 1.24 | 1.26 | I. 29 | 1.31 |
| 11 | 1.33 | 1.35 | 1. 38 | 1.40 | 1.42 | 1.34 | 1.36 | 1.38 | I. 41 | 1.43 |
| 12 | 1.45 | 1.47 | 1.50 | r. 52 | I. 54 | 1.46 | 1.48 | 1.51 | 1.53 | 1. 55 |
| 13 | 1.57 | 1.59 | 1.62 | 1.64 | 1.66 | I. 58 | 1.60 | 1.63 | 1.65 | 1.68 |
| 14 | 1.69 | 1.71 | 1.74 | 1.76 | 1.78 | 1.70 | 1.72 | 1.75 | 1.77 | I. 80 |
| 15 | r. 81 | 1.83 | 1.86 | 1.88 | 1.90 | 1.82 | 1.85 | 1.87 | 1.89 | 1.92 |
| 16 | 1.93 | 1.95 | 1.98 | 2.00 | 2.03 | 1.94 | 1.97 | 1.99 | 2.01 | 2.04 |
| 17 | 2.05 | 2.07 | 2.10 | 2.12 | 2.15 | 2.06 | 2.09 | 2.11 | 2.14 | 2. 16 |
| 18 | 2.17 | 2.19 | 2.22 | 2.24 | 2.27 | 2.18 | 2.21 | 2.23 | 2.26 | 2.28 |
| 19 | 2.29 | 2.31 | 2.34 | 2.36 | 2.39 | 2.31 | 2.33 | 2.35 | 2.38 | 2.40 |
| 20 | 2.41 | 2.43 | 2.46 | 2.48 | 2.51 | 2.43 | 2.45 | 2.47 | 2.50 | 2.52 |
| 21 | 2.53 | 2.55 | 2.58 | 2.60 | 2.63 | 2.55 | 2.57 | 2.59 | 2.62 | 2.64 |
| 22 | 2.65 | 2.67 | 2.70 | 2.72 | 2.75 | 2.67 | 2.69 | 2.72 | 2.74 | 2.76 |
| 23 | 2.77 | 2.79 | 2.82 | 2.84 | 2.87 | 2.79 | 2.81 | 2.84 | 2.86 | 2.88 |
| 24 | 2.89 | 2.91 | 2.94 | 2.96 | 2.99 | 2.91 | 2.93 | 2.96 | 2.98 | 3.01 |
| 25 | 3.01 | 3.03 | 3.06 | 3.08 | 3.11 | 3.03 | 3.05 | 3.08 | 3.10 | 3.13 |
| 26 | 3.13 | 3.15 | 3.18 | 3.20 | 3.22 | 3.15 | 3.17 | 3.20 | 3.22 | 3.25 |
| 27 | 3.25 | 3.27 | 3.30 | 3.32 | 3.34 | 3.27 | 3.29 | 3.32 | 3.34 | 3.37 |
| 28 | 3.37 | 3.39 | 3.42 | 3.44 | 3.46 | 3.39 | 3.42 | 3.44 | 3.46 | 3.49 |
| 29 | 3.49 | 3.51 | 3.54 | 3.56 | 3.58 | 3.51 | 3.54 | 3.56 | 3.58 | 3.61 |
| 30 | 3.61 | 3.63 | 3.66 | 3.68 | 3.70 | 3.63 | 3.66 | 3.68 | 3.70 | 3.73 |
| 3 I | 3.73 | 3.75 | 3.78 | 3.80 | 3.82 | 3.75 | 3.78 | 3.80 | 3.82 | 3.85 |
| 32 | 3.85 | 3.87 | 3.89 | 3.92 | 3.94 | 3.87 | 3.90 | 3.92 | 3.95 | 3.97 |
| 33 | 3.97 | 3.99 | 4.01 | 4.04 | 4.06 | 3.99 | 4.02 | 4.04 | 4.07 | 4.09 |
| 34 | 4.09 | 4.II | 4.13 | 4.16 | 4.18 | 4.II | 4.14 | 4.16 | 4. 19 | 4.21 |
| 35 | 4.21 | 4.23 | 4.25 | 4.28 | 4.30 | 4.23 | 4.26 | 4.28 | 4.31 | 4.33 |

Smithsonian Tableg.

TABLE 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 750 mm . |  |  |  |  | HEIGIIT OF THE BAROMETER 755 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm . | mm . | mm. | mm . | mm . | mm . | mm . | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.10 | 0.00 | 0.02 | 0.05 | 0.07 | 0. 10 |
| 1 | . 12 | . 15 | . 17 | . 20 | . 22 | . 12 | . 15 | . 17 | . 20 | . 22 |
| 2 | . 25 | . 27 | . 29 | . 32 | . 34 | . 25 | . 27 | - 30 | - 32 | - 35 |
| 3 | . 37 | . 39 | . 42 | . 44 | . 47 | . 37 | - 39 | . 42 | . 44 | . 47 |
| 4 | . 49 | . 51 | . 54 | . 56 | . 59 | . 49 | . 52 | . 54 | . 57 | . 59 |
| 5 | 0.61 | 0.64 | 0.66 | 0.69 | 0.71 | 0.62 | 0.64 | 0.67 | 0.69 | 0.71 |
| 6 | . 73 | . 76 | . 78 | . 81 | . 83 | . 74 | . 76 | . 79 | .81 | . 84 |
| 7 | . 86 | . 88 | . 91 | . 93 | . 95 | . 86 | . 89 | .91 | . 94 | . 96 |
| 8 | . 98 | 1.00 | 1.03 | 1.05 | 1.08 | . 99 | 1.or | 1.03 | 1.06 | I. 08 |
| 9 | 1. 10 | 1.13 | 1.15 | 1.17 | 1.20 | I.II | I. 13 | I. 16 | 1. 18 | I. 21 |
| 10 | 1.22 | 1. 25 | 1.27 | 1.30 | 1.32 | 1.23 | 1. 26 | 1.28 | 1.31 | 1. 33 |
| II | 1.35 | I. 37 | 1.39 | 1.42 | 1.44 | 1.35 | 1.38 | 1.40 | 1.43 | I. 45 |
| 12 | r. 47 | 1.49 | 1.52 | 1.54 | 1.56 | 1.48 | 1.50 | I. 53 | I. 55 | 1.58 |
| 13 | 1.59 | 1.61 | 1.64 | 1.66 | 1.69 | 1.60 | 1.62 | 1.65 | 1.67 | 1.70 |
| 14 | 1.71 | 1.74 | 1.76 | 1.78 | 1.81 | r. 72 | 1.75 | 1.77 | 1.80 | 1.82 |
| 15 | 1.83 | 1. 86 | 1.88 | 1.91 | 1.93 | 1.85 | 1. 87 | 1. 89 | 1.92 | 1.94 |
| 16 | 1.96 | 1.98 | 2.00 | 2.03 | 2.05 | 1.97 | 1.99 | 2.02 | 2.04 | 2.07 |
| 17 | 2.08 | 2.10 | 2.13 | 2.15 | 2.17 | 2.09 | 2.12 | 2.14 | 2.16 | 2.19 |
| 18 | 2.20 | 2.22 | 2.25 | 2.27 | 2.30 | 2.21 | 2.24 | 2.26 | 2.29 | 2.31 |
| 19 | 2.32 | 2.34 | 2.37 | 2.39 | 2.42 | 2.34 | 2.36 | 2.38 | 2.41 | 2.43 |
| 20 | 2.44 | 2.47 | 2.49 | 2.52 | 2.54 | 2.46 | 2.48 | 2.51 | 2.53 | 2.56 |
| 21 | 2.56 | 2.59 | 2.61 | 2.64 | 2.66 | 2.58 | 2.61 | 2.63 | 2.65 | 2.68 |
| 22 | 2.69 | 2.71 | 2.73 | 2.76 | 2.78 | 2.70 | 2.73 | 2.75 | 2.78 | 2.80 |
| 23 | 2.81 | 2.83 | 2.86 | 2.88 | 2.90 | 2.83 | 2.85 | 2.87 | 2.90 | 2.92 |
| 24 | 2.93 | 2.95 | 2.98 | 3.00 | 3.03 | 2.95 | 2.97 | 3.00 | 3.02 | 3.05 |
| 25 | 3.05 | 3.07 | 3.10 | 3.12 | 3.15 | 3.07 | 3.09 | 3.12 | 3.14 | 3.17 |
| 26 | 3.17 | 3.20 | 3.22 | 3.24 | 3.27 | 3.19 | 3.22 | 3.24 | 3.27 | 3.29 |
| 27 | 3.29 | 3.32 | 3.34 | 3.37 | 3.39 | $3 \cdot 31$ | 3.34 | 3.36 | 3.39 | 3.41 |
| 28 | 3.41 | 3.44 | 3.46 | 3.49 | 3.51 | 3.44 | 3.46 | 3.49 | 3.51 | 3.53 |
| 29 | 3.54 | 3.56 | 3.58 | 3.61 | 3.63 | 3.56 | 3.58 | 3.61 | 3.63 | 3.66 |
| 30 | 3.66 | 3.68 | 3.71 | 3.73 | 3.75 | 3.68 | 3.71 | 3.73 | 3.75 | 3.78 |
| 31 | 3.78 | 3.80 | 3.83 | 3.85 | 3.87 | 3.80 | 3.83 | 3.85 | 3.88 | 3.90 |
| 32 | 3.90 | 3.92 | 3.95 | 3.97 | 4.00 | 3.92 | 3.95 | 3.97 | 4.00 | 4.02 |
| 33 | 4.02 | 4.04 | 4.07 | 4.09 | 4. 12 | 4.05 | 4.07 | 4.10 | 4.12 | 4.14 |
| 34 | 4. 14 | 4.17 | 4.19 | 4.21 | 4.24 | 4.17 | 4.19 | 4.22 | 4.24 | 4.27 |
| 35 | 4.26 | 4.29 | $4 \cdot 3 \mathrm{I}$ | 4.33 | 4.36 | 4.29 | $4 \cdot 3 \mathrm{I}$ | 4.34 | 4.36 | 4.39 |

Smithbonian Tables.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 760 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 765 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0:2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm . |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.10 | 0.00 | 0.03 | 0.05 | 0.07 | 0.10 |
| 1 | . 12 | . 15 | .17 | . 20 | . 22 | . 13 | . 15 | . 17 | . 20 | . 22 |
| 2 | . 25 | . 27 | .30 | . 32 | . 35 | . 25 | . 27 | . 30 | . 32 | . 35 |
| 3 | . 37 | . 40 | . 42 | . 45 | . 47 | - 37 | . 40 | . 42 | . 45 | . 47 |
| 4 | . 50 | . 52 | . 55 | . 57 | . 60 | . 50 | . 52 | . 55 | . 57 | . 60 |
| 5 | 0.62 | 0.65 | 0.67 | 0.69 | 0.72 | 0.62 | 0.65 | 0.67 | 0.70 | 0.72 |
| 6 | . 74 | . 77 | . 79 | . 82 | . 84 | . 75 | . 77 | . 80 | . 82 | . 85 |
| 7 | . 87 | . 89 | . 92 | . 94 | . 97 | . 87 | . 90 | . 92 | . 95 | . 97 |
| 8 | . 99 | 1.02 | 1.04 | 1.07 | 1.09 | 1.00 | 1.02 | 1.05 | 1.07 | 1.10 |
| 9 | I. 12 | I. 14 | I. 17 | I. 19 | I. 21 | I. 12 | I. 15 | 1.17 | 1.20 | 1.22 |
| 10 | 1.24 | 1.26 | 1.29 | 1.31 | 1.34 | 1.25 | 1.27 | 1.30 | 1.32 | 1.35 |
| 11 | I. 36 | I. 39 | I.4I | 1.44 | I. 46 | I. 37 | 1.40 | 1.42 | 1.45 | 1.47 |
| 12 | I. 49 | 1.51 | 1.54 | 1.56 | 1.59 | 1.50 | 1.52 | 1. 55 | 1.57 | 1.60 |
| 13 | I.6I | I. 64 | I. 66 | 1.68 | 1.71 | 1.62 | 1.65 | 1.67 | 1.70 | 1.72 |
| 14 | 1.73 | 1. 76 | 1.78 | I.8I | 1.83 | 1.75 | 1.77 | 1.80 | 1.82 | I. 85 |
| 15 | 1. 86 | 1. 88 | I.9I | 1.93 | 1.96 | 1.87 | 1.89 | 1.92 | 1.94 | 1.97 |
| 16 | 1.98 | 2.01 | 2.03 | 2.06 | 2.08 | 1.99 | 2.02 | 2.04 | 2.07 | 2.09 |
| 17 | 2. 10 | 2.13 | 2.15 | 2.18 | 2.20 | 2.12 | 2.14 | 2.17 | 2.19 | 2.22 |
| 18 | 2.23 | 2.25 | 2.28 | 2.30 | 2.33 | 2.24 | 2.27 | 2.29 | 2.32 | 2.34 |
| 19 | 2.35 | 2.38 | 2.40 | 2.43 | 2.45 | 2.37 | 2.39 | 2.42 | 2.44 | 2.47 |
| 20 | 2.47 | 2.50 | 2.52 | 2.55 | 2.57 | 2.49 | 2.52 | 2.54 | 2.57 | 2.59 |
| 21 | 2.60 | 2.62 | 2.65 | 2.67 | 2.70 | 2.62 | 2.64 | 2.66 | 2.69 | 2.71 |
| 22 | 2.72 | 2.75 | 2.77 | 2.80 | 2.82 | 2.74 | 2.76 | 2.79 | 2.81 | 2.84 |
| 23 | 2.84 | 2.87 | 2.89 | 2.92 | 2.94 | 2.86 | 2.89 | 2.91 | 2.94 | 2.96 |
| 24 | 2.97 | 2.99 | 3.02 | 3.04 | 3.07 | 2.99 | 3.01 | 3.04 | 3.06 | 3.09 |
| 25 | 3.09 | 3.12 | 3.14 | 3.16 | 3.19 | 3.11 | 3.14 | 3. 16 | 3.19 | 3.21 |
| 26 | 3.21 | 3.24 | 3.26 | 3.29 | 3.31 | 3.23 | 3.26 | 3.28 | 3.31 | 3.33 |
| 27 | 3.34 | 3.36 | 3.39 | 3.41 | 3.43 | 3.36 | 3.38 | 3.41 | 3.43 | 3.46 |
| 28 | 3.46 | 3.48 | 3.51 | 3.53 | 3.56 | 3.48 | 3.51 | 3.53 | 3.56 | 3.58 |
| 29 | 3.58 | 3.61 | 3.63 | 3.66 | 3.68 | 3.61 | 3.63 | 3.66 | 3.68 | 3.70 |
| 30 | 3.71 | 3.73 | 3.75 | 3.78 | 3.80 | 3.73 | 3.75 | 3.78 | 3.80 | 3.83 |
| 31 | 3.83 | 3.85 | 3.88 | 3.90 | 3.93 | 3.85 | 3.88 | 3.90 | 3.93 | 3.95 |
| 32 | 3.95 | 3.98 | 4.00 | 4.02 | 4.05 | 3.98 | 4.00 | 4.03 | 4.05 | 4.08 |
| 33 | 4.07 | 4.10 | 4. 12 | 4.15 | 4.17 | 4.10 | 4.13 | 4.15 | 4.17 | 4.20 |
| 34 | 4.20 | 4.22 | 4.25 | 4.27 | 4.29 | 4.22 | 4.25 | 4.27 | $4 \cdot 30$ | 4.32 |
| 35 | $4 \cdot 32$ | 4.34 | 4.37 | $4 \cdot 39$ | 4.42 | $4 \cdot 35$ | $4 \cdot 37$ | 4.40 | 4.42 | 4.45 |

Smithsonian Tables.

Table 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 770 mm . |  |  |  |  | HEIGIIT OF THE BAROMETER 775 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 |
| 1 | . 13 | . 15 | . 18 | . 20 | . 23 | . 13 | . 15 | . 18 | . 20 | . 23 |
| 2 | .25 | . 28 | - 30 | - 33 | - 35 | . 25 | . 28 | . 30 | - 33 | - 35 |
| 3 | . 38 | . 40 | . 43 | . 45 | . 48 | . 38 | . 40 | . 43 | . 46 | . 48 |
| 4 | . 50 | . 53 | . 55 | . 58 | . 60 | . 51 | - 53 | . 56 | . 58 | .6I |
| 5 | 0.63 | 0.65 | 0.68 | 0.70 | 0.73 | 0.63 | 0.66 | 0.68 | 0.71 | 0.73 |
| 6 | . 75 | . 78 | . 80 | . 83 | . 85 | . 76 | . 78 | .81 | . 83 | . 86 |
| 7 | . 88 | . 90 | . 93 | . 95 | . 98 | . 89 | . 91 | . 94 | . 96 | . 99 |
| 8 | I.OI | 1.03 | 1.06 | 1.08 | I. II | I. OI | I. 04 | 1.06 | 1.09 | I. 11 |
| 9 | I. 13 | I. 16 | I. 18 | I.2I | I. 23 | I. 14 | I. 16 | 1. 19 | I. 21 | 1.24 |
| 10 | I. 26 | I. 28 | 1.3I | 1.33 | 1. 36 | 1.26 | 1.29 | 1.31 | I. 34 | 1. 36 |
| II | I. 38 | 1.41 | 1.43 | 1.46 | I. 48 | I. 39 | 1.42 | I. 44 | 1.47 | I. 49 |
| 12 | 1.51 | 1.53 | I. 56 | I. 58 | I. 61 | 1.52 | 1.54 | I. 57 | I. 59 | 1.62 |
| 13 | 1.63 | 1.66 | 1.68 | 1.71 | 1.73 | 1.64 | 1.67 | 1.69 | 1.72 | 1.74 |
| 14 | 1.76 | 1.78 | I.8I | 1.83 | 1.86 | 1.77 | 1. 79 | 1. 82 | 1.84 | 1.87 |
| 15 | I. 88 | 1.91 | 1.93 | 1.96 | 1.98 | 1.89 | 1.92 | 1.94 | 1.97 | 2.00 |
| 16 | 2.01 | 2.03 | 2.06 | 2.08 | 2.11 | 2.02 | 2.05 | 2.07 | 2.10 | 2.12 |
| 17 | 2.13 | 2.16 | 2.18 | 2.21 | 2.23 | 2.15 | 2.17 | 2.20 | 2.22 | 2.25 |
| I8 | 2.26 | 2.28 | 2.31 | 2.33 | 2.36 | 2.27 | 2.30 | 2.32 | 2.35 | 2.37 |
| 19 | 2.38 | 2.41 | 2.43 | 2.46 | 2.48 | 2.40 | 2.42 | 2.45 | 2.47 | 2.50 |
| 20 | 2.51 | 2.53 | 2.56 | 2.58 | 2.61 | 2.52 | 2.55 | 2.57 | 2.60 | 2.62 |
| 21 | 2.63 | 2.66 | 2.68 | 2.71 | 2.73 | 2.65 | 2.67 | 2.70 | 2.72 | 2.75 |
| 22 | 2.76 | 2.78 | 2.81 | 2.83 | 2.86 | 2.77 | 2.80 | 2.83 | 2.85 | 2.88 |
| 23 | 2.88 | 2.91 | 2.93 | 2.96 | 2.98 | 2.90 | 2.93 | 2.95 | 2.98 | 3.00 |
| 24 | 3.01 | 3.03 | 3.06 | 3.08 | 3.11 | 3.03 | 3.05 | 3.08 | 3.10 | 3.13 |
| 25 | 3.13 | 3.16 | 3.18 | 3.21 | 3.23 | 3.15 | 3.18 | 3.20 | 3.23 | 3.25 |
| 26 | 3.26 | 3.28 | 3.31 | 3.33 | 3.36 | 3.28 | 3.30 | 3.33 | 3.35 | 3.38 |
| 27 | 3.38 | 3.41 | 3.43 | 3.46 | 3.48 | 3.40 | 3.43 | 3.45 | 3.48 | 3.50 |
| 28 | 3.51 | 3.53 | 3.56 | 3.58 | 3.60 | 3.53 | 3.55 | 3.58 | 3.60 | 3.63 |
| 29 | 3.63 | 3.65 | 3.68 | 3.70 | 3.73 | 3.65 | 3.68 | 3.70 | 3.73 | 3.75 |
| 30 | 3.75 | 3.78 | 3.80 | 3.83 | 3.85 | 3.78 | 3.80 | 3.83 | 3.85 | 3.88 |
| 31 | 3.88 | 3.90 | 3.93 | 3.95 | 3.98 | 3.90 | 3.93 | 3.95 | 3.98 | 4.00 |
| 32 | 4.00 | 4.03 | 4.05 | 4.08 | 4.10 | 4.03 | 4.05 | 4.08 | 4. 10 | 4.13 |
| 33 | 4.13 | 4.15 | 4.18 | 4.20 | 4.23 | 4.15 | 4.18 | 4.20 | 4.23 | 4.25 |
| 34 | 4.25 | 4.28 | 4.30 | 4.33 | 4.35 | 4.28 | 4.30 | 4.33 | 4.35 | 4.38 |
| 35 | 4.38 | 4.40 | 4.43 | 4.45 | 4.48 | 4.40 | 4.43 | 4.45 | 4.48 | 4.50 |

Smithoonian Tables.

TAble 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

## METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 780 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 785 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm . |
| $0^{\circ}$ | 0.00 | 0.03 | 0.05 | 0.08 | 0.10 | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 |
| 1 | . 13 | . 15 | . 18 | . 20 | . 23 | . 13 | . 15 | . 18 | . 21 | . 23 |
| 2 | . 25 | . 28 | . 31 | - 33 | - 36 | . 26 | . 28 | . 31 | . 33 | . 36 |
| 3 | . 38 | .41 | . 43 | . 46 | . 48 | . 38 | . 41 | . 44 | . 46 | . 49 |
| 4 | .5I | . 53 | . 56 | . 59 | .6I | .5I | . 54 | . 56 | . 59 | . 62 |
| 5 | 0.64 | 0.66 | 0.69 | 0.71 | 0.74 | 0.64 | 0.67 | 0.69 | 0.72 | 0.74 |
| 6 | . 76 | . 79 | .81 | . 84 | . 87 | . 77 | . 79 | . 82 | . 85 | . 87 |
| 7 | . 89 | . 92 | . 94 | . 97 | . 99 | . 90 | . 92 | . 95 | . 97 | 1.00 |
| 8 | 1.02 | 1.04 | 1.07 | 1.09 | I. 12 | 1.02 | 1.05 | 1.08 | 1. 10 | 1.13 |
| 9 | I. 15 | 1.17 | 1.20 | 1.22 | 1.25 | I. 15 | I. 18 | I. 20 | 1.23 | 1.25 |
| 10 | 1.27 | 1.30 | 1.32 | 1.35 | 1.37 | 1.28 | 1.31 | I. 33 | 1. 36 | 1.38 |
| II | 1.40 | 1.42 | I. 45 | 1.48 | 1.50 | 1.41 | 1.43 | 1.46 | 1.48 | I. 51 |
| 12 | 1.53 | I. 55 | 1. 58 | 1.60 | 1.63 | 1.54 | I. 56 | I. 59 | 1.61 | 1.64 |
| 13 | 1.65 | 1.68 | 1.70 | 1.73 | 1.75 | 1.66 | 1.69 | 1.71 | 1.74 | 1.77 |
| 14 | 1.78 | I.81 | 1.83 | 1.86 | 1.88 | 1.79 | 1.82 | I. 84 | 1.87 | 1.89 |
| 15 | 1.91 | 1.93 | 1.96 | 1.98 | 2.01 | 1.92 | 1.94 | 1.97 | 2.00 | 2.02 |
| 16 | 2.03 | 2.06 | 2.08 | 2.11 | 2.13 | 2.05 | 2.07 | 2.10 | 2.12 | 2. 15 |
| 17 | 2.16 | 2.19 | 2.21 | 2.24 | 2.26 | 2.17 | 2.20 | 2.22 | 2.25 | 2.28 |
| 18 | 2.29 | 2.31 | 2.34 | 2.36 | 2.39 | 2.30 | 2.33 | 2.35 | 2.38 | 2.40 |
| 19 | 2.41 | 2.44 | 2.46 | 2.49 | 2.51 | 2.43 | 2.45 | 2.48 | 2.51 | 2.53 |
| 20 | 2.54 | 2.57 | 2.59 | 2.62 | 2.64 | 2.56 | 2.58 | 2.61 | 2.63 | 2.66 |
| 21 | 2.67 | 2.69 | 2.72 | 2.74 | 2.77 | 2.68 | 2.71 | 2.73 | 2.76 | 2.79 |
| 22 | 2.79 | 2.82 | 2.84 | 2.87 | 2.89 | 2.81 | 2.84 | 2.86 | 2.89 | 2.91 |
| 23 | 2.92 | 2.94 | 2.97 | 3.00 | 3.02 | 2.94 | 2.96 | 2.99 | 3.01 | 3.04 |
| 24 | 3.05 | 3.07 | 3.10 | 3.12 | 3.15 | 3.07 | 3.09 | 3.12 | 3.14 | 3.17 |
| 25 | 3.17 | 3.20 | 3.22 | 3.25 | 3.27 | 3. 19 | 3.22 | 3.24 | 3.27 | 3.29 |
| 26 | 3.30 | 3.32 | 3.35 | 3.37 | 3.40 | 3.32 | 3.34 | 3.37 | 3.40 | 3.42 |
| 27 | 3.42 | 3.45 | 3.47 | 3.50 | 3.53 | 3.45 | 3.47 | 3.50 | 3.52 | 3.55 |
| 28 | 3.55 | 3.58 | 3.60 | 3.63 | 3.65 | 3.57 | 3.60 | 3.62 | 3.65 | 3.67 |
| 29 | 3.68 | 3.70 | 3.73 | 3.75 | 3.78 | 3.70 | 3.73 | 3.75 | 3.78 | 3.80 |
| 30 | 3.80 | 3.83 | 3.85 | 3.88 | 3.90 | 3.83 | 3.85 | 3.88 | 3.90 | 3.93 |
| 31 | 3.93 | 3.95 | 3.98 | 4.00 | 4.03 | 3.95 | 3.98 | 4.00 | 4.03 | 4.06 |
| 32 | 4.05 | 4.08 | 4.11 | 4.13 | 4.16 | 4.08 | 4.11 | 4.13 | 4.16 | 4. 18 |
| 33 | 4.18 | 4.21 | 4.23 | 4.26 | 4.28 | 4.21 | 4.23 | 4.26 | 4.28 | 4.31 |
| 34 | 4.31 | 4.33 | 4.36 | 4.38 | 4.41 | 4.33 | 4.36 | 4.39 | 4.41 | 4.44 |
| 35 | 4.43 | 4.46 | 4.48 | 4.51 | 4.53 | 4.46 | 4.49 | 4.51 | 4.54 | 4.56 |

Smithsonian Tables.

Table 11.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

## METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 790 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 795 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm . | mm . | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.03 | 0.05 | 0.08 | 0.10 | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 |
| 1 | . 13 | . 15 | . 18 | . 21 | . 23 | . 13 | . 16 | . 18 | . 21 | . 23 |
| 2 | . 26 | . 28 | . 31 | - 34 | - 36 | . 26 | . 29 | . 31 | . 34 | . 36 |
| 3 | . 39 | . 41 | . 44 | . 46 | . 49 | . 39 | . 42 | . 44 | . 47 | . 49 |
| 4 | . 52 | . 54 | . 57 | . 59 | . 62 | . 52 | . 55 | . 57 | . 60 | . 62 |
| 5 | 0.64 | 0.67 | 0.70 | 0.72 | 0.75 | 0.65 | 0.67 | 0.70 | 0.73 | 0.75 |
| 6 | . 77 | . 80 | . 83 | . 85 | . 88 | . 78 | . 80 | . 83 | . 86 | . 88 |
| 7 | . 90 | . 93 | . 95 | . 98 | I. OI | .91 | . 93 | . 96 | . 99 | I. OI |
| 8 | 1.03 | 1.06 | 1.08 | I. II | 1.13 | 1.04 | 1.06 | 1.09 | 1.12 | 1. 14 |
| 9 | I. 16 | I. 19 | I. 21 | 1.24 | 1.26 | I. 17 | I. 19 | 1.22 | 1.24 | 1.27 |
| 10 | 1.29 | 1.3I | 1.34 | 1.37 | 1.39 | 1. 30 | 1.32 | 1.35 | 1.37 | 1.40 |
| II | 1. 42 | I. 44 | 1.47 | 1. 49 | 1.52 | 1.43 | 1.45 | 1.48 | 1.50 | 1.53 |
| 12 | I. 55 | 1.57 | 1.60 | 1.62 | 1.65 | 1. 56 | 1.58 | 1.61 | 1.63 | 1.66 |
| 13 | 1.67 | 1.70 | 1.73 | 1.75 | 1.78 | 1.68 | 1.71 | 1.74 | 1.76 | 1.79 |
| 14 | 1.80 | 1.83 | 1.85 | 1.88 | 1.91 | 1.81 | 1.84 | 1.87 | 1.89 | 1.92 |
| 15 | I. 93 | 1.96 | I. 98 | 2.01 | 2.03 | 1.94 | 1.97 | 1.99 | 2.02 | 2.05 |
| 16 | 2.06 | 2.09 | 2.11 | 2.14 | 2.16 | 2.07 | 2.10 | 2.12 | 2.15 | 2.18 |
| 17 | 2.19 | 2.21 | 2.24 | 2.26 | 2.29 | 2.20 | 2.23 | 2.25 | 2.28 | 2.30 |
| 18 | 2.32 | 2.34 | 2.37 | 2.39 | 2.42 | 2.33 | 2.36 | 2.38 | 2.41 | 2.43 |
| 19 | 2.44 | 2.47 | 2.50 | 2.52 | 2.55 | 2.46 | 2.49 | 2.51 | 2.54 | 2.56 |
| 20 | 2.57 | 2.60 | 2.62 | 2.65 | 2.67 | 2.59 | 2.61 | 2.64 | 2.67 | 2.69 |
| 21 | 2.70 | 2.73 | 2.75 | 2.78 | 2.80 | 2.72 | 2.74 | 2.77 | 2.79 | 2.82 |
| 22 | 2.83 | 2.85 | 2.88 | 2.91 | 2.93 | 2.85 | 2.87 | 2.90 | 2.92 | 2.95 |
| 23 | 2.96 | 2.98 | 3.01 | 3.03 | 3.06 | 2.98 | 3.00 | 3.03 | 3.05 | 3.08 |
| 24 | 3.08 | 3.11 | 3.14 | 3.16 | 3.19 | 3.10 | 3.13 | 3.16 | 3.18 | 3.2 I |
| 25 | 3.21 | 3.24 | 3.26 | 3.29 | 3.31 | 3.23 | 3.26 | 3.28 | 3.3 I | 3.34 |
| 26 | 3.34 | 3.37 | 3.39 | 3.42 | 3.44 | 3.36 | 3.39 | 3.41 | 3.44 | 3.46 |
| 27 | 3.47 | 3.49 | 3.52 | 3.54 | 3.57 | 3.49 | 3.52 | 3.54 | 3.57 | 3.59 |
| 28 | 3.60 | 3.62 | 3.65 | 3.67 | 3.70 | 3.62 | 3.64 | 3.67 | 3.70 | 3.72 |
| 29 | 3.72 | 3.75 | 3.77 | 3.80 | 3.83 | 3.75 | 3.77 | 3.80 | 3.82 | 3.85 |
| 30 | 3.85 | 3.88 | 3.90 | 3.93 | 3.95 | 3.88 | 3.90 | 3.93 | 3.95 | 3.98 |
| 31 | 3.98 | 4.00 | 4.03 | 4.06 | 4.08 | 4.00 | 4.03 | 4.06 | 4.08 | 4.11 |
| 32 | 4.11 | 4.13 | 4.16 | 4.18 | 4.21 | 4.13 | 4.16 | 4.18 | 4.21 | 4.24 |
| 33 | 4.23 | 4.26 | 4.29 | $4 \cdot 31$ | 4.34 | 4.26 | 4.29 | $4 \cdot 31$ | $4 \cdot 34$ | 4.36 |
| 34 | $4 \cdot 36$ | 4.39 | 4.41 | 4.44 | 4.46 | $4 \cdot 39$ | 4.42 | 4.44 | 4.47 | 4.49 |
| 35 | 4.49 | $4 \cdot 5 \mathrm{I}$ | 4.54 | 4.57 | 4.59 | 4.52 | 4.54 | 4.57 | 4.59 | 4.62 |

Smithbonian Tableb.

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TABLE 12.
REDUCTION OF THE BAROMETER TO STANDARD GRAVITY.
ENGLISH MEASURES.
Reduction to Latitude $45^{\circ}$.
From latitude $0^{\circ}$ to $45^{\circ}$, the correction is to be subtracted.
From latitude $90^{\circ}$ to $45^{\circ}$, the correction is to be added.

| Latitude. |  | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| $0{ }^{\circ}$ | $90^{\circ}$ | $\begin{aligned} & \text { Inch. } \\ & 0.05 \mathrm{I} \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { Inch. } \\ 0.053 \end{array}$ | $\begin{aligned} & \text { Inch. } \\ & 0.056 \end{aligned}$ | $\begin{array}{l\|l} \text { Inch. } \\ 0.059 \end{array}$ | $\begin{aligned} & \text { Inch. } \\ & 0.061 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.064 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.067 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.069 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.072 \end{aligned}$ | Inch. | $\begin{aligned} & \text { Inch. } \\ & 0.077 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.080 \end{aligned}$ |
| 5 | 85 | 0.050 | 0.052 | 0.055 | 0.058 | 0.060 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 | 0.076 | 0.079 |
| 6 | 84 | . 049 | . 052 | . 055 | . 057 | . 060 | . 062 | . 065 | . 068 | . 070 | . 073 | . 076 | . 078 |
| 7 | 83 | . 049 | . 052 | . 054 | . 057 | . 059 | . 062 | . 065 | . 067 | . 070 | . 072 | . 075 | . 077 |
| 8 | 82 | . 040 | . 051 | . 054 | . 056 | . 059 | .06I | . 064 | . 067 | . 069 | . 072 | . 074 | . 077 |
| 9 | 81 | . 048 | .05I | . 053 | . 056 | . 058 | . 061 | . 063 | . 066 | . 068 | . 071 | . 073 | . 076 |
| 10 | 80 | 0.048 | 0.050 | 0.053 | 0.055 | 0.058 | 0.060 | 0.063 | 0.065 | 0.068 | 0.070 | 0.073 | 0.075 |
| 11 | 79 | . 047 | . 049 | . 052 | . 054 | . 057 | . 059 | . 062 | . 064 | . 067 | . 069 | . 072 | . 074 |
| 12 | 78 | . 046 | . 049 | .05I | . 054 | . 056 | . 058 | . 061 | . 063 | . 066 | . 068 | . 071 | . 073 |
| 13 | 77 | . 045 | . 048 | . 050 | . 053 | . 055 | . 057 | . 060 | . 062 | . 065 | . 067 | . 069 | . 072 |
| 14 | 76 | . 045 | . 047 | . 049 | . 052 | . 054 | . 056 | . 059 | . 06 I | . 063 | . 066 | . 068 | . 071 |
| 15 | 75 | 0.044 | 0.046 | 0.048 | 0.05I | 0.053 | 0.055 | 0.058 | 0.060 | 0.062 | 0.065 | 0.067 | 0.069 |
| 16 | 74 | . 043 | . 045 | . 047 | . 050 | . 052 | . 054 | . 056 | . 059 | .06I | . 063 | . 065 | . 068 |
| 17 | 73 | . 042 | . 044 | . 046 | . 049 | .051 | . 053 | . 055 | . 057 | . 060 | . 062 | . 064 | . 066 |
| 18 | 72 | .041 | . 043 | . 045 | . 047 | . 050 | . 052 | . 054 | . 056 | . 058 | . 060 | . 062 | . 065 |
| 19 | 71 | . 040 | . 042 | . 044 | . 046 | . 048 | . 050 | . 052 | . 055 | . 057 | . 059 | .06I | . 053 |
| 20 | 70 | 0.039 | 0.04 I | 0.043 | 0.045 | 0.047 | 0.049 | 0.051 | 0.053 | 0.055 | 0.057 | 0.059 | 0.061 |
| 21 | 69 | . 038 | . 040 | . 042 | . 044 | . 045 | . 047 | . 049 | .05I | . 053 | . 055 | . 057 | . 059 |
| 22 | 68 | . 036 | . 038 | . 040 | . 042 | . 044 | . 046 | . 048 | . 050 | . 052 | . 054 | . 056 | . 057 |
| 23 | 67 | . 035 | . 037 | . 039 | . 041 | . 043 | . 044 | . 046 | . 048 | .050 | . 052 | . 054 | . 055 |
| 24 | 66 | . 034 | . 036 | . 037 | . 039 | . 041 | . 043 | . 045 | . 046 | . 048 | . 050 | . 052 | . 053 |
| 25 | 65 | 0.033 | 0.034 | 0.036 | 0.038 | 0.039 | 0.04 I | 0.043 | 0.044 | 0.046 | 0.048 | 0.050 | 0.05I |
| 26 | 64 | .03I | . 033 | . 034 | . 036 | . 038 | . 039 | .041 | . 043 | . 044 | . 046 | . 048 | . 049 |
| 27 | 63 | . 030 | . 031 | . 033 | . 034 | . 036 | . 038 | . 039 | .04I | . 042 | . 044 | . 045 | . 047 |
| 28 | 62 | . 028 | . 030 | . 031 | . 033 | . 034 | . 036 | . 037 | . 039 | . 040 | . 042 | . 043 | . 045 |
| 29 | 6I | . 027 | . 028 | . 030 | . 031 | . 032 | . 034 | . 035 | . 037 | . 038 | . 039 | . 041 | . 042 |
| 30 | 60 | 0.025 | 0.027 | 0.028 | 0.029 | 0.03I | 0.032 | 0.033 | 0.035 | 0.036 | 0.037 | 0.039 | 0.040 |
| 31 | 59 | . 024 | . 025 | . 026 | . 027 | . 029 | . 030 | . 33 I | . 032 | . 034 | . 035 | . 036 | . 037 |
| 32 | 58 | . 022 | . 023 | . 025 | . 026 | . 027 | . 028 | . 029 | . 030 | . 032 | . 033 | . 034 | . 035 |
| 33 | 57 | . 021 | . 022 | . 023 | . 024 | . 025 | . 026 | . 027 | . 028 | . 029 | . 030 | . 031 | . 032 |
| 34 | 56 | . 019 | . 020 | . 021 | . 022 | . 023 | . 024 | . 025 | . 026 | . 027 | . 028 | . 029 | . 030 |
| 35 | 55 | 0.017 | 0.018 | 0.019 | 0.020 | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.025 | 0.026 | 0.027 |
| 36 | 54 | . 016 | . 016 | . 017 | . 018 | . 019 | . 020 | . 021 | . 021 | . 022 | . 023 | . 024 | . 025 |
| 37 | 53 | . 014 | . 015 | . 15 | . 016 | . 017 | . 018 | . 018 | . 019 | . 020 | . 021 | . 021 | . 022 |
| 38 | 52 | . 12 | .or3 | . 014 | . 014 | . 1015 | . 015 | .or6 | . 017 | . 017 | . 218 | . 019 | . 019 |
| 39 | 5 I | . 011 | . 011 | . 012 | . 012 | . 013 | . 013 | . 014 | . 014 | . 015 | . 015 | . 016 | . 017 |
| 40 | 50 | 0.009 | 0.009 | 0.010 | 0.010 | 0.01I | O.OII | 0.012 | 0.012 | 0.012 | 0.013 | 0.013 | 0.014 |
| 4 I | 49 | . 007 | . 007 | . 008 | . 008 | . 009 | . 009 | . 009 | . 010 | . 010 | . 10 | . 011 | . OI 1 |
| 42 | 48 | . 005 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 008 |
| 43 | 47 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 005 | . 005 | . 005 | . 005 | . 005 | . 006 |
| 44 | 46 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 003 | . 003 | . 003 | . 003 |
| 45 | 45 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

TABLE 13.
REDUCTION OF THE BAROMETER TO STANDARD GRAVITY.
METRIC MEASURES.

## Reduction to Latitude $45^{\circ}$.

From latitude $0^{\circ}$ to $45^{\circ}$, the correction is to be subtracted. From latitude $90^{\circ}$ to $45^{\circ}$, the correction is to be added.

| Latitude. |  | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 520 | 540 | 560 | 580 | 600 | 620 | 640 | 660 | 680 | 700 | 720 | 740 | 760 | 780 |
|  |  | m. | mm. | m | m | mm. | mm. | mm . | mm. | mm . | m | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | $90^{\circ}$ | 1. 38 | 1.44 | 1.49 | I. 54 | 1.60 | 1.65 | 1.70 | 1.76 | I.8I | 1.86 | 1.92 | 1.97 | 2.02 | 2.08 |
| 5 | 85 | I. 36 | 1.42 | 1.47 | I. 52 | 1.57 | 1.63 | 1.68 | 1.73 | 1.78 | 1. 84 | I. 89 | 1.94 | 1.99 | 2.04 |
| 6 | 84 | I. 35 | I.4I | 1.46 | 1. 51 | 1.56 | 1.61 | 1.67 | 1.72 | 1.77 | 1.82 | 1.87 | 1.93 | 1.98 | 2.03 |
| 7 | 83 | I. 34 | I. 39 | I. 45 | 1. 50 | I. 55 | 1.60 | 1.65 | 1.70 | 1.76 | I.8r | 1.86 | 1.91 | 1.96 | 2.01 |
| 8 | 82 | I. 33 | I. 38 | I. 43 | 1.48 | 1.54 | 1.59 | 1.64 | I. 69 | 1.74 | 1.79 | 1.84 | I. 89 | 1.94 | 2.00 |
| 9 | 81 | I. 32 | 1.37 | 1.42 | I. 47 | I. 52 | 1.57 | 1.62 | I. 67 | 1.72 | 1.77 | 1.82 | 1.87 | 1.92 | 1.97 |
| 10 | 80 | 1.30 | I. 35 | I. 40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1. 85 | 1.90 | 1.95 |
| II | 79 | 1.28 | I. 33 | 1.38 | 1.43 | 1.48 | 1.53 | 1.58 | 1.63 | 1.68 | 1.73 | 1.78 | 1.83 | 1.88 | 1.93 |
| 12 | 78 | I. 26 | 1.31 | I. 36 | I. 41 | I. 46 | I. 51 | I. 56 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.90 |
| 13 | 77 | 1.24 | I. 29 | I. 34 | I. 39 | 1.44 | 1.48 | I. 53 | 1.58 | 1.63 | 1.67 | 1.72 | 1.77 | 1.82 | 1.87 |
| 14 | 76 | 1.22 | 1.27 | 1.32 | 1.36 | 1.41 | 1.46 | 1.50 | I. 55 | 1.60 | I. 65 | 1.69 | 1.74 | 1.79 | 1.83 |
| 15 | 75 | 1.20 | 1.24 | 1.29 | 1.34 | 1.38 | 1.43 | 1.48 | 1.52 | 1.57 | 1.61 | 1.66 | 1.71 | 1.75 | 1.80 |
| 16 | 74 | 1.17 | 1.22 | I. 26 | 1.31 | 1.35 | 1.40 | 1.44 | 1.49 | I. 54 | I. 58 | 1.63 | 1. 67 | 1.72 | 1.76 |
| 17 | 73 | I. 5 | I. 19 | 1.24 | 1.28 | 1.32 | 1.37 | I. 41 | 1.45 | 1.50 | I. 54 | 1.59 | 1.63 | 1.68 | 1.72 |
| 18 | 72 | 1.12 | 1.16 | 1.21 | 1.25 | I. 29 | 1.34 | 1. 38 | 1.42 | I. 46 | I. 51 | 1.55 | I. 59 | 1.64 | 1.68 |
| 19 | 71 | 1.09 | I. 13 | r. 17 | 1.22 | I. 26 | 1.30 | I. 34 | I. 38 | I. 43 | 1.47 | I.5I | I. 55 | I. 59 | 1.64 |
| 20 | 70 | 1.06 | I. 10 | I. 14 | I. 18 | 1.22 | 1.26 | 1.31 | 1.35 | I. 39 | 1.43 | 1.47 | 1.51 | 1. 55 | 1.59 |
| 21 | 69 | 1.03 | 1.07 | I. 11 | 1.15 | I. 19 | 1.23 | 1.27 | I. 31 | I. 35 | 1.38 | I. 42 | 1.46 | 1.50 | I. 54 |
| 22 | 68 | 1.00 | 1.03 | 1.07 | I.II | I. 15 | I. 19 | 1.23 | 1.26 | I. 30 | I. 34 | 1.38 | 1.42 | 1.46 | I. 49 |
| 23 | 67 | 0.96 | 1.00 | 1.04 | 1.07 | I. II | I. 15 | I. 18 | 1.22 | I. 26 | 1.29 | I. 33 | I. 37 | I. 41 | 1.44 |
| 24 | 66 | . 93 | 0.96 | 1.00 | 1.03 | 1.07 | I.10 | I. 14 | I. 18 | I. 21 | 1.25 | I. 28 | I. 32 | I. 35 | I. 39 |
| 25 | 65 | 0.89 | 0.92 | 0.96 | 0.99 | 1.03 | 1.06 | I. 10 | I. 13 | I.16 | 1.20 | 1.23 | 1.27 | 1.30 | 1.33 |
| 26 | 64 | . 85 | . 88 | . 92 | . 95 | 0.98 | 1.02 | 1.05 | 1.08 | I.II | I. 15 | I. 18 | 1.21 | 1.25 | 1.28 |
| 27 | 63 | .8I | . 84 | . 88 | . 91 | . 94 | 0.97 | 1.00 | 1.03 | 1.06 | I. 10 | 1.13 | 1.16 | I.19 | 1.22 |
| 28 | 62 | . 77 | . 80 | . 83 | . 86 | . 89 | . 92 | 0.95 | 0.98 | I.OI | 1.04 | 1.07 | I. 10 | I. 13 | I. 16 |
| 29 | 6 I | . 73 | .76 | . 79 | . 82 | . 85 | . 87 | . 90 | . 93 | 0.96 | 0.99 | 1.02 | 1.04 | 1.07 | I. 10 |
| 30 | 60 | 0.69 | 0.72 | 0.75 | 0.77 | 0.80 | 0.83 | 0.85 | 0.88 | 0.91 | 0.94 | 0.96 | 0.98 | I.OI | 1.04 |
| 31 | 59 | . 65 | . 67 | . 70 | . 72 | . 75 | . 77 | . 80 | . 82 | . 85 | . 87 | . 90 | . 92 | 0.95 | 0.97 |
| 32 | 58 | .61 | . 63 | . 65 | . 68 | . 70 | . 72 | . 75 | . 77 | . 79 | . 82 | . 84 | . 86 | . 89 | . 91 |
| 33 | 57 | . 56 | . 58 | .6I | . 63 | . 65 | . 67 | . 69 | . 71 | . 74 | .76 | .78 | . 80 | . 82 | . 84 |
| 34 | 56 | . 52 | . 54 | . 56 | . 58 | . 60 | . 62 | . 64 | . 66 | . 63 | . 70 | .72 | . 74 | .76 | .78 |
| 35 | 55 | 0.47 | 0.49 | 0.51 | 0. 53 | 0.55 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.66 | 0.67 | 0.69 | 0.71 |
| 36 | 54 | . 43 | . 44 | . 46 | . 48 | . 49 | . 51 | . 53 | . 54 | . 56 | . 58 | . 59 | . 61 | . 63 | . 64 |
| 37 | 53 | . 38 | . 40 | . 41 | . 43 | . 44 | . 45 | . 47 | . 48 | . 50 | . 51 | . 53 | . 54 | . 56 | . 57 |
| 38 | 52 | - 33 | - 35 | . 36 | . 37 | - 39 | . 40 | . 41 | . 43 | . 44 | . 45 | . 46 | . 48 | . 49 | . 50 |
| 39 | 5 I | . 29 | . 30 | -31 | . 32 | - 33 | - 34 | - 35 | - 37 | . 38 | - 39 | . 40 | .4I | . 42 | . 43 |
| 40 | 50 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.3I | 0.3I | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 |
| 41 | 49 | . 19 | . 20 | . 21 | . 21 | . 22 | . 23 | . 24 | . 24 | . 25 | . 26 | . 27 | . 27 | . 28 | . 29 |
| 42 | 48 | . 14 | . 15 | . 16 | . 16 | .17 | . 17 | . 18 | . 18 | . 19 | . 19 | . 20 | . 21 | . 21 | . 22 |
| 43 | 47 | . 10 | . 10 | . 10 | . 11 | . 11 | . 12 | . 12 | . 12 | . 13 | . 13 | . 13 | . 14 | . 14 | . 14 |
| 44 | 46 | . 05 | . 05 | . 05 | . 05 | . 06 | . 06 | . 06 | . 06 | . 06 | . 07 | . 07 | . 07 | . 07 | . 07 |
| 45 | 45 | . 00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

Smithbonian Tables.

Table 14.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.

Values of $2000 \times \mathrm{m}$.
$m=\frac{z}{56573+123 \cdot 1 \theta+.003 z} \cdot \frac{\mathrm{I}}{\mathrm{I}-\boldsymbol{\beta}}$

| Mean Temperature of air column. $\theta$ Fahr. | alfitude of Station in feet (z). |  |  |  |  |  |  |  |  |  | Difference for 100 Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 |  |
| $-20^{\circ}$ | 3.7 | 7.4 | 11.1 | 14.8 | 18.5 | 22.2 | 25.9 | 29.6 | 33.3 | 37.0 | 3.7 |
| 16 | 3.7 | 7.3 | 11.0 | 14.6 | 18.3 | 22.0 | 25.6 | 29.3 | 33.0 | 36.6 | 3.7 |
| 12 | 3.6 | $7 \cdot 3$ | 10.9 | 14.5 | 18.1 | 21.8 | 25.4 | 29.0 | 32.7 | 36.3 | 3.6 |
| - 8 | 3.6 | 7.2 | 10.8 | 14.4 | 18.0 | 21.6 | 25.2 | 28.8 | 32.4 | 36.0 | 3.6 |
| 6 | 3.6 | 7.2 | 10.7 | 14.3 | 17.9 | 21.5 | 25.1 | 28.6 | 32.2 | 35.8 | 3.6 |
| - 4 | 3.6 | 7.1 | 10.7 | 14.3 | 17.8 | 21.4 | 25.0 | 28.5 | 32.1 | 35.6 | 3.6 |
| 2 | 3.5 | 7.1 | 10.7 | 14.2 | 17.7 | 21.3 | 24.8 | 28.4 | 31.9 | 35.4 | 3.5 |
| 0 | 3.5 | 7.1 | 10.6 | 14.1 | 17.7 | 21.2 | 24.7 | 28.3 | 31.8 | 35.3 | 3.5 |
| + 2 | 3.5 | 7.0 | 10.6 | 14.1 | 17.6 | 21.1 | 24.6 | 28.1 | 31.7 | 35.2 | 3.5 |
| 4 | 3.5 | 7.0 | 10.5 | 14.0 | 17.5 | 21.0 | 24.5 | 28.0 | 31.5 | 35.0 | 3.5 |
| 6 | 3.5 | 7.0 | 10.5 | 13.9 | 17.4 | 20.9 | 24.4 | 27.9 | 3 I .4 | 34.9 | 3.5 |
| 8 | 3.5 | 6.9 | 10.4 | 13.9 | 17.4 | 20.8 | 24.3 | 27.8 | 31.2 | 34.7 | 3.5 |
| 10 | 3.5 | 6.9 | 10.4 | 13.8 | 17.3 | 20.7 | 24.2 | 27.7 | 3 I .1 | 34.6 | 3.5 |
| 12 | 3.4 | 6.9 | 10.3 | 13.8 | 17.2 | 20.6 | 24.1 | 27.5 | 31.0 | 34.4 | 3.4 |
| 14 | 3.4 | 6.9 | 10.3 | 13.7 | 17.1 | 20.6 | 24.0 | 27.4 | 30.8 | $34 \cdot 3$ | 3.4 |
| 16 | 3.4 | 6.8 | 10.2 | 13.6 | 17.1 | 20.5 | 23.9 | 27.3 | 30.7 | 34.1 | 3.4 |
| 18 | 3.4 | 6.8 | 10.2 | 13.6 | 17.0 | 20.4 | 23.8 | 27.2 | 30.6 | 34.0 | 3.4 |
| 20 | 3.4 | 6.8 | 10. | 13.5 | 16.9 | 20.3 | 23.7 | 27.1 | 30.4 | 33.8 | 3.4 |
| 22 | 3.4 | 6.7 | 10.1 | 13.5 | 16.8 | 20.2 | 23.6 | 26.9 | 30.3 | 33.7 | 3.4 |
| 24 | 3.4 | 6.7 | 10.1 | 13.4 | 16.8 | 20.1 | 23.5 | 26.8 | 30.2 | 33.5 | 3.4 |
| 26 | $3 \cdot 3$ | 6.7 | 10.0 | I 3.4 | 16.7 | 20.0 | 23.4 | 26.7 | 30.1 | 33.4 | 3.3 |
| 28 | $3 \cdot 3$ | 6.7 | 10.0 | 13.3 | 16.6 | 20.0 | 23.3 | 26.6 | 29.9 | 33.3 | $3 \cdot 3$ |
| 30 | $3 \cdot 3$ | 6.6 | 9.9 | 13.2 | 16.6 | 19.9 | 23.2 | 26.5 | 29.8 | 33.1 | $3 \cdot 3$ |
| 32 | $3 \cdot 3$ | 6.6 | 9.9 | 13.2 | 16.5 | 19.8 | 23.1 | 26.4 | 29.7 | 33.0 | $3 \cdot 3$ |
| 34 | $3 \cdot 3$ | 6.6 | 9.9 | 13.1 | 16.4 | 19.7 | 23.0 | 26.3 | 29.6 | 32.8 | 3.3 |
|  | $3 \cdot 3$ | 6.5 | 9.8 | 13.1 | 16.4 | 19.6 | 22.9 | 26.2 | 29.4 | 32.7 | 3.3 |
| 38 | $3 \cdot 3$ | 6.5 | 9.8 | 13.0 | 16.3 | 19.5 | 22.8 | 26.0 | 29.3 | 32.6 | 3.3 |
| 40 | 3.2 | 6.5 | 9.7 | 13.0 | 16.2 | 19.5 | 22.7 | 25.9 | 29.2 | 32.4 | 3.2 |
| 42 | 3.2 | 6.5 | 9.7 | 12.9 | 16. 1 | 19.4 | 22.6 | 25.8 | 29.1 | 32.3 | 3.2 |
| 44 | 3.2 | 6.4 | 9.6 | 12.9 | 16.1 | 19.3 | 22.5 | 25.7 | 28.9 | 32.1 | 3.2 |
| 46 | 3.2 | 6.4 | 9.6 | 12.8 | 16.0 | 19.2 | 22.4 | 25.6 | 28.8 | 32.0 | 3.2 |
| 48 | 3.2 | 6.4 | 9.6 | 12.7 | 15.9 | 19.1 | 22.3 | 25.5 | 28.7 | 31.9 | 3.2 |
| 50 | 3.2 | 6.3 | 9.5 | 12.7 | 15.9 | 19.0 | 22.2 | 25.4 | 28.6 | 31.7 | 3.2 |
| 52 | 3.2 | 6.3 | 9.5 | 12.6 | 15.8 | 19.0 | 22. | 25.3 | 28.4 | 31.6 | 3.2 |
| 54 | 3.1 | 6.3 | 9.4 | 12.6 | 15.7 | 18.9 | 22.0 | 25.2 | 28.3 | 31.5 | 3.1 |
| 56 | 3.1 | 6.3 | 9.4 | 12.5 | 15.7 | 18.8 | 21.9 | 25.1 | 28.2 | 3 I .3 | 3. I |
| 58 | 3.1 | 6.2 | 9.4 | 12.5 | 15.6 | 18.7 | 21.8 | 25.0 | 28.1 | 31.2 | 3.I |
| 60 | 3.1 | 6.2 | 9.3 | 12.4 | 15.5 | 18.6 | 21.7 | 24.8 | 28.0 | 31.1 | 3.1 |
| 62 | 3.1 | 6.2 | 9.3 | 12.4 | 15.5 | 18.6 | 21.6 | 24.7 | 27.8 | 30.9 | 3.1 |
| 64 | $3 \cdot 1$ | 6.2 | 9.2 | 12.3 | 15.4 | 18.5 | 21.6 | 24.6 | 27.7 | 30.8 | 3.1 |
| 66 | 3.1 | 6.1 | 9.2 | 12.3 | 15.3 | 18.4 | 21.5 | 24.5 | 27.6 | 30.7 | 3.1 |
| 68 | 3.1 | 6.1 | 9.2 | 12.2 | 15.3 | 18.3 | 21.4 | 24.4 | 27.5 | 30.5 | 3.1 |
| 70 | 3.0 | 6.1 | 9.1 | 12.2 | 15.2 | 18.2 | 21.3 | 24.3 | 27.4 | 30.4 | 3.0 |
| 72 | 3.0 | 6.1 | 9.1 | 12.1 | 15.1 | 18.2 | 21.2 | 24.2 | 27.3 | 30.3 | 3.0 |
| 76 | 3.0 | 6.0 | 9.0 | 12.0 | 15.0 | 18.0 | 21.0 | 24.0 | 27.0 | 30.0 | 3.0 |
| 80 | 3.0 | 6.0 | 8.9 | 11.9 | 14.9 | 17.9 | 20.9 | 23.8 | 26.8 | 29.8 | 3.0 |
| 84 | 3.0 | 5.9 | 8.9 | 11.8 | 14.8 | 17.7 | 20.7 | 23.6 | 26.6 | 29.6 | 3.0 |
| 88 | 2.9 | 5.9 | 8.8 | 11.7 | 14.7 | 17.6 | 20.5 | 23.5 | 26.4 | 29.3 | 2.9 |
| 92 | 2.9 | 5.8 | 8.7 | 11.6 | 14.5 | 17.4 | 20.4 | 23.3 | 26.2 | 29.1 | 2.9 |
| 96 | 2.9 | 5.8 | 8.7 | 11.5 | 14.4 | 17.3 | 20.2 | 23.1 | 26.0 | 28.9 | 2.9 |

TABLE 14.
REDUCTION OF THE BAROMETER TO SEA LEVEL.
ENGLISH MEASURES.
Values of $2000 \times \mathbf{m}$.
$m=\frac{\mathrm{Z}}{56573+\mathrm{I} 23 \cdot 1 \theta+.003 \mathrm{Z}} \cdot \frac{\mathrm{I}}{1-\beta}$

| Mean Temperature of air column. $\theta$ Fahr. | alititude of Station in feet (z). |  |  |  |  |  |  |  |  |  | $\left\lvert\, \begin{gathered} \text { Differ- } \\ \text { ence } \\ \text { for } \\ 100 \\ \text { Feet. } \end{gathered}\right.$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1100 | 1200 | 1300 | 1400 | 1500 | 1600 | 1700 | 1800 | 1900 | 2000 |  |
| $-20^{\circ}$ | 40.7 | 44.3 | 48.0 | 51.7 | 55.4 | 59. I | 62.8 | 66.5 | 70.2 | 73.9 | 3.7 |
| - 16 | 40.3 | 43.9 | 47.6 | 51.3 | 54.9 | 58.6 | 62.2 | 65.9 | 69.6 | 73.2 | 3.7 |
| - 12 | 39.9 | 43.5 | 47.2 | 50.8 | 54.4 | 58.1 | 6 I .7 | 65.3 | 68.9 | 72.6 | 3.6 |
| - 8 | 39.6 | 43.2 | 46.7 | 50.3 | 53.9 | 57.5 | 61.1 | 64.7 | 68.3 | 71.9 | 3.6 |
| - 6 | 39.4 | 43.8 | 46.5 | 50.1 | 53.7 | 57.3 | 60.9 | 64.4 | 68.0 | 71.6 | 3.6 |
| 4 | 39.2 | 42.8 | 46.3 | 49.9 | 53.5 | 57.0 | 60.6 | 64.2 | 67.7 | 71.3 | 3.6 |
| - 2 | 39.0 | 42.6 | 46.1 | 49.7 | 53.2 | 56.8 | 60.3 | 63.9 | 67.4 | 71.0 | 3.6 |
| 0 | 38.9 | 42.4 | 45.9 | 49.5 | 53.0 | 56.5 | 60.1 | 63.6 | 67.1 | 70.6 | 3.5 |
| + 2 | 38.7 | 42.2 | 45.7 | 49.2 | 52.8 | 56.3 | 59.8 | 63.3 | 66.8 | 70.3 | 3.5 |
|  | 38.5 | 42.0 | 45.5 | 49.0 | 52.5 | 56.0 | 59.5 | 63.0 | 66.5 | 70.0 | 3.5 |
| 6 | 38.4 | 41.8 | $45 \cdot 3$ | 48.8 | 52.3 | 55.8 | 59.3 | 62.8 | 66.2 | 69.7 | 3.5 |
| 8 | 38.2 | 41.7 | 45. I | 48.6 | 52.1 | 55.5 | 59.0 | 62.5 | 66.0 | 69.4 | 3.5 |
| 10 | 38.0 | 41.5 | 44.9 | 48.4 | 51.8 | 55.3 | 58.8 | 62.2 | 65.7 | 69.1 | 3.5 |
| 12 | 37.9 | 4 r .3 | 44.7 | 48.2 | 51.6 | 55. ${ }^{\text {I }}$ | 58.5 | 61.9 | 65.4 | 68.8 | 3.4 |
| 14 | 37.7 | 41.1 | 44.5 | 48.0 | 5 I .4 | 54.8 | 58.2 | 61.7 | 65.1 | 68.5 | 3.4 |
| 16 | 37.5 | 40.9 | 44.4 | 47.8 | 51.2 | 54.6 | 58.0 | 61.4 | 64.8 | 68.2 | 3.4 |
| 18 | 37.4 | 40.8 | 44.2 | 47.6 | 51.0 | 54.4 | 57.8 | 6 r .1 | 64.5 | 67.9 | 3.4 |
| 20 | 37.2 | 40.6 | 44.0 | 47.4 | 50.7 | 54.1 | 57.5 | 60.9 | 64.3 | 67.7 | 3.4 |
| 22 | 37. 1 | 40.4 | 43.8 | 47.2 | 50.5 | 53.9 | 57.3 | 60.6 | 64.0 | 67.4 | 3.4 |
| 24 | 36.9 | 40.3 | 43.6 | 47.0 | 50.3 | 53.7 | 57.0 | 60.4 | 63.7 | 67.1 | 3.4 |
| 26 | 36.7 | 40.1 | 43.4 | 46.8 | 50.1 | 53.4 | 56.8 | 60.1 | 63.5 | 66.8 | 3.3 |
| 28 | 36.6 | 39.9 | 43.2 | 46.6 | 49.9 | 53.2 | 56.5 | 59.9 | 63.2 | 66.5 | 3.3 |
| 30 | 36.4 | 39.7 | 43.1 | 46.4 | 49.7 | 53.0 | 56.3 | 59.6 | 62.9 | 66.2 |  |
| 32 | 36.3 | 39.6 | 42.9 | 46.2 | 49.5 | 52.8 | 56. 1 | 59.4 | 62.7 | 66.0 | 3.3 |
| 34 | 36. I | 39.4 | 42.7 | 46.0 | 49.3 | 52.5 | 55.8 | 59.1 | 62.4 | 65.7 | $3 \cdot 3$ |
| 36 | 36.0 | 39.2 | 42.5 | 45.8 | 49.0 | 52.3 | 55.6 | 58.9 | 62.1 | 65.4 | $3 \cdot 3$ |
| 38 | 35.8 | 39.1 | 42.3 | 45.6 | 48.8 | 52.1 | 55.3 | 58.6 | 61.9 | 65.1 | 3.3 |
| 40 | 35.7 | 38.9 | 42.1 | 45.4 | 48.6 | 51.9 | 55.1 | 58.4 | 61.6 | 64.8 | 3.2 |
| 42 | 35.5 | 38.7 | 42.0 | 45.2 | 48.4 | 51.6 | 54.9 | 58.1 | ${ }_{61.3}$ | 64.6 | 3.2 |
|  | 35.4 | 38.6 | 4 I .8 | 45.0 | 48.2 | 51.4 | 54.6 | 57.9 | 61.1 | 64.3 | 3.2 |
| 46 | 35.2 | 38.4 | 4 I .6 | 44.8 | 48.0 | 51.2 | 54.4 | 57.6 | 60.8 | 64.0 | 3.2 |
| 48 | 35. 1 | 38.2 | 41.4 | 44.6 | 47.8 | 51.0 | 54.2 | 57.4 | 60.5 | 63.7 | 3.2 |
| 50 | 34.9 | 38.1 | 41.2 | 44.4 | 47.6 | 50.8 | 53.9 | 57.1 | 60.3 | 63.4 | 3.2 |
| 52 | 34.8 | 37.9 | 41.1 | 44.2 | 47.4 | 50.5 | 53.7 | 56.9 | 60.0 | 63.2 | 3.2 |
| 54 | 34.6 | 37.7 | 40.9 | 44.0 | 47.2 | 50.3 | 53.5 | 56.6 | 59.8 | 62.9 | 3.1 |
| 56 | 34.5 | 37.6 | 40.7 | 43.9 | 47.0 | 50.1 | 53.2 | 56.4 | 59.5 | 62.6 | 3.1 |
| 58 | 34.3 | 37.4 | 40.5 | 43.7 | 46.8 | 49.9 | 53.0 | 56.1 | 59.3 | 62.4 | 3.1 |
| 60 | 34.2 | 37.3 | 40.4 | 43.5 | 46.6 | 49.7 | 52.8 | 55.9 | 59.0 | 62.1 | 3.1 |
| 62 | 34.0 | 37.1 | 40.2 | 43.3 | 46.4 | 49.5 | 52.6 | 55.7 | 58.8 | 61.9 | 3.1 |
| 64 | 33.9 | 37.0 | 40.0 | 43.1 | 46.2 | 49.3 | 52.4 | 55.4 | 58.5 | 61.6 | 3. I |
| 66 | 33.7 | 36.8 | 39.9 | 42.9 | 46.0 | 49.1 | 52.1 | 55.2 | 58.3 | 6 I .3 | 3.1 |
| 68 | 33.6 | 36.6 | 39.7 | 42.8 | 45.8 | 48.9 | 51.9 | 55.0 | 58.0 | 61.1 | 3. I |
| 70 | 33.5 | 36.5 | 39.5 | 42.6 | 45.6 | 48.7 | 51.7 | 54:7 | 57.8 | 60.8 | 3.0 |
| 72 | 33.3 | 36.3 | 39.4 | 42.4 | 45.4 | 48.5 | 51.5 | 54.5 | 57.5 | 60.6 | 3.0 |
| 76 | 33.0 | 36.0 | 39.1 | 42.1 | 45.1 | 48.1 | 51.1 | 54.1 | 57.1 | 60.1 | 3.0 |
| 80 | 32.8 | 35.8 | 38.7 | 41.7 | 44.7 | 47.7 | 50.6 | 53.6 | 56.6 | 59.6 | 3.0 |
| 84 | 32.5 | 35.5 | 38.4 | 41.4 | 44.3 | 47.3 | 50.2 | 53.2 | 56.2 | 59.1 | 3.0 |
| 88 | 32.2 | 35.2 | 38.1 | 4 I .0 | 44.0 | 46.9 | 49.8 | 52.8 | 55.7 | 58.6 | 2.9 |
| 92 | 32.0 | 34.9 | 37.8 | 40.7 | 43.6 | 46.5 | 49.4 | 52.3 | 55.3 | 58.2 | 2.9 |
| 96 | 31.7 | 34.6 | 37.5 | 40.4 | 43.3 | 46.2 | 49.0 | 51.9 | 54.8 | 57.7 | 2.9 |

Table 14.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.

Values of $2000 \times \mathbf{m}$.
$m=\frac{z}{56573+123 \cdot 1 \theta+.003 z} \cdot \frac{1}{1 \div \beta}$

| Mean Temperature of air column. $\theta$ Fahr. | altitude of station in feet (z). |  |  |  |  |  |  |  |  |  | Difference for 100 Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2100 | 2200 | 2300 | 2400 | 2500 | 2600 | 2700 | 2800 | 2900 | 3000 |  |
| $-20^{\circ}$ | 77.6 | 81.3 | 85.0 | 88.7 | 92.4 | 96.1 | 99.8 | 103.5 | 107.2 | 110.9 | 3.7 |
| - 16 | 76.9 | 80.6 | 84.2 | 87.9 | 91.5 | 95.2 | 98.9 | 102.5 | 106.2 | 109.8 | 3.7 |
| - 12 | 76.2 | 79.8 | 83.5 | 87. 1 | 90.7 | 94.3 | 98.0 | 101.6 | 105.2 | 108.8 | 3.6 |
| - 8 | 75.5 | 79.1 | 82.7 | 86.3 | 89.9 | 93.5 | 97.1 | 100.7 | 104.3 | 107.9 | 3.6 |
| 6 | 75.2 | 78.8 | 82.3 | 85.9 | 89.5 | 93.1 | 96.6 | 100.2 | 103.8 | 107.4 | 3.6 |
| - 4 | 74.8 | 78.4 | 82.0 | 85.5 | 89.1 | 92.7 | 96.2 | 99.8 | 103.3 | 106.9 | 3.6 |
| 2 | 74.5 | 78.1 | 8 r .6 | 85.2 | 88.7 | 92.2 | 95.8 | 99.3 | 102.9 | 106.4 | 3.5 |
| 0 | 74.2 | 77.7 | 81.2 | 84.8 | 88.3 | 9 c .8 | 95.4 | 98.9 | 102.5 | 106.0 | 3.5 |
| + 2 | 73.9 | 77.4 | 80.9 | 84.4 | 87.9 | 91.4 | 95.0 | 98.5 | 102.0 | 105.5 | 3.5 |
|  | 73.5 | 77.0 | 80.5 | 84.0 | 87.5 | 91.0 | 94.5 | 98.0 | 101.5 | 105.0 | 3.5 |
| 6 | 73.2 | 76.7 | 80.2 | 83.7 | 87.2 868 | 90.6 | 94.1 | 97.6 | IOI. 1 | 104.6 | 3.5 |
| 8 | 72.9 | 76.4 | 79.8 | 83.3 | 86.8 | 90.2 | 93.7 | 97.2 | 100.7 | 104.1 | 3.5 |
| 10 | 72.6 | 76.0 | 79.5 | 82.9 | 86.4 | 89.9 | 93.3 | 96.8 | 100.2 | 103.7 | 3.5 |
| 12 | 72.3 | 75.7 | 79.1 | 82.6 | 86.0 | 89.5 | 92.9 | 96.3 | 99.8 | $1{ }^{1} 3.2$ | 3.4 |
| 14 | 72.0 | 75.4 | 78.8 | 82.2 | 85.7 | 89.1 | 92.5 | 95.9 | 99.4 | 102.8 | 3.4 |
| 16 | 71.6 | 75.I | 78.5 | 8 I .9 | 85.3 | 88.7 | 92.1 | 95.5 | 98.9 | 102.3 | 3.4 |
| 18 | 71.3 | 74.7 | 78.1 | 81.5 | 84.9 | 88.3 | 91.7 | 95.1 | 98.5 | IOI. 9 | 3.4 |
| 20 | 71.0 | 74.4 | 77.8 | 81.2 | 84.6 | 87.9 | 91.3 | 94.7 | 98.1 | IOI. 5 | 3.4 |
| 22 | 70.7 | 74.1 | 77.5 | 80.8 | 84.2 | 87.6 | 90.9 | 94.3 | 97.7 | IOI. 0 | 3.4 |
| 24 | 70.4 | 73.8 | 77.1 | 80.5 | 83.8 | 87.2 | 90.6 | 93.9 | 97.3 | 100. | 3.4 |
| 26 | 70.1 | 73.5 | 76.8 | 80.2 | 83.5 | 86.8 | 90.2 | 93.5 | 96.9 | 100. | 3.3 |
| 28 | 69.8 | 73.2 | 76.5 | 79.8 | 83.1 | 86.5 | 89.8 | 93.1 | 96.4 | 99.8 | $3 \cdot 3$ |
| 30 | 69.5 | 72.9 | 76.2 | 79.5 | 82.8 | 86. 1 | 89.4 | 92.7 | 96.0 | 99.3 | $3 \cdot 3$ |
| 32 | 69.2 | 72.5 | 75.8 | 79.1 | 82.4 | 85.7 | 89.0 | 92.3 | 95.6 | 98.9 | 3.3 |
| 34 | 69.0 | 72.2 | 75.5 | 78.8 | 82.1 | 85.4 | 88.7 | 91.9 | 95.2 | 98.5 | $3 \cdot 3$ |
| 36 | 68.7 | 71.9 | 75.2 | 78.5 | 81.7 | 85.0 | 88.3 | 91.5 | 94.8 | 98.1 | $3 \cdot 3$ |
| 38 | 68.4 | 71.6 | 74.9 | 78.1 | 8 I .4 | 84.6 | 87.9 | 91.2 | 94.4 | 97.7 | $3 \cdot 3$ |
| 40 | 68.1 | 71.3 | 74.6 | 77.8 | 8 I .0 | 84.3 | 87.5 | 90.8 | 94.0 | 97.2 | 3.2 |
| 42 | 67.8 | 71.0 | 74.2 | 77.5 | 80.7 | 83.9 | 87.1 | 90.4 | 93.6 | 96.8 | 3.2 |
| 44 | 67.5 | 70.7 | 73.9 | 77.1 | 80.3 | 83.6 | 86.8 | 90.0 | 93.2 | 96.4 | 3.2 |
| 46 | 67.2 | 70.4 | 73.6 | 76.8 | 80.0 | 83.2 | 86.4 | 89.6 | 92.8 | 96.0 | 3.2 |
| 48 | 66.9 | 70.1 | 73.3 | 76.5 | 79.7 | 82.8 | 86. | 89.2 | 92.4 | 95.6 | 3.2 |
| 50 | 66.6 | 69.8 | 73.0 | 76.1 | 79.3 | 82.5 | 85.7 | 88.8 | 92.0 | 95.2 | 3.2 |
| 52 | 66.3 | 69.5 | 72.7 | 75.8 | 79.0 | 82.1 | 85.3 | 88.4 | 91.6 | 94.8 | 3.2 |
|  | 66.1 |  | 72.3 | 75.5 |  | 81. 8 | 84.9 | 88.1 | 91.2 | 94.4 | 3. 1 |
| 56 | 65.8 | 68.9 | 72.0 | 75.2 | 78.3 | 8 I .4 | 84.6 | 87.7 | 90.8 | 94.0 | 3.1 |
| 58 | 65.5 | 68.6 | 71.7 | 74.9 | 78.0 | 81.1 | 84.2 | 87.3 | 90.4 | 93.6 | 3.1 |
| 60 | 65.2 | 68.3 | 71.4 | 74.5 | 77.6 | 80.7 | 83.8 | 87.0 | 90.1 | 93.2 | 3.1 |
| 62 | 64.9 | 68.0 | 71.1 | 74.2 | 77.3 | 80.4 | 83.5 | 86.6 | 89.7 | 92.8 | 3.1 |
| 64 | 64.7 | 67.8 | 70.8 | 73.9 | 77.0 | 80.1 | 83.1 | 86.2 | 89.3 | 92.4 | 3.1 |
| 66 | 64.4 | 67.5 | 70.5 | $73 \cdot 6$ | 76.7 | 79.7 | 8 | 85.9 | 88.9 | 92.0 | 3. I |
| 68 | 64.I | 67.2 | 70.2 | 73.3 | 76.3 | 79.4 | 82.5 | 85.5 | 88.6 | 91.6 | 3.1 |
| 70 | 63.9 | 66.9 | 69.9 | 73.0 | 76.0 | 79.1 | 82.1 | 85.1 | 88.2 | 91.2 | 3.0 |
| 72 | 63.6 | 66.6 | 69.7 | 72.7 | 75.7 | 78.7 | 8 r .8 | 84.8 | 87.8 | 90.9 | 3.0 |
| 76 | 63.1 | 66. I | 69. I | 72.1 | 75.1 | 78.1 | 8 I .1 | 84.1 | 87.1 | 90.1 | 3.0 |
| 80 | 62.6 | 65.5 | 68.5 | 71.5 | 74.5 | 77.5 | 80.5 | 83.4 | 86.4 | 89.4 | 3.0 |
| 84 | 62.1 | 65.0 | 68.0 | 70.9 | 73.9 | 76.8 | 79.8 | 82.7 | 85.7 | 88.6 | 3.0 |
| 88 | 6 r .6 | 64.5 | 67.4 | 70.4 | 73.3 | 76.2 | 79.1 | 82.1 | 85.0 | 87.9 | 2.9 |
| 92 | 61.I | 64.0 | 66.9 | 69.8 | 72.7 | 75.6 | 78.5 | 8 8 .4 | 84.3 | 87.2 | 2.9 |
| 96 | 60.6 | 63.5 | 66.4 | 69.2 | 72.1 | 75.0 | 77.9 | 80.8 | 83.7 | 86.5 | 2.9 |

TAble 14.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.
Values of $2000 \times m . \quad m=\frac{z}{56573+123 \cdot 1 \theta+.003 z} \cdot \frac{1}{1-\beta}$

| Mean Temperature of air column. $\theta$ Fahr. | alititude of station in feet (z). |  |  |  |  |  |  |  |  |  | $\begin{array}{\|l\|} \hline \text { Differ- } \\ \text { ence } \\ \text { for } \\ 100 \\ 10 e e t . \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3100 | 3200 | 3300 | 3400 | 3500 | 3600 | 3700 | 3800 | 3900 | 4000 |  |
| $-20^{\circ}$ | 114.5 | 118.2 | 121.9 | 125.6 | 129.3 | 133.0 | 136.7 | 140.4 | I44. I | 147.8 | 3.7 |
| 16 | 113.5 | 117.2 | 120.8 | 124.5 | 128.1 | I 31.8 | 135.5 | 139.1 | 142.8 | 146.4 | 3.7 |
| 2 | 12.5 | 116.1 | 119.7 | 123.3 | 127.0 | 130.6 | 134.2 | 137.9 | 141.5 | I45. 1 | 3.6 |
| - 8 | III. 5 | II5.1 | 188.7 | 122.3 | 125.9 | 129.4 | 133.0 | 136.6 | 140.2 | 143.8 | 3.6 |
| 6 | 111.0 | 114.5 | 188.1 | 121.7 | 125.3 | 128.9 | 132.4 | 136.0 | 139.6 | 143.2 | 3.6 |
| 4 | 110.5 | 114.0 | 117.6 | 121.2 | 124.7 | 128.3 | 131.9 | 135.4 | 139.0 | 142.5 | 3.6 |
| 2 | 110.0 | 113.5 | 117.1 | 120.6 | 124.2 | 127.7 | 131.3 | 134.8 | I 38.4 | 141.9 | 3.5 |
| 0 | 109.5 | 113.0 | 116.6 | 120.1 | 123.6 | 127.2 | 130.7 | 134.2 | 137.8 | 141.3 | 3.5 |
| + 2 | 109.0 | 112.5 | 116. | 119.6 | 123.1 | 126.6 | 130.1 | 133.6 | 137.1 | 140.7 | 3.5 |
| 4 | 108.5 | 12.0 | 115.5 | 119.0 | 122.5 | 126.0 | 129.5 | 133.0 | 136.5 | 140.0 | 3.5 |
| 6 | 108.1 | III. 6 | 115.0 | 188.5 | 122.0 | 125.5 | 129.0 | 132.5 | 135.9 | 139.4 | 3.5 |
| 8 | 107.6 | III. 1 | 114.5 | 118.0 | 121.5 | 124.9 | 128.4 | 131.9 | I 35.4 | 138.8 | 3.5 |
| 10 | 107.1 | 110.6 | 114.0 | 117.5 | 121.0 | 124.4 | 127.9 | 13 I .3 | 134.8 | 138.2 | 3.5 |
| 12 | 106.7 | 110.1 | 113.6 | 117.0 | 120.4 | 123.9 | 127.3 | 130.7 | 134.2 | 137.6 | 3.4 |
| 14 | 106.2 | 109.6 | 113.1 | 116.5 | 119.9 | 123.3 | 126.8 | 130.2 | 133.6 | 137.0 | 3.4 |
| 16 | 105.8 | 109. 2 | 112.6 | 116.0 | 119.4 | 122.8 | 126.2 | 129.6 | 133.0 | 136.5 | 3.4 |
| 18 | 105.3 | 108.7 | II2.I | 115.5 | 118.9 | 122.3 | 125.7 | 129.1 | 132.5 | I 35.9 | 3.4 |
| 20 | 104.9 | 108.2 | 111.6 | 115.0 | 118.4 | 121.8 | 125.1 | 128.5 | 131.9 | 135.3 | 3.4 |
| 22 | 104.4 | 107.8 | III. 1 | 114.5 | 117.9 | 12 | 124.6 | 128.0 | 131.3 | 134.7 | 3.4 |
| 24 | 104.0 | 107.3 | 110.7 | 114.0 | 117.4 | 120.7 | 124.1 | 127.4 | 130.8 | 134.I | 3.4 |
| 26 | 103.5 | 106.9 | 110.2 | 113.5 | 116.9 | 120.2 | 123.6 | 126.9 | 130.2 | I33.6 | 3.3 |
| 28 | 103.1 | 106.4 | 109.7 | II3.1 | 116.4 | 119.7 | 123.0 | 126.4 | 129.7 | 133.0 | 3.3 |
| 30 | 102.7 | 106.0 | 109.3 | 112.6 | 115.9 | 119.2 | 122.5 | 125.8 | 129.1 | 132.4 | 3.3 |
| 32 | 102.2 | 105.5 | 108.8 | 122.1 | 115.4 | 118.7 | 122.0 | 125.3 | 128.6 | 131.9 | 3.3 |
| 34 | 1о1. 8 | 105.I | 108.3 | 111.6 | 114.9 | 188.2 | 121.5 | 124.8 | 128.0 | 131.3 | $3 \cdot 3$ |
| 36 | IOI. 3 | 104.6 | 107.9 | III. 2 | 114.4 | 117.7 | 121.0 | 124.2 | 127.5 | 130.8 | 3.3 |
| 38 | 100.9 | 104.1 | 107.4 | 110.7 | II3.9 | 117.2 | 120.4 | 123.7 | 126.9 | 130.2 | 3.3 |
| 40 | 100. | 103.7 | 107.0 | 110. | 113.4 | 116.7 | 119.9 | 123.2 | 126.4 | 129.6 | 3.2 |
| 42 | 100.0 | 103.3 | 106.5 | 109.7 | 113.0 | 116.2 | 119.4 | 122.6 | 125.9 | 129.1 | 3.2 |
| 44 | 99.6 | 102.8 | 106.0 | 109.3 | 112.5 | 115.7 | 118.9 | 122.1 | 125.3 | 128.5 | 3.2 |
| 46 | 99.2 | 102.4 | 105.6 | 108.8 | 112.0 | 155.2 | 118.4 | 121.6 | 124.8 | 128.0 | 3.2 |
| 48 | 98.8 | 101.9 | 105.1 | 108.3 | III. 5 | 114.7 | 117.9 | 121. | 124.2 | 127.4 | 3.2 |
| 50 | 98.3 | 101. 5 | 104.7 | 107.9 | III.O | 114.2 | 117.4 | 120.5 | 123.7 | 126.9 | 3.2 |
| 52 | 97.9 | 101. 1 | 104.2 | 107.4 | 110.5 | 113.7 | 116.9 | 120.0 | 123.2 | 126.3 | 3.2 |
| 54 | 97.5 | 100. 6 | 103.8 | 106.9 | Iro. 1 | 113.2 | 116.4 | 119.5 | 122.7 | 125.8 | 3.1 |
| 56 | 97.1 | 100.2 | 103.3 | 106.5 | 109.6 | 112.7 | 115.9 | 119.0 | 122.1 | 125.2 | 3.1 |
| 58 | 96.7 | 99.8 | 102.9 | 106.0 | 109. 1 | 112.3 | 115.4 | 118.5 | 121.6 | 124.7 | 3.1 |
| 60 | 96.3 | 99.4 | 102.5 | 105.6 | 108.7 | 111.8 | 114.9 | 188.0 | 121.1 | 124.2 | 3.1 |
| 62 | 95.9 | 98.9 | 102.0 | 105.1 | 108.2 | 111.3 | 114.4 | 117.5 | 120.6 | 123.7 | 3. I |
| 64 | 95.5 | 98.5 | 101. 6 | 104.7 | 107.8 | 110.8 | 113.9 | 117.0 | 120.1 | 123.1 | 3.1 |
| 66 | 95.1 | 98.1 | IOI. 2 | 104.3 | 107.3 | 110.4 | 113.5 | 116.5 | 119.6 | 122.6 | 3.1 |
| 68 | 94.7 | 97.7 | 100.8 | 103.8 | 105.9 | 109.9 | 113.0 | 116.0 | 119.1 | 122.1 | 3.1 |
| 70 | 94.3 | 97.3 | 100.3 | 103.4 | 106.4 | 109.5 | 112.5 | 115.5 | 188.6 | 121.6 | 3.0 |
| 72 | 93.9 | 96.9 | 99.9 | 103.0 | 106.0 | 109.0 | 112.0 | 115.1 | 118. | 121. | 3.0 |
| 76 | 93.1 | 96.1 | 99.1 | 102.1 | 105. 1 | 108. 1 | III.I | II4.I | 117.1 | 120.1 | 3.0 |
| 80 | 92.3 | 95.3 | 98.3 | 101. 3 | 104.3 | 107.2 | 110.2 | 113.2 | 116.2 | 119.2 | 3.0 |
| 84 | 91.6 | 94.5 | 97.5 | 100.5 | 103.4 | 106.4 | 109.3 | 12.3 | 115.2 | 118.2 | 3.0 |
| 88 | 90.9 | 93.8 | 96.7 | 99.7 | 102.6 | 105.5 | 108.4 | IIt. 4 | 154.3 | 117.2 | 2.9 |
| 92 | 90.1 | 93.0 | 96.0 | 98.9 | 101. 8 | 104.7 | 107.6 | 110.5 | 113.4 | 116.3 | 2.9 |
| 96 | 89.4 | 92.3 | 95.2 | 98.1 | IOI. 0 | 103. 8 | 106.7 | 109.6 | 112.5 | 115.4 | 2.9 |

Table 14.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.

Values of $2000 \times \mathrm{m}$.
$m=\frac{\mathrm{z}}{56573+\mathrm{I} 23 \cdot \mathrm{I} \theta+.003 \mathrm{z}} \cdot \frac{\mathrm{I}}{\mathrm{I}-\beta}$

| Mean Temperature of alr column. $\theta$ Fahr. | altitude of station in feet (z). |  |  |  |  |  |  |  |  |  | $\left\|\begin{array}{c} \text { Differ- } \\ \text { ence } \\ \text { for } \\ \text { f00 } \\ \text { Feet. } \end{array}\right\|$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4100 | 4200 | 4300 | 4400 | 4500 | 4600 | 4700 | 4800 | 4900 | 5000 |  |
| $-20^{\circ}$ | 151.5 | 155.2 | 158.9 | 162.6 | 166.3 | 170.0 | 173.7 | 177.3 | 181.0 | 184.7 | 3.7 |
| 16 | 150.1 | 153.8 | 157.4 | 161.1 | 164.8 | 168.4 | 172.1 | 175.7 | 179.4 | 183.1 | 3.7 |
| - 12 | I48.8 | ${ }_{152}{ }^{2} 4$ | 156.0 | ${ }^{1} 59.6$ | 163.3 | 166.9 | 170.5 | 174.I | 177.8 | 181.4 | 3.6 |
| 8 | 147.4 | 151.0 | 154.6 | 158.2 | 161.8 | 165.4 | 169.0 | 172.6 | 176.2 | 179.8 | 3.6 |
| 6 | 146.8 | 150.3 | 153.9 | 157.5 | 161.1 | 164.7 | 168.2 | 171.8 | 175.4 | 179.0 | 3.6 |
| 4 | 146.1 | 149.7 | 153.2 | 156.8 | 160.4 | 163.9 | 167.5 | 171.0 | 174.6 | 178.2 | 3.6 |
| - 2 | 145.5 | 149.0 | 152.5 | 156.1 | 159.6 | 163.2 | 166.7 | 170.3 | 173.8 | 177.4 | 3.5 |
| 0 | 144.8 | 148.3 | 151.9 | 155.4 | 158.9 | 162.5 | 166.0 | 169.5 | 173.1 | 176.6 | 3.5 |
| + 2 | 144.2 | 147.7 | 151.2 | 154.7 | 158.2 | 16 I .8 | 165.3 | 168.8 | 172.3 | 175.8 | 3.5 |
|  | 143.5 | 147.0 | 155.5 | 154.0 | 157.5 | 161.0 | 164.5 | 168.0 | 171.5 | 175.0 | 3.5 |
| 6 | 142.9 | 146.4 | 149.9 | 153.4 | 156.9 | 160.3 | 163.8 | 167.3 | 170.8 | 174.3 | 3.5 |
| 8 | 142.3 | 145.8 | 149.2 | 152.7 | 156.2 | 159.6 | 163. 1 | 166.6 | 170. 1 | 173.5 | 3.5 |
| 10 | 141.7 | 145. I | I48.6 | 152.0 | 155.5 | 159.0 | 162.4 | 165.9 | 169.3 | 172.8 | 3.5 |
| 12 | 141.1 | 144.5 | 147.9 | 151.4 | 154.8 | 158.3 | 16 I .7 | 165. I | 168.6 | 172.0 | 3.4 |
| 14 | 140.5 | 143.9 | 147.3 | 150.7 | 154.2 | 157.6 | 16 I .0 | 164.4 | 167.9 | 171.3 | 3.4 |
| 16 | 139.9 | 143.3 | 146.7 | 150.1 | 153.5 | 156.9 | 160.3 | 163.7 | 167.1 | 170.6 | 3.4 |
| 18 | 139.3 | 142.7 | 146. 1 | I49.5 | 152.9 | 156.2 | 159.6 | 162.0 | 166.4 | 169.8 | 3.4 |
| 20 | 138.7 | 142.1 | 145.4 | 148.8 | 152.2 | 155.6 | 159.0 | 162.3 | 165.7 | 169.1 | 3.4 |
| 22 | 138.1 | 141.5 | 144.8 | 148.2 | 151.6 | 154.9 | 158.3 | 161.7 | 165.0 | 168.4 | 3.4 |
| 24 | 137.5 | 140.9 | 144.2 | 147.6 | 150.9 | 154.3 | 157.6 | 16 I .0 | 164.3 | 167.7 | 3.4 |
| 26 | 136.9 | 140.3 | 143.6 | 146.9 | 150.3 | 153.6 | 157.0 | 160.3 | 163.6 | 167.0 | $3 \cdot 3$ |
| 28 | I36.3 | 139.7 | 143.0 | 146.3 | I49.6 | 153.0 | 156.3 | 159.6 | 162.9 | 166.3 | 3.3 |
| 30 | 135.8 | 139. 1 | 142.4 | 145.7 | 149.0 | 152.3 | 155.6 | 158.9 | 162.2 | 165.6 | 3.3 |
| 32 | 135.2 | 138.5 | 141.8 | 145. 1 | 148.4 | 151.7 | 155.0 | 158.3 | 161.6 | 164.8 | 3.3 |
| 34 | I 34.6 | 137.9 | 141.2 | 144.5 | 147.7 | 151.0 | 154.3 | 157.6 | 160.9 | 164.1 | $3 \cdot 3$ |
| 36 | 134.0 | 137.3 | 140.6 | 143.8 | 147.1 | 150.4 | 153.6 | 156.9 | 160.2 | 163.4 | $3 \cdot 3$ |
| 38 | I 33.5 | I36.7 | 140.0 | 143.2 | 146.5 | 149.7 | 153.0 | 156.2 | 159.5 | 162.7 | $3 \cdot 3$ |
| 40 | 132.9 | 136. 1 | 139.4 | 142.6 | 145.8 | 149.1 | 152.3 | 155.6 | 158.8 | 162.0 |  |
| 42 | 132.3 | 135.5 | 138.8 | 142.0 | 145.2 | 148.4 | 151.7 | 154.9 | 158.1 | 161.4 | 3.2 |
| 44 | 131.7 | 135.0 | I38.2 | 141.4 | 144.6 | 1478 | 151.0 | 154.2 | 157.4 | 160.7 | 3.2 |
| 46 | 131.2 | 134.4 | 137.6 | 140.8 | 144.0 | 147.2 | 150.4 | 153.6 | 156.8 | 160.0 | 3.2 |
| 48 | I30.6 | 133.8 | 137.0 | 140.2 | 143.4 | 146.5 | 149.7 | 152.9 | 156.1 | 159.3 | 3.2 |
| 50 | 130.1 | 133.2 | 136.4 | 139.6 | 142.7 | 145.9 | I49. 1 | 152.2 | 155.4 | 158.6 | 3.2 |
| 52 | 129.5 | 132.6 | 135.8 | 139.0 | I42.1 | 145.3 | 148.4 | 151.6 | 154.8 | 157.9 | 3.2 |
| 54 | 129.0 | ${ }^{132.1}$ | 135.2 | 138.4 | 141.5 | 144.7 | 147.8 | 151.0 | 154. I | 157.2 | 3. I |
| 56 | 128.4 | ${ }_{1} 131.5$ | 134.7 | 137.8 | 140.9 | 144.0 | 147.2 | 150.3 | 153.4 | 156.6 | 3.1 |
| 58 | 127.9 | 131.0 | 134.I | 137.2 | 140.3 | 143.4 | 146.6 | 149.7 | 152.8 | 155.9 | 3. 1 |
| 60 | 127.3 | 130.4 | 133.5 | 136.6 | 139.7 | 142.8 | 145.9 | 149.0 | 152.1 | 155.2 | 3. 1 |
| 62 | 126.8 | 129.9 | I33.0 | I36.0 | I39. 1 | 142.2 | $145 \cdot 3$ | 148.4 | 151.5 | 154.6 | 3. I |
| 64 | 126.2 | 129.3 | I32.4 | I 35.5 | 138.6 | 141.6 | 144.7 | 147.8 | 150.9 | 153.9 | 3. I |
| 66 | 125.7 | 128.8 | 131.8 | 134.9 | 138.0 | 141.0 | 144. I | 147.2 | 150.2 | 153.3 | 3. I |
| 68 | 125.2 | 128.2 | 131.3 | I 34.3 | 137.4 | 140.5 | 143.5 | 146.6 | 149.6 | 152.7 | 3. I |
| 70 | 124.7 | 127.7 | 130.7 | 133.8 | 136.8 | 139.9 | 142.9 | 145.9 | 149.0 | 152.0 | 3.0 |
| 72 | 124.2 | 127.2 | 130.2 | 133.2 | I36.3 | 139.3 | 142.3 | 145.3 | 148.4 | 151.4 | 3.0 |
| 76 | 123. 1 | 126.1 | 129.1 | I32.I | 135.1 | 138.1 | 141.2 | 144.2 | 147.2 | 150.2 | 3.0 |
| 80 | 122.1 | 125.1 | 128.1 | 131.1 | I34.0 | 137.0 | 140.0 | 143.0 | 146.0 | 148.9 | 3.0 |
| 84 | I21. 1 | 124.0 | 127.0 | 130.0 | 133.0 | 135.9 | 138.9 | 141.8 | 144.8 | 147.7 | 3.0 |
| 88 | 120 | 123.1 | 126.0 | 129.0 | 131.9 | 134.8 | 137.7 | 140.7 | 143.6 | 146.5 | 2.9 |
| 92 | 119.2 | 122.I | 125.0 | 127.9 | I30.8 | 133.7 | I 36.6 | 139.6 | 142.5 | 145.4 | 2.9 |
| 96 | 118.3 | 121.1 | 124.0 | 126.9 | 129.8 | 132.7 | 135.6 | I 38.4 | 141.3 | 144.2 | 2.9 |

TABLE 14.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.

Values of $2000 \times \mathrm{m}$.

$$
m=\frac{Z}{56573+123 \cdot 1 \theta+.003 Z} \cdot \frac{1}{1-\beta}
$$

| Mean Temperature of air column. $\theta$ Fahr. | ALTITUDE OF STATION IN FEET (z). |  |  |  |  |  |  |  |  |  | Difference for 100 Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 5100 | 5200 | 5300 | 5400 | 5500 | 5600 | 5700 | 5800 | 5900 | 6000 |  |
| $-20^{\circ}$ | 188.4 | 192.1 | 195.8 | 199.5 | 203.2 | 206.9 | 210.6 | 214.3 | 218.0 | 221.7 | 3.7 |
| 16 | 186.7 | 190.4 | 194.0 | 197.7 | 201.4 | 205.0 | 208.7 | 212.3 | 216.0 | 219.7 | 3.7 |
| 12 | 185.0 | 188.7 | 192.3 | 195.9 | 199.5 | 203.2 | 206.8 | 210.4 | 214.0 | 217.7 | 3.6 |
| -8 | 183.4 | 187.0 | 190.5 | 194.1 | 197.7 | 201.3 | 204.9 | 208.5 | 212.1 | 215.7 | 3.6 |
| 6 | 182.5 | 186.1 | 189.7 | 193.3 | 196.9 | 200.4 | 204.0 | 207.6 | 211.2 | 214.7 | 3.6 |
| - 4 | 181.7 | 185.3 | 188.9 | 192.4 | 196.0 | 199.5 | 203.1 | 206.7 | 210.2 | 213.8 | 3.6 |
| 2 | 180.9 | 184.5 | 188.0 | 191.6 | 195.1 | 198.7 | 202.2 | 205.7 | 209.3 | 212.8 | 3.5 |
| 0 | 180. 1 | 183.7 | 187.2 | 190.7 | 194.3 | 197.8 | 201.3 | 204.8 | 208.4 | 211.9 | 3.5 |
| +2 | 179.3 | 182.8 | 186.4 | 189.9 | 193.4 | 196.9 | 200.4 | 203.9 | 207.5 | 211.0 | $3 \cdot 5$ |
| 4 | 178.5 | 182.0 | 185.5 | 189.0 | 192.5 | 196.0 | 199.5 | 203.0 | 206.5 | 210.0 | 3.5 |
| 6 | 177.8 | 181.3 | 184.7 | 188.2 | 191.7 | 195.2 | 198.7 | 202.2 | 205.6 | 209. 1 | $3 \cdot 5$ |
| 8 | 177.0 | 180.5 | 183.9 | 187.4 | 190.9 | 194.3 | 197.8 | 201.3 | 204.8 | 208.2 | 3.5 |
| 10 | 176.2 | 179.7 | 183.1 | 186.6 | 190.0 | 193.5 | 197.0 | 200.4 | 203.9 | 207.3 | $3 \cdot 5$ |
| 12 | 175.5 | 178.9 | 182.3 | 185.8 | 189.2 | 192.7 | 196.1 | 199.5 | 203.0 | 206.4 | 3.4 |
| 14 | 174.7 | 178.1 | 181.6 | 185.0 | 188.4 | 191.8 | 195.3 | 198.7 | 202.1 | 205.5 | 3.4 |
| 16 | 174.0 | 177.4 | 180.8 | 184.2 | 187.6 | 191.0 | 194.4 | 197.8 | 201.2 | 204.7 | 3.4 |
| 18 | I73.2 | 176.6 | 180.0 | 183.4 | 186.8 | 190.2 | 193.6 | 197.0 | 200.4 | 203.8 | 3.4 |
| 20 | 172.5 | 175.9 | 179.2 | 182.6 | 186.0 | 189.4 | 192.8 | 196.2 | 199.5 | 202.9 | 3.4 |
| 22 | 171.8 | 175.1 | 178.5 | 181.9 | 185.2 | 188.6 | 192.0 | 195.3 | 198.7 | 202.1 | 3.4 |
| 24 | 171.0 | 174.4 | 177.7 | 181. 1 | 184.4 | 187.8 | 191. 1 | 194.5 | 197.8 | 201.2 | 3.4 |
| 26 | 170.3 | 173.6 | 177.0 | 180.3 | 183.7 | 187.0 | 190.3 | 193.7 | 197.0 | 200.3 | $3 \cdot 3$ |
| 28 | 169.6 | 172.9 | I76.2 | 179.6 | 182.9 | 186.2 | 189.5 | 192.9 | 196.2 | 199.5 | $3 \cdot 3$ |
| 30 | 168.9 | 172.2 | 175.5 | 178.8 | 182.1 | 185.4 | 188.7 | 192.0 | 195.3 | 198.7 | $3 \cdot 3$ |
| 32 | 168. 1 | 171.4 | 174.7 | 178.0 | 181.3 | 184.6 | 187.9 | 191.2 | 194.5 | 197.8 | $3 \cdot 3$ |
| 34 | 167.4 | 170.7 | 174.0 | 177.3 | 180.6 | 183.8 | 187. 1 | 190.4 | 193.7 | 197.0 | $3 \cdot 3$ $3 \cdot 3$ |
| 36 | 166.7 | 170.0 | 173.2 | 176.5 | 179.8 | 183.1 | 186.3 | 189.6 | 192.9 | 196. I | 3.3 |
| 38 | 166.0 | 169.3 | 172.5 | 175.8 | 179.0 | 182.3 | 185.5 | 188.8 | 192.0 | 195.3 | $3 \cdot 3$ |
| 40 | 165.3 | 168.5 | 171.8 | 175.0 | 178.2 | 181.5 | 184.7 | 188.0 | 191.2 | 194.4 | 3.2 |
| 42 | 164.6 | 167.8 | 171.0 | 174.3 | 177.5 | 180.7 | 183.9 | 187.2 | 190.4 | 193.6 | 3.2 |
| 44 | 163.9 | 167.1 | 170.3 | 173.5 | 176.7 | 179.9 | 183. 1 | 186.4 | 189.6 | 192.8 | 3.2 |
| 46 | 163.2 | 166.4 | 169.6 | 172.8 | 176.0 | 179.2 | 182.4 | 185.6 | 188.7 | 192.0 | 3.2 |
| 48 | 162.5 | 165.6 | 168.8 | 172.0 | 175.2 | 178.4 | 181.6 | 184.8 | 187.9 | 191.1 | 3.2 |
| 50 | 161.8 | 164.9 | 168. 1 | 171.3 | 174.4 | 177.6 | 180.8 | 184.0 | 187.1 | 190.3 | 3.2 |
| 52 | 161. I | 164.2 | 167.4 | 170.5 | 173.7 | 176.9 | 180.0 | 183.2 | 186.3 | 189.5 | 3.2 |
| 54 | 160.4 | 163.5 | 166.7 | 169.8 | 173.0 | 176.I | 179.2 | 182.4 | 185.5 | 188.7 | 3.1 |
| 56 | 159.7 | 162.8 | 166.0 | 169.1 | 172.2 | 175.4 | 178.5 | 181.6 | 184.7 | 187.9 | 3.1 |
| 58 | 159.0 | 162.I | 165.3 | 168.4 | 171.5 | 174.6 | 177.7 | 180.8 | 184.0 | 187.1 | 3.I |
| 60 | 158.4 | 161.5 | 164.6 | 167.7 | 170.8 | 173.9 | 177.0 | 180. 1 | 183.2 | 186.3 | 3.1 |
| 62 | 157.7 | 160.8 | 163.9 | 167.0 | 170.1 | 173.1 | 176.2 | 179.3 | 182.4 | 185.5 | 3.1 |
| 64 | 157.0 | 160. 1 | 163.2 | 166.3 | 169.3 | 172.4 | 175.5 | 178.6 | 181.6 | 184.7 | 3.1 |
| 66 | 156.4 | 159.4 | 162.5 | 165.6 | 168.6 | 171.7 | 174.8 | 177.8 | 180.9 | 184.0 | 3.1 |
| 68 | 155.7 | 158.8 | 161.8 | 164.9 | 167.9 | 171.0 | 174.0 | 177.1 | 180.1 | 183.2 | 3.1 |
| 70 | 155.1 | 158.1 | 161. 1 | 164.2 | 167.2 | 170.3 | 173.3 | 176.3 | 179.4 | 182.4 | 3.0 |
| 72 | 154.4 | 157.5 | 160.5 | 163.5 | 166.5 | 169.6 | 172.6 | 175.6 | 178.6 | 181.7 | 3.0 |
| 76 | 153.2 | 156.2 | 159.2 | 162.2 | 165.2 | 168.2 | 171.2 | 174.2 | 177.2 | 180.2 | 3.0 |
| 80 | 151.9 | I54.9 | 157.9 | 160.8 | 163.8 | 166.8 | 169.8 | 172.8 | 175.7 | 178.7 | 3.0 |
| 84 88 | I50.7 | I53.6 | 156.6 | 159.5 158.3 | 162.5 | 165.5 <br> 164.1 | 168.4 167.0 | 171.4 | 174.3 | 177.3 | 3.0 |
| 88 | 149.5 148.3 | 152.4 151.2 | 155.3 154.1 | 158.3 157.0 | 161.2 159.9 | 164.1 162.8 | 167.0 165.7 | 170.0 168.6 | 172.9 171.5 | 175.8 174.4 | 2.9 2.9 |
| 96 | 147.1 | 150.0 | 152.9 | 155.7 | 158.6 | 161.5 | 164.4 | $167 \cdot 3$ | 170.2 | 173.0 | 2.9 |

TABLE 14.

## REDUCTION OF THE BAROMETER TO SEA LEVEL.

 ENGLISH MEASURES.Values of $2000 \times \mathrm{m}$.

$$
m=\frac{z}{56573+123 \cdot 1 \theta+.003 z} \cdot \frac{1}{1-\beta}
$$

| Mean Temperature of air column. $\theta$ Fahr. | ALTITUDE OF STATION IN FEET (z). |  |  |  |  |  |  |  |  |  | Difference for 100 feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6100 | 6200 | 6300 | 6400 | 6500 | 6600 | 6700 | 6800 | 6900 | 7000 |  |
| $-20^{\circ}$ | 225.4 | 229. I | 232.8 | 236.4 | 240.1 | 243.8 | $247 \cdot 5$ | 251.2 | 254.9 | 258.6 | 3.7 |
| 16 | 223.3 | 227.0 | 230.6 | 234.3 | 237.9 | 241.6 | 245.3 | 248.9 | 252.6 | 256.2 | 3.7 |
| - 12 | 221.3 | 224.9 | 228.5 | 232.2 | 235.8 | 239.4 | 243.0 | 246.7 | 250.3 | 253.9 | 3.6 |
| - 8 | 219.3 | 222.9 | 226.5 | 230.1 | 233.7 | 237.3 | 240.9 | 244.5 | 248. 1 | 251.6 | 3.6 |
| 6 | 218.3 | 221.9 | 225.5 | 229. 1 | 232.6 | 236.2 | 239.8 | 243.4 | 246.9 | 250.5 | 3.6 |
| 4 | 217.4 | 220.9 | 224.5 | 228.0 | 231.6 | 235.2 | 238.7 | 242.3 | 245.8 | 249.4 | 3.6 |
| 2 | 216.4 | 219.9 | 223.5 | 227.0 | 230.6 | 234. 1 | 237.7 | 241.2 | 244.8 | 248.3 | 3.5 |
| 0 | 215.4 | 219.0 | 222.5 | 226.0 | 229.6 | 233.1 | 236.6 | 240. I | 243.7 | 247.2 | 3.5 |
| +2 | 214.5 | 218.0 | 221.5 | 225.0 | 228.5 | 232.1 | 235.6 | 239.1 | 242.6 | 246.1 | 3.5 |
| 4 | 213.5 | 217.0 | 220.5 | 224.0 | 227.5 | 231.0 | 234.5 | 238.0 | 241.5 | 245.0 | 3.5 |
| 6 | 212.6 | 216.1 | 219.6 | 223. I | 226.6 | 230.0 | 233.5 | 237.0 | 240.5 | 244.0 | 3.5 |
| 8 | 211.7 | 215.2 | 218.6 | 222.1 | 225.6 | 229.0 | 232.5 | 236.0 | 239.4 | 242.9 | 3.5 |
| 10 | 210.8 | 214.2 | 217.7 | 221.1 | 224.6 | 228.0 | 231.5 | 235.0 | 238.4 | 24 I .9 | 3.5 |
| 12 | 209.9 | 213.3 | 216.7 | 220.2 | 223.6 | 227.1 | 230.5 | 233.9 | 237.4 | 240.8 | $3 \cdot 4$ |
| 14 | 209.0 | 212.4 | 215.8 | 219.2 | 222.7 | 226.1 | 229.5 | 232.9 | 236.4 | 239.8 | 3.4 |
| 16 | 208.1 | 211.5 | 214.9 | 218.3 | 221.7 | 225. I | 228.5 | 231.9 | 235.3 | 238.8 | 3.4 |
| 18 | 207.2 | 210.6 | 214.0 | 217.4 | 220.8 | 224.2 | 227.6 | 230.9 | 234.3 | 237.7 | 3.4 |
| 20 | 206.3 | 209.7 | 213.1 | 216.4 | 219.8 | 223.2 | 226.6 | 230.0 | 233.3 | 236.7 | 3.4 |
| 22 | 205.4 | 208.8 | 212.2 | 215.5 | 218.9 | 222.3 | 225.6 | 229.0 | 232.4 | 235.7 | 3.4 |
| 24 | 204.6 | 207.9 | 211.3 | 214.6 | 218.0 | 221.3 | 224.7 | 228.0 | 231.4 | 234.7 | 3.4 |
| 26 | 203.7 | 207.0 | 210.4 | 213.7 | 217.0 | 220.4 | 223.7 | 227.0 | 230.4 | 233.7 | $3 \cdot 3$ |
| 28 | 202.8 | 206.2 | 209.5 | 212.8 | 216.1 | 219.4 | 222.8 | 226.1 | 229.4 | 232.7 | $3 \cdot 3$ |
| 30 | 202.0 | 205.3 | 208.6 | 211.9 | 215.2 | 218.5 | 221.8 | 225.1 | 228.4 | 231.8 | $3 \cdot 3$ |
| 32 | 201. I | 204.4 | 207.7 | 211.0 | 214.3 | 217.6 | 220.9 | 224.2 | 227.5 | 230.8 | $3 \cdot 3$ |
| 34 | 200.2 | 203.5 | 206.8 | 210.1 | 213.4 | 216.7 | 219.9 | 223.2 | 226.5 | 229.8 | $3 \cdot 3$ |
| 36 | 199.4 | 202.7 | 205.9 | 209. 2 | 212.5 | 215.7 | 219.0 | 222.3 | 225.5 | 228.8 | $3 \cdot 3$ |
| 38 | 198.5 | 201.8 | 205.0 | 208.3 | 2 I1. 6 | 214.8 | 218.1 | 221.3 | 224.6 | 227.8 | 3.3 |
| 40 | 197.7 | 200.9 | 204.2 | 207.4 | 210.6 | 213.9 | 217. I | 220.4 | 223.6 | 226.8 | 3.2 |
| 42 | 196.8 | 200.1 | 203.3 | 206.5 | 209.7 | 213.0 | 216.2 | 219.4 | 222.6 | 225.9 | 3.2 |
| 44 | 196.0 | 199.2 | 202.4 | 205.6 | 208.8 | 212.1 | 215.3 | 218.4 | 221.7 | 224.9 | 3.2 |
| 46 | 195.2 | 198.4 | 201.5 | 204.7 | 207.9 | 21 I .1 | 214.3 | 217.5 | 220.7 | 223.9 | 3.2 |
| 48 | 194.3 | 197.5 | 200.7 | 203.9 | 207.0 | 210.2 | 213.4 | 216.6 | 219.8 | 223.0 | 3.2 |
| 50 | 193.5 | 196.6 | 199.8 | 203.0 | 206.2 | 209.3 | 212.5 | 215.7 | 218.8 | 222.0 | 3.2 |
| 52 | 192.6 | 195.8 | 199.0 | 202.1 | 205.3 | 208.4 | 211.6 | 214.7 | 217.9 | 221. I | 3.2 |
| . 54 | 191.8 | 195.0 | 198.1 | 201.3 | 204.4 | 207.5 | 210.7 | 213.8 | 217.0 | 220.1 | 3.I |
| 56 | 191.0 | 194. I | 197.3 | 200.4 | 203.5 | 206.7 | 209.8 | 212.9 | 216.0 | 219.2 | 3.I |
| 58 | 190.2 | 193.3 | 196.4 | 199.5 | 202.7 | 205.8 | 208.9 | 212.0 | 215.1 | 218.3 | 3.I |
| 60 | 189.4 | 192.5 | 195.6 | 198.7 | 201.8 | 204.9 | 208.0 | 211.1 | 214.2 | 217.3 | 3.1 |
| 62 | 188.6 | 191.7 | 194.8 | 197.9 | 201.0 | 204. I | 207.2 | 210.2 | 213.3 | 216.4 | 3. I |
| 64 | 187.8 | 190.9 | 194.0 | 197.0 | 200.1 | 203.2 | 206.3 | 209.3 | 212.4 | 215.5 | 3.1 |
| 66 | 187.0 | 190.1 | 193.1 | 196.2 | 199.3 | 202.3 | 205.4 | 208.5 | 211.5 | 214.6 | 3.1 |
| 68 | 186.2 | 189.3 | 192.3 | 195.4 | 198.4 | 201.5 | 204.6 | 207.6 | 210.7 | 213.7 | 3.0 |
| 70 | 185.5 | 188.5 | 191.5 | 194.6 | 197.6 | 200.7 | 203.7 | 206.7 | 209.8 | 212.8 | 3.0 |
| 72 | 184.7 | 187.7 | 190.8 | 193.8 | 196.8 | 199.8 | 202.9 | 205.9 | 208.9 | 211.9 | 3.0 |
| 76 | 183.2 | 186.2 | 189.2 | 192.2 | 195.2 | 198.2 | 201.2 | 204.2 | 207.2 | 210.2 | 3.0 |
| 80 | I81.7 | 184.7 | 187.6 | 190.6 | 193.6 | 196.6 | 199.6 | 202.5 | 205.5 | 208.5 | 3.0 |
| 84 | 180. 2 | 183.2 | 186.1 | 189.1 | 192.0 | 195.0 | 197.9 | 200.9 | 203.8 | 206.8 | 3.0 |
| 88 | 178.8 | 181.7 | 184.6 | 187.6 | 190.5 | 193.4 | 196.3 | 199.3 | 202.2 | 205.1 | 2.9 |
| 92 | 177.3 | 180. 2 | 183.2 | IS6. 1 | 189.0 | 191.9 | 194.8 | 197.7 | 200.6 | 203.5 | 2.9 |
| 96 | I75.9 | 178.8 | 181.7 | I84.6 | 187.5 | 190.3 | 193.2 | 196.1 | 199.0 | 201.9 | 2.9 |

Table 14.
REDUCTION OF THE BAROMETER TO SEA LEVEL.
ENGLISH MEASURES.


| Mean Temperature of air column. $\theta$ Fahr. | ALTITUDE OF STATION IN FEET ( $z$ ). |  |  |  |  |  |  |  |  |  | Differ- <br> ence for 100 Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7100 | 7200 | 7300 | 7400 | 7500 | 7600 | 7700 | 7800 | 7900 | 8000 |  |
| $-20^{\circ}$ | 262.3 | 266.0 | 269.7 | 273.4 | 277.1 | 280. 8 | 284.5 | 288. 1 | 291.8 | 295.5 | 3.7 |
| 16 | 259.9 | 263.6 | 267.2 | 270.9 | 274.5 | 278.2 | 281.9 | 285.5 | 289.2 | 292.8 | 3.7 |
| 12 | 257.6 | 26I. 2 | 264.8 | 268.4 | 272.I | 275.7 | 279.3 | 282.9 | 286.6 | 290.2 | 3.6 |
| - 8 | 255.2 | 258.8 | 262.4 | 266.0 | 269.6 | 273.2 | 276.8 | 280.4 | 284.0 | 287.6 | 3.6 |
| 6 | 254.1 | 257.7 | 261.3 | 264.8 | 268.4 | 272.0 | 275.6 | 279.1 | 282.7 | 286.3 | 3.6 |
| - 4 | 253.0 | 256.5 | 260. I | 263.7 | 267.2 | 270.8 | 274.3 | 277.9 | 281.5 | 285.0 | 3.6 |
| 2 | 251.8 | 255.4 | 258.9 | 262.5 | 266.0 | 269.6 | 273.1 | 276.7 | 280. 2 | 283.8 | 3.5 |
| 0 | 250.7 | 254.3 | 257.8 | 261.3 | 264.9 | 268.4 | 271.9 | 275.4 | 279.0 | 282.5 | $3 \cdot 5$ |
| + 2 | 249.6 | 253.1 | 256.7 | 260.2 | 263.7 | 267.2 | 270.7 | 274.2 | 277.8 | 281.3 | $3 \cdot 5$ |
|  | 248.5 | 252.0 | 255.5 | 259.0 | 262.5 | 266.0 | 269.5 | 273.0 | 276.5 | 280.0 | $3 \cdot 5$ |
| 8 | 247.5 | 250.9 | 254.4 | 257.9 | 26I. 4 | 264.9 | 268.4 | 271.8 | 275.3 | 278.8 | 3.5 |
| 8 | 246.4 | 249.8 | 253.3 | 256.8 | 260.3 | 263.7 | 267.2 | 270.7 | 274.I | 277.6 | 3.5 |
| 10 | 245.3 | 248.8 | 252.2 | 255.7 | 259. I | 262.6 | 266.0 | 269.5 | 272.9 | 276.4 | 3.5 |
| 12 | 244.3 | 247.7 | 251.1 | 254.6 | 258.0 | 261.4 | 264.9 | 268.3 | 271.8 | 275.2 | 3.4 |
| 14 | 243.2 | 246.6 | 250.1 | 253.5 | 256.9 | 260.3 | 263.8 | 267.2 | 270.6 | 274.0 | 3.4 |
| 16 | 242.2 | 245.6 | 249.0 | 252.4 | 255.8 | 259.2 | 262.6 | 266.0 | 269.4 | 272.8 | 3.4 |
| 18 | 24I. I | 244.5 | 247.9 | 251.3 | 254.7 | 258. I | 261.5 | 264.9 | 268.3 | 271.7 | 3.4 |
| 20 | 240. I | 243.5 | 246.9 | 250.2 | 253.6 | 257.0 | 260.4 | 263.8 | 267. I | 270.5 | 3.4 |
| 22 | 239. I | 242.4 | 245.8 | 249.2 | 252.5 | 255.9 | 259.3 | 262.6 | 266.0 | 269.4 | 3.4 |
| 24 | 238.1 | 241.4 | 244.8 | 248.1 | 251.5 | 254.8 | 258.2 | 261.5 | 264.9 | 268.2 | $3 \cdot 4$ |
| 26 | 237.1 | 240.4 | 243.7 | 247.I | 250.4 | 253.8 | 257. I | 260.4 | 263.8 | 267. I | $3 \cdot 3$ |
| 28 | 236.1 | 239.4 | 242.7 | 246.0 | 249.4 | 252.7 | 256.0 | 259.3 | 262.7 | 266.0 | $3 \cdot 3$ |
| 30 | 235. I | 238.4 | 241.7 | 245.0 | 248.3 | 251.6 | 254.9 | 258.2 | 261.5 | 264.8 | $3 \cdot 3$ |
| 32 | 234. I | 237.4 | 240.7 | 243.9 | 247.2 | 250.5 | 253.8 | 257.1 | 260.4 | 263.7 | $3 \cdot 3$ |
| 34 | 233.1 | 236.3 | 239.6 | 242.9 | 246.2 | 249.5 | 252.8 | 256.0 | 259.3 | 262.6 | $3 \cdot 3$ |
| 36 | 232.1 | $235 \cdot 3$ | 238.6 | 241.9 | 245. I | 248.4 | 251.7 | 254.9 | 258.2 | 261.5 | $3 \cdot 3$ |
| 38 | 231.1 | $234 \cdot 3$ | 237.6 | 240.8 | 244. 1 | 247.3 | 250.6 | 253.9 | 257.1 | 260.4 | $3 \cdot 3$ |
| 40 | 230.1 | 233.3 | 236.6 | 239.8 | 243.0 | 246.3 | 249.5 | 252.8 | 256.0 | 259.2 | 3.2 |
| 42 | 229.1 | 232.3 | 235.5 | 238.8 | 242.0 | 245.2 | 248.4 | 251.7 | 254.9 | 258.1 | 3.2 |
| 44 | 228.1 | 231.3 | 234.5 | 237.7 | 241.0 | 244.2 | 247.4 | 250.6 | 253.8 | 257.0 | 3.2 |
| 46 | 227. I | 230.3 | 233.5 | 236.7 | 239.9 | 243. I | 246.3 | 249.5 | 252.7 | 255.9 | 3.2 |
| 48 | 226.2 | 229.3 | 232.5 | 235.7 | 238.9 | 242. I | $245 \cdot 3$ | 248.4 | 251.6 | 254.8 | 3.2 |
| 50 | 225.2 | 228.4 | 231.5 | 234.7 | 237.9 | 241.0 | 244.2 | 247.4 | 250.5 | 253.7 | 3.2 |
| 52 | 224.2 | 227.4 | 230.5 | 233.7 | 236.8 | 240.0 | 243.2 | 246.3 | 249.5 | 252.6 | 3.2 |
| 54 | 223.3 | 226.4 | 229.5 | 232.7 | 235.8 | 239.0 | 242.1 | 245.3 | 248.4 | 251.5 | 3.1 |
| 56 | 222.3 | 225.4 | 228.6 | 231.7 | 234.8 | 238.0 | 241.1 | 244.2 | 247.3 | 250.5 | 3.1 |
| 58 | 221.4 | 224.5 | 227.6 | 230.7 | 233.8 | 236.9 | 240. 1 | 243.2 | 246.3 | 249.4 | 3.1 |
| 60 | 220.4 | 223.5 | 226.6 | 229.7 | 232.8 | 235.9 | 239. I | 242.2 | $245 \cdot 3$ | 248.4 | 3. I |
| 62 | 219.5 | 222.6 | 225.7 | 228.8 | 231.9 | 235.0 | 238.0 | 241.1 | 244.2 | 247.3 | 3.1 |
| 64 | 218.6 | 221.7 | 224.7 | 227.8 | 230.9 | 234.0 | 237.0 | 240.1 | 243.2 | 246.3 | 3.1 |
| 66 | 217.7 | 220.7 | 223.8 | 226.9 | 229.9 | 233.0 | 236.1 | 239.I | 242.2 | 245.2 | 3.1 |
| 68 | 216.8 | 219.8 | 222.9 | 225.9 | 229.0 | 232.0 | 235. I | 238.1 | 241.2 | 244.2 | 3.0 |
| 70 | 215.9 | 218.9 | 221.9 | 225.0 | 228.0 | 231.1 | 234.1 | 237.1 | 240.2 | 243.2 | 3.0 |
| 72 | 215.0 | 218.0 | 221.0 | 224.1 | 227.1 | 230. I | 233.1 | 236.2 | 239.2 | 242.2 | 3.0 |
| 76 | 213.2 | 216.2 | 219.2 | 222.2 | 225.2 | 228.2 | 231.2 | 234.2 | 237.2 | 240. 2 | 3.0 |
| 80 | 211.5 | 214.4 | 217.4 | 220.4 | 223.4 | 226.4 | 229.3 | 232.3 | 235.3 | 238.3 | 3.0 |
| 84 | 209.8 | 212.7 | 215.7 | 218.6 | 221.6 | 224.5 | 227.5 | 230.4 | 233.4 | 236.3 | 2.9 |
| 88 | 208.1 | 211.0 | 213.9 | 216.9 | 219.8 | 222.7 | 225.6 | 228.6 | 23 I .5 | 234.4 | 2.9 |
| 92 | 206.4 | 209.3 | 212.2 | 215.1 | 218.0 | 220.9 | 223.8 | 226.7 | 229.7 | 232.6 | 2.9 |
| 96 | 204.8 | 207.6 | 210.5 | 213.4 | 216.3 | 219.2 | 222.1 | 224.9 | 227.8 | 230.7 | 2.9 |

TABLE 14.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.
Values of $2000 \times \mathrm{m} . \quad m=\frac{\mathrm{Z}}{56573+\mathrm{I} 23 \cdot \mathrm{I} \theta+.003 \mathrm{Z}} \cdot \frac{\mathrm{I}}{\mathrm{r}-\boldsymbol{\beta}}$

| Mean Temperature of air column. $\theta$ Fahr. | ALTITUDE OF STATION IN FEET ( z ). |  |  |  |  |  |  |  |  |  | Difference for 100 Feet. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8100 | 8200 | 8300 | 8400 | 8500 | 8600 | 8700 | 8800 | 8900 | 9000 |  |
| $-20^{\circ}$ | 299.2 | 302.9 | 306.6 | 310.3 | 314.0 | 317.7 | 321.4 | 325.1 | 328.8 | 332.5 | 3.7 |
| r6 | 296.5 | 300.2 | 303.8 | 307.5 | 3II.1 | 314.8 | 318.4 | 322.1 | 325.8 | 329.4 | 3.7 |
| 12 | 293.8 | 297.4 | 301. 1 | 304.7 | 308.3 | 3II. 9 | 315.6 | 319.2 | 322.8 | 326.4 | 3.6 |
| $-8$ | 291.2 | 294.8 | 298.4 | 302.0 | 305.5 | 309.1 | 312.7 | 316.3 | 319.9 | 323.5 | 3.6 |
| - 6 | 289.9 | 293.5 | 297.0 | 300.6 | 304.2 | 307.8 | 3 Ir .3 | 314.9 | 318.5 | 322.1 | 3.6 |
| - 4 | 288.6 | 292.1 | 295.7 | 299.3 | 302.8 | 306.4 | 309.9 | 313.5 | 317.1 | 320.6 | 3.6 |
| 2 | 287.3 | 290.9 | 294.4 | 297.9 | 301.5 | 305.0 | 308.6 | 312.1 | 315.7 | 319.2 | 3.5 |
| 0 | 286.0 | 289.6 | 293. I | 296.6 | 300.2 | 303.7 | 307.2 | 310.7 | 314.3 | 317.8 | 3.5 |
| + 2 | 284.8 | 288.3 | 291.8 | 295.3 | 298.8 | 302.4 | 305.9 | 309.4 | 312.9 | 316.4 | $3 \cdot 5$ |
|  | 283.5 | 287.0 | 290.5 | 294.0 | 297.5 | 301.0 | 304.5 | 308.0 | 3 II .5 | 315.0 | 3.5 |
| 6 | 282.3 | 285.8 | 289.3 | 292.7 | 296.2 | 299.7 | 303.2 | 306.7 | 310.2 | 313.6 | 3.5 |
| 8 | 28I.1 | 284.5 | 288.0 | 291.5 | 294.9 | 298.4 | 301.9 | 305.3 | 308.8 | 312.3 | 3.5 |
| 10 | 279.8 | 283.3 | 286.8 | 290.2 | 293.7 | 297.1 | 300.6 | 304.0 | 307.5 | 310.9 | 3.5 |
| 12 | 278.6 | 282.1 | 285.5 | 289.0 | 292.4 | 295.8 | 299.3 | 302.7 | 306.2 | 309.6 | 3.4 |
| 14 | 277.5 | 280.9 | 284.3 | 287.7 | 291. 1 | 294.6 | 298.0 | 301.4 | 304.8 | 308.3 | 3.4 |
| 16 | 276.3 | 279.7 | 283.1 | 286.5 | 289.9 | 293.3 | 296.7 | 300. 1 | 303.5 | 306.9 | 3.4 |
| 18 | 275. I | 278.5 | 281.9 | 285.3 | 288.7 | 292.1 | 295.4 | 298.8 | 302.2 | 305.6 | 3.4 |
| 20 | 273.9 | 277.3 | 280.7 | 284.0 | 287.4 | 290.8 | 294.2 | 297.6 | 300.9 | 304.3 | 3.4 |
| 22 | 272.7 | 276. 1 | 279.5 | 282.8 | 286.2 | 289.6 | 292.9 | 296.3 | 299.7 | 303.0 | 3.4 |
| 24 | 271.6 | 274.9 | 278.3 | 281.6 | 285.0 | 288.3 | 291.7 | 295.0 | 298.4 | 301.8 | 3.4 |
| 26 | 270.4 | 273.8 | 277.1 | 280.5 | 283.8 | 287.1 | 290.5 | 293.8 | 297. I | 300.5 | $3 \cdot 3$ |
| 28 | 269.3 | 272.6 | 275.9 | 279.3 | 282.6 | 285.9 | 289.2 | 292.6 | 295.9 | 299.2 | $3 \cdot 3$ |
| 30 | 268.2 | 271.5 | 274.8 | 278.1 | 281.4 | 284.7 | 288.0 | 291.3 | 294.6 | 297.9 | 3.3 |
| 32 | 267.0 | 270.3 | 273.6 | 276.9 | 280.2 | 283.5 | 286.8 | 290. 1 | 293.4 | 296.7 | $3 \cdot 3$ |
| 34 | 265.9 | 269.2 | 272.4 | 275.7 | 279.0 | 282.3 | 285.6 | 288.8 | 292.1 | 295.4 | $3 \cdot 3$ |
| 36 | 254.7 | 268.0 | 271.3 | 274.5 | 277.8 | 281.1 | 284.3 | 287.6 | 290.9 | 294. I | $3 \cdot 3$ |
| 38 | 263.6 | 266.9 | 270.1 | 273.4 | 276.6 | 279.9 | 283. 1 | 286.4 | 289.6 | 292.9 | 3.3 |
| 40 | 262.5 | 265.7 | 269.0 | 272.2 | 275.4 | 278.7 | 281.9 | 285.2 | 288.4 | 291.6 | 3.2 |
| 42 | 261.4 | 264.6 | 267.8 | 271.0 | 274.3 | 277.5 | 280.7 | 283.9 | 287.2 | 290.4 | 3.2 |
| 44 | 260.2 | 263.4 | 266.7 | 269.9 | 273. 1 | 276.3 | 279.5 | 282.7 | 285.9 | 289. I | 3.2 |
| 46 | 259.1 | 262.3 | 265.5 | 268.7 | 271.9 | 275. I | 278.3 | 281.5 | 284.7 | 287.9 | 3.2 |
| 48 | 258.0 | 26 I .2 | 264.4 | 267.5 | 270.7 | 273.9 | 277. 1 | 280.3 | 283.5 | 286.6 | 3.2 |
| 50 | 256.9 | 260.1 | 263.2 | 266.4 | 269.6 | 272.7 | 275.9 | 279.1 | 282.2 | 285.4 | 3.2 |
| 52 | 255.8 | 258.9 | 262.1 | 265.3 | 268.4 | 271.6 | 274.7 | 277.9 | 281.0 | 284.2 | 3.1 |
| 54 | 254.7 | 257.8 | 261.0 | 264.1 | 267.3 | 270.4 | 273.5 | 276.7 | 279.8 | 283.0 | 3.1 |
| 56 | 253.6 | 256.7 | 259.9 | 263.0 | 266. 1 | 269.3 | 272.4 | 275.5 | 278.6 | 28 r .8 | 3. I |
| 58 | 252.5 | 255.6 | 258.8 | 26 r .9 | 265.0 | 268. I | 271.2 | 274.3 | 277.5 | 280.6 | 3. I |
| 60 | 251.5 | 254.6 | 257.7 | 260.8 | 263.9 | 267.0 | 270. 1 | 273.2 | 276.3 | 279.4 | 3.1 |
| 62 | 250.4 | 253.5 | 256.6 | 259.7 | 262.8 | 265.9 | 268.9 | 272.0 | 275. I | 278.2 | 3.1 |
| 64 | 249.4 | 252.4 | 255.5 | 258.6 | 261.7 | 264.7 | 267.8 | 270.9 | 274.0 | 277.1 | 3.1 |
| 66 | 248.3 | 251.4 | 254.4 | 257.5 | 260.6 | 263.6 | 266.7 | 269.8 | 272.8 | 275.9 | 3.1 |
| 68 | 247.3 | 250.3 | 253.4 | 256.4 | 259.5 | 262.5 | 265.6 | 268.6 | 271.7 | 274.7 | 3.0 |
| 70 | 246.3 | 249.3 | 252.3 | 255.4 | 258.4 | 26 r .4 | 264.5 | 267.5 | 270.6 | 273.6 | 3.0 |
| 72 | 245.2 | 248.3 | 251.3 | 254.3 | 257.3 | 260.4 | 263.4 | 266.4 | 269.4 | 272.5 | 3.0 |
| 76 | 243.2 | 246.2 | 249.2 | 252.2 | 255.2 | 258.2 | 261.2 | 264.2 | 267.2 | 270.2 | 3.0 |
| 80 | 241.2 | 244.2 | 247.2 | 250.2 | 253. 1 | 256. 1 | 259.1 | 262.1 | 265.1 | 268.0 | 3.0 |
| 84 | 239.3 | 242.2 | 245.2 | 248. 1 | 251.1 | 254. 1 | 257.0 | 260.0 | 262.9 | 265.9 | 2.9 |
| 88 | 237.4 | 240.3 | 243.2 | 246. I | 249. 1 | 252.0 | 254.9 | 257.9 | 260.8 | 263.7 | 2.9 |
| 92 | 235.5 | 238.4 | 241.3 | 244.2 | 247. 1 | 250.0 | 252.9 | 255.8 | 258.7 | 261.6 | 2.9 |
| 96 | 233.6 | 236.5 | 239.4 | 242.2 | 245. 1 | 248.0 | 250.9 | 253.8 | 256.7 | 259.5 | 2.9 |

TABLE 15.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.

Correction of 2000 m for Latitude : $2000 m \times 0.002662 \cos 2 \phi$.
For latitudes $0^{\circ}$ to $45^{\circ}$, the correction is to be subtracted.
For latitudes $45^{\circ}$ to $90^{\circ}$, the correction is to be added.

| 2000 m. | LATITUDE. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ | $45^{\circ}$ |
| 10 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 20 | O.I | O. I | O. 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 30 | O.I | O.I | O.I | O. I | O. I | O. I | 0.0 | 0.0 | 0.0 | 0.0 |
| 40 | O.I | 0.1 | O. 1 | O. I | O.I | O.I | 0.1 | 0.0 | 0.0 | 0.0 |
| 50 | O. I | O.I | 0.1 | 0.1 | O. I | 0.1 | O. I | 0.0 | 0.0 | 0.0 |
| 60 | 0.2 | 0.2 | 0.2 | O. 1 | O.I | O. 1 | O. 1 | O.I | 0.0 | 0.0 |
| 70 | 0.2 | 0.2 | 0.2 | 0.2 | O. I | O. 1 | O.I | O. 1 | 0.0 | 0.0 |
| So | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | O.I | O.I | 0.1 | 0.0 | 0.0 |
| 90 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | O.I | O.I | 0.0 | 0.0 |
| 100 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.2 | O.I | 0.1 | 0.0 | 0.0 |
| 110 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.1 | O.I | 0.1 | 0.0 |
| 120 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.2 | O. 1 | - 0.1 | 0.0 |
| 130 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.1 | 0.1 | 0.0 |
| 140 | 0.4 | 0.4 | 0.4 | 0.3 | $0 \cdot 3$ | 0.2 | 0.2 | O.I | O.I | 0.0 |
| 150 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.3 | 0.2 | O. I | O.I | 0.0 |
| 160 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | O. I | O.I | 0.0 |
| 170 | 0.5 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | 0.2 | 0.1 | 0.0 |
| 180 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 | 0.2 | 0.2 | 0.1 | 0.0 |
| 190 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | 0.1 | 0.0 |
| 200 | 0.5 | 0.5 | 0.5 | 0.5 | 0.4 | 0.3 | 0.3 | 0.2 | 0.1 | 0.0 |
| 210 | 0.6 | 0.6 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 | 0.2 | O.I | 0.0 |
| 220 | 0.6 | 0.6 | 0.6 | 0.5 | 0.4 | 0.4 | 0.3 | 0.2 | O.I | 0.0 |
| 230 | 0.6 | 0.6 | 0.6 | 0.5 | 0.5 | 0.4 | 0.3 | 0.2 | 0.1 | 0.0 |
| 240 | 0.6 | 0.6 | 0.6 | 0.6 | 0.5 | 0.4 | 0.3 | 0.2 | 0.1 | 0.0 |
| 250 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.4 | 0.3 | 0.2 | O.I | 0.0 |
| 260 | 0.7 | 0.7 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | 0.2 | 0.1 | 0.0 |
| 270 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.4 | 0.2 | 0.1 | 0.0 |
| 280 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.4 | 0.3 | O.I | 0.0 |
| 290 | 0.8 | 0.8 | 0.7 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | 0.1 | 0.0 |
| 300 | 0.8 | 0.8 | 0.8 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | O.I | 0.0 |
| 310 | 0.8 | 0.8 | 0.8 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | 0.1 | 0.0 |
| 320 | 0.9 | 0.8 | 0.8 | 0.7 | 0.7 | 0.5 | 0.4 | 0.3 | 0.1 | 0.0 |
| 330 | 0.9 | 0.9 | 0.8 | 0.8 | 0.7 | 0.6 | 0.4 | 0.3 | 0.2 | 0.0 |
| 340 | 0.9 | 0.9 | 0.9 | 0.8 | 0.7 | 0.6 | 0.5 | 0.3 | 0.2 | 0.0 |
| 350 | 0.9 | 0.9 | 0.9 | 0.8 | 0.7 | 0.6 | 0.5 | 0.3 | 0.2 | 0.0 |
|  | $90^{\circ}$ | $85^{\circ}$ | $80^{\circ}$ | $75^{\circ}$ | $70^{\circ}$ | $65^{\circ}$ | $60^{\circ}$ | $55^{\circ}$ | $50^{\circ}$ | $45^{\circ}$ |

Smitheonian Tables.

TABLE 16.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES. <br> $$
B_{0}-B=B\left(10^{m}-1\right) .
$$

Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 31.0 | 30.5 | 30.0 | 29.5 | 29.0 | 28.5 | 28.0 | 27.5 | 27.0 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| I | 0.04 | 0.04 | 0.03 | 0.03 | 0.03 | 0.03 |  |  |  |
| 2 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |  |  |  |
| 3 | O. II | O. 11 | o. Io | o. 10 | o. 10 | -. 10 |  |  |  |
| 4 | -. 14 | 0. 14 | 0. 14 | 0.14 | 0. 13 | 0. 13 |  |  |  |
| 5 | 0. 18 | 0. 18 | 0.17 | 0.17 | 0.17 | o 16 |  |  |  |
| 6 | 0.2I | 0.21 | 0.21 | 0.20 | 0.20 | 0.20 | 0. 19 |  |  |
| 7 | 0.25 | 0.25 | 0.24 | 0.24 | 0.23 | 0.23 | 0.23 |  |  |
| 8 | 0.29 | 0.28 | 0.28 | 0.27 | 0.27 | 0.26 | 0.26 |  |  |
| 9 | 0.32 | 0.32 | 0.31 | 0.31 | 0.30 | 0.30 | 0.29 |  |  |
| 10 | 0.36 | 0.35 | 0.35 | 0.34 | 0.34 | 0.33 | 0.32 |  |  |
| II | 0.40 | 0.39 | 0.38 | 0.38 | 0.37 | 0.36 | 0.36 |  |  |
| 12 | 0.43 | 0.42 | 0.42 | 0.41 | 0.40 | 0.40 | 0.39 |  |  |
| 13 | 0.47 | 0.46 | 0.45 | 0.44 | 0.44 | 0.43 | 0.42 |  |  |
| 14 | 0.50 | 0.50 | 0.49 | 0.48 | 0.47 | 0.46 | 0.46 |  |  |
| 15 | 0.54 | 0.53 | 0.52 | 0.51 | 0.51 | 0.50 | 0.49 |  |  |
| 16 | 0.58 | 0.57 | 0.56 | 0. 55 | 0.54 | 0.53 | 0.52 |  |  |
| 17 | 0.61 | 0.60 | 0.59 | 0.58 | 0.57 | 0.56 | 0.55 |  |  |
| 18 | 0.65 | 0.64 | 0.63 | 0.62 | 0.61 | 0.60 | 0.59 |  |  |
| 19 | 0.69 | 0.67 | 0.66 | 0.65 | 0.64 | 0.63 | 0.62 |  |  |
| 20 | 0.72 | 0.71 | 0.70 | 0.69 | 0.68 | 0.66 | 0.65 |  |  |
| 21 |  | 0.75 | 0.73 | 0.72 | 0.71 | 0.70 | 0.69 |  |  |
| 22 |  | 0.78 | 0.77 | 0.76 | 0. 74 | 0.73 | 0.72 | 0.71 |  |
| 23 |  | 0.82 | 0.80 | 0.79 | 0.77 | 0.76 | 0.75 | 0.74 |  |
| 24 |  | 0.85 | 0.84 | 0.83 | 0.81 | 0.80 | 0.78 | 0.77 |  |
| 25 |  | 0.89 | 0.88 | 0.86 | 0.85 | 0.83 | 0.82 | 0.80 |  |
| 26 |  | 0.93 | 0.91 | 0.90 | 0.88 | 0.87 | 0.85 | 0.84 |  |
| 27 |  | 0.96 | 0.95 | 0.93 | 0.92 | 0.90 | 0.88 | 0.87 |  |
| 28 |  | 1.00 | 0.98 | 0.97 | 0.95 | 0.93 | 0.92 | 0.90 |  |
| 29 |  | I. 04 | 1.02 | 1.00 | 0.98 | 0.97 | 0.95 | 0.93 |  |
| 30 |  | 1.07 | 1.05 | 1.04 | 1.02 | 1.00 | 0.98 | 0.97 |  |
| 3 I |  | I. II | 1.09 | 1.07 | 1.05 | 1.04 | I. 02 | 1.00 |  |
| 32 |  | I. 14 | I. 13 | I. II | 1.09 | 1.07 | 1.05 | 1.03 |  |
| 33 |  | I. 18 | x. 16 | I. 14 | I. 12 | I. 10 | I. 08 | 1.06 |  |
| 34 |  | 1.22 | 1.20 | I. 18 | I. 16 | I. 14 | 1.12 | I. 10 |  |
| 35 |  | I. 25 | 1.23 | 1.21 | I. 19 | 1.17 | 1.15 | I. 13 |  |
| 36 |  |  | 1.27 | 1.25 | 1.23 | I. 21 | I. 18 | I. 16 |  |
| 37 |  |  | 1.31 | I. 28 | I. 26 | I. 24 | 1.22 | 1.20 |  |
| 38 |  |  | I. 34 | 1.32 | 1.30 | 1.27 | 1.25 | 1.23 | I. 21 |
| 39 |  |  | I. 38 | I. 35 | I. 33 | 1.31 | 1.29 | I. 26 | 1.24 |
| 40 |  |  | I 41 | I. 39 | 1.37 | I. 34 | I. 32 | 1.30 | 1.27 |
| 4 I |  |  | I. 45 | r. 43 | I. 40 | I. 38 | 1.35 | 1.33 | 1.30 |
| 42 |  |  | I. 49 | I. 46 | I. 44 | I. 41 | 1.39 | 1.36 | 1.34 |
| 43 |  |  | I. 52 | I. 50 | I. 47 | I. 45 | I. 42 | I. 40 | I. 37 |
| 44 |  |  | 1.56 | 1.53 | I. 51 | I. 48 | I. 45 | 1.43 | 1.40 |
| 45 |  |  | 1.60 | 1.57 | I. 54 | I. 52 | I. 49 | . 146 | 1.44 |

TABLE 16
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.
$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.5 | 29.0 | 28.5 | 28.0 | 27.5 | 27.0 | 26.5 | 26.0 | 25.5 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 45 | 1.57 | I. 54 | 1.52 | I. 49 | 1.46 | 1.44 |  |  |  |
| 46 | 1.60 | 1.58 | 1.55 | 1.52 | 1. 50 | I. 47 |  |  |  |
| 47 | I. 64 | 1.61 | I. 58 | I. 56 | 1. 53 | I. 50 |  |  |  |
| 48 | 1. 68 | 1. 65 | 1.62 | I. 59 | 1.56 | I. 53 |  |  |  |
| 49 | 1.71 | I. 68 | 1. 65 | 1.62 | 1.60 | I. 57 |  |  |  |
| 50 | 1.75 | 1. 72 | 1. 69 | 1. 66 | 1.63 | 1.60 |  |  |  |
| 51 | 1.78 | 1. 75 | 1.72 | 1.69 | 1.66 | I. 63 |  |  |  |
| 52 | 1.82 | I. 79 | I. 76 | 1. 73 | 1.70 | 1. 67 |  |  |  |
| 53 | 1.86 | 1.82 | I. 79 | 1.76 | 1.73 | I. 70 |  |  |  |
| 54 | 1. 89 | 1. 86 | 1. 83 | 1.80 | 1.76 | 1.73 | 1.70 |  |  |
| 55 | 1.93 | 1.90 | 1. 86 | I. 83 | 1.80 | 1.76 | 1.73 |  |  |
| 56 | 1.96 | 1.93 | I. 90 | 1.86 | 1.83 | 1. 80 | 1.76 |  |  |
| 57 | 2.00 | 1.97 | 1.93 | 1.90 | 1.87 | 1.83 | 1.80 |  |  |
| 58 | 2.04 | 2.00 | I. 97 | I. 93 | 1.90 | I. 86 | 1.83 |  |  |
| 59 | 2.07 | 2.04 | 2.00 | 1.97 | 1.93 | 1.90 | 1.86 |  |  |
| 60 | 2.11 | 2.07 | 2.04 | 2.00 | 1.97 | 1.93 | 1.90 |  |  |
| 61 |  | 2.11 | 2.07 | 2.04 | 2.00 | I. 96 | I. 93 |  |  |
| 62 |  | 2.15 | 2.11 | 2.07 | 2.03 | 2.00 | I. 96 |  |  |
| 63 |  | 2.18 | 2.14 | 2.11 | 2.07 | 2.03 | 1.99 |  |  |
| 64 |  | 2.22 | 2.18 | 2.14 | 2.10 | 2.06 | 2.03 |  |  |
| 65 |  | 2.25 | 2.21 | 2.18 | 2.14 | 2.10 | 2.06 |  |  |
| 66 |  | 2.29 | 2.25 | 2.21 | 2.17 | 2.13 | 2.09 |  |  |
| 67 |  | 2.33 | 2.29 | 2.25 | 2.21 | 2.17 | 2.13 |  |  |
| 68 |  | 2.36 | 2.32 | 2.28 | 2.24 | 2.20 | 2.16 |  |  |
| 69 |  | 2.40 | 2.36 | 2.32 | 2.27 | 2.23 | 2.19 |  |  |
| 70 |  | 2.43 | 2.39 | 2.35 | 2.31 | 2.27 | 2.22 |  |  |
| 71 |  | 2.47 | 2.43 | 2.38 | 2.34 | 2.30 | 2.26 | 2.21 |  |
| 72 |  | 2.51 | 2.46 | 2.42 | 2.38 | 2.33 | 2.29 | 2.25 |  |
| 73 |  | 2.54 | 2.50 | 2.45 | 2.41 | 2.37 | 2.32 | 2.28 |  |
| 74 |  |  | 2.53 | 2.49 | 2.45 | 2.40 | 2.36 | 2.31 |  |
| 75 |  |  | 2.57 | 2.53 | 2.48 | 2.43 | 2.39 | 2.34 |  |
| 76 |  |  | 2.61 | 2.56 | 2.51 | 2.47 | 2.42 | 2.38 |  |
| 77 |  |  | 2.64 | 2.60 | 2.55 | 2.50 | 2.46 | 2.41 |  |
| 78 |  |  | 2.68 | 2.63 | 2.58 | 2.54 | 2.49 | 2.44 |  |
| 79 |  |  | 2.71 | 2.67 | 2.62 | 2.57 | 2.52 | 2.48 |  |
| 80 |  |  | 2.75 | 2.70 | 2.65 | 2.60 | 2.56 | 2.51 |  |
| 81 |  |  | 2.79 | 2.74 | 2.69 | 2.64 | 2.59 | 2.54 |  |
| 82 |  |  | 2.82 | 2.77 | 2.72 | 2.67 | 2.62 | 2.57 |  |
| 83 |  |  | 2.86 | 2.81 | 2.76 | 2.71 | 2.66 | 2.61 |  |
| 84 |  |  | 2.89 | 2.84 | 2.79 | 2.74 | 2.69 | 2.64 |  |
| 85 |  |  | - 2.93 | 2.88 | 2.83 | 2.78 | 2.72 | 2.67 |  |
| 86 |  |  | 2.97 | 2.91 | 2.86 | 2.81 | 2.76 | 2.71 |  |
| 87 |  |  | 3.00 | 2.95 | 2.90 | 2.84 | 2.79 | 2.74 |  |
| 88 |  |  | 3.04 | 2.99 | 2.93 | 2.88 | 2.83 | 2.77 | 2.72 |
| 89 |  |  | 3.08 | 3.02 | 2.97 | 2.91 | 2.86 | 2.81 | 2.75 |
| 90 |  |  | 3.11 | 3.06 | 3.00 | 2.95 | 2.89 | 2.84 | 2.78 |

TAble 16.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.
$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28.0 | 27.5 | 27.0 | 26.5 | 26.0 | 25.5 | 25.0 | 24.5 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 90 | 3.06 | 3.00 | 2.95 | 2.89 | 2.84 | 2.78 |  |  |
| 91 | 3.09 | 3.04 | 2.98 | 2.93 | 2.87 | 2.82 |  |  |
| 92 | 3.13 | 3.07 | 3.02 | 2.96 | 2.91 | 2.85 |  |  |
| 93 | 3.16 | 3.11 | 3.05 | 2.99 | 2.94 |  |  |  |
| 94 | 3.20 | 3.14 | 3.09 | 3.03 | 2.97 | 2.91 |  |  |
| 95 | 3.24 | 3.18 | 3.12 | 3.06 | 3.01 | 2.95 |  |  |
| 96 | 3.27 | 3.21 | 3.16 | 3.10 | 3.04 | 2.98 |  |  |
| 97 | 3.31 | 3.25 | 3.19 | 3.13 | 3.07 | 3.01 |  |  |
| 98 | 3.34 | 3.28 | 3.22 | 3.17 | 3.11 | 3.05 |  |  |
| 99 | 3.38 | 3.32 | 3.26 | 3.20 | 3.14 | 3.08 |  |  |
| 100 | 3.42 | 3.36 | 3.29 | 3.23 | 3.17 | 3.11 |  |  |
| Ior | 3.45 | 3.39 | 3.33 | 3.27 | 3.21 | 3.14 |  |  |
| 102 | 3.49 | 3.43 | 3.36 | 3.30 | 3.24 | 3.18 |  |  |
| 103 | 3.53 | 3.46 | 3.40 | 3.34 | 3.27 | 3.21 |  |  |
| 104 | 3.56 | $3 \cdot 50$ | 3.43 | $3 \cdot 37$ | $3 \cdot 31$ | 3.24 |  |  |
| 105 | 3.60 | 3.53 | 3.47 | 3.41 | 3.34 | 3.28 | 3.21 |  |
| 106 |  | 3.57 | 3.50 | 3.44 | 3.37 | 3.31 | 3.24 |  |
| 107 |  | 3.61 | 3.54 | 3.47 | 3.41 | 3.34 | 3.28 |  |
| 108 |  | 3.64 | 3.57 | 3.51 | 3.44 | $3 \cdot 38$ | 3.31 |  |
| 109 |  | 3.68 | 3.61 | 3.54 | 3.48 | 3.41 | 3.34 |  |
| 110 |  | 3.71 | 3.65 | 3.58 | 3.51 | 3.44 | 3.38 |  |
| 111 |  | 3.75 | 3.68 | 3.61 | 3.54 | 3.48 | 3.41 |  |
| 112 |  | 3.78 3.82 3.8 | 3.72 3 | 3.65 | 3.58 | 3.51 | 3.44 |  |
| 113 |  | 3.82 3.86 | 3.75 | 3.68 | 3.61 | 3.54 | 3.47 |  |
| 114 |  | 3.86 | 3.79 | 3.72 | 3.65 | 3.58 | 3.51 |  |
| 115 |  | 3.89 | 3.82 | 3.75 | 3.68 | 3.61 | 3.54 |  |
| 116 |  | 3.93 | 3.86 | 3.79 |  | 3.64 | 3.57 |  |
| 117 |  | 3.97 | 3.89 | 3.82 | 3.75 | 3.68 | 3.60 |  |
| 118 |  | 4.00 | 3.93 | 3.86 | 3.78 | 3.71 | 3.64 |  |
| 119 |  | 4.04 | 3.96 | 3.89 | 3.82 | 3.74 | 3.67 |  |
| 120 |  | 4.07 | 4.00 |  |  |  |  |  |
| 121 |  | 4. 1 I | 4.04 | 3.96 | 3.89 | 3.81 | 3.74 |  |
| 122 |  |  | 4.07 | 4.00 | 3.92 | 3.85 | 3.77 | 3.69 |
| 123 |  |  | 4.11 | 4.03 | 3.96 | 3.88 | 3.80 | 3.73 |
| 124 |  |  | 4.14 | 4.07 | 3.99 | 3.91 | 3.84 | 3.76 |
| 125 |  |  | 4.18 | 4. 10 | 4.02 | 3.95 | 3.87 | 3.79 |
| 126 |  |  | 4.22 | 4.14 | 4.06 | 3.98 | 3.90 | 3.82 |
| 127 |  |  | 4.25 | 4.17 | 4.09 | 4.01 | 3.94 | 3.86 |
| 128 |  |  | 4.29 | 4.21 | 4.13 | 4.05 | 3.97 | 3.89 |
| 129 |  |  | 4.32 | 4.24 | 4.16 | 4.08 | 4.00 | 3.92 |
| 130 |  |  | 4.36 | 4.28 | 4.20 | ${ }^{4} 4.12$ | 4.04 | 3.96 |
| 131 |  |  | 4.40 | 4.31 | 4.23 | 4.15 | 4.07 | 3.99 |
| 132 |  |  | 4.43 | 4.35 | 4.27 | 4.19 | 4.10 | 4.02 |
| 133 |  |  | 4.47 | 4.38 | 4.30 | 4.22 | 4.14 | 4.05 |
| 134 |  |  | 4.50 | 4.42 | 4.34 | 4.25 | 4.17 | 4.09 |
| 135 |  |  | 4.54 | 4.46 | 4.37 | 4.29 | 4.20 | 4.12 |

Smithbonian Tableg.

Table 16.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.
$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26.5 | 26.0 | 25.5 | 25.0 | 24.5 | 24.0 | 23.5 | 23.0 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 135 | 4.46 | 4.37 | 4.29 | 4.20 | 4.12 |  |  |  |
| 136 | 4.49 | 4.41 | 4.32 | 4.24 | 4.15 |  |  |  |
| 137 | 4.53 | 4.44 | $4 \cdot 36$ | 4.27 | 4.19 |  |  |  |
| 138 | 4.56 | 4.48 | 4.39 | 4.30 | 4.22 |  |  |  |
| 139 | 4.60 | 4.5 I | 4.43 | $4 \cdot 34$ | 4.25 |  |  |  |
| 140 | 4.63 | 4.55 | 4.46 | $4 \cdot 37$ | 4.28 | 4.20 |  |  |
| 141 | 4.67 | 4.58 | 4.49 | 4.41 | $4 \cdot 32$ | 4.23 |  |  |
| 142 | 4.71 | 4.62 | 4.53 | 4.44 | 4.35 | 4.26 |  |  |
| 143 | 4.74 | 4.65 | 4.56 | - 4.47 | 4.38 | 4.30 |  |  |
| 144 | 4.78 | 4.69 | 4.60 | 4.51 | 4.42 | 4.33 |  |  |
| 145 | 4.8 I | 4.72 | 4.63 | 4.54 | 4.45 | 4.36 |  |  |
| 146 | 4.85 | 4.76 | 4.67 | 4.58 | 4.48 | $4 \cdot 39$ |  |  |
| 147 | 4.89 | 4.79 | 4.70 | 4.61 | 4.52 | 4.43 |  |  |
| 148 | 4.92 | 4.83 | 4.74 | 4.64 | 4.55 | 4.46 |  |  |
| 149 | 4.96 | 4.87 | 4.77 | 4.68 | 4.58 | 4.49 |  |  |
| 150 | $5.00{ }^{-}$ | 4.90 | 4.81 | 4.71 | 4.62 | 4.52 |  |  |
| 151 | 5.03 | 4.94 | 4.84 | 4.75 | 4.65 | 4.56 |  |  |
| 152 | 5.07 | 4.97 | 4.88 | 4.78 | 4.69 | 4.59 |  |  |
| 153 | 5.10 | 5.01 | 4.91 | 4.82 | 4.72 | 4.62 |  |  |
| 154 |  | 5.04 | 4.95 | 4.85 | 4.75 | 4.66 |  |  |
| 155 |  | 5.08 | $4.98{ }^{\prime}$ | 4.88 | 4.79 | 4.69 |  |  |
| 156 |  | 5.12 | 5.02 | 4.92 | 4.82 | 4.72 |  |  |
| 157 |  | 5.15 | 5.05 | 4.95 | 4.85 | 4.75 |  |  |
| 158 |  | 5.19 | 5.09 | 4.99 | 4.89 | 4.79 |  |  |
| 159 |  | 5.22 | 5.12 | 5.02 | 4.92 | 4.82 | 4.72 |  |
| 160 |  | 5.26 | 5.16 | 5.06 | 4.96 | 4.85 | 4.75 |  |
| 161 |  | 5.29 | 5.19 | 5.09 | 4.99 | 4.89 | 4.79 |  |
| 162 |  | 5.33 | 5.23 | 5.13 | 5.02 | 4.92 | 4.82 |  |
| 163 |  | $5 \cdot 37$ | 5.26 | 5.16 | 5.06 | 4.95 | 4.85 |  |
| 164 |  | 5.40 | 5.30 | 5.20 | 5.09 | 4.99 | 4.88 |  |
| 165 |  | 5.44 | 5.33 | 5.23 | 5.13 | 5.02 | 4.92 |  |
| 166 |  | 5.48 | $5 \cdot 37$ | 5.26 | 5.16 | 5.05 | 4.95 |  |
| 167 |  | 5.51 | 5.4 I | $5 \cdot 30$ | 5.19 | 5.09 | 4.98 |  |
| 168 |  | 5.55 | 5.44 | $5 \cdot 33$ | 5.23 | 5.12 | 5.01 |  |
| 169 |  | 5.58 | 5.48 | 5.37 | 5.26 | 5.15 | 5.05 |  |
| 170 |  | 5.62 | $5 \cdot 5 \mathrm{I}$ | 5.40 | $5 \cdot 30$ | 5.19 | 5.08 |  |
| 171 |  |  | 5.55 | 5.44 | 5.33 | 5.22 | 5.11 |  |
| 172 |  |  | 5.58 | 5.47 | 5.37 | 5.26 | 5.15 |  |
| 173 |  |  | 5.62 | 5.51 | 5.40 | 5.29 | 5.18 |  |
| 174 |  |  | 5.66 | 5.54 | 5.43 | $5 \cdot 32$ | 5.21 |  |
| 175 |  |  | 5.69 | 5.58 | 5.47 | 5.36 |  |  |
| 176 |  |  | 5.73 | 5.62 | 5.50 | $5 \cdot 39$ | 5.28 |  |
| 177 |  |  | 5.76 | 5.65 | 5.54 | 5.42 | 5.31 | 5.20 |
| 178 |  |  | 5.80 | 5.69 | 5.57 | 5.46 | $5 \cdot 34$ | 5.23 |
| 179 |  |  | 5.84 | 5.72 | 5.61 | 5.49 | $5 \cdot 38$ | 5.26 |
| 180 |  |  | 5.87 | 5.76 | 5.64 | 5.53 | 5.41 | $5 \cdot 30$ |

Smithbonian Tables.

Table 16.
REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.
$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25.5 | 25.0 | 24.5 | 24.0 | 23.5 | 23.0 | 22.5 | 22.0 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 180 | 5.87 | 5.76 | 5.64 | 5.53 | 5.41 | 5.30 |  |  |
| 181 | 5.91 | 5.79 | 5.68 | 5.56 | 5.44 | $5 \cdot 33$ |  |  |
| 182 | 5.94 | 5.83 | 5.71 | 5.59 | 5.48 | $5 \cdot 36$ |  |  |
| 183 184 | 5.98 6.02 | 5.86 5.90 | 5.75 5.78 | 5.63 5.66 | 5.51 5.54 | 5.39 5.43 |  |  |
| 185 |  | 5.93 | 5.82 | 5.70 | 5.58 | 5.46 |  |  |
| 186 |  | 5.97 | 5.85 | 5.73 | 5.61 | 5.49 |  |  |
| 187 |  | 6.01 | 5.89 | 5.77 | 5.65 | 5.53 |  |  |
| 188 |  | 6.04 | 5.92 | 5.80 | 5.68 | 5.56 |  |  |
| 189 |  | 6.08 | 5.96 | 5.83 | 5.71 | 5.59 |  |  |
| 190 |  | 6.11 | 5.99 | 5.87 | 5.75 | 5.62 |  |  |
| 191 |  | 6.15 | 6.03 | 5.90 | 5.78 | 5.66 |  |  |
| 192 |  | 6.18 | 6.06 | 5.94 | 5.81 | 5.69 |  |  |
| 193 |  | 6.22 6.26 | 6.10 6.13 | 5.97 6.01 | 5.85 5.88 | 5.72 5.76 |  |  |
| 194 |  |  |  |  |  |  |  |  |
| 195 |  | 6.29 | 6.17 | 6.04 | 5.91 | 5.79 |  |  |
| 196 |  | 6.33 | 6.20 | 6.08 | 5.95 |  | 5.70 |  |
| 197 |  | 6.36 | 6.24 | 6.11 | 5.98 | 5.86 | 5.73 |  |
| 198 |  | 6.40 | 6.27 | 6. 14 | 6.02 | 5.89 | 5.76 |  |
| 199 |  | 6.44 | 6.31 | 6.18 | 6.05 | 5.92 | 5.79 |  |
| 200 |  | 6.47 | 6.34 | 6.21 | 6.08 | 5.96 | 5.83 |  |
| 201 |  | 6.51 | 6.38 | 6.25 | 6.12 | 5.99 | 5.86 |  |
| 202 |  | 6.55 | 6.41 | 6.28 | 6.15 | 6.02 | 5.89 |  |
| 203 |  | 6.58 | 6.45 | 6.32 | 6.19 | 6.06 | 5.92 |  |
| 204 |  | 6.62 | 6.49 | 6.35 | 6.22 | 6.09 | 5.96 |  |
| 205 |  |  | 6.52 | 6.39 | 6.26 | 6.12 |  |  |
| 206 |  |  | 6.56 | 6.42 | 6.29 | 6.16 | 6.02 |  |
| 207 |  |  | 6.59 | 6.46 | 6.32 | 6. 19 | 6.06 |  |
| 208 |  |  | 6.63 | 6.49 | 6.36 | 6.22 | 6.09 | 7 |
| 209 |  |  | 6.66 | 6.53 | 6.39 | 6.26 | 6.12 |  |
| 210 |  |  | 6.70 | 6.56 | 6.43 | 6.29 | 6.15 |  |
| 211 |  |  | 6.74 | 6.60 | 6.46 | 6.32 | 6.19 |  |
| 212 |  |  | 6.77 | 6.63 | 6.50 | 6.36 | 6.22 |  |
| 213 |  |  | 6.81 | 6.67 | 6.53 | 6.39 | 6.25 |  |
| 214 |  |  | 6.84 | 6.71 | 6.57 | 6.43 | 6.29 |  |
| 215 |  |  | 6.88 | 6.74 | 6.60 | 6.46 | 6.32 |  |
| 216 |  |  | 6.92 | 6.78 | 6.63 | 6.49 | 6.35 | 6.21 |
| 217 |  |  | 6.95 | 6.81 | 6.67 | 6.53 | 6.39 | 6.24 |
| 218 |  |  | 6.99 | 6.85 | 6.70 | 6.56 | 6.42 |  |
| 219 |  |  | 7.03 | 6.88 | 6.74 | 6.60 | 6.45 | 6.31 |
| 220 |  |  |  | 6.92 | 6.77 | 6.63 | 6.49 | 6.34 |
| 221 |  |  |  | 6.95 | 6.81 | 6.66 | 6.52 | 6.37 |
| 222 |  |  |  | 6.99 | 6.84 | 6.70 | 6.55 | 6.41 |
| 223 |  |  |  | 7.02 | 6.88 | 6.73 | 6.59 6.62 | 6.44 6.47 |
| 224 |  |  |  | 7.06 | 6.91 | 6.77 | 6.62 | 6.47 |
| 225 |  |  |  | 7.10 | 6.95 | 6.80 | 6.65 | 6.51 |

Smithbonian Tables. ENGLISH MEASURES.

$$
B_{0}-B=B\left(10^{m}-1\right) .
$$

Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 23.5 | 23.0 | 22.5 | 22.0 | 21.5 | 21.0 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 225 | 7.10 | 6.95 | 6.80 | 6.65 | 6.51 |  |  |
| 226 | 7.13 | 6.98 | 6.84 | 6.69 | 6.54 |  |  |
| 227 | 7.17 | 7.02 | 6.87 | 6.72 | 6.57 |  |  |
| 228 | 7.20 | 7.05 | 6.90 | 6.75 | 6.60 |  |  |
| 229 | 7.24 | 7.09 | 6.94 | 6.79 | 6.64 |  |  |
| 230 | 7.28 | 7.12 | 6.97 | 6.82 | 6.67 |  |  |
| 231 | 7.31 | 7.16 | 7.01 | 6.86 | 6.70 |  |  |
| 232 | 7.35 | 7.20 | 7.04 | 6.89 | 6.74 |  |  |
| 233 | 7.38 | 7.23 | 7.08 | 6.92 | 6.77 |  |  |
| 234 | 7.42 | 7.27 | 7.11 | 6.96 | 6.80 |  |  |
| 235 | 7.46 | 7.30 | 7.15 | 6.99 | 6.84 | 6.68 |  |
| 236 | 7.49 | 7.34 | 7.18 | 7.02 | 6.87 | 6.71 |  |
| 237 | 7.53 | $7 \cdot 37$ | 7.22 | 7.06 | 6.90 | 6.74 |  |
| 238 |  | 7.41 | 7.25 | 7.09 | 6.93 | 6.78 |  |
| 239 |  | 7.44 | 7.29 | 7.13 | 6.97 | 6.81 |  |
| 240 |  | 7.48 | 7.32 | 7.16 | 7.00 | 6.84 |  |
| 241 |  | 7.51 | 7.35 | 7.19 | 7.04 | 6.88 |  |
| 242 |  | 7.55 | 7.39 | 7.23 | 7.07 | 6.91 |  |
| 243 |  | 7.59 | 7.42 | 7.26 | 7.10 | 6.94 |  |
| 244 |  | 7.62 | 7.46 | 7.30 | 7.14 | 6.97 |  |
| 245 |  | 7.66 | 7.49 | 7.33 | 7.17 | 7.01 |  |
| 246 |  | 7.69 | 7.53 | 7.37 | 7.20 | 7.04 |  |
| 247 |  | 7.73 | 7.57 | 7.40 | 7.24 | 7.07 |  |
| 248 |  | 7.77 | 7.60 | 7.44 | 7.27 | 7.10 |  |
| 249 |  | 7.80 | 7.64 | 7.47 | 7.30 | 7.14 |  |
| 250 |  | 7.84 | 7.67 | 7.50 | 7.34 | 7.17 |  |
| 251 |  | 7.87 | 7.71 | 7.54 | 7.37 | 7.20 |  |
| 252 |  | 7.91 | 7.74 | 7.57 | 7.41 | 7.24 |  |
| 253 |  | 7.95 | 7.78 | 7.61 | 7.44 | 7.27 |  |
| 254 |  | 7.98 | 7.81 | 7.64 | 7.47 | 7.30 |  |
| 255 |  | 8.02 | 7.85 | 7.68 | 7.51 | 7.34 |  |
| 256 |  | 8.05 | 7.88 | 7.71 | 7.54 | 7.37 | 7.20 |
| 257 |  | 8.09 | 7.92 | 7.75 | 7.57 | 7.40 | 7.23 |
| 258 |  | 8.13 | 7.95 | 7.78 | 7.61 | 7.44 | 7.26 |
| 259 |  | 8.16 | 7.99 | 7.82 | 7.64 | 7.47 | 7.30 |
| 260 |  |  | 8.03 | 7.85 | 7.68 | 7.50 | 7.33 |
| 261 |  |  | 8.06 | 7.89 | 7.71 | 7.54 | 7.36 |
| 262 |  |  | 8.10 | 7.92 | 7.75 | 7.57 | 7.39 |
| 263 |  |  | 8.13 | 7.96 | 7.78 | 7.60 | 7.43 |
| 264 |  |  | 8.17 | 7.99 | 7.81 | 7.64 | 7.46 |
| 265 |  |  | 8.21 | 8.03 | 7.85 | 7.67 | 7.49 |
| 266 |  |  | 8.24 | 8.06 | 7.88 | 7.70 | 7.52 |
| 267 |  |  | 8.28 | 8.10 | 7.92 | 7.74 | 7.56 |
| 268 |  |  | 8.31 | 8.13 | 7.95 | 7.77 | 7.59 |
| 269 |  |  | 8.35 | 8.17 | 7.99 | 7.80 | 7.62 |
| 270 |  |  | 8.39 | 8.20 | 8.02 | 7.84 | 7.66 |

Table 16.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES. <br> $B_{0}-B=B\left(10^{m}-1\right)$.

Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 23.0 | 22.5 | 22.0 | 21.5 | 21.0 | 20.5 | 20.0 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 270 | 8.39 | 8.20 | 8.02 | 7.84 | 7.66 |  |  |
| 271 | 8.42 | 8.24 | 8.06 | 7.87 | 7.69 |  |  |
| 272 | 8.46 | 8.27 | 8.09 | 7.91 | 7.72 |  |  |
| 273 | 8.49 | 8.31 | 8.12 | 7.94 | 7.76 |  |  |
| 274 | 8.53 | 8.34 | 8.16 | 7.97 | 7.79 |  |  |
| 275 | 8.57 | 8.38 | 8.19 | 8.01 | 7.82 |  |  |
| 276 | 8.60 | 8.42 | 8.23 | 8.04 | 7.85 |  |  |
| 277 |  | 8.45 | 8.26 | 8.08 | 7.89 | 7.70 |  |
| 278 |  | 8.49 | 8.30 | 8.11 | 7.92 | 7.73 |  |
| 279 |  | 8.52 | 8.33 | 8.14 | 7.95 | 7.77 |  |
| 280 |  | 8.56 | 8.37 | 8.18 | 7.99 | 7.80 |  |
| 281 |  | 8.59 | 8.40 | 8.21 | 8.02 | 7.83 |  |
| 282 |  | 8.63 | 8.44 | 8.25 | 8.05 | 7.86 |  |
| 283 |  | 8.67 | 8.47 | 8.28 | 8.09 | 7.90 |  |
| 284 |  | 8.70 | 8.5 I | 8.32 | 8.12 | 7.93 |  |
| 285 |  | 8.74 | 8.54 | 8.35 | 8.16 | 7.96 |  |
| 286 |  | 8.77 | 8.58 | 8.38 | 8.19 | 7.99 |  |
| 287 |  | 8.81 | 8.61 | 8.42 | 8.22 | 8.03 |  |
| 288 289 |  | 8.85 8.88 | 8.65 8.68 | 8.45 | 8.26 8.29 | 8.06 |  |
| 290 |  | 8.92 | 8.72 | 8.52 | 8.32 | 8.13 |  |
| 291 |  | 8.95 | 8.76 | 8.56 | 8.36 | 8.16 |  |
| 292 |  | 8.99 | 8.79 | 8.59 | 8.39 | 8.19 |  |
| 293 |  | 9.03 | 8.83 | 8.63 | 8.43 | 8.22 |  |
| 294 |  | 9.06 | 8.86 | 8.66 | 8.46 | 8.26 |  |
| 295 |  | 9.10 | 8.90 | 8.70 | 8.49 | 8.29 | 8.09 |
| 296 |  | 9.14 | 8.93 | 8.73 | 8.53 | 8.32 | 8.12 |
| 297 |  |  | 8.97 | 8.76 | 8.56 | 8.36 | 8.15 |
| 298 |  |  | 9.00 | 8.80 | 8.60 | 8.39 | 8.19 |
| 299 |  |  | 9.04 | 8.83 | 8.63 | 8.42 | 8.22 |
| 300 |  |  | 9.08 | 8.87 | 8.66 | 8.46 | 8.25 |
| 301 |  |  | 9.11 | 8.90 | 8.70 | 8.49 | 8.28 |
| 302 |  |  | 9.15 | 8.94 | 8.73 | 8.52 | 8.32 |
| 303 |  |  | 9.18 | 8.97 | 8.77 | 8.56 | 8.35 |
| 304 |  |  | 9.22 | 9.01 | 8.80 | 8.59 | 8.38 |
| 305 |  |  | 9.26 | 9.04 | 8.83 | 8.62 | 8.41 |
| 306 |  |  | 9.29 | 9.08 | 8.87 | 8.66 | 8.45 |
| 307 |  |  | 9.33 | 9.12 | 8.90 | 8.69 | 8.48 |
| 309 |  |  | 9.40 | 9.19 | 8.97 | 8.76 | 8.54 |
| 310 |  |  | 9.44 | 9.22 | 9.01 | 8.79 | 8.58 |
| 311 |  |  | 9.47 | 9.26 | 9.04 | 8.83 | 8.61 |
| 312 |  |  | 9.51 | 9.29 | 9.08 | 8.86 | 8.64 |
| 313 |  |  | 9.54 | 9.33 | 9.11 | 8.89 | 8.68 |
| 314 |  |  | 9.58 | 9.36 | 9.15 | 8.93 | 8.71 |
| 315 |  |  | 9.62 | 9.40 | 9.18 | 8.96 | 8.74 |

TAble 16.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. ENGLISH MEASURES.

$$
\mathbf{B}_{0}-\mathbf{B}=\mathbf{B}\left(10^{m}-1\right)
$$

Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 14.

| 2000 m. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 22.0 | 21.5 | 21.0 | 20.5 | 20.0 | 19.5 |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 315 | 9.62 | 9.40 | 9.18 | 8.96 | 8.74 | 8.52 |
| 316 | 9.65 | 9.43 | 9.21 | 9.00 | 8.78 | 8.56 |
| 317 | 9.69 | 9.47 | 9.25 | 9.03 | 8.81 | 8.59 |
| 318 | 9.73 | 9.51 | 9.28 | 9.06 | 8.84 | 8.62 |
| 319 | 9.76 | 9.54 | 9.32 | 9.10 | 8.88 | 8.65 |
| 320 | 9.80 | 9.58 | 9.35 | 9.13 | 8.91 | 8.69 |
| 321 |  | 9.61 | 9.39 | 9.17 | 8.94 | 8.72 |
| 322 |  | 9.65 | 9.42 | 9.20 | 8.98 | 8.75 |
| 323 |  | 9.68 | 9.46 | 9.23 | 9.01 | 8.78 |
| 324 |  | 9.72 | 9.49 | 9.27 | 9.04 | 8.82 |
| 325 |  | 9.76 | 9.53 | $9 \cdot 30$ | 9.08 | 8.85 |
| 326 |  | 9.79 | 9.56 | $9 \cdot 34$ | 9.11 | 8.88 |
| 327 |  | 9.83 | 9.60 | 9.37 | 9.14 | 8.91 |
| 328 |  | 9.86 | 9.64 | 9.41 | 9.18 | 8.95 |
| 329 |  | 9.90 | 9.67 | 9.44 | 9.21 | 8.98 |
| 330 |  | 9.94 | 9.71 | 9.47 | 9.24 | 9.01 |
| 331 |  | 9.97 | 9.74 | 9.51 | 9.28 | 9.05 |
| 332 |  | 10.01 | 9.78 | 9.54 | 9.31 | 9.08 |
| 333 |  | 10.05 | 9.81 | 9.58 | 9.34 | 9.11 |
| 334 |  |  | 9.85 | 9.61 | $9 \cdot 38$ | 9.14 |

Smithbonian Tables.

TABLE 17.
REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.
Values of $2000 \times \mathrm{m}$.

$$
m=\frac{z}{18444+67.53 \theta+.003 z} \cdot \frac{1}{1-\beta}
$$

| Altitude in metres. 2. | mean temperature of air column in centigrade degrees ( $\theta$ ). |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | $-12^{\circ}$ | $-8^{\circ}$ | $-4^{\circ}$ | $-2^{\circ}$ | $0^{\circ}$ | $+2^{\circ}$ | $+4^{\circ}$ | + $6^{\circ}$ | $+8^{\circ}$ | $+10^{\circ}$ |
| 10 | 1.2 | I. 1 | I.I | I. I | I.I | I.I | I. 1 | I.I | 1. | 1. | 1.0 |
| 20 | 2.3 | 2.3 | 2.2 | 2.2 | 2.2 | 2.2 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 |
| 30 | 3.5 | $3 \cdot 4$ | 3.3 | 3.3 | $3 \cdot 3$ | 3.2 | 3.2 | 3.2 | 3.2 | 3.1 | 3.1 |
| 40 | 4.6 | 4.5 | 4.5 | $4 \cdot 4$ | 4.4 | 4.3 | 4.3 | $4 \cdot 3$ | 4.2 | 4.2 | 4.2 |
| 50 | 5.8 | 5.7 | 5.6 | 5.5 | $5 \cdot 5$ | 5.4 | 5.4 | $5 \cdot 3$ | $5 \cdot 3$ | 5.2 | 5.2 |
| 60 | 6.9 | 6.8 | 6.7 | 6.6 | 6.5 | 6.5 | 6.4 | 6.4 | 6.3 | 6.3 | 6.2 |
| 70 | 8.1 | 7.9 | 7.8 | 7.7 | 7.6 | 7.6 | 7.5 | 7.5 | 7.4 | 7.3 | 7.3 |
| 80 | 9.2 | 9. 1 | 8.9 | 8.8 | 8.7 | 8.7 | 8.6 | 8.5 | 8.5 | 8.4 | 8.3 |
| 90 | Io. 4 | 10.2 | 10.0 | 9.9 | 9.8 | 9.7 | 9.7 | 9.6 | 9.5 | 9.4 | 9.4 |
| 100 | 11.5 | 11.3 | 11.2 | II.O | 10.9 | 10.8 | 10.7 | 10.7 | 10.6 | 10.5 | 10.4 |
| 110 | 12.7 | 12.5 | 12.3 | 12.1 | 12.0 | 11.9 | 11.8 | 11.7 | 1 I .6 | 11.5 | 1 I .4 |
| 120 | 13.8 | 13.6 | 13.4 | 13.2 | I3.I | 13.0 | 12.9 | 12.8 | 12.7 | 12.6 | 12.5 |
| 130 | 15.0 | 14.7 | 14.5 | 14.3 | 14.2 | 14.1 | 14.0 | 13.9 | 13.7 | 13.6 | 13.5 |
| 140 | 16.1 | 15.9 | 15.6 | 15.4 | 15.3 | 15.1 | 15.0 | 14.9 | 14.8 | 14.7 | 14.6 |
| 150 | 17.3 | 17.0 | 16.7 | 16.5 | 16.4 | 16.2 | 16.1 | 16.0 | 15.9 | 15.7 | 15.6 |
| 160 | 18.4 | 18.1 | 17.8 | 17.6 | 17.4 | 17.3 | 17.2 | 17.0 | 16.9 | 16.8 | 16.7 |
| 170 | 19.6 | 19.3 | 19.0 | 18.7 | 18.5 | 18.4 | 18.3 | 18.1 | 18.0 | 17.8 | 17.7 |
| 180 | 20.7 | 20.4 | 20.1 | 19.8 | 19.6 | 19.5 | 19.3 | 19.2 | 19.0 | 18.9 | 18.7 |
| 190 | 21.9 | 21.5 | 21.2 | 20.9 | 20.7 | 20.6 | 20.4 | 20.2 | 20.1 | 19.9 | 19.8 |
| 200 | 23.0 | 22.7 | 22.3 | 22.0 | 21.8 | 21.6 | 21.5 | 21.3 | 21.1 | 21.0 | 20.8 |
| 210 | 24.2 | 23.8 | 23.4 | 23.1 | 22.9 | 22.7 | 22.6 | 22.4 | 22.2 | 22.0 | 21.9 |
| 220 | 25.3 | 24.9 | 24.5 | 24.2 | 24.0 | 23.8 | 23.6 | 23.4 | 23.3 | 23.1 | 22.9 |
| 230 | 26.5 | 26.1 | 25.7 | 25.3 | 25.1 | 24.9 | 24.7 | 24.5 | 24.3 | 24.1 | 23.9 |
| 240 | 27.6 | 27.2 | 26.8 | 26.4 | 26.2 | 26.0 | 25.8 | 25.6 | 25.4 | 25.2 | 25.0 |
| 250 | 28.8 | 28.3 | 27.9 | 27.5 | 27.3 | 27.0 | 26.8 | 26.6 | 26.4 | 26.2 | 26.0 |
| 260 | 29.9 | 29.5 | 29.0 | 28.6 | 28.3 | 28.1 | 27.9 | 27.7 | 27.5 | 27.3 | 27.1 |
| 270 | 31.1 | 30.6 | 30.1 | 29.7 | 29.4 | 29.2 | 29.0 | 28.8 | 28.5 | 28.3 | 28.1 |
| 280 | 32.2 | 31.7 | 31.2 | 30.8 | 30.5 | 30.3 | 30.1 | 29.8 | 29.6 | 29.4 | 29.1 |
| 290 | 33.4 | 32.9 | 32.4 | 31.9 | 31.6 | 31.4 | 31.1 | 30.9 | 30.7 | 30.4 | 30.2 |
| 300 | 34.5 | 34.0 | 33.5 | 33.0 | 32.7 | 32.5 | 32.2 | 32.0 | 31.7 | 31.5 | 31.2 |
| 310 | 35.7 | 35.1 | 34.6 | 34.1 | 33.8 | 33.5 | 33.3 | 33.0 | 32.8 | 32.5 | 32.3 |
| 320 | 36.8 | 36.3 | 35.7 | 35.2 | 34.9 | 34.6 | 34.4 | 34.I | 33.8 | 33.6 | 33.3 |
| 330 | 38.0 | 37.4 | 36.8 | 36.3 | 36.0 | 35.7 | 35.4 | 35.2 | 34.9 | 34.6 | 34.3 |
| 340 | 39. 1 | 38.5 | 37.9 | 37.4 | 37. 1 | 36.8. | 36.5 | 36.2 | 35.9 | 35.7 | 35.4 |
| 350 | 40.3 | 39.7 | 39.0 | 38.5 | 38.2 | 37.9 | 37.6 | 37.3 | 37.0 | 36.7 | 36.4 |
| 360 | 41.4 | 40.8 | 40.2 | 39.5 | 39.2 | 38.9 | 38.6 | 38.4 | 38.1 | 37.8 | 37.5 |
| 370 | 42.6 | 41.9 | 4 I .3 | 40.6 | 40.3 | 40.0 | 39.7 | 39.4 | 39.1 | 38.8 | 38.5 |
| 380 | 43.7 | 43.1 | 42.4 | 41.7 | 4 I .4 | 4 I .1 | 40.8 | 40.5 | 40.2 | 39.9 | 39.6 |
| 390 | 44.9 | 44.2 | 43.5 | 42.8 | 42.5 | 42.2 | 4 I .9 | 4 I .5 | 4 I .2 | 40.9 | 40.6 |
| 400 | 46.0 | $45 \cdot 3$ | 44.6 | 43.9 | 43.6 | 43.3 | 42.9 | 42.6 | 42.3 | 42.0 | 41.6 |
| 410 | 47.2 | 46.4 | 45.7 | 45.0 | 44.7 | 44.4 | 44.0 | 43.7 | 43.3 | 43.0 | 42.7 |
| 420 | 48.3 | 47.6 | 46.9 | 46.1 | 45.8 | 45.4 | 45.1 | 44.7 | 44.4 | 44.I | 43.7 |
| 430 | 49.5 | 48.7 | 48.0 | 47.2 | 46.9 | 46.5 | 46.2 | 45.8 | 45.5 | 45.1 | 44.8 |
| 440 | 50.6 | 49.8 | 49. 1 | 48.3 | 48.0 | 47.6 | 47.2 | 46.9 | 46.5 | 46.2 | 45.8 |
| 450 | 51.8 | 51.0 | 50.2 | 49.4 | 49.1 | 48.7 | 48.3 | 47.9 | 47.6 | 47.2 | 46.8 |
| 460 | 52.9 | 52.1 | 51.3 | 50.5 | 50.1 | 49.8 | 49.4 | 49.0 | 48.6 | 48.2 | 47.9 |
| 470 | 54.I | 53.2 | 52.4 | 51.6 | 5 I .2 | 50.8 | 50.5 | 50.1 | 49.7 | 49.3 | 48.9 |
| 480 | 55.2 | 54.4 | 53.5 | 52.7 | 52.3 | 51.9 | 51.5 | 5 I .1 | 50.7 | 50.3 | 50.0 |
| 490 | 56.4 | 55.5 | 54.7 | 53.8 | 53.4 | 53.0 | 52.6 | 52.2 | 51.8 | 51.4 | 51.0 |
| 500 | 57.5 | 56.6 | 55.8 | 54.9 | 54.5 | 54.1 | 53.7 | 53.3 | 52.9 | 52.4 | 52.0 |

TABLE 17. REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Values of $2000 \times \mathrm{m}$.
$m=\frac{z}{18444+67.53 \theta+.003 z} \cdot \frac{I}{I-\beta}$

| Altitude in metres. <br> 2. | MEAN TEMPERATURE OF AIR COLUMN IN CENTIGRADE DEGREES ( $\theta$ ). |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $+12^{\circ}$ | $+14^{\circ}$ | $+16^{\circ}$ | $+18^{\circ}$ | $+20^{\circ}$ | $+22^{\circ}$ | $+24^{\circ}$ | $+26^{\circ}$ | $+28^{\circ}$ | $+32^{\circ}$ | $+36^{\circ}$ |
| 10 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 0.9 |
| 20 | 2.1 | 2.1 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 1.9 | 1.9 | 1.9 |
| 30 | 3.1 | 3.1 | 3.1 | 3.0 | 3.0 | 3.0 | 3.0 | 2.9 | 2.9 | 2.9 | 2.8 |
| 40 | 4.I | 4.1 | 4.1 | 4.0 | 4.0 | 4.0 | 3.9 | $3 \cdot 9$ | 3.9 | 3.8 | 3.8 |
| 50 | 5.2 | 5.1 | 5.I | 5.0 | 5.0 | 5.0 | 4.9 | 4.9 | 4.9 | 4.8 | 4.7 |
| 60 | 6.2 | 6.2 | 6.1 | 6.1 | 6.0 | 6.0 | $5 \cdot 9$ | 5.9 | 5.8 | 5.8 | 5.7 |
| 70 | 7.2 | 7.2 | 7.1 | 7.1 | 7.0 | 7.0 | 6.9 | 6.9 | 6.8 | 6.7 | 6.6 |
| 80 | 8.3 | 8.2 | 8.1 | 8.1 | 8.0 | 8.0 | 7.9 | 7.8 | 7.8 | 7.7 | 7.6 |
| 90 | 9.3 | 9.2 | 9.2 | 9.1 | 9.0 | 9.0 | 8.9 | 8.8 | 8.8 | 8.6 | 8.5 |
| 100 | 10.3 | 10.3 | 10.2 | 10. 1 | 10.0 | 9.9 | 9.9 | 9.8 | 9.7 | 9.6 | 9.5 |
| 110 | $\underline{11.4}$ | 11.3 | 11.2 | II.I | 11.0 | 10.9 | 10.9 | 10.8 | 10.7 | 10.5 | 10.4 |
| 120 | 12.4 | 12.3 | 12.2 | 12.I | 12.0 | 11.9 | 11.8 | 11.8 | 11.7 | 11.5 | II. 3 |
| 130 | 13.4 | 13.3 | 13.2 | 13.1 | 13.0 | 12.9 | 12.8 | 12.7 | 12.7 | 12.5 | 12.3 |
| 140 | 14.5 | 14.3 | 14.2 | 14.1 | 14.0 | 13.9 | I3.8 | 13.7 | 13.6 | 13.4 | 13.2 |
| 150 | I5.5 | I5.4 | 15.3 | 15.1 | 15.0 | 14.9 | 14.8 | 14.7 | 14.6 | 14.4 | 14.2 |
| 160 | 16.5 | 16.4 | 16.3 | 16.2 | 16.0 | 15.9 | 15.8 | 15.7 | 15.6 | 15.3 | 15.1 |
| 170 | 17.6 | 17.4 | 17.3 | 17.2 | 17.0 | 16.9 | 16.8 | 16.7 | 16.5 | 16.3 | 16.1 |
| 180 | 18.6 | 18.4 | 18.3 | 18.2 | 18.0 | 17.9 | 17.8 | 17.6 | 17.5 | 17.3 | 17.0 |
| 190 | 19.6 | 19.5 | 19.3 | 19.2 | 19.0 | 18.9 | 18.8 | 18.6 | 18.5 | 18.2 | 18.0 |
| 200 | 20.7 | 20.5 | 20.3 | 20.2 | 20.0 | 19.9 | 19.7 | 19.6 | 19.5 | 19.2 | 18.9 |
| 210 | 21.7 | 21.5 | 21.4 | 21.2 | 21.0 | 20.9 | 20.7 | 20.6 | 20.4 | 20.1 | 19.8 |
| 220 | 22.7 | 22.5 | 22.4 | 22.2 | 22.0 | 21.9 | 21.7 | 21.6 | 21.4 | 2 I .1 | 20.8 |
| 230 | 23.8 | 23.6 | 23.4 | 23.2 | 23.0 | 22.9 | 22.7 | 22.5 | 22.4 | 22.0 | 21.7 |
| 240 | 24.8 | 24.6 | 24.4 | 24.2 | 24.0 | 23.9 | 23.7 | 23.5 | 23.3 | 23.0 | 22.7 |
| 250 | 25.8 | 25.6 | 25.4 | 25.2 | 25.0 | 24.9 | 24.7 | 24.5 | 24.3 | 24.0 | 23.6 |
| 260 | 26.9 | 26.6 | 26.4 | 26.2 | 26.1 | 25.9 | 25.7 | 25.5 | 25.3 | 24:9 | 24.6 |
| 270 | 27.9 | 27.7 | 27.5 | 27.3 | 27.1 | 26.9 | 26.7 | 26.5 | 26.3 | 25.9 | 25.5 |
| 280 | 28.9 | 28.7 | 28.5 | 28.3 | 28.1 | 27.8 | 27.6 | 27.4 | 27.2 | 26.8 | 26.5 |
| 290 | 29.0 | 29.7 | 29.5 | 29.3 | 29.1 | 28.8 | 28.6 | 28.4 | 28.2 | 27.8 | 27.4 |
| 300 | 31.0 | 30.7 | 30.5 | 30.3 | 30.1 | 29.8 | 29.6 | 29.4 | 29.2 | 28.8 | 28.4 |
| 310 | 32.0 | 31.8 | 3 I .5 | 3 I .3 | 3 I .1 | 30.8 | 30.6 | 30.4 | 30.2 | 29.7 | 29.3 |
| 320 | 33.1 | 32.8 | 32.6 | 32.3 | 32.1 | 31.8 | 31.6 | 31.4 | 3 I .1 | 30.7 | 30.3 |
| 330 | 34. I | 33.8 | 33.6 | $33 \cdot 3$ | 33. I | 32.8 | 32.6 | 32.3 | 32. I | 31.6 | 31.2 |
| 340 | 35. I | 34.8 | 34.6 | $34 \cdot 3$ | 34. 1 | 33.8 | 33.6 | 33.3 | 33.1 | 32.6 | 32.1 |
| 350 | 36.2 | 35.9 | 35.6 | $35 \cdot 3$ | 35. I | 34.8 | 34.6 | 34.3 | 34.0 | 33.5 | 33. 1 |
| 360 | 37.2 | 36.9 | 36.6 | 36.3 | 36.1 | 35.8 | 35.5 | $35 \cdot 3$ | 35.0 | $34 \cdot 5$ | 34.0 |
| 370 | 38.2 | 37.9 | 37.6 | 37.4 | 37. I | 36.8 | 36.5 | 36.3 | 36.0 | 35.5 | 35.0 |
| 380 | 39.2 | 38.9 | 38.7 | 38.4 | 38.1 | 37.8 | 37.5 | 37.2 | 37.0 | 36.4 | 35.9 |
| 390 | 40.3 | 40.0 | 39.7 | 39.4 | 39.1 | 38.8 | 38.5 | 38.2 | 37.9 | 37.4 | 36.9 |
| 400 | 4 I .3 | 41.0 | 40.7 | 40.4 | 40.1 | 39.8 | 39.5 | 39.2 | 38.9 | 38.3 | 37.8 |
| 410 | 42.3 | 42.0 | 41.7 | 4 I .4 | 41. I | 40.8 | 40.5 | 40.2 | 39.9 | 39.3 | 38.7 |
| 420 | 43.4 | 43.0 | 42.7 | 42.4 | 42. I | 4 I .8 | 41.5 | 41.2 | 40.8 | 40.3 | 39.7 |
| 430 | 44.4 | 44. 1 | 43.7 | 43.4 | 43. I | 42.8 | 42.4 | 42.1 | 41.8 | 41.2 | 40.6 |
| 440 | 45.4 | 45. I | 44.8 | 44.4 | 44. 1 | 43.8 | 43.4 | 43. 1 | 42.8 | 42.2 | 41.6 |
| 450 | 46.5 | 46.1 | 45.8 | 45.4 | 45. I | 44.8 | 44.4 | 44. I | 43.8 | 43. I | 42.5 |
| 460 | 47.5 | 47.1 | 46.8 | 46.4 | 46.1 | 45.7 | 45.4 | 45. I | 44.7 | 44 I | 43.5 |
| 470 | 48.5 | 48.2 | 47.8 | 47.4 | 47.1 | 46.7 | 46.4 | 46.1 | 45.7 | 45.0 | 44.4 |
| 480 | 49.6 | 49.2 | 48.8 | 48.5 | 48.1 | 47.7 | 47.4 | 47.0 | 46.7 | 46.0 | 45.4 |
| 490 | 50.6 | 50.2 | 49.8 | 49.5 | 49.1 | 48.7 | 48.4 | 48.0 | 47.6 | 47.0 | 46.3 |
| 500 | 5 I .6 | 5 I .2 | 50.9 | 50.5 | 50.1 | 49.7 | 49.4 | 49.0 | 48.6 | 47.9 | 47.2 |

Table 17.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

$$
\text { Values of } 2000 \times \mathrm{m} . \quad m=\frac{\mathrm{z}}{18444+67 \cdot 53 \theta+.003 Z} \cdot \frac{\mathrm{I}}{\mathrm{I}-\beta}
$$

| Altitude in metres. Z. | MEAN TEMPERATURE OF AIR COLUMN IN CENTIGRADE DEGREES ( $\theta$ ). |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | $-12^{\circ}$ | $-8^{\circ}$ | $-4^{\circ}$ | $-2^{\circ}$ | $0^{\circ}$ | $+2^{\circ}$ | $+4^{\circ}$ | $+6^{\circ}$ | $+8^{\circ}$ | $+10^{\circ}$ |
| 500 | 57.5 | 56.6 | 55.8 | 54.9 | 54.5 | 54.1 | 53.7 | 53.3 | 52.9 | 52.4 | 52.0 |
| 510 | 58.7 | 57.8 | 56.9 | 56.0 | 55.6 | 55.2 | 54.8 | 54.3 | 53.9 | 53.5 | 53.1 |
| 520 | 59.8 | 58.9 | 58.0 | 57.1 | 56.7 | 56.3 | 55.8 | 55.4 | 55.0 | 54.5 | 54.1 |
| 530 | 61.0 | 60.0 | 59.1 | 58.2 | 57.8 | 57.3 | 56.9 | 56.5 | 56.0 | 55.6 | 55.2 |
| 540 | 62.1 | 6 I .2 | 60.2 | 59.3 | 58.9 | 58.4 | 58.0 | 57.5 | 57.I | 56.6 | 56.2 |
| 550 | 63.3 | 62.3 | 6I. 4 | 60.4 | 60.0 | 59.5 | 59.0 | 58.6 | 58.1 | 57.7 | 57.2 |
| 560 | 64.4 | 63.4 | 62.5 | 61.5 | 61.I | 60.6 | 60.1 | 59.7 | 59.2 | 58.7 | 58.3 |
| 570 | 65.6 | 64.6 | 63.6 | 62.6 | 62.1 | 6 I .7 | 6 I .2 | 60.7 | 60.3 | 59.8 | 59.3 |
| 580 | 66.7 | 65.7 | 64.7 | 63.7 | 63.2 | 62.7 | 62.3 | 61.8 | 6 I .3 | 60.8 | 60.4 |
| 590 | 67.9 | 66.8 | 65.8 | 64.8 | 64.3 | 63.8 | 63.3 | 62.9 | 62.4 | 61.9 | 61.4 |
| 600 | 69.0 | 68.0 | 66.9 | 65.9 | 65.4 | 64.9 | 64.4 | 63.9 | 63.4 | 62.9 | 62.4 |
| 610 | 70.2 | 69.1 | 68.0 | 67.0 | 66.5 | 66.0 | 65.5 | 65.0 | 64.5 | 64.0 | 63.5 |
| 620 | 71.4 | 70.2 | 69.2 | 68.1 | 67.6 | 67.1 | 66.6 | 66.0 | 65.5 | 65.0 | 64.5 |
| 630 | 72.5 | 71.4 | 70.3 | 69.2 | 68.7 | 68.2 | 67.6 | 67.1 | 66.6 | 66.1 | 65.6 |
| 640 | 73.7 | 72.5 | 71.4 | 70.3 | 69.8 | 69.2 | 68.7 | 68.2 | 67.7 | 67.1 | 66.6 |
| 650 | 74.8 | 73.6 | 72.5 | 7 I .4 | 70.9 | 70.3 | 69.8 | 69.2 | 68.7 | 68.2 | 67.6 |
| 660 | 76.0 | 74.8 | 73.6 | 72.5 | 72.0 | 71.4 | 70.9 | 70.3 | 69.8 | 69.2 | 68.7 |
| 670 | 77.1 | 75.9 | 74.7 | 73.6 | 73.0 | 72.5 | 71.9 | 71.4 | 70.8 | 70.3 | 69.7 |
| 680 | 78.3 | 77.0 | 75.9 | 74.7 | 74.I | 73.6 | 73.0 | 72.4 | 71.9 | 71.3 | 70.8 |
| 690 | 79.4 | 78.2 | 77.0 | 75.8 | 75.2 | 74.6 | 74.1 | 73.5 | 72.9 | 72.4 | 71.8 |
| 700 | 80.6 | 79.3 | 78.1 | 76.9 | 76.3 | 75.7 | 75.I | 74.6 | 74.0 | 73.4 | 72.9 |
| 710 | 81.7 | 80.4 | 79.2 | 78.0 | 77.4 | 76.8 | 76.2 | 75.6 | 75.1 | 74.5 | 73.9 |
| 720 | 82.9 | 8 I .6 | 80.3 | 79.1 | 78.5 | 77.9 | 77.3 | 76.7 | 76.1 | 75.5 | 74.9 |
| 730 | 83.0 | 82.7 | 8 I .4 | 80.2 | 79.6 | 79.0 | 78.4 | 77.8 | 77.2 | 76.6 | 76.0 |
| 740 | 85.2 | 83.8 | 82.5 | 8 I .3 | 80.7 | 80.1 | 79.4 | 78.8 | 78.2 | 77.6 | 77.0 |
| 750 | 86.3 | 85.0 | 83.7 | 82.4 | 81. 8 | 8 I .1 | 80.5 | 79.9 | 79.3 | 78.7 | 78.1 |
| 760 | 87.5 | 86.1 | 84.8 | 83.5 | 82.9 | 82.2 | 81.6 | 81.0 | 80.3 | 79.7 | 79.1 |
| 770 | 88.6 | 87.2 | 85.9 | 84.6 | 83.9 | 83.3 | 82.7 | 82.0 | 8 r .4 | 80.8 | 80.1 |
| 780 | 89.8 | 88.4 | $87.0{ }^{-}$ | 85.7 | 85.0 | 84.4 | 83.7 | 83.1 | 82.5 | 8 I .8 | 8 I .2 |
| 790 | 90.9 | 89.5 | 88.1 | 86.8 | 86.1 | 85.5 | 84.8 | 84.2 | 8.3.5 | 82.9 | 82.2 |
| 800 | 92.I | 90.6 | 89.2 | 87.9 | 87.2 | 86.5 | 85.9 | 85.2 | 84.6 | 83.9 | 83.3 |
| 810 | 93.2 | 91.8 | 90.4 | 89.0 | 88.3 | 87.6 | 87.0 | 86.3 | 85.6 | 85.0 | 84.3 |
| 820 | 94.4 | 92.9 | 91.5 | 90.1 | 89.4 | 88.7 | 88.0 | 87.4 | 86.7 | 86.0 | 85.3 |
| 830 | 95.5 | 94.0 | 92.6 | 91.2 | 90.5 | 89.8 | 89.1 | 88.4 | 87.7 | 87.1 | 86.4 |
| 840 | 96.7 | 95.2 | 93.7 | 92.3 | 91.6 | 90.9 | 90.2 | 89.5 | 88.8 | 88.1 | 87.4 |
| 850 | 97.8 | 96.3 | 94.8 | 93.4 | 92.7 | 92.0 | 91.2 | 90.5 | 89.8 | 89.2 | 88.5 |
| 860 | 99.0 | 97.4 | 95.9 | 94.5 | 93.8 | 93.0 | 92.3 | 91.6 | 90.9 | 90.2 | 89.5 |
| 870 | 100.1 | 98.6 | 97.0 | 95.6 | 94.8 | 94.I | 93.4 | 92.7 | 92.0 | 91.3 | 90.5 |
| 880 | IOI. 3 | 99.7 | 98.2 | 96.7 | 95.9 | 95.2 | 94.5 | 93.7 | 93.0 | 92.3 | 91.6 |
| 890 | 102.4 | 100.8 | 99.3 | 97.8 | 97.0 | 96.3 | 95.5 | 94.8 | 94.1 | 93.3 | 92.6 |
| 900 | 103.6 | 102.0 | 100.4 | 98.9 | 98.1 | 97.4 | 96.6 | 95.9 | 95.1 | 94.4 | 93.7 |
| 910 | 104.7 | 103.1 | 101.5 | 100.0 | 99.2 | 98.4 | 97.7 | 96.9 | 96.2 | 95.4 | 94.7 |
| 920 | 105.9 | 104.2 | 102.6 | IOI.I | 100.3 | 99.5 | 98.8 | 98.0 | 97.2 | 96.5 | 95.7 |
| 930 | 107.0 | 105.4 | 103.7 | 102.2 | IOI. 4 | 100.6 | 99.8 | 99.1 | 98.3 | 97.5 | 96.8 |
| 940 | 108.2 | 106.5 | 104.9 | 103.3 | 102.5 | 101.7 | 100.9 | 100.1 | 99.4 | 98.6 | 97.8 |
| 950 | 109.3 | 107.6 | 106.0 | 104.4 | 103.6 | 102.8 | 102.0 | IOI. 2 | 100.4 | 99.6 | 98.9 |
| 960 | 110.5 | 108.8 | 107.1 | 105.5 | 104.7 | 103.9 | 103.I | 102.3 | IOI. 5 | 100.7 | 99.9 |
| 970 | III. 6 | 109.9 | 108.2 | 106.6 | 105.7 | 104.9 | 104.I | 103.3 | 102.5 | 101.7 | 100.9 |
| 980 | 112.8 | 111.0 | 109.3 | 107.6 | 106.8 | 106.0 | 105.2 | 104.4 | 103.6 | 102.8 | 102.0 |
| 990 | 113.9 | II2.I | IIO. 4 | 108.7 | 107.9 | 107.I | 106.3 | 105.5 | 104.6 | 103.8 | 103.0 |
| 1000 | II5.I | II3.3 | III. 5 | 109.8 | 109.0 | 108.2 | 107.3 | 106.5 | 105.7 | 104.9 | 104.1 |

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Values of $2000 \times \mathrm{m} . \quad m=\frac{\mathrm{z}}{18444+67.53 \theta+.003 Z} \cdot \frac{1}{1-\beta}$

| Altitude in metres. $Z$. | MEAN TEMPERATURE O |  |  |  | AIR | M | IN |  |  | EES | $\theta)$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $+12^{\circ}$ | $+14^{\circ}$ | $+16^{\circ}$ | $+18^{\circ}$ | $+20^{\circ}$ | $+22^{\circ}$ | $+24^{\circ}$ | $+26^{\circ}$ | $+28^{\circ}$ | $+32^{\circ}$ | $+36^{\circ}$ |
| 500 | 51.6 | 51.2 | 50.9 | 50.5 | 50.1 | 49.7 | 49.4 | 49.0 | 48.6 | 47.9 | 47.2 |
| 510 | 52.7 | 52.3 | 51.9 | 51.5 | 51.1 | 50.7 | 50.3 | 50.0 | 49.6 | 48.9 | 48.2 |
| 520 | 53.7 | $53 \cdot 3$ | 52.9 | 52.5 | 52.1 | 51.7 | 51.3 | 51.0 | 50.6 | 49.8 | 49.1 |
| 530 | 54.7 | $54 \cdot 3$ | 53.9 | 53.5 | 53.1 | 52.7 | 52.3 | 51.9 | 51.5 | 50.8 | 50.1 |
| 540 | 55.8 | 55.3 | 54.9 | 54.5 | 54.I | 53.7 | 53.3 | 52.9 | 52.5 | 51.8 | 51.0 |
| 550 | 56.8 | 56.4 | 55.9 | 55.5 | 55.1 | 54.7 | 54.3 | 53.9 | 53.5 | 52.7 | 52.0 |
| 560 | 57.8 | 57.4 | 57.0 | 56.5 | 56.1 | 55.7 | 55.3 | 54.9 | 54.4 | 53.7 | 52.9 |
| 570 | 58.9 | 58.4 | 58.0 | 57.5 | 57.1 | 56.7 | 56.3 | 55.8 | 55.4 | 54.6 | 53.9 |
| 580 | 59.9 | 59.4 | 59.0 | 58.5 | 58.1 | 57.7 | 57.2 | 56.8 | 56.4 | 55.6 | 54.8 |
| 590 | 60.9 | 60.5 | 60.0 | 59.6 | 59.1 | 58.7 | 58.2 | 57.8 | 57.4 | 56.5 | 55.7 |
| 600 | 62.0 | 6 I .5 | 61.0 | 60.6 | 60.1 | 59.7 | 59.2 | 58.8 | 58.3 | 57.5 | 56.7 |
| 610 | 63.0 | 62.5 | 62.0 | 61.6 | 61.1 | 60.7 | 60.2 | 59.8 | 59.3 | 58.5 | 57.6 |
| 620 | 64.0 | 63.5 | 63.1 | 62.6 | 62.1 | 61.7 | 61.2 | 60.7 | 60.3 | 59.4 | 58.6 |
| 630 | 65.1 | 64.6 | 64.1 | 63.6 | 63.1 | 62.6 | 62.2 | 61.7 | 61.3 | 60.4 | 59.5 |
| 640 | 66.1 | 65.6 | 65.1 | 64.6 | 64.1 | 63.6 | 63.2 | 62.7 | 62.2 | 6 I .3 | 60.5 |
| 650 | 67.1 | 66.6 | 66.1 | 65.6 | 65.1 | 64.6 | 64.2 | 63.7 | 63.2 | 62.3 | 6 I .4 |
| 660 | 68.2 | 67.6 | 67.1 | 66.6 | 66.1 | 65.6 | 65.1 | 64.7 | 64.2 | 63.3 | 62.4 |
| 670 | 69.2 | 68.7 | 68.1 | 67.6 | 67.1 | 66.6 | 66.1 | 65.6 | 65.1 | 64.2 | 63.3 |
| 680 | 70.2 | 69.7 | 69.2 | 68.6 | 68.1 | 67.6 | 67.1 | 66.6 | 66.1 | 65.2 | 64.2 |
| 690 | 71.3 | 70.7 | 70.2 | 69.6 | 69.1 | 68.6 | 68.1 | 67.6 | 67.1 | 66.1 | 65.2 |
| 700 | 72.3 | 71.7 | 7 x .2 | 70.7 | 70.1 | 69.6 | 69.1 | 68.6 | 68.1 | 67.1 | 66.1 |
| 710 | 73.3 | 72.8 | 72.2 | 71.7 | 7 I .1 | 70.6 | 70.1 | 69.6 | 69.0 | 68.0 | 67.1 |
| 720 | 74.4 | 73.8 | 73.2 | 72.7 | 72.1 | 71.6 | 71.1 | 70.5 | 70.0 | 69.0 | 68.0 |
| 730 | 75.4 | 74.8 | 74.2 | 73.7 | 73.1 | 72.6 | 72.0 | 7 I .5 | 71.0 | 70.0 | 69.0 |
| 740 | 76.4 | 75.8 | $75 \cdot 3$ | 74.7 | 74.1 | 73.6 | 73.0 | 72.5 | 72.0 | 70.9 | 69.9 |
| 750 | 77.5 | 76.9 | 76.3 | 75.7 | 75.1 | 74.6 | 74.0 | 73.5 | 72.9 | 71.9 | 70.9 |
| 760 | 78.5 | 77.9 | 77.3 | 76.7 | 76.1 | 75.6 | 75.0 | 74.5 | 73.9 | 72.8 | 71.8 |
| 770 | 79.5 | 78.9 | 78.3 | 77.7 | 77.1 | 76.6 | 76.0 | 75.4 | 74.9 | 73.8 | 72.8 |
| 780 | 80.6 | 79.9 | 79.3 | 78.7 | 78.1 | 77.6 | 77.0 | 76.4 | 75.9 | 74.8 | 73.7 |
| 790 | 8 I .6 | 81.0 | 80.3 | 79.7 | 79.1 | 78.6 | 78.0 | 77.4 | 76.8 | 75.7 | 74.6 |
| 800 | 82.6 | 82.0 | 8 8 .4 | 80.8 | $8 \mathrm{o.I}$ | 79.6 | 79.0 | 78.4 | 77.8 | 76.7 | 75.6 |
| 810 | 83.7 | 83.0 | 82.4 | 8 f .8 | 81.2 | 80.5 | 79.9 | 79.4 | 78.8 | 77.6 | 76.5 |
| 820 | 84.7 | 84.0 | 83.4 | 82.8 | 82.2 | 8 I .5 | 80.9 | 80.3 | 79.7 | 78.6 | 77.5 |
| 830 | 85.7 | 85.1 | 84.4 | 83.8 | 83.2 | 82.5 | 81.9 | 8 I .3 | 80.7 | 79.5 | 78.4 |
| 840 | 86.8 | 86.1 | 85.4 | 84.8 | 84.2 | 83.5 | 82.9 | 82.3 | 8 I .7 | 80.5 | 79.4 |
| 850 | 87.8 | 87.1 | 86.4 | 85.8 | 85.2 | 84.5 | 83.9 | 83.3 | 82.7 | 8 r .5 | 80.3 |
| 860 | 88.8 | 88.1 | 87.5 | 86.8 | 86.2 | 85.5 | 84.9 | 84.3 | 83.6 | 82.4 | 8 r .3 |
| 870 | 89.9 | 89.2 | 88.5 | 87.8 | 87.2 | 86.5 | 85.9 | 85.2 | 84.6 | 83.4 | 82.2 |
| 880 | 90.9 | 90.2 | 89.5 | 88.8 | 88.2 | 87.5 | 86.9 | 86.2 | 85.6 | 84.3 | 83.1 |
| 890 | 91.9 | 91.2 | 90.5 | 89.8 | 89.2 | 88.5 | 87.8 | 87.2 | 86.6 | 85.3 | 84.I |
| 900 | 93.0 | 92.2 | 91.5 | 90.8 | 90.2 | 89.5 | 88.8 | 88.2 | 87.5 | 86.3 | 85.0 |
| 910 | 94.0 | 93.3 | 92.6 | 91.9 | 91.2 | 90.5 | 89.8 | 89.2 | 88.5 | 87.2 | 86.0 |
| 920 | 95.0 | 94.3 | 93.6 | 92.9 | 92.2 | 91.5 | 90.8 | 90.1 | 89.5 | 88.2 | 86.9 |
| 930 | 96.0 | 95.3 | 94.6 | 93.9 | 93.2 | 92.5 | 91.8 | 91.1 | 90.4 | 89.1 | 87.9 |
| 940 | 97.1 | 96.3 | 95.6 | 94.9 | 94.2 | 93.5 | 92.8 | 92.1 | 91.4 | 90.1 | 88.8 |
| 950 | 98.1 | 97.4 | 96.6 | 95.9 | 95.2 | 94.5 | 93.8 | 93.1 | 92.4 | 91.1 | 89.8 |
| 960 | 99.1 | 98.4 | 97.6 | 96.9 | 96.2 | 95.5 | 94.8 | 94.I | 93.4 | 92.0 | 90.7 |
| 970 | 100.2 | 99.4 | 98.7 | 97.9 | 97.2 | 96.5 | 95.7 | 95.0 | 94.3 | 93.0 | 91.6 |
| 980 | IOI. 2 | 100.4 | 99.7 | 98.9 | 98.2 | 97.4 | 96.7 | 96.0 | 95.3 | 93.9 | 92.6 |
| 990 | 102.2 | 101.5 | 100.7 | 99.9 | 99.2 | 98.4 | 97.7 | 97.0 | 96.3 | 94.9 | 93.5 |
| 1000 | 103.3 | 102.5 | 101.7 | 100.9 | 100.2 | 99.4 | 98.7 | 98.0 | $97 \cdot 3$ | 95.9 | 94.5 |

TABLE 17.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Values of $2000 \times \mathrm{m}$.
$m=\frac{z}{18444+67.53 \theta+.003 z} \cdot \frac{1}{1-\beta}$

| Altitude in metres. 2. | MEAN TEMPERATURE O |  |  |  | AIR | MN I |  |  |  | ( $\theta$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | $-12^{\circ}$ | $-8^{\circ}$ | $-4^{\circ}$ | $-2^{\circ}$ | $0^{\circ}$ | $+2^{\circ}$ | $+4^{\circ}$ | $+6^{\circ}$ | $+8^{\circ}$ | $+10^{\circ}$ |
| 1000 | II5.I | 113.3 | III. 5 | 109.8 | 109.0 | 108.2 | 107.3 | 106.5 | 105.7 | 104.9 | 104.I |
| 1010 | II6.2 | II4.4 | I 12.7 | 110.9 | IIO. | 109.3 | 108.4 | 107.6 | 106.8 | 105.9 | 105.1 |
| 1020 | 117.4 | 115.5 | II3.8 | 112.0 | III. 2 | 110.3 | 109.5 | 108.7 | 107.8 | 107.0 | 106.2 |
| 1030 | 118.5 | 116.7 | 114.9 | II3.I | II2.3 | III. 4 | I10.6 | 109.7 | 108.9 | 108.0 | 107.2 |
| 1040 | I 19.7 | 117.8 | 116.0 | II4.2 | 113.4 | 112.5 | III. 6 | I Io. 8 | 109.9 | 109.1 | 108.2 |
| 1050 | 120.8 | II8.9 | I17.1 | 115.3 | II4.5 | II3. 6 | 112.7 | III. 8 | III.O | IIO.I | 109.3 |
| 1060 | 122.0 | 120.1 | I18.2 | 116.4 | 115.6 | 114.7 | II3.8 | II2.9 | 112.0 | III. | 110.3 |
| 1070 | 123.1 | 121.2 | 119.3 | 117.5 | 116.6 | i 15.7 | II4.9 | II4.0 | II3.I | 112.2 | 111.4 |
| 1080 | 124.3 | 122.3 | 120.5 | 118.6 | 117.7 | 116.8 | I 15.9 | 115.0 | 114.2 | 113.3 | II2.4 |
| 1090 | 125.4 | 123.5 | 121.6 | 119.7 | 118.8 | 117.9 | 117.0 | 116.1 | II5.2 | 114.3 | II3.4 |
| 1100 | 126.6 | 124.6 | 122.7 | 120.8 | 119.9 | 119.0 | 118.1 | II7.2 | II6.3 | 115.4 | 114.5 |
| IIIO | 127.7 | 125.7 | 123.8 | 121.9 | 121.0 | 120.1 | I 19.2 | II8.2 | 117.3 | 116.4 | I15.5 |
| II20 | 128.9 | 126.9 | 124.9 | 123.0 | 122.1 | 121.2 | 120.2 | 119.3 | 118.4 | 117.5 | II6.6 |
| II30 | 130.0 | 128.0 | 126.0 | I24.1 | 123.2 | 122.2 | 121.3 | 120.4 | 119.4 | I 18.5 | 117.6 |
| II40 | I31.2 | 129.1 | 127.2 | 125.2 | 124.3 | 123.3 | 122.4 | 121.4 | 120.5 | II9.6 | 118.6 |
| 1150 | 132.3 | 130.3 | 128.3 | 126.3 | 125.4 | 124.4 | 123.4 | 122.5 | 121.6 | 120.6 | 119.7 |
| 1160 | 133.5 | 131.4 | 129.4 | 127.4 | 126.4 | 125.5 | 124.5 | 123.6 | 122.6 | 121.7 | 120.7 |
| 1170 | 134.6 | 132.5 | I30.5 | 128.5 | 127.5 | I26.6 | 125.6 | 124.6 | 123.7 | 122.7 | 121.8 |
| 1180 | 135.8 | 133.7 | 131.6 | 129.6 | 128.6 | 127.6 | 126.7 | 125.7 | 124.7 | 123.8 | 122.8 |
| 1190 | I36.9 | I 34.8 | I 32.7 | I30.7 | 129.7 | 128.7 | 127.7 | 126.8 | 125.8 | 124.8 | 123.8 |
| 1200 | I38.I | 135.9 | 133.8 | 131.8 | 130.8 | 129.8 | 128.8 | 127.8 | 126.8 | 125.9 | 124.9 |
| 1210 | I 39.2 | 137.1 | 135.0 | 132.9 | 131.9 | I30.9 | 129.9 | 128.9 | 127.9 | 126.9 | 125.9 |
| 20 | 140.4 | 138.2 | I36.I | 134.0 | 133.0 | 132.0 | 131.0 | 130.0 | 129.0 | 128.0 | 127.0 |
| 1230 | 14 I .5 | 139.3 | 137.2 | I35.I | I34.I | I33.I | 132.0 | 131.0 | 130.0 | 129.0 | 128.0 |
| 1240 | 142.7 | 140.5 | 138.3 | I36.2 | I 35.2 | I34.I | 133.1 | 132.1 | I3I.I | 130.1 | 129.0 |
| 1250 | 143.8 | 14 I .6 | I39.4 | 137.3 | 136.3 | 135.2 | 134.2 | 133.I | I32.I | 131.I | I30.1 |
| 1260 | 145.0 | 142.7 | 140.5 | 138.4 | 137.3 | I36.3 | I 35.3 | I 34.2 | 133.2 | 132.1 | 131.1 |
| 1270 | I46.I | 143.9 | 141.7 | 139.5 | 138.4 | 137.4 | 136.3 | I 35.3 | I 34.2 | 133.2 | 132.2 |
| 1280 | 147.3 | 145.0 | 142.8 | 140.6 | 139.5 | 138.5 | 137.4 | 136.3 | ${ }^{1} 35.3$ | 134.2 | 133.2 |
| 1290 | 148.4 | 146.1 | 143.9 | 141.7 | 140.6 | 139.5 | I38.5 | 137.4 | I36.3 | 135.3 | I 34.2 |
| 1300 | 149.6 | 147.3 | 145.0 | 142.8 | 141.7 | 140.6 | 139.5 | 138.5 | 137.4 | I36.3 | 135.3 |
| 1310 | 150.7 | 148.4 | 146.1 | 143.9 | 142.8 | 141.7 | 140.6 | 139.5 | 138.5 | 137.4 | 136.3 |
| I320 | 151.9 | 149.5 | 147.2 | 145.0 | 143.9 | 142.8 | 141.7 | 140.6 | 139.5 | 138.4 | 137.4 |
| 1330 | 153.0 | 150.7 | 148.3 | I46.1 | 145.0 | 143.9 | 142.8 | 141.7 | 140.6 | I 39.5 | 138.4 |
| I 340 | I54.2 | ${ }^{1} 51.8$ | 149.5 | 147.2 | 146.I | 145.0 | 143.8 | 142.7 | 141.6 | 140.5 | I 39.5 |
| 1350 | 155.3 | 152.9 | 150.6 | 148.3 | 147.2 | 146.0 | 144.9 | 143.8 | 142.7 | 141.6 | 140.5 |
| I360 | 156.5 | I54.I | 151.7 | 149.4 | 148.2 | 147.1 | 146.0 | 144.9 | 143.7 | 142.6 | 141.5 |
| I370 | I 57.6 | I55.2 | 152.8 | 150.5 | 149.3 | 148.2 | 147.1 | 145.9 | 144.8 | 143.7 | 142.6 |
| 1380 | 158.8 | 156.3 | 153.9 | 151.6 | 150.4 | 149.3 | 148.1 | 147.0 | 145.9 | 144.7 | 143.6 |
| 1390 | 159.9 | ${ }^{1} 57.5$ | 155.0 | 152.7 | 151.5 | 150.4 | 149.2 | 148.I | 146.9 | 145.8 | 144.7 |
| 1400 | 16I.I | 158.6 | 156.2 | 153.8 | 152.6 | 151.4 | 150.3 | 149.1 | 148.0 | 146.8 | 145.7 |
| 1410 | 162.2 | 159.7 | 157.3 | 154.9 | 153.7 | 152.5 | ${ }^{1} 51.4$ | 150.2 | 149.0 | 147.9 | 146.7 |
| 1420 | 163.4 | 160.8 | 158.4 | 156.0 | 154.8 | I 53.6 | 152.4 | 151.3 | 150.1 | 148.9 | 147.8 |
| 1430 | 164.5 | 162.0 | 159.5 | 157.1 | 155.9 | 154.7 | 153.5 | 152.3 | I5I.I | 150.0 | 148.8 |
| 1440 | 165.7 | 163.1 | 160.6 | 158.2 | 157.0 | 155.8 | 154.6 | 153.4 | 152.2 | 151.0 | 149.9 |
| 1450 | ı66.8 | 164.2 | 161.7 | 159.3 | 158.1 | 156.8 | ${ }^{1} 55.7$ | 154.5 | 153.3 | 152.1 | 150.9 |
| 1460 | 168.0 | 165.4 | 162.8 | 160.4 | 159.1 | 157.9 | 156.7 | 155.5 | 154.3 | 153.1 | 151.9 |
| 1470 | 169.1 | 166.5 | 164.0 | 161.5 | 160.2 | 159.0 | 157.8 | ${ }^{1} 56.6$ | 155.4 | 154.2 | 153.0 |
| 1480 | 170.3 | 167.6 | 165.I | 162.6 | 161.3 | 160.1 | 158.9 | 157.6 | 156.4 | 155.2 | 154.0 |
| 1490 | 171.4 | 168.8 | 166.2 | 163.7 | 162.4 | 161.2 | 159.9 | 158.7 | 157.5 | 156.3 | ${ }^{1} 55.1$ |
| 1500 | 172.6 | 169.9 | 167.3 | 164.8 | 163.5 | I62.3 | 161.0 | I59.8 | 158.5 | 157.3 | ${ }^{1} 56.1$ |

TAble 17.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Values of $2000 \times \mathrm{m}$.
$m=\frac{z}{18444+6753 \theta+.003 z} \cdot \frac{I}{I-\beta}$

| Altitude in metres. 2. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $+12^{\circ}$ | $+14^{\circ}$ | $+16^{\circ}$ | $+18^{\circ}$ | $+20^{\circ}$ | $+22^{\circ}$ | $+24^{\circ}$ | $+26^{\circ}$ | $+28^{\circ}$ | $+32^{\circ}$ | $+36^{\circ}$ |
| 1000 | 103.3 | 102.5 | 101.7 | 100.9 | 100.2 | 99.4 | 98.7 | 98.0 | 97.3 | 95.9 | 94.5 |
| 1010 | 104.3 | 103.5 | 102.7 | IOI. 9 | IOI | 100.4 | 99.7 | 99.0 | 98.2 | 96.8 | 95.4 |
| 1020 | 105.3 | 104.5 | 103.7 | 103.0 | 102.2 | IOI. 4 | 100.7 | 99.9 | 99.2 | 97.8 | 96.4 |
| 1030 | 106.4 | 105.6 | 104.8 | 104.0 | 103.2 | 102.4 | 101.7 | 100.9 | 100.2 | 98.7 | 97.3 |
| 1040 | 107.4 | 106.6 | 105.8 | 105.0 | 104.2 | 103.4 | 102.6 | 101.9 | IOI.I | 99.7 | 98.3 |
| 1050 | Io8.4 | 107.6 | 106.8 | 106.0 | 105.2 | 104.4 | 103.6 | 102.9 | IO2.I | 100.6 | 99.2 |
| 1060 | 109.5 | 108.6 | 107.8 | 107.0 | 106.2 | 105.4 | 104.6 | 103.9 | 103.1 | 101. 6 | 100.1 |
| 1070 | 110.5 | 109.7 | 108.8 | 108.0 | 107.2 | 106.4 | 105.6 | 104.8 | 104.1 | 102.6 | IOI.I |
| 10So | III. 5 | 110.7 | 109.8 | 109.0 | 108.2 | 107.4 | 106.6 | 105.8 | 105.0 | 103.5 | 102.0 |
| Iogo | II2.6 | III 1.7 | 110.9 | I 10.0 | 109.2 | 108.4 | 107.6 | 106.8 | 106.0 | 104.5 | 103.0 |
| 1100 | II3.6 | 112.7 | II I. 9 | III.O | I 10.2 | 109.4 | I08.6 | 107.8 | 107.0 | 105.4 | 103.9 |
| I 110 | 114.6 | 113.8 | 112.9 | I 12.0 | III. 2 | I 10.4 | 109.6 | 108.8 | 108.0 | 106.4 | 104.9 |
| II 20 | I 15.7 | 114.8 | 113.9 | 113.1 | II2.2 | III. 4 | 110.5 | 109.7 | 108.9 | 107.4 | 105.8 |
| 1130 | 116.7 | II 5.8 | 114.9 | II4.1 | II 3.2 | I 12.4 | III. 5 | I I 0.7 | 109.9 | 108.3 | 106.8 |
| I 140 | II 7.7 | 116.8 | II5.9 | II5.1 | I 14.2 | II 3.4 | II 2.5 | III. 7 | 110.9 | 109.3 | 107.7 |
| 1150 | II8.8 | 117.9 | 117.0 | I16.1 | II 5.2 | II4.4 | II3.5 | II2.7 | I 11.8 | 110.2 | 108.6 |
| 1160 | 119.8 | II8.9 | 118.0 | 117.1 | II6.2 | 115.3 | 114.5 | II3.6 | 112.8 | III. 2 | 109.6 |
| 1170 | 120.8 | 119.9 | 119.0 | 118.1 | I 77.2 | 116.3 | II 5.5 | 114.6 | 113.8 | II2.I | 110.5 |
| I 180 | 121.9 | 120.9 | 120.0 | II9.I | I 18.2 | 117.3 | II6.5 | II5.6 | 114.8 | II3.I | III. 5 |
| 1190 | 122.9 | 122.0 | 12 I .0 | 120.1 | I 19.2 | II8.3 | I 17.4 | II6.6 | 115.7 | II4.I | 112.4 |
| 1200 | 123.9 | 123.0 | 122.0 | 12I.I | 120.2 | 119.3 | I 18.4 | 117.6 | 116.7 | I 15.0 | 113.4 |
| 1210 | 125.0 | 124.0 | 123.1 | 122.1 | 121.2 | 120.3 | II9.4 | 118.5 | 117.7 | 116.0 | 114.3 |
| 1220 | 126.0 | 125.0 | 124.I | 123.1 | 122.2 | 121.3 | 120.4 | 119.5 | 118.6 | 116.9 | 115.3 |
| 1230 | 127.0 | I26.I | 125.I | 124.2 | 123.2 | 122.3 | I2 2.4 | 120.5 | 119.6 | 117.9 | 116.2 |
| 1240 | I28.1 | I27.1 | 126.1 | 125.2 | 124.2 | 123.3 | I22.4 | 121.5 | 120.6 | II8.9 | 117.2 |
| 1250 | 129.1 | 128.1 | 127.1 | 126.2 | 125.2 | 124.3 | 123.4 | 122.5 | 121.6 | 119.8 | II8.1 |
| 1260 | 130.1 | 129.1 | 128.1 | 127.2 | I 26.2 | 125.3 | 124.4 | 123.4 | 122.5 | 120.8 | 119.0 |
| 1270 | I3I. 2 | I30.2 | 129.2 | 128.2 | 127.2 | 126.3 | 125.3 | 124.4 | 123.5 | 121.7 | 120.0 |
| 1280 | 132.2 | 131.2 | 130.2 | 129.2 | 128.2 | 127.3 | 126.3 | 125.4 | 124.5 | 122.7 | 120.9 |
| 1290 | 133.2 | 132.2 | 131.2 | 130.2 | 129.2 | 128.3 | 127.3 | 126.4 | 125.5 | 123.6 | 121.9 |
| 1300 | I 34.3 | 133.2 | I32.2 | 131.2 | I30.2 | 129.3 | 128.3 | 127.4 | 126.4 | 124.6 | 122.8 |
| 1310 | 135.3 | I 34.3 | 133.2 | 132.2 | I31.2 | I30.3 | 129.3 | 128.3 | 127.4 | 125.6 | 123.8 |
| 1320 | 136.3 | 135.3 | 134.2 | 133.2 | 132.2 | 131.3 | I30.3 | 129.3 | 128.4 | 126.5 | 124.7 |
| 1330 | 137.4 | 136.3 | 135.3 | I 34.2 | 133.2 | 132.2 | 131.3 | 130.3 | 129.3 | 127.5 | 125.7 |
| I 340 | I 38.4 | 137.3 | I36.3 | 135.3 | I 34.2 | 133.2 | 132.2 | I3I. 3 | I30.3 | 128.4 | 126.6 |
| 1350 | 139.4 | I38.4 | 137.3 | 136.3 | I 35.2 | I34.2 | 133.2 | 132.3 | 131.3 | 129.4 | 127.5 |
| 1360 | 140.5 | I 39.4 | 138.3 | 137.3 | 136.2 | 135.2 | I 34.2 | 133.2 | 132.3 | 130.3 | 128.5 |
| 1370 | 141.5 | 140.4 | 139.3 | 138.3 | 137.2 | 136.2 | I35.2 | I 34.2 | 133.2 | 131.3 | 129.4 |
| I 380 | 142.5 | 141.4 | 140.3 | 139.3 | 138.2 | 137.2 | I 36.2 | 135.2 | I 34.2 | 132.3 | 130.4 |
| 1390 | 143.5 | 142.4 | 141.4 | 140.3 | I 39.2 | 138.2 | 137.2 | I 36.2 | 135.2 | 133.2 | 131.3 |
| 1400 | 144.6 | 143.5 | 142.4 | I41. 3 | 140.2 | 139.2 | I38.2 | 137.2 | I36.2 | I34.2 | 132.3 |
| I410 | 145.6 | 144.5 | 143.4 | 142.3 | 141.3 | 140.2 | 139.2 | 138.1 | 137.1 | I 35.1 | I 33.2 |
| 1420 | 146.6 | 145.5 | 144.4 | 143.3 | 142.3 | 141.2 | 140.I | 139.1 | 138.1 | I36.1 | 134.2 |
| 1430 | 147.7 | 146.5 | 145.4 | 144.3 | 143.3 | 142.2 | 14 I .1 | 140.1 | 139.1 | 137.1 | 135.1 |
| 1440 | 148.7 | 147.6 | 146.4 | 145.3 | I44.3 | 143.2 | 142.I | 14 I .1 | 140.0 | I38.0 | I36.0 |
| 1450 | 149.7 | 148.6 | 147.5 | 146.4 | 145.3 | 144.2 | 143.1 | 142.1 | 141.0 | I39.0 | 137.0 |
| 1460 | 150.8 | I 49.6 | 148.5 | 147.4 | 146.3 | 145.2 | 144.I | 143.0 | 142.0 | I 39.9 | I 37.9 |
| 1470 | 151.8 | 150.6 | 149.5 | 148.4 | 147.3 | 146.2 | I45.I | 144.0 | 143.0 | 140.9 | I 38.9 |
| 1480 | 152.8 | 151.7 | 150.5 | 149.4 | 148.3 | 147.2 | I46.I | 145.0 | 143.9 | I4I. 8 | 139.8 |
| 1490 | 153.9 | 152.7 | 151.5 | 150.4 | 149.3 | 148.2 | 147.1 | 146.0 | 144.9 | 142.8 | 140.8 |
| 1500 | I54.9 | 153.7 | 152.5 | 151.4 | 150.3 | 149.I | I48.0 | 147.0 | 145.9 | 143.8 | 141.7 |

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC, MEASURES.

$V$ alues of $2000 \times \mathrm{m}$.

$$
m=\frac{Z}{18444+67.53 \theta+.003 z} \cdot \frac{\mathrm{I}}{\mathrm{I}-\beta}
$$

| Altitude in metres. Z. | MEAN TEMPERATURE OF AIR COLUMN IN CENTIGRADE DEGREES ( $\boldsymbol{\theta}$ ) . |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | $-12^{\circ}$ | $-8^{\circ}$ | $-4^{\circ}$ | $-2^{\circ}$ | $0^{\circ}$ | $+2^{\circ}$ | $+4^{\circ}$ | $+6^{\circ}$ | $+8^{\circ}$ | $+10^{\circ}$ |
| 1500 | 172.6 | 169.9 | 167.3 | 164.8 | 163.5 | 162.3 | 161.0 | 159.8 | I 58.5 | 157.3 | 156.1 |
| 1510 | 173.7 | 171.0 | 168.4 | 165.9 | 164.6 | 163.3 | 162.1 | 160.8 | I 59.6 | I58.4 | 157.1 |
| 1520 | 174.9 | 172.2 | 169.5 | 167.0 | 165.7 | 164.4 | 163.2 | 161.9 | 160.7 | I 59.4 | 158.2 |
| 1530 | I76.0 | 173.3 | 170.7 | 168.1 | 166.8 | 165.5 | 164.2 | 163.0 | 161.7 | 160.5 | 159.2 |
| 1540 | 177.2 | 174.4 | 171.8 | 169.1 | 167.9 | 166.6 | 165.3 | 164.0 | 162.8 | 161.5 | 160.3 |
| 1550 | 178.3 | 175.6 | 172.9 | 170.2 | 169.0 | 167.7 | 166.4 | 165.1 | 163.8 | 162.6 | 161.3 |
| 1560 | 179.5 | 176.7 | 174.0 | 171.3 | 170.0 | 168.7 | 167.5 | 166.2 | 164.9 | 163.6 | 162.3 |
| 1570 | 180.6 | 177.8 | 175.1 | 172.4 | 171.1 | 169.8 | 168.5 | 167.2 | 165.9 | 164.7 | 163.4 |
| 1580 | 181. 8 | 179.0 | 176.2 | 173.5 | 172.2 | 170.9 | 169.6 | 168.3 | 167.0 | 165.7 | 164.4 |
| I590 | 182.9 | 180.1 | 177.3 | I 74.6 | I73.3 | 172.0 | 170.7 | 169.4 | 168.1 | 166.8 | 165.5 |
| 1600 | 184.I | I8I. 2 | I78.5 | I75.7 | 174.4 | 173.1 | 171.7 | 170.4 | 169.1 | 167.8 | 166.5 |
| 1610 | 185.2 | 182.4 | 179.6 | 176.8 | 175.5 | 174.2 | 172.8 | 171.5 | 170.2 | 168.9 | 167.5 |
| 1620 | 186.4 | 183.5 | 180.7 | 177.9 | 176.6 | 175.2 | 173.9 | 172.6 | 171.2 | 169.9 | 168.6 |
| 1630 | 187.5 | 184.6 | 181.8 | 179.0 | 177.7 | 176.3 | 175.0 | 173.6 | 172.3 | 170.9 | 169.6 |
| 1640 | 188.7 | 185.8 | 182.9 | 180.1 | 178.8 | 177.4 | 176.0 | 174.7 | 173.3 | 172.0 | 170.7 |
| 1650 | 189.8 | 186.9 | 184.0 | 181.2 | 179.8 | 178.5 | 177.1 | 175.7 | 174.4 | 173.0 | 171.7 |
| 1660 | 191.0 | 188.0 | 185.1 | 182.3 | 180.9 | 179.6 | 178.2 | 176.8 | 175.4 | I74.I | 172.7 |
| 1670 | 192.2 | 189.2 | 186.3 | 183.4 | 182.0 | 180.6 | 179.3 | 177.9 | 176.5 | 175.I | 173.8 |
| 1680 | 193.3 | 190.3 | 187.4 | 184.5 | 183.1 | 181.7 | 180.3 | 178.9 | 177.6 | 176.2 | 174.8 |
| 1690 | 194.5 | 191.4 | 188.5 | 185.6 | 184.2 | 182.8 | 181.4 | 180.0 | 178.6 | I77.2 | 175.9 |
| 1700 | 195.6 | 192.6 | 189.6 | 186.7 | 185.3 | 183.9 | 182.5 | 181.I | 179.7 | 178.3 | 176.9 |
| 1710 | 196.8 | 193.7 | 190.7 | 187.8 | 186.4 | 185.0 | 183.5 | 182.1 | 180.7 | 179.3 | 177.9 |
| 1720 | 197.9 | 194.8 | 191.8 | 188.9 | 187.5 | I86.0 | 184.6 | 183.2 | 181.8 | 180.4 | 179.0 |
| 1730 | 199.1 | 196.0 | 193.0 | 190.0 | 188.6 | 187.1 | 185.7 | 184.3 | 182.8 | 181.4 | 180.0 |
| 1740 | 200.2 | I97.I | 194.I | 191.I | 189.7 | I88.2 | I86.8 | 185.3 | 183.9 | 182.5 | I81.1 |
| 1750 | 201.4 | 198.2 | 195.2 | 192.2 | 190.7 | 189.3 | 187.8 | 186.4 | I85.0 | 183.5 | 182.1 |
| 1760 | 202.5 | 199.3 | 196.3 | 193.3 | 191.8 | 190.4 | 188.9 | 187.5 | 186.0 | 184.6 | 183.1 |
| 1770 | 203.7 | 200.5 | 197.4 | 194.4 | 192.9 | 191.5 | 190.0 | 188.5 | 187.1 | I85.6 | 184.2 |
| 1780 | 204.8 | 201.6 | 198.5 | 195.5 | 194.0 | 192.5 | 191.1 | 189.6 | 188.1 | 186.7 | 185.2 |
| 1790 | 206.0 | 202.7 | 199.6 | 196.6 | 195.I | 193.6 | 192.I | 190.7 | I89.2 | I87.7 | 186.3 |
| 1800 | 207.1 | 203.9 | 200.8 | 197.7 | 196.2 | 194.7 | 193.2 | 191.7 | 190.2 | 188.8 | 187.3 |
| 1810 | 208.3 | 205.0 | 201.9 | 198.8 | 197.3 | 195.8 | 194.3 | 192.8 | 191. 3 | 189.8 | 188.3 |
| 1820 | 209.4 | 206.1 | 203.0 | 199.9 | 198.4 | 196.9 | 195.3 | 193.8 | 192.4 | 190.9 | I89.4 |
| 1830 | 210.6 | 207.3 | 204.1 | 201.0 | 199.5 | 197.9 | 196.4 | 194.9 | 193.4 | 191. 9 | 190.4 |
| 1840 | 211.7 | 208.4 | 205.2 | 202.1 | 200.6 | 199.0 | 197.5 | 196.0 | 194.5 | 193.0 | 191.5 |
| 1850 | 212.9 | 209.5 | 206.3 | 203.2 | 201.6 | 200.1 | 198.6 | 197.0 | 195.5 | 194.0 | 192.5 |
| 1860 | 214.0 | 210.7 | 207.4 | 204.3 | 202.7 | 201.2 | 199.6 | 198.1 | 196.6 | 195.I | 193.6 |
| 1870 | 215.2 | 211.8 | 208.6 | 205.4 | 203.8 | 202.3 | 200.7 | 199.2 | 197.6 | 196.1 | 194.6 |
| 1880 | 216.3 | 212.9 | 209.7 | 206.5 | 204.9 | 203.3 | 201.8 | 200.2 | 198.7 | 197.2 | 195.6 |
| 1890 | 217.5 | 214.1 | 210.8 | 207.6 | 206.0 | 204.4 | 202.9 | 201.3 | 199.7 | 198.2 | 196.7 |
| 1900 | 218.6 | 215.2 | 211.9 | 208.7 | 207.1 | 205.5 | 203.9 | 202.4 | 200.8 | 199.3 | 197.7 |
| 1910 | 219.8 | 216.3 | 213.0 | 209.8 | 208.2 | 206.6 | 205.0 | 203.4 | 201.9 | 200.3 | 198.8 |
| 1920 | 220.9 | 217.5 | 214.1 | 210.9 | 209.3 | 207.7 | 206.1 | 204.5 | 202.9 | 201.3 | 199.8 |
| 1930 | 222.1 | 218.6 | 215.2 | 212.0 | 210.4 | 208.8 | 207.2 | 205.6 | 204.0 | 202.4 | 200.8 |
| 1940 | 223.2 | 219.7 | 216.4 | 213.1 | 211.4 | 209.8 | 208.2 | 206.6 | 205.0 | 203.4 | 201.9 |
| 1950 | 224.4 | 220.9 | 217.5 | 214.2 | 212.5 | 210.9 | 209.3 | 207.7 | 206.1 | 204.5 | 202.9 |
| 1960 | 225.5 | 222.0 | 218.6 | 215.3 | 213.6 | 212.0 | 210.4 | 208.8 | 207.1 | 205.5 | 204.0 |
| 1970 | 226.7 | 223.1 | 219.7 | 216.4 | 214.7 | 213.1 | 211.4 | 209.8 | 208.2 | 206.6 | 205.0 |
| 1980 | 227.8 | 224.3 | 220.8 | 217.5 | 215.8 | 214.2 | 212.5 | 210.9 | 209.3 | 207.6 | 206.0 |
| 1990 | 229.0 | 225.4 | 221.9 | 218.6 | 216.9 | 215.2 | 213.6 | 211.9 | 210.3 | 208.7 | 207.1 |
| 2000 | 230.1 | 226.5 | 223.0 | 219.7 | 218.0 | 216.3 | 214.7 | 213.0 | 211.4 | 209.7 | 208.1 |

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.



## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Values of $2000 \times \mathbf{m}$.

$$
m=\frac{z}{18444+67.53 \theta+.003 Z} \cdot \frac{I}{1-\beta}
$$

| Altitude in metres. $Z$. | MEAN TEMPERATURE O |  |  |  | c | COLUMN IN C |  | NTIGRADE DE |  | GREES ( $\boldsymbol{\theta}$ ). |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | $-12^{\circ}$ | $-8^{\circ}$ | $-4^{\circ}$ | $-2^{\circ}$ | $0^{\circ}$ | $+2^{\circ}$ | $+4^{\circ}$ | $+6^{\circ}$ | $+8^{\circ}$ | $+10^{\circ}$ |
| 2000 | 230.1 | 226.5 | 223.0 | 219.7 | 218.0 | 216.3 | 214.7 | 213.0 | 211.4 | 209.7 | 208. 1 |
| IO | 231.3 | 227.7 | 224.2 | 220.8 | 219.1 | 217.4 | 215.7 | 214.1 | 212.4 | 210.8 | 209.2 |
| 2 | 232.4 | 228.8 | 225.3 | 221.9 | 220.2 | 218.5 | 216.8 | 215.1 | 213.5 | 211.8 | 210.2 |
| 2030 | 233.6 | 229.9 | 226.4 | 223.0 | 221.3 | 219.6 | 217.9 | 216.2 | 214.5 | 212.9 | 211.2 |
| 2040 | 234.7 | 231.1 | 227.5 | 224.0 | 222.3 | 220.6 | 219.0 | 217.3 | 215.6 | 213.9 | 212.3 |
| 2050 | 235.9 | 232.2 | 228.6 | 225.1 | 223.4 | 221.7 | 220.0 | 218.3 | 216.7 | 215.0 | 213.3 |
| 2060 | 237.0 | 233.3 | 229.7 | 226.2 | 224.5 | 222.8 | 22I.1 | 219.4 | 217.7 | 216.0 | 214.4 |
| 2070 | 238.2 | 234.4 | 230.9 | 227.3 | 225.6 | 223.9 | 222.2 | 220.5 | 218.8 | 217.1 | 215.4 |
| 2080 | 239.3 | 235.6 | 232.0 | 228.4 | 226.7 | 225.0 | 223.2 | 221.5 | 219.8 | 218.1 | 216.4 |
| 2090 | 240.5 | 236.7 | 233.1 | 229.5 | 227.8 | 22.6.1 | 224.3 | 222.6 | 220.9 | 219.2 | 217.5 |
| 2100 | 241.6 | 237.8 | 234.2 | 230.6 | 228.9 | 227.1 | 225.4 | 223.7 | 221.9 | 220.2 | 218.5 |
| 2110 | 242.8 | 239.0 | 235.3 | 231.7 | 230.0 | 228.2 | 226.5 | 224.7 | 223.0 | 221.3 | 219.6 |
| 2120 | 243.9 | 240.1 | 236.4 | 232.8 | 231.1 | 229.3 | 227.5 | 225.8 | 224.0 | 222.3 | 220.6 |
| 2130 | 245.I | 241.2 | 237.5 | 233.9 | 232.2 | 230.4 | 228.6 | 226.9 | 225.1 | 223.4 | 221.6 |
| 2140 | 246.2 | 242.4 | 238.7 | 235.0 | 233.2 | 231.5 | 229.7 | 227.9 | 226.2 | 224.4 | 222.7 |
| 2150 | 247.4 | 243.5 | 239.8 | 236.1 | 234.3 | 232.5 | 230.8 | 229.0 | 227.2 | 225.5 | 223.7 |
| 2160 | 248.5 | 244.6 | 240.9 | 237.2 | 235.4 | 233.6 | 231.8 | 230.0 | 228.3 | 226.5 | 224.8 |
| 2170 | 249.7 | 245.8 | 242.0 | 238.3 | 236.5 | 234.7 | 232.9 | 231.1 | 229.3 | 227.6 | 225.8 |
| 2180 | 250.8 | 246.9 | 243.1 | 239.4 | 237.6 | 235.8 | 234.0 | 232.2 | 230.4 | 228.6 | 226.8 |
| 2190 | 252.0 | 248.0 | 244.2 | 240.5 | 238.7 | 236.9 | 235.I | 233.2 | 231.4 | 229.7 | 227.9 |
| 2200 | 253.1 | 249.2 | 245.4 | 241.6 | 239.8 | 237.9 | 236.1 | 234.3 | 232.5 | 230.7 | 228.9 |
| 2210 | 254.3 | 250.3 | 246.5 | 242.7 | 240.9 | 239.0 | 237.2 | 235.4 | 233.6 | 231.7 | 230.0 |
| 2220 | 255.4 | 251.4 | 247.6 | 243.8 | 242.0 | 240.1 | 238.3 | 236.4 | 234.6 | 232.8 | 231.0 |
| 2230 | 256.6 | 252.6 | 248.7 | 244.9 | 243.0 | 241.2 | 239.3 | 237.5 | 235.7 | 233.8 | 232.0 |
| 2240 | 257.7 | 253.7 | 249.8 | 246.0 | 244.I | 242.3 | 240.4 | 238.6 | 236.7 | 234.9 | 233.1 |
| 2250 | 258.9 | 254.8 | 250.9 | 247.1 | 245.2 | 243.4 | 241.5 | 239.6 | 237.8 | 235.9 | 234.1 |
| 2260 | 260.0 | 256.0 | 252.0 | 248.2 | 246.3 | 244.4 | 242.6 | 240.7 | 238.8 | 237.0 | 235.2 |
| 2270 | 261.2 | 257.1 | 253.2 | 249.3 | 247.4 | 245.5 | 243.6 | 241.8 | 239.9 | 238.0 | 236.2 |
| 2280 | 262.3 | 258.2 | 254.3 | 250.4 | 248.5 | 246.6 | 244.7 | 242.8 | 241.0 | 239.I | 237.2 |
| 2290 | 263.5 | 259.4 | 255.4 | 251.5 | 249.6 | 247.7 | 245.8 | 243.9 | 242.0 | 240.I | 238.3 |
| 2300 | 264.6 | 260.5 | 256.5 | 252.6 | 250.7 | 248.8 | 246.9 | 245.0 | 243.1 | 241.2 | 239.3 |
| 2310 | 265.8 | 261.6 | 257.6 | 253.7 | 251.8 | 249.8 | 247.9 | 246.0 | 244.I | 242.2 | 240.4 |
| 2320 | 266.9 | 262.8 | 258.7 | 254.8 | 252.9 | 250.9 | 249.0 | 247.1 | 245.2 | $243 \cdot 3$ | 24 I .4 |
| 2330 | 268.1 | 263.9 | 259.8 | 255.9 | 253.9 | 252.0 | 250.1 | 248.1 | 246.2 | 244.3 | 242.4 |
| 2340 | 269.2 | 265.0 | 261.0 | 257.0 | 255.0 | 253.1 | 251.1 | 249.2 | 247.3 | 245.4 | 243.5 |
| 2350 | 270.4 | 266.1 | 262.1 | 258.1 | 256.1 | 254.2 | 252.2 | 250.3 | 248.3 | 246.4 | 244.5 |
| 2360 | 271.5 | 267.3 | 263.2 | 259.2 | 257.2 | 255.2 | 253.3 | 251.3 | 249.4 | 247.5 | 245.6 |
| 2370 | 272.7 | 268.4 | 264.3 | 260.3 | 258.3 | 256.3 | 254.4 | 252.4 | 250.5 | 248.5 | 246.6 |
| 2380 | 273.8 | 269.5 | 265.4 | 261.4 | 259.4 | 257.4 | 255.4 | 253.5 | 251.5 | 249.6 | 247.6 |
| 2390 | 275.0 | 270.7 | 266.5 | 262.5 | 260.5 | 258.5 | 256.5 | 254.5 | 252.6 | 250.6 | 248.7 |
| 2400 | 276.1 | 271.8 | 267.7 | 263.6 | 261.6 | 259.6 | 257.6 | 255.6 | 253.6 | 251.7 | 249.7 |
| 2410 | 277.3 | 272.9 | 268.8 | 264.7 | 262.7 | 260.7 | 258.7 | 256.7 | 254.7 | 252.7 | 250.8 |
| 2420 | 278.4 | 274.I | 269.9 | 265.8 | 263.7 | 261.7 | 259.7 | 257.7 | 255.7 | 253.8 | 251.8 |
| 2430 | 279.6 | 275.2 | 271.0 | 266.9 | 264.8 | 262.8 | 260.8 | 258.8 | 256.8 | 254.8 | 252.8 |
| 2440 | 280.7 | 276.3 | 272.1 | 268.0 | 265.9 | 263.9 | 261.9 | 259.9 | 257.9 | 255.9 | 253.9 |
| 2450 | 281.9 | 277.5 | 273.2 | 269.1 | 267.0 | 265.0 | 262.9 | 260.9 | 258.9 | 256.9 | 254.9 |
| 2460 | 283.0 | 278.6 | 274.3 | 270.2 | 268.1 | 266.1 | 264.0 | 262.0 | 260.0 | 258.0 | 256.0 |
| 2470 | 284.2 | 279.7 | 275.5 | 271.3 | 269.2 | 267.1 | 265.1 | 263.1 | 26 I .0 | 259.0 | 257.0 |
| 2480 | 285.3 | 280.9 | 276.6 | 272.4 | 270.3 | 268.2 | 266.2 | 264.1 | 262.1 | 260.1 | 258.0 |
| 2490 | 286.5 | 282.0 | 277.7 | 273.5 | 271.4 | 269.3 | 267.2 | 265.2 | 263.1 | 261. 1 | 259.1 |
| 2500 | 287.6 | 283.I | 278.8 | 274.5 | 272.5 | 270.4 | 268.3 | 266.2 | 264.2 | 262.2 | 260.1 |

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES. <br> Values of $2000 \times \mathrm{m}$. <br> $m=\frac{z}{18444+67.53 \theta+.003 z} \cdot \frac{1}{1-\beta}$

| Altitude in metres. $Z$. | MEAN TEMPERATURE O |  |  |  | AIR | OLU | IN C |  |  | REE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $+12^{\circ}$ | $+14^{\circ}$ | $+16^{\circ}$ | $+18^{\circ}$ | $+20^{\circ}$ | $+22^{\circ}$ | $+24^{\circ}$ | $+26^{\circ}$ | $+28^{\circ}$ | $+32^{\circ}$ | $+36^{\circ}$ |
| 2000 | 206.5 | 204.9 | 203.4 | 201.9 | 200.3 | 198.8 | 197.4 | 195.9 | 194.5 | 191.7 | 188.9 |
| 2 | 207.6 | 206.0 | 204.4 | 202.9 | 201.3 | 199.8 | 198.4 | 196.9 | 195.5 | 192.6 | I89.9 |
| 2020 | 208.6 | 207.0 | 205.4 | 203.9 | 202.3 | 200.8 | 199.3 | 197.9 | 196.4 | 193.6 | 190.8 |
| 2030 | 209.6 | 208.0 | 206.4 | 204.9 | 203.3 | 201.8 | 200.3 | 198.8 | 197.4 | 194.6 | 191.8 |
| 2040 | 210.7 | 209.0 | 207.5 | 205.9 | 204.3 | 202.8 | 201.3 | 199.8 | 198.4 | 195.5 | 192.7 |
| 2050 | 2 II. 7 | 210.1 | 208.5 | 206.9 | 205.3 | 203.8 | 202.3 | 200.8 | 199.3 | 196.5 | 193.7 |
| 2060 | 212.7 | 2II.I | 209.5 | 207.9 | 206.3 | 204.8 | 203.3 | 201.8 | 200.3 | 197.4 | 194.6 |
| 2070 | 213.8 | 212.1 | 210.5 | 208.9 | 207.3 | 205.8 | 204.3 | 202.8 | 201.3 | 198.4 | 195.5 |
| 2080 | 214.8 | 213.1 | 211.5 | 209.9 | 208.3 | 206.8 | 205.3 | 203.7 | 202.3 | 199.3 | 196.5 |
| 2090 | 215.8 | 214.2 | 212.5 | 210.9 | 209.3 | 207.8 | 206.3 | 204.7 | 203.2 | 200.3 | 197.4 |
| 2100 | 216.8 | 215.2 | 213.5 | 211.9 | 210.4 | 208.8 | 207.2 | 205.7 | 204.2 | 201.3 | 198.4 |
| 2110 | 217.9 | 216.2 | 214.6 | 213.0 | 2II. 4 | 209.8 | 208.2 | 206.7 | 205.2 | 202.2 | 199.3 |
| 2120 | 218.9 | 217.2 | 215.6 | 214.0 | 212.4 | 210.8 | 209.2 | 207.7 | 206.2 | 203.2 | 200.3 |
| 2130 | 219.9 | 218.3 | 216.6 | 215.0 | 213.4 | 211.8 | 210.2 | 208.6 | 207.1 | 204.1 | 201.2 |
| 2140 | 221.0 | 219.3 | 217.6 | 216.0 | 214.4 | 212.8 | 211.2 | 209.6 | 208.1 | 205.1 | 202.2 |
| 2150 | 222.0 | 220.3 | 218.6 | 217.0 | 215.4 | 213.8 | 212.2 | 210.6 | 209.1 | 206.1 | 203.1 |
| 2160 | 223.0 | 221.3 | 219.6 | 218.0 | 216.4 | 214.7 | 213.2 | 211.6 | 210.0 | 207.0 | 204.0 |
| 2170 | 224.I | 222.4 | 220.7 | 219.0 | 217.4 | 215.7 | 214.1 | 212.6 | 211.0 | 208.0 | 205.0 |
| 2180 | 225.1 | 223.4 | 221.7 | 220.0 | 218.4 | 216.7 | 215.1 | 213.5 | 212.0 | 208.9 | 205.9 |
| 2190 | 226.I | 224.4 | 222.7 | 221.0 | 219.4 | 217.7 | 216.1 | 214.5 | 213.0 | 209.9 | 206.9 |
| 2200 | 227.2 | 225.4 | 223.7 | 222.0 | 220.4 | 218.7 | 217.1 | 215.5 | 213.9 | 210.8 | 207.8 |
| 2210 | 228.2 | 226.5 | 224.7 | 223.0 | 221.4 | 219.7 | 218.1 | 216.5 | 214.9 | 211.8 | 208.8 |
| 2220 | 229.2 | 227.5 | 225.7 | 224.0 | 222.4 | 220.7 | 219.1 | 217.5 | 215.9 | 212.8 | 209.7 |
| 2230 | 230.3 | 228.5 | 226.8 | 225.1 | 223.4 | 221.7 | 220.1 | 218.4 | 216.8 | 213.7 | 210.7 |
| 2240 | 231.3 | 229.5 | 227.8 | 226.1 | 224.4 | 222.7 | 221.0 | 219.4 | 217.8 | 214.7 | 211.6 |
| 2250 | 232.3 | 230.6 | 228.8 | 227.1 | 225.4 | 223.7 | 222.0 | 220.4 | 218.8 | 215.6 | 212.5 |
| 2260 | 233.4 | 231.6 | 229.8 | 228.1 | 226.4 | 224.7 | 223.0 | 221.4 | 219.8 | 216.6 | 213.5 |
| 2270 | 234.4 | 232.6 | 230.8 | 229.1 | 227.4 | 225.7 | 224.0 | 222.4 | 220.7 | 217.6 | 214.4 |
| 2280 | 235.4 | 233.6 | 231.8 | 230.1 | 228.4 | 226.7 | 225.0 | 223.3 | 221.7 | 218.5 | 215.4 |
| 2290 | 236.5 | 234.7 | 232.9 | 231.1 | 229.4 | 227.7 | 226.0 | 224.3 | 222.7 | 219.5 | 216.3 |
| 2300 | 237.5 | 235.7 | 233.9 | 232.1 | 230.4 | 228.7 | 227.0 | 225.3 | 223.6 | 220.4 | 217.3 |
| 2310 | 238.5 | 236.7 | 234.9 | 233.1 | 231.4 | 229.7 | 228.0 | 226.3 | 224.6 | 22 I .4 | 218.2 |
| 2320 | 239.6 | 237.7 | 235.9 | 234.1 | 232.4 | 230.7 | 228.9 | 227.3 | 225.6 | 222.3 | 219.2 |
| 2330 | 240.6 | 238.7 | 236.9 | 235.1 | 233.4 | 231.6 | 229.9 | 228.2 | 226.6 | 223.3 | 220.1 |
| 2340 | 241.6 | 239.8 | 237.9 | 236.2 | 234.4 | 232.6 | 230.9 | 229.2 | 227.5 | 224.3 | 221.0 |
| 2350 | 242.7 | 240.8 | 239.0 | 237.2 | 235.4 | 233.6 | 231.9 | 230.2 | 228.5 | 225.2 | 222.0 |
| 2360 | 243.7 | 241.8 | 240.0 | 238.2 | 236.4 | 234.6 | 232.9 | 231.2 | 229.5 | 226.2 | 222.9 |
| 2370 | 244.7 | 242.8 | 241.0 | 239.2 | 237.4 | 235.6 | 233.9 | 232.2 | 230.4 | 227.1 | 223.9 |
| 2380 | 245.7 | 243.9 | 242.0 | 240.2 | 238.4 | 236.6 | 234.9 | 233.1 | 231.4 | 228.1 | 224.8 |
| 2390 | 246.8 | 244.9 | 243.0 | 241.2 | 239.4 | 237.6 | 235.8 | 234.I | 232.4 | 229.1 | 225.8 |
| 2400 | 247.8 | 245.9 | 244.0 | 242.2 | 240.4 | 238.6 | 236.8 | 235.I | 233.4 | 230.0 | 226.7 |
| 2410 | 248.8 | 246.9 | 245.I | 243.2 | 241.4 | 239.6 | 237.8 | 236.1 | 234.3 | 231.0 | 227.7 |
| 2420 | 249.9 | 248.0 | 246.1 | 244.2 | 242.4 | 240.6 | 238.8 | 237.1 | 235.3 | 231.9 | 228.6 |
| 2430 | 250.9 | 249.0 | 247.I | 245.2 | 243.4 | 24 I .6 | 239.8 | 238.0 | 236.3 | 232.9 | 229.5 |
| 2440 | 251.9 | 250.0 | 248.1 | 246.2 | 244.4 | 242.6 | 240.8 | 239.0 | 237.3 | 233.8 | 230.5 |
| 2450 | 253.0 | 251.0 | 249.1 | 247.3 | 245.4 | 243.6 | 241.8 | 240.0 | 238.2 | 234.8 | 231.4 |
| 2460 | 254.0 | 252.1 | 250.1 | 248.3 | 246.4 | 244.6 | 242.8 | 241.0 | 239.2 | 235.8 | 232.4 |
| 2470 | 255.0 | 253.1 | 251.2 | 249.3 | 247.4 | 245.6 | 243.7 | 241.9 | 240.2 | 236.7 | 233.3 |
| 2480 | 256.1 | 254. 1 | 252.2 | 250.3 | 248.4 | 246.6 | 244.7 | 242.9 | 241.1 | 237.7 | $234 \cdot 3$ |
| 2490 | 257.1 | 255.1 | 253.2 | 251.3 | 249.4 | 247.5 | 245.7 | 243.9 | 242.1 | 238.6 | 235.2 |
| 2500 | 258.1 | 256.2 | 254.2 | 252.3 | 250.4 | 248.5 | 246.7 | 244.9 | 243.1 | 239.6 | 236.2 |

Smithsomian Tables.

TAble. 17.
REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.
Values of $2000 \times m . \quad m=\frac{z}{18444+67.53 \theta+.003 z} \cdot \frac{1}{1-\beta}$

|  | mean temperature of air column in centigrade degrees ( $\theta$ ). |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-16^{\circ}$ | $-12^{\circ}$ | $-8^{\circ}$ | $-4^{\circ}$ | $-2^{\circ}$ | $0^{\circ}$ | $+2^{\circ}$ | $+4^{\circ}$ | $+6^{\circ}$ | $+8^{\circ}$ | $+10^{\circ}$ |
| 2500 | 287.6 | 283.1 | 278.8 | 274.5 | 272.5 | 270.4 | 268.3 | 266.2 | 264.2 | 262.2 | 260.1 |
| 2510 | 288.8 | 284.3 | 279.9 | 275.6 | 273.6 | 271.5 | 269.4 | 267.3 | 265.2 | 263.2 | 261.2 |
| 2520 | 289.9 | 285.4 | 281.0 | 276.7 | 274.6 | 272.5 | 270.5 | 268.4 | 266.3 | 264.2 | 262.2 |
| 2530 | 291.1 | 286.5 | 282.I | 277.8 | 275.7 | 273.6 | 271.5 | 269.4 | 267.4 | 265.3 | 263.2 |
| 2540 | 292.2 | 287.7 | 283.3 | 278.9 | 276.8 | 274.7 | 272.6 | 270.5 | 268.4 | 266.3 | 264.3 |
| 2550 | 293.4 | 288.8 | 284.4 | 280.0 | 277.9 | 275.8 | 273.7 | 271.6 | 269.5 | 267.4 | 265.3 |
| 2560 | 294.5 | 289.9 | 285.5 | 28 I .1 | 279.0 | 276.9 | 274.7 | 272.6 | 270.5 | 268.4 | 266.4 |
| 2570 | 295.7 | 291.I | 286.6 | 282.2 | 280.1 | 277.9 | 275.8 | 273.7 | 271.6 | 269.5 | 267.4 |
| 2580 | 296.8 | 292.2 | 287.7 | 283.3 | 281.2 | 279.0 | 276.9 | 274.8 | 272.6 | 270.5 | 268.4 |
| 2590 | 298.0 | 293.3 | 288.8 | 284.4 | 282.3 | 280.1 | 278.0 | 275.8 | 273.7 | 271.6 | 269.5 |
| 2600 | 299.1 | 294.5 | 290.0 | 285.5 | 283.4 | 281.2 | 279.0 | 276.9 | 274.8 | 272.6 | 270.5 |
| 2610 | 300.3 | 295.6 | 291.1 | 286.6 | 284.4 | 282.3 | 280.1 | 278.0 | 275.8 | 273.7 | 271.6 |
| 2620 | 301.4 | 296.7 | 292.2 | 287.7 | 285.5 | 283.4 | 281.2 | 279.0 | 276.9 | 274.7 | 272.6 |
| 2630 | 302.6 | 297.8 | 293.3 | 288.8 | 286.6 | 284.4 | 282.3 | 280.1 | 277.9 | 275.8 | 273.6 |
| 2640 | 303.7 | 299.0 | 294.4 | 289.9 | 287.7 | 285.5 | 283.3 | 281.1 | 279.0 | 276.8 | 274.7 |
| 2650 | 304.9 | 300.I | 295.5 | 291.0 | 288.8 | 286.6 | 284.4 | 282.2 | 280.0 | 277.9 | 275.7 |
| 2660 | 306.0 | 301.2 | 296.6 | 292.I | 289.9 | 287.7 | 285.5 | 283.3 | 281.1 | 278.9 | 276.8 |
| 2670 | 307.2 | 302.4 | 297.8 | 293.2 | 291.0 | 288.8 | 286.5 | 284.3 | 282.1 | 280.0 | 277.8 |
| 2680 | 308.3 | 303.5 | 298.9 | 294.3 | 292.1 | 289.8 | 287.6 | 285.4 | 283.2 | 281.0 | 278.8 |
| 2690 | 309.5 | 304.6 | 300.0 | 295.4 | 293.2 | 290.9 | 288.7 | 286.5 | 284.3 | 282.1 | 279.9 |
| 2700 | 310.6 | 305.8 | 301.1 | 296.5 | 294.2 | 292.0 | 289.8 | 287.5 | 285.3 | 283.1 | 280.9 |
| 2710 | 311.8 | 306.9 | 302.2 | 297.6 | 295.3 | 293.I | 290.8 | 288.6 | 286.4 | 284.2 | 282.0 |
| 2720 | 312.9 | 308.0 | 303.3 | 298.7 | 296.4 | 294.2 | 291.9 | 289.7 | 287.4 | 285.2 | 283.0 |
| 2730 | 314.1 | 309.2 | 304.5 | 299.8 | 297.5 | 295.2 | 293.0 | 290.7 | 288.5 | 286.3 | 284.0 |
| 2740 | 315.2 | 310.3 | 305.6 | 300.9 | 298.6 | 296.3 | 294.I | 291.8 | 289.5 | 287.3 | 285.1 |
| 2750 | 316.4 | 311.4 | 306.7 | 302.0 | 299.7 | 297.4 | 295.I | 292.9 | 290.6 | 288.4 | 286.I |
| 2760 | 317.5 | 312.6 | 307.8 | 303.1 | 300.8 | 298.5 | 296.2 | 293.9 | 291.7 | 289.4 | 287.2 |
| 2770 | 318.7 | 313.7 | 308.9 | 304.2 | 301.9 | 299.6 | 297.3 | 295.0 | 292.7 | 290.5 | 288.2 |
| 2780 | 319.8 | 314.8 | 310.0 | 305.3 | 303.0 | 300.6 | 298.3 | 296.1 | 293.8 | 291.5 | 289.2 |
| 2790 | 321.0 | 3 | 3 II.I | 30 | 304.I | 301.7 | 299.4 | 297.1 | 294 | 292.5 | 290.3 |
| 2800 | 322.I | 317.1 | 312.3 | 307.5 | 305.I | 302.8 | 300.5 | 298.2 | 295.9 | 293.6 | 291.3 |
| 2810 | 323.3 | 318.2 | 313.4 | 308.6 | 306.2 | 303.9 | 301.6 | 299.2 | 296.9 | 294.6 | 292.4 |
| 2820 | 324.4 | 319.4 | 314.5 | 309.7 | 307.3 | 305.0 | 302.6 | 300.3 | 298.0 | 295.7 | 293.4 |
| 2830 | 325.6 | 320.5 | 315.6 | 310.8 | 308.4 | 306.I | 303.7 | 301.4 | 299.0 | 296.7 | 294.4 |
| 2840 | 326.7 | 321.6 | 316.7 | 311.9 | 309.5 | 307.1 | 304.8 | 302.4 | 300.1 | 297.8 | 295.5 |
| 2850 | 327.9 | 322.8 | 317.8 | 313.0 | 310.6 | 308.2 | 305.9 | 303.5 | 301.2 | 298.8 | 296.5 |
| 2860 | 329.0 | 323.9 | 318.9 | 314.I | 311.7 | 309.3 | 306.9 | 304.6 | 302.2 | 299.9 | 297.6 |
| 2870 | 330.2 | 325.0 | 320.1 | 315.2 | 312.8 | 310.4 | 308.0 | 305.6 | 303.3 | 300.9 | 298.6 |
| 2880 | 331.3 | 326.1 | 321.2 | 316.3 | 313.9 | 311.5 | 309.1 | 306.7 | 304.3 | 302.0 | 299.6 |
| 2890 | 332.5 | 327.3 | 322.3 | 317.4 | 314.9 | 312.5 | 310.I | 307.8 | 305.4 | 303.0 | 300.7 |
| 2900 | 333.6 | 328.4 | 323.4 | 318.4 | 316.0 | 313.6 | 311.2 | 308.8 | 306.4 | 304.I | 301.7 |
| 2910 | 334.8 | 329.5 | 324.5 | 319.5 | 317.1 | 314.7 | 312.3 | 309.9 | 307.5 | 305.I | 302.8 |
| 2920 | 335.9 | 330.7 | 325.6 | 320.6 | 318.2 | 315.8 | 313.4 | 311.0 | 308.6 | 306.2 | 303.8 |
| 2930 | 337.I | 331.8 | 326.7 | 321.7 | 319.3 | 316.9 | 314.4 | 312.0 | 309.6 | 307.2 | 304.8 |
| 2940 | 338.2 | 332.9 | 327.9 | 322.8 | 320.4 | 317.9 | 315.5 | 313.1 | 310.7 | 308.3 | 305.9 |
| 2950 | 339.4 | 334.1 | 329.0 | 323.9 | 321.5 | 319.0 | 316.6 | 314.2 | 311.7 | 309.3 | 306.9 |
| 2960 | 340.5 | 335.2 | 330.1 | 325.0 | 322.6 | 320.1 | 317.7 | 315.2 | 312.8 | 31 IO .4 | 308.0 |
| 2970 | 341.7 | 336.3 | 331.2 | 326.1 | 323.7 | 321.2 | 318.7 | 316.3 | 313.8 | 311.4 | 309.0 |
| 2980 | 342.8 | 337.5 | 332.3 | 327.2 | 324.7 | 322.3 | 319.8 | 317.3 | 314.9 | 312.5 | 310.0 |
| 2990 | 344. | 338.6 | 333.4 | 328.3 | 325.8 | 323.3 | 320.9 | 318.4 | 315.9 | 313.5 | 3II.I |
| 3000 | 345.1 | 339.7 | 334.5 | 329.4 | 326.9 | 324.4 | 321.9 | 319.5 | 317.0 | 314.6 | 312.1 |

[^8]TABLE 17.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Values of $2000 \times \mathrm{m} . \quad m=\frac{\mathrm{Z}}{18444+67.53 \theta+.003 \mathrm{Z}} \cdot \frac{\mathrm{I}}{\mathrm{I}-\boldsymbol{\beta}}$

| Altitude in metres. 2. | MEAN TEMPERATURE O |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $+12^{\circ}$ | $+14^{\circ}$ | $+16^{\circ}$ | $+18^{\circ}$ | $+20^{\circ}$ | $+22^{\circ}$ | $+24^{\circ}$ | $+26^{\circ}$ | $+28^{\circ}$ | + $32^{\circ}$ | $+36^{\circ}$ |
| 2500 | 258.1 | 256.2 | 254.2 | 252.3 | 250.4 | 248.5 | 246.7 | 244.9 | 243.1 | 239.6 | 236.2 |
| 2510 | 259.2 | 257.2 | 255.2 | 253.3 | 251.4 | 249.5 | 247.7 | 245.9 | 244.I | 240.6 | 237.1 |
| 2520 | 260.2 | 258.2 | 256.2 | 254.3 | 252.4 | 250.5 | 248.7 | 246.8 | 245.0 | 241.5 | 238.0 |
| 2530 | 261. 2 | 259.2 | 257.3 | 255.3 | 253.4 | 251.5 | 249.7 | 247.8 | 246.0 | 242.5 | 239.0 |
| 2540 | 262.3 | 260.3 | 258.3 | 256.3 | 254.4 | 252.5 | 250.6 | 248.8 | 247.0 | 243.4 | 239.9 |
| 2550 | 263.3 | 261.3 | 259.3 | 257.3 | 255.4 | 253.5 | 251.6 | 249.8 | 247.9 | 244.4 | 240.9 |
| 2560 | 264.3 | 262.3 | 260.3 | 258.4 | 256.4 | 254.5 | 252.6 | 250.7 | 248.9 | 245.3 | 241.8 |
| 2570 | 265.4 | 263.3 | 261.3 | 259.4 | 257.4 | 255.5 | 253.6 | 251.7 | 249.9 | 246.3 | 242.8 |
| 2580 | 265.4 | 264.4 | 262.3 | 260.4 | 258.4 | 256.5 | 254.6 | 252.7 | 250.9 | 247.3 | 243.7 |
| 2590 | 267.4 | 265.4 | 263.4 | 261.4 | 259.4 | 257.5 | 255.6 | 253.7 | 251.8 | 248.2 | 244.7 |
| 2600 | 268.5 | 266.4 | 264.4 | 262.4 | 260.4 | 258.5 | 256.6 | 254.7 | 252.8 | 249.2 | 245.6 |
| 2610 | 269.5 | 267.4 | 265.4 | 263.4 | 261.4 | 259.5 | 257.5 | 255.6 | 253.8 | 250.1 | 246.5 |
| 2620 | 270.5 | 268.5 | 266.4 | 264.4 | 262.4 | 260.5 | 258.5 | 256.6 | 254.8 | 251.1 | 247.5 |
| 2630 | 271.6 | 269.5 | 267.4 | 265.4 | 263.4 | 20 I. 5 | 259.5 | 257.6 | 255.7 | 252.0 | 248.4 |
| 2640 | 272.6 | 270.5 | 268.4 | 266.4 | 264.4 | 262.5 | 260.5 | 258.6 | 256.7 | 253.0 | 249.4 |
| 2650 | 273.6 | 271.5 | 269.5 | 267.4 | 265.4 | 263.4 | 261.5 | 259.6 | 257.7 | 254.0 | 250.3 |
| 2660 | 274.7 | 272.6 | 270.5 | 268.4 | 266.4 | 264.4 | 262.5 | 260.5 | 258.6 | 254.9 | 251.3 |
| 2670 | 275.7 | 273.6 | 271.5 | 269.4 | 267.4 | 265.4 | 263.5 | 26 I .5 | 259.6 | 255.9 | 252.2 |
| 2680 | 276.7 | 274.6 | 272.5 | 270.5 | 268.4 | 266.4 | 264.4 | 262.5 | 260.6 | 256.8 | 253.1 |
| 2690 | 277.7 | 275.6 | 273.5 | 271.5 | 269.4 | 267.4 | 265.4 | 263.5 | 261.6 | 257.8 | 254.I |
| 2700 | 278.8 | 276.6 | 274.5 | 272.5 | 270.4 | 268.4 | 266.4 | 264.5 | 262.5 | 258.8 | 255.0 |
| 2710 | 279.8 | 277.7 | 275.6 | 273.5 | 271.4 | 269.4 | 267.4 | 265.4 | 263.5 | 259.7 | 256.0 |
| 2720 | 280.8 | 278.7 | 276.6 | 274.5 | 272.4 | 270.4 | 268.4 | 266.4 | 264.5 | 260.7 | 256.9 |
| 2730 | 281.9 | 279.7 | 277.6 | 275.5 | 273.4 | 271.4 | 269.4 | 267.4 | 265.4 | 261.6 | 257.9 |
| 2740 | 282.9 | 280.7 | 278.6 | 276.5 | 274.4 | 272.4 | 270.4 | 268.4 | 266.4 | 262.6 | 258.8 |
| 2750 | 283.9 | 281.8 | 279.6 | 277.5 | 275.4 | 273.4 | 271.4 | 269.4 | 267.4 | 263.5 | 259.8 |
| 2760 | 285.0 | 282.8 | 280.6 | 278.5 | 276.4 | 274.4 | 272.3 | 270.3 | 268.4 | 264.5 | 260.7 |
| 2770 | 286.0 | 283.8 | 28 I .7 | 279.5 | 277.4 | 275.4 | 273.3 | 271.3 | 269.3 | 265.5 | 26ז. 6 |
| 2780 | 287.0 | 284.8 | 282.7 | 280.5 | 278.4 | 276.4 | 274.3 | 272.3 | 270.3 | 266.4 | 262.6 |
| 2790 | 2S8.I | 285.9 | 283.7 | 281.5 | 279.4 | 277.4 | 275.3 | 273.3 | 271.3 | 267.4 | 263.5 |
| 2800 | 289.1 | 286.9 | 284.7 | 282.6 | 280.4 | 278.3 | 276.3 | $274 \cdot 3$ | 272.2 | 268.3 | 264.5 |
| 2810 | 290.1 | 287.9 | 285.7 | 283.6 | 281.4 | 279.3 | 277.3 | 275.2 | 273.2 | 269.3 | 265.4 |
| 2820 | 291.2 | 288.9 | 286.7 | 284.6 | 282.4 | 280.3 | 278.3 | 276.2 | 274.2 | 270.3 | 266.4 |
| 2830 | 292.2 | 290.0 | 287.8 | 285.6 | 283.4 | 28 I .3 | 279.2 | 277.2 | 275.2 | 271.2 | 267.3 |
| 2840 | 293.2 | 291.0 | 288.8 | 286.6 | 284.4 | 282.3 | 280.2 | 278.2 | 276.1 | 272.2 | 268.3 |
| 2850 | 294.3 | 292.0 | 289.8 | 287.6 | 255.4 | 283.3 | 28I. 2 | 279.2 | 277.I | 273.1 | 269.2 |
| 2860 | 295.3 | 293.0 | 290.8 | 288.6 | 286.4 | 284.3 | 282.2 | 280.1 | 278.1 | 274.1 | 270.1 |
| 2870 | 296.3 | 294.1 | 291.8 | 289.6 | 287.4 | 285.3 | 283.2 | 281.1 | 279.0 | 275.0 | 271.1 |
| 2880 | 297.4 | 295.I | 292.8 | 290.6 | 288.4 | 286.3 | 284.2 | 282.1 | 280.0 | 276.0 | 272.0 |
| 2890 | 298.4 | 296.1 | 293.8 | 291.6 | 289.4 | 287.3 | 285.2 | 283.1 | 281.0 | 277.0 | 273.0 |
| 2900 | 299.4 | 297.I | 294.9 | 292.6 | 290.4 | 288.3 | 286.2 | 284.I | 282.0 | 277.9 | 27.3 .9 |
| 2910 | 300.4 | 298.1 | 295.9 | 293.7 | 291.5 | 289.3 | 287.1 | 285.0 | 282.9 | 278.9 | 274.9 |
| 2920 | 301.5 | 299.2 | 296.9 | 294.7 | 292.5 | 290.3 | 288.1 | 286.0 | 283.9 | 279.8 | 275.8 |
| 2930 | 302.5 | 300.2 | 297.9 | 295.7 | 293.5 | 291.3 | 289.I | 287.0 | 284.9 | 280.8 | 276.8 |
| 2940 | 303.5 | 301.2 | 298.9 | 296.7 | 294.5 | 292.3 | 290.1 | 288.0 | 285.9 | 2SI. 8 | 277.7 |
| 2950 | 304.6 | 302.2 | 299.9 | 297.7 | 295.5 | 293.3 | 291.I | 289.0 | 286.8 | 282.7 | 278.6 |
| 2960 | 305.6 | 303.3 | 301.0 | 298.7 | 296.5 | 294.2 | 292.1 | 289.9 | 287.8 | 283.7 | 279.6 |
| 2970 | 306.6 | 304.3 | 302.0 | 299.7 | 297.5 | 295.2 | 293.I | 290.9 | 288.8 | 284.6 | 280.5 |
| 2980 | 307.7 | 305.3 | 303.0 | 300.7 | 298.5 | 296.2 | 294.0 | 291.9 | 289.7 | 285.6 | 281.5 |
| 2990 | 308.7 | 306.3 | 304.0 | 301.7 | 299.5 | 297.2 | 295.0 | 292.9 | 290.7 | 286.5 | 282.4 |
| 3000 | 309.7 | 307.4 | 305.0 | 302.7 | 300.5 | 298.2 | 296.0 | 293.8 | 291.7 | 287.5 | 283.4 |

Table 18.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

Correction of 2000 m for Latitude : $2000 m \times 0.002662 \cos 2 \phi$.
For latitudes $0^{\circ}$ to $45^{\circ}$, the correction is to be subtracted.
For latitudes $45^{\circ}$ to $90^{\circ}$, the correction is to be added.

| 2000 m . | LATITUDE. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ | $45^{\circ}$ |
| 10 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 20 | o. 1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 30 | o. 1 | O.I | o. 1 | o. 1 | o. 1 | o.r | 0.0 | 0.0 | 0.0 | 0.0 |
| 40 | 0.1 | 0.1 | o. 1 | 0.I | o. 1 | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 |
| 50 | 0.1 | 0.1 | 0.1 | 0.1 | o. I | o.r | 0.I | 0.0 | 0.0 | 0.0 |
| 60 | 0.2 | 0.2 | 0.2 | 0.1 | o.r | 0.1 | 0.I | о. 1 | 0.0 | 0.0 |
| 70 | 0.2 | 0.2 | 0.2 | 0.2 | o. 1 | 0.1 | 0.I | o. 1 | 0.0 | 0.0 |
| 80 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.0 | 0.0 |
| 90 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.I | O. 1 | 0.0 | 0.0 |
| 100 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.2 | o.r | o. I | 0.0 | 0.0 |
| İо | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.1 | O. 1 | o.r | 0.0 |
| 120 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.2 | o. 1 | o. 1 | 0.0 |
| 130 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.1 | 0.1 | 0.0 |
| 140 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | 0.2 | o. 1 | 0.1 | 0.0 |
| 150 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.3 | 0.2 | o. 1 | 0.1 | 0.0 |
| 160 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | o. 1 | 0.1 | 0.0 |
| 170 | 0.5 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | 0.2 | o. 1 | 0.0 |
| 180 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 | 0.2 | 0.2 | 0.1 | 0.0 |
| 190 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 | 0.1 | 0.0 |
| 200 | 0.5 | 0.5 | 0.5 | 0.5 | 0.4 | 0.3 | 0.3 | 0.2 | 0.1 | 0.0 |
| 210 | 0.6 | 0.6 | 0.5 | 0.5 | 0.4 | 0.4 | 0.3 | 0.2 | 0.1 | 0.0 |
| 220 | 0.6 | 0.6 | 0.6 | 0.5 | 0.4 | 0.4 | 0.3 | 0.2 | o.r | 0.0 |
| 230 | 0.6 | 0.6 | 0.6 | 0.5 | 0.5 | 0.4 | 0.3 | 0.2 | 0.1 | 0.0 |
| 240 | 0.6 | 0.6 | 0.6 | 0.6 | 0.5 | 0.4 | 0.3 | 0.2 | O. 1 | 0.0 |
| 250 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.4 | 0.3 | 0.2 | O.I | 0.0 |
| 260 | 0.7 | 0.7 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | 0.2 | 0.1 | 0.0 |
| 270 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.4 | 0.2 | O.I | 0.0 |
| 280 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | 0.5 | 0.4 | 0.3 | O. 1 | 0.0 |
| 290 | 0.8 | 0.8 | 0.7 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | O. 1 | 0.0 |
| 300 | 0.8 | 0.8 | 0.8 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | 0.I | 0.0 |
| 310 | 0.8 | 0.8 | 0.8 | 0.7 | 0.6 | 0.5 | 0.4 | 0.3 | 0.1 | 0.0 |
| 320 | 0.9 | 0.8 | 0.8 | 0.7 | 0.7 | 0.5 | 0.4 | 0.3 | 0.1 | 0.0 |
| 330 | 0.9 | 0.9 | 0.8 | 0.8 | 0.7 | 0.6 | 0.4 | 0.3 | 0.2 | 0.0 |
| 340 | 0.9 | 0.9 | 0.9 | 0.8 | 0.7 | 0.6 | 0.5 | 0.3 | 0.2 | 0.0 |
| 350 | 0.9 | 0.9 | 0.9 | 0.8 | 0.7 | 0.6 | 0.5 | 0.3 | 0.2 | 0.0 |
|  | $90^{\circ}$ | $85^{\circ}$ | $80^{\circ}$ | $75^{\circ}$ | $70^{\circ}$ | $65^{\circ}$ | $60^{\circ}$ | $55^{\circ}$ | $50^{\circ}$ | $45^{\circ}$ |

Table 19.

## REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES. <br> $B-B=B\left(10^{m}-1\right)$.

Top argument: Height of the barometer ( $B$ ).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m . | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 790 | 780 | 770 | 760 | 750 | 740 | 730 | 720 | 710 | 700 | 690 |
|  | mm. | mm. | mm . | mm . | mm . | mm. | mm . | mm . | mm . | mm . | mm . |
| I | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| 2 | 1.8 | 1.8 | 1.8 | 1.8 | 1.7 | 1.7 | 1.7 | 1.7 | 1.6 | 1.6 | I. 6 |
| 3 | 2.7 | 2.7 | 2.7 | 2.6 | 2.6 | 2.6 | 2.5 | 2.5 | 2.5 | 2.4 | 2.4 |
| 4 | 3.6 | 3.6 | 3.6 | $3 \cdot 5$ | 3.5 | 3.4 | 3.4 | $3 \cdot 3$ | $3 \cdot 3$ | 3.2 | 3.2 |
| 5 | 4.6 | $4 \cdot 5$ | 4.4 | 4.4 | $4 \cdot 3$ | $4 \cdot 3$ | 4.2 | 4.2 | 4. 1 | 4.0 | 4.0 |
| 6 | $5 \cdot 5$ | 5.4 | $5 \cdot 3$ | $5 \cdot 3$ | 5.2 | 5.1 | 5.1 | 5.0 | 4.9 | 4.9 | 4.8 |
| 7 | 6.4 | 6.3 | 6.2 | 6.1 | 6.1 | 6.0 | 5.9 | 5.8 | 5.7 | 5.7 | 5.6 |
| 8 | $7 \cdot 3$ | 7.2 | 7.1 | 7.0 | 6.9 | 6.8 | 6.8 | 6.7 | 6.6 | 6.5 | 6.4 |
| 9 | 8.2 | 8.1 | 8.0 | 7.9 | 7.8 | 7.7 | 7.6 | 7.5 | $7 \cdot 4$ | 7.3 | 7.2 |
| 10 | 9.1 | 9.0 | 8.9 | 8.8 | 8.7 | 8.6 | 8.5 | 8.3 | 8.2 | 8.1 | 8.0 |
| II | IO. I | 9.9 | 9.8 | 9.7 | 9.6 | 9.4 | 9.3 | 9.2 | 9.0 | 8.9 | 8.8 |
| 12 | 11.0 | 10.9 | 10.7 | 10.6 | 10.4 | 10.3 | 10.2 | 10.0 | 9.9 | 9.7 | 9.6 |
| 13 | II. 9 | 11.8 | 11.6 | 11.5 | 11.3 | II. 2 | 11.0 | 10.9 | 10.7 | 10.6 | 10.4 |
| 14 | 12.8 | 12.7 | 12.5 | 12.3 | 12.2 | 12.0 | 11.9 | 11.7 | 11.5 | II. 4 | 11.2 |
| 15 | 13.8 | 13.6 | 13.4 | 13.2 | 13. 1 | 12.9 | 12.7 | 12.5 | 12.4 | 12.2 | 12.0 |
| 16 | 14.7 | 14.5 | 14.3 | 14.1 | 13.9 | 13.8 | 13.6 | 13.4 | 13.2 | 13.0 | 12.8 |
| 17 | 15.6 | 15.4 | 15.2 | 15.0 | 14.8 | 14.6 | 14.4 | 14.2 | 14.0 | 13.8 | 13.6 |
| 18 | 16.5 | 16.3 | 16.1 | 15.9 | 15.7 | 15.5 | 15.3 | 15.1 | 14.9 | 14.7 | 14.4 |
| I9 | 17.5 | 17.3 | 17.0 | 16.8 | 16.6 | 16.4 | 16. 1 | 15.9 | 15.7 | 15.5 | 15.3 |
| 20 | I8.4 | 18.2 | 17.9 | 17.7 | 17.5 | 17.2 | 17.0 | 16.8 | 16.5 | 16.3 | 16.1 |
| 21 | 19.3 | 19.1 | 18.8 | 18.6 | 18.4 | 18.1 | 17.9 | 17.6 | 17.4 | 17.1 | 16.9 |
| 22 |  | 20.0 | 19.8 | 19.5 | 19.2 | 19.0 | 18.7 | 18.5 | 18.2 | 18.0 | 17.7 |
| 23 |  | 20.9 | 20.7 | 20.4 | 20.1 | 19.9 | 19.6 | 19.3 | 19.1 | 18.8 | 18.5 |
| 24 |  | 21.9 | 21.6 | 21.3 | 21.0 | 20.7 | 20.5 | 20.2 | 19.9 | 19.6 | 19.3 |
| 25 |  | 22.8 | 22.5 | 22.2 | 21.9 | 21.6 | 21.3 | 21.0 | 20.7 | 20.4 | 20.1 |
| 26 |  | 23.7 | 23.4 | 23.1 | 22.8 | 22.5 | 22.2 | 21.9 | 21.6 | 21.3 | 21.0 |
| 27 |  | 24.6 | 24.3 | 24.0 | 23.7 | 23.4 | 23.0 | 22.7 | 22.4 | 22.1 | 21.8 |
| 28 |  | 25.6 | 25.2 | 24.9 | 24.6 | 24.2 | 23.9 | 23.6 | 23.3 | 22.9 | 22.6 |
| 29 |  | 26.5 | 26.1 | 25.8 | 25.5 | 25.1 | 24.8 | 24.4 | 24.1 | 23.8 | 23.4 |
| 30 |  | 27.4 | 27.1 | 26.7 | 26.4 | 26.0 | 25.7 | 25.3 | 25.0 | 24.6 | 24.2 |
| 3 I |  | 28.3 | 28.0 | 27.6 | 27.3 | 26.9 | 26.5 | 26.2 | 25.8 | 25.4 | 25. I |
| 32 |  | 29.3 | 28.9 | 28.5 | 28.1 | 27.8 | 27.4 | 27.0 | 26.6 | 26.3 | 25.9 |
| 33 |  | 30.2 | 29.8 | 29.4 | 29.0 | 28.7 | 28.3 | 27.9 | 27.5 | 27.1 | 26.7 |
| 34 |  |  | 30.7 | 30.3 | 29.9 | 29.5 | 29.I | 28.7 | 28.3 | 27.9 | 27.5 |
|  |  |  |  | 31.2 | 30.8 | 30.4 | 30.0 | 29.6 | 29.2 | 28.8 | 28.4 |
| 36 |  |  | 32.6 | 32.2 | 31.7 | 3 I .3 | 30.9 | 30.5 | 30.0 | 29.6 | 29.2 |
| 37 |  |  | 33.5 | 33. 1 | 32.6 | 32.2 | 31.8 | 31.3 | 30.9 | 30.5 | 30.0 |
| 38 |  |  | 34.4 | 34.0 | 33.5 | 33.1 | 32.6 | 32.2 | 31.8 | 31.3 | 30.9 |
| 39 |  |  | 35.4 | 34.9 | 34.4 | 34.0 | 33.5 | 33.1 | 32.6 | 32.1 | 31.7 |
| 40 |  |  | 36.3 | 35.8 | $35 \cdot 3$ | 34.9 | 34.4 | 33.9 | 33.5 | 33.0 | 32.5 |

Table 19.
REDUCTION OF THE BAROMETER TO SEA LEVEL.
METRIC MEASURES.
$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m. | height of the barometer in millimetres. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 760 | 750 | 740 | 730 | 720 | 710 | 700 | 690 | 680 | 670 | 660 |
|  | mm. | mm. | mm. | mm. | mm. | mm . | mm. | mm. | mm | mm. | mm. |
| 40 | 35.8 | 35.3 | 34.9 | 34.4 | 33.9 | 33.5 | 33.0 | 32.5 | 32.0 | 31.6 | 3 I .1 |
| 4 I | 36.7 | 36.3 | 35.8 | 35.3 | 34.8 | 34.3 | 33.8 | 33.4 | 32.9 | 32.4 | 31.9 |
| 42 | 37.7 | 37.2 | 36.7 | 36.2 | 35.7 | 35.2 | 34.7 | 34.2 | 33.7 | 33.2 | 32.7 |
| 43 | 38.6 | 38.1 | 37.6 | 37.0 | 36.5 | 36.0 | 35.5 | 35.0 | 34.5 | 34.8 | 33.5 |
| 44 | 39.5 | 39.0 | 38.5 | 37.9 | 37.4 | 36.9 | 36.4 | 35.9 | $35 \cdot 3$ | 34.8 | 34.3 |
| 45 | 40.4 | 39.9 | 39.3 | 38.8 | 38.3 | 37.8 | 37.2 | 36.7 | 36.2 | 35.6 | 35. I |
| 46 | 4 I .3 | 40.8 | 40.2 | 39.7 | 39.2 | 38.6 | 38. 1 | 37.5 | 37.0 | 36.4 | 35.9 |
| 47 | 42.3 | 41.7 | 4 I .1 | 40.6 | 40.0 | 39.5 | 38.9 | 38.4 | 37.8 | 37.3 | 36.7 |
| 48 | 43.2 | 42.6 | 42.0 | 41.5 | 40.9 | 40.3 | 39.8 | 39.2 | 38.6 | 38.1 | 37.5 |
| 49 | 44. I | 43.5 | 42.9 | 42.4 | 4 I .8 | 41.2 | 40.6 | 40.0 | 39.5 | 38.9 | 38.3 |
| 50 | 45.0 | 44.4 | 43.8 | 43.3 | 42.7 | 42.1 | 4 I .5 | 40.9 | 40.3 | 39.7 | 39.1 |
| 51 | 46.0 | 45.4 | 44.8 | 44.1 | 43.5 | 42.9 | 42.3 | 41.7 | 4 I .1 | 40.5 | 39.9 |
| 52 | 46.9 | 46.3 | 45.7 | 45.0 | 44.4 | 43.8 | 43.2 | 42.6 | 42.0 | 41.3 | 40.7 |
| 53 | 47.8 | 47.2 | 46.6 | 45.9 | 45.3 | 44.7 | 44.0 | 43.4 | 42.8 | 42.2 | 41.5 |
| 54 | 48.7 | 48.1 | 47.5 | 46.8 | 46.2 | 45.5 | 44.9 | 44.3 | 43.6 | 43.0 | 42.3 |
| 55 | 49.7 | 49.0 | 48.4 | 47.7 | 47.1 | 46.4 | 45.8 | 45. I | 44.5 | 43.8 | 43.1 |
| 56 | 50.6 | 49.9 | 49.3 | 48.6 | 47.9 | 47.3 | 46.6 | 46.0 | 45.3 | 44.6 | 44.0 |
| 57 | 51.5 | 50.9 | 50.2 | 49.5 | 48.8 | 48.2 | 47.5 | 46.8 | 46.1 | 45.4 | 44.8 |
| 58 | 52.5 | 51.8 | 5 I .1 | 50.4 | 49.7 | 49.0 | 48.3 | 47.6 | 47.0 | 46.3 | 45.6 |
| 59 | 53.4 | 52.7 | 52.0 | 51.3 | 50.6 | 49.9 | 49.2 | 48.5 | 47.8 | 47. I | 46.4 |
| 60 |  | 53.6 | 52.9 | 52.2 | 51.5 | 50.8 | 50.1 | 49.3 | 48.6 | 47.9 | 47.2 |
| 61 |  | 54.6 | 53.8 | 53. 1 | 52.4 | 51.7 | 50.9 | 50.2 | 49.5 | 48.7 | 48.0 |
| 62 |  | 55.5 | 54.8 | 54.0 | 53.3 | 52.5 | 51.8 | 51.1 | 50.3 | 49.6 | 48.8 |
| 63 |  | 56.4 | 55.7 | 54.9 | 54.2 | 53.4 | 52.7 | 51.9 | 51.2 | 50.4 | 49.6 |
| 64 |  | 57.3 | 56.6 | 55.8 | 55.I | $54 \cdot 3$ | 53.5 | 52.8 | 52.0 | 51.2 | 50.5 |
| 65 |  | 58.3 | 57.5 | 56.7 | 55.9 | 55.2 | 54.4 | 53.6 | 52.8 | 52.1 | 5 I .3 |
| 66 |  | 59.2 | 58.4 | 57.6 | 56.8 | 56.1 | 55.3 | 54.5 | 53.7 | 52.9 | 52.1 |
| 67 |  | 60.1 | 59.3 | 58.5 | 57.7 | 56.9 | 56.1 | 55.3 | 54.5 | 53.7 | 52.9 |
| 68 |  |  | 60.3 | 59.4 | 58.6 | 57.8 | 57.0 | 56.2 | 55.4 | 54.6 | 53.7 |
| 69 |  |  | 6 I .2 | 60.4 | 59.5 | 58.7 | 57.9 | 57.0 | 56.2 | 55.4 | 54.6 |
| 70 |  |  | 62.1 | 61.3 | 60.4 | 59.6 | 58.7 | 57.9 | 57.1 | 56.2 | 55.4 |
| 71 |  |  | 63.0 | 62.2 | 61.3 | 60.5 | 59.6 | 58.8 | 57.9 | 57.1 | 56.2 |
| 72 |  |  | 64.0 | 63.1 | 62.2 | $6 \mathrm{6I} 4$ | 60.5 | 59.6 | 58.8 | 57.9 | 57.0 |
| 73 |  |  |  | 64.0 | 63.1 | 62.3 |  | 60.5 | 59.6 | 58.7 | 57.9 |
| 74 |  |  | 65.8 | 64.9 | 64.0 | 63.1 | 62.3 | 61.4 | 60.5 | 59.6 | 58.7 |
| 75 |  |  | 66.7 | 65.8 | 64.9 | 64.0 | 63.1 | 62.2 | 61.3 | 60.4 | 59.5 |
| 76 |  |  | 67.7 | 66.8 | 65.8 | 64.9 | 64.0 | 63.1 | 62.2 | 6 I .3 | 60.4 |
| 77 |  |  | 68.6 | 67.7 | 66.7 | 65.8 | 64.9 | 64.0 | 63.0 | 62.1 | 61.2 |
| 78 |  |  | 69.5 | 68.6 | 67.6 | 66.7 | 65.8 | 64.8 | 63.9 | 63.0 | 62.0 |
| 79 |  |  | 70.5 | 69.5 | 68.6 | 67.6 | 66.7 | 65.7 | 64.7 | 63.8 | 62.8 |
| 80 |  |  |  | 70.4 | 69.5 | 68.5 | 67.5 | 66.6 | 65.6 | 64.6 | 63.7 |
| 81 |  |  |  | 7 I .4 | 70.4 | 69.4 | 68.4 | 67.4 | 66.5 | 65.5 | 64.5 |
| 82 |  |  |  | 72.3 | 71.3 | 70.3 | 69.3 | 68.3 | 67.3 | 66.3 | 65.3 |
| 83 |  |  |  | 73.2 | 72.2 | 71.2 | 70.2 | 69.2 | 68.2 | 67.2 | 66.2 |
| 84 |  |  |  | 74.1 | 73.1 | 72.1 | 71.1 | 70.1 | 69.0 | 68.0 | 67.0 |
| 85 |  |  |  | 75.0 | 74.0 | 73.0 | 72.0 | 70.9 | 69.9 | 68.9 | 67.9 |

TABLE 19.
REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.
$B 0-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m. | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 720 | 710 | 700 | 690 | 680 | 670 | 660 | 650 | 640 | 630 |
|  | mm. | mm. | mm . | mm . | mm . | mm . | mm . | mm . | mm . | mm . |
| 80 | 69.5 | 68.5 | 67.5 | 66.6 | 65.6 | 64.6 | 63.7 | 62.7 | 61.7 | 60.8 |
| 81 | 70.4 | 69.4 | 68.4 | 67.4 | 66.5 | 65.5 | 64.5 | 63.5 | 62.6 | 61.6 |
| 82 | 71.3 | 70.3 | 69.3 | 68.3 | 67.3 | 66.3 | 65.3 | 64.4 | 63.4 | 62.4 |
| 83 | 72.2 | 71.2 | 70.2 | 69.2 | 68.2 | 67.2 | 66.2 | 65.2 | 64.2 | 63.2 |
| 84 | 73.1 | 72.1 | 7 I .1 | 70.1 | 69.0 | 68.0 | 67.0 | 66.0 | 65.0 | 64.0 |
| 85 | 74.0 | 73.0 | 72.0 | 70.9 | 69.9 | 68.9 | 67.9 | 66.8 | 65.8 | 64.8 |
| 86 | 74.9 | 73.9 | 72.9 | 71.8 | 70.8 | 69.7 | 68.7 | 67.7 | 66.6 | 65.6 |
| 87 | 75.9 | 74.8 | 73.7 | 72.7 | 71.6 | 70.6 | 69.5 | 68.5 | 67.4 | 66.4 |
| 88 | 76.8 | 75.7 | 74.6 | 73.6 | 72.5 | 71.4 | 70.4 | 69.3 | 68.2 | 67.2 |
| 89 | 77.7 | 76.6 | 75.5 | 74.5 | 73.4 | 72.3 | 71.2 | 70.1 | 69.1 | 68.0 |
| 90 | 78.6 | 77.5 | 76.4 | 75.3 | 74.2 | 73.1 | 72.1 | 71.0 | 69.9 | 68.8 |
| 91 | 79.5 | 78.4 | 77.3 | 76.2 | 75.1 | 74.0 | 72.9 | 71.8 | 70.7 | 69.6 |
| 92 | 80.4 | 79.3 | 78.2 | 77. I | 76.0 | 74.9 | 73.7 | 72.6 | 71.5 | 70.4 |
| 93 | 8 I .4 | 80.2 | 79.1 | 78.0 | 76.8 | 75.7 | 74.6 | 73.5 | 72.3 | 71.2 |
| 94 | 82.3 | 8I. I | 80.0 | 78.9 | 77.7 | 76.6 | 75.4 | $74 \cdot 3$ | 73.1 | 72.0 |
| 95 | 83.2 | 82.1 | 80.9 | 79.7 | 78.6 | 77.4 | 76.3 | 75.I | 74.0 | 72.8 |
| 96 | 84.1 | 83.0 | 8 r .8 | 80.6 | 79.5 | 78.3 | 77.1 | 76.0 | 74.8 | 73.6 |
| 97 | 85.1 | 83.9 | 82.7 | 8 I .5 | 80.3 | 79.2 | 78.0 | 76.8 | 75.6 | 74.4 |
| 98 | 86.0 | 84.8 | 83.6 | 82.4 | 8 I .2 | 80.0 | 78.8 | 77.6 | 76.4 | 75.2 |
| 99 | 86.9 | 85.7 | 84.5 | 83.3 | S2. I | 80.9 | 79.7 | 78.5 | 77.3 | 76.1 |
| 100 | 87.9 | 86.6 | 85.4 | 84.2 | 83.0 | 8r 8 | 80.5 | 79.3 | 78.1 | 76.9 |
| IOI | 88.8 | 87.6 | 86.3 | 85.1 | 83.9 | 82.6 | 8 I .4 | 80.2 | 78.9 | 77.7 |
| 102 | 89.7 | 88.5 | 87.2 | 86.0 | 84.7 | 83.5 | 82.2 | 81.0 | 79.7 | 78.5 |
| 103 | 90.6 | 89.4 | 88.1 | 86.9 | 85.6 | 84.4 | 83.1 | 8 I .8 | 80.6 | 79.3 |
| 104 |  | 90.3 | 89.0 | 87.8 | 86.5 | 85.2 | 84.0 | 82.7 | 81.4 | 80.1 |
| 105 |  | 91.2 | 89.9 | 88.7 | 87.4 | 86. I | 84.8 | 83.5 | 82.2 | 8 I .0 |
| 106 |  | 92.2 | 90.9 | 89.6 | 88.3 | 87.0 | 85.7 | 84.4 | 83.1 | 81. 8 |
| 107 |  | 93.1 | 91.8 | 90.5 | 89.1 | 87.8 | 86.5 | 85.2 | 83.9 | 82.6 |
| 108 |  | 94.0 | 92.7 | 91.4 | 90.0 | 88.7 | 87.4 | 86. 1 | 84.7 | 83.4 |
| 109 |  | 94.9 | 93.6 | 92.3 | 90.9 | 89.6 | 88.2 | 86.9 | 85.6 | 84.2 |
| 110 |  | 95.9 | 94.5 | 93.2 | 91.8 | 90.5 | 89.1 | 87.8 | 86.4 | 85.1 |
| III |  | 96.8 | 95.4 | 94.1 | 92.7 | 91.3 | 90.0 | 88.6 | 87.2 | 85.9 |
| 112 |  | 97.7 | 96.3 | 95.0 | 93.6 | 92.2 | 90.8 | 89.5 | 88.1 | 86.7 |
| II3 |  | 98.6 | 97.3 | 95.9 | 94.5 | 93.1 | 91.7 | 90.3 | 88.9 | 87.5 |
| II4 |  | 99.6 | 98.2 | 96.8 | 95.4 | 94.0 | 92.6 | 91.2 | 89.8 | 88.4 |
| 115 |  | 100.5 | 99.1 | 97.7 | 96.3 | 94.8 | 93.4 | 92.0 | 90.6 | 89.2 |
| 116 |  |  | 100.0 | 98.6 | 97.2 | 95.7 | 94.3 | 92.9 | 91.4 | 90.0 |
| 117 |  |  | 100.9 | 99.5 | 98.1 | 96.6 | 95.2 | 93.7 | 92.3 | 90.8 |
| 118 |  |  | 101. 9 | 100.4 | 98.9 | 97.5 | 96.0 | 94.6 | 93.1 | 91.7 |
| I19 |  |  | 102.8 | 101.3 | 99.8 | 98.4 | 96.9 | 95.4 | 94.0 | 92.5 |
| 120 |  |  | 103.7 | 102.2 | 100.7 | 99.3 | 97.8 | 96.3 | 94.8 | $93 \cdot 3$ |
| 121 |  |  | 104.6 | 103. 1 | 101.6 | 100. 1 | 98.7 | 97.2 | 95.7 | 94.2 |
| 122 |  |  | 105.6 | 104.1 | 102.5 | Ioi.o | 99.5 | 98.0 | 96.5 | 95.0 |
| 123 |  |  | 106.5 | 105.0 | 103.4 | IOI. 9 | 100.4 | 98.9 | 97.4 | 95.8 |
| 124 |  |  | 107.4 | 105.9 | 104.3 | 102.8 | IOI. 3 | 99.7 | 98.2 | 96.7 |
| 125 |  |  | 108.3 | 106.8 | 105.3 | 103.7 | 102.2 | 100.6 | 99. I | 97.5 |

Table 19.
REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.
$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m. | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 690 | 680 | 670 | 660 | 650 | 640 | 630 | 620 | 610 | 600 |
|  | mm. | mm. | mm . | mm . | mm . | mm . | mm. | mm. | mm . | mm . |
| 125 | 106.8 | 105.3 | 103.7 | 102.2 | 100.6 | 99.1 | 97.5 | 96.0 | 94.4 | 92.9 |
| 126 | 107.7 | 106.2 | 104.6 | 103.0 | IOI. 5 | 99.9 | 98.4 | 96.8 | 95.2 | 93.7 |
| 127 | 108.6 | 107.1 | 105.5 | 103.9 | 102.3 | 100.8 | 99.2 | 97.6 | 96.0 | 94.5 |
| 128 | 109.6 | 108.0 | 106.4 | 104.8 | 103.2 | IOI. 6 | 100.0 | 98.4 | 96.9 | 95.3 |
| 129 | IIO. 5 | 108.9 | 107.3 | 105.7 | 104. 1 | 102.5 | 100.9 | 99.3 | 97.7 | 96.1 |
| 130 | III. 4 | 109.8 | 108.2 | 106.6 | 104.9 | 103.3 | 101.7 | 100. 1 | 98.5 | 96.9 |
| 131 | II2.3 | 110.7 | 109. 1 | 107.4 | 105.8 | 104.2 | 102.6 | 100.9 | 99.3 | 97.7 |
| 132 | II 3.2 | III. 6 | 110.0 | 108.3 | 106.7 | 105.0 | 103.4 | 101. 8 | 100.1 | 98.5 |
| 133 | II4.2 | II2.5 | 110.9 | 109.2 | 107.6 | 105.9 | 104.2 | 102.6 | 100.9 | 99.3 |
| 134 | II5.I | II3.4 | 111.8 | IIO.I | 108.4 | 106.8 | 105.I | 103.4 | IOI. 8 | 100.1 |
| 135 | II6.0 | II4.3 | II 2.7 | III.O | 109.3 | 107.6 | 105.9 | $104 \cdot 3$ | 102.6 | 100.9 |
| 136 | 117.0 | II5.3 | 113.6 | III. 9 | 110.2 | 108.5 | 106.8 | 105.1 | 103.4 | 101.7 |
| 137 | 117.9 | I16.2 | 114.5 | II2.8 | III.I | 109.3 | 107.6 | 105.9 | 104.2 | 102.5 |
| 138 | I 18.8 | 117.1 | 115.4 | 113.6 | III. 9 | I 10.2 | 108.5 | 106.8 | 105.0 | 103.3 |
| 139 | 119.7 | I 18.0 | II6.3 | II4.5 | II 2.8 | III.I | 109.3 | 107.6 | 105.9 | 104.I |
| 140 | 120.7 | II8.9 | 117.2 | 115.4 | 113.7 | III. 9 | 110.2 | 108.4 | 106.7 | IU4.9 |
| 141 | I21. 6 | 119.9 | 118.1 | II6.3 | 114.6 | 112.8 | III.O | 109.3 | 107.5 | 105.8 |
| 142 |  | 120.8 | 119.0 | 117.2 | 115.4 | 113.7 | III. 9 | IIO.I | 108.3 | 106.6 |
| 143 |  | 121.7 | 119.9 | II8.I | 116.3 | II4.5 | II2.7 | III.O | 109.2 | 107.4 |
| 144 |  | 122.6 | 120.8 | II9.0 | 117.2 | II 5.4 | II 3.6 | III. 8 | I 10.0 | 108.2 |
| 145 |  | 123.5 | 121.7 | 119.9 | II8. 1 | II6.3 | I14.5 | 112.6 | 110.8 | 109.0 |
| 146 |  | 124.5 | 122.6 | 120.8 | 119.0 | 117.1 | II5.3 | II3.5 | III.7 | 109.8 |
| 147 |  | 125.4 | 123.6 | 121.7 | 119.9 | 118.0 | I16.2 | 114.3 | II2.5 | IIO 6 |
| 148 |  | 126.3 | 124.5 | 122.6 | 120.7 | 118.9 | 117.0 | 115.2 | 113.3 | III. 5 |
| 149 |  | 127.3 | 125.4 | 123.5 | 121.6 | 119.8 | II7.9 | II6.0 | II4.2 | II 2.3 |
| 150 |  | 128.2 | I26.3 | 124.4 | 122.5 | 120.6 | II8.8 | II6.9 | 115.0 | II3. 1 |
| 151 |  | 129.1 | 127.2 | 125.3 | 123.4 | 121.5 | 119.6 | 117.7 | II5.8 | II3.9 |
| 152 |  | 130.0 | 128.I | I26.2 | 124.3 | 122.4 | 120.5 | II8.6 | II6.7 | 114.7 |
| 153 |  | 13 I .0 | 129.1 | 127.1 | 125.2 | 123.3 | 121.3 | I19.4 | 117.5 | II5.6 |
| I54 |  |  | 130.0 | 128.0 | 126.1 | 124.2 | 122.2 | 120.3 | 118.3 | 116.4 |
| 155 |  |  | I30.9 | 128.9 | 127.0 | 125.0 | 123.1 | 121.1 | I19.2 | 117.2 |
| I56 |  |  | 131.8 | 129.8 | 127.9 | 125.9 | 123.9 | 122.0 | 120.0 | 118.0 |
| 157 |  |  | 132.7 | 130.8 | 128.8 | 126.8 | 124.8 | 122.8 | 120.9 | 118.9 |
| 158 |  |  | 133.7 | 131.7 | 129.7 | 127.7 | 125.7 | 123.7 | 121.7 | 119.7 |
| 159 |  |  | I34.6 | I32.6 | I30.6 | 128.6 | 126.6 | 124.5 | 122.5 | 120.5 |
| 160 |  |  | I35.5 | I 33.5 | 131.5 | 129.4 | 127.4 | 125.4 | 123.4 | 121.4 |
| 161 |  |  | 136.4 | I 34.4 | I32.4 | 130.3 | 128.3 | 126.3 | 124.2 | 122.2 |
| 162 |  |  | I 37.4 | I 35.3 | 133.3 | 131.2 | 129.2 | 127.1 | 125.1 | 123.0 |
| 163 |  |  | 138.3 | I 36.2 | 134.2 | 132.1 | 130.0 | 128.0 | 125.9 | 123.9 |
| 164 |  |  | I 39.2 | I 37.2 | I 35. I | I 33.0 | 130.9 | I28.8 | 126.8 | 124.7 |
| 165 |  |  | 140.2 | 138.1 | 136.0 | 133.9 | 1.31. 8 | 129.7 | 127.6 | 125.5 |
| 166 |  |  | 141. I | I39.0 | I36.9 | I 34.8 | 132.7 | 130.6 | 128.5 | 126.4 |
| 167 |  |  | 142.0 | I39.9 | 137.8 | I 35.7 | 133.6 | 131.4 | 129.3 | 127.2 |
| 168 |  |  |  | 140.8 | 138.7 | I 36.6 | I 34.4 | 132.3 | I30.2 | 128.0 |
| 169 |  |  |  | 141.8 | I39.6 | I 37.5 | I 35.3 | I 33.2 | 131.0 | 128.9 |
| 170 |  |  |  | 142.7 | 140.5 | I38.4 | I36.2 | 134.0 | 131.9 | 129.7 |

TABLE 19.

## REDUCTION OF THE BAROMETER TO SEA LEVEL.

 METRIC MEASURES.$B_{0}-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m. | HEIGHT OF THE BAROMETER IN MILIIMETRES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 650 | 640 | 630 | 620 | 610 | 600 | 590 | 580 | 570 | 560 |
|  | mm . | mm. | mm . | mm. | mm. | mm . | mm . | mm . | mm . | mm . |
| 170 | 140.5 | I38.4 | I36.2 | I34.0 | 131.9 | 129.7 | 127.5 | 125.4 | 123.2 | 12I.I |
| 171 | 141.4 | 139.3 | 137.1 | 134.9 | 132.7 | 130.6 | 128.4 | 126.2 | 124.0 | 121.8 |
| 172 | 142.3 | 140.2 | 138.0 | 135.8 | 133.6 | I31. 4 | 129.2 | 127.0 | 124.8 | 122.6 |
| 173 | 143.3 | 141.I | 138.8 | 136.6 | 134.4 | I32.2 | 130.0 | 127.8 | I25.6 | 123.4 |
| 174 | 144.2 | 142.0 | 139.7 | 137.5 | 135.3 | 133.I | I30.9 | 128.6 | 126.4 | 124.2 |
| 175 | 145. I | 142.9 | 140.6 | I38.4 | 136.2 | 133.9 | 131.7 | 129.5 | I27.2 | 125.0 |
| 176 | 146.0 | 143.8 | 141.5 | 139.3 | 137.0 | 134.8 | ${ }^{1} 32.5$ | 130.3 | 128.0 | 125.8 |
| 177 | 146.9 | 144.7 | 142.4 | 140.1 | 137.9 | I 35.6 | 133.4 | 13 I .1 | 128.8 | I26.6 |
| 178 | 147.8 | 145.6 | 143.3 | 141.0 | 138.7 | I36.5 | I34.2 | 131.9 | 129.6 | 127.4 |
| 179 | 148.8 | 146.5 | 144.2 | 141.9 | 139.6 | 137.3 | 135.0 | 132.7 | I30.4 | 128.2 |
| 180 | 149.7 | 147.4 | I45.1 | 142.8 | 140.5 | I38.2 | 135.9 | 133.6 | 131.3 | 129.0 |
| 181 | 150.6 | 148.3 | 146.0 | 143.6 | 141.3 | 139.0 | 136.7 | 134.4 | I32.I | 129.7 |
| 182 | 151.5 | 149.2 | 146.9 | 144.5 | 142.2 | 139.9 | 137.5 | 135.2 | 132.9 | 130.5 |
| 183 | 152.4 | 150. 1 | 147.8 | 145.4 | 143.1 | 140.7 | ${ }^{1} 38.4$ | 136.0 | I 33.7 | I31.3 |
| 184 | 153.4 | 151.0 | 148.6 | 146.3 | 143.9 | 141.6 | 139.2 | I36.8 | I 34.5 | 132.1 |
| 185 | 154.3 | 151.9 | 149.5 | 147.2 | 144.8 | 142.4 | 140.0 | 137.7 | 135.3 | 132.9 |
| 186 | 155.2 | 152.8 | 150.4 | 148. I | 145.7 | 143.3 | 140.9 | 138.5 | I36. I | 133.7 |
| 187 | 156. 1 | 153.7 | 151.3 | 148.9 | 146.5 | 144.1 | 141.7 | 139.3 | 136.9 | 134.5 |
| 188 | 157. I | 154.7 | 152.2 | 149.8 | 147.4 | 145.0 | 142.6 | 140.2 | 137.7 | 135.3 |
| 189 | 158.0 | I55.6 | I53. I | 150.7 | 148.3 | 145.8 | 143.4 | 141.0 | I38.6 | I36. I |
| 190 | 158.9 | 156.5 | 154.0 | 151.6 | 149.2 | 146.7 | 144.3 | 141.8 | I39.4 | I36.9 |
| 191 | 159.9 | 157.4 | 154.9 | 152.5 | 150.0 | 147.6 | I45. I | 142.7 | 140.2 | 137.7 |
| 192 | 160.8 | 158.3 | 155.9 | 153.4 | 150.9 | 148.4 | 146.0 | 143.5 | 141.0 | 138.5 |
| 193 | 161.7 | 159.2 | 156.8 | 154.3 | 151.8 | 149.3 | 146.8 | 144.3 | 141.8 | 139.3 |
| 194 |  | 160.2 | ${ }^{1} 57.7$ | I55.2 | 152.7 | 150.2 | 147.7 | 145.2 | 142.6 | I40. 1 |
| 195 |  | 161.I | 158.6 | 156. 1 | 153.5 | 151.0 | 148.5 | 146.0 | 143.5 | 141.0 |
| 196 |  | 162.0 | 159.5 | 156.9 | I54.4 | 151.9 | 149.4 | 146.8 | 144.3 | 141.8 |
| 197 |  | 162.9 | 160.4 | 157.8 | 155.3 | 152.8 | 150.2 | 147.7 | 145. I | 142.6 |
| 198 |  | 163.9 | 161.3 | 158.7 | 156.2 | 153.6 | 15 I .1 | 148.5 | 145.9 | 143.4 |
| 199 |  | 164.8 | 162.2 | 159.6 | 157.1 | 154.5 | 151.9 | 149.3 | 146.8 | 144.2 |
| 200 |  | 165.7 | 163.1 | 160.5 | 157.9 | 155.4 | 152.8 | 150.2 | 147.6 | 145.0 |
| 201 |  | 166.6 | 164.0 | 161.4 | 158.8 | 156.2 | 153.6 | 151.0 | 148.4 | 145.8 |
| 202 |  | 167.6 | 165.0 | 162.3 | 159.7 | 157.1 | ${ }^{1} 54.5$ | ${ }_{151} 5$ | 149.2 | 146.6 |
| 203 |  | 168.5 | 165.9 | 163.2 | 160.6 | 158.0 | ${ }^{1} 55.3$ | 152.7 | 150.1 | 147.4 |
| 204 |  | 169.4 | 166.8 | 164.1 | 161.5 | 158.8 | 156.2 | I53.5 | 150.9 | 148.3 |
| 205 |  | 170.4 | 167.7 | 165.0 | 162.4 | 159.7 | 157.1 | 154.4 | 151.7 | I49.I |
| 206 |  | 171.3 | 168.6 | 165.9 | 163.3 | 160.6 | 157.9 | 155.2 | 152.6 | 149.9 |
| 207 |  | 172.2 | 169.5 | 166.8 | 164.2 | 161.5 | 158.8 | 156.1 | 153.4 | 150.7 |
| 208 |  |  | 170.5 | 167.8 | 165.1 | 162.3 | 159.6 | 156.9 | 154.2 | ${ }^{1} 51.5$ |
| 209 |  |  | 171.4 | 168.7 | 165.9 | 163.2 | 160.5 | 157.8 | 155. I | 152.3 |
| 210 |  |  | 172.3 | 169.6 | 166.8 | 164.1 | 161.4 | 158.6 | 155.9 | 153.2 |
| 211 |  |  | 173.2 | 170.5 | 167.7 | 165.0 | 162.2 | 159.5 | 156.7 | 154.0 |
| 212 |  |  | 174.2 | 171.4 | 168.6 | 165.9 | 163.1 | 160.3 | 157.6 | 154.8 |
| 213 |  |  | 175.1 | 172.3 | 169.5 | 166.7 | 164.0 | 161.2 | 158.4 | ${ }^{1} 55.6$ |
| 214 |  |  | 176.0 | 173.2 | 170.4 | 167.6 | 164.8 | 162.0 | 159.2 | I56.5 |
| 215 |  |  | r76.9 | 174.I | 171.3 | 168.5 | 165.7 | 162.9 | 160. 1 | 157.3 |

table 19.
REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.
$B-B=B\left(10^{m}-1\right)$.
Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m. | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 620 | 610 | 600 | 590 | 580 | 570 | 560 | 550 | 540 | 530 |
|  | mm. | mm. | mm | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| 215 | 174. 1 | ${ }^{171.3}$ | 168.5 | 165.7 | 162.9 | 160.1 | 157.3 | 154.5 | 151.7 | 148.9 |
| 216 | 175.0 | 172.2 | 169.4 | 166.6 | 163.8 | 160.9 | 158.1 | 155.3 | ${ }_{152.5}$ | 149.6 |
| 217 | 176.0 | 173.1 | 170.3 | 167.4 | 164.6 | 161.8 | 158.9 | 156.1 | 153.3 | 150.4 |
| 218 | 176.9 | 174.0 | 171.2 | 168.3 | 165.5 | 162.6 | 159.8 | 156.9 | 154.I | 151.2 |
| 219 | 177.8 | 174.9 | 172.1 | 169.2 | 166.3 | 163.5 | 160.6 | 157.7 | 154.9 | 152.0 |
| 220 | 178.7 | 175.8 | 172.9 | 170.1 | 167.2 | 164.3 | ${ }^{161.4}$ | 158.5 | 155.7 | 152.8 |
| 221 | 179.6 | 176.7 | 173.8 | 170.9 | 168.0 | 165.1 | 162.3 | 159.4 | 156.5 | 153.6 |
| 222 | 180.6 | 177.6 | 174.7 | 171.8 | 168.9 | 166.0 | 163.1 | 160.2 | 157.3 | 154.3 |
| 223 | 18 I .5 | 178.6 | 175.6 | 172.7 | 169.8 | 166.8 | 163.9 | 161.0 | 158.1 | 155.1 |
| 224 | 182.4 | 179.5 | 176.5 | 173.6 | 170.6 | 167.7 | 164.7 | 161. 8 | 158.9 | 155.9 |
| 225 | 183.3 | 180.4 | 177.4 | 174.5 | 171.5 | 168.5 | 165.6 | 162.6 | 159.7 | 156.7 |
| 226 | 184.3 | 181.3 | 178.3 | 175.3 | 172.4 | 169.4 | 166.4 | 163.4 | 160.5 | 157.5 |
| 227 | 185.2 | 182.2 | 179.2 | 176.2 | 173.2 | 170.2 | 167.3 | 164.3 | 161.3 | 158.3 |
| 228 | 186.1 | 183.1 | 180.1 | 177.1 | 174. I | 171.1 | 168.1 | 165.1 | 162.1 | 159. 1 |
| 229 | 187.0 | 184.0 | 181.0 | 178.0 | 175.0 | 172.0 | 168.9 | 165.9 | 162.9 | 159.9 |
| 230 | 188.0 | 184.9 | 181.9 | 178.9 | 175.8 | 172.8 | 169.8 | 166.7 | 163.7 | 160.7 |
| 231 | 188.9 | 185.8 | 182.8 | 179.8 | 176.7 | 173.7 | 170.6 | 167.6 | 164.5 | ${ }^{161.5}$ |
| 232 | 189.8 | 186.8 | 183.7 | 180.6 | 177.6 | 174.5 | 171.5 | 168.4 | 165.3 | 162.3 |
| 233 | 190.8 | 187.7 | 184.6 | 181.5 | 178.5 | 175.4 | 172.3 | 169.2 | 166.1 | 163.1 |
| 234 | 191.7 | 188.6 | 185.5 | 182.4 | 179.3 | 176.2 | 173. 1 | 170.0 | 167.0 | 163.9 |
| 235 | 192.6 | 189.5 |  |  | 180.2 |  | 174.0 | 170.9 | 167.8 | 164.7 |
| 236 |  | 190.4 | 187.3 | 184.2 | 18 r .1 | 178.0 | 174.8 | 171.7 | 168.6 | 165.5 |
| 237 |  | 191.4 | 188.2 | 185.1 | 182.0 | 178.8 | 175.7 | 172.5 | 169.4 | 166.3 |
| 238 |  | 192.3 | 189.1 | 186.0 | 182.8 | 179.7 | 176.5 | 173.4 | 170.2 | 167. I |
| 239 |  | 193.2 | 190.0 | 186.9 | 183.7 | 180.5 | 177.4 | 174.2 | 171.0 | 167.9 |
| 240 |  | 194.1 | 191.0 | 187.8 | 184.6 | 181.4 | 178.2 | 175.0 | 171.9 | 168.7 |
| 241 |  | 195. I | 191.9 | 188.7 | 185.5 | 182.3 | 179.1 | 175.9 | 172.7 | 169.5 |
| 242 |  | 196.0 | 192.8 | 189.6 | 186.4 | 183. 1 | 179.9 | 176.7 | 173.5 | 170.3 |
| 243 |  | 196.9 | 193.7 | 190.5 | 187.2 | 184.0 | 180.8 | 177.5 | 174.3 | 17 I .1 |
| 244 |  | 197.8 | 194.6 | 191.4 | I88. 1 | 184.9 | 181.6 | 178.4 | 175. 1 | 171.9 |
| 245 |  | 198.8 | 195.5 | 192.3 | 189.0 | 185.7 | 182.5 | 179.2 | 176.0 | 172.7 |
| 246 |  | 199.7 | 196.4 | 193.2 | 189.9 | 186.6 | 183.3 | 180.1 | 176.8 | 173.5 |
| 247 |  | 200.6 | 197.4 | 194. I | 190.8 | 187.5 | 184.2 | 180.9 | 177.6 | 174.3 |
| 248 |  | 201.6 | 198.3 | 195.0 | 191.7 | 188.4 | 185.1 | 181.7 | 178.4 | 175.1 |
| 249 |  | 202.5 | 199.2 | 195.9 | 192.6 | 189.2 | 185.9 | 182.6 | 179.3 | 176.0 |
| 250 |  |  | 200.1 | 196.8 | 193.4 | 190.1 | 186.8 | 183.4 | 180.1 | 176.8 |
| 251 |  |  | 201.0 | 197.7 | 194.3 | 191.0 | 187.6 | 184.3 | 180.9 | 177.6 |
| 252 |  |  | 202. | 198.6 | 195.2 | 191.9 | 188.5 | 185.1 | 181.8 | 178.4 |
| 253 |  |  | 202.9 | 199.5 | 196.I | 192.7 | 189.4 |  | 182.6 | 179.2 |
| 254 |  |  | 203.8 | 200.4 | 197.0 | 193.6 | 190.2 | 186.8 | 183.4 | 180.0 |
| 255 |  |  | 204.7 | 201.3 | 197.9 | 194.5 | 191.1 | 187.7 | 184.3 | 180.8 |
| 256 |  |  | 205.7 | 202.2 | 198.8 | 195.4 | 191.9 | 188.5 | 185.1 | 181.7 |
| ${ }^{257}$ |  |  | 206.6 | 203.1 | 199.7 | 196.3 | 192.8 | 189.4 | 185.9 | 182.5 |
| 258 259 |  |  | 207.5 208.4 | 204.1 205.0 | 200.6 201.5 | 197.1 198.0 | 193.7 194.6 | 190.2 191.1 | 186.8 1876 | 183.3 184.1 |
| 260 |  |  | 209.4 | 205.9 | 202.4 | 198.9 | 195.4 | 191.9 | 188.4 | 185.0 |

TABLE 13.
REDUCTION OF THE BAROMETER TO SEA LEVEL.
METRIC MEASURES.

$$
B_{0}-B=B\left(10^{m}-1\right)
$$

Top argument: Height of the barometer (B).
Side argument: Values of 2000 m obtained from Table 17.

| 2000 m. | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 590 | 580 | 570 | 560 | 550 | 540 | 530 | 520 | 510 |
|  | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm . |
| 260 | 205.9 | 202.4 | 198.9 | 195.4 | 191.9 | 188.4 | 185.0 | 181.5 | 178.0 |
| 261 | 206.8 | 203.3 | 199.8 | 196.3 | 192.8 | 189.3 | 185.8 | 182.3 | 178.8 |
| 262 | 207.7 | 204.2 | 200.7 | 197.2 | 193.6 | 190.1 | 186.6 | 183.1 | 179.6 |
| 263 | 208.6 | 205. I | 201.6 | 198.0 | 194.5 | 191.0 | 187.4 | 183.9 | 180.4 |
| 264 | 209.6 | 206.0 | 202.5 | 198.9 | 195.4 | 191.8 | 188.3 | 184.7 | 181. 1 |
| 265 | 210.5 | 206.9 | 203.3 | 199.8 | 196.2 | 192.6 | 189.1 | 185.5 | 181.9 |
| 266 | 211.4 | 207.8 | 204.2 | 200.7 | 197.1 | 193.5 | 189.9 | 186.3 | 182.7 |
| 267 | 212.3 | 208.7 | 205. 1 | 201.5 | 197.9 | 194.3 | 190.7 | 187.1 | 183.5 |
| 268 | 213.3 | 209.6 | 206.0 | 202.4 | 198.8 | 195.2 | 191.6 | 188.0 | 184.3 |
| 269 | 214.2 | 210.5 | 206.9 | 203.3 | 199.7 | 196.0 | 192.4 | 188.8 | 185.1 |
| 270 | 215.1 | 211.5 | 207.8 | 204.2 | 200.5 | 196.9 | 193.2 | 189.6 | 185.9 |
| 271 | 216.0 | 212.4 | 208.7 | 205.0 | 201.4 | 197.7 | 194.1 | 190.4 | 186.7 |
| 272 | 217.0 | 213.3 | 209.6 | 205.9 | 202.3 | 198.6 | 194.9 | 191.2 | 187.5 |
| 273 | 217.9 | 214.2 | 210.5 | 206.8 | 203.1 | 199.4 | 195.7 | 192.0 | 188.3 |
| 274 | 218.8 | 215.1 | 211.4 | 207.7 | 204.0 | 200.3 | 196.6 | 192.9 | 189. 1 |
| 275 | 219.8 | 216.0 | 212.3 | 208.6 | 204.9 | 201.1 | 197.4 | 193.7 | 190.0 |
| 276 | 220.7 | 216.9 | 213.2 | 209.5 | 205.7 | 202.0 | 198.2 | 194.5 | 190.8 |
| 277 | 221.6 | 217.9 | 214.1 | 210.3 | 206.6 | 202.8 | 199.I | 195.3 | 191. 6 |
| 278 | 222.6 | 218.8 | 215.0 | 211.2 | 207.5 | 203.7 | 199.9 | 196.1 | 192.4 |
| 279 | 223.5 | 219.7 | 215.9 | 212.1 | 208.3 | 204.5 | 200.8 | 197.0 | 193.2 |
| 280 |  | 220.6 | 216.8 | 213.0 | 209.2 | 205.4 | 201.6 | 197.8 | 194.0 |
| 281 |  | 221.5 | 217.7 | 213.9 | 210.1 | 206.3 | 202.4 | 198.6 | 194.8 |
| 282 |  | 222.5 | 218.6 | 214.8 | 211.0 | 207.1 | 203.3 | 199.5 | 195.6 |
| 283 |  | 223.4 | 219.5 | 215.7 | 211.8 | 208.0 | 203.1 | 200.3 | 196.4 |
| 284 |  | 224.3 | 220.5 | 216.6 | 212.7 | 208.8 | 205.0 | 201.1 | 197.2 |
| 285 |  | 225.2 | 221.4 | 217.5 | 213.6 | 209.7 | 205.8 | 201.9 | 198. 1 |
| 286 |  | 226.2 | 222.3 | 218.4 | 214.5 | 210.6 | 206.7 | 202.8 | 198.9 |
| 287 |  | 227.1 | 223.2 | 219.3 | 215.4 | 2 II .4 | 207.5 | 203.6 | 199.7 |
| 288 |  | 228.0 | 224.1 | 220.2 | 216.2 | 212.3 | 208.4 | 204.4 | 200.5 |
| 289 |  | 229.0 | 225.0 | 221. I | 217.1 | 213.2 | 209.2 | 205.3 | 20 I .3 |
| 290 |  | 229.9 | 225.9 | 222.0 | 218.0 | 214.0 | 210.1 | 206.1 | 202.I |
| 291 |  | 230.8 | 226.8 | 222.9 | 218.9 | 214.9 | 210.9 | 206.9 | 203.0 |
| 292 |  | 231.8 | 227.8 | 223.8 | 219.8 | 215.8 | 211.8 | 207.8 | 203.8 |
| 293 |  | 232.7 | 228.7 | 224.7 | 220.7 | 216.6 | 212.6 | 208.6 | 204.6 |
| 294 |  | 233.6 | 229.6 | 225.6 | 221.5 | 217.5 | 2 I 3.5 | 209.5 | 205.4 |
| 295 |  |  | 230.5 | 226.5 | 222.4 | 218.4 | 214.3 | 210.3 | 206.3 |
| 296 |  |  | 231.4 | 227.4 | 223.3 | 219.3 | 215.2 | 211.1 | 207. I |
| 297 |  |  | 232.4 | 228.3 | 224.2 | 220.1 | 216.1 | 212.0 | 207.9 |
| 298 |  |  | $233 \cdot 3$ | 229.2 | 225.1 | 221.0 | 216.9 | 212.8 | 208.7 |
| 299 |  |  | 234.2 | 230.1 | 226.0 | 221.9 | 217.8 | 213.7 | 209.6 |
| 300 |  |  | 235. I | 231.0 | 226.9 | 222.8 | 218.6 | 214.5 | 210.4 |
| 301 |  |  | 236.1 | 231.9 | 227.8 | 223.6 | 219.5 | 215.4 | 2 II .2 |
| 302 |  |  | 237.0 | 232.8 | 228.7 | 224.5 | 220.4 | 216.2 | 212.1 |
| 303 |  |  | 237.9 | 233.8 | 229.6 | 225.4 | 221.2 | 217.1 | 212.9 |
| 304 |  | - | 238.9 | 234.7 | 230.5 | 226.3 | 222.I | 217.9 | 213.7 |
| 305 |  |  | 239.8 | 235.6 | 231.4 | 227.2 | 223.0 | 218.8 | 214.6 |

TAble 19.
REDUCTION OF THE BAROMETER TO SEA LEVEL. METRIC MEASURES.

$$
B_{0}-B=B\left(10^{m}-1\right) \text {. }
$$

Top argument: Height of the barometer (B).
Side argument : Values of 2000 m obtained from Table 17.

| 2000 m. | HEIGHT OF THE BAROMETER IN MILLIMETRES. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 560 | 550 | 540 | 530 | 520 | 510 | 500 | 490 | 480 |
|  | mm . | mm . | mm. | mm. | mm . | mm. | mm. | mm. | mm. |
| 305 | 235.6 | 231.4 | 227.2 | 223.0 | 218.8 | 214.6 | 210.3 | 206. I | 201.9 |
| 306 | 236.5 | 232.3 | 228.0 | 223.8 | 219.6 | 215.4 | 211.2 | 206.9 | 202.7 |
| 307 | 237.4 | 233.2 | 228.9 | 224.7 | 220.5 | 216.2 | 212.0 | 207.7 | 203.5 |
| 308 | 238.3 | 234 . 1 | 229.8 | 225.6 | 221.3 | 217.1 | 212.8 | 208.5 | 204.3 |
| 309 | 239.2 | 235.0 | 230.7 | 226.4 | 222.2 | 217.9 | 213.6 | 209.4 | 205. 1 |
| 310 | 240.2 | 235.9 | 231.6 | 227.3 | 223.0 | 218.7 | 214.4 | 210.1 | 205.9 |
| 3 II | 241. I | 236.8 | 232.5 | 228.2 | 223.9 | 219.6 | 215.3 | 211.0 | 206.7 |
| 312 | 242.0 | 237.7 | 233.4 | 229.1 | 224.7 | 220.4 | 216.1 | 2II. 8 | 207.5 |
| 313 | 242.9 | 238.6 | 234.3 | 229.9 | 225.6 | 221.2 | 216.9 | 2I 2.6 | 208.2 |
| 314 | 243.9 | 239.5 | 235.2 | 230.8 | 226.4 | 222. 1 | 217.7 | 213.4 | 209.0 |
| 315 | 244.8 | 240.4 | 236.0 | 231.7 | 227.3 | 222.9 | 218.6 | 214.2 | 209.8 |
| 316 | 245.7 | 241.3 | 237.0 | 232.6 | 228.2 | 223.8 | 219.4 | 215.0 | 210.6 |
| 317 | 246.6 | 242.2 | 237.8 | 233.4 | 229.0 | 224.6 | 220.2 | 215.8 | 2 II .4 |
| 318 | 247.6 | 243.2 | 238.7 | 234.3 | 229.9 | 225.5 | 22I. 1 | 216.6 | 212.2 |
| 319 | 248.5 | 244.1 | 239.6 | 235.2 | 230.8 | 226.3 | 221.9 | 217.4 | 213.0 |
| 320 | 249.4 | 245.0 | 240.5 | 236. 1 | 231.6 | 227.2 | 222.7 | 218.3 | 213.8 |
| 321 | 250.4 | 245.9 | 241.4 | 237.0 | 232.5 | 228.0 | 223.6 | 219.1 | 214.6 |
| 322 | 251.3 | 246.8 | 242.3 | 237.8 | 233.4 | 228.9 | 224.4 | 219.9 | 215.4 |
| 323 | 252.2 | 247.7 | 243.2 | 238.7 | 234.2 | 229.7 | 225.2 | 220.7 | 216.2 |
| 324 | 253.2 | 248.7 | 244. I | 239.6 | 235.1 | 230.6 | 226.0 | 221.5 | 217.0 |
| 325 | 254. I | 249.6 | 245.0 | 240.5 | 236.0 | 231.4 | 226.9 | 222.4 | 217.8 |
| 326 |  | 250.5 | 245.9 | 241.4 | 236.8 | 232.3 | 227.7 | 223.2 | 218.6 |
| 327 |  | 25 I .4 | 246.8 | 242.3 | 237.7 | 233.1 | 228.6 | 224.0 | 219.4 |
| 328 |  | 252.3 | 247.7 | 243.2 | 238.6 | 234.0 | 229.4 | 224.8 | 220.2 |
| 329 |  | 253.3 | 248.7 | 244.0 | 239.4 | 234.8 | 230.2 | 225.6 | 221.0 |
| 330 |  | 254.2 | 249.6 | 244.9 | 240.3 | 235.7 | 231.1 | 226.5 | 221.8 |
| 331 |  | 255. I | 250.5 | 245.8 | 241.2 | 236.6 | 231.9 | 227.3 | 222.6 |
| 332 |  | 256.0 | 25 I .4 | 246.7 | 242.1 | 237.4 | 232.8 | 228. 1 | 223.5 |
| 333 |  | 257.0 | 252.3 | 247.6 | 243.0 | 238.3 | 233.6 | 228.9 | 224.3 |
| 334 |  | 257.9 | 253.2 | 248.5 | 243.8 | 239.2 | 234.5 | 229.8 | 225. I |
| 335 |  | 258.8 | 254. I | 249.4 | 244.7 | 240.0 | 235.3 | 230.6 |  |
| 336 |  | 259.8 | 255.0 | 250.3 | 245.6 | 240.9 | 236.2 | 231.4 | 226.7 |
| 337 |  | 260.7 | 256.0 | 251.2 | 246.5 | 241.7 | 237.0 | 232.3 | 227.5 |
| 338 |  | 261.6 | 256.9 | 252.1 | 247.4 | 242.6 | 237.8 | 233.1 | 228.3 |
| 339 |  | 262.6 | 257.8 | 253.0 | 248.2 | 243.5 | 238.7 | 233.9 | 229.2 |
| 340 |  | 263.5 | 258.7 | 253.9 | 249. 1 | 244.4 | 239.6 | 234.8 | 230.0 |
| 341 |  | 264.4 | 259.6 | 254.8 | 250.0 | 245.2 | 240.4 | 235.6 | 230.8 |
| 342 |  |  | 260.6 | 255.7 | 250.9 | 246. I | 24.3 | 236.4 | 231.6 |
| 343 |  |  | 261.5 | 256.6 | 25 I .8 | 247.0 | 242.1 | 237.3 | 232.4 |
| 344 |  |  | 262.4 | 257.5 | 252.7 | 247.8 | 243.0 | 238.1 | 233.2 |
| 345 |  |  | 263.3 | 258.4 | 253.6 | 248.7 | 243.8 | 238.9 | 234. 1 |

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DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$.

| Barometric Pressure. B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 12.00 | 24814 | 24791 | 24769 | 24746 | 24723 | 24701 | 24678 | 24656 | 24633 | 246II |
| 12.10 | 24588 | 24566 | 24543 | 24521 | 24499 | 24476 | 24454 | 24431 | 24409 | 24387 |
| 12.20 | 24365 | 24342 | 24320 | 24298 | 24276 | 24253 | 24231 | 24209 | 24187 | 24165 |
| 12.30 | 24143 | 24121 | 24098 | 24076 | 24054 | 24032 | 24010 | 23988 | 23966 | 23944 |
| 12.40 | 23923 | 23901 | 23879 | 23857 | 23835 | 23813 | 23791 | 23770 | 23748 | 23726 |
| 12.50 | 23704 | 23682 | 23661 | 23639 | 23617 | 23596 | 23574 | 23552 | 23531 | 23509 |
| 12.60 | 23488 | 23466 | 23445 | 23423 | 23402 | 23380 | 23359 | 23337 | 23316 | 23294 |
| 12.70 | 23273 | 23251 | 23230 | 23209 | 23187 | 23166 | 23145 | 23123 | 23102 | 23081 |
| 12.80 | 23060 | 23038 | 23017 | 22996 | 22975 | 22954 | 22933 | 22911 | 22890 | 22869 |
| 12.90 | 22848 | 22827 | 22806 | 22785 | 22764 | 22743 | 22722 | 22701 | 22680 | 22659 |
| 13.00 | 22638 | 22617 | 22596 | 22576 | 22555 | 22534 | 22513 | 22492 | 22471 | 22451 |
| 13.10 | 22430 | 22409 | 22388 | 22368 | 22347 | 22326 | 22306 | 22285 | 22264 | 22244 |
| I3.20 | 22223 | 22203 | 22182 | 22162 | 22141 | 22121 | 22100 | 22080 | 22059 | 22039 |
| I3.30 | 22018 | 21998 | 21977 | 21957 | 21937 | 21916 | 21896 | 21876 | 21855 | 21835 |
| 13.40 | 21815 | 21794 | 21774 | 21754 | 21734 | 21713 | 21693 | 21673 | 21653 | 21633 |
| 13.50 | 21612 | 21592 | 21572 | 21552 | 21532 | 21512 | 21492 | 21472 | 21452 | 21432 |
| 13.60 | 21412 | 21392 | 21372 | 21352 | 21332 | 21312 | 21292 | 21272 | 21252 | 21233 |
| 13.70 | 21213 | 21193 | 21173 | 21153 | 21134 | 2III4 | 21094 | 21074 | 21054 | 21035 |
| 13.80 | 21015 | 20995 | 20976 | 20956 | 20936 | 20917 | 20897 | 20878 | 20858 | 20838 |
| 13.90 | 20819 | 20799 | 20780 | 20760 | 20741 | 20721 | 20702 | 20682 | 20663 | 20643 |
| 14.00 | 20624 | 20605 | 20585 | 20566 | 20546 | 20527 | 20508 | 20488 | 20469 | 20450 |
| 14.10 | 20431 | 20411 | 20392 | 20373 | 20354 | 20334 | 20315 | 20296 | 20277 | 20258 |
| 14.20 | 20238 | 20219 | 20200 | 20181 | 20162 | 20143 | 20124 | 20105 | 20086 | 20067 |
| 14.30 | 20048 | 20029 | 20010 | 19991 | 19972 | 19953 | 19934 | 19915 | 19896 | 19877 |
| 14.40 | 19858 | 19839 | 19821 | 19802 | 19783 | 19764 | 19745 | 19727 | 19708 | 19689 |
| 14.50 | 19670 | 19651 | 19633 | 19614 | 19595 | 19577 | 19558 | 19539 | 19521 | 19502 |
| 14.60 | 19483 | 19465 | 19446 | 19428 | 19409 | 19390 | 19372 | 19353 | 19335 | 19316 |
| 14.70 | 19298 | 19279 | 1926I | 19242 | 19224 | 19206 | 19187 | 19169 | 19150 | 19132 |
| 14.80 | 19114 | 19095 | 19077 | 19059 | 19040 | 19022 | 19004 | 18985 | 18967 | 18949 |
| 14.90 | 1893I | 18912 | 18894 | 18876 | 18858 | I8840 | I882I | 18803 | 18785 | 18767 |
| 15.00 | 18749 | 18731 | 18713 | 18694 | 18676 | I8658 | 18640 | I8622 | 18604 | I8586 |
| 15.10 | 18568 | 18550 | 18532 | 18514 | 18496 | 18478 | 18460 | 18442 | 18425 | 18407 |
| 15.20 | 18389 | 18371 | 18353 | 18335 | 18317 | 18300 | 18282 | 18264 | 18246 | 18228 |
| 15.30 | 18211 | 18193 | 18175 | I8I57 | 18140 | 18122 | I8104 | I8o86 | 18069 | 18051 |
| 15.40 | I8033 | I8016 | 17998 | 17981 | 17963 | I7945 | 17928 | 17910 | 17893 | 17875 |
| 15.50 | I7858 | 17840 | 17823 . | 17805 | 17788 | 17770 | 17753 | 17735 | 17718 | 17700 |
| 15.60 | 17683 | 17665 | 17648 | 17631 | 17613 | 17596 | 17578 | 17561 | 17544 | 17526 |
| 15.70 | 17509 | 17492 | 17474 | 17457 | 17440 | 17423 | 17405 | 17388 | 17371 | 17354 |
| 15.80 | 17337 | 17319 | 17302 | 17285 | 17268 | 17251 | 17234 | 17216 | 17199 | 17182 |
| 15.90 | I7165 | 17148 | 17131 | I7II4 | 17097 | 17080 | 17063 | 17046 | 17029 | 17012 |
| 16.00 | 16995 | 16978 | 1696I | 16944 | 16927 | 16910 | 16893 | 16876 | 16859 | 16842 |
| 16.10 | 16825 | 16808 | 16792 | 16775 | 16758 | 16741 | 16724 | 16707 | 16691 | 16674 |
| 16.20 | 16657 | 16640 | 16623 | 16607 | 16590 | 16573 | 16557 | 16540 | 16523 | 16506 |
| 16.30 | 16490 | 16473 | 16456 | 16440 | 16423 | 16406 | 16390 | 16373 | 16357 | 16340 |
| 16.40 | 16324 | 16307 | 16290 | 16274 | 16257 | 1624I | 16224 | 16208 | 16191 | 16175 |
| 16.50 | 16158 | 16142 | 16125 | 16109 | 16092 | 16076 | 16060 | 16043 | 16027 | 16010 |
| 16.60 | 15994 | 15978 | 15961 | 15945 | 15929 | 15912 | 15896 | 15880 | 15863 | 15847 |
| 16.70 | 15831 | 15815 | 15798 | 15782 | 15766 | 15750 | 15733 | 15717 | 15701 | 15685 |
| 16.80 | 15669 | 15652 | 15636 | 15620 | 15604 | 15588 | 15572 | ${ }^{1} 5556$ | 15539 | 15523 |
| 16.90 | 15507 | 15491 | 15475 | I5459 | I5443 | 15427 | 15411 | I5395 | I5379 | 15363 |
| 17.00 | 15347 | 15331 | 15315 | 15299 | 15283 | 15267 | 15251 | 15235 | 15219 | 15203 |

Smithsonian Tables.

TABLE 20.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$.

| Barometric Pressure B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 17.00 | I5347 | 1533 I | 15315 | I5299 | 15283 | 15267 | 15251 | 15235 | 15219 | 15203 |
| 17.10 | 15187 | 15172 | I5156 | 15140 | 15124 | 15108 | 15092 | 15076 | 15061 | 15045 |
| 17.20 | 15029 | 15013 | 14997 | 14982 | 14966 | 14950 | 14934 | 14919 | 14903 | 14887 |
| 17.30 | 14871 | 14856 | 14840 | 14824 | 14809 | 14793 | 14777 | 14762 | 14746 | 14730 |
| 17.40 | 14715 | 14699 | 14684 | 14668 | 14652 | 14637 | 1462I | 14606 | 14590 | I4575 |
| 17.50 | 14559 | 14544 | 14528 | 14512 | 14497 | 1448I | 14466 | 1445I | 14435 | 14420 |
| 17.60 | 14404 | 14389 | 14373 | 14358 | 14342 | 14327 | 14312 | 14296 | 14281 | 14266 |
| 17.70 | 14250 | 14235 | 14219 | 14204 | 14189 | 14173 | 14158 | 14143 | 14128 | 14112 |
| 17.80 | 14097 | 14082 | 14067 | 14051 | 14036 | 14021 | 14006 | 13990 | 13975 | 13960 |
| 17.90 | I 3945 | I 3930 | 13914 | 13899 | I 3884 | 13869 | 13854 | 13839 | 13824 | 13808 |
| 18.00 | I 3793 | 13778 | 13763 | 13748 | 13733 | 13718 | 13703 | I3688 | 13673 | I3658 |
| 18.10 | 13643 | I3628 | 13613 | 13598 | 13583 | 13568 | I 3553 | 13538 | 13523 | I3508 |
| 18.20 | 13493 | I 3478 | I 3463 | 13448 | 13433 | 13418 | 13404 | 13389 | 13374 | I 3359 |
| 18.30 | 13314 | I 3329 | I 3314 | 13300 | 13285 | 13270 | 13255 | 13240 | 13226 | I32II |
| 18.40 | 13196 | I3I81 | I3166 | 13152 | I3137 | 13122 | 13107 | 13093 | 13078 | I3063 |
| 18.50 | 13049 | I3034 | 13019 | 13005 | 12990 | 12975 | 12961 | 12946 | 12931 | 12917 |
| 18.60 | 12902 | 12888 | 12873 | 12858 | 12844 | 12829 | 12815 | 12800 | 12785 | 12771 |
| 18.70 | 12756 | 12742 | 12727 | 12713 | 12698 | 12684 | 12669 | 12655 | 12640 | 12626 |
| 18.80 | T26II | 12597 | 12583 | 12568 | 12554 | 12539 | 12525 | 12510 | 12496 | 12482 |
| 18.90 | 12467 | 12453 | 12438 | 12424 | 12410 | 12395 | 12381 | 12367 | 12352 | 12338 |
| 19.00 | 12324 | 12310 | 12295 | 1228I | 12267 | 12252 | 12238 | 12224 | 12210 | 12195 |
| 19.10 | 12181 | 12167 | I2153 | 12138 | 12124 | 12110 | 12096 | 12082 | 12068 | 12053 |
| 19.20 | 12039 | 12025 | 12011 | 11997 | 11983 | 11969 | 11954 | 11940 | 11926 | 11912 |
| 19.30 | 11898 | II884 | 11870 | 11856 | II842 | II828 | IISI4 | 11800 | 11786 | 11772 |
| 19.40 | 11758 | II744 | 11730 | II716 | 11702 | 11688 | II674 | 11660 | 11646 | 11632 |
| 19.50 | II6I8 | II604 | II590 | II576 | I 1562 | I I548 | II534 | II520 | 11507 | I I493 |
| 19.60 | II479 | I 1465 | II451 | II437 | I 1423 | 11410 | II396 | II382 | II368 | II354 |
| 19.70 | II340 | II327 | I13I3 | II299 | I 1285 | 11272 | 11258 | II244 | 11230 | 11217 |
| 19.80 | 11203 | III89 | III75 | III62 | III48 | III34 | III2I | I I 107 | 11093 | 11080 |
| 19.90 | 11066 | 11052 | IIO39 | 11025 | IIOII | 10998 | 10984 | 10970 | 10957 | 10943 |
| 20.00 | 10930 | 10916 | 10903 | 10889 | 10875 | 10862 | 10848 | 10835 | 10821 | 10808 |
| 20.10 | 10794 | 10781 | 10767 | 10754 | 10740 | 10727 | 10713 | 10700 | 10686 | 10673 |
| 20.20 | 10659 | 10646 | 10632 | 10619 | 10605 | 10592 | 10579 | I0565 | 10552 | 10538 |
| 20.30 | 10525 | 10512 | 10498 | 10485 | 10472 | 10458 | 10445 | 1043I | 10418 | 10405 |
| 20.40 | 10391 | 10378 | 10365 | 10352 | 10338 | 10325 | 10312 | 10298 | IO 285 | 10272 |
| 20.50 | 10259 | 10245 | 10232 | 10219 | 10206 | Ior92 | IOI79 | IOI66 | IOI53 | IOI39 |
| 20.60 | 10126 | IOII3 | 10100 | 10087 | 10074 | 10060 | 10047 | 10034 | 10021 | 10008 |
| 20.70 | 9995 | 9982 | 9968 | 9955 | 9942 | 9929 | 9916 | 9903 | 9890 | 9877 |
| 20.80 | 9864 | 985 I | 9838 | 9825 | 9812 | 9799 | 9786 | 9772 | 9759 | 9746 |
| 20.90 | 9733 | 9720 | 9707 | 9694 | 968I | 9668 | 9655 | 9642 | 9629 | 9617 |
| 21.00 | 9604 | 9591 | 9578 | 9565 | 9552 | 9539 | 9526 | 9513 | 9500 | 9487 |
| 2 I .10 | 9474 | 9462 | 9449 | 9436 | 9423 | 9410 | 9397 | 9384 | 9372 | 9359 |
| 21.20 | 9346 | 9333 | 9320 | 9307 | 9295 | 9282 | 9269 | 9256 | 9244 | 9231 |
| 21.30 | 92 I 8 | 9205 | 9193 | 9180 | 9167 | 9154 | 9142 | 9129 | 9116 | 9103 |
| 21.40 | 9091 | 9078 | 9065 | 9053 | 9040 | 9027 | 9015 | 9002 | 8989 | 8977 |
| 21.50 | 8964 | 8951 | 8939 | 8926 | 8913 | 8901 | 8888 | 8876 | 8863 | 8850 |
| 21.60 | 8838 | 8825 | 8813 | 8800 | 8788 | 8775 | 8762 | 8750 | 8737 | 8725 |
| 21.70 | 8712 | 8700 | 8687 | 8675 | 8662 | 8650 | 8637 | 8625 | 8612 | 8600 |
| 21.80 | 8587 | 8575 | 8562 | 8550 | 8538 | 8525 | 8513 | 8500 | 8488 | 8475 |
| 21.90 | 8463 | 845 I | 8438 | 8426 | 8413 | 8401 | 8389 | 8376 | 8364 | 8352 |
| 22.00 | 8339 | 8.327 | 8314 | 8302 | 8290 | 8277 | 8265 | 8253 | 8240 | 8228 |

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$.

| Barometric Pressure. B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 22.00 | 8339 | 8327 | 8314 | 8302 | 8290 | 8277 | 8265 | 8253 | 8240 | 8228 |
| 22.10 | 8216 | 8204 | 8191 | 8179 | 8167 | 8 I 54 | 8142 | 8130 | 8ı18 | 8105 |
| 22.20 | So93 | 8081 | 8069 | 8056 | 8044 | 8032 | 8020 | 8008 | 7995 | 7983 |
| 22.30 | 7971 | 7959 | 7947 | 7935 | 7922 | 7910 | 7898 | 7886 | 7874 | 7862 |
| 22.40 | 7849 | 7837 | 7825 | 7813 | 7801 | 7789 | 7777 | 7765 | 7753 | 7740 |
| 22.50 | 7728 | 7716 | 7704 | 7692 | 7680 | 7668 | 7656 | 7644 | 7632 | 7620 |
| 22.60 | 7608 | 7596 | 7584 | 7572 | 7560 | 7548 | 7536 | 7524 | 7512 | 7500 |
| 22.70 | 7488 | 7476 | 7464 | 7452 | 7440 | 7428 | 7416 | 7404 | 7392 | 7380 |
| 22.80 | 7368 | 7356 | 7345 | 7333 | 7321 | 7309 | 7297 | 7285 | 7273 | 7261 |
| 22.90 | 7249 | 7238 | 7226 | 7214 | 7202 | 7190 | 7178 | 7166 | 7155 | 7143 |
| 23.00 | 7131 | 7119 | 7107 | 7096 | 7084 | 7072 | 7060 | 7048 | 7037 | 7025 |
| 23.10 | 7013 | 7001 | 6990 | 6978 | 6966 | 6954 | 6943 | 6931 | 6919 | 6907 |
| 23.20 | 6896 | 6884 | 6872 | 686I | 6849 | 6837 | 6825 | 6814 | 6802 | 6790 |
| 23.30 | 6779 | 6767 | 6755 | 6744 | 6732 | 6721 | 6709 | 6697 | 6686 | 6674 |
| 23.40 | 6662 | 6651 | 6639 | 6628 | 6616 | 6604 | 6593 | 6581 | 6570 | 6558 |
| 23.50 | 6546 | 6535 | 6523 | 6512 | 6500 | 6489 | 6477 | 6466 | 6454 | 6443 |
| 23.60 | 6431 | 6420 | 6408 | 6397 | 6385 | 6374 | 6362 | 6351 | 6339 | 6328 |
| 23.70 | 6316 | 6305 | 6293 | 6282 | 6270 | 6259 | 6247 | 6236 | 6225 | 6213 |
| 23.80 | 6202 | 6190 | 6179 | 6167 | 6156 | 6145 | 6 I 33 | 6122 | 6110 | 6099 |
| 23.90 | 6088 | 6076 | 6065 | 6054 | 6042 | 6031 | 6020 | 6008 | 5997 | 5986 |
| 24.00 | 5974 | 5963 | 5952 | 5940 | 5929 | 5918 | 5906 | 5895 | 5884 | 5872 |
| 24.10 | 5861 | 5850 | 5839 | 5827 | 5816 | 5805 | 5794 | 5782 | 5771 | 5760 |
| 24.20 | 5749 | 5737 | 5726 | 5715 | 5704 | 5693 | 568ı | 5670 | 5659 | 5648 |
| 24.30 | 5637 | 5625 | 5614 | 5603 | 5592 | 558 I | 5570 | 5558 | 5547 | 5536 |
| 24.40 | 5525 | 5514 | 5503 | 5492 | 5480 | 5469 | 5458 | 5447 | 5436 | 5425 |
| 24.50 | 5414 | 5403 | 5392 | 5381 | 5369 | 5358 | 5347 | 5336 | 5325 | 5314 |
| 24.60 | 5303 | 5292 | 5281 | 5270 | 5259 | 5248 | 5237 | 5226 | 5215 | 5204 |
| 24.70 | 5193 | 5182 | 5171 | 5160 | 5149 | 5138 | 5127 | 5116 | 5105 | 5094 |
| 24.80 | 5083 | 5072 | 506I | 5050 | 5039 | 5028 | 5017 | 5006 | 4995 | 4985 |
| 24.90 | 4974 | 4963 | 4952 | 4941 | 4930 | 4919 | 4908 | 4897 | 4886 | 4876 |
| 25.00 | 4865 | 4854 | 4843 | 4832 | 4821 | 4810 | 4800 | 4789 | 4778 | 4767 |
| 25.10 | 4756 | 4745 | 4735 | 4724 | 4713 | 4702 | 4691 | 468 I | 4670 | 4659 |
| 25.20 | 4648 | 4637 | 4627 | 4616 | 4605 | 4594 | 4584 | 4573 | 4562 | 4551 |
| 25.30 | 4540 | 4530 | 4519 | 4508 | 4498 | 4487 | 4476 | 4465 | 4455 | 4444 |
| 25.40 | 4433 | 4423 | 4412 | 4401 | 4391 | 4380 | 4369 | 4358 | 4348 | 4337 |
| 25.50 | 4326 | 4316 | 4305 | 4295 | 4284 | 4273 | 4263 | 4252 | 4241 | 4231 |
| 25.60 | 4220 | 4209 | 4199 | 4188 | 4178 | 4167 | 4156 | 4146 | 4135 | 4125 |
| 25.70 | 4114 | 4104 | 4093 | 4082 | 4072 | 4061 | 4051 | 4040 | 4030 | 4019 |
| 25.80 | 4009 | 3998 | 3988 | 3977 | 3966 | 3956 | 3945 | 3935 | 3924 | 3914 |
| 25.90 | 3903 | 3893 | 3882 | 3872 | 3861 | 3851 | 384 I | 3830 | 3820 | 3809 |
| 26.00 | 3799 | 3788 | 3778 | 3767 | 3757 | 3746 | 3736 | 3726 | 3715 | 3705 |
| 26.10 | 3694 | 3684 | 3674 | 3663 | 3653 | 3642 | 3632 | 3622 | 3611 | 3601 |
| 26.20 | 3590 | 3580 | 3570 | 3559 | 3549 | 3539 | 3528 | 3518 | 3508 | 3497 |
| 26.30 | 3487 3384 | 3477 | 3466 | 3456 | 3446 | 3435 | 3425 3322 | 3415 | 3404 | 3394 |
| 26.40 | 3384 | 3373 | 3363 | 3353 | 3343 | 3332 | 3322 | 3312 | 3301 | 3291 |
| 26.50 | 3281 | 3270 | 3260 | 3250 | 3240 | 3230 | 3219 | 3209 | 3199 | 3189 |

TABLE 20.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \underset{B}{29.90}$

| Barometric Pressure. B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 26.50 | 328I | 3270 | 3260 | 3250 | 3240 | 3230 | 3219 | 3209 | 3199 | 3189 |
| 26.60 | 3179 | 3168 | 3158 | 3148 | 3138 | 3128 | 3117 | 3107 | 3097 | 3087 |
| 26.70 | 3077 | 3066 | 3056 | 3046 | 3036 | 3026 | 3016 | 3005 | 2995 | 2985 |
| 26.80 | 2975 | 2965 | 2955 | 2945 | 2934 | 2924 | 2914 | 2904 | 2894 | 2884 |
| 26.90 | 2874 | 2864 | 2854 | 2843 | 2833 | 2823 | 2813 | 2 SO 3 | 2793 | 2783 |
| 27.00 | 2773 | 2763 | 2753 | 2743 | 2733 | 2723 | 2713 | 2703 | 2692 | 2682 |
| 27.10 | 2672 | 2662 | 2552 | 2642 | 2632 | 2622 | 2612 | 2602 | 2592 | 2582 |
| 27.20 | 2572 | 2562 | 2552 | 2542 | 2532 | 2522 | 2512 | 2502 | 2493 | 2483 |
| 27.30 | 2473 | 2463 | 2453 | 2443 | 2433 | 2423 | 2413 | 2403 | 2393 | 2383 |
| 27.40 | 2373 | 2363 | 2353 | 2343 | 2334 | 2324 | 2314 | 2304 | 2294 | 2284 |
| 27.50 | 2274 | 2264 | 2254 | 2245 | 2235 | 2225 | 2215 | 2205 | 2195 | 2185 |
| 27.60 | 2176 | 2166 | 2156 | 2146 | 2 I 36 | 2126 | 2116 | 2107 | 2097 | 2087 |
| 27.70 | 2077 | 2067 | 2058 | 2048 | 2038 | 2028 | 2018 | 2009 | 1999 | 1989 |
| 27.80 | 1979 | 1970 | 1960 | 1950 | 1940 | 1930 | 1921 | 1911 | I901 | 1891 |
| 27.90 | I882 | 1872 | 1862 | 1852 | 1843 | 1833 | 1823 | 1814 | 1804 | I794 |
| 28.00 | 1784 | 1775 | 1765 | 1755 | 1746 | 1736 | 1726 | 1717 | 1707 | 1697 |
| 28.10 | 1688 | 1678 | 1668 | 1659 | I649 | 1639 | 1630 | 1620 | 1610 | I601 |
| 28.20 | 1591 | 1581 | 1572 | 1562 | I552 | I 543 | 1533 | 1524 | 1514 | I 504 |
| 28.30 | 1495 | 1485 | 1476 | 1466 | 1456 | 1447 | 1437 | 1428 | 1418 | 1408 |
| 28.40 | I 399 | 1389 | 1380 | I 370 | I36I | 1351 | I 342 | 1332 | 1322 | I3 13 |
| 28.50 | 1303 | 1294 | 1284 | 1275 | I 265 | 1256 | 1246 | 1237 | 1227 | 1218 |
| 28.60 | 1208 | I 199 | 1189 | 1180 | 1170 | 1161 | 1151 | 1142 | 11.32 | 1123 |
| 28.70 | 1113 | 1104 | 1094 | 1085 | 1075 | 1066 | 1057 | 1047 | 10,38 | 1028 |
| 28.80 | Ior9 | 1009 | 1000 | 990 | 981 | 972 | 962 | 953 | 943 | 934 |
| 28.90 | 925 | 915 | 906 | 896 | 887 | 878 | 868 | 859 | 849 | 840 |
| 29.00 | 831 | 82 I | 8 I 2 | 803 | 793 | 784 | 775 | 765 | 756 | 746 |
| 29.10 | 737 | 728 | 718 | 709 | 700 | 690 | 681 | 672 | 663 | 653 |
| 29.20 | 644 | 635 | 625 | 616 | 607 | 597 | 588 | 579 | 570 | 560 |
| 29.30 | 55 I | 542 | 532 | 523 | 514 | 505 | 495 | 486 | 477 | 468 |
| 29.40 | 458 | 449 | 440 | 43 I | 421 | 412 | 403 | 394 | 384 | 375 |
| 29.50 | 366 | 357 | 348 | 338 | 329 | 320 | 3 II | 302 | 292 | 283 |
| 29.60 | 274 | 265 | 256 | 247 | 237 | 228 | 219 | 210 | 201 | 192 |
| 29.70 | 182 | 173 | 164 | 155 | 146 | 137 | 128 | 118 | 109 | 100 |
| 29.80 | +91 | + 82 | + 73 | + 64 | $+55$ | + 45 | $+36$ | + 27 | + 18 | + 9 |
| 29.90 | 0 | - 9 | - 18 | $-27$ | - 36 | - 45 | - 55 | - 64 | - 73 | $-82$ |
| 30.00 | - 91 | - 100 | - 109 | - 118 | - 127 | - 136 | - I45 | - I54 | $-163$ | - 172 |
| 30.10 | - 181 | - 190 | - 199 | $-208$ | -217 | -226 | - 235 | - 244 | $-253$ | - 262 |
| 30.20 | -271 | - 280 | -289 | $-298$ | $-307$ | $-316$ | $-325$ | -334 | -343 | $-352$ |
| 30.30 | $-361$ | -370 | -379 | $-388$ | -397 | -406 | -415 | -424 | -433 | -442 |
| 30.40 | -451 | $-460$ | -469 | $-478$ | $-486$ | -495 | $-504$ | $-513$ | $-522$ | $-531$ |
| 30.50 | - 540 | - 549 | - 558 | -567 | - 576 | $-585$ | - 593 | -602 | -6II | $-620$ |
| 30.60 | -629 | -638 | -647 | -656 | -665 | -673 | -682 | -691 | -700 | $-709$ |
| 30.70 | -718 | -727 | $-735$ | $-744$ | $-753$ | -762 | $-771$ | -780 | $-788$ | -797 |
| 30.80 | $-806$ | -8I5 | -824 | $-833$ | -841 | $-850$ | -859 | $-868$ | $-877$ | $-885$ |

Table 21.
DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Term for Temperature : $0.002039\left(\theta-50^{\circ}\right) \mathrm{z}$.
For temperatures $\left\{\begin{array}{l}\text { above } 50^{\circ} \mathrm{F} . \\ \text { below } 50^{\circ} \mathrm{F}\end{array}\right\}$ the values are to be $\left\{\begin{array}{l}\text { added. } \\ \text { adder }\end{array}\right.$ $\left.\begin{array}{l}\text { above } 50^{\circ} \mathrm{F} . \\ \text { below } 50^{\circ} \mathrm{F} .\end{array}\right\}$ the values are to be $\left\{\begin{array}{l}\text { added. } \\ \text { subtracted. }\end{array}\right.$

| $\begin{aligned} & \text { Mean } \\ & \text { Temperature. } \\ & \theta . \end{aligned}$ |  | APPROXIMATE DIFFERENCE OF HEIGHT OBTAINED FROM TABLE 20. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 20 | 40 | 60 | 80 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |
| F. | F. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $49^{\circ}$ | $51^{\circ}$ | 0 | - | - | $\bigcirc$ | $\bigcirc$ | 0 | 1 | 1 | 1 | 1 | 1 | 2 | 2 |
| 48 | 52 | - | $\bigcirc$ | - | - | - | 1 | 1 | 2 | 2 | 2 | 3 | 3 | 4 |
| 47 | 53 | - | - | - | - | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 46 | 54 | - | o | o | I | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 |
| 45 | 55 | $\bigcirc$ | - | I | 1 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 44 | 56 | - | o | I | 1 | 1 | 2 | 4 | 5 | 6 | 7. | 9 | 10 | II |
| 43 | 57 | $\bigcirc$ | I | ${ }_{1}$ | ${ }_{1}$ | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 11 | - 13 |
| 42 | 58 | - | 1 | I | 1 | 2 | 3 | 5 | 7 | 8 | 10 | 11 | 13 | 15 |
| 4 I | 59 | - | 1 | 1 | 1 | 2 | 4 | 6 | 7 | 9 | II | 13 | 15 | 17 |
| 40 | 60 | $\bigcirc$ | 1 | I | 2 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| 39 | 61 | - | 1 | I | 2 | 2 | 4 | 7 | 9 | 11 | 13 | 16 | 18 | 20 |
| 38 | 62 | o | I | 1 | 2 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 |
| 37 | 63 | I | I | 2 | 2 | 3 | 5 | 8 | II | 13 | 16 | 19 | 21 | 24 |
| 36 | 64 | 1 | 1 | 2 | 2 |  | 6 | 9 | II | 14 | 17 | 20 | 23 | 26 |
| 35 | 65 | I | 1 | 2 | 2 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 | 28 |
| 34 | 66 | I | 1 | 2 | 3 | 3 | 7 | 10 | 13 | 16 | 20 | 23 | 26 | 29 |
| 33 | 67 | 1 | 1 | 2 | 3 | 3 | 7 | 10 | 14 | 17 | 21 | 24 | 28 | 31 |
| 32 | 68 | 1 | 1 | 2 | 3 | 4 | 7 | 11 | 15 | 18 | 22 | 26 | 29 | 33 |
| 31 | 69 | I | 2 | 2 | 3 | 4 | 8 | 12 | 15 | 19 | 23 | 27 | 3 I | 35 |
| 30 | 70 | 1 | 2 | 2 | 3 | 4 | 8 | 12 | 16 | 20 | 24 | 29 | 33 | 37 |
| 29 | 71 | 1 | 2 | 3 | 3 | 4 | 9 | 13 | 17 | 21 | 26 | 30 | 34 | 39 |
| 28 | 72 | 1 | 2 | 3 | 4 | 4 |  | 13 | 18 | 22 | 27 | 3 I | 36 | 40 |
| 27 | 73 | I | 2 | 3 | 4 | 5 | 9 | 14 | 19 | 23 | 28 | 33 | 38 | 42 |
| 26 | 74 | I | 2 | 3 | 4 | 5 | Io | 15 | 20 | 24 | 29 | 34 | 39 | 44 |
| 25 | 75 | 1 | 2 | 3 | 4 | 5 | 10 | 15 | 20 | 25 | 3 I | 36 | 4 I | 46 |
| 24 | 76 | I | 2 | 3 | 4 | 5 | 11 | 16 | 21 | 27 | 32 | 37 | 42 | 48 |
| 23 | 77 | 1 | 2 | 3 | 4 | 6 | II | 17 | 22 | 28 | 33 | 39 | 44 | 50 |
| 22 | 78 | I | 2 | 3 | 5 | 6 | 11 | 17 | 23 | 29 | 34 | 40 | 46 | 51 |
| 21 | 79 | 1 | 2 | 4 | 5 | 6 | 12 | 18 | 24 | 30 | 35 | 4 I | 47 | 53 |
| 20 | 80 | I | 2 | 4 | 5 |  | 12 | 18 | 24 | 31 | 37 | 43 | 49 | 55 |
| 19 | 8 I | I | 3 | 4 | 5 | 6 | 13 | 19 | 25 | 32 | 38 | 44 | 51 | 57 |
| 18 | 82 | I |  | 4 | 5 | 7 | 13 | 20 | 26 | 33 | 39 | 46 | 52 | 59 |
| 17 | 83 | I | 3 | 4 | 5 | 7 | 13 | 20 | 27 | 34 | 40 | 47 | 54 | 61 |
| 16 | 84 | 1 | 3 | 4 | 6 | 7 | 14 | 21 | 28 | 35 | 42 | 49 | 55 | 62 |
| 15 | 85 | 1 | 3 | 4 | 6 | 7 | 14 | 21 | 29 | 36 | 43 | 50 | 57 | 64 |
| 14 | 86 | 1 | 3 | 4 | 6 | 7 | 15 | 22 | 29 | 37 | 44 | 5 I | 59 | 66 |
| 13 | 87 | 2 | 3 | 5 | 6 | 8 | 15 | 23 | 30 | 38 | 45 | 53 | 60 | 68 |
| 12 | 88 | 2 | 3 | 5 | 6 | 8 | 15 | 23 | 31 | 39 | 46 | 54 | 62 | 70 |
| 11 | 89 | 2 | 3 | 5 | 6 | 8 | 16 | 24 | 32 | 40 | 48 | 56 | 64 | 72 |
| 10 | 90 | 2 | 3 | 5 | 7 | 8 | 16 | 24 | 33 | 41 | 49 | 57 | 65 | 73 |
| 9 | 91 | 2 | 3 | 5 | 7 | 8 | 17 | 25 | 33 | 42 | 50 | 59 | 67 | 75 |
| 8 | 92 | 2 | 3 | 5 | 7 | 9 | 17 | 26 | 34 | 43 | 51 | 60 | 69 | 77 |
| 7 | 93 | 2 | 4 | 5 | 7 | 9 | 18 | 26 | 35 | 44 | 53 | 61 | 70 | 79 |
| 6 | 94 | 2 | 4 | 5 | 7 | 9 | 18 | 27 | 36 | 45 | 54 | 63 | 72 | 81 |
| 5 | 95 | 2 | 4 | 6 | 7 | 9 | 18 | 28 | 37 | 46 | 55 | 64 | 73 | 83 |
| 4 | 96 | 2 | 4 | 6 | 8 | 9 | 19 | 28 | 38 | 47 | 56 | 66 | 75 | 84 86 86 |
| 3 2 | 97 98 | 2 | 4 | 6 | 8 | 10 | 19 20 | 29 29 | 38 39 | 48 | 57 59 | 67 69 | 77 78 | 86 |
|  | 99 |  | 4 | 6 | 8 |  |  | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| 0 | 100 | 2 | 4 | 6 | 8 | Iо | 20 | 31 | 41 | 51 | 61 | 71 | 82 | 92 |

TABLE 21.

## DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Term for Temperature : $0.002039\left(\theta-50^{\circ}\right) \mathrm{z}$.
For temperatures $\left\{\begin{array}{l}\text { above } 50^{\circ} \mathrm{F} \text {. } \\ \text { below } 50^{\circ} \mathrm{F} .\end{array}\right\}$ the values are to be $\{$ added. $\left\{\begin{array}{l}\left.\text { below } 50^{\circ} \mathrm{F} .\right\} \text { the values are to be }\left\{\begin{array}{l}\text { added. } \\ \text { subtracted }\end{array}\right.\end{array}\right.$

| Mean Temperature. $\theta$. |  | APPROXIMATE DIFFERENCE OF HEIGHT OBTAINED FROM TABLE 20. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 20000 |
| F. | F. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $49^{\circ}$ | $51^{\circ}$ | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 4 I |
| 48 | 52 | 4 | 8 | 12 | 16 | 20 | 24 | 29 | 33 | 37 | 4 I | 82 |
| 47 | 53 | 6 | 12 | 18 | 24 | 31 | 37 | 43 | 49 | 55 | 61 | 122 |
| 46 | 54 | 8 | 16 | 24 | 33 | 41 | 49 | 57 | 65 | 73 | 82 | 163 |
| 45 | 55 | 10 | 20 | 3 I | 41 | 51 | 6 I | 71 | 82 | 92 | 102 | 204 |
| 44 | 56 | 12 | 24 | 37 | 49 | 61 | 73 | 86 | $98^{\circ}$ | 110 | 122 | 245 |
| 43 | 57 | 14 | 29 | 43 | 57 | 7 I | S6 | 100 | 114 | 128 | 143 | 285 |
| 42 | 58 | 16 | 33 | 49 | 65 | 82 | 98 | I 14 | 130 | 147 | 163 | 326 |
| 41 | 59 | 18 | 37 | 55 | 73 | 92 | 110 | 128 | 147 | 165 | I84 | 367 |
| 40 | 60 | 20 | 41 | 61 | S2 | 102 | 122 | 143 | 163 | 184 | 204 | 408 |
| 39 | 61 | 22 | 45 | 67 | 90 | I 12 | 135 | 157 | 179 | 202 | 224 | 449 |
| 38 | 62 | 24 | 49 | 73 | 98 | 122 | 147 | 171 | 196 | 220 | 245 | 489 |
| 37 | 63 | 27 | 53 | 80 | 106 | 133 | 159 | IS6 | 212 | 239 | 265 | 530 |
| 36 | 64 | 29 | 57 | 86 | 114 | 143 | 171 | 200 | 228 | 257 | 285 | 571 |
| 35 | 65 | 3 I | 61 | 92 | 122 | ${ }^{1} 53$ | I84 | 2 I 4 | 245 | 275 | 306 | 612 |
| 34 | 66 | 33 | 65 | 98 | 130 | 163 | 196 | 228 | 261 | 294 | 326 | 652 |
| 33 | 67 | 35 | 69 | 104 | I 39 | 173 | 2 C 8 | 243 | 277 | 312 | 347 | 693 |
| 32 | 68 | 37 | 73 | 110 | 147 | I84 | 220 | 257 | 294 | 330 | 367 | 734 |
| 31 | 69 | 39 | 77 | 116 | ${ }^{1} 55$ | 194 | 232 | 271 | 310 | 349 | 387 | 775 |
| 30 | 70 | 4 I | 82 | 122 | 163 | 204 | 245 | 285 | 326 | 367 | 408 | 816 |
| 29 | 71 | 43 | 86 | 128 | 171 | 214 | 257 | 300 | 343 | 385 | 428 | 856 |
| 28 | 72 | 45 | 90 | 135 | 179 | 224 | 269 | 314 | 359 | 404 | 449 | 897 |
| 27 | 7.3 | 47 | 94 | 141 | 188 | 234 | 2 SI | 328 | 375 | 422 | 469 | 938 |
| 26 | 74 | 49 | 98 | 147 | 196 | 245 | 294 | 343 | 391 | 440 | 489 | 979 |
| 25 | 75 | 5 I | 102 | 153 | 204 | 255 | 306 | 357 | 408 | 459 | 510 | 1020 |
| 24 | 76 | 53 | 106 | 159 | 212 | 265 | 318 | 371 | 424 | 477 | 530 | 1060 |
| 23 | 77 | 55 | 110 | 165 | 220 | 275 | 330 | 385 | 440 | 495 | 551 | I IOI |
| 22 | 78 | 57 | 114 | 171 | 228 | 285 | 343 | 400 | 457 | 514 | 57 I | 1142 |
| 21 | 79 | 59 | 118 | 177 | 236 | 296 | 355 | 414 | 473 | 532 | 591 | 1183 |
| 20 | 80 | 61 | 122 | I84 | 245 | 306 | 367 | 428 | 489 | 551 | 612 | 1223 |
| 19 | 8 I | 63 | 126 | 190 | 253 | 316 | 379 | 442 | 506 | 569 | 632 | 1264 |
| 18 | 82 | 65 | 130 | 196 | 261 | 326 | 391 | 457 | 522 | 587 | 652 | 1305 |
| 17 | 83 | 67 | I 35 | 202 | 269 | 336 | 404 | 471 | 538 | 606 | 673 | I 346 |
| 16 | 84 | 69 | I39 | 208 | 277 | 347 | 416 | 485 | 555 | 624 | 693 | 1387 |
| 15 | 85 | 71 | 143 | 214 | 2 S 5 | 357 | 428 | 500 | 57 I | 642 | 714 | 1427 |
| 14 | 86 | 73 | 147 | 220 | 294 | 367 | 440 | 514 | 587 | 661 | 734 | 1468 |
| 13 | 87 | 75 | 151 | 226 | 302 | 377 | 453 | 52 S | 604 | 679 | 754 | 1509 |
| 12 | 88 | 77 | I 55 | 232 | 310 | 387 | 465 | 542 | 620 | 697 | 775 | I 550 |
| II | S9 | 80 | I59 | 239 | 318 | 398 | 477 | 557 | 636 | 716 | 795 | I590 |
| 10 | 90 | 82 | 163 | 245 | 326 | 408 | 489 | 57 I | 652 | 734 | 816 | 1631 |
| 9 | 91 | 84 | 167 | 251 | 334 | 418 | 502 | 585 | 669 | 752 | 836 | 1672 |
| 8 | 92 | 86 | 171 | 257 | 343 | 428 | 514 | 599 | 685 | 771 | 856 | 1713 |
| 7 | 93 | 88 | 175 | 263 | 35 I | 438 | 526 | 614 | 7 O | 789 | 877 | I 754 |
| 6 | 94 | 90 | 179 | 269 | 359 | 449 | 538 | 628 | 718 | 807 | 897 | I794 |
| 5 | 95 | 92 | 184 | 275 | 367 | 459 | 551 | 642 | 734 | 826 | 918 | 1835 |
| 4 | 96 | 94 | 188 | 2 SI | 375 | 469 | 563 | 657 | 750 | 844 | 938 | 1876 |
| 3 | 97 | 96 | 192 | 287 | 383 | 479 | 575 | 671 | 767 | 862 | 958 | 1917 |
| 2 | 98 | 98 | 196 | 294 | 391 | 489 | 587 | 685 | 783 | 881 | 979 | 1957 |
| 0 | 99 | 100 | 200 | 300 | 400 | 500 | 599 | 699 | 799 | 899 | 999 | 1998 |
| 0 | 100 | 102 | 204 | 306 | 408 | 510 | 612 | 714 | 8 I 6 | 918 | 1020 | 2039 |

TABLE 22.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Correction for Latitude and Weight of Mercury: $\mathbf{z}(0.002662 \cos 2 \phi+0.00239)$.

| Lati- <br> tude. $\phi$. | APPROXIMATE DIFFERENCE OF HEIGHT ObTAINED FROM TAbles 20-21. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 |
|  | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $0{ }^{\circ}$ | +3 | +5 | +8 | + 10 | + 13 | +15 | + 18 | +20 | $+23$ | +25 | +28 |
| 2 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 20 | 23 | 25 | 28 |
| 4 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 20 | 23 | 25 | 28 |
| 6 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 | 25 | 27 |
| 8 | 2 | 5 | 7 | וо | 12 | 15 | 17 | 20 | 22 | 25 | 27 |
| 10 | +2 | +5 | $+7$ | + ı0 | $+12$ | + 15 | +17 | +20 | +22 | +24 | $+27$ |
| 12 | 2 | 5 | 7 | 10 | 12 | 14 | 17 | 19 | 22 | 24 | 27 |
| 14 | 2 | 5 | 7 | 9 | 12 | 14 | 17 | 19 | 21 | 24 | 26 |
| 16 | 2 | 5 | 7 | 9 | 12 | 14 | 16 | 19 | 21 | 23 | 26 |
| 18 | 2 | 5 | 7 | 9 | II | 14 | 16 | 18 | 20 | 23 | 25 |
| 20 | +2 | +4 | +7 | + 9 | + II | +13 | +16 | +17 | +20 | +22 | +24 |
| 22 | 2 | 4 | 6 | 9 | 11 | 13 | 15 | 17 | 19 | 22 | 24 |
| 24 | 2 | 4 | 6 | 8 | ı | 13 | 15 | 17 | 19 | 21 | 23 |
| 26 | 2 | 4 | 6 | 8 | ı | 12 | 14 | 16 | 18 | 20 | 22 |
| 28 | 2 | 4 | 6 | 8 | ıо | 12 | 14 | 16 | 17 | 19 | 2 T |
| 30 | +2 | +4 | +6 | $+7$ | + 9 | + II | + 13 | +15 | +17 | +19 | +20 |
| 32 | 2 |  | 5 | 7 | 9 | 11 | 12 | 14 | 16 | 18 | 20 |
| 34 | 2 | 3 | 5 | 7 | 8 | 10 | 12 | 14 | 15 | 17 | 19 |
| 36 | 2 | 3 | 5 | 6 | 8 | Iо | 11 | 13 | 14 | 16 | 18 |
| 38 | 2 | 3 | 5 | 6 | 8 | 9 | Ir | 12 | 14 | 15 | 17 |
| 40 | + I | +3 | +4 | + 6 | $+7$ | + 9 | + 10 | + II | +13 | +14 | +16 |
| 42 | I | 3 | 4 | 5 |  |  | 9 | Ir | 12 | 13 | 15 |
| 44 | 1 | 2 | 4 | 5 | 6 | 7 | 9 | 10 | II | 12 | 14 |
| 45 | + I | +2 | +4 | $+5$ | + 6 | $+7$ | $+8$ | + 10 | + II | +12 | +13 |
| 46 | + 1 | $+2$ | $+3$ | + 5 | + 6 |  |  |  |  |  |  |
| 48 50 | I. | 2 | 3 3 | 4 4 | 5 5 | 6 6 | 7 7 | 8 8 | 10 9 | II IO | 12 II |
| 52 | +r | +2 | +3 | $+3$ | + 4 | + 5 | $+6$ |  | $+8$ | + 9 | + 10 |
| 54 | I | 2 | 2 | 3 | 4 | 5 | 5 |  |  | 8 | 9 |
| 56 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 7 | 8 |
| 58 | I | I | 2 | 2 | 3 | 4 | 4 | 5 | 6 | 6 | 7 |
| 60 | 1 | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 5 | 6 |
| 62 | 0 | + r | + 1 | + 2 | + 2 | + 3 | + 3 | + 4 | + 4 | $+5$ | + 5 |
| 64 | - | $\underline{1}$ | I | 2 | 2 | 2 | 3 |  |  |  | 4 3 3 |
| 66 | $\bigcirc$ | 1 | I | 1 | 2 | 2 | 2 | 2 | 3 | 3 | 3 |
| 68 | - | - | I | 1 | I | 1 | 2 1 | $\stackrel{2}{1}$ | 2 2 | 2 2 | 3 2 |
| 70 | o | - | I | 1 | 1 | 1 |  |  |  |  |  |
| 72 |  | $\bigcirc$ | O | - | + 1 | + 1 | $\begin{array}{r}1 \\ +1 \\ \hline\end{array}$ | 1 +1 |  |  |  |
| 74 76 | $\bigcirc$ | o | - | $\bigcirc$ |  |  |  |  |  | + | + $\begin{array}{r}1 \\ 0\end{array}$ |
| 76 78 | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | - | - | O | - |
| 80 | - | o | - | - | 0 | - | 0 | $\bigcirc$ | 0 | - I | - I |

TABLE 22.
DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Correction for Latitude and Weight of Mercury: $\mathrm{z}(0.002662 \cos 2 \phi+0.00239)$.

| Latitude. $\phi$. | APPROXIMATE DIFFERENCE OF HEIGHT OBTAINED FROM TABLES 20-21. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6000 | 7000 | 8000 | 9000 | 10000 | 11000 | 12000 | 13000 | 14000 | 15000 | 20000 |
|  | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $0^{\circ}$ | $+30$ | $+35$ | $+40$ | $+45$ | $+51$ | $+56$ | +6I | +66 | +71 | +76 | + IOI |
| 2 | 30 | 35 | 40 | 45 | 50 | 56 | 61 | 66 | 71 | 76 | 101 |
| 4 | 30 | 35 | 40 | 45 | 50 | 56 | 60 | 65 | 70 | 75 | IOI |
| 6 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 100 |
| 8 | 30 | 35 | 40 | 45 | 49 | 54 | 59 | 64 | 69 | 74 | 99 |
| 10 | $+29$ | $+34$ | $+39$ | $+44$ | +49 | $+54$ | +59 | +64 | +68 | $+73$ | +98 |
| 12 | 29 | 34 | 39 | 43 | 48 | 53 | 58 | 63 | 68 | 72 | 96 |
| 14 | 28 | 33 | 38 | 43 | 47 | 52 | 57 | 62 | 66 | 71 | 95 |
| 16 | 28 | 33 | 37 | 42 | 46 | 51 | 56 | 60 | 65 | 70 | 93 |
| 18 | 27 | 32 | 36 | 41 | 45 | 50 | 55 | 59 | 64 | 68 | 91 |
| 20 | $+27$ | +3I | $+35$ | $+40$ | $+44$ | $+49$ | $+53$ | $+58$ | $+62$ | $+66$ | +89 |
| 22 | 26 | 30 | 34 | 39 | 43 | 47 | 52 | 56 | 60 | 65 | 86 |
| 24 | 25 | 29 | 33 | 38 | 42 | 46 | 50 | 54 | 58 | 63 | 83 |
| 26 | 24 | 28 | 32 | 36 | 40 | 44 | 48 | 52 | 56 | 60 | 8 I |
| 28 | 23 | 27 | 3 I | 35 | 39 | 43 | 47 | 50 | 54 | 58 | 78 |
| 30 | $+22$ | $+26$ | $+30$ | $+33$ | $+37$ | +41 | $+45$ | $+48$ | $+52$ | $+56$ | + 74 |
| 32 | 21 | 25 | 28 | 32 | 36 | 39 | 43 | 46 | 50 | 53 | 71 |
| 34 | 20 | 24 | 27 | 30 | 34 | 37 | 4 I | 44 | 47 | 51 | 68 |
| 36 | 19 | 22 | 26 | 29 | 32 | 35 | - 39 | 42 | 45 | 48 | 64 |
| 38 | 18 | 21 | 24 | 27 | 30 | 33 | 36 | 39 | 42 | 46 | 6 I |
| 40 | +17 | $+20$ | $+23$ | $+26$ | +29 | $+3 \mathrm{I}$ | $+34$ | $+37$ | $+40$ | $+43$ | $+57$ |
| 42 | 16 | 19 | 21 | 24 | 27 | 29 | 32 | 35 | 37 | 40 | 53 |
| 44 | 15 | 17 | 20 | 22 | 25 | 27 | 30 | 32 | 35 | 37 | 50 |
| 45 | +14 | $+17$ | + 19 | $+22$ | +24 | $+26$ | +29 | $+3 \mathrm{I}$ | $+33$ | $+36$ | $+48$ |
| 46 | +14 | + 16 | + 18 | $+21$ | $+23$ | $+25$ | $+28$ | $+30$ | $+32$ | $+35$ | $+46$ |
| 48 | 13 | 15 | 17 | 19 | 21 | 23 | 25 | 27 | 30 | 32 | 42 |
| 50 | 12 | I 3 | 15 | 17 | 19 | 21 | 23 | 25 | 27 | 29 | 39 |
| 52 | + 10 | + 12 | + 14 | $+16$ | +17 | $+19$ | +21 | $+23$ | $+24$ | $+26$ | $+35$ |
| 54 |  | II | 13 | 14 | 16 | 17 | 19 | 20 | 22 | 24 | 3 I |
| 56 | 8 | 10 | 11 | 13 | 14 | 15 | 17 | 18 | 20 | 21 | 28 |
| 58 | 7 | 9 | 10 | II | 12 | 13 | 15 | 16 | 17 | 18 | 24 |
| 60 | 6 | 7 | 8 | 10 | II | 12 | 13 | 14 | 15 | 16 | 21 |
| 62 | $+5$ | + 6 | $+7$ | $+8$ | + 9 | + 10 | + II | +12 | +13 | + 14 | $+18$ |
| 64 | 5 |  | 6 | 7 | 8 | 8 | 9 | 10 | II | 11 | 15 |
| 66 | 4 | 4 | 5 | 5 | 6 | 7 | 7 | 8 | 9 | 9 | 12 |
| 68 | 3 | 3 | 4 | 4 | 5 | 5 | 6 | 6 | 7 | 7 | 10 |
| 70 | 2 | 2 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 5 | 7 |
| 72 | $+1$ | + 2 | $+2$ | $+2$ | $+2$ |  |  |  |  |  |  |
| 74 | +1 | + 1 | +1 | + 1 | + 1 |  |  |  |  |  |  |
| 76 | 0 | 0 | 0 | 0 |  |  |  |  |  |  | * |
| 80 | [ 0 | 0 $-\quad \mathrm{I}$ | 0 $-\quad 1$ |  | 0 $-\quad 1$ |  |  |  |  |  |  |

TABLE 23.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Correction for an Average Degree of Humidity.

| Mean Temperature. | APPROXIMATE DIFFERENCE OF HEIGHT OBTAINED FROM TABLES 20-21. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 500 | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 20000 |
| F. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $-20^{\circ}$ | 0 | O | 0 | 0 | 0 | 0 | 0 | +1 | + I | + I | + I | +2 |
| $-\mathrm{I} 6$ | - | - | - | + I | + I | + I | +1 | I | 2 | 2 | 2 | 4 |
| - 12 | $\bigcirc$ | - | + I | I | I | 2 | 2 | 2 | 3 | 3 | 3 | 6 |
| - 8 | 0 | 0 | 1 | I | 2 | 2 | 3 | 3 | 4 | 4 | 4 | 9 |
| - 6 | o | o | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 10 |
| - 4 | o | + I | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 6 | I I |
| $-2$ | 0 | I | I | 2 | 2 | 3 | 4 | 4 | 5 | 6 | 6 | 12 |
| 0 | 0 | 1 | I | 2 | 3 | 3 | 4 | 5 | 5 | 6 | 7 | 14 |
| $+2$ | o | I | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 7 | 15 |
| 4 | o | I | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 | 8 | 16 |
| 6 | 0 | I | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 | 9 | 18 |
| 8 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 19 |
| 10 | + I | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 21 |
| 12 | I | I | 2 | 3 | 4 | 6 | 7 | 8 | 9 | 10 | 11 | 22 |
| 14 | I | I | 2 | 4 | 5 | 6 | 7 | 8 | 9 | II | 12 | 24 |
| 16 | I | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 11 | 13 | 25 |
| 18 | 1 | I | 3 | 4 | 5 | 7 | 8 | 9 | 11 | 12 | 13 | 27 |
| 20 | I | 1 | 3 | 4 | 6 | 7 | 9 | 10 | II | 13 | 14 | 29 |
| 22 | I | 2 | 3 | 5 | 6 | 8 | 9 | I I | 12 | 14 | 15 | 3 I |
| 24 | 1 | 2 | 3 | 5 | 7 | 8 | IO | II | I3 | 15 | 16 | 33 |
| 26 | I | 2 | 3 | 5 | 7 | 9 | 10 | 12 | 14 | 16 | 17 | 35 |
| 28 | I | 2 | 4 | 6 | 7 | 9 | II | 13 | 15 | 17 | 19 | 37 |
| 30 | I | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 41 |
| 32 | I | 2 | 4 | 7 | 9 | II | 13 | 16 | 18 | 20 | 22 | 44 |
| 34 | I | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 19 | 22 | 24 | 49 |
| 36 | 1 | 3 | 5 | 8 | II | 13 | 16 | 19 | 21 | 24 | 27 | 53 |
| 38 | I | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 23 | 26 | 29 | 59 |
| 40 | 2 | 3 | 6 | 10 | 13 | 16 | 19 | 23 | 26 | 29 | 32 | 64 |
| 42 | 2 | 4 | 7 | II | 14 | 18 | 21 | 25 | 28 | 32 | 35 | 71 |
| 44 | 2 | 4 | 8 | 12 | 15 | 19 | 23 | 27 | 31 | 35 | 39 | 77 |
| 46 | 2 | 4 | 8 | 13 | 17 | 21 | 25 | 29 | 34 | 38 | 42 | 84 |
| 48 | 2 | 5 | 9 | 14 | 18 | 23 | 27 | 32 | 37 | 41 | 46 | 92 |
| 50 | 2 | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 99 |
| 52 | 3 | 5 | 11 | 16 | 2 I | 27 | 32 | 37 | 43 | 48 | 53 | 107 |
| 54 | 3 | 6 | 11 | 17 | 23 | 29 | 34 | 40 | 46 | 5 I | 57 | II4 |
| 56 | 3 | 6 | 12 | 18 | 24 | 30 | 37 | 43 | 49 | 55 | 61 | 122 |
| 58 | 3 | 6 | 13 | 19 | 26 | 32 | 39 | 45 | 52 | 58 | 65 | 130 |
| 60 | 3 | 7 | 14 | 2 I | 27 | 34 | 4 I | 48 | 55 | 62 | 69 | 137 |
| 62 | 4 | 7 | 14 | 22 | 29 | 36 | 43 | 5 I | 58 | 65 | 72 | 145 |
| 64 | 4 | 8 | 15 | 23 | 30 | 38 | 46 | 53 | 61 | 69 | 76 | 152 |
| 66 | 4 | 8 | 16 | 24 | 32 | 40 | 48 | 56 | 64 | 72 | 80 | 160 |
| 68 | 4 | 8 | 17 | 25 | 34 | 42 | 50 | 59 | 67 | 76 | 84 | 168 |
| 70 | 4 | 9 | 18 | 26 | 35 | 44 | 53 | 61 | 70 | 79 | 88 | 175 |
| 72 | 5 | 9 | 18 | 27 | 37 | 46 | 55 | 64 | 73 | 82 | 9 I | I83 |
| 76 | 5 | 10 | 20 | 30 | 40 | 49 | 59 | 69 | 79 | 89 | 99 | 198 |
| 80 | 5 | II | 21 | 32 | 43 | 53 | 64 | 75 | 85 | 96 | 106 | 213 |
| 84 | 6 | II | 23 | 34 | 46 | 57 | 68 | 80 | 91 | 103 | I 14 | 228 |
| 88 | 6 | 12 | 24 | 37 | 49 | 61 | 73 | 85 | 97 | I 10 | 122 | 243 |
| 92 | 6 | 13 | 26 | 39 | 52 | 65 | 78 | 91 | 103 | II6 | 129 | 259 |
| 96 | 7 | 14 | 27 | 4 I | 55 | 68 | 82 | 96 | I 10 | I23 | I 37 | 274 |

TABLE 24.
DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Correction for the Variation of Gravity with Altitude: $\frac{z\left(z+2 h_{0}\right)}{R}$.

| Approximate difference of height. 2. | HEIGHT OF LOWER STATION IN FEET ( $h_{0}$ ) . |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 12000 |
| Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 500 | 0 | 0 | 0 | 0 | - | o | o | 0 | 0 | 0 | 0 | + I |
| 1000 | 0 | 0 | - | $\bigcirc$ | - | + I | + I | +1 | + I | + I | + 1 | I |
| 1500 | - | 0 | o | + I | $+1$ | 1 | 1 | I | 1 | 1 | 2 | 2 |
| 2000 | 0 | - | + I | I | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 |
| 2500 | 0 | +1 | 1 | 1 | I | I | 2 | 2 | 2 | 2 | 3 | 3 |
| 3000 | 0 | 1 | I | 1 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 |
| 3500 | + I | I | 1 | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 | 5 |
| 4000 | 1 | 1 | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 | 5 | 5 |
| 4500 | 1 | I | 2 | 2 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 6 |
| 5000 | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 5 | 6 | 6 | 7 |
| 5500 | 1 | 2 | 3 | 3 | 4 | 4 | 5 | 5 | 6 | 6 | 7 | 8 |
| 6000 | 2 | 2 | 3 | 3 | 4 | 5 | 5 | 6 | 6 | 7 | 7 | 9 |
| 6500 | 2 | 3 | 3 | 4 | 5 | 5 | 6 | 6 | 7 | 8 | 8 | 9 |
| 7000 | 2 | 3 | 4 | 4 | 5 | 6 | 6 | 7 | S | 8 | 9 | Io |
| 7500 | 3 | 3 | 4 | 5 | 6 | 6 | 7 | 8 | 8 | 9 | 10 | II |
| 8000 | 3 | 4 | 5 | 5 | 6 | 7 | 8 | 8 | 9 | 10 | II | 12 |
| 8500 | 3 | 4 | 5 | 6 | 7 | 8 | 8 | 9 | 10 | 11 | 12 | 13 |
| 9000 | 4 | 5 | 6 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 12 | 14 |
| 9500 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | I I | 12 | 13 | 13 | 15 |
| 10000 | 5 | 6 | 7 | 8 | 9 | 10 | II | I I | 12 | 13 | 14 | 16 |
| 11000 | 6 | 7 | 8 | 9 | 10 | II | 12 | 13 | 14 | 15 | 16 | 18 |
| 12000 | 7 | 8 | 9 | 10 | 1 I | 13 | 14 | 15 | 16 | 17 | 18 | 21 |
| 13000 | 8 | 9 | II | 12 | 13 | 14 | 16 | 17 | 18 | 19 | 21 | 23 |
| 14000 | 9 | II | 12 | 13 | 15 | 16 | 17 | 19 | 20 | 21 | 23 | 25 |
| 15000 | II | 12 | 14 | ${ }^{1} 5$ | 17 | I8 | 19 | 2 I | 22 | 24 | 25 | 28 |
| 16000 | 12 | 14 | 15 | 17 | 18 | 20 | 21 | 23 | 25 | 26 | 28 | 31 |
| 17000 | 14 | 15 | 17 | 19 | 20 | 22 | 24 | 25 | 27 | 28 | 30 |  |
| 18000 | 16 | 17 | 19 | 21 | 22 | 24 | 26 | 28 | 30 | 31 |  |  |
| 19000 | 17 | 19 | 2 I | 23 | 25 | 26 | 28 | 30 | 32 |  |  |  |
| 20000 | 19 | 21 | 23 | 25 | 27 | 29 | 31 |  |  |  |  |  |

Smithbonian Tables.

TABLE 25.

## DETERMINATION OF HEIGHTS BY THE BAROMETER.

METRIC MEASURES.
Values of $18400 \log \frac{760}{B}$.

| Barometric Pressure. | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm. | m. | m. | m. | m | m. | m. | m. | m. | m. | m. |
| 300 | 7428 | 7401 | 7375 | 7348 | 7322 | 7296 | 7270 | 7244 | 7218 | 7192 |
| 310 | 7166 | 7140 | 7115 | 7089 | 7064 | 7038 | 7013 | 6987 | 6962 | 6937 |
| 320 | 6912 | 6887 | 6862 | 6838 | 6813 | 6789 | 6764 | 6740 | 6715 | 6691 |
| 330 | 6666 | 6642 | 6618 | 6594 | 6570 | 6546 | 6522 | 6498 | 6475 | 6451 |
| 340 | 6428 | 6405 | 6381 | 6358 | 6334 | 6311 | 6288 | 6265 | 6242 | 6219 |
| 350 | 6196 | 6173 | 6151 | 6128 | 6106 | 6083 | 606I | 6038 | 6016 | 5993 |
| 360 | 5971 | 5949 | 5927 | 5905 | 5883 | 5861 | 5839 | 5817 | 5795 | 5773 |
| 370 | 5752 | 5730 | 5709 | 5687 | 5666 | 5644 | 5623 | 5602 | 558 I | 5560 |
| 380 | 5539 | 5518 | 5497 | 5476 | 5455 | 5434 | 5414 | 5393 | 5373 | 5352 |
| 390 | 5332 | 53 II | 5291 | 5270 | 5250 | 5229 | 5209 | 5189 | 5169 | 5149 |
| 400 | 5129 | 5109 | 5089 | 5069 | 5049 | 5029 | 5010 | 4990 | 4971 | 4951 |
| 410 | 4932 | 4912 | 4893 | 4873 | 4854 | 4834 | 4815 | 4796 | 4777 | 4758 |
| 420 | 4739 | 4720 | 4701 | 4682 | 4663 | 4644 | 4625 | 4606 | 4588 | 4569 |
| 430 | 4551 | 4532 | 4514 | 4495 | 4477 | 4458 | 4440 | 4422 | 4404 | 4386 |
| 440 | 4368 | 4350 | 4332 | 4314 | 4296 | 4278 | 4260 | 4242 | 4224 | 4206 |
| 450 | 4188 | 4170 | 4152 | 4134 | 4117 | 4099 | 4082 | 4064 | 4047 | 4029 |
| 460 | 4012 | 3994 | 3977 | 3959 | 3942 | 3925 | 3908 | 3791 | 3774 | 3757 |
| 470 | 3840 | 3823 | 3806 | 3789 | 3772 | 3755 | 3738 | 3721 | 3705 | 3688 |
| 480 | 3672 | 3655 | 3639 | 3622 | 3606 | 3589 | 3573 | 3556 | 3540 | 3523 |
| 490 | 3507 | 3490 | 3474 | 3458 | 3442 | 3426 | 3410 | 3394 | 3378 | 3362 |
| 500 | 3346 | 3330 | 3314 | 3298 | 3282 | 3266 | 3250 | 3235 | 3219 | 3203 |
| 510 | 3188 | 3172 | 3157 | 3141 | 3126 | 3110 | 3095 | 3079 | 3064 | 3048 |
| 520 | 3033 | 3017 | 3002 | 2986 | 2971 | 2955 | 2940 | 2925 | 2910 | 2895 |
| 530 | 2880 | 2865 | 2850 | 2835 | 2820 | 2 SO | 2790 | 2775 | 2760 | 2745 |
| 540 | 2731 | 2716 | 2701 | 2687 | 2672 | 2657 | 2643 | 2628 | 2613 | 2599 |
| 550 | 2584 | 2570 | 2555 | 2541 | 2526 | 2512 | 2497 | 2483 | 2468 | 2454 |
| 560 | 2440 | 2426 | 2411 | 2397 | 2383 | 2369 | 2355 | 2341 | 2327 | 2313 |
| 570 | 2299 | 2285 | 2271 | 2257 | 2243 | 2229 | 2215 | 2201 | 2188 | 2174 |
| 580 | 2160 | 2146 | 2133 | 2119 | 2105 | 2092 | 2078 | 2064 | 2051 | 2037 |
| 590 | 2023 | 2010 | 1996 | 1983 | 1969 | 1956 | 1942 | 1929 | 1915 | 1902 |
| 600 | 1889 | 1875 | I862 | 1848 | 1835 | 1822 | 1809 | 1796 | 1783 | 1770 |
| 610 | 1757 | 1744 | 1731 | 1718 | 1705 | 1692 | 1679 | 1666 | 1653 | 1640 |
| 620 | 1627 | 1614 | 1601 | 1588 | 1576 | 1563 | 1550 | 1537 | 1525 | 1512 |
| 630 | 1499 | 1486 | 1474 | 1461 | 1448 | 1436 | 1423 | 1411 | I 398 | I386 |
| 640 | I 373 | I361 | 1348 | 1336 | 1323 | 1311 | 1298 | 1286 | 1273 | 126I |
| 650 | I249 | 1236 | 1224 | 1212 | 1199 | 1187 | I 175 | 1163 | 1151 | 1139 |
| 660 | 1127 | III5 | 1103 | 1091 | 1079 | 1067 | 1055 | 1043 | 1031 | 1019 |
| 670 | 1007 | 995 | 983 | 971 | 960 | 948 | 936 | 924 | 913 | 901 |
| 680 | 889 | 877 | 866 | 854 | 842 | 831 | 819 | 807 | 796 | 784 |
| 690 | 772 | 761 | 749 | 738 | 726 | 715 | 703 | 692 | 680 | 669 |
| 700 | 657 | 646 | 635 | 623 | 612 | 601 | 589 | 578 | 567 | 555 |
| 710 | 544 | 533 | 52 I | 510 | 499 | 487 | 476 | 465 | 454 | . 443 |
| 720 | 432 | 42 I | 410 | 399 | 388 | 377 | 366 | 355 | 344 | 333 |
| 730 | 322 | 311 | 300 | 289 | 278 | 267 | 256 | 245 | 234 | 224 |
| 740 | 213 | 202 | 192 | 181 | 170 | 160 | 149 | 138 | 128 | 117 |
|  | + 106 |  |  | + 74 | $+64$ |  |  | + 32 | + 22 | + II |
| 760 | - | - IO | - 21 | - 31 | - 42 | + 53 | - 63 | - 73 | - 83 | - 94 |
| 770 | - 104 | - II5 | - 125 | - I36 | - 146 | $-156$ | - I66 | - I77 |  |  |

TAble 26.

## DETERMINATION OF HEIGHTS BY THE BAROMETER.

 METRIC MEASURES.Term for Temperature : $0.00367 \theta \times \mathrm{z}$.
For temperatures $\left\{\begin{array}{l}\text { above } \circ^{\circ} \mathrm{C} . \\ \text { below } 0^{\circ} \mathrm{C} .\end{array}\right\}$ the values are to be $\left\{\begin{array}{l}\text { added. } \\ \text { subtracted. }\end{array}\right.$

| Approximate difference of height. $z$. | MEAN TEMPERATURE OF AIR COLUMN IN CENTIGRADE DEGREES ( $\boldsymbol{\theta}$ ) . |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ |
| m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 100 | 0 | 1 | I | 1 | 2 | 2 | 3 | 3 | 3 | 4 | 7 | 11 | 15 |
| 200 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 7 | 15 | 22 | 29 |
| 300 | 1 | 2 | 3 | 4 | 6 | 7 | 8 | 9 | 10 | 11 | 22 | 33 | 44 |
| 400 | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 12 | 13 | 15 | 29 | 44 | 59 |
| 500 | 2 | 4 | 6 | 7 | 9 | 11 | 13 | 15 | 17 | 18 | 37 | 55 | 73 |
| 600 | 2 | 4 | 7 | 9 | 1 I | 13 | 15 | 18 | 20 | 22 | 44 | 66 | 88 |
| 700 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 2 I | 23 | 26 | 5 I | 77 | 103 |
| 800 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 23 | 26 | 29 | 59 | 88 | 117 |
| 900 | 3 | 7 | 10 | I 3 | 17 | 20 | 23 | 26 | 30 | 33 | 66 | 99 | 132 |
| 1000 | 4 | 7 | 11 | 15 | 18 | 22 | 26 | 29 | 33 | 37 | 73 | 110 | 147 |
| 1100 | 4 | 8 | 12 | 16 | 20 | 24 | 28 | 32 | 36 | 40 | 81 | 121 | 161 |
| 1200 | 4 | 9 | 13 | 18 | 22 | 26 | 31 | 35 | 40 | 44 | 88 | 132 | 176 |
| 1300 | 5 | 10 | 14 | 19 | 24 | 29 | 33 | 38 | 43 | 48 | 95 | 143 | 191 |
| 1400 | 5 | 10 | 15 | 2 I | 26 | 3 I | 36 | 4 I | 46 | 51 | 103 | 154 | 206 |
| 1500 | 6 | II | 17 | 22 | 28 | 33 | 39 | 44 | 50 | 55 | 110 | 165 | 220 |
| 1600 | 6 | 12 | 18 | 23 | 29 | 35 | 4 I | 47 | 53 | 59 | 117 | 176 | 235 |
| 1700 | 6 | 12 | 19 | 25 | 3 I | 37 | 44 | 50 | 56 | 62 | 125 | 187 | 250 |
| 1800 | 7 | 13 | 20 | 26 | 33 | 40 | 46 | 53 | 59 | 66 | 132 | 198 | 264 |
| 1900 | 7 | 14 | 21 | 28 | 35 | 42 | 49 | 56 | 63 | 70 | 139 | 209 | 279 |
| 2000 | 7 | 15 | 22 | 29 | 37 | 44 | 51 | 59 | 66 | 73 | 147 | 220 | 294 |
| 2100 | 8 | ${ }^{1} 5$ | 23 | 31 | 39 | 46 | 54 | 62 | 69 | 77 | 154 | 231 | 308 |
| 2200 | 8 | 16 | 24 | 32 | 40 | 48 | 57 | 65 | 73 | 81 | 161 | 242 | 323 |
| 2300 | 8 | 17 | 25 | 34 | 42 | 5 I | 59 | 68 | 76 | 84 | 169 | 253 | 338 |
| 2400 | 9 | 18 | 26 | 35 | 44 | 53 | 62 | 70 | 79 | 88 | 176 | 264 | 352 |
| 2500 | 9 | 18 | 28 | 37 | 46 | 55 | 64 | 73 | 83 | 92 | 184 | 275 | 367 |
| 2600 | 10 | 19 | 29 | 38 | 48 | 57 | 67 | 76 | 86 | 95 | 19 I | 286 | 382 |
| 2700 | 10 | 20 | 30 | 40 | 50 | 59 | 69 | 79 | 89 | 99 | 198 | 297 | 396 |
| 2800 | 10 | 21 | 31 | 41 | 51 | 62 | 72 | 82 | 92 | 103 | 206 | 308 | 4II |
| 2900 | II | 21 | 32 | 43 | 53 | 64 | 75 | 85 | 96 | 106 | 213 | 319 | 426 |
| 3000 | II | 22 | 33 | 44 | 55 | 66 | 77 | 88 | 99 | 110 | 220 | 330 | 440 |
| 3100 | 11 | 23 | 34 | 46 | 57 | 68 | 80 | 91 | 102 | 114 | 228 | 341 | 455 |
| 3200 | 12 | 23 | 35 | 47 | 59 | 70 | 82 | 94 | 106 | 117 | 235 | 352 | 470 |
| 3300 | 12 | 24 | 36 | 48 | 61 | 73 | 85 | 97 | 109 | 121 | 242 | 363 | 484 |
| 3400 | 12 | 25 | 37 | 50 | 62 | 75 | 87 | 100 | II2 | 125 | 250 | 374 | 499 |
| 3500 | 13 | 25 | 39 | 51 | 64 | 77 | 90 | 103 | 116 | 128 | 257 | 385 | 514 |
| 3600 | 13 | 26 | 40 | 53 | 66 | 79 | 92 | 106 | I 19 | 132 | 264 | 396 | 528 |
| 3700 | 14 | 27 | 4 I | 54 | 68 | 8 I | 95 | 109 | 122 | 136 | 272 | 407 | 543 |
| 3800 | 14 | 28 | 42 | 56 | 70 | 84 | 98 | 112 | 126 | 139 | 279 | 418 | 558 |
| 3900 | 14 | 29 | 43 | 57 | 72 | 86 | 100 | I 15 | 129 | 143 | 286 | 429 | 573 |
| 4000 | 15 | 29 | 44 | 59 | 73 | 88 | 103 | 117 | 132 | 147 | 294 | 440 | 587 |
| 5000 | 18 | 37 | 55 | 73 | 92 | 110 | 128 | 147 | 165 | 183 | 367 | 551 | 734 |
| 6000 | 22 | 44 | 66 | 88 | I IO | 132 | ${ }^{1} 54$ | 176 | 198 | 220 | 440 | 661 | 881 |
| 7000 | 26 | 5 I | 77 | 103 | 128 | ${ }^{1} 54$ | 180 | 206 | 231 | 257 | 514 | 77 I | 1028 |

METRIC MEASURES.
Correction for Humidity: Values of $10000 \beta$.
$\beta=0.378 \frac{e}{b}=0.378 \begin{aligned} & f+f_{0} \\ & B+B_{\circ}\end{aligned}$.

| Mean Vapor | MEAN BA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $e=\frac{f+f_{0}}{2}$ | 500 | 520 | 540 | 560 | 580 | 600 | 620 | 640 | 660 | 680 | 700 | 720 | 740 | 760 |
| mm . | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm . | mm . |
| 1 | 8 | 7 | 7 | 7 | 7 | 6 | 6 | 6 | 6 | 6 | 5 | 5 | 5 | 5 |
| 2 | 15 | 15 | 14 | 14 | 13 | 13 | 12 | 12 | 11 | 11 | 11 | 11 | 10 | 10 |
| 3 | 23 | 22 | 21 | 20 | 20 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 15 |
| 4 | 30 | 29 | 28 | 27 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 20 | 20 |
| 5 | 38 | 36 | 35 | 34 | 33 | 31 | 30 | 30 | 29 | 28 | 27 | 26 | 26 | 25 |
| 6 | 45 | 44 | 42 | 4 I | 39 | 38 | 37 | 35 | 34 | 33 | 32 | 32 | 31 | 30 |
| 7 | 53 | 51 | 49 | 47 | 46 | 44 | 43 | 4 I | 40 | 39 | 38 | 37 | 36 | 35 |
| 8 | 60 | 58 | 56 | 54 | 52 | 50 | 49 | 47 | 46 | 44 | 43 | 42 | 4 I | 40 |
| 9 | 68 | 65 | 63 | 6 I | 59 | 57 | 55 | 53 | 52 | 50 | 49 | 47 | 46 | 45 |
| 10 | 76 | 73 | 70 | 68 | 65 | 63 | 61 | 59 | 57 | 56 | 54 | 53 | 51 | 50 |
| 11 | 83 | 80 | 77 | 74 | 72 | 69 | 67 | 65 | 63 | 61 | 59 | 58 | 56 | 55 |
| 12 | 9 I | 87 | 84 | 81 | 78 | 76 | 73 | 7 I | 69 | 67 | 65 | 63 | 61 | 60 |
| 13 | 98 | 95 | 91 | 88 | 85 | 82 | 79 | 77 | 74 | 72 | 70 | 68 | 66 | 65 |
| 14 | 106 | 102 | 98 | 95 | 9 I | 88 | 85 | 83 | 80 | 78 | 76 | 74 | 72 | 70 |
| 15 | II3 | 109 | 105 | 101 | 98 | 95 | 91 | 89 | 86 | 83 | 81 | 79 | 77 | 75 |
| 16 | 121 | 116 | 112 | 108 | 104 | 101 | 98 | 94 | 92 | 89 | 86 | 84 | 82 | So |
| 17 | 129 | 124 | 119 | II5 | III | 107 | 104 | 100 | 97 | 94 | 92 | 89 | 87 | 85 |
| 18 | 136 | 131 | 126 | 122 | II7 | II3 | 110 | 106 | 103 | 100 | 97 | 95 | 92 | 90 |
| 19 | 144 | I38 | I 33 | 128 | 124 | 120 | II6 | 112 | 109 | 106 | 103 | 100 | 97 | 95 |
| 20 | 151 | 145 | 140 | I35 | 130 | 126 | 122 | 118 | I 15 | III | 108 | 105 | 102 | 99 |
| 21 | 159 | 153 | 147 | 142 | I 37 | 132 | 128 | 124 | 120 | 117 | 113 | IIO | 107 | 104 |
| 22 | 166 | 160 | I 54 | 149 | 143 | 139 | 134 | 130 | 126 | 122 | 119 | 116 | 112 | 109 |
| 23 | 174 | 167 | 161 | 155 | 150 | 145 | 140 | 136 | 132 | 128 | 124 | 121 | 117 | 114 |
| 24 | I8I | 174 | 168 | 162 | I 56 | 151 | 146 | 142 | 137 | I 33 | 130 | 126 | 123 | 119 |
| 25 | 189 | 182 | 175 | 169 | 163 | 157 | 152 | 148 | 143 | 139 | 135 | I3I | 128 | 124 |
| 26 | 197 | I89 | 182 | 175 | 169 | 164 | 159 | 154 | 149 | 145 | 140 | 137 | 133 | 129 |
| 27 | 204 | 196 | 189 | 182 | 176 | 170 | 165 | 159 | I55 | 150 | 146 | 142 | 138 | 134 |
| 28 | 2 I 2 | 204 | 196 | 189 | 182 | 176 | 171 | 165 | 160 | 156 | 151 | 147 | 143 | I 39 |
| 29 | 219 | 211 | 203 | 196 | I89 | 183 | 177 | 171 | 166 | 161 | I57 | 152 | 148 | 144 |
| 30 | 227 | 218 | 210 | 203 | 196 | 189 | 183 | 177 | 172 | 167 | 162 | 158 | I53 | 149 |
| 31 | 234 | 225 | 217 | 209 | 202 | 195 | 189 | 183 | 178 | 172 | 167 | 163 | 158 | 154 |
| 32 | 242 | 233 | 224 | 216 | 209 | 202 | 195 | 189 | 183 | 178 | 173 | 168 | 163 | 159 |
| 33 | 249 | 240 | 231 | 223 | 215 | 208 | 201 | 195 | 189 | 183 | 178 | 173 | 169 | 164 |
| 34 | 257 | 247 | 238 | 230 | 222 | 214 | 207 | 201 | 195 | 189 | 184 | 179 | 174 | I69 |
| 35 | 265 | 254 | 245 | 236 | 228 | 220 | 213 | 207 | 200 | 195 | IS9 | 184 | 179 | 174 |
| 36 | 272 | 262 | 252 | 243 | 235 | 227 | 219 | 213 | 206 | 200 | 194 | I89 | 184 | 179 |
| 37 | 280 | 269 | 259 | 250 | 241 | 233 | 226 | 219 | 212 | 206 | 200 | 194 | I89 | 184 |
| 38 | 287 | 276 | 266 | 257 | 248 | 239 | 232 | 224 | 218 | 2 II | 205 | 200 | 194 | 189 |
| 39 | 295 | 283 | 273 | 263 | 254 | 246 | 238 | 230 | 223 | 217 | 211 | 205 | 199 | 194 |
| 40 | 302 | 291 | 280 | 270 | 26 I | 252 | 244 | 236 | 229 | 222 | 216 | 210 | 204 | 199 |

TABLE 27.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
METRIC MEASURES.
Correction for Humidity: $10000 \beta \times \mathbf{z}$.
Top argument: Values of $10000 \beta$ obtained from page 112.
Side argument: Approximate difference of height (z).

| Approximate Difference of Height. Z. | $10000 \beta$. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25 | 50 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 | 275 | 300 |
| m . | m. | m . | m. | m . | m. | m . | m . | m. | m. | m. | m. | m. |
| 100 | 0.3 | 0.5 | 0.8 | 1.0 | 1.3 | 1.5 | 1.8 | 2.0 | 2.3 | 2.5 | 2.8 | 3.0 |
| 200 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | $3 \cdot 5$ | 4.0 | 4.5 | 5.0 | $5 \cdot 5$ | 6.0 |
| 300 | 0.8 | I. 5 | 2.3 | 3.0 | 3.8 | 4.5 | $5 \cdot 3$ | 6.0 | 6.8 | $7 \cdot 5$ | 8.3 | 9.0 |
| 400 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 9.0 | 10.0 | 11.0 | 12.0 |
| 500 | 1.3 | 2.5 | 3.8 | 5.0 | 6.3 | 7.5 | 8.8 | 10.0 | 11.3 | 12.5 | 13.8 | 15.0 |
| 600 | 1.5 | 3.0 | 4.5 | 6.0 | 7.5 | 9.0 | 10.5 | 12.0 | 13.5 | 15.0 | 16.5 | 18.0 |
| 700 | 1.8 | 3.5 | $5 \cdot 3$ | 7.0 | 8.8 | 10.5 | 12.3 | 14.0 | 15.8 | 17.5 | 19.3 | 21.0 |
| 800 | 2.0 | 4.0 | 6.0 | 8.0 | 10.0 | 12.0 | 14.0 | 16.0 | 18.0 | 20.0 | 22.0 | 24.0 |
| 900 | 2.3 | 4.5 | 6.8 | 9.0 | II. 3 | 13.5 | 15.8 | 18.0 | 20.3 | 22.5 | 24.8 | 27.0 |
| 1000 | 2.5 | 5.0 | 7.5 | 10.0 | 12.5 | 15.0 | 17.5 | 20.0 | 22.5 | 25.0 | 27.5 | 30.0 |
| 1100 | 2.8 | 5.5 | 8.3 | 11.0 | 13.8 | 16.5 | 19.3 | 22.0 | 24.8 | 27.5 | 30.3 | 33.0 |
| 1200 | 3.0 | 6.0 | 9.0 | 12.0 | 15.0 | 18.0 | 21.0 | 24.0 | 27.0 | 30.0 | 33.0 | 36.0 |
| 1300 | 3.3 | 6.5 | 9.8 | 13.0 | 16.3 | 19.5 | 22.8 | 26.0 | 29.3 | 32.5 | 35.8 | 39.0 |
| 1400 | $3 \cdot 5$ | 7.0 | 10.5 | 14.0 | 17.5 | 21.0 | 24.5 | 28.0 | 31.5 | 35.0 | 38.5 | 42.0 |
| 1500 | 3.8 | 7.5 | 11.3 | 15.0 | 18.8 | 22.5 | 26.3 | 30.0 | 33.8 | 37.5 | 41.3 | 45.0 |
| 1600 | 4.0 | 8.0 | 12.0 | 16.0 | 20.0 | 24.0 | 28.0 | 32.0 | 36.0 | 40.0 | 44.0 | 48.0 |
| I700 | $4 \cdot 3$ | 8.5 | 12.8 | 17.0 | 21.3 | 25.5 | 29.8 | 34.0 | 38.3 | 42.5 | 46.8 | 51.0 |
| 1800 | 4.5 | 9.0 | 13.5 | 18.0 | 22.5 | 27.0 | 3 I .5 | 36.0 | 40.5 | 45.0 | 49.5 | 54.0 |
| 1900 | 4.8 | 9.5 | 14.3 | 19.0 | 23.8 | 28.5 | 33.3 | 38.0 | 42.8 | 47.5 | 52.3 | 57.0 |
| 2000 | 5.0 | 10.0 | 15.0 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 | 45.0 | 50.0 | 55.0 | 60.0 |
| 2100 | $5 \cdot 3$ | 10.5 | 15.8 | 21.0 | 26.3 | 31.5 | 36.8 | 42.0 | 47.3 | 52.5 | 57.8 | 63.0 |
| 2200 | 5.5 | 11.0 | 16.5 | 22.0 | 27.5 | 33.0 | 38.5 | 44.0 | 49.5 | 55.0 | 60.5 | 66.0 |
| 2300 | 5.8 | II. 5 | 17.3 | 23.0 | 28.8 | 34.5 | 40.3 | 46.0 | 5 I .8 | 57.5 | 63.3 | 69.0 |
| 2400 | 6.0 | 12.0 | 18.0 | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 |
| 2500 | 6.3 | 12.5 | 18.8 | 25.0 | 31.3 | 37.5 | 43.8 | 50.0 | 56.3 | 62.5 | 68.8 | 75.0 |
| 2600 | 6.5 | 13.0 | 19.5 | 26.0 | 32.5 | 39.0 | 45.5 | 52.0 | 58.5 | 65.0 | 71.5 | 78.0 |
| 2700 | 6.8 | 13.5 | 20.3 | 27.0 | 33.8 | 40.5 | 47.3 | 54.0 | 60.8 | 67.5 | 74.3 | 81.0 |
| 2800 | 7.0 | 14.0 | 21.0 | 28.0 | 35.0 | 42.0 | 49.0 | 56.0 | 63.0 | 70.0 | 77.0 | 84.0 |
| 2900 | $7 \cdot 3$ | 14.5 | 21.8 | 29.0 | 36.3 | 43.5 | 50.8 | 58.0 | 65.3 | 72.5 | 79.8 | 87.0 |
| 3000 | 7.5 | 15.0 | 22.5 | 30.0 | 37.5 | 45.0 | 52.5 | 60.0 | 67.5 | 75.0 | 82.5 | 90.0 |
| 3100 | 7.8 | 15.5 | 23.3 | 31.0 | 38.8 | 46.5 | 54.3 | 62.0 | 69.8 | 77.5 | 85.3 | 93.0 |
| 3200 | 8.0 | 16.0 | 24.0 | 32.0 | 40.0 | 48.0 | 56.0 | 64.0 | 72.0 | 80.0 | 88.0 | 96.0 |
| 3300 | 8.3 | 16.5 | 24.8 | 33.0 | 41.3 | 49.5 | 57.8 | 66.0 | 74.3 | 82.5 | 90.8 | 99.0 |
| 3400 | 8.5 | 17.0 | 25.5 | 34.0 | 42.5 | 51.0 | 59.5 | 68.0 | 76.5 | 85.0 | 93.5 | 102.0 |
| 3500 | 8.8 | 17.5 | 26.3 | 35.0 | 43.8 | 52.5 | 61.3 | 70.0 | 78.8 | 87.5 | 96.3 | 105.0 |
| 3600 | 9.0 | 18.0 | 27.0 | 36.0 | 45.0 | 54.0 | 63.0 | 72.0 | 81.0 | 90.0 | 99.0 | 108.0 |
| 3700 | $9 \cdot 3$ | 18.5 | 27.8 | 37.0 | 46.3 | 55.5 | 64.8 | 74.0 | 83.3 | 92.5 | 101.8 | 111.0 |
| 3800 | 9.5 | 19.0 | 28.5 | 38.0 | 47.5 | 57.0 | 66.5 | 76.0 | 85.5 | 95.0 | 104.5 | 114.0 |
| 3900 | 9.8 | 19.5 | 29.3 | 39.0 | 48.8 | 58.5 | 68.3 | 78.0 | 87.8 | 97.5 | 107.3 | 117.0 |
| 4000 | 10.0 | 20.0 | 30.0 | 40.0 | 50.0 | 60.0 | 70.0 | 80.0 | 90.0 | 100.0 | 110.0 | 120.0 |
| 5000 | 12.5 | 25.0 | 37.5 | 50.0 | 62.5 | 75.0 | 87.5 | 100.0 | 112.5 | 125.0 | 137.5 | 150.0 |
| 6000 | 15.0 | 30.0 | 45.0 | 60.0 | 75.0 | 90.0 | 105.0 | 1200 | 135.0 | 150.0 | 165.0 | 180.0 |
| 7000 | 17.5 | 35.0 | 52.5 | 70.0 | 87.5 | 105.0 | 122.5 | 140.0 | I57.5 | 175.0 | 192.5 | 210.0 |

8mithbonian Tables.

## METRIC MEASURES.

Correction for Latitude and Weight of Mercury : $\mathrm{z}(0.002662 \cos 2 \boldsymbol{\phi}+0.00239)$.

| Approximate difference of Height. Z. | LATITUDE ( $\phi$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0{ }^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ | $45^{\circ}$ | $50^{\circ}$ | $55^{\circ}$ | $60^{\circ}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ |
| metres. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 100 | 1 | I | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 200 | I | 1 | I | 1 | 1 | 1 | 1 | 1 | 1 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 |
| 300 | 2 | 2 | 1 | 1 | I | 1 | 1 | I | I | 1 | 1 | 0 | 0 | 0 | o | - |
| 400 | 2 | 2 | 2 | 2 | 2 | 2 | I | I | I | I | 1 | I | 0 | 0 | 0 | 0 |
| 500 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | I | I | 1 | I | 0 | 0 | 0 |
| 600 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 1 | 1 | I | I | 0 | - | 0 |
| 700 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 1 | 1 | I | 0 | - | - |
| 800 | 4 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 2 | 2 | 2 | I | 1 | I | - | - |
| 900 | 5 | 5 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 2 | 2 | I | I | 1 | 0 | 0 |
| 1000 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 3 | 3 | 2 | 2 | 1 | I | I | 0 | 0 |
| 1100 | 6 | 6 | 5 | 5 | 5 | 5 | 4 | 4 | 3 | 3 | 2 | 2 | I | I | - | - |
| 1200 | 6 | 6 | 6 | 6 | 5 | 5 | 4 | 4 | 3 | 3 | 2 | 2 | I | I | 0 | - |
| 1300 | 7 | 7 | 6 | 6 | 6 | 5 | 5 | 4 | 4 | 3 | 3 | 2 | I | I | 0 | o |
| 1400 | 7 | 7 | 7 | 7 | 6 | 6 | 5 | 5 | 4 | 3 | 3 | 2 | I | I | 0 | - |
| 1500 | 8 | 8 | 7 | 7 | 7 | 6 | 6 | 5 | 4 | 4 | 3 | 2 | 2 | 1 | I | 0 |
| 1600 | 8 | 8 | 8 | 8 | 7 | 7 | 6 | 5 | 5 | 4 | 3 | 2 | 2 | I | I | 0 |
| 1700 | 9 | 9 | 8 | 8 | 8 | 7 | 6 | 6 | 5 | 4 | 3 | 3 | 2 | 1 | 1 | 0 |
| 1800 | 9 | 9 | 9 | 8 | 8 | 7 | 7 | 6 | 5 | 4 | 3 | 3 | 2 | I | 1 | - |
| 1900 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | 6 | 5 | 5 | 4 | 3 | 2 | I | I | 0 |
| 2000 | 10 | 10 | 10 | 9 | 9 | 8 | 7 | 7 | 6 | 5 | 4 | 3 | 2 | I | I | o |
| 2100 | II | II | 10 | 10 | 9 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | I | I | - |
| 2200 | II | II | II | 10 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | I | I | 0 |
| 2300 | 12 | 12 | II | II | 10 | 9 | 9 | 8 | 7 | 5 | 4 | 3 | 2 | 2 | 1 | o |
| 2400 | 12 | 12 | 12 | II | II | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | I | 0 |
| 2500 | 13 | I3 | 12 | 12 | II | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 2600 | 13 | 13 | I3 | 12 | 12 | II | 10 | 9 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 2700 | 14 | 14 | 13 | 13 | 12 | II | 10 | 9 | 8 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 2800 | 14 | 14 | 14 | 13 | 12 | II | IO | 9 | 8 | 7 | 5 | 4 | 3 | 2 | I | - |
| 2900 | I5 | I5 | 14 | 14 | 13 | 12 | II | 10 | 8 | 7 | 6 | 4 | 3 | 2 | I | 0 |
| 3000 | I5 | I5 | I5 | 14 | 13 | 12 | II | 10 | 9 | 7 | 6 | 4 | 3 | 2 |  | - |
| 3100 | 16 | 16 | I5 | 15 | 14 | 13 | 12 | 10 | 9 | 7 | 6 | 5 | 3 | 2 | I | - |
| 3200 | 16 | 16 | 16 | 15 | 14 | 13 | 12 | II | 9 | 8 | 6 | 5 | 3 | 2 | 1 | - |
| 3300 | 17 | 17 | 16 | 15 | 15 | 14 | 12 | II | 9 | 8 | 6 | 5 | 3 | 2 | I | 0 |
| 3400 | 17 | 17 | 17 | 16 | 15 | 14 | 13 | II | 10 | 8 | 7 | 5 | 4 | 2 | 1 | 0 |
| 3500 | 18 | 18 | 17 | 16 | 16 | 14 | 13 | 12 | 10 | 8 | 7 | 5 | 4 | 2 | I | 0 |
| 3600 | 18 | 18 | 18 | 17 | 16 | 15 | 13 | 12 | 10 | 9 | 7 | 5 | 4 | 2 | I | o |
| 3700 | 19 | 19 | 18 | 17 | 16 | 15 | 14 | 12 | II | 9 | 7 | 5 | 4 | 3 | I | 0 |
| 3800 | 19 | 19 | 19 | 18 | 17 | 16 | 14 | 13 | II | 9 | 7 | 6 | 4 | 3 | I | 0 |
| 3900 | 20 | 20 | 19 | 18 | 17 | 16 | I5 | I3 | II | 9 | 8 | 6 | 4 | 3 | I | 0 |
| 4000 | 20 | 20 | 20 | 19 | 18 | 16 | 15 | I3 | II | 10 | 8 | 6 | 4 | 3 | 1 | 0 |
| 4500 | 23 | 23 | 22 | 21 | 20 | 18 | 17 | 15 | 13 | II | 9 | 7 | 5 | 3 | 2 | 0 |
| 5000 | 25 | 25 | 24 | 23 | 22 | 21 | 19 | 17 | 14 | 12 | 10 |  | 5 | 3 | 2 | 0 |
| 5500 | 28 | 28 | 27 | 26 | 24 | 23 | 20 | 18 | 16 | 13 | II | 8 | 6 | 4 | 2 | 0 |
| 6000 | 30 | 30 | 29 | 28 | 27 | 25 | 22 | 20 | 17 | 14 | 12 | 9 | 6 | 4 | 2 | I |
| 6500 | 33 | 33 | 32 | 3I | 29 | 27 | 24 | 2 I | 19 | 16 | 13 | 10 | 7 | 4 | 2 | I |
| 7000 | 35 | 35 | 34 | 33 | 3 I | 29 | 26 | 23 | 20 | 17 | 13 | 10 | 7 | 5 | 2 | I |

TABLE 29.
DETERMINATION OF HEIGHTS BY THE BAROMETER. METRIC MEASURES.
Correction for the variation of gravity with altitude: $\frac{\mathrm{z}\left(\mathrm{z}+2 h_{\mathrm{o}}\right)}{R}$

| Approximate difference of height. 2. | HEIGHT OF LOWER STATION IN METRES ( $h_{\text {O }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 200 | 400 | 600 | 800 | 1000 | 1200 | 1400 | 1600 | 1800 | 2000 | 2500 | 3000 | 4000 |
| metres. | m . | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 200 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | o | 0 |
| 300 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 400 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 1 |
| 500 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $I$ | 1 |
| 600 | 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | I | I |
| 700 | o | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | I | 1 | 1 | 1 |
| 800 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | I | 1 | 1 | 1 |
| 900 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 1000 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | I | I | I | 1 | 1 | I | 1 |
| 1100 | 0 | 0 | 0 | 0 | - | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2 |
| 1200 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | I | 2 |
| 1300 | 0 | 0 | 0 | I | I | 1 | 1 | 1 | 1 | I | 1 | I | 1 | 2 |
| 1400 | 0 | 0 | 0 | I | I | I | I | I | 1 | 1 | 1 | 1 | 2 | 2 |
| 1500 | 0 | 0 | I | I | I | I | 1 | I | I | I | I | 2 | 2 | 2 |
| 1600 | 0 | I | I | 1 | I | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 |
| 1700 | 0 | I | I | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 3 |
| 1800 | I | I | I | I | I | 1 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 3 |
| 1900 | I | I | I | I | I | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 3 |
| 2000 | I | I | 1 | I | I | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 3 | 3 |
| 2100 | I | I | I | I | I | I | 1 | 2 | 2 | 2 | 2 | 2 | 3 | 3 |
| 2200 | I | I | 1 | 1 | I | I | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 4 |
| 2300 | I | I | 1 | I | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 4 |
| 2400 | I | I | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 4 |
| 2500 | I | I | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 |
| 2600 | 1 | I | I | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 |
| 2700 | 1 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 5 |
| 2800 | I | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 5 |
| 2900 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 5 |
| 3000 | 1 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 5 |
| 3100 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 5 |
| 3200 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 5 | 6 |
| 3300 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 5 | 6 |
| 3400 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 6 |
| 3500 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 6 |
| 3600 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 7 |
| 3700 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 4 | 5 | 6 | 7 |
| 3800 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 6 | 7 |
| 3900 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 6 | 7 |
| 4000 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 6 | 6 | 8 |
| 4500 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 5 | 5 | 6 | 6 | 7 | 7 | 9 |
| 5000 | 4 | 4 | 5 | 5 | 5 | 5 | 6 | 6 | 6 | 7 | 7 | 8 | 9 | 10 |
| 5500 | 5 | 5 | 5 | 6 | 6 | 6 | 7 | 7 | 8 | 8 | 8 | 9 | 10 | 12 |
| 6000 | 6 | 6 | 6 | 7 | 7 | 8 | 8 | 8 | 9 | 9 | 9 | 10 | II | 13 |
| 6500 | 7 | 7 | 7 | 8 | 8 | 9 | 9 | 9 | 10 | 10 | II | 12 | 13 | 15 |
| 7000 | 8 | 8 | 9 | 9 | 9 | 10 | 10 | II | II | 12 | 12 | I3 | 14 | 16 |

TAble 30.

## DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF O.1 INCH IN THE BAROMETER.

## ENGLISH MEASURES.

| Barometric Pressure. | MEAN TEMPERATURE OF THE AIR IN |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ | $45^{\circ}$ | $50^{\circ}$ | $55^{\circ}$ | $60^{\circ}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ |
| Inches | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 22.0 | 119.2 | 120.5 | 121.8 | 123.I | 124.4 | 125.8 | 127.1 | 128.5 | 129.8 | I3I. 2 | I32.5 | 133.9 |
| . 2 | II8.2 | 119.4 | 120.7 | 122.0 | 123.3 | 124.7 | 126.0 | 127.3 | 128.7 | I30.0 | I3I. 3 | I32.7 |
| . 4 | 117.1 | 118.3 | I 19.6 | 120.9 | 122.2 | 123.6 | 124.9 | 126.2 | 127.5 | 128.8 | I30.2 | I3I. 5 |
| . 6 | II6.I | 117.3 | II8.6 | 119.8 | 121.1 | 122.5 | 123.8 | 125.1 | 126.4 | 127.7 | 129.0 | I30.3 |
| . 8 | II5.0 | 116.3 | 117.5 | I18.8 | 120.I | 121.4 | 122.7 | 124.0 | 125.3 | 126.6 | 127.9 | 129.2 |
| 23.0 | II4.0 | 115.3 | 116.5 | 117.8 | 119.0 | 120.3 | 121.6 | 122.9 | 124.2 | 125.5 | 126.8 | 128.1 |
| . 2 | II3.I | 114.3 | 115.5 | 116.8 | 118.0 | 119.3 | I20.6 | 121.8 | 123. 1 | 124.4 | 125.7 | 127.0 |
| . 4 | II2.I | 113.3 | 114.5 | 115.8 | 117.0 | II8.3 | 119.5 | 120.8 | 122.1 | 123.3 | 124.6 | 125.9 |
| . 6 | III.I | II2.3 | II 3.5 | II4.8 | II6.0 | 117.3 | II8.5 | 119.8 | 121.0 | 122.3 | 123.5 | 124.8 |
| . 8 | IIO. 2 | III. 4 | II2.6 | II3.8 | II5.I | II6.3 | II7.5 | II8.8 | 120.0 | 12I. 3 | 122.5 | 123.8 |
| 24.0 | 109.3 | 110.5 | 111.7 | II2.9 | II4. I | 115.3 | 116.5 | 117.8 | 119.0 | 120.2 | 121.5 | 122.7 |
| . 2 | 108.4 | 109.5 | 110.7 | III. 9 | I13.I | II4.4 | II5.6 | 116.8 | I18.0 | 119.2 | 120.5 | 121. 7 |
| . 4 | 107.5 | 108.6 | 109.8 | III.O | II2.2 | II3.4 | II4.6 | II5.9 | II7. 1 | 118.3 | 119.5 | 120.7 |
| . 6 | 106.6 | 107.8 | 108.9 | IIO. I | IIII. 3 | II2.5 | 113.7 | II4.9 | II6.I | 117.3 | 118.5 | 119.7 |
| . 8 | 105.8 | 106.9 | 108.I | 109.2 | 110.4 | III. 6 | I12.8 | II4.0 | II5.2 | II6.4 | 117.6 | 118.8 |
| 25.0 | 104.9 | 106.0 | 107.2 | 108.3 | 109.5 | 110.7 | III. 9 | II3.I | II4.2 | II5.4 | II6.6 | 117.8 |
| . 2 | 104. 1 | 105.2 | 106.3 | 107.5 | 108.7 | 109.8 | III.O | II2.2 | II3.3 | II4.5 | II 5.7 | 116.9 |
| . 4 | 103.3 | 104.4 | 105.5 | 106.6 | 107.8 | 109.0 | IIO. I | III. 3 | II2.4 | II3.6 | II4.8 | I16.0 |
| . 6 | 102.5 | 103.6 | 104.7 | 105.8 | 107.0 | 108. 1 | 109.3 | 110.4 | III. 6 | II2.7 | II 3.9 | 115.I |
| . 8 | IOI. 7 | 102.8 | 103.9 | 105.0 | 106. I | 107.3 | 108.4 | 109. 6 | 110.7 | III. 9 | II3.0 | II4.2 |
| 26.0 | 100.9 | 102.0 | 103. I | 104.2 | 105.3 | 106.4 | 107.6 | 108.7 | 109.9 | III.O | II2.I | II3.3 |
| . 2 | 100. 1 | 101.2 | 102.3 | 103.4 | 104.5 | 105.6 | 106.8 | 107.9 | 109.0 | IIO. 1 | III. 3 | II2.4 |
| . 4 | 99.4 | 100.4 | 101. 5 | 102.6 | 103.7 | 104.8 | 106.0 | 107. 1 | 108.2 | 109.3 | 110.4 | III. 6 |
| . 6 | 98.6 | 99.7 | 10.7 | IOI. 8 | 102.9 | 104.0 | 105.2 | 106.3 | 107.4 | 108.5 | 109.6 | 110.7 |
| . 8 | 97.9 | 98.9 | 10.0 | IOI. I | 102.2 | 103.3 | 104.4 | 105.5 | 106.6 | 107.7 | 108.8 | 109.9 |
| 27.0 | 97.1 | 98.2 | 99.2 | 100.3 | IOI. 4 | 102.5 | 103.6 | 104.7 | 105.8 | 106.9 | 108.0 | 109. 1 |
| . 2 | 96.4 | 97.5 | 98.5 | 99.6 | 100.7 | 101. 8 | 102.8 | 103.9 | 105.0 | 106. I | 107.2 | 108.3 |
| . 4 | 95.7 | 96.8 | 97.8 | 98.9 | 99.9 | 101.0 | IO2. I | 103.2 | 104.2 | 105.3 | 106.4 | 107.5 |
| . 6 | 95.0 | 96.1 | 97. 1 | 98.1 | 99.2 | 100.3 | roi. 3 | 102.4 | 103.5 | 104.6 | 105.6 | 106.7 |
| . 8 | 94.3 | 95.4 | 96.4 | 97.4 | 98.5 | 99.6 | 100.6 | IOI. 7 | 102.7 | 103.8 | I04.9 | 105.9 |
| 28.0 | 93.7 | 94.7 | 95.7 | 96.7 | 97.8 | 98.8 | 99.9 | IOI. 0 | 102.0 | 103. I | 104. 1 | 105.2 |
| . 2 | 93.0 | 94.0 | 95.0 | 96.1 | 97. 1 | 98.1 | 99.2 | 100.2 | 101. 3 | 102.3 | 103.4 | 104.4 |
| . 4 | 92.4 | 93.4 | 94.4 | 95.4 | 96.4 | 97.5 | 98.5 | 99.5 | 100. 6 | IOI. 6 | 102.7 | 103.7 |
| . 6 | 91.7 | 92.7 | 93.7 | 94.7 | 95.7 | 96.8 | 97.8 | 98.8 | 99.9 | 100.9 | IOI. 9 | 103.0 |
| . 8 | 91.1 | 92.1 | 93.1 | 94.1 | 95.1 | 96.1 | 97.1 | 98.2 | 99.2 | 100.2 | IOI. 2 | 102.3 |
| 29.0 | 90.4 | 91.4 | 92.4 | 93.4 | 94.4 | 95.4 | 96.5 | 97.5 | 98.5 | 99.5 | 100.5 | IOI. 6 |
| . 2 | 89.8 | 90.8 | 91.8 | 92.8 | 93.8 | 94.8 | 95.8 | 96.8 | 97.8 | 98.8 | 99.9 | 100.9 |
| . 4 | 89.2 | 90.2 | 91.1 | 92.1 | 93.1 | 94.I | 95.1 | 96.1 | 97. 1 | 98.2 | 99.2 | 100.2 |
| . 6 | 88.6 | 89.6 | 90.5 | 91.5 | 92.5 | 93.5 | 94.5 | 95.5 | 96.5 | 97.5 | 98.5 | 99.5 |
| . 8 | 88.0 | 89.0 | 89.9 | 90.9 | 91.9 | 92.9 | 93.9 | 94.9 | 95.8 | 96.8 | 97.8 | 98.8 |
| 30.0 | 87.4 | 88.4 | 89.3 | 90.3 | 91.3 | 92.3 | 93.2 | 94.2 | 95.2 | 96.2 | 97.2 | 98.2 |
| . 2 | 86.8 | 87.8 | 88.7 | 89.7 | 90.7 | 91.7 | 92.6 | 93.6 | 94.6 | 95.6 | 96.5 | 97.5 |
| . 4 | 86.3 | 87.2 | 88.2 | 89.1 | 90.1 | 91.1 | 92.0 | 93.0 | 94.0 | 94.9 | 95.9 | 96.9 |
| . 6 | 85.7 | 86.7 | 87.6 | 88.5 | 89.5 | 90.5 | 91.4 | 92.4 | 93.3 | 94.3 | 95.3 | 96.2 |
| . 8 | 85.2 | 86. 1 | 87.0 | 88.0 | 88.9 | 89.9 | 90.8 | 91.8 | 92.7 | 93.7 | 94.7 | 95.6 |

Table 31.
DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 1 MILLIMETRE IN THE BAROMETER.

METRIC MEASURES.

| Barometric Pressure. | MEAN TEMPERATURE OF THE AIR IN CENTIGRADE DEGREES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-2^{\circ}$ | $0^{\circ}$ | $2^{\circ}$ | $4^{\circ}$ | $6^{\circ}$ | $8^{\circ}$ | $10^{\circ}$ | $12^{\circ}$ | $14^{\circ}$ | $16^{\circ}$ |
| m | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. | Metres. |
| 760 | 10.48 | 10.57 | 10.65 | 10.73 | 10.81 | 10.89 | 10.98 | 11.06 | II. 15 | 11.23 |
| 750 | 10.62 | 10.71 | 10.79 | 10.87 | 10.95 | 11.04 | I1.13 | II.2I | 11.30 | 11.38 |
| 740 | 10.77 | 10.85 | 10.93 | 11.02 | II.10 | II.19 | 11.28 | 11.36 | 11.45 | II. 54 |
| 730 | 10.91 | 11.00 | 11.08 | 11.17 | II. 26 | II. 35 | 11.43 | II. 52 | 11.61 | 11.70 |
| 720 | 11.06 | 11.15 | II. 24 | 11.32 | 11.42 | 11.51 | II. 59 | 11.68 | 11.77 | 11.86 |
| 710 | II 1.22 | II. 31 | II. 40 | II. 48 | II.58. | 11.67 | II. 75 | II. 85 | 11.94 | 12.03 |
| 700 | II. 38 | II. 47 | 11.56 | 11.65 | 11.74 | 11.83 | 11.92 | 12.02 | 12.11 | 12.20 |
| 690 | II. 55 | 11.63 | 11.72 | 11.82 | 11.91 | 12.00 | 12.09 | 12.19 | 12.28 | 12.38 |
| 680 | II. 72 | 11.80 | 11.89 | I1. 99 | 12.08 | 12.18 | 12.27 | 12.37 | 12.46 | 12.56 |
| 670 | 11.89 | 11.98 | 12.07 | 12.17 | 12.26 | 12.36 | 12.46 | 12.55 | 12.65 | 12.75 |
| 660 | 12.07 | 12.16 | 12.26 | 12.35 | 12.45 | 12.55 | 12.65 | 12.74 | 12.84 | 12.94 |
| 650 | 12.26 | 12.35 | 12.45 | 12.54 | 12.64 | 12.74 | 12.84 | 12.94 | 13.04 | 13.14 |
| 640 | 12.45 | 12.55 | 12.64 | 12.74 | 12.84 | 12.94 | 13.04 | 13.14 | 13.24 | 13.35 |
| 630 | 12.65 | 12.75 | 12.84 | 12.94 | 13.04 | 13.15 | 13.25 | 13.35 | 13.45 | 13.56 |
| 620 | 12.85 | 12.96 | 13.05 | 13.15 | 13.25 | 13.36 | 13.46 | 13.57 | 13.67 | 13.78 |
| 610 | 13.06 | 13.17 | 13.27 | 13.37 | 13.47 | 13.58 | 13.68 | 13.79 | 13.89 | 14.01 |
| 600 | 13.28 | 13.39 | 13.49 | 13.59 | 13.70 | 13.80 | 13.91 | 14.02 | 14.13 | 14.24 |
| 590 | 13.51 | 13.62 | 13.72 | 13.82 | 13.93 | 14.03 | 14.15 | 14.26 | 14.37 | 14.48 |
| 580 | 13.74 | 13.85 | 13.96 | 14.06 | 14.17 | 14.28 | 14.39 | 14.51 | 14.62 | 14.73 |
| 570 | 13.98 | 14.09 | 14.20 | 14.31 | 14.42 | 14.53 | 14.64 | 14.76 | 14.88 | 14.99 |
| 560 | 14.23 | 14.34 | 14.45 | 14.57 | 14.68 | 14.79 | 14.90 | 15.02 | 15.14 | 15.25 |
| Barometric <br> Pressure. | MEAN TEMPERATURE OF THE AIR IN CENTIGRADE DEGREES. |  |  |  |  |  |  |  |  |  |
|  | $18^{\circ}$ | $20^{\circ}$ | $22^{\circ}$ | $24^{\circ}$ | $26^{\circ}$ | $28^{\circ}$ | $30^{\circ}$ | $32^{\circ}$ | $34^{\circ}$ | $36^{\circ}$ |
| $\begin{aligned} & \mathrm{mm} . \\ & 760 \end{aligned}$ | Metres. <br> II. 32 | Metres. $\text { II. } 4 \mathrm{I}$ | Metres. $\text { II } .49$ | Metres. $\text { II. } 58$ | Metres. <br> II. 66 | Metres. $\text { II. } 75$ | Metres. $11.84$ | Metres. $\text { II. } 92$ | Metres. $12.01$ | Metres. 12.10 |
| 750 | 11.47 | 11.56 | II. 64 | 11.73 | 11.82 | II.9I | 12.00 | 12.08 | 12.17 | 12.26 |
| 740 | 11.63 | 11.72 | 11.80 | 11.89 | 11.98 | 12.07 | 12.16 | 12.24 | 12.33 | 12.42 |
| 730 | II. 79 | II. 88 | 11.96 | 12.05 | 12.15 | 12.23 | 12.32 | 12.41 | 12.50 | 12.59 |
| 720 | 11.95 | 12.04 | 12.13 | 12.22 | 12.32 | 12.40 | 12.49 | 12.58 | 12.68 | 12.77 |
| 710 | 12.12 | 12.2I | 12.30 | 12.39 | 12.49 | 12.58 | 12.67 | 12.76 | 12.86 | 12.95 |
| 700 | 12.29 | 12.39 | 12.48 | 12.57 | 12.67 | 12.76 | 12.85 | 12.94 | 13.04 | 13.13 |
| 690 | 12.47 | 12.57 | 12.66 | 12.75 | 12.85 | 12.94 | 13.04 | 13.13 | 13.23 | 13.32 |
| 680 | 12.66 | 12.75 | 12.85 | 12.94 | 13.04 | 13.13 | 13.23 | 13.32 | 13.42 | 13.52 |
| 670 | 12.85 | 12.94 | 13.04 | 13.14 | 13.23 | 13.33 | 13.43 | 13.52 | 13.62 | 13.72 |
| 660 | 13.04 | 13.14 | 13.24 | 13.34 | 13.43 | 13.53 | 13.63 | 13.73 | 13.83 | 13.93 |
| 650 | 13.24 | 13.34 | 13.44 | 13.54 | 13.64 | 13.74 | 13.84 | 13.94 | 14.04 | 14.15 |
| 640 | I 3.45 | 13.55 | 13.65 | 13.75 | 13.85 | 13.96 | 14.06 | 14.15 | 14.26 | 14.37 |
| 630 | 13.66 | 13.76 | 13.87 | 13.97 | 14.07 | 14.18 | 14.28 | 14.38 | 14.49 | 14.60 |
| 620 | 13.88 | 13.98 | 14.09 | 14.20 | 14.30 | 14.41 | 14.51 | 14.62 | 14.72 | 14.83 |
| 610 | 14.II | 14.21 | 14.32 | 14.43 | 14.54 | 14.64 | 14.75 | 14.86 | 14.96 | 15.07 |
| 600 | 14.35 | 14.45 | 14.56 | 14.67 | 14.78 | 14.89 | 15.00 | 15.11 | 15.21 | 15.32 |
| 590 | 14.59 | 14.70 | 14.81 | 14.92 | 15.03 | 15.14 | 15.25 | 15.36 | ${ }^{5} 5.47$ | 15.59 |
| 580 | 14.84 | 14.95 | 15.07 | 15.17 | 15.29 | 15.40 | ${ }^{1} 5.52$ | 15.63 | 15.74 | 15.86 |
| 570 560 | 15.10 15.37 | 15.21 | 15.33 | 15.44 | 15.56 | 15.67 | 15.79 | 15.91 | 16.02 | 16.14 |
| 560 | 15.37 | 15.48 | 15.60 | 15.72 | 15.84 | 15.95 | 16.07 | 16.19 | 16.30 | 16.42 |

Table 32.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
Formula of Babinet.

$$
z=C \frac{B_{0}-B}{B_{0}+B}
$$

$C($ in feet $)=52494\left[\mathrm{x}+\frac{t_{0}+t-64}{900}\right]$-English Measures.
$C$ (in metres) $=16000\left[\mathrm{r}+\frac{2\left(t_{0}+t\right)}{1000}\right]$-Metric Measures.
In which $Z=$ Difference of height of two stations in feet or metres.
$B_{0}, B=$ Barometric readings at the lower and upper stations respectively, corrected for all sources of instrumental error.
$t_{\mathrm{o}}, \boldsymbol{t}=$ Air temperatures at the lower and upper stations respectively.
Values of $\mathbf{C}$.
ENGLISH MEASURES.

| 1/2 $\left(t_{0}+\mathbf{t}\right)$. | $\log C$. | C. | 1/2 $\left(t_{0}+\mathbf{t}\right)$. | $\log C$. | C. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| F. |  | Feet. | c. |  | Metres. |
| $10^{\circ}$ | 4.69834 | 49928 | $-10^{\circ}$ | 4.18639 | 15360 |
| 15 | .70339 | 50511 | -8 | . 19000 | 15488 |
| 20 | . 70837 | 51094 | -6 | . 19357 | 15616 |
| 25 | . 71330 | 51677 | -4 | . 19712 | 15744 |
| 30 | .71818 | 52261 | -2 | . 20063 | 15872 |
|  |  |  | 0 | 4.20412 | 16000 |
| 35 |  |  | +2 | . 20758 | 16128 |
| 35 | 4.72300 | 52844 | 4 | .21101 | 16256 |
| 40 | . 72777 | 53428 | 6 | . 21442 | 16384 |
| 45 | . 73248 | 5401 I | 8 | . 21780 | 16512 |
| 50 | . 73715 | 54595 |  |  |  |
| 55 | .74177 | 55178 | 12 | 4.22115 .22448 | $\begin{aligned} & 16640 \\ & 16768 \end{aligned}$ |
|  |  |  | 14 | . 22778 | 16896 |
| 60 | 4.74633 | 55761 | 16 | . 23106 | 17024 |
| 65 | . 75085 | 56344 | 18 | . 23431 | 17152 |
| 70 | . 75532 | 56927 | 20 | 4.23754 | 17280 |
| 75 | . 75975 | 57511 | 22 | . 24075 | 17408 |
| 80 | .76413 | 58094 | 24 | . 24393 | 17536 |
|  |  |  | 26 | . 24709 | 17664 |
|  |  |  | 28 | . 25022 | 17792 |
| 85 | 4.76847 | 58677 |  |  |  |
| 90 | . 77276 | 59260 | 30 | 4.25334 | 17920 |
| 95 |  |  | 32 | . 25643 | 18048 |
| 100 | .78123 | 60427 | 34 | . 25950 | 18176 |
|  | . 7812 |  | 36 | . 26255 | 18304 |

Smithbonian Tables.

TABLE 33.
BAROMETRIC PRESSURES CORRESPONDING TO THE TEMPERATURE OF THE BOILING POINT OF WATER.

ENGLISH MEASURES.

| Temperature. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | $0 \% 5$ | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $185^{\circ}$ | 17.05 | 17.08 | 17.12 | 17.16 | 17.20 | 17.23 | 17.27 | 17.31 | 17.35 | 17.39 |
| 186 | 17.42 | 17.46 | 17.50 | 17.54 | 17.58 | 17.61 | 17.65 | 17.69 | 17.73 | 17.77 |
| 187 | 17.81 | 17.84 | 17.88 | 17.92 | 17.96 | 18.00 | 18.04 | 18.08 | 18.12 | 18.16 |
| 188 | 18.20 | 18.24 | 18.27 | 18.31 | 18.35 | 18.39 | 18.43 | 18.47 | 18.5I | 18.55 |
| 189 | 18.59 | 18.63 | 18.67 | 18.71 | 18.75 | 18.79 | 18.83 | 18.87 | 18.91 | 18.95 |
| 190 | 19.00 | 19.04 | 19.08 | 19.12 | 19.16 | 19.20 | 19.24 | 19.28 | 19.32 | 19.36 |
| 191 | 19.41 | 19.45 | 19.49 | 19.53 | 19.57 | 19.61 | 19.66 | 19.70 | 19.74 | 19.78 |
| 192 | 19.82 | 19.87 | 19.91 | 19.95 | 19.99 | 20.04 | 20.08 | 20.12 | 20.17 | 20.21 |
| 193 | 20.25 | 20.29 | 20.34 | 20.38 | 20.42 | 20.47 | 20.51 | 20.55 | 20.60 | 20.64 |
| 194 | 20.68 | 20.73 | 20.77 | 20.82 | 20.86 | 20.90 | 20.95 | 20.99 | 21.04 | 21.08 |
| 195 | 21.13 | 21.17 | 21.22 | 21.26 | 21.30 | 21.35 | 2 L .39 | 21.44 | 21.48 | 21.53 |
| 196 | 21.58 | 21.62 | 21.67 | 21.71 | 21.76 | 21.80 | 21.85 | 21.89 | 21.94 | 21.99 |
| 197 | 22.03 | 22.08 | 22.12 | 22.17 | 22.22 | 22.26 | 22.31 | 22.36 | 22.40 | 22.45 |
| 198 | 22.50 | 22.54 | 22.59 | 22.64 | 22.69 | 22.73 | 22.78 | 22.83 | 22.88 | 22.92 |
| 199 | 22.97 | 23.02 | 23.07 | 23.11 | 23.16 | 23.21 | 23.26 | 23.31 | 23.36 | 23.40 |
| 200 | 23.45 | 23.50 | 23.55 | 23.60 | 23.65 | 23.70 | 23.75 | 23.80 | 23.85 | 23.89 |
| 201 | 23.94 | 23.99 | 24.04 | 24.09 | 24. I4 | 24.19 | 24.24 | 24.29 | 24.34 | 24.39 |
| 202 | 24.44 | 24.49 | 24.54 | 24.59 | 24.64 | 24.69 | 24.74 | 24.80 | 24.85 | 24.90 |
| 203 | 24.95 | 25.00 | 25.05 | 25.10 | 25.15 | 25.21 | 25.26 | 25.31 | 25.36 | 25.41 |
| 204 | 25.46 | 25.52 | 25.57 | 25.62 | 25.67 | 25.73 | 25.78 | 25.83 | 25.88 | 25.94 |
| 205 | 25.99 | 26.04 | 26.10 | 26.15 | 26.20 | 26.25 | 26.31 | 26.36 | 26.42 | 26.47 |
| 206 | 26.52 | 26.58 | 26.63 | 26.68 | 26.74 | 26.79 | 26.85 | 26.90 | 26.96 | 27.01 |
| 207 | 27.07 | 27.12 | 27.18 | 27.23 | 27.29 | 27.34 | 27.40 | 27.45 | 27.51 | 27.56 |
| 208 | 27.62 | 27.67 | 27.73 | 27.79 | 27.84 | 27.90 | 27.95 | 28.01 | 28.07 | 28.12 |
| 209 | 28.18 | 28.24 | 28.29 | 28.35 | 28.41 | 28.46 | 28.52 | 28.58 | 28.64 | 28.69 |
| 210 | 28.75 | 28.81 | 28.87 | 28.92 | 28.98 | 29.04 | 29.10 | 29.16 | 29.21 | 29.27 |
| 211 | 29.33 | 29.39 | 29.45 | 29.51 | 29.57 | 29.62 | 29.68 | 29.74 | 29.80 | 29.86 |
| 212 | 29.92 | 29.98 | 30.04 | 30.10 | 30.16 | 30.22 | 30.28 | 30.34 | 30.40 | 30.46 |

METRIC MEASURES.
TAble 34.

| Temperature. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0\%5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | m | n. | mm | mm. | mm . |  |  |  | m | . |
| $80^{\circ}$ | 354.6 | 356. 1 | 357.5 | 359.0 | 360.4 | 361.9 | 363.3 | 364.8 | 366.3 | 367.8 |
| 81 | 369.3 | 370.8 | 372.3 | 373.8 | 375.3 | 376.8 | 378.3 | 379.8 | 38 I .3 | 382.9 |
| 82 | 384.4 | 385.9 | 387.5 | 389.0 | 390.6 | 392.2 | 393.7 | 395.3 | 396.9 | 398.5 |
| 83 | 400. I | 401.7 | 403.3 | 404.9 | 406.5 | 408.1 | 409.7 | 411.3 | 413.0 | 414.6 |
| 84 | 416.3 | 417.9 | 419.6 | 421.2 | 422.9 | 424.6 | 426.2 | 427.9 | 429.6 | 43 I .3 |
| 85 | 433.0 | 434.7 | 436.4 | 438.1 | 439.9 | 441.6 | $443 \cdot 3$ | 445. I | 446.8 | 448.6 |
| 86 | 450.3 | 452.1 | 453.8 | 455.6 | 457.4 | 459.2 | 46 I .0 | 462.8 | 464.6 | 466.4 |
| 87 | 468.2 | 470.0 | 471.8 | 473.7 | 475.5 | 477.3 | 479.2 | 481.0 | 482.9 | 484.8 |
| 88 | 486.6 | 488.5 | 490.4 | 492.3 | 494.2 | 496. I | 498.0 | 499.9 | 501.8 | 503.8 |
| 89 | 505.7 | 507.6 | 509.6 | 511.5 | 513.5 | 515.5 | 517.4 | 519.4 | 521.4 | 523.4 |
| 90 | 525.4 | 527.4 | 529.4 | 531.4 | 533.4 | 535.5 | 537.5 | 539.6 | 541.6 | 543.7 |
| 91 | 545.7 | 547.8 | 549.9 | 551.9 | 554.0 | 556. I | 558.2 | 560.3 | 562.4 | 564.6 |
| 92 | 566.7 | 568.8 | 5710 | 573.1 | 575.3 | 577.4 | 579.6 | 581.8 | 584.0 | 586.1 |
| 93 | 588.3 | 590.5 | 592.7 | 595.0 | 597.2 | 599.4 | 601.6 | 603.9 | 606. I | 608.4 |
| 94 | 610.7 | 612.9 | 615.2 | 617.5 | 619.8 | 622.I | 624.4 | 626.7 | 629.0 | 631.4 |
| 95 | 633.7 | 636.0 | 638.4 | 640.7 | 643.1 | 645.5 | 647.9 | 650.2 | 652.6 | 655.0 |
| 96 | 657.4 | 659.9 | 662.3 | 664.7 | 667.1 | 669.6 | 672.0 | 674.5 | 677.0 | 679.4 |
| 97 | 681.9 | 684.4 | 686.9 | 689.4 | 691.9 | 694.5 | 697.0 | 699.5 | 702.1 | 704.6 |
| 98 | 707.2 | 709.7 | 712.3 | 714.9 | 717.5 | 720.1 | 722.7 | 725.3 | 727.9 | 730.5 |
| 99 | 733.2 | 735.8 | 738.5 | 741.2 | 743.8 | 746.5 | 749.2 | 751.9 | 754.6 | 757.3 |
| 100 | 760.0 | 762.7 | 765.5 | 768.2 | 770.9 | 773.7 | 776.5 | 779.2 | 782.0 | 784.8 |

Smithsonian Tables.

## HYGROMETRICAL TABLES.

Pressure of aqueous vapor (Broch) -
English measures ..... 35
Metric measures ..... $\left\{\begin{array}{l}36 \\ 43\end{array}\right.$Pressure of aqueous vapor at low temperatures (C. F. Marvin) -English and Metric measuresTable 37
Weight of aqueous vapor in a cubic foot of saturated air -
English measures ..... Table 38
Weight of aqueous vapor in a cubic metre of saturated air -Metric measuresTable 39
Reduction of psychrometric observations - English measures.
Pressure of aqueous vapor ..... Table 40Values of $0.000367 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{157 \mathrm{I}}\right)$41
Relative humidity - Temperature Fahrenheit ..... Table 42
Reduction of psychrometric observations - Metric measures.Pressure of aqueous vapor .Table 43
Values of $0.000660 B\left(t-t_{1}\right)\left(\mathrm{I}+\frac{t-t_{1}}{873}\right)$ ..... 44
Relative humidity - Temperature Centigrade ..... Table 45
Reduction of snowfall measurements.
Depth of water corresponding to the weight of snow(or rain) collected in an 8 -inch gageTable 46
Rate of decrease of vapor pressure with altitude ..... Table 47

ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | Diff. for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} F . \\ -20.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ 0.0167 \end{gathered}$ |  | $\begin{gathered} F . \\ -10.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ 0.0277 \end{gathered}$ |  | $\begin{gathered} \text { F. } \\ 0.0 \end{gathered}$ | Inch. |  | $\begin{gathered} F . \\ 10.0 \end{gathered}$ | Inch. 0.0710 |  |
|  |  | I |  |  | I | +0.2 | . 0454 | 2 | 10.2 | . 0716 | 3 |
| -19.8 | 0.0168 | I | -9.8 | 0.0280 | I | 0.4 | . 0458 | 2 | 10.4 | . 0723 | 3 |
| 19.6 | . 0170 | I | 9.6 | . 0283 | I | 0.6 | . 0462 | 2 | 10.6 | . 0729 | 3 |
| 19.4 | . 0172 | 1 | 9.4 | . 0286 | I | 0.8 | . 0467 | 2 | 10.8 | . 0736 | 3 |
| 19.2 | . 0174 | 1 | 9.2 | . 0289 | I |  |  | 2 |  |  | 3 |
| 19.0 | . 0176 |  | 9.0 | . 0292 |  | 1.0 | 0.0471 | 2 | 11.0 | 0.0742 | 3 |
| -18.8 | 0.0177 | I | -8.8 | 0.0294 | I | I. 2 | . 0475 | 2 | 11.2 | . 0749 | 3 |
| 18.6 | . 0179 | I | 8.6 | . 0297 | I | I. 4 I .6 | . 0488 | 2 | 11.4 II. 6 | . 0756 | 3 |
| 18.4 | .OI8I | I | 8.4 | . 0300 | 2 | I. 8 | . 0489 | 2 | 11.8 | . 0769 | 3 |
| 18.2 | . Or 83 | I | 8.2 | . 0303 | 2 |  |  | 2 |  |  | 3 |
| 18.0 | . 0185 | 1 | 8.0 | . 0306 | 2 | 2.0 | 0.0493 | 2 | 12.0 | 0.0776 | 3 |
| -17.8 | 0.0187 | I | - 7.8 | 0.0309 | 2 | 2.2 | . 0498 | 2 | 12.2 | . 0783 | 3 3 |
| 17.6 | . 0.0189 | I | 7.6 | .0312 | 2 | 2.4 2.6 | .0503 | 2 | 12.4 | . 0790 | 3 |
| 17.4 | . 0191 | 1 | 7.4 | .0315 | 2 | 2.8 | .0512 | 2 | 12.8 | . 0804 | 4 |
| 17.2 | . 0193 | 1 | 7.2 | .0318 | 2 |  |  | 2 |  |  | 4 |
| 17.0 | . 0195 |  | 7.0 | . 0322 |  | 3.0 | 0.0517 | 2 | 13.0 | 0.0811 | 4 |
| -16.8 | 0.0 | I | -6.8 |  | 2 | 3.2 | . 0522 | 2 | 13.2 | .0818 | 4 |
| 16.6 | . 0199 | I | 6.6 | . 0328 | 2 | $3 \cdot 4$ | . 0526 | 2 | 13 | 5 | 4 |
| 16.4 | . 0201 | I | 6.4 | .033I | 2 | 3.6 3.8 | .0531 | 2 | 13.6 13.8 | . 0840 | 4 |
| 16.2 | . 0203 | I | 6.2 | . 0334 | 2 |  |  | 2 |  |  | 4 |
| 16.0 | . 0205 | 1 | 6.0 | . 0338 | 2 | 4.0 | 0.0541 |  | 14.0 | 0.0847 |  |
|  |  | I |  |  | 2 | 4.2 | . 0546 |  | 14.2 | . 0854 | 4 |
| -15.8 | 0.0207 | I | -5.8 | 0.0341 | 2 | 4.4 | .055I | 3 | 14.4 | . 0862 | 4 |
| 15.6 | -0209 | I | 5.6 | . 0344 | 2 | 4.6 | . 0556 | 3 | 14.6 | . 0869 | 4 |
| 15.4 | . 0211 | I | 5.4 | . 0347 | 2 | 4.8 | .056I | 3 | 14.8 | . 0877 | 4 |
| 15.2 | . 0213 | 1 | 5.2 | .0351 | 2 |  |  | 3 |  |  | 4 |
| 15.0 | . 0216 |  | 5.0 | . 0354 |  | 5.0 | 0.0567 |  | 15.0 | 0.0885 |  |
| -14.8 | 0.0218 | I | -4.8 | 0.03 | 2 | 5.2 | . 0572 | 3 | 15.2 | . 0892 | 4 |
| 14.6 | 0.0218 .0220 | I | -4.8 4.6 | 0.0358 .0361 | 2 | 5.4 5.6 | . 05777 | 3 | 15.4 | . 0900 | 4 |
| 14.4 | . 0222 | I | 4.4 | .0365 | 2 | 5.8 | . 0588 | 3 | 15.8 | .0916 | 4 |
| 14.2 | . 0225 | I | 4.2 | . 0368 | 2 |  |  | 3 |  |  | 4 |
| 14.0 | . 0227 |  | 4.0 | . 0372 |  | 6.0 | 0.0593 |  | 16.0 | 0.0924 |  |
|  |  | I |  |  | 2 | 6.2 | . 0598 |  | 16.2 | . 0932 | 4 |
| $-13.8$ | 0.0229 | I | -3.8 | 0.0375 | 2 | 6.4 | . 0604 | 3 | 16.4 | . 0940 | 4 |
| 13.6 | . 0232 | I | 3.6 | . 0379 | 2 | 6.6 | . 0609 | 3 | 16.6 | . 0948 | 4 |
| 13.4 | . 0234 | I | $3 \cdot 4$ | . 0383 | 2 | 6.8 | .06I5 | 3 | 16.8 | . 0956 | 4 |
| 13.2 | . 0236 | I | 3.2 | . 0386 | 2 |  |  | 3 |  |  | 4 |
| 13.0 | . 0239 |  | 3.0 | . 0390 |  | 7.0 | 0.0620 |  | 17.0 | 0.0965 |  |
| -12.8 | 0.024 I | I | -2.8 | 0.0394 | 2 | 7.2 | . 0626 | 3 | 17.2 | . 0973 | 4 |
| 12.6 | . 0244 | I | 2.6 | . 0397 | 2 | 7.4 | . 0632 | 3 | 17.4 | .0981 | 4 |
| 12.4 | . 0246 | I | 2.4 | . 0401 | 2 | 7.6 | . 0637 | 3 | 17.6 17.8 | . 0990 | 4 |
| 12.2 | . 0249 | I | 2.2 | . 0405 | 2 | 7.8 | . 0643 | 3 | 17.8 | . 0999 | 4 |
| 12.0 | .025I |  | 2.0 | . 0409 | 2 | 8.0 | 0.0649 |  | 18.0 | 0. 1007 |  |
| -11.8 | 0.0254 | 1 | $-1.8$ | 0.0413 | 2 | 8.2 | . 0655 | 3 3 | 18.2 | . 1016 | 4 |
| 11.6 | . 0256 |  | 1.6 | . 0417 | 2 | 8.4 | .0661 | 3 3 | 18.4 | . 1024 | 4 |
| II. 4 | . 0259 | I | I. 4 | . 0421 |  | 8.6 | . 0667 | 3 | I8.6 | .1033 | 4 |
| II. 2 | .026I |  | 1.2 | . 0425 | 2 | 8.8 | . 0673 | 3 | 18.8 | . 1042 | 4 |
| 11.0 | . 0264 |  | 1.0 | . 0429 | 2 | 9.0 | 0.0679 | 3 | 19.0 | 0.105I | 4 |
| -10.8 | 0.0267 |  | $-0.8$ | 0.0433 |  | 9.2 | . 0685 | 3 | 19.2 | . 1060 | 5 |
| 10.6 | . 0269 |  | 0.6 | . 0437 | 2 | 9.4 | .0691 | 3 | 19.4 | . 1069 | 5 |
| 10.4 | . 0272 |  | 0.4 | . 0441 | 2 | 9.6 | . 0697 | 3 | 19.6 | . 1078 | 5 |
| 10.2 | . 0275 | 1 | 0.2 | . 0445 | 2 | 9.8 | . 0704 | 3 3 | 19.8 | . 1087 | 5 |

## TABLE 35.

PRESSURE OF AQUEOUS VAPOR.
(Broch.)
ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | D.ff. tor 0.1 | Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. |  | F. | Inch |  | F. | Inch |  | F. | Inch. |  |
| 20.0 | 0. 1097 |  | 30.0 | 0. 1660 |  | 40.0 | 0. 2465 |  | 50.0 | 0.3598 |  |
| 20.2 | . 1106 | 5 | 30.2 | . 1673 | 7 | 40.2 | . 2484 | 10 | 50.2 | . 3625 | I3 |
| 20.4 | . 1115 | 5 | 30.4 | . 1687 | 7 | 40.4 | . 2503 | 10 | 50.4 | . 3652 | I4 |
| 20.6 | . 1125 | 5 | 30.6 | . 1700 | 7 | 40.6 | .2523 | 10 | 50.6 | . 3679 | 14 |
| 20.8 | . II 34 | 5 | 30.8 | .1714 | 7 | 40.8 | . 2542 | 10 | 50.8 | . 3706 | 14 |
| 21.0 | O. 1144 | 5 | 31.0 | 0. 1728 | 7 | 41.0 | 0.2562 | 10 | 51.0 | 0.3734 | I |
| 21.2 | . 1154 | 5 | 31.2 | . 1742 | 7 | 41.2 | . 2582 | 10 | 51.2 | . 3761 | 14 |
| 21.4 | .1163 | 5 | 3 I .4 | . 1756 | 7 | 4 II .4 | . 2601 | 10 | 5 I .4 | . 3789 | 14 |
| 21.6 | . 1173 | 5 | 31.6 | .1770 | 7 | 41.6 | . 2621 | 10 | 51.6 | .3817 | 14 |
| 21.8 | . 1183 | 5 | 31.8 | . 1784 | 7 | 41.8 | . 2642 | 10 | 51.8 | - 3845 | 14 |
| 22.0 | O. 1193 | 5 | 32.0 | 0. 1799 | 7 | 42.0 | 0. 2662 | 10 | 52.0 | 0.3874 | 14 |
| 22.2 | . 1203 | 5 | 32.2 | . 18 I 3 | 7 | 42.2 | . 2683 | 10 | 52.2 | . 3902 | 14 |
| 22.4 | . 1213 | 5 | 32.4 | . 1828 | 7 | 42.4 | . 2703 | IO | 52.4 | . 3931 | 14 |
| 22.6 | . 1223 | 5 | 32.6 | . 1842 | 7 | 42.6 | . 2724 | 10 | 52.6 | . 3960 | 14 |
| 22.8 | . 1234 | 5 | 32.8 | . 1857 | 7 | 42.8 | . 2745 | 11 | 52.8 | . 3989 | 15 |
| 23.0 | O. 1244 | 5 | 33.0 | 0. 1872 | 7 | 43.0 | 0.2766 |  | 53.0 | 0.4018 | 15 |
| 23.2 | . 1255 | 5 | 33.2 | . 1887 | 8 | 43.2 | . 2787 | II | 53.2 | . 4048 | I5 |
| 23.4 | . 1265 | 5 | 33.4 | . 1902 | 8 | 43.4 | . 2808 | II | 53.4 | . 4077 | 15 |
| 23.6 | . 1276 | 5 | 33.6 | .1917 | 8 | 43.6 | . 2830 | 11 | 53.6 | .4107 | 15 |
| 23.8 | . 1287 | 5 | 33.8 | . 1933 | 8 | 43.8 | . 2851 | II | 53.8 | .4137 | 15 |
| 24.0 | O. 1297 | 5 | 34.0 | 0. 1948 | 8 | 44.0 | 0.2873 |  | 54.0 | 0.4168 | 15 |
| 24.2 | . 1308 | 5 | 34.2 | . 1964 | 8 | 44.2 | . 2895 | II | 54.2 | .4198 | 15 |
| 24.4 | . 1319 | 5 | 34.4 | . 1979 | 8 | 44.4 | . 2917 | II | 54.4 | . 4229 | 15 |
| 24.6 | . 1330 | 6 | 34.6 | . 1995 | 8 | 44.6 | . 2939 | II | 54.6 | . 4259 | 16 |
| 24.8 | . 1341 | 6 | 34.8 | . 2011 | 8 | 44.8 | . 2962 | II | 54.8 | . 4290 | 16 |
| 25.0 | O. 1352 | 6 | 35.0 | 0.2027 | 8 | 45.0 | 0.2984 | II | 55.0 | 0.4322 | 16 |
| 25.2 | . 1364 | 6 | 35.2 | . 2043 | 8 | 45.2 | .3007 | II | 55.2 | . 4353 | 16 |
| 25.4 | . 1375 | 6 | 35.4 | . 2059 | 8 | 45.4 | . 3030 | 12 | 55.4 | . 4385 | 16 |
| 25.6 | . 1386 | 6 | 35.6 | . 2076 | 8 | 45.6 | . 3053 | 12 | 55.6 | .4417 | 16 |
| 25.8 | . 1398 | 6 | 35.8 | . 2092 | 8 | 45.8 | -3076 | 12 | 55.8 | . 4449 | 16 |
| 26.0 | 0.1409 | 6 | 36.0 | 0.2109 | 8 | 46.0 | 0.3099 |  | 56.0 | 0.448 I | 16 |
| 26.2 | . 1421 | 6 | 36.2 | . 2125 | 8 | 46.2 | .3123 | 12 | 56.2 | .4513 | 16 |
| 26.4 | . 1433 | 6 | 36.4 | . 2142 | 8 | 46.4 | - 3146 | 12 | 56.4 | . 4546 | 16 |
| 26.6 | . 1445 | 6 | 36.6 | . 2159 | 8 | 46.6 | .3170 | 12 | 56.6 | . 4579 | 17 |
| 26.8 | . 1457 | 6 | 36.8 | . 2176 | 9 | 46.8 | . 3194 | 12 | 56.8 | .4612 | 17 |
| 27.0 | o. 1469 | 6 | 37.0 | 0.2193 | 9 | 47.0 | 0.3218 | 12 | 57.0 | 0.4645 | 17 |
| 27.2 | .1481 | 6 | 37.2 | . 2210 | 9 | 47.2 | . 3242 | 12 | 57.2 | 0.4645 .4679 | 17 |
| 27.4 | . 1493 | 6 | 37.4 | . 2228 | 9 | 47.4 | . 3267 | 12 | 57.4 | . 4712 | 17 |
| 27.6 | . 1505 | 6 | 37.6 | . 2245 | 9 | 47.6 | . 3291 | 12 | 57.6 | . 4746 | 17 |
| 27.8 | . 1518 | 6 | 37.8 | . 2263 | 9 | 47.8 | . 3316 | 2 | 57.8 | .4780 | 17 |
| 28.0 |  | 6 | 38.0 |  | 9 | 48.0 |  | 12 | 53.0 |  | 17 |
| 28.2 | 0.1530 .1543 | 6 | 38.2 | 0.2281 .2298 | 9 | 48.2 | 0.3341 .3366 | 13 | 58.2 | 0.4815 .4849 | 17 |
| 28.4 | . 1555 | 6 | 38.4 | . 2316 | 9 | 48.4 | . 3391 | 13 | 58.4 | . 4888 | 17 |
| 28.6 | . 1568 | 6 | 38.6 | . 2334 | 9 | 48.6 | . 3416 | 13 | 58.6 | . 4919 | I8 |
| 28.8 | .158I | 6 | 38.8 | . 2353 | 9 | 48.8 | . 3442 | 13 | 58.8 | . 4954 | 18 |
| 29.0 | O. 1594 | 6 | 39.0 | 0.2371 | 9 | 49.0 | 0.3467 | 13 | 59.0 |  | 18 |
| 29.2 | . 1607 | 7 | 39.2 | . 2390 | 9 | 49.2 | .3493 | 13 | 59.2 | 0.4990 .5025 | 18 |
| 29.4 | . 1620 | 7 | 39.4 | . 2408 | 9 | 49.4 | -3519 | 13 | 59.4 | . 5061 | 18 |
| 29.6 | . 1633 | 7 | 39.6 | . 2427 | 9 | 49.6 | . 3546 | 13 | 59.6 | . 5097 | 18 |
| 29.8 | . 1646 | 7 7 | 39.8 | . 2446 | 9 10 | 49.8 | - 3572 | I3 | 59.8 | .5134 | 18 |

(Broch.)
ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. |  | F. | Inch. |  | F. | Inches. |  | F. | Incnes. |  |
| 60.0 | 0.5170 | 18 | 70.0 | 0.7320 |  | 80.0 | 1.0219 | 34 | 90.0 | 1.4081 |  |
| 60.2 | . 5207 | 19 | 70.2 | . 7370 | 25 | 80.2 | . 0286 | 34 34 | 90.2 | . 4170 | 44 |
| 60.4 | . 5244 | 19 | 70.4 | . 7420 | 25 | 80.4 | . 0354 | 34 | 90.4 | . 4259 | 45 |
| 60.6 | . 5282 | 19 | 70.6 | .7471 | 26 | 80.6 | . 0422 | 34 | 90.6 | . 4349 | 45 |
| 60.8 | . 5319 | 19 | 70.8 | . 7522 | 26 | 80.8 | . 0490 | 34 | 90.8 | . 4439 | 45 |
| 61.0 | 0.5357 |  | 71.0 | 0.7573 | 26 | 81.0 | 1.0558 | 4 | 91.0 | 1. 4530 | 45 |
| 61.2 | . 5395 | 19 19 | 71.2 | . 7625 | 26 | 81.2 | . 0627 | 35 | 91.2 | . 4621 | 46 |
| 6I. 4 | . 5433 | 19 19 | 71.4 | . 7676 | 26 | 8 I .4 | . 0697 | 35 | 91.4 | . 4712 | 46 |
| 61.6 | . 5471 | 19 | 71.6 | . 7728 | 26 | 8 8 .6 | . 0767 | 35 | 91.6 | . 4805 | 46 |
| 61. 8 | . 5510 | 19 | 71.8 | .778x | 26 | 81. 8 | . 0837 | 35 | 91.8 | . 4897 | 46 |
| 62.0 | O. 55 | 19 | 72.0 | 0.7 | 26 | 82.0 | 1.09 | 35 | 92.0 |  | 47 |
| 62.2 | . 5588 | 20 | 72.2 | .7884 .7887 | 27 | 82.2 | . 0978 | 36 | 92.2 | 1.4990 .5084 | 47 |
| 62.4 | . 5628 | 20 | 72.4 | . 7940 | 27 | 82.4 | . 1050 | 36 | 92.2 92.4 | . 5178 | 47 |
| 62.6 | . 5667 | 20 | 72.6 | . 7994 | 27 | 82.6 | .II2I | 36 | 92.6 | . 5273 | 47 48 |
| 62.8 | . 5707 | 20 | 72.8 | . 8048 | 27 | 82.8 | . 1194 | 36 | 92.8 | . 5368 | 48 |
| 63.0 | 0.5748 | 20 | 73.0 | 0.8102 | 27 | 83.0 | I. 1266 | 7 | 93.0 | 1. 5464 | 8 |
| 63.2 | . 5788 | 20 | 73.2 | .8157 | 27 | 83.2 | . 1339 | 37 | 93.2 | . 5560 | 48 |
| 63.4 | . 5829 | 2 I | 73.4 | . 8212 | 28 | 83.4 | . 1413 | 37 37 | 93.4 | . 5657 | 49 |
| 63.6 | . 5870 | 21 | 73.6 | . 8267 | 28 | 83.6 | . 1487 | 37 37 | 93.6 | . 5755 | 49 |
| 63.8 | .5911 | 21 | 73.8 | . 8323 |  | 83.8 | . 1561 | 37 | 93.8 | . 5853 | 49 |
| 64.0 | 0.5952 | 2 I | 74.0 | 0. 837 | 28 | 84.0 | I. 1635 | 38 | 94.0 | I.5951 | 9 |
| 64.2 | . 5994 | 2 I | 74.2 | . 8435 | 28 | 84.2 | . 1710 | 38 | 94.2 | . 6050 | 49 |
| 64.4 | . 6036 | 21 | 74.4 | . 8492 | 28 | 84.4 | . 1786 | 38 | 94.4 | .6149 | 50 |
| 64.6 | . 6078 | 21 | 74.6 | .8549 | 29 29 | 84.6 | . 1862 | 38 | 94.6 | . 6249 | 50 |
| 64.8 | .6120 | 21 | 74.8 | . 8606 | 29 | 84.8 | . 1938 | 38 | 94.8 | . 6350 | 5 |
| 65.0 | 0.6163 | 21 | 75.0 | o. 8664 | 29 | 85.0 | 1. 2015 | 8 | 95.0 | 1.6451 | 5 I |
| 65.2 | . 6206 | 22 | 75.2 | . 8722 | 29 | 85.2 | . 2093 | 39 | 95.2 | . 6552 | 5 I |
| 65.4 | . 6249 | 22 | 75.4 | . 8780 | 29 | 85.4 | . 2170 | 39 39 | 95.4 | . 6655 | 51 |
| 65.6 | . 6293 | 22 | 75.6 | . 8839 | 29 30 | 85.6 | . 2248 | 39 39 | 95.6 | . 6758 | 5 |
| 65.8 | . 6337 | 22 | 75.8 | . 8898 | 30 | 85.8 | . 2327 | 39 | 95.8 | .686I | 52 |
| 66.0 | 0.6381 | 22 | 76.0 | 0. 8957 | 30 | 86.0 | I. 2406 | 39 | 96.0 | 1. 6964 | 52 |
| 66.2 | . 6425 | 22 | 76.2 | . 9017 | 30 | 86.2 | . 2485 | 40 | 96.2 | . 7069 | 52 |
| 66.4 | . 6470 | 22 | 76.4 | . 9077 | 30 | 86.4 | . 2565 | 40 | 96.4 | . 7174 | 52 |
| 66.6 | . 6514 | 22 | 76.6 | .9137 | 30 | 86.6 | . 2645 | 40 | 96.6 | .7279 | 53 |
| 66.8 | . 6560 | 23 | 76.8 | . 9198 | 30 | 86.8 | . 2726 | 40 | 96.8 | . 7385 | 53 |
| 67.0 | 0.6605 | 23 | 77.0 | 0.92 | 3 I | 87.0 | 1.2807 | 4I | 97.0 | 1.7492 | 53 |
| 67.2 | . 6651 | 23 | 77.2 | 0.9259 .9321 | 3 I | 87.2 | . 2889 | 4 I | 97.2 | 1.7492 .7599 | 54 |
| 67.4 | . 6697 | 23 | 77.4 | . 9383 | 3 I | 87.4 | . 2971 | 4 r | 97.4 | . 7707 | 54 |
| 67.6 | . 6743 | 23 | 77.6 | . 9445 | 31 31 | 87.6 | . 3054 | 41 | 97.6 | .7815 | 54 |
| 67.8 | .6789 | 23 | 77.8 | . 9507 | 31 | 87.8 | -3137 | 42 | 97.8 | . 7924 | 54 |
| 68.0 | 0.6836 | 23 | 78.0 | 0.9570 | 31 | 88.0 | 1.3220 | 42 | 98.0 | I. 8034 | 55 |
| 68.2 | . 6883 | 24 | 78.2 | . 9633 | 32 | 88.2 | . 3304 | 42 | 98.2 | . 8144 | 55 |
| 68.4 | . 6930 | 24 | 78.4 | . 9697 | 32 32 | 88.4 | . 3388 | 42 | 98.4 | . 8254 | 56 |
| 68.6 | . 6978 | 24 | 78.6 | . 9761 | 32 32 | 88.6 | . 3473 | 42 | 98.6 | . 8366 | 56 |
| 68.8 | . 7026 | 24 | 78.8 | . 9825 | 32 | 88.8 | . 3558 | 3 | 98.8 | . 8477 | 56 |
| 69.0 | 0.7074 | 24 | 79.0 | 0.9890 | 32 33 | 89.0 | I. 3644 | 43 | 99.0 | 1.8590 | 56 57 |
| 69.2 | . 7123 | 24 | 79.2 | . 9955 | 33 33 | 89.2 | .3731 | 43 | 99.2 | .8703 | 57 |
| 69.4 69.6 | .7172 .7221 | 24 25 | 79.4 | 1.0021 | 33 33 | 89.4 89.6 | . 3818 | 44 | 99.4 99.6 | .8817 | 57 |
| 69.6 69.8 | .7221 .7270 | 25 | 79.6 79.8 | .0087 | 33 33 | 89.6 89.8 | .3905 | 44 | 99.6 99.8 | . 8931 | 57 |
| 69.8 | . 7270 | 25 | 79.8 | . 0153 | 33 | 89.8 | -3993 | 44 | 99.8 | . 9046 | 58 |

TABLE 35.
(Broch.)
ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | Diff. for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | In |  | F. | Inches. |  |  | Inche |  | F. | Inches. |  |
| 100:0 | 1.9161 | 58 | 110.0 | 2.5765 |  | 120.0 | 3.4253 | 6 | 130.0 | 4.5044 |  |
| 100.2 | . 9277 | 58 | 110.2 | . 5915 | 75 | 120.2 | . 4445 | 96 | I30.2 | . 5286 | 121 |
| 100.4 | . 9394 | 58 | 110.4 | . 6066 | 75 | 120.4 | . 4637 | 96 | I30.4 | . 5530 | 122 |
| 100.6 | . 9511 | 59 | 110.6 | . 6217 | 76 | 120.6 | . 4831 | 97 | 130.6 | . 5775 | 123 |
| 100.8 | . 9629 | 59 | 110.8 | .6369 | 76 | 120.8 | . 5026 | 97 | 130.8 | . 6020 | 123 |
| 101.0 | 1.9747 | 59 | 11.0 | 2.6522 | 77 | 121.0 | .522I | 98 | 131.0 | 4.6267 | 123 |
| 101.2 | . 9867 | 60 | III. 2 | . 6676 | 77 | 121.2 | . 5417 | 8 | 131.2 | . 6515 | 124 |
| 101.4 | . 9986 | 60 | III. 4 | . 6831 | 78 | 12I. 4 | -56I5 | 99 | I31.4 | . 6764 | 125 |
| ros. 6 | 2.0107 | 60 | III. 6 | . 6986 | 78 | I21. 6 | . 5813 | 99 | 131.6 | . 7015 | 125 |
| 101.8 | . 0228 | 6 | III. 8 | . 7142 | 78 | 121.8 | . 6012 |  | 131.8 | . 7266 | 126 |
| 102.0 | 2.0349 | 61 | 112.0 | 2.7299 | 78 | 122.0 | 3.6213 | 100 | 132.0 |  | 126 |
| 102.2 | . 0471 | 61 | 112.2 | . 7457 | 79 | 122.2 | .6414 | IOI | I32.2 | 7773 | 127 |
| 102.4 | . 0594 | 62 | II2.4 | . 7616 | 80 | 122.4 | .6616 | 102 | I 32.4 | . 8028 | 7 |
| 102.6 | .0718 | 62 | II2.6 | . 7775 | 80 | 122.6 | .6819 | 102 | I 32.6 | . 8284 | 128 |
| 102.8 | . 0842 |  | 112.8 | . 7935 | 80 | 122.8 | . 7023 | 102 | I 32.8 | . 8541 | 9 |
| 103.0 | 2.0967 |  | 113.0 | 2.8096 | 8I | 123.0 | 3.7228 | 10 | 133.0 | 4.8800 | 129 |
| 103.2 | .1092 | 63 | II3.2 | . 8257 | 8 I | 123.2 | 3.7228 .743 | 3 | I33.2 | . 9059 | 130 |
| 103.4 | . 1218 | 63 | II 3.4 | . 8420 | 82 | 123.4 | .764I | 1 | I 33.4 | . 9320 | O |
| 103.6 | . 1345 | 64 | II 3.6 | . 8583 | 82 | 123.6 | . 7849 | 1 | I33.6 | . 9582 | ${ }^{1} 31$ |
| 103.8 | . 1473 | 6 | II3.8 | . 8747 |  | 123.8 | . 8058 |  | I 33.8 | . 9845 | 2 |
| 104.0 | 2.1601 |  | 114.0 | 2.8912 |  | 124.0 | 3.82 | 5 | 134.0 | 5.0110 | I32 |
| 104.2 | . 1730 | 64 | II4.2 | . 9078 | 83 | 124.2 | . 8.8478 | 105 | I 34.2 | . 0375 | 133 |
| 104.4 | . 1859 | 65 | II4.4 | . 9244 | 8 | 124.4 | . 8690 | 106 | I 34.4 | . 0642 | I33 |
| 104.6 | . 1989 | 65 | 114.6 | . 9412 | 84 | 124.6 | . 8903 | 106 | I 34.6 | . 0910 | I 34 |
| 104.8 | . 2120 | 66 | II4.8 | . 9580 | 84 | 124.8 | .9117 | 107 | I 34.8 | .1179 | 135 |
|  |  | 66 | 115 |  | 85 | 125. |  | 107 | 135.0 |  | 135 |
|  | 2.2 | 66 | 115.0 | 2.9749 | 85 | 125.0 | 3.9332 | 108 | 135.0 | 5.1450 | 136 |
| 105.2 105.4 | . 2381 | 66 | II5.2 II 5.4 | .9919 3.0089 | 85 | 125.2 125.4 | . 9548 | 109 | I 35.2 r 35.4 | .1722 .1994 | I36 |
| 105.4 105.6 | . 2516 | 67 | II5.4 | 3.0089 .0261 | 86 | 125.4 | . 976 | 109 | 135.4 | . 1994 | 137 |
| 105.8 | . 2784 | 67 | 115.8 | . 0433 | 86 | 125.8 | 4.9898 | 110 | I 35.8 | . 2544 | I38 |
|  |  | 67 |  |  | 8 |  | 4.0202 | 110 | - 35.8 | . 2544 | I38 |
| 106.0 | 2.2919 | 68 | 116.0 | 3.0606 | 87 | 126.0 | 4.0422 | 1 II | 136.0 | 5.2820 |  |
| 106.2 | . 3054 | 68 | 116.2 | . 0780 | 87 | 126.2 | . 0643 | III | 136.2 | . 3098 | 139 139 |
| 106.4 | . 3190 | 68 | 116.4 | . 0955 | 88 | 126.4 | . 0865 | 112 | 136.4 | . 3377 | 139 140 |
| 106.6 | . 3327 | 69 | 116.6 | . 113I | 88 | 126.6 | . 1088 | 112 | 136.6 | . 3657 | 141 |
| 106.8 | - 3465 | 69 | II6.8 | . 1308 |  | 126.8 | . 1312 | 112 | 136.8 | - 3939 | 14 |
| 107.0 | 2.3603 |  | 117.0 | 3.1485 |  | 127.0 | 4.1537 |  | 137.0 | 5.422 I | 1 |
| 107.2 | . 3742 | 70 | 117.2 | . 1663 | 90 | 127.2 | . 1764 | II3 | I37.2 | . 4505 | 42 |
| 107.4 | . 3882 | 70 | 117.4 | . 1842 | 90 | 127.4 | .1991 | 114 | I 37.4 | . 4791 | 143 |
| 107.6 | . 4023 | 71 | 117.6 | . 2023 | 91 | 127.6 | . 2219 | 115 | 137.6 | . 5077 | 143 |
| 107.8 | . 4164 | 71 | 117.8 | . 2204 | 91 | 127.8 | . 2448 |  | 137.8 | . 5365 | 144 |
| 108.0 | 2.4306 |  | 118.0 | 3.2386 | 9 | 128.0 | 4.26 | 115 | 138.0 | 5.5654 | 145 |
| 108.2 | . 4449 | 71 | 118.2 | . 2568 | 91 | 128.2 | . 2910 | 116 | 138.2 | - 5.5945 | 145 |
| 108.4 | . 4592 | 72 | II8.4 | . 2752 | 92 | 128.4 | . 3143 | 116 | I38.4 | . 6237 | 146 |
| 108.6 | . 4736 | 72 | 118.6 | . 2937 | 93 | 128.6 | . 3377 |  | I 38.6 | . 6530 | 147 |
| 108.8 | .4881 | 7 | 118.8 | . 3122 | 93 | 128.8 | . 3612 | 117 | I38.8 | . 6824 | 147 |
| 109.0 | 2.5026 | 73 | 119.0 |  | 93 | 129.0 | 4.3848 | 118 | 139.0 | 71 | 148 |
| 109.2 | 2. .5172 | 73 | 119.2 | 3.3308 .3495 | 94 | 129.2 | 4.38885 | 119 | 139.2 | .7417 | 149 |
| 109.4 | . 5319 | 73 | 119.4 | . 3683 | 94 | 129.4 | . 4323 | 119 | I 39.4 | .7715 | 149 |
| 109.6 | . 5467 | 74 | 119.6 | . 3872 | 95 | 129.6 | . 4562 | 120 | I 39.6 | . 8014 | 150 |
| 109.8 | . 5616 | 74 75 | 119.8 | . 4062 | 95 | 129.8 | . 4802 | 120 | I 39.8 | . 8315 | 150 151 |

Smithbonian Tables.

PRESSURE OF AQUEOUS VAPOR.
(Broch.)
ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. <br> for <br> 0.1 | Temperature. | Vapor Pressure. | $\begin{gathered} \text { Diff. } \\ \text { for } \\ \mathbf{0 . 1} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches |  | 15 | Inches. |  | F. | Inches. |  | F. | Inches. |  |
| 140\% | 5.8617 |  | 150.0 | 7.5521 | 188 | 160.0 | 9.6374 |  | 170.0 | 12.1870 |  |
| 140.2 | . 8921 | 152 152 | 150.2 | . 5897 | 189 | 160.2 | . 6836 | 231 | 170.2 | . 2432 | 281 282 |
| 140.4 | . 9226 | 153 | 150.4 | . 6275 | 190 | 160.4 | . 7300 | 233 | 170.4 | . 2997 | 283 |
| 140.6 | . 9532 | I54 | 150.6 | . 6654 | I9I | 160.6 | . 7765 | 234 | 170.6 | . 3564 | 285 |
| 140.8 | . 9839 | 154 | 150.8 | . 7035 | 191 | 160.8 | . 8233 | 234 | I70.8 | . 4133 |  |
| 141.0 | 6.0148 | I54 | 151.0 | 7.7418 |  | 161.0 | 9.8702 | 235 | 171.0 | 12.4704 | 286 |
| I41.2 | . 0458 | I55 I56 | 151.2 | .7802 .8188 | 192 | 16I. 2 | . 9173 | 236 | 171.2 | 2.47278 .5 | 287 |
| 141.4 | . 0770 | + | ${ }^{1} 51.4$ | .8188 | 1 | 161.4 | . 9647 | 237 238 | 171.4 | . 5853 | 288 |
| 141.6 141.8 | .1083 .1397 | I57 | I51. 6 I5I. 8 | .8575 .8964 | I95 | 161.6 161. 8 | 10.0122 .0599 | 239 239 | 171.6 171. 8 | .643I | 280 |
| 141.8 | . 1397 | 158 | 151.8 | . 8964 | 195 | 161.8 | . 0599 | 240 | I71.8 | .701I | 291 |
| 142.0 | 6.1713 |  | 152.0 | 7.9355 | 196 | 162.0 | 10.1078 |  | 172.0 | 12.7593 |  |
| 142.2 | . 2030 | 159 | ${ }^{1} 52.2$ | . 9747 | 19 | 162.2 | . 1559 | 241 | 172.2 | .8177 | 292 |
| 142.4 | . 2348 | 150 | I52.4 I52.6 | 8.0141 | 198 | 162.4 162.6 | . 2042 | 241 | 172.4 I 72.6 | . 8764 | 293 |
| 142.6 I42.8 | . 2668 | 161 | 152.6 I52.8 | . 0536 | 199 | 162.6 162.8 | . 2526 | 243 | 172.6 172.8 | . 9353 | 296 |
|  |  | 16 | 15 |  | 199 |  |  | 244 |  |  | 297 |
| 143.0 | 6.3312 | 162 | 153.0 | 8.1332 | 200 | 163.0 | 10.3501 |  | 173.0 | 13.0538 | 98 |
| 143.2 | . 3636 | 163 | ${ }^{1} 53.2$ | . 1733 | 201 | 163.2 | . 3992 | 246 | 173.2 | .1134 | 299 |
| 143.4 | .3961 | 164 | ${ }^{1} 53.4$ | . 2135 | 202 | 163.4 | . 4484 | 247 | 173.4 | . 1732 | 300 |
| 143.6 | . 4288 | 164 | I 53.6 I53.8 | . 2539 | 203 | 163.6 163.8 | . 4979 | 248 | 173.6 | . 2332 | 301 |
| 143.8 | .4616 | I65 | I53.8 | . 2944 | 203 | 163.8 | . 5475 | 248 | 173.8 | . 2935 | 301 303 |
| 144.0 | 6.4946 | I6 | 154.0 | 8.3351 |  | 164.0 | 10.5974 |  | 174.0 | 13.3540 |  |
| 144.2 | . 5277 | 166 | 154.2 | . 3760 | 205 | 164.2 | . 6474 | 25 I | 174.2 | . 4147 | 304 |
| 144.4 | . 5610 | 166 | I54.4 | . 4171 | 205 | 164.4 | . 6976 | 251 | 174.4 | . 4756 | 305 306 |
| 144.6 | . 5944 | 168 | ${ }^{1} 54.6$ | . 4583 | 207 | 164.6 | . 7488 | 253 | 174.6 | . 5368 | 307 |
| 144.8 | . 6279 | 168 | ${ }^{\text {I } 54.8}$ | . 4997 | 208 | I64.8 | . 7986 | 253 254 | 174.8 | . 5982 | 307 308 |
| 145.0 | 6.6616 | 169 | 155.0 | 8.5413 |  | 165.0 | 10.8495 |  | 175.0 | 13.6599 |  |
| 145.2 | . 6954 | 170 | 155.2 | . 5830 | 210 | 165.2 | .9005 | 256 | 175.2 | . 7218 | 309 311 |
| 145.4 | . 7294 | 171 | ${ }^{1} 55.4$ | . 6249 | 210 | 165.4 | .9517 | 257 | ${ }^{1} 75.4$ | .7839 | 311 312 |
| 145.6 | . 7635 | 171 | ${ }^{1} 55.6$ | . 6670 | 2 II | 165.6 | 11.0032 | 258 | 175.6 | . 8462 | 313 |
| 145.8 | . 7978 | 171 | I 55.8 | .7092 | 211 | 165.8 | . 0548 | 258 | I75.8 | . 9088 | 313 |
| 146.0 | 6.8322 |  | 156.0 | 8.7516 |  | 166.0 | II.1067 |  | 176.0 | 13.9716 |  |
| 146.2 | . 8668 | 1 | ${ }^{1} 56.2$ | . 7942 | 213 | 166.2 | . 1587 | 26I | 176.2 | 14.0347 | 315 317 |
| 146.4 | . 9015 | 174 174 | I56.4 | . 8370 | 215 | 166.4 | . 2109 | 261 262 | 176.4 | . 0980 | 317 318 |
| I46.6 | . 9363 | 174 175 | I 56.6 | . 8799 | 215 | 166.6 | . 2634 | 263 | 176.6 | .1616 | 318 |
| I46.8 | .9713 | 17 | I56.8 | .923I |  | 166.8 | . 3160 | 263 | 176.8 | . 2253 |  |
| 147.0 | 7.0065 | 176 | 157.0 | 8.9664 | 21 | 167.0 | 11.3689 | 264 | 177.0 | I4.28 | 320 |
| 147.2 | . 0418 | 17 | 157.2 | 9.0098 |  | 167.2 | . 4220 |  | 177.2 | . 3536 | 321 |
| 147.4 | . 0773 | 178 | 157.4 | . 0535 |  | 167.4 | . 4752 | 7 | 177.4 | .4181 | 323 |
| 147.6 | . 1129 | 179 | I57.6 | . 0973 | 220 | 167.6 | . 5287 | 268 | 177.6 | . 4828 | 324 |
| 147.8 | . 1486 | 179 | I57.8 | .1413 | 220 | 167.8 | . 5824 | 268 | 177.8 | . 5478 | 325 |
| 148.0 | 7.1845 |  | 158.0 | 9. 1855 |  | 168.0 | 11.6363 |  | 178.0 | 14.613I | 326 |
| 148.2 | . 2206 |  | I58.2 | 9.1859 | 222 | 168.2 | 11.6904 | 271 | 178.2 | 14.6785 .6785 | 327 |
| 148.4 | . 2568 | I81 | I58.4 | . 2745 | 223 | 168.4 | . 7447 | 272 | 178.4 | . 7443 | 329 |
| 148.6 | . 2932 | 182 | ${ }^{1} 58.6$ | . 3192 |  | 168.6 | . 7993 | 273 | 178.6 | .8102 | 330 |
| I48.8 | . 3297 | 183 | I58.8 | . 3641 |  | 168.8 | . 8540 | 27 | 178.8 | . 8764 | 331 |
| 149.0 | 7.3664 | 183 | 159.0 | 9.4092 | 226 | 169.0 | 11.9090 | 275 | 179.0 |  | 332 |
| 149.2 | . 4032 | 18 | I59.2 | . 4545 |  | 169.2 | 11.9641 |  | 179.2 | 15.0096 | 334 |
| 149.4 | . 4402 | 186 | 159.4 | . 4999 | 228 | 169.4 | 12.0195 | 278 | 179.4 | . 0765 | 335 |
| 149.6 | . 4774 |  | 159.6 | . 5456 | 229 | 169.6 | .0751 | 279 | 179.6 | . 1437 | 336 337 |
| 149.8 | . 5147 | 187 187 | I59.8 | . 5914 | 229 230 | 169.8 | . 1309 | 279 280 | 179.8 | . 2112 | 337 339 |

TABLE 35.

## PRESSURE OF AQUEOUS VAPOR.

(Broch.)
ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | Diff. for 0.1 | Temperature. | Vapor Pressure. | $\begin{aligned} & \text { Diff. } \\ & \text { for } \\ & 0.1 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. |  |  | Inches. |  |  | Inches. |  |  | Inches. |  |
| 180.0 | 15.2789 |  | 190.0 | 19.0009 | 408 | 200.0 | 23.4530 | 486 | 210.0 | 28.7497 | 577 |
| 180.2 | . 3468 | 340 341 | 190.2 | . 0825 | 408 | 200.2 | . 5502 | 488 | 210.2 | . 8651 | 579 |
| 180.4 | . 4150 | 341 342 | 190.4 | . 1643 | 4 lI | 200.4 | . 6478 | 480 | 210.4 | . 9809 | 58 I |
| 180.6 | . 4835 | 344 | 190.6 | . 2464 | 412 | 200.6 | . 7457 | 491 | 210.6 | 29.0972 | 583 |
| 180.8 | . 5522 | 344 | 190.8 | . 3288 |  | 200.8 | . 8440 | 491 | 210.8 | . 2138 | 583 585 |
| 181.0 | 15.6212 | 345 | 191.0 | 19.4115 | 41 | 201.0 | 23.9426 | 493 | 211.0 | 29.3308 | 585 587 |
| 181.2 | . 6904 | 346 347 | 191.2 | . 4945 | 4 | 201.2 | 24.0415 | 495 | 211.2 | . 4482 | 589 |
| 181.4 | . 7599 | 347 349 | 191.4 | . 5778 | 416 | 201.4 | . 1408 | 497 | 2 II .4 | . 5660 | 589 |
| 181. 6 | . 8296 | 349 350 | 191.6 | . 6614 | 419 | 201.6 | . 2404 | 490 | 211.6 | . 6842 | 593 |
| I81. 8 | . 8996 | 350 | 191.8 | . 7453 | 419 | 201.8 | . 3404 | 500 502 | 211.8 | . 8028 | 593 |
| 182.0 | 15.9699 | 351 | 192.0 | 19.8295 | 421 | 202.0 | 24.4407 | 502 503 | 212.0 | 29.9218 | 595 |
| 182.2 | 16.0404 | 353 354 | 192.2 | . 9140 | 422 | 202.2 | . 5414 | 5 | 212.2 | 30.0412 | 597 |
| 182.4 | . III2 | 354 | 192.4 | . 9988 | 424 | 202.4 | . 6424 | 505 507 | 212.4 | .1610 | 601 |
| 182.6 | . 1822 | 355 | 192.6 | 20.0839 | 427 | 202.6 | .7438 | 509 | 212.6 | .2813 | 603 |
| 182.8 | . 2535 | 357 358 | 192.8 | . 1693 | 427 | 202.8 | . 8455 | 509 510 | 212.8 | . 4019 | 605 |
| 183.0 | 16.3250 | 35 | 193.0 | 20.2550 |  | 203.0 | 24.9476 | 510 | 213.0 | 30.5229 | 7 |
| 183.2 | . 3968 | 359 361 | 193.2 | . 3410 | 430 432 | 203.2 | 25.0500 | 512 | 213.2 | . 6444 | O97 |
| 183.4 | . 4689 | 361 362 | 193.4 | . 4273 | 432 433 | 203.4 | . 1528 | 516 | 213.4 | . 7682 | 611 |
| 183.6 | . 5413 | 363 | 193.6 | . 5139 | 435 | 203.6 | . 2559 | 518 | 213.6 | . 8885 | 613 |
| 183.8 | .6I39 | 363 | 193.8 | . 6008 | 435 | 203.8 | - 3594 |  | 213.8 | 31.01II |  |
| 184.0 | I6.6868 |  | 194.0 | 20.6881 |  | 204.0 | 25.4633 |  | 214.0 | 31.I342 |  |
| 184.2 | . 7599 | 366 | 194.2 | . 7756 | 438 | 204.2 | . 5675 | 521 523 |  |  |  |
| 184.4 | . 8334 | 368 | 194.4 | .8635 | 441 | 204.4 | . 6720 | 525 |  |  |  |
| 184.6 | . 9071 | 370 | 194.6 | .9517 | 4412 | 204.6 | . 7769 | 527 |  |  |  |
| 184.8 | .9810 | 370 | 194.8 | 21.0402 | 442 | 204.8 | . 8822 | 52 |  |  |  |
| 185.0 | 17.0552 | 371 | 195.0 | 21.1289 | 444 | 205.0 | 25.9878 | 5 |  |  |  |
| 185.2 | . 1297 | 373 | 195.2 | . 2180 | 446 | 205.2 | 26.0939 | 530 |  |  |  |
| 185.4 | . 2045 | 374 375 | 195.4 | . 3074 | 449 | 205.4 | . 2002 | 534 |  |  |  |
| 185.6 | . 2795 | 375 377 | 195.6 | . 3971 | 459 | 205.6 | . 3070 | 536 |  |  |  |
| 185.8 | - 3548 | 377 | 195.8 | . 4872 |  | 205.8 | .4141 | 53 |  |  |  |
| 186.0 | 17.4304 | 37 | 196.0 | 21.5776 | 452 | 206.0 | 26.5215 | 537 |  |  |  |
| 186.2 | + 5 | 379 381 | 196.2 | . 6683 | 454 | 206.2 | . 6294 | 539 541 |  |  |  |
| 186.4 | . 5824 | 381 382 | 196.4 | . 7593 | 457 | 206.4 | .7376 | 543 |  |  |  |
| 186.6 | . 6588 | 384 | I96.6 | . 8506 | 458 | 206.6 | .846I | 545 |  |  |  |
| I86.8 | . 7355 | 384 385 | 196.8 | . 9422 | 458 460 | 206.8 | . 9551 | 545 |  |  |  |
| 187.0 | 17.8125 | 385 | 197.0 | 22.0342 | 460 | 207.0 | 27.0644 | 547 549 |  |  |  |
| I87.2 | r 8.8897 | 386 | 197.2 | .1265 | 462 463 | 207.2 | $\begin{array}{r}1.1741 \\ \hline\end{array}$ | 549 |  |  |  |
| 187.4 | . 9672 | 389 | 197.4 | . 2191 | 465 | 207.4 | . 2842 | 552 |  |  |  |
| 187.6 | 18.045 I | 389 391 | 197.6 | . 3120 | 466 | 207.6 | . 3946 | 554 |  |  |  |
| 187.8 | . 1231 | 391 | 197.8 | . 4053 | 468 | 207.8 | . 5054 | 556 |  |  |  |
| 188.0 | 18.2015 |  | 198.0 | 22.4989 |  | 208.0 | 27.6166 |  |  |  |  |
| 188.2 | . 2802 | 393 | 198.2 | . 5928 | 470 | 208.2 | . 7282 | 558 560 |  |  |  |
| 188.4 | . 3591 | 395 | 198.4 | . 6871 | 473 | 208.4 | . 8402 | 562 |  |  |  |
| 188.6 | . 4383 | 398 | 198.6 | .78I6 | 475 | 208.6 | . 9525 | 564 |  |  |  |
| I88.8 | .5178 | 398 | 198.8 | . 8765 | 476 | 208.8 | 28.0652 |  |  |  |  |
| 189.0 | 18.5976 | 399 | 199.0 | 22.9718 | 476 | 209.0 | 28.1784 | 566 |  |  |  |
| I89.2 | . 6777 | 400 | 199.2 | 23.0673 | 4780 | 209.2 | . 2919 | 568 569 |  |  |  |
| 189.4 | .7581 | 402 | 199.4 | .1632 | 481 | 209.4 | .4057 | 571 |  |  |  |
| I89.6 I89.8 | .8388 | 405 | 199.6 | . 2595 | 483 | 209.6 | $.5200$ | 573 |  |  |  |
| 189.8 | .9197 | 406 | 199.8 | . 3560 | 485 | 209.8 | . 6346 | 575 |  |  |  |

TAble 36.
PRESSURE OF AQUEOUS VAPOR.
(Broch.)
METRIC MEASURES.

| Tempsrature. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | mm . | mm . | mm . | mm . | mm . | mm. | mm. | mm . | mm . | mm . |
| $-29^{\circ}$ | 0.42 | 0.41 | 0.41 | 0.41 | 0.40 | 0.40 | 0.40 | 0.39 | 0.39 | 0.38 |
| 28 | 0.46 | 0.46 | 0.45 | 0.45 | 0.44 | 0.44 | 0.43 | 0.43 | 0.43 | 0.42 |
| 27 | 0.50 | 0.50 | 0.50 | 0.49 | 0.49 | 0.48 | 0.48 | 0.47 | 0.47 | 0.46 |
| 26 | 0.55 | 0.55 | 0.54 | 0.54 | 0.53 | 0.53 | 0.52 | 0.52 | 0.5I | 0.5I |
| $-25$ | 0.61 | 0.60 | 0.60 | 0.59 | 0.58 | 0.58 | 0.57 | 0.57 | 0.56 | 0.56 |
| 24 | 0.66 | 0.66 | 0.65 | 0.65 | 0.64 | 0.63 | 0.63 | 0.62 | 0.62 | 0.61 |
| 23 | 0.73 | 0.72 | 0.71 | 0.71 | 0.70 | 0.69 | 0.69 | 0.68 | 0.68 | 0.67 |
| 22 | 0.79 | 0.79 | 0.78 | 0.77 | 0.77 | 0.76 | 0.75 | 0.75 | 0.74 | 0.73 |
| 21 | 0.87 | 0.86 | 0.85 | 0.84 | 0.84 | 0.83 | 0.82 | 0.81 | 0.81 | 0.80 |
| - 20 | 0.94 | 0.94 | 0.93 | 0.92 | 0.91 | 0.90 | 0.90 | 0.89 | 0.88 | 0.87 |
| 19 | 1.03 | 1.02 | 1.OI | 1.00 | 0.99 | 0.99 | 0.98 | 0.97 | 0.96 | 0.95 |
| 18 | I. 12 | I.II | I. 10 | 1.09 | 1.08 | 1.07 | 1.06 | 1.06 | 1.05 | 1.04 |
| 17 | 1.22 | 1.21 | 1.20 | 1.19 | I. 18 | I. 17 | I. 16 | I. 15 | I. 14 | I. 13 |
| 16 | I. 32 | I. 31 | I. 30 | 1.29 | 1.28 | 1.27 | I. 26 | I. 25 | I. 24 | 1.23 |
| - 15 | 1.44 | 1.43 | 1.42 | 1.40 | 1.39 | 1.38 | 1.37 | I. 36 | 1.35 | I. 34 |
| 14 | I. 56 | 1.55 | I. 54 | I. 52 | 1.51 | 1.50 | I. 49 | 1. 48 | 1. 46 | r. 45 |
| 13 | 1.69 | r. 68 | I. 67 | 1.65 | r. 64 | 1.63 | r. 61 | 1.60 | 1.59 | 1.57 |
| 12 | I. 84 | r. 82 | I.8I | 1.79 | 1.78 | 1.76 | 1.75 | 1.74 | 1.72 | 1.71 |
| II | 1.99 | 1.97 | 1.96 | 1.94 | 1.93 | 1.91 | 1.90 | r. 88 | r. 87 | 1.85 |
| $-10$ | 2.15 | 2.13 | 2.12 | 2.10 | 2.08 | 2.07 | 2.05 | 2.04 | 2.02 | 2.00 |
| 9 | 2.33 | 2.31 | 2.29 | 2.27 | 2.26 | 2.24 | 2.22 | 2.20 | 2.19 | 2.17 |
| 8 | 2.51 | 2.50 | 2.48 | 2.46 | 2.44 | 2.42 | 2.40 | 2.38 | 2.36 | 2.34 |
| 7 | 2.72 | 2.69 | 2.67 | 2.65 | 2.63 | 2.61 | 2.59 | 2.57 | 2.55 | 2.53 |
| 6 | 2.93 | 2.91 | 2.89 | 2.86 | 2.84 | 2.82 | 2.80 | 2.78 | 2.76 | 2.74 |
| 5 | 3.16 | 3.14 | 3.11 | 3.09 | 3.07 | 3.04 | 3.02 | 3.00 | 2.98 | 2.95 |
| 4 | 3.41 | $3 \cdot 38$ | $3 \cdot 36$ | 3.33 | 3.31 | 3.28 | 3.26 | 3.23 | 3.21 | 3.18 |
| 3 | 3.67 | 3.64 | 3.62 | 3.59 | 3.56 | 3.54 | 3.51 | 3.48 | 3.46 | 3.43 |
| 2 | 3.95 | 3.92 | 3.89 | 3.86 | 3.84 | 3.8 I | 3.78 | 3.75 | 3.72 | 3.70 |
| 1 | 4.25 | 4.22 | 4.19 | 4.16 | 4.13 | 4.10 | 4.07 | 4.04 | 4.01 | 3.98 |
| - 0 | 4.57 | 4.54 | 4.50 | 4.47 | 4.44 | 4.4 I | 4.37 | 4.34 | 4.31 | 4.28 |
|  | Values for temperatures between $0^{\circ}$ and $45^{\circ}$ are given in Table 43. |  |  |  |  |  |  |  |  |  |
| $+45^{\circ}$ | 71.36 | 71.73 | 72.10 | 72.48 | 72.85 | 72.23 | 73.60 | 73.98 | $74 \cdot 36$ | 74.75 |
| 46 | 75.13 | 75.52 | 75.91 | 76.30 | 76.69 | 77.08 | 77.47 | 77.87 | 78.27 | 78.67 |
| 47 | 79.07 | 79.47 | 79.88 | 80.29 | 80.70 | 8 I .11 | 8 I .52 | 81.93 | 82.35 | 82.77 |
| 48 | 83.19 | 83.61 | 84.03 | 84.46 | 84.89 | 84.32 | 85.75 | 86.18 | 86.6I | 87.05 |
| 49 | 87.49 | 87.93 | 88.37 | 88.81 | 89.26 | 89.71 | 90.16 | 90.61 | 91.06 | 91.52 |
| 50 | 91.98 | 92.44 | 92.90 | 93.36 | 93.83 | 94.30 | 94.77 | 95.24 | 95.71 | 96.19 |
| 51 | 96.66 | 97.14 | 97.63 | 98.11 | 98.60 | 99.08 | 99.57 | 100.07 | 100.56 | 101.06 |
| 52 | 101.55 | 102.05 | 102.56 | 103.06 | 103.57 | 104.08 | 104.59 | 105.10 | 105.62 | 106. 14 |
| 53 | 106.65 | 107.18 | 107.70 | 108.23 | 108.76 | 109.29 | 109.82 | 110.35 | 110.89 | III. 43 |
| 54 | III. 97 | 112.52 | II3.06 | 113.6I | 114.16 | II4.72 | 115.27 | 115.83 | 116.39 | II6.95 |
| 55 | 117.52 | ri8.08 | 118.65 | I19.22 | 119.80 | 120.37 | 120.95 | 121.53 | 122.12 | 122.70 |
| 56 | 123.29 | 123.88 | 124.48 | 125.07 | 125.67 | 126.27 | 126.87 | 127.48 | 128.09 | 128.70 |
| 57 | 129.31 | 129.92 | 130.54 | 131.16 | 131.79 | 132.41 | 133.04 | 133.67 | 134.30 | 134.94 |
| 58 | 135.58 | 136.22 | 136.86 | 137.50 | 138.15 | 138.80 | 139.46 | 140.11 | 140.77 | 141.43 |
| 59 | 142.10 | 142.76 | 143.43 | 144.11 | 144.78 | 145.46 | 146.14 | 146.82 | 147.51 | 148.19 |
| 60 | 148.88 | 149.58 | I50.27 | 150.97 | 151.68 | 152.38 | 153.09 | 153.80 | 154.5I | 155.23 |

## TAble 36.

## PRESSURE OF AQUEOUS VAPOR.

## (Broch.)

METRIC MEASURES.

| Temperature. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | mm . | mm . | mm . | mm . | mm . | mm . | mm . | mm . | mm . | mm . |
| $60^{\circ}$ | 148.88 | 149.58 | 150.27 | 150.97 | 151.68 | 152.38 | 153.09 | 153.80 | I54.51 | 155.23 |
| 61 | 155.95 | 156.67 | 157.39 | 158.12 | 158.85 | 159.58 | 160.32 | 161.06 | 161.80 | 162.54 |
| 62 | 163.29 | 164.04 | 164.79 | 165.55 | 166.31 | 167.07 | 167.83 | 168.60 | 169.37 | 170.15 |
| 63 | 170.92 | 171.70 | 172.49 | 173.27 | I74.06 | 174.85 | 175.65 | 176.45 | 177.25 | 178.05 |
| 64 | I 78.86 | 179.67 | 180.48 | 181.30 | 182.12 | 182.94 | 183.77 | 184.60 | 185.43 | I86. 26 |
| 65 | 187.10 | 187.94 | 188.79 | 189.64 | 190.49 | 191.34 | 192.20 | 193.06 | 193.93 | 194.80 |
| 66 | 195.67 | 196.54 | 197.42 | 198.30 | 199.18 | 200.07 | 200.96 | 201.86 | 202.75 | 203.65 |
| 67 | 204.56 | 205.47 | 206.38 | 207.29 | 208.21 | 209. 13 | 210.06 | 210.98 | 211.92 | 212.85 |
| 68 | 213.79 | 214.73 | 215.68 | 216.63 | 217.58 | 218.54 | 219.50 | 220.46 | 221. 43 | 222.40 |
| 69 | 223.37 | 224.35 | 225.33 | 226.3 I | 227.30 | 228.29 | 229.29 | 230.29 | 231.29 | 232.30 |
| 70 | 233.3 I | 234.32 | 235.34 | 236.36 | 237.39 | 238.42 | 239.45 | 240.48 | 241.52 | 242.57 |
| 71 | 243.62 | 244.67 | 245.72 | 246.78 | 247.85 | 248.91 | 249.98 | 251.06 | 252.14 | 253.22 |
| 72 | 254.30 | 255.40 | 256.49 | 257.59 | 258.69 | 259.80 | 260.91 | 262.02 | 263.14 | 264.26 |
| 73 | 265.38 | 266.5I | 267.65 | 268.79 | 269.93 | 271.08 | 272.23 | 273.38 | 274.54 | 275.70 |
| 74 | 276.87 | 278.04 | 279.21 | 280.39 | 281. 58 | 282.76 | 283.95 | 285. 15 | 286.35 | 287.56 |
| 75 | 288.76 | 289.98 | 291. 19 | 292.42 | 293.64 | 294.87 | 296. 11 | 297.34 | 298.59 | 299.83 |
| 76 | 301.09 | 302.34 | 303.60 | 304.87 | 306.14 | 307.41 | 308.69 | 309.97 | 311.26 | 312.55 |
| 77 | 313.85 | 315.15 | 316.45 | 317.76 | 319.07 | 320.39 | 321.72 | 323.04 | 324.38 | 325.71 |
| 78 | 327.05 | 328.40 | 329.75 | 331.1I | 332.47 | 333.83 | 335.20 | 336.58 | 337.95 | 339.34 |
| 79 | 340.73 | 342.12 | 343.52 | 344.92 | 346.33 | 347.74 | 349.16 | 350.58 | 352.01 | 353.44 |
| 80 | 354.87 | 356.3I | 357.76 | 359.21 | 360.67 | 362.13 | 363.59 | 365.07 | 366.54 | 368.02 |
| 8 I | 369.51 | 371.00 | 372.49 | 374.00 | 375.50 | 377.01 | 378.53 | 380.05 | 381. 58 | 383.11 |
| 82 | 384.64 | 386. I8 | 387.73 | 389.28 | 390.84 | 392.40 | 393.97 | 395.54 | 397.12 | 398.70 |
| 83 | 400.29 | 401.89 | 403.49 | 405.09 | 406.70 | 408.32 | 409.94 | 411.56 | 413.19 | 414.83 |
| 84 | 416.47 | 418.12 | 419.77 | 421.43 | 423.09 | 424.76 | 426.44 | 428.12 | 429.8 I | 431.50 |
| 85 | 433.19 | 434.90 | 436.60 | 438.32 | 440.04 | 441.76 | 443.49 | 445.23 | 446.97 | 448.72 |
| 86 | 450.47 | 452.23 | 454.00 | 455.77 | 457.54 | 459.33 | 461.1I | 462.91 | 464.71 | 466.51 |
| 87 | 468.32 | 470.14 | 471.96 | 473.79 | 475.63 | 477.47 | 479.32 | 481. 77 | 483.03 | 484.89 |
| 88 | 486.76 | 488.64 | 490.52 | 492.41 | 494.3I | 496.2 I | 498. 12 | 500.03 | 5 OI .95 | 503.87 |
| 89 | 505.81 | 507.74 | 509.69 | 511.64 | 513.60 | 515.56 | 517.53 | 519.50 | 52 I .48 | 523.47 |
| 90 | 525.47 | 527.47 | 529.48 | 531.49 | 533.51 | 535.54 | 537.57 | 539.61 | 541.65 | 543.71 |
| 91 | 545.77 | 547.83 | 549.90 | 551.98 | 554.07 | 556.16 | 558.26 | 560.36 | 562.47 | 564.59 |
| 92 | 566.7 I | 568.85 | 570.98 | 573.13 | 575.28 | 577.44 | 579.61 | 581.78 | 583.96 | 586.14 |
| 93 | 588.33 | 590.53 | 592.74 | 594.95 | 597.17 | 599.40 | 601.64 | 603.88 | 606.13 | 608.38 |
| 94 | 610.64 | 6I2.91 | 615.19 | 6 I 7.47 | 619.76 | 622.06 | 624.37 | 626.68 | 629.00 | 631.32 |
| 95 | 633.66 | 636.00 | 638.35 | 640.70 | 643.06 | 645.43 | 647.81 | 650.20 | 652.59 | 654.99 |
| 96 | 657.40 | 659.81 | 662.23 | 664.66 | 667.10 | 669.54 | 672.00 | 674.45 | 676.92 | 679.40 |
| 97 | 681. 88 | 684.37 | 686.87 | 689.37 | 691.89 | 694.41 | 696.93 | 699.47 | 702.02 | 704.57 |
| 98 | 707.13 | 709.69 | 712.27 | 714.85 | 717.44 | 720.04 | 722.65 | 725.27 | 727.89 | 730.52 |
| 99 | 733.16 | 735.8I | 738.46 | 741. 13 | 743.80 | 746.48 | 749.17 | 751.86 | 754.57 | 757.28 |
| 100 101 | $\begin{aligned} & 760.00 \\ & 787.67 \end{aligned}$ | 762.73 | 765.47 | 768.21 | 770.97 | 773.73 | 776.50 | 779.28 | 782.07 | 784.86 |

TABLE 37.
PRESSURE OF AQUEOUS VAPOR AT-LOW TEMPERATURES.
(C. F. Marvin.)

ENGLISH AND METRIC MEASURES.

| Temperatures. | $0 \% 0$ |  | 0.2 |  | 0.4 |  | 0.6 |  | 0.8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. | mm . | Inch. | mm . | Inch. | mm . | Inch. | mm. | Inch. | mm . |
| $-60^{\circ}$ | 0.0010 | 0.026 |  |  |  |  |  |  |  |  |
| 59 | . 0011 | . 028 | 0.0011 | 0.028 | 0.0011 | 0.027 | 0.00I I | 0.027 | 0.0010 | 0.026 |
| 58 | . 0012 | . 030 | . 0012 | . 030 | . 0011 | . 029 | . 0011 | . 029 | . 0011 | . 028 |
| 57 | .0013 | . 032 | .0013 | . 032 | . 0012 | . 031 | . 0012 | . 031 | . 0012 | . 030 |
| 56 | .0013 | . 034 | .0013 | . 034 | .0013 | . 033 | .0013 | . 033 | .0013 | . 032 |
| $-55^{\circ}$ | 0.0015 | 0.037 | 0.0014 | 0.036 | 0.0014 | 0.036 | 0.0014 | 0.035 | 0.0014 | 0.035 |
| 54 | .0016 | . 040 | . 0015 | . 039 | .0015 | . 039 | .0015 | . 038 | . 0015 | . 037 |
| 53 | . 0017 | . 043 | . 0017 | . 042 | . 0017 | . 042 | .0016 | .041 | .0016 | . 040 |
| 52 | .OOI8 | . 046 | .0018 | . 045 | . 0018 | . 045 | .0017 | . 044 | .0017 | . 043 |
| 5 I | .0019 | . 049 | .0019 | . 048 | .0019 | . 048 | .0019 | . 047 | .0018 | . 046 |
| $-50^{\circ}$ | 0.002 I | 0.053 | 0.0020 | 0.052 | 0.0020 | 0.05I | 0.0020 | 0.05I | 0.0020 | 0.050 |
| 49 | . 0022 | . 057 | . 0022 | . 056 | . 0022 | . 055 | . 0022 | . 055 | . 0021 | . 054 |
| 48 | . 0024 | .06I | . 0024 | . 060 | . 0023 | . 059 | . 0023 | . 059 | . 0023 | . 058 |
| 47 | . 0026 | . 065 | . 0025 | . 064 | . 0025 | . 063 | . 0025 | . 063 | . 0024 | . 062 |
| 46 | . 0027 | . 069 | . 0027 | . 068 | . 0027 | . 068 | . 0026 | . 067 | . 0026 | . 066 |
| $-45^{\circ}$ | 0.0029 | 0.074 | 0.0029 | 0.073 | 0.0028 | 0.072 | 0.0028 | 0.071 | 0.0028 | 0.070 |
| 44 | .0031 | . 079 | .0031 | . 078 | . 0030 | . 077 | . 0030 | . 076 | . 0030 | . 075 |
| 43 | . 0033 | . 084 | . 0033 | . 083 | . 0032 | . 082 | . 0032 | .081 | .003I | .080 |
| 42 | . 0035 | . 089 | . 0035 | . 088 | . 0034 | . 087 | . 0034 | . 086 | . 0033 | . 085 |
| 4 I | . 0037 | . 094 | . 0037 | . 093 | . 0036 | . 092 | . 0036 | . 091 | . 0035 | . 090 |
| $-40^{\circ}$ | 0.0039 | 0.100 | 0.0039 | 0.098 | 0.0038 | 0.097 | 0.0038 | 0.096 | 0.0037 | 0.095 |
| 39 | .004I | . 105 | . 0041 | .104 | .004I | . 103 | . 0040 | . 102 | . 0040 | . 101 |
| 38 | . 0044 | . III | . 0043 | . 109 | . 0043 | . 108 | . 0042 | . 107 | . 0042 | . 106 |
| 37 | . 0046 | . 117 | . 0045 | . 115 | . 0045 | . 114 | . 0044 | . II3 | . 0044 | . 112 |
| 36 | . 0048 | . 123 | . 0048 | . 12 I | . 0047 | . 120 | . 0047 | . II9 | . 0046 | . 118 |
| $-35^{\circ}$ | 0.0051 | 0.130 | 0.0051 | 0. 129 | 0.0050 | 0.127 | 0.0050 | 0.126 | 0.0049 | 0. 124 |
| 34 | . 0054 | . 138 | . 0054 | . 136 | . 0053 | . 135 | . 0052 | . 133 | . 0052 | . 132 |
| 33 | . 0057 | . 146 | . 0057 | . 144 | . 0056 | . 142 | . 0056 | . 141 | . 0055 | . 139 |
| 32 | .006I | . 155 | . 0060 | . 153 | . 0059 | . 151 | . 0059 | . 149 | . 0058 | . 147 |
| 31 | . 0065 | . 165 | . 0064 | . 163 | . 0063 | .161 | . 0063 | . 159 | . 0062 | . 157 |
| $-30^{\circ}$ | 0.0069 | 0. 176 | 0.0069 | 0.174 | 0.0067 | 0.171 | 0.0067 | 0.169 | 0.0066 | 0. 167 |
| 29 | . 0074 | . 187 | . 0073 | . 185 | . 0072 | . 183 | . 0071 | . 180 | . 0070 | . 178 |
| 28 | . 0078 | . 199 | .0078 | . 197 | . 0077 | . 195 | . 0076 | . 192 | . 0075 | . 190 |
| 27 | .0083 | . 212 | . 0083 | . 210 | .0081 | . 207 | . 0080 | . 204 | .0080 | . 202 |
| 26 | .0089 | . 225 | . 0088 | . 223 | . 0087 | . 220 | . 0085 | . 217 | . 0085 | . 215 |
| $-25^{\circ}$ | 0.0094 | 0.239 | 0.0093 | 0.236 | 0.0092 | 0.233 | 0.0091 | 0.230 | 0.0089 | 0.227 |
| 24 | . 0100 | . 253 | . 0098 | . 250 | . 0097 | . 247 | .0096 | . 244 | . 0095 | . 242 |
| 23 | . 0106 | . 268 | . 0104 | . 265 | . 0103 | . 262 | . 0102 | . 259 | . Or 1 | . 256 |
| 22 | . OI 12 | . 284 | . 0111 | . 281 | . 0109 | . 278 | . 0108 | . 274 | . 0107 | . 271 |
| 21 | .OII9 | . 301 | . 0117 | . 297 | . 0116 | . 294 | .or15 | . 291 | . 0113 | . 287 |
| $-20^{\circ}$ | 0.0126 | 0.319 | 0.0124 | 0.315 | 0.0122 | 0.311 | 0.0121 | 0.308 | 0.0120 | 0.304 |
| 19 | . 0133 | . 338 | .0131 | . 334 | .OI30 | . 330 | . 0128 | . 326 | . 0127 | - 322 |
| 18 | . 0141 | -358 | .or39 | . 354 | .or38 | -350 | .0136 | . 346 | . 0135 | -342 |
| 17 | . 0150 | . 380 | .or48 | -375 | . 0146 | -371 | . 0144 | -366 | . 0143 | - 362 |
| 16 | . 0159 | . 403 | . 0157 | -398 | . 0155 | -393 | . 0153 | -389 | . 0151 | -384 |
| $-15^{\circ}$ | 0.0168 | 0.427 | 0.0166 | 0.422 | 0.0164 | 0.417 | 0.0162 | 0.412 | 0.0160 | 0.407 |

PRESSURE OF AQUEOUS VAPOR AT LOW TEMPERATURES.

## (C. F. Marvin.)

ENGLISH AND METRIC MEASURES.

| Temperature. | 0.0 |  | 0.2 |  | 0.4 |  | 0.6 |  | 0.8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. | mm . | Inch. | mm . | Inch. | mm . | Inch. | mm. | Inch. | mm. |
| $-15^{\circ}$ | 0.0168 | 0.427 | 0.0166 | 0.422 | 0.0164 | 0.417 | 0.0162 | 0.412 | 0.0160 | 0.407 |
| 14 | . 0178 | . 452 | .0176 | . 447 | . 0174 | . 442 | . 0172 | . 437 | . 0170 | . 432 |
| 13 | . 0188 | . 478 | . 0186 | . 473 | . 0184 | . 468 | .or82 | . 462 | . 0180 | . 457 |
| 12 | .or99 | . 505 | . 0196 | . 499 | . 0194 | . 494 | . 0192 | . 488 | . 0190 | . 483 |
| II | . 0210 | . 534 | . 0208 | . 528 | . 0206 | . 522 | . 0203 | . 516 | . 0201 | . 510 |
| $-10$ | 0.0222 | 0.564 | 0.0220 | 0.558 | 0.0217 | 0.552 | 0.0215 | 0.546 | 0.0213 | 0.540 |
| 9 | . 0234 | . 595 | . 0232 | . 588 | . 0229 | . 582 | . 0227 | . 576 | . 0224 | . 570 |
| 8 | . 0247 | . 627 | . 0244 | . 620 | . 0242 | . 614 | . 0239 | . 607 | . 0237 | . 601 |
|  | . 0260 | .66I | . 0257 | . 654 | . 0255 | . 647 | . 0252 | . 640 | . 0249 | . 633 |
| 6 | . 0275 | . 698 | . 0272 | . 691 | . 0269 | . 683 | . 0266 | . 676 | . 0263 | . 669 |
| -5 | 0.0291 | 0.738 | 0.0287 | 0.730 | 0.0284 | 0.722 | 0.0281 | 0.714 | 0.0278 | 0.706 |
| 4 | . 0307 | .781 | . 0304 | . 772 | . 0301 | . 764 | . 0297 | . 755 | . 0294 | . 747 |
| 3 | . 0325 | . 826 | . 0322 | .817 | . 0318 | . 808 | . 0315 | . 799 | . 0311 | . 790 |
| 2 | . 0344 | . 873 | . 0340 | . 863 | . 0336 | . 854 | . 0332 | . 844 | . 0329 | . 835 |
| 1 | . 0363 | . 922 | . 0359 | .912 | . 0355 | . 902 | .035I | . 892 | . 0347 | . 882 |
| -o | . 0383 | . 972 | . 0379 | . 962 | . 0375 | . 952 | . 0371 | . 942 | . 0367 | . 932 |
| $+0$ | 0.0383 | 0.972 | 0.0387 | 0.982 | 0.0391 | 0.992 | 0.0394 | 1.002 | 0.0398 | 1.012 |
| I | . 0403 | 1.023 | . 0407 | 1.033 | .04II | 1.043 | .0415 | 1.054 | .0419 | 1.064 |
| 2 | . 0423 | 1.075 | . 0428 | 1.086 | .043I | 1.096 | . 0436 | I. 107 | . 0440 | I.II8 |
| 3 | . 0444 | I.129 | . 0449 | I.140 | . 0453 | I.15I | . 0458 | I. 163 | . 0462 | I. 174 |
| 4 | . 0467 | 1.186 | . 0472 | I.198 | . 0476 | 1.210 | .048I | I. 222 | . 0486 | 1.234 |
| 5 | 0.049I | 1.246 | 0.0495 | 1.258 | 0.0500 | 1.27I | 0.0505 | 1.283 | 0.0510 | 1.296 |
| 6 | .05I5 | 1.309 | . 0520 | 1.322 | . 0526 | 1.335 | . 0531 | 1.349 | . 0536 | I. 362 |
| 7 | . 0542 | 1.376 | . 0547 | 1.390 | . 0553 | 1.404 | . 0558 | 1.418 | . 0564 | 1.433 |
| 8 | . 0570 | I. 447 | . 0576 | 1.462 | . 0582 | 1.477 | . 0587 | I. 492 | . 0594 | 1.508 |
| 9 | . 0600 | 1.523 | . 0606 | 1.539 | .06I2 | 1.555 | .0618 | 1.571 | . 0625 | I. 587 |
| 10 | 0.0631 | 1.603 | 0.0638 | 1.620 | 0.0644 | 1.636 | 0.0651 | 1.653 | 0.0657 | 1.670 |
| II | . 0665 | 1.688 | .0671 | 1.705 | . 0678 | 1.722 | . 0685 | 1.740 | . 0692 | 1.758 |
| 12 | . 0699 | 1.776 | . 0706 | 1.794 | . 0713 | I.812 | . 0720 | 1.830 | . 0728 | r. 848 |
| 13 | . 0735 | 1.867 | . 0742 | 1.885 | . 0750 | 1. 904 | . 0757 | 1.923 | . 0765 | 1.942 |
| 14 | . 0772 | 1.96I | . 0780 | 1.980 | . 0787 | 1.999 | . 0794 | 2.018 | . 0802 | 2.038 |
| 15 | 0.0810 | 2.058 | 0.0818 | 2.078 | 0.0826 | 2.098 | 0.0834 | 2.118 | 0.0842 | 2.138 |
| 16 | . 0850 | 2.158 | . 0857 | 2.178 | . 0866 | 2.199 | . 0874 | 2.220 | . 0882 | 2.241 |
| 17 | .0891 | 2.262 | . 0899 | 2.283 | . 0907 | 2.305 | .0916 | 2.327 | . 0925 | 2.349 |
| 18 | . 0933 | 2.371 | . 0942 | 2.393 | .0951 | 2.416 | . 0960 | 2.439 | . 0969 | 2.462 |
| 19 | . 0979 | 2.486 | . 0988 | 2.510 | . 0998 | 2.534 | . 1007 | 2.558 | .1017 | 2.582 |
| 20 | 0.1026 | 2.607 | 0.1036 | 2.632 | 0.1046 | 2.657 | 0.1056 | 2.683 | 0.1067 | 2.709 |
| 21 | . 1077 | 2.735 | .1087 | 2.761 | . 1098 | 2.788 | .1108 | 2.815 | .1119 | 2.842 |
| 22 | .1130 | 2.869 | .1141 | 2.897 | .II52 | 2.925 | .1163 | 2.953 | . 1174 | 2.981 |
| 23 | .1185 | 3.009 | . 1196 | 3.037 | . 1207 | 3.066 | .1219 | 3.095 | . 1230 | 3.125 |
| 24 | . 1242 | 3.155 | . 1254 | 3.185 | . 1266 | 3.215 | . 1278 | 3.245 | . 1290 | 3.276 |
| 25 | 0.1302 | 3.307 | 0.1314 | 3.338 | 0.1327 | 3.370 | O.I339 | 3.402 | 0.1352 | 3.434 |
| 26 | . 1365 | 3.466 | .I377 | 3.498 | . 1390 | 3.53 I | . 1403 | 3.564 | . 1416 | 3.597 |
| 27 | .I430 | 3.631 | . 1443 | 3.665 | . 1456 | 3.699 | . 1470 | 3.733 | .1483 | 3.768 |
| 28 | . 1497 | 3.803 | . 1511 | 3.838 | . 1525 | 3.874 | .1539 | 3.910 | . 1554 | 3.946 |
| 29 | . 1568 | 3.982 | . 1582 | 4.018 | . 1596 | 4.055 | .16II | 4.093 | . 1626 | 4.I3I |
| 30 | 0.1641 | 4.169 | 0.1656 | 4.207 | 0.1671 | 4.245 | 0.1687 | 4.284 | 0.1702 | 4.324 |
| 31 32 | .1718 .1798 | 4.364 4.568 | . 1734 | 4.404 | . 1750 | 4.444 | . 1766 | 4.485 | . 1782 | $4 \cdot 526$ |

Smithbonian Tables.

TABLE 38.

## WEIGHT OF AQUEOUS VAPOR IN A CUBIC FOOT OF SATURATED AIR.

ENGLISH MEASURES.

| Temperature. | 0.0 | 0.5 | $\begin{aligned} & \text { Diff. } \\ & \text { for } \\ & \text { for } \end{aligned}$ | Temperature. | 0.0 | 0\% 5 | Diff. for 0.1 | Temperature. | 0:0 | 0.5 | $\begin{aligned} & \text { Diff. } \\ & \text { for } \\ & 0.1 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Grains troy. | Grains troy. |  | F. | Grains troy. | Grains troy. |  | F. | Grains troy. | Grains troy. |  |
| $-19^{\circ}$ | 0.230 | 0.224 | I | $26^{\circ}$ | 1.675 | 1.709 | 7 | $71^{\circ}$ | 8.240 | 8.372 | 27 |
| - I8 | . 242 | . 236 | I | 27 | 1.743 | 1.777 | 7 | 72 | 8.508 | 8.644 | 27 |
| - 17 | . 254 | . 248 | I | 28 | 1.812 | 1.847 | 7 | 73 | 8.782 | 8.923 | 28 |
| - 16 | . 267 | . 260 | I | 29 | 1.882 | 1.919 | 7 | 74 | 9.066 | 9.210 | 29 |
| - 15 | 0.280 | 0.273 | I | 30 | 1. 956 | I. 995 | 8 | 75 | 9.356 | 9.504 | 30 |
| $-14$ | . 294 | . 286 | I | 31 | 2.034 | 2.073 | 8 | 76 | 9.655 | 9.807 | 31 |
| - 13 | . 309 | . 301 | 1 | 32 | 2.113 | 2. 153 | 8 | 77 | 9.962 | Io. 118 | 32 |
| 12 | . 324 | . 316 | 2 | 33 | 2.194 | 2.236 | 8 | 78 | 10.277 | 10.438 | 33 |
| - II | . 340 | . 332 | 2 | 34 | 2.279 | 2.322 | 9 | 79 | 10.601 | 10.766 | 33 |
| $-10$ | 0.356 | 0.348 | 2 | 35 | 2.366 | 2.41 I | 9 | 80 | 10.934 | II.103 | 34 |
| - 9 | . 373 | . 365 | 2 | 36 | 2.457 | 2.503 | 9 | 8 I | II. 275 | II.450 | 35 |
| - 8 | . 391 | . 382 | 2 | 37 | 2.550 | 2.598 | 10 | 82 | 11.626 | II. 805 | 36 |
|  | . 41 I | . 400 | 2 | 38 | 2.646 | 2.695 | 10 | 83 | 11.987 | 12.170 | 37 |
| - 6 | . 430 | . 420 | 2 | 39 | 2.746 | 2.797 | 10 | 84 | 12.356 | 12.545 | 38 |
| - 5 | 0.450 | 0.439 | 2 | 40 | 2.849 | 2.901 | II | 85 | 12.736 | 12.930 | 39 |
| - 4 | . 47 I | . 460 | 2 | 41 | 2.955 | 3.009 | II | 86 | 13.127 | 13.325 | 40 |
| - 3 | . 493 | . 482 | 2 | 42 | 3.064 | 3. 120 | II | 87 | 13.526 | 13.730 | 41 |
| - 2 | . 516 | . 504 | 2 | 43 | 3.177 | 3.235 | 12 | 88 | 13.937 | 14.146 | 42 |
| J | . 540 | . 52 S | 2 | 44 | 3.294 | 3.354 | 12 | 89 | 14.359 | 14.573 | 43 |
| - 0 | . 564 | . 552 | 2 |  |  |  |  |  |  |  |  |
| $+0$ | 0.564 | 0.577 | 3 | 45 | 3.414 | 3.477 | 12 | 90 | 14.790 | 15.01 I | 44 |
|  | . 590 | . 603 | 3 | 46 | 3.539 | 3.603 | 13 | 91 | 15.234 | 15.460 | 45 |
| 2 | .617 | . 630 | 3 | 47 | 3.667 | 3.733 | I3 | 92 | 15.689 | 15.920 | 47 |
| 3 | . 645 | . 659 | 3 | 48 | 3.800 | 3.868 | 14 | 93 | 16.155 | 16.393 | 48 |
| 4 | . 674 | . 689 | 3 | 49 | 3.936 | 4.006 | 14 | 94 | 16.634 | 16.877 | 49 |
| 5 | 0.705 | 0.719 | 3 | 50 | 4.076 | 4.148 | 15 | 95 | 17.124 | 17.374 | 50 52 |
| 6 | . 735 | .75I | 3 | 51 | 4.222 | 4.296 | 15 | 96 | 17.626 | 17.883 | 52 |
| 7 | .767 | . 784 | 3 | 52 | 4.372 | 4.448 | 15 | 97 | 18.142 | 18.404 | 53 |
| 8 | . 801 | . 819 | 4 | 53 | 4.526 | 4.604 | 16 | 98 | 18.671 | 18.940 | 54 |
| 9 | . 837 | . 854 | 4 | 54 | 4.685 | 4.766 | 16 | 99 | 19.212 | 19.487 | 55 |
| 10 | 0.873 | 0.891 | 4 | 55 | 4.849 | 4.933 | 17 | 100 | 19.766 | 20.049 | 57 |
| II | . 910 | . 930 | 4 | 56 | 5.016 | 5.103 | 17 | IOI | 20.335 | 20.624 | 58 |
| 12 | . 950 | . 970 | 4 | 57 | 5.191 | 5.280 | I8 | 102 | 20.917 | 21.214 | 60 |
| 13 | . 991 | I. OII | 4 | 58 | 5.370 | 5.462 | 18 | 103 | 21.514 | 21.817 | 61 |
| 14 | 1.033 | 1.054 | 4 | 59 | $5 \cdot 555$ | 5.649 | 19 | 104 | 22.125 | 22.436 | 62 |
| 15 | 1.077 | 1.098 | 5 | 60 | 5.745 | 5.842 | 20 | 105 | 22.750 | 23.070 | 64 |
| 16 | 1.122 | I. 144 | 5 | 61 | 5.94 I | 6.040 | 20 | 106 | 23.392 | 23.718 | 66 |
| 17 | 1.169 | I. 193 | 5 | 62 | 6.142 | 6.245 | 21 | 107 | 24.048 | 24.382 | 67 |
| 18 | I. 217 | I. 242 | 5 | 63 | 6.349 | 6.456 | 21 | 108 | 24.720 25.408 | 25.062 25.758 | 69 70 |
| 19 | 1. 268 | 1.294 | 5 | 64 | 6.563 | 6.672 | 22 | 109 | 25.408 | 25.758 | 70 |
| 20 | I.321 | 1.347 | 5 | 65 | 6.782 | 6.895 | 23 | 110 | 26.112 | 26.470 | 72 |
| 21 | 1.374 | 1.402 | 6 | 66 | 7.009 | 7.124 | 23 | III | 26.832 | 27.199 | 74 |
| 22 | 1. 430 | I. 459 | 6 | 67 | 7.241 | $7 \cdot 360$ | 24 | 112 | 27.570 | 27.946 | 75 |
| 23 | I. 488 | 1.518 | 6 | 68 | 7.480 | 7.602 | 25 | 113 | 28.325 | 28.708 | 77 |
| 24 | I. 549 | 1.580 | 6 | 69 | 7.726 | 7.852 | 25 | 114 | 29.096 | 29.489 | 79 |
| 25 | I.6II | I. 643 | 6 | 70 | 7.980 | 8.109 | 26 | 115 | 29.887 |  |  |

TAble 39.

## WEIGHT OF AQUEOUS VAPOR IN A CUBIC METRE OF SATURATED AIR.

METRIC MEASURES.

| Tem- pera- ture. |  | Temperature. | 0.0 | 0.5 | Temperature. | 0.0 | 0.2 | 0.4 | 0.6 | $0: 8$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | Gram's. | c. | Gram's. | Gram's. | c. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. |
| $-29^{\circ}$ | 0.496 | $-17^{\circ}$ | 1. 375 | I. 32 I | $-5^{\circ}$ | 3.407 | 3.359 | 3.311 | 3.263 | 3.217 |
| 28 | . 542 | 16 | 1. 489 | I. 432 | 4 | 3.659 | 3.607 | 3.556 | 3.506 | 3.456 |
| 27 | . 593 | 15 | I.6II | I. 549 | 3 | 3.926 | 3.871 | 3.817 | 3.763 | 3.711 |
| 26 | . 647 | 14 | 1.742 | 1.676 | 2 | 4.2 II | 4.152 | 4.095 | 4.038 | 3.982 |
| 25 | . 706 | 13 | 1.882 | 1.811 | 1 | 4.513 | 4.45 I | 4.390 | 4.329 | 4.270 |
| 24 | . 770 | 12 | 2.032 | 1.956 | -0 | 4.835 | 4.769 | 4.704 | 4.640 | 4.576 |
| -23 | 0.839 | - II | 2.192 | 2.111 | +0 | 4.835 | $4 \cdot 901$ | 4.969 | 5.037 | 5.106 |
| 22 | . 913 | 10 | 2.363 | 2.276 | I | 5.176 | 5.247 | 5.318 | 5.391 | 5.464 |
| 21 | . 992 | 9 | 2.546 | 2.453 | 2 | 5.538 | 5.6I3 | 5.689 | 5.766 | 5.844 |
| 20 | 1.078 | 8 | 2.741 | 2.642 | 3 | 5.922 | 6.002 | 6.082 | 6.164 | 6.246 |
| 19 | 1.170 | 7 | 2.949 | 2.843 | 4 | 6.430 | 6.414 | 6.499 | 6.585 | 6.673 |
| 18 | 1.269 | 6 | 3.171 | 3.058 | $+5$ | 6.761 | 6.85 I | 6.94 I | 7.033 | 7.125 |
| $\begin{aligned} & \text { Tem- } \\ & \text { pera- } \\ & \text { ture. } \end{aligned}$ | $0 \%$ | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| C. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. | Gram's. |
| $+6^{\circ}$ | 7.219 | 7.266 | 7.313 | 7.361 | 7.409 | 7.457 | 7.506 | 7.555 | 7.614 | 7.653 |
| 7 | 7.703 | 7.753 | 7.803 | 7.853 | 7.904 | 7.955 | 8.007 | 8.058 | 8.110 | 8.162 |
| 8 | 8.215 | 8.268 | 8.32 I | 8.374 | 8.428 | 8.482 | 8.536 | 8.591 | 8.646 | 8.701 |
| 9 | 8.757 | 8.813 | 8.869 | 8.926 | 8.982 | 9.039 | 9.097 | 9.155 | 9.213 | 9.27 I |
| 10 | 9.330 | 9.389 | 9.448 | 9.508 | 9.568 | 9.628 | 9.689 | 9.750 | 9.8II | 9.873 |
| 11 | 9.935 | 9.997 | 10.060 | 10. 123 | 10.186 | 10.250 | 10.314 | 10.378 | 10.443 | 10.508 |
| 12 | 10.574 | 10.640 | 10.706 | 10.773 | 10.840 | 10.907 | 10.975 | II. 043 | II.III | II.180 |
| 13 | II. 249 | 11.318 | II. 388 | II. 458 | II. 529 | 11.600 | 11.672 | II. 744 | II.816 | II. 888 |
| 14 | II.96I | 12.035 | 12.108 | 12.182 | 12.257 | 12.332 | 12.407 | 12.483 | 12.559 | 12.635 |
| 15 | 12.712 | 12.790 | 12.867 | 12.945 | 13.024 | 13.103 | 13.182 | 13.262 | 13.342 | 13.423 |
| 16 | 13.505 | I3.586 | 13.668 | 13.750 | 13.833 | 13.916 | 14.000 | 14.085 | 14.169 | 14.254 |
| 17 | 14.339 | 14.425 | 14.51I | 14.598 | 14.685 | 14.773 | 14.86 I | 14.950 | 15.039 | I5.128 |
| 18 | 15.218 | 15.308 | 15.399 | 15.491 | 15.583 | 15.675 | 15.768 | 15.86 I | 15.955 | 16.049 |
| 19 | 16.144 | 16.239 | 16.335 | 16.43 I | 16.528 | 16.625 | 16.723 | 16.821 | 16.920 | 17.019 |
| 20 | I7.118 | 17.218 | 17.319 | 17.420 | 17.522 | 17.624 | 17.727 | 17.830 | 17.934 | 18.039 |
| 21 | 18.143 | 18.248 | 18.353 | 18.460 | 18.568 | 18.676 | 18.784 | 18.893 | 19.002 | 19. 111 |
| 22 | 19.222 | 19.332 | 19.444 | 19.556 | 19.668 | 19.78I | 19.895 | 20.009 | 20.124 | 20.239 |
| 23 | 20.355 | 20.471 | 20.588 | 20.706 | 20.824 | 20.943 | 21.062 | 21.182 | 21.303 | 21.424 |
| 24 | 21.546 | 21.668 | 21.791 | 21.914 | 22.038 | 22.163 | 22.287 | 22.414 | 22.541 | 22.668 |
| 25 | 22.796 | 22.925 | 23.054 | 23.184 | 23.314 | 23.445 | 23.577 | 23.709 | 23.842 | 23.975 |
| 26 | 24.109 | 24.244 | 24.380 | 24.516 | 24.653 | 24.790 | 24.928 | 25.067 | 25.207 | 25.347 |
| 27 | 25.487 | 25.629 | 25.771 | 25.914 | 26.058 | 26.202 | 26.347 | 26.492 | 26.639 | 26.786 |
| 28 | 26.933 | 27.082 | 27.231 | 27.38I | 27.53I | 27.682 | 27.834 | 27.988 | 28.142 | 28.295 |
| 29 | 28.450 | 28.605 | 28.762 | 28.919 | 29.077 | 29.235 | 29.394 | 29.555 | 29.715 | 29.877 |
| 30 | 30.039 | 30.202 | 30.366 | 30.530 | 30.696 | 30.862 | 31.029 | 31.197 | 31.365 | 31.534 |
| 31 | 31.704 | 3 I .875 | 32.047 | 32.219 | 32.392 | 32.567 | 32.74 I | 32.917 | 33.094 | 33.27 I |
| 32 | 33.449 | 33.628 | 33.807 | 33.988 | 34.169 | 34.351 | 34.534 | 34.718 | 34.903 | 35.089 |
| 33 | 35.275 | 35.462 | 35.651 | 35.840 | 36.030 | 36.220 | 36.412 | 36.604 | 36.798 | 36.992 |
| 34 | 37.187 | 37.383 | 37.580 | 37.777 | 37.976 | 38.176 | 38.376 | 38.577 | 38.780 | 38.983 |
| 35 | 39.187 | 39.390 | 39.598 | 39.805 | 40.012 | 40.221 | 40.43I | 40.64I | 40.853 | 41.065 |
| 36 | 41.279 | 4 I .493 | 4 I .708 | 4 I .924 | 42.142 | 42.360 | 42.579 | 42.799 | 43.020 | 43.242 |
| 37 | 43.465 | 43.690 | 43.914 | 44.140 | 44.367 | 44.596 | 44.825 | 45.054 | 45.286 | 45.518 |
| 38 | 45.75 I | 45.985 | 46.220 | 46.456 | 46.693 | 46.931 | 47.171 | 47.41 I | 47.653 | 47.895 |
| 39 | 48.138 | 48.385 | 48.628 | 48.875 | 49.123 | 49.372 | 49.621 | 49.872 | 50.124 | 50.377 |

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

ENGLISH MEASURES.
Pressure of Aqueous Vapor.

| Temperature. | $0^{\circ}$ | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7{ }^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \mathrm{F} . \\ -30^{\circ} \end{array}$ | $\begin{aligned} & \text { Inch. } \\ & 0.007 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & \text { 0.006 } \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.006 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.006 \end{aligned}$ | Inch. 0.005 | Inch. $0.005$ | $\begin{aligned} & \text { Inch. } \\ & 0.005 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & 0.005 \end{aligned}$ | Inch. <br> 0.004 | $\begin{aligned} & \text { Inch. } \\ & 0.004 \end{aligned}$ |
| - 20 | . 013 | . 012 | . OII | . OII | . 010 | . 0009 | . 009 | . 0008 | 0.004 .008 | . 0.007 |
| 10 | . 022 | . 021 | . 020 | . 019 | . 018 | . 017 | . 016 | . 015 | . 014 | . 013 |
| - 0 | . 038 | . 036 | . 034 | . 033 | .O3I | . 029 | . 027 | . 026 | . 025 | . 023 |
| + 0 | 0.038 | 0.0 | 0.042 | 0.044 | 0.047 | 0.049 | 0.052 |  | 0.057 | 0.060 |
|  | . 063 | . 066 | . 070 | . 074 | . 077 | .08I | . 085 | . 089 | . 093 | . 098 |
| 20 | . 103 | . 108 | . I I3 | . 118 | . 124 | . 130 | . 136 | . 143 | . 150 | . 157 |
| Temperature. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch | Inch. | Inch. | Inch. | Inch. |
| $+30^{\circ}$ | O. 164 | 0.165 | -. 166 | 0.166 | 0.167 | 0. 168 | O. 169 | 0.169 | 0.170 | 0.171 |
| 31 | . 172 | . 173 | . 173 | . 174 | . 175 | . 176 | . 177 | . 177 | . 178 | . 179 |
| 32 | . 180 | . 18 I | .181 | . 182 | . 183 | . 184 | . 184 | . 185 | . 186 | . 186 |
| 33 | . 187 | . 188 | . 189 | . 190 | . 190 | .191 | . 192 | . 193 | . 193 | . 194 |
| 34 | . 195 | . 196 | . 196 | . 197 | . 198 | . 199 | . 200 | . 200 | . 201 | . 202 |
| 35 | 0.203 | 0.204 | 0.204 | 0.205 | 0.206 | 0.207 | 0.208 | 0.208 | 0.209 | 0.210 |
| 36 | . 211 | . 212 | . 213 | . 213 | . 214 | . 215 | . 216 | . 217 | . 218 | . 219 |
| 37 | . 219 | . 220 | . 221 | . 222 | . 223 | . 224 | . 225 | . 225 | . 226 | . 227 |
| 38 | . 228 | . 229 | . 230 | . 23 I | . 232 | . 233 | . 233 | . 234 | . 235 | . 236 |
| 39 | . 237 | .238 | . 239 | . 240 | . 241 | . 242 | . 243 | . 244 | . 245 | . 246 |
| 40 | 0.247 | 0.247 | 0.248 | 0.249 | 0.250 | 0.25I | 0.252 | 0.253 | 0.254 | 0.255 |
| 41 | . 256 | . 257 | . 258 | . 259 | . 260 | . 261 | . 262 | . 263 | . 264 | . 265 |
| 42 | . 266 | . 267 | . 268 | . 269 | . 270 | . 271 | . 272 | . 273 | . 274 | . 276 |
| 43 | . 277 | . 278 | . 279 | . 280 | .28I | . 282 | . 283 | . 284 | .285 | . 286 |
| 44 | . 287 | . 288 | . 289 | . 291 | . 292 | . 293 | . 294 | . 295 | . 296 | . 297 |
| 45 | 0.298 | 0.300 | 0.301 | 0.302 | 0.303 | 0.304 | 0.305 | 0. 306 | 0.308 | 0.309 |
| 46 | .310 | .311 | . 312 | . 313 | . 315 | . 316 | -317 | -318 | -319 | . 32 I |
| 47 | . 322 | . 323 | . 324 | . 325 | . 327 | . 328 | . 329 | - 330 | . 332 | . 333 |
| 48 | . 334 | . 335 | . 337 | -338 | . 339 | -340 | . 342 | . 343 | -344 | . 345 |
| 49 | - 347 | . 348 | . 349 | .35I | . 352 | -353 | . 355 | . 356 | -357 | -358 |
| 50 | 0.360 | 0.361 | 0.362 | 0.364 | 0.365 | 0.367 | 0.368 | 0.369 | 0.371 | 0.372 |
| 51 | . 373 | . 375 | . 376 | . 377 | . 379 | . 380 | . 382 | . 383 | . 384 | . 386 |
| 52 | . 387 | . 389 | . 390 | . 392 | . 393 | . 394 | -396 | - 397 | -399 | . 400 |
| 53 | . 402 | . 403 | . 405 | . 406 | . 408 | . 409 | .4II | .412 | . 414 | .415 |
| 54 | .417 | .418 | . 420 | . 42 I | . 423 | . 424 | . 426 | . 427 | . 429 | . 43 I |
|  | 0.432 | 0.434 | 0.435 | 0.437 | 0.438 | 0.440 | 0.442 | 0.443 | 0.445 | 0.446 |
| 56 | . 448 | . 450 | . 451 | . 453 | . 455 | . 456 | . 458 | . 460 | . 461 | . 463 |
| 57 | . 465 | . 466 | . 468 | . 470 | . 471 | . 473 | . 475 | . 476 | . 478 | . 480 |
| 58 | . 482 | . 483 | . 485 | . 487 | . 488 | . 490 | .492 | . 494 | .495 | . 497 |
| 59 | . 499 | . 501 | . 503 | . 504 | . 506 | . 508 | . 510 | . 512 | . 513 | . 515 |
| 60 | 0.517 | 0.519 | 0.52 I | 0.523 | 0.524 | 0.526 | 0.528 | 0.530 | 0.532 | 0.534 |
| 61 | . 536 | . 538 | . 539 | . 541 | . 543 | . 545 | . 547 | . 549 | .55I | . 553 |
| 62 | . 555 | . 557 | . 559 | . 561 | . 563 | . 565 | . 567 | . 569 | . 571 | . 573 |
| 63 | . 575 | . 577 | . 579 | .58I | . 583 | . 585 | . 587 | . 589 | .591 | . 593 |
| 64 | . 595 | . 597 | . 599 | . 601 | . 604 | . 606 | . 608 | . 610 | . 612 | . 614 |
| 65 | 0.616 | 0.6I8 | 0.621 | 0.623 | 0.625 | 0.627 | 0.629 | 0.631 | 0.634 | 0.636 |
| 66 | . 638 | . 640 | . 643 | . 645 | . 647 | . 649 | .65I | . 654 | . 656 | .658 |
| 67 | . 66 I | . 663 | . 665 | . 667 | . 670 | . 672 | . 674 | . 677 | . 679 | .681 |
| 68 | . 684 | . 686 | . 688 | . 691 | . 693 | . 695 | . 698 | . 700 | . 703 | .705 |
| 69 | . 707 | . 710 | .712 | .715 | . 717 | . 720 | .722 | .725 | . 727 | . 729 |

TABLE 40.
REDUCTION-OF PSYCHROMETRIC OBSERVATIONS.
ENGLISH MEASURES.
Pressure of Aqueous Vapor.

| Temperature. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | $0: 9$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| $70^{\circ}$ | 0.732 | 0.734 | 0.737 | 0.739 | 0.742 | 0.744 | 0.747 | 0.750 | 0.752 | 0.755 |
| 71 | 0.757 | 0.760 | 0.762 | 0.765 | 0.768 | 0.770 | 0.773 | 0.775 | 0.778 | 0.78 I |
| 72 | 0.783 | 0.786 | 0.789 | 0.791 | 0.794 | 0.797 | 0.799 | 0.802 | 0.805 | 0.807 |
| 73 | 0.810 | 0.813 | 0.816 | 0.818 | 0.821 | 0.824 | 0.827 | 0.830 | 0.832 | 0.835 |
| 74 | 0.838 | 0.84I | 0.843 | 0.846 | 0.849 | 0.852 | 0.855 | 0.858 | 0.86I | 0.863 |
| 75 | 0.866 | 0.869 | 0.872 | 0.875 | 0.878 | 0.881 | 0.884 | 0.887 | 0.890 | 0.893 |
| 76 | 0.896 | 0.899 | 0.902 | 0.905 | 0.908 | 0.911 | 0.914 | 0.917 | 0.920 | 0.923 |
| 77 | 0.926 | 0.929 | 0.932 | 0.935 | 0.938 | 0.941 | 0.944 | 0.948 | 0.951 | 0.954 |
| 78 | 0.957 | 0.960 | 0.963 | 0.966 | 0.970 | 0.973 | 0.976 | 0.979 | 0.982 | 0.986 |
| 79 | 0.989 | 0.992 | 0.995 | 0.999 | 1.002 | 1.005 | 1.009 | 1.012 | 1.015 | 1.019 |
| 80 | 1.022 | 1.025 | 1.029 | 1.032 | 1.035 | 1.039 | 1.042 | 1.046 | 1.049 | 1.052 |
| 81 | 1.056 | 1.059 | 1.063 | 1.066 | 1.070 | 1.073 | 1.077 | 1.080 | 1.084 | 1.087 |
| 82 | 1.09I | 1.094 | I. 098 | I. IOI | 1.105 | 1.109 | I. II 2 | 1.116 | 1.119 | 1.123 |
| 83 | 1.127 | I.130 | I. 134 | 1.138 | 1.14 I | I. 145 | 1. 149 | I.I52 | I. 156 | I. 160 |
| 84 | 1.163 | I. 167 | 1.171 | 1.175 | 1.179 | 1.182 | I. 186 | 1.190 | I. 194 | 1. 198 |
| 85 | 1.201 | 1.205 | I. 209 | 1.213 | 1.217 | 1.22I | $1.225^{\circ}$ | 1.229 | 1.233 | 1.237 |
| 86 | 1.241 | 1. 245 | 1.248 | 1.253 | I. 256 | 1.260 | 1.264 | 1.269 | 1.273 | 1.277 |
| 87 | 1.28I | 1. 285 | I. 289 | 1.293 | 1.297 | 1.301 | 1.305 | 1.310 | I. 314 | 1.318 |
| 88 | 1.322 | I. 326 | 1.330 | 1.335 | I. 339 | 1.343 | 1. 347 | 1.352 | r. 356 | 1.360 |
| 89 | 1.364 | 1.369 | I. 373 | 1.377 | 1.382 | I. 386 | I. 390 | 1.395 | 1.399 | I. 404 |
| 90 | 1. 408 | 1.413 | 1.417 | 1.42I | 1.426 | 1.430 | 1.435 | I. 439 | 1.444 | 1. 448 |
| 91 | 1. 453 | 1. 458 | I. 462 | r. 467 | 1.47I | I. 476 | I. 480 | 1. 485 | I. 490 | 1. 494 |
| 92 | 1.499 | 1. 504 | I. 508 | 1.513 | 1.518 | 1.523 | 1.527 | 1.532 | 1.537 | 1.542 |
| 93 | 1.546 | 1.551 | I. 556 | 1.56I | 1.566 | 1.57 I | 1.576 | 1.580 | 1.585 | 1.590 |
| 94 | 1.595 | 1.600 | 1.605 | 1.610 | 1.6I5 | 1.620 | 1.625 | 1.630 | 1.635 | 1.640 |
| 95 | 1. 645 | 1.650 | 1. 655 | 1.660 | r. 665 | r.671 | 1.676 | r.68ı | 1.686 | 1.691 |
| 96 | 1.696 | 1.702 | r. 707 | 1.712 | 1.717 | 1.723 | I. 728 | 1.733 | 1.738 | 1.744 |
| 97 | 1.749 | 1. 755 | 1.760 | 1.765 | 1.771 | 1.776 | 1.781 | 1. 787 | 1.792 | 1.798 |
| 98 | 1.803 | 1.809 | 1.814 | 1.820 | 1.825 | 1.831 | 1.837 | 1.842 | 1. 848 | 1. 853 |
| 99 | 1.859 | 1. 865 | 1.870 | 1.876 | r. 882 | I. 887 | 1.893 | 1. 899 | 1.905 | 1.910 |
| 100 | 1.916 | 1.922 | 1. 928 | 1.934 | 1.939 | 1.945 | 1.951 | 1.957 | 1.963 | 1.969 |
| IOI | 1.975 | I.98I | 1.987 | 1.993 | 1.999 | 2.005 | 2.011 | 2.017 | 2.023 | 2.029 |
| 102 | 2.035 | 2.041 | 2.047 | 2.053 | 2.059 | 2.066 | 2.072 | 2.078 | 2.084 | 2.090 |
| 103 | 2.097 | 2.103 | 2.109 | 2.116 | 2.122 | 2.128 | 2.134 | 2.141 | 2.147 | 2. 154 |
| 104 | 2.160 | 2. 166 | 2.173 | 2.179 | 2.186 | 2.192 | 2. 199 | 2.205 | 2.212 | 2.219 |
| 105 | 2.225 | 2.232 | 2.238 | 2.245 | 2.252 | 2.258 | 2.265 | 2.272 | 2.278 | 2.285 |
| 106 | 2.292 | 2.299 | 2.305 | 2.312 | 2.319 | 2.326 | 2.333 | 2.340 | 2.346 | 2.353 |
| 107 | 2.360 | 2.367 | 2.374 | 2.381 | 2.388 | 2.395 | 2.402 | 2.409 | 2.416 | 2.423 |
| 108 | 2.431 | 2.438 | 2.445 | 2.452 | 2.459 | 2.466 | 2.474 | 2.48 I | 2.488 | 2.495 |
| 109 | 2.503 | 2.510 | 2.517 | 2.525 | 2.532 | 2.539 | 2.547 | 2.554 | 2.562 | 2.569 |
| 110 | 2.576 | 2.584 | 2.591 | 2.599 | 2.607 | 2.614 | 2.622 | 2.629 | 2.637 | 2.645 |
| III | 2.652 | 2.660 | 2.668 | 2.675 | 2.683 | 2.691 | 2.699 | 2.706 | 2.714 | 2.722 |
| 112 | 2.730 | 2.738 | 2.746 | 2.754 | 2.762 | 2.770 | 2.777 | 2.785 | 2.793 | 2.801 |
| II3 | 2.810 | 2.818 | 2.826 | 2.834 | 2.842 | 2.850 | 2.858 | 2.866 | 2.875 | 2.883 |
| 114 | 2.89 I | 2.899 | 2.908 | 2.916 | 2.924 | 2.933 | 2.941 | 2.950 | 2.958 | 2.966 |
| 115 | 2.975 | 2.983 | 2.992 | 3.000 | 3.009 | 3.017 | 3.026 | 3.035 | 3.043 | 3.052 |
| 116 | 3.061 | 3.069 | 3.078 | 3.087 | 3.095 | 3.104 | 3.113 | 3.122 | 3.131 | 3.140 |
| 117 | 3.148 | 3.157 | 3.166 | 3.175 | 3.184 | 3.193 | 3.202 | 3.211 | 3.220 | 3.229 |
| II8 | 3.239 | 3.248 | 3.257 | 3.266 | 3.275 | 3.284 | 3.294 | 3.303 | 3.312 | $3 \cdot 321$ |
| 119 | 3.33 I | $3 \cdot 340$ | 3.349 | 3.359 | 3.368 | 3.378 | 3.387 | 3.397 | 3.406 | 3.416 |

Smithsonian Tables.

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

## ENGLISH MEASURES.

Values of $0.000367 \mathrm{~B}\left(t-t_{1}\right)\left(1+\frac{t-t_{1}}{1571}\right)$. $B=$ Barometric pressure.
$t=$ Temperature of the dry-bulb thermometer.
$t_{1}=$ Temperature of the wet-bulb thermometer.

| $t-t_{1}$ | barometric pressure in inches ( $B$ ). |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 30.5 | 30.0 | 29.5 | 29.0 | 28.5 | 28.0 | 27.5 | 27:0 | 26.5 | 26.0 | 25.5 | 25.0 |
| F. | Inch. | Inch | Inch. | ch. | ch. | Inch. | Inch. | h. | Inch. | Inch. | In | In |
| $1{ }^{\circ}$ | 0.oIr | 0.011 | O.oIr | O.OII | 0.010 | 0.010 | o.oio | o.oio | o.oıo | o.oio | 0.009 | 0.009 |
| 2 | . 022 | . 022 | . 022 | . 021 | . 021 | . 021 | . 020 | . 020 | . 019 | . 019 | .or9 | .or8 |
| 3 | . 034 | . 033 | . 033 | . 032 | . 031 | .031 | . 030 | . 030 | . 029 | . 029 | . 028 | . 027 |
| 4 | . 045 | . 044 | . 043 | . 043 | . 042 | . 041 | . 040 | . 040 | . 039 | . 038 | .038 | . 037 |
| 5 | 0.056 | 0.055 | 0.054 | 0.053 | 0.052 | 0.052 | 0.051 | 0.050 | 0.049 | 0.048 | 0.047 | 0.046 |
| 6 | . 067 | . 066 | . 065 | . 064 | . 063 | . 062 | .06I | . 060 | . 059 | . 057 | . 056 | . 055 |
| 7 | . 079 | . 077 | . 076 | . 075 | . 073 | . 072 | . 071 | . 070 | . 068 | . 067 | . 066 | . 064 |
| 8 | . 090 | . 088 | . 087 | . 086 | . 084 | . 083 | .081 | . 080 | . 078 | . 077 | . 075 | . 074 |
| 9 | . 101 | . 099 | . 098 | . 096 | . 095 | . 093 | . 091 | . 090 | . 088 | . 086 | . 085 | . 083 |
| 10 | 0.113 | O.III | 0.109 | 0. 107 | 0. 105 | o. 103 | 0.102 | 0. 100 | 0.098 | 0.096 | 0.094 | 0.092 |
| 11 | . 124 | . 122 | . 120 | . 118 | . 116 | .114 | . 112 | . 110 | . 108 | . 106 | . 104 | . 102 |
| 12 | . 135 | . 133 | . 131 | . 129 | . 126 | . 124 | . 122 | . 120 | . 118 | . 115 | . 113 | .iII |
| 13 | . 147 | . 144 | . 142 | . 140 | .137 | . 135 | .132 | . 130 | . 127 | . 125 | . 123 | . 120 |
| 14 | . 158 | . 156 | . 153 | . 150 | . 148 | . 145 | . 143 | . 140 | . 137 | . 135 | . 132 | . 130 |
| 15 | 0.170 | 0.167 | o. 164 | o.16I | 0. 158 | o. 156 | 0. 153 | 0. 150 | 0.147 | 0.144 | 0.142 | 0.139 |
| 16 | .181 | . 178 | . 175 | . 172 | .169 | . 166 | . 163 | . 160 | . 157 | . 154 | . 151 | . 148 |
| 17 | . 192 | . 189 | . 186 | . 183 | . 180 | . 177 | . 173 | . 170 | . 167 | . 164 | . 161 | .158 |
| 18 | . 204 | . 200 | . 197 | . 194 | . 190 | . 187 | . 184 | . 180 | . 177 | . 174 | . 170 | . 167 |
| 19 | . 215 | . 212 | . 208 | . 205 | . 201 | . 198 | . 194 | . 191 | . 187 | . 183 | . 180 | . 176 |
| 20 | 0.227 | 0.223 | 0.219 | 0.216 | 0.212 | 0.208 | 0.204 | 0.201 | 0. 197 | o. 193 | 0. 190 | 0. 186 |
| 21 | . 238 | . 234 | . 230 | . 226 | . 223 | . 219 | . 215 | 11 | . 207 | . 203 | . 199 | . 195 |
| 22 | . 250 | . 246 | . 242 | . 237 | . 233 | . 229 | . 225 | . 221 | . 217 | . 213 | . 209 | . 205 |
| 23 | . 261 | . 257 | . 253 | . 248 | . 244 | . 240 | . 236 | . 231 | . 227 | . 223 | . 218 | . 214 |
| 24 | . 273 | . 268 | . 264 | . 259 | . 255 | . 250 | . 246 | .241 | . 237 | . 233 | . 228 | . 224 |
| 25 | 0. 284 | 0.280 | 0. 275 | 0.270 | 0.266 | 0.261 | 0.256 | 0.252 | 0.247 | 0.242 | 0.238 | 0.233 |
| 26 | . 296 | . 291 | . 286 | . 281 | . 277 | . 272 | . 267 | . 262 | . 257 | . 252 | . 247 | . 243 |
| 27 | . 307 | . 302 | . 297 | . 292 | . 287 | . 282 | . 277 | . 272 | . 267 | . 262 | . 257 | . 252 |
| 28 | -319 | . 314 | . 309 | . 303 | . 298 | . 293 | . 288 | . 282 | . 277 | . 272 | . 267 | . 261 |
| 29 | -33I | . 325 | -320 | -314 | -309 | -304 | . 298 | . 293 | . 287 | . 282 | . 276 | . 271 |
| 30 | 0.342 | 0.337 | 0.331 | 0.325 | 0.320 | 0.314 | 0.309 | 0.303 | 0.297 | 0.292 | 0.286 | 0.281 |
| 31 | - 354 | - 348 | -342 | . 336 | .331 | - 325 | . 319 | . 313 | . 307 | - 302 | . 296 | . 290 |
| 32 | . 365 | - 359 | - 354 | -348 | -342 | - 336 | . 330 | - 324 | -318 | -312 | - 306 | . 300 |
| 33 | -377 | -371 | -365 | . 359 | -352 | - 346 | -340 | - 334 | -328 | -322 | . 315 | . 309 |
| 34 | -389 | . 382 | . 376 | - 370 | -363 | -357 | -351 | - 344 | -338 | .331 | . 325 | -319 |
| 35 | 0.401 | 0.394 | 0.387 | 0.381 | 0.374 | 0.368 | 0.361 | 0.355 | 0. 348 | 0.341 | 0.335 | 0.328 |
| 36 | . 412 | . 405 | . 399 | . 392 | . 385 | . 378 | . 372 | . 365 | . 358 | . 351 | . 345 | . 338 |
| 37 | . 424 | . 417 | . 410 | . 403 | - 396 | . 389 | . 382 | . 375 | - 368 | -361 | - 354 | - 347 |
| 38 | . 436 | . 428 | . 421 | . 414 | . 407 | . 400 | - 393 | . 386 | - 379 | -371 | - 364 | - 357 |
| 39 | . 447 | . 440 | . 433 | . 425 | . 418 | .4II | . 403 | - 396 | - 389 | -38I | - 374 | - 367 |
| 40 | 0.459 | 0.452 | 0.444 | 0.437 | 0.429 | 0.422 | 0.414 | 0.406 | 0.399 | 0.391 | 0.384 | 0.376 |

Table 41.

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

ENGLISH MEASURES.
Values of $0.000367 B\left(t-t_{1}\right)\left(1+\frac{t-t_{1}}{1571}\right)$.
$B=$ Barometric pressure.
$t=$ Temperature of the dry-bulb thermometer.
$t_{1}=$ Temperature of the wet-bulb thermometer.

| $t-t_{1}$ | BAROMETRIC PRESSURE IN INCHES ( $B$ ). |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.5 | 24.0 | 235 | 23.0 | 22.5 | 22.0 | 21.5 | 21.0 | 20.5 | 20.0 | 195 | 19:0 | 18.5 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| $1{ }^{\circ}$ | 0.009 | 0.009 | 0.009 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 | 0.007 | 0.007 | 0.007 | 0.007 |
| 2 | . 018 | . OI 8 | . 017 | . 017 | . 016 | . O 6 | . 016 | . 015 | . OL 5 | . OL 5 | . 014 | . 014 | . OI 4 |
| 3 | . 028 | . 026 | . 026 | . 025 | . 025 | . 024 | . 024 | . 023 | . 023 | . 022 | . 02 I | . 021 | . 020 |
| 4 | . 036 | . 035 | . 035 | . 034 | . 033 | . 032 | . 032 | .03I | . 030 | . 029 | . 029 | . 028 | . 027 |
| 5 | 0.045 | 0.044 | 0.043 | 0.042 | 0.041 | 0.040 | 0.040 | 0.039 | 0.038 | 0.037 | 0.036 | 0.035 | 0.034 |
| 6 | . 054 | . 053 | . 052 | .05I | . 050 | . 049 | . 048 | . 046 | . 045 | . 044 | . 043 | . 042 | . 041 |
| 7 | . 063 | . 062 | .06I | . 059 | . 058 | . 057 | . 055 | . 054 | . 053 | . 052 | . 050 | . 049 | . 048 |
| 8 | . 072 | . 071 | . 070 | . 068 | . 066 | . 065 | . 063 | . 062 | . 060 | . 059 | . 057 | . 056 | . 055 |
| 9 | .08I | . 080 | . 078 | . 076 | . 075 | . 073 | . 07 I | . 070 | . 068 | . 066 | . 064 | . 063 | .06I |
| 10 | 0.090 | 0.089 | 0.087 | 0.085 | 0.083 | 0.08I | 0.079 | 0.077 | 0.076 | 0.074 | 0.072 | 0.070 | 0.068 |
| 11 | . 100 | . 097 | . 095 | . 093 | . 091 | .089 | . 087 | . 085 | . 083 | .081 | . 079 | . 077 | . 075 |
| 12 | . 109 | . 106 | . 104 | . 102 | . 100 | . 097 | . 095 | . 093 | .091 | .089 | . 086 | . 084 | . 082 |
| 13 | . 118 | . 115 | .II3 | .110 | . 108 | . 106 | .103 | . 101 | . 098 | . 096 | . 093 | . 091 | . 089 |
| 14 | . 127 | . 124 | . 122 | . 119 | . 117 | .II4 | .III | . 109 | . 106 | . 104 | . 101 | . 098 | . 095 |
| 15 | 0.136 | 0. 133 | 0.131 | 0.128 | 0.125 | 0.122 | O.119 | O.II7 | O.II4 | O.III | 0.108 | o.105 | 0.102 |
| 16 | . 145 | . 142 | . 139 | . 136 | . 133 | . 130 | . 127 | . 124 | . 121 | .118 | . 116 | .II3 | . 110 |
| 17 | . 155 | .15I | . 148 | . 145 | . 142 | . 139 | . 135 | . 132 | . 129 | . 126 | . 123 | . 120 | .117 |
| I8 | . 164 | .160 | . 157 | . 154 | .151 | .I47 | .I43 | . 140 | . 137 | . 134 | . 130 | . 127 | . 124 |
| 19 | . 173 | .169 | . 166 | .162 | . 159 | . 155 | . 152 | . 148 | . 144 | .14I | . 137 | . 134 | .13I |
| 20 | 0.182 | 0.178 | 0.175 | 0.171 | 0.167 | 0.163 | 0.160 | 0.156 | 0.152 | 0.148 | 0.144 | 0.141 | 0.137 |
| 21 | .191 | .187 | .183 | . 180 | . 176 | . 172 | . 168 | .164 | . 160 | . 156 | . 152 | . 148 | . 144 |
| 22 | . 201 | . 196 | . 192 | . 188 | .184 | .180 | . 176 | . 172 | . 168 | .164 | . 160 | . 155 | . 151 |
| 23 | . 210 | . 205 | . 201 | . 197 | . 193 | . 188 | . 184 | . 180 | . 175 | .171 | . 167 | . 163 | . 158 |
| 24 | .219 | . 214 | . 210 | . 205 | . 201 | . 196 | . 192 | . 188 | .183 | . 179 | .174 | . 170 | . 165 |
| 25 | 0.228 | 0.223 | 0.219 | 0.2I4 | 0.210 | 0.205 | 0.200 | 0.196 | 0.19I | 0. 186 | 0.181 | 0.177 | 0.172 |
| 26 | . 238 | . 233 | . 228 | . 223 | . 218 | . 213 | . 208 | . 203 | . 199 | . 194 | . 189 | . 184 | . 179 |
| 27 | . 247 | . 242 | . 237 | . 232 | . 227 | . 222 | . 216 | . 211 | . 206 | . 201 | . 196 | .191 | . 186 |
| 28 | . 256 | .251 | . 245 | . 240 | . 235 | . 230 | . 225 | . 219 | . 214 | . 209 | . 203 | . 198 | . 193 |
| 29 | . 266 | . 260 | . 254 | . 249 | . 244 | . 238 | . 233 | . 227 | . 222 | . 216 | . 211 | . 206 | . 200 |
| 30 | 0.275 | 0.269 | 0.263 | 0.258 | 0.252 | 0.247 | 0.241 | 0.235 | 0.230 | 0.224 | 0.218 | 0.213 | 0.207 |
| 3 I | . 284 | . 278 | . 272 | . 267 | . 261 | . 255 | . 249 | . 243 | . 238 | . 232 | . 226 | . 220 | . 214 |
| 32 | . 294 | . 287 | . 281 | . 275 | . 269 | . 263 | . 257 | . 25 I | . 245 | . 239 | . 233 | . 227 | . 22 I |
| 33 | . 303 | . 296 | . 290 | . 284 | . 278 | . 272 | . 266 | . 259 | . 253 | . 247 | .241 | . 235 | . 229 |
| 34 | . 312 | . 306 | . 299 | . 293 | . 286 | . 280 | . 274 | . 267 | . 261 | . 255 | . 248 | . 242 | . 236 |
| 35 | 0.322 | 0.315 | 0.308 | 0.302 | 0.295 | 0.289 | 0.282 | 0.275 | 0.268 | 0.262 | 0.255 | 0.249 | 0.243 |
| 36 | . 331 | . 324 | . 317 | .311 | . 304 | . 297 | . 290 | . 284 | . 277 | . 270 | . 263 | . 257 | . 250 |
| 37 | .34I | . 333 | . 326 | -319 | . 312 | . 305 | . 299 | . 292 | . 285 | . 278 | . 271 | . 264 | . 257 |
| 38 | . 350 | - 342 | . 335 | -328 | . 321 | -314 | . 307 | . 300 | . 293 | . 285 | . 278 | . 271 | . 264 |
| 39 | -359 | . 352 | . 344 | -337 | . 330 | . 322 | . 315 | . 308 | .300 | . 293 | . 285 | . 278 | . 271 |
| 40 | 0.369 | 0.36I | 0.353 | 0.346 | 0.338 | 0.33I | 0.323 | 0.316 | 0.308 | 0.301 | 0.293 | 0.286 | 0.278 |

Smithsonian Tables.

RELATIVE HUMIDITY.
TEMPERATURES FAHRENHEIT.

| Air | DEPRESSION OF THE DEW-POINT ( $t-d$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $t$. | $0^{\circ}$ | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 4.5 | 5.0 | 5.5 | 6.0 | 6.5 | 7.0 | 7.5 |
| F. ${ }^{\text {F. }}$ | 100 | 97 | 94 | 92 | 89 |  |  |  |  |  |  |  |  |  |  |  |
| -28 | 100 | 97 | 94 | 92 | 89 | 86 | 83 | 8 I | 78 | 75 | 73 | 7 I | 69 | 67 | 65 | 63 |
| -24 | 100 | 97 | 94 | 92 | 89 | 87 | 84 | 8 I | 79 | 76 | 74 | 72 | 70 | 67 | 65 | 63 |
| -20 | 100 | 97 | 94 | 92 | 89 | 87 | 84 | 82 | 79 | 77 | 75 | 73 | 71 | 69 | 66 | 65 |
| -16 | 100 | 97 | 94 | 92 | 90 | 87 | 85 | 82 | 80 | 78 | 75 | 73 | 71 | 69 | 67 | 65 |
| -12 | 100 | 97 | 95 | 92 | 90 | 87 | 85 | 82 | 80 | 78 | 75 | 73 | 71 | 69 | 67 | 65 |
| -8 | 100 | 97 | 95 | 92 | 90 | 87 | 85 | 83 | 80 | 78 | 76 | 74 | 72 | 70 | 68 | 66 |
| -4 | 100 | 97 | 95 | 92 | 90 | 87 | 85 | 83 | 80 | 78 | 76 | 74 | 72 | 70 | 68 | 66 |
| 0 | 100 | 97 | 95 | 92 | 90 | 87 | 85 | 83 | 80 | 78 | 76 | 74 | 72 | 70 | 68 | 66 |
| + 4 | 100 | 98 | 95 | 93 | 90 | 88 | 86 | 84 | 82 | 80 | 78 | 76 | 74 | 71 | 70 | 68 |
| S | 100 | 98 | 95 | 93 | 90 | 88 | 86 | 84 | 82 | 80 | 78 | 76 | 74 | 72 | 71 | 69 |
| 12 | 100 | 98 | 95 | 93 | 90 | 88 | 86 | 84 | 82 | 80 | 78 | 76 | 74 | 72 | 71 | 69 |
| 16 | 100 | 98 | 95 | 93 | 91 | 89 | 86 | 84 | 82 | 80 | 78 | 76 | 74 | 72 | 71 | 69 |
| 20 | 100 | 98 | 95 | 93 | 91 | 89 | 87 | 85 | 83 | 81 | 79 | 77 | 75 | 73 | 72 | 70 |
| 24 | 100 | 98 | 95 | 93 | 91 | 89 | 87 | 85 | 83 | 81 | 79 | 77 | 75 | 73 | 72 | 70 |
| 28 | 100 | 98 | 95 | 93 | 91 | 89 | 87 | 85 | 83 | 81 | 79 | 77 | 76 | 74 | 72 | 70 |
| 32 | 100 | 98 | 96 | 94 | 92 | 90 | 87 | 85 | 83 | 81 | 79 | 78 | 76 | 74 | 72 | 71 |
| 36 | 100 | 98 | 96 | 94 | 92 | 91 | 89 | 87 | 85 | 83 | 81 | 80 | 78 | 76 | 74 | 73 |
| 40 | 100 | 98 | 96 | 94 | 93 | 91 | 89 | 87 | 86 | 84 | 82 | 8 I | 79 | 78 | 76 | 74 |
| 44 | 100 | 98 | 96 | 94 | 93 | 91 | 89 | 87 | 86 | 84 | 83 | 8 I | 79 | 78 | 76 | 75 |
| 48 | 100 | 98 | 96 | 95 | 93 | 91 | 89 | 88 | 86 | 84 | 83 | 81 | 80 | 78 | 77 | 75 |
| 52 | 100 | 98 | 96 | 95 | 93 | 91 | 89 | 88 | 86 | 85 | 83 | 82 | 80 | 79 | 77 | 76 |
| 56 | 100 | 98 | 96 | 95 | 93 | 91 | 90 | 88 | 86 | 85 | 83 | 82 | 80 | 79 | 77 | 76 |
| 60 | 100 | 98 | 97 | 95 | 93 | 91 | 90 | 88 | 87 | 85 | 84 | 82 | 8 I | 79 | 78 | 76 |
| 64 | 100 | 98 | 97 | 95 | 93 | 92 | 90 | 88 | 87 | 85 | 84 | 82 | 81 | 79 | 78 | 77 |
| 68 | 100 | 98 | 97 | 95 | 93 | 92 | 90 | 89 | 87 | 86 | 84 | 83 | 8I | 80 | 78 | 77 |
| 72 | 100 | 98 | 97 | 95 | 93 | 92 | 90 | 89 | 87 | 86 | 84 | 83 | 8 I | 80 | 79 | 77 |
| 76 | 100 | 98 | 97 | 95 | 94 | 92 | 90 | 89 | 87 | 86 | 85 | 83 | 82 | 80 | 79 | 77 |
| 80 | 100 | 98 | 97 | 95 | 94 | 92 | 9 I | 89 | 88 | 86 | 85 | 83 | 82 | 81 | 79 | 78 |
| 84 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 89 | 88 | 86 | 85 | 84 | 82 | 8 I | 80 | 78 |
| 88 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 89 | 88 | 87 | 85 | 84 | 83 | 8 I | 80 | 79 |
| 92 | 100 | 98 | 97 | 95 | 94 | 92 | 91 | 90 | 88 | 87 | 85 | 84 | 83 | 8 I | 80 | 79 |
| 96 | 100 | 98 | 97 | 95 | 94 | 93 | 91 | 90 | 88 | 87 | 86 | 84 | 83 | 82 | 80 | 79 |
| 100 | 100 | 99 | 97 | 96 | 94 | 93 | 91 | 90 | 89 | 87 | 86 | 85 | 83 | 82 | 8 I | 79 |
| 104 | 100 | 99 | 97 | 96 | 94 | 93 | 91 | 90 | 89 | 87 | 86 | 85 | 83 | 82 | 8 I | 80 |
| 108 | 100 | 99 | 97 | 96 | 94 | 93 | 92 | 90 | 89 | 88 | 86 | 85 | 84 | 82 | 81 | 80 |
| 112 | 100 | 99 | 97 | 96 | 94 | 93 | 92 | 90 | 89 | 88 | 86 | 85 | 84 | 83 | 82 | 80 |
| 116 | 100 | 99 | 97 | 96 | 94 | 93 | 92 | 90 | 89 | 88 | 87 | 85 | 84 | 83 | 82 | 8I |
| 120 | 100 | 99 | 97 | 96 | 95 | 93 | 92 | 91 | 89 | 88 | 87 | 86 | 84 | 83 | 82 | 81 |

## RELATIVE HUMIDITY.

TEMPERATURES FAHRENHEIT.

| Air Temperature. $t$. | DEPRESSION OF THE DEW-POINT ( $t-d$ ) . |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8.0 | 8.5 | 9.0 | 9.5 | 10.0 | 10.5 | 11.0 | 11.5 | 12.0 | 12.5 | 13.0 | 13.5 | 14.0 | 14.5 | 15.0 |
| F. ${ }^{\text {F }}$ - ${ }^{\circ}$ | 6I | 60 | 58 | 56 | 55 | 53 | 51 | 50 | 49 |  |  |  |  |  |  |
| -20 | 62 | 61 | 59 | 57 | 55 | 53 | 52 | 50 | 49 | 47 | 46 | 45 | 43 | 42 | 41 |
| -16 | 63 | 61 | 59 | 58 | 56 | 54 | 53 | 51 | 49 | 48 | 46 | 45 | 44 | 42 | 41 |
| -12 | 63 | 6I | 60 | 58 | 56 | 55 | 53 | 52 | 50 | 49 | 47 | 46 | 45 | 43 | 42 |
| -8 | 64 | 62 | 61 | 59 | 57 | 56 | 54 | 52 | 51 | 49 | 48 | 47 | 45 | 44 | 43 |
| - 4 | 65 | 63 | 6I | 60 | 58 | 56 | 55 | 53 | 52 | 50 | 49 | 47 | 46 | 45 | 43 |
| 0 | 65 | 63 | 6r | 60 | 58 | 57 | 55 | 53 | 52 | 51 | 49 | 48 | 47 | 45 | 44 |
| +4 | 66 | 64 | 62 | 61 | 59 | 57 | 56 | 54 | 52 | 51 | 50 | 49 | 48 | 46 | 45 |
| 8 | 67 | 65 | 64 | 62 | 60 | 59 | 57 | 55 | 54 | 52 | 51 | 50 | 48 | 47 | 46 |
| 12 | 67 | 65 | 64 | 62 | 61 | 59 | 58 | 56 | 55 | 53 | 52 | 51 | 49 | 48 | 47 |
| 16 | 67 | 65 | 64 | 62 | 61 | 60 | 58 | 56 | 55 | 54 | 52 | 51 | 50 | 49 | 47 |
| 20 | 68 | 66 | 65 | 63 | 61 | 60 | 58 | 57 | 56 | 54 | 53 | 51 | 50 | 49 | 48 |
| 24 | 68 | 67 | 65 | 64 | 62 | 61 | 59 | 58 | 56 | 55 | 54 | 52 | 5 I | 50 | 48 |
| 28. | 69 | 67 | 65 | 64 | 62 | 61 | 59 | 58 | 57 | 55 | 54 | 53 | 52 | 50 | 49 |
| 32 | 69 | 68 | 66 | 64 | 63 | 61 | 60 | 58 | 57 | 56 | 54 | 53 | 52 | 51 | 50 |
| 36 | 71 | 69 | 68 | 66 | 65 | 63 | 62 | 60 | 59 | 58 | 56 | 55 | 54 | 52 | 51 |
| 40 | 73 | 71 | 70 | 68 | 67 | 65 | 64 | 62 | 61 | 59 | 58 | 57 | 55 | 54 | 53 |
| 44 | 73 | 72 | 71 | 69 | 68 | 66 | 65 | 64 | 63 | 61 | 60 | 58 | 57 | 56 | 55 |
| 48 | 74 | 72 | 71 | 70 | 68 | 67 | 66 | 64 | 63 | 62 | 61 | 59 | 58 | 57 | 56 |
| 52 | 74 | 73 | 71 | 70 | 69 | 67 | 66 | 65 | 64 | 62 | 61 | 60 | 59 | 58 | 57 |
| 56 | 75 | 73 | 72 | 70 | 69 | 68 | 67 | 65 | 64 | 63 | 62 | 61 | 59 | 58 | 57 |
| 60 | 75 | 74 | 72 | 71 | 70 | 68 | 67 | 66 | 65 | 63 | 62 | 61 | 60 | 59 | 58 |
| 64 | 75 | 74 | 73 | 71 | 70 | 69 | 68 | 66 | 65 | 64 | 63 | 62 | 60 | 59 | 58 |
| 68 | 76 | 74 | 73 | 72 | 70 | 69 | 68 | 67 | 66 | 64 | 63 | 62 | 61 | 60 | 59 |
| 72 | 76 | 75 | 73 | 72 | 71 | 70 | 68 | 67 | 66 | 65 | 64 | 63 | 61 | 60 | 59 |
| 76 | 76 | 75 | 74 | 72 | 71 | 70 | 69 | 68 | 66 | 65 | 64 | 63 | 62 | 6I | 60 |
| 80 | 77 | 75 | 74 | 73 | 72 | 70 | 69 | 68 | 67 | 66 | 65 | 64 | 62 | 61 | 60 |
| 84 | 77 | 76 | 74 | 73 | 72 | 71 | 70 | 68 | 67 | 66 | 65 | 64 | 63 | 62 | 61 |
| 88 | 77 | 76 | 75 | 74 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 64 | 63 | 62 | 61 |
| 92 | 78 | 76 | 75 | 74 | 73 | 72 | 70 | 69 | 68 | 67 | 66 | 65 | 64 | 63 | 62 |
| 96 | 78 | 77 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 67 | 66 | 65 | 64 | 63 | 62 |
| 100 | 78 | 77 | 76 | 75 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 | 64 | 63 |
| 104 | 79 | 77 | 76 | 75 | 74 | 73 | 72 | 70 | 69 | 68 | 67 | 66 | 65 | 64 | 63 |
| 103 | 79 | 78 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 | 64 |
| 112 | 79 | 78 | 77 | 76 | 75 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 | 64 |
| 116 | 79 | 78 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 67 | 66 | 65 | 65 |
| 120 | 80 | 79 | 77 | 76 | 75 | 74 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 |

Smithbonian Tables.

## RELATIVE HUMIDITY.

TEMPERATURES FAHRENHEIT.

| $\begin{gathered} \text { Air } \\ \text { Temper- } \\ \text { ature. } \\ t . \end{gathered}$ | DEPRESSION OF THE DEW-POINT ( $t-d$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $15^{\circ}$ | $16^{\circ}$ | $17^{\circ}$ | $18^{\circ}$ | $19^{\circ}$ | $20^{\circ}$ | $21^{\circ}$ | $22^{\circ}$ | $23^{\circ}$ | $24^{\circ}$ | $25^{\circ}$ | $26^{\circ}$ | $27^{\circ}$ | $28^{\circ}$ | $29^{\circ}$ | $30^{\circ}$ |
| F. ${ }^{\text {F }}$ | 4I | 39 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - 16 | 41 | 39 | 36 | 34 | 32 | 3 I | 29 |  |  |  |  |  |  |  |  |  |
| - 12 | 42 | 39 | 37 | 35 | 33 | 3I | 29 | 27 | 26 | 24 | 23 | 22 | 2 I |  |  |  |
| - 8 | 43 | 40 | 38 | 36 | 34 | 32 | 30 | 28 | 26 | 25 | 23 | 22 | 21 | 20 | 19 | 18 |
| - 4 | 43 | 41 | 39 | 36 | 34 | 32 | 3 I | 29 | 27 | 25 | 24 | 23 | 21 | 20 | 19 | 18 |
| 0 | 44 | 42 | 39 | 37 | 35 | 33 | 31 | 29 | 28 | 26 | 25 | 23 | 22 | 2I | 19 | 18 |
| + 4 | 45 | 43 | 40 | 38 | 36 | 34 | 32 | 30 | 29 | 27 | 25 | 24 | 23 | 2I | 20 | 19 |
| 8 | 46 | 43 | 41 | 39 | 37 | 35 | 33 | 3 I | 30 | 28 | 26 | 25 | 23 | 22 | 21 | 20 |
| 12 | 47 | 44 | 42 | 39 | 37 | 35 | 34 | 32 | 30 | 28 | 27 | 25 | 24 | 23 | 21 | 20 |
| 16 | 47 | 45 | 43 | 40 | 38 | 36 | 34 | 32 | 3 I | 29 | 28 | 26 | 25 | 23 | 22 | 21 |
| 20 | 48 | 46 | 43 | 4 I | 39 | 37 | 35 | 33 | 32 | 30 | 28 | 27 | 25 | 24 | 23 | 22 |
| 24 | 48 | 46 | 44 | 42 | 40 | 38 | 36 | 34 | 32 | 31 | 29 | 28 | 26 | 25 | 23 | 22 |
| 28 | 49 | 47 | 44 | 42 | 40 | 38 | 36 | 34 | 33 | 31 | 30 | 28 | 27 | 26 | 24 | 23 |
| 32 | 50 | 47 | 45 | 43 | 4I | 39 | 37 | 35 | 33 | 32 | 30 | 29 | 27 | 26 | 25 | 24 |
| 36 | 51 | 49 | 46 | 44 | 42 | 40 | 38 | 37 | 35 | 33 | 32 | 30 | 28 | 27 | 26 | 25 |
| 40 | 53 | 50 | 48 | 46 | 44 | 42 | 40 | 38 | 36 | 34 | 33 | 3 I | 30 | 28 | 27 | 26 |
| 44 | 55 | 52 | 50 | 48 | 45 | 43 | 41 | 39 | 38 | 36 | 34 | 32 | 3I | 30 | 28 | 27 |
| 48 | 56 | 54 | 5 I | 49 | 47 | 45 | 43 | 41 | 39 | 37 | 35 | 34 | 32 | 31 | 29 | 28 |
| 52 | 57 | 54 | 52 | 50 | 48 | 46 | 44 | 42 | 4 1 | 39 | 37 | 35 | 34 | 32 | 31 | 29 |
| 56 | 57 | 55 | 53 | 5I | 49 | 47 | 45 | 43 | 42 | 40 | 38 | 37 | 35 | 33 | 32 | 30 |
| 60 | 58 | 56 | 54 | 51 | 50 | 48 | 46 | 44 | 42 | 41 | 39 | 38 | 36 | 35 | 33 | 32 |
| 64 | 58 | 56 | 54 | 52 | 50 | 48 | 46 | 45 | 43 | 4 I | 40 | 38 | 37 | 35 | 34 | 33 |
| 68 | 59 | 57 | 55 | 53 | 5I | 49 | 47 | 45 | 44 | 42 | 40 | 39 | 37 | 36 | 35 | 33 |
| 72 | 59 | 57 | 55 | 53 | 5I | 49 | 48 | 46 | 44 | 43 | 4 I | 40 | 38 | 37 | 35 | 34 |
| 76 | 60 | 58 | 56 | 54 | 52 | 50 | 48 | 47 | 45 | 43 | 42 | 40 | 39 | 37 | 36 | 35 |
| 80 | 60 | 58 | 56 | 54 | 52 | 5I | 49 | 47 | 45 | 44 | 42 | 41 | 39 | 38 | 37 | 35 |
| 84 | 6I | 59 | 57 | 55 | 53 | 51 | 49 | 48 | 46 | 44 | 43 | 4 I | 40 | 39 | 37 | 36 |
| 88 | 61 | 59 | 57 | 55 | 54 | 52 | 50 | 48 | 47 | 45 | 43 | 42 | 4I | 39 | 38 | 36 |
| 92 | 62 | 60 | 58 | 56 | 54 | 52 | 51 | 49 | 47 | 46 | 44 | 43 | 4 | 40 | 38 | 37 |
| 96 | 62 | 60 | 58 | 56 | 55 | 53 | 5I | 49 | 48 | 46 | 45 | 43 | 42 | 40 | 39 | 38 |
| 100 | 63 | 61 | 59 | 57 | 55 | 53 | 52 | 50 | 48 | 47 | 45 | 44 | 42 | 4 1 | 40 | 38 |
| 104 | 63 | 6I | 59 | 57 | 56 | 54 | 52 | 50 | 49 | 47 | 46 | 44 | 43 | 4I | 40 | 39 |
| 108 | 64 | 62 | 60 | 58 | 56 | 54 | 53 | 51 | 49 | 48 | 46 | 45 | 43 | 42 | 41 | 39 |
| 112 | 64 | 62 | 60 | 58 | 57 | 55 | 53 | 52 | 50 | 48 | 47 | 45 | 44 | 43 | 41 | 40 |
| 116 | 65 | 63 | 61 | 59 | 57 | 55 | 54 | 52 | 51 | 49 | 48 | 46 | 45 | 43 | 42 | 41 |
| 120 | 65 | 63 | 61 | 59 | 58 | 56 | 54 | 53 | 51 | 50 | 48 | 47 | 45 | 44 | 42 | 41 |

## RELATIVE HUMIDITY.

TEMPERATURES FAHRENHEIT.

| Air | DEPRESSION OF THE DEW-POINT $(t-d)$. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $t$. | $33^{\circ}$ | $36^{\circ}$ | $39^{\circ}$ | $42^{\circ}$ | $45^{\circ}$ | $48^{\circ}$ | $51^{\circ}$ | $54^{\circ}$ | $57^{\circ}$ | $60^{\circ}$ | $63^{\circ}$ | $66^{\circ}$ | $69^{\circ}$ | $72^{\circ}$ | $75^{\circ}$ |
| $\begin{gathered} F \\ -4 \end{gathered}$ | I5 | 13 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0 | I5 | 13 | II |  |  |  |  |  |  |  |  |  |  |  |  |
| +4 | 16 | 13 | II | 9 | 8 |  |  |  |  |  |  |  |  |  |  |
| 8 | 17 | 14 | II | IO | 8 | 7 |  |  |  |  |  |  |  |  |  |
| 12 | 17 | 14 | 12 | 10 | 8 | 7 | 6 |  |  |  |  |  |  |  |  |
| 16 | 18 | 15 | 12 | 10 | 9 | 7 | 6 | 5 | 4 |  |  |  |  |  |  |
| 20 | 18 | 15 | I3 | II | 9 | 8 | 6 | 5 | 4 | 4 |  |  |  |  |  |
| 24 | 19 | 16 | 14 | II | IO | 8 | 7 | 6 | 5 | 4 | 3 |  |  |  |  |
| 28 | 19 | 16 | 14 | 12 | 10 | 8 | 7 | 6 | 5 | 4 | 3 | 3 |  |  |  |
| 32 | 20 | 17 | 14 | 12 | 10 | 9 | 7 | 6 | 5 | 4 | 4 | 3 | 3 | 2 |  |
| 36 | 21 | I8 | 15 | 13 | II | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 3 | 2 | 2 |
| 40 | 22 | 19 | 16 | 14 | 12 | 10 | 9 | 7 | 6 | 5 | 4 | 4 | 3 | 2 | 2 |
| 44 | 23 | 20 | 17 | 15 | 13 | II | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 3 | 2 |
| 48 | 24 | 2 I | 18 | 15 | 13 | II | 10 | 8 | 7 | 6 | 5 | 4 | 4 | 3. | 2 |
| 52 | 25 | 22 | 19 | 16 | 14 | 12 | IO | 9 | 8 | 6 | 5 | 5 | 4 | 3 | 3 |
| 56 | 26 | 23 | 20 | 17 | 15 | 13 | II | 9 | 8 | 7 | 6 | 5 | 4 | 4 | 3 |
| 60 | 28 | 24 | 2 I | 18 | 16 | 13 | 12 | 10 | 9 | 7 | 6 | 5 | 5 | 4 | 3 |
| 64 | 29 | 25 | 22 | 19 | 16 | 14 | 12 | II | 9 | 8 | 7 | 6 | 5 | 4 | 4 |
| 68 | 30 | 26 | 23 | 20 | 17 | 15 | 13 | II | 10 | 8 | 7 | 6 | 5 | 5 | 4 |
| 72 | 30 | 27 | 24 | 2 I | 18 | 16 | 14 | 12 | 10 | 9 | 8 | 7 | 6 | 5 | 4 |
| 76 | 3 I | 28 | 24 | 22 | 19 | 17 | 15 | 13 | II | 9 | 8 | 7 | 6 | 5 | 4 |
| 80 | 3 I | 28 | 25 | 22 | 20 | 18 | 15 | 13 | 12 | 10 | 9 | 8 | 7 | 6 | 5 |
| 84 | 32 | 29 | 26 | 23 | 20 | 18 | 16 | 14 | 12 | II | 9 | 8 | 7 | 6 | 5 |
| 88 | 33 | 29 | 26 | 23 | 2 I | 19 | 17 | 15 | 13 | II | 10 | 9 | 8 | 7 | 6 |
| 92 | 33 | 30 | 27 | 24 | 2 I | 19 | 17 | 15 | 14 | 12 | 10 | 9 | 8 | 7 | 6 |
| 96 | 34 | 30 | 27 | 25 | 22 | 20 | 18 | 16 | 14 | 12 | II | 10 | 8 | 7 | 6 |
| 100 | 34 | 3 I | 28 | 25 | 23 | 20 | 18 | 16 | 14 | I3 | II | 10 | 9 | 8 | 7 |
| 104 | 35 | 32 | 29 | 26 | 23 | 2 I | 19 | 17 | 15 | 13 | 12 | II | 9 | 8 | 7 |
| 108 | 36 | 32 | 29 | 26 | 24 | 21 | 19 | 17 | I5 | 14 | 12 | II | 10 | 9 | 8 |
| 112 | 36 | 33 | 30 | 27 | 24 | 22 | 20 | 18 | 16 | 14 | 13 | II | 10 | 9 | 8 |
| 116 | 37 | 33 | 30 | 27 | 25 | 22 | 20 | 18 | 16 | 15 | 13 | 12 | II | 9 | 8 |
| 120 | 37 | 34 | 31 | 28 | 25 | 23 | 2 I | 19 | 17 | 15 | 14 | 12 | II | 10 | 9 |

Smithsonian Tables.

Pressure of Aqueous Vapor.
(Broch.)

| Temperature. | $0^{\circ}$ | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | mm. | mm. | mm . | mm . | mm . | mm. | mm . | min. | mm. | mm. |
| $-30^{\circ}$ | 0.38 | 0.35 | 0.32 | 0.29 | 0.26 | 0.23 | 0.21 | 0.19 | 0.17 | 0. 15 |
| 20 | 0.94 | 0.87 | 0.79 | 0.73 | 0.66 | 0.61 | 0.55 | 0.50 | 0.46 | 0.42 |
| 10 | 2. 15 | 1.99 | 1.84 | 1.69 | 1.56 | 1. 44 | 1.32 | 1.22 | I. 12 | 1.03 |
| o | 4.57 | 4.25 | 3.95 | 3.67 | 3.41 | 3.16 | 2.93 | 2.72 | 2.51 | 2.33 |
| Temperatu e. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| C. | mm. | mm. | mm. | mm. | mm. | mm . | mm. | mm . | mm. | mm. |
| $+0^{\circ}$ | 4.57 | 4.60 | 4.64 | 4.67 | $4.70$ | $4.74$ | $4.77$ | 4.80 | 4.84 | $4.87$ |
| I | 4.91 | 4.94 | 4.98 | 5.02 | 5.05 | 5.09 | 5.12 | 5.16 | 5.20 | 5.23 |
| 2 | 5.27 | $5 \cdot 31$ | $5 \cdot 35$ | $5 \cdot 39$ | 5.42 | 5.46 | 5.50 | 5.54 | 5.58 | 5.62 |
| 3 | 5.66 | 5.70 | 5.74 | 5.78 | 5.82 | 5.86 | 5.90 | 5.94 | 5.99 | 6.03 |
| 4 | 6.07 | 6.11 | 6.15 | 6.20 | 6.24 | 6.28 | 6.33 | 6.37 | 6.42 | 6.46 |
| 5 | 6.51 | 6.55 | 6.60 | 6.64 | 6.69 | 6.74 | 6.78 | 6.83 | 6.88 | 6.92 |
| 6 | 6.97 | 7.02 | 7.07 | 7.12 | 7.17 | 7.22 | 7.26 | 7.31 | 7.36 | 7.42 |
| 7 | 7.47 | 7.52 | 7.57 | 7.62 | 7.67 | 7.72 | 7.78 | 7.83 | 7.88 | 7.94 |
| 8 | 7.99 | 8.05 | 8.10 | 8.15 | 8.21 | 8.27 | 8.32 | 8.38 | 8.43 | 8.49 |
| 9 | 8.55 | 8.61 | 8.66 | 8.72 | 8.78 | 8.84 | 8.90 | 8.96 | 9.02 | 9.08 |
| 10 | 9.14 | 9.20 | 9.26 | 9.32 | 9.39 | 9.45 | 9.51 | 9.58 | 9.64 | 9.70 |
| II | 9.77 | 9.83 | 9.90 | 9.96 | 10.03 | 10.09 | 10.16 | 10.23 | 10.30 | 10.36 |
| 12 | 10.43 | 10.50 | 10.57 | 10.64 | 10.71 | 10.78 | 10.85 | 10.92 | 10.99 | 11.07 |
| 13 | II. 14 | II. 21 | 11.28 | 11.36 | 11.43 | 11.50 | 11.58 | 11.66 | 11.73 | II.81 |
| 14 | II. 88 | 11.96 | 12.04 | 12.12 | 12.19 | 12.27 | 12.35 | 12.43 | 12.51 | 12.59 |
| 15 | 12.67 | 12.76 | 12.84 | 12.92 | 13.00 | 13.09 | 13.17 | 13.25 | 13.34 | 13.42 |
| 16 | 13.51 | 13.60 | 13.68 | 13.77 | 13.86 | 13.95 | 14.04 | 14.12 | 14.21 | 14.30 |
| 17 | 14.40 | 14.49 | 14.58 | 14.67 | 14.76 | 14.86 | 14.95 | 15.04 | 15.14 | 15.23 |
| 18 | 15.33 | 15.43 | 15.52 | 15.62 | 15.72 | 15.82 | 15.92 | 16.02 | 16.12 | 16.22 |
| 19 | 16.32 | 16.42 | 16.52 | 16.63 | 16.73 | 16.83 | 16.94 | 17.04 | 17.15 | 17.26 |
| 20 | 17.36 | 17.47 | 17.58 | 17.69 | 17.80 | 17.91 | 18.02 | 18.13 | 18.24 | 18.35 |
| 21 | 18.47 | 18.58 | 18.69 | 18.81 | 18.92 | 19.04 | 19.16 | 19.27 | 19.39 | 19.51 |
| 22 | 19.63 | 19.75 | 19.87 | 19.99 | 20.11 | 20.24 | 20.36 | 20.48 | 20.61 | 20.73 |
| 23 | 20.86 | 20.98 | 21.11 | 2 I .24 | 21.37 | 21.50 | 21.63 | 21.76 | 21.89 | 22.02 |
| 24 | 22.15 | 22.29 | 22.42 | 22.55 | 22.69 | 22.83 | 22.96 | 23.10 | 23.24 | 23.38 |
| 25 | 23.52 | 23.66 | 23.80 | 23.94 | 24.08 | 24.23 | 24.37 | 24.52 | 24.66 | 24.8I |
| 26 | 24.96 | 25.10 | 25.25 | 25.40 | 25.55 | 25.70 | 25.86 | 26.01 | 26.16 | 26.32 |
| 27 | 26.47 | 26.63 | 26.78 | 26.94 | 27.10 | 27.26 | 27.42 | 27.58 | 27.74 | 27.90 |
| 28 | 28.07 | 28.23 | 28.39 | 28.56 | 28.73 | 28.89 | 29.06 | 29.23 | 29.40 | 29.57 |
| 29 | 29.74 | 29.92 | 30.09 | 30.26 | 30.44 | 30.62 | 30.79 | 30.97 | 31.15 | 31.33 |
| 30 | 31.51 | 31.69 | 31.87 | 32.06 | 32.24 | 32.43 | 32.61 | 32.80 | 32.99 | 33.18 |
| 31 | 33.37 | 33.56 | 33.75 | 33.94 | 34.14 | 34.33 | 34.53 | 34.72 | 34.92 | 35.12 |
| 32 | 35.32 | 35.52 | 35.72 | 35.92 | 36. I3 | 36.33 | 36.54 | 36.74 | 36.95 | 37.16 |
| 33 | 37.37 | 37.58 | 37.79 | 38.00 | 38.22 | 38.43 | 38.65 | 38.87 | 39.08 | 39.30 |
| 34 | 39.52 | 39.74 | 39.97 | 40.19 | 40.41 | 40.64 | 40.87 | 41.09 | 41.32 | 41.55 |
| 35 | 41.78 | 42.02 | 42.25 | 42.48 | 42.72 | 42.96 | 43. 19 | 43.43 | 43.67 |  |
| 36 | 44.16 | 44.40 | 44.65 | 44.89 | 45.14 | 45.39 | 45.64 | 45.89 | 46.14 | 46.39 |
| 37 | 46.65 | 46.90 | 47.16 | 47.42 | 47.68 | 47.94 | 48.20 | 48.46 | 48.73 | 48.99 |
| 38 | 49.26 | 49.53 | 49.80 52 | 50.07 | 50.34 | 50.61 | 50.89 | 51.16 | 51.44 | 51.72 54.57 |
| 39 | 52.00 | 52.28 | 52.56 | 52.84 | 53.13 | 53.41 | 53.70 | 53.99 | 54.28 | 54.57 |
| 40 | 54.87 | 55. 16 | 55.46 | 55.75 | 56.05 | 56.35 | 56.65 | 56.95 | 57.26 | 57.56 |
| 41 | 57.87 | 58.18 | 58.49 | 58.80 | 59.11 | 59.43 | 59.74 | 60.06 | 60.38 | 60.70 |
| 42 | 61.02 | 6 I .34 | 61.66 | 6 I .99 | 62.32 | 62.65 | 62.98 | 63.31 | 63.64 | 63.97 |
| 43 | 64.31 | 64.65 | 64.99 | 65.33 | 65.67 | 66.01 | 66.36 | 66.71 | 67.05 | 67.41 |
| 44 | 67.76 | 68. I I | 68.47 | 68.82 | 69.18 | 69.54 | 69.90 | 70.26 | 70.63 | 70.99 |
| 45 | 71.36 | 71.73 | 72.10 | 72.48 | 72.85 | 73.23 | 73.60 | 73.98 | 74.36 | 74.75 |

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

 METRIC MEASURES.
## Values of $0.000660 \mathrm{~B}\left(t-t_{1}\right)\left(1+\frac{t-t_{1}}{873}\right)$.

$t=$ Temperature of the dry-bulb thermometer.
$t_{1}=$ Temperature of the wet-bulb thermometer.

| $t-t_{1}$ | barometric pressure in millimetres ( $B$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 770 | 760 | 750 | 740 | 730 | 720 | 710 | 700 | 690 | 680 | 670 | 660 | 650 | 640 | 630 |
| c. | mm. | mm. | mm. | mm. | mm. | m | mi | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $1{ }^{\circ}$ | 0.52 | 0.51 | 0.50 | 0.50 | 0.49 | 0.48 | 0.48 | 0.47 | 0.46 | 0.46 | 0.45 | 0.44 | 0.44 | 0.43 | 0.42 |
| 2 | 1.03 | I. 1. | I.00 | 0.98 | 0.97 | 0.96 | 0.94 | 0.93 | 0.92 | 0.90 | 0. 89 | 0.88 | 0.87 | 0.85 | 0.84 |
| 3 | I. 54 | I. 52 | I. 49 | I. 47 | I. 45 | 1.43 | 1.41 | 1.39 | 1.37 | 1.35 | I. 33 | 1.32 | 1.30 | I. 28 | 1.26 |
| 4 | 2.04 | 2.02 | I. 99 | I. 97 | I. 94 | 1.91 | 1.89 | 1.86 | 1. 83 | 1.81 | 1.78 | 1.75 | 1.73 | 1.70 | 1.67 |
| 5 | 2.56 | 2.52 | 2.49 | 2.46 | 2.43 | 2.39 | 2.36 | 2.32 | 2.29 | 2.26 | 2.23 | 2.19 | 2.17 | 2.13 | 2.09 |
| 6 | 3.07 | 3.03 | 2.99 | 2.95 | 2.91 | 2.87 | 2.83 | 2.79 | 2.75 | 2.71 | 2.67 | 2.63 | 2.59 | 2.55 | 2.51 |
| 8 | 3.59 | 3.54 | 3.50 | 3.45 | 3.40 | 3.36 | 3.31 | 3.26 | 3.22 | 3.17 | 3.12 | 3.08 | 3.04 | 2.99 | 2.94 |
| 8 | 4.11 4.62 | 4.05 | 4.00 | 3.95 | 3.89 4.38 | 3.84 4.32 | 3.79 | 3.73 | 3.68 | 3.63 | 3.58 | 3.53 | 3.48 | 3.42 <br> 3.85 | 3.36 3.79 |
| 9 | 4.62 | 4.56 | 4.50 | 4.44 | 4.38 | 4.32 | 4.27 | 4.2 I | 4.15 | 4.09 | 4.03 | 3.97 | 3.91 | 3.85 | 3.79 |
| 10 | 5.15 | 5.08 | 5.OI | 4.94 | 4.88 | 4.8I | 4.74 | 4.68 | 4.61 | 4.54 | 4.47 | 4.41 | 4.35 | 4.28 | 4.21 |
| 11 | 5.66 | 5.59 | 5.51 | 5.44 | 5.37 | 5.30 | 5.22 | 5.15 | 5.08 | 5.00 | 4.93 | 4.86 | 4.79 | 4.71 | 4.63 |
| 12 | 6.19 | 6.11 | 6.02 | 5.94 | 5.86 | 5.78 | 5.70 | 5.62 | 5.54 | 5.46 | 5.38 | 5.30 | 5.22 | 5.14 | 5.06 |
| 13 | 6.71 | 6.62 | 6.53 | 6.45 | 6.36 | 6.27 | 6.18 | 6.10 | 6.01 | 5.92 | 5.83 | 5.75 | 5.66 | 5.57 | 5.49 |
| 14 | 7.23 | 7.14 | 7.05 | 6.95 | 6.86 | 6.76 | 6.67 | 6.58 | 6.48 | 6.39 | 6.29 | 6.20 | 6.1I | 6.01 | 5.92 |
| 15 | 7.76 | 7.66 | 7.56 | 7.46 | 7.36 | 7.26 | 7.16 | 7.06 | 6.95 | 6.85 | 6.75 | 6.65 | 6.55 | 6.45 | 6.35 |
| 16 | 8.29 | 8.18 | 8.07 | 7.96 | 7.86 | 7.75 | 7.64 | 7.54 | 7.43 | 7.32 | 7.21 | 7.11 | 7.00 | 6.89 | 6.78 |
| 17 | 8.82 | 8.70 | 8.59 | 8.47 | 8.36 | 8.24 | 8.13 | 8.02 | 7.90 | 7.79 | 7.67 | 7.56 | 7.45 | 7.33 | 7.21 |
| 18 | 9. | 9.22 | 9.10 | 8.98 | 8.86 | 8.74 | 8.62 | 8.50 | 8.37 | 8.25 | 8.13 | 8.01 | 7.89 | 7.77 | 7.65 |
| 19 | 9.87 | 9.75 | 9.62 | 9.49 | 9.36 | 9.23 | 9.11 | 8.98 | 8.85 | 8.72 | 8.59 | 8.47 | 8.34 | 8.21 | 8. |
| 20 |  | 10.2 | IO. 14 | 10.00 | 9.87 | 9.73 | 9.60 | 9.46 | 9.32 | 9.19 | 9.05 | 8.92 | 8.78 | 8.65 | 8.51 |
| $t-t_{1}$ | barometric pressure in millimetres ( $B$ ) . |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 620 | 610 | 600 | 590 | 580 | 570 | 560 | 550 | 540 | 530 | 520 | 510 | 500 | 490 | 480 |
|  | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | . | mm. |
| $1{ }^{\circ}$ | 0.42 | 0.41 | 0.40 | 0.40 | 0.39 | 0.38 | 0.38 | 0.37 | 0.36 | 0.36 | 0.35 | 0.34 | 0.34 | 0.33 | 0.32 |
| 2 | 0.82 | 0.81 | 0.80 | 0.78 | 0.77 | 0.76 | 0.75 | 0.73 | 0.72 | 0.70 | 0.69 | 0.68 | 0.67 | 0.65 | 0.64 |
|  | I. 24 | 1.22 | 1.20 | 1.17 | 1.15 | 1.13 | I.12 | I.10 | 1.08 | 1.06 | 1. 04 | 1.02 | 1.00 | 0.98 | 0:96 |
| 4 | 1. 65 | I. 62 | 1.60 | I. 57 | I. 54 | 1.51 | 1.49 | 1.46 | I. 44 | 1.41 | 1. 38 | 1.36 | 1.33 | 1.30 | 1.28 |
| 5 | 2.06 | 2.03 | I. 99 | I. 96 | I. 93 | 1.90 | 1.86 | 1. 83 | 1.80 | 1.76 | 1.73 | 1.70 | 1.66 | 1. 63 | 1.60 |
| 6 | 2.47 | 2.43 | 2.39 | 2.35 | 2.32 | 2.28 | 2.24 | 2.20 | 2.16 | 2.12 | 2.08 | 2.04 | 2.00 | 1.96 | 1.92 |
| 7 | 2.89 | 2.84 | 2.80 | 2.75 | 2.71 | 2.66 | 2.61 | 2.56 | 2.52 | 2.47 | 2.43 | 2.38 | 2.33 | 2.28 | 2.24 |
| 8 | 3.31 | 3.26 | 3.20 | 3.15 | 3.10 | 3.04 | 2.99 | 2.94 | 2.88 | 2.83 | 2.78 | 2.72 | 2.67 | 2.62 | 2.56 |
| 9 | 3.73 | 3.67 | 3.61 | 3.55 | 3.49 | 3.43 | 3.37 | 3.31 | 3.25 | 3.19 | 3.13 | 3.06 | 3.00 | 2.94 | 2.88 |
| 10 | 4.14 | 4.07 | 4.01 | 3.94 | 3.88 | 3.81 | 3.74 | 3.67 | 3.61 | 3.54 | 3.48 | 3.41 | 3.34 | 3.27 | 3.21 |
| 11 | 4.56 | 4.49 | 4.42 | 4.34 | 4.27 | 4.19 | 4.12 | 4.05 | 3.97 | 3.90 | 3.83 | 3.75 | 3.68 | 3.60 | 3.53 |
| 12 | 4.98 | 4.90 | 4.82 | 4.74 | 4.66 | 4.58 | 4.50 | 4.42 | 4.34 | 4.26 | 4.18 | 4.10 | 4.02 | 3.93 | 3.85 |
| 13 | 5.40 | 5.31 | 5.23 | 5.14 | 5.05 | 4.96 | 4.88 | 4.79 | 4.70 | 4.62 | 4.53 | 4.44 | 4.36 | 4.27 | 4.18 |
| 14 | 5.83 | 5.73 | 5.64 | 5.54 | 5.45 | 5.35 | 5.26 | 5.17 | 5.07 | 4.98 | 4.88 | 4. | 4.70 | 4.60 | 4.51 |
| 15 | 6.25 | 6.15 | 6.05 | 5.95 | 5.85 | 5.74 | 5.64 | 5.54 | 5.44 | $5 \cdot 34$ | 5.24 | 5.14 | 5.04 | 4.94 | 4.84 |
| 16 | 6.68 | 6.57 | 6.46 | 6.35 | 6.24 | 6.14 | 6.03 | 5.92 | 5.81 | 5.71 | 5.60 | 5.49 | 5.38 | 5.27 | 5.17 |
| 17 | 7.10 | 6.98 | 6.87 | 6.75 | 6.64 | 6.53 | 6.41 | 6.30 | 6.18 | 6.07 | 5.95 | 5.84 | 5.72 | 5.61 | 5.50 |
| 18 | 7.52 | 7.40 | 7.28 | 7.16 | 7.04 | 6.92 | 6.80 | 6.67 | 6.55 | 6.43 | 6.31 | 6.19 | 6.07 | 5.95 | 5.83 |
| 19 | 7.95 | 7.82 | 7.70 | 7.57 | 7.44 | 7.31 | 7.18 | 7.05 | 6.93 | 6.8 | 6.67 | 6.54 | 6.42 | 6.29 | 6.16 |
| 20 | 8.38 | 8.24 | 8.11 | 7.97 | 7.84 | 7.70 | 7.57 | 7.43 | 7.30 | 7.16 | 7.03 | 6.90 | 6.76 | 6.62 | 6.49 |

RELATIVE HUMIDITY.
TEMPERATURE CENTIGRADE.

| Depression of the dew-point. | DEW-POINT (d). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-15^{\circ}$ | $-10^{\circ}$ | $-5^{\circ}$ | $0^{\circ}$ | $+5^{\circ}$ | $+10^{\circ}$ | $+15^{\circ}$ | $+20^{\circ}$ | $+25^{\circ}$ | $+30^{\circ}$ |
| $\begin{gathered} c . \\ 0.0 \end{gathered}$ | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| 0.2 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 99 | 99 | 99 |
| 0.4 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 98 | 98 | 98 |
| 0.6 | 95 | 95 | 96 | 96 | 96 | 96 | 96 | 96 | 97 | 97 |
| o. 8 | 94 | 94 | 94 | 94 | 95 | 95 | 95 | 95 | 95 | 96 |
| 1.0 | 92 | 92 | 93 | 93 | 93 | 94 | 94 | 94 | 94 | 94 |
| r. 2 | 91 | 91 | 91 | 92 | 92 | 92 | 93 | 93 | 93 | 93 |
| 1. 4 | 89 | 90 | 90 | 90 | 91 | 91 | 91 | 92 | 92 | 92 |
| I. 6 | 88 | 88 | 89 | 89 | 90 | 90 | 90 | 91 | 91 | 91 |
| r. 8 | 86 | 87 | 87 | 88 | 88 | 89 | 89 | 90 | 90 | 90 |
| 2.0 | 85 | 86 | 86 | 87 | 87 | 88 | 88 | 88 | 89 |  |
| 2.2 | 84 | 84 | 85 | 85 | 86 | 86 | 87 | 87 | 88 | 88 |
| 2.4 | 83 | 83 | 84 | 84 | 85 | 85 | 86 | 86 | 87 | 87 |
| 2.6 | 82 | 82 | 82 | 83 | 84 | 84 | 85 | 85 | 86 | 86 |
| 2.8 | 80 | 80 | 8 I | 82 | 83 | 83 | 84 | 84 | 85 | 85 |
| 3.0 | 78 | 79 | 80 | 81 | $8 \mathrm{8r}$ | 82 | 83 | 83 | 84 | 84 |
| 3.2 | 77 | 78 | 79 | 80 | 80 | 8 r | 82 | 82 | 83 | 83 |
| 3.4 | 76 | 77 | 78 | 79 | 79 | 80 | $8 \mathrm{8I}$ | $8 \mathrm{8r}$ | 82 | 82 |
| 3.6 | 75 | 76 | 77 | 77 | 78 | 79 | 80 | 80 | 8 | 82 |
| 3.8 | 74 | 75 | 75 | 76 | 77 | 78 | 79 | 79 | So | 81 |
| 4.0 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 78 | 79 | 80 |
| 4.2 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 77 | 78 | 79 |
| 4.4 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 77 | 78 |
| 4.6 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 76 | 77 |
| 4.8 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 75 | 76 |
| 5.0 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 75 |
| 5.2 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 |
| 5.4 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 |
| 5.6 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 |
| 5.8 | 63 | 64 | 65 | 66 | 68 | 69 | 69 | 70 | 71 | 72 |
| 6.0 | 62 | 63 | 64 | 66 | 67 | 68 |  |  | 70 | 71 |
| 6.2 | 61 | 62 | 63 | 65 | 66 | 67 | 68 | 69 |  | 71 |
| 6.4 | 60 | 61 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 |
| 6.6 | 59 | 60 | 62 | 63 | 64 | 65 | 66 | 67 66 | 68 | 69 68 |
| 6.8 | 58 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 |
| 7.0 | 57 | 59 | 60 | 61 | 62 | 63 | 65 | 66 65 |  | 68 |
| 7.2 | 56 | 58 | 59 | 60 | 62 | 63 | 64 | 65 | 66 65 | 67 |
| 7.4 | 55 | 57 56 | 58 57 | 60 59 | 61 | 62 61 | 63 62 | 64 63 | 65 64 | 65 |
| 7.8 | 54 | 55 | 57 | 58 | 59 | 60 | 62 | 63 | 64 | 65 |
| 8.0 | 53 | 54 | 56 | 57 | 58 | 60 | 6r | 62 | 63 | 64 |

TABLE 45.

RELATIVE HUMIDITY.
TEMPERATURE CENTIGRADE.

| Depression of the dew-point.$t-d$ | DEW-POINT (d). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-15^{\circ}$ | $-10^{\circ}$ | $-5^{\circ}$ | $0^{\circ}$ | $+5^{\circ}$ | $+10^{\circ}$ | $+15^{\circ}$ | $+20^{\circ}$ | $+25^{\circ}$ | $+30^{\circ}$ |
| c. |  |  |  |  |  |  |  |  |  |  |
| 8.0 | 53 | 54 | 56 | 57 | 58 | 60 | 61 | 62 | 63 | 64 |
| 8.2 | 52 | 54 | 55 | 56 | 57 | 59 | 60 | 6 I | 62 | 63 |
| 8.4 | 51 | 53 | 54 | 56 | 57 | 58 | 59 | 60 | 62 | 63 |
| 8.6 | 51 | 52 | 54 | 55 | 56 | 57 | 58 | 60 | 61 | 62 |
| 8.8 | 50 | 51 | 53 | 54 | 55 | 57 | 58 | 59 | 60 | 6I |
| 9.0 | 49 | 51 | 52 | 53 | 55 | 56 | 57 | 58 | 60 | 61 |
| 9.2 | 48 | 50 | 51 | 53 | 54 | 55 | 57 | 58 | 59 | 60 |
| 9.4 | 48 | 49 | 5 I | 52 | 53 | 55 | 56 | 57 | 58 | 59 |
| 9.6 | 47 | 48 | 50 | 51 | 53 | 54 | 55 | 56 | 58 | 59 |
| 9.8 | 46 | 48 | 49 | 51 | 52 | 53 | 55 | 56 | 57 | 58 |
| 10.0 | 46 | 47 | 49 | 50 | 5 I | 53 | 54 | 55 | 56 | 57 |
| 10.5 | 44 | 45 | 47 | 48 | 50 | 51 | 52 | 54 | 55 |  |
| 11.0 | 42 | 44 | 45 | 47 | 48 | 49 | 51 | 52 | 53 |  |
| 11.5 | 41 | 42 | 44 | 45 | 47 | 48 | 49 | 51 | 52 |  |
| 12.0 | 39 | 41 | 42 | 44 | 45 | 47 | 48 | 49 | 50 |  |
| 12.5 | 38 | 39 | 4 I | 42 | 44 | 45 | 46 | 48 | 49 |  |
| 13.0 | 36 | 38 | 40 | 41 | 43 | 44 | 45 | 46 | 48 |  |
| 13.5 | 35 | 37 | 38 | 40 | 42 | 43 | 44 | 45 | 46 |  |
| 14.0 | 34 | 35 | 37 | 38 | 40 | 41 | 43 | 44 | 45 |  |
| 14.5 | 33 | 34 | 36 | 37 | 39 | 40 | 41 | 43 | 44 |  |
| 15.0 | 3 I | 33 | 35 | 36 | 37 | 39 | 40 | 42 |  |  |
| 15.5 | 30 | 32 | 33 | 35 | 36 | 38 | 39 | 40 |  |  |
| 16.0 | 29 | 31 | 32 | 34 | 35 | 37 | 38 | 39 |  |  |
| 16.5 | 28 | 30 | 31 | 33 | 34 | 36 | 37 | 38 |  | , |
| 17.0 | 27 | 29 | 30 | 32 | 33 | 35 | 36 | 37 |  |  |
| 17.5 | 26 | 28 | 29 | 31 | 32 | 34 | 35 | 36 |  |  |
| 18.0 | 25 | 27 | 28 | 30 | 31 | 33 | 34 | 35 |  |  |
| 18.5 | 25 | 26 | 27 | 29 | 30 | 32 | 33 | 34 |  |  |
| 19.0 | 24 | 25 | 27 | 28 | 29 | 3 I | 32 | 33 |  |  |
| 19.5 | 23 | 24 | 26 | 27 | 29 | 30 | 3 I | 33 |  |  |
| 20.0 | 22 | 24 | 25 | 26 | 28 | 29 | 30 | 32 |  |  |
| 21.0 | 21 | 22 | 23 | 25 | 26 | 27 | 29 |  |  |  |
| 22.0 | 19 | 21 | 22 | 23 | 25 | 26 | 27 |  |  |  |
| 23.0 | 18 | 19 | 21 | 22 | 23 | 24 | 26 |  |  |  |
| 24.0 | 17 | 18 | 19 | 21 | 22 | 23 | 24 |  |  |  |
| 25.0 | 16 | I7 | 18 | 19 | 21 | 22 | 23 |  |  |  |
| 26.0 | 15 | 16 | 17 | 18 | 20 | 21 |  |  |  |  |
| 27.0 | 14 | 15 | 16 | 17 | 18 | 20 |  |  |  |  |
| 28.0 | 13 | 14 | 15 | 16 | 17 | 19 |  |  |  |  |
| 29.0 | 12 | 13 | 14 | 15 | 16 | 18 |  |  |  |  |
| 30.0 | II | 12 | I3 | 14 | 16 | 17 |  |  |  |  |

Smithbonian Tables.

REDUCTION OF SNOWFALL MEASUREMENTS.
Depth of water corresponding to the weight of snow (or rain) collected in an 8 -inch gage.

| Weight of Snow. | $\begin{gathered} 0 z \\ 0 \end{gathered}$ | $\begin{gathered} 0 z . \\ \frac{1}{4} \end{gathered}$ | $\begin{gathered} \text { Oz. } \\ \frac{1}{2} \end{gathered}$ | $\begin{gathered} 0 z \\ \frac{3}{4} \end{gathered}$ | $\begin{gathered} \text { Weight } \\ \text { of } \\ \text { nnow. } \end{gathered}$ | $\begin{gathered} 0 z . \\ 0 \end{gathered}$ | $\begin{gathered} 0 z \\ \frac{1}{4} \end{gathered}$ | $\begin{gathered} 0 z . \\ \frac{1}{2} \end{gathered}$ | $\begin{gathered} \mathrm{Oz} . \\ \frac{3}{4} \end{gathered}$ | $\begin{aligned} & \text { Weight } \\ & \text { of } \\ & \text { Snow. } \end{aligned}$ | $\begin{gathered} 0 z . \\ 0 \end{gathered}$ | $\begin{gathered} 0 z . \\ \frac{1}{4} \end{gathered}$ | $\begin{gathered} 0 z \\ \frac{1}{2} \end{gathered}$ | 02 $\frac{3}{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lb.Oz. | Inch. | Inch. | Inch. | Inch. | Lb.Oz. | Inch's | Inch's | Inch's | Inch's | Lb.Oz. | Inch's | Inch's | Inch's | Inch's |
| 0 | 0.00 | 0.01 | 0.02 | 0.03 | 18 | 0.83 | 0.83 | 0.84 | 0.85 | 213 | I. 55 | 1.56 | 1.57 | I. 57 |
| 1 | . 03 | . 04 | . 05 | . 06 | I 9 | . 86 | . 87 | . 88 | . 89 | 214 | 1.58 | 1.59 | 1.60 | 1.61 |
| 2 | . 07 | . 08 | . 09 | . 09 | 110 | . 89 | . 90 | . 91 | . 92 | 215 | I. 62 | I'63 | 1. 63 | I. 64 |
| 3 | . 10 | . 11 | . 12 | . 13 | I II | . 93 | . 94 | . 94 | . 95 |  |  |  |  |  |
| 4 | . 14 | . 15 | . 15 | . 16 | 1 I 2 | . 96 | . 97 | . 98 | . 99 |  |  |  |  |  |
| 5 | 0.17 | 0.18 | 0.19 | 0.20 | 113 | 1.00 | I.OI | 1.01 | 1.02 | 30 | 1. 65 | 1.66 | 1.67 | 1.68 |
| 6 | . 21 | . 22 | . 22 | . 23 | 114 | 1.03 | 1.04 | 1.05 | 1.06 | 3 I | 1.69 | 1.69 | 1.70 | 1.71 |
| 7 | . 24 | . 25 | . 26 | . 27 | I 15 | 1.07 | 1.08 | 1.08 | 1.09 | 32 | 1.72 | 1.73 | 1.74 | 1.75 |
| 8 | . 28 | . 28 | . 29 | . 30 |  |  |  |  |  | 31 | 1.75 | 1.76 | 1.77 | 1.78 |
| 9 | .31 | . 32 | -33 | . 34 |  |  |  |  |  | 34 | 1.79 | 1.80 | I.8I | I.81 |
| 10 | 0.34 | 0.35 | 0.36 | 0.37 | 20 | 1.10 | I.II | 1.12 | 1.13 | 35 | 1.82 | 1.83 | I. 84 | 1. 85 |
| 11 | . 38 | . 39 | . 40 | . 41 | 2 I | I.14 | I. 14 | 1.15 | 1.16 | 36 | 1.86 | 1.87 | 1.87 | I. 88 |
| 12 | . 41 | . 42 | . 43 | . 44 | 22 | I. 17 | 1.18 | 1.19 | 1.20 | 37 | 1.89 | 1.90 | I.91 | 1.92 |
| 13 | . 45 | . 46 | . 46 | . 47 | 23 | 1.20 | I.21 | 1.22 | 1.23 | 38 | 1.93 | 1.94 | 1.94 | 1.95 |
| 14 | . 48 | . 49 | . 50 | . 51 | 24 | 1.24 | 1.25 | I. 26 | 1.26 | 39 | 1.96 | I. 97 | I. 98 | I. 99 |
| 15 | . 52 | . 52 | . 53 | . 54 |  |  |  |  |  |  |  |  |  |  |
| 10 | 0.55 | 0.56 | 0.57 | 0.58 | 25 | 1.27 | 1. 28 | 1.29 | 1.30 | 310 | 2.00 | 2.00 | 2.01 | 2.02 |
| I I | . 58 | . 59 | . 60 | . 61 | 26 | 1.31 | 1.32 | 1.32 | 1.33 | 311 | 2.03 | 2.04 | 2.05 | 2.06 |
| I 2 | . 62 | . 63 | . 64 | . 65 |  | I. 34 | 1.35 | I. 36 | I. 37 | 312 | 2.06 | 2.07 | 2.08 | 2.09 |
| I 3 | . 65 | . 66 | . 67 | . 68 | 28 | I. 38 | 1.38 | 1.39 | I. 40 | 3 I 3 | 2.10 | 2.11 | 2.12 | 2.12 |
| I 4 | . 69 | . 70 | .71 | . 71 | 29 | I. 41 | 1.42 | 1.43 | I. 44 | 314 | 2.13 | 2.14 | 2.15 | 2.16 |
| 15 | 0.72 | 0.73 | 0.74 | 0.75 | 210 | 1.44 | 1.45 | 1.46 | 1.47 | 315 | 2.17 | 2.18 | 2.18 | 2.19 |
| I 6 | . 76 | . 77 | . 77 | . 78 | 2 II | 1.48 | I. 49 | 1.50 | 1.51 | 40 | 2.20 |  |  |  |
| I 7 | . 79 | . 80 | .8I | . 82 | 212 | I.5I | 1.52 | 1.53 | 1.54 | 50 | 2.75 |  |  |  |

TAble 47.
RATE OF DECREASE OF VAPOR PRESSURE WITH ALTITUDE.
(According to the empirical formula of Dr. J. Hann).

$$
\frac{f}{f_{0}}=10^{-\frac{h}{6517}}
$$

$f, f_{0}=$ Vapor pressures at an upper and a lower station respectively.
$h=$ Difference of altitude in metres.

| Difference of Altitude. |  | $\frac{f}{f_{0}}$ | Difference of Altitude. |  | $\frac{f}{f_{0}}$ | Difference of Altitude. |  | $\frac{f}{f_{0}}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| metres. | Feet. |  | metres. | Feet. |  | metres. | Feet. |  |
| 200 | 656 | 0.93 | 1800 | 5905 | 0.53 | 3400 | III55 | 0.30 |
| 400 | 1312 | . 87 | 2000 | 6562 | . 49 | 3600 | II8II | . 28 |
| 600 | 1968 | . 81 | 2200 | 7218 | . 46 | 3800 | 12467 | . 26 |
| 800 | 2625 | . 75 | 2400 | 7874 | . 43 | 4000 | 13123 | . 24 |
| 1000 | 3281 | 0.70 | 2600 | 8530 | 0.40 | 4500 | 14764 | 0.20 |
| I 200 | 3937 | . 65 | 2800 | 9186 | . 37 | 5000 | 16404 | . 17 |
| 1400 | 4593 | .6I | 3000 | 9842 | . 35 | 5500 | 18045 | . 14 |
| 1600 | 5249 | . 57 | 3200 | 10499 | .32 | 6000 | 19685 | .12 |

## WIND TABLES.

Mean direction of the wind by Lambert's formula -
Multiples of $\cos 45^{\circ}$; form and example of computation . Table 48
Values of the mean direction (a) or its complement ( $90-a$ ) ..... 49
Synoptic conversion of velocities ..... Table 50
Miles per hour into feet per second ..... 51
Feet per second into miles per hour ..... Table 52
Metres per second into miles per hour ..... 53
Miles per hour into metres per second ..... Table 54
Metres per second into kilometres per hour ..... Table 55
Kilometres per hour into metres per second ..... Table $5^{6}$
Beaufort wind scale and its conversion into velocity ..... Table 57

TABLE 48.
MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.

$$
\tan \alpha=\frac{E-W+(N E+S E-N W-S W) \cos 45^{\circ}}{N-S+(N E+N W-S E-S W) \cos 45^{\circ}}
$$

Multiples of $\cos 45^{\circ}$.

| Number. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.0 | 0.7 | 1. 4 | 2.1 | 2.8 | 3.5 | 4.2 | 4.9 | 5.7 | 6.4 |
| 10 | 7.1 | 7.8 | 8.5 | 9.2 | 9.9 | 10.6 | 11.3 | 12.0 | 12.7 | 13.4 |
| 20 | 14.1 | 14.8 | 15.6 | 16.3 | 17.0 | 17.7 | 18.4 | 19.1 | 19.8 | 20.5 |
| 30 | 21.2 | 21.9 | 22.6 | 23.3 | 24.0 | 24.7 | 25.5 | 26.2 | 26.9 | 27.6 |
| 40 | 28.3 | 29.0 | 29.7 | 30.4 | 31.1 | 31.8 | 32.5 | 33.2 | 33.9 | 34.6 |
| 50 | 35.4 | 36.1 | 36.8 | 37.5 | 38.2 | 38.9 | 39.6 | 40.3 | 41.0 | 41.7 |
| 60 | 42.4 | 43.1 | 43.8 | 44.5 | 45.3 | 46.0 | 46.7 | 47.4 | 48.1 | 48.8 |
| 70 | 49.5 | 50.2 | 50.9 | 51.6 | 52.3 | 53.0 | 53.7 | 54.4 | 55.2 | 55.9 |
| 80 | 56.6 | 57.3 | 58.0 | 58.7 | 59.4 | 60.1 | 60.8 | 6 I .5 | 62.2 | 62.9 |
| 90 | 63.6 | 64.3 | 65.1 | 65.8 | 66.5 | 67.2 | 67.9 | 68.6 | 69.3 | 70.0 |
| 100 | 70.7 | 71.4 | 72.1 | 72.8 | 73.5 | 74.2 | 75.0 | 75.7 | 76.4 | 77.1 |
| 110 | 77.8 | 78.5 | 79.2 | 79.9 | 80.6 | 81.3 | 82.0 | 82.7 | 83.4 | 84. ${ }^{\text {I }}$ |
| 120 | 84.9 | 85.6 | 86.3 | 87.0 | 87.7 | 88.4 | 89.I | 89.8 | 90.5 | 91.2 |
| 130 | 91.9 | 92.6 | 93.3 | 94.0 | 94.8 | 95.5 | 96.2 | 96.9 | 97.6 | 98.3 |
| 140 | 99.0 | 99.7 | 100.4 | IOI. 1 | 101. 8 | 102.5 | 103.2 | 103.9 | 104.7 | 105.4 |
| 150 | 106. 1 | 106.8 | 107.5 | 108.2 | 108.9 | 109.6 | IIO. 3 | III.O | 111.7 | I12.4 |
| 160 | II3.1 | II3.8 | II4.6 | 115.3 | 116.0 | I16.7 | II7.4 | II8. 1 | II8.8 | I19.5 |
| 170 | 120.2 | 120.9 | 121.6 | 122.3 | 123.0 | 123.7 | 124.5 | 125.2 | 125.9 | 126.6 |
| 180 | 127.3 | 128.0 | 128.7 | 129.4 | I30.1 | 130.8 | I31.5 | I32.2 | 132.9 | 133.6 |
| 190 | 134.4 | I35. 1 | 135.8 | 136.5 | 137.2 | 137.9 | I 38.6 | I 39.3 | 140.0 | 140.7 |
| 200 | 141.4 | 142.I | 142.8 | 143.5 | 144.2 | 145.0 | 145.7 | 146.4 | 147.1 | 147.8 |

Form for Computing the Numerator and Denominator.

$\alpha$ is the angle between the mean wind direction and the meridian.
The signs of the numerator $(n)$ and denominator $(d)$ determine the quadrant in which $\alpha$ lies.
When $n$ and $d$ are positive, $a$ lies between N and E :

$$
\begin{aligned}
& \frac{ \pm}{+}=N E \\
& \frac{ \pm}{-}=S E \\
& \frac{ \pm}{-}=S W
\end{aligned}
$$

When $n$ is negative and $d$ positive, a lies between N and $\mathrm{W}: \bar{\mp}=N W$.

TAble 49.
MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.
Values of the mean direction ( $\alpha$ ) or its complement ( $90^{\circ}-\alpha$ ).
$\alpha=\tan ^{-1} n / d$

| $n$ | DENOMINATOR OR NUMERATOR ( $d$ OR $n$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d. | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 |
| 1 | $6^{\circ}$ | $4^{\circ}$ | $3^{\circ}$ | $2{ }^{\circ}$ | $2^{\circ}$ | $2^{\circ}$ | $\mathrm{I}^{\circ}$ | $1{ }^{\circ}$ | $\mathrm{I}^{\circ}$ | $I^{\circ}$ | $\mathrm{I}^{\circ}$ | $\mathrm{I}^{\circ}$ | $\mathrm{I}^{\circ}$ | $1{ }^{\circ}$ | $\mathrm{I}^{\circ}$ | $1{ }^{\circ}$ | $\mathrm{I}^{\circ}$ | $\mathrm{I}^{\circ}$ | $\mathrm{I}^{\circ}$ |
| 2 | 11 | 8 | 6 | 5 | 4 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 1 |
| 3 | 17 | 11 | 9 | 7 | 6 | 5 | 4 | 4 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 4 | 22 | 15 | II | 9 | 8 | 7 | 6 | 5 | 5 | 4 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 2 | 2 |
| 5 | 27 | 18 | 14 | 11 | 9 | 8 | 7 | 6 | 6 | 5 | 5 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 3 |
| 6 | 31 | 22 | 17 | 13 | 11 | Io | 9 | 8 | 7 | 6 | 6 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 3 |
| 7 | 35 | 25 | 19 | 16 | 13 | II | 10 | 9 | 8 | 7 | 7 | 6 | 6 | 5 | 5 | 5 | 4 | 4 | 4 |
| 8 | 39 | 28 | 22 | 18 | 15 | 13 | II | 10 | 9 | 8 | 8 | 7 | 7 | 6 | 6 | 5 | 5 | 5 | 5 |
| 9 | 42 | 31 | 24 | 20 | 17 | 14 | 13 | II | 10 | 9 | 9 | 8 | 7 | 7 | 6 | 6 | 6 | 5 | 5 |
| 10 | 45 | 34 | 27 | 22 | 18 | 16 | 14 | I3 | II | 10 | 9 | 9 | 8 | 8 | 7 | 7 | 6 | 6 | 6 |
| 1 I |  | 36 | 29 | 24 | 20 | 17 | 15 | 14 | 12 | II | 10 | Io | 9 | 8 | 8 | 7 | 7 | 7 | 6 |
| 12 |  | 39 | 31 | 26 | 22 | 19 | 17 | 15 | 13 | 12 | II | Io | 10 | 9 | 9 | 8 | 8 | 7 | 7 |
| 13 |  | 41 | 33 | 27 | 23 | 20 | 18 | 16 | 15 | 13 | 12 | II | II | Io | 9 | 9 | 8 | 8 | 7 |
| 14 |  | 43 | 35 | 29 | 25 | 22 | 19 | 17 | 16 | 14 | I3 | 12 | II | II | 10 | 9 | 9 | 8 | 8 |
| 15 |  | 45 | 37 | 31 | 27 | 23 | 21 | 18 | 17 | 15 | 14 | 13 | 12 | 11 | II | 10 | 9 | 9 | 9 |
| 16 |  |  | 39 | 33 | 28 | 25 | 22 | 20 | 18 | 16 | 15 | 14 | 13 | 12 | II | 11 | 10 | 10 | 9 |
| 17 |  |  | 40 | 34 | 30 | 26 | 23 | 21 | 19 | 17 | 16 | 15 | 14 | 13 | 12 | II | 11 | 10 | 10 |
| 18 |  |  | 42 | 36 | 31 | 27 | 24 | 22 | 20 | 18 | 17 | 15 | 14 | I3 | 13 | 12 | 11 | 11 | ıo |
| 19 |  |  | 44 | 37 | 32 | 28 | 25 | 23 | 2I | 19 | 18 | 16 | 15 | 14 | 13 | 13 | 12 | II | II |
| 20 |  |  | 45 | 39 | 34 | 30 | 27 | 24 | 22 | 20 | 18 | 17 | 16 | 15 | 14 | 13 | 13 | 12 | II |
| 21 |  |  |  | 40 | 35 | 31 | 28 | 25 | 23 | 21 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 12 |
| 22 |  |  |  | 4 I | 36 | 32 | 29 | 26 | 24 | 22 | 20 | 19 | 17 | 16 | 15 | 15 | 14 | 13 | 12 |
| 23 |  |  |  | 43 | 37 | 33 | 30 | 27 | 25 | 23 | 21 | 19 | 18 | 17 | 16 | 15 | 14 | 14 | 13 |
| 24 |  |  |  | 44 | 39 | 34 | 31 | 28 | 26 | 24 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 |
| 25 |  |  |  | 45 | 40 | 36 | 32 | 29 | 27 | 24 | 23 | 21 | 20 | 18 | 17 | 16 | 16 | 15 | 14 |
| 26 |  |  |  |  | 4 I | 37 | 33 | 30 | 27 | 25 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 15 |
| 27 |  |  |  |  | 42 | 38 | 34 | 31 | 28 | 26 | 24 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 15 |
| 28 |  |  |  |  | 43 | 39 | 35 | 32 | 29 | 27 | 25 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | 16 |
| 29 |  |  |  |  | 44 | 40 | 36 | 33 | 30 | 28 | 26 | 24 | 23 | 2I | 20 | 19 | 18 | 17 | 16 |
| 30 |  |  |  |  | 45 | 41 | 37 | 34 | 31 | 29 | 27 | 25 | 23 | 22 | 21 | 19 | 18 | 18 | 17 |
| 3 I |  |  |  |  |  | 42 | 38 | 35 | 32 | 29 | 27 | 25 | 24 | 22 | 21 | 20 | 19 | 18 | 17 |
| 32 |  |  |  |  |  | 42 | 39 | 35 | 33 | 30 | 28 | 26 | 25 | 23 | 22 | 21 | 20 | 19 | 18 |
| 33 |  |  |  |  |  | 43 | 40 | 36 | 33 | 31 | 29 | 27 | 25 | 24 | 22 | 21 | 20 | 19 | 18 |
| 34 |  |  |  |  |  | 44 | 40 | 37 | 34 | 32 | 30 | 28 | 26 | 24 | 23 | 22 | 21 | 20 | 19 |
| 35 |  |  |  |  |  | 45 | 4 | 38 | 35 | 32 | 30 | 28 | 27 | 25 | 24 | 22 | 21 | 20 | 19 |
| 36 |  |  |  |  |  |  | 42 | 39 | 36 | 33 | 31 | 29 | 27 | 26 | 24 | 23 | 22 | 21 | 20 |
| 37 |  |  |  |  |  |  | 43 | 39 | 37 | 34 | 32 | 30 | 28 | 26 | 25 | 24 | 22 | 21 | 20 |
| 38 |  |  |  |  |  |  | 44 | 40 | 37 | 35 | 32 | 30 | 28 | 27 | 25 | 24 | 23 | 22 | 21 |
| 39 |  |  |  |  |  |  | 44 | 4 | 38 | 35 | 33 | 31 | 29 | 27 | 26 | 25 | 23 | 22 | 21 |
| 40 |  |  |  |  |  |  | 45 | 42 | 39 | 36 | 34 | 32 | 30 | 28 | 27 | 25 | 24 | 23 | 22 |
| 4 I |  |  |  |  |  |  |  | 42 | 39 | 37 | 34 | 32 | 30 | 29 | 27 | 26 | 24 | 23 | 22 |
| 42 |  |  |  |  |  |  |  | 43 | 40 | 37 | 35 | 33 | 31 | 29 | 28 | 26 | 25 | 24 | 23 |
| 43 |  |  |  |  |  |  |  | 44 | 4 I | 38 | 36 | 33 | 32 | 30 | 28 | 27 |  | 24 | 23 |
| 44 |  |  |  |  |  |  |  | 44 | 4 I | 39 | 36 | 34 | 32 | 30 | 29 | 27 | 26 | 25 | 24 |
| 45 |  |  |  |  |  |  |  | 45 | 42 | 39 | 37 | 35 | 33 | 31 | 29 | 28 | 27 |  | 24 |
| 46 |  |  |  |  |  |  |  |  | 43 | 40 | 37 | 35 | 33 | 32 | 30 | 28 | 27 | 26 | 25 |
| 47 |  |  |  |  |  |  |  |  | 43 | 41 | 38 | 36 | 34 | 32 | 30 | 29 | 28 | 26 | 25 |
| 48 |  |  |  |  |  |  |  |  | 44 | 4 4 | 39 | 36 | 34 | 33 | 31 <br> 31 | 29 | 28 | 27 | 26 |
| 50 |  |  |  |  |  |  |  |  | 45 | 42 | 40 | 38 | 36 | 34 | 32 | 30 | 29 | 28 | 27 |

TABLE 49.
MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.
Values of the mean direction ( $\alpha$ ) or its complement ( $90^{\circ}-\alpha$ ).

| $n$ or $d$. | DENOMINATOR OR NUMERATOR ( $d$ OR $\boldsymbol{n}$ ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 105 | 110 | 115 | 120 | 125 | 130 | 135 | 140 | 145 | 150 |
| 1 | $\mathrm{I}^{\circ}$ | $\mathrm{I}^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ |
| 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 3 | 2 | 2 | 1 | 1 | 1 | 1 | I | 1 | I | I |
| 4 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 5 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 6 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 |
| 7 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 8 | 4 | 4 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 3 |
| 9 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 3 |
| 10 | 5 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 4 |
| 11 | 6 | 6 | 5 | 5 | 5 | 5 | 5 | 4 | 4 | 4 |
| 12 | 7 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 5 | 5 |
| 13 | 7 | 7 | 6 | 6 | 6 | 6 | 6 | 5 | 5 | 5 |
| 14 | 8 | 7 | 7 | 7 | 6 | 6 | 6 | 6 |  |  |
| 15 | 8 | 8 | 7 | 7 | 7 | 7 | 6 | 6 | 6 | 6 |
| 16 | 9 | 8 | 8 | 8 | 7 | 7 | 7 | 7 | 6 | 6 |
| 17 | 9 | 9 | 8 | 8 | 8 | 7 | 7 | 7 | 7 | 6 |
| 18 | 10 | 9 | 9 | 9 | 8 | 8 | 8 | 7 | 7 | 7 |
| 19 | 10 | 10 | 9 | 9 | 9 | 8 | 8 | 8 | 7 | 7 |
| 20 | II | 10 | 10 | 9 | 9 | 9 | 8 | 8 | 8 | 8 |
| 21 | 11 | 11 | 10 | 10 | 10 | 9 | 9 | 9 | 8 | 8 |
| 22 | 12 | 11 | 11 | 10 | 10 | 10 | 9 | 9 | 9 | 8 |
| 23 | 12 | 12 | 11 | II | 10 | ı0 | 10 | 9 | 9 | 9 |
| 24 | 13 | 12 | 12 | II | II | 10 | 10 | 10 | 9 | 9 |
| 25 | 13 | 13 | 12 | 12 | II | II | 10 | ıо | 10 | 9 |
| 26 | 14 | 13 | 13 | 12 | 12 | II | 11 | 11 | 10 | 10 |
| 27 | 14 | 14 | 13 | 13 | 12 | 12 | 11 | II | II | 10 |
| 28 | 15 | 14 | 14 | 13 | 13 | 12 | 12 | II | II | II |
| 29 | 15 | 15 | 14 | 14 | 13 | 13 | 12 | 12 | II | II |
| 30 | 16 | 15 | 15 | 14 | 13 | 13 | 13 | 12 | 12 | 11 |
| 31 | 16 | 16 | 15 | 14 | 14 | 13 | 13 | 12 | 12 | 12 |
| 32 | 17 | 16 | 16 | 15 | 14 | 14 | 13 | 13 | 12 | 12 |
| 33 | 17 | 17 | 16 | 15 | 15 | 14 | 14 | 13 | 13 | 12 |
| 34 | 18 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 13 | 13 |
| 35 | 18 | 18 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 13 |
| 36 | 19 | 18 | 17 | 17 | 16 | 15 | 15 | 14 | 14 | 13 |
| 37 | 19 | 19 | 18 | 17 | 16 | 16 | 15 | 15 | 14 | 14 |
| 38 | 20 | 19 | 18 | 18 | 17 | 16 | 16 | 15 | 15 | 14 |
| 39 | 20 | 20 | 19 | 18 | 17 | 17 | 16 | 16 | 15 | 15 |
| 40 | 21 | 20 | 19 | 18 | 18 | 17 | 17 | 16 | 15 | 15 |
| 4 I | 21 | 20 | 20 | 19 | 18 | 18 | 17 | 16 | 16 | 15 |
| 42 | 22 | 21 | 20 | 19 | 19 | 18 | 17 | 17 | 16 | 16 |
| 43 | 22 | 21 | 21 | 20 | 19 | 18 | 18 | 17 | 17 | 16 |
| 44 | 23 | 22 | 21 | 20 | 19 | 19 | 18 | 17 | 17 | 16 |
| 45 | 23 | 22 | 21 | 21 | 20 |  | 18 | 18 | 17 |  |
| 46 | 24 | 23 | 22 | 21 | 20 | 19 | 19 | 18 | 18 | 17 |
| 47 | 24 | 23 | 22 | 21 | 21 | 20 | 19 | 19 | 18 | 17 |
| 48 | 25 | 24 | 23 | 22 | 21 | 20 | 20 | 19 | 18 | 18 |
| 49 | 25 | 24 | 23 | 22 | 21 | 21 | 20 | 19 | 19 | 18 |
| 50 | 25 | 24 | 23 | 23 | 22 | 21 | 20 | 20 | 19 | 18 |

MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.
Values of the mean direction ( $\alpha$ ) or its complement $\left(90^{\circ}-\alpha\right)$.

| $n$ or $d$. | DENOMINATOR OR NUMERATOR ( $d$ OR $n$ ). |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 155 | 160 | 165 | 170 | 175 | 180 | 185 | 190 | 195 | 200 |
| 1 | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ |
| 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 3 | 1 | 1 | I | I | I | 1 | 1 | 1 | 1 | 1 |
| 4 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | I | 1 | 1 |
| 5 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | 1 |
| 6 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 7 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 8 | 3 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 2 |
| 9 | 3 | 3 | 3 | 3 |  | 3 | 3 | 3 | 3 | 3 |
| 10 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 11 | 4 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 3 | 3 |
| 12 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 3 |
| 13 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 14 | 5 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 4 |
| 15 | 6 | 5 |  | 5 | 5 | 5 | 5 | 5 | 4 | 4 |
| 16 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| 17 | 6 | 6 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 5 |
| 18 | 7 | 7 | 6 | 6 | 6 | 6 | 6 | 6 | 5 | 5 |
| 19 | 7 | 7 | 7 | 6 | 6 | 6 | 6 | 6 | 6 | 5 |
| 20 |  | 7 | 7 | 7 | 7 | 6 | 6 | 6 | 6 | 6 |
| 21 | 8 | 7 | 7 | 7 | 7 | 7 | 6 | 6 | 6 | 6 |
| 22 | 8 | 8 | 8 | 7 | 7 | 7 | 7 | 7 | 6 | 6 |
| 23 | 8 | 8 | 8 | 8 | 7 | 7 | 7 | 7 | 7 | 7 |
| 24 | 9 | 9 | 8 | 8 | 8 | 8 | 7 | 7 | 7 | 7 |
| 25 | 9 | 9 | 9 | 8 | 8 | 8 | 8 |  |  | 7 |
| 26 | 10 | 9 | 9 | 9 | 8 | 8 | 8 | 8 | 8 | 7 |
| 27 | ${ }^{10}$ | 10 | 9 | 9 | 9 | 9 | 8 | 8 | 8 | 8 |
| 28 | 10 | 10 | 10 | 9 | 9 | 9 | 9 | 8 | 8 | 8 |
| 29 | 11 | 10 | ıо | 10 | 9 | 9 | 9 | 9 | 8 | 8 |
| 30 | II | II | 10 | 10 | 10 | 9 | 9 | 9 | 9 | 9 |
| 31 | 11 | II | 11 | ıо | ı0 | 10 | 10 | 9 | 9 | 9 |
| 32 | 12 | 11 | 11 | 11 | 10 | 10 | 10 | 10 | 9 | 9 |
| 33 | 12 | 12 | II | 11 | II | 10 | 10 | ıо | 10 | 9 |
| 34 | 12 | 12 | 12 | II | II | II | о | ıо | ıо | 10 |
| 35 | 13 | 12 | 12 | 12 | II | II | II | 10 | 10 | 10 |
| 36 | 13 | 13 | 12 | 12 | 12 | 11 | II | 11 | 10 | 10 |
| 37 | 13 | 13 | 13 | 12 | 12 | 12 | II | 11 | 11 | Io |
| 38 | 14 | 13 | 13 | 13 | 12 | 12 | 12 | 11 | 11 | 1 I |
| 39 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 12 | II | II |
| 40 | 14 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 12 | 11 |
| 4 I | 15 | 14 | 14 | 14 | 13 | 13 | 12 | 12 | 12 | 12 |
| 42 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 12 | 12 | 12 |
| 43 | 16 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 12 | 12 |
| 44 | 16 | 15 | 15 | 15 | 14 | 14 | 13 | 13 | 13 | 12 |
| 45 | 16 | 16 | 15 | 15 | 14 | 14 | 14 | 13 | 13 | 13 |
| 46 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 14 | 13 | 13 |
| 47 | 17 | 16 | 16 | 15 | 15 | 15 | 14 | 14 | 14 | 13 |
| 48 | 17 | 17 | 16 | 16 | 15 | 15 | 15 | 14 | 14 | 13 |
| 49 | 18 | 17 | 17 | 16 | 16 | 15 | 15 | 14 | 14 | 14 |
| 50 | 18 | 17 | 17 | 16 | 16 | 16 | 15 | 15 | 14 | 14 |

TABLE 49.
MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.
Values of the mean direction (a) or its complement ( $90^{\circ}-a$ ).

$$
\alpha=\tan ^{-1} \frac{n}{d} .
$$

|  | denominator or numerator ( $d$ OR $\boldsymbol{n}$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d. | 55 | 60 | 65 | 70 | 75 | 80 | 85 | 90 | 95 | 100 | 105 | 110 | 115 | 120 | 125 | 130 |
| 50 | $42^{\circ}$ | $40^{\circ}$ | $35^{\circ}$ | $36^{\circ}$ | $34^{\circ}$ | $32^{\circ}$ | $30^{\circ}$ | $29^{\circ}$ | $28^{\circ}$ | $27^{\circ}$ | $25^{\circ}$ | $24^{\circ}$ | $23^{\circ}$ | $23^{\circ}$ | $22^{\circ}$ | $21^{\circ}$ |
| 52 | 43 | 41 | 39 | 37 | 35 | 33 | 31 | 30 | 29 | 27 | 26 | 25 | 24 | 23 | 23 | 22 |
| 54 | 44 | 42 | 40 | 38 | 36 | 34 | 32 | 31 | 30 | 28 | 27 | 26 | 25 | 24 | 23 | 22 |
| 56 |  | 43 | 41 | 39 | 37 | 35 | 33 | 32 | 3 I | 29 | 28 | 27 | 26 | 25 | 24 | 23 |
| 58 |  | 44 | 42 | 40 | 38 | 36 | 34 | 33 | 31 | 30 | 29 | 28 | 27 | 26 | 25 | 24 |
| 60 |  | 45 | 43 | 41 | 39 | 37 | 35 | 34 | 32 | 31 | 30 | 29 | 28 | 27 | 26 | 25 |
| 62 |  |  | 44 | 42 | 40 | 38 | 36 | 35 | 33 | 32 | 31 | 29 | 28 | 27 | 26 | 25 |
| 64 |  |  | 45 | 42 | 40 | 39 | 37 | 35 | 34 | 33 | 31 | 30 | 29 | 28 | 27 | 26 |
| 66 |  |  |  | 43 | 4 I | 40 | 38 | 36 | 35 | 33 | 32 | 31 | 30 | 29 | 28 | 27 |
| 68 |  |  |  | 44 | 42 | 40 | 39 | 37 | 36 | 34 | 33 | 32 | 31 | 30 | 29 | 28 |
| 70 |  |  |  | 45 | 43 | 41 | 39 | 38 | 36 | 35 | 34 | 32 | 31 | 30 | 29 | 28 |
| 72 |  |  |  |  | 44 | 42 | 40 | 39 | 37 | 36 | 34 | 33 | 32 | 31 | 30 | 29 |
| 74 |  |  |  |  | 45 | 43 | 41 | 39 | 38 | 37 | 35 | 34 | 33 | 32 | 31 | 30 |
| 76 |  |  |  |  |  | 44 | 42 | 40 | 39 | 37 | 36 | 35 | 33 | 32 | 3 I | 30 |
| 78 |  |  |  |  |  | 44 | 43 | 41 | 39 | 38 | 37 | 35 | 34 | 33 | 32 | 3 I |
| 80 |  |  |  |  |  | 45 | 43 | 42 | 40 | 39 | 37 | 36 | 35 | 34 | 33 | 32 |
| 82 |  |  |  |  |  |  | 44 | 42 | 41 | 39 | 38 | 37 | 35 | 34 | 33 | 32 |
| 84 86 86 |  |  |  |  |  |  | 45 | 43 | 41 | 40 | 39 | 37 | 36 | 35 | 34 | 33 |
| 88 |  |  |  |  |  |  |  | 44 | 42 | 4 4 | 40 | 38 | 37 | 36 36 | 35 | 33 34 |
| 90 |  |  |  |  |  |  |  | 45 | 43 | 42 | 41 | 39 | 38 | 37 | 36 | 35 |
| 92 |  |  |  |  |  |  |  |  | 44 | 43 | 41 | 40 | 39 | 37 | 36 | 35 |
| 94 |  |  |  |  |  |  |  |  | 45 | 43 | 42 | 4 I | 39 | 38 | 37 | 36 |
| 988 |  |  |  |  |  |  |  |  |  | 44 | 42 | 4 4 | 40 | 39 39 | 38 | 36 37 |
| 100 |  |  |  |  |  |  |  |  |  | 45 | 44 | 42 | 41 | 40 | 39 |  |
| 102 |  |  |  |  |  |  |  |  |  |  | 44 | 43 | 42 | 40 | 39 | 38 |
| 104 |  |  |  |  |  |  |  |  |  |  | 45 | 43 | 42 | 41 | 40 | 39 |
| 106 |  |  |  |  |  |  |  |  |  |  |  | 44 | 43 | 4 4 | 4 4 | 39 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 110 |  |  |  |  |  |  |  |  |  |  |  | 45 | 44 | 43 | 41 | 40 |
| 112 |  |  |  |  |  |  |  |  |  |  |  |  | 44 | 43 | 42 | 4I |
| 114 |  |  |  |  |  |  |  |  |  |  |  |  | 45 | 44 | 42 | 4 4 |
| 118 |  |  |  |  |  |  |  |  |  |  |  |  |  | 45 | 43 | 42 |
| 120 |  |  |  |  |  |  |  |  |  |  |  |  |  | 45 | 44 |  |
| 122 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 44 | 43 |
| 124 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 45 | 44 |
| 126 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 44 |
| 128 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 45 |
| 130 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 45 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

MEAN DIRECTION OF THE WIND BY LAMBERT'S FORMULA.
Values of the mean direction ( $\alpha$ ) or its complement ( $90^{\circ}-\alpha$ ).

| $n$ <br> or <br> $d$. | DENOMINATOR OR NUMERATOR ( $d$ OR $\boldsymbol{n}$ ). |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 130 | 135 | 140 | 145 | 150 | 155 | 160 | 165 | 170 | 175 | 180 | 185 | 190 | 195 | 200 |
| 50 | $21^{\circ}$ | $20^{\circ}$ | $20^{\circ}$ | $19^{\circ}$ | $18^{\circ}$ | $18^{\circ}$ | $17^{\circ}$ | $17^{\circ}$ | $16^{\circ}$ | $16^{\circ}$ | $16^{\circ}$ | $15^{\circ}$ | $15^{\circ}$ | $14^{\circ}$ | $14^{\circ}$ |
| 52 | 22 | 21 | 20 | 20 | 19 | 19 | 18 | 17 | 17 | 17 | 16 | 16 | 15 | 15 | 15 |
| 54 | 22 | 22 | 2 I | 20 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 15 | 15 |
| 56 | 23 | 23 | 22 | 21 | 20 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 16 | 16 | 16 |
| 58 | 24 | 23 | 23 | 22 | 2 I | 21 | 20 | 19 | 19 | 18 | 18 | 17 | 17 | 17 | 16 |
| 60 | 25 | 24 | 23 | 22 | 22 | 21 | 2 I | 20 | 19 | 19 | 18 | 18 | 18 | 17 | 17 |
| 62 | 25 | 25 | 24 | 23 | 22 | 22 | 21 | 2 I | 20 | 20 | 19 | 19 | 18 | 18 | 17 |
| 64 | 26 | 25 | 25 | 24 | 23 | 22 | 22 | 2 I | 21 | 20 | 20 | 19 | 19 | 18 | 18 |
| 66 | 27 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 2 I | 21 | 20 | 20 | 19 | 19 | 18 |
| 68 | 28 | 27 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 21 | 20 | 20 | 19 | 19 |
| 70 | 28 | 27 | 27 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 21 | 20 | 20 | 19 |
| 72 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 2 I | 21 | 20 | 20 |
| 74 | 30 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 | 22 | 22 | 21 | 2 I | 20 |
| 76 | 30 | 29 | 28 | 28 | 27 | 26 | 25 | 25 | 24 | 23 | 23 | 22 | 22 | 21 | 21 |
| 78 | 3 I | 30 | 29 | 28 | 27 | 27 | 26 | 25 | 25 | 24 | 23 | 23 | 22 | 22 | 21 |
| 80 | 32 | 3 I | 30 | 29 | 28 | 27 | 27 | 26 | 25 | 25 | 24 | 23 | 23 | 22 | 22 |
| S2 | 32 | 31 | 30 | 29 | 29 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 | 23 | 22 |
| 84 | 33 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 | 23 |
| 86 | 33 | 32 | 32 | 3 I | 30 | 29 | 28 | 28 | 27 | 26 | 26 | 25 | 24 | 24 | 23 |
| 88 | 34 | 33 | 32 | 31 | 30 | 30 | 29 | 28 | 27 | 27 | 26 | 25 | 25 | 24 | 24 |
| 90 | 35 | 34 | 33 | 32 | 31 | 30 | 29 | 29 | 28 | 27 | 27 | 26 | 25 | 25 | 24 |
| 92 | 35 | 34 | 33 | 32 | 32 | 31 | 30 | 29 | 28 | 28 | 27 | 26 | 26 | 25 | 25 |
| 94 | 36 | 35 | 34 | 33 | 32 | 3 I | 30 | 30 | 29 | 28 | 28 | 27 | 26 | 26 | 25 |
| 96 | 36 | 35 | 34 | 34 | 33 | 32 | 31 | 30 | 29 | 29 | 28 | 27 | 27 | 26 | 26 |
| 98 | 37 | 36 | 35 | 34 | 33 | 32 | 3 I | 3 I | 30 | 29 | 29 | 28 | 27 | 27 | 26 |
| 100 | 38 | 37 | 36 | 35 | 34 | 33 | 32 | 3 I | 30 | 30 | 29 | 28 | 28 | 27 | 27 |
| 102 | 38 | 37 | 36 | 35 | 34 | 33 | 33 | 32 | 3 I | 30 | 30 | 29 | 28 | 28 | 27 |
| 104 | 39 | 38 | 37 | 36 | 35 | 34 | 33 | 32 | 3 I | 3 I | 30 | 29 | 29 | 28 | 27 |
| 106 | 39 | 38 | 37 | 36 | 35 | 34 | 34 | 33 | 32 | 3 I | 30 | 30 | 29 | 29 | 28 |
| 108 | 40 | 39 | 38 | 37 | 36 | 35 | 34 | 33 | 32 | 32 | 31 | 30 | 30 | 29 | 28 |
| 110 | 40 | 39 | 38 | 37 | 36 | 35 | 35 | 34 | 33 | 32 | 31 | 3 I | 30 | 29 | 29 |
| 112 | 4 I | 40 | 39 | 38 | 37 | 36 | 35 | 34 | 33 | 33 | 32 | 31 | 3 I | 30 | 29 |
| 114 | 41 | 40 | 39 | 38 | 37 | 36 | 35 | 35 | 34 | 33 | 32 | 32 | 3 I | 30 | 30 |
| 116 | 42 | 41 | 40 | 39 | 38 | 37 | 36 | 35 | 34 | 34 | 33 | 32 | 3I | 3 I | 30 |
| 118 | 42 | 41 | 40 | 39 | 38 | 37 | 36 | 36 | 35 | 34 | 33 | 33 | 32 | 3 I | 31 |
| 120 | 43 | 42 | 4 I | 40 | 39 | 38 | 37 | 36 | 35 | 34 | 34 | 33 | 32 | 32 | 3 I |
| 122 | 43 | 42 | 4 I | 40 | 39 | 38 | 37 | 36 | 36 | 35 | 34 | 33 | 33 | 32 | 31 |
| 124 | 44 | 43 | 42 | 4 I | 40 | 39 | 38 | 37 | 36 | 35 | 35 | 34 | 33 | 32 | 32 |
| 126 | 44 | 43 | 42 | 4 I | 40 | 39 | 38 | 37 | 37 | 36 | 35 | 34 | 34 | 33 | 32 |
| 128 | 45 | 43 | 42 | 4 I | 40 | 40 | 39 | 38 | 37 | 36 | 35 | 35 | 34 | 33 | 33 |
| 130 | 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 | 37 | 37 | 36 | 35 | 34 | 34 | 33 |
| 132 |  | 44 | 43 | 42 | 41 | 40 | 40 | 39 | 38 | 37 | 36 | 35 | 35 | 34 | 33 |
| 134 |  | 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 | 37 | 37 | 36 | 35 | 34 | 34 |
| 136 |  |  | 44 | 43 | 42 | 41 | 40 | 39 | 39 | 38 | 37 | 36 | 36 | 35 | 34 |
| I 38 |  |  | 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 | 37 | 37 | 36 | 35 | 35 |
| 140 |  |  | 45 | 44 | 43 | 42 | 41 | 40 | 39 | 39 | 38 | 37 | 36 | 36 | 35 |
| 142 |  |  |  | 44 | 43 | 42 | 42 | 4 I | 40 | 39 | 38 | 38 | 37 | 36 | 35 |
| 144 |  |  |  | 45 | 44 | 43 | 42 | 4 I | 40 | 39 | 39 | 38 | 37 | 36 | 36 |
| 146 |  |  |  |  | 44 | 43 | 42 | 42 | 41 | 40 | 39 | 38 | 38 | 37 | 36 |
| 148 |  |  |  |  | 45 | 44 | 4.3 | 42 | 4 I | 40 | 39 | 39 | 38 | 37 | 37 |
| 150 |  |  |  |  | 45 | 44 | 43 | 42 | 4I | 4I | 40 | 39 | 38 | 38 | 37 |

Smithsonian Tables.

SYNOPTIC CONVERSION OF VELOCITIES.
Miles per hour into metres per second, feet per second
and kilometres per hour.

| Miles per hour. | Metres per second. | Feet per second. | Kilometres per hour. | Miles per hour. | Metres per second. | $\begin{gathered} \text { Feet } \\ \text { per } \\ \text { second. } \end{gathered}$ | Kilometres per hour. | Miles per hour. | Metres per second. | $\begin{gathered} \text { Feet } \\ \text { per } \\ \text { second. } \end{gathered}$ | Kilometres per hour. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0.0 | 0.0 | 0.0 | 26.0 | ri. 6 | 38.1 | 41.8 | 52.0 | 23.2 | 76.3 | 83.7 |
| 0.5 | 0.2 | 0.7 | 0.8 | 26.5 | 11.8 | 38.9 | 42.6 | 52.5 | 23.5 | 77.0 | 84.5 |
| 1.0 | 0.4 | 1.5 | r. 6 | 27.0 | 12.1 | 39.6 | 43.5 | 53.0 | 23.7 | 77.7 | 85.3 |
| 1.5 | 0.7 | 2.2 | 2.4 | 27.5 | 12.3 | 40.3 | 44.3 | 53.5 | 23.9 | 78.5 | 86.1 |
| 2.0 | 0.9 | 2.9 | 3.2 | 28.0 | 12.5 | 4 I .1 | 45.1 | 54.0 | 24.1 | 79.2 | 86.9 |
| 2.5 | I.I | 3.7 | 4.0 | 28.5 | 12.7 | 41.8 | 45.9 | 54.5 | 24.4 | 79.9 | 87.7 |
| 3.0 | 1.3 | 4.4 | 4.8 | 29.0 | 13.0 | 42.5 | 46.7 | 55.0 | 24.6 | 80.7 | 88.5 |
| 3.5 | 1.6 | 5.1 | 5.6 | 29.5 | I3.2 | 43.3 | 47.5 | 55.5 | 24.8 | 81. 4 | 89.3 |
| 4.0 | I. 8 | 5.9 | 6.4 | 30.0 | I3.4 | 44.0 | 48.3 | 56.0 | 25.0 | 82.1 | 90.1 |
| 4.5 | 2.0 | 6.6 | 7.2 | 30.5 | I3.6 | 44.7 | 49.1 | 56.5 | 25.3 | 82.9 | 90.9 |
| 5.0 | 2.2 | 7.3 | 8.0 | 31.0 | I3.9 | 45.5 | 49.9 | 57.0 | 25.5 | 83.6 | 91.7 |
| 5.5 | 2.5 | 8.1 | 8.9 | 31.5 | 14.I | 46.2 | 50.7 | 57.5 | 25.7 | 84.3 | 92.5 |
| 6.0 | 2.7 | 8.8 | 9.7 | 32.0 | 14.3 | 46.9 | 51.5 | 58.0 | 25.9 | 85.1 | 93.3 |
| 6.5 | 2.9 | 9.5 | 10.5 | 32.5 | 14.5 | 47.7 | 52.3 | 58.5 | 26.2 | 85.8 | 94.1 |
| 7.0 | 3.1 | 10.3 | II. 3 | 33.0 | 14.8 | 48.4 | 53.1 | 59.0 | 26.4 | 86.5 | 95.0 |
| 7.5 | 3.4 | 11.0 | 12.1 | 33.5 | 15.0 | 49.1 | 53.9 | 59.5 | 26.6 | 87.3 | 95.8 |
| 8.0 | 3.6 | 11.7 | 12.9 | 34.0 | 15.2 | 49.9 | 54.7 | 60.0 | 26.8 | 88.0 | 96.6 |
| 8.5 | 3.8 | 12.5 | 13.7 | 34.5 | 15.4 | 50.6 | 55.5 | 60.5 | 27.0 | 88.7 | 97.4 |
| 9.0 | 4.0 | 13.2 | 14.5 | 35.0 | 15.6 | 51.3 | 56.3 | 61.0 | 27.3 | 89.5 | 98.2 |
| 9.5 | 4.2 | 13.9 | 15.3 | 35.5 | 15.9 | 52.1 | 57.1 | 61.5 | 27.5 | 90.2 | 99.0 |
| 10.0 | 4.5 | 14.7 | 16.1 | 36.0 | 16.1 | 52.8 | 57.9 | 62.0 | 27.7 | 90.9 | 99.8 |
| 10.5 | 4.7 | 15.4 | 16.9 | 36.5 | 16.3 | 53.5 | 58.7 | 62.5 | 27.9 | 91.7 | 100.6 |
| 11.0 | 4.9 | 16.I | 17.7 | 37.0 | 16.5 | 54.3 | 59.5 | 63.0 | 28.2 | 92.4 | ror. 4 |
| II. 5 | 5.I | 16.9 | 18.5 | 37.5 | 16.8 | 55.0 | 60.4 | 63.5 | 28.4 | 93.1 | 102.2 |
| 12.0 | 5.4 | 17.6 | 19.3 | 38.0 | 17.0 | 55.7 | 6 I .2 | 64.0 | 28.6 | 93.9 | 103.0 |
| 12.5 | 5.6 | 18.3 | 20.1 | 38.5 | 17.2 | 56.5 | 62.0 | 64.5 | 28.8 | 94.6 | 103.8 |
| I3.0 | 5.8 | 19.1 | 20.9 | 39.0 | 17.4 | 57.2 | 62.8 | 65.0 | 29.1 | 95.3 | 104.6 |
| 13.5 | 6.0 | 19.8 | 21.7 | 39.5 | 17.7 | 57.9 | 63.6 | 65.5 | 29.3 | 96.1 | 105.4 |
| 14.0 | 6.3 | 20.5 | 22.5 | 40.0 | 17.9 | 58.7 | 64.4 | 66.0 | 29.5 | 96.8 | 106.2 |
| 14.5 | 6.5 | 21.3 | 23.3 | 40.5 | 18.1 | 59.4 | 65.2 | 66.5 | 29.7 | 97.5 | 107.0 |
| 15.0 | 6.7 | 22.0 | 24.1 | 41.0 | 18.3 | 60.1 | 66.0 | 67.0 | 30.0 | 98.3 | 107.8 |
| 15.5 | 6.9 | 22.7 | 24.9 | 41.5 | 18.6 | 60.9 | 66.8 | 67.5 | 30.2 | 99.0 | 108.6 |
| 16.0 | 7.2 | 23.5 | 25.7 | 42.0 | 18.8 | 61.6 | 67.6 | 68.0 | 30.4 | 99.7 | 109.4 |
| 16.5 | 7.4 | 24.2 | 26.6 | 42.5 | 19.0 | 62.3 | 68.4 | 68.5 | 30.6 | 100.5 | 110.2 |
| 17.0 | 7.6 | 24.9 | 27.4 | 43.0 | 19.2 | 63.1 | 69.2 | 69.0 | 30.8 | 101.2 | III.O |
| 17.5 | 7.8 | 25.7 | 28.2 | 43.5 | 19.4 | 63.8 | 70.0 | 69.5 | 31.1 | IOI. 9 | III. 8 |
| 18.0 | 8.0 | 26.4 | 29.0 | 44.0 | 19.7 | 64.5 | 70.8 | 70.0 | 31.3 | 102.7 | 112.7 |
| 18.5 | 8.3 | 27.1 | 29.8 | 44.5 | 19.9 | 65.3 | 71.6 | 70.5 | 31.5 | 103.4 | I 13.5 |
| 19.0 | 8.5 | 27.9 | 30.6 | 45.0 | 20.1 | 66.0 | 72.4 | 71.0 | 31.7 | 104.1 | 114.3 |
| 19.5 | 8.7 | 28.6 | 31.4 | 45.5 | 20.3 | 66.7 | 73.2 | 71.5 | 32.0 | 104.9 | 115.1 |
| 20.0 | 8.9 | 29.3 | 32.2 | 46.0 | 20.6 | 67.5 | 74.0 | 72.0 | 32.2 | 105.6 | 115.9 |
| 20.5 | 9.2 | 30.1 | 33.0 | 46.5 | 20.8 | 68.2 | 74.8 | 72.5 | 32.4 | 106.3 | II6.7 |
| 21.0 | 9.4 | 30.8 | 33.8 | 47.0 | 21.0 | 68.9 | 75.6 | 73.0 | 32.6 | 107.1 | I17.5 |
| 21.5 | 9.6 | 31.5 | 34.6 | 47.5 | 21.2 | 69.7 | 76.4 | 73.5 | 32.9 | 107.8 | 118.3 |
| 22.0 | 9.8 | 32.3 | 35.4 | 48.0 | 21.5 | 70.4 | 77.2 | 74.0 | 33.1 | 108.5 | 119.1 |
| 22.5 | 10.1 | 33.0 | 36.2 | 48.5 | 21.7 | 71.1 | 78.1 | 74.5 | 33.3 | 109.3 | 119.9 |
| 23.0 | 10.3 | 33.7 | 37.0 | 49.0 | 21.9 | 71.9 | 78.9 | 75.0 | 33.5 | 110.0 | 120.7 |
| 23.5 | 10.5 | 34.5 | 37.8 | 49.5 | 22.1 | 72.6 | 79.7 | 75.5 | 33.8 | I 10.7 | 121.5 |
| 24.0 | 10.7 | 35.2 | 38.6 | 50.0 | 22.4 | 73.3 | So. 5 | 76.0 | 34.0 | III. 5 | 122.3 |
| 24.5 | 11.0 | 35.9 | 39.4 | 50.5 | 22.6 | 74.1 | 81.3 | 76.5 | 34.2 | 112.2 | 123.1 |
| 25.0 | 1 I .2 | 36.7 | 40.2 | 51.0 | 22.8 | 74.8 | 82.1 | 77.0 | 34.4 | II2.9 | 123.9 |
| 25.5 | II. 4 | 37.4 | 41.0 | 51.5 | 23.0 | 75.5 | 82.9 | 77.5 | 34.6 | 113.7 | 124.7 |
| 26.0 | 11.6 | 38.1 | 41.8 | 52.0 | 23.2 | 76.3 | 83.7 | 78.0 | 34.9 | II4.4 | 125.5 |

## MILES PER HOUR INTO FEET PER SECOND.

I mile per hour $=\frac{44}{30}$ feet per second.

| $\begin{gathered} \text { Miles } \\ \text { per hour. } \end{gathered}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\left\|\begin{array}{c} \text { Feet per } \\ \text { sec. } \end{array}\right\|$ | $\begin{gathered} \text { Feet per } \\ \text { sec. } \end{gathered}$ | $\begin{aligned} & \text { Feet per } \\ & \text { sec. } \end{aligned}$ | $\begin{aligned} & \text { Feet per } \\ & \text { sec. } \end{aligned}$ | $\begin{aligned} & \text { Feet per } \\ & \text { sec } \end{aligned}$ | Feet per sec. | Feet per sec. | $\begin{aligned} & \text { Feet per } \\ & \text { sec. } \end{aligned}$ | $\begin{array}{r} \text { Feet per } \\ \text { sec. } \end{array}$ | $\begin{gathered} \text { Feet per } \\ \text { sec. } \end{gathered}$ |
| 0 | 0.0 | I. 5 | 2.9 | 4.4 | 5.9 | 7.3 | 8.8 | 12.3 | 11.7 | 13.2 |
| 10 | 14.7 | 16.1 | 17.6 | 19.1 | 20.5 | 22.0 | 23.5 | 24.9 | 26.4 | 27.9 |
| 20 | 29.3 | 30.8 | 32.3 | 33.7 | 35.2 | 36.7 | 38.1 | 39.6 | $4 \mathrm{II.I}$ | 42.5 |
| 30 | 44.0 | 45.5 | 46.9 | 48.4 | 49.9 | 5 I .3 | 52.8 | 54.3 | 55.7 | 57.2 |
| 40 | 58.7 | 60.1 | 61.6 | 63.1 | 64.5 | 66.0 | 67.5 | 68.9 | 70.4 | 71.9 |
| 50 | 73.3 | 74.8 | 76.3 | 77.7 | 79.2 | 80.7 | 82.1 | 83.6 | 85. 1 | 86.5 |
| 60 | 88.0 | 89.5 | 90.9 | 92.4 | 93.9 | 95.3 | 96.8 | 98.3 | 99.7 | 101.2 |
| 70 | 102.7 | 104. 1 | 105.6 | 107.1 | 108.5 | Iro.0 | 111.5 | 112.9 | 114.4 | 115.9 |
| 80 | 117.3 | 118.8 | 120.3 | 121.7 | 123.2 | 124.7 | 126. 1 | 127.6 | 129.1 | I30.5 |
| 90 | 132.0 | I 33.5 | 134.9 | I36.4 | 137.9 | 139.3 | 140.8 | 142.3 | 143.7 | I45.2 |
| 100 | 146.7 | 148.1 | 149.6 | 151.1 | 152.5 | 154.0 | 155.5 | 156.9 | 158.4 | 159.9 |
| 110 | 16 I .3 | 162.8 | 164.3 | 165.7 | 167.2 | 168.7 | 170.1 | 171.6 | 173.1 | 174.5 |
| 120 | 176.0 | 177.5 | 178.9 | 180.4 | 181.9 | 183.3 | 184.8 | 186.3 | 187.7 | 189.2 |
| 130 | 190.7 | 192.1 206.8 | 193.6 208.3 | 195.1 209.7 | 196.5 211.2 | 198.0 212.7 | 199.5 | 200.9 | 202.4 | 203.9 |
| 140 | 205.3 | 206.8 | 208.3 | 209.7 | 211.2 | 212.7 | 214. I | 215.6 | 217.1 | 218.5 |

TAble 52.

## FEET PER SECOND INTO MILES PER HOUR.

I foot per second $=\frac{30}{44}$ miles per hour.

| Feet per sec. | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr | Miles per hr. | Miles per hr. | Miles <br> per hr. | Miles per hr. |
| 0 | 0.0 | $0.7{ }^{\circ}$ | 1.4 | 2.0 | 2.7 | 3.4 | 4.1 | 4.8 | 5.5 | 6.1 |
| 10 | 6.8 | 7.5 | 8.2 | 8.9 | 9.5 | 10.2 | 10.9 | 11.6 | 12.3 | 13.0 |
| 20 | 13.6 | 14.3 | 15.0 | 15.7 | 16.4 | 17.0 | 17.7 | 18.4 | 19.1 | 19.8 |
| 30 | 20.5 | 21.1 | 21.8 | 22.5 | 23.2 | 23.9 | 24.5 | 25.2 | 25.9 | 26.6 |
| 40 | 27.3 | 28.0 | 28.6 | 29.3 | 30.0 | 30.7 | 31.4 | 32.0 | 32.7 | 33.4 |
| 50 | 34. 1 | 34.8 | 35.5 | 36.1 | 36.8 | 37.5 | 38.2 | 38.9 | 39.5 | 40.2 |
| 60 | 40.9 | 41.6 | 42.3 | 43.0 | 43.6 | 44.3 | 45.0 | 45.7 | 46.4 | 47.0 |
| 70 | 47.7 | 48.4 | 49.1 | 49.8 | 50.5 | 51.1 | 5 I .8 | 52.5 | 53.2 | 53.9 |
| 80 | 54.5 | 55.2 | 55.9 | 56.6 | 57.3 | 58.0 | 58.6 | 59.3 | 60.0 | 60.7 |
| 90 | 61.4 | 62.0 | 62.7 | 63.4 | 64.1 | 64.8 | 65.5 | 66.1 | 66.8 | 67.5 |
| 100 | 68.2 | 68.9 | 69.5 | 70.2 | 70.9 | 71.6 | 72.3 | 73.0 | 73.6 | 74.3 |
| 110 | 75.0 | 75.7 | 76.4 | 77.0 | 77.7 | 78.4 | 79.1 | 79.8 | 80.5 | 8 I .1 |
| 120 | 81.8 | 82.5 | 83.2 | 83.9 | 84.5 | 85.2 | 85.9 | 86.6 | 87.3 | 88.0 |
| 130 | 88.6 | 89.3 | 90.0 | 90.7 | 91.4 | 92.0 | 92.7 | 93.4 | 94.1 | 94.8 |
| 140 | 95.5 | 96.1 | 96.8 | 97.5 | 98.2 | 98.9 | 99.5 | 100.2 | 100.9 | 101. 6 |
| 150 | 102.3 | 103.0 | 103. 6 | 104.3 | 105.0 | 105.7 | 106.4 | 107.0 | 107.7 | 108.4 |
| 160 | 109.1 | 109.8 | 110.5 | 111.I | 111.8 | 112.5 | 113.2 | 113.9 | 114.5 | 115.2 |
| 170 | 115.9 | 116.6 | 117.3 | 118.0 | 118.6 | 119.3 | 120.0 | 120.7 | 121.4 | 120.0 |
| 180 | 122.7 | 123.4 | 124.1 | 124.8 | 125.5 | I26.1 | 126.8 | 127.5 | 128.2 | 128.9 |
| 190 | 129.5 | 130.2 | 130.9 | 131.6 | 132.3 | 133.0 | 133.6 | 134.3 | 135.0 | 135.7 |

Smithbonian Tables.

## METRES PER SECOND INTO MILES PER HOUR.

1 metre per second $=\mathbf{2 . 2 3 6 9 3 2}$ miles per hour.

| Metres per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Miles } \\ & \text { per hr. } \end{aligned}$ | $\begin{aligned} & \text { Miles } \\ & \text { per hr. } \end{aligned}$ | $\begin{aligned} & \text { Miles } \\ & \text { per hr. } \end{aligned}$ | $\begin{aligned} & \text { Miles } \\ & \text { per hr. } \end{aligned}$ | $\underset{\text { per } \mathrm{hr} \text {. }}{\substack{\text { Miles } \\ \hline}}$ | $\begin{aligned} & \text { Miles } \\ & \text { per hr. } \end{aligned}$ | $\underset{\text { per hr. }}{\substack{\text { Miles } \\ \hline}}$ | $\begin{aligned} & \text { Miles } \\ & \text { per hr. } \end{aligned}$ | Miles per hr. | Miles per hr. |
| 0 | 0.0 | 0.2 | 0.4 | 0.7 | 0.9 | I.I | 1.3 | 1.6 | 1.8 | 2.0 |
| 1 | 2.2 | 2.5 | 2.7 | 2.9 | 3.1 | 3.4 | 3.6 | 3.8 | 4.0 | 4.3 |
| 2 | 4.5 | 4.7 | 4.9 | 5.1 | 5.4 | 5.6 | 5.8 | 6.0 | 6.3 | 6.5 |
| 3 | 6.7 | 6.9 | 7.2 | 7.4 | 7.6 | 7.8 | 8.1 | 8.3 | 8.5 | 8.7 |
| 4 | 8.9 | 9.2 | 9.4 | 9.6 | 9.8 | 10.1 | 10.3 | 10.5 | 10.7 | 11.0 |
| 5 | 11.2 | 11.4 | 11.6 | 11.9 | 12.1 | 12.3 | 12.5 | 12.8 | 13.0 | 13.2 |
| 6 | 13.4 | 13.6 | 13.9 | 14.1 | 14.3 | 14.5 | 14.8 | 15.0 | 15.2 | 15.4 |
| 7 | 15.7 | 15.9 | 16.1 | 16.3 | 16.6 | 16.8 | 17.0 | 17.2 | 17.4 | 17.7 |
| 8 | 17.9 | 18.1 | 18.3 | 18.6 | 18.8 | 19.0 | 19.2 | 19.5 | 19.7 | 19.9 |
| 9 | 20.1 | 20.4 | 20.6 | 20.8 | 21.0 | 2 I .3 | 21.5 | 21.7 | 21.9 | 22.1 |
| 10 | 22.4 | 22.6 | 22.8 | 23.0 | 23.3 | 23.5 | 23.7 | 23.9 | 24.2 | 24.4 |
| 11 | 24.6 | 24.8 | 25.1 | 25.3 | 25.5 | 25.7 | 25.9 |  | 26.4 | 26.6 |
| 12 | 26.8 | 27.1 | 27.3 | 27.5 | 27.7 | 28.0 | 28.2 | 28.4 | 28.6 | 28.9 |
| 13 | 29.1 | 29.3 | 29.5 | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.9 | 31.1 |
| 14 | 31.3 | 31.5 | 31.8 | 32.0 | 32.2 | 32.4 | 32.7 | 32.9 | 33.1 | 33.3 |
| 15 | 33.6 | 33.8 | 34.0 | 34.2 | 34.4 | 34.7 | 34.9 | 35.1 | 35.3 | 35.6 |
| 16 | 35.8 | 36.0 | 36.2 | 36.5 | 36.7 | 36.9 | 37.1 | 37.4 | 37.6 | 37.8 |
| 17 | 38.0 | 38.3 | 38.5 | 38.7 | 38.9 | 39.1 | 39.4 | 39.6 | 39.8 | 40.0 |
| 18 | 40.3 | 40.5 | 40.7 | 40.9 | 4 I .2 | 4 I .4 | 4 I .6 | 4 I .8 | 42.1 | 42.3 |
| 19 | 42.5 | 42.7 | 43.0 | 43.2 | 43.4 | 43.6 | 43.8 | 44.1 | 44.3 | 44.5 |
| 20 | 44.7 | 45.0 | 45.2 | 45.4 | 45.6 | 45.9 | 46.1 | 46.3 | 46.5 | 46.8 |
| 21 | 47.0 | 47.2 | 47.4 | 47.6 | 47.9 | 48.1 | 48.3 | 48.5 | 48.8 | 49.0 |
| 22 | 49.2 | 49.4 | 49.7 | 49.9 | 50.1 | 50.3 | 50.6 | 50.8 | 51.0 | 51.2 |
| 23 | 51.5 | 51.7 | 51.9 | 52.1 | 52.3 | 52.6 | 52.8 | 53.0 | 53.2 | 53.5 |
| 24 | 53.7 | 53.9 | 54.1 | 54.4 | 54.6 | 54.8 | 55.0 | 55.3 | 55.5 | 55.7 |
| 25 | 55.9 | 56.1 | 56.4 | 56.6 | 56.8 | 57.0 | 57.3 | 57.5 | 57.7 | 57.9 |
| 26 | 58.2 | 58.4 |  | 58.8 | 59.1 | 59.3 | 59.5 | 59.7 | 60.0 | 60.2 |
| 27 | 60.4 | 60.6 | 60.8 | 61.1 | 61.3 | 61.5 | 61.7 | 62.0 | 62.2 | 62.4 |
| 28 | 62.6 | 62.9 | 63.1 | 63.3 | 63.5 | 63.8 66.0 | 64.0 66.2 | 64.2 66.4 | 64.4 66.7 | 64.6 66.9 |
| 29 | 64.9 | 65.1 | 65.3 | 65.5 | 65.8 | 66.0 | 66.2 | 66.4 | 66.7 | 66.9 |
| 30 | 67.1 | 67.3 | 67.6 | 67.8 | 68.0 | 68.2 | 68.5 | 68.7 | 68.9 | 69.1 |
| 31 | 69.3 | 69.6 | 69.8 | 70.0 | 70.2 | 70.5 | 70.7 | 70.9 | 71.1 | 71.4 |
| 32 | 71.6 | 71.8 | 72.0 | 72.3 | 72.5 | 72.7 | 72.9 | 73.1 | 73.4 | 73.6 |
| 33 | 73.8 | 74.0 | 74.3 | 74.5 | 74.7 | 74.9 | 75.2 | 75.4 | 75.6 | 75.8 |
| 34 | 76.1 | 76.3 | 76.5 | 76.7 | 77.0 | 77.2 | 77.4 | 77.6 | 77.8 | 78.1 |
| 35 | 78.3 | 78.5 | 78.7 | 79.0 | 79.2 | 79.4 | 79.6 | 79.9 | 80.1 | 80.3 |
| 36 | 80.5 | 80.8 | 81.0 | 81.2 | 8 I .4 | 8 I .6 | 81.9 | 82.1 | 82.3 | 82.5 |
| 37 | 82.8 | 83.0 | 83.2 | 83.4 | 83.7 | 84.0 | 84.I | 84.3 | 84.6 | 84.8 |
| 38 | 85.0 | 85.2 | 85.5 | 85.7 | 85.9 | 86.1 | 86.3 | 86.6 | 86.8 | 87.0 |
| 39 | 87.2 | 87.5 | 87.7 | 87.9 | 88.1 | 88.4 | 88.6 | 88.8 | 89.0 | 89.3 |
| 40 | 89.5 | 89.7 | 89.9 | 90.2 | 90.4 | 90.6 | 90.8 | 91.0 | 91.3 | 91.5 |
| 4 I | 9 T .7 | 91.9 | 92.2 | 92.4 | 92.6 | 92.8 | 93.1 | 93.3 | 93.5 | 93.7 |
| 42 | 94.0 | 94.2 | 94.4 | 94.6 | 94.8 | 95.1 | 95.3 | 95.5 | 95.7 | 96.0 |
| 43 | 96.2 | 96.4 | 96.6 | 96.9 | 97.1 | 97.3 | 97.5 | 97.8 | 98.0 | 98.2 |
| 44 | 98.4 | 98.7 | 98.9 | 99.I | 99.3 | 99.5 | 99.8 | 100.0 | 100.2 | 100.4 |

TABLE 53.
METRES PER SECOND INTO MILES PER HOUR.

| Metres per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. |
| 45 | 100.7 | 100.9 | IOI. I | 101.3 | 101. 6 | 101.8 | 102.0 | 102.2 | 102.5 | 102.7 |
| 46 | 102.9 | 103. 1 | 103.3 | 103.6 | 103.8 | 104.0 | 104.2 | 104.5 | 104.7 | 104.9 |
| 47 | 105.1 | 105.4 | 105.6 | 105.8 | 106.0 | 106.3 | 106.5 | 106.7 | 106.9 | 107.2 |
| 48 | 107.4 | 107.6 | 107.8 | 108.0 | 108.3 | 108.5 | 108.7 | 108.9 | 109. 2 | 109.4 |
| 49 | 109.6 | 109.8 | IIO.I | 110.3 | 110.5 | I 10.7 | III.O | III. 2 | III. 4 | III. 6 |
| 50 | III. 8 | II2.I | 112.3 | 112.5 | 112.7 | 113.0 | 113.2 | II 3.4 | 113.6 | 113.9 |
| 51 | II4. I | 114.3 | 114.5 | I 14.8 | 115.0 | 115.2 | II5.4 | 115.7 | 115.9 | II6. I |
| 52 | 116.3 | 116.6 | 116.8 | 117.0 | 117.2 | II7.4 | 117.7 | 117.9 | II8. 1 | 118.3 |
| 53 | I 18.6 | 118.8 | 119.0 | II9.2 | 119.5 | I 19.7 | 119.9 | 120.1 | 120.4 | 120.6 |
| 54 | 120.8 | 121.0 | 12 I .3 | 121.5 | 121.7 | 121.9 | 122.I | 122.4 | 122.6 | 122.8 |
| 55 | 123.0 | 123.3 | 123.5 | 123.7 | 123.9 | 124.2 | 124.4 | 124.6 | 124.8 | 125. I |
| 56 | 125.3 | 125.5 | 125.7 | 126.0 | 126.2 | 126.4 | 126.6 | 126.8 | 127.1 | 127.3 |
| 57 | 127.5 | 127.8 | 128.0 | 128.2 | I28.4 | I28.6 | 128.9 | 129.1 | 129.3 | 129.5 |
| 58 | I29.8 | 130.0 | I 30.2 | 130.4 | I30.7 | 130.9 | 13 I .1 | 131.3 | 131.6 | 13 I .8 |
| 59 | 132.0 | 132.2 | 132.5 | 132.7 | I32.9 | 133.1 | 133.3 | 133.6 | 133.8 | 134.0 |

TABLE 54.

## MILES PER HOUR INTO METRES PER SECOND.

1 mile per hour $=0.4470409$ metres per second.

| Miles per hour. | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. |
| 0 | 0.00 | 0.45 | 0.89 | 1.34 | 1. 79 | 2.24 | 2.68 | 3.13 | 3.58 | 4.02 |
| 10 | 4.47 | 4.92 | $5 \cdot 36$ | 5.81 | 6.26 | 6.71 | 7.15 | 7.60 | 8.05 | 8.49 |
| 20 | 8.94 | 9.39 | 9.83 | 10.28 | 10.73 | II.18 | 11.62 | 12.07 | 12.52 | 12.96 |
| 30 | 13.41 | 13.86 | 14.31 | 14.75 | 15.20 | 15.65 | 16.09 | 16.54 | 16.99 | 17.43 |
| 40 | 17.88 | 18.33 | 18.78 | 19.22 | 19.67 | 20.12 | 20.56 | 21.01 | 21.46 | 2 I .91 |
| 50 | 22.35 | 22.80 | 23.25 | 23.69 | 24.14 | 24.59 | 25.03 | 25.48 | 25.93 | 26.38 |
| 60 | 26.82 | 27.27 | 27.72 | 28.16 | 28.61 | 29.06 | 29.50 | 29.95 | 30.40 | 30.85 |
| 70 | 31.29 | 31.74 | 32.19 | 32.63 | 33.08 | 33.53 | 33.98 | 34.42 | 34.87 | 35.32 |
| 80 | 35.76 | 36.21 | 36.66 | 37.10 | 37.55 | 38.00 | 38.45 | 38.89 | 39.34 | 39.79 |
| 90 | 40.23 | 40.68 | 41. 13 | 4 I .57 | 42.02 | 42.47 | 42.92 | 43.36 | 43.81 | 44.26 |
| 100 | 44.70 | 45.15 | 45.60 | 46.05 | 46.49 | 46.94 | 47.39 | 47.83 | 48.28 | 48.73 |
| 110 | 49. 17 | 49.62 | 50.07 | 50.52 | 50.96 | 51.41 | 51.86 | 52.30 | 52.75 | 53.20 |
| 120 | 53.64 | 54.09 | 54.54 | 54.99 | 55.43 | 55.88 | 56.33 | 56.77 | 57.22 | 57.67 |
| 130 | 58.12 | 58.56 | 59.01 | 59.46 | 59.90 | 60.35 | 60.80 | 61.24 | 61.69 | 62.14 |
| I40 | 62.59 | 63.03 | 63.48 | 63.93 | 64.37 | 64.82 | 65.27 | 65.72 | 66.16 | 66.61 |

[^9]METRES PER SECOND INTO KILOMETRES PER HOUR.
1 metre per second $=3.6$ kilometres per hour.

| Metres per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \mathrm{km} . \\ & \text { per hr. } \end{aligned}$ | km . per hr. | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km}} .$ | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km} .}$ | $\underset{\text { per } \mathrm{hr}}{\mathrm{km}}$. | $\stackrel{\mathrm{km}}{\mathrm{per}} \mathrm{hr}$. | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km} .}$ | km . per hr. | $\underset{\text { per } \mathrm{hr}}{\mathrm{km}}$. | $\begin{aligned} & \mathrm{km} . \\ & \text { per } \mathrm{hr} . \end{aligned}$ |
| 0 | 0.0 | 0.4 | 0.7 | I.I | 1.4 | I. 8 | 2.2 | 2.5 | 2.9 | 3.2 |
| 1 | 3.6 | 4.0 | $4 \cdot 3$ | $4 \cdot 7$ | 5.0 | 5.4 | 5.8 | 6.1 | 6.5 | 6.8 |
| 2 | 7.2 | 7.6 | $7 \cdot 9$ | 8.3 | 8.6 | 9.0 | 9.4 | 9.7 | 10. 1 | 10.4 |
| 3 | 10.8 | II. 2 | 11.5 | 11.9 | 12.2 | 12.6 | 13.0 | 13.3 | 13.7 | 14.0 |
| 4 | 14.4 | 14.8 | 15.1 | 15.5 | 15.8 | 16.2 | 16.6 | 16.9 | 17.3 | 17.6 |
| 5 | 18.0 | 18.4 | 18.7 | 19.1 | 19.4 | 19.8 | 20.2 | 20.5 | 20.9 | 21.2 |
| 6 | 21.6 | 22.0 | 22.3 | 22.7 | 23.0 | 23.4 | 23.8 | 24. 1 | 24.5 | 24.8 |
| 7 | 25.2 | 25.6 | 25.9 | 26.3 | 26.6 | 27.0 | 27.4 | 27.7 | 28.1 | 28.4 |
| 8 | 28.8 | 29.2 | 29.5 | 29.9 | 30.2 | 30.6 | 3 I .0 | 3 I .3 | 31.7 | 32.0 |
| 9 | 32.4 | 32.8 | 33.1 | 33.5 | 33.8 | 34.2 | 34.6 | 34.9 | $35 \cdot 3$ | 35.6 |
| 10 | 36.0 | 36.4 | 36.7 | 37. 1 | 37.4 | 37.8 | 38.2 | 38.5 | 38.9 | 39.2 |
| II | 39.6 | 40.0 | 40.3 | 40.7 | 41.0 | 4 I .4 | 41.8 | 42.1 | 42.5 | 42.8 |
| 12 | 43.2 | 43.6 | 43.9 | 44.3 | 44.6 | 45.0 | 45.4 | 45.7 | 46.1 | 46.4 |
| 13 | 46.8 | 47.2 | 47.5 | 47.9 | 48.2 | 48.6 | 49.0 | 49.3 | 49.7 | 50.0 |
| 14 | 50.4 | 50.8 | 5 I .1 | 51.5 | 51.8 | 52.2 | 52.6 | 52.9 | 53.3 | 53.6 |
| 15 | 54.0 | 54.4 | 54.7 | 55. I | 55.4 | 55.8 | 56.2 | 56.5 | 56.9 | 57.2 |
| 16 | 57.6 | 58.0 | 58.3 | 58.7 | 59.0 | 59.4 | 59.8 | 60.1 | 60.5 | 60.8 |
| 17 | 6 I .2 | 61.6 | 61.9 | 62.3 | 62.6 | 63.0 | 63.4 | 63.7 | 64.1 | 64.4 |
| 18 | 64.8 | 65.2 | 65.5 | 65.9 | 66.2 | 66.6 | 67.0 | 67.3 | 67.7 | 68.0 |
| 19 | 68.4 | 68.8 | 69.1 | 69.5 | 69.8 | 70.2 | 70.6 | 70.9 | 71.3 | 71.6 |
| 20 | 72.0 | 72.4 | 72.7 | 73. 1 | 73.4 | 73.8 | 74.2 | 74.5 | 74.9 | 75.2 |
| 2 I | 75.6 | 76.0 | 76.3 | 76.7 | 77.0 | 77.4 | 77.8 | 78.1 | 78.5 | 78.8 |
| 22 | 79.2 | 79.6 | 79.9 | 80.3 | 80.6 | 8 I .0 | 8 8 .4 | 81.7 | 82.1 | 82.4 |
| 23 | 82.8 | 83.2 | 83.5 | 83.9 | 84.2 | 84.6 | 85.0 | 85.3 | 85.7 | 86.0 |
| 24 | 86.4 | 86.8 | 87.1 | 87.5 | 87.8 | 88.2 | 88.6 | 88.9 | 89.3 | 89.6 |
| 25 | 90.0 | 90.4 | 90.7 | 91.1 | 91.4 | 91.8 | 92.2 | 92.5 | 92.9 | 93.2 |
| 26 | 93.6 | 94.0 | $94 \cdot 3$ | 94.7 | 95.0 | 95.4 | 95.8 | 96.1 | 96.5 | 96.8 |
| 27 | 97.2 | 97.6 | 97.9 | 98.3 | 98.6 | 99.0 | 99.4 | 99.7 | 100. I | 100.4 |
| 28 | 100.8 | 101.2 | 101.5 | IOI. 9 | 102.2 | 102.6 | 103.0 | 103.3 | 103.7 | 104.0 |
| 29 | 104.4 | 104.8 | 105. I | 105.5 | 105.8 | 106.2 | 106.6 | 106. 9 | 107.3 | 107.6 |
| 30 | 108.0 | 108.4 | 108.7 | 109. 1 | 109.4 | 109.8 | 110.2 | 110.5 | I 10.9 | III. 2 |
| 3 I | III. 6 | 112.0 | 112.3 | II2.7 | II3.0 | II3.4 | II3.8 | II4.I | I 14.5 | 114.8 |
| 32 | II5.2 | II5.6 | 115.9 | I16.3 | I16.6 | 117.0 | 117.4 | 117.7 | II8. 1 | 118.4 |
| 33 | II8.8 | 119.2 | 119.5 | II9.9 | 120.2 | 120.6 | 121.0 | 121.3 | 121.7 | 122.0 |
| 34 | 122.4 | 122.8 | 123. 1 | 123.5 | 123.8 | 124.2 | 124.6 | 124.9 | 125.3 | 125.6 |
| 35 | 126.0 | 126.4 | I26.7 | 127.I | 127.4 | 127.8 | 128.2 | 128.5 | 128.9 | 129.2 |
| 36 | 129.6 | 130.0 | 130.3 | 130.7 | 131.0 | 13 I .4 | 13 I .8 | 132.1 | I32.5 | I32.8 |
| 37 | 133.2 | I 33.6 | 133.9 | ${ }^{1} 34.3$ | 134.6 | I 35.0 | ${ }^{1} 35.4$ | ${ }^{1} 355$ | I36. 1 | I 36.4 |
| 38 | ${ }^{1} 36.8$ | 137.2 | 137.5 | 137.9 | 138.2 | 138.6 | I 39.0 | 139.3 | 139.7 | 140.0 |
| 39 | 140.4 | I40.8 | 141. 1 | 141.5 | 14 I .8 | I42.2 | 142.6 | 142.9 | 143.3 | 143.6 |
| 40 | 144.0 | 144.4 | 144.7 | I45.I | 145.4 | 145.8 | 1.46.2 | 146.5 | I46.9 | 147.2 |
| 41 | 147.6 | 148.0 | 148.3 | 148.7 | 149.0 | 149.4 | I. 49.8 | 150.1 | 150.5 | 150.8 |
| 42 | 15 I .2 | 15 I .6 | 151.9 | 152.3 | 152.6 | 153.0 | 153.4 | 153.7 | 154.1 | 154.4 |
| 43 | 154.8 | ${ }^{1} 55.2$ | 155.5 | ${ }^{1} 55.9$ | 156.2 | 156.6 | 157.0 | 157.3 | 157.7 | 158.0 |
| 44 | ${ }^{1} 58.4$ | I58.8 | 159. I | I 59.5 | 159.8 | 160.2 | 160.6 | 160.9 | 161. 3 | 161.6 |

TABLE 55.
METRES PER SECOND INTO KILOMETRES PER HOUR.

| Metres per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km} .}$ | $\underset{\text { per } \mathrm{hr}}{\mathrm{~km} .}$ | $\underset{\text { per } \mathrm{hr} \text {. }}{\mathrm{km} \text {. }}$ | $\underset{\text { per } \mathrm{kr} .}{\mathrm{km} .}$ | km. per hr. |  | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km}_{2}}$ | $\underset{\text { per } \mathrm{km} .}{\mathrm{km} .}$ | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km} .}$ | $\underset{\text { per } \mathrm{hr} .}{\mathrm{km} .}$ |
| 45 | 162.0 | 162.4 | 162.7 | 163.1 | 163.4 | 163.8 | 164.2 | 164.5 | 164.9 | 165.2 |
| 46 | 165.6 | 166.0 | 166.3 | 166.7 | 167.0 | 167.4 | 167.8 | 168.1 | 168.5 | 168.8 |
| 47 | 169.2 | 169.6 | 169.9 | 170.3 | 170.6 | 171.0 | 171.4 | 171.7 | 172.1 | 172.4 |
| 48 | 172.8 | 173.2 | 173.5 | ${ }^{1} 73.9$ | 174.2 | 174.6 | 175.0 | 175.3 | 175.7 | 176.0 |
| 49 | 176.4 | 176.8 | 177.1 | 177.5 | I77.8 | 178.2 | 178.6 | 178.9 | 179.3 | 179.6 |
| 50 | 180.0 | 180.4 | 180.7 | 181. 1 | 181.4 | I81. 8 | 182.2 | 182.5 | 182.9 | 183.2 |
| 51 | 183.6 | 184.0 | 184.3 | I84.7 | 185.0 | 185.4 | 185.8 | 186.1 | 186.5 | 186.8 |
| 52 | 187.2 | 187.6 | 187.9 | 188.3 | 188.6 | 189.0 | 189.4 | 189.7 | 190.1 | 190.4 |
| 53 | 190.8 | 191.2 | 191.5 | 191.9 | 192.2 | 192.6 | 193.0 | 193.3 | 193.7 | 194.0 |
| 54 | 194.4 | 194.8 | 195. I | 195.5 | 195.8 | 196.2 | 196.6 | 196.9 | 197.3 | 197.6 |
| 55 | 198.0 | 198.4 | 198.7 | 199.1 | 199.4 | 199.8 | 200.2 | 200.5 | 200.9 | 201.2 |
| 56 | 201.6 | 202.0 | 202.3 | 202.7 | 203.0 | 203.4 | 203.8 | 204.1 | 204.5 | 204.8 |
| 57 | 205.2 | 205.6 | 205.9 | 206.3 | 206.6 | 207.0 | 207.4 | 207.7 | 208. I | 208.4 |
| 58 | 208.8 | 209.2 | 209.5 | 209.9 | 210.2 | 210.6 | 211.0 | 211.3 | 211.7 | 212.0 |
| 59 | 212.4 | 212.8 | 213.1 | 213.5 | 213.8 | 214.2 | 214.6 | 214.9 | 215.3 | 215.6 |

TAble 56.

## KILOMETRES PER HOUR INTO METRES PER SECOND.

I kilometre per hour $=\frac{10}{36}$ metres per second.

| Kilome'res per hour. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. | metres per sec. |
| 0 | 0.00 | 0.28 | 0.56 | 0.83 | I.II | 1.39 | 1.67 | 1.94 | 2.22 | 2.50 |
| 10 | 2.78 | 3.06 | 3.33 | 3.61 | 3.89 | 4.17 | 4.44 | 4.72 | 5.00 | 5.28 |
| 20 | 5.56 | 5.83 | 6.11 | 6.39 | 6.67 | 6.94 | 7.22 | 7.50 | 7.78 | 8.06 |
| 30 | 8.33 | 8.6I | 8.89 | 9.17 | 9.44 | 9.72 | 10.00 | 10.28 | 10.56 | 10.83 |
| 40 | II. I I | II. 39 | II. 67 | 11.94 | 12.22 | 12.50 | 12.78 | 13.06 | 13.33 | 13.61 |
| 50 | 13.89 | 14.17 | 14.44 | 14.72 | 15.00 | 15.28 | I5.56 | 15.83 | 16.11 | 16.39 |
| 60 | 16.67 | 16.94 | 17.22 | 17.50 | 17.78 | 18.06 | 18.33 | I8.6I | 18.89 | 19.17 |
| 70 | 19.44 | 19.72 | 20.00 | 20.28 | 20.56 | 20.83 | 21.11 | 21.39 | 21.67 | 21.94 |
| 80 | 22.22 | 22.50 | 22.78 | 23.06 | 23.33 | 23.61 | 23.89 | 24.17 | 24.44 | 24.72 |
| 90 | 25.00 | 25.28 | 25.56 | 25.83 | 26. 11 | 26.39 | 26.67 | 26.94 | 27.22 | 27.50 |
| 100 | 27.78 | 28.06 | 28.33 | 28.61 | 28.89 | 29.17 | 29.44 | 29.72 | 30.00 | 30.28 |
| 110 | 30.56 | 30.83 | 31.11 | 31.39 | 31.67 | 3 I .94 | 32.22 | 32.50 | 32.78 | 33.06 |
| 120 | 33.33 | 33.61 | 33.89 | 34.17 | 34.44 | 34.72 | 35.00 | 35.28 | 35.56 | 35.83 |
| 130 | 36.11 | 36.39 | 36.67 | 36.94 | 37.22 | 37.50 | 37.78 | 38.06 | 38.33 | 38.61 |
| 140 | 38.89 | 39.17 | 39.44 | 39.72 | 40.00 | 40.28 | 40.56 | 40.83 | 41.11 | 41. 39 |
| 150 | 41.67 | 41.94 | 42.22 | 42.50 | 42.78 | 43.06 | 43.33 | 43.61 | 43.89 | 44.17 |
| 160 | 44.44 | 44.72 | 45.00 | 45.28 | 45.56 | 45.83 | 46.11 | 46.39 | 46.67 | 46.94 |
| 170 | 47.22 | 47.50 | 47.78 | 48.06 | 48.33 | 48.61 | 48.89 | 49.17 | 49.44 | 49.72 |
| 180 | 50.00 | 50.28 | 50.56 | 50.83 | 51.11 | 51.39 | 51.67 | 51.94 | 52.22 | 52.50 |
| 190 | 52.78 | 53.06 | 53.33 | 53.61 | 53.89 | 54.17 | 54.44 | 54.72 | 55.00 | 55.28 |

Smithbonian Tables.

TABLE 57.
BEAUFORT WIND SCALE AND ITS CONVERSION INTO VELOCITY.

| Grade. | Designation. | Velocity in miles per hour. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $a$ | $b$ | $c$ | $d$ | $e$ |
| $\bigcirc$ | Calm. | - | 3.3* | o | o | 3 |
| I | Light air. | 7 | 6.6 | 2 | I | 8 |
| 2 | Light breeze. | 14 | 10.0 | 4 | 4 | 13 |
| 3 | Gentle breeze. | 21 | 17.5 | 8 | 10 | 18 |
| 4 | Moderate breeze. | 28 | 25.0 | 16 | 17 | 23 |
| 5 | Fresh breeze. | 35 | 32.5 | 24 | 24 | 28 |
| 6 | Strong breeze. | 42 | 40.0 | 32 | 32 | 34 |
| 7 | Moderate gale. | 49 | 47.5 | 40 | 40 | 40 |
| 8 | Fresh gale. | 56 | 55.0 | 50 | 48 | 48 |
| 9 | Strong gale. | 63 | 62.5 | 62 | 56 | 56 |
| 10 | Whole gale. | 70 | 70.0 | 78 | 67 | 65 |
| II | Storm. | 77 | 77.5 | 96 | 82 | 75 |
| 12 | Hurricane. | 84 | 85.0 | 120 | 100 | 90 |

* Velocity 3.3 is assigned to 0.5 grade.
(a.) Colonel Sir Henry James: Instructions for taking meteorological observations; with tables for their correction and notes on meteorological phenomena. 8vo. Lond., 1860.
(b.) George Neumayer: Discussion of the meteorological and magnetical observations made at the Flagstaff Observatory, Melbourne, during the years 1858 to 1863. 4to. Mannheim, 1867.
(c.) J. K. Laughton: Physical geography and its relation to the prevailing winds and currents. 8vo. Lond., 1870. 2d ed., 8vo. Lond., 1873.
(d.) C. A. Schotт : Meteorological observations in the Arctic seas. By Sir Francis Leopold McClintock, R. N. Made on board the Arctic searching yacht "Fox," in Baffin Bay and Prince Regent's Inlet, in 1857, 1858 and 1859. Reduced and discussed by Charles A. Schott. Smithsonian Contributions to Knowledge, 146. Washington, 1862.
(e.) Robert H. Scott: An attempt to establish a relation between the velocity of the wind and its force (Beaufort scale). Quarterly Journal Meteorological Society, Lond., 1874-'75, ii, p. 109-123.

Instructions in the use of meteorological instruments. Compiled by direction of the Meteorological Committee. 8vo. Lond., 1877.

## GEODETICAL TABLES.

Relative acceleration of gravity at different latitudes . . . TABLE 58
Length of one degree of the meridian at different latitudes . . TABLE 59
Length of one degree of the parallel at different latitudes . . TABLE 60
Duration of sunshine at different latitudes . . . . . . . TABLE 6I
Declination of the sun for the year 1894 . . . . . . . TABLE 62
Relative intensity of solar radiation at different latitudes for the first and sixteenth day of each month . . . . . . TABLE 63

TABLE 58.
RELATIVE ACCELERATION OF GRAVITY AT DIFFERENT LATITUDES.
Ratio of the acceleration of gravity at sea level for each $10^{\prime}$ of latitude, to its acceleration at latitude $45^{\circ}$.
$\frac{g_{\phi}}{g_{45}}=\mathrm{I}-0.002662 \cos 2 \phi$

| Latitude. $\phi$. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | 50' |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 0.997338 | 0.997338 | 0.997338 | 0.997338 | 0.997339 | 0.997339 |
| 1 | 340 | 340 | 341 | 342 | 343 | 344 |
| 2 | 345 | 346 | 347 | 348 | 350 | 351 |
| 3 | 353 | 354 | 356 | 358 | 360 | 362 |
| 4 | 364 | 366 | 368 | 371 | 373 | 376 |
| 5 | 0.997378 | 0.997 381 | 0.997384 | 0.997387 | 0.997390 | 0.997393 |
| 6 | 396 | 399 | 403 | 406 | 410 | 413 |
| 7 | 417 | 421 | 425 | 429 | 433 | 437 |
| 8 | 44 I | 445 | 450 | 454 | 459 | 564 |
| 9 | 468 | 473 | 478 | 483 | 488 | 493 |
| 10 | 0.997499 | 0.997504 | 0.997509 | 0.997515 | 0.997520 | 0.997526 |
| 11 | 532 | 538 | 544 | 550 | 556 | 562 |
| 12 | 568 | 574 | 581 | 587 | 594 | 601 |
| I3 | 607 | 614 | 621 | 628 | 635 | 642 |
| 14 | 650 | 657 | 664 | 672 | 679 | 687 |
| 15 | 0.997695 | 0.997702 | 0.997710 | 0.997718 | 0.997726 | 0.997734 |
| 16 | 742 | 751 | 759 | 767 | 776 | 786 |
| 17 | 793 | 802 856 | 811 | 819 | 828 | 837 |
| 18 | 846 | 856 | 865 | 874 | 883 | 893 |
| 19 | 902 | 912 | 922 | 931 | 941 | 951 |
| 20 | 0.997961 | 0.99797 I | 0.997 98r | 0.997991 | 0.998001 | 0.998 or I |
| 21 | 0.998022 | 0.998 032 | 0.998043 | 0.998053 | 064 | 074 |
| 22 | 085 | o96 | 107 | 118 | 129 | 140 |
| 23 | 151 | 162 | 173 | 185 | 196 | 207 |
| 24 | 219 | 230 | 242 | 254 | 265 | 277 |
| 25 | 0.998289 | 0.998301 | 0.998313 | 0.998325 | 0.998337 | 0.998349 |
| 26 | 36 I | 373 | 386 | 398 | 410 | 423 |
| 27 | 435 | 448 | 460 | 473 | 486 | 499 |
| 28 29 | 511 589 | 524 603 | 537 616 | 550 629 | 563 642 | 576 656 |
| 30 | 0.998669 | 0.998682 | 9.998696 | 0.998709 | 0.998723 | 0.998737 |
| 31 | 750 | 764 | 778 | 791 | 805 | 819 |
| 32 | 833 | 847 | 861 | 875 | 889 | 903 |
| 33 | 917 | 931 | 946 | 960 | 974 | 988 |
| 34 | 0.999003 | 0.999017 | 0.999032 | 0.999046 | 0.999060 | 0.999075 |
| 35 | 0.999090 | 0.999104 | 0.999119 | 0.999 I33 | 0.999148 | 0.999 163 |
| 36 | 177 | 192 | 207 | 222 | 237 | 251 |
| 37 | 266 | 28I | 296 | 311 | 326 | 34 I |
| 38 | 356 447 | 371 462 | 386 477 | 401 | 416 507 | 431 523 |
| 39 | 447 | 462 | 477 | 492 | 507 | 523 |
| 40 |  |  | 0.999568 |  |  | 0.999614 706 |
| 41 | 630 | 645 | 660 | 676 | $\begin{aligned} & 691 \\ & 782 \end{aligned}$ | 706 |
| 42 | 722 | 737 | 753 | 768 | 783 | 799 |
| 43 | 814 | 830 | 845 | 861 | 876 | 892 |
| 44 | 907 | 923 | 938 | 954 | 970 | 985 |
| 45 | 1.000000 | 1.000 015 | 1.000030 | 1.000046 | 1.000062 | 1.000077 |

Smithsonian Tables.

TABLE 58.
RELATIVE ACCELERATION OF GRAVItY AT DIFFERENT LATITUDES.
Ratio of the acceleration of gravity at sea level for each $10^{\prime}$ of latitude, to its acceleration at latitude $45^{\circ}$.
$\frac{g_{\phi}}{g_{45}}=1-0.002662 \cos 2 \phi$

| Latitude. $\phi$. | 0 ' | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | $50^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $45^{\circ}$ | 1.000000 | 1.000015 | 1.000030 | 1.000 046 | 1.000062 | 1.000 077 |
| 46 | 093 | 108 | 124 | 139 | 155 | 170 |
| 47 | I86 | 201 | 217 | 232 | 247 | 263 |
| 48 | 278 | 294 | 309 | 324 | 340 | 355 |
| 49 | 370 | 386 | 401 | 416 | 432 | 447 |
| 50 | 1.000 462 | 1.000477 | 1.000 493 | 1.000 508 | 1.000 523 | 1.000 538 |
| 51 | 553 | 569 | 584 | 599 | 614 | 629 |
| 52 | 644 | 659 | 674 | 689 | 704 | 719 |
| 53 | 734 | 749 | 763 | 778 | 793 | 808 |
| 54 | 823 | 837 | 852 | 867 | 88I | 896 |
| 55 | 1.000910 | 1.000925 | 1.000940 | 1.000 954 | 1.000968 | 1.000 983 |
| 56 | - 997 | 1 Ol 2 | I 026 | 1040 | I 054 | 1069 |
| 57 | 1083 | I 097 | I III | I 125 | , I I39 | I 153 |
| 58 | I 167 | I I81 | I 195 | I 209 | - 1222 | I 236 |
| 59 | I 250 | I 263 | I 277 | I 291 | I 304 | 1318 |
| 60 | I.OOI 33I | x.OOI 344 | I.oor 358 | 1.001 371 | 1.001 384 | 1.OOI 397 |
| 61 | 14 II | I 424 | I 437 | I 450 | I 463 | I 476 |
| 62 | I 489 | I 501 | I 514 | I 527 | I 540 | - 552 |
| 63 | I 565 | I 577 | 1590 | 1 602 | I 614 | 1627 |
| 64 | I 639 | 1651 | I 663 | I 675 | r 687 | I 699 |
| 65 | I.OOI 711 | I.OOI 723 | 1.001 735 | 1.001 746 | 1.001 758 | 1.OOI 770 |
| 66 | I 781 | 1793 | 1804 | 1815 | I 827 | 1838 |
| 67 | I 849 | I 860 | I 871 | I 882 | I 893 | I 904 |
| 68 | I 915 | 1926 | I 936 | I 947 | 1 957 | I 968 |
| 69 | 1978 | I 989 | I 999 | 2009 | 2019 | 2029 |
| 70 | 1.002 039 | 1.002049 | 1.002059 | 1.002 069 | 1.002078 | 1.002088 |
| 71 | 2098 | 2107 | 2117 | 2126 | 2135 | 2144 |
| 72 | 2154 | 2163 | 2172 | 2 I8I | 2189 | 2198 |
| 73 | 2207 | 2216 | 2224 | 2233 | 2241 | 2249 |
| 74 | 2258 | 2266 | 2274 | 2282 | 2290 | 2298 |
|  | 1.002305 | 1.002313 | 1.00232 I | 1.002 328 | 1.002336 | 1.002343 |
| 76 | 2350 | 2358 | 2365 | 2372 | 2379 | 2386 |
| 77 | 2393 | 2399 | 2406 | 2413 | 2419 | 2426 |
| 78 | 2432 | 2438 | 2444 | 2450 | 2456 | 2462 |
| 79 | 2468 | 2474 | 2480 | 2485 | 2491 | 2496 |
| 80 | I. 002501 | 1.002 507 | 1.002512 | 1.002517 | 1.002 522 | 1.002 527 |
| 8 I | 2532 | 2536 | 2541 | 2546 | 2550 | 2555 |
| 82 | 2559 | 2563 | 2567 | 2571 | 2575 | 2579 |
| 83 | 2583 | 2587 | 2590 | 2594 | 2597 | 2601 |
| 84 | 2604 | 2607 | 2610 | 2613 | 2616 | 2619 |
| 85 | 1.002 622 | 1.002 624 | 1.002 627 | 1.002 629 | 1.002632 |  |
| 86 | 2636 | 2638 | 2640 | 2642 | 2644 | $2646$ |
| 87 | 2647 | 2649 | 2650 | 2652 | 2653 | 2654 |
| 88 | 2655 | $2656$ | 2657 | 2658 | 2659 | 2660 |
| 89 | 2660 | 2661 | 2661 | 2662 | 2662 | 2662 |

Smithsonian Tables.

TABLE 59.

## LENGTH OF ONE DEGREE OF THE MERIDIAN AT DIFFERENT LATITUDES.

| Latitude. | Metres. | Statute Miles. | Geographic Miles. <br> $\mathbf{I}^{\prime}$ of the Eq. | Latitude. | Metres. | Statute Miles. | Geographic Miles. <br> $1^{\prime}$ of the Eq |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | I 10568.5 | 68.703 | 59.594 | $45^{\circ}$ | III 132.1 | 69.054 | 59.898 |
| I | I 10 568.8 | 68.704 | 59.594 | 46 | IIII51.9 | 69.067 | 59.908 |
| 2 | I 10569.8 | 68.705 | 59.595 | 47 | I II I71.6 | 69.079 | 59.919 |
| 3 | 110 571.5 | 68.706 | 59.596 | 48 | III I91. 3 | 69.091 | 59.929 |
| 4 | I 10573.9 | 68.707 | 59.597 | 49 | III 210.9 | 69.103 | 59.940 |
| 5 | I 10 577.0 | 68.709 | 59.598 | 50 | III 230.5 | 69.115 | 59.951 |
| 6 | I 10 580.7 | 68.71 I | 59.600 | 5 I | I I I 249.9 | 69.127 | 59.96I |
| 7 | I IO 585.I | 68.714 | 59.603 | 52 | I II 269.2 | 69.139 | 59.972 |
| 8 | I 10 590.2 | 68.717 | 59.606 | 53 | I I I 288.3 | 69.151 | 59.982 |
| 9 | 110595.9 | 68.72 I | 59.609 | 54 | 111307.3 | 69.163 | 59.992 |
| 10 | I 10602.3 | 68.725 | 59.612 | 55 | III 326.0 | 69.175 | 60.002 |
| II | 110609.3 | 68.729 | 59.616 | 56 | I I I 344.5 | 69.186 | 60.012 |
| 12 | 110 617.0 | 68.734 | 59.620 | 57 | I I 1 362.7 | 69.198 | 60.022 |
| 13 | 1 10625.3 | 68.739 | 59.625 | 58 | I I I 380.7 | 69.209 | 60.032 |
| 14 | I 10634.2 | 68.745 | 59.629 | 59 | III 398.4 | 69.220 | 60.04 I |
| 15 | 110643.7 | 68.751 | 59.634 | 60 | III 415.7 | 69.230 | 60.051 |
| 16 | 110653.8 | 68.757 | 59.640 | 61 | III 432.7 | 69.24 I | 60.060 |
| 17 | I 10 664.5 | 68.763 | 59.646 | 62 | I I I 449.4 | 69.251 | 60.069 |
| 18 | I 10 675.7 | '68.770 | 59.652 | 63 | I II 465.7 | 69.261 | 60.077 |
| 19 | 1 10687.5 | 68.778 | 59.658 | 64 | III 481.5 | 69.271 | 60.086 |
| 20 | ı 10699.9 | 68.786 | 59.665 | 65 | III 497.0 | 69.281 | 60.094 |
| 21 | 110712.8 | 68.794 | 59.672 | 66 | III 512.0 | 69.290 | 60.102 |
| 22 | I 10 726.2 | 68.802 | 59.679 | 67 | III 526.5 | 69.299 | 60.110 |
| 23 | 1 10740.1 | 68.810 | 59.686 | 68 | I II 540.5 | 69.308 | 60.118 |
| 24 | I 10754.4 | 68.819 | 59.694 | 69 | III 554. I | 69.316 | 60.125 |
| 25 | I 10 769.2 | 68.829 | 59.702 | 70 | III 567.1 | 69.324 | 60.132 |
| 26 | I 10 784.5 | 68.838 | 59.710 | 71 | III 579.7 | 69.332 | 60.139 |
| 27 | 110800.2 | 68.848 | 59.719 | 72 | III 591.6 | 69.340 | 60.145 |
| 28 | I 10816.3 | 68.858 | 59.727 | 73 | III 603.0 | 69.347 | 60.151 |
| 29 | I 10832.8 | 68.868 | 59.736 | 74 | III 6I3.9 | 69.354 | 60.157 |
| 30 | I 10849.7 | 68.879 | 59.745 | 75 | III 624.1 | 69.360 | 60.163 |
| 31 | 110866.9 | 68.889 | 59.755 | 76 | III 633.8 | 69.366 | 60.168 |
| 32 | I 10884.4 | 68.900 | 59.764 | 77 | III 642.8 | 69.372 | 60.173 |
| 33 | I10 902.3 | 68.911 | 59.774 | 78 | III 651.2 | 69.377 | 60.177 |
| 34 | I 10920.4 | 68.923 | 59.784 | 79 | III 659.0 | 69.382 | 60.182 |
| 35 | I10 938.8 | 68.934 | 59.794 | 80 | III 666.2 | 69.386 | 60.186 |
| 36 | I 10957.4 | 68.946 | 59.804 | 81 | III 672.6 | 69.390 | 60.189 |
| 37 | 110976.3 | 68.957 | 59.814 | 82 | 111678.5 | 69.394 | 60.192 |
| 38 | I 10995.3 | 68.969 | 59.824 | 83 | III 683.6 | 69.397 | 60.195 |
| 39 | III OI4.5 | 68.981 | 59.834 | 84 | I I I 688. 1 | 69.400 | 60.197 |
| 40 | III 033.9 | 68.993 | 59.845 | 85 | 111591.9 | 69.402 | 60.199 |
| 4 I | III 053.4 | 69.005 | 59.855 | 86 | III 695.0 | 69.404 | 60.201 |
| 42 | 111073.0 | 69.017 | 59.866 | 87 | III 697.4 | 69.405 | 60.202 |
| 43 | III 092.6 | 69.029 | 59.876 | 88 | II I 699.2 | 69.407 | 60.203 |
| 44 | III II2.4 | 69.042 | 59.887 | 89 | III 700.2 | 69.407 | 60.204 |
| 45 | III I32.I | 69.054 | 59.898 | 90 | III 700.6 | 69.407 | 60.204 |

LENGTH OF ONE DEGREE OF THE PARALLEL AT DIFFERENT LATITUDES.

| Latitude. | Metres. | Statute Miles. | Geographic Miles. <br> $1^{\prime}$ of the Eq. | Latitude. | Metres. | Statute Miles. | Geographic Miles. $1^{\prime}$ of the Eq. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | III 321.9 | 69.171 | 60.000 | $45^{\circ}$ | 78850.0 | 48.995 | 42.498 |
| 1 | 111305.2 | 69.162 | 59.991 | 46 | 77466.5 | 48.135 | 41.753 |
| 2 | III 254.6 | 69.130 | 59.964 | 47 | 76059.2 | 47.26I | 40.994 |
| 3 | III 170.4 | 69.078 | 59.918 | 48 | 74628.5 | 46.372 | 40.223 |
| 4 | III 052.6 | 69.005 | 59.855 | 49 | 73174.9 | 45.469 | 39.440 |
| 5 | IIO 901. 2 | 68.911 | 59.773 | 50 | 71698.9 | 44.552 | 38.644 |
| 6 | 110716.2 | 68.796 | 59.673 | 51 | 70200.8 | 43.621 | 37.837 |
| 7 | 110497.7 | 68.660 | 59.556 | 52 | 6868 I .1 | 42.676 | 37.018 |
| 8 | I 10245.8 | 68.503 | 59.420 | 53 | 67 I40. 3 | 41.719 | 36.187 |
| 9 | 109960.5 | 68.326 | 59.266 | 54 | 65578.8 | 40.749 | 35.346 |
| 10 | 109641.9 | 68.128 | 59.095 | 55 | 63 997. 1 | 39.766 | 34.493 |
| II | 109290.1 | 67.909 | 58.905 | 56 | 62395.7 | 38.771 | 33.630 |
| 12 | 108905.2 | 67.670 | 58.697 | 57 | 60775.1 | 37.764 | 32.757 |
| 13 | 108487.3 | 67.41I | 58.472 | 58 | 59135.7 | 36.745 | 31.873 |
| 14 | 108 036.6 | 67.131 | 58.229 | 59 | 57478. I | 35.715 | 30.979 |
| 15 | 107553.1 | 66.830 | 57.969 | 60 | 55802.8 | 34.674 | 30.076 |
| 16 | 107037.0 | 66.510 | 57.690 | 61 | 54 I 10. 2 | 33.622 | 29.164 |
| 17 | 106488.5 | 66.169 | 57.395 | 62 | 52400.9 | 32.560 | 28.243 |
| 18 | 105907.7 | 65.808 | 57.082 | 63 | 50675.4 | 31.488 | 27.313 |
| 19 | IO5 294.7 | 65.427 | 56.751 | 64 | $48934 \cdot 3$ | 30.406 | 26.374 |
| 20 | 104 649.8 | 65.026 | 56.404 | 65 | 47178.0 | 29.315 | 25.428 |
| 21 | 103 973.2 | 64.606 | 56.039 | 66 | 45 407.1 | 28.215 | 24.473 |
| 22 | 103265.0 | 64.166 | 55.657 | 67 | 43622.2 | 27.106 | 23.51 I |
| 23 | IO2 525.4 | 63.706 | 55.259 | 68 | 41823.8 | 25.988 | 22.542 |
| 24 | IOI 754.6 | 63.227 | 54.843 | 69 | 40012.4 | 24.862 | 21.566 |
| 25 | 100953.0 | 62.729 | 54.41 I | 70 | 38188.6 | 23.729 | 20.583 |
| 26 | 100120.6 | 62.212 | 53.963 | 71 | 36353.0 | 22.589 | 19.593 |
| 27 | 99257.8 | 61.676 | 53.498 | 72 | 34506.2 | 21.441 | 18.598 |
| 28 | 98364.8 | 61.121 | 53.016 | 73 | 32648.6 | 20.287 | 17.597 |
| 29 | 97 441.9 | 60.548 | 52.519 | 74 | 30780.9 | 19.126 | 16.590 |
| 30 | 96489.3 | 59.956 | 52.006 | 75 | 28903.6 | 17.960 | 15.578 |
| 31 | 05507.3 | 59.345 | 51.476 | 76 | 27017.4 | 16.788 | 14.562 |
| 32 | 94496.2 | 58.717 | 50.93 I | 77 | 25122.8 | 15.611 | 13.541 |
| 33 | 93456.3 | 58.071 | 50.371 | 78 | 23220.4 | 14.428 | 12.515 |
| 34 | 92387.9 | 57.407 | 49.795 | 79 | 21 310.8 | I 3.242 | 11.486 |
| 35 | 91291.3 | 56.726 | 49.204 | 80 | 19394.6 | 12.051 | 10.453 |
| 36 | 90166.8 | 56.027 | 48.598 | 81 | 17472.4 | 10.857 | 9.417 |
| 37 | 89 OI4.8 | 55.311 | 47.977 | 82 | 15544.7 | 9.659 | 8.378 |
| 38 | 87835.6 | 54.578 | 47.34 I | 83 | 13612.2 | 8.458 | $7 \cdot 337$ |
| 39 | 86629.6 | 53.829 | 46.691 | 84 | I 675.5 | 7.255 | 6.293 |
| 40 | 85397.0 | 53.063 | 46.027 | 85 | 9735.1 | 6.049 | 5.247 |
| 4 I | 84138.4 | 52.28 I | 45.349 | S6 | 7791.7 | 4.84 I | 4.200 |
| 42 | 82854.0 | 51.483 | 44.656 | 87 | 5845.9 | 3.632 | 3.151 |
| 43 | 81 544.2 | 50.669 | 43.950 | 88 | 3898.3 | 2.422 | 2.101 |
| 44 | 80209.4 | 49.840 | 43.231 | 89 | I 949.4 | I. 211 | 1.051 |
| 45 | 78850.0 | 48.995 | 42.498 | 90 | 0.0 | 0.000 | 0.000 |

Emithbonian Tables.

TAble 61.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { the of Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ |
|  | h. mi. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-23^{\circ} 27^{\prime}$ | 127 | II 50 | II 32 | II I4 | 10 55 | 10 35 | 10 I3 | 948 | 919 |
| $-2320$ | 127 | II 50 | II 32 | II I4 | 10 56 | Io 36 | IO 14 | 949 | 920 |
| $-230$ | 127 | II 50 | II 33 | II 15 | 10 57 | 10 37 | 10 I 5 | 951 | 923 |
| -2240 | 127 | II 50 | II 33 | II 16 | 10 58 | 10 38 | 1017 | 953 | 926 |
| -22 20 | 127 | II 51 | II 34 | II 17 | IO 59 | IO 40 | IO 19 | 955 | 929 |
| -22 0 | 127 | II 5I | II 34 | II 18 | II 0 | Io 4I | 1020 | 958 | 931 |
| - 2140 | 127 | 1151 | II 35 | II 19 | II I | 10 43 | IO 22 | 10 0 | 934 |
| -2I 20 | 127 | II 52 | II 35 | II 19 | II 2 | Io 44 | 1024 | Io | 937 |
| $-210$ | 127 | II 52 | II 36 | II 20 | II 4 | Io 46 | 10 26 | IO 4 | 940 |
| $-2040$ | 127 | II 52 | II 37 | II 21 | II 5 | 10 47 | 10 28 | 10 6 | 942 |
| $-2020$ | 127 | II 52 | II 37 | II 22 | II 6 | 10 49 | IO 29 | 10 8 | 945 |
| $-200$ | 127 | II 53 | II 38 | II 23 | II 7 | 1050 | 1031 | Io Ir | 947 |
| -1940 | 127 | II 53 | II 38 | 1123 | II 8 | 10 5 I | Io 33 | Io I3 | 950 |
| - 19 20 | 127 | II 53 | II 39 | II 24 | II 9 | IO 53 | Io 35 | IO I5 | 953 |
| -19 0 | 127 | II 53 | II 39 | II 25 | II 10 | IO 54 | 10 37 | 10 17 | 955 |
| - 1840 | 127 | II 54 | II 40 | II 26 | II II | 1055 | 10 38 | IO 19 | 958 |
| - I8 20 | 127 | II 54 | II 40 | II 27 | II 12 | 10 57 | 1040 | 1021 | 101 |
| - i8 o | 127 | II 54 | II 41 | II 28 | II 13 | 10 58 | IO 42 | 1023 | IO 3 |
| $-1740$ | 127 | II 54 | II 41 | II 28 | II 14 | IO 59 | Io 43 | Io 26 | 105 |
| $-1720$ | 127 | II 55 | II 42 | II 29 | 1115 | II I | 10 45 | IO 28 | IO 8 |
| $-170$ | 127 | II 55 | II 42 | II 30 | II I6 | II 2 | Io 47 | 1030 | IO 10 |
| $-1640$ | 127 | II 55 | II 43 | II 31 | II 17 | II 4 | Io 49 | 10 32 | IO 13 |
| - I6 20 | 127 | II 55 | II 43 | II 31 | II 18 | II 5 | Io 50 | IO 34 | IO 16 |
| - 160 | 127 | II 56 | II 44 | II 32 | II 19 | II 6 | 10 52 | 10 36 | 10 18 |
| -1540 | 127 | II 56 | II 44 | II 33 | II 20 | II 8 | 1053 | Io 38 | 1020 |
| - I5 20 | 127 | II 56 | II 45 | II 34 | II 2I | II 9 | 10 55 | 1040 | 10 23 |
| - I5 O | 127 | II 56 | II 45 | II 34 | II 22 | II 10 | Io 57 | Io 42 | 10 25 |
| $-1440$ | 127 | II 57 | II 46 | II 35 | II 23 | II II | Io 59 | 1044 | IO 28 |
| - 1420 | 127 | II 57 | II 46 | II 36 | II 25 | II 13 | II 0 | Io 46 | Io 30 |
| -I4 0 | 127 | II 57 | II 47 | II 37 | II 26 | II 14 | II | Io 48 | IO 32 |
| -13 40 | 127 | II 57 | II 47 | II 37 | II 27 | Ii 16 | II 4 | Io 50 | 10 35 |
| - I3 20 | $127$ | II 58 | II 48 | II 38 | II 28 | $\begin{array}{lll}\text { II } & 17\end{array}$ | II 5 | Io 52 | IO 37 |
| - I3 0 | 127 | II 58 | II 48 | II 39 | II 29 | II 18 | II 7 | Io 54 | 10 40 |
| -1240 | 127 | II 58 | II 49 | II 40 | II 30 | II 19 | $\begin{array}{ll}\text { II } & 8\end{array}$ | Io 56 | IO 42 |
| - 1220 | 127 | II 58 | II 49 | II 40 | II 31 | II 2I | II 10 | Io 58 | IO 44 |
| - 120 | 127 | II 58 | II 50 | II 4I | II 32 | II 22 | II II | II 0 | IO 47 |
| - 1140 | 127 | II 59 | II 50 | II 42 | II 33 | II 23 | II 13 | II 2 | Io 49 |
| - II 20 | 127 | II 59 | II 51 | II 43 | II 34 | II 25 | II 15 | II 4 | 10 52 |
| - II 0 | 127 | II 59 | II 5 I | II 43 | II 35 | II 26 | II 16 | II 6 | 10 54 |
| $-1040$ | 127 | II 59 | II 52 | II 44 | II 36 | II 27 | II 18 | $\begin{array}{ll}\text { II } & 8 \\ \end{array}$ | Io 56 |
| - 1020 | 127 | 120 | II 52 | II 45 | II 37 | II 28 II | II 20 | II 10 | IO 59 |
| - 100 | 127 | 120 | II 53 | II 46 | II 38 | II 30 | II 2I | II 12 | II I |
| - 940 | 127 | 12 O | II 53 | II 46 | II 39 | II 3I | II 23 | II 14 | II 3 |
| - 920 | 127 | 120 | II 54 | II 47 | II 40 | II 32 | II 24 | 1116 | $\begin{array}{ll}\text { II } & 5\end{array}$ |
| -90 | 127 | 12 | II 54 | II 47 | II 4I | II 34 | II 26 | II 17 | II 8 |
| $-840$ | 127 | 12 | II 55 | II 48 | II 42 | II 35 | II 28 | II 19 | II 10 |
| -- 820 | 127 | 12 | $\text { II } 55$ | II 49 | II 43 | $\begin{array}{ll}\text { II } & 36\end{array}$ | II 29 | II 21 | 11 12 <br> 1  |
| - 8 o | 127 | 12 I | II 56 | II 50 | II 44 | II 37 | II 31 | II 23 | II 14 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { the of Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $42^{\circ}$ | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | $52^{\circ}$ | $54^{\circ}$ | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-23^{\circ} 27^{\prime}$ |  | 853 | 838 | 822 | 84 | 744 | 722 | 656 | 627 | 552 |
| $-2320$ | 98 | 854 | 839 | 823 | 85 | 745 | 724 | 658 | 629 | 554 |
| $-230$ | 9 II | 858 | 843 | 828 | 8 10 | 750 | 729 | 74 | 636 | 62 |
| -2240 | 914 | 9 I | 846 | 831 | 8 I4 | 755 | 734 | 710 | 643 | $6 \quad 9$ |
| -22 20 | 917 | 94 | 850 | 835 | 818 | 8 o | 739 | 716 | 649 | 617 |
| 22 | 920 | 97 | 853 | 838 | 822 | 84 | 744 | 722 | 655 | 625 |
| -2140 | 923 | 9 Io | 857 | 842 | 826 | 89 | 749 | 727 | 7 | 632 |
| -21 20 | 926 | 913 | 9 I | 846 | 830 | 8 I3 | 754 | 732 | 78 | 638 |
| 210 | 928 | 917 | 94 | 850 | 834 | 8 I8 | 759 | 738 | 714 | 646 |
| -20 40 | 93 I | 920 | 97 | 853 | 838 | 822 | 84 | 743 | 720 | 652 |
| -20 20 | 934 | 923 | 9 II | 857 | 842 | 826 | 88 | 749 | 725 | 659 |
| 20 0 | 937 | 926 | 914 | 9 I | 846 | 83 I | 8 I3 | 754 | 7 3I | 75 |
| -1940 | 940 | 929 | 9 I7 | 94 | 850 | 835 | 8 I8 | 759 | 737 | 712 |
| - I9 20 | 943 | 932 | 920 | 97 | 854 | 839 | 823 | 84 | 743 | 718 |
| - I9 0 | 946 | 935 | 924 | 9 II | 858 | 843 | 827 | 89 | 748 | 725 |
| -1840 | 948 | 938 | 927 | 915 | 92 | 847 | 832 | 8 I4 | 754 | 731 |
| - I8 20 | 95 I | 94 I | 930 | 9 I9 | 96 | 852 | 836 | 8 I9 | 759 | 737 |
| 18 o | 954 | 944 | 934 | 922 | 9 10 | 856 | 841 | 824 | 85 | 743 |
| - 1740 | 956 | 947 | 937 | 925 | 913 | 9 | 845 | 8 8 8 8 | 8 1о | 749 <br> 7 |
| $-1720$ | 959 | 950 | 940 | 929 | 917 | 9 4 | 850 854 | 8 8 8 38 | 815 8120 | 755 |
| - 17 o | IO 2 | 953 | 943 | 932 | 92 I | 98 | 854 | 838 | 820 | 8 I |
| - 1640 | 105 | 956 | 946 | 935 | 925 | 912 | 858 | 843 | 826 | 86 |
| - I6 20 | IO 7 | 959 | 949 | 939 | 928 | 916 | 92 | 847 | 831 | 812 |
| - 160 | 10 10 | Io I | 952 | 943 | 932 | 920 | 97 | 852 | 836 | 8 I7 |
| -1540 | 1012 | IO 4 | 955 | 946 | 935 | 924 | 9 II | 857 | 841 | 823 |
| - 1520 | 1015 | 10 7 | 958 | 949 | 939 | 928 | 9 I5 | 92 | 846 | 829 |
| - I5 o | 10 18 | Io Io | 10 I | 952 | 943 | 93 I | 919 | 96 | 85 I | 834 |
| -14 40 | 1020 | 10 I3 | 10 4 | 956 | 946 | 935 | 923 | 9 II | 856 | 840 |
| -14 20 | 1023 | 10 16 | 10 7 | 959 | 949 | 939 | 928 | 915 | $9 \quad 1$ | 845 |
| -14 o | 10 26 | 10 19 | Io 10 | IO 2 | 953 | 943 | 932 | 919 | 96 | 850 |
| $-1340$ | 10 28 | 1021 | 10 I3 | 105 | 956 | 947 | 936 | 924 | 9 II | 856 |
| - I3 20 | 10 31 | 10 24 | 10 16 | Io 8 | Io 0 | 950 | 940 | 928 | 916 | 9 I |
| - I3 0 | 10 33 | 10 26 | 1019 | IO II | 10 | 954 | 944 | 933 | 920 | 96 |
| -1240 | 10 36 | 1029 | IO 22 | IO 15 | 107 | 958 | 948 | 937 | 925 | 9 II |
| - 1220 | 10 38 | Io 32 | Io 25 | Io 18 | Io Io | Io I | 952 | 941 | 930 | 917 |
| 120 | Io 4I | 10 35 | IO 28 | Io 21 | Io 13 | Io 5 | 956 | 946 | 935 | 922 |
| - 1140 | 1044 | Io 38 | 103 I | 1025 | 1017 | IO 9 | 10 O | 950 | 939 | 927 |
| - II 20 | 10 46 | Io 40 | Io 34 | 10 28 | 10 20 | 10 I3 | 10 4 | 955 | 944 | 932 |
| II O | IO 49 | 10 43 | 10 37 | 1031 | 10 23 | Io 16 | 10 8 | 959 | 949 | 937 |
| -1040 | 10 51 | Io 46 | IO 40 | IO 34 | 1027 | 10 19 | 1012 | Io 3 | 953 | 942 |
| 1020 | Io 53 | 10 49 | 10 43 | 10 37 | 10 31 | 10 23 | 1016 | 107 | 958 | 947 |
| 10 O | 10 56 | 10 51 | 10 46 | 10 40 | 10 34 | IO 27 | 10 19 | 10 II | 10 3 | 952 |
| - 940 | 1059 | IO 54 | 10 49 | 1043 | 10 37 | 1031 | 1023 | 1016 | 10 7 | 957 |
| - 920 | II I | 10 56 | Io 52 | Io 46 | Io 40 | Io 34 | IO 27 | 1020 | 10 II | 10 2 |
| - 90 | II 3 | IO 59 | 10 55 | 10 49 | 10 44 | 10 37 | IO 31 | 10 24 | 10 16 | 107 |
| - 840 | II 6 | II 2 | IO 57 | 1052 | IO 47 | 1041 | 10 34 | 10 28 | Io 20 | Io II |
| - 820 | II 8 | II 4 | II 0 | 10 55 | 10 50 | 10 44 | 10 38 | Io 32 | Io 25 | 10 16 |
| - 80 | II 10 | II 7 | II 3 | Io 58 | 10 53 | 10 48 | 10 42 | Io 36 | IO 29 | 10 21 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} 0^{\prime}$ | 127 | 12 I | II 55 | II 50 | II 44 | II 37 | II 3I | II 23 | II 14 |
| -740 | 127 | 12 | II 56 | II 50 | II 45 | II 38 | II 32 | II 25 | II 17 |
| 720 | 127 | 12 | II 56 | II 51 | II 46 | II 40 | II 34 | II 27 | II 19 |
| -7 0 | 127 | 122 | II 57 | II 52 | II 47 | II 4I | II 35 | II 29 | II 22 |
| -640 | 127 | 122 | II 57 | II 53 | II 48 | II 42 | II 37 | II 31 | II 24 |
| -6 20 | 127 | 122 | II 58 | II 53 | II 49 | II 43 | II 38 | II 32 | II 26 |
| -6 o | 127 | 122 | II 58 | II 54 | II 50 | II 45 | II 40 | II 34 | II 28 |
| -5 40 | 127 | 123 | II 59 | II 55 | II 5I | II 46 | II 41 | II 36 | II 3 I |
| -5 20 | 127 | 123 | II 59 | II 55 | II 52 | II 47 | II 43 | II 38 | II 33 |
| -5 o | 127 | 123 | 120 | II 56 | II 53 | II 49 | II 44 | II 40 | II 35 |
| -4 40 | 127 | 123 | 120 | II 57 | II 54 | II 50 | II 46 | II 42 | II 37 |
| -4 20 | 127 | 124 | 12 | II 58 | II 55 | II 51 | II 47 | II 44 | II 40 |
| -4 0 | 127 | 124 | 12 | II $5^{8}$ | II 56 | II 52 | II 49 | II 46 | II 42 |
| -340 | 127 | 124 | 122 | II 59 | II 57 | II 53 | II 51 | II 47 | II 44 |
| 320 | 127 | 124 | 122 | 120 | II 58 | II 55 | II 52 | II 49 | II 46 |
| -3 0 | 127 | 125 | 123 | 12 | II 58 | II 56 | II 54 | II 5I | II 49 |
| -2 40 | 127 | 125 | 123 | 12 | II 59 | II 58 | II 55 | II 53 | II 51 |
| 220 | 127 | 125 | 124 | 12 | 120 | II 59 | II 57 | II 55 | II 53 |
| -2 0 | 127 | 125 | 124 | 123 | 12 | 120 | II 58 | II 57 | II 55 |
| -1 40 | 127 | 125 | 124 | 124 | 122 | 12 I | 120 | II 59 | II 58 |
| I 20 | 127 | 126 | 125 | 124 | 123 | 122 | 122 | 12 I | 120 |
| 10 | 127 | 126 | 125 | 125 | 124 | 124 | 123 | 122 | 122 |
| -0 40 | 127 | 126 | 126 | 125 | 125 | 125 | 125 | 124 | 124 |
| - 20 | 127 | 126 | 126 | 126 | 126 | 126 | 126 | 126 | 127 |
| 00 | 127 | 127 | 127 | 12 | 127 | 12 | 128 | 128 | 129 |
| +o 20 | 127 | 127 | 127 | 128 | 128 | 128 | 129 | 12 Io | 12 II |
| O 40 | 127 | 127 | 128 | 128 | 129 | 1210 | 12 II | 1212 | 12 I 3 |
| 10 | 12 | 127 | 128 | 129 | 1210 | 12 II | 12 I | 1214 | 12 I 5 |
| I 20 | 127 | 128 | 129 | 1210 | 12 II | 12 I 3 | 1214 | 1216 | 1217 |
| 140 | 127 | 128 | 129 | 1210 | 1212 | 1214 | 1216 | 1217 | 1220 |
| 20 | 127 | 128 | 12 IO | 12 II | 12 I 3 | 1215 | 1217 | 1219 | 1222 |
| 220 | 127 | 128 | 12 IO | 1212 | 12 I 4 | 1216 | 1219 | 12 2I | 1225 |
| 240 | 127 | 129 | 12 II | 12 I 3 | 1215 | 1217 | 1220 | 1223 | 1227 |
| 30 | 127 | 129 | I2 II | 1213 | 1216 | 1219 | 1222 | 1225 | 1229 |
| 320 | 127 | 129 | 1212 | 12 I 4 | 1217 | 1220 | 1223 | 1227 | 1231 |
| 340 | 127 | 129 | 1212 | 1215 | 1218 | 1221 | 1225 | 1229 | 1233 |
| 40 | 127 | 1210 | 1213 | 1216 | 1219 | 1222 | 1226 | 1231 | 1235 |
| 420 | 127 | 1210 | 1213 | 1216 | 1220 | 1223 | 1228 | 1232 | 1238 |
| 440 | 127 | 12 Io | 1214 | 1217 | 1221 | 1225 | 1229 | 1234 | 1240 |
| 50 | 27 | 12 IO | 12 I | 1218 | 1222 | 1226 | 1231 | 1236 | 1243 |
| 520 | 127 | 12 Io | 1215 | 1219 | 1223 | 1228 | 1232 | 1238 | 1245 |
| 540 | 127 | 12 II | 1215 | 1219 | 1224 | 1229 | 1234 | 1240 | 1247 |
| 60 | 127 | 12 II | 1216 | 1220 | 1225 | 1230 | 1235 | 1242 | 1249 |
| 620 | 127 | 12 II | 1216 | 1221 | 1226 | 1231 | 1237 | 1244 | 1252 |
| 640 | 127 | 12 II | 1216 | 1222 | 1227 | 1232 | 1239 | 1246 | 1254 |
| 70 | 127 | 1212 | 1217 | 1222 | 1228 | 1234 | 1240 | 1248 | 1256 |
| 720 | 127 | 1212 | 1217 | 1223 | 1229 | 1235 | 1242 | 1250 | 1258 |
| 740 | 127 | 1212 | 1218 | 1223 | 1230 | 1236 | 1243 | 1252 | 13 I |
| 80 | 127 | 12 I 3 | 1218 | 1224 | 1231 | 1238 | 1245 | 1253 | 13 |

TABLE 6I
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $42^{\circ}$ | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | $52^{\circ}$ | $54^{\circ}$ | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} 0^{\prime}$ | II II | II 7 | II 3 | II 58 | 10 53 | IO 48 | 1043 | 10 36 | 1030 | 1021 |
| -740 | II 13 | II IO | II 5 | II | IO 57 | 1052 | 10 46 | Io 40 | 10 34 | IO 26 |
| 720 | II 16 | II 12 | II 8 | II 4 | II | 10 55 | 1050 | Io 44 | Io 38 | 1031 |
| $-7 \quad 0$ | II I9 | II 15 | II II | II 7 | II 3 | IO 59 | Io 54 | 10 48 | IO 42 | IO 35 |
| -640 | II 21 | II 17 | II I4 | II 10 | II 7 | II 2 | 10 58 | IO 52 | IO 47 | Io 40 |
| 620 | II 23 | II 20 | II 17 | II I3 | II 10 | II 5 | II | 10 56 | 10 51 | 10 45 |
| 6 o | II 26 | II 23 | II 20 | II 16 | II 13 | II 9 | II 5 | II 0 | IO 55 | 10 50 |
| -5 40 | II 28 | II 25 | II 23 | II 19 | II 16 | II 13 | II 8 | II | Io 59 | 1055 |
| -5 20 | Ir 31 | II 28 | II 25 | II 22 | II 19 | II 16 | II I3 | II 8 | II 4 | Io 59 |
| -5 o | II 33 | II 31 | II 28 | II 25 | II 23 | II I9 | II 16 | II 12 | II 8 | II 4 |
| -4 40 | II 35 | II 33 | II 3I | II 28 | II 26 | II 23 | II 20 | II 16 | II 13 | II 8 |
| 420 | 1138 | II 36 | II 34 | II 31 | II 29 | II 26 | II 23 | II 20 | II 17 | II 13 |
| 4 - | II 40 | II $3^{8}$ | II 37 | II 34 | II 32 | II 30 | II 27 | II 24 | II 21 | II 18 |
| -340 | II 43 | II 41 | II 39 | II 37 | II 35 | II 33 | II 31 | II 28 | II 26 | II 22 |
| 320 | II 45 | II 43 | II 42 | II 40 | II $3^{8}$ | I I 37 | II 35 | II 32 | II 30 | II 27 |
| 30 | II 47 | II 46 | II 45 | II 43 | II 42 | II 40 | II 38 | II 36 | II 34 | II 32 |
| -240 | II 50 | II 49 | II 47 | II 46 | II 45 | II 44 | II 42 | II 40 | II $3^{8}$ | II 37 |
| 220 | II 52 | II 5I | II 50 | II 49 | II 48 | II 47 | II 46 | II 44 | II 43 | II 41 |
| 20 | II 55 | II 54 | II 53 | II $5^{2}$ | II 52 | II 50 | II 49 | II 48 | II 47 | II 46 |
| $-140$ | II 57 | II 56 | II 55 | II 55 | II 55 | II 54 | II 53 | II 52 | II 51 | II 50 |
| 20 | II 59 | II 59 | II $5^{8}$ | II $5^{8}$ | II $5^{8}$ | II 57 | II 57 | II 56 | II 56 | II 55 |
| 10 | 122 | 122 | 12 I | 12 I | 12 I | 12 I | 12 I | 120 | 120 | II 59 |
| -0 40 | 12 | 12 | 124 | 124 | 124 | 124 | 12 | 12 | 124 | 124 |
| O 20 | 127 | 127 | 127 | 127 | 127 | 127 | 128 | 128 | 128 | 129 |
| +00 | 129 | 129 | 12 10 | 1210 | 12 Io | 12 II | 12 II | 1212 | 12 I 3 | 12 I 3 |
| - 20 | 12 II | 1212 | 1213 | 1213 | 1214 | 1214 | 1215 | 1216 | 1217 | 1218 |
| O 40 | 1214 | 12 I 4 | 1215 | 1216 | 1217 | 1217 | 1219 | 1220 | 1221 | 1223 |
| I. 0 | 1216 | 12 I 7 | 1218 | 12 I 9 | 1220 | 1221 | 1222 | 1224 | 1225 | I2 27 |
| I 20 | 12 I9 | 1220 | 1220 | 1222 | 1223 | 1225 | 1226 | 1228 | 1229 | $\begin{array}{ll}12 & 32 \\ 12\end{array}$ |
| I 40 | 1221 | 1222 | 1223 | 1225 | 1226 | 1228 | 1230 | 1232 | 1234 | 1237 |
| 20 | 1223 | 1225 | 1226 | 1228 | 1229 | 1231 | 1234 | 1236 | 1238 | 1241 |
| 220 | 1226 | 1228 | $12 \quad 29$ | 1231 | 1232 | 1235 | 1237 | 1240 | 1243 | 1246 |
| 240 | 1228 | 1230 | 1232 | 1234 | I2 36 | 1238 | 124 I | 1244 | 1247 | 1250 |
| 30 | 1231 | 1232 | 1235 | 1237 | 1239 | 1241 | 1244 | 1248 | 1251 | 1255 |
| 320 | 1233 | 1235 | 1237 | 1240 | 1242 | 1245 | 1248 | 1252 | 1255 | 130 |
| 340 | 1235 | $123^{8}$ | 1240 | 1243 | 1246 | 1249 | 1252 | 1256 | 130 | 134 |
| 40 | 1238 | 1240 | 1243 | 1246 | 1249 | 1252 | 1256 | 130 | I3 4 | 139 |
| 420 | 1240 | 1243 | 1246 | 1249 | 1252 | 1255 | 1259 | 13 | 138 | 1314 |
| 440 | 1243 | 1246 | 1249 | 1252 | 1255 | 1259 | 133 | 138 | 1313 | I3 19 |
| 50 | 1245 | 1248 | 1251 | 1255 | 1258 | 13 2 | 13 7 | 1312 | 1317 | 1323 |
| 520 | 1247 | 1251 | 1254 | 1258 | 13 | 136 | 13 II | 1316 | 1322 | I3 28 |
| 540 | 1250 | 1253 | 1257 | I3 I | 135 | 1310 | I3 14 | I3 20 | I3 26 | I3 33 |
| 60 | 1253 | 1256 | 1259 | 134 | 138 | 1313 | 1318 | 1324 | 1331 | 1338 |
| 620 | 1255 | 1259 | 132 | 137 | 13 Ir | 1316 | I3 22 | I3 28 | I3 35 | 1343 |
| 640 | 1258 | 13 I | 135 | I3 10 | 13 I4 | 1320 | 1326 | I3 32 | I3 39 | I3 47 |
| 70 | 130 | 134 | 138 | 13 I3 | 1318 | 1323 | 1329 | $13 \quad 36$ | 1344 | 1352 |
| 720 | I3 2 | 13 | 13 II | 1316 | 1321 | 1327 | I3 33 | 1340 | 1348 | 1357 |
| 740 | 135 | I3 9 | 1314 | I3 I9 | I3 25 | 13 3I | 1337 | I3 44 | 1353 | 142 |
|  | I3 7 | 1312 | 1317 | I3 22 | 1328 | 1334 | I3 4I | 1348 | 13 57 | $14 \quad 7$ |

Smithsonian Tableg.

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $+8^{\circ} 0^{\prime}$ | 127 | 12 I 3 | 12 I 8 | 1224 | 1231 | 1238 | 1245 | 1253 | 133 |
| 820 | 127 | 1213 | 12 I9 | 1225 | 1232 | 1239 | 1247 | 1255 | I3 5 |
| 840 | 127 | 12 I3 | 1219 | 1226 | 1233 | 1240 | 1248 | 1257 | I3 8 |
| 90 | 127 | 1213 | 1220 | 1226 | 1234 | 1241 | 1250 | 1259 | 13 Io |
| 920 | 127 | 1213 | 1220 | $\begin{array}{ll}12 & 27\end{array}$ | 1235 | 1243 | 1252 | 13 I | 1313 |
| 940 | 127 | 1214 | 1221 | 1228 | 1236 | 1244 | 1253 | I3 3 | 1314 |
| 100 | 127 | 1214 | 1221 | 1229 | 1237 | 1245 | 1255 | 135 | 1317 |
| 1020 | 127 | 1214 | 1222 | 1229 | 1238 | 1247 | 1256 | I3 7 | 1319 |
| 1040 | 127 | 1214 | 1222 | 1230 | 1239 | 1248 | 1258 | I3 9 | 1322 |
| 110 | 127 | 12 I 5 | 1223 | 1231 | 1240 | 1249 | 1259 | 13 II | 1324 |
| II 20 | 127 | 12 I 5 | 1223 | 1232 | 124 I | 1250 | 13 I | 1313 | 1326 |
| II 40 | 127 | 1215 | 1224 | 1232 | 1242 | 1252 | I3 2 | 1315 | I3 29 |
| 120 | 127 | 12 I 5 | 1224 | 1233 | 1243 | 1253 | 134 | 1317 | 13 3I |
| 1220 | 127 | 1216 | 1225 | 1234 | 1244 | 1255 | I3 6 | 1319 | I3 34 |
| 1240 | 127 | 1216 | 1225 | 1235 | 1245 | 1256 | I3 8 | I3 2I | I3 36 |
| 130 | 127 | 1216 | 1226 | I2 35 | 1246 | 1257 | 139 | 1323 | 1338 |
| 1320 | 127 | 1216 | 1226 | 1236 | 1247 | 1258 | I3 II | I3 25 | 13 4I |
| I3 40 | 127 | 12 I 7 | 1227 | 1237 | 1248 | I3 0 | I3 I3 | 1327 | 1343 |
| 140 | 127 | 1217 | 1227 | 1238 | 1249 | 13 | 1314 | 1329 | 1346 |
| 1420 | 127 | 1217 | 1228 | 1239 | 1250 | 13 | 1316 | I3 3I | I3 48 |
| 1440 | 127 | 1217 | 1228 | 1240 | 1251 | I3 4 | I3 I7 | I3 33 | 13 5I |
| 150 | 127 | 12 I 8 | 1229 | 1240 | 1252 | 135 | 13 I9 | I3 35 | 1353 |
| 1520 | 127 | 12 I 8 | 1229 | 1241 | 1253 | 137 | I3 2I | 1337 | I3 56 |
| 1540 | 127 | 12 I 8 | 1230 | 1241 | 1254 | I3 8 | I3 23 | I3 39 | 1358 |
| 160 | 127 | 12 I9 | 1230 | 1242 | 1255 | 139 | I3 25 | 13 4I | 14 I |
| 1620 | 127 | 1219 | 1231 | 1243 | 1256 | 13 II | I3 26 | I3 43 | 143 |
| 1640 | 127 | 12 I9 | 1231 | 1244 | 1258 | I3 12 | I3 28 | 1345 | I4. 6 |
| 170 | 127 | 12 I9 | 1232 | 1245 | 1259 | 1313 | I3 29 | I3 47 | 148 |
| 1720 | 127 | 1220 | 1232 | 1246 | I3 0 | I3 I5 | I3 31 | I3 50 | 14 II |
| 1740 | 127 | 1220 | 1233 | 1246 | 13 I | I3 16 | 1333 | I3 52 | I4 I4 |
| 180 | 127 | 1220 | 1233 | 1247 | 132 | 1317 | I3 35 | I3 54 | 1416 |
| 1820 | 127 | 1220 | 1234 | 1248 | I3 3 | I3 I9 | 1337 | I3 56 | 1419 |
| 1840 | 127 | 1221 | 1234 | 1249 | I3 4 | 1320 | 1338 | 1358 | 1422 |
| 190 | 127 | 1221 | 1235 | 1250 | 135 | 1322 | 1340 | 14 o |  |
| 1920 | 127 | 1221 | 1235 | 1251 | I3 6 | I3 23 | 1342 | $14 \quad 2$ | 1426 |
| 1940 | 127 | 1222 | 1236 | 1252 | I3 7 | I3 25 | 1344 | 145 | I4 29 |
| 200 | 127 | 1222 | 1236 | 1252 | I3 8 | I3 26 | I3 46 | 147 | 1432 |
| 2020 | 127 | 1222 | 1237 | 1253 | 13 Io | I3 28 | I3 47 | 14 Io | 1435 |
| 2040 | 127 | 1222 | 1237 | 1254 | 13 II | I3 29 | I3 49 | 1412 | 1437 |
| 210 | 127 | 1223 | 1238 | 1255 | 1312 | 1331 | 13 5I | 1414 | 1440 |
| 2120 | 127 | 1223 | $12 \cdot 39$ | 1256 | 13 I3 | 1332 | I3 53 | 1416 | 1443 |
| 2140 | 127 | 1223 | 1239 | 1256 | 1314 | I3 34 | I3 55 | 1419 | 1446 |
| 220 | 127 | 1224 | 1240 | 1257 | 1316 | 1335 | I3 56 | 1421 | 1449 |
| 2220 | 127 | 1224 | 124 I | 1258 | I3 I7 | I3 37 | 1358 | 1423 | 1452 |
| 2240 | 127 | 1224 | 1241 | I2 59 | I3 18 | 1338 | 14 o | 1425 | 1454 |
| 230 | 12 | 1225 | 1242 | I3 0 | 1319 | I3 40 | $14 \quad 2$ | 1428 | 1457 |
| 2320 | 127 | 1225 | 1242 | 13 | I3 20 | 13 4I | 144 | I4 30 | 150 |
| $23 \quad 27$ | 127 | 1225 | 1243 | I3 I | I3 20 | I3 4I | 145 | 14 3I | 15 I |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $42^{\circ}$ | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | $52^{\circ}$ | $54^{\circ}$ | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $+8^{\circ} 0^{\prime}$ | $13 \quad 7$ | 1312 | 1317 | I3 22 | 1328 | I3 34 | I3 4I | 1349 | 1358 | 147 |
| 820 | 13 Io | I3 14 | I3 20 | I3 25 | 13 3I | I3 38 | I3 45 | I3 53 | 142 | I4 12 |
| 840 | I3 12 | I3 17 | I3 23 | I3 28 | 1334 | I3 4I | I3 49 | I3 57 | 146 | 1417 |
| 90 | 1315 | I3 20 | I3 25 | 1331 | 1338 | 1345 | I3 53 | 14 I | 14 II | 1422 |
| 920 | 1317 | I3 23 | I3 28 | I3 34 | 1341 | I3 49 | I3 56 | I4 5 | 14 I5 | 1426 |
| 940 | I3 20 | I3 25 | 13 3I | I3 38 | I3 44 | I3 $5^{2}$ | 14 o | 14 Io | 1420 | 1431 |
| 100 | I3 22 | 1328 | I3 34 | 1341 | 1348 | 1356 | 144 | I4 I4 | 1425 | 1436 |
| 1020 | I3 25 | 13 3I | 1337 | I3 44 | 13 5I | 1359 | 148 | 14 I8 | 1429 | I4 4I |
| 1040 | I3 28 | I3 34 | I3 40 | I3 47 | I3 55 | 143 | 1412 | 1422 | 1434 | I4 47 |
| 110 | I3 30 | 13136 | I3 43 | 1350 | 1358 | 147 | 1416 | 1427 | 1438 | 1452 |
| II 20 | I3 32 | I3 39 | I3 46 | I3 53 | 14 I | I4 10 | 1420 | 1431 | 1443 | 1457 |
| II 40 | I3 35 | I3 4I | I3 49 | I3 56 | 145 | 1414 | I4 24 | I4 35 | 1448 | I5 2 |
| 120 | 1338 | 1344 | I3 52 | 14 O | 148 | 14 I8 | I4 28 | 1440 | 1453 | I5 8 |
| 1220 | I3 40 | I3 47 | I3 55 | I4 3 | 1412 | 1422 | I4 32 | 1444 | 1458 | I5 I3 |
| 1240 | I3 43 | I3 50 | I3 58 | I4 6 | I4 16 | 1425 | I4 37 | 1449 | I5 2 | I5 I8 |
| 130 | I3 46 | I3 53 | 14 I | 14 IO | 1419 | 1429 | I4 4I | 14.53 | 157 | I5 23 |
| 1320 | I3 48 | 1356 | 144 | 1413 | 1422 | 1433 | 1445 | 1458 | I5 I3 | I5 29 |
| 1340 | I3 50 | I3 58 | 147 | 1416 | I4 26 | 1437 | 1449 | $15 \quad 2$ | 1517 | I5 35 |
| 140 | I3 53 | 14 I | 14 Io | 14 I9 | I4 29 | 1441 | 1453 | 157 | 1522 | I5 40 |
| 1420 | I3 56 | I4 4 | 1413 | 1423 | I4 33 | 1445 | 1457 | 15 II | 1528 | I5 46 |
| 1440 | I3 59 | I4 7 | I4 I6 | I4 26 | 1437 | 1449 | $15 \quad 2$ | I5 16 | 1533 | I5 51 |
| 150 | 14 | 14 Io | 1419 | 1429 | 1440 | 1452 | I5 6 | 15 21 | 1538 | I5 57 |
| 1520 | I4 4 | 1413 | I4 22 | 1433 | I4 44 | 1456 | I5 10 | 1526 | 1543 | 162 |
| 1540 | 147 | 1416 | 1426 | 1436 | 1448 | 15 o | I5 14 | I5 30 | 1548 | 168 |
| 160 | 1410 | I4 I9 | I4 29 | 1440 | 1452 | 154 | 1519 | 1535 | 1553 | I6 I4 |
| 1620 | 1412 | 1422 | 1432 | 1443 | 1455 | I5 8 | 1523 | 1540 | 1559 | 1620 |
| 1640 | I4 15 | I4 25 | I4 35 | I4 46 | 1459 | 15 I3 | I5 28 | 1545 | 164 | I6 26 |
| 170 | 14 I7 | $14 \quad 28$ | 1438 | 1450 | I5 3 | 15 I7 | $15 \quad 32$ | 1550 | 16 Io | 1632 |
| 1720 | I4 20 | I4 3I | I4 4I | I4 53 | I5 7 | I5 21 | I5 37 | I5 55 | 16 I | 1638 |
| 1740 | I4 23 | I4 34 | 1445 | 1457 | 1510 | 1525 | I5 41 | 16 o | 1620 | 1645 |
| 180 | 1426 | I4 37 | 1448 | 15 I | 15 I 4 | 1529 | I5 46 | 165 | I6 26 | 16 5I |
| $18 \quad 20$ | I4 29 | 1440 | 1452 | I5 4 | I5 18 | I5 34 | I5 50 | 16 Io | 1632 | 1658 |
| I8 40 | 1432 | 1443 | I4 55 | I5 8 | I5 22 | I5 38 | I5 55 | 16 I5 | 1638 | 174 |
| 190 | 1435 | I4 46 | I4 58 | 15 II | I5 26 | 1542 | 16 o | 1620 | 1644 | 17 II |
| I9 20 | I4 37 | 1449 | 15 | I5 I5 | I5 30 | I5 46 | $16 \quad 5$ | 1625 | 1650 | 17 I 7 |
| 1940 | I4 40 | $145^{2}$ | 15 | I5 I9 | I5 34 | 15 51 | 16 Io | 1631 | 1656 | 1724 |
|  | 1443 | I4 55 | 158 | 1522 | I5 38 | 1555 | 16 I 5 | 1637 | $17 \quad 2$ |  |
| $20 \quad 20$ | I4 46 | 1458 | 15 II | I5 26 | I5 42 | 160 | 1620 | 16 42 | 178 | 1738 |
| 2040 | 1449 | $15 \quad 2$ | 1515 | 1530 | I5 46 | 164 | 1625 | 1647 | 1714 | I7 46 |
| 210 | 1452 | 155 | I5 I9 | I5 34 | 1550 | 16 9 | 16 30 | 1653 | 1720 | 1753 |
| 2 L 20 | 1455 | I5 8 | 1522 | 1538 | 1555 | 1613 | 1635 | 1659 | I7 27 | 18 I |
| 2140 | 1458 | 15 II | I5 26 | I5 42 | I5 59 | 16 ı8 | 1640 | 175 | 1734 | 188 |
| 220 | 15 I | I5 14 | $15 \quad 29$ | I5 46 | 163 | 1623 | 1645 | 17 II | 1740 | I8 16 |
| 22.20 | I5 4 | 1518 | I5 33 | I5 49 | 16 | I6 28 | 1650 | 1717 | 1747 | I8 24 |
| 2240 | I5 7 | I5 22 | 1537 | 1553 | 1612 | 1632 | 1656 | 1723 | 1754 | I8 32 |
| 230 | 1510 | 1525 | 1540 | 1557 | 1616 | 1637 | 17 I | 1729 | 18 I | 184 I |
| 2320 | I5 13 | I5 28 | 1544 | 16 I | 1621 | 1642 | 17 | 1735 | I8 8 | I8 49 |
| 2327 | I5 14 | I5 29 | I5 46 | 163 | 1623 | 1644 | I7 9 | 1737 | 18 II | I8 52 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $60^{\circ}$ | $61^{\circ}$ | $62^{\circ}$ | $63^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | $67^{\circ}$ | $68^{\circ}$ | $69^{\circ}$ | $70^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h.m. |
| $-23^{\circ} 27^{\prime}$ | 552 | 53 I | 58 | 442 | 4 II | 334 | 246 | I 29 |  |  |  |
| $-2320$ | 555 | 534 | 512 | 446 | 416 | 340 | 253 | I 41 |  |  |  |
| -23 o | 62 | 543 | 521 | 456 | 428 | 353 | 3 II | 2 II |  |  |  |
| -22 40 | 610 | 55 I | 530 | 56 | 439 | 47 | 327 | 235 | - 59 |  |  |
| 2220 | 617 | 559 | 539 | 516 | 450 | 420 | 343 | 256 | I 43 |  |  |
| 22 o | 625 | 67 | 547 | 525 | 5 I | 432 | 358 | 314 | 2 I 3 |  |  |
| -2140 | 632 | 614 | 556 | 534 | 5 II | 443 | 4 II | 3 3I | 238 | 1 I |  |
| -21 20 | 639 | 622 | 64 | 543 | 520 | 455 | 424 | 347 | 259 | 145 |  |
| 210 | 646 | 629 | 612 | 552 | 530 | 55 | 436 | 4 I | 318 | 216 |  |
| -20 40 | 652 | 637 | 620 | 6 I | 540 | 516 | 448 | 416 | 335 | 2 4I | 12 |
| - 2020 | 659 | 644 | 627 | $6 \quad 9$ | 549 | 526 | 459 | 429 | 351 | 32 | I 47 |
| -20 0 | 75 | 651 | 634 | 617 | 558 | 535 | 5 10 | 4 4I | 46 | 322 | 219 |
| $-1940$ | 712 | 658 | 642 | 625 | 66 | 545 | 52 I | 453 | 420 | 339 | 244 |
| - I9 20 | 718 | 74 | 649 | 633 | 6 I4 | 554 | 531 | 55 | 434 | 355 | 36 |
| - I9 0 | 725 | 7 II | 656 | 64 I | 623 | 63 | 54 I | 516 | 447 | 4 II | 326 |
| -1840 | 731 | 717 | 74 | 648 | 631 | 612 | 5 5I | 526 | 459 | 425 | 344 |
| - I8 20 | 737 | 724 | 7 Io | 655 | 639 | 620 | 6 I | 537 | 5 II | 439 | 4 I |
| - I8 o | 743 | 731 | 717 | 73 | 647 | 629 | 6 10 | 547 | 522 | 452 | 416 |
| $-1740$ | 749 | 737 | 724 | 7 10 | 655 | 638 | 619 | 557 | 533 | 55 | 431 |
| $-1720$ | 755 | 743 | 731 | 717 | 72 | 646 | 628 | 67 | 543 | 517 | 445 |
| $-170$ | 8 I | 749 | 737 | 724 | 79 | 653 | 636 | 616 | 554 | 528 | 458 |
| $-1640$ | 86 | 755 | 744 | 731 | 7 I7 | 7 I | 644 | 626 | 64 | 540 | 5 II |
| - I6 20 | 812 | 8 I | 750 | 738 | 724 | $7 \quad 9$ | 652 | 635 | 614 | 551 | 523 |
| - 16 o | 817 | 87 | 756 | 744 | 731 | 717 | 7 I | 644 | 624 | 62 | 535 |
| $-1540$ | 823 | 813 | $8 \quad 2$ | 7 51 | 738 | 725 | $\begin{array}{ll}7 & 9\end{array}$ | 652 | 634 | 612 | 547 |
| - I5 20 | 829 | 8 I9 | 8 8 | 758 | 745 | 732 | 717 | 7 I | 643 | 622 | 559 |
| - 15 o | 834 | 825 | 815 | 84 | 752 | 739 | 725 | 79 | 652 | 632 | 6 10 |
| -14 40 | 840 | 831 | 821 | 810 | 759 | 746 | 732 | 717 | 7 I | 642 | 620 |
| - 14 20 | 845 | 836 | 827 | 8 I7 | 85 | 753 | 740 | 726 | 710 | 651 | 63 I |
| - I4 0 | 850 | 842 | 833 | 823 | 812 | 8 I | 747 | 734 | 7 I 8 | 7 I | 64 I |
| -13 40 | 856 | 847 | 838 | 829 | 8 19 | 87 | 755 | 7 4I | 726 | 7 10 | 651 |
| - I3 20 | 91 | 853 | 844 | 835 | 825 | 814 | 82 | 749 | 735 | 719 | 7 I |
| - I3 0 | 96 | 858 | 850 | 84 I | 832 | 821 | 8 го | -757 | 743 | 728 | 7 10 |
| $-1240$ | 9 II | 94 | 856 | 847 | 838 | 828 | 817 | 85 | 7 51 | 737 | 720 |
| - 1220 | 917 | 9 10 | 92 | 853 | 844 | 834 | 824 | 812 | 759 | 745 | 729 |
| I2 0 | 922 | 915 | 97 | 859 | 850 | 841 | 831 | 820 | 87 | 753 | 738 |
| - 1140 | 927 | 920 | 913 | 95 | 856 | 847 | 838 | 827 | 815 | $8 \quad 2$ | 747 |
| - II 20 | 932 | 925 | 919 | 9 II | 93 | 854 | 844 | 834 | 823 | 810 | 756 |
| 110 | 937 | 931 | 924 | 917 | 99 | 90 | 85 I | 84 I | 83 I | 8 I8 | 85 |
| $-1040$ | 942 | 936 | 929 | 922 | 915 | 97 | 858 | 849 | 838 | 826 | 814 |
| - 1020 | 947 | 941 | 935 | 928 | 921 | 913 | 95 | 856 | 846 | 834 | 822 |
| - 100 | 952 | 946 | 940 | 934 | 927 | 919 | 9 II | 93 | 853 | 842 | 83 I |
| $-940$ | 957 | 951 | 946 | 940 | 933 | 926 | 918 | 910 | 9 O | 850 | 839 |
| - 920 | 102 | 956 | 951 | 945 | 939 | 932 | 925 | 916 | 98 | 858 | 847 |
| - 90 | 10 7 | IO 2 | 956 | 950 | 944 | 938 | 931 | 923 | 915 | 95 | 855 |
| $-840$ | 10 II | 10 7 | $10 \quad 2$ | 956 | 950 | 944 | 937 | 930 | 922 | 9 I3 | 93 |
| - 820 | 1016 | 1012 | 10 7 | IO 2 | 956 | 950 | 944 | 937 | 929 | 921 | 9 II |
| - 80 | IO 21 | IO 17 | 1012 | 10 7 | 10 2 | 956 | 950 | 943 | 936 | 928 | 919 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.


DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $60^{\circ}$ | $61^{\circ}$ | $62^{\circ}$ | $63^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | $67^{\circ}$ | $68^{\circ}$ | $69^{\circ}$ | $70^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} 0^{\prime}$ | 10 21 | 1017 | 10 | 10 7 | Io | 956 | 950 | 943 | 936 | 928 | 9 I9 |
| -740 | IO 26 | 1022 | 1017 | IO I3 | 10 8 | Io 2 | 956 | 950 | 943 | 935 | 927 |
| $-7 \quad 20$ | Io 3I | 10 27 | 1023 | IO 18 | 1013 | 10 8 | Io 3 | 957 | 950 | 943 | 935 |
| 7 - | 1035 | 1032 | 1028 | IO 23 | 1019 | 10 I 4 | IO 9 | IO 4 | 957 | 950 | 943 |
| --640 | 10 40 | 10 37 | 10 33 | 10 29 | 10 25 | 1020 | 10 15 | 10 10 | Io 4 | 957 | 951 |
| 620 | Io 45 | 10 42 | 10 38 | Io 34 | 10 31 | 10 26 | 10 22 | Io 16 | 10 II | 10 5 | 958 |
| 6 - | to 50 | 10 47 | 10 43 | 10 40 | 10 36 | 10 32 | 1028 | IO 23 | Io 18 | 1012 | 10 6 |
| -5 40 | Io 55 | IO 52 | 10 49 | 10 45 | 1041 | 10 38 | 10 34 | IO 29 | IO 25 | 1019 | 1014 |
| -5 20 | 1059 | 10 56 | Io 54 | 1050 | 1047 | Io 44 | 1040 | 10 36 | 1031 | Io 26 | 1021 |
| -5 0 | II 4 | II I | Io 59 | IO 56 | 1053 | 1050 | 10 46 | IO 42 | Io 38 | Io 34 | 1029 |
| -4 40 | II 8 | II 6 | II 4 | II I | Io 58 | Io 55 | 1052 | 1049 | IO 45 | 1041 | 10 36 |
| -4 20 | II I3 | II II | II 9 | II 7 | II 4 | II 1 | 1058 | 10 55 | Io 52 | 10 48 | Io 44 |
| - 0 | II I8 | II I6 | II I4 | II I2 | II 10 | II 7 | II 4 | II 1 | Io 58 | IO 55 | 1051 |
| -3 40 | II 22 | II 2I | II 19 | II 17 | II 15 | II 13 | II 10 | II 8 | II 5 | II 2 | 10 59 |
| 320 | II 27 | II 26 | II 24 | II 22 | II 20 | II 19 | II 16 | II 14 | II II | II 9 | II 6 |
| -3 | II 32 | II 3 I | II 29 | II 28 | II 26 | II 24 | II 22 | II 20 | II I8 | II 16 | II I3 |
| -2 40 | II 37 | II 35 | II 34 | II 33 | II 3I | II 30 | II 28 | II 27 | II 25 | II 23 | II 21 |
| 220 | II 41 | II 40 | II 39 | II 38 | II 37 | II 36 | II 34 | II 33 | II 32 | II 30 | II 28 |
| 20 | II 46 | II 45 | II 44 | II 43 | II 43 | II 4I | II 40 | II 40 | II 38 | II 37 | II 35 |
| - 140 | II 50 | II 50 | II 49 | II 49 | II 48 | II 47 | II 46 | II 46 | II 45 | II 44 | II 43 |
| 120 | II 55 | II 55 | II 54 | II 54 | II 53 | II 53 | II 52 | II 52 | II 52 | II 5I | II 50 |
| 10 | II 59 | II 59 | II 59 | II 59 | II 59 | II 59 | II 58 | II 58 | II 58 | II 58 | II 58 |
| -040 | 124 | I2 4 | 124 | 124 | 124 | 124 | 124 | 124 | 125 | $\begin{array}{ll}12 & 5\end{array}$ | 125 |
| O 20 | 129 | 129 | 129 | 1210 | 1210 | 1210 | 12 10 | 12 II | 12 II | 1212 | 1212 |
| 00 | 1213 | 1214 | 12 I 4 | 1215 | I2 I5 | 1216 | 1216 | 1217 | 12 I | 1219 | 1219 |
| +o 20 | I2 I8 | 1219 | 1219 | 1220 | 1220 | 1222 | 1222 | 1223 | 1225 | 1226 | 1227 |
| - 40 | 1222 | 1223 | 1224 | I2 25 | 1226 | 1227 | 1228 | 1229 | 123 I | 1233 | 1234 |
| 10 | 1227 | 1228 | 1229 | I2 31 | 1232 | 1233 | I2 34 | 1236 | 1238 | 1240 | 1241 |
| I 20 | 1232 | 1233 | I2 34 | 1236 | 1237 | 1239 | 1240 | 1242 | 1244 | 1247 | 1249 |
| I 40 | 1237 | 1238 | 1239 | 124 I | 1243 | 1244 | 1246 | 1249 | 1251 | 1254 | 1256 |
| 20 | 1241 | 1243 | 1244 | 1246 | 1248 | 1250 | 1252 | 1255 | 1258 |  | I3 4 |
| 220 | 1246 | 12 47 | 1249 | 1252 | 1253 | 1256 | 1259 | 13 I | 134 | 138 | 13 II |
| 240 | 1250 | 1252 | 1254 | 1257 | 1259 | 132 | I3 5 | I3 7 | I3 II | 1315 | I3 19 |
| 30 | I2 55 | 1257 | 1259 | I3 2 | 135 | 138 | 13 II | 1314 | 1317 | 1322 | I3 26 |
| 320 | I3 0 | I3 2 | I3 5 | I3 7 | I3 10 | 13 I3 | 1317 | 1320 | 1324 | I3 29 | I3 34 |
| 340 | I3 4 | I3 7 | 1310 | I3 I3 | I3 I6 | 1319 | 1323 | I3 27 | 1331 | I3 36 | 1341 |
| 40 | I3 9 | I3 I2 | I3 15 | 1318 | 1322 | 1325 | 1329 | I3 33 | 1338 | 1343 | I3 49 |
| 420 | I3 I4 | 1317 | 1320 | 1323 | 1327 | 1331 | 1335 | I3 40 | 1345 | I3 50 | 1356 |
| 440 | I3 19 | I3 22 | I3 25 | I3 29 | I3 32 | I3 37 | 1341 | I3 46 | 1352 | 1358 | 144 |
| 50 | I3 23 | I3 27 | I3 30 | I3 34 | I3 38 | I3 43 | 1347 | I3 53 | $135^{8}$ | $14 \quad 5$ | 14 II |
| 520 | 1328 | I3 32 | I3 35 | I3 40 | I3 44 | I3 49 | 1354 | I3 59 | 14 | 14 I2 | 1419 |
| 540 | I3 33 | I3 37 | I3 4I | I3 45 | 1350 | I3 55 | 14 O | 146 | 1412 | 1419 | 1427 |
| 60 | 1338 | 13 42 | 1346 | 1350 | I3 55 | 14 I | 146 | 1413 | 1419 | 1426 | 1435 |
| 620 | I3 43 | I3 47 | I3 51 | I3 56 | 14 I | 147 | 1412 | 1419 | 1426 | 1434 | 1443 |
| 640 | I3 47 | I3 52 | 13 56 | 14 I | 147 | 14 I3 | 14 I 8 | 1426 | 1433 | 1442 | 1451 |
| 70 | I3 52 | I3 57 | 14 I | 147 | 1412 | 1419 | 1425 | 1432 | 1440 | 1449 |  |
| 720 | I3 57 | 142 | $14 \quad 7$ | 1413 | 1418 | 1425 | 1431 | 1439 | I4 48 | 1457 | 15 |
| 740 | 142 | 147 | 1412 | 1418 | 1424 | 1431 | 1438 | 1446 | I4 55 | I5 4 | I5 I5 |
| 80 | 147 | 14 I 2 | 1417 | 1423 | 1430 | 1437 | 1445 | I4 52 | I5 2 | 1512 | 1523 |

Smithsonian Tables.

Table 61.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| Declination of the Sun. | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $71^{\circ}$ | $72^{\circ}$ | $73^{\circ}$ | $74^{\circ}$ | $75^{\circ}$ | $76^{\circ}$ | $77^{\circ}$ | $78^{\circ}$ | $79^{\circ}$ | $80^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} 0^{\prime}$ | 9 1о | 859 | 847 | 833 | 817 | 758 | 737 | 7 10 | 638 | 556 |
| -740 | 918 | 908 | 856 | 843 | 828 | 8 II | 750 | 726 | 656 | 6 I8 |
| -720 | 926 | 917 | 96 | 853 | 839 | 823 | 84 | 741 | 7 I4 | 638 |
| -7 o | 935 | 926 | 9 16 | 93 | 850 | 835 | 817 | 756 | 7 31 | 658 |
| -640 | 943 | 934 | 925 | 914 | 9 I | 847 | 830 | 8 II | 747 | 7 I7 |
| -6 20 | 9 5I | 943 | 934 | 924 | 912 | 859 | 843 | 825 | 83 | 736 |
| -6 | 959 | 952 | 943 | 934 | 923 | 9 II | 856 | 839 | 8 I9 | 754 |
| -540 | 10 7 | 101 | 953 | 944 | 934 | 922 | 99 | 853 | 834 | 8 II |
| 520 | 10 15 | IO 9 | IO 2 | 953 | 944 | 934 | 922 | 97 | 850 | 828 |
| -5 | I0 23 | 1017 | IO II | 10 3 | 955 | 945 | 934 | 920 | 95 | 846 |
| -440 | Io 31 | Io 26 | Io 20 | 1013 | 105 | 956 | 946 | 934 | 9 I9 | 92 |
| -420 | IO 39 | IO 34 | IO 29 | IO 22 | 1015 | 10 7 | 958 | 947 | 934 | 918 |
| -4 o | IO 47 | IO 43 | IO 38 | IO 32 | IO 26 | Io I8 | Io Io | 10 O | 949 | 934 |
| -340 | Io 55 | 10 5 I | Io 46 | IO 4I | Io 36 | IO 29 | IO 22 | 10 I3 | IO 3 | 950 |
| -320 | II 3 | Io 59 | IO 55 | Io 5I | IO 46 | IO 40 | IO 34 | 10 26 | IO 17 | Io 6 |
| 30 | II II | II 8 | II 4 | II 0 | IO 56 | Io 5 I | 10 45 | Io 39 | Io 3 I | IO 22 |
| -2 40 | II 19 | II 16 | II 13 | II Io | II 6 | II 2 | IO 57 | IO 52 | IO 45 | IO 37 |
| 220 | II 26 | II 24 | II 22 | II 19 | II I6 | II I3 | II 8 | II 4 | Io 59 | Io 52 |
| 20 | II 34 | II 32 | II 3I | II 28 | II 26 | II 23 | II 20 | II 17 | II I3 | II 8 |
| - 140 | II 42 | II 41 | II 39 | II 38 | II 36 | II 34 | II 32 | II 29 | II 26 | II 23 |
| 120 | II 49 | II 49 | II 48 | II 47 | II 46 | II 45 | II 43 | II 42 | II 40 | II 38 |
| 10 | II 57 | II 57 | II 56 | II 56 | II 56 | II 55 | II 55 | II 55 | II 54 | II 53 |
| -040 | 125 | 125 | 125 | 125 | 126 | 126 | 127 | 127 | I2 8 | 128 |
| O 20 | 12 I3 | 12 I3 | 1214 | 12 I5 | 1216 | $\begin{array}{lll}12 & 17\end{array}$ | 1218 | 1220 | 1221 | 1223 |
| 00 | 1220 | 1222 | 1222 | 1224 | 1226 | 1228 | 1229 | 1232 | 1235 | 1238 |
| +020 | 1228 | 1230 | 1231 | 1234 | 1236 | 1238 | 1241 | 1244 | 1249 | 1253 |
| O 40 | 1236 | 1238 | 1240 | 1243 | 1246 | I2 49 | 1253 | 1257 | I3 2 | I3 9 |
| 10 | 1244 | 1246 | 1249 | 1252 | 1256 | 130 | I3 5 | 1310 | 1316 | I3 24 |
| I 20 | 1252 | 1255 | 1258 | I3 2 | I3 6 | I3 II | I3 16 | I3 23 | I3 30 | I3 40 |
| 140 | 1259 | I3 3 | I3 7 | I3 II | I3 I6 | I3 22 | I3 28 | I3 36 | I3 44 | I3 55 |
| 20 | 137 | 13 II | 1316 | I3 20 | I3 26 | I3 32 | 1340 | I3 49 | 1359 | I4 II |
| 220 | 13 I5 | I3 19 | I3 25 | I3 30 | I3 36 | I3 43 | 1352 | I4 I | 14 I3 | 1427 |
| 240 | I3 23 | I3 28 | I3 33 | I3 40 | I3 46 | I3 54 | I4 4 | 1414 | I4 28 | 1443 |
| 30 | I3 3I | 1336 | I3 42 | I3 49 | I3 57 | 145 | 1416 | I4 28 | 1442 | 1459 |
| 320 | I3 39 | I3 44 | 1351 | 1359 | 147 | 1417 | I4 28 | 1441 | 1456 | I5 16 |
| 340 | I3 47 | I3 53 | I4 I | 148 | 1417 | 1428 | I4 40 | 1455 | I5 II | I5 33 |
| 40 | 1355 | $14 \quad 2$ | 14 IO | 1418 | 1428 | 1440 | 1453 | I5 8 | 1527 | I5 50 |
| 420 | I4 3 | I4 10 | I4 19 | I4 28 | I4 $3^{8}$ | 1451 | I5 5 | I5 22 | I5 43 | 167 |
| 440 | 14 II | I4 19 | I4 28 | 1438 | I4 49 | 152 | I5 I8 | I5 36 | I5 58 | 1625 |
| 50 | I4 19 | 1428 | 1437 | 1448 | I5 0 | 15 | 1531 | 1550 | 16 I 4 | 1644 |
| 520 | 1427 | I4 37 | 1446 | 1458 | 15 II | I5 26 | 1544 | 165 | 1631 | 17 |
| 540 | I4 35 | I4 45 | I4 56 | 158 | I5 22 | I5 38 | I5 57 | 1620 | 1647 | 1722 |
| 60 | I4 44 | 1454 | $15 \quad 5$ | 15 I9 | 1533 | 1550 | 16 II | 16 35 | I7 5 | 1743 |
| 620 | I4 52 | $15 \quad 3$ | 15 | I5 29 | I5 44 | 163 | 1625 | 1651 | 1723 | I8 5 |
| 640 | 15 I | 15 I2 | I5 25 | I5 40 | 1556 | 16 I6 | I6 39 | 177 | 1741 | I8 27 |
| 70 | $\mathrm{I}_{5} \mathrm{Io}$ | I5 22 | I5 35 | 1550 | 168 | 1629 | 1653 | 1723 | I8 I | I8 50 |
| 720 | 15 | 1231 | 1545 | 16 I | 1620 | I6 42 | 178 | 1740 | 1821 | I9 16 |
| 740 | I5 27 | I5 40 | 1555 | 1612 | I6 32 | 1655 | 1723 | 1758 | I8 42 | I9 44 |
| 80 | I5 35 | 1550 | 165 | 1623 | I6 44 | I7 9 | 1739 | I8 16 | I9 5 | 2015 |

TABLE 61.

## DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $60^{\circ}$ | $61^{\circ}$ | $62^{\circ}$ | $63^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | $67^{\circ}$ | $68^{\circ}$ | $69^{\circ}$ | $70^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $+8^{\circ} 0^{\prime}$ | $14 \quad 7$ | 1412 | 1417 | 1423 | 1430 | 1437 | 1445 | 1453 | $15 \quad 2$ | 1512 | 1523 |
| 820 | 1412 | 14 It | 1423 | 1429 | 1436 | 1443 | 1452 | 150 | 1510 | 1520 | 1532 |
| 840 | 14 17 | 1422 | 1428 | I4 35 | 1442 | 1450 | 1458 | I5 7 | 1517 | 1528 | I5 40 |
| 90 | 1422 | 1427 | 1434 | 1441 | 1448 | 1456 | $15 \quad 5$ | 1514 | I5 25 | I5 36 | 1549 |
| 920 | 1427 | 1432 | 1439 | 1446 | 1454 | 152 | 15 II | 15.21 | I5 32 | I5 44 | I5 57 |
| 940 | 1432 | 1438 | 1445 | 1452 | 150 | I5 9 | 1518 | 1528 | 1540 | I5 52 | 166 |
| 100 | 1437 | 1443 | 1450 | 1458 | 156 | 1515 | 1525 | I5 35 | I5 47 | 16 o | 16 I5 |
| 1020 | 1442 | 1449 | 1456 | 154 | 1513 | 1522 | 1532 | I5 43 | I5 55 | 168 | 1624 |
| 1040 | 1447 | 1454 | 152 | 1510 | I5 I9 | 1528 | 1539 | 1550 | 163 | 1617 | 16 33 |
| 110 | 1452 | 1459 | 157 | 1516 | 1525 | 1535 | 1546 | I5 58 | I6 II | 1626 | 1642 |
| II 20 | 1457 | $15 \quad 5$ | 15 I3 | 1522 | 1531 | 1541 | 1553 | 165 | 1619 | 1634 | 1652 |
| II 40 | $15 \quad 2$ | 1510 | 1519 | 1528 | 1538 | 1548 | 16 o | 16 I3 | 16 27 | 1643 | I7 I |
| 120 | 158 | I5 16 | 1525 | I5 34 | 1544 | 1555 | 167 | 1621 | I6 35 | 1652 | 17 II |
| 1220 | 15 I 3 | I5 2I | 1531 | 1540 | 1550 | 162 | 1615 | 1629 | 1644 | 17 | I7 21 |
| 1240 | 15 I8 | 1527 | 1536 | 1546 | I5 57 | $16 \quad 9$ | 1622 | 1637 | I6 53 | 17 II | 1731 |
| 130 | 1523 | 1533 | 1542 | 1553 | 164 | I6 I6 | 1630 | 16 45 | 172 | 1720 | 1741 |
| 1320 | 1529 | 1539 | 1548 | 1559 | 16 II | 1623 | 1637 | 1653 | 1710 | 1730 | 1752 |
| 1340 | 1535 | 1544 | 1555 | 165 | 16 I7 | 1631 | 1645 | I7 I | I7 19 | 1740 | 183 |
| 140 | 1540 | I5 50 | 16 I | 16 I2 | 1624 | 1638 | 1653 | 1710 | 1729 | 1750 | 1814 |
| 1420 | 1546 | 1556 | 167 | 1619 | 163 I | 1646 | 17 I | 1719 | 1738 | 18 o | IS 26 |
| 1440 | 15 51 | 162 | 16 I 3 | 1625 | 1638 | I6 53 | 179 | 1728 | 1748 | I8 II | I8 38 |
| 150 | 1557 | 168 | 1619 | 1632 | 1646 | 17 I | 1717 | 1737 | 1758 | 1822 | I8 50 |
| 1520 | 162 | 1614 | 1626 | 1639 | 1653 | 178 | 1726 | I7 46 | 188 | 1833 | 193 |
| 1540 | 168 | 1620 | 1632 | 1646 | 17 I | 1717 | 1735 | 1755 | 18 I8 | 1845 | 1916 |
| 160 | 1614 | 1626 | 1639 | 1653 | 178 | 1725 | I7 44 | 185 | 1829 | 1857 | 1930 |
| 1620 | 1620 | 1632 | 1646 | 17 o | 1716 | 1733 | 1753 | I8 15 | 1840 | I9 Io | I9 45 |
| 1640 | 1626 | 1639 | 1652 | 177 | 1723 | 174 I | $18 \quad 2$ | 1825 | 1851 | 1923 | 201 |
| 170 | 1632 | 1645 | 1659 | 1714 | 1731 | 1750 | 18 II | 1835 | 193 | 1936 | 2017 |
| 1720 | 1638 | 1652 | 176 | 1722 | 1739 | 1759 | 1821 | 1846 | 19 I5 | 1950 | 2035 |
| 1740 | 1645 | 1658 | 1713 | 1729 | 1747 | 188 | 183 I | I8 57 | 19 28 | 206 | 2055 |
| 180 | 16 51 | 175 | 1720 | I7 37 | I7 56 | I8 17 | I8 4I | 19 8 | 1941 | 2022 | 2117 |
| 1820 | 1658 | 1712 | 1728 | 1745 | I8 5 | I8 26 | 1852 | 19 20 | 19 55 | 2040 | 2 I 42 |
| 1840 | 174 | 1719 | 1735 | 1753 | I8 I4 | I8 36 | I9 3 | 19 33 | 2010 | 2059 | 2213 |
| 190 | 17 II | 1726 | 1743 | 182 | 1823 | I8 46 | I9 I4 | 19 46 | 2026 | 2120 | 2258 |
| 1920 | 1717 | 1733 | 1751 | 18 ıo | 1832 | I8 56 | 1925 | 200 | 2044 | 2145 |  |
| 1940 | I7 24 | 1741 | 1759 | 1819 | 184 I | 197 | 1937 | 2014 | 2 I 3 | 2216 |  |
| 200 | I7 3I | 1748 | 187 | 1828 | 185 I | 19 I9 | 1950 | 2030 | 2I 23 | 2259 |  |
| 2020 | 1738 | 1756 | 1815 | 1837 | I9 I | 1930 | 204 | 2047 | 2447 |  |  |
| 2040 | 1745 | I8 4 | 1823 | 1846 | 19 I2 | 1942 | 2019 | 215 | 2217 |  |  |
| 210 | I7 52 | 14 II | 1832 | 1856 | 1923 | $1925$ | 2034 | 21 26 | 23 I |  |  |
| 2 L 20 | 18 o | 2820 | 184 I | 196 | I9 34 | 208 | 2050 | 2150 |  |  |  |
| 2140 | 188 | I8 28 | 1850 | 19 I6 | I9 46 | 2022 | 2 I 8 | 22 I9 |  |  |  |
| 220 | IS 16 | 1837 | I9 0 | 1927 | 1958 | 2037 | 21 29 | $23 \quad 2$ |  |  |  |
| 2220 | 1824 | I8 46 | 19 Io | 1938 | 2011 | 2053 | 2152 |  |  |  |  |
| 2240 | I8 32 | 1855 | I9 20 | 1950 | 2025 | 2111 | 2221 |  |  |  |  |
| 230 | 1841 | 194 | 1931 | $20 \quad 2$ | 2040 | 2131 | 233 |  |  |  |  |
| 2320 | 1849 | 19 I3 | I9 4I | 20 I4 | 2056 | 2154 |  |  |  |  |  |
| $23 \quad 27$ | I8 52 | 19 17 | 19 46 | 2019 | 2 I 2 | 223 |  |  |  |  |  |

8mithbonian Tableb.

## DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $71^{\circ}$ | $72^{\circ}$ | $73^{\circ}$ | $74^{\circ}$ | $75^{\circ}$ |
| $+8^{\circ} 0^{\prime}$ | h. m. | h. m. | h. m. | h. m. | h. m. |
|  | 1535 | 1550 | 165 | I6 23 | I6 44 |
| 820 | I5 44 | I5 59 | 1616 | 1635 | 16 57 |
| 840 | 1553 | 169 | 1626 | 1646 | 17 10 |
| 90 | 163 | 1619 | 16 37 | 1658 | 1723 |
| 920 | 16 I2 | 1629 | 1648 | 17 Io | I7 37 |
| 940 | 1622 | 1639 | 1659 | 1723 | 1751 |
| 100 | 1631 | 1650 | 17 II | 1735 | I8 5 |
| 1020 | 1641 | 17 | 1722 | 1749 | 1820 |
| IO 40 | 1650 | 17 II | 1734 | 182 | I8 36 |
| 110 | 17 I | 1722 | 1747 | 18 I6 | 1852 |
| II 20 | 17 II | 1734 | 1759 | 1831 | 199 |
| II 40 | 1722 | 1745 | 18 I3 | I8 46 | 19 27 |
| 120 | 1732 | 1757 | I8 26 | 19 I | I9 46 |
| 1220 | 1743 | 189 | 1840 | I9 18 | 207 |
| 1240 | 1755 | 1822 | 1855 | 1935 | 2029 |
| 130 | I8 6 | 1835 | 19 II | 1954 | 2055 |
| 1320 | I8 I8 | I8 49 | 1926 | 2014 | 2123 |
| I3 40 | 1830 | 192 | 1943 | 2035 | 21. 59 |
| $\begin{array}{rrr}14 & 0 \\ 14 & 20\end{array}$ | 1843 | 1917 | 20 I | 2 O | 2250 |
|  | I8 56 | I9 33 | 2020 | 2128 |  |
| 1440 | 1910 | I9 49 | 2041 | 222 |  |
| 150 | 1924 | 207 | 2 I 5 | 2252 |  |
| 1520 | I9 40 | 2026 | 2132 |  |  |
| 1540 | 1955 | 2046 | 225 |  |  |
| 160 | 2013 | 2110 | 2254 |  |  |
| 1620 | 20 3I | 2136 |  |  |  |
| 164 | 2051 | 228 |  |  |  |
| 17 | 2113 | 2256 |  |  |  |
| 17 17 17 | 2139 |  |  |  |  |
| 1740 | 22 II |  |  |  |  |
|  | $76^{\circ}$ | $77^{\circ}$ | $78^{\circ}$ | $79^{\circ}$ | $80^{\circ}$ |
| $+8^{\circ} 0^{\prime}$ | 179 | 1739 | 1816 | 195 | 20 I5 |
| 820 | 1723 | 1755 | I8 35 | 1929 | 2050 |
| 8 | 1738 | I8 12 | I8 56 | 1956 | 21 33 |
| 90 | I7 53 | 1830 | I9 17 | 2025 | 2235 |
| 920 | 188 | 1848 | 1941 | 2059 |  |
| 940 | IS 25 | 198 | 206 | 21 40 |  |
| 100 | I8 4 r | 1928 | 2031 | 2239 |  |
| 1020 | I3 59 | 1950 | 216 |  |  |
| IO 40 | 19 18 | 20 I5 | 21 46 |  |  |
| 110 | 1938 | 2041 | 2243 |  |  |
| II 20 | 1959 | 21.13 |  |  |  |
| II 40 | 2023 | 2I 50 |  |  |  |
| 120 | 2049 | 2246 |  |  |  |
| 1220 | 2119 |  |  |  |  |
| 1240 | 2I 55 |  |  |  |  |


| Day of Month | Jan. | Feb. | Mar. |
| :---: | :---: | :---: | :---: |
| 1 | $-22^{\circ} 59^{\prime}$ | $-17^{\circ} \mathrm{I}^{\prime}$ | $-7^{\circ} 29^{\prime}$ |
| 4 | 2242 | 168 | 620 |
| 7 | 22 21 | 15 I 3 | 5 10 |
| 10 | 2 I 55 | 14 I5 | 4 O |
| 13 | 2 L 26 | 1315 | 249 |
| 16 | -20 53 | $\begin{array}{lll}-12 & 14\end{array}$ | - I 38 |
| 19 | 2017 | II Io | -0 27 |
| 2 I | 1950 | 1027 | +o 21 |
| 24 | 198 | 921 | I 32 |
| 27 | 1823 | 814 | 242 |
| 30 | 1735 |  | 352 |
|  | Apr. | May. | June. |
| 1 | $+4^{\circ} 39^{\prime}$ | $+\mathrm{I} 5^{\circ}{ }^{\prime} \mathrm{IO}^{\prime}$ | $+22^{\circ} 6^{\prime}$ |
| 4 | 548 | 163 | 2228 |
| 7 | 656 | 1653 | 2247 |
| 10 | 83 | 1742 | 23 |
| 13 | $9 \quad 9$ | $18 \quad 27$ | 2314 |
| 16 | +10 13 | +19 10 | +23 22 |
| 19 | II 16 | 1950 | 2327 |
| 21 | II 57 | 2015 | $23 \quad 27$ |
| 24 | 1257 | 2049 | 2325 |
| 27 | I3 55 | 2 I 2I | 2320 |
| 30 | 1451 | 2149 | 23 II |
|  | July. | Aug. | Sept. |
| 1 | $+23^{\circ} 7^{\prime}$ | +17 $7^{\circ} 58^{\prime}$ | $+8^{\circ} \mathrm{I2}{ }^{\prime}$ |
| 4 | 2252 | 1712 | 76 |
| 7 | 2235 | 1622 | 559 |
| 10 | 22 I 3 | 1530 | 4 5I |
| 13 | 2149 | 1437 | 342 |
| 16 | +2I 21 | +13 41 | +233 |
| 19 | 2049 | 1243 | 123 |
| 2 I | 2027 | 123 | +o37 |
| 24 | 1950 | II 2 | -o 34 |
| 27 | 19 II | 959 | I 44 |
| 30 | $18 \quad 28$ | 855 | 254 |
|  | Oct. | Nov. | Dec. |
| 4 | $-3^{3^{\circ}} 17^{\prime}{ }^{\prime}$ | $\begin{array}{rrr}-14^{\circ} & 32^{\prime} \\ 15 & 28\end{array}$ | $\left\lvert\, \begin{array}{cc} -2 I^{\circ} 52^{\prime} \\ 22 & 18 \end{array}\right.$ |
| 4 | 427 | I5 28 | 22 I8 |
| 7 | 536 | 1622 | $\begin{array}{lll}22 & 39\end{array}$ |
| 10 | 645 | 1714 | 2257 |
| 13 | 753 | I8 3 | 23 II |
| 16 | $-859$ | -I8 49 | $-231$ |
| 19 | 105 | 1933 | 2326 |
| 21 | Io 48 | 20 0 | 2327 |
| 24 | 1151 | 2037 | 2326 |
| 27 | 1253 | $2 \mathrm{I} \quad 12$ | 2320 |
| 30 | I3 53 | 2I 42 | 23 IO |

## RELATIVE INTENSITY OF SOLAR RADIATION.

Mean vertical intensity for 24 hours of solar radiation $J$ and the solar constant $A$, in terms of the mean solar constant $A_{0}$.

| Date. | Motion of the Sun in Longitude. | RELATIVE MEAN VERTICAL INTENSITY $\left(\frac{J}{A_{0}}\right)$. |  |  |  |  |  |  |  |  |  | $\frac{A}{A_{\circ}}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
|  |  | $0^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ | $90^{\circ}$ |  |
| Jan. I | 0.99 | 0.303 | 0.265 | 0.220 | 0.169 | 0.117 | 0.066 | 0.018 |  |  |  | 1.0335 |
|  | 15.78 | . 307 | . 271 | . 229 | . 180 | . 129 | . 078 | . 028 |  |  |  | 1.0324 |
| Feb. I | 31.54 | -312 | . 282 | . 244 | . 200 | . 150 | . 100 | . 048 | 0.006 |  |  | 1.0288 |
| 15 | 45.34 | . 317 | . 293 | . 261 | . 223 | . 177 | . 118 | . 075 | . 027 |  |  | 1.0235 |
| Mar. 1 | 59.14 | . 320 | - 303 | . 279 | . 245 | . 204 | . 158 | . 108 | . 056 | 0.013 |  | I.or 73 |
| 16 | 73.93 | . 321 | -313 | . 296 | . 270 | . 236 | . 795 | . 148 | . 097 | . 057 |  | 1.0096 |
| $A p r . ~ 1 ~$ | 89.70 | . 317 | . 319 | . 312 | . 295 | . 269 | . 235 | . 195 | . 148 | . IOI | 0.082 | 1.0009 |
| 16 | 104.49 | . 311 | -32I | . 323 | . 315 | . 297 | . 271 | .238 | . 201 | . 175 | . 177 | 0.9923 |
| May I | 119.29 | . 303 | . 318 | . 330 | - 329 | - 320 | - 302 | . 278 | . 253 | . 255 | . 259 | 0.9841 |
| 16 | 134.05 | . 294 | -318 | . 333 | . 339 | . 337 | . 327 | $\cdot 312$ | . 298 | . 317 | . 322 | 0.9772 |
| June 1 | 149.82 | . 287 | . 315 | - 334 | - 345 | - 349 | - 345 | - 337 | - 344 | . 360 | . 366 | 0.9714 |
| 16 | 164.60 | . 283 | -313 | - 334 | . 348 | -354 | - 353 | . 348 | .36I | . 378 | . 384 | 0.9679 |
| July 1 | 179.39 | . 283 | - 312 | - 333 | - 347 | - 352 | -35I | - 345 | . 356 | - 373 | . 379 | 0.9666 |
| 16 | 194.13 | . 287 | . 314 | -332 | -342 | - 345 | -340 | - 329 | .33I | . 347 | . 352 | 0.9674 |
| Aug. 1 | 209.94 | . 294 | . 316 | - 330 | - 334 | . 330 | . 318 | -300 | . 282 | . 295 | . 300 | 0.9709 |
| 16 | 224.73 | . 303 | . 318 | . 325 | - 322 | . 310 | . 291 | . 264 | . 234 | . 227 | . 23 I | 0.9760 |
| Sept. 1 | 240.50 | - 310 | . 318 | . 316 | - 305 | . 285 | . 256 | . 220 | . 180 | . 139 | . 140 | 0.9828 |
| 16 | 255.29 | . 315 | . 315 | . 305 | . 284 | . 256 | . 220 | . 178 | . 130 | . 107 | . 043 | 0.9909 |
| Oct. I | 270.07 | . 317 | . 308 | . 289 | . 26 I | . 225 | . 183 | . 135 | . 084 | . 065 |  | 0.9995 |
| 16 | 284.86 | . 316 | . 298 | . 271 | . 236 | . 194 | . 147 | . 097 | . 047 | . OI 5 |  | 1.0080 |
| Nov. I | 300.63 | -312 | . 286 | . 251 | . 211 | . 164 | . 114 | . 063 | . OI 8 |  |  | 1.0164 |
| 16 | 315.42 | . 308 | . 276 | . 235 | . 190 | . 140 | . 089 | . 040 |  |  |  | 1.0235 |
| Dec. I | 330.19 | . 304 | . 267 | . 224 | . 175 | . 124 | . 072 | . 024 |  |  |  | 1.0288 |
| 16 | 344.98 | . 302 | . 263 | . 218 | . 167 | . 115 | . 064 | . 016 |  |  |  | 1.0323 |
| Year.... |  | 0.305 | 0.301 | 0.289 | 0. 268 | 0.241 | 0.209 | 0. 173 | O. 144 | 0. 133 | 0. 126 |  |

## CONVERSION OF LINEAR MEASURES.

Inches into millimetres Table 64
Millimetres into inches Table 65
Feet into metres ..... Table 66
Metres into feet ..... Table 67
Miles into kilometres ..... Table 68
Kilometres into miles ..... Table 69
Interconversion of nautical and statute miles ..... Table 70Continental measures of length with their metric and EnglishequivalentsTable 71

1 inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm . |
| 0.00 | 0.00 | 0.25 | 0.51 | 0.76 | 1.02 | 1.27 | 1.52 | 1.78 | 2.03 | 2.29 |
| 0.10 | 2.54 | 2.79 | 3.05 | 3.30 | 3.56 | 3.81 | 4.06 | 4.32 | 4.57 | 4.83 |
| 0.20 | 5.08 | 5.33 | 5.59 | 5.84 | 6.10 | 6.35 | 6.60 | 6.86 | 7.11 | 7.37 |
| 0.30 | 7.62 | 7.87 | 8.13 | 8.38 | 8.64 | 8.89 | 9.14 | 9.40 | 9.65 | 9.91 |
| 0.40 | 10.16 | 10.41 | 10.67 | 10.92 | 11.18 | 11.43 | 1 I .68 | II. 94 | 12.19 | 12.45 |
| 0.50 | 12.70 | 12.95 | 13.21 | 13.46 | 13.72 | 13.97 | 14.22 | 14.48 | 14.73 | 14.99 |
| 0.60 | 15.24 | 15.49 | 15.75 | 16.00 | 16.26 | 16.51 | 16.76 | 17.02 | 17.27 | 17.53 |
| 0.70 | 17.78 | 18.03 | 18.29 | 18.54 | 18.80 | 19.05 | 19.30 | 19.56 | 19.81 | 20.07 |
| 0.80 | 20.32 | 20.57 | 20.83 | 21.08 | 21.34 | 21.59 | 21.84 | 22.10 | 22.35 | 22.61 |
| 0.90 | 22.86 | 23.11 | 23.37 | 23.62 | 23.88 | 24.13 | 24.38 | 24.64 | 24.89 | 25.15 |
| 1.00 | 25.40 | 25.65 | 25.91 | 26.16 | 26.42 | 26.67 | 26.92 | 27.18 | 27.43 | 27.69 |
| r.10 | 27.94 | 28.19 | 28.45 | 28.70 | 28.96 | 29.21 | 29.46 | 29.72 | 29.97 | 30.23 |
| 1.20 | 30.48 | 30.73 | 30.99 | 31.24 | 31.50 | 31.75 | 32.00 | 32.26 | 32.51 | 32.77 |
| 1.30 | 33.02 | 33.27 | 33.53 | 33.78 | 34.04 | 34.29 | 34.54 | 34.80 | 35.05 | 35.31 |
| 1.40 | 35.56 | 35.8 I | 36.07 | 36.32 | 36.58 | 36.83 | 37.08 | 37.34 | 37.59 | 37.85 |
| 1.50 | 38.10 | 38.35 | 38.61 | 38.86 | 39.12 | 39.37 | 39.62 | 39.88 | 40.13 | 40.39 |
| 1.60 | 40.64 | 40.89 | 41.15 | 41.40 | 4 I .66 | 41.91 | 42.16 | 42.42 | 42.67 | 42.93 |
| 1.70 | 43.18 | 43.43 | 43.69 | 43.94 | 44.20 | 44.45 | 44.70 | 44.96 | 45.21 | 45.47 |
| 1.80 | 45.72 | 45.97 | 46.23 | 46.48 | 46.74 | 46.99 | 47.24 | 47.50 | 47.75 | 48.01 |
| 1.90 | 48.26 | 48.51 | 48.77 | 49.02 | 49.28 | 49.53 | 49.78 | 50.04 | 50.29 | 50.55 |
| 2.00 | 50.80 | 51.05 | 51.31 | 51.56 | 51.82 | 52.07 | 52.32 | 52.58 | 52.83 | 53.09 |
| 2.10 | 53.34 | 53.59 | 53.85 | 54.10 | 54.36 | 54.61 | 54.86 | 55.12 | 55.37 | 55.63 |
| 2.20 | 55.88 | 56.13 | 56.39 | 56.64 | 56.90 | 57.15 | 57.40 | 57.66 | 57.91 | 58.17 |
| 2.30 | 58.42 | 58.67 | 58.93 | 59.18 | 59.44 | 59.69 | 59.94 | 60.20 | 60.45 | 60.71 |
| 2.40 | 60.96 | 6 I .2 I | 61.47 | 61.72 | 61.98 | 62.23 | 62.48 | 62.74 | 62.99 | 63.25 |
| 2.50 | 63.50 | 63.75 | 64.01 | 64.26 | 64.52 | 64.77 | 65.02 | 65.28 | 65.53 | 65.79 |
| 2.60 | 66.04 | 66.29 | 66.55 | 66.80 | 67.05 | 67.31 | 67.56 | 67.82 | 68.07 | 68.33 |
| 2.70 | 68.58 | 68.83 | 69.09 | 69.34 | 69.60 | 69.85 | 70.10 | 70.36 | 70.61 | 70.87 |
| 2.80 | 71.12 | 71.37 | 71.63 | 71.88 | 72.14 | 72.39 | 72.64 | 72.90 | 73.15 | 73.4 I |
| 2.90 | 73.66 | 73.91 | 74.17 | 74.42 | 74.68 | 74.93 | 75.18 | 75.44 | 75.69 | 75.95 |
| 3.00 | 76.20 | 76.45 | 76.71 | 76.96 | 77.22 | 77.47 | 77.72 | 77.98 | 78.23 | 78.49 |
| 3.10 | 78.74 | 78.99 | 79.25 | 79.50 | 79.76 | 80.OI | 80.26 | 80.52 | 80.77 | 81.03 |
| 3.20 | 81.28 | 81.53 | 81.79 | 82.04 | 82.30 | 82.55 | 82.8o | 83.06 | 83.31 | 83.57 |
| 3.30 | 83.82 | 84.07 | 84.33 | 84.59 | 84.84 | 85.09 | 85.34 | 85.60 | 85.85 | S6.II |
| 3.40 | 86.36 | 86.61 | 86.87 | 87.12 | 87.38 | 87.63 | 87.88 | 88.14 | 88.39 | 88.65 |
| 3.50 | 88.90 | 89.15 | 89.41 | 89.66 | 89.92 | 90.17 | 90.42 | 90.68 | 90.93 | 91.19 |
| 3.60 | 91.44 | 91.69 | 91.95 | 92.20 | 92.46 | 92.71 | 92.96 | 93.22 | 93.47 | 93.73 |
| 3.70 | 93.98 | 94.23 | 94.49 | 94.74 | 95.00 | 95.25 | 95.50 | 95.76 | 96.01 | 96.27 |
| 3.80 | 96.52 | 96.77 | 97.03 | 97.28 | 97.54 | 97.79 | 98.04 | 98.30 | 98.55 | 98.81 |
| 3.90 | 99.06 | 99.3 I | 99.57 | 99.82 | 100.08 | 100.33 | 100.58 | 100.84 | 101.09 | 101. 35 |
| 4.00 | 101. 60 | 101. 85 | ro2.II | 102.36 | 102.62 | 102.87 | 103.12 | 103.38 | 103.63 | 103.89 |
| 4.10 | 104.14 | 104.39 | 104.65 | 104.90 | 105.16 | 105.41 | 105.66 | 105.92 | 106.17 | 106.43 |
| 4.20 | 106.68 | 106.93 | 107.19 | 107.44 | 107.70 | 107.95 | 108.20 | 108.46 | 108.71 | 108.97 |
| 4.30 | 109.22 | 109.47 | 109.73 | 109.98 | 110.24 | IIO. 49 | 110.74 | 111.00 | III. 25 | III.5I |
| 4.40 | 111.76 | II2.01 | I I2.27 | I 12.52 | 112.78 | II 3.03 | II 3.28 | II 3.54 | I 13.79 | 114.05 |
| 4.50 | II4.30 | I 14.55 | II4.8I | II5.06 | II5.32 | 115.57 | 115.82 | 116.08 | II6.33 | 116.59 |
| 4.60 | II 6.84 | 117.09 | 117.35 | 117.60 | 117.86 | IIS.II | 118.36 | 118.62 | I 18.87 | 119.13 |
| 4.70 | 119.38 | II9.63 | I19.89 | 120.14 | 120.40 | 120.65 | 120.90 | 121.16 | I2I.4I | 121.67 |
| 4.80 | 121.92 | 122.17 | 122.43 | 122.68 | 122.94 | 123.19 | 123.44 | 123.70 | 123.95 | 124.21 |
| 4.90 | 124.46 | 124.71 | 124.97 | 125.22 | 125.48 | 125.73 | 125.98 | 126.24 | I26.49 | 126.75 |
| 5.00 | 127.00 | 127.25 | 127.5 1 | 127.76 | 128.02 | 128.27 | 128.52 | 128.78 | 129.03 | 129.29 |
| Proportional Parts |  | Inch. mm . | 0.001 | 0.002 | 0.0030 | $\begin{aligned} & 0.004 \\ & 0.102 \end{aligned}$ | $5 \quad 0.006$ | 0.007 | . 008 | $\begin{aligned} & 0.009 \\ & 0.229 \end{aligned}$ |
|  |  |  | 0.051 | 0.0760. | $7 \quad 0.152$ |  | 0.178 | 0.203 |  |

INCHES INTO MILLIMETRES.
I inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm. | mm. | mm. | mm. | mm. | mr | mm . | mm. | mm. | mm. |
| 5.00 | 127.00 | 127.25 | 127.51 | 127.76 | 128.02 | 128.27 | 128.52 | 128.78 | 129.03 | 129.29 |
| 5.10 | I29.54 | 129.79 | 130.05 | 130.30 | 130.56 | 130.81 | 131.06 | 131.32 | I31.57 | 131.83 |
| 5.20 | 1 32.08 | 132.33 | 132.59 | 132.84 | 133.10 | 133.35 | 133.60 | 133.86 | I 34.11 | 134.37 |
| 5.30 | I 34.62 | 134.87 | 135.13 | 135.38 | 135.64 | 135.89 | 136.14 | 136.40 | I 36.65 | I36.91 |
| 5.40 | 137.16 | I 37.41 | 137.67 | 137.92 | 138.18 | I 38.43 | 138.68 | I38.94 | I 39.19 | I 39.45 |
| 5.50 | 139.70 | I 39.95 | 140.21 | 140.46 | 140.72 | 140.97 | 141.22 | 141.48 | 141.73 | 141.99 |
| 5.60 | 142.24 | 142.49 | 142.75 | 143.00 | 143.26 | 143.51 | 143.76 | 144.02 | 144.27 | 144.53 |
| 5.70 | 144.78 | 145.03 | 145.29 | 145.54 | 145.80 | 146.05 | 146.30 | 146.56 | 146.81 | 147.07 |
| 5.80 | 147.32 | 147.57 | 147.83 | 148.08 | 148.34 | 148.59 | 148.84 | 149.10 | 149.35 | 149.61 |
| 5.90 | 149.86 | 150.11 | 150.37 | 150.62 | 150.88 | 151.13 | 151.38 | 151.64 | 15 I .89 | 152.15 |
| 6.00 | 152.40 | 152.66 | 152.91 | 153.16 | 153.42 | 153.67 | 153.92 | 154.18 | 154.43 | 154.69 |
| 6.10 | 154.94 | 155.19 | 155.45 | 155.70 | 155.96 | 156.21 | 156.46 | 156.72 | 156.97 | 157.23 |
| 6.20 | 157.48 | ${ }^{157.73}$ | 157.99 | 158.24 | 158.50 | 158.75 | 159.00 | 159.26 | 159.51 | 159.77 |
| 6.30 | 160.02 | 160.27 | 160.53 | 160.78 | 161.04 | 161.29 | 161.54 | 161.8o | 162.05 | 162.31 |
| 6.40 | 162.56 | 162.81 | 163.07 | 163.32 | 163.58 | 163.83 | 164.08 | 164.34 | 164.59 | 164.85 |
| 6.50 | 165.10 | 165.35 | 165.61 | 165.86 | 166.12 | 166.37 | 166.62 | 166.88 | 167.13 | 167.39 |
| 6.60 | 167.64 | 167.89 | 168.15 | 168.40 | 168.66 | 168.91 | 169. 16 | 169.42 | 169.67 | 169.93 |
| 6.70 | 170.18 | 170.43 | 170.69 | 170.94 | 171.20 | 171.45 | 171.70 | 171.96 | 172.21 | 172.47 |
| 6.80 | 172.72 | 172.97 | 173.23 | 173.48 | 173.74 | 173.99 | 174.24 | 174.50 | 174.75 | 175.01 |
| 6.90 | 175.26 | 175.51 | 175.77 | 176.02 | 176.28 | 176.53 | 176.78 | 177.04 | 177.29 | 177.55 |
| 7.00 | 177.80 | 178.05 | 178.31 | 178.56 | 178.82 | 179.07 | 179.32 | 179.58 | 179.83 | I80.09 |
| 7.10 | 180.34 | 180.59 | 180.85 | 181.10 | 181. 36 | 18 I .61 | 18 I .86 | 182.12 | 182.37 | 182.63 |
| 7.20 | 182.88 | 183.13 | 183.39 | 183.64 | 183.90 | 184.15 | 184.40 | 184.66 | 184.91 | 185.17 |
| 7.30 | 185.42 | 185.67 | 185.93 | 186. 18 | 186.44 | 186.69 | 186.94 | 187.20 | 187.45 | 187.71 |
| 7.40 | 187.96 | 188.21 | 188.47 | 188.72 | 188.98 | 189.23 | 189.48 | 189.74 | 189.99 | 190.25 |
| 7.50 | 190.50 | 190.75 | 191.01 | 191.26 | 191.52 | 191.77 | 192.02 | 192.28 | 192.53 | 192.79 |
| 7.60 | 193.04 | 193.29 | 193.55 | 193.80 | 194.06 | 194.31 | 194.56 | 194.82 | 195.07 | 195.33 |
| 7.70 | 195.58 | 195.83 | 196.09 | 196.34 | 196.60 | 196.85 | 197. Io | 197.36 | 197.61 | 197.87 |
| 7.80 | 198.12 | 198.37 | 198.63 | 198.88 | 199.14 | 199.39 | 199.64 | 199.90 | 200.15 | 200.4 I |
| 7.90 | 200.66 | 200.91 | 201.17 | 201.42 | 201.68 | 201.93 | 202.18 | 202.44 | 202.69 | 202.95 |
| 8.00 | 203.20 | 203.45 | 203.71 | 203.96 | 204.22 | 204.47 | 204.72 | 204.98 | 205.23 | 205.49 |
| 8.10 | 205.74 | 205.99 | 206.25 | 206.50 | 206.76 | 207.01 | 207.26 | 207.52 | 207.77 | 208.03 |
| 8.20 | 208.28 | 208.53 | 208.79 | 209.04 | 209.30 | 209.55 | 209.80 | 210.06 | 210.31 | 210.57 |
| 8.30 | 210.82 | 211.07 | 211.33 | 211.58 | 211.84 | 212.09 | 212.34 | 212.60 | 212.85 | 213.11 |
| 8.40 | 213.36 | 213.61 | 213.87 | 214.12 | 214.38 | 214.63 | 214.88 | 215.14 | 215.39 | 215.65 |
| 8.50 | 215.90 | 216.15 | 216.41 | 216.66 | 216.92 | 217.17 | 217.42 | 217.68 | 217.93 | 218.19 |
| 8.60 | 218.44 | 218.69 | 218.95 | 219.20 | 219.46 | 219.71 | 219.96 | 220.22 | 220.47 | 220.73 |
| 8.70 | 220.98 | 221.23 | 221.49 | 221.74 | 222.00 | 222.25 | 222.50 | 222.76 | 223.01 | 223.27 |
| 8.80 | 223.52 | 223.77 | 224.03 | 224.28 | 224.54 | 224.79 | 225.04 | 225.30 | 225.55 | 225.81 |
| 8.90 | 226.06 | 226.31 | 226.57 | 226.82 | 227.08 | 227.33 | 227.58 | 227.84 | 228.09 | 228.35 |
| 9.00 | 228.60 | 228.85 | 229.11 | 229.36 | 229.62 | 229.87 | 230.12 | 230.38 | 230.63 | 230.89 |
| 9.10 | 231.14 | 231.39 | 231.65 | 23 I .90 | 232.16 | 232.41 | 232.66 | 232.92 | 233.17 | 233.43 |
| 9.20 | 233.68 | 233.93 | 234.19 | 234.44 | 234.70 | 234.95 | 235.20 | 235.46 | 235.71 | 235.97 |
| 9.30 | 236.22 | 236.47 | 236.73 | 236.98 | 237.24 | 237.49 | 237.74 | 238.00 | 238.25 | 238.51 |
| 9.40 | 238.76 | 239.01 | 239.27 | 239.52 | 239.78 | 240.03 | 240 | 240.54 | 240.79 | 241.05 |
| 9.50 | 241.30 | 241.55 | 241.81 | 242.06 | 242.32 | 242.57 | 242.82 | 243.08 | 243.33 | 243.59 |
| 9.60 | 243.84 | 244.09 |  | 244.60 | 244.86 | 245. II | 245.36 | 245.62 | 245.87 | 246.13 |
| 9.70 | 246.38 | 246.63 | 246.89 | 247.14 | 247.40 | 247.65 | 247.90 | 248.16 | 248.41 | 248.67 |
| 9.80 | 248.92 | 249.17 | 249.43 | 249.68 | 249.94 | 250.19 | 250.44 | 250.70 | 250.95 | 251.21 |
| 9.90 | 251.46 | 251.71 | 251.97 | 252.22 | 252.48 | 252.73 | 252.98 | 253.24 | 253.49 | 253.75 |
| 10.00 | 254.00 | 254.25 | 254.51 | 254.76 | 255.02 | 255.27 | 255.52 | 255.78 | 256.03 | 256.29 |
| Proportional Parts. |  |  | . | 0.002 | $\begin{array}{ll}0.03 & 0.004 \\ 0.076 & 0.102\end{array}$ |  | $\begin{aligned} & 0.006 \\ & 0.152 \end{aligned}$ | $\begin{aligned} & 0.007 \\ & 0.178 \end{aligned}$ | 0.008 | $\begin{aligned} & 0.009 \\ & 0.229 \end{aligned}$ |
|  |  |  | . | . 51 |  |  | 0.203 |  |  |

Smithsonian Tables.

I inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | m | mm. | mm . | mm. | m | mm. | mm. | mm. | mm . | mm. |
| 10.00 | 254.00 | 254.25 | 254.5I | 254.76 | 255.02 | 255.27 | 255.52 | 255.78 | 256.03 | 256.29 |
| 10.10 | 256.54 | 256.79 | 257.05 | 257.30 | 257.56 | 257.81 | 258.06 | 258.32 | 258.57 | 258.83 |
| 10.20 | 259.08 | 259.33 | 259.59 | 259.84 | 260. 10 | 260.35 | 260.60 | 260.86 | 26I. II | 261.37 |
| 10.30 | 26 t .62 | 261.87 | 262.13 | 262.38 | 262.64 | 262.89 | 263.14 | 263.40 | 263.65 | 263.91 |
| 10.40 | 264.16 | 264.4I | 264.67 | 264.92 | 265.18 | 265.43 | 265.68 | 265.94 | 266.19 | 266.45 |
| 10.50 | 266.70 | 266.95 | 267.21 | 267.46 | 267.72 | 267.97 | 268.22 | 268.48 | 268.73 | 268.99 |
| 10.60 | 269.24 | 269.49 | 269.75 | 270.00 | 270.26 | 270.51 | 270.76 | 271.02 | 271.27 | 271.53 |
| 10.70 | 271.78 | 272.03 | 272.29 | 272.54 | 272.80 | 273.05 | 273.30 | 273.56 | 273.81 | 274.07 |
| 10.80 | 274.32 | 274.57 | 274.93 | 275.08 | 275.34 | 275.59 | 275.84 | 276.10 | 276.35 | 276.61 |
| 10.90 | 276.86 | 277.11 | 277.37 | 277.62 | 277.88 | 278.13 | 278.38 | 278.64 | 278.89 | 279.15 |
| 11.00 | 279.40 | 279.65 | 279.91 | 280.16 | 280.42 | 280.67 | 280.92 | 281.18 | 281.43 | 281. 69 |
| 11.10 | 281.94 | 282.19 | 282.45 | 282.70 | 282.96 | 283.21 | 283.46 | 283.72 | 283.97 | 284.23 |
| I1. 20 | 284.48 | 284.73 | 284.99 | 285.24 | 285.50 | 285.75 | 286.00 | 286.26 | 286.51 | 286.77 |
| 11.30 | 287.02 | 287.27 | 287.53 | 287.78 | 288.04 | 288.29 | 288.54 | 288.80 | 289.05 | 289.3I |
| I 1.40 | 289.56 | 289.81 | 290.07 | 290.32 | 290.58 | 290.83 | 291.08 | 291.34 | 291.59 | 291.85 |
| 11.50 | 292.10 | 292.35 | 292.6I | 292.86 | 293.12 | 293.37 | 293.62 | 293.88 | 294.13 | 294.39 |
| 11.60 | 294.64 | 294.89 | 295. I5 | 295.40 | 295.66 | 295.91 | 296.16 | 296.42 | 296.67 | 296.93 |
| 11.70 | 297.18 | 297.43 | 297.69 | 297.94 | 298.20 | 298.45 | 298.70 | 298.96 | 299.21 | 299.47 |
| 11.80 | 299.72 | 299.97 | 300.23 | 300.48 | 300.74 | 300.99 | 301.24 | 301.50 | 301.75 | 302.01 |
| I 1.90 | 302.26 | 302.51 | 302.77 | 303.02 | 303.28 | 303.53 | 303.78 | 304.04 | 304.29 | 304.55 |
| 12.00 | 304.80 | 305.05 | 305.3I | 305.56 | 305.82 | 306.07 | 306.32 | 306.58 | 306.83 | 307.09 |
| 12.10 | 307.34 | 307.59 | 307.85 | 308.10 | 308.36 | 308.6I | 308.86 | 309.12 | 309.37 | 309.63 |
| 12.20 | 309.88 | 310.13 | 310.39 | 310.64 | 310.90 | 3II.15 | 311.40 | 3 II .66 | 3 II .91 | 312.17 |
| 12.30 | 312.42 | 312.67 | 312.93 | 313.18 | 313.44 | 313.69 | 3 I 3.94 | 314.20 | 314.45 | 314.71 |
| 12.40 | 314.96 | 315.21 | 315.47 | 315.72 | 315.98 | 316.23 | 316.48 | 316.74 | 316.99 | 317.25 |
| 12.50 | 317.50 | 317.75 | 318.01 | 318.26 | 318.52 | 318.77 | 319.02 | 319.28 | 319.53 | 319.79 |
| 12.60 | 320.04 | 320.29 | 320.55 | 320.80 | 321.06 | 321.31 | 32 I .56 | 321.82 | 322.07 | 322.33 |
| 12.70 | 322.58 | 322.83 | 323.09 | 323.34 | 323.60 | 323.85 | 324.10 | 324.36 | 324.61 | 324.87 |
| 12.80 | 325.12 | 325.37 | 325.63 | 325.88 | 326. 14 | 326.39 | 326.64 | 326.90 | 327.15 | 327.41 |
| 12.90 | 327.66 | 327.91 | 328.17 | 328.42 | 328.68 | 328.93 | 329.18 | 329.44 | 329.69 | 329.95 |
| 13.00 | 330.20 | 330.45 | 330.71 | 330.96 | 33 I .22 | 331.47 | 331.72 | 331.98 | 332.23 | 332.49 |
| 13.10 | 332.74 | 332.99 | 333.25 | 333.50 | 333.76 | 334.01 | 334.26 | 334.52 | 334.77 | 335.03 |
| 13.20 | 335.28 | 335.53 | 335.79 | 336.04 | 336.30 | 336.55 | 336.80 | 337.06 | 337.31 | 337.57 |
| 13.30 | 337.82 | 338.07 | 338.33 | 338.58 | 338.84 | 339.09 | 339.34 | 339.60 | 339.85 | 340.11 |
| 13.40 | 340.36 | 340.6I | 340.87 | 341.12 | 341. 38 | 341.63 | 341.88 | 342.14 | 342.39 | 342.65 |
| 13.50 | 342.90 | 343. 5 | 343.41 | 343.66 | 343.92 | 344.17 | 344.42 | 344.68 | 344.93 | 345.19 |
| 13.60 | 345.44 | 345.69 | 345.95 | 346.20 | 346.46 | 346.71 | 346.96 | 347.22 | 347.47 | 347.73 |
| 13.70 | 347.98 | 348.23 | 348.49 | 348.74 | 349.00 | 349.25 | 349.50 | 349.76 | 350.01 | 350.27 |
| 13.80 | 350.52 | 350.77 | 351.03 | 351.28 | 351. 54 | 351.79 | 352.04 | 352.30 | 352.55 | 352.8I |
| 13.90 | 353.06 | 353.3 I | 353.57 | 353.82 | 354.08 | 354.33 | 354.58 | 354.84 | 355.09 | 355.35 |
| 14.00 | 355.60 | 355.85 | 356.11 | 356.36 | 356.62 | 356.87 | 357.12 | 357.38 | 357.63 | 357.89 |
| 14.10 | 358.14 | 358.39 | 358.65 | 358.90 | 359.16 | 359.41 | 359.66 | 359.92 | 360.17 | 360.43 |
| 14.20 | 360.68 | 360.93 | 361.19 | 361.44 | 361.70 | 36 I .95 | 362.20 | 362.46 | 362.71 | 362.97 |
| 14.30 | 363.22 | 363.47 | 363.73 | 363.98 | 364.24 | 364.49 | 364.74 | 365.00 | 365.25 | 365.51 |
| 14.40 | 365.76 | 366.01 | 366.27 | 366.52 | 366.78 | 367.03 | 367.28 | 367.54 | 367.79 | 368.05 |
| 14.50 | 368.30 | 368.55 | 368.8ı | 369.06 | 369.32 | 369.57 | 369.82 | 370.08 | 370.33 | 370.59 |
| 14.60 | 370.84 | 371.09 | 371.35 | 371.60 | 371.86 | 372.11 | 372.36 | 372.62 | 372.87 | 373.13 |
| 14.70 | 373.38 | 373.63 | 373.89 | 374.14 | 374.40 | 374.65 | 374.90 | 375.16 | 375.4I | 375.67 |
| 14.80 | 375.92 | 376.17 | 376.43 | 376.68 | 376.94 | 377.19 | 377.44 | 377.70 | 377.95 | 378.21 |
| 14.90 | 378.46 | 378.71 | 378.97 | 379.22 | 379.48 | 379.73 | 379.98 | 380.24 | 380.49 | 380.75 |
| 15.00 | 38 r .00 | 38 r .25 | 381.5I | 381.76 | 382.02 | 382.27 | 382.52 | 382.78 | 383.03 | 383.29 |
| Proportional Parts |  | S. $\begin{gathered}\text { Inch } \\ \mathrm{mm}\end{gathered}$ | . 0.001 | 0.002 | 0.003 | $\begin{array}{ll} 4 & 0.005 \\ 2 & 0.127 \end{array}$ | $\begin{array}{ll} 5 & 0.006 \\ 7 & 0.152 \end{array}$ | 0.007 | 0.008 | 0.0090.229 |
|  |  |  | 0.051 | 0.076 | 0.178 |  |  | 0.203 |  |

INCHES INTO MILLIMETRES.
I inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm. |  | mm. | mm. | mm. | mm. |  |  | mm. | mm . |
| 15.00 | 381.00 | 38 I .25 | $3^{81} 1.51$ | 381.76 | 382.02 | 382.27 | 382.52 | 382.78 | 383.03 | 383.29 |
| 15.10 | 383.54 | 383.79 | 384.05 | 384.30 | 384.56 | 384.8I | 385.06 | 385.32 | 385.57 | 385.83 |
| 15.20 | 386.08 | 386.33 | 386.59 | 386.84 | 387.10 | 387.35 | 387.60 | 387.86 | 388.11 | 388.37 |
| 15.30 | 388.62 | 388.87 | 389.13 | 389.38 | 389.64 | 389.89 | 390.14 | 390.40 | 390.65 | 390.91 |
| 15.40 | 391.16 | 391.41 | 391.67 | 391.92 | 392.18 | 392.43 | 392.68 | 392.94 | 393.19 | 393.45 |
| 15.50 | 393.70 | 393.95 | 394.21 | 394.46 | 394.72 | 394.97 | 395.22 | 395.48 | 395.73 | 395.99 |
| 15.60 | 396.24 | 39.649 | 396.75 | 397.00 | 397.26 | 397.5I | 397.76 | 398.02 | 398.27 | 398.53 |
| 15.70 | 398.78 | 399.03 | 399.29 | 399.54 | 399.80 | 400.05 | 400.30 | 400.56 | 400.8r | 401.07 |
| 15.80 | 401.32 | 401.57 | 401.83 | 402.08 | 402.34 | 402.59 | 402.84 | 403.10 | 403.35 | 403.61 |
| 15.90 | 403.86 | 404.1I | 404.37 | 404.62 | 404.88 | 405. 13 | 405.38 | 405.64 | 405.89 | 406. 15 |
| 16.00 | 406.40 | 406.65 | 406.91 | 407.16 | 407.52 | 407.67 | 407.92 | 408.18 | 408.43 | 408.69 |
| 16.10 | 408.94 | 409.19 | 409.45 | 409.70 | 409.96 | 410.21 | 410.46 | 410.72 | 410.97 | 41 I .23 |
| 16.20 | 411.48 | 411.73 | 411.99 | 412.24 | 412.50 | 412.75 | 413.00 | 413.26 | 413.51 | 413.77 |
| 16.30 | 414.02 | 414.27 | 414.53 | 414.78 | 415.04 | 415.29 | 415.54 | 415.80 | 416.05 | 416.31 |
| 16.40 | 416.56 | 416.81 | 417.07 | 417.32 | 417.58 | 417.83 | 418.08 | 418.34 | 418.59 |  |
| 16.50 | 419.10 | 419.35 | 419.61 | 419.86 | 420.12 | 420.37 | 420.62 | 420.88 | 421. I3 | 421.39 |
| 16.60 | 42 I .64 | 421.89 | 422.15 | 422.40 | 422.66 | 422.91 | 423.16 | 423.42 | 423.67 | 423.93 |
| 16.70 | 424. 18 | 424.43 | 424.69 | 424.94 | 425.20 | 425.45 | 425.70 | 425.96 | 426.21 | 426.47 |
| 16.80 | 426.72 | 426.97 | 427.23 | 427.48 | 427.74 | 427.99 | 428.24 | 428.50 | 428.75 | 429.01 |
| 16.90 | 429.26 | 429.51 | 429.77 | 430.02 | 430.28 | 430.53 | 430.78 | 431.04 | 431.29 | 43 I .55 |
| 17.00 | 431.80 | 432.05 | 432.31 | 432.56 | 432.82 | 433.07 | 433.32 | 433.58 | 433.83 | 434.09 |
| 17.10 | 434.34 | 434.59 | 434.85 | 435. 10 | 435.36 | 435.61 | 435.86 | 436.12 | 436.37 | 436.63 |
| 17.20 | 436:88 | 437.13 | 437.39 | 437.64 | 437.90 | 438.15 | 438.40 | 438.66 | 438.91 | 439.17 |
| 17.30 | 439.42 | 439.67 | 439.93 | 440.18 | 440.44 | 440.69 | 440.94 | 441.20 | 44 I .45 | 44r.71 |
| 17.40 | 441.96 | 442.2 I | 442.47 | 442.72 | 442.98 | 443.23 | 443.48 | 443.74 | 443.99 | 444.25 |
| 17.50 | 444.50 | 444.75 | 445.01 | 445.26 | 445.52 | 445.77 | 446.02 | 446.28 | 446.53 | 446.79 |
| 17.60 | 447.04 | 447.29 | 447.55 | 447.80 | 448.06 | 448.31 | 448.56 | 448.82 | 449.07 | 449.33 |
| 17.70 1780 | 449.58 | 449.83 | 450.09 | 450.34 | 450.60 | 450.85 | 451.10 | 451.36 | 451.61 | 451.87 |
| 17.80 | 452.12 | 452.37 | 452.63 | 452.88 | 453.14 | 453.39 | 453.64 | 453.90 | 454.15 | 454.41 |
| 17.90 | 66 | 454.91 | 455.17 | 455.42 | 455.68 | 455.93 | 456.18 | 456.44 | 456.69 | 456.95 |
| 18.00 | 457.20 | 457.45 | 457.71 | 457.96 | 458.22 | 458.47 | 458.72 | 458.98 | 459.23 | 459.49 |
| 18.10 | 459.74 | 459.99 | 460.25 | 460.50 | 460.76 | 461.01 | 461. 26 | 461.52 | 46 I .77 | 462.03 |
| 18.20 | 462.28 | 462.53 | 462.79 | 463.04 | 463.30 | 463.55 | 463.80 | 464.06 | 464.31 | 464.57 |
| 18.30 | 464.82 | 465.07 | 465.33 | 465.58 | 465.84 | 466.09 | 466.34 | 466.60 | 466.85 | 467.11 |
| 18.40 | 467.36 | 467.61 | 467.87 | 468.12 | 468 | 468.63 | 468.88 | 469.14 | 469.39 | 469.35 |
| 18.50 | 469.90 | 470.15 | 470.41 | 470.66 | 470.92 | 47 I .17 | 471.42 | 47 I .68 | 471.93 | 472.19 |
| 18.60 | 472.44 | 472.69 | 472.95 | 473.20 | 473.46 | 473.71 | 473.96 | 474.22 | 474.47 | 474.73 |
| 18.70 | 474.98 | 475.23 | 475.49 | 475.74 | 476.00 | 476.25 | 476.50 | 476.76 | 477.01 | 477.27 |
| 18.80 | 477.52 | 477.77 | 478.03 | 478.28 | 478.54 | 478.79 | 479.04 | 479.30 | 479.55 | 479.81 |
| 18.90 | 48 | 480.31 | 480.57 | 48 | 481.08 | 481.33 | 481.58 | 48 r .84 | 482.09 | 482.35 |
| 19.00 | 482.60 | 482.85 | 483.11 | 483.36 | 483.62 | 483.87 | 484.12 | 484.38 | 484.63 | 484.89 |
| 19.10 | 485.14 | 485.39 | 485.65 | 485.90 | 486.16 | 486.41 | 486.66 | 486.92 | 487.17 | 487.43 |
| 19.20 | 487.68 | 487.93 | 488.19 | 488.44 | 488.70 | 488.95 | 489.20 | 489.46 | 489.71 | 489.97 |
| 19.30 | 490.22 | 490.47 | 490.73 | 490.98 | 491. 24 | 491.49 | 491. 74 | 492.00 | 492.25 | 492.51 |
| 19.40 | 492.76 | 493.01 | 493.27 | 493.52 | 493.78 | 494.03 | 494.28 | 494.54 | 494.79 | 495.05 |
| 19.50 | 495.30 | 495.55 | 495.81 | 496.06 | 496.32 | 496.57 | 496.82 | 497.08 | 497.33 |  |
| 19.60 | 497.84 | 498.09 | 498.35 | 498.60 | 498.86 | 499.11 | 499.36 | 499.62 | 499.87 | 500.13 |
| 19.70 | 500.38 | 500.34 | 500.89 | 501.14 | 501.40 | 501.65 | 501.91 | 502.16 | 502.41 | 502.67 |
| 19.80 | 502.92 | 503.18 | 503.43 | 503.68 | 503.94 | 504.19 | 504.45 | 504.70 | 504.95 | 505.21 |
| 19.90 | 505.46 | 505.72 | 505.97 | 506.22 | 506.48 | 506.73 | 506.99 | 507.24 | 507.49 | 507.75 |
| 20.00 | 508.00 | 508.26 | 508.51 | 508.76 | 509.02 | 509.27 | 509.53 | 509.78 | 510.03 | 510.29 |
| Proportional Part |  | Inch.mm. | . | 0.002 | 0.003 | 0.0040.102 | $\begin{aligned} & 0.006 \\ & 0.152 \end{aligned}$ | 0.007 | 0.008 | $\begin{aligned} & 0.009 \\ & 0.229 \end{aligned}$ |
|  |  | . | . 05 | 0.076 | 0.178 |  |  | 0.203 |  |

## INCHES INTO MILLIMETRES.

$I$ inch $=25.40005 \mathrm{~mm}$.


INCHES INTO MILLIMETRES.
1 inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | .01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm. | mm. | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm |
| 25.00 | 635 | 635.26 | 635 | 635.76 | 636.02 | 636:27 | 636.53 | 636.78 | 637.03 | 637.29 |
| 25.10 | 637.54 | 637.80 | 638.05 | 638.30 | 638.56 | 638.81 | 639.07 | 639.32 | 639.57 | 639.83 |
| 25.20 | 640.08 | 640.34 | 640.59 | 640.84 | 641.10 | 641.35 | 641.6I | 641.86 | 642.11 | 642.37 |
| 25.30 | 642.62 | 642.88 | 643.13 | 643.38 | 643.64 | 643.89 | 644.15 | 644.40 | 644.65 | 644.91 |
| 25.40 | 645.16 | 645.42 | 645.67 | 645.92 | 646. 18 | 646.43 | 646.69 | 646.94 | 647.19 | 647.45 |
| 25.50 | 647.70 | 647.96 | 648.21 | 648.46 | 648.72 | 648.97 | 649.23 | 649.48 | 649.73 | 649.99 |
| 25.60 | 650.24 | 650.50 | 650.75 | 651.00 | 651.26 | 651.51 | 651.77 | 652.02 | 654.27 | 652.53 |
| 25.70 | 652.78 | 653.04 | 653.29 | 653.54 | 653.80 | 654.05 | 654.31 | 654.56 | 654.81 | 655.07 |
| 25.80 | 655.32 | 655.58 | 655.83 | 656.08 | 656.34 | 656.59 | 656.85 | 657.10 | 657.35 | 657.6I |
| 25.90 | 657.86 | 658.12 | 658.37 | 658.62 | 658.88 | 659. I3 | 659.39 | 659.64 | 659.89 | 660.15 |
| 26.00 | 660.40 | 660.66 | 660.91 | 66I.16 | 661.42 | 661.67 | 661.93 | 662.18 | 662.43 | 662.69 |
| 26.10 | 662.94 | 663.20 | 663.45 | 663.70 | 663.96 | 664.21 | 664.47 | 664.72 | 664.97 | 665.23 |
| 26.20 | 665.48 | 665.74 | 665.99 | 666.24 | 666.50 | 666.75 | 667.01 | 667.26 | 667.5I | 667.77 |
| 26.30 | 668.02 | 668.28 | 668.53 | 668.78 | 669.04 | 669.29 | 669.55 | 669.80 | 670.05 | 670.31 |
| 26.40 | 670.56 | 670.82 | 671.07 | 671.32 | 671.58 | 671.83 | 672.09 | 672.34 | 672.59 | 672.85 |
| 26.50 | 673.10 | 673.36 | 673.61 | 673.86 | 674.12 | 674.37 | 674.63 | 674.88 | 675.13 | 675.39 |
| 26.60 | 675.64 | 675.90 | 676.15 | 676.40 | 676.66 | 676.91 | 677.17 | 677.42 | 677.67 | 677.93 |
| 26.70 | 678.18 | 678.44 | 678.69 | 678.94 | 679.20 | 679.45 | 679.71 | 679.96 | 680.21 | 680.47 |
| 26.80 | 680.72 | 680.98 | 681.23 | 681. 48 | 681.74 | 681.99 | 682.25 | 682.50 | 682.75 | 683.01 |
| 26.90 | 683.2 | 683.52 | 683.77 | 684.02 | 684.28 | 684.53 | 684.79 | 685.04 | 685.29 | 685.55 |
| 27.00 | 685.80 | 686.06 | 686.3I | 686.56 | 686.82 | 687.07 | 687.33 | 687.58 | 687.83 | 688.09 |
| 27.10 | 688.34 | 688.60 | 688.85 | 689.10 | 689.36 | 689.6I | 689.87 | 690.12 | 690.37 | 690.63 |
| 27.20 | 690.88 | 691.14 | 691.39 | 691.64 | 691.90 | 692.15 | 692.41 | 692.66 | 692.91 | 693. 7 |
| 27.30 | 693.42 | 693.68 | 693.93 | 694.18 | 694.44 | 694.69 | 694.95 | 695.20 | 695.45 | 695.7 I |
| 27.40 | 695.96 | 696.22 | 696.47 | 696.72 | 696.98 | 697.23 | 697.49 | 697.74 | 697.99 | 698.25 |
| 27.50 | 698.50 | 698.76 | 699.01 | 699.26 | 699.52 | 699.77 | 700.03 | 700.28 | 700.53 | 700.79 |
| 27.60 | 701.04 | 701.30 | 701.55 | 701.80 | 702.06 | 702.21 | 702.57 | 702.82 | 703.07 | 703.33 |
| 27.70 | 703.58 | 703.84 | 704.09 | 704.34 | 704.60 | 704.85 | 705.11 | 705.36 | 705.6I | 705.87 |
| 27.80 | 706.12 | 706.38 | 706.63 | 706.88 | 707.14 | 707.39 | 707.65 | 707.90 | 708.15 | 708.41 |
| 27.90 | 708.66 | 708.92 | 709.17 | 709.42 | 709.68 | 709.93 | 710.19. | 710.44 | 710.69 | 710.95 |
| 28.00 | 7 II .20 | 711.46 | 711.71 | 711.96 | 712.22 | 712.47 | 712.73 | 712.98 | 713.23 | 713.49 |
| 28.10 | 713.74 | 714.00 | 714.25 | 714.50 | 714.76 | 715.01 | 715.27 | 715.52 | 715.77 | 716.03 |
| 28.20 | 716.28 | 716.54 | 716.79 | 717.04 | 717.30 | 717.55 | 717.81 | 718.06 | 718.31 | 718.57 |
| 28.30 | 718.82 | 719.08 | 719.33 | 719.58 | 719.84 | 720.09 | 720.35 | 720.60 | 720.85 | 721.11 |
| 28.40 | 721.36 | 721.62 | 721.87 | 722.12 | 722.39 | 722.63 | 722.89 | 723.14 | 723.39 | 723.65 |
| 28.50 | 723.90 | 724.16 | 724.4 r | 724.66 | 724.92 | 725.17 | 725.43 | 725.68 | 725.93 | 726. 19 |
| 28.60 | 726.44 | 726.70 | 726.95 | 727.20 | 727.46 | 727.71 | 727.97 | 728.22 | 728.47 | 728.73 |
| 28.70 | 728.98 | 729.24 | 729.49 | 729.74 | 730.00 | 730.25 | 730.5I | 730.76 | 73 I .01 | 731.27 |
| 28.80 | 731.52 | 731.78 | 732.03 | 732.28 | 732.54 | 732.79 | 733.05 | 733.30 | 733.55 | 733.8I |
| 28.90 | 734.06 | 734.32 | 734.57 | 734.82 | 735.08 | 735.33 | 735.59 | 735.84 | 736.09 | 736.35 |
| 29.00 | 736.60 | 736.86 | 737.11 | 737.36 | 737.62 | 737.87 | 738.13 | 738.38 | 738.63 | 738.89 |
| 29.10 | 739.14 | 739.40 | 739.65 | 739.90 | 740.16 | 740.41 | 740.67 | 740.92 | 741.17 | 741.43 |
| 29.20 | $74 \times .68$ | 741.94 | 742. 19 | 742.44 | 742.70 | 742.95 | 743.21 | 743.46 | 743.7 I | 743.97 |
| 29.30 | 744.22 | 744.48 | 744.73 | 744.98 | 745.24 | 745.49 | 745.75 | 746.00 | 746.25 | 746.5I |
| 29.40 | 746.76 | 747.02 | 747.27 | 747.52 | 747.78 | 748.03 | 748.29 | 748.54 | 748.79 | 749.05 |
| 29.50 | 749.30 | 749.56 | 749.81 | 750.06 | 750.32 | 750.57 | 750.83 | 751.08 | 751.33 | 751. 59 |
| 29.60 | 751.84 | 752.10 | 752.35 | 752.60 | 752.86 | 753.11 | 753.37 | 753.62 | 753.87 | 754.13 |
| 29.70 | 754.38 | 754.64 | 754.89 | 755.14 | 755.40 | 755.65 | 755.91 | 756.16 | 756.41 | 756.67 |
| 29.80 | 756.92 | 757.18 | 757.43 | 757.68 | 757.94 | 758.19 | 758.45 | 758.70 | 758.95 | 759.21 |
| 29.90 | 759.46 | 759.72 | 759.97 | 760.22 | 760.48 | 760.73 | 760.99 | 761.24 | 761.49 | 761.75 |
| 30.00 | 762.00 | 762.26 | 762.51 | 762.76 | 763.02 | 763.27 | 763.53 | 763.78 | 764.03 | 764.29 |
| Proportional Parts |  | Inch. mm . | . 0.001 | 0.002 | 0.0030 | $\begin{aligned} & 0.004 \\ & 0.102 \end{aligned}$ | $\begin{aligned} & 0.006 \\ & 0.152 \end{aligned}$ | 0.007 | 0.008 | $\begin{aligned} & 0.009 \\ & 0.229 \end{aligned}$ |
|  |  | 0.025 | 0.051 | 0.076 0. | 0.178 |  |  | 0.203 |  |

INCHES INTO MILLIMETRES.
1 inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm . | mm. | mm. | mm. | mm . | mm. | mm. | mm. | mm . | mm . |
| 30.00 | 762.00 | 762.26 | 762.51 | 762.76 | 763.02 | 763.27 | 763.53 | 763.78 | 764.03 | 764.29 |
| 30.10 | 764.54 | 764.80 | 765.05 | 765.30 | 765.56 | 765.81 | 766.07 | 766.32 | 766.57 | 766.83 |
| 30.20 | 767.08 | 767.34 | 767.59 | 767.84 | 768.10 | 768.35 | 768.61 | 768.86 | 769.11 | 769.37 |
| 30.30 | 769.62 | 769.88 | 770.13 | 770.38 | 770.64 | 770.89 | 771.15 | 771.40 | 771.65 | 771.91 |
| 30.40 | 772.16 | 772.42 | 772.67 | 772.92 | 773.18 | 773.43 | 773.69 | 773.94 | 774.19 | 774.45 |
| 30.50 | 774.70 | 774.96 | 775.2I | 775.46 | 775.72 | 775.97 | 776.23 | 776.48 | 776.73 | 776.99 |
| 30.60 | 777.24 | 777.50 | 777.75 | 778.00 | 778.26 | 778.51 | 778.77 | 779.02 | 779.27 | 779.53 |
| 30.70 | 779.78 | 780.04 | 780.29 | 780.54 | 780.80 | 78 I .05 | 781.31 | 781.56 | 781.81 | 782.07 |
| 30.80 | 782.32 | 782.58 | 782.83 | 783.08 | 783.34 | 783.59 | 783.85 | 784.10 | 784.35 | 784.6I |
| 30.90 | 784.86 | 785.12 | 785.37 | 785.62 | 785.88 | 786.13 | 786.39 | 786.64 | 786.89 | 787.15 |
| 31.00 | 787.40 | 787.66 | 787.91 | 788.16 | 788.42 | 788.67 | 788.93 | 789.18 | 789.43 | 789.69 |
| 31.10 | 789.94 | 790.20 | 790.45 | 790.70 | 790.96 | 791.21 | 791.47 | 791.72 | 791.97 | 792.23 |
| 31.20 | 792.48 | 792.74 | 792.99 | 793.24 | 793.50 | 793.75 | 794.01 | 794.26 | 794.5I | 794.77 |
| 31.30 | 795.02 | 795.28 | 795.53 | 795.78 | 796.04 | 796.29 | 796.55 | 796.80 | 797.05 | 797.3I |
| 31.40 | 797.56 | 797.82 | 798.07 | 798.32 | 798.58 | 798.83 | 799.09 | 799.34 | 799.59 | 799.85 |
| 31.50 | 800.10 | 800.36 | 800.6 I | 800.86 | 8 l .12 | 8or. 37 | $80 r .63$ | 8or. 88 | 802.13 | 802.39 |
| 31.60 | 802.64 | 802.90 | 803.15 | 803.40 | 803.66 | 803.91 | 804.17 | 804.42 | 804.67 | 804.93 |
| 31.70 | 805.18 | 805.44 | 805.69 | 805.94 | 806.20 | 806.45 | 806.71 | 806.96 | 807.21 | 807.47 |
| 31.80 | 807.72 | 807.98 | 808.23 | 808.48 | 808.74 | 808.99 | 809.25 | 809.50 | 809.75 | 810.01 |
| 31.90 | 810.26 | 810. 52 | 810.77 | 8if. 02 | 8II. 28 | 8II. 53 | 8r1.79 | 812.04 | 8I2.29 | 812.55 |
| 32.00 | 812.80 |  |  |  |  |  |  |  |  |  |
| Proportional Parts |  | Inch. <br> mm . | . 0.001 | 0.002 | 0.0030 | $4 \quad 0.005$ | -0.006 | 0.007 | 0.008 | 0.009 |
|  |  | 0.025 | 0.051 | 0.076 0. | 20.127 | 0.152 | 0.178 | 0.203 | 0.229 |

Smithsonian Tableg.

## MILLIMETRES INTO INCHES.

I mm. $=0.03937$ inch.

$1 \mathrm{~mm} .=0.03937$ inch .

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Iuches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 400 | 15.748 | 15.752 | 15.756 | 15.760 | 15.764 | 15.768 | 15.772 | 15.776 | 15.779 | 15.783 |
| 401 | 15.787 | 15.791 | 15.795 | 15.799 | 15.803 | 15.807 | 15.811 | 15.815 | 15.819 | 15.823 |
| 402 | 15.827 | 15.831 | 15.835 | 15.839 | 15.842 | 15.846 | 15.850 | I 5.854 | 15.858 | I 5.862 |
| 403 | 15.866 | 15.870 | 15.874 | 15.878 | 15.882 | 15.886 | 15.890 | I5.894 | 15.898 | 15.902 |
| 404 | 15.905 | 15.909 | 15.913 | 15.917 | 15.921 | 15.925 | 15.929 | 15.933 | 15.937 | 15.941 |
| 405 | 15.945 | 15.949 | 15.953 | 15.957 | 15.961 | 15.965 | 15.968 | 15.972 | 15.976 | 15.980 |
| 406 | 15.984 | 15.988 | 15.992 | 15.996 | 16.000 | 16.004 | 16.008 | 16.012 | 16.016 | 16.020 |
| 407 | 16.024 | 16.028 | 16.031 | 16.035 | 16.039 | 16.043 | 16.047 | 16.051 | 16.055 | 16.059 |
| 408 | 16.063 | 16.067 | 16.071 | 16.075 | 16.079 | 16.083 | 16.087 | 16.091 | 16.094 | 16.098 |
| 409 | 16. 102 | 16.106 | 16.110 | 16.114 | 16.118 | 16.122 | 16.126 | 16.130 | 16.134 | 16.138 |
| 410 | 16. 142 | 16.146 | 16. 150 | 16.154 | 16.157 | 16.16r | 16.165 | 16.169 | 16.173 | 16.177 |
| 411 | 16.18I | 16.185 | 16.189 | 16.193 | 16.197 | 16.201 | 16.205 | 16.209 | 16.213 | 16.217 |
| 412 | 16.220 | 16.224 | 16.228 | 16.232 | 16.236 | 16.240 | 16.244 | 16.248 | 16.252 | 16.256 |
| 413 | 16.260 | 16.264 | 16.268 | 16.272 | 16.276 | 16.279 | 16.283 | 16.287 | 16.291 | 16.295 |
| 414 | 16.299 | 16.303 | 16.307 | 16.311 | 16.315 | 16.319 | 16.323 | 16.327 | 16.33 I | 16.335 |
| 415 | 16.339 | 16.342 | 16.346 | 16.350 | 16.354 | 16.358 | 16.362 | 16.366 | 16.370 | 16.374 |
| 416 | 16.378 | 16.382 | 16.386 | 16.390 | 16.394 | 16.398 | 16.402 | 16.405 | 16.409 | 16.413 |
| 417 | 16.417 | 16.421 | 16.425 | 16.429 | 16.433 | 16.437 | 16.441 | 16.445 | 16.449 | 16.453 |
| 418 | 16.457 | 16.46 I | 16.465 | 16.468 | 16.472 | 16.476 | 16.480 | 16.484 | 16.488 | 16.492 |
| 419 | 16.496 | 16.500 | 16.504 | 16.508 | 16.512 | 16.516 | 16.520 | 16.524 | 16.528 | 16.53 I |
| 420 | 16.535 | 16.539 | 16.543 | 16.547 | 16.55 I | 16.555 | 16.559 | 16.563 | 16.567 | 16.57 I |
| 421 | 16.575 | 16.579 | 16.583 | 16.587 | 16.591 | r6.594 | 16.598 | 16.602 | 16.606 | 16.610 |
| 422 | 16.614 | 16.618 | I6.622 | 16.626 | 16.630 | 16.634 | 16.638 | 16.642 | 16.646 | 16.650 |
| 423 | 16.654 | 16.657 | 16.66I | 16.665 | 16.669 | 16.673 | 16.677 | 16.68 I | 16.685 | 16.689 |
| 424 | 16.693 | 16.697 | 16.701 | 16.705 | 16.709 | 16.713 | 16.717 | 16.720 | 16.724 | 16.728 |
| 425 | 16.732 | 16.736 | 16.740 | 16.744 | 16.748 | 16.752 | 16.756 | 16.760 | 16.764 | 16.768 |
| 426 | 16.772 | 16.776 | 16.779 | 16.783 | 16.787 | 16.791 | 16.795 | 16.799 | 16.803 | 16.807 |
| 427 | 16.81 I | 16.815 | 16. ${ }^{1} 19$ | 16.823 | 16.827 | 16.831 | 16.835 | 16.839 | 16.842 | 16.846 |
| 428 | 16.850 | 16.854 | 16.858 | 16.862 | 16.866 | 16.870 | 16.874 | 16.878 | 16.882 | 16.886 |
| 429 | 16.890 | 16.894 | 16.898 | 16.902 | 16.905 | 16.909 | 16.913 | 16:917 | 16.92 I | 16.925 |
| 430 | 16.929 | 16.933 | 16.937 | 16.941 | 16.945 | 16.949 | 16.953 | 16.957 | 16.961 | 16.965 |
| 431 | 16.968 | 16.972 | 16.976 | I6.980 | 16.984 | 16.988 | 16.992 | 16.996 | 17.000 | 17.004 |
| 432 | 17.008 | 17.012 | 17.016 | 17.020 | 17.024 | 17.028 | 17.031 | 17.035 | 17.039 | 17.043 |
| 433 | 17.047 | 17.051 | 17.055 | 17.059 | 17.063 | 17.067 | 17.071 | 17.075 | 17.079 | 17.083 |
| 434 | 17.087 | 17.091 | 17.094 | 17.098 | 17.102 | 17.106 | 17.110 | 17.114 | 17.118 | 17.122 |
| 435 | 17.126 | 17.130 | 17.134 | 17.138 | 17.142 | 17.146 | 17.150 | 17.154 | 17.157 | 17.161 |
| 436 | 17.165 | 17.169 | 17.173 | 17.177 | 17.181 | 17.185 | 17.189 | 17.193 | 17.197 | 17.201 |
| 437 | 17.205 | 17.209 | 17.213 | ${ }^{17.217}$ | 17.220 | 17.224 | 17.228 | 17.232 | 17.236 | 17.240 |
| 438 | 17.244 | 17.248 | 17.252 | 17.256 | 17.260 | 17.264 | 17.268 | 17.272 | 17.276 | 17.279 |
| 439 | 17.283 | 17.287 | 17.291 | 17.295 | 17.299 | 17.303 | 17.307 | 17.311 | 17.315 | 17.319 |
| 440 | 17.323 | 17.327 | 17.33 I | 17.335 | 17.339 | 17.342 | 17.346 | 17.350 | 17.354 | ${ }^{1} 7.358$ |
| 441 | 17.362 | 17.366 | 17.370 | 17.374 | 17.378 | 17.382 | 17.386 | 17.390 | 17.394 | 17.398 |
| 442 | 17.402 | 17.405 | 17.409 | 17.413 | 17.417 | 17.42 I | 17.425 | 17.429 | 17.433 | 17.437 |
| 443 | 17.44 I | 17.445 | 17.449 | 17.453 | 17.457 | 17.461 | 17.465 | 17.468 | 17.472 | 17.476 |
| 444 | 17.480 | 17.484 | 17.488 | 17.492 | 17.496 | 17.500 | 17.504 | 17.508 | 17.512 | 17.516 |
| 445 | 17.520 | 17.524 | 17.528 | 17.531 | 17.535 | 17.539 | 17.543 | 17.547 | ${ }^{1} 7.551$ | 17.555 |
| 446 | 17.559 | 17.563 | 17.567 | 17.571 | 17.575 | 17.579 | 17.583 | 17.587 | 17.591 | 17.594 |
| 447 | 17.598 | 17.602 | 17.606 | 17.610 | 17.614 | 17.618 | 17.622 | 17.626 | 17.630 | 17.634 |
| 448 | 17.638 | 17.642 | 17.646 17.685 | 17.650 17.689 | 17.654 | 17.657 | 17.661 | 17.665 | 17.669 17.709 | 17.673 17.713 |
| 449 | 17.677 | 17.681 | 17.685 | 17.689 | 17.693 | 17.697 | 17.701 | 17.705 | 17.709 | 17.713 |
| 450 | 17.717 | 17.720 | 17.724 | 17.728 | 17.732 | 17.736 | 17.740 | 17.744 | 17.74 S | 17.752 |

MILLIMETRES INTO INCHES.
I mm. $=0.03937$ inch.

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | 6 | . 7 | 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 450 | 17.717 | 17.720 | 17.724 | 17.728 | 17.732 | 17.736 | 17.740 | 17.744 | 17.748 | 17.752 |
| 451 | 17.756 | 17.760 | 17.764 | 17.768 | 17.772 | 17.776 | 17.779 | 17.783 | 17.787 | 17.791 |
| 452 | 17.795 | 17.799 | 17.803 | 17.807 | 17.81 I | I7.815 | 17.819 | 17.823 | 17.827 | 17.83 I |
| 453 | 17.835 | 17.839 | 17.842 | 17.846 | 17.850 | 17.854 | 17.858 | 17.862 | 17.866 | 17.870 |
| 454 | 17.874 | 17.878 | 17.882 | 17.886 | 17.890 | 17.894 | 17.898 | 17.902 | 17.905 | 17.909 |
| 455 | 17.913 | 17.917 | 17.921 | 17.925 | 17.929 | 17.933 | 17.937 | 17.941 | 17.945 | 17.949 |
| 456 | 17.953 | 17.957 | 17.961 | 17.965 | 17.968 | 17.972 | 17.976 | 17.980 | 17.984 | 17.988 |
| 457 | 17.992 | 17.996 | 18.000 | 18.004 | 18.008 | 18.012 | 18.016 | 18.020 | 18.024 | 18.028 |
| 458 | 18.031 | 18.035 | 18.039 | 18.043 | 18.047 | 18.05I | 18.055 | 18.059 | 18.063 | 18.067 |
| 459 | 18.071 | 18.075 | 18.079 | 18.083 | 18.087 | 18.091 | 18.094 | 18.098 | 18.102 | 18.106 |
| 460 | 18.110 | 18.114 | I8.118 | 18. 122 | 18.126 | 18.130 | 18. 134 | 18.138 | 18.142 | 18.146 |
| 461 | 18.150 | 18.154 | 18.157 | 18.16I | 18.165 | 18.169 | 18.173 | 18.177 | 18.18I | 18.185 |
| 462 | 18.189 | 18.193 | 18.197 | 18.201 | I8.205 | 18.209 | 18.213 | 18.216 | 18.220 | 18.224 |
| 463 | 18.228 | 18.232 | 18.236 | 18.240 | 18.244 | 18.248 | 18.252 | I8.256 | 18.260 | 18.264 |
| 464 | 18.268 | 18.272 | 18.276 | 18.279 | 18.283 | 18.287 | 18.291 | 18.295 | 18.299 | 18.303 |
| 465 | 18.307 | 18.311 | 18.315 | 18.319 | 18.323 | 18.327 | 18.33I | 18.335 | 18.339 | 18.342 |
| 466 | 18.346 | 18.350 | 18.354 | 18.358 | 18.362 | I8.366 | 18.370 | 18.374 | 18.378 | 18.382 |
| 467 | 18.386 | 18.390 | 18.394 | 18.398 | 18.402 | 18.405 | 18.409 | 18.413 | 18.417 | 18.42 I |
| 468 | I8.425 | 18.429 | 18.433 | 18.437 | 18.441 | 18.445 | 18.449 | 18.453 | 18.457 | 18.46 I |
| 469 | 18.465 | 18.468 | 18.472 | 18.476 | 18.480 | 18.484 | 18.488 | 18.492 | 18.496 | 18.500 |
| 470 | 18.504 | 18.508 | 18.512 | 18.516 | 18.520 | 18.524 | 18.528 | 18.53I | 18.535 | 18.539 |
| 471 | 18.543 | 18.547 | 18.55 I | 18.555 | 18.559 | 18.563 | 18.567 | 18.571 | 18.575 | 18.579 |
| 472 | 18.583 | 18.587 | 18.591 | 18.594 | 18.598 | 18.602 | 18.606 | 18.610 | 18.614 | 18.618 |
| 473 | 18.622 | 18.626 | 18.630 | 18.634 | 18.638 | 18.642 | 18.646 | I8.650 | 18.654 | 18.657 |
| 474 | 18.661 | 18.665 | 18.669 | 18.673 | 18.677 | 18.681 | 18.685 | 18.689 | 18.693 | 18.697 |
| 475 | 18.701 | 18.705 | 18.709 | 18.713 | 18.716 | 18.720 | 18.724 | 18.728 | 18.732 | 18.736 |
| 476 | 18.740 | 18.744 | 18.748 | 18.752 | 18.756 | 18.760 | 18.764 | 18.768 | 18.772 | 18.776 |
| 477 | 18.779 | 18.783 | 18.787 | 18.791 | 18.795 | 18.799 | 18.803 | 18.807 | 18.811 | 18.815 |
| 478 | 18.819 | 18.823 | 18.827 | 18.83 I | 18.835 | 18.839 | I8.842 | 18.846 | 18.850 | 18.854 |
| 479 | 18.858 | 18.862 | 18.866 | 18.870 | 18.874 | 18.878 | 18.882 | 18.886 | 18.890 | 18.894 |
| 480 | 18.898 | 18.902 | 18.905 | 18.909 | 18.913 | 18.917 | 18.921 | 18.925 | 18.929 | 18.933 |
| 481 | 18.937 | 18.941 | 18.945 | 18.949 | 18.953 | 18.957 | 18.961 | 18.965 | 18.968 | 18.972 |
| 482 | 18.976 | 18.980 | 18.984 | 18.988 | 18.992 | 18.996 | 19.000 | 19.004 | 19.008 | 19.012 |
| 483 | 19.016 | 19.020 | 19.024 | 19.028 | 19.03I | 19.035 | 19.039 | 19.043 | 19.047 | 19.05 I |
| 484 | 19.055 | 19.059 | 19.063 | 19.067 | 19.071 | 19.075 | 19.079 | 19.083 | 19.087 | 19.091 |
| 485 | 19.094 | 19.098 | 19.102 | 19.106 | 19.110 | 19.114 | 19.118 | 19.122 | 19. 126 | 19.130 |
| 486 | 19.134 | 19.138 | 19.142 | 19.146 | 19.150 | 19.154 | 19. 157 | 19.16I | 19.165 | 19.169 |
| 487 | 19.173 | 19.177 | 19.181 | 19.185 | 19.189 | 19.193 | I9.197 | 19.201 | 19.205 | 19.209 |
| 488 | 19.213 | 19.216 | 19.220 | 19.224 | 19.228 | 19.232 | 19.236 | 19.240 | 19.244 | 19.248 |
| 489 | 19.252 | 19.256 | 19.260 | 19.264 | 19.268 | 19.272 | 19.276 | 19.279 | 19.283 | 19.287 |
| 490 | 19.291 | 19.295 | 19.299 | 19.303 | 19.307 | 19.3II | 19.315 | 19.319 | 19.323 | 19.327 |
| 49 I | 19.33 I | 19.335 | 19.339 | 19.342 | 19.346 | 19.350 | 19.354 | 19.358 | 19.362 | 19.366 |
| 492 | 19.370 | 19.374 | 19.378 | 19.382 | 19.386 | 19.390 | 19.394 | 19.398 | 19.402 | 19.405 |
| 493 | 19.409 | 19.413 | 19.417 | 19.42 I | 19.425 | 19.429 | 19.433 | 19.437 | 19.441 | 19.445 |
| 494 | 19.449 | 19.453 | 19.457 | 19.461 | 19.465 | 19.468 | 19.472 | 19.476 | 19.480 | 19.484 |
| 495 | 19.488 | 19.492 | 19.496 | 19.500 | 19.504 | 19.508 | 19.512 | 19.516 | 19.520 | 19.524 |
| 496 | 19.528 | 19.53 I | 19.535 | 19.539 | 19.543 | 19.547 | 19.551 | 19.555 | 19.559 | 19.563 |
| 497 | I9.567 | 19.571 | 19.575 | 19.579 | 19.583 | 19.587 | 19.591 | 19.594 | 19.598 | 19.602 |
| 498 | 19.606 | 19.610 | 19.614 | 19.618 | 19.622 | 19.626 | 19.630 | 19.634 | 19.638 | 19.642 |
| 499 | 19.646 | 19.650 | 19.654 | 19.657 | 19.66I | 19.665 | 19.669 | 19.673 | 19.677 | 19.68I |
| 500 | 19.685 | 19.689 | 19.693 | 19.697 | 19.701 | 19.705 | 19.709 | 19.713 | 19.716 | 19.720 |

MILLIMETRES INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch .

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 500 | 19.685 | 19.689 | 19.693 | 19.697 | 19.701 | 19.705 | 19.709 | 19.713 | 19.716 | 19.720 |
| 501 | 19.724 | 19.728 | 19.732 | 19.736 | 19.740 | 19.744 | 19.748 | 19.752 | 19.756 | 19.760 |
| 502 | 19.764 | 19.768 | 19.772 | 19.776 | 19.779 | 19.783 | 19.787 | 19.791 | 19.795 | 19.799 |
| 503 | 19.803 | 19.807 | 19.811 | 19.815 | 19.819 | 19.823 | 19.827 | 19.831 | 19.835 | 19.839 |
| 504 | 19.842 | 19.846 | 19.850 | 19.854 | 19.858 | 19.862 | 19.866 | 19.870 | 19.874 | 19.878 |
| 505 | 19.882 | 19.886 | 19.890 | 19.894 | 19.898 | 19.902 | 19.905 | 19.909 | 19.913 | 19.917 |
| 506 | 19.92 I | 19.925 | 19.929 | 19.933 | 19.937 | 19.94 I | 19.945 | 19.949 | 19.953 | 19.957 |
| 507 | 19.961 | 19.965 | 19.968 | 19.972 | 19.976 | 19.980 | 19.984 | 19.988 | 19.992 | 19.996 |
| 508 | 20.000 | 20.004 | 20.008 | 20.012 | 20.016 | 20.025 | 20.024 | 20.028 | 20.03 I | 20.035 |
| 509 | 20.039 | 20.043 | 20.047 | 20.051 | 20.055 | 20.059 | 20.063 | 20.067 | 20.07 I | 20.075 |
| 510 | 20.079 | 20.083 | 20.087 | 20.091 | 20.094 | 20.098 | 20.102 | 20.106 | 20.110 | 20.114 |
| 511 | 20.118 | 20.122 | 20.126 | 20.130 | 20.134 | 20.138 | 20.142 | 20.146 | 20.150 | 20.154 |
| 512 | 20.157 | 20.16I | 20.165 | 20.169 | 20.173 | 20.177 | 20.181 | 20.185 | 20.189 | 20.193 |
| 513 | 20.197 | 20.201 | 20.205 | 20.209 | 20.213 | 20.216 | 20.220 | 20.224 | 20.228 | 20.232 |
| 5I4 | 20.236 | 20.240 | 20.244 | 20.248 | 20.252 | 20.256 | 20.260 | 20.264 | 20.268 | 20.272 |
| 515 | 20.276 | 20.279 | 20.283 | 20.287 | 20.291 | 20.295 | 20.299 | 20.303 | 20.307 | 20.311 |
| 516 | 20.315 | 20.319 | 20.323 | 20.327 | 20.33I | 20.335 | 20.339 | 20.342 | 20.346 | 20.350 |
| 517 | 20.354 | 20.358 | 20.362 | 20.366 | 20.370 | 20.374 | 20.378 | 20.382 | 20.386 | 20.390 |
| 518 | 20.394 | 20.398 | 20.402 | 20.405 | 20.409 | 20.413 | 20.417 | 20.42 I | 20.425 | 20.429 |
| 519 | 20.433 | 20.437 | 20.44 I | 20.445 | 20.449 | 20.453 | 20.457 | 20.461 | 20.465 | 20.468 |
| 520 | 20.472 | 20.476 | 20.480 | 20.484 | 20.488 | 20.492 | 20.496 | 20.500 | 20.504 | 20.508 |
| 521 | 20.512 | 20.516 | 20.520 | 20.524 | 20.528 | 20.53 I | 20.535 | 20.539 | 20.543 | 20.547 |
| 522 | 20.55 I | 20.555 | 20.559 | 20.563 | 20.567 | 20.571 | 20.575 | 20.579 | 20.583 | 20.587 |
| 523 | 20.591 | 20.594 | 20.598 | 20.602 | 20.606 | 20.610 | 20.614 | 20.618 | 20.622 | 20.626 |
| 524 | 20.630 | 20.634 | 20.638 | 20.642 | 20.646 | 20.650 | 20.654 | 20.657 | 20.66I | 20.665 |
| 525 | 20.669 | 20.673 | 20.677 | 20.68I | 20.685 | 20.689 | 20.693 | 20.697 | 20.701 | 20.705 |
| 526 | 20.709 | 20.713 | 20.716 | 20.720 | 20.724 | 20.728 | 20.732 | 20.736 | 20.740 | 20.744 |
| 527 | 20.748 | 20.752 | 20.756 | 20.760 | 20.764 | 20.768 | 20.772 | 20.776 | 20.779 | 20.783 |
| 528 | 20.787 | 20.791 | 20.795 | 20.799 | 20.803 | 20.807 | 20.81 I | 20.815 | 20.819 | 20.823 |
| 529 | 20.827 | 20.83 I | 20.835 | 20.839 | 20.842 | 20.846 | 20.850 | 20.854 | 20.858 | 20.862 |
| 530 | 20.866 | 20.870 | 20.874 | 20.878 | 20.882 | 20.886 | 20.890 | 20.894 | 20.898 | 20.902 |
| 531 | 20.905 | 20.909 | 20.913 | 20.917 | 20.92 I | 20.925 | 20.929 | 20.933 | 20.937 | 20.941 |
| 532 | 20.945 | 20.949 | 20.953 | 20.957 | 20.96I | 20.965 | 20.968 | 20.972 | 20.976 | 20.980 |
| 533 | 20.984 | 20.988 | 20.992 | 20.996 | 21.000 | 21.004 | 21.008 | 21.012 | 21.016 | 21.020 |
| 534 | 21.024 | 21.028 | 21.03I | 21.035 | 21.039 | 21.043 | 21.047 | 21.051 | 21.055 | 21.059 |
| 535 | 21.063 | 21.067 | 21.07I | 21.075 | 2 I .079 | 21.083 | 21.087 | 21.091 | 21.094 | 21.098 |
| 536 | 21.102 | 21.106 | 21.110 | 21.114 | 21.118 | 21.122 | 21.126 | 21.130 | 21.134 | 21.138 |
| 537 | 21.142 | 21.146 | 21.150 | 21.154 | 2 I .157 | 21.16I | 21.165 | 21.169 | 21.173 | 21.177 |
| 538 | 21.18I | 21.185 | 21.189 | 21.193 | 21.197 | 21.201 | 21.205 | 21.209 | 21.213 | 21.216 |
| 539 | 21.220 | 21.224 | 21.228 | 21.232 | 21.236 | 21.240 | 21.244 | 21.248 | 21.252 | 21.256 |
| 540 | 21.260 | 21.264 | 21.268 | 21.272 | 21.276 | 21.279 | 21.283 | 21.287 | 21.29I | 21.295 |
| 541 | 21.299 | 21.303 | 21.307 | 21.311 | 2 I .315 | 21.319 | 21.323 | 21.327 | 21.33I | 21.335 |
| 542 | 21.339 | 21.342 | 21.346 | 21.350 | 2 I .354 | 2 I .358 | 21.362 | 21.366 | 21.370 | 21.374 |
| 543 | 21.378 | 21.382 | 21.386 | 21.390 | 21.394 | 2 I .398 | 21.402 | 21.405 | 21.409 | 2 I .413 |
| 544 | 21.417 | 21.421 | 21.425 | 21.429 | 21.433 | 21.437 | 21.441 | 21.445 | 21.449 | 21.453 |
| 545 | 2 I .457 | 21.461 | 21.465 | 21.468 | 21.472 | 21.476 | 21.48o | 21.484 | 21.488 | 2 I .492 |
| 546 | 21.496 | 21.500 | 21.504 | 21.508 | 21.512 | 21.516 | 21.520 | 21.524 | 21.528 | 21.53 I |
| 547 | 21.535 | 21. 539 | 21.543 | 21.547 | 21.55I | 21.555 | 21.559 | 21.563 | $21.567$ | 21.57 I |
| 548 | 21.575 | 21.579 | 21.583 | 21.587 | 21.591 | 21.594 | 21.598 | 21.602 | 21.606 | 21.610 |
| 549 | 21.614 | 21.618 | 21.622 | 21.626 | 21.630 | 21.634 | 21.638 | 21.642 | 21.646 | 21.650 |
| 550 | 21.654 | 21.657 | 21.661 | 21.665 | 21.66s | 21.673 | 21.677 | 21.68I | 21.685 | 21.689 |

## MILLIMETRES INTO INCHES.

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 550 | 21.654 | 21.657 | 21.66r | 21.665 | 21.669 | 21.673 | 21.677 | 21.68I | 21.685 | 21.689 |
| 551 | 21.693 | 21.697 | 21.701 | 21.705 | 21.709 | 21.713 | 21.716 | 21.720 | 21.724 | 21.728 |
| 552 | 21.732 | 21.736 | 21.740 | 21.744 | 21.748 | 21.752 | 21.756 | 21.760 | 21.764 | 21.768 |
| 553 | 21.772 | 21.776 | 21.779 | 21.783 | 21.787 | 21.791 | 21.795 | 21.799 | 21.803 | 21.807 |
| 554 | 21.8II | 21.815 | 21.819 | 21.823 | 21.827 | 21.83 I | 21.835 | 21.839 | 21.842 | 21.846 |
| 555 | 21.850 | 21.854 | 21.858 | 21.862 | 21.866 | 21.870 | 21.874 | 21.878 | 21.882 | 21.886 |
| 556 | 21.890 | 21.894 | 21.898 | 21.902 | 21.905 | 21.909 | 21.913 | 21.917 | 21.921 | 21.925 |
| 557 | 21.929 | 21.933 | 21.937 | 21.941 | 21.945 | 21.949 | 21.953 | 21.957 | 21.961 | 21.965 |
| 558 | 21.968 | 21.972 | 21.976 | 21.980 | 21.984 | 21.988 | 21.992 | 21.996 | 22.000 | 22.004 |
| 559 | 22.008 | 22.012 | 22.016 | 22.020 | 22.024 | 22.028 | 22.03 I | 22.035 | 22.039 | 22.043 |
| 560 | 22.047 | 22.051 | 22.055 | 22.059 | 22.063 | 22.067 | 22.071 | 22.075 | 22.079 | 22.083 |
| 561 | 22.087 | 22.091 | 22.094 | 22.098 | 22.102 | 22.106 | 22.110 | 22.114 | 22.118 | 22.122 |
| 562 | 22.126 | 22.130 | 22.134 | 22.138 | 22.142 | 22.146 | 22.150 | 22.153 | 22.157 | 22.16I |
| 563 | 22.165 | 22.169 | 22.173 | 22.177 | 22.181 | 22.185 | 22.189 | 22.193 | 22.197 | 22.201 |
| 564 | 22.205 | 22.209 | 22.213 | 22.216 | 22.220 | 22.224 | 22.228 | 22.232 | 22.236 | 22.240 |
| 565 | 22.244 | 22.248 | 22.252 | 22.256 | 22.260 | 22.264 | 22.268 | 22.272 | 22.276 | 22.279 |
| 566 | 22.283 | 22.287 | 22.29 I | 22.295 | 22.299 | 22.303 | 22.307 | 22.311 | 22.315 | 22.319 |
| 567 | 22.323 | 22.327 | 22.33 I | 22.335 | 22.339 | 22.342 | 22.346 | 22.350 | 22.354 | 22.358 |
| 568 | 22.362 | 22.366 | 22.370 | 22.374 | 22.378 | 22.382 | 22.386 | 22.390 | 22.394 | 22.398 |
| 569 | 22.402 | 22.405 | 22.409 | 22.413 | 22.417 | 22.42 I | 22.425 | 22.429 | 22.433 | 22.437 |
| 570 | 22.44 I | 22.445 | 22.449 | 22.453 | 22.457 | 22.46 I | 22.465 | 22.468 | 22.472 | 22.476 |
| 571 | 22.480 | 22.484 | 22.488 | 22.492 | 22.496 | 22.500 | 22.504 | 22.508 | 22.512 | 22.516 |
| 572 | 22.520 | 22.524 | 22.528 | 22.53 I | 22.535 | 22.539 | 22.543 | 22.547 | 22.55 I | 22.555 |
| 573 | 22.559 | 22.563 | 22.567 | 22.57 I | 22.575 | 22.579 | 22.583 | 22.587 | 22.59 I | 22.594 |
| 574 | 22.598 | 22.602 | 22.606 | 22.610 | 22.614 | 22.618 | 22.622 | 22.626 | 22.630 | 22.634 |
| 575 | 22.638 | 22.642 | 22.646 | 22.650 | 22.653 | 22.657 | 22.661 | 22.665 | 22.669 | 22.673 |
| 576 | 22.677 | 22.681 | 22.685 | 22.689 | 22.693 | 22.697 | 22.701 | 22.705 | 22.709 | 22.713 |
| 577 | 22.716 | 22.720 | 22.724 | 22.728 | 22.732 | 22.736 | 22.740 | 22.744 | 22.748 | 22.752 |
| 578 | 22.756 | 22.760 | 22.764 | 22.768 | 22.772 | 22.776 | 22.779 | 22.783 | 22.787 | 22.791 |
| 579 | 22.795 | 22.799 | 22.803 | 22.807 | 22.8II | 22.815 | 22.819 | 22.823 | 22.827 | 22.83 r |
| 580 | 22.835 | 22.839 | 22.842 | 22.846 | 22.850 | 22.854 | 22.858 | 22.862 | 22.866 | 22.870 |
| 581 | 22.874 | 22.878 | 22.882 | 22.886 | 22.890 | 22.894 | 22.898 | 22.902 | 22.905 | 22.909 |
| 582 | 22.913 | 22.917 | 22.921 | 22.925 | 22.929 | 22.933 | 22.937 | 22.94 I | 22.945 | 22.949 |
| 583 | 22.953 | 22.957 | 22.961 | 22.965 | 22.968 | 22.972 | 22.976 | 22.980 | 22.984 | 22.988 |
| 584 | 22.992 | 22.996 | 23.000 | 23.004 | 23.008 | 23.012 | 23.016 | 23.020 | 23.024 | 23.028 |
| 585 | 23.031 | 23.035 | 23.039 | 23.043 | 23.047 | 23.051 | 23.055 | 23.059 | 23.063 | 23.067 |
| 586 | 23.071 | 23.075 | 23.079 | 23.083 | 23.087 | 23.091 | 23.094 | 23.098 | 23.102 | 23.106 |
| 587 | 23.110 | 23.114 | 23.118 | 23.122 | 23.126 | 23.130 | 23.134 | 23.138 | 23.142 | 23.146 |
| 588 | 23.150 | 23.153 | 23.157 | 23.16I | 23.165 | 23.169 | 23.173 | 23.177 | 23.181 | 23.185 |
| 589 | 23.189 | 23.193 | 23. 197 | 23.201 | 23.205 | 23.209 | 23.213 | 23.216 | 23.220 | 23.224 |
| 590 | 23.228 | 23.232 | 23.236 | 23.240 | 23.244 | 23.248 | 23.252 | 23.256 | 23.260 | 23.264 |
| 591 | 23.268 | 23.272 | 23.276 | 23.279 | 23.283 | 23.287 | 23.291 | 23.295 | 23.299 | 23.303 |
| 592 | 23.307 | 23.311 | 23.315 | 23.319 | 23.323 | 23.327 | 23.331 | 23.335 | 23.339 | 23.342 |
| 593 | 23.346 | 23.350 | 23.354 | 23.358 | 23.362 | 23.366 | 23.370 | 23.374 | 23.378 | 23.382 |
| 594 | 23.386 | 23.390 | 23.394 | 23.398 | 23.402 | 23.405 | 23.409 | 23.413 | 23.417 | 23.42 I |
| 595 | 23.425 | 23.429 | 23.433 | 23.437 | 23.44 I | 23.445 | 23.449 | 23.453 | 23.457 | 23.461 |
| 596 | 23.465 | 23.468 | 23.472 | 23.476 | 23.480 | 23.484 | 23.488 | 23.492 | 23.496 | 23.500 |
| 597 | 23.504 | 23.508 | 23.512 | 23.516 | 23.520 | 23.524 | 23.528 | 23.53 I | 23.535 | 23.539 |
| 598 | 23.543 | 23.547 | 23.551 | 23.555 | 23.559 | 23.563 | 23.567 | 23.57 I | 23.575 | 23.579 |
| 599 | 23.583 | 23.587 | 23.591 | 23.594 | 23.598 | 23.602 | 23.606 | 23.610 | 23.614 | 23.618 |
| 600 | 23.622 | 23.626 | 23.630 | 23.634 | 23.638 | 23.642 | 23.646 | 23.650 | 23.653 | 23.657 |

I mm. $=0.03937$ inch.

| Millimetres. | . 0 | . | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 600 | 23.622 | 23.626 | 23.630 | 23.634 | 23.638 | 23.642 | 23.646 | 23.650 | 23.653 | 23.657 |
| 601 | 23.661 | 23.665 | 23.669 | 23.673 | 23.677 | 23.68I | 23.685 | 23.689 | 23.693 | 23.697 |
| 602 | 23.701 | 23.705 | 23.709 | 23.713 | 23.716 | 23.720 | 23.724 | 23.728 | 23.732 | 23.736 |
| 603 | 23.740 | 23.744 | 23.748 | 23.752 | 23.756 | 23.760 | 23.764 | 23.768 | 23.772 | 23.776 |
| 604 | 23.779 | 23.783 | 23.787 | 23.791 | 23.795 | 23.799 | 23.803 | 23.807 | 23.8 II | 23.815 |
| 605 | 23.819 | 23.823 | 23.827 | 23.831 | 23.835 | 23.839 | 23.842 | 23.846 | 23.850 | 23.854 |
| 606 | 23.858 | 23.862 | 23.866 | 23.870 | 23.874 | 23.878 | 23.882 | 23.886 | 23.890 | 23.894 |
| 607 | 23.898 | 23.902 | 23.905 | 23.909 | 23.913. | 23.917 | 23.921 | 23.925 | 23.929 | 23.933 |
| 608 | 23.937 | 23.941 | 23.945 | 23.949 | 23.953 | 23.957 | 23.96I | 23.965 | 23.968 | 23.972 |
| 609 | 23.976 | 23.980 | 23.984 | 23.988 | 23.992 | 23.996 | 24.000 | 24.004 | 24.008 | 24.012 |
| 610 | 24.016 | 24.020 | 24.024 | 24.028 | 24.031 | 24.035 | 24.039 | 24.043 | 24.047 | 24.05 I |
| 611 | 24.055 | 24.059 | 24.063 | 24.067 | 24.071 | 24.075 | 24.079 | 24.083 | 24.087 | 24.091 |
| 612 | 24.094 | 24.098 | 24. 102 | 24.106 | 24. 110 | 24. II 4 | 24.118 | 24.122 | 24.126 | 24.130 |
| 613 | 24.134 | 24.138 | 24.142 | 24.146 | 24.150 | 24.153 | 24.157 | 24.16I | 24.165 | 24.169 |
| 614 | 24.173 | 24.177 | 24.181 | 24.185 | 24.189 | 24. 193 | 24.197 | 24.201 | 24.205 | 24.209 |
| 615 | 24.213 | 24.216 | 24.220 | 24.224 | 24.228 | 24.232 | 24.236 | 24.240 | 24.244 | 24.248 |
| 616 | 24.252 | 24.256 | 24.260 | 24.264 | 24.268 | 24.272 | 24.276 | 24.279 | 24.283 | 24.287 |
| 617 | 24.291 | 24.295 | 24.299 | 24.303 | 24.307 | 24.311 | 24.315 | 24.319 | 24.323 | 24.327 |
| 6 I 8 | 24.331 | 24.335 | 24.339 | 24.342 | 24.346 | 24.350 | 24.354 | 24.358 | 24.362 | 24.366 |
| 619 | 24.370 | 24.374 | 24.378 | 24.382 | 24.386 | 24.390 | 24.394 | 24.398 | 24.402 | 24.405 |
| 620 | 24.409 | 24.413 | 24.417 | 24.42 I | 24.425 | 24.429 | 24.433 | 24.437 | 24.44 I | 24.445 |
| 621 | 24.449 | 24.453 | 24.457 | 24.461 | 24.465 | 24.468 | 24.472 | 24.476 | 24.480 | 24.484 |
| 622 | 24.488 | 24.492 | 24.496 | 24.500 | 24.504 | 24.508 | 24.512 | 24.516 | 24.520 | 24.524 |
| 623 | 24.528 | 24.531 | 24.535 | 24.539 | 24.543 | 24.547 | 24.55I | 24.555 | 24.559 | 24.563 |
| 624 | 24.567 | 24.57 I | 24.575 | 24.579 | 24.583 | 24.587 | 24.59I | 24.594 | 24.598 | 24.602 |
| 625 | 24.606 | 24.610 | 24.614 | 24.618 | 24.622 | 24.626 | 24.630 | 24.634 | 24.638 | 24.642 |
| 626 | 24.646 | 24.650 | 24.653 | 24.657 | 24.661 | 24.665 | 24.669 | 24.673 | 24.677 | 24.68I |
| 627 | 24.685 | 24.689 | 24.693 | 24.697 | 24.701 | 24.705 | 24.709 | 24.713 | 24.716 | 24.720 |
| 628 | 24.724 | 24.728 | 24.732 | 24.736 | 24.740 | 24.744 | 24.748 | 24.752 | 24.756 | 24.760 |
| 629 | 24.764 | 24.768 | 24.772 | 24.776 | 24.779 | 24.783 | 24.787 | 24.79I | 24.795 | 24.799 |
| 630 | 24.803 | 24.807 | 24.8 II | 24.815 | 24.819 | 24.823 | 24.827 | 24.83 I | 24.835 | 24.839 |
| 631 | 24.842 | 24.846 | 24.850 | 24.854 | 24.858 | 24.862 | 24.866 | 24.870 | 24.874 | 24.878 |
| 632 | 24.882 | 24.886 | 24.890 | 24.894 | 24.898 | 24.902 | 24.905 | 24.909 | 24.913 | 24.917 |
| 633 | 24.92 I | 24.925 | 24.929 | 24.933 | 24.937 | 24.94 I | 24.945 | 24.949 | 24.953 | 24.957 |
| 634 | 24.961 | 24.965 | 24.968 | 24.972 | 24.976 | 24.980 | 24.984 | 24.988 | 24.992 | 24.996 |
| 635 | 25.000 | 25.004 | 25.008 | 25.012 | 25.016 | 25.020 | 25.024 | 25.028 | 25.031 | 25.035 |
| 636 | 25.039 | 25.043 | 25.047 | 25.05I | 25.055 | 25.059 | 25.063 | 25.067 | 25.07 I | 25.075 |
| 637 | 25.079 | 25.083 | 25.087 | 25.091 | 25.094 | 25.098 | 25. IO2 | 25.106 | 25.110 | 25.1 I4 |
| 638 | 25.118 | 25.122 | 25.126 | 25.130 | 25.134 | 25.138 | 25.142 | 25.146 | 25.150 | 25.153 |
| 639 | 25.157 | 25.16I | 25.165 | 25.169 | 25.173 | 25.177 | 25.181 | 25.185 | 25.189 | 25.193 |
| 640 | 25:197 | 25.201 | 25.205 | 25.209 | 25.213 | 25.216 | 25.220 | 25.224 | 25.228 | 25.232 |
| 641 | 25.236 | 25.240 | 25.244 | 25.248 | 25.252 | 25.256 | 25.260 | 25.264 | 25.268 | 25.272 |
| 642 | 25.276 | 25.279 | 25.283 | 25.287 | 25.29 I | 25.295 | 25.299 | 25.303 | 25.307 | 25.3 II |
| 643 | 25.315 | 25.319 | 25.323 | 25.327 | 25.33I | 25.335 | 25.339 | 25.342 | 25.346 | 25.350 |
| 644 | 25.354 | 25.358 | 25.362 | 25.366 | 25.370 | 25.374 | 25.378 | 25.382 | 25.386 | 25.390 |
| 645 | 25.394 | 25.398 | 25.402 | 25.405 | 25.409 | 25.413 | 25.417 | 25.42 I | 25.425 | 25.429 |
| 646 | 25.433 | 25.437 | 25.441 | 25.445 | 25.449 | 25.453 | 25.457 | 25.46 I | 25.465 | 25.468 |
| 647 | 25.472 | 25.476 | 25.480 | 25.484 | 25.488 | 25.492 | 25.496 | 25.500 | 25.504 | 25.508 |
| 648 | 25.512 | 25.516 | 25.520 | 25.524 | 25.528 | 25.53 I | 25.535 | 25.539 | 25.543 | 25.547 |
| 649 | 25.55 I | 25.555 | 25.559 | 25.563 | 25.567 | 25.571 | 25.575 | 25.579 | 25.583 | 25.587 |
| 650 | 25.59I | 25.594 | 25.598 | 25.602 | 25.606 | 25.610 | 25.614 | 25.618 | 25.622 | 25.626 |

## TABLE 65.

MILLIMETRES INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch .

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 650 | 25.591 | 25.594 | 25.598 | 25.602 | 25.606 | 25.610 | 25.614 | 25.618 | 25.622 | 25.626 |
| 651 | 25.630 | 25.634 | 25.638 | 25.642 | 25.646 | 25.650 | 25.653 | 25.657 | 25.661 | 25.665 |
| 652 | 25.669 | 25.673 | 25.677 | 25.681 | 25.685 | 25.689 | 25.693 | 25.697 | 25.7 OI | 25.705 |
| 653 | 25.709 | 25.713 | 25.716 | 25.720 | 25.724 | 25.728 | 25.732 | 25.736 | 25.740 | 25.744 |
| 654 | 25.748 | 25.752 | 25.756 | 25.760 | 25.764 | 25.768 | 25.772 | 25.776 | 25.779 | 25.783 |
| 655 | 25.787 | 25.791 | 25.795 | 25.799 | 25.803 | 25.807 | 25.8 II | 25.815 | 25.819 | 25.823 |
| 656 | 25.827 | 25.831 | 25.835 | 25.839 | 25.842 | 25.846 | 25.850 | 25.854 | 25.858 | 25.862 |
| 657 | 25.866 | 25.870 | 25.874 | 25.878 | 25.882 | 25.886 | 25.890 | 25.894 | 25.898 | 25.902 |
| 658 | 25.905 | 25.909 | 25.913 | 25.917 | 25.921 | 25.925 | 25.929 | 25.933 | 25.937 | 25.941 |
| 659 | 25.945 | 25.949 | 25.953 | 25.957 | 25.961 | 25.965 | 25.968 | 25.972 | 25.976 | 25.980 |
| 660 | 25.984 | 25.988 | 25.992 | 25.996 | 26.000 | 26.004 | 26.008 | 26.012 | 26.016 | 26.020 |
| 661 | 26.024 | 26.028 | 26.031 | 26.035 | 26.039 | 26.043 | 26.047 | 26.051 | 26.055 | 26.059 |
| 662 | 26.063 | 26.067 | 26.071 | 26.075 | 26.079 | 26.083 | 26.087 | 26.090 | 26.094 | 26.098 |
| 663 | 26.102 | 26.106 | 26.110 | 26.114 | 26.118 | 26.122 | 26.126 | 26.130 | 26.134 | 26.138 |
| 664 | 26.142 | 26.146 | 26.150 | 26.153 | 26.157 | 26.16I | 26.165 | 26.169 | 26.173 | 26.177 |
| 665 | 26.181 | 26.185 | 26.189 | 26.193 | 26.197 | 26.201 | 26.205 | 26.209 | 26.213 | 26.216 |
| 666 | 26.220 | 26.224 | 26.228 | 26.232 | 26.236 | 26.240 | 26.244 | 26.248 | 26.252 | 26.256 |
| 667 | 26.260 | 26.264 | 26.268 | 26.272 | 26.276 | 26.279 | 26.283 | 26.287 | 26.291 | 26.295 |
| 668 | 26.299 | 26.303 | 26.307 | 26.311 | 26.315 | 26.319 | 26.323 | 26.327 | 26.33 I | 26.335 |
| 669 | 26.339 | 26.342 | 26.346 | 26.350 | 26.354 | 26.358 | 26.362 | 26.366 | 26.370 | 26.374 |
| 670 | 26.378 | 26.382 | 26.386 | 26.390 | 26.394 | 26.398 | 26.402 | 26.405 | 26.409 | 26.413 |
| 671 | 26.417 | 26.421 | 26.425 | 26.429 | 26.433 | 26.437 | 26.44 I | 26.445 | 26.449 | 26.453 |
| 672 | 26.457 | 26.461 | 26.465 | 26.468 | 26.472 | 26.476 | 26.480 | 26.484 | 26.488 | 26.492 |
| 673 | 26.496 | 26.500 | 26.504 | 26.508 | 26.512 | 26.516 | 26.520 | 26.524 | 26.528 | 26.531 |
| 674 | 26.535 | 26.539 | 26.543 | 26.547 | 26.55 I | 26.555 | 26.559 | 26.563 | 26.567 | 26.571 |
| 675 | 26.575 | 26.579 | 26.583 | 26.587 | 26.590 | 26.594 | 26.598 | 26.602 | 26.606 | 26.610 |
| 676 | 26.614 | 26.618 | 26.622 | 26.626 | 26.630 | 26.634 | 26.638 | 26.642 | 26.646 | 26.650 |
| 677 | 26.653 | 26.657 | 26.66I | 26.665 | 26.669 | 26.673 | 26.677 | 26.68I | 26.685 | 26.689 |
| 678 | 26.693 | 26.697 | 26.701 | 26.705 | 26.709 | 26.713 | 26.716 | 26.720 | 26.724 | 26.728 |
| 679 | 26.732 | 26.736 | 26.740 | 26.744 | 26.748 | 26.752 | 26.756 | 26.760 | 26.764 | 26.768 |
| 680 | 26.772 | 26.776 | 26.779 | 26.783 | 26.787 | 26.791 | 26.795 | 26.799 | 26.803 | 26.807 |
| 681 | 26.81 I | 26.815 | 26.819 | 26.823 | 26.827 | 26.831 | 26.835 | 26.838 | 26.842 | 26.846 |
| 682 | 26.850 | 26.854 | 26.858 | 26.862 | 26.866 | 26.870 | 26.874 | 26.878 | 26.882 | 26.886 |
| 683 | 26.890 | 26.894 | 26.898 | 26.902 | 26.905 | 26.909 | 26.913 | 26.917 | 26.92 I | 26.925 |
| 684 | 26.929 | 26.933 | 26.937 | 26.94 I | 26.945 | 26.949 | 26.953 | 26.957 | 26.96I | 26.965 |
| 685 | 26.968 | 26.972 | 26.976 | 26.980 | 26.984 | 26.988 | 26.992 | 26.996 | 27.000 | 27.004 |
| 686 | 27.008 | 27.012 | 27.016 | 27.020 | 27.024 | 27.028 | 27.031 | 27.035 | 27.039 | 27.043 |
| 687 | 27.047 | 27.051 | 27.055 | 27.059 | 27.063 | 27.067 | 27.071 | 27.075 | 27.079 | 27.083 |
| 688 | 27.087 | 27.090 | 27.094 | 27.098 | 27.102 | 27.106 | 27.110 | 27.114 | 27.118 | 27.122 |
| 689 | 27.126 | 27.130 | 27.134 | 27.138 | 27.142 | 27.146 | 27.150 | 27.153 | 27.157 | 27.16I |
| 690 | 27.165 | 27.169 | 27.173 | 27.177 | 27.181 | 27.185 | 27.189 | 27.193 | 27.197 | 27.201 |
| 691 | 27.205 | 27.209 | 27.213 | 27.216 | 27.220 | 27.224 | 27.228 | 27.232 | 27.236 | 27.240 |
| 692 | 27.244 | 27.248 | 27.252 | 27.256 | 27.260 | 27.264 | 27.268 | 27.272 | 27.276 | 27.279 |
| 693 | 27.283 | 27.287 | 27.291 | 27.295 | 27.299 | 27.303 | 27.307 | $27 \cdot 311$ | 27.315 | 27.319 |
| 694 | 27.323 | 27.327 | 27.33I | 27.335 | 27.339 | 27.342 | 27.346 | 27.350 | 27.354 | 27.358 |
| 695 | 27.362 | 27.366 | 27.370 | 27.374 | 27.378 | 27.382 | 27.386 | 27.390 | 27.394 | 27.398 |
| 696 | 27.402 | 27.405 | 27.409 | 27.413 | 27.417 | 27.421 | 27.425 | 27.429 | 27.433 | 27.437 |
| 697 | 27.44 I | 27.445 | 27.449 | 27.453 | 27.457 | 27.461 | 27.465 | 27.468 | 27.472 | 27.476 |
| 698 | 27.480 | 27.484 | 27.488 | 27.492 | 27.496 | 27.500 | 27.504 | 27.508 | 27.512 | 27.516 |
| 699 | 27.520 | 27.524 | 27.528 | 27.53 I | 27.535 | 27.539 | 27.543 | 27.547 | 27.551 | 27.555 |
| 700 | 27.559 | 27.563 | 27.567 | 27.57 I | 27.575 | 27.579 | 27.583 | 27.587 | 27.590 | 27.594 |

## Millimetres into inches.

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches |
| 700 | 27.559 | 27.563 | 27.567 | 27.57 I | 27.575 | 27.579 | 27.583 | 27.587 | 27.590 | 27.594 |
| 701 | 27.598 | 27.602 | 27.606 | 27.610 | 27.614 | 27.618 | 27.622 | 27.626 | 27.630 | 27.634 |
| 702 | 27.638 | 27.642 | 27.646 | 27.650 | 27.653 | 27.657 | 27.661 | 27.665 | 27.669 | 27.673 |
| 703 | 27.677 | 27.68 I | 27.685 | 27.689 | 27.693 | 27.697 | 27.701 | 27.705 | 27.709 | 27.713 |
| 704 | 27.716 | 27.720 | 27.724 | 27.728 | 27.732 | 27.736 | 27.740 | 27.744 | 27.748 | 27.752 |
| 705 | 27.756 | 27.760 | 27.764 | 27.768 | 27.772 | 27.776 | 27.779 | 27.783 | 27.787 | 27.791 |
| 706 | 27.795 | 27.799 | 27.803 | 27.807 | 27.811 | 27.815 | 27.819 | 27.823 | 27.827 | 27.83 I |
| 707 | 27.835 | 27.839 | 27.842 | 27.846 | 27.850 | 27.854 | 27.858 | 27.862 | 27.866 | 27.870 |
| 708 | 27.874 | 27.878 | 27.882 | 27.886 | 27.890 | 27.894 | 27.898 | 27.902 | 27.905 | 27.909 |
| 709 | 27.913 | 27.917 | 27.92I | 27.925 | 27.929 | 27.933 | 27.937 | 27.94I | 27.945 | 27.949 |
| 710 | 27.953 | 27.957 | 27.961 | 27.965 | 27.968 | 27.972 | 27.976 | 27.980 | 27.984 | 27.988 |
| 711 | 27.992 | 27.996 | 28.000 | 28.004 | 28.008 | 28.012 | 28.016 | 28.020 | 28.024 | 28.028 |
| 712 | 28.031 | 28.035 | 28.039 | 28.043 | 28.047 | 28.051 | 28.055 | 28.059 | 28.063 | 28.067 |
| 713 | 28.071 | 28.075 | 28.079 | 28.083 | 28.087 | 28.090 | 28.094 | 28.098 | 28.102 | 28.106 |
| 714 | 28.110 | 28.114 | 28. 118 | 28. 122 | 28. 126 | 28. 130 | 28.134 | 28.138 | 28.142 | 28.146 |
| 715 | 28.150 | 28. 153 | 28. 157 | 28.16I | 28.165 | 28.169 | 28. 173 | 28.177 | 28.181 | 28.185 |
| 716 | 28.189 | 28. 193 | 28.197 | 28.201 | 28.205 | 28.209 | 28.213 | 28.216 | 28.220 | 28.224 |
| 717 | 28.228 | 28.232 | 28.236 | 28.240 | 28.244 | 28.248 | 28.252 | 28.256 | 28.260 | 28.264 |
| 718 | 28.268 | 28.272 | 28.276 | 28.279 | 28.283 | 28.287 | 28.291 | 28.295 | 28.299 | 2 S .303 |
| 719 | 28.307 | 28.311 | 28.315 | 28.319 | 28.323 | 28.327 | 28.331 | 28.335 | 28.339 | 28.342 |
| 720 | 28.346 | 28.350 | 28.354 | 28.358 | 28.362 | 28.366 | 28.370 | 28.374 | 28.378 | 28.382 |
| 721 | 28.386 | 28.390 | 28.394 | 28.398 | 28.402 | 28.405 | 28.409 | 28.413 | 28.417 | 28.42 I |
| 722 | 28.425 | 28.429 | 28.433 | 28.437 | 28.44 I | 28.445 | 28.449 | 28.453 | 28.457 | 28.461 |
| 723 | 28.465 | 28.468 | 28.472 | 28.476 | 28.480 | 28.484 | 28.488 | 28.492 | 28.496 | 28.500 |
| 724 | 28.504 | 28.508 | 28.512 | 28.516 | 28.520 | 28.524 | 28.528 | 28.531 | 28.535 | 28.539 |
| 725 | 28.543 | 28.547 | 28.55 I | 28.555 | 28.559 | 28.563 | 28.567 | 28.571 | 28.575 | 28.579 |
| 726 | 28.583 | 28.587 | 28.590 | 28.594 | 28.598 | 28.602 | 28.606 | 28.610 | 28.614 | 28.618 |
| 727 | 28.622 | 28.626 | 28.630 | 28.634 | 28.638 | 28.642 | 28.646 | 28.650 | 28.653 | 28.657 |
| 728 | 28.661 | 28.665 | 28.669 | 28.673 | 28.677 | 28.681 | 28.685 | 28.689 | 28.693 | 28.697 |
| 729 | 28.701 | 28.705 | 28.709 | 28.713 | 28.716 | 28.720 | 28.724 | 28.728 | 28.732 | 28.736 |
| 730 | 28.740 | 28.744 | 28.748 | 28.752 | 28.756 | 28.760 | 28.764 | 28.768 | 28.772 | 28.776 |
| 731 | 28.779 | 28.783 | 28.787 | 28.791 | 28.795 | 28.799 | 28.803 | 28.807 | 28.811 | 28.815 |
| 732 | 28.819 | 28.823 | 28.827 | 28.831 | 28.835 | 28.839 | 28.842 | 28.846 | 28.850 | 28.854 |
| 733 | 28.858 | 28.862 | 28.866 | 28.870 | 28.874 | 28.878 | 28.882 | 28.886 | 28.890 | 28.594 |
| 734 | 28.898 | 28.902 | 28.905 | 28.909 | 28.913 | 28.917 | 28.92 I | 28.925 | 28.929 | 28.933 |
| 735 | 28.937 | 28.941 | 28.945 | 28.949 | 28.953 | 28.957 | 28.961 | 28.965 | 28.968 | 28.972 |
| 736 | 28.976 | 28.980 | 28.984 | 28.988 | 28.992 | 28.996 | 29.000 | 29.004 | 29.008 | 29.012 |
| 737 | 29.016 | 29.020 | 29.024 | 29.028 | 29.031 | 29.035 | 29.039 | 29.043 | 29.047 | 29.051 |
| 738 | 29.055 | 29.059 | 29.063 | 29.067 | 29.071 | 29.075 | 29.079 | 29.083 | 29.087 | 29.090 |
| 739 | 29.094 | 29.098 | 29.102 | 29.106 | 29.110 | 29.114 | 29.118 | 29.122 | 29.126 | 29.130 |
| 740 | 29. I34 | 29.138 | 29.142 | 29.146 | 29.150 | 29.153 | 29.157 | 29.16I | 29.165 | 29.169 |
| 741 | 29.173 | 29.177 | 29.181 | 29.185 | 29.189 | 29.193 | 29.197 | 29.201 | 29.205 | 29.209 |
| 742 | 29.213 | 29.216 | 29.220 | 29.224 | 29.228 | 29.232 | 29.236 | 29.240 | 29.244 | 29.248 |
| 743 | 29.252 | 29.256 | 29.260 | 29.264 | 29.268 | 29.272 | 29.276 | 29.279 | 29.283 | 29.287 |
| 744 | 29.291 | 29.295 | 29.299 | 29.303 | 29.307 | 29.311 | 29.315 | 29.319 | 29.323 | 29.327 |
| 745 | 29.331 | 29.335 | 29.339 | 29.342 | 29.346 | 29.350 | 29.354 | 29.358 | 29.362 | 29.366 |
| 746 | 29.370 | 29.374 | 29.378 | 29.382 | 29.386 | 29.390 | 29.394 | 29.398 | 29.402 | 29.405 |
| 747 | 29.409 | 29.413 | 29.417 | 29.421 | 29.425 | 29.429 | 29.433 | 29.437 | 29.44 I | 29.445 |
| 748 | 29.449 | 29.453 | 29.457 | 29.46 I | 29.465 | 29.468 | 29.472 | 29.476 | 29.480 | 29.484 |
| 749 | 29.488 | 29.492 | 29.496 | 29.500 | 29.504 | 29.508 | 29.512 | 29.516 | 29.520 | 29.524 |
| 750 | 29.528 | 29.53 I | 29.535 | 29.539 | 29.543 | 29.547 | 29.55 I | 29.555 | 29.559 | 29.563 |

MILLIMETRES INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch.

| Milli- metres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 750 | 29.528 | 29.53 I | 29.535 | 29.539 | 29.543 | 29.547 | 29.551 | 29.555 | 29.559 | 29.563 |
| 751 | 29.567 | 29.571 | 29.575 | 29.579 | 29.583 | 29.587 | 29.590 | 29.594 | 29.598 | 29.602 |
| 752 | 29.606 | 29.610 | 29.614 | 29.618 | 29.622 | 29.626 | 29.630 | 29.634 | 29.638 | 29.642 |
| 753 | 29.646 | 29.650 | 29.653 | 29.657 | 29.66I | 29.665 | 29.669 | 29.673 | 29.677 | 29.68I |
| 754 | 29.685 | 29.689 | 29.693 | 29.697 | 29.701 | 29.705 | 29.709 | 29.713 | 29.716 | 29.720 |
| 755 | 29.724 | 29.728 | 29.732 | 29.736 | 29.740 | 29.744 | 29.748 | 29.752 | 29.756 | 29.760 |
| 756 | 29.764 | 29.768 | 29.772 | 29.776 | 29.779 | 29.783 | 29.787 | 29.791 | 29.795 | 29.799 |
| 757 | 29.803 | 29.807 | 29.811 | 29.815 | 29.819 | 29.823 | 29.827 | 29.83 I | 29.835 | 29.839 |
| 758 | 29.842 | 29.846 | 29.850 | 29.854 | 29.858 | 29.862 | 29.866 | 29.870 | 29.874 | 29.878 |
| 759 | 29.882 | 29.886 | 29.890 | 29.894 | 29.898 | 29.902 | 29.905 | 29.909 | 29.913 | 29.917 |
| 760 | 29.921 | 29.925 | 29.929 | 29.933 | 29.937 | 29.941 | 29.945 | 29.949 | 29.953 | 29.957 |
| 761 | 29.96I | 29.965 | 29.968 | 29.972 | 29.976 | 29.980 | 29.984 | 29.988 | 29.992 | 29.996 |
| 762 | 30.000 | 30.004 | 30.008 | 30.012 | 30.016 | 30.020 | 30.024 | 30.027 | 30.03 I | 30.035 |
| 763 | 30.039 | 30.043 | 30.047 | 30.051 | 30.055 | 30.059 | 30.063 | 30.067 | 30.071 | 30.075 |
| 764 | 30.079 | 30.083 | 30.087 | 30.090 | 30.094 | 30.098 | 30.102 | 30.106 | 30.110 | 30.114 |
| 765 | 30.118 | 30.122 | 30.126 | 30.130 | 30.134 | 30.138 | 30.142 | 30.146 | 30.150 | 30. 153 |
| 766 | 30.157 | 30.16I | 30.165 | 30.169 | 30.173 | 30.177 | 30.181 | 30.185 | 30.189 | 30. 193 |
| 767 | 30.197 | 30.201 | 30.205 | 30.209 | 30.213 | 30.216 | 30.220 | 30.224 | 30.228 | 30.232 |
| 768 | 30.236 | 30.240 | 30.244 | 30.248 | 30.252 | 30.256 | 30.260 | 30.264 | 30.268 | 30.272 |
| 769 | 30.276 | 30.279 | 30.283 | 30.287 | 30.29 I | 30.295 | 30.299 | 30.303 | 30.307 | 30.31 I |
| 770 | 30.315 | 30.319 | 30.323 | 30.327 | 30.33 I | 30.335 | 30.339 | 30.342 | 30.346 | 30.350 |
| 771 | 30.354 | 30.358 | 30.362 | 30.366 | 30.370 | 30.374 | 30.378 | 30.382 | 30.386 | 30.390 |
| 772 | 30.394 | 30.398 | 30.402 | 30.405 | 30.409 | 30.413 | 30.417 | 30.42 I | 30.425 | 30.429 |
| 773 | 30.433 | 30.437 | 30.44 I | 30.445 | 30.449 | 30.453 | 30.457 | 30.46I | 30.465 | 30.468 |
| 774 | 30.472 | 30.476 | 30.480 | 30.484 | 30.488 | 30.492 | 30.496 | 30.500 | 30.504 | 30.508 |
| 775 | 30.512 | 30.516 | 30.520 | 30.524 | 30.528 | 30.53 I | 30.535 | 30.539 | 30.543 | 30.547 |
| 776 | 30.551 | 30.555 | 30.559 | 30.563 | 30.567 | 30.57 I | 30.575 | 30.579 | 30.583 | 30.587 |
| 777 | 30.590 | 30.594 | 30.598 | 30.602 | 30.606 | 30.610 | 30.614 | 30.618 | 30.622 | 30.626 |
| 778 | 30.630 | 30.634 | 30.638 | 30.642 | 30.646 | 30.650 | 30.653 | 30.657 | 30.66 I | 30.665 |
| 779 | 30.669 | 30.673 | 30.677 | 30.68I | 30.685 | 30.689 | 30.693 | 30.697 | 30.701 | 30.705 |
| 780 | 30.709 | 30.713 | 30.716 | 30.720 | 30.724 | 30.728 | 30.732 | 30.736 | 30.740 | 30.744 |
| 781 | 30.748 | 30.752 | 30.756 | 30.760 | 30.764 | 30.768 | 30.772 | 30.776 | 30.779 | 30.783 |
| 782 | 30.787 | 30.791 | 30.795 | 30.799 | 30.803 | 30.807 | 30.8II | 30.815 | 30.819 | 30.823 |
| 783 | 30.827 | 30.831 | 30.835 | 30.839 | 30.842 | 30.846 | 30.850 | 30.854 | 30.858 | 30.862 |
| 784 | 30.866 | 30.870 | 30.874 | 30.878 | 30.882 | 30.886 | 30.890 | 30.894 | 30.898 | 30.902 |
| 735 | 30.905 | 30.909 | 30.913 | 30.917 | 30.92 I | 30.925 | 30.929 | 30.933 | 30.937 | 30.941 |
| 786 | 30.945 | 30.949 | 30.953 | 30.957 | 30.96 I | 30.965 | 30.968 | 30.972 | 30.976 | 30.980 |
| 787 | 30.984 | 30.988 | 30.992 | 30.996 | 31.000 | 31.004 | 31.008 | 3 I .012 | 31.016 | 31.020 |
| 788 | 31.024 | 31.027 | 31.031 | 31.035 | 31.039 | 31.043 | 31.047 | 31.05I | 3 I .055 | 31.059 |
| 789 | 31.063 | 31.067 | 31.071 | 31.075 | 31.079 | 31.083 | 31.087 | 31.090 | 31.094 | 31.098 |
| 790 | 31.102 | 3 I .106 | 31.110 | 31.II4 | 31.118 | 31.122 | 31.126 | 31.130 | 31.134 | 31.138 |
| 791 | 31.142 | 31.146 | 31.150 | 31.153 | 31.157 | 31.16I | 31.165 | 3 I .169 | 31.173 | 31.177 |
| 792 | 3 I .181 | 3 I .185 | 31.189 | 31. 193 | 31.197 | 31.201 | 31.205 | 3 I .209 | 31.213 | 31.216 |
| 793 | 31.220 | 31.224 | 31.228 | 31.232 | 31.236 | 31.240 | 31.244 | 3 I .248 | 31.252 | 31.256 |
| 794 | 31.260 | 31.264 | 31.268 | 31.272 | 31.276 | 31.279 | 31.283 | 31.287 | 31.29I | 31.295 |
| 795 | 31.299 | 31.303 | 31.307 | 3I.3II | 3 I .315 | 31.319 | 31.323 | 31.327 | 31.331 | 31.335 |
| 796 | 3 I .339 | 31.342 | 31.346 | 31.350 | 3 I .354 | 31.358 | 31.362 | 31.366 | 3 r .370 | 31.374 |
| 797 | 3 I .378 | 3 I .382 | 31. 386 | 3 I .390 | 3 T .394 | 31.398 | 31.402 | 31.405 | 31.409 | 3 I .413 |
| 798 | 31.417 | 3 I .42 I | 3 I .425 | 31.429 | 31.433 | 31.437 | 31.44I | 31.445 | 31.449 | 31.453 |
| 799 | 3 I .457 | 31.46 I | 31.465 | 31.468 | 31.472 | 31.476 | 31.480 | 31.484 | 31.488 | 31.492 |
| 800 | 3 I .496 | 31.500 | 31.504 | 31.508 | 31.512 | 31.516 | 31.520 | 3 I .524 | 31.527 | 3 I .53 I |

MILLIMETRES INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch .

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 800 | 31.496 | 31.500 | 31.504 | 31.508 | 31.512 | 3 I .516 | 31.520 | 31.524 | 31.527 | 31.53I |
| 8 O | 3 I .535 | 31.539 | 31.543 | 31.547 | 3 I .55 I | 3 I .555 | 31.559 | 31.563 | 31.567 | 31.571 |
| 802 | 31.575 | 31.579 | 31.583 | 31.587 | 31.590 | 31.594 | 31.598 | 31.602 | 31.606 | 31.610 |
| 803 | 31.614 | 31.618 | 31.622 | 31.626 | 31.630 | 31.634 | 31.638 | 31.642 | 31.646 | 31.650 |
| 804 | 31.653 | 31.657 | 3 I .66 I | 31.665 | 31.669 | 31.673 | 31.677 | 3 I .68 I | 3 r .685 | 3 I .689 |
| 805 | 31.693 | 31.697 | 31.701 | 31.705 | 31.709 | 31.713 | 31.716 | 31.720 | 31.724 | 3 T .728 |
| 806 | 31.732 | 31.736 | 3 I .740 | 3 I .744 | 31.748 | 31.752 | 31.756 | 31.760 | 3 r .764 | 31.768 |
| 807 | 31.772 | 31.776 | 31.779 | 31.783 | 31.787 | 3 I .791 | 31.795 | 31.799 | 31.803 | 31.807 |
| 808 | 3 I .81 I | 3 I .815 | 31.819 | 31.823 | 31.827 | 31.83 I | 31.835 | 31.839 | 31.842 | 31.846 |
| 809 | 31.850 | 31.854 | 3 I .853 | 31.862 | 31.866 | 31.870 | 31.874 | 31.878 | 3 I .882 | 31.886 |
| 810 | 31.890 | 31.894 | 31.898 | 31.902 | 31.905 | 31.909 | 31.913 | 31.917 | 31.92I | 31.925 |
| 8 II | 31.929 | 31.933 | 31.937 | 31.941 | 31.945 | 3 I .949 | 31.953 | 31.957 | 31.961 | 31.965 |
| 812 | 31.968 | 31.972 | 31.976 | 31.930 | 31.984 | 31.988 | 31.992 | 31.996 | 32.000 | 32.004 |
| 8 I 3 | 32.008 | 32.012 | 32.016 | 32.020 | 32.024 | 32.027 | 32.031 | 32.035 | 32.039 | 32.043 |
| 814 | 32.047 | 32.05 I | 32.055 | 32.059 | 32.063 | 32.067 | 32.071 | 32.075 | 32.079 | 32.083 |
| 815 | 32.087 | 32.090 | 32.094 | 32.098 | 32.102 | 32.106 | 32.110 | 32.114 | 32.118 | 32.122 |
| 816 | 32.126 | 32.130 | 32. I34 | 32.138 | 32.142 | 32.146 | 32.150 | 32.153 | 32.157 | 32.16 I |
| 817 | 32.165 | 32.169 | 32. 173 | 32.177 | 32.181 | 32.185 | 32.189 | 32.193 | 32.197 | 32.201 |
| 8 I 8 | 32.205 | 32.209 | 32.213 | 32.216 | 32.220 | 32.224 | 32.228 | 32.232 | 32.236 | 32.240 |
| 819 | 32.244 | 32.248 | 32.252 | 32.256 | 32.260 | 32.264 | 32.268 | 32.272 | 32.276 | 32.279 |
| 820 | 32.283 | 32.287 | 32.291 | 32.295 | 32.299 | 32.303 | 32.307 | 32.3 II | 32.315 | 32.319 |
| 821 | 32.323 | 32.327 | 32.33 I | 32.335 | 32.339 | 32.342 | 32.346 | 32.350 | 32.354 | 32.358 |
| 822 | 32.362 | 32.366 | 32.370 | 32.374 | 32.373 | 32.382 | 32.386 | 32.390 | 32.394 | 32.398 |
| 823 | 32.402 | 32.405 | 32.409 | 32.413 | 32.417 | 32.42 I | 32.425 | 32.429 | 32.433 | 32.437 |
| 824 | 32.44 I | 32.445 | 32.449 | . 32.453 | 32.457 | 32.46 I | 32.465 | 32.468 | 32.472 | 32.476 |
| 825 | 32.48 o | 32.484 | 32.488 | 32.492 | 32.496 | 32.500 | 32.504 | 32.508 | 32.512 | 32.516 |
| 826 | 32.520 | 32.524 | 32.527 | 32.53 I | 32.535 | 32.539 | 32.543 | 32.547 | 32.551 | 32.555 |
| 827 | 32.559 | 32.563 | 32.567 | 32.571 | 32.575 | 32.579 | 32.583 | 32.587 | 32.590 | 32.594 |
| 828 | 32.598 | 32.602 | 32.606 | 32.610 | 32.614 | 32.618 | 32.622 | 32.626 | 32.630 | 32.634 |
| 829 | 32.638 | 32.642 | 32.646 | 32.650 | 32.653 | 32.657 | 32.661 | 32.665 | 32.669 | 32.673 |
| 830 | 32.677 | 32.68I | 32.685 | 32.689 | 32.693 | 32.697 | 32.701 | 32.705 | 32.709 | 32.713 |
| 831 | 32.716 | 32.720 | 32.724 | 32.72 S | 32.732 | 32.736 | 32.740 | 32.744 | 32.748 | 32.752 |
| 832 | 32.756 | 32.760 | 32.764 | 32.768 | 32.772 | 32.776 | 32.779 | 32.783 | 32.787 | 32.791 |
| 833 | 32.795 | 32.799 | 32.803 | 32.807 | 32.81 I | 32.815 | 32.819 | 32.823 | 32.827 | 32.831 |
| 834 | 32.835 | 32.839 | 32.842 | 32.846 | 32.850 | 32.854 | 32.858 | 32.862 | 32.866 | 32.870 |
| 835 | 32.874 | 32.878 | 32.882 | 32.886 | 32.890 | 32.894 | 32.898 | 32.902 | 32.905 | 32.909 |
| 836 | 32.913 | 32.917 | 32.92 I | 32.925 | 32.929 | 32.933 | 32.937 | 32.941 | 32.945 | 32.949 |
| 837 | 32.953 | 32.957 | 32.96 I | 32.965 | 32.968 | 32.972 | 32.976 | 32.980 | 32.984 | 32.988 |
| 838 | 32.992 | 32.996 | 33.000 | 33.004 | 33.008 | 33.012 | 33.016 | 33.020 | 33.024 | 33.027 |
| 839 | 33.03 I | 33.035 | 33.039 | 33.043 | 33.047 | 33.051 | 33.055 | 33.059 | 33.063 | 33.067 |
| 840 | 33.071 | 33.075 | 33.079 | 33.083 | 33.087 | 33.090 | 33.094 | 33.098 | 33.102 | 33.106 |
| 841 | 33.110 | 33.114 | 33.118 | 33.122 | 33.126 | 33.130 | 33.134 | 33.138 | 33.142 | 33.146 |
| 842 | 33.150 | 33.153 | 33.157 | 33.16 I | 33.165 | 33.169 | 33.173 | 33.177 | 33.181 | 33.185 |
| 843 | 33.189 | 33.193 | 33.197 | 33.201 | 33.205 | 33.209 | 33.213 | 33.216 | 33.220 | 33.224 |
| 844 | 33.228 | 33.232 | 33.236 | 33.240 | 33.244 | 33.248 | 33.252 | 33.256 | 33.260 | 33.264 |
| 845 | 33.268 | 33.272 | 33.276 | 33.279 | 33.283 | 33.287 | 33.291 | 33.295 | 33.299 | 33.303 |
| 846 | 33.307 | 33.311 | 33.315 | 33.319 | 33.323 | 33.327 | 33.331 | 33.335 | 33.339 | 33.342 |
| 847 | 33.346 | 33.350 | 33.354 | 33.358 | 33.362 | 33.366 | 33.370 | 33.374 | 33.378 | 33.382 |
| 848 | 33.386 | 33.390 | 33.394 | 33.398 | 33.402 | 33.405 | 33.409 | 33.413 | 33.417 | 33.42 I |
| 849 | 33.425 | 33.429 | 33.433 | 33.437 | 33.44I | 33.445 | 33.449 | 33.453 | 33.457 | 33.461 |
| 850 | 33.464 | 33.468 | 33.472 | 33.476 | 33.480 | 33.484 | 33.488 | 33.492 | 33.496 | 33.500 |

MILLIMETRES INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch .

| Milli- metres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 850 | 33.464 | 33.468 | 33.472 | 33.476 | 33.480 | 33.484 | 33.488 | 33.492 | 33.496 | 33.500 |
| 851 | 33.504 | 33.508 | 33.512 | 33.516 | 33.520 | 33.524 | 33.527 | 33.531 | 33.535 | 33.539 |
| 852 | 33.543 | 33.547 | 33.55I | 33.555 | 33.559 | 33.563 | 33.567 | 33.571 | 33.575 | 33.579 |
| 853 | 33.583 | 33.587 | 33.590 | 33.594 | 33.598 | 33.602 | 33.606 | 33.610 | 33.614 | 33.618 |
| 854 | 33.622 | 33.626 | 33.630 | 33.634 | 33.638 | 33.642 | 33.646 | 33.650 | 33.653 | 33.657 |
| 855 | 33.66I | 33.665 | 33.669 | 33.673 | 33.677 | 33.681 | 33.685 | 33.689 | 33.693 | 33.697 |
| 856 | 33.701 | 33.705 | 33.709 | 33.713 | 33.716 | 33.720 | 33.724 | 33.728 | 33.732 | 33.736 |
| 857 | 33.740 | 33.744 | 33.748 | 33.752 | 33.756 | 33.760 | 33.764 | 33.768 | 33.772 | 33.776 |
| 858 | 33.779 | 33.783 | 33.787 | 33.791 | 33.795 | 33.799 | 33.803 | 33.807 | 33.8II | 33.8I5 |
| 859 | 33.819 | 33.823 | 33.827 | 33.831 | 33.835 | 33.839 | 33.842 | 33.846 | 33.850 | 33.854 |
| 860 | 33.858 | 33.862 | 33.866 | 33.870 | 33.874 | 33.878 | 33.882 | 33.886 | 33.890 | 33.894 |
| 861 | 33.898 | 33.902 | 33.905 | 33.909 | 33.913 | 33.917 | 33.921 | 33.925 | 33.929 | 33.933 |
| 862 | 33.937 | 33.94 I | 33.945 | 33.949 | 33.953 | 33.957 | 33.96I | 33.964 | 33.968 | 33.972 |
| 863 | 33.976 | 33.980 | 33.984 | 33.988 | 33.992 | 33.996 | 34.000 | 34.004 | 34.008 | 34.012 |
| S64 | 34.016 | 34.020 | 34.024 | 34.027 | 34.03 I | 34.035 | 34.039 | 34.043 | 34.047 | 34.051 |
| 865 | 34.055 | 34.059 | 34.063 | 34.067 | 34.07 I | 34.075 | 34.079 | 34.083 | 34.087 | 34.090 |
| 856 | $34 . \mathrm{c94}$ | 34.098 | 34. 102 | 34. 106 | 34.1 10 | 34. I 14 | 34.118 | 34. 122 | 34.126 | 34.130 |
| 867 | 34. 134 | 34.138 | 34.142 | 34.146 | 34.150 | 34. 153 | 34. 157 | 34.16I | 34.165 | 34.169 |
| 853 | 34. 173 | 34.177 | 34.181 | 34.185 | 34.189 | 34. 193 | 34.197 | 34.201 | 34.205 | 34.209 |
| 869 | 34.213 | 34.216 | 34.220 | 34.224 | 34.228 | 34.232 | 34.236 | 34.240 | 34.244 | 34.248 |
| 870 | 34.252 | 34.256 | 34.260 | 34.264 | 34.268 | 34.272 | 34.276 | 34.279 | 34.283 | 34.287 |
| 871 | 34.291 | 34.295 | 34.299 | 34.303 | 34.307 | 34.31 I | 34.315 | 34.319 | 34.323 | 34.327 |
| 872 | 34.331 | 34.335 | 34.339 | 34.342 | 34.346 | 34.350 | 34.354 | 34.358 | 34.362 | 34.366 |
| 873 | 34.370 | 34.374 | 34.378 | 34.382 | 34.386 | 34.390 | 34.394 | 34.398 | 34.402 | 34.405 |
| 874 | 34.409 | 34.413 | 34.417 | 34.42 I | 34.425 | 34.429 | 34.433 | 34.437 | 34.44I | 34.445 |
| 875 | 34.449 | 34.453 | 34.457 | 34.46I | 34.464 | 24.468 | 34.472 | 34.476 | 34.480 | 34.484 |
| 876 | 34.488 | 34.492 | 34.496 | 34.500 | 34.504 | 34.508 | 34.512 | 34.516 | 34.520 | 34.524 |
| 877 | 34.527 | 34.53 I | 34.535 | 34.539 | 34.543 | 34.547 | 34.55I | 34.555 | 34.559 | 34.563 |
| 878 | 34.567 | 34.57 I | 34.575 | 34.579 | 34.583 | 34.587 | 34.590 | 34.594 | 34.598 | 34.602 |
| 879 | 34.606 | 34.610 | 34.6I4 | 34.618 | 34.622 | 34.626 | 34.630 | 34.634 | 34.638 | 34.642 |
| 880 | 34.646 | 34.650 | 34.653 | 34.657 | 34.66I | 34.665 | 34.669 | 34.673 | 34.677 | 34.68I |
| 88 I | 34.685 | 34.689 | 34.693 | 34.697 | 34.7 OI | 34.705 | 34.709 | 34.713 | 34.716 | 34.720 |
| 882 | 34.724 | 34.728 | 34.732 | 34.736 | . 34.740 | 34.744 | 34.748 | 34.752 | 34.756 | 34.760 |
| 883 | 34.764 | 34.768 | 34.772 | 34.776 | 34.779 | 34.783 | 34.787 | 34.791 | 34.795 | 34.799 |
| 884 | 34.803 | 34.807 | 34.81 I | 34.815 | 34.819 | 34.823 | 34.827 | 34.83 I | 34.835 | 34.839 |
| 885 | 34.842 | 34.846 | 34.850 | 34.854 | 34.858 | 34.862 | 34.866 | 34.870 | 34.874 | 34.878 |
| 886 | 34.882 | 34.886 | 34.890 | 34.894 | 34.898 | 34.902 | 34.905 | 34.909 | 34.913 | 34.917 |
| 887 | 34.921 | 34.925 | 34.929 | 34.933 | 34.937 | 34.941 | 34.945 | 34.949 | 34.953 | 34.957 |
| 888 | 34.96 I | 34.964 | 34.968 | 34.972 | 34.976 | 34.980 | 34.984 | 34.988 | 34.992 | 34.996 |
| 889 | 35.000 | 35.004 | 35.008 | 35.012 | 35.016 | 35.020 | 35.024 | 35.027 | 35.03 I | 35.035 |
| 890 | 35.039 | 35.043 | 35.047 | 35.05I | 35.055 | 35.059 | 35.063 | 35.067 | 35.071 | 35.075 |
| 891 | 35.079 | 35.083 | 35.087 | 35.090 | 35.094 | 35.098 | 35.102 | 35.106 | 35.110 | 35. I 14 |
| 892 | 35.118 | 35.122 | 35.126 | 35.130 | 35. 134 | 35.138 | 35.142 | 35.146 | 35.150 | 35. I 53 |
| 893 | 35.157 | 35.16I | 35.165 | 35.169 | 35.173 | 35.177 | 35.181 | 35.185 | 35.189 | 35.193 |
| 894 | 35.197 | 35.201 | 35.205 | 35.209 | 35.213 | 35.216 | 35.220 | 35.224 | 35.228 | 35.232 |
| 895 | 35.236 | 35.240 | 35.244 | 35.248 | 35.252 | 35.256 | 35.260 | 35.264 | 35.268 | 35.272 |
| 896 | 35.276 | 35.279 | 35.283 | 35.287 | 35.291 | 35.295 | 35.299 | 35.303 | 35.307 | 35.3 II |
| 897 | 35.315 | 35.319 | 35.323 | 35.327 | 35.33 I | 35.335 | 35.339 | 35.342 | 35.346 | 35.350 |
| 898 | 35.354 | 35.358 | 35.362 | 35.366 | 35.37 O | 35.374 | 35.378 | 35.382 | 35.386 | 35.390 |
| S99 | 35.394 | 35.398 | 35.402 | 35.405 | 35.409 | 35.413 | 35.417 | 35.42 I | 35.425 | 35.429 |
| 900 | 35.433 | 35.437 | 35.44 I | 35.445 | 35.449 | 35.453 | 35.457 | 35.46I | 35.464 | 35.468 |

Smithsonian Tables.

TABLE 65.

## MILLIMETRES INTO INCHES.

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimetres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 900 | 35.433 | 35.437 | 35.44I | 35.445 | 35.449 | 35.453 | 35.457 | 35.46I | 35.464 | 35.468 |
| 901 | 35.472 | 35.476 | 35.480 | 35.484 | 35.488 | 35.492 | 35.496 | 35.500 | 35.504 | 35.508 |
| 902 | 35.512 | 35.516 | 35.520 | 35.524 | 35.527 | 35.53 I | 35.535 | 35.539 | 35.543 | 35.547 |
| 903 | 35.55 I | 35.555 | 35.559 | 35.563 | 35.567 | 35.57 I | 35.575 | 35.579 | 35.583 | 35.587 |
| 904 | 35.590 | 35.594 | 35.598 | 35.602 | 35.606 | 35.610 | 35.614 | 35.618 | 35.622 | 35.626 |
| 905 | 35.630 | 35.634 | 35.638 | 35.642 | 35.646 | 35.650 | 35.653 | 35.657 | 35.66I | 35.665 |
| 906 | 35.669 | 35.673 | 35.677 | 35.68I | 35.685 | 35.689 | 35.693 | 35.697 | 35.701 | 35.705 |
| 907 | 35.709 | 35.713 | 35.716 | 35.720 | 35.724 | 35.728 | 35.732 | 35.736 | 35.740 | 35.744 |
| 908 | 35.748 | 35.752 | 35.756 | 35.760 | 35.764 | 35.768 | 35.772 | 35.776 | 35.779 | 35.783 |
| 909 | 35.787 | 35.79 I | 35.795 | 35.799 | 35.803 | 35.807 | 35.81 I | 35.815 | 35.819 | 35.823 |
| 910 | 35.827 | 35.83 I | 35.835 | 35.839 | 35.842 | 35.846 | 35.850 | 35.854 | 35.858 | 35.862 |
| 911 | 35.866 | 35.870 | 35.874 | 35.878 | 35.882 | 35.886 | 35.890 | 35.894 | 35.898 | 35.902 |
| 912 | 35.905 | 35.909 | 35.913 | 35.917 | 35.92 I | 35.925 | 35.929 | 35.933 | 35.937 | 35.941 |
| 913 | 35.945 | 35.949 | 35.953 | 35.957 | 35.96I | 35.964 | 35.968 | 35.972 | 35.976 | 35.980 |
| 914 | 35.984 | 35.988 | 35.992 | 35.996 | 36.000 | 36.004 | 36.008 | 36.012 | 36.016 | 36.020 |
| 915 | 36.024 | 36.027 | 36.03I | 36.035 | 36.039 | 36.043 | 36.047 | 36.051 | 36.055 | 36.059 |
| 916 | 36.063 | 36.067 | 36.071 | 36.075 | 36.079 | 36.083 | 36.087 | 36.090 | 36.094 | 36.098 |
| 917 | 36. 102 | 36. 106 | 36.110 | 36.114 | 36.118 | 36.122 | 36.126 | 36.130 | 36.134 | 36.138 |
| 918 | 36.142 | 36.146 | 36.150 | 36.153 | 36.157 | 36.16I | 36.165 | 36.169 | 36.173 | 36.177 |
| 919 | 36.181 | 36.185 | 36.189 | 36.193 | 36.197 | 36.201 | 36.205 | 36.209 | 36.213 | 36.216 |
| 920 | 36.220 | 36.224 | 36.228 | 36.232 | 36.236 | 36.240 | 36.244 | 36.248 | 36.252 | 36.256 |
| 921 | 36.260 | 36.264 | 36.268 | 36.272 | 36.276 | 36.279 | 36.283 | 36.287 | 36.291 | 36.295 |
| 922 | 36.299 | 36.303 | 36.307 | 36.31 I | 36.315 | 36.319 | 36.323 | 36.327 | 36.33 I | 36.335 |
| 923 | 36.339 | 36.342 | 36.346 | 36.350 | 36.354 | 36.358 | 36.362 | 36.366 | 36.370 | 36.374 |
| 924 | 36.378 | 36.382 | 36.386 | 36.390 | 36.394 | 36.398 | 36.402 | 36.405 | 36.409 | 36.413 |
| 925 | 36.417 | 36.42 I | 36.425 | 36.429 | 36.433 | 36.437 | 36.44 I | 36.445 | 36.449 | 36.453 |
| 926 | 36.457 | 36.46 I | 36.464 | 36.468 | 36.472 | 36.476 | 36.48 o | 36.484 | 36.488 | 36.492 |
| 927 | 36.496 | 36.500 | 36.504 | 36.508 | 36.512 | 36.516 | 36.520 | 36.524 | 36.527 | 36.53 I |
| 928 | 36.535 | 36.539 | 36.543 | 36.547 | 36.55 I | 36.555 | 36.559 | 36.563 | 36.567 | 36.57 I |
| 929 | 36.575 | 36.579 | 36.583 | 36.587 | 36.590 | 36.594 | 36.598 | 36.602 | 36.606 | 36.610 |
| 930 | 36.614 | 36.618 | 36.622 | 36.626 | 36.630 | 36.634 | 36.638 | 36.642 | 36.646 | 36.650 |
| 931 | 36.653 | 36.657 | 36.66 I | 36.665 | 36.669 | 36.673 | 36.677 | 36.681 | 36.685 | 36.639 |
| 932 | 36.693 | 36.697 | 36.701 | 36.705 | 36.709 | 36.713 | 36.716 | 36.720 | 36.724 | 36.728 |
| 933 | 36.732 | 36.736 | 36.740 | 36.744 | 36.748 | 36.752 | 36.756 | 36.760 | 36.764 | 36.768 |
| 934 | 36.772 | 36.776 | 36.779 | 36.783 | 36.787 | 36.791 | 36.795 | 36.799 | 36.803 | 36.807 |
| 935 | 36.8 II | 36.815 | 36.819 | 36.823 | 36.827 | 36.83 I | 36.835 | 36.839 | 36.842 | 36.846 |
| 936 | 36.850 | 36.854 | 36.858 | 36.862 | 36.866 | 36.870 | 36.874 | 36.878 | 36.882 | 36.886 |
| 937 | 36.890 | 36.894 | 36.898 | 36.902 | 36.905 | 36.909 | 36.913 | 36.917 | 36.921 | 36.925 |
| 938 | 36.929 | 36.933 | 36.937 | 36.94 I | 36.945 | 36.949 | 36.953 | 36.957 | 36.961 | 36.964 |
| 939 | 36.968 | 36.972 | 36.976 | 36.980 | 36.984 | 36.988 | 36.992 | 36.996 | 37.000 | 37.004 |
| 940 | 37.008 | 37.012 | 37.016 | 37.020 | 37.024 | 37.027 | 37.03I | 37.035 | 37.039 | 37.043 |
| 941 | 37.047 | 37.05I | 37.055 | 37.059 | 37.063 | 37.067 | 37.07 I | 37.075 | 37.079 | 37.083 |
| 942 | 37.087 | 37.090 | 37.094 | 37.098 | 37.102 | 37.106 | 37.110 | 37.114 | 37.118 | 37. 122 |
| 943 | 37.126 | 37.130 | 37.134 | 37.138 | 37.142 | 37.146 | 37.150 | 37.153 | 37.157 | 37.16I |
| 944 | 37.165 | 37.169 | 37.173 | 37.177 | 37.181 | 37.185 | 37.189 | 37.193 | 37.197 | 37.201 |
| 945 | 37.204 | 37.208 | 37.212 | 37.216 | 37.220 | 37.224 | 37.228 | 37.232 | 37.236 | 37.240 |
| 946 | 37.244 | 37.248 | 37.252 | 37.256 | 37.260 | 37.264 | 37.268 | 37.272 | 37.276 | 37.279 |
| 947 | 37.283 | 37.287 | 37.291 | 37.295 | 37.299 | 37.303 | 37.307 | 37.311 | 37.315 | 37.319 |
| 948 | 37.323 | 37.327 | 37.33 I | 37.335 | 37.339 | 37.342 | 37.346 | 37.350 | 37.354 | 37.358 |
| 949 | 37.362 | 37.366 | 37.370 | 37.374 | 37.378 | $37 \cdot 382$ | 37.386 | 37.390 | 37.394 | 37.398 |
| 950 | 37.402 | 37.405 | 37.409 | 37.413 | 37.417 | 37.42 I | 37.425 | 37.429 | 37.433 | 37.437 |

MILLIMETRES INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch.

| Milli- metres. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inche | Inches. | Inches. | Inch | Inch | Inches. | Inches. | Inches. |
| 950 | 37.402 | 37.405 | 37.409 | 37.413 | 37.417 | 37.421 | 37.425 | 37.429 | 37.433 | 37.437 |
| 951 | 37.44 I | 37.445 | 37.449 | 37.453 | 37.457 | 37.461 | 37.464 | 37.468 | 37.472 | 37.476 |
| 952 | 37.480 | 37.484 | 37.488 | 37.492 | 37.496 | 37.500 | 37.504 | 37.508 | 37.512 | 37.516 |
| 953 | 37.520 | 37.524 | 37.527 | 37.531 | 37.535 | 37.539 | 37.543 | 37.547 | 37.551 | 37.555 |
| 954 | 37.559 | 37.563 | 37.567 | 37.57 | 37.575 | 37.579 | 37.583 | 37.587 | 37.590 | 37.594 |
| 955 | 37.598 | 37.602 | 37.606 | 37.610 | 37.614 | 37.618 | 37.622 | 37.626 | 37.630 | 37.634 |
| 956 | 37.638 | 37.642 | 37.646 | 37.650 | 37.653 | 37.657 | 37.661 | 37.665 | 37.669 | 37.673 |
| 957 | 37.677 | 37.681 | 37.685 | 37.689 | 37.693 | 37.697 | 37.701 | 37.705 | 37.709 | 37.713 |
| 958 | 37.716 37.756 | 37.720 | 37.724 | 37.728 | 37.732 | 37.736 | 37.740 | 37.744 | 37.748 | 37.752 |
| 959 | 37.756 | 37.760 | 37.764 | 37.768 | 37.772 | 37.776 | 37.779 | 37.783 | 37.787 | 37.791 |
| 960 | 37.795 | 37.799 | 37.803 | 37.807 | 37.811 | 37.815 | 37.819 | 37.823 | 37.827 | 37.831 |
| 961 | 37.835 | 37.839 | 37.842 | 37.846 | 37.850 | 37.854 | 37.858 | 37.862 | 37.866 | 37.870 |
| 962 | 37.874 | 37.878 | 37.882 | 37.886 | 37.890 | 37.894 | 37.898 | 37.901 | 37.905 | 37.909 |
| 963 | 37.913 | 37.917 | 37.921 | 37.925 | 37.929 | 37.933 | 37.937 | 37.94 I | 37.945 | 37.949 |
| 964 | 37.953 | 37.957 | 37.961 | 37.964 | 37.968 | 37.972 | 37.976 | 37.980 | 37.984 | 37.988 |
| 965 | 37.992 | 37.996 | 38.000 | 38.004 | 38.008 | 38.012 | 38.016 | 38.020 | 38.024 | 38.027 |
| 966 | 38.031 | 38.035 | 38.039 | 38.043 | 38.047 | 38.05 I | 38.055 | 38.059 | 38.063 | 38.067 |
| 967 | 38.071 | 38.075 | 38.079 | 38.083 | 38.087 | 38.090 | 38.094 | 38.098 | 38.102 | 38. 106 |
| 968 | 38.110 | 38.114 | 38.118 | 38. 122 | 38.126 | 38.130 | 38.134 | 38.138 | 38.142 | 38.146 |
| 969 | 38.150 | 38.153 | 38.157 | 38.161 | 38.165 | 38.169 | 38.173 | 38.177 | 38.181 | 38.185 |
| 970 | 38.189 | 38.193 | 38.197 | 38.201 | 38.205 | 38.209 | 38.213 | 38.216 | 38.220 | 38.224 |
| 971 | 38.228 | 38.232 | 38.236 | 38.240 | 38.244 | 38.248 | 38.252 | 38.256 | 38.260 | 38.264 |
| 972 | 38.268 | 38.272 | 38.276 | 38.279 | 38.283 | 38.287 | 38.291 | 38.295 | 38.299 | 38.303 |
| 973 | 38.307 | 38.311 | 38.315 | 38.319 | 38.323 | 38.327 | 38.331 | 38.335 | 38.339 | 38.342 |
| 974 | 38.346 | 38.350 | 38.354 | 38.358 | 38.362 | 38.366 | 38.370 | 38.374 | 38.378 | 38.382 |
| 975 | 38.386 | 38.390 | 38.394 | 38.398 | 38.401 | 38.405 | 38.409 | 38.413 | 38.417 | 38.421 |
| 976 | 38.425 | 38.429 | 38.433 | 38.437 | 38.44 I | 38.445 | 38.449 | 38.453 | 38.457 | 38.46 I |
| 977 | 38.464 | 38.468 | 38.472 | 38.476 | 38.480 | 38.484 | 38.488 | 38.492 | 38.496 | 38.500 |
| 978 | 38.504 | 38.508 | 38.512 | 38.516 | 38.520 | 38.524 | 38.527 | 38.53 I | 38.535 | 38.539 |
| 979 | 38.543 | 38.547 | 38.55I | 38.555 | 38.559 | 38.563 | 38.567 | 38.57 I | 38.575 | 38.579 |
| 980 | 38.583 | 38.587 | 38.590 | 38.594 | 38.598 | 38.602 | 38.606 | 38.610 | 38.614 | 38.618 |
| 981 982 | 38.622 38.66 I | 38.626 38.665 38.7 | 38.630 38.669 | 38.634 38.673 | 38.639 38.677 3 | 38.642 | 38.646 <br> 38.685 <br> 8. | 38.650 | 38.653 | 38.657 |
| 982 | 38.66 I 38.70 I | 38.665 38.705 | 38.669 38.709 | 38.673 38.713 | 38.677 38.716 | 38.68I | 38.685 38.724 | 38.689 38.728 | 38.693 | 38.697 |
| 984 | 38.701 38.740 | 38.705 38.744 | 38.709 38.748 | 38.713 38.752 | 38.716 38.756 | 38.720 38.760 | 38.724 38.764 | 38.728 38.768 | 38.732 38.772 | 38.736 38.776 |
| 985 | 38.780 | 38.783 | 38.787 | 38.791 | 38.795 | 38.799 | 38.803 | 38.807 | 38.811 | 38.815 |
| 986 | 38.819 | 38.823 | 38.827 | 38.831 | 38.835 | 38.839 | 38.842 | 38.846 | 38.850 | 38.854 |
| 987 | 38.858 | 38.862 | 38.866 | 38.870 | 38.874 | 38.878 | 38.882 | 38.886 | 38.890 | 38.894 |
| 988 | 38.898 | 38.901 | 38.905 | 38.909 | 38.913 | 38.917 | 38.921 | 38.925 | 38.929 | 38.933 |
| 989 | 38.937 | 38.941 | 38.945 | 38.949 | 38.953 | 38.957 | 38.96I | 38.964 | 38.968 | 38.972 |
| 990 | 38.976 | 38.980 | 38.984 | 38.988 | 38.992 | 38.996 | 39.000 | 39.004 | 39.008 | 39.012 |
| 991 | 39.016 | 39.020 | 39.024 | 39.027 | 39.031 | 39.035 | 39.039 | 39.043 | 39.047 | 39.05I |
| 992 | 39.055 | 39.059 | 39.063 | 39.067 | 39.071 | 39.075 | 39.079 | 39.083 | 39.087 | 39.090 |
| 993 | 39.094 | 39.098 | 39.102 | 39. 106 | 39.110 | 39.114 | 39.118 | 39.122 | 39.126 | 39.130 |
| 994 | 39.134 | 39.138 | 39.142 | 39.146 | 39.150 | 39.153 | 39.157 | 39.161 | 39.165 | 39.169 |
| 995 | 39.173 | 39.177 | 39.18I | 39.185 | 39.189 | 39.193 | 39.197 | 39.201 | 39.205 | 39.209 |
| 996 | 39.213 | 39.216 | 39.220 | 39.224 | 39.228 | 39.232 | 39.236 | 39.240 | 39.244 | 39.248 |
| 997 | 39.252 | 39.256 | 39.260 | 39.264 | 39.268 | 39.272 | 39.276 | 39.279 | 39.283 | 39.287 |
| 998 | 39.291 | 39.295 | 39.299 | 39.303 | 39.307 | 39.311 | 39.315 | 39.319 | 39.323 | 39.327 |
| 999 | 39.33I | 39.335 | 39.339 | 39.342 | 39.346 | 39.350 | 39.354 | 39.358 | 39.362 | 39.366 |
| 1000 | 39.370 | 39.374 | 39.378 | 39.382 | 39.386 | 39.390 | 39.394 | 39.398 | 39.401 | 39.405 |

Smithsonian Tableg.

I foot $=0.3048006$ metre.

| Feet. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $m$ | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 0 | 0.000 | 0.305 | 0.610 | 0.914 | 1. 219 | 1. 524 | 1.829 | 2. 134 | 2.438 | 2.743 |
| 10 | 3.048 | $3 \cdot 353$ | 3.658 | 3.962 | 4.267 | 4.572 | 4.877 | 5.182 | 5.486 | 5.791 |
| 20 | 6.096 | 6.401 | 6.706 | 7.010 | $7 \cdot 315$ | 7.620 | 7.925 | 8.230 | 8.534 | 8.839 |
| 30 | 9.144 | 9.449 | 9.754 | 10.058 | 10.363 | 10.668 | 10.973 | 11.278 | 11.582 | II. 887 |
| 40 | 12.192 | 12.497 | 12.802 | 13.106 | 13.411 | 13.716 | 14.021 | 14.326 | 14.630 | 14.935 |
| 50 | I5.240 | 15.545 | 15.850 | 16.154 | 16.459 | 16.764 | 17.069 | 17.374 | 17.678 | 17.983 |
| 60 | 18.288 | 18.593 | 18.898 | 19.202 | 19.507 | 19.812 | 20.117 | 20.422 | 20.726 | 21.031 |
| 70 | 21.336 | 21.64I | 21.946 | 22.250 | 22.555 | 22.860 | 23.165 | 23.470 | 23.774 | 24.079 |
| 80 | 24.384 | 24.689 | 24.994 | 25.298 | 25.603 | 25.908 | 26.213 | 26.518 | 26.822 | 27.127 |
| 90 | 27.432 | 27.737 | 28.042 | 28.346 | 28.651 | 28.956 | 29.26I | 29.566 | 29.870 | 30.175 |
|  | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| 100 | 30.48 | 33.53 | 36.58 | 39.62 | 42.67 | 45.72 | 48.77 | 51.82 | 54.86 | 57.91 |
| 200 | 60.96 | 64.01 | 67.06 | 70.10 | 73.15 | 76.20 | 79.25 | 82.30 | 85.34 | 88.39 |
| 300 | 91. 44 | 94.49 | 97.54 | 100.58 | 103.63 | 106.68 | 109.73 | II2.78 | 115.82 | 118.87 |
| 400 | 121.92 | 124.97 | 128.02 | I3I.06 | 134.11 | 137.16 | 140.21 | 143.26 | 146.30 | 149.35 |
| 500 | 152.40 | 155.45 | I58.50 | 16 I .54 | 164.59 | 167.64 | 170.69 | 173.74 | 176.78 | 179.83 |
| 600 | I 82.88 | 185.93 | 188.98 | 192.02 | 195.07 | 198.12 | 201.17 | 204.22 | 207.26 | 210.31 |
| 700 | 213.36 | 216.41 | 219.46 | 222.50 | 225.55 | 228.60 | 231.65 | 234.70 | 237.74 | 240.79 |
| 800 | 243.84 | 246.89 | 249.94 | 252.98 | 256.03 | 259.08 | 262.13 | 265.18 | 268.22 | 271.27 |
| 900 | 274.32 | 277.37 | 280.42 | 283.46 | 286.5I | 289.56 | 292.61 | 295.66 | 298.70 | 301.75 |
| 1000 | 304.80 | 307.85 | 310.90 | 313.94 | 316.99 | 320.04 | 323.09 | 326.14 | 329.18 | 332.23 |
| 1100 | 335.28 | 33 S. 33 | 341.38 | 344.42 | 347.47 | 350.52 | 353.57 | 356.62 | 359.67 | 362.71 |
| 1200 | 365.76 | 368.8 I | 371.86 | 374.90 | 377.95 | 38 I .00 | 384.05 | 387.10 | 390. 14 | 393.19 |
| 1300 | 396.24 | 399.29 | 402.34 | 405.38 | 408.43 | 4II. 48 | 414.53 | 4I7.58 | 420.62 | 423.67 |
| 1400 | 426.72 | 429.77 | 432.82 | 435.86 | 438.91 | 441.96 | 445.01 | 448.06 | 451.10 | 454. 5 |
| 1500 | 457.20 | 460.25 | 463.30 | 466.34 | 469.39 | 472.44 | 475.49 | 478.54 | 481.58 | 484.63 |
| 1600 | 487.68 | 490.73 | 493.78 | 496.82 | 499.87 | 502.92 | 505.97 | 509.02 | 512.07 | 515.11 |
| 1700 | 518.16 | 52 I .21 | 524.26 | 527.3 I | 530.35 | 533.40 | 536.45 | 539.50 | 542.55 | 545.59 |
| 1800 | 548.64 | 551.69 | 554.74 | 557.79 | 560.83 | 563.88 | 566.93 | 569.98 | 573.03 | 576.07 |
| 1900 | 579.12 | 582.17 | 585.22 | 588.27 | 591.3I | 594.36 | 597.41 | 600.46 | 603.5I | 606.55 |
| 2000 | 609.60 | 612.65 | 615.70 | 618.75 | 621.79 | 624.84 | 627.89 | 630.94 | 633.99 | 637.03 |
| 2100 | 640.08 | 643.13 | 646. 18 | 649.23 | 652.27 | 655.32 | 658.37 | 66 I .42 | 664.47 | 667.51 |
| 2200 | 670.56 | 673.61 | 676.66 | 679.7 I | 682.75 | 685.80 | 688.85 | 691.90 | 694.95 | 697.99 |
| 2300 | 701.04 | 704.09 | 707.14 | 710.19 | 713.23 | 716.28 | 719.33 | 722.38 | 725.43 | 728.47 |
| 2400 | 73 I .52 | 734.57 | 737.62 | 740.67 | 743.7 I | 746.76 | 749.81 | 752.86 | 755.91 | 758.95 |
| 2500 | 762.00 | 765.05 | 768.10 | 771.15 | 774.19 | 777.24 | 780.29 | 783.34 | 786.39 | 789.43 |
| 2600 | 792.48 | 795.53 | 798.58 | 801.63 | 804.67 | 807.72 | 810.77 | 813.82 | 816.87 | 819.91 |
| 2700 | 822.96 | 826.01 | 829.06 | 832.11 | 835.15 | 838.20 | 841.25 | 844.30 | 847.35 | 850.39 |
| 2800 | 853.44 | 856.49 | 859.54 | 862.59 | 865.63 | 868.68 | 871.73 | 874.78 | 877.83 | 88 c 87 |
| 2900 | 883.92 | 886.97 | 890.02 | 893.07 | 896.1 1 | 899.16 | 902.2 I | 905.26 | 908.3I | 911.35 |
| 3000 | 914.40 | 917.45 | 920.50 | 923.55 | 926.59 | 929.64 | 932.69 | 935.74 | 938.79 | 941.83 |
| 3100 | 944.88 | 947.93 | 950.98 | 954.03 | 957.07 | 960.12 | 963.17 | 966.22 | 969.27 | 972.31 |
| 3200 | 975.36 | 978.41 | 981.46 | 984.5 1 | 987.55 | 990.60 | 993.65 | 996.70 | 999.75 | 1002.79 |
| 3300 | roo5.84 | 1008.89 | IOII. 94 | 1014.99 | 1018.03 | 1021.08 | 1024.13 | 1027.18 | 1030.23 | 1033.27 |
| 3400 | 1036.32 | 1039.37 | 1042.42 | 1045.47 | 1048.5I | 1051.56 | 1054.61 | 1057.66 | 1060.71 | 1063.75 |
| 3500 | 1066.80 | 1069.85 | 1072.90 | 1075.95 | 1078.99 | Io82.04 | 1085.09 | Io88.14 | I091.19 | Iog4.23 |
| 3600 | I097.28 | 1100.33 | 1103.38 | I 106.43 | 1109.47 | II 12.52 | 1115.57 | I I I 8.62 | 1121.67 | 1124.71 |
| 3700 | II 27.76 | II30.8I | 1133.86 | I I 36.91 | I 139.95 | I 1443.00 | II 46.05 | I I 49.10 | 1152.15 | I 155.19 |
| 3800 | II58.24 | II61.29 | II 64.34 | I167.39 | 1170.43 | II73.48 | 1176.53 | II79.58 | 1182.63 | I185.67 |
| 3900 | 1 I 88.72 | I 191.77 | I 194.82 | 1197.87 | 1200.91 | 1203.96 | 1207.01 | 1210.06 | 1213.11 | I216.15 |
| 4000 | 1219.20 | I222.25 | 1225.30 | 1228.35 | 1231.39 | 1234.44 | 1237.49 | I240.54 | I243.59 | I246.63 |

FEET INTO METRES.
I $\mathrm{foot}=0.3048006$ metre.

| Fect. | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 4000 | 1219.2 | 1222.3 | 1225.3 | 1228.3 | 1231.4 | 1234.4 | 1237.5 | 1240. 5 | 1243.6 | 1246.6 |
| 4100 | 1249.7 | 1252.7 | 1255.8 | 1258.8 | 1261.9 | 1264.9 | 1268.0 | 1271.0 | 1274. 1 | 1277. I |
| 4200 | 1280.2 | 1283.2 | 1286.3 | 1289.3 | 1292.4 | 1295.4 | 1298.5 | 1301.5 | I304.5 | I 307.6 |
| 4300 | 1310.6 | 1313.7 | I316.7 | 1319.8 | I322.8 | 1325.9 | 1328.9 | 1332.0 | I335.0 | I 338.1 |
| 4400 | I341.1 | I 344.2 | I 347.2 | 1350.3 | I 353.3 | I 356.4 | 1359.4 | 1362.5 | I365.5 | I368.6 |
| 4500 | 1371.6 | 1374.7 | 1377.7 | 1380.7 | 1383.8 | I386.8 | 1389.9 | 1392.9 | 1396.0 | 1399.0 |
| 4600 | 1402.1 | 1405.1 | 1408.2 | 1411.2 | 1414.3 | 1417.3 | 1420.4 | 142 j. 4 | 1426.5 | 1429.5 |
| 4700 | 1432.6 | 1435.6 | 1438.7 | 1441.7 | 1444.8 | I447.8 | 1450.9 | 1453.9 | 1456.9 | 1460.0 |
| 4800 | 1463.0 | 1466.1 | 1469.1 | 1472.2 | 1475.2 | 1478.3 | 148r. 3 | I484.4 | 1487.4 | 1490.5 |
| 4900 | 1493.5 | 1496.6 | 1499.6 | 1502.7 | 1505.7 | 1508.8 | I5II.8 | 1514.9 | 1517.9 | 1521.0 |
| 5000 | 1524.0 | 1527.1 | 1530.1 | 1533.1 | 1536.2 | 1539.2 | 1542.3 | 1545.3 | 1548.4 | 1551.4 |
| 5100 | I554.5 | 1557.5 | 1560.6 | 1563.6 | I566.7 | 1569.7 | 1572.8 | I575.8 | 1578.9 | I581.9 |
| 5200 | 1585.0 | I588.0 | 1591. 1 | I594.1 | 1597.2 | 1600.2 | 1603.3 | 1606.3 | 1609.3 | 1612.4 |
| 5300 | 16 I 5.4 | 1618.5 | 1621.5 | 1624.6 | 1627.6 | 1630.7 | 1633.7 | 1636.8 | 1639.8 | 1642.9 |
| 5400 | 1645.9 | 1649.0 | 1652.0 | 1655. I | 1658. 1 | 166I. 2 | 1664.2 | 1667.3 | 1670.3 | 1673.4 |
| 5500 | 1676.4 | 1679.5 | 1682.5 | 1685.5 | 1688.6 | 1691.6 | 1694.7 | 1697.7 | 1700.8 | 1703.8 |
| 5600 | 1706.9 | 1709.9 | 1713.0 | 1716.0 | 1719.1 | 1722.1 | 1725.2 | 1728.2 | 1731.3 | 1734.3 |
| 5700 | 1737.4 | 1740.4 | 1743.5 | 1746.5 | 1749.6 | 1752.6 | 1755.7 | 1758.7 | 1761.7 | 1764.8 |
| 5800 | 1767.8 | 1770.9 | 1773.9 | 1777.0 | 1780.0 | 1783.1 | 1786. 1 | 1789.2 | 1792.2 | 1795.3 |
| 5900 | 1798.3 | 1801. 4 | 1804.4 | 1807.5 | 1810.5 | 1813.6 | 1816.6 | 1819.7 | 1822.7 | 1825.8 |
| 6000 | 1828.8 | 1831.9 | 1834.9 | 1837.9 | 1841.0 | 1844.0 | 1847.1 | 1850.1 | 1853.2 | 1856.2 |
| 6100 | 1859.3 | 1862.3 | 1865.4 | 1868.4 | 1871.5 | 1874.5 | 1877.6 | 1880.6 | 1883.7 | 1886.7 |
| 6200 | 1889.8 | 1892.8 | 1895.9 | 1898.9 | 1902.0 | 1905.0 | 1908. 1 | 1911.1 | 1914.1 | 1917.2 |
| 6300 | 1920.2 | 1923.3 | 1926.3 | 1929.4 | 1932.4 | 1935.5 | 1938.5 | 1941.6 | 1944.6 | 1947.7 |
| 6400 | 1950.7 | 1953.8 | 1956.8 | 1959.9 | 1962.9 | 1966.0 | 1969.0 | 1972.1 | 1975.1 | 1978.2 |
| 6500 | 1981. 2 | 1984.3 | 1987.3 | 1990.3 | 1993.4 | 1996.4 | 1999.5 | 2002.5 | 2005.6 | 2008.6 |
| 6600 | 2011.7 | 2014.7 | 2017.8 | 2020.8 | 2023.9 | 2026.9 | 2030.0 | 2033.0 | 2036.1 | 2039.1 |
| 6700 | 2042.2 | 2045.2 | 2048.3 | 2051.3 | 2054.4 | 2057.4 | 2060.5 | 2063.5 | 2066.5 | 2069.6 |
| 6800 | 2072.6 | 2075.7 | 2078.7 | 2081.8 | 2084.8 | 2087.9 | 2090.9 | 2094.0 | 2097.0 | 2100.1 |
| 6900 | 2103.1 | 2106.2 | 2109.2 | 2112.3 | 2115.3 | 2118.4 | 2121.4 | 2124.5 | 2127.5 | 2130.6 |
| 7000 | 2133.6 | 2136.7 | 2139.7 | 2142.7 | 2145.8 | 2148.8 | 2151.9 | 2154.9 | 2158.0 | 2161.0 |
| 7100 | 2164.1 | 2167.1 | 2170.2 | 2173.2 | 2176.3 | 2179.3 | 2182.4 | 2185.4 | 2188.5 | 2191.5 |
| 7200 | 2194.6 | 2197.6 | 2200.7 | 2203.7 | 2206.8 | 2209.8 | 2212.9 | 2215.9 | 2218.9 | 2222.0 |
| 7300 | 2225.0 | 2228. 1 | 2231.1 | 2234.2 | 2237.2 | 2240.3 | 2243.3 | 2246.4 | 2249.4 | 2252.5 |
| 7400 | 2255.5 | 2258.6 | 2261.6 | 2264.7 | 2267.7 | 2270.8 | 2273.8 | 2276.9 | 2279.9 | 2283.0 |
| 7500 | 2286.0 | 2289. I | 2292.1 | 2295. I | 2298.2 | 2301.2 | 2304.3 | 2307.3 | 2310.4 | 2313.4 |
| 7600 | 2316.5 | 2319.5 | 2322.6 | 2325.6 | 2328.7 | 2331.7 | 2334.8 | 2337.8 | 2340.9 | 2343.9 |
| 7700 | 2347.0 | 2350.0 | 2353.1 | 2356.1 | 2359.2 | 2362.2 | 2365.3 | 2368.3 | 2371.3 | 2374.4 |
| 7800 | 2377.4 | 2380.5 | 2383.5 | 2386.6 | 2389.6 | 2392.7 | 2395.7 | 2398.8 | 2401.8 | 2404.9 |
| 7900 | 2407.9 | 2411.0 | 2414.0 | 2417.1 | 2420.1 | 2423.2 | 2426.2 | 2429.3 | 2432.3 | 2435.4 |
| 8000 | 2438.4 | 2441.5 | 2444.5 | 2447.5 | 2450.6 | 2453.6 | 2456.7 | 2459.7 | 2462.8 | 2465.8 |
| 8100 | 2468.9 | 2471.9 | 2475.0 | 2478.0 | 2481. I | 2484. I | 2487.2 | 2490.2 | 2493.3 | 2496.3 |
| 8200 | 2499.4 | 2502.4 | 2505.5 | 2508.5 | 25 II. 6 | 2514.6 | 2517.7 | 2520.7 | 2523.7 | 2526.8 |
| 8300 | 2529.8 | 2532.9 | 2535.9 | 2539.0 | 2542.0 | 2545. I | 2548.1 | 2551.2 | 2554.2 | 2557.3 |
| 8400 | 2560.3 | 2563.4 | 2566.4 | 2569.5 | 2572.5 | 2575.6 | 2578.6 | 2581.7 | 2584.7 | 2587.8 |
| 8500 | 2590.8 | 2593.9 | 2596.9 | 2599.9 | 2603.0 | 2606.0 | 2609. 1 | 2612.1 | 2615.2 | 2618.2 |
| 8600 | 2621.3 | 2624.3 | 2627.4 | 2630.4 | 2633.5 | 2636.5 | 2639.6 | 2642.6 | 2645.7 | 2648.7 |
| 8700 | 2651.8 | 2654.8 | 2657.9 | 2660.9 | 2664.0 | 2667.0 | 2670.1 | 2673.1 | 2676. 1 | 2679.2 |
| 8800 | 2682.2 | 2685.3 | 2688.3 | 2691.4 | 2694.4 | 2697.5 | 2700.5 | 2703.6 | 2706.6 | 2709.7 |
| 8900 | 2712.7 | 2715.8 | 2718.8 | 2721.9 | 2724.9 | 2728.0 | 2731.0 | 2734. I | 2737. 1 | 2740.2 |
| 9000 | 2743.2 | 2746.3 | 2749.3 | 2752.3 | 2755.4 | 2758.4 | 2761.5 | 2764.5 | 2767.6 | 2770.6 |

## METRES INTO FEET.

1 metre $=39.3700$ inches $=3.280833$ feet

| Metres. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Feet. | Feet. | Feet. | Feet. | Fee | Feet. | Feet. | Feet. | Feet. | Feet. |
| 0 | 0.00 | 3.28 | 6.56 | 9.84 | 13.12 | 16.40 | 19.68 | 22.97 | 26.25 | 53 |
| 10 | 32.81 | 36.09 | 39.37 | 42.65 | 45.93 | 49.21 | 52.49 | 55.77 | 59.05 | 62.34 |
| 20 | 65.62 | 68.90 | 72.18 | 75.46 | 78.74 | 82.02 | 85.30 | 88.58 | 91.86 | 95.14 |
| 30 | 98.42 | 101.71 | 104.99 | 108.27 | III. 55 | 114.83 | II8.11 | 121.39 | 124.67 | 127.95 |
| 40 | I31.23 | 134.51 | 137.79 | 141.08 | 144.36 | 147.64 | 150.92 | 154.20 | 157.48 | 160.76 |
| 50 | 164.04 | 167.32 | 170.60 | 173.88 | 177.16 | 180.45 | 183.73 | 187.01 | 190.29 | 193.57 |
| 60 | 196.85 | 200.13 | 203.41 | 206.69 | 209.97 | 213.25 | 216.53 | 219.82 | 223.10 | 226.38 |
| 70 | 229.66 | 232.94 | 236.22 | 239.50 | 242.78 | 246.06 | 249.34 | 252.62 | 255.90 | 259.19 |
| 80 | 262.47 | 265.75 | 269.03 | 272.31 | 275.59 | 278.87 | 282.15 | 285.43 | 288.71 | 291.99 |
| 90 | 295.27 | 298.56 | 301.84 | 305.12 | 308.40 | 311.68 | 314.96 | 318.24 | 321.52 | 324.80 |
| 100 | 328.08 | 331.36 | 334.64 | 337.93 | 341.2I | 344.49 | 347.77 | 351.05 | 354.33 | 357.61 |
| 110 | 360.89 | 364.17 | 367.45 | 370.73 | 374.01 | 377.30 | 380.58 | 383.86 | 387.14 | 390.42 |
| 120 | 393.70 | 396.98 | 400.26 | 403.54 | 4.06 .82 | 410.10 | 413.38 | 416.67 | 419.95 | 423.23 |
| 130 | 426.5 I | 429.79 | 433.07 | 436.35 | 439.63 | 442.91 | 446.19 | 449.47 | 452.75 | 456.04 |
| 140 | 459.32 | 462.60 | 465.88 | 469.16 | 472.44 | 475.72 | 479.00 | 482.28 | 485.56 | 488.84 |
| 150 | 492.12 | 495.4I | 498.69 | 501.97 | 505.25 | 508.53 | 5II.8I | 515.09 | 518.37 | 521.65 |
| 160 | 524.93 | 528.21 | 531.49 | 534.78 | 538.06 | 541.34 | 544.62 | 547.90 | 551.18 | 554.46 |
| 170 | 557.74 | 561.02 | 564.30 | 567.58 | 570.86 | 574.15 | 577.43 | 580.71 | 583.99 | 587.27 |
| 180 | 590.55 | 593.83 | 597.11 | 600.39 | 603.67 | 606.95 | 610.23 | 613.52 | 616.80 | 620.08 |
| 190 | 623.36 | 626.64 | 629.92 | 633.20 | 636.48 | 639.76 | 643.04 | 646.32 | 649.60 | 652.89 |
| 200 | 656.17 | 659.45 | 662.73 | 666.0I | 669.29 | 672.57 | 675.85 | 679.13 | 682.41 | 685.69 |
| 210 | 688.97 | 692.26 | 695.54 | 698.82 | 702.10 | 705.38 | 708.66 | 711.94 | 715.22 | 718.50 |
| 220 | 721.78 | 725.06 | 728.34 | 731.63 | 734.91 | 738.19 | 741.47 | 744.75 | 748.03 | 751.31 |
| 230 | 754.59 | 757.87 | 76 t .15 | 764.43 | 767.71 | 771.00 | 774.28 | 777.56 | 780.84 | 784.12 |
| 240 | 787.40 | 790.68 | 793.96 | 797.24 | 800.52 | 803.80 | 807.08 | 810.37 | 813.65 | 816.93 |
| 250 | 820.21 | 823.49 | 826.77 | 830.05 | 833.33 | 836.61 | 839.89 | 843.17 | 846.45 | 849.74 |
| 260 | 853.02 | 856.30 | 859.58 | 862.86 | 866.14 | 869.42 | 872.70 | 875.98 | 879.26 | 882.54 |
| 270 | 885.82 | 889.11 | 892.39 | 895.67 | 898.95 | 902.23 | 905.5I | 908.79 | 912.07 | 915.35 |
| 280 | 918.63 | 92I.91 | 925.19 | 928.48 | 931.76 | 935.04 | 938.32 | 941.60 | 944.88 | 948.16 |
| 290 | 951.44 | 954.72 | 958.00 | 961.28 | 964.56 | 967.85 | 971.13 | 974.4I | 977.69 | 980.97 |
| 300 | 984.25 | 987.53 | 990.81 | 994.09 | 997.37 | 1000. 65 | 1003.93 | 1007.22 | 1010.50 | IOI3.78 |
| 310 | IOI7.06 | 1020.34 | I023.62 | IO26.90 | 1030.18 | 1033.46 | 1036.74 | 1040.02 | 1043.30 | 1046.59 |
| 320 | 1049.87 | I053.15 | 1056.43 | 1059.71 | 1062.99 | 1066.27 | 1069.55 | 1072.83 | 1076.1I | 1079.39 |
| 330 | Io82.67 | 1085.96 | Io89.24 | Io92.52 | 1095.80 | 1099.08 | I 102.36 | 1105.64 | 1109.92 | III 2.20 |
| 340 | I I 15.48 | I I I 8.76 | I122.04 | I 125.33 | II28.6I | II31.89 | II35.17 | I 138.45 | 1141.73 | II45.01 |
| 350 | I 148.29 | I 151.57 | I 154.85 | I 158.13 | II61.41 | I 164.70 | 1167.98 | II 71.26 | II74.54 | 1177.82 |
| 360 | i181.10 | II84.38 | I 187.66 | I 190.94 | I 194.22 | I 197.50 | 1200.78 | 1204.07 | I207.35 | 1210.63 |
| 370 | [213.91 | 1217.19 | I220.47 | 1223.75 | 1227.03 | 1230.3 I | 1233.59 | 1236.87 | I240.15 | 1243.44 |
| 380 | 1246.72 | 1250.00 | 1253.28 | 1256.56 | 1259.84 | 1263.12 | 1266.40 | I269.68 | I272.96 | 1276.24 |
| 390 | 1279.52 | 1282.81 | 1286.09 | 1289.37 | 1292.65 | 1295.93 | 1299.2I | I 302.49 | I 305.77 | I 309.05 |
| 400 | ${ }^{1} 312.33$ | I315.6I | I318.89 | I322.18 | I 325.46 | 1328.74 | 1332.02 | I 335.30 | I338.58 | I341.86 |
| 410 | I345.14 | I348.42 | I 351.70 | I 354.98 | I358.26 | I36I.55 | 1364.83 | I368.11 | I371.39 | I 374.67 |
| 420 | I377.95 | I381.23 | I 384.5 I | I 387.79 | 1391.07 | I394.35 | I397.63 | 1400.92 | 1404.20 | 1407.48 |
| 430 | 1410.76 | I414.04 | I417.32 | 1420.60 | 1423.88 | 1427.16 | I430.44 | 1433.72 | 1437.00 | I440.29 |
| 440 | I443.57 | I446.85 | 1450.13 | I453.4I | 1456.69 | I459.97 | 1463.25 | 1466.53 | 1469.81 | 1473.09 |
| 450 | 1476.37 | 1479.66 | I482.94 | I486.22 | 1489.50 | 1492.78 | 1496.06 | 1499.34 | 1502.62 | 1505.90 |
| 460 | r509.18 | 1512.46 | 1515.74 | I519.03 | I 522.3 I | 1525.59 | I 528.87 | 1532.15 | I535.43 | 1538.71 |
| 470 | r 54 I .99 | ${ }^{1} 545.27$ | 1548.55 | ${ }^{1} 551.83$ | ${ }^{1} 555.11$ | 1558.40 | 1561.68 | 1564.96 | 1568.24 | ${ }^{1} 571.52$ |
| 480 | r574.80 | 1578.08 | 1581.36 | I584.64 | 1587.92 | I591.20 | ${ }^{1} 594.48$ | 1597.77 | 1601.05 | 1604.33 |
| 490 | r607.61 | 1610.89 | 1614.17 | 1617.45 | 1620.73 | 1624.01 | 1627.29 | 1630.57 | 1633.85 | 1637.14 |
| 500 | 1640.42 | 1643.70 | 1646.98 | 1650.26 | 1653.54 | r656.82 | 1660.10 | 1663.38 | I666.66 | 1669.94 |

## METRES INTO FEET.

1 metre $=39.3700$ inches $=\mathbf{3 . 2 8 0 8 3 3}$ feet


I mile $=1.609347$ kilometres

| Miles. | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | km . | km. | km . | km. | km. | km . | km. | km . | km . | km. |
| 0 | 0 | 2 | 3 | 5 | 6 | 8 | 10 | II | 13 | 14 |
| 10 | 16 | 18 | 19 | 21 | 23 | 24 | 26 | 27 | 29 | 31 |
| 20 | 32 | 34 | 35 | 37 | 39 | 40 | 42 | 43 | 45 | 47 |
| 30 | 48 | 50 | 51 | 53 | 55 | 56 | 58 | 60 | 61 | 63 |
| 40 | 64 | 66 | 68 | 69 | 71 | 72 | 74 | 76 | 77 | 79 |
| 50 | 80 | 82 | 84 | 85 | 87 | 89 | 90 | 92 | 93 | 95 |
| 60 | 97 | 98 | 100 | 101 | 103 | 105 | 106 | 108 | 109 | III |
| 70 | II3 | 114 | 116 | 117 | 119 | 121 | 122 | 124 | 126 | 127 |
| 80 | 129 | 130 | 132 | 134 | 135 | 137 | 138 | 140 | 142 | 143 |
| 90 | 145 | 146 | 148 | 150 | 151 | 153 | 154 | 156 | I 58 | [59 |
| 100 | 16I | 163 | 164 | 166 | 167 | 169 | 171 | 172 | 174 | 175 |
| 110 | 177 | 179 | 180 | 182 | 183 | 185 | 187 | 188 | 190 | 192 |
| 120 | 193 | 195 | 196 | 198 | 200 | 201 | 203 | 204 | 206 | 208 |
| 130 | 209 | 211 | 212 | 214 | 216 | 217 | 219 | 220 | 222 | 224 |
| 140 | 225 | 227 | 229 | 230 | 232 | 233 | 235 | 237 | 238 | 240 |
| 150 | 241 | 243 | 245 | 246 | 248 | 249 | 251 | 253 | 254 | 256 |
| 160 | 257 | 259 | 261 | 262 | 264 | 266 | 267 | 269 | 270 | 272 |
| 170 | 274 | 275 | 277 | 278 | 280 | 282 | 283 | 285 | 286 | 288 |
| I8o | 290 | 291 | 293 | 295 | 296 | 298 | 299 | 301 | 303 | 304 |
| 190 | 306 | 307 | 309 | 3 II | 312 | 314 | 315 | 317 | 319 | 320 |
| 200 | 322 | 323 | 325 | 327 | 328 | 330 | 332 | 333 | 335 | 336 |
| 210 | 338 | 340 | 341 | 343 | 344 | 346 | 348 | 349 | 351 | 352 |
| 220 | 354 | 356 | 357 | 359 | 360 | 362 | 364 | 365 | 367 | 369 |
| 230 | 370 | 372 | 373 | 375 | 377 | 378 | 380 | 381 | 383 | 385 |
| 240 | 386 | 388 | 389 | 391 | 393 | 394 | 396 | 398 | 399 | 401 |
| 250 | 402 | 404 | 406 | 407 | 409 | 410 | 412 | 414 | 415 | 417 |
| 260 | 418 | 420 | 422 | 423 | 425 | 426 | 428 | 430 | 431 | 433 |
| 270 | 435 | 436 | 438 | 439 | 441 | 443 | 444 | 446 | 447 | 449 |
| 280 | 45 I | 452 | 454 | 455 | 457 | 459 | 460 | 462 | 463 | 465 |
| 290 | 467 | 468 | 470 | 472 | 473 | 475 | 476 | 478 | 480 | 481 |
| 300 | 483 | 484 | 486 | 488 | 489 | 491 | 492 | 494 | 496 | 497 |
| 310 | 499 | 5 OI | 502 | 504 | 505 | 507 | 509 | 510 | 512 | 513 |
| 320 | 5 I 5 | 517 | 518 | 520 | 521 | 523 | 525 | 526 | 528 | 529 |
| 330 | 53 I | 533 | 534 | 536 | 538 | 539 | 541 | 542 | 544 | 546 |
| 340 | 547 | 549 | 550 | 552 | 554 | 555 | 557 | 558 | 560 | 562 |
| 350 | 563 | 565 | 566 | 568 | 570 | 571 | 573 | 575 | 576 | 578 |
| 360 | 579 | 581 | 583 | 584 | 586 | 587 | 589 | 591 | 592 | 594 |
| 370 | 595 | 597 | 599 | 600 | 602 | 604 | 605 | 607 | 608 | 610 |
| 380 | 612 | 613 | 6 I 5 | 616 | 618 | 620 | 621 | 623 | 624 | 626 |
| 390 | 628 | 629 | 631 | 632 | 634 | 636 | 637 | 639 | 641 | 642 |
| 400 | 644 | 645 | 647 | 649 | 650 | 652 | 653 | 655 | 657 | 658 |
| 410 | 660 | 661 | 663 | 665 | 666 | 668 | 669 | 671 | 673 | 674 |
| 420 | 676 | 678 | 679 | 681 | 682 | 684 | 686 | 687 | 689 | 690 |
| 430 | 692 | 694 | 695 | 697 | 698 | 700 | 702 | 703 | 705 | 706 |
| 440 | 708 | 710 | 711 | 713 | 715 | 716 | 718 | 719 | 721 | 723 |
| 450 | 724 | 726 | 727 | 729 | 731 | 732 | 734 | 735 | 737 | 739 |
| 460 | 740 | 742 | 744 | 745 | 747 | 748 | 750 | 752 | 753 | 755 |
| 470 | 756 | 758 | 760 | 761 | 763 | 764 | 766 | 768 | 769 | 771 |
| 480 | 772 | 774 | 776 | 778 | 779 | 781 | 782 | 784 | 785 | 787 803 |
| 490 | 789 | 790 | 792 | 793 | 795 | 797 | 798 | 800 | 801 | 803 |
| 500 | 805 | 806 | 808 | 809 | 8 II | 813 | 814 | 816 | 818 | 819 |
| 510 | 821 | 822 | 824 | 826 | 827 | 829 | 830 | 832 | 834 | 835 |
| 520 | 837 | 838 | 840 | 842 | 843 | 845 | 847 | 848 | 850 | 851 |
| 530 | 853 | 855 | 856 | 858 | 859 | 861 | 863 | 864 | 866 | 867 |
| 540 | 869 | 87 I | 872 | 874 | 875 | 877 | 879 | 880 | 882 | 884 |
| 550 | 885 | 887 | 888 | 890 | 892 | 893 | 895 | 896 | 898 | 900 |

Smithbonian Tableb.

MILES INTO KILOMETRES.

| Miles. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | km . | km. | km. | km . | km. | km. | km. | km. | km . | km. |
| 550 | 885 | 887 | 888 | 890 | 892 | 893 | S95 | 896 | 898 | 900 |
| 560 | 901 | 903 | 904 | 906 | 908 | 909 | 911 | 912 | 914 | 916 |
| 570 | 917 | 919 | 921 | 922 | 924 | 925 | 927 | 929 | 930 | 932 |
| 580 | 933 | 935 | 937 | 938 | 940 | 941 | 943 | 945 | 946 | 948 |
| 590 | 950 | 951 | 953 | 954 | 956 | 958 | 959 | 961 | 962 | 964 |
| 600 | 966 | 967 | 969 | 970 | 972 | 974 | 975 | 977 | 978 | 980 |
| 610 | 982 | 983 | 985 | 987 | 988 | 990 | 991 | 993 | 995 | 996 |
| 620 | 998 | 999 | 1001 | 1003 | 1004 | 1006 | 1007 | 1009 | IOII | 1012 |
| 630 | 1014 | 1015 | 1017 | 1019 | 1020 | 1022 | 1024 | 1025 | 1027 | 1028 |
| 640 | 1030 | 1032 | 1033 | 1035 | 1036 | 1038 | 1040 | 1041 | 1043 | 1044 |
| 650 | 1046 | 1048 | 1049 | 1051 | 1053 | 1054 | 1056 | 1057 | 1059 | 1061 |
| 660 | 1062 | 1064 | 1065 | 1067 | 1069 | 1070 | 1072 | 1073 | 1075 | 1077 |
| 670 | 1078 | 1080 | 1081 | 1083 | 1085 | 1086 | ro88 | 1090 | 1091 | 1093 |
| 680 | 1094 | 1096 | 1098 | 1099 | IIOI | 1102 | 1104 | 1106 | 1107 | 1109 |
| 690 | IIIO | 1112 | III4 | III5 | III7 | 1118 | 1120 | 1122 | 1123 | 1125 |
| 700 | 1127 | 1128 | 1130 | II3I | 1133 | 1135 | II 36 | 1138 | 1139 | 1141 |
| 710 | 1143 | 1144 | 1146 | 1147 | 1149 | 1151 | I 152 | 1154 | I 156 | 1157 |
| 720 | 1159 | 1160 | 1162 | 1164 | 1165 | 1167 | I 168 | 1170 | 1172 | 1173 |
| 730 | 1175 | 1176 | 1178 | 1180 | II81 | 1183 | 1184 | IIS6 | 1188 | 1189 |
| 740 | II9I | 1193 | II94 | 1196 | 1197 | 1199 | I2OI | 1202 | 1204 | 1205 |
| 750 | 1207 | 1209 | 1210 | 1212 | 1213 | 1215 | 1217 | 1218 | 1220 | 1221 |
| 760 | 1223 | 1225 | 1226 | 1228 | 1230 | 1231 | 1233 | 1234 | 1236 | 1238 |
| 770 | 1239 | 1241 | 1242 | 1244 | 1246 | 1247 | 1249 | 1250 | 1252 | 1254 |
| 780 | 1255 | 1257 | 1259 | 1260 | 1262 | 1263 | 1265 | 1267 | 1268 | 1270 |
| 790 | 1271 | 1273 | 1275 | 1276 | 1278 | 1279 | 1281 | 1283 | 1284 | 1286 |
| 800 | 1287 | 1289 | 1291 | 1292 | 1294 | 1296 | 1297 | 1299 | 1300 | 1302 |
| 810 | 1304 | 1305 | 1307 | 1308 | 1310 | 1312 | I3I3 | 1315 | I316 | 1318 |
| 820 | 1320 | 1321 | 1323 | 1324 | 1326 | 1328 | I 329 | 1331 | 1333 | 1334 |
| 830 | 1336 | 1337 | I 339 | 1341 | I 342 | I 344 | I 345 | 1347 | 1349 | 1350 |
| 840 | 1352 | 1353 | I 355 | 1357 | 1358 | I360 | I362 | 1363 | 1365 | I 366 |
| 850 | ป368 | 1370 | 1371 | 1373 | 1374 | 1376 | I378 | 1379 | 1381 | 1382 |
| 860 | 1384 | 1386 | 1387 | 1389 | 1390 | 1392 | I394 | 1395 | 1397 | 1399 |
| 870 | 1400 | 1402 | 1403 | 1405 | 1407 | 1408 | 1410 | 14II | 1413 | 1415 |
| 880 | 1416 | 1418 | 1419 | 1421 | 1423 | 1424 | 1426 | 1427 | 1429 | 1431 |
| S90 | 1432 | 1434 | 1436 | 1437 | 1439 | 1440 | 1442 | 1444 | 1445 | 1447 |
| 900 | 1448 | 1450 | 1452 | 1453 | 1455 | 1456 | 1458 | 1460 | 1461 | 1463 |
| 910 | 1464 | 1466 | 1468 | 1469 | 1471 | 1473 | 1474 | 1476 | 1477 | 1479 |
| 920 | 1481 | 1482 | 1484 | 1485 | 1487 | 1489 | 1490 | 1492 | 1493 | 1495 |
| 930 | 1497 | 1498 | 1500 | 1502 | 1503 | 1505 | 1506 | 1508 | 1510 | 1511 |
| 940 | 1513 | 1514 | I516 | I5I8 | 1519 | 1521 | I 522 | 1524 | 1526 | 1527 |
| 950 | 1529 | 1530 | 1532 | 1534 | 1535 | 1537 | 1539 | 1540 | 1542 | 1543 |
| 960 | 1545 | 1547 | 1548 | I550 | 1551 | 1553 | 1555 | 1556 | 1558 | 1559 |
| 970 | 1561 | I563 | 1564 | I 566 | 1567 | 1569 | 1571 | 1572 | 1574 | 1576 |
| 980 | 1577 | 1579 | 1580 | 1582 | 1584 | 1585 | 1587 | 1588 | 1590 | 1592 |
| 990 | I593 | 1595 | 1596 | ${ }^{1} 598$ | 1600 | 1601 | 1603 | 1605 | 1606 | 1608 |
| 1000 | 1609 | 1611 | 1613 | 1614 | 1616 | 1617 | 1619 | 162I | 1622 | 1624 |
|  | Miles. | km. |  |  |  | , | km. | Miles. | km. |  |
|  | 1000 | 1609 |  |  |  |  | 17703 | 16000 | 25750 |  |
|  | 2000 | 3219 |  |  |  | 000 | 19312 | 17000 | $27359$ |  |
|  | 3000 | 4828 |  |  |  | 000 | 20922 | 18000 | $28968$ |  |
|  | 4000 | 6437 |  |  |  | 000 | 22531 | 19000 | 30578 |  |
|  | 5000 | 8047 | 100 |  |  | 000 | 24140 | 20000 | 32187 |  |

I kilometre $=0.621370 \mathrm{mile}$.

| Kilometres. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. |
| 0 | 0.0 | 0.6 | I. 2 | I. 9 | 2.5 | 3.1 | 3.7 | 4.3 | 5.0 | 5.6 |
| Io | 6.2 | 6.8 | $7 \cdot 5$ | 8.1 | 8.7 | $9 \cdot 3$ | 9.9 | 10.6 | II. 2 | II. 8 |
| 20 | 12.4 | 13.0 | 13.7 | 14.3 | 14.9 | 15.5 | 16.2 | 16.8 | 17.4 | 18.0 |
| 30 | 18.6 | 19.3 | 19.9 | 20.5 | 2 I. 1 | 21.7 | 22.4 | 23.0 | 23.6 | 24.2 |
| 40 | 24.9 | 25.5 | 26. I | 26.7 | 27.3 | 28.0 | 28.6 | 29.2 | 29.8 | 30.4 |
| 50 | 3 I .1 | 3 I .7 | 32.3 | 32.9 | 33.6 | 34.2 | 34.8 | 35.4 | 36.0 | 36.7 |
| 60 | 37.3 | 37.9 | 38.5 | 39.1 | 39.8 | 40.4 | 41.0 | 41.6 | 42.3 | 42.9 |
| 70 | 43.5 | 44.1 | 44.7 | 45.4 | 46.0 | 46.6 | 47.2 | 47.8 | 48.5 | 49.1 |
| 80 | 49.7 | 50.3 | 51.0 | 51.6 | 52.2 | 52.8 | 53.4 | 54.1 | 54.7 | 55.3 |
| 90 | 55.9 | 56.5 | 57.2 | 57.8 | 58.4 | 59.0 | 59.7 | 60.3 | 60.9 | 61.5 |
| 100 | 62.1 | 62.8 | 63.4 | 64.0 | 64.6 | 65.2 | 65.9 | 66.5 | 67.1 | 67.7 |
| 110 | 68.4 | 69.0 | 69.6 | 70.2 | 70.8 | 71.5 | 72.1 | 72.7 | 73.3 | 73.9 |
| 120 | 74.6 | 75.2 | 75.8 | 76.4 | 77.0 | 77.7 | 78.3 | 78.9 | 79.5 | 80.2 |
| 130 | 80.8 | 8 r .4 | 82.0 | 82.6 | 83.3 | 83.9 | 84.5 | 85. I | 85.7 | 86.4 |
| 140 | 87.0 | 87.6 | 88.2 | 88.9 | 89.5 | 90.1 | 90.7 | 91.3 | 92.0 | 92.6 |
| 150 | 93.2 | 93.8 | 94.4 | 95. I | 95.7 | 96.3 | 96.9 | 97.6 | 98.2 | 98.8 |
| 160 | 99.4 | 100.0 | 100.7 | IOI. 3 | IOI. 9 | 102.5 | 103.1 | 103.8 | 104.4 | 105.0 |
| 170 | 105.6 | 106.3 | 106.9 | 107.5 | 108. 1 | 108.7 | 109.4 | I10.O | 110.6 | III. 2 |
| I80 | III. 8 | 112.5 | II3. I | I 13.7 | 114.3 | II5.0 | I 15.6 | II6.2 | I 16.8 | 117.4 |
| 190 | IIS. I | II8.7 | 119.3 | 119.9 | 120.5 | 121.2 | 121.8 | 122.4 | 123.0 | 123.7 |
| 200 | 124.3 | 124.9 | 125.5 | I26. 1 | 126.8 | 127.4 | 128.0 | I28.6 | 129.2 | 129.9 |
| 210 | I30.5 | I3I.I | 131.7 | 132.4 | 133.0 | 133.6 | I 34.2 | I 34.8 | I 35.5 | 136.I |
| 220 | 136.7 | 137.3 | I 37.9 | I 38.6 | 139.2 | 139.8 | 140.4 | I41.I | 141.7 | 142.3 |
| 230 | 142.9 | 143.5 | 144.2 | 144.8 | 145.4 | 146.0 | 146.6 | 147.3 | 147.9 | 148.5 |
| 240 | 149.1 | 149.8 | 150.4 | 151.0 | 151.6 | 152.2 | ${ }^{1} 52.9$ | 153.5 | I54. I | 154.7 |
| 250 | 155.3 | 156.0 | I56.6 | 157.2 | 157.8 | 158.4 | 159.1 | I59.7 | 160.3 | 160.9 |
| 260 | 161.6 | 162.2 | 162.8 | 163.4 | 164.0 | 164.7 | 165.3 | 165.9 | 166.5 | 167.1 |
| 270 | 167.8 | 168.4 | 169.0 | 169.6 | 170.3 | 170.9 | 171.5 | 172.I | 172.7 | 173.4 |
| 280 | 174.0 | 174.6 | 175.2 | 175.8 | 176.5 | 177.1 | 177.7 | 178.3 | 179.0 | 179.6 |
| 290 | 180.2 | 180.8 | I8I. 4 | 182. 1 | I82.7 | 183.3 | 183.9 | 184.5 | I85.2 | 185.8 |
| 300 | 186.4 | 187.0 | 187.7 | 188.3 | 188.9 | 189.5 | 190.1 | 190.8 | 191.4 | 192.0 |
| 310 | 192.6 | 193.2 | 193.9 | 194.5 | 195.I | 195.7 | 196.4 | 197.0 | 197.6 | 198.2 |
| 320 | 198.8 | 199.5 | 200. 1 | 200.7 | 201.3 | 201.9 | 202.6 | 203.2 | 203.8 | 204.4 |
| 330 | 205.1 | 205.7 | 206.3 | 206.9 | 207.5 | 208.2 | 208.8 | 209.4 | 210.0 | 210.6 |
| 340 | 211.3 | 211.9 | 212.5 | 213.1 | 213.8 | 214.4 | 215.0 | 215.6 | 216.2 | 216.9 |
| 350 | 217.5 | 218.1 | 218.7 | 219.3 | 220.0 | 220.6 | 221.2 | 22 I .8 | 222.5 | 223. I |
| 360 | 223.7 | 224.3 | 224.9 | 225.6 | 226.2 | 226.8 | 227.4 | 228.0 | 228.7 | 229.3 |
| 370 | 229.9 | 230.5 | 231.1 | 23 I .8 | 232.4 | 233.0 | 233.6 | 234.3 | 234.9 | 235.5 |
| 380 | 236.I | 236.7 | 237.4 | 238.0 | 238.6 | 239.2 | 239.8 | 240.5 | 241.I | 24 I .7 |
| 390 | 242.3 | 243.0 | 243.6 | 244.2 | 244.8 | 245.4 | 246.1 | 246.7 | 247.3 | 247.9 |
| 400 | 248.5 | 249.2 | 249.8 | 250.4 | 251.0 | 251.7 | 252.3 | 252.9 | 253.5 | 254. I |
| 410 | 254.8 | 255.4 | 256.0 | 256.6 | 257.2 | 257.9 | 258.5 | 259.I | 259.7 | 260.4 |
| 420 | 261.0 | 261.6 | 262.2 | 262.8 | 263.5 | 264.I | 264.7 | 265.3 | 265.9 | 266.6 |
| 430 | 267.2 | 267.8 | 268.4 | 269.1 | 269.7 | 270.3 | 270.9 | 271.5 | 272.2 | 272.8 |
| 440 | 273.4 | 274.0 | 274.6 | 275.3 | 275.9 | 276.5 | 277.I | 277.8 | 278.4 | 279.0 |
| 450 | 279.6 | 280.2 | 280.9 | 281.5 | 282.I | 282.7 | 283.3 | 284.0 | 284.6 | 285.2 |
| 460 | 285.8 | 286.5 | 287.1 | 287.7 | 288.3 | 288.9 | 289.6 | 290.2 | 290.8 | 291.4 |
| 470 | 292.0 | 292.7 | 293.3 | 293.9 | 294.5 | 295.2 | 295.8 | 296.4 | 297.0 | 297.6 |
| 480 | 298.3 | 298.9 | 299.5 | 300. 1 | 300.7 | 301.4 | 302.0 | 302.6 | 303.2 | 303.8 |
| 490 | 304.5 | 305.I | 305.7 | 306.3 | 307.0 | 307.6 | 308.2 | 308.8 | 309.4 | 310.1 |
| 500 | 310.7 | 311.3 | 3II. 9 | 312.5 | 313.2 | 3 I 3.8 | 314.4 | 315.0 | 315.7 | 316.3 |
| 510 | 316.9 | 317.5 | 318.I | 318.8 | 319.4 | 320.0 | 320.6 | 321.2 | 32 I .9 | 322.5 |
| 520 | 323.1 | 323.7 | 324.4 | 325.0 | 325.6 | 326.2 | 326.8 | 327.5 | 328.1 | 328.7 |
| 530 | 329.3 | 329.9 | 330.6 | 331.2 | 331.8 | 332.4 | 333.1 | 333.7 | $334 \cdot 3$ | 334.9 |
| 540 | 335.5 | 336.2 | 336.8 | 337.4 | 338.0 . | 338.6 | 339.3 | 339.9 | 340.5 | 341. I |

## KILOMETRES INTO MILES.

| Kilometres. | 0 | I | 2 |  |  | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles. | Miles. | Miles. | Mil |  | Miles. | Miles. | Miles. | Miles. | Mile | Miles. |
| 550 | 341.8 | 342.4 | 343.0 | 343 |  | 344.2 | 344.9 | 345.5 | 346. I | 346.7 | 347.3 |
| 560 | 348.0 | 348.6 | 349.2 | 349 |  | 350.5 | 35 I . I | 351.7 | 352.3 | 352.9 | 353.6 |
| 570 | 354.2 | 354.8 | 355.4 | 356 |  | 356.7 | 357.3 | 357.9 | 358.5 | 359.2 | 359.8 |
| 580 | 360.4 | 361.0 | 36 I .6 | 362 |  | 362.9 | 363.5 | 364.1 | 364.7 | 365.4 | 366.0 |
| 590 | 366.6 | 367.2 | 367.9 |  |  | 369.I | 369.7 | 370.3 | 371.0 | 37 I .6 | 372.2 |
| 600 | 372.8 | 373.4 | 374.I | 374 |  | $375 \cdot 3$ | 375.9 | 376.6 | 377.2 | 377.8 | 378.4 |
| 610 | 379.0 | 379.7 | 380.3 | 380 |  | 38 I .5 | 382.1 | 382.8 | 383.4 | 384.0 | 384.6 |
| 620 | 385.2 | 385.9 | 386.5 | 387 |  | 387.7 | 388.4 | 389.0 | 389.6 | 390.2 | 390.8 |
| 630 | 391.5 | 392.1 | 392.7 | 393 |  | 393.9 | 394.6 | 395.2 | 395.8 | 396.4 | 397. I |
| 640 | 397.7 | 398.3 | 398.9 | 399 |  | 400.2 | 400.8 | 401.4 | 402.0 | 402.6 | 403.3 |
| 650 | 403.9 | 404.5 | 405.I | 405 |  | 406.4 | 407.0 | 407.6 | 408.2 | 408.9 | 409.5 |
| 660 | 410.1 | 410.7 | 411.3 | 412 |  | 412.6 | 413.2 | 413.8 | 414.5 | 415. 1 | 415.7 |
| 670 | 416.3 | 416.9 | 417.6 | 418 |  | 418.8 | 419.4 | 420.0 | 420.7 | 421.3 | 42 I .9 |
| 680 | 422.5 | 423.2 | 423.8 | 424 |  | 425.0 | 425.6 | 426.3 | 426.9 | 427.5 | 428. I |
| 690 | 428.7 | 429.4 | 430.0 | 430 |  | 431.2 | 431.9 | 432.5 | 433. I | 433.7 | 434.3 |
| 700 | 435.0 | 435.6 | 436.2 |  |  | 437.4 | 438. 1 | 438.7 | 439.3 | 439.9 | 440.6 |
| 710 | 441.2 | 441.8 | 442.4 | 443 |  | 443.7 | 444.3 | 444.9 | $445 \cdot 5$ | 446.1 | 446.8 |
| 720 | 447.4 | 448.0 | 448.6 | 449 |  | 449.9 | 450.5 | 45 I .1 | 451.7 | 452.4 | 453.0 |
| 730 | 453.6 | 454.2 | 454.8 | 455 |  | 456.1 | 456.7 | $457 \cdot 3$ | $457 \cdot 9$ | 458.6 | 459.2 |
| 740 | 459.8 | 460.4 | 461.1 | 461 |  | 462.3 | 462.9 | 463.5 | 464.2 | 464.8 | 465.4 |
| 750 | 466.0 | 466.6 | 467.3 |  |  | 468.5 | 469. 1 | 469.8 | 470.4 | 471.0 | 471.6 |
| 760 | 472.2 | 472.9 | 473.5 | 474 |  | 474.7 | 475.3 | 476.0 | 476.6 | 477.2 | 477.8 |
| 770 | 478.5 | 479. 1 | 479.7 | 48 |  | 480.9 | 48 I .6 | 482.2 | 482.8 | 483.4 | 484.0 |
| 780 | 484.7 | 485.3 | 485.9 | 486 |  | 487.2 | 487.8 | 488.4 | 489.0 | 489.6 | 490.3 |
| 790 | 490.9 | 491.5 | 492. I | 492 |  | 493.4 | 494.0 | 494.6 | 495.2 | 495.9 | 496.5 |
| 800 | 497. 1 | 497.7 | 498.3 | 499 |  | 499.6 | 500.2 | 500.8 | 501.4 | 502. I | 502.7 |
| 810 | 503.3 | 503.9 | 504.6 | 505 |  | 505.8 | 506.4 | 507.0 | 507.7 | 508.3 | 508.9 |
| 820 | 509.5 | 510.1 | 510.8 | 5 II |  | 512.0 | 512.6 | 513.3 | 513.9 | 514.5 | 515. I |
| 830 | 515.7 | 516.4 | 517.0 | 517 |  | 518.2 | 518.8 | 519.5 | 520.1 | 520.7 | 52 I .3 |
| 840 | 522.0 | 522.6 | 523.2 | 523 |  | 524.4 | 525. 1 | 525.7 | 526.3 | 526.9 | 527.5 |
| 850 | 528.2 | 528.8 | 529.4 | 53 |  | 530.6 | 531.3 | 531.9 | 532.5 | 533. I | 533.8 |
| 860 | 534.4 | 535.0 | 535.6 | 53 |  | 536.9 | 537.5 | 538.I | 538.7 | 539.3 | 540.0 |
| 870 | 540.6 | 541.2 | 541.8 | 54 |  | 543. 1 | 543.7 | 544.3 | 544.9 | 545.6 | 546.2 |
| 880 | 546.8 | 547.4 | 548.0 | 548 |  | 549.3 | 549.9 | 550.5 | 55 I .2 | 551.8 | 552.4 |
| 890 | 553.0 | 553.6 | 554.3 | 55 |  | 555.5 | 556. I | 556.7 | 557.4 | 558.0 | 558.6 |
| 900 | 559.2 | 559.9 | 560.5 | 561 |  | 56 I .7 | 562.3 | 563.0 | 563.6 | 564.2 | 564.8 |
| 910 | 565.4 | 566. I | 566.7 | 567 | . 3 | 567.9 | 568.6 | 569.2 | 569.8 | 570.4 | 571.0 |
| 920 | 571.7 | 572.3 | 572.9 | 573 | . 5 | 574. 1 | 574.8 | 575.4 | 576.0 | 576.6 | $577 \cdot 3$ |
| 930 | 577.9 | 578.5 | 579. I | 579 | - 7 | 580.4 | 581.0 | 5 Si .6 | 582.2 | 582.8 | 583.5 |
| 940 | 584. 1 | 584.7 | 585.3 |  |  | 586.6 | 587.2 | 587.8 | 588.4 | 589.1 | 589.7 |
| 950 | 590.3 | 590.9 | 591.5 | 59 | 2.2 | 592.8 | 593.4 | 594.0 | 594.7 | 595.3 | 595.9 |
| 960 | 596.5 | 597.1 | 597.8 |  | 8.4 | 599.0 | 599.6 | 600.2 | 600.9 | 601.5 | 602.1 |
| 970 | 602.7 | 603.4 | 604.0 | 60 | 4.6 | 605.2 | 605.8 | 606.5 | 607.1 | 607.7 | 608.3 |
| 980 | 608.9 | 609.6 | 610.2 | 610 | . 8 | 611.4 | 612.0 | 6I2.7 | 613.3 | 613.9 | 614.5 |
| 990 | 615.2 | 615.8 | 616.4 |  |  | 617.6 | 618.3 | 618.9 | 619.5 | 620.1 | 620.7 |
| 1000 | 621.4 | 622.0 | 622.6 | 62 | 3.2 | 623.9 | 624.5 | 625.1 | 625.7 | 626.3 | 627.0 |
|  | km. | Miles. |  |  | M |  | km. | Miles. | km. | Miles. |  |
|  | 1000 | 621.4 |  |  |  |  | 1000 | 6835. 1 | 16000 | 9941.9 |  |
|  | 2000 | 1242.7 |  |  | 434 |  | 12000 | 7456.4 | 17000 | 10563.3 |  |
|  | 3000 | 1864. 1 |  |  |  |  | 13000 | 8077.8 | 18000 | 11184.7 |  |
|  | 4000 | 2485.5 |  |  |  |  | 14000 | 8699.2 | 19000 | 11806.0 |  |
|  | 5000 | 3106.8 | 100 |  | 621 |  | 15000 | 9320.5 | 20000 | 12427.4 |  |

TABLE 70.
INTERCONVERSION OF NAUTICAL AND STATUTE MILES.
I nautical mile* $=6080.27$ feet.

| Nautical Miles. | Statute Miles. | Statute Miles. | Nautical Miles. |
| :---: | :---: | :---: | :---: |
|  | 1.1516 | 1 | 0.8684 |
| 2 | 2.3031 | 1.7368 |  |
| 3 | 3.4547 | 2.6052 |  |
| 4 | 4.6062 | 3 | 3.4736 |
| 5 | 5.7578 | 4 | 4.3420 |
| 6 | 6.9093 | 5 | 6.2104 |
| 7 | 8.0609 | 6 | 6.9788 |
| 8 | 9.2124 | 7 | 7.8155 |
| 9 | 10.3640 | 9 |  |

*As defined by the United States Coast Survey.

TABLE 71.

## CONTINENTAL MEASURES OF LENGTH WITH THEIR METRIC AND ENGLISH EQUIVALENTS.

The asterisk $\left(^{*}\right)$ indicates that the measure is obsolete or seldom used.

| Measure | Metric Equivalent. | English Equivalent. |
| :---: | :---: | :---: |
| El (Netherlands) | metre. | 3.2808 feet. |
| Fathom, Swedish $=6$ feet | r.7814 " | 5.8445 " |
| Foot, Austrian* | 0.31608 " | r. 0370 " |
| old French* | 0.32484 " | 1.0657 " |
| Russian | 0.30480 " | " |
| Rheinlandisch or Rhenish (Prussia*, Denmark, Norway*). | 0.31385 " | 1.0297 " |
| Swedish* | 0.2969 " | 0.9741 " |
| Spanish* $=1 / 3$ vara | 0.2786 " | 0.9140 " |
| *Klafter, Wiener (Vienna) | r. 89648 " | 6.2221 " |
| *Line, old French $=\frac{1}{144}$ foot | 0.22558 cm . | 0.0888 inch. |
| Mile, Austrian post* $=24000$ feet | $\begin{aligned} & 7.58594 \mathrm{~km} . \\ & \text { I. } 852 \quad \text { " } \end{aligned}$ | 4.714 statute miles. <br> 1. 1508 |
| Swedish $=36000$ feet | 10.69 " | 6.642 " " |
| Norwegian $=36000$ feet | II. 2986 " | 7.02 " |
| Netherlands (mijl) | " | 0.6214 " " |
| Prussian (law of 1868) | 7.500 | 4.660 " " |
| Danish | 7.5324 | 4.6804 |
| Palm, Netherlands | 0.1 metre. | 0.328I feet. |
| *Rode, Danish | 3.7662 | 12.356 " |
| *Ruthe, Prussian, Norwegian | 3.7662 | 12.356 " |
| Sagene (Russian) | 2.1336 | 7 " |
| *Toise, old French $=6$ feet | 1.9490 | 6.3943 |
| *Vara, Spanish | 0.8359 " | 2.7424 " |
| Mexican . | 0.8380 | 2.7293 " |
| Werst, or versta (Russian) $=500$ sagene | 1. 0668 km . | 3.500 " |

## CONVERSION OF MEASURES OF TIME AND ANGLE.

Arc into time ..... 72
Time into arc ..... 73
Days into decimals of a year and angle ..... 74
Hours, minutes and seconds into decimals of a day ..... Table 75
Decimals of a day into hours, minutes and seconds Table 76
Minutes and seconds into decimals of an hour ..... Table 77
Mean time at apparent noon ..... 78
Sidereal time into mean solar time ..... Table 79
Mean solar time into sidereal time ..... Table 80

TAble 72.

## ARC INTO TIME.

| - | h. m. | - | h. m. | $\bigcirc$ | h. m. | - | h m. | - | h. m. | - | h. m. | , | m. s. | // | s. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 00 | 60 | 4 o | 120 | 8 o | 180 | 12 O | 240 | 16 o | 300 | 200 | 0 | 0 O | 0 | 0.000 |
| 1 | - 4 | 61 | 44 | 121 | 84 | 181 | 124 | 24 I | 164 | 301 | 204 | 1 | - 4 | I | 0.067 |
| 2 | - 8 | 62 | 48 | 122 | 88 | 182 | 128 | 242 | I6 8 | 302 | 208 | 2 | - 8 | 2 | 0. 133 |
| 3 | O 12 | 63 | 412 | 123 | 812 | 183 | 12 I 2 | 243 | 1612 | 303 | 2012 | 3 | - 12 | 3 | 0.200 |
| 4 | o 16 | 64 | 416 | 124 | 816 | 184 | 1216 | 244 | 1616 | 304 | 2016 | 4 | - 16 | 4 | 0.267 |
| 5 | - 20 | 65 | 420 | 125 | 820 | 185 | 1220 | 245 | 1620 | 305 | 2020 | 5 | O 20 | 5 | 0.333 |
| 6 | O 24 | 66 | 424 | 126 | 824 | 186 | 1224 | 246 | 1624 | 306 | 2024 | 6 | O 24 | 6 | 0.400 |
| 7 | - 28 | 67 | 428 | 127 | 828 | 187 | 1228 | 247 | 1628 | 307 | 2028 | 7 | - 28 | 7 | 0.467 |
| 8 | - 32 | 68 | 432 | 128 | 832 | 188 | 1232 | 248 | 1632 | 308 | 2032 | 8 | - 32 | 8 | 0.533 |
| 9 | - 36 | 69 | 436 | 129 | 836 | 189 | 1236 | 249 | 1636 | 309 | 2036 | 9 | - 36 | 9 | 0.600 |
| 10 | - 40 | 70 | 440 | 130 | 840 | 190 | 1240 | 250 | 1640 | 310 | 2040 | 10 | 040 | 10 | 0.667 |
| II | - 44 | 71 | 444 | 131 | 844 | 191 | 1244 | 251 | 1644 | 3 II | 2044 | II | O 44 | II | 0.733 |
| 12 | - 48 | 72 | 448 | I32 | 848 | 192 | 1248 | 252 | 1648 | 312 | 2048 | 12 | 048 | 12 | 0.800 |
| 13 | - 52 | 73 | 452 | 133 | 852 | 193 | 1252 | 253 | 1652 | 313 | 2052 | 13 | - 52 | 13 | 0.867 |
| 14 | - 56 | 74 | 456 | I 34 | 856 | 194 | 1256 | 254 | 1656 | 314 | 2056 | 14 | - 56 | 14 | 0.933 |
| 15 | I 0 | 75 | 5 o | 135 | 9 o | 195 | I3 0 | 255 | 17 o | 315 | 210 | 15 | 10 | 15 | 1.000 |
| 16 | I 4 | 76 | 54 | 136 | 94 | 196 | I3 4 | 256 | I7 4 | 316 | 214 | 16 | I 4 | 16 | 1.067 |
| 17 | 18 | 77 | 58 | 137 | 98 | 197 | 138 | 257 | 178 | 317 | 218 | 17 | I 8 | 17 | I. 133 |
| 18 | 112 | 78 | 5 I 2 | 138 | 912 | 198 | 13 I2 | 258 | 1712 | 318 | 2112 | 18 | 112 | 18 | I. 200 |
| 19 | 116 | 79 | 516 | 139 | 916 | 199 | 1316 | 259 | 1716 | 319 | 2116 | 19 | 116 | 19 | 1.267 |
| 20 | 120 | 80 | 520 | 140 | 920 | 200 | 1320 | 260 | 1720 | 320 | 2120 | 20 | 120 | 20 | 1.333 |
| 2 | 124 | 81 | 524 | 141 | 924 | 201 | 13 | 261 | 1724 | 32 I | 21 24 | 2 I | 24 | 2 I | I. 400 |
| 22 | I 28 | 82 | 528 | 142 | 928 | 202 | 1328 | 262 | 1728 | 322 | 2128 | 22 | I 28 | 22 | 1.467 |
| 23 | 132 | 83 | 532 | 143 | 932 | 203 | I3 32 | 263 | 1732 | 323 | 2132 | 23 | 132 | 23 | 1.533 |
| 24 | 136 | 8 | 536 | 144 | 936 | 204 | I3 36 | 264 | 1736 | 324 | 2136 | 24 | I 36 | 24 | 1.600 |
| 25 | 140 | 85 | 540 | 145 | 940 | 205 | I3 40 | 265 | 1740 | 325 | 2140 | 25 | I 40 | 25 | 1.667 |
| 26 | I 44 | 86 | 544 | 146 | 944 | 206 | I3 44 | 266 | 1744 | 326 | 2I 44 | 26 | I 44 | 26 | 1.733 |
| 27 | 148 | 87 | 548 | 147 | 948 | 207 | I3 48 | 267 | 1748 | 327 | 2148 | 27 | 148 | 27 | 1.800 |
| 28 | I 52 | 88 | 552 | 148 | 952 | 208 | I3 52 | 268 | 1752 | 328 | 2I 52 | 28 | I 52 | 28 | 1. 867 |
| 29 | 1 56 | 89 | 556 | 149 | 956 | 209 | 1356 | 269 | 1756 | 329 | 2156 | 29 | I 56 | 29 | 1.933 |
| 30 |  | 90 | $6 \quad 0$ | 150 | $10 \quad 0$ | 210 | 14 0 | 270 | 18 o | 330 | 220 | 30 | 2 | 30 | 2.000 |
| 31 | 24 | 91 | 6 4 | 151 | 104 | 2 II | 144 | 271 | 184 | 331 | 22 | 31 |  | 31 | 2.067 |
| 32 | 28 | 92 | 68 | 152 | Io 8 | 212 | 148 | 72 | 18 8 | 332 | 22 | 32 | 2 | 32 | 2.133 |
| 33 | 212 | 93 | 612 | 153 | 1012 | 213 | 1412 | 273 | 1812 | 333 | 2212 | 33 | 212 | 33 | 2.200 |
| 34 | 216 | 94 | 616 | 154 | 1016 | 214 | 1416 | 274 | I8 16 | 334 | 2216 | 34 | 216 | 34 | 2.267 |
| 35 | 220 | 95 | 620 | 155 | Io | 215 | 1420 | 275 | I8 20 | 335 | 2220 | 35 | 2 | 35 | 2.333 |
| 36 | 224 | 96 | 624 | 156 | Io 24 | 216 | 1424 | 276 | I8 24 | 336 | 2224 | 36 | 224 | 36 | 2.400 |
| 37 | 228 | 97 | 628 | 157 | 10 | 217 | 1428 | 277 | I8 28 | 337 | 2228 | 37 | 228 | 37 | 2.467 |
| 38 | 232 | 98 | 632 | 158 | 1032 | 21 | 1432 | 278 | 1832 | 338 | 2232 | 38 | 232 | 38 | 2.533 |
| 39 | 236 | 99 | 636 | 159 | 10 36 | 219 | 1436 | 279 | 1836 | 339 | 2236 | 39 | 236 | 39 | 2.600 |
| 40 | 240 | 100 | 640 | 160 | 1040 | 22 | 1440 | 280 | 1840 | 340 | 2240 | 40 | 240 | 40 | 2.667 |
| 41 | 244 | IOI | 644 | 161 | IO 44 | 221 | 1444 | 281 | I8 44 | 341 | 2244 | 4 | 244 | 41 | 2.733 |
| 42 | 248 | 102 | 648 | 162 | 1o 48 | 222 | I4 48 | 282 | 1848 | 342 | 2248 | 42 | 248 | 42 | 2.800 |
| 43 | 252 | 103 | 652 | 163 | 1052 | 223 | 1452 | 283 | 1852 | 343 | 2252 | 43 | 252 | 43 | 2.867 |
| 45 | 256 | 104 | 656 | 164 | Io 56 | 224 | 1456 | 284 | 1856 | 345 | 2256 | 44 | 256 | 44 | 2.933 |
| 45 | 3 3 | 105 | 7 0 | 165 | II 0 | 225 | 150 | 285 | 190 | 345 | 230 | 45 | 3 0 | 45 | 3.000 |
| 46 | 3 | 106 | $7 \begin{array}{ll}7 & 4\end{array}$ | 166 | II 4 | 226 | I5 4 | 286 | I9 4 | 346 | 234 | 46 | 3 | 46 | 3.067 |
| 47 | 38 | 107 | 78 | 167 | II 8 | 227 | I5 8 | 287 | 198 | 347 | 238 | 47 | 38 | 47 | 3. I33 |
| 48 | $\begin{array}{ll}312 \\ 3 & 16\end{array}$ | 108 | 712 | 168 | II 12 | 228 | 1512 | 288 | 19 I2 | 348 | 2312 | 48 | 312 | 48 | 3.200 |
| 49 | 316 | 109 | 716 | 169 | II 16 | 229 | 1516 | 289 | 19 I6 | 349 | 2316 | 49 | 316 | 49 | 3.267 |
| 50 | 320 | 110 | 720 | 170 | II 20 | 230 | 1520 | 290 | 1920 | 350 | 2320 | 50 | 320 | 50 | $3 \cdot 333$ |
| 51 | 324 | III | 724 | 171 | II 24 | 231 | I5 24 | 291 | 1924 | 351 | 2324 | 51 | 324 | 51 | 3.400 |
| 52 | 328 | 112 | 728 | 172 | II 28 | 232 | 1528 | 292 | 1928 | 352 | 2328 | 52 | 328 | 52 | 3.467 |
| 53 | 332 | II3 | 732 | 173 | II 32 | 233 | 1532 | 293 | 1932 | 353 | 2332 | 53 | 332 | 53 | 3.533 |
| 54 | 336 | 114 | 736 | 174 | II 36 | 234 | I5 36 | 294 | I9 36 | 354 | 2336 | 54 | 336 | 54 | 3.600 |
| 55 | 340 | 115 | 740 | 175 | II 40 | 235 | 1540 | 295 | 1940 | 355 | 2340 | 55 | 340 | 55 | 3.667 |
| 56 | 344 | II6 | 744 | 176 | II 44 | 236 | 1544 | 296 | 1944 | 356 | 2344 | 56 | 344 | 56 | 3.733 |
| 57 | 348 | 117 | 748 | 177 | II 48 | 237 | 1548 | 297 | 1948 | 357 | 2348 | 57 | 348 | 57 | 3.800 |
| 58 59 | 3 3 3 5 | II8 | 752 | 178 | II 52 | 238 | 1552 | 298 | I9 52 | 358 | 2352 | 58 | 352 <br> 3 | 58 | 3.867 |
| $\frac{59}{60}$ | 356 | I19 | 756 | 179 | 1156 | 239 | 1556 | 299 | 1956 | 359 | 2356 | 59 | 356 | 59 | 3.933 |
| 60 | 40 | 120 | 8 o | 180 | 12 O | 240 | 16 0 | 300 | 20 0 | 360 | 24 O | 60 | 40 | 60 | 4.000 |

TABLE 73.
TIME INTO ARC.

Hours into Arc.

| Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| hrs. | - | hrs. | - | hrs. | - | hrs. | - | hrs. | - | hrs. | - |
| 1 | 15 | 5 | 75 | 9 | 135 | 13 | 195 | 17 | 255 | 21 | 315 |
| 2 | 30 | 6 | 90 | 10 | 150 | 14 | 210 | 18 | 270 | 22 | 330 |
| 3 | 45 | 7 | 105 | 11 | 165 | 15 | 225 | 19 | 285 | 23 | 345 |
| 4 | 60 | 8 | 120 | 12 | 180 | 16 | 240 | 20 | 300 | 24 | 360 |

Minutes of Time into Arc.
Seconds of Time into Arc.

| m. | $\bigcirc 1$ | m. | - , | m. | $\bigcirc 1$ | s. | , /1 | S | /1 | s. | 1 | 11 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | - I5 | 21 | 515 | 41 | 10 I5 | 1 | - 15 | 21 | 515 | 41 | 10 | 15 |
| 2 | - 30 | 22 | 530 | 42 | 1030 | 2 | - 30 | 22 | 530 | 42 | 10 | 30 |
| 3 | - 45 | 23 | 545 | 43 | IO 45 | 3 | - 45 | 23 | 545 | 43 | 10 | 45 |
| 4 | I 0 | 24 | 60 | 44 | II 0 | 4 | I 0 | 24 | 6 0 | 44 | II | 0 |
| 5 | I 15 | 25 | 6 I5 | 45 | 1115 | 5 | I 15 | 25 | 615 | 45 | II | 15 |
| 6 | I 30 | 26 | 630 | 46 | II 30 | 6 | I 30 | 26 | 630 | 46 | II | 30 |
| 7 | I 45 | 27 | 645 | 47 | II 45 | 7 | I 45 | 27 | 645 | 47 | II | 45 |
| 8 | 20 | 28 | 7 0 | 48 | 120 | 8 | 20 | 28 | 7 0 | 48 | 12 | 0 |
| 9 | 2 I5 | 29 | 715 | 49 | 12 I 5 | 9 | 2 I5 | 29 | 715 | 49 | 12 | 15 |
| 10 | 230 | 30 | 730 | 50 | 1230 | 10 | 230 | 30 | 730 | 50 | 12 | 30 |
| II | 245 | 3 I | 745 | 5I | 1245 | II | 245 | 31 | 745 | 5 I | 12 | 45 |
| 12 | 30 | 32 | 8 0 | 52 | 130 | 12 | 30 | 32 | 8 o | 52 | 13 | 0 |
| I3 | 3 I5 | 33 | 8 I5 | 53 | 13 I5 | 13 | 3 I5 | 33 | 8 I5 | 53 | 13 | 15 |
| 14 | $3 \quad 30$ | 34 | 830 | 54 | I3 30 | 14 | 330 | 34 | 830 | 54 | I3 | 30 |
| 15 | 345 | 35 | 845 | 55 | I3 45 | 15 | 345 | 35 | 845 | 55 | 13 | 45 |
| 16 | 40 | 36 | 90 | 56 | 14 O | 16 | 40 | 36 | 90 | 56 | 14 | 0 |
| 17 | 4 I5 | 37 | 9 I5 | 57 | 1415 | 17 | 4 I5 | 37 | 915 | 57 | 14 | 15 |
| 18 | 430 | 38 | 930 | 58 | 1430 | 18 | 430 | 38 | 930 | 58 | 14 | 30 |
| 19 | 445 | 39 | 945 | 59 | 1445 | 19 | 445 | 39 | 945 | 59 | 14 | 45 |
| 20 | 5 ○ | 40 | 10 0 | 60 | 150 | 20 | 50 | 40 | 100 | 60 | 15 | 0 |

Hundredths of a Second of Time into Arc.

| Hundredths of a Second of Time. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { s. } \\ 0.00 \end{gathered}$ | ó.00 | O.15 | 0.10 | 0.10 | \% 0.60 | 0.75 | 0.190 | 1.05 | I'120 | I. 35 |
| .10 | 1.50 | 1.65 | 1.30 1.80 | 0.45 1.95 | 2.10 | 0.75 2.25 | 0.90 2.40 | 1.05 2.55 | 1.20 2.70 | 1.35 2.85 |
| . 20 | 3.00 | 3.15 | 3.30 | 3.45 | 3.60 | 3.75 | 3.90 | 4.05 | 4.20 | 4.35 |
| . 30 | 4.50 | 4.65 | 4.80 | 4.95 | 5.10 | 5.25 | 5.40 | 5.55 | 5.70 | 5.85 |
| . 40 | 6.00 | 6.15 | 6.30 | 6.45 | 6.60 | 6.75 | 6.90 | 7.05 | 7.20 | $7 \cdot 35$ |
| 0.50 | 7.50 | 7.65 | 7.80 | 7.95 | 8.10 | 8.25 | 8.40 | 8.55 | 8.70 | 8.85 |
| . 60 | 9.00 | 9.15 | 9.30 | 9.45 | 9.60 | 9.75 | 9.90 | 10.05 | 10.20 | 10.35 |
| . 70 | 10.50 | 10.65 | 10.80 | 10.95 | II.10 | II. 25 | II. 40 | II. 55 | 11.70 | II. 85 |
| . 80 | 12.00 | 12.15 | 12.30 | 12.45 | 12.60 | 12.75 | 12.90 | 13.05 | 13.20 | 13.35 |
| . 90 | 13.50 | 13.65 | 13.80 | 13.95 | 14.10 | 14.25 | 14.40 | 14.55 | 14.70 | 14.85 |

Smithsonian Tableg.

Table 74.

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | Decimal of a Year. | Angle. | Day of | Month. | $\begin{aligned} & \text { Day } \\ & \text { of } \\ & \text { Year. } \end{aligned}$ | Decimal <br> a Year. | Angle. | Day of Month. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Common Year. | Bissextile Year. |  |  |  | Common Year. | Bissextile Year. |
| 1 | 0.00000 | $0^{\circ} \mathrm{o}^{\prime}$ | Jan. I | Jan. 1 | 51 | 0.13689 | $49^{\circ} 17^{\prime}$ | Feb. 20 | Feb. 20 |
| 2 | . 00274 | - 59 |  |  | 52 | . 13963 | 5016 | 2 I | 21 |
| 3 | . 00548 | I 58 | 3 | 3 | 53 | . 14237 | 5115 | 22 | 22 |
| 4 | . 00821 | 257 | 4 | 4 | 54 | . 14511 | 5214 | 23 | 23 |
| 5 | 0.01095 | 357 | 5 | 5 | 55 | 0.14784 | 5313 | 24 | 24 |
| 6 | .01369 | 456 | 6 | 6 | 56 | . 15058 | 54 I3 | 25 | 25 |
| 7 | . 01643 | 555 | 7 | 7 | 57 | . 15332 | 5512 | 26 | 26 |
| 8 | .01916 | 654 | 8 | 8 | 58 | . 15606 | 56 II | 27 | 27 |
| 9 | .02190 | 753 | 9 | 9 | 59 | . 15880 | 57 10 | 28 | 28 |
| 10 | 0.02464 | 852 | 10 | 10 | 60 | 0.16I53 | 589 | Mar. 1 | 29 |
| 11 | . 02738 | 95 I | 11 | II | 6I | . 16427 | 598 |  | Mar. 1 |
| 12 | .03011 | 10 51 | 12 | 12 | 62 | . 16701 | 607 | 3 | 2 |
| I3 | . 03285 | II 50 | 13 | 13 | 63 | . 16975 | 617 | 4 | 3 |
| 14 | . 03559 | 1249 | 14 | 14 | 64 | . 17248 | 626 | 5 | 4 |
| 15 | 0.03833 | 1348 | 15 | 15 | 65 | 0. 17522 | 635 | 6 | 5 |
| 16 | .04107 | 1447 | 16 | 16 | 66 | . 17796 | 644 | 7 | 6 |
| 17 | .0438I | 1546 | 17 | 17 | 67 | . 18070 | 65 | 8 | 7 |
| 18 | . 04654 | 1645 | 18 | 18 | 68 | . 18344 | 662 | 9 | 8 |
| 19 | . 04928 | 1744 | 19 | 19 | 69 | .186I7 | 67 I | 10 | 9 |
| 20 | 0.05202 | I8 44 | 20 | 20 | 70 | 0.18891 | 68 o | II | 10 |
| 21 | . 05476 | 1943 | 21 | 21 | 71 | .19165 | 69 - | 12 | II |
| 22 | . 05749 | 2042 | 22 | 22 | 72 | . 19439 | 6959 | 13 | 12 |
| 23 | . 06023 | 2141 | 23 | 23 | 73 | .19713 | 7058 | 14 | 13 |
| 24 | . 06297 | 2240 | 24 | 24 | 74 | . 19986 | 7157 | 15 | 14 |
| 25 | 0.06571 | 2339 | 25 | 25 | 75 | 0.20260 | 7256 | 16 | 15 |
| 26 | . 06845 | 2438 | 26 | 26 | 76 | . 20534 | 7355 | 17 | 16 |
| 27 | . 07118 | 2538 | 27 | 27 | 77 | . 20808 | 7454 | I8 | 17 |
| 28 | . 07392 | 2637 | 28 | 28 | 78 | . 2108I | 7554 | 19 | 18 |
| 29 | . 07666 | 2736 | 29 | 29 | 79 | . 21355 | 7653 | 20 | 19 |
| 30 | 0.07940 | $28 \quad 35$ | 30 | 30 | 80 | 0.21629 | 7752 | 2 I | 20 |
| 31 | . 08214 | 2934 | 31 | 3 I | 81 | . 21903 | 78 51 | 22 | 21 |
| 32 | . 08487 | 3033 | Feb. I | Feb. 1 | 82 | . 22177 | 7950 | 23 | 22 |
| 33 | . 08761 | 3132 |  | 2 | 83 | . 22450 | 8049 | 24 | 23 |
| 34 | . 09035 | 3232 | 3 | 3 | 84 | . 22724 | 81 48 | 25 | 24 |
| 35 | 0.09309 | 33 31 | 4 | 4 | 85 | 0.22998 | 8248 | 26 | 25 |
| 36 | . 09582 | 3430 | 5 | 5 | 86 | . 23272 | 8347 | 27 | 26 |
| 37 | . 09856 | $35 \quad 29$ | 6 | 6 | 87 | . 23546 | 8446 | 28 | 27 |
| 38 | . IOI30 | 3628 | 7 | 7 | 88 | .23819 | 8545 | 29 | 28 |
| 39 | . 10404 | $37 \quad 27$ | 8 | 8 | 89 | . 24093 | 8644 | 30 | 29 |
| 40 | 0. 10678 | 3826 | 9 | 9 | 90 | 0.24367 | 8743 | $3^{31}$ | 30 |
| 41 | .1095I | 3926 | 10 | Io | 91 | . 24641 | 8842 | Apr. 1 | 31 |
| 42 | . 11225 | 4025 | II | II | 92 | . 24914 | 8942 |  | Apr. ${ }^{1}$ |
| 43 | . 11499 | 41 | 12 | 12 | 93 | .25188 | 9041 | 3 | 2 |
| 44 | . 11773 | 4223 | 13 | 13 | 94 | . 25462 | 9140 | 4 | 3 |
| 45 | 0.12047 | 4322 | 14 | 14 | 95 | $0.25736^{\circ}$ | 9239 | 5 | 4 |
| 46 | . 12320 | 44 21 | 15 | 15 | 96 | . 26010 | $93 \quad 38$ | 6 | 5 |
| 47 | . 12594 | 4520 | 16 | 16 | 97 | . 26283 | 9437 | 7 | 6 |
| 48 | . 12868 | 46 I9 | 17 | 17 | 98 | . 26557 | 9536 | 8 | 7 |
| 49 | . 13142 | 47 19 | 18 | 18 | 99 | . 2683 I | 9635 | 9 | 8 |
| 50 | 0.13415 | $48 \quad 18$ | 19 | 19 | 100 | 0.27105 | 9735 | 10 | 9 |

Emithsonian Tables.

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | Decimal of a Year. | Angle. | Day of Month. |  | $\begin{aligned} & \text { Day } \\ & \text { of } \\ & \text { Year. } \end{aligned}$ | Decimal of a Year. | Angle. | Day of Month. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Common Year. | Bissextile Year. |  |  |  | Common Year. | Bissextile Year. |
| 101 | 0.27379 | $98^{\circ} 34^{\prime}$ | Apr. 11 | Apr. 10 | 151 | 0.41068 | $147^{\circ} 51^{\prime}$ | May 3I | May 30 |
| 102 | . 27652 | 9933 | 12 | II | 152 | . 41342 | 14850 | June 1 | $3 I$ |
| 103 | . 27926 | IOO 32 | I3 | 12 | I 53 | .416I5 | 14949 |  | June I |
| 104 | . 28200 | IOI 3I | 14 | 13 | 154 | .41889 | 15048 | 3 | 2 |
| 105 | 0.28474 | 10230 | 15 | 14 | 155 | 0.42163 | 15147 | 4 | 3 |
| 106 | . 28747 | 10329 | 16 | 15 | 156 | . 42437 | 15246 | 5 | 4 |
| 107 | . 2902 I | 10429 | 17 | 16 | 157 | . 42710 | I53 45 | 6 | 5 |
| 108 | . 29295 | 10528 | 18 | 17 | 158 | . 42984 | 154 45 | 7 | 6 |
| 109 | . 29569 | 10627 | 19 | 18 | 159 | . 43258 | I5544 | 8 | 7 |
| 110 | 0.29843 | 10726 | 20 | 19 | 160 | 0.43532 | 15643 | 9 | 8 |
| III | . 30116 | 108 25 | 21 | 20 | 161 | . 43806 | 15742 | 10 | 9 |
| II 2 | . 30390 | 10924 | 22 | 2 I | 162 | . 44079 | 1584 I | II | IO |
| II3 | - 30664 | IIO 23 | 23 | 22 | 163 | . 44353 | I59 40 | 12 | II |
| II4 | - 30938 | III 23 | 24 | 23 | 164 | . 44627 | 160 39 | 13 | 12 |
| 115 | 0.31211 | 11222 | 25 | 24 | 165 | 0.44901 | 161 39 | 14 | 13 |
| 116 | . 31485 | II3 2I | 26 | 25 | 166 | . 45175 | 16238 | 15 | 14 |
| 117 | -31759 | II4 20 | 27 | 26 | 167 | . 45448 | 16337 | 16 | I5 |
| 118 | - 32033 | 11519 | 28 | 27 | 168 | . 45722 | 16436 | 17 | 16 |
| 119 | . 32307 | 11618 | 29 | 28 | 169 | . 45996 | 16535 | 18 | 17 |
| 120 | 0.32580 | 11717 | 30 | 29 | 170 | 0.46270 | 16634 | 19 | 18 |
| 121 | . 32854 | 11817 | May I | 30 | 17 ! | . 46543 | 16733 | 20 | 19 |
| 122 | . 33128 | 11916 | 2 | May I | 172 | .46817 | 16833 | 21 | 20 |
| 123 | -33402 | 12015 | 3 |  | 173 | .47091 | 169 32 | 22 | 21 |
| 124 | -3.3676 | 12114 | 4 | 3 | 174 | . 47365 | 17031 | 23 | 22 |
| 125 | 0.33949 | 122 I3 | 5 | 4 | 175 | 0.47639 | 17130 | 24 | 23 |
| 126 | . 34223 | 12312 | 6 | 5 | 176 | . 47912 | 17229 | 25 | 24 |
| 127 | - 34497 | 124 II | 7 | 6 | 177 | . 48186 | 17328 | 26 | 25 |
| 128 | -34771 | 12510 | 8 | 7 | 178 | . 48460 | 17427 | 27 | 26 |
| 129 | -35044 | 126 IO | 9 | 8 | 179 | . 48734 | 17526 | 28 | 27 |
| 130 | 0.35318 | 1279 | IO | 9 | 180 | 0.49008 | 17626 | 29 | 28 |
| 131 | . 35592 | 1288 | II | IO | 181 | . 4928 I | 17725 | 30 | 29 |
| 132 | . 35866 | 1297 | 12 | 11 | 182 | . 49555 | 17824 | July 1 | $3^{30}$ |
| 133 | -36140 | 1306 | I3 | 12 | 183 | . 49829 | 17923 |  | July 1 |
| 134 | . 36413 | 1315 | 14 | I3 | 184 | . 50103 | 180 22 | 3 | 2 |
| 135 | 0.36687 | 1324 | 15 | 14 | 185 | 0.50376 | 181 21 | 4 | 3 |
| 136 | . 36961 | I33 4 | 16 | 15 | 186 | . 50650 | 18220 | 5 | 4 |
| 137 | . 37235 | 1343 | 17 | 16 | 187 | . 50924 | 18320 | 6 | 5 |
| 138 | . 37509 | 1352 | 18 | 17 | 188 | -51198 | 18419 | 7 | 6 |
| 139 | . 37782 | 136 I | 19 | 18 | I89 | . 51472 | 18518 | 8 | 7 |
| 140 | 0.38056 | 137 0 | 20 | 19 | 190 | 0.51745 | 18617 | 9 | 8 |
| 141 | . 38330 | 13759 | 21 | 20 | 191 | . 52019 | 18716 | 10 | 9 |
| 142 | . 38604 | I38 58 | 22 | 21 | 192 | . 52293 | 188 I5 | II | 10 |
| 143 | - 38877 | 13958 | 23 | 22 | 193 | . 52567 | 18914 | 12 | II |
| 144 | -3915I | 14057 | 24 | 23 | 194 | . 52841 | 19014 | 13 | 12 |
| 145 | 0.39425 | 141 56 | 25 | 24 | 195 | 0.53114 | I91 I3 | 14 | 13 |
| 146 | . 39699 | 14255 | 26 | 25 | 196 | . 53388 | 192 I2 | 15 | 14 |
| 147 | . 39973 | 14354 | 27 | 26 | 197 | . 53662 | 193 II | 16 | 15 |
| 148 | . 40246 | 14453 | 28 | 27 | 198 | . 53936 | 194 10 | 17 | 16 |
| 149 | . 40520 | 14552 | 29 | 28 | 199 | . 54209 | 1959 | 18 | 17 |
| 150 | 0.40794 | 14651 | 30 | 29 | 200 | 0.54483 | 196 8 | 19 | 18 |

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{array}{\|c} \text { Day } \\ \text { of } \\ \text { Year. } \end{array}$ | $\begin{aligned} & \text { Decimal } \begin{array}{c} \text { af } \\ \text { a Year. } \end{array} . \end{aligned}$ | Angle. | Day of Month. |  | $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | Decimal of a Year. | Angle. | Day of Month. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { Common } \\ & \text { Year. } \end{aligned}$ | $\begin{aligned} & \text { Bissextile } \\ & \text { Year. } \end{aligned}$ |  |  |  | Common Year. | Bissextile Year. |
| 201 | 0.54757 | $197^{\circ} 8^{\prime}$ | July 20 | July 19 | 251 | 0.68446 | $246^{\circ} 24^{\prime}$ | Sept. 8 | Sept. 7 |
| 202 | . 55031 | 1987 | 21 | 20 | 252 | . 68720 | 24724 | 9 | 8 |
| 203 | - 55305 | 1996 | 22 | 21 | 253 | . 68994 | 24823 | 10 | 9 |
| 204 | - 55578 | 2005 | 23 | 22 | 254 | . 69268 | 24922 | II | Iо |
| 205 | 0.55852 | 2014 | 24 | 23 | 255 | 0.69541 | 25021 | 12 | II |
| 206 | . 56126 | 2023 | 25 | 24 | 256 | . 69815 | 25120 | 13 | 12 |
| 207 | . 56400 | 2032 | 26 | 25 | 257 | . 70089 | 25219 | 14 | 13 |
| 208 | . 56674 | 204 I | 27 | 26 | 258 | . 70363 | 25318 | 15 | 14 |
| 209 | . 56947 | 205 I | 28 | 27 | 259 | . 70637 | 25417 | 16 | 15 |
| 210 | 0.57221 | 206 o | 29 | 28 | 260 | 0.70910 | 25517 | 17 | 16 |
| 2 II | . 57495 | 20659 | 30 | 29 | 261 | .71184 | 25616 | 18 | 17 |
| 212 | . 57769 | 20758 | 3 I | 30 | 262 | . 71458 | 25715 | 19 | 18 |
| 213 | . 58042 | 20857 | Aug. 1 | 31 | 263 | . 71732 | 258 I4 | 20 | 19 |
| 214 | . 58316 | 20956 | 2 | Aug. 1 | 264 | . 72005 | 259 I3 | 21 | 20 |
| 215 | 0.58590 | 21055 | 3 | 2 | 265 | 0.72279 | 26012 | 22 | 21 |
| 216 | . 58864 | 2 II 55 | 4 | 3 | 266 | . 72553 | 26I II | 23 | 22 |
| 217 | . 59138 | 21254 | 5 | 4 | 267 | . 72827 | 262 II | 24 | 23 |
| 218 | -59411 | 21353 | 6 | 5 | 268 | .73101 | 263 Io | 25 | 24 |
| 219 | - 59685 | 21452 | 7 | 6 | 269 | . 73374 | 2649 | 26 | 25 |
| 220 | 0.59959 | 215 51 | 8 | 7 | 270 | 0.73648 | 2658 | 27 | 26 |
| 221 | . 60233 | 21650 | 9 | 8 | 271 | . 73922 | 2667 | 28 | 27 |
| 222 | . 60507 | 21749 | 10 | 9 | 272 | .74196 | 2676 | 29 | 28 |
| 223 | .60780 | 21849 | II | 10 | 273 | . 74470 | 2685 | - 30 | 29 |
| 224 | .61054 | 21948 | 12 | II | 274 | . 74743 | 2695 | Oct. | 30 |
| 225 | 0.61328 | 22047 | 13 | 12 | 275 | 0.75017 | 2704 | 2 | Oct. I |
| 226 | .61602 | 221 46 | 14 | 13 | 276 | . 75291 | 271 | 3 | 2 |
| 227 | .61875 | 22245 | 15 | 14 | 277 | . 75565 | 2722 | 4 | 3 |
| 228 | . 62149 | 22344 | 16 | 15 | 278 | . 75838 | 273 I | 5 | 4 |
| 229 | . 62423 | 22443 | 17 | 16 | 279 | .76112 | 274 o | 6 | 5 |
| 230 | 0.62697 | 22543 | 18 | 17 | 280 | 0.76386 | 27459 | 7 | 6 |
| 231 | .62971 | 22642 | 19 | 18 | 281 | . 76660 | 27559 | 8 | 7 |
| 232 | . 63244 | 227 41 | 20 | 19 | 282 | . 76934 | 27658 | 9 | 8 |
| 233 | . 63518 | 22840 | 21 | 20 | 283 | . 77207 | 27757 | Io | 9 |
| 234 | . 63792 | 22939 | 22 | 21 | 284 | .7748I | 27856 | 11 | то |
| 235 | 0.64066 | 23038 | 23 | 22 | 285 | 0.77755 | 27955 | 12 | 11 |
| 236 | . 64339 | 23137 | 24 | 23 | 286 | . 78029 | 28054 | 13 | 12 |
| 237 | . 64613 | 23236 | 25 | 24 | 287 | . 78303 | 281 53 | 14 | 13 |
| 238 | . 64887 | 23336 | 26 | 25 | 288 | . 78576 | 28252 | 15 | 14 |
| 239 | .6516r | 23435 | 27 | 26 | 289 | . 78850 | 28352 | 16 | 15 |
| 240 | 0.65435 | 23534 | 28 | 27 | 290 | 0.79124 | 28451 | 17 | 16 |
| 241 | . 65708 | 23633 | 29 | 28 | 291 | . 79398 | 28550 | 18 | 17 |
| 242 | . 65982 | 23732 | 30 | 29 | 292 | . 7967 I | 28649 | 19 | 18 |
| 243 | . 66256 | 23831 | 3 I | 30 | 293 | . 79945 | 28748 | 20 | 19 |
| 244 | . 66530 | 23930 | Sept. 1 | 31 | 294 | . 80219 | 28847 | 2 I | 20 |
| 245 | 0.66804 | 24030 | 2 | Sept. I | 295 | 0.80493 | 28946 | 22 | 2 I |
| 246 | . 67077 | 24129 | 3 | 2 | 296 | . 80767 | 29046 | 23 | 22 |
| 247 | . 6735 I | 24228 | 4 | 3 | 297 | . 81040 | 291 45 | 24 | 23 |
| 248 | . 67625 | 24327 | 5 | 4 | 298 | . 81314 | 29244 | 25 | 24 |
| 249 | . 67899 | 24426 | 6 | 5 | 299 | . 81588 | 29343 | 26 | 25 |
| 250 | 0.68172 | 24525 | 7 | 6 | 300 | 0.81862 | 29442 | 27 | 26 |

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{aligned} & \text { Day } \\ & \text { of } \\ & \text { Year. } \end{aligned}$ | Decimal of a Year. | Angle. | Day of Month. |  | $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ |  | Angle | Day of Month. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Common Year | Bissextile Year. |  |  |  |  | Common Year. | Bissextile Year. |
| 301 | 0.82136 | $295{ }^{\circ} 4 \mathrm{I}^{\prime}$ | Oct. 28 | Oct. 27 | 351 | 0.95825 | $344^{\circ}$ | $8{ }^{\prime}$ | Dec. 17 | Dec. 16 |
| 302 | . 82409 | 29640 |  | 28 | 352 | . 96099 | 345 |  | 18 |  |
| 303 | . 82683 | 29740 | 30 | 29 | 353 | . 96372 | 346 |  | 19 | 18 |
| 304 | . 82957 | 29839 | 3 I | 30 | 354 | . 96646 | 347 |  | 20 | 19 |
| 305 | 0.83231 | 29938 | Nov. I | -31 | 355 | 0.96920 | 348 |  | 21 | 20 |
| 306 | . 83504 | 30037 | 2 | Nov. 1 | 356 | .97194 | 3495 | 4 | 22 | 21 |
| 307 | . 83778 | 30136 | 3 | 2 | 357 | . 97467 | 350 | 3 | 23 | 22 |
| 308 | . 84052 | 30235 | 4 | 3 | 358 | .9774I | 351 | 2 | 24 | 23 |
| 309 | . 84326 | 30334 | 5 | 4 | 359 | .98015 | 352 |  | 25 | 24 |
| 310 | 0.84600 | 30434 | 6 | 5 | 360 | 0.98289 | 353 |  | 26 | 25 |
| 3 II | . 84873 | 30533 | 7 | 6 | 361 | . 98563 | 354 |  | 27 | 26 |
| 312 | . 85147 | 30632 | 8 | 7 | 362 | . 98836 | 355 |  | 28 | 27 |
| 3 I 3 | . 8542 I | 30731 | 9 | 8 | 363 | .9910 | 356 |  | 29 | 28 |
| 314 | . 85695 | 30830 | 10 | 9 | 364 | . 99384 | 357 |  | 30 | 29 |
| 315 | 0.85969 | 30929 | II | 10 |  | 0.99658 | 358 |  | 31 | 30 |
| 316 | . 86242 | 31028 | 12 | II | 366 | . 99932 | 359 |  |  | 3 I |
| 317 | . 86516 | 3 II 27 | 13 | 12 |  |  |  |  |  |  |
| 318 | . 86790 | 31227 | 14 | 13 |  |  |  |  |  |  |
| 319 | . 87064 | 31326 | 15 | 14 | Conv | ersion for | ours. | Conv | version for | Minutes. |
| 320 | 0.87337 | 31425 | 16 | 15 |  |  |  |  |  |  |
| 321 | . 87611 | 315 316 | 17 | 16 | Hrs. | Dec. of Year. | Angle. | Min. | Dec. of | Angle. |
| 322 | . 87885 | 31623 | 18 | 17 |  |  |  |  |  |  |
| 323 | . 88159 | 31722 | 19 | 18 |  |  |  |  |  |  |
| 324 | . 88433 | 3 I 8 2I | 20 | 19 | I | 0.00011 | 2.5 | 1 | 0.00000 | 0.04 |
| 325 | 0.88706 | 319 2I | 21 | 20 | 2 | 23 | 4.9 | 2 | 0 | . 08 |
| 326 | . 88980 | 32020 | 22 | 2 I | 3 | 34 | 7.4 | 3 | I | . 12 |
| 327 | . 89254 | 32119 | 23 | 22 | 4 | 46 | 9.9 | 4 | I | . 16 |
| 328 | . 89528 | 322 18 | 24 | 23 |  |  |  | 5 |  |  |
| 329 | . 89802 | 32317 | 25 | 24 | 6 | $\begin{gathered} 57 \\ 68 \end{gathered}$ | 12.3 | 6 | 0.00001 | 0.21 .25 |
| 330 | 0.90075 | 32416 | 26 | 25 | 7 | 80 | 17.2 | 7 | I | . 29 |
| 331 | . 90349 | 32515 | 27 | 26 | 8 | 91 | 19.7 | 8 | 2 | . 33 |
| 332 | . 90623 | 32615 | 28 | 27 | 9 | 103 | 22.2 | 9 | 2 | . 37 |
| 333 | -90897 | 32714 | 29 | 28 |  |  |  |  |  |  |
| 334 | .91170 | 32813 | 30 | 29 | 10 | 0.00114 | 24.6 | 10 | 0.00002 | 0.41 |
| 335 |  |  | Dec. 1 |  | II | 126 | 27.1 | 20 | - 4 | . 82 |
|  | 0.91444 .91718 | 329 I2 330 | Dec. 1 | Dec. ${ }^{30}$ | 12 | 137 | 29.6 | 30 | 6 | 1.23 |
| 336 | -91718 | 330 II | 2 | Dec. 1 | I3 | 148 | 32.0 | 40 | 8 | 1.64 |
| 337 | .91992 | 33110 | 3 | 2 | 14 | 160 | 34.5 | 50 | 10 | 2.05 |
| 338 | . 92266 | 3329 | 4 | 3 |  |  |  |  |  |  |
| 339 | . 92539 | 3339 | 5 | 4 | 15 | 0.00171 | 37.0 | 60 | 0.00011 | 2.46 |
| 340 | 0.92813 | 3348 | 6 |  | 16 | 183 | 39.4 |  |  |  |
| 341 | . 93087 | 335 | 7 | 6 | I7 | 194 | 41.9 |  |  |  |
| 342 | . 93361 | 3366 | 8 | 7 | 18 | 2 5 | 44.4 |  |  |  |
| 343 | . 93634 | 3375 | 9 | 8 | 19 | 217 | 46.8 |  |  |  |
| 344 | . 93908 | 3384 | 10 | 9 | 20 | 0.00228 | 49.3 |  |  |  |
| 345 | 0.94182 | 3393 | II | Io | 21 | 240 | 51.7 |  |  |  |
| 346 | . 94456 | 3402 | 12 | II | 22 | 251 | 54.2 |  |  |  |
| 347 | . 94730 | 34 I 2 | 13 | 12 | 23 | 262 | 56.7 |  |  |  |
| 348 | . 95003 | 342 I | 14 | 13 | 24 | 274 | 59.1 |  |  |  |
| 349 | . 95277 | 343 o | 15 | 14 |  |  | - |  |  |  |
| 350 | 0.95551 | 34359 | 16 | 15 |  |  |  |  |  |  |

Smithbonian Tablee

TABLE 75.
HOURS, MINUTES AND SECONDS INTO DECIMALS OF A DAY.

| Hours. | Day. | Min. | Day. | Min. | Day. | Sec. | Day. | Sec. | Lay. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - I | 0.041 667 | 1 | 0.000694 | 31 | 0.021 528 | I | 0.000012 | 31 | 0.000359 |
| 2 | . 083333 | 2 | .OOI 389 | 32 | . 022222 | 2 | . 000023 | 32 | . 000 |
| 3 | . 125000 | 3 | . 002083 | 33 | . 022917 | 3 | . 000035 | 33 | . 000382 |
| 4 | .166667 | 4 | . 002778 | 34 | . 023611 | 4 | . 000046 | 34 | . 000394 |
| 5 | 0.208333 | 5 | 0.003472 | 35 | 0.024305 | 5 | 0.000058 | 35 | 0.000405 |
| 6 | . 250000 | 6 | . 004167 | 36 | . 025000 | 6 | . 000069 | 36 | . 000417 |
| 7 | . 291667 | 7 | . 004 86r | 37 | . 025694 | 7 | . 000081 | 37 | . 000428 |
| 8 | . 333333 | 8 | . 005556 | 38 | .026389 | 8 | . 000093 | 38 | . 000440 |
| 9 | . 375000 | 9 | . 006250 | 39 | . 027083 | 9 | . 000104 | 39 | . 000 451 |
| 10 | 0.416667 | 10 | 0.006944 | 40 | 0.027778 | 10 | 0.000 I16 | 40 | 0.000463 |
| 11 | . 458333 | 11 | . 007639 | 4 I | . 028472 | 11 | . 000127 | 41 | . 000475 |
| 12 | . 500000 | 12 | . 008333 | 42 | .029167 | 12 | . 000 I39 | 42 | . 000486 |
| I3 | . 541667 | 13 | . 009028 | 43 | . 029 861 | I3 | . 000 I50 | 43 | . 000498 |
| 14 | . 583333 | 14 | . 009722 | 44 | . 030556 | 14 | .000 I62 | 44 | . 000509 |
| 15 | 0.625000 | 15 | 0.010417 | 45 | 0.031250 | 15 | 0.000174 | 45 | 0.00052 I |
| 16 | . 666667 | 16 | . OII III | 46 | .031 944 | 16 | . 000185 | 46 | . 000532 |
| 17 | . 708333 | 17 | . 011806 | 47 | . 032639 | 17 | . 000197 | 47 | . 000544 |
| 18 | . 750000 | 18 | .OI2 500 | 48 | . 033333 | 18 | . 000208 | 48 | . 000556 |
| 19 | .791 667 | 19 | .OI3 I94 | 49 | . 034028 | 19 | . 000220 | 49 | . 000567 |
| 20 | 0.833333 | 20 | 0.013889 | 50 | 0.034722 | 20 | 0.00023 I | 50 | 0.000579 |
| 21 | . 875000 | 21 | .OI4 583 | 5 I | . 035417 | 2 I | . 000243 | 5 I | . 000590 |
| 22 | . 916667 | 22 | . 015278 | 52 | . 036 III | 22 | . 000255 | 52 | . 000602 |
| 23 | .958 333 | 23 | .OI5 972 | 53 | . 036806 | 23 | . 000266 | 53 | . 000613 |
| 24 | 1.000000 | 24 | .or6 667 | 54 | . 037500 | 24 | . 000278 | 54 | . 000625 |
|  |  | 25 | 0.017361 | 55 | 0.038194 | 25 | 0.000289 | 55 | 0.000637 |
|  |  | 26 | . 018 O56 | 56 | . 038889 | 26 | . 000301 | 56 | . 000648 |
|  |  | 27 | .or8 750 | 57 | . 039583 | 27 | . 000313 | 57 | . 000660 |
|  |  | 28 | .or9 444 | 58 | . 040278 | 28 | . 000324 | 58 | . 000671 |
|  |  | 29 | .020 I39 | 59 | . 040972 | 29 | . 000336 | 59 | . 000683 |
|  |  | 30 | 0.020833 | 60 | 0.04I 667 | 30 | 0.000347 | 60 | . 000694 |

Table 76.
DECIMALS OF A DAY INTO HOURS, MINUTES AND SECONDS.

| Hundredths of a Day. |  |  | Ten Thousandths of a Day. |  | Millionths of a Day. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d. | h. m. | S. | d. | min. sec. | d. | sec. |
| 0.01 | 14 |  | 0.0001 | 8.64 | 0.000001 | 0.09 |
| . 02 | 28 |  | 2 | 17.28 | 2 | 0.17 |
| . 03 | 43 |  | 3 | 25.92 | 3 | 0.26 |
| . 04 | 57 | 36 | 4 | 34.56 | 4 | 0.35 |
| 0.05 | I 12 | 0 | 0.0005 | 4.3 .20 | 0.000005 | 0.43 |
| . 06 | I 26 |  | 6 | 5 I .84 | 6 | 0.52 |
| . 07 | I 40 |  | 7 | I 0.48 | 7 | 0.60 |
| . 08 | I 55 |  | 8 | I 9.12 | 8 | 0.69 |
| . 09 | 29 |  | 9 | I 17.76 | 9 | 0.78 |
| 0.10 | 224 | 0 | 0.0010 | I 26.40 | 0.000010 | 0.86 |
| . 20 | 448 | 0 | 20 | 252.80 | 20 | 1.73 |
| . 30 | 7 12 | o | 30 | 419.20 | 30 | 2.59 |
| . 40 | 936 | - | 40 | $5 \quad 45.60$ | 40 | 3.46 |
| 0.50 | 120 |  | 0.0050 | 712.00 | 0.000050 | 4.32 |
| . 60 | 1424 |  | 60 | $8 \quad 38.40$ | 60 | 5.18 |
| . 70 | 1648 |  | 70 | 104.80 | 70 | 6.05 |
| . 80 | 19. 12 |  | 80 | II 31.20 | 80 | 6.91 |
| . 90 | $2 \mathrm{I}^{*} 36$ | 0 | 90 | $12 \quad 57.60$ | 90 | $7 \cdot 78$ |

TABLE 77.
MINUTES AND SECONDS INTO DECIMALS OF AN HOUR.

| Min. | Decimals of an hour. | Min. | Decimals of an hour. | Sec. | Decimals of an hour. | Sec. | Decimals of an hour. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 0.016 667 | 31 | 0.516 667 | 1 | 0.000278 | 31 | 0.0086 II |
| 2 | . 033333 | 32 | . 533333 | 2 | . 000556 | 32 | .008 889 |
| 3 | . 050000 | 33 | . 550000 | 3 | . 000833 | 33 | . 009167 |
| 4 | . 066667 | 34 | . 566667 | 4 | .OOI III | 34 | . 009444 |
| 5 | 0.083333 | 35 | 0.583333 | 5 | 0.001389 | 35 | 0.009722 |
| 6 | . 100000 | 36 | . 600000 | 6 | .001 667 | 36 | . 010000 |
| 7 | .ri6 667 | 37 | . 616667 | 7 | .OOI 944 | 37 | .OIO 278 |
| 8 | . 133333 | 38 | . 633333 | 8 | . 002222 | 38 | .oIO 556 |
| 9 | . 150000 | 39 | . 650000 | 9 | . 002500 | 39 | . 010833 |
| 10 | 0.166 667 | 40 | 0.666667 | 10 | 0.002778 | 40 | O.OII III |
| II | .183 333 | 4 I | . 683333 | II | . 003056 | 41 | .oir 389 |
| 12 | . 200000 | 42 | . 700000 | 12 | . 003333 | 42 | .OII 667 |
| 13 | . 216667 | 43 | .716 667 | 13 | . 0036 II | 43 | . OI I 944 |
| 14 | . 233333 | 44 | . 733333 | 14 | . 003889 | 44 | .OI2 222 |
| 15 | 0.250000 | 45 | 0.750000 | 15 | 0.004167 | 45 | 0.012500 |
| 16 | . 266667 | 46 | . 766667 | 16 | . 004444 | 46 | . 012778 |
| 17 | . 283333 | 47 | . 783333 | 17 | . 004722 | 47 | .OI3 056 |
| 18 | . 300000 | 48 | . 800000 | 18 | . 005000 | 48 | .OI3 333 |
| 19 | .316 667 | 49 | .816 667 | 19 | . 005278 | 49 | .OI36II |
| 20 | 0.333333 | 50 | 0.833333 | 20 | 0.005556 | 50 | 0.013 889 |
| 21 | . 350000 | 5 I | . 850000 | 21 | . 005833 | 5 I | .OI4 167 |
| 22 | . 366667 | 52 | . 866667 | 22 | . 006 I II | 52 | .OI4 444 |
| 23 | . 383333 | 53 | . 883333 | 23 | . 006389 | 53 | .OI4 722 |
| 24 | . 400000 | 54 | . 900000 | 24 | . 006667 | 54 | .OI5 000 |
|  | 0.416667 | 55 | 0.916667 | 25 | 0.006944 | 55 | 0.015278 |
| 26 | . 433333 | 56 | . 933333 | 26 | . 007222 | 56 | .OI5 556 |
|  | . 450000 |  | . 950000 |  | . 007500 | 57 | . 015833 |
| 28 | . 466667 | 58 | . 966667 | 28 | . 007778 | 58 | . 016111 |
| 29 | . 483333 | 59 | . 983333 | 29 | . 008056 | 59 | .016 389 |
| 30 | 0.500000 | 60 | 1.000000 | 30 | 0.008333 | 60 | 0.016667 |

Table 78.
MEAN TIME AT APPARENT NOON.

| Day of Month. | JAN. | FEB. | MAR. | APR. | MAY. | JUNE. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 181624 | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
|  | 124 | 1214 | 12 12 | 124 | II 57 | II 58 |
|  | 127 | 1214 | 12 II | 122 | II 56 | II 59 |
|  | 12 10 | 1214 | 129 | 12 O | II 56 | 120 |
|  | $12 \quad 12$ | 12 I3 | 126 | II 58 | II 57 | 122 |
|  | JUL, | AUG. | SEPT. | OCT. | Nov. | DEC. |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
|  | 123 | 126 | 12 O | II 50 | II 44 | II 50 |
| 8 | 125 | 125 | II 58 | II 48 | II 44 | II 53 |
| 16 | 126 | 124 | II 55 | II 46 | II 45 | II 56 |
| 24 | 126 | 122 | II 52 | II 45 | II 47 | 120 |

TABLE 79.

## SIDEREAL TIME INTO MEAN SOLAR TIME.

The tabular values are to be subtracted from a sidereal time interval.

| Hrs. | Reduction to <br> Mean Time. | Min. | Reduc- <br> to Mean <br> Time. | Min. | Reducto Mon Time. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| h. | m. s. | m. | s. | m. | s. |
| 1 | - 9.83 | 1 | 0.16 | 31 | 5.08 |
| 2 | - 19.66 | 2 | 0.33 | 32 | 5.24 |
| 3 | - 29.49 | 3 | 0.49 | 33 | 5.41 |
| 4 | - 39.32 | 4 | 0.66 | 34 | $5 \cdot 57$ |
| 5 | - 49.15 | 5 | 0.82 | 35 | 5.73 |
| 6 | - 58.98 | 6 | 0.98 | 36 | 5.90 |
| 7 | I 8.8 I | 7 | I. 15 | 37 | 6.06 |
| 8 | 1 I 8.64 | 8 | 1.31 | 38 | 6.23 |
| 9 | I 28.47 | 9 | 1.47 | 39 | 6.39 |
| 10 | I 38.30 | 10 | I. 64 | 40 | 6.55 |
| 11 | I 48.13 | 11 | 1.80 | 41 | 6.72 |
| 12 | I 57.96 | 12 | 1.97 | 42 | 6.88 |
| 13 | $2 \quad 7.78$ | 13 | 2.I3 | 43 | 7.05 |
| 14 | 217.61 | 14 | 2.29 | 44 | 7.21 |
| 15 | 227.44 | 15 | 2.46 | 45 | 7.37 |
| 16 | 237.27 | 16 | 2.62 | 46 | 7.54 |
| 17 | 2 47.10 | 17 | 2.79 | 47 | 7.70 |
| 18 | 256.93 | 18 | 2.95 | 48 | 7.86 |
| 19 | $3 \quad 6.76$ | 19 | 3.11 | 49 | 8.03 |
| 20 | 316.59 | 20 | 3.28 | 50 | 8.19 |
| 21 | 326.42 | 21 | 3.44 | 51 | 8.36 |
| 22 | 336.25 | 22 | 3.60 | 52 | 8.52 |
| 23 | 346.08 | 23 | 3.77 | 53 | 8.68 |
| 24 | 3 55.91 | 24 | 3.93 | 54 | 8.85 |
|  |  | 25 | 4. 10 | 55 | 9.01 |
|  |  | 26 | 4.26 | 56 | 9.17 |
|  |  | 27 | 4.42 | 57 | 9.34 |
|  |  | 28 29 | 4.59 | 58 | 9.50 |
|  |  | 29 | 4.75 | 59 | 9.67 |
|  |  | 30 | 4.92 | 60 | 9.83 |

TABLE 80.

## MEAN SOLAR TIME INTO SIDEREAL TIME.

The tabular values are to be added to a mean solar time interval.

| Hrs. | Reduction to Sidereal Time. | Min. | Reduction to Siderea Time. | Min. | Reduc- tion to Sidereal Time. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| h. | m. s. | m. | s. | m. | s. |
| 1 | - 9.86 | 1 | 0.16 | 31 | 5.09 |
| 2 | - 19.71 | 2 | 0.33 | 32 | 5.26 |
| 3 | - 29.57 | 3 | 0.49 | 33 | 5.42 |
| 4 | - 39.43 | 4 | 0.66 | 34 | $5 \cdot 59$ |
| 5 | - 49.28 | 5 | 0.82 | 35 | 5.75 |
| 6 | - 59.14 | 6 | 0.99 | 36 | 5.91 |
| 7 | I 9.00 | 7 | 1.15 | 37 | 6.08 |
|  | $\begin{array}{ll}1 & 18.85\end{array}$ | 8 | I. 31 | 38 | 6.24 |
| 9 | 1828.71 | 9 | I. 48 | 39 | 6.41 |
| 10 | I 38.57 | 10 | 1. 64 | 40 | 6.57 |
| 11 | I 48.42 | 11 | 1.81 | 4 I | 6.74 |
| 12 | I 58.28 | 12 | I. 97 | 42 | 6.90 |
| 13 | 28.13 | 13 | 2.14 | 43 | 7.06 |
| 14 | 217.99 | 14 | 2.30 | 44 | 7.23 |
| 15 | 227.85 | 15 | 2.46 | 45 | 7.39 |
| 16 | 237.70 | 16 | 2.63 | 46 | 7.56 |
| 17 | 247.56 | 17 | 2.79 | 47 | 7.72 |
| 18 | 257.42 | 18 | 2.96 | 48 | 7.89 |
| 19 | $3 \quad 7.27$ | 19 | 3.12 | 49 | 8.05 |
| 20 | 317.13 | 20 | 3.29 | 50 | 8.21 |
| 21 | 326.99 | 21 | 3.45 | 5 I | 8.38 |
| 22 | 336.84 | 22 | 3.61 | 52 | 8.54 |
| 23 | 346.70 | 23 | 3.78 | 53 | 8.71 |
| 24 | 356.56 | 24 | 3.94 | 54 | 8.87 |
|  |  | 25 | 4.11 | 55 | 9.04 |
|  |  | 26 | 4.27 | 56 | 9.20 |
|  |  | 27 | 4.43 | 57 | 9.36 |
|  |  | 28 | 4.60 | 58 | 9.53 |
|  |  | 29 | 4.76 | 59 | 9.69 |
|  |  | 30 | 4.93 | 60 | 9.86 |

## Reduction for Seconds-sidereal or mean solar.

The tabular values are to be $\left\{\begin{array}{l}\text { subtracted from a sidereal } \\
\text { added to a mean solar }\end{array}\right\}$ time interval.

| $\left\|\begin{array}{c} \text { Sidereal } \\ \text { or } \\ \text { or Time. } \end{array}\right\|$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| s. | s. | s. | s. | s. | s. | s. | s. | s. | s. | s. |
| 0 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.02 | 0.02 | 0.02 | 0.03 |
| 10 | . 03 | . 03 | . 03 | . 04 | . 04 | . 04 | . 04 | . 05 | . 05 | . 05 |
| 20 | . 06 | . 06 | . 06 | . 06 | . 07 | . 07 | . 07 | . 07 | . 08 | . 08 |
| 30 | . 08 | . 09 | . 09 | . 09 | . 09 | . 10 | .ro | .ro | .10 | . 11 |
| 40 | . 11 | .II | . 12 | . 12 | . 12 | . 12 | . 13 | . 13 | . 13 | . 13 |
| 50 | 0.14 | 0.14 | 0.14 | 0.15 | 0.15 | 0.15 | 0.15 | 0.16 | 0.16 | 0.16 |

Smithbonian Tables.

## MISCELLANEOUS TABLES.

Density of air at different temperatures Fahrenheit . Table ..... 8I
Density of air at different humidities and pressures-Englishmeasures.
Term for humidity : auxiliary to Table 83 ..... Table 82
Values of $\frac{h}{29.92 \mathrm{I}}=\frac{b-0.378 e}{29.92 \mathrm{I}}$ ..... 83
Density of air at different temperatures Centigrade Table 84
Density of air at different humidities and pressures - Metricmeasures.
Term for humidity : auxiliary to Table 86 Table 85
Values of $\frac{h}{760}=\frac{b-0.378 e}{760}$ ..... 86
Conversion of avoirdupois pounds and ounces into kilogrammes Table ..... 87
Conversion of kilogrammes into avoirdupois pounds and ounces ..... 88
Conversion of grains into grammes ..... 89
Conversion of grammes into grains ..... 90
Conversion of units of magnetic intensity Table 9I
Quantity of water corresponding to given depths of rainfall . TABLE ..... 92
Dates of Dove's pentades ..... 93
Division by 28 of numbers from 28 to 867972 ..... 94
Division by 29 of numbers from 29 to 898971 ..... 95
Division by 31 of numbers from 31 to 960969 ..... 96
Natural sines and cosines ..... Table 97
Natural tangents and cotangents ..... Table 98
Logarithms of numbers ..... Table 99
List of meteorological stations ..... Table 100

## TAble 81.

DENSITY OF AIR AT DIFFERENT TEMPERATURES FAHRENHEIT.

$$
\delta_{t}=\frac{0.00129305}{1+0.0020389\left(t-32^{\circ}\right)} .
$$

I cubic centimetre of dry air at the temperature $32^{\circ} F$. and pressure 760 mm ., and under the standard value of gravity at latitude $45^{\circ}$ and sea-level, weighs 0.00129305 gramme.

| Temperature. | $\delta_{t}$ | $\log \delta_{t}$ | Temperature. | $\delta_{t}$ | $\log \delta_{t}$ | Temperature. | $\delta_{t}$ | $\log \delta_{t}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | 0.00 | - Io | F. | 0.00 | - 10 | F. | 0.00 | - 10 |
| $-45^{\circ}$ | 15339 | 7.18579 | $30^{\circ}$ | 12983 | 7.11339 | $75^{\circ}$ | 11888 | 7.07512 |
| -40 | 15155 | . 18056 | 31 | 12957 | . II 250 | 76 | 11866 | . 07430 |
| -35 | 14977 | . 17541 | 32 | I2931 | . 11162 | 77 | 11844 | . 07349 |
| -30 | 14802 | .17031 | 33 | 12904 | . 11073 | 78 | 11822 | . 07268 |
| $-25$ | 14631 | . 16527 | 34 | 12878 | . 10985 | 79 | 11800 | .07187 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -20 | 14464 | 7.16029 | 35 | 12852 | 7.10897 | 80 | 11778 | 7.07107 |
| $-18$ | 14398 | . 1583 I | 36 | 12826 | . 10809 | 81 | İ756 | . 07026 |
| - 16 | 14333 | . 15634 | 37 | 12800 | . 1072I | 82 | 11734 | . 06946 |
| - I4 | 14269 | . 15439 | 38 | 12774 | . 10633 | 83 | 11713 | . 06865 |
| - 12 | 14205 | . 15244 | 39 | 12749 | . 10546 | 84 | 11691 | . 06785 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| $-10$ | 14142 | 7.15050 | 40 | 12723 | 7.10459 | 85 | 11670 | 7.06705 |
| $-8$ | 14079 | . 14856 | 41 | I2698 | . 10372 | 86 | 11648 | . 06625 |
| - 6 | 14017 | . 14664 | 42 | 12672 | . 10285 | 87 | 11627 | . 06546 |
| - 4 | I3955 | . 14472 | 43 | I2647 | . 10198 | 88 | 11605 | . 06466 |
| - 2 | 13894 | . 14282 | 44 | 12622 | . 10112 | 89 | II584 | . 06387 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| + 0 | 13833 | 7.14092 | 45 | 12597 | 7.10025 | 90 | 11563 | 7.06307 |
|  | 13803 | . 13997 | 46 | 12572 | . 09939 | 91 | 11542 | . 06228 |
| 2 | 13773 | . 13903 | 47 | 12547 | . 09853 | 92 | II52I | .06I49 |
| 3 | 13743 | . 13808 | 48 | 12522 | . 09767 | 93 | I 1500 | . 06070 |
| 4 | 13713 | . 13714 | 49 | 12497 | . 09682 | 94 | 11479 | . 05992 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 5 | 13684 | 7.13621 | 50 | 12473 | 7.09596 | 95 | 11458 | 7.05913 |
| 6 | 13654 | . 13527 | 51 | 12448 | .095II | 96 | 11438 | . 05835 |
| 7 | 13625 | . 13434 | 52 | 12424 | . 09426 | 97 | II418 | . 05757 |
| 8 | 13596 | . 13340 | 53 | 12400 | . 09341 | 98 | 11397 | . 05678 |
| 9 | 13567 | . 13247 | 54 | 12375 | . 09256 | 99 | 11376 | . 05600 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 10 | 13538 | 7.13155 | 55 | 12351 | 7.09171 | 100 | II356 | 7.05523 |
| 11 | 13509 | .13062 | 56 | 12327 | . 09087 | IOI | II336 | . 05445 |
| 12 | 13480 | . 12970 | 57 | 12303 | . 09002 | 102 | 11315 | .05367 |
| 13 | 13452 | . 12877 | 58 | 12280 | .08918 | 103 | 11295 | . 05290 |
| 14 | 13423 | . 12785 | 59 | 12256 | . 08834 | 104 | 11275 | .05213 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 15 | I 3395 | 7.12694 | 60 | 12232 | 7.08750 | 105 | 11255 | 7.05136 |
| 16 | 13367 | . 12602 | 61 | 12209 | . 08667 | 106 | II235 | . 05058 |
| 17 | 13338 | . 12510 | 62 | 12185 | .08583 | 107 | II2I5 | . 04982 |
| I8 | 13310 | . 12419 | 63 | I2162 | . 08500 | 108 | III96 | . 04905 |
| 19 | 13282 | . 12328 | 64 | 12138 | .08416 | 109 | III76 | . 04828 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 20 | 13255 | 7.12237 | 65 | I2II5 | 7.08334 | 110 | 11156 | 7.04752 |
| 21 | 13227 I3200 | . 12147 | 66 | 12092 | .0825I | 112 | IIII7 | . 04599 |
| 22 | 13200 | . 12056 | 67 | 12069 | .08168 | II4 | 11078 | . 04447 |
| 23 24 | I3I72 | . 11966 | 68 | 12046 | . 08085 | II6 | I 1040 | . 04296 |
|  | 0.00 |  |  | 0.00 | .0803 |  | 0.00 |  |
| 25 | 13118 | 7.11786 | 70 | 12001 | 7.07921 | 120 | 10963 | 7.03994 |
| 26 | 13091 | .11696 | 71 | 11978 | .07839 | 125 | 10870 | .0362I . |
| 27 | I3064 | . 11606 | 72 | 11956 | . 07757 | 130 | 10776 | .03248 |
| 28 | 13037 | . 11517 | 73 | 11933 | . 07675 | I35 | 10686 | . 02883 |
| 29 | I3010 | . 11428 | 74 | I1910 | . 07593 | 140 | 10597 | .02518 |

TABLE 82.

## DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES.

ENGLISH MEASURES.
Term for Humidity: Values of $0.378 e$. Auxiliary to Table 83 .
$e=$ Vapor pressure in inches.

| DewPoint. | Vapor Pressure. $e$. | 0.378e. | DewPoint. | Vapor Pres. sure. $e$. | 0.378 e. | DewPoint. | Vapor Prese. | 0.378 e | Dew. Point. | Vapor Pres. $e$. | 0.378 e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. | Inch. | F. | Inch. | Inch. | F. | Inch. | Inch. | F. | Inches. | Inches. |
| $-40^{\circ}$ | 0.0054 | 0.002 | $5^{\circ}$ | 0.057 | 0.021 | $50^{\circ}$ | 0.360 | 0.136 | $95^{\circ}$ | 1.645 | 0.622 |
| -39 | . 0058 | . 002 | 6 | . 059 | 022 | 5 I | . 373 | . 141 | 96 | 1.696 | .641 |
| $-38$ | .0061 | . 002 | 7 | . 062 | . 023 | 52 | . 387 | . 146 | 97 | 1.749 | .66I |
| $-37$ | . 0065 | . 002 | 8 | . 065 | . 025 | 53 | . 402 | . 152 | 98 | 1.803 | . 682 |
| $-36$ | . 0069 | . 003 | 9 | . 068 | . 026 | 54 | . 417 | . 158 | 99 | I. 859 | . 703 |
| $-35$ | 0.0073 | 0.003 | 10 | 0.071 | 0.027 | 55 | 0.432 | 0.163 | 100 | 1.916 | 0.724 |
| -34 | . 0077 | . 003 | II | . 074 | . 028 | 56 | . 448 | . 169 | 101 | 1.975 | . 747 |
| -33 | . 0082 | . 003 | 12 | . 078 | . 029 | 57 | . 465 | . 176 | 102 | 2.035 | . 769 |
| $-32$ | . 0087 | . 003 | 13 | .081 | . 031 | 58 | .48I | . 182 | 103 | 2.097 | . 793 |
| $-31$ | .0092 | . 003 | 14 | . 085 | . 032 | 59 | . 499 | .189 | 104 | 2.160 | .8I6 |
| $-30$ | 0.0097 | 0.004 | 15 | 0.088 | 0.033 | 60 | 0.517 | 0. 195 | 105 | 2.225 | 0.841 |
| -29 | . 0103 | . 004 | 16 | . 092 | . 035 | 6 I | . 536 | . 203 | 106 | 2.292 | . 866 |
| -28 | . 0109 | . 004 | 17 | . 096 | . 036 | 62 | . 555 | . 210 | 107 | 2.360 | . 892 |
| -27 | . OII 5 | . 004 | 18 | . 101 | . 038 | 63 | . 575 | . 217 | 108 | 2.431 | . 919 |
| -26 | . 0121 | . 005 | 19 | . 105 | . 040 | 64 | . 595 | . 225 | 109 | 2.503 | . 946 |
| -25 | 0.0128 | 0.005 | 20 | 0.110 | 0.042 | 65 | 0.616 | 0.233 | 110 | 2.576 | 0.974 |
| -24 | . 0135 | . 005 | 21 | .114 | . 043 | 66 | . 638 | . 241 | III | 2.652 | 1.002 |
| $-23$ | .OI42 | . 005 | 22 | .119 | . 045 | 67 | . 661 | . 250 | 112 | 2.730 | 1.031 |
| -22 | . 0150 | . 006 | 23 | . 124 | . 047 | 68 | . 684 | . 259 | 113 | 2.810 | 1.062 |
| -2I | . 0158 | . 006 | 24 | . 130 | . 049 | 69 | . 707 | . 267 | 114 | 2.891 | 1.093 |
| $-20$ | 0.0167 | 0.006 | 25 | 0.135 | 0.051 | 70 | 0.732 | 0.277 | 115 | 2.975 | 1.125 |
| - 19 | . 0176 | . 007 | 26 | .141 | . 053 | 71 | . 757 | . 286 | 116 | 3.061 | I. 157 |
| - 18 | . 0185 | . 007 | 27 | . 147 | . 056 | 72 | . 783 | . 296 | 117 | 3.148 | I. 190 |
| - I7 | . 0195 | . 007 | 28 | . 153 | . 058 | 73 | . 810 | -306 | 118 | 3.239 | 1.224 |
| - 16 | . 0205 | . 008 | 29 | . 159 | . 060 | 74 | . 838 | -317 | 119 | $3 \cdot 33$ I | 1.259 |
| - 15 | 0.0216 | 0.008 | 30 | 0.166 | 0.063 | 75 | 0.866 | 0.327 | 120 | 3.425 | I. 295 |
| - 14 | . 0227 | . 009 | 31 | . 173 | . 065 | 76 | . 896 | - 339 | 121 | 3.522 | 1.33 I |
| - 13 | . 0239 | . 009 | 32 | . 180 | . 068 | 77 | . 926 | -350 | 122 | 3.621 | I. 369 |
| $-12$ | . 0251 | . 009 | 33 | . 187 | . 071 | 78 | . 957 | - 362 | 123 | 3.723 | 1.407 |
| II | . 0264 | . 010 | 34 | . 195 | . 074 | 79 | . 989 | - 374 | 124 | 3.827 | 1.447 |
| $-10$ | 0.0277 | 0.010 | 35 | 0.203 | 0.077 | 80 | 1.022 | 0.386 | 125 | 3.933 | 1. 487 |
| - 9 | . 0292 | . 011 | 36 | . 211 | . 080 | 8 I | 1.056 | - 399 | 126 | 4.042 | 1.528 |
| - 8 | . 0306 | . 012 | 37 | . 219 | . 083 | 82 | 1.091 | .412 | 127 | 4. 154 | 1.570 |
| -7 | . 0322 | . 012 | 38 | . 228 | . 086 | 83 | 1.127 | . 426 | 128 | 4.268 | 1.613 |
| - 6 | . 0338 | . 013 | 39 | . 237 | . 090 | 84 | 1.163 | . 440 | 129 | $4 \cdot 385$ | 1.658 |
| $-5$ | 0.0354 | 0.013 | 40 | 0.246 | 0.093 | 85 | I. 201 | 0.454 | 130 | 4.504 | 1.703 |
| - 4 | . 0372 | . 014 | 4 I | . 256 | . 097 | 86 | 1.241 | . 469 | 131 | 4.627 | 1.749 |
| - 3 | . 0390 | . 015 | 42 | . 266 | 101 | 87 | 1.281 | . 484 | 132 | 4.752 | 1. 796 |
| - 2 | . 0409 | . 015 | 43 | . 276 | . 105 | 88 | I. 322 | . 500 | 133 | 4.880 | 1.844 |
| $-\mathrm{I}$ | . 0429 | . 1016 | 44 | . 287 | . 109 | 89 | 1.364 | . 516 | 134 | 5.011 | 1.894 |
| 0 | 0.0449 | 0.017 | 45 | 0.298 | O.113 | 90 | 1.408 | 0.532 | 135 | 5.145 | 1.945 |
| + 1 | . 0471 | . 018 | 46 | -310 | . 117 | 91 | I. 453 | . 549 | 136 | 5.282 | 1.997 |
|  | . 0493 | . 019 | 47 | - 322 | . 122 | 92 | 1.499 | . 567 | 137 | 5.422 | 2.050 |
| 3 | .0517 | . 020 | 48 | . 334 | . 126 | 93 | 1.546 | . 584 | 138 | $5 \cdot 565$ | 2.104 |
| 4 | .054I | . 020 | 49 | -347 | . 131 | 94 | 1.595 | . 603 | 139 | $5 \cdot 712$ | 2.159 |
| 5 | 0.0567 | 0.021 | 50 | 0.360 | 0.136 | 95 | 1.645 | 0.622 | 140 | 5.862 | 2.216 |

TABLE 83.
DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES. ENGLISH MEASURES.
Values of $\frac{h}{29.92 I}$.
$\frac{\delta}{\delta_{0}}=\frac{h}{29.92 \mathrm{I}}=\frac{b-0.378 e}{29.92 \mathrm{I}}$.
$b=$ Barometric pressure in inches ; $e=$ Vapor pressure in inches.

| h. | $\frac{h}{29.92 \mathrm{I}}$. | $\log \frac{h}{29.92 \mathrm{I}}$ | h. | $\frac{h}{29.291}$. | $\log \frac{h}{29.92 \mathrm{I}}$. | h. | $\frac{\mathrm{h}}{29.92 \mathrm{I}}$. | $\log \frac{h}{29.92 I}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inch's. |  | - 10 | Inches. |  | - 10 | Inches. |  | - 10 |
| 10.0 | 0.3342 | 9.52402 | 15.0 | 0.5013 | 9.70012 | 20.0 | 0.6684 | 9.82505 |
| 10. 1 | . 3376 | . 52835 | 15. 1 | . 5047 | . 70300 | 20.1 | . 6718 | . 82722 |
| 10.2 | . 3409 | . 53262 | 15.2 | . 5080 | . 70587 | 20.2 | .6751 | . 82938 |
| 10.3 | - 3442 | . 53686 | 15.3 | .5113 | . 70871 | 20.3 | . 6784 | .83152 |
| 10.4 | . 3476 | .54106 | 15.4 | . 5147 | . 71154 | 20.4 | .68I8 | . 83365 |
| 10.5 | 0.3509 | 9.5452 I | 15.5 | 0.5180 | 9.71435 | 20.5 | 0.6851 | 9.83578 |
| 10.6 | . 3543 | . 54933 | 15.6 | . 5214 | . 71715 | 20.6 | . 6885 | . 83789 |
| 10.7 | -3576 | . 55341 | 15.7 | . 5247 | . 71992 | 20.7 | . 6918 | . 83999 |
| 10.8 | . 3609 | . 55745 | 15.8 | .528I | . 72268 | 20.8 | . 6952 | . 84209 |
| 10.9 | . 3643 | . 56145 | 15.9 | . 5314 | . 72542 | 20.9 | . 6985 | . 84417 |
| 11.0 | 0.3676 | 9.56542 | 16.0 | 0.5347 | 9.72814 | 21.0 | 0.7018 | 9.84624 |
| II. I | . 3710 | . 56935 | 16. 1 | . 5381 | . 73085 | 21.1 | . 7052 | . 84831 |
| II. 2 | . 3743 | . 57324 | 16.2 | . 5414 | . 73354 | 21.2 | . 7085 | . 85036 |
| 11.3 | . 3777 | . 57710 | 16.3 | . 5448 | .7362I | 21.3 | .7119 | . 85240 |
| II. 4 | . 38 Io | . 58093 | 16.4 | .548I | . 73887 | 21.4 | .7152 | . 85444 |
| 11.5 | 0.3843 | 9.58472 | 16.5 | 0.5515 | 9.74151 | 21.5 | 0.7186 | 9.85646 |
| 11.6 | . 3877 | . 58848 | 16.6 | . 5548 | . 74413 | 21.6 | . 7219 | . 85848 |
| 11.7 | . 3910 | . 5922 I | 16.7 | .5581 | . 74674 | 21.7 | . 7252 | . 86048 |
| II. 8 | - 3944 | . 59591 | 16.8 | .5615 | . 74933 | 21.8 | . 7286 | . 86248 |
| II. 9 | . 3977 | . 59957 | 16.9 | . 5648 | .75191 | 21.9 | .7319 | . 86447 |
| 12.0 | 0.4011 | 9.6032I | 17.0 | 0. 5682 | 9.75447 | 22.0 | 0.7353 | 9.86645 |
| 12.1 | . 4044 | .6068I | 17.1 | . 5715 | . 75702 | 22.1 | . 7386 | . 86842 |
| 12.2 | . 4077 | .61038 | 17.2 | . 5748 | . 75955 | 22.2 | . 7420 | . 87038 |
| 12.3 | .4III | .61393 | 17.3 | . 5782 | . 76207 | 22.3 | . 7453 | . 87233 |
| 12.4 | .4144 | .6I745 | 17.4 | .5815 | . 76457 | 22.4 | . 7486 | . 87427 |
| 12.5 | 0.4178 | 9.62093 | 17.5 | 0.5849 | 9.76706 | 22.5 | 0.7520 | 9.87621 |
| 12.6 | .42II | . 62439 | 17.6 | . 5882 | . 76954 | 22.6 | . 7553 | . 87813 |
| 12.7 | . 4244 | . 62782 | 17.7 | . 5916 | . 77200 | 22.7 | . 7587 | . 88005 |
| 12.8 | . 4278 | . 63123 | 17.8 | . 5949 | . 77444 | 22.8 | . 7620 | .88196 |
| 12.9 | .43II | .6346I | 17.9 | . 5982 | . 77687 | 22.9 | . 7653 | . 88386 |
| 13.0 | 0.4345 | 9.63797 | 18.0 | 0.6016 | 9.77930 | 23.0 | 0.7687 | 9.88575 |
| 13.1 | . 4378 | . 64130 | 18.1 | . 6049 | . 78170 | 23.1 | . 7720 | . 88764 |
| 13.2 | . 4412 | . 64460 | 18.2 | . 6083 | . 78410 | 23.2 | . 7754 | .88951 |
| 13.3 | . 4445 | . 64788 | 18.3 | .6II6 | . 78648 | 23.3 | . 7787 | . 89138 |
| 13.4 | . 4478 | .65113 | 18.4 | . 6149 | . 78884 | 23.4 | .7821 | . 89324 |
| 13.5 | 0.4512 | 9.65436 | 18.5 | 0.6183 | 9.79120 | 23.5 | 0.7854 | 9.89509 |
| 13.6 | . 4545 | . 65756 | 18.6 | . 6216 | . 79354 | 23.6 | . 7887 | . 89693 |
| 13.7 | . 4579 | . 66074 | 18.7 | . 6250 | . 79587 | 23.7 | . 7921 | . 89877 |
| I 3.8 | .4612 | . 66390 | 18.8 | . 6283 | .79818 | 23.8 | . 7954 | . 90060 |
| 13.9 | . 4646 | . 66704 | 18.9 | . 6317 | . 80049 | 23.9 | . 7988 | . 90242 |
| 14.0 | 0.4679 | 9.67015 | 19.0 | 0.6350 | 9.80278 | 24.0 | 0.8021 | 9.90424 |
| 14. 1 | . 4712 | . 67324 | 19.1 | . 6383 | . 80506 | 24.1 | . 8054 | . 90604 |
| 14.2 | . 4746 | .6763I | 19.2 | .6417 | . 80733 | 24.2 | . 8088 | . 90784 |
| 14.3 | . 4779 | . 67936 | 19.3 | . 6450 | . 80958 | 24.3 | .8I2I | . 90963 |
| 14.4 | .4813 | . 68239 | 19.4 | . 6484 | .8II83 | 24.4 | .8155 | .9114I |
| 14.5 | 0.4846 | 9.68539 | 19.5 | 0.6517 | 9.81406 | 24.5 | 0.8188 | 9.91319 |
| 14.6 | . 4879 | . 68837 | 19.6 | . 6551 | . 81628 | 24.6 | . 8222 | . 91496 |
| 14.7 | . 4913 | . 69134 | 19.7 | . 6584 | .81849 | 24.7 | . 8255 | . 91672 |
| 14.8 | . 4946 | . 69429 | 19.8 | .6617 | . 82069 | 24.8 | . 8289 | .91848 |
| 14.9 | . 4980 | . 6972 I | 19.9 | .665I | . 82288 | 24.9 | .8322 | . 92022 |

TAble 83.
DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES.

## ENGLISH MEASURES.

Values of $\frac{{ }^{h}{ }^{h} .921}{}$.

$$
\frac{\delta}{\delta_{0}}=\frac{h}{29.92 \mathrm{I}}=\frac{b-0.378 e}{29.92 \mathrm{I}} .
$$

$b=$ Barometric pressure in inches ; $e=$ Vapor pressure in inches.

| h. | $\frac{h}{29.92 \mathrm{I}}$ | $\log \frac{h}{29.921}$ | h. | $\frac{h}{29.921}$ | $\log \frac{h}{29.92 I}$ | h. | $\frac{h}{29.921}$ | $\log \frac{h}{29.92 \mathrm{I}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. |  | - 10 | Inches. |  | - 10 | Inches. |  | - 10 |
| 25.00 | 0.8355 | 9.92196 | 27.25 | 0.9107 | 9.95939 | 29.50 | 0.9859 | 9.99385 |
| 25.05 | . 8372 | . 92283 | 27.30 | . 9124 | . 96019 | 29.55 | . 9876 | . 99458 |
| 25.10 | . 8389 | . 92370 | 27.35 | .9141 | . 96098 | 29.60 | . 9893 | . 99532 |
| 25.15 | . 8405 | . 92456 | 27.40 | .9157 | .96I77 | 29.65 | . 9909 | . 99605 |
| 25.20 | . 8422 | . 92542 | 27.45 | . 9174 | . 96256 | 29.70 | . 9926 | . 99678 |
| 25.25 | 0.8439 | 9.92628 | 27.50 | 0.9191 | 9.96336 | 29.75 | 0.9943 | 9.99751 |
| 25.30 | . 8456 | . 92714 | 27.55 | . 9208 | .96414 | 29.80 | . 9960 | . 99824 |
| 25.35 | . 8472 | . 92800 | 27.60 | . 9224 | . 96493 | 29.85 | . 9976 | . 99897 |
| 25.40 | . 8489 | . 92886 | 27.65 | .924I | . 96572 | 29.90 | . 9993 | . 99970 |
| 25.45 | . 8506 | .9297I | 27.70 | . 9258 | . 96650 | 29.95 | 1.0010 | 0.00042 |
| 25.50 | 0.8522 | 9.93056 | 27.75 | 0.9274 | 9.96728 | 30.00 | 1.0026 | 0.00115 |
| 25.55 | . 8539 | .93141 | 27.80 | . 9291 | . 96807 | 30.05 | 1.0043 | .00187 |
| 25.60 | . 8556 | . 93226 | 27.85 | . 9308 | . 96885 | 30. 10 | 1.0060 | . 00259 |
| 25.65 | . 8573 | .933II | 27.90 | . 9325 | . 96963 | 30.15 | 1.0076 | .0033I |
| 25.70 | . 8589 | . 93396 | 27.95 | .934I | . 97040 | 30.20 | 1.0093 | . 00403 |
| 25.75 | 0.8606 | 9.93480 | 28.00 | 0.9358 | 9.971 18 | 30.25 | 1.OIIO | 0.00475 |
| 25.80 | . 8623 | . 93564 | 28.05 | . 9375 | .97195 | 30.30 | 1.0127 | . 00547 |
| 25.85 | . 8639 | . 93648 | 28.10 | . 9391 | . 97273 | 30.35 | I. 0143 | .00618 |
| 25.90 | . 8656 | . 93732 | 28.15 | . 9408 | . 97350 | 30.40 | I.or60 | .00690 |
| 25.95 | . 8673 | .93816 | 28.20 | . 9425 | . 97427 | 30.45 | I.OI77 | .0076I |
| 26.00 | 0.8690 | 9.93900 | 28.25 | 0.944 I | 9.97504 | 30.50 | 1.OI93 | 0.00832 |
| 26.05 | . 8706 | . 93983 | 28.30 | . 9458 | .9758I | 30.55 | 1.0210 | . 00903 |
| 26. IO | . 8723 | . 94066 | 28.35 | . 9475 | . 97657 | 30.60 | 1.0227 | . 00975 |
| 26. 15 | . 8740 | . 94149 | 28.40 | . 9492 | . 97734 | 30.65 | 1.0244 | .oro45 |
| 26.20 | . 8756 | . 94233 | 28.45 | . 9508 | .97810 | 30.70 | 1.0260 | .oril 6 |
| 26.25 | 0.8773 | 9.94315 | 28.50 | 0.9525 | 9.97887 | 30.75 | 1.0277 | 0.01187 |
| 26.30 | . 8790 | . 94398 | 28.55 | . 9542 | . 97963 | 30.80 | 1.0294 | . 01257 |
| 26.35 | . 8806 | . 94480 | 28.60 | . 9558 | . 98039 | 30.85 | 1.0310 | .OI328 |
| 26.40 | . 8823 | . 94563 | 28.65 | . 9575 | .98115 | 30.90 | 1.0327 | . O1398 |
| 26.45 | . 8840 | . 94645 | 28.70 | . 9592 | .98i91 | 30.95 | I. 0344 | . 01468 |
| 26.50 | 0.8857 | 9.94727 | 28.75 | 0.9609 | 9.98266 | 31.00 | 1.0361 | 0.OI539 |
| 26.55 | . 8873 | . 94809 | 28.80 | . 9625 | . 98342 | 31.05 | 1.0377 | . 01608 |
| 26.60 | . 8890 | . 94891 | 28.85 | . 9642 | . 98417 | 31.10 | 1.0394 | . 01678 |
| 26.65 | . 8907 | . 94972 | 28.90 | . 9659 | . 98492 | 3 I .15 | I.04II | .OI748 |
| 26.70 | . 8924 | . 95054 | 28.95 | . 9675 | . 98567 | 31.20 | 1.0427 | .or8i8 |
| 26.75 | 0.8940 | $9.95{ }^{1} 35$ | 29.00 | 0.9692 | 9.98642 | 31.25 | 1.0444 | 0.01887 |
| 26.80 | . 8957 | . 95216 | 29.05 | . 9709 | . 98717 | 3 I .30 | 1.0461 | . 01957 |
| 26.85 | . 8974 | . 95297 | 29. IO | . 9726 | . 98792 | 3 I .35 | I. 0478 | . 02026 |
| 26.90 26.95 | . 8990 | . 95378 | 29.15 | . 9742 | . 98866 | 31.40 | 1.0494 | . 02095 |
| 26.95 | .9007 | . 95458 | 29.20 | . 9759 | .98941 | 31.45 | 1.05II | . 02164 |
| 27.00 | 0.9024 | 9.95539 | 29.25 | 0.9776 | 9.99015 | 31.50 | 1.0528 | 0.02233 |
| 27.05 | . 9040 | . 95619 | 29.30 | . 9792 | . 99089 | 31.55 | 1.0544 | . 02302 |
| 27.10 | . 9057 | . 95699 | 29.35 | . 9809 | . 99163 | 31.60 | 1.0561 | . 02371 |
| 27.15 | . 9074 | . 95779 | 29.40 | . 9826 | . 99237 | 31.65 | 1.0578 | . 02439 |
| 27.20 | .9091 | . 95859 | 29.45 | . 9843 | .993II | 31.70 | 1. 0594 | . 02508 |

TABLE 84.
DENSITY OF AIR AT DIFFERENT TEMPERATURES CENTIGRADE.

$$
\delta_{t, 760}=\frac{0.00129305}{1+0.003670 t} .
$$

I cubic metre of dry air at the temperature $\circ^{\circ} C$. and pressure 760 mm ., and under the standard value of gravity at latitude $45^{\circ}$ and sea level, weighs x .29305 kilogramme.

| t. | $\delta_{t, 760}$ | $\log \delta_{\mathrm{t}, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | 0.00 | - Io | c. | 0.00 | - Io | c. | 0.00 | - 10 |
| $-34^{\circ}$ | 14774 | 7.16950 | $-4.5$ | 13148 | 7.11885 | 18.0 | 12129 | 7.08383 |
| -33 | 14712 | . 16768 | - 4.0 | 13123 | . 11804 | 18.5 | 12108 | 8309 |
| -32 | 14651 | . 16587 | $-3.5$ | 13099 | .11723 | 19.0 | 12088 | 8234 |
| $-3 \mathrm{I}$ | 14590 | . 16407 | $-3.0$ | 13074 | . 11642 | 19.5 | 12067 | 8160 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -30 | 14530 | 7.16227 | - 2.5 | 13050 | 7.11562 | 20.0 | 12046 | 7.08085 |
| -29 | 14471 | . 16049 | 2.0 | 13026 | .11481 | 20.5 | 12026 | 8011 |
| -28 | 14412 | .r5871 | - 1.5 | 13002 | . 11401 | 21.0 | 12005 | 7937 |
| -27 | 14353 | . 15693 | - 1.0 | 12978 | .II32I | 21.5 | 11985 | 7863 |
| -26 | 14295 | . 15517 | - 0.5 | 12954 | . 11241 | 22.0 | 11965 | 7789 |
| -25 | 0.00 I4237 | 7.153 | 0.0 | ${ }_{\text {I }}^{0.00}$ | 7.111 | 22.5 | ${ }_{0}^{0.00} 11944$ | 07716 |
| -24 | 14179 | . 15166 | + 0.5 | 12907 | . 1108 | 23.0 | 11924 | 7642 |
| 23 | 14123 | . 14991 | 1.0 | 12884 | . 11006 | 23.5 | 11904 | 7569 |
| 22 | 14066 | . 14818 | I. 5 | 12860 | . 10923 | 24.0 | 11884 | 7496 |
| 21 | I4010 | . 14645 | 2.0 | 12836 | . 10844 | 24.5 | 11864 | 7422 |
| -20.0 | 0.00 |  |  | 0.00 |  |  | $\stackrel{0.00}{\text { I } 1844}$ |  |
|  | 13955 | 7.14472 | 2.5 | 12813 | 7.1076 | 25.0 | 11844 | 7.07349 |
| - 19.5 | 13927 | . 14386 | 3.0 | 12790 | . 10686 | 25.5 | 11824 | 7276 |
| - 19.0 -18.5 | 13900 13872 | . I 432 I 5 | 3.5 4.0 | 12766 | .10607 | 26.0 26.5 | 11804 11784 | 7204 7131 |
| 8.0 | I3845 | .14130 | 4.5 | 12720 | . 10450 | 27.0 | 11765 | 7058 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| - 17.5 | 13818 | 7.14044 | 5.0 | 12698 | 7.10372 | 27.5 | 11745 | 7.06986 |
| - 17.0 | 13791 | . 13959 | 5.5 | 12675 | . 10294 | 28.0 | 11726 | 6913 |
| - 16.5 | 13764 | . 13874 | 6.0 | 12652 | . 10215 | 28.5 | 11706 | 6841 |
| - 16.0 | 13737 | . 13790 | 6.5 | 12629 | .10138 | 29.0 | 11687 | 6769 |
| - 15.5 | 13710 | . 13705 | 7.0 | 12607 | . 10069 | 29.5 | 11667 | 6697 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| - 15.0 | 13684 | 7.13621 | 7.5 | 12584 | 7.09982 | 30.0 | 11648 | 7.06625 |
| $-14.5$ | 13657 | . 13536 | 8.0 | 12562 | 9905 | 30.5 | 11629 | 6554 |
| - 14.0 | 13631 | . 13452 | 8.5 | 12539 | 9828 | 31.0 | 11610 | 6482 |
| $-13.5$ | 13604 | . 13368 | 9.0 | 12517 | 9750 | 31.5 | 11591 | 6411 6340 |
| - 13.0 | ${ }_{\text {13578 }}$ | . 13285 | 9.5 | ${ }_{0}^{12495}$ | 9673 | 32.0 | ${ }_{0.00}^{11572}$ | 6340 |
| - 12.5 |  | 7.13201 | 10.0 | ${ }^{0.00} 12473$ | 7.09596 | 32.5 | ${ }_{\text {II553 }}^{0.00}$ | 7.06268 |
| - 12.0 | 13526 | . 13117 | 10.5 | 1245 I | 9519 | 33.0 | ${ }^{1} 1534$ | 6197 |
| - II. 5 | ${ }^{1} 3500$ | . 13034 | 11.0 | 12429 | 9443 | 33.5 | 11515 | 6126 |
| - I1.0 | 13473 | . 12951 | 11.5 | 12407 | 9366 | 34.0 | 11496 | 6055 |
| - 10.5 | 13449 | . 12868 | 12.0 | 12385 | $9290^{\circ}$ | 34. | 11477 | 5984 |
| - 10.0 | ${ }_{\text {I }}^{0.00}$ | 7.12785 | 12.5 | ${ }^{0.00} 12363$ | 7.09214 | 35.0 | ${ }_{\text {I }}^{0.00}$ | 7.05913 |
| - 9.5 | I3398 | . 12703 | 13. | 12342 | 9137 | 35.5 | 11440 | 5843 |
| - 9.0 | ${ }_{1} 13372$ | . 12620 | 13.5 | 12320 | 9061 | 36.0 | 11421 | 5772 |
| -8.5 | ${ }_{1} 13347$ | . 12538 | 14.0 | 12299 | 8986 | 36.5 | 11403 | 5702 |
| - 8.0 | ${ }^{1} 13322$ | . 12456 | 14.5 | ${ }_{\text {o. }} 12277$ | 8910 | 37.0 | ${ }_{\text {I }}^{11} 388$ | 5632 |
| - 7.5 | -0.00 | 7.12374 | 15.0 | 0.00 I2256 | 7.08834 | 37.5 |  | 7.05562 |
| - 7.0 | 13271 | . 12292 | 15.5 | 12235 | 8759 | 38.0 | r1348 | 5492 |
| - 6.5 | 13246 | . 12210 | 16.0 | 12213 | 8683 | 38.5 | 11330 | 5422 |
| - 6.0 | 13222 | . 12128 | 16.5 | 12192 | 8608 | 39.0 | 11311 | 5352 |
| - 5.5 | 13197 | . 12047 | 17.0 | 12171 | 8533 | 39.5 | 11293 | 5282 |
| - 5.0 | ${ }_{\text {- }}^{0.00} 13172$ | 7.11966 | 17.5 | ${ }_{12150}^{0.00}$ | 7.08458 | 40.0 | ${ }^{0.00} 11275$ | 7.05213 |

TAble 84
DENSITY OF AIR AT DIFFERENT TEMPERATURES CENTIGRADE.
(Continued.)

| t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{\text {t, } 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | 0.00 | - 10 | c. | 0.00 | - 10 | C. | 0.00 | - 10 |
| $40^{\circ}$ | 11275 | 7.05213 | $50^{\circ}$ | 10926 | 7.03845 | $60^{\circ}$ | 10597 | 7.02518 |
| 41 | 11239 | . 05074 | 5 I | 10892 | . 03710 | 6I | 10565 | . 02388 |
| 42 | 11204 | . 04936 | 52 | IoS58 | . 03576 | 62 | 10534 | . 02258 |
| 43 | 11168 | . 04798 | 53 | 10825 | . 03443 | 63 | 10502 | . 02128 |
| 44 | III33 | . 04660 | 54 | 10792 | . 03309 | 64 | 10471 | .OI999 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 45 | 11098 | 7.04523 | 55 | 10759 | 7.03177 | 65 | , I0440 | 7.01870 |
| 46 | $1 \mathrm{I}_{0} 63$ | . 04387 | 56 | 10726 | . 03044 | 66 | 10489 | .or742 |
| 47 | 11028 | .0425I | 57 | 10694 | . 02912 | 67 | 10379 | .OI6I4 |
| 48 | 10994 | .04115 | 58 | 10661 | . 02780 | 68 | 10348 | .OI486 |
| 49 | 10960 | .03980 | 59 | 10629 | . 02649 | 69 | 10318 | . OI 358 |

TABLE 85.
DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES. METRIC MEASURES.
Term for humidity: values of $0.378 e$. Auxiliary to Table 86.
$\rho=$ vapor pressure in mm .

| Dewpoint. | Vapor Pressure. $e$ | $0.378 e$ | Dewpoint. | Vapor Pressure. $e$ | 0.378 e | Dewpoint. | Vapor Pressure. $e$ | $0.378 e$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | mm . | mm . | c. | mm . | mm . | c. | mm. | mm. |
| $-30^{\circ}$ | 0.38 | o. 14 | $0^{\circ}$ | 4.57 | 1.73 | $30^{\circ}$ | 31.51 | II.9I |
| 29 | . 42 | . 16 | I | $4 \cdot 91$ | 1.86 | 3 I | 33.37 | 12.61 |
| 28 | . 46 | . 17 | 2 | 5.27 | I. 99 | 32 | $35 \cdot 32$ | 13.35 |
| 27 | . 50 | . 19 | 3 | 5.66 | 2. 14 | 33 | $37 \cdot 37$ | 14. I3 |
| 26 | . 55 | . 21 | 4 | 6.07 | 2.29 | 34 | 39.52 | 14.94 |
| $-25$ | 0.61 | 0.23 | 5 | 6.51 | 2.46 | 35 | 4 I .78 | 15.79 |
| 24 | . 66 | . 25 | 6 | 6.97 | 2.63 | 36 | 44.16 | 16.69 |
| 23 | . 73 | . 28 | 7 | 7.47 | 2.82 | 37 | 46.65 | 17.63 |
| 22 | . 79 | . 30 | 8 | 7.99 | 3.02 | 38 | 49.26 | 18.62 |
| 21 | . 87 | . 33 | 9 | 8.55 | 3.23 | 39 | 52.00 | 19.66 |
| $-20$ | 0.94 | 0. 36 | 10 | 9.14 | 3.45 | 40 | 54.87 | 20.74 |
| 19 | 1.03 | . 39 | 11 | 9.77 | 3.69 | 41 | 57.87 | 21.86 |
| 18 | 1.12 | . 42 | 12 | 10.43 | 3.94 | 42 | 61.02 | 23.06 |
| 17 | 1.22 | . 46 | 13 | II. 14 | 4.21 | 43 | 64.31 | 24.31 |
| 16 | 1.32 | . 50 | 14 | II. 88 | 4.49 | 44 | 67.76 | 25.61 |
| $-15$ | I. 44 | 0.54 | 15 | 12.67 | 4.79 | 45 | 71.36 | 26.97 |
| 14 | 1.56 | . 59 | 16 | 13.51 | 5.11 | 46 | 75.13 | 28.40 |
| 13 | I. 69 | . 64 | 17 | 14.40 | 5.44 | 47 | 79.07 | 29.89 |
| 12 | I. 84 | . 70 | 18 | 15.33 | 5.79 | 48 | 83.19 | 31.45 |
| II | 1.99 | . 75 | 19 | 16.32 | 6.17 | 49 | 87.49 | 33.07 |
| $-10$ | 2. I5 | 0.81 | 20 | 17.36 |  | 50 | 91.98 | 34.77 |
| 9 | 2.33 | . 88 | 21 | 18.47 | 6.98 | 51 | 96.66 | 36.54 |
| 8 | 2.51 | . 95 | 22 | 19.63 | 7.42 | 52 | 101.55 | 38.39 |
| 7 | 2.72 | 1.03 | 23 | 20.86 | 7.89 | 53 | 106.65 | 40.31 |
| 6 | 2.93 | I.II | 24 | 22.15 | 8.37 | 54 | III. 97 | 42.32 |
| $-5$ | 3.16 | I. 19 | 25 | 23.52 | 8.89 | 55 | 117.52 | 44.42 |
| 4 | 3.41 | I. 29 | 26 | 24.96 | 9.43 | 56 | 123.29 | 46.60 |
| 3 | 3.67 | I. 39 | 27 | $26.47{ }^{\circ}$ | Io.OI | 57 | 129.31 | 48.88 |
| 2 | 3.95 | 1.49 | 28 | 28.07 | 10.61 | 58 | I 35.58 | 51.25 |
| I | 4.25 | 1.6I | 29 | 29.74 | 11.24 | 59 | 142.10 | 53.71 |

Smithsonian Tables.

TAble 86.
DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES. METRIC MEASURES.
Values of $\frac{h}{760}$.

$$
\frac{\delta}{\delta_{0}}=\frac{h}{760}=\frac{b-0.378 e}{760}
$$

$b=$ Barometric pressure in mm.; $e=$ Vapor pressure in mm .

| h. | $\frac{\mathrm{h}}{760}$. | $\log \frac{h}{760}$. | h. | $\frac{h}{760}$. | Log $\frac{h}{760}$. | h. | $\frac{\mathrm{h}}{760}$. | Log $\frac{\mathrm{h}}{760}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm. |  | - 10 | mm. |  | Io | mm. |  | o |
| 300 | 0.3947 | 9.59631 | 400 | 0.5263 | 9.72125 | 450 | 0.5921 | 9.77240 |
| 302 | -3974 | . 59919 | 401 | . 5276 | . 72233 | 451 | . 5934 | . 77336 |
| 304 | . 4000 | . 60206 | 402 | . 5289 | .72341 | 452 | . 5947 | . 77432 |
| 306 | . 4026 | . 60491 | 403 | . 5303 | . 72449 | 453 | .5961 | . 77528 |
| 308 | . 4053 | . 60774 | 404 | .5316 | . 72557 | 454 | . 5974 | . 77624 |
| 310 | 0.4079 | 9.61055 | 405 | 0.5329 | 9.72664 | 455 | 0.5987 | 9.77720 |
| 312 | .4105 | .61334 | 406 | . 5342 | .72771 | 456 | . 6000 | .77815 |
| 314 | .4132 | . 61612 | 407 | . 5355 | . 72878 | 457 | . 6013 | .77910 |
| 316 | .4158 | . 61887 | 408 | . 5369 | . 72985 | 458 | . 6026 | .78005 |
| 318 | -4184 | .62161 | 409 | . 5382 | .73091 | 459 | . 6040 | .78100 |
| 320 | 0.4211 | 9.62434 | 410 | 0.5395 | 9.73197 | 460 | 0.6053 | 9.78194 |
| 322 | . 4237 | . 62704 | 411 | . 5408 | . 73303 | 461 | . 6066 | . 78289 |
| 324 | . 4263 | . 62973 | 412 | . 5421 | . 73408 | 462 | . 6079 | . 78383 |
| 326 | . 4289 | . 63240 | 413 | . 5434 | . 73514 | 463 | . 6092 | .78477 |
| 328 | .4316 | . 63506 | 414 | . 5447 | . 73619 | 464 | .6105 | . 78570 |
| 330 | 0.4342 | 9.63770 | 415 | 0.5461 | 9.73723 | 465 | 0.6118 | 9.78664 |
| 332 | . 4368 | . 64032 | 416 | . 5474 | . 73828 | 466 | .6132 | . 78757 |
| 334 | . 4395 | . 64293 | 417 | . 5487 | . 73932 | 467 | .6145 | . 78850 |
| 336 | .442I | . 64552 | 418 | . 5500 | . 74036 | 468 | .6158 | . 78943 |
| 338 | . 4447 | .64810 | 419 | .5513 | . 74140 | 469 | .6171 | . 79036 |
| 340 | 0.4474 | 9.65066 | 420 | 0.5526 | 9.74244 | 470 | 0.6184 | 9.79128 |
| 342 | . 4500 | . 6532 I | 421 | . 5540 | . 74347 | 47 I | .6197 | .7922I |
| 344 | -4526 | . 65574 | 422 | . 5553 | . 74450 | 472 | . 6210 | .79313 |
| 346 | -4553 | . 65826 | 423 | . 5566 | . 74553 | 473 | . 6224 | . 79405 |
| 348 | . 4579 | . 66076 | 424 | . 5579 | . 74655 | 474 | . 6237 | . 79496 |
| 350 | 0.4605 | 9.66325 | 425 | 0. 5592 | 9.74758 | 475 | 0.6250 | 9.79588 |
| 352 | . 4632 | . 66573 | 426 | . 5605 | . 74860 | 476 | . 6263 | . 79679 |
| 354 | . 4658 | . 66819 | 427 | . 5618 | .74961 | 477 | . 6276 | . 79770 |
| 356 | . 4684 | . 67064 | 428 | . 5632 | . 75063 | 478 | . 6289 | .79861 |
| 358 | .471I | . 67307 | 429 | . 5645 | . 75164 | 479 | . 6303 | .7995 ${ }^{2}$ |
| 360 | 0.4737 | 9.67549 | 430 | 0. 5658 | 9.75265 | 480 | 0.6316 | 9.80043 |
| 362 | . 4763 | . 67790 | 431 | . 5671 | . 75366 | 48 I | . 6329 | . 80133 |
| 364 | . 4789 | . 68029 | 432 | . 5684 | . 75467 | 482 | . 6342 | . 80223 |
| 366 | .4816 | . 68267 | 433 | . 5697 | . 75567 | 483 | . 6355 | . 80313 |
| 368 | . 4842 | . 68503 | 434 | . 5711 | . 75668 | 484 | . 6368 | . 80403 |
| 370 | 0.4868 | 9.68739 | 435 | 0.5724 | 9.75768 | 485 | 0. 6382 | 9.80493 |
| 372 | . 4895 | . 68973 | 436 | . 5737 | . 75867 | 486 | . 6395 | . 80582 |
| 374 | .492I | . 69206 | 437 | . 5750 | . 75967 | 487 | . 6408 | . 80672 |
| 376 | -4947 | . 69437 | 438 | . 5763 | . 76066 | 488 | . 642 I | . 80761 |
| 378 | . 4974 | . 69668 | 439 | . 5776 | . 76165 | 489 | . 6434 | . 80850 |
| 380 | 0.5000 | 9.69897 | 440 | 0.5790 | 9.76264 | 490 | 0.6447 | 9.80938 |
| 382 | . 5026 | .70125 | 44 I | . 5803 | . 76362 | 49 I | .6461 | . 81027 |
| 384 | . 5053 | . 70352 | 442 | . 5816 | . 76461 | 492 | . 6474 | .81115 |
| 386 | . 5079 | . 70577 | 443 | . 5829 | . 76559 | 493 | . 6487 | .81203 |
| 388 | . 5105 | . 70802 | 444 | . 5842 | . 76657 | 494 | .6500 | .81291 |
| 390 | 0.5132 | 9.71025 | 445 | 0. 5855 | 9.76755 | 495 | 0.6513 | 9.81379 |
| 392 | . 5158 | . 71247 | 446 | . 5868 | . 76852 | 496 | . 6526 | . 81467 |
| 394 | . 5184 | . 71468 | 447 | . 5882 | . 76949 | 497 | . 6540 | . 81556 |
| 396 | .5211 | . 71688 | 448 | . 5895 | . 77046 | 498 | . 6553 | .81642 |
| 398 | . 5237 | .71907 | 449 | . 5908 | . 77143 | 499 | . 6566 | .81729 |

TABLE 86.
DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES. METRIC MEASURES.
Values of ${ }_{760^{h}}{ }^{\boldsymbol{h}} \quad \frac{\delta}{\delta_{0}}=\frac{h}{760}=\frac{b-0.378 e}{760}$.
$b=$ Barometric pressure in mm.; $e=$ Vapor pressure in mm .

| h. | $\frac{h}{760}$. | $\log \frac{h}{760}$. | h. | $\frac{h}{760}$. | $\log \frac{h}{760}$. | h. | $\frac{\mathrm{h}}{760}$. | $\log \frac{h}{760}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm . |  | - 10 | mm . |  | - 10 | mm . |  | - 10 |
| 500 | 0.6579 | 9.81816 | 550 | 0.7237 | 9.85955 | 600 | 0.7895 | 9.89734 |
| 501 | . 6592 | .81902 | 551 | . 7250 | . 86034 | 601 | . 7908 | . 89806 |
| 502 | . 6605 | .81989 | 552 | . 7263 | .86112 | 602 | .7921 | . 89878 |
| 503 | .66I8 | . 82075 | 553 | . 7276 | .86191 | 603 | . 7934 | . 89950 |
| 504 | . 6632 | . 82162 | 554 | . 7290 | . 86270 | 604 | . 7947 | .90022 |
| 505 | 0.6645 | 9.82248 | 555 | 0.7303 | 9.86348 | 605 | 0.7961 | 9.90094 |
| 506 | . 6658 | . 82334 | 556 | . 7316 | . 86426 | 606 | . 7974 | . 90166 |
| 507 | . 6671 | . 82419 | 557 | . 7329 | . 86504 | 607 | . 7987 | . 90238 |
| 508 | . 6684 | . 82505 | 558 | . 7342 | . 86582 | 608 | . 8000 | . 90309 |
| 509 | . 6697 | . 82590 | 559 | . 7355 | . 86660 | 609 | . 8013 | . 90380 |
| 510 | 0.67 II | 9.82676 | 560 | 0. 7368 | 9.86737 | 610 | 0.8026 | 9.90452 |
| 511 | . 6724 | . 82761 | 561 | . 7382 | .86815 | 6II | . 8040 | . 90523 |
| 512 | . 6737 | . 82846 | 562 | . 7395 | . 86892 | 612 | . 8053 | . 90594 |
| 513 | . 6750 | . 82930 | 563 | . 7408 | . 86969 | 613 | . 8066 | . 90665 |
| 514 | . 6763 | .83015 | 564 | . 742 I | . 87046 | 614 | . 8079 | . 90735 |
| 515 | 0.6776 | 9.83099 | 565 | 0.7434 | 9.87123 | 615 | 0.8092 | 9.90806 |
| 516 | . 6789 | . 83184 | 566 | . 7447 | . 87200 | 616 | .8105 | . 90877 |
| 517 | . 6803 | . 83268 | 567 | . 7461 | . 87277 | 617 | .8Ir8 | . 90947 |
| 518 | .6816 | . 83352 | 568 | . 7474 | . 87353 | 618 | .8I32 | .91017 |
| 519 | . 6829 | . 83435 | 569 | . 7487 | . 87430 | 619 | .8145 | .91088 |
| 520 | 0.6842 | 9.83519 | 570 | 0.7500 | 9.87506 | 620 | o.8158 | 9.91158 |
| 521 | . 6855 | . 83602 | 571 | .7513 | . 87582 | 621 | .8171 | .91228 |
| 522 | . 6869 | . 83686 | 572 | . 7526 | . 87658 | 622 | .8184 | -91298 |
| 523 | . 6882 | . 83769 | 573 | . 7540 | . 87734 | 623 | .8197 | .91367 |
| 524 | . 6895 | . 83852 | 574 | . 7553 | .87810 | 624 | .82II | .91437 |
| 525 | 0.6908 | 9.83934 | 575 | 0.7566 | 9.87885 | 625 | 0.8224 | 9.91507 |
| 526 | .692I | . 84017 | 576 | . 7579 | . 87961 | 626 | . 8237 | .91576 |
| 527 | . 6934 | . 84100 | 577 | . 7592 | . 88036 | 627 | . 8250 | . 91645 |
| 528 | . 6947 | . 84182 | 578 | . 7605 | .88III | 628 | . 8263 | .91715 |
| 529 | .696I | . 84264 | 579 | .76I8 | .88I86 | 629 | . 8276 | .91784 |
| 530 | 0.6974 | 9.84346 | 580 | 0.7632 | 9.8826 I | 630 | 0.8289 | 9.91853 |
| 531 | . 6987 | . 84428 | 581 | . 7645 | . 883336 | 631 | . 8303 | . 91922 |
| 532 | . 7000 | . 84510 | 582 | . 7658 | .884II | 632 | . 8316 | . 91990 |
| 533 | .7013 | . 84591 | 583 | . 7671 | . 88486 | 633 | . 8329 | . 92059 |
| 534 | . 7026 | . 84673 | 584 | .7684 | . 88560 | 634 | . 8342 | .92128 |
| 535 | 0.7040 | 9.84754 | 585 | 0.7697 | 9.88634 | 635 | 0.8355 | 9.92196 |
| 536 | . 7053 | . 84835 | 586 | .771 I | . 88708 | 636 | . 8368 | . 92264 |
| 537 | . 7066 | . 84916 | 587 | . 7724 | . 88782 | 637 | . 8382 | . 92332 |
| 538 | . 7079 | . 84997 | 588 | . 7737 | . 88856 | 638 | . 8395 | .92401 |
| 539 | .7092 | . 85078 | 589 | . 7750 | . 88930 | 639 | . 8408 | . 92469 |
| 540 | 0.7105 | 9.85158 | 590 | 0.7763 | 9.89004 | 640 | 0.842I |  |
| 541 | . 7118 | . 85238 | 591 | . 7776 | . 89077 | 641 | . 8434 | . 92604 |
| 542 | .7132 | . 85318 | 592 | .7789 | .8915I | 642 | . 8447 | . 92672 |
| 543 | . 7145 | . 85399 | 593 | .7803 | . 89224 | 643 | . 8461 | . 92740 |
| 544 | .7158 | . 85478 | 594 | .7816 | . 89297 | 644 | . 8474 | .92807 |
| 545 | 0.7171 | 9.85558 | 595 | 0.7829 | 9.89370 | 645 | 0.8487 | 9.92875 |
| 546 | . 7184 | . 85638 | 596 | .7842 | . 89443 | 646 | . 8500 | . 92942 |
| 547 | . 7197 | . 85717 | 597 | .7855 | . 89516 | 647 | . 8513 | . 93009 |
| 548 | .7211 | . 85797 | 598 | . 7868 | . 89589 | 648 | . 8526 | . 93076 |
| 549 | .7224 | . 85876 | 599 | .7882 | . 89662 | 649 | . 8539 | .93143 |

TABLE 86.
DENSITY OF AIR AT DIFFERENT HUMIDITIES AND PRESSURES. METRIC MEASURES.

Values of ${ }_{760^{\mathrm{h}}}$.

$$
\frac{\delta}{\delta_{o}}=\frac{h}{760}=\frac{b-0.378 e}{760}
$$

$b=$ Barometric pressure in mm.; $e=$ Vapor pressure in mm.

| h. | $\frac{\mathrm{h}}{760}$. | Log $\frac{\mathrm{h}}{760}$. | h. | $\frac{\mathrm{h}}{760}$. | $\log \frac{\mathrm{h}}{760}$. | h. | $\frac{\mathrm{h}}{760}$. | Log $\frac{\mathrm{h}}{760}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm. |  | - 10 | mm. |  | - 10 | mm. |  | - 10 |
| 650 | 0. 8553 | 9.93210 | 700 | 0.9211 | 9.96428 | 750 | 0. 9868 | 9.99425 |
| 651 | . 8566 | .93277 | 701 | . 9224 | . 96490 | 751 | . 9882 | . 99483 |
| 652 | . 8579 | .9334I | 702 | . 9237 | . 96552 | 752 | . 9895 | . 99540 |
| 653 | . 8592 | .93410 | 703 | . 9250 | . 96614 | 753 | . 9908 | . 99598 |
| 654 | . 8605 | . 93476 | 704 | . 9263 | . 96676 | 754 | .992I | . 99656 |
| 655 | 0.8618 | 9.93543 | 705 | 0.9276 | 9.96738 | 755 | 0.9934 | 9.99713 |
| 656 | . 8632 | . 93609 | 706 | . 9289 | . 96799 | 756 | . 9947 | . 9977 I |
| 657 | . 8645 | . 93675 | 707 | . 9303 | . 96860 | 757 | .9961 | . 99828 |
| 658 | . 8658 | .9374I | 708 | .9316 | . 96922 | 758 | . 9974 | . 99886 |
| 659 | . 8671 | . 93807 | 709 | . 9329 | . 96983 | 759 | . 9987 | . 99943 |
| 660 | 0.8684 | 9.93873 | 710 | 0.9342 | 9.97044 | 760 | 1.0000 | 0.00000 |
| 661 | . 8697 | . 93939 | 711 | . 9355 | .97106 | 761 | . 0013 | . 00057 |
| 662 | . 8711 | . 94004 | 712 | . 9368 | . 97167 | 762 | . 0026 | . 00114 |
| 663 | . 8724 | . 94070 | 713 | . 9382 | . 97228 | 763 | . 0039 | .00171 |
| 664 | . 8737 | .94I35 | 714 | . 9395 | . 97288 | 764 | . 0053 | . 00228 |
| 665 | 0.8750 | 9.94201 | 715 | 0.9408 | 9.97349 | 765 | 1.0066 | 0.00285 |
| 666 | . 8763 | . 94266 | 716 | . 942 I | . 97410 | 766 | . 0079 | . 00342 |
| 667 | . 8776 | . 94331 | 717 | . 9434 | . 97470 | 767 | . 0092 | . 00398 |
| 668 | . 8790 | . 94396 | 718 | . 9447 | .9753I | 768 | . 0105 | . 00455 |
| 669 | . 8803 | .9446I | 719 | .946I | . 97592 | 769 | . 118 | . 00515 |
| 670 | 0.8816 | 9.94526 | 720 | 0.9474 | 9.97652 | 770 | I.OI32 | 0.00568 |
| 671 | . 8829 | . 94591 | 721 | . 9487 | . 97712 | 771 | .or45 | . 00624 |
| 672 | . 8842 | . 94656 | 722 | . 9500 | . 97772 | 772 | . 0158 | . 00680 |
| 673 | . 8855 | . 94720 | 723 | .9513 | . 97832 | 773 | .0171 | . 00736 |
| 674 | . 8869 | . 94785 | 724 | . 9526 | . 97892 | 774 | .or84 | . 00793 |
| 675 | 0.8882 | 9.94849 | 725 | 0.9539 | $9.9795{ }^{2}$ | 775 | 1.0197 | 0.00849 |
| 676 | . 8895 | .94913 | 726 | . 9553 | .98012 | 776 | . 0211 | .00905 |
| 677 | . 8908 | . 94978 | 727 | . 9566 | . 98072 | 777 | . 0224 | .0096I |
| 678 | . 8921 | . 95042 | 728 | . 9579 | . 98132 | 778 | . 0237 | . 01017 |
| 679 | . 8934 | .95106 | 729 | . 9592 | .98191 | 779 | . 0250 | .01072 |
| 680 | 0.8947 | 9.95170 | 730 | 0.9605 | 9.98250 | 780 | 1.0263 | 0.01128 |
| 681 | . 8960 | . 95233 | 731 | . 9618 | . 98310 | 781 | . 0276 | .ori84 |
| 682 | . 8974 | . 95297 | 732 | . 9632 | . 98370 | 782 | . 0289 | .O1239 |
| 683 | . 8987 | .95361 | 733 | . 9645 | . 98429 | 783 | . 0303 | .OI295 |
| 684 | . 9000 | . 95424 | 734 | . 9658 | . 98488 | 784 | . 0316 | .oI350 |
| 685 | 0.9013 | 9.95488 | 735 | 0.967 I | 9.98547 | 785 | 1.0329 | 0.01406 |
| 686 | . 9026 | .95551 | 736 | . 9684 | . 98606 | 786 | . 0342 | . 01461 |
| 687 | . 9039 | . 95614 | 737 | . 9697 | . 98665 | 787 | . 0355 | .orsi6 |
| 688 | . 9053 | . 95677 | 738 | .9711 | . 98724 | 788 | . 0368 | .0157I |
| 689 | . 9066 | . 95740 | 739 | . 9724 | . 98783 | 789 | . 0382 | .oi626 |
| 690 | 0.9079 | 9.95804 | 740 | 0.9737 | 9.98842 | 790 | 1.0395 | 0.01681 |
| 691 | . 9092 | . 95866 | 741 | . 9750 | . 98900 | 791 | . 0408 | . 01736 |
| 692 | .9105 | . 95929 | 742 | . 9763 | . 98959 | 792 | . 042 I | .oI791 |
| 693 | .9118 | . 95992 | 743 | . 9776 | . 99018 | 793 | . 0434 | .o1846 |
| 694 | .9132 | . 96054 | 744 | . 9789 | . 99076 | 794 | . 0447 | .01901 |
| 695 | 0.9145 | 9.96117 | 745 | 0.9803 | 9.99134 | 795 | 1.0461 | 0.01955 |
| 696 | . 9158 | . 96180 | 746 | . 9816 | . 99192 | 796 | . 0474 | . 02010 |
| 697 | .9171 | . 96242 | 747 | . 9829 | . 99251 | 797 | . 0487 | . 02064 |
| 698 | .9184 | . 96304 | 748 | . 9842 | . 99309 | 798 | . 0500 | . 02119 |
| 699 | .9197 | . 96366 | 749 | . 9855 | . 99367 | 799 | .0513 | . 02173 |

## AVOIRDUPOIS POUNDS AND OUNCES INTO KILOGRAMMES.

I avoirdupois pound $=0.4535924$ kilogramme.
I avoirdupois ounce $=0.0283495$ kilogramme.

| Pounds. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | kg. | kg. | kg. | kg . | kg. | kg. | kg. | kg. | kg. | kg. |
| 0 | 0.0000 | 0.0454 | 0.0907 | 0.1361 | 0.1814 | 0.2268 | 0.2722 | 0.3175 | 0.3629 | 0.4082 |
| 1 | 0.4536 | 0.4990 | 0.5443 | 0.5897 | 0.6350 | 0.6804 | 0.7257 | 0.77 II | 0.8165 | 0.8618 |
| 2 | 0.9072 | 0.9525 | 0.9979 | 1.0433 | 1. 0886 | I. 1340 | 1.1793 | 1.2247 | 1.2701 | I.3154 |
| 3 | 1.3608 | 1.4061 | 1.4515 | I. 4969 | 1.5422 | I. 5876 | 1.6329 | 1.6783 | 1.7237 | 1.7690 |
| 4 | 1.8144 | 1. 8597 | 1.905 1 | 1.9504 | I. 9958 | 2.0412 | 2.0865 | 2.1319 | 2.1772 | 2.2226 |
| 5 | 2.2680 | 2.3133 | 2.3587 | 2.4040 | 2.4494 | 2.4948 | 2.5401 | 2.5855 | 2.6308 | 2.6762 |
| 6 | 2.7216 | 2.7669 | 2.8123 | 2.8576 | 2.9030 | 2.9484 | 2.9937 | 3.0391 | 3.0844 | 3.1298 |
| 7 | 3.175I | 3.2205 | 3.2659 | 3.3112 | 3.3566 | 3.4019 | 3.4473 | 3.4927 | 3.5380 | 3.5834 |
| 8 | 3.6287 | 3.6741 | 3.7195 | 3.7648 | 3.8102 | 3.8555 | 3.9009 | 3.9463 | 3.9916 | 4.0370 |
| 9 | 4.0823 | 4.1277 | 4.173 I | 4.2184 | 4.2638 | 4.3091 | 4.3545 | 4.3998 | 4.4452 | 4.4906 |
| Ounces. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
|  | kg . | kg. | kg. | kg. | kg. | kg. | kg. | kg . | kg. | kg. |
| 0 | 0.0000 | 0.0028 | 0.0057 | 0.0085 | 0.0113 | 0.0142 | 0.0170 | 0.0198 | 0.0227 | 0.0255 |
| 1 | . 0283 | .0312 | . 0340 | . 0369 | . 0397 | . 0425 | . 0454 | . 0482 | . 0510 | . 0539 |
| 2 | . 0567 | . 0595 | . 0624 | . 0652 | .0680 | . 0709 | . 0737 | . 0765 | . 0794 | . 0822 |
| 3 | . 0850 | .0879 | . 0907 | . 0936 | . 0964 | . 0992 | . 1021 | . 1049 | . 1077 | . 1106 |
| 4 | . 1134 | . 1162 | .ri9I | . 1219 | . 1247 | . 1276 | . 1304 | . 1332 | . 136 I | . 1389 |
| 5 | 0.1417 | 0.1446 | 0.1474 | 0. 1503 | 0.153I | O. 1559 | 0.1588 | 0.1616 | 0. 1644 | -. 1673 |
| 6 | .1701 | . 1729 | . 1758 | . 1786 | .18I4 | . 1843 | .1871 | . 1899 | . 1928 | . 1956 |
| 7 | . 1984 | . 2013 | . 2041 | . 2070 | . 2098 | . 2126 | . 2155 | . 2183 | . 22 II | . 2240 |
| 8 | . 2268 | . 2296 | . 2325 | . 2353 | . 2381 | .2410 | . 2438 | . 2466 | . 2495 | . 2523 |
| 9 | . 2551 | .2580 | . 2608 | . 2637 | . 2665 | . 2693 | . 2722 | . 2750 | . 2778 | . 2807 |
| 10 | 0.2835 | 0.2863 | 0.2892 | 0.2920 | 0.2948 | 0.2977 | 0.3005 | 0.3033 | 0.3062 | 0.3090 |
| 11 | . 3118 | . 3147 | . 3175 | . 3203 | . 3232 | . 3260 | . 3289 | . 3317 | . 3345 | . 3374 |
| 12 | - 3402 | . 3430 | - 3459 | - 3487 | -3515 | - 3544 | . 3572 | . 3600 | . 3629 | . 3657 |
| 13 | . 3685 | . 3714 | . 3742 | . 3770 | - 3799 | . 3827 | .3856 | . 3884 | .3912 | . 394 I |
| 14 | . 3969 | . 3997 | . 4026 | . 4054 | . 4082 | .4III | . 4139 | .4167 | .4196 | . 4224 |
| 15 | .4252 | .428r | . 4309 | . 4337 | .4366 | . 4394 | .4423 | .445 ${ }^{\text {I }}$ | . 4479 | . 4508 |

Emthionian Tables.

Table 88.
KILOGRAMMES INTO AVOIRDUPOIS POUNDS AND OUNCES.
I kilogramme $=\mathbf{2 . 2 0 4 6 2 2}$ avoirdupois pounds.


Table 89.

## GRAINS INTO GRAMMES.

I grain $=0.06479892$ gramme.


Smithbonian Tableg.

GRAMMES INTO GRAINS.
TAble 90.

I gramme $=15.43235$ I grains.


TAble 91.
CONVERSION OF UNITS OF MAGNETIC INTENSITY.

| English Units. | Dynes. | Dynes. | English Units. |
| :---: | :---: | :---: | :---: |
| 1 | 0.046108 | 0.1 | 2.16882 |
| 2 | .092216 | .2 | 4.33764 |
| 3 | .138324 | .5 | 8.60646 |
| 4 | .184432 | .4 |  |
| $\mathbf{5}$ | 0.230540 | 0.5 | 10.84410 |
| 6 | .276648 | .6 | 13.01292 |
| 7 | .322756 | .7 | 15.18174 |
| 8 | .368864 | .8 | 17.35056 |
| 9 | .414972 | .9 | 19.51938 |

The English unit of magnetic intensity is the force which acting for 1 second on a unit of magnetism, associated with a mass of I grain, produces a velocity of $I$ foot per second.
The C. G. S. unit of magnetic intensity is the dyne-the force which, acting on one gramme for one second, generates a velocity of $I$ centimetre per second.
The dimensions of magnetic intensity are $\left[M^{\frac{1}{3}} / L^{\frac{1}{2}} T\right]$.

TAble 92.
QUANTITY OF RAINFALL CORRESPONDING TO GIVEN DEPTHS.
r inch of rainfall $=22624.0417$ imperial gallons per acre. $\quad 1$ inch of rainfall $=113.3068$ tons per acre.

$$
=226613.713 \mathrm{lbs} . \text { per acre. }
$$

$=72516.3^{8} 78$ tons persq. mile.

| $\begin{gathered} \text { Depth } \\ \text { of } \\ \text { Rainfall. } \end{gathered}$ | Imperial Gallons per acre. | Tons per square Mile. | Depth of <br> Rainfall. | Imperial Gallons per acre. | Tons per square Mile. | Depth of Rainfall. | Imperial Gallons per acre. | Tons per square Mile. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. <br> 0.00 |  |  | Inches. $0.20$ |  |  | Inches. $0.40$ |  |  |
| . OI | 226.24 | 725.16 | . 21 | 4751.04 | 15228.44 | 0.40 .41 | 9275.85 |  |
| . 02 | 452.48 | 14.50 .32 | . 22 | 4977 . 28 | 1 5953.60 | . 42 | 9502.09 | 30456.88 |
| . 03 | 678.72 | 2175.49 | . 23 | $5203 \cdot 52$ | 1667S.76 | . 43 | 9728.33 | 31182.04 |
| . 04 | 904.96 | 2900.65 | . 24 | $5429 \cdot 77$ | 17403.93 | . 44 | 9954.57 | 31907.21 |
| 0.05 | 1131.20 | 3625.8 I | 0.25 | $5656 . \mathrm{ol}$ | 18129.09 | 0.45 | 10180.8r | 32632.37 |
| . 06 | 1357.44 | 4350.98 | . 26 | 5882.25 | 18854.26 | . 46 | 10407.05 | 33357.53 |
| . 07 | 1583.68 | 5076.14 | . 27 | 6108.49 | 19579.42 | . 47 | 10633.29 | 34082.70 |
| . 08 | 1809.92 | $5 \mathrm{SOI} \cdot 31$ | . 28 | $6334 \cdot 73$ | 20304.58 | . 48 | 10859.53 | 34807.86 |
| . 09 | 2036.16 | 6526.47 | . 29 | 6560.97 | 21029.75 | . 49 | $11085 \cdot 77$ | 35533.03 |
| 0.10 | 2262.40 | 7251.63 | 0.30 | 6787.21 | 21754.91 | 0.50 | 11312.02 | 36258.19 |
| . 11 | 2488.64 | 7976.80 | . 31 | 7013.45 | 22480.08 | . 60 | 13574.42 | 43.509 .83 |
| . 12 | 2714.88 | 8701.96 | . 32 | 7239.69 | 23205.24 | . 70 | 15836.82 | 5076ı. 47 |
| . 13 | 2941.12 | 9427.13 | - 33 | 7465.93 | 23930.40 | . 80 | 18099.23 | 58013.11 |
| . 14 | 3167:36 | 10152.29 | . 34 | 7692.17 | 24655.57 | . 90 | 20361.63 | 6526474 |
| 0.15 | 3393.60 | 10877.45 | 0.35 | 79 I 8.41 | 25380.73 | 1.00 | 22624.04 | 72516.38 |
| . 16 | 3619.84 | 11602.62 | -36 | 8144.65 | 26105.89 | 2.00 | 45248.08 | 145032.77 |
| . 17 | 3846.08 | 12327.78 | . 37 | 8370.89 | 26831.06 | 3.00 | 67872.12 | 217549.16 |
| . 18 | 4072.32 | 13052.94 | -38 | 8597.13 | 275.56 .22 | 4.00 | 90496.16 | 290065.55 |
| . 19 | 4298.56 | 13778.11 | . 39 | $8823 \cdot 37$ | 2828I. 39 | 5.00 | 113120.20 | 362581.93 |
| 0.20 | 4524.80 | 14503.27 | 0.40 | 9049.6I | 29006. 55 | 6.00 | 1 35744.24 | 435098. 32 |

TABLE 93.
DATES OF DOVE'S PENTADES.

| No. of Pentade. | Epoch of the Year. | No. ${ }^{\circ} \mathrm{P}$ tade | Epoch of the Year. | No. of Pen- tade | Epoch of the Year. | No. of Pen- tade | Epoch of the Year. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Jan. I to 5 | 19 | Apr. I to 5 | 37 | June 30 to July 4 | 55 | Sept. 28 to Oct. 2 |
| 2 | 610 | 20 | 6 Io | 38 | July 59 | 56 | Oct. 37 |
| 3 | II 15 | 2 I | II 15 | 39 | 1014 | 57 | 8 12 |
| 4 | 1620 | 22 | 1620 | 40 | 1519 | 58 | $13 \quad 17$ |
| 5 | Jan. 21 to 25 | 23 | Apr.2I to 25 | 41 | $\text { July } 20 \text { to } 24$ | 59 | Oct. 18 to 22 |
| 6 | $26{ }^{26} 30$ | 24 | 2630 | 42 | $25,29$ | 60 | 23 27 27 |
| 7 | Feb. ${ }^{31} 50.4$ | 25 | $\begin{array}{llr}\text { May } & \text { I } & 5 \\ & 6 & 10\end{array}$ | 43 44 | Aug. ${ }^{30}$ Aug. 3 | $6 \mathrm{6I}$ | Nov. ${ }^{28}$ Nov. 1 |
| 9 | Feb. 5 10 $\quad 94$ | 27 | $\begin{array}{rr}6 & 10 \\ 11 & 15\end{array}$ | 45 | Aug. 4 9 9 | 63 | Nov. $2 \times r$ |
| 10 | Feb. 15 to 19 | 28 | May 16 to 20 | 46 | Aug. 14 to 18 | 64 | Nov. 12 to 16 |
| II | 20.24 | 29 | 21.25 | 47 | 1923 | 65 | $17 \quad 2 \mathrm{I}$ |
| 12* | Mar 25 Mar. 1 | 30 | $26 \quad 30$ | 48 | 24 28 | 66 | $22 \quad 26$ |
| 13 | Mar. 26 | 31 | 31 June 4 | 49 | S 29 Sept. 2 | 67 | ${ }^{27}$ Dec. 1 |
| 14 | 7 II | 32 | June 59 | 50 | Sept. 37 | 68 | Dec. 26 |
| 15 | Mar. 12 to 16 | 33 | Tune io to I4 | 51 | Sept. 8 to 12 | 69 70 | $\begin{array}{rr}7 & \text { II } \\ \text { 12 } & \text { I6 }\end{array}$ |
| 16 | $\begin{array}{cc}17 & 21\end{array}$ | 34 | 15 19 | 52 | Sept. 1317 | 7 I | $17 \begin{array}{ll}12 & \\ 7\end{array}$ |
| 17 | 2226 | 35 | $20 \quad 24$ | 53 | $18 \quad 22$ | 72 | $22 \quad 26$ |
| 18 | 27 3I | 36 | $25 \quad 29$ | 54 | $23 \quad 27$ | 73 | 27 3I |

* In the bissextile year the 12 th pentade contains six days.

DIVISION BY 28 OF NUMBERS FROM 28 TO 867972.

| 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | 28 | 56 | 84 | 112 | 140 | 168 | 196 | 224 | 252 | D. | - | 28 | 56 | 84 | 840 |
| 1 | 29 | 57 | 85 | 113 | 141 | 169 | 197 | 225 | 253 | ${ }_{\text {D }}$ D. | 12 | 40 | 68 | ${ }^{03}$ | ${ }^{30}$ |
| 2 | 30 | 58 | 86 | 14 | 142 | 170 | 198 | 226 |  | Q. | 04 | 05 | 06 | 07 | 29 |
|  |  |  |  |  |  |  |  |  | 25 | Q. | 28 | ${ }_{0}^{52}$ | 10 |  | $\begin{array}{r}784 \\ 28 \\ \hline\end{array}$ |
| 3 | 3 I | 59 | 87 | 115 | 143 | 171 | 199 | 227 | 255 | D. | $\left\lvert\, \begin{aligned} & 08 \\ & 08 \\ & 11 \end{aligned}\right.$ | 12 | 13 | 14 | 756 27 |
| 4 | 32 | 60 | 88 | 116 | 144 | 172 | 200 | 228 | 256 | D. | 20 | 48 | 76 |  | 28 |
| 5 | 33 | 6 I | 89 | 117 | 145 | 173 | 201 | 229 | 257 | D. | 15 | 16 | 17 60 | 88 | 26 700 |
| 6 | 34 | 62 | 90 | 118 | 146 |  |  |  |  | Q. | 18 | 19 | 20 | 21 | 25 |
|  | 34 |  | 90 | 118 | 146 | 174 | 202 | 230 | 258 | ${ }_{\text {D }} \mathrm{D}$. | ${ }_{22}^{16}$ | 44 | ${ }_{2}{ }^{72}$ |  | 672 24 |
| 7 | 35 | 63 | 91 | 119 | 147 | 175 | 203 | 231 | 259 | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{D}} .}{\mathrm{O}}$ | $\begin{aligned} & 00 \\ & 02 \\ & 25 \end{aligned}$ | $\begin{aligned} & 28 \\ & 26 \end{aligned}$ | $\begin{aligned} & 56 \\ & 27 \end{aligned}$ | 84 28 | 644 23 |
| 8 | 36 | 64 | 92 | 120 | 148 | 176 | 204 | 232 | 260 | D. | 12 | 40 | 68 |  | 616 |
|  |  |  |  |  |  |  |  |  |  | ${ }_{\sim}^{\text {D. }}$ | 29 | 30 | 31 | 32 | 22 |
| 9 | 37 | 65 | 93 | 121 | 149 | 177 | 205 | 233 | 261 | D. | 24 | 32 | 80 35 |  | 588 28 21 |
| го | 38 | 66 | 94 | 122 | 150 | 178 | 206 | 234 | 262 | D. | os | 36 | 64 | 92 | 560 |
| 11 | 39 | 67 | 95 | 123 | 151 | 179 | 207 | 235 | 263 | ${ }_{\text {D }}$. | 36 20 | 48 |  |  | 20 532 |
| 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | Q. | 40 | 41 | 42 |  | 19 |
| 12 | 40 | 68 | 96 | 124 | 15 | 180 | 208 | 236 | 264 | D. | 04 | 32 | 60 | 88 | 504 |
| 13 | 41 | 69 | 97 | 125 | 153 | 181 | 209 | 237 | 265 | ${ }^{\text {D. }}$ | 16 | 44 | 72 |  | 476 |
| 14 | 42 | 70 | 98 | 126 | 154 | 182 | 210 | 238 | 266 | D. | 47 | ${ }_{28}^{48}$ | 49 |  | 17 448 |
|  |  |  |  |  |  |  |  |  |  | Q. | 50 | 51 | 52 | 53 | 14 |
| 15 | 43 | 71 | 99 | 127 | 155 | 183 | 211 | 239 | 267 | $\begin{aligned} & \mathrm{O}, \\ & \mathrm{O} \\ & \mathrm{O} \end{aligned}$ | I2 54 | 4 | $\begin{aligned} & 68 \\ & 56 \end{aligned}$ | $\begin{aligned} & 96 \\ & 57 \end{aligned}$ | 420 15 |
| 16 | 44 | 72 | 100 | 128 | 156 | 184 | 212 | 240 | 268 | D. | 24 |  | 80 |  | 392 |
| 17 | 45 | 73 | ror | 129 | 157 | 185 | 213 | 241 | 269 | ${ }_{\text {D }}$ | -88 | 59 36 |  |  | 14 <br> 364 |
| 18 | 46 | 74 | 102 | 130 | 158 | 186 | 214 | 242 | 270 | ${ }_{\text {D }}$ | 21 | 62 |  | 64 | 13 336 |
|  |  |  |  |  |  |  |  |  |  | Q. | 65 | 66 | 67 |  | 13 12 |
| 19 | 47 | 75 | 103 | 131 | 159 | 187 | 215 | 243 | 271 | $\begin{aligned} & \mathrm{Q} .0 \\ & \mathrm{O} \\ & \hline \end{aligned}$ | $\begin{aligned} & 04 \\ & 08 \\ & 68 \end{aligned}$ | $\begin{aligned} & 32 \\ & 32 \\ & 69 \end{aligned}$ | $\begin{aligned} & 60 \\ & 70 \end{aligned}$ | $\begin{aligned} & 88 \\ & 71 \end{aligned}$ | 308 11 |
| 20 | 48 | 76 | 104 | 132 | 160 | 188 | 216 | 244 | 272 | D. | 16 |  |  |  | 280 |
| 21 | 49 | 77 | 105 | 133 | 161 | 189 | 217 | 245 | 273 | D. | 72 | ${ }_{28}^{73}$ | 74 |  | 10 |
| 22 | 50 | 78 | 106 | 134 | 162 | 190 | 218 | 246 | 27 | ${ }_{\text {D }} \mathrm{D}$ | 75 | 76 | 77 | 78 | 9 |
|  |  |  |  |  |  |  |  |  |  | Q. | 79 | 80 | 81 | 82 | 224 |
| 23 | 51 | 79 | 107 | 135 | 163 | 191 | 219 | 247 | 275 | $\begin{aligned} & \stackrel{\mathrm{C}}{\mathrm{D}} . \\ & \mathrm{Q} \end{aligned}$ | $\begin{aligned} & 24 \\ & 83 \\ & 83 \end{aligned}$ | $\begin{aligned} & 52 \\ & 54 \\ & 84 \end{aligned}$ | $\begin{aligned} & 80 \\ & 85 \\ & 85 \end{aligned}$ |  | ${ }^{196}$ |
| 24 | 52 | 80 | 108 | ${ }_{136}$ | 164 | 192 | 22 | 248 | 276 | D. | 08 | 36 |  | 92 | 168 |
| 25 | 53 | 81 | 109 | 137 | I65 | 193 | 221 | 249 | 277 | ${ }_{\text {D }}$ D. | ${ }^{86}$ | 48 | 76 | 89 | 6 4 0 |
| 26 | 54 | 82 | İо | 138 | 166 | 194 | 222 | 250 | 278 | D. | O4 | 91 | 92 |  | 5 112 |
| 27 | 55 | 83 | II | 139 | 167 | 195 |  |  |  | ${ }_{\text {D }}$ | 93 | 94 | 95 | 96 | 4 |
| 0 | 100 | 200 | 300 | 400 | 500 | $\frac{195}{600}$ | $\frac{22}{700}$ | $\frac{251}{800}$ | $\frac{279}{900}$ | D. | 16 97 | 44 98 | 72 99 |  | 84 3 |

TABLE 95.
DIVISION BY 29 OF NUMBERS FROM 29 TO 898971.


TABLE 96.
DIVISION BY 31 OF NUMBERS FROM 31 TO 960969.


Table 97.
NATURAL SINES AND COSINES.
Natural Sines.

| Angle. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | 30' | $40^{\prime}$ | $50^{\prime}$ | 60' | Angle. | Prop <br> Parts <br> for $1^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0{ }^{\circ}$ | . 000000 | . 002909 | . 005818 | . 008727 | . 011635 | . 014544 | .Or $745^{2}$ | $89^{\circ}$ |  |
| 1 | . $01745^{2}$ | . 02036 | .02327 | .02618 | . 02908 | .0319 9 | . 03490 | 88 |  |
| 2 | . 03490 | . 0378 I | .0407 I | . 04362 | . 04653 | . 04943 | . 05234 | 87 |  |
| 3 | .05234 | . 05524 | .0581 4 | . 06105 | . 06395 | . 06685 | . 06976 | 86 |  |
| 4 | . 06976 | . 07266 | . 07556 | . 07846 | .08I3 6 | . 08426 | .0871 6 | 85 |  |
| 5 | .0871 6 | . 09005 | . 09295 | . 09585 | . 09874 | .ro16 4 | . 10453 | 84 |  |
| 6 | . 10453 | .1074 2 | .1103 I | .1132 ${ }^{\text {o }}$ | .rr60 9 | .1189 8 | . 12187 | 83 |  |
| 7 | . 12187 | . 12476 | . 12764 | . 13053 | .1334 | . 1363 | . 1392 | 82 |  |
| 8 | . 1392 | . 1421 | . 1449 | . 1478 | . 1507 | . 1536 | . 1564 | 8 8 | 2.9 |
| 9 | . 1564 | . 1593 | . 1622 | . 1650 | . 1679 | . 1708 | . 1736 | 80 | 2.9 |
| 10 | . 1736 | . 1765 | .1794 | . 1822 | .1851 | . 1880 | . 1908 | 79 | 2.9 |
| II | . 1908 | . 1937 | . 1965 | . 1994 | . 2022 | . 2051 | . 2079 | 78 | 2.9 |
| 12 | . 2079 | . 2108 | . 2136 | . 2164 | . 2193 | . 2221 | . 2250 | 77 | 2.8 |
| 13 | . 2250 | . 2278 | . 2306 | . 2334 | . 2363 | .2391 | . 2419 | 76 | 2.8 |
| 14 | . 2419 | . 2447 | . 2476 | . 2504 | . 2532 | . 2560 | . 2588 | 75 | 2.8 |
| 15 | . 2588 | . 2616 | . 2644 | . 2672 | . 2700 | . 2728 | . 2756 | 74 | 2.8 |
| 16 | . 2756 | . 2784 | . 2812 | . 2840 | . 2868 | . 2896 | . 2924 | 73 | 2.8 |
| 17 | . 2924 | . 2952 | . 2979 | . 3007 | -3035 | - 3062 | -3090 | 72 | 2.8 |
| 18 | -3090 | -3118 | -3145 | . 3173 | -3201 | -3228 | . 3256 | 71 | 2.8 |
| 19 | . 3256 | - 3283 | .33II | - 3338 | . 3365 | - 3393 | . 3420 | 70 | 2.7 |
| 20 | . 3420 | . 3448 | . 3475 | . 3502 | . 3529 | - 3557 | - 3584 | 69 | 2.7 |
| 21 | . 3584 | -3611 | -3638 | - 3665 | -3692 | -3719 | - 3746 | 68 | 2.7 |
| 22 | - 3746 | . 3773 | -3800 | - 3827 | -3854 | -388I | - 3907 | 67 | 2.7 |
| 23 | - 3907 | - 3934 | -396I | - 3987 | -4014 | -404I | -4067 | 66 | 2.7 |
| 24 | . 4067 | . 4094 | . 4120 | .4147 | .4173 | . 4200 | . 4226 | 65 | 2.7 |
| 25 | . 4226 | . 4253 | . 4279 | . 4305 | . 4331 | . 4358 | . 4384 | 64 | 2.6 |
| 26 | . 4384 | .4410 | . 4436 | . 4462 | . 4488 | . 4514 | . 4540 | 63 | 2.6 |
| 27 | . 4540 | . 4566 | . 4592 | -4617 | . 4643 | . 4669 | . 4695 | 62 | 2.6 |
| 28 | . 4695 | . 4720 | . 4746 | -4772 | . 4797 | . 4823 | . 4848 | 61 60 | 2.6 2.5 |
| 29 | . 4848 | . 4874 | . 4899 | . 4924 | . 4950 | -4975 | . 5000 | 60 | 2.5 |
| 30 | . 5000 | . 5025 | . 5050 | . 5075 | . 5100 | . 5125 | . 5150 | 59 | 2.5 |
| 31 | . 5150 | . 5175 | . 5200 | . 5225 | . 5250 | . 5275 | . 5299 | 58 | 2.5 |
| 32 | . 5299 | . 5324 | - 5348 | . 5373 | . 5398 | . 5422 | -5446 | 57 | 2.5 |
| 33 | . 5446 | . 547 I | . 5495 | .5519 | . 5544 | . 5568 | . 55592 | 56 | 2.4 |
| 34 | . 5592 | . 5616 | - 5640 | . 5664 | . 5688 | . 5712 | -5736 | 55 | 2.4 |
| 35 | . 5736 | . 5760 | .5783 | . 5807 | . 5831 | . 5854 | . 5878 | 54 | 2.4 |
| 36 | . 5878 | . 5901 | . 5925 | . 5948 | . 5972 | . 5995 | . 6018 | 53 | 2.3 |
| 37 | . 6018 | . 6041 | . 6065 | . 6088 | . 6111 | . 6134 | . 6157 | 52 | 2.3 |
| 38 39 | . 6157 | . 6180 | . 6202 | . 6225 | . 6248 | . 6271 | . 6293 | 51 50 | 2.3 |
| 39 | . 629 |  | . 6338 | . 6361 | . 6383 | . 6406 | . 6428 | 50 | 2.3 |
| 40 | . 6428 | . 6450 | . 6472 | . 6494 | . 6517 | . 6539 | .656r | 49 | 2.2 |
| 4 I | .6561 | . 6583 | . 6604 | . 6626 | . 6648 | . 6670 | . 6691 | 48 | 2.2 |
| 42 | . 6691 | . 6713 | . 6734 | . 6756 | . 6777 | . 6799 | . 6820 | 47 | 2.2 |
| 43 | . 6820 | . 684 4 | . 6862 | . 6884 | . 6905 | . 6926 | . 6947 | 46 | 2.1 |
| 44 | . 6947 | . 6967 | . 6988 | . 7009 | . 7030 | . 7050 | . 7071 | 45 | 2.1 |
|  | $60^{\prime}$ | $50^{\prime}$ | $40^{\prime}$ | $30^{\prime}$ | $20^{\prime}$ | $10^{\prime}$ | $0^{\prime}$ | Angle. |  |

Smithsonian Tableg.
Natural Cosines.

NATURAL SINES AND COSINES.
Natural Sines.

| Angle. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | $50^{\prime}$ | $60^{\prime}$ | Angle. | Prop. Parts for $1^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $45^{\circ}$ | . 7071 | . 7092 | . 7112 | . 7133 | . 7153 | . 7173 | . 7193 | $44^{\circ}$ | 2.0 |
| 46 | . 7193 | . 7214 | . 7234 | . 7254 | . 7274 | . 7294 | . 7314 | 43 | 2.0 |
| 47 | . 7314 | . 7333 | . 7353 | . 7373 | . 7392 | .7412 | . 7431 | 42 | 2.0 |
| 48 | . 7431 | . 7451 | . 7470 | . 7490 | .7509 | . 7528 | . 7547 | 4 I | 1.9 |
| 49 | . 7547 | . 7566 | . 7585 | . 7604 | . 7623 | . 7642 | . 7660 | 40 | 1.9 |
| 50 | . 7660 | . 7679 | . 7698 | . 7716 | . 7735 | . 7753 | . 7771 | 39 | 1.9 |
| 51 | . 7771 | . 7790 | . 7808 | . 7826 | . 7844 | . 7862 | . 7880 | 38 | 1.8 |
| 52 | . 7880 | . 7898 | . 7916 | . 7934 | . 7951 | . 7969 | . 7986 | 37 | 1.8 |
| 53 | . 7986 | . 8004 | . 8021 | . 8039 | . 8056 | . 8073 | .8090" | 36 | 1.7 |
| 54 | . 8090 | .8107 | .8124 | .8I4I | .8r58 | .8175 | .8192 | 35 | 1.7 |
| 55 | . 8192 | . 8208 | . 8225 | . 8241 | . 8258 | . 8274 | . 8290 | 34 | 1.6 |
| 56 | . 8290 | . 8307 | . 8323 | . 8339 | . 8355 | .837I | . 8387 | 33 | 1.6 |
| 57 | . 8387 | . 8403 | . 8418 | . 8434 | . 8450 | . 8465 | . 8480 | 32 | 1.6 |
| 58 | . 8480 | . 8496 | . 8511 | . 8526 | . 8542 | . 8557 | . 8572 | 31 | I. 5 |
| 59 | . 8572 | . 8587 | . 8601 | .8616 | . 8631 | . 8646 | . 8660 | 30 | 1.5 |
| 60 | . 8660 | . 8675 | . 8689 | . 8704 | . 8718 | . 8732 | . 8746 | 29 | 1.4 |
| 61 | . 8746 | . 8760 | . 8774 | . 8788 | . 8802 | .88ı6 | . 8829 | 28 | I. 4 |
| 62 | . 8829 | . 8843 | . 8857 | . 8870 | . 8884 | . 8897 | . 8910 | 27 | 1.4 |
| 63 | . 8910 | . 8923 | . 8936 | . 8949 | . 8962 | . 8975 | . 8988 | 26 | 1.3 |
| 64 | . 8988 | .9001 | . 9013 | . 9026 | . 9038 | .9051 | :9063 | 25 | I. 3 |
| 65 | . 9063 | . 9075 | . 9088 | . 9100 | . 9112 | . 9124 | . 9135 | 24 | 1.2 |
| 66 | 9135 | . 9147 | . 9159 | . 9171 | -9182 | . 9194 | . 9205 | 23 | 1.2 |
| 67 | . 9205 | . 9216 | -9228 | . 9239 | -9250 | . 9261 | - 9272 | 22 | I.I |
| 68 | . 9272 | . 9283 | . 9293 | . 9304 | . 9315 | . 9325 | . 9336 | 21 | I.I |
| 69 | . 9336 | . 9346 | . 9356 | . 9367 | . 9377 | . 9387 | . 9397 | 20 | 1.0 |
| 70 | -9397 | . 9407 | -9417 | . 9426 | . 9436 | . 9446 | . 9455 | 19 | 1.0 |
| 71 | . 9455 | . 9465 | . 9474 | . 9483 | . 9492 | . 9502 | .95II | 18 | 0.9 |
| 72 | . 951 I | . 9520 | . 9528 | . 9537 | . 9546 | . 9555 | . 9563 | 17 | 0.9 |
| 73 | .9563 | . 9572 | . 9580 | . 9588 | . 9596 | . 9605 | . 9613 | 16 | 0.8 |
| 74 | . 9613 | . 962 I | . 9628 | . 9636 | 9644 | . 9652 | . 9659 | 15 | 0.8 |
| 75 | . 9659 | . 9667 | . 9674 | .9681 | . 9689 | . 9696 | . 9703 | 14 | 0.7 |
| 76 | . 9703 | . 9710 | . 9717 | . 9724 | . 9730 | . 9737 | . 9744 | 13 | 0.7 |
| 77 | - 9744 | . 9750 | . 9757 | . 9763 | . 9769 | . 9775 | .978i | 12 | 0.6 |
| 78 | .9781 | . 9787 | .9793 | . 9799 | . 9805 | .98II | .9816 | 11 | 0.6 |
| 79 | .9816 | . 9522 | . 9827 | . 9833 | .9838 | . 9843 | . 9848 | 10 | 0.5 |
| 80 | . 9848 | . 9853 | . 9858 | . 9863 | . 9868 | . 9872 | . 9877 |  | 0.5 |
| 81 | . 9877 | . 988 I | . 9886 | . 9890 | . 9894 | . 9899 | . 9903 | 8 | 0.4 |
| 82 | . 9903 | . 9907 | .991 1 | . 9914 | . 9918 | . 9922 | . 9925 | 7 | 0.4 |
| 83 | . 9925 | . 9929 | . 9932 | . 9936 | . 9939 | . 9942 | . 9945 | 6 | 0.3 |
| 84 | . 9945 | . 9948 | .9951 | . 9954 | . 9957 | . 9959 | . 9962 | 5 | 0.3 |
| 85 | . 9962 | . 9964 | . 9967 | . 9969 | .9971 | . 9974 |  |  | 0.2 |
| 86 | . 9976 | . 9978 | . 9980 | .998i | . 9983 | . 9985 | . 9986 | 3 | 0.2 |
| 87 | . 9986 | . 9988 | . 9989 | . 9990 | . 9992 | . 9993 | . 9994 | 2 | O. I |
| 88 | . 9994 | . 9995 | . 9996 | . 9997 | . 9997 | . 9998 | . 9998 | 0 | O. 1 |
| 89 | . 9998 | . 9999 | . 9999 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 0 | 0.0 |
|  | $60^{\prime}$ | $50^{\prime}$ | $40^{\prime}$ | $30^{\prime}$ | $20^{\prime}$ | $10^{\prime}$ | $0^{\prime}$ | Angle. |  |

TABLE 98.
NATURAL TANGENTS AND COTANGENTS.
Natural Tangents.

| Angle. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | $50^{\prime}$ | $60^{\prime}$ | Angle. | Prop. Parts for $1^{\prime}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | . 00000 | . 0029 I | . 00582 | . 00873 | .ori6 4 | .OI45 5 | . 01746 | $89^{\circ}$ | 2.9 |
| 1 | . 01746 | . 02036 | . 02328 | .026I 9 | . 02910 | . 0320 I | . 03492 | 88 | 2.9 |
| 2 | . 03492 | . 03783 | . 04075 | . 04366 | . 04658 | . 04949 | . 0524 I | 87 | 2.9 |
| 3 | . 0524 I | . 05533 | .05824 | .06II 6 | . 06408 | . 06700 | . 06993 | 86 | 2.9 |
| 4 | . 06993 | . 07285 | . 07578 | . 07870 | .08I6 3 | . 08456 | . 08749 | 85 | 2.9 |
| 5 | . 08749 | . 09042 | . 09335 | . 09629 | .09923 | .102I 6 | . 10510 | 84 | 2.9 |
| 6 | .105I 0 | . .1080 5 | .1109 9 | .II39 4 | .II688 | .II98 3 | . 12278 | 83 | 2.9 |
| 7 | . 12278 | . 12574 | . 12869 | .13I6 5 | . 1346 | . 1376 | . 1405 | 82 | 3.0 |
| 8 | . 1405 | . 1435 | . 1465 | . 1495 | . 1524 | . 1554 | . 1584 | 8 I | 3.0 |
| 9 | .IS84 | .16I4 | . 1644 | . 1673 | . 1703 | . 1733 | . 1763 | 80 | 3.0 |
| 10 | . 1763 | . 1793 | . 1823 | .I853 | .1883 | .1914 | . 1944 | 79 | 3.0 |
| II | . 1944 | . 1974 | . 2004 | . 2035 | . 2065 | . 2095 | . 2126 | 78 | 3.0 |
| 12 | . 2126 | . 2156 | . 2186 | .2217 | . 2247 | . 2278 | . 2309 | 77 | 3.1 |
| 13 | . 2309 | . 2339 | . 2370 | .2401 | . 2432 | . 2462 | . 2493 | 76 | 3.1 |
| 14 | . 2493 | . 2524 | . 2555 | . 2586 | .2617 | . 2648 | . 2679 | 75 | 3.1 |
| 15 | . 2679 | . 2711 | . 2742 | . 2773 | . 2805 | . 2836 | . 2867 | 74 | 3.1 |
| 16 | . 2867 | . 2899 | . 2931 | . 2962 | . 2994 | . 3026 | . 3057 | 73 | 3.2 |
| 17 | . 3057 | . 3089 | . 3121 | .3I53 | . 3185 | . 3217 | . 3249 | 72 | 3.2 |
| 18 | . 3249 | .3281 | . 3314 | . 3346 | . 3378 | .34II | . 3443 | 7 I | 3.2 |
| 19 | . 3443 | . 3476 | . 3508 | .354I | . 3574 | . 3607 | . 3640 | 70 | $3 \cdot 3$ |
| 20 | . 3640 | . 3673 | . 3706 | . 3739 | - 3772 | .3805 | . 3839 | 69 | $3 \cdot 3$ |
| 21 | .3839 | . 3872 | . 3906 | . 3939 | - 3973 | . 4006 | . 4040 | 68 | $3 \cdot 4$ |
| 22 | . 4040 | . 4074 | . 4108 | . 4142 | . 4176 | . 4210 | . 4245 | 67 | 3.4 |
| 23 | . 4245 | . 4279 | . 4314 | . 4348 | . 4383 | . 4417 | . 4452 | 66 | $3 \cdot 5$ |
| 24 | . 4452 | . 4487 | . 4522 | . 4557 | .4592 | . 4628 | . 4663 | 65 | $3 \cdot 5$ |
| 25 | . 4663 | . 4699 | . 4734 | . 4770 | . 4806 | . 4841 | . 4877 | 64 | 3.6 |
| 26 | . 4877 | .4913 | . 4950 | . 4986 | . 5022 | . 5059 | . 5095 | 63 | 3.6 |
| 27 | . 5095 | .5132 | . 5169 | . 5206 | . 5243 | . 5280 | .5317 | 62 | 3.7 |
| 28 | . 5317 | . 5354 | . 5392 | . 5430 | . 5467 | . 5505 | . 5543 | 6 I | 3.8 |
| 29 | . 5543 | .558r | .5619 | . 5658 | .5696 | . 5735 | . 5774 | 60 | 3.8 |
| 30 | . 5774 | . 58 I 2 | . 5851 | . 5890 | . 5930 | . 5969 | . 6009 | 59 | $3 \cdot 9$ |
| 31 | . 6009 | . 6048 | . 6088 | .6128 | . 6168 | . 6208 | . 6249 | 58 | 4.0 |
| 32 | . 6249 | . 6289 | . 6330 | . 6371 | . 6412 | . 6453 | . 6494 | 57 | 4. I |
| 33 | . 6494 | . 6536 | . 6577 | .6619 | .666I | . 6703 | . 6745 | 56 | 4.2 |
| 34 | . 6745 | . 6787 | . 6830 | . 6873 | . 6916 | . 6959 | . 7002 | 55 | 4.3 |
| 35 | . 7002 | . 7046 | . 7089 | . 7133 | .7177 | .722I | . 7265 | 54 | 4.4 |
| 36 | . 7265 | .7310 | . 7355 | . 7400 | . 7445 | . 7490 | . 7536 | 53 | 4.5 |
| 37 | . 7536 | .7581 | . 7627 | . 7673 | . 7720 | . 7766 | .7813 | 52 | 4.6 |
| 38 | .7813 | . 7860 | . 7907 | . 7954 | . 8002 | . 8050 | . 8098 | 5 I | 4.7 |
| 39 | . 8098 | . 8146 | .8195 | . 8243 | . 8292 | . 8342 | . 8391 | 50 | 4.9 |
| 40 | . 8391 | .844I | . 8491 | .854I | .8591 | . 8642 | . 8693 | 49 | 5.0 |
| 41 | . 8693 | . 8744 | . 8796 | . 8847 | . 8899 | . 8952 | . 9004 | 48 | 5.2 |
| 42 | . 9004 | . 9057 | .91 10 | .9163 | . 9217 | .927I | . 9325 | 47 | $5 \cdot 4$ |
| 43 | . 9325 | . 9380 | . 9435 | . 9490 | . 9545 | .9601 | . 9657 | 46 | $5 \cdot 5$ |
| 44 | . 9657 | .9713 | . 9770 | . 9827 | . 9884 | . 9942 | 1.0000 | 45 | $5 \cdot 7$ |
|  | $60^{\prime}$ | $50^{\prime}$ | $40^{\prime}$ | $30^{\prime}$ | $20^{\prime}$ | $10^{\prime}$ | $0^{\prime}$ | Angle. |  |

NATURAL TANGENTS AND COTANGENTS.
Natural Tangents.

| Angle. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | $50^{\prime}$ | $60^{\prime}$ | Angle. | Prop. Parts for $1^{\prime}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $45^{\circ}$ | 1.0000 | 1.0058 | I.OII7 | I.0176 | 1.0235 | 1.0295 | 1.0355 | $44^{\circ}$ | 5.9 |
| 46 | 1.0355 | 1.0416 | 1.0477 | 1.0538 | 1.0599 | 1.066I. | 1.0724 | 43 | 6.1 |
| 47 | 1.0724 | 1.0786 | 1.0850 | r.o913 | 1.0977 | I.104I | I. 1106 | 42 | 6.4 |
| 48 | I. 1106 | 1.1171 | I. 1237 | I.1303 | r. 1369 | 1.1436 | I. 1504 | 4 I | 6.6 |
| 49 | 1. 1504 | 1.157I | I. 1640 | I. 1708 | r. 1778 | I. 1847 | I. 1918 | 40 | 6.9 |
| 50 | 1.1918 | 1. 1988 | I. 2059 | 1.2I3I | 1.2203 | 1.2276 | 1.2349 | 39 | 7.2 |
| 5 I | I. 2349 | 1.2423 | I. 2497 | 1.2572 | I. 2647 | 1.2723 | I. 2799 | 38 | $7 \cdot 5$ |
| 52 | 1.2799 | 1.2876 | 1.2954 | 1.3032 | I.3III | 1.3190 | 1.3270 | 37 | $7 \cdot 9$ |
| 53 | 1.3270 | I.3351 | 1. 3432 | I.3514 | I. 3597 | 1.3680 | 1.3764 | 36 | 8.2 |
| 54 | I. 3764 | 1.3848 | I. 3934 | 1.4019 | 1.4106 | 1.4193 | 1.428 I | 35 | 86 |
| 55 | 1.4281 | 1.4370 | 1.4460 | 1.4550 | 1.4641 | 1.4733 | 1.4826 | 34 | 9.1 |
| 56 | 1.4826 | 1.4919 | 1.5013 | 1.5108 | I. 5204 | 1.5301 | I. 5399 | 33 | 9.6 |
| 57 | I. 5399 | 1.5497 | I. 5597 | I. 5697 | 1.5798 | 1.5900 | 1.6003 | 32 | 10.I |
| 58 | 1.6003 | 1.6107 | 1.6212 | 1.6319 | 1.6426 | 1.6534 | 1.6643 | 3 I | 10.7 |
| 59 | 1. 6643 | 1. 6753 | 1. 6864 | 1. 6977 | 1.7090 | 1.7205 | 1.732I | 30 | II. 3 |
| 60 | 1.732 I | 1.7437 | 1. 7556 | 1.7675 | 1.7796 | 1.7917 | 1.8040 | 29 | 12.0 |
| 6 I | 1.8040 | I.8165 | 1.8291 | 1.8418 | 1. 8546 | 1.8676 | 1.8807 | 28 | 12.8 |
| 62 | 1.8807 | 1.8940 | 1.9074 | 1.9210 | 1.9347 | 1.9486 | 1.9626 | 27 | 13.6 |
| 63 | I. 9626 | 1.9768 | 1.9912 | 2.0057 | 2.0204 | 2.0353 | 2.0503 | 26 | 14.6 |
| 64 | 2.0503 | 2.0655 | 2.0809 | 2.0965 | 2.1123 | 2.1283 | 2.1445 | 25 | I5.7 |
| 65 | 2.1445 | 2.1609 | 2. 1775 | 2. 1943 | 2.2113 | 2.2286 | 2.2460 | 24 | 16.9 |
| 66 | 2.2460 | 2.2637 | 2.2817 | 2.2998 | 2.3183 | 2.3369 | 2.3559 | 23 | 18.3 |
| 67 | 2.3559 | 2.3750 | 2.3945 | 2.4142 | 2.4342 | 2.4545 | 2.475 I | 22 | 19.9 |
| 68 | 2.475 I | 2.4960 | 2.5172 | 2.5386 | 2.5605 | 2.5826 | 2.6051 | 21 | 21.7 |
| 69 | 2.6051 | 2.6279 | 2.651 I | 2.6746 | 2.6985 | 2.7228 | 2.7475 | 20 | 23.7 |
| 70 | 2.7475 | 2.7725 | 2.7980 | 2.8239 | 2.8502 | 2.8770 | 2.9042 | 19 |  |
| 71 | 2.9042 | 2.9319 | 2.9600 | 2.9887 | 3.0178 | 3.0475 | 3.0777 | 18 |  |
| 72 | 3.0777 | 3.1084 | 3. I397 | 3.1716 | 3.2041 | 3.2371 | 3.2709 | 17 |  |
| 73 | 3.2709 | 3.3052 | $3 \cdot 3402$ | $3 \cdot 3759$ | 3.4124 | 3.4495 | 3.4874 | 16 |  |
| 74 | 3.4874 | $3 \cdot 526 \mathrm{I}$ | 3.5656 | 3.6059 | 3.6470 | 3.6891 | 3.732 I | 15 |  |
| 75 | 3.732 I | 3.7760 | 3.8208 | 3.8667 | 3.9136 | 3.9617 | 4.0108 | 14 |  |
| 76 | 4.0108 | 4.0611 | 4.1126 | 4.1653 | 4.2193 | 4.2747 | 4.3315 | 13 |  |
| 77 | 4.3315 | $4 \cdot 3897$ | 4.4494 | 4.5107 | 4.5736 | 4.6382 | 4.7046 | 12 |  |
| 78 | 4.7046 | 4.7729 | 4.8430 | 4.9152 | 4.9894 | 5.0658 | 5.1446 | II |  |
| 79 | 5.1446 | 5.2257 | 5.3093 | $5 \cdot 3955$ | 5.4845 | 5.5764 | 5.67 I 3 | IO |  |
| 80 | 5.6713 | 5.7694 | 5.8708 | 5.9758 | 6.0844 | 6.1970 | 6.3138 | 9 |  |
| 81 | 6.3138 | 6.4348 | 6.5606 | 6.6912 | 6.8269 | 6.9682 | 7.1154 | 8 |  |
| 82 | 7.1154 | 7.2687 | 7.4287 | 7.5958 | 7.7704 | 7.9530 | 8.1443 | 7 |  |
| 83 | 8. 1443 | 8.3450 | 8.5555 | 8.7769 | 9.0098 | 9.2553 | 9.5144 | 6 |  |
| 84 | 9.5144 | 9.7882 | 10.0780 | 10.3854 | 10.7119 | II. 0594 | 11.4301 | 5 |  |
| 85 | II.4301 | 11.8262 | 12.2505 | 12.7062 | 13.1969 | 13.7267 | 14.3007 | 4 |  |
| 86 | 14.3007 | 14.9244 | 15.6048 | 16.3499 | 17.1693 | 18.0750 | 19.08I I | 3 |  |
| 87 | 19.081 I | 20.2056 | 21.4704 | 22.9038 | 24.5418 | 26.4316 | 28.6363 | 2 |  |
| 88 | 28.6363 | 31.2416 | 34.3678 | 38.1885 | 42.9641 | 49.1039 | 57.2900 | 1 |  |
| 89 | 57.2900 | 68.7501 | 85.9398 | II 4.5887 | 171.8854 | 343.7737 | $\infty$ | 0 |  |
|  | $60^{\prime}$ | $50^{\prime}$ | $40^{\prime}$ | $30^{\prime}$ | $20^{\prime}$ | $10^{\prime}$ | $0^{\prime}$ | Angle. |  |


| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 |  | 7 | 8 | 9 | d. | Prop. Parts. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 0 | 00003 | 3010 | 4771 | 6021 | 699 | 778 | 84 | 451 | 9031 | 9542 |  |  |  |  |  |  |
| 1 | 00000 | 0414 | O792 | II39 | 146I | 176 | 20 | 23 | 04 | 2553 | 2788 |  |  |  |  |  |  |
| 2 | 3010 | 3222 | 3424 | 3617 | 3802 | 397 |  |  | 14 | 4472 | 4624 |  |  |  |  |  |  |
| 3 | 4771 | 49145 | 5051 | 5185 | 5315 | 54 |  | 56 | 682 | 5798 | 5911 |  |  | 4,3 | 4,2 | 4,1 |  |
| 4 | 60216 | 6128 | 6232 | 6335 | 6435 | 653 |  |  | 721 | 6812 | 6902 |  |  | 8,6 |  | 8,2 |  |
| 5 | 69907 | 70767 | 7160 | 7243 | 7324 | 740 | 748 | 75 | 559 | 7634 | 7709 |  |  | 12,9 17,2 | 12,6 | 12,3 16,4 |  |
| 6 | 77827 | 78537 | 7924 | 7993 | 8062 | 812 | 819 |  | 6I | 8325 | 8388 |  |  | 12, | 21,0 | 120, |  |
| 7 | 845I 8 | 85138 | 8573 | 8633 | 8692 | 875 | 880 | 88 | 865 | 8921 | 8976 |  | 6 | 25,8 | 25,2 29,4 | 24,6 | 24,0 28,0 |
| 8 | 90319 | 9085 | 9138 | 9191 | 9243 | 929 | 93 |  | 395 | 9445 | 9494 |  | 8 | 34,4 |  |  | 32,0 |
| 9 | 95429 | 95909 | 9638 | 9685 | 973I | 977 | 98 | 98 | 68 | 9912 | 9956 |  |  |  |  |  |  |
| 10 | 0000 | 0043 | 0086 | OI28 | or70 | 021 | 025 | 02 | 94 | 0334 | 0374 | 4 I |  |  |  |  |  |
| II | 0414 | 04530 | 0492 | 0531 | 0569 | 06 | 06 | 06 | 82 | 0719 | O755 | 38 |  |  |  |  |  |
| 12 | 07920 | 0828 | 0864 | 0899 | 0934 | 096 | 100 |  | 038 | 1072 | 1106 | 35 |  |  |  |  | 36 |
| 13 | 11391 | 1173 | 1206 | 1239 | 1271 | 130 | I33 | I3 | 367 | I 399 | 1430 | 32 | 1 | 3,9 7,8 | 3,8 7,6 | 3,7 <br> 7,4 <br> 1 |  |
| 14 | 1461 | 1492 I | 1523 | ${ }^{1} 553$ | 1584 | 161 | 164 | 16 | 673 | 1703 | 1732 | 30 | 2 | 11,7 |  | II, $\begin{array}{r}7, \\ \text { II, }\end{array}$ |  |
| 15 | I76I I | 17901 | 1818 | 1847 | 1875 | 190 | 193 |  | 959 | 1987 | 2014 | 28 | 4 | 15,6 19,5 |  |  |  |
| 16 | 20412 | 20682 | 2095 | 2122 | 2148 | 217 | 220 |  | 227 | 2253 | 2279 | 26 | 5 | 19,5 23,4 |  |  |  |
| 17 | 23042 | 23302 | 2355 | 2380 | 2405 | 243 | 245 |  | 480 | 2504 | 2529 | 25 | 7 |  |  |  |  |
| 18 | 25532 27882 | 25772 | 2601 | 2625 | 2648 | 2672 | 269 |  | 718 | 2742 | 2765 | 24 | 8 | 31,2 35,1 |  |  |  |
| 20 | 30103 | 30323 | 3054 | 3075 | 3096 | 3 I | 31 | 31 | 60 | 3181 | 3201 | 21 |  |  |  |  |  |
| 2 I | 32223 | 3243 | 3263 | 3284 | 3304 | 332 | 334 | 33 | 365 | 3385 | 3404 | 20 |  |  |  |  |  |
| 22 | 34243 | 3444 | 3464 | 3483 | 3502 | 352 | 354 |  | 560 | 3579 | 3598 | 19 |  |  |  | 33 | 32 |
| 23 | 36173 | 36363 | 3655 | 3674 | 3692 | 371 | 372 |  | 777 | 3766 | 3784 | 18 | 1 |  | 3,4 | 3,6 |  |
| 24 | 38023 | 38203 | 3838 | 3856 | 3874 | 389 | 390 |  | 927 | 3945 | 3962 | 18 | 3 |  |  |  |  |
| 25 | 39793 | 39974 | 4014 | 4031 | 4048 | 406 | 408 |  | 099 | 4116 | 4133 | 17 | 4 |  |  |  |  |
| 26 | 41504 | 41664 | 4183 | 4200 | 4216 | 423 | 424 |  | 5 | 4281 | 4298 | 16 | 5 |  |  |  |  |
| 27 | 43144 | 43304 | 4346 | 4362 | 4378 | 439 |  |  | 425 | 4440 | 4456 | 16 | 7 |  | 23,8 |  |  |
| 28 | 44724 | 44874 | 4502 | 4518 | 4533 | 454 | 456 |  | 579 | 4594 | 4609 | 15 | 8 9 |  |  |  |  |
| 29 | 46244 | 46394 | 4654 | 4669 | 4683 | 4698 | 471 |  | 728 | 4742 | 4757 | 15 |  |  |  |  |  |
| 30 | 4771 | 4786 | 4800 | 48I4 | 4829 | 48 | 48 | 48 | 71 | 4886 | 4900 | 14 |  |  |  |  |  |
| 31 | 49144 | 49284 | 4942 | 4955 | 4969 | 498 | 499 | 5 | OII | 5024 | 5038 | 14 |  |  |  |  |  |
| 32 | 50515 51855 | 50655 | 50795 | 5092 | 5105 | 511 | 513 |  | 145 | 5159 | 5172 5302 | 13 |  |  |  |  |  |
| 33 | 51855 | 51985 | 5211 | 5224 | 5237 | 525 | 526 |  | 276 | 5289 | 5302 | 13 | 2 | 6,2 |  | 5,8 | 5,6 |
| 34 | 53155 | 53285 | 5340 | 5353 | 5366 | 5378 | 539 |  | 403 | 5416 | 5428 | 13 | 4 | 9,3 |  |  | 8,4 11,2 |
| 35 | 54415 | 54535 | 54655 | 5478 | 5490 | 550 | 551 |  | 527 | 5539 | 5551 | 12 | 4 |  |  |  |  |
| 36 | 55635 | 55755 | 5587 | 5599 | 5611 | 562 | 563 |  | 647 | 5658 | 5670 | 12 |  | 18,6 |  |  | 16,8 19,6 |
| 37 38 | 56825 | 56945 | 5705 | 5717 | 5729 | 574 |  |  | 763 | 5775 | 5786 | 12 | 8 | 2, 2,7 24,8 |  |  | 22,4 |
| 38 39 | 57985 | 58095 | 5821 | 5832 | 5843 | 585 | 586 |  | 8775 |  | 5899 | II |  | 27,9 | 27,0 |  | 25,2 |
| 39 | 5911 5 | 59225 | 5933 | 5944 | 5955 | 596 | 597 |  | 988 | 5999 | 6010 | II |  |  |  |  |  |
| 40 | 60216 | 60316 | 6042 | 605 | 6064 | 60 | 608 | 60 | 6 | O7 | 6117 | II |  |  |  |  |  |
| 4 | 6i28 6 | 6 I 386 | 6149 | 6160 | 6170 | 618 |  | 62 | I | 212 | 6222 | IO |  | 27 | 26 | 25 | 24 |
| 42 | 62326 | 62436 | 6253 | 6263 | 6274 | 628 | 629 |  | 304 | 6314 | 6325 | 10 | 2 | 2,7 5,4 | 2,6 5,2 | 2,5 | 2,4 4,8 |
| 43 | 63356 | 6345 | 6355 | 6365 | 6375 | 638 | 639 |  | 405 | 6415 | 6425 | 10 | 2 | 5,4 | 5,2 | 5,0 | 4,8 7,2 |
| 44 | 64356 | 64446 | 6454 | 6464 | 6474 | 648 | 649 |  | 503 | 6513 | 6522 | 10 |  | 10,8 13,5 | 10,4 13,0 | $\begin{aligned} & 10,0 \\ & 12,5 \end{aligned}$ | 9,6 r2,0 |
| 45 | 65326 | 65426 | 6551 | 6561 | 6571 | 658 | 659 |  | 599 | 6609 | 6618 | 10 | 6 | 16,2 | 15,6 | 15,0 | 14,4 |
| 46 | 66286 | 6637 | 6646 | 6656 | 6665 | 667 | 668 |  | 693 | 6702 | 6712 | 9 |  |  | 18,2 18,2 2,8 |  | 16,8 19,2 |
| 47 | 67216 | 67306 | 67396 | 6749 | 6758 | 676 |  |  | 785 | 6794 | 6803 | 9 | 8 | 21,6 24,3 | 20,8 23,4 | 20,0 | 19,2 21,6 |
| 48 | 68126 | 6821 | 6830 | 6839 | 6848 | 685 | 686 |  | 875 | 6884 | 6893 | 9 |  |  |  |  |  |
| 49 | 69026 | 69116 | 6920 | 6928 | 6937 | 694 | 695 |  | 964 | 6972 | 6981 |  |  |  |  |  |  |
| 50 | 69906 | 69987 | 7007 | 7016 | 7024 | 703 | 70 |  | 50 | 7059 | 7067 | 9 |  |  |  |  |  |
| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 |  | 7 | 8 | 9 | d. |  | Pro | p. P | Parts |  |

LOGARITHMS OF NUMBERS.

| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | d. | Prop. Parts. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 69906 | 6998 | 7007 | 7016 | 7024 | 70337 | 7042 | 7050 | 7059 | 7067 | 9 |  |  |  |  |  |
| 51 | 70767 | 7084 | 7093 | 7101 | 7110 | 71187 | 7126 | 7135 | 7143 | 7152 | 8 |  |  |  |  |  |
| 52 | 71607 | 7168 | 7177 | 7185 | 7193 | 72027 | 7210 | 7218 | 7226 | 7235 | 8 |  |  |  |  |  |
| 53 | 72437 | 7251 | 7259 | 7267 | 7275 | 72847 | 7292 | 7300 | 7308 | 7316 | 8 |  |  |  |  |  |
| 54 | 73247 | 7332 | 7340 | 7348 | 7356 | 73647 | 7372 | 7380 | 7388 | 7396 | 8 |  |  |  |  |  |
| 55 | 74047 | 7412 | 7419 | 7427 | 7435 | 74437 | 7451 | 7459 | 7466 | 7474 | 8 | $\begin{array}{ll}1 & 23 \\ \text { 2,3 }\end{array}$ | 2, 22 |  |  |  |
| 56 | 74827 | 7490 | 7497 | 7505 | 7513 | 75207 | 7528 | 7536 | 7543 | 7551 | 8 | 1 2 <br> 2 4,6 <br> 3 6 | 4,4 | 4, | 4, |  |
| 57 | 75597 | 7566 | 7574 | 7582 | 7589 | 75977 | 7604 | 7612 | 7619 | 7627 | 8 | 3 6,9 <br> 4 9,2 <br>   | 6,6 |  |  |  |
| 58 | 76347 | 7642 | 7649 | 7657 | 7664 | 76727 | 7679 | 7686 | 7694 | 7701 | 7 |  | II, 0 |  |  |  |
| 59 | 77097 | 7716 | 7723 | 7731 | 7738 | 77457 | 7752 | 7760 | 7767 | 7774 | 7 |  | 13,2 15,4 |  |  |  |
| 60 | 77827 | 7789 | 7796 | 7803 | 7810. | 78187 | 7825 | 7832 | 7839 | 7846 | 7 | 8 18,4 <br> 9 20,7 |  |  |  |  |
| 6I | 78537 | 7860 | 7868 | 7875 | 7882 | 78897 | 7896 | 7903 | 7910 | 7917 | 7 |  |  |  |  |  |
| 62 | 79247 | 7931 | 7938 | 7945 | 7952 | 79597 | 7966 | 7973 | 7980 | 7987 | 7 |  |  |  |  |  |
| 63 | 79938 | 8000 | 8007 | 8014 | 8021 | 80288 | 8035 | 804I | 8048 | 8055 | 7 |  |  |  |  |  |
| 64 | 80628 | 8069 | 8075 | 8082 | 8089 | 80968 | 8102 | 8ı09 | 8116 | 8122 | 7 |  |  |  |  |  |
| 65 | 81298 | 8136 | 8142 | 8149 | 8ı56 | 8162 8 | 8169 | 8176 | 8182 | 8189 | 7 |  |  |  |  |  |
| 66 | 8195 8 | 8202 | 8209 | 8215 | 8222 | 82288 | 8235 | 8241 | 8248 | 8254 | 7 |  |  |  |  |  |
| 67 | 8261 | S267 | 8274 | 8280 | 8287 | 82938 | 8299 | 8306 | 8312 | 8319 | 6 | 1 18 <br> 2 1,8 <br> 3 6 | I,7 |  |  |  |
| 68 | 8325 | 833 I | 8338 | 8344 | 8351 | 83578 | 8363 | 8370 | 8376 | 8382 | 6 | 2 3,6 <br> 3 5,4 | 3,4 |  |  |  |
| 69 | 83888 | 8395 | 8401 | 8407 | 8414 | 84208 | 8426 | 8432 | 8439 | 8445 | 6 | $\begin{array}{lll}3 & 3 \\ 4 & 5,4 \\ 7,2\end{array}$ | 6,8 | 6,4 | 6,0 |  |
| 70 | 845I 8 | 8457 | 8463 | 8470 | 8476 | 84828 | 8488 | 8494 | 8500 | 8506 | 6 |  | 8,5 102 |  | 7,5 |  |
| 71 | 85138 | 8519 | 8525 | 8531 | 8537 | 85438 | 8549 | 8555 | 856I | 8567 | 6 |  | 15 |  |  |  |
| 72 | 8573.8 | 8579 | 8585 | 8591 | 8597 | 8603.8 | 8609 | 8615 | 8621 | 8627 | 6 |  |  |  |  |  |
| 73 | 86338 | 8639 | 8645 | 8651 | 8657 | 86638 | 8669 | 8675 | 868I | 8686 | 6 |  |  |  |  |  |
| 74 | 86928 | 8698 | 8704 | 8710 | 8716 | 87228 | 8727 | 8733 | 8739 | 8745 | 6 |  |  |  |  |  |
| 75 | S751 8 | 8756 | 8762 | 8768 | 8774 | 87798 | 8785 | 8791 | 8797 | 8802 | 6 |  |  |  |  |  |
| 76 | 88088 | 8814 | 8820 | 8825 | 883 I | 88378 | 8842 | 8848 | 8854 | 8859 | 6 |  |  |  |  |  |
| 77 | 88658 | 8871 | 8876 | 8882 | 8887 | 88938 | 8899 | 8904 | 8910 | 8915 | 6 |  |  |  |  |  |
| 78 | 89218 | 8927 | 8932 | 8938 | 8943 | 89498 | 8954 | 8960 | 8965 | 8971 | 6 | 13 |  |  |  |  |
| 79 | 89768 | 8982 | 8987 | 8993 | 8998 | 90049 | 9009 | 9015 | 9020 | 9025 | 5 | 1 1,3 <br> 2 2,6 | I,2 | I, I | 1,0 2,0 S |  |
| 80 | 90319 | 9036 | 9042 | 9047 | 9053 | 9058 | 9063 | 9069 | 9074 | 9079 | 5 | 3 3,6 <br> 4 3,9 <br> 5 5,2 | 3,6 |  |  |  |
| 8 I | 90859 | 9090 | 9096 | 9101 | 9106 | 91129 | 9117 | 9122 | 9128 | 9133 | 5 | 5 6,5 <br> 6 7,8 | 6,0 |  |  |  |
| 82 | 9138 | 9143 | 9149 | 9154 | 9159 | 91659 | 9170 | 9175 | 9180 | 9186 | 5 | 7 7 9,1 | 8,4 |  |  |  |
| 83 | 91919 | 9196 | 9201 | 9206 | 9212 | 92179 | 9222 | 9227 | 9232 | 9238 | 5 |  | ¢0,8 |  |  | 7,2 <br> 8,1 |
| 84 | 92439 | 9248 | 9253 | 9258 | 9263 | 92699 | 9274 | 9279 | 9284 | 9289 | 5 |  |  |  |  |  |
| 85 | 92949 | 9299 | 9304 | 9309 | 9315 | 93209 | 9325 | 9330 | 9335 | 9340 | 5 |  |  |  |  |  |
| 86 | 93459 | 9350 | 9355 | 9360 | 9365 | 93709 | 9375 | 9380 | 9385 | 9390 | 5 |  |  |  |  |  |
| 87 | 93959 | 9400 | 9405 | 9410 | 9415 | 94209 | 9425 | 9430 | 9435 | 9440 | 5 |  |  |  |  |  |
| 85 | 94459 | 9450 | 9455 | 9460 | 9465 | 94699 | 9474 | 9479 | 9484 | 9489 | 5 |  |  |  |  |  |
| 89 | 94949 | 9499 | 9504 | 9509 | 9513 | 95189 | 9523 | 9528 | 9533 | 9538 | 5 |  |  |  |  |  |
| 90 | 95429 | 9547 | 9552 | 9557 | 9562 | 95669 | 9571 | 9576 | 9581 | 9586 | 5 | $\xrightarrow{1}{ }_{\text {8 }}^{8}$ | 0,7 |  | -5 | 4 <br> 0,4 |
| 91 | 95909 | 9595 | 9600 | 9605 | 9609 | 96149 | 9619 | 9624 | 9628 | 9633 | 5 |   <br> 3 2, | [1,1 | 1,8 |  |  |
| 92 | 96389 | 9643 | 9647 | 9652 | 9657 | 96619 | 9666 | 9671 | 9675 | 9680 | 5 | 4 3,2 <br> 5 4,0 | 2,8 | 2,4 |  |  |
| 93 | 96859 | 9689 | 9694 | 9699 | 9703 | 97089 | 9713 | 9717 | 9722 | 9727 | 5 |   <br> 5 3,8 <br> 7 4,8 <br> 5  <br> 5  | 4,2 | 3,6 |  |  |
| 94 | 97319 | 9736 | 9741 | 9745 | 9750 | $97549$ | 9759 | 9763 | 9768 | 9773 | 5 | 7 5,8 <br> 88  <br> 8,6  <br> 6  | 4,9 | 4,2 | 3,5 |  |
| 95 | 97779 | 9782 | 9786 | 9791 | 9795 | 98009 | 9805 | 9809 | 9814 | 9818 | 5 | 8  <br> 9 6,4 <br> 7,2  | 6,3 |  |  |  |
| 96 | 98239 | 9827 | 9832 | 9836 | 9841 | 98459 | 9850 | 9854 | 9859 | 9863 | 4 |  |  |  |  |  |
| 97 | 9868 | 9872 | 9877 | 9881 | 9886 | 9890 | 9894 | 9899 | 9903 | 9908 | 4 |  |  |  |  |  |
| 98 | 99129 | 9917 | 9921 | 9926 | 9930 | 99349 | 9939 | 9943 | 9948 | 9952 | 4 |  |  |  |  |  |
| 99 | 99569 | 9961 | 9965 | 9969 | 9974 | 99789 | 9983 | 9987 | 9991 | 9996 | 4 |  |  |  |  |  |
| 100 | 0000 | 0004 | 0009 | OOI3 | 0017 | 00220 | 0026 | 0030 | 0035 | 0039 | 4 |  |  |  |  |  |
| N. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | d. |  | rop. | Par | rts. |  |

Smithsonian Tablee.

## LIST OF METEOROLOGICAL STATIONS.

North America -
Canada ..... PAGE 244
Central America ..... 244
Greenland ..... 244
Mexico ..... 244
United States ..... 245
West Indies ..... 244
South America Page 246
Europe-
Austro-Hungary ..... Page 247
Belgium ..... 248
British Isles ..... 248
Denmark ..... 249
France ..... 249
Germany ..... 250
Greece ..... 248
Holland ..... 248
Italy ..... 25 I
Norway ..... 249
Portugal ..... 253
Roumania ..... 248
Russia ..... 251
Spain ..... 253
Sweden ..... 249
Switzerland ..... 253
Turkey ..... 248
Asia Page 254
Australasia ..... Page 256
Africa and neighboring islands ..... Page 256
International polar stations ..... PAGE 257
Miscellaneous islands Page ..... 257

TABLE 100.

## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| NORTH AMERICA. | Latitude. | Longitude from $\underset{\text { Greenwich. }}{\substack{\text { from } \\ \hline}}$ | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| CANADA. |  |  |  |  |
| Father Point | $48^{\circ} 3 \mathrm{I}^{\prime} \mathrm{N}$. | $68^{\circ} 28^{\prime} \mathrm{W}$. | 20 | 6 |
| * Frederickton | $45 \quad 57$ | 6638 | 164 | 50 |
| * Halifax | 4439 | $63 \quad 36$ | 122 | 37 |
| * Kingston | $44 \quad 14$ | $76 \quad 29$ | 307 | 94 |
| * Montreal | 4530 | $73 \quad 35$ | 187 | 57 |
| Parry Sound | $45 \quad 19$ | 80 o | 641 | 195 |
| Qu'Appelle | 5044 | 10342 |  |  |
| * Quebec. | $46 \quad 48$ | 71 | 293 | 89 |
| * Saint John | $\begin{array}{ll}45 & 17\end{array}$ | 663 | 116 | 35 |
| *Sydney . | 468 | 60 10 | 37 | 11 |
| * Toronto | 4329 | $79 \quad 23$ | 350 | 107 |
| * Westminster | 4912 | 12253 | 33 | ı |
| * Winnepeg | 49 51 | $97 \quad 7$ | 758 | 231 |
| * Woodstock | 438 | 8047 | 980 | 299 |
| CENTRAL AMERICA. (See Mexico.) |  |  |  |  |
| GREENLAND. |  |  |  |  |
| Godthaab | 64 II N. | 5 L 46 W. | 36 | 11 |
| Iviktut | 6112 | 48 II | 16 | 5 |
| Upernivik | 7247 | $55 \quad 53$ | 39 | 12 |
| MEXICO, CENTRAL AMERICA, WEST INDIES, ETC. |  |  |  |  |
| Bermuda, West Indies | $32 \quad 18 \mathrm{~N}$. | $64 \quad 47$ W. | 151 | 46 |
| Guanajuato, Mexico | 210 | 101 15 | 6759 | 2060 |
| * Habana, Cuba . . | $23 \quad 8$ | $76 \quad 35$ | 62 | 19 |
| Kingston, West Indies | $17 \quad 58$ | $76 \quad 48$ | 10 | 3 |
| Leon, Mexico | 217 | IOI 41 | 5899 | 1798 |
| Mazatlan, Mexico | 23 II | 10625 | 249 | 76 |
| Mexico (City of) | 1926 | $99 \quad 8$ | 7487 | 2282 |
| * Nassau, Bahamas | 25 5 | 77 21 | 44 | 13 |
| New Castle, Jamaica | $18 \quad 6$ | $76 \quad 42$ | 3800 | 1158 |
| Pabellon, Mexico | $22 \quad 4$ | 10212 | 6312 | 1924 |
| Port au Prince, Haiti. | 1834 | 72 21 | 1 I 8 | 36 |
| Puebla, Mexico | $19 \quad 2$ | 98 II | 7119 | 2170 |
| St. Thomas, West Indies . | $18 \quad 20$ | 6456 | 131 | 40 |
| Saltillo, Mexico | $25 \quad 25$ | 10038 | 5358 | 1633 |
| San Luis Potosi, Mexico. | $22 \quad 9$ | 10058 | 6201 | 1890 |
| San Salvador, Central America | 1344 | 899 | 2156 | 657 |
| Santiago, Cuba | 1955 | 75 50 | 21 | 6 |
| Tacubaya, Mexico. | 1924 | 9912 | 7621 | 2323 |
| Vera Cruz, Mexico | 1912 | 968 | 23 | 7 |
| Zacatecas, Mexico | $22 \quad 47$ | 10015 | 8189 | 2496 |

## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| WEST INDIES. <br> (See Mexico.) | Latitude. | $\begin{gathered} \text { Longitude } \\ \text { from } \end{gathered}$ Greenwich. | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| UNITED STATES. |  |  |  |  |
| * Abilene, Texas | $32^{\circ} 23^{\prime} \mathrm{N}$. | $99^{\circ} 40^{\prime} \mathrm{W}$. | 1748 | 533 |
| * Albany, New York | 4239 | 7345 | 85 | 26 |
| * Alpena, Michigan | $45 \quad 5$ | 8330 | 609 | 186 |
| * Atlanta, Georgia | 3345 | 8423 | 1131 | 345 |
| * Augusta, Georgia | $33 \quad 28$ | 81 54 | 209 | 64 |
| * Bismarck, North Dakota | $46 \quad 47$ | 10038 | 1698 | 518 |
| * Blue Hill, Massachusetts | 42 13 | 7 7 | 640 | 195 |
| * Boston, Massachusetts | $42 \quad 21$ | 71 | 125 | 38 |
| * Buffalo, New York | 4253 | $78 \quad 53$ | 690 | 210 |
| * Chicago, Illinois. | 4152 | $87 \quad 38$ | 824 | 251 |
| * Cincinnati, Ohio | 396 | 8430 | 628 | 191 |
| * Cleveland, Ohio. | 4130 | 81 42 | 751 | 229 |
| * Columbus, Ohio. | $39 \quad 58$ | 83 o | 837 | 255 |
| * Davenport, Iowa | 4130 | $90 \quad 38$ | 613 | 187 |
| * Denver, Colorado | 3945 | 105 o | 5287 | 1612 |
| * Des Moines, Iowa | 415 | $93 \quad 37$ | 869 | 265 |
| * Detroit, Michigan | $42 \quad 20$ | 83 | 724 | 221 |
| * Dodge City, Kansas . | $37 \quad 45$ | 100 | 2523 | 769 |
| * Duluth, Minnesota | $46 \quad 48$ | 926 | 656 | 200 |
| * Eastport, Maine | 4454 | 6659 | 53 | 16 |
| * E1 Paso, Texas | 3147 | 10630 | 3796 | 1157 |
| * Fort Assiniboine, Montana | $48 \quad 32$ | 10942 | 2690 | 820 |
| * Galveston, Texas | 29.18 | 9450 | 42 | 13 |
| * Hamilton, Mount, California | $37 \quad 20$ | 12 I 39 | 4300 | 1311 |
| * Helena, Montana | $46 \quad 34$ | 1124 | 4118 | 1255 |
| * Huron, South Dakota | 44 21 | $98 \quad 14$ | 1310 | 399 |
| * Indianapolis, Indiana. | $39 \cdot 46$ | 86 то | 766 | 234 |
| *Jacksonville, Florida | 3020 | 8r 39 | 43 | 13 |
| * Kansas City, Missouri | 395 | 9437 | 963 | 294 |
| * Keeler, California | $36 \quad 35$ | 11750 | 3622. | 1104 |
| * Key West, Florida | $24 \quad 34$ | 81 49 | 22 | 7 |
| * Knoxville, Tennessee | $35 \quad 56$ | 8358 | 980 | 299 |
| * Lynchburg, Virginia | $37 \quad 25$ | 799 | 685 | 209 |
| * Manistee, Michigan . | $44 \quad 13$ | 86 16 | 615 | 187 |
| * Marquette, Michigan | 4634 | 8724 | 734 | 224 |
| * Memphis, Tennessee | 359 | 903 | 330 | IOI |
| * Milwaukee, Wisconsin | $43 \quad 2$ | $87 \quad 54$ | 673 | 205 |
| * Moorhead, Minnesota . | $46 \quad 52$ | 9644 | 935 | 285 |
| * Nantucket, Massachusetts | 417 | 706 | 14 | 4 |
| * Nashville, Tennessee | 36 10 | 8647 | 553 | 169 |
| * New Orleans, Louisiana | 2958 | 904 | 54 | 16 |
| * New York City, ( Weather Bureau). | 4043 | $74 \quad 0$ | 185 | 56 |
| * New York, (Central Park) | $40 \quad 46$ | $73 \quad 58$ | 97 | 30 |
| * Norfolk, Virginia. | $36 \quad 51$ | $\begin{array}{ll}76 & 17\end{array}$ | 43 | 13 |

## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| UNITED STATES. (Continued.) | Latitude. | Longitude Greenwich. Greenwich | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
|  | $47^{\circ} \quad 3^{\prime} \mathrm{N}$. | $122^{\circ} 53^{\prime} \mathrm{W}$. | 44 | 13 |
| * Omaha, Nebraska | 4 I 16 | $95 \quad 56$ | 1113 | 339 |
| * Philadelphia, (Girard College) | $39 \quad 58$ | 75 11 | 112 | 34 |
| * Philadelphia, ( Weather Bureau) | 3957 | $75 \quad 9$ | 117 | 36 |
| * Pike's Peak, Colorado. | $38 \quad 50$ | 1052 | 14134 | 4308 |
| * Pittsburg, Pennsylvania | 4032 | 80 2 | 847 | 258 |
| * Portland, Oregon | $45 \quad 32$ | 12243 | 80 | 24 |
| * Rochester, New York | 438 | $77 \quad 42$ | 523 | 159 |
| * Roseburg, Oregon | 43 I3 | 12320 | 523 | 159 |
| * St. Louis, Missouri | $38 \quad 38$ | $90 \quad 12$ | 571 | 174 |
| * St. Paul, Minnesota | 4458 | 933 | 851 | 259 |
| * Salt Lake City, Utah | $40 \quad 46$ | 11154 | 4345 | 1324 |
| * San Diego, California | 3243 | 117 10 | 93 | 28 |
| * San Francisco, California | 3748 | 12226 | 109 | 33 |
| * Santa Fe, New Mexico | 3541 | 105. 57 | 7026 | 2142 |
| * Sault de Ste. Marie, Michigan | $46 \quad 28$ | 8422 | 642 | 196 |
| * Savannah, Georgia | 325 | 81 5 | 87 | 26 |
| Sitka, Alaska | 57 | $135 \quad 19$ | 63 | 19 |
| * Spokane, Washington | 4740 | 11725 | 1938 | 591 |
| * Tampa, Florida | $27 \quad 57$ | $82 \quad 27$ | 36 | 11 |
| * Toledo, Ohio | 4140 | $83 \quad 34$ | 674 | 205 |
| Unalaska, Alaska | 5353 | 16632 | 13 | 4 |
| * Vicksburg, Mississippi | $32 \quad 22$ | $90 \quad 53$ | 254 | 77 |
| * Washington City, (Weather Bureau) | 3854 | $77 \quad 3$ | 112 | 34 |
| * Washington City, (Naval Obs'v'y). | $38 \quad 54$ | 77 3 | 110 | 33 |
| Washington, Mount, N. H | 4416 | 718 | 6279 | 1914 |
| * Wilmington, North Carolina | $\begin{array}{lll}34 & 14\end{array}$ | $77 \quad 57$ | 78 | 24 |
| * Yuma, Arizona | 3245 | 11436 | 141 | 43 |
| SOUTH AMERICA. |  |  |  |  |
| Arequipa . . . . . . . . . . . | 1622 S. | 7122 W. | 8050 | 2454 |
| Bahia-Blanca, Argentine Republic | 3844 S . | 62 II | 49 | 15 |
| Bogota, United States of Colombia | 436 N. | 7315 |  |  |
| Buenos Aires, Argentine Republic | 3436 S . | $58 \quad 22$ | 72 | 22 |
| Caldera, Chile | 273 S . | 7053 | 85 | 26 |
| Caracas, Venezuela | 10 31 N . | 6655 |  |  |
| Catamarca, Argentine Republic | 2828 S. | $65 \quad 56$ | 1788 | 545 |
| Cayenne, French Guiana | 456 N. | 52 21 |  |  |
| Charchani, Peru, (Arequipa) |  |  | 16650 | 5075 |
| Concordia, Argentine Republic . . | 3 I 23 S . | $58 \quad 4$ | 200 | 61 |
| Coquimbo, Chile | 2956 S . | 7121 | 72 | 22 |
| Cordoba, Argentine Republic | 3 I 25 S . | $64 \quad 12$ | 1434 | 437 |
| Corrientes, Argentine Republic . | 2728 S . | 5850 | 253 | 77 |
| El Misti, Peru, (Arequipa) |  |  | 19300 | 5883 |
| Georgetown, British Guiana | 647 N. |  |  |  |
| Iquique, Chile | 2012 S . | 70 11 | 26 | 8 |
| La Plata, Argentine Republic | 3455 S . | $57 \quad 54$ |  |  |

LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)


## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| AUSTRO-HUNGARY. (Continued.) | Latitude. | $\begin{gathered} \text { Longitude } \\ \text { from } \\ \text { Greenwich. } \end{gathered}$ | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| Schafberg | $47^{\circ} 47^{\prime} \mathrm{N}$. | $13^{\circ} 26^{\prime} \mathrm{E}$. | 5827 | 1776 |
| Sonnblick | 473 | 1257 | 10154 | 3095 |
| *Triest | $45 \quad 39$ | 1346 | 85 | 26 |
| * Wien | $48{ }^{\circ} \mathrm{I} 5$ | 16 2I | 663 | 202 |
| Zágráb (see Agram) |  |  |  |  |
| GREECE, ROUMANIA, TURKEY. |  |  |  |  |
| Athens, Greece | 3758 N. | 2345 E. |  |  |
| Bagdad, Asiatic Turkey . | 3319 | 4426 |  |  |
| Beirut, Turkey . | 3354 | $35 \quad 28$ | 112 | 34 |
| * Bucarest, Roumania | 4425 | $26 \quad 6$ | 285 | 87 |
| Constantinople, Turkey | 412 | 2859 |  |  |
| Samsoun, Asiatic Turkey | 418 | 3619 | 26 | 8 |
| Sinaia, Roumania | 45 21 | $25 \quad 34$ | 2822 | 860 |
| Sinope, Turkey | 42 I | $35 \quad 19$ | 49 | 15 |
| Sulina, Roumania | 459 | 2940 | 7 |  |
| Trebizond, Asiatic Turkey | 4 I | 3945 | 92 | 28 |
| BELGIUM AND HOLLAND. |  |  |  |  |
| Arlon, Belgium | 4940 N. | 548 E . | 1286 | 392 |
| Bruxelles, Belgium | 50 51 | 422 | 177 | 54 |
| Furnes, Belgium | 51 | 240 | 1о | 3 |
| * Groningen, Holland | 53 I3 | 634 | 49 | 15 |
| * Helder, Holland . | 5257 | 445 | - | 0 |
| * Liè̀ge, Belgium . | 5037 | 534 | 200 | 61 |
| Maeseyck, Belgium | 51 | 548 | 115 | 35 |
| Maestricht, Holland | 50 51 | 541 | 164 | 50 |
| * Ostende, Belgium | 5114 | 255 | 16 |  |
| * Utrecht, Holland | 525 | 57 | 43 | 13 |
| BRITISH ISLES. |  |  |  |  |
| * Aberdeen. | 57 ıo N. | 26 W. | 88 | 27 |
| * Armagh | 54 21 | 639 | 196 | 60 |
| * Ben Nevis | 5648 | 58 | 4406 | 1343 |
| Dublin | 5322 | 621 | 155 | 47 |
| Dundee. | $56 \quad 28$ | 256 | 160 | 49 |
| Edinburgh | $55 \quad 56$ | 3 II |  |  |
| * Falmouth | 509 | 54 | 183 | 56 |
| * Glasgow | $55 \quad 53$ | $4 \quad 18$ | 180 | 55 |
| * Kew | $\begin{array}{ll}51 & 28\end{array}$ | - 19 | 34 | 10 |
| Londonderry. | 55 - | $7 \quad 19$ | 220 | 67 |
| * Markree Castle . | 54 II | $8 \quad 27$ | 122 | 37 |
| * Oxford | 51 46 | 120 | 212 | 65 |
| Greenwich Observatory | 51 29 | - 0 | 159 | 48 |

## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| $\underset{\text { (Continued.) }}{\text { BRITSH }}$ | Latitude. | Longitude Greromich. | Height above Seai-vel. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| Southampton . | $50^{\circ} 55^{\prime} \mathrm{N}$. | $\mathrm{I}^{\circ} 24^{\prime} \mathrm{W}$. | 78 | 24 |
| Southbourne | 5044 | I 48 | 295 | 90 |
| * Stonyhurst | 5351 | 228 | 375 | 114 |
| * Valencia | 5155 | 1о 18 | 23 | 7 |
| York | 5357 | 1 | 167 | 51 |
| DENMARK, NORWAY, SWEDEN. |  |  |  |  |
| Bodö, Norway | $67 \quad 17 \mathrm{~N}$. | $14 \quad 24 \mathrm{E}$. | 23 | 7 |
| Carlshamn, Sweden | 56 ıо | $14 \quad 52$ | 30 | 9 |
| * Christiania, Norway . | 5955 | 10 43 | 82 | 25 |
| Christiansund, Norway | 637 | 745 | 52 | 16 |
| Dovre, Norway | 625 | 97 | 2110 | 643 |
| Fanö, Denmark | $55 \quad 27$ | 824 | 20 | 6 |
| Florö, Norway | 61 36 | $5 \quad 2$ | 26 | 8 |
| Haparanda, Sweden | 6550 | $24 \quad 9$ | 30 | 9 |
| Hernösand, Sweden | 6238 | $17 \quad 57$ | 49 | 15 |
| Kjöbenhavn, Denmark | 5541 | 1236 | 43 | 13 |
| Skagen, Denmark | 5744 | 10 38 | ıо | 3 |
| Skudesnes, Norway | 599 | 516 | 13 | 4 |
| Stockholm, Sweden | 59 21 | 184 | 144 | 44 |
| * Upsal, Sweden | 5952 | $17 \quad 38$ |  |  |
| * Vandrup, Denmark | 5525 | 9 18 | 13 I | 40 |
| FRANCE. |  |  |  |  |
| Bagnères-de-Bigorre | $43 \quad 4 \mathrm{~N}$. | $\bigcirc 9 \mathrm{E}$. | ${ }^{1795}$ | 547 |
| Besançon | $47 \quad 14$ | $559 \mathrm{E}$. . | 896 | 273 |
| Bordeaux | 4450 | - 3r W. |  |  |
| Brest | 4824 | 430 W. | 210 | 64 |
| Cherbourg | 4939 | 130 W. |  |  |
| Chamonix | 4555 | 72 E . | 3406 | 1038 |
| Dunkerque | 513 | 222 E . | 23 | 7 |
| Langres | $47 \quad 52$ | 520 E . | 1529 | 466 |
| * Lyon | 4541 | 447 E . | 98ı | 299 |
| * Marseille | 4317 | $523 \mathrm{E}$. . | 246 | 75 |
| Mont Blanc (Haute Savoie) | 45 50 | 72 E . | 15780 | 4810 |
| * Mont Ventoux | 4417 | $516 \mathrm{E}$. . | 6234 | 1900 |
| Nautes | 47 I3 | 133 W. | 135 | 41 |
| Nice | 4343 | 718 E . | 1115 | 340 |
| * Paris, (Parc de Saint-Maur) | 4849 | 230 E . | 161 | 49 |
| * Paris, (Tour Eiffel) | 4852 | 218 E . | 1027 | 313 |
| Paris, (Montsouris) | 4849 | 220 E . |  |  |
| * Perpignan | 4242 | 253 E . | 105 | 32 |
| * Pic-du-Midi . | 4257 | - 8 E . | 9380 | 2859 |
| Puy-de-Dome, (Plaine) | 4546 | 35 E . | 1273 | 388 |
| * Puy-de-Dome, (Sommet) | 4547 | 257 E. | 4813 | 1467 |
| * Saint-Martin-de-Hinx | 4335 | 116 W. | 131 | 40 |
| * Toulouse | $43 \quad 37$ | I 26 E . | 636 | 194 |

## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| GERMANY. <br> Bamberg, Bavaria | Latitude. | Longitude from Greenwich. | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
|  | $49^{\circ} 54^{\prime} \mathrm{N}$. | $10^{\circ} 53^{\prime} \mathrm{E}$. | 817 | 249 |
| Berlin, Prussia | 5230 | 1323 | 161 | 49 |
| Borkum, Prussia | 5335 | 640 | 33 | ı |
| Bremen | 53 51 | 848 | 13 | 4 |
| Breslau, Prussia | 517 | $17 \quad 2$ | 482 | 147 |
| Bromberg, Prussia | 538 | 18 o | 138 | 42 |
| Chemnitz, Saxony | 5050 | 1255 | 1037 | 316 |
| Danzig, Prussia | 54 21 | 1840 | 72 | 22 |
| Dresden, Saxony . | 51 | 1344 | 390 | 119 |
| Eichberg, Prussia | 5055 | 1548 | 1145 | 349 |
| Freiberg, Saxony | 5055 | 13 21 | 1335 | 407 |
| Friedrichshafen, Württemberg | 4739 | 928 | 1335 | 407 |
| Göttingen, Prussia . | 51 | 956 | 492 | 150 |
| Halle, Prussia | 5129 | 1138 | 364 | III |
| * Hamburg | 5333 | 958 | 85 | 26 |
| Heidelberg, Baden. | $49 \quad 25$ | 842 | 394 | 120 |
| Hirschberg, Bavaria | 4740 | II 42 | 4954 | 1510 |
| Hohenpeissenberg, Bavaria | $47 \quad 48$ | II | 3261 | 994 |
| Jena, Saxony | 5056 | 1135 | 525 | 160 |
| * Kaiserslautern, Bavaria | $49 \quad 27$ | 746 | 794 | 242 |
| Karlsruhe, Baden | 49 I | 825 | 407 | 124 |
| Kassel, Prussia | 51.19 | 930 | 669 | 204 |
| * Keitum, Prussia | 5454 | 822 | 30 | 9 |
| Kiel, Prussia | 5420 | 10 9 | 154 | 47 |
| Leipzig, Saxony | 5 I 20 | $12 \quad 23$ | 390 | 119 |
| * Magdeburg, Prussia | 528 | $\begin{array}{ll}11 & 38\end{array}$ | 177 | 54 |
| Mannheim, Baden | $49 \quad 29$ | 828 | 367 | 112 |
| * Memel, Prussia | 5543 | 217 | 13 | 4 |
| Metz, Lorraine | 497 | 6 ıо | 600 | 183 |
| Mülhausen, Alsace | $47 \quad 45$ | $7 \quad 20$ | 787 | 240 |
| * München, Bavaria | $48 \quad 9$ | 1136 | 1736 | 529 |
| * Neufahrwasser, Prussia | $54 \quad 24$ | 1840 | 13 | 4 |
| Nürnberg, Bavaria | $49 \quad 27$ | 114 | 1033 | 315 |
| Regensburg, Bavaria | 49 I | 126 | 1175 | 358 |
| Rostock, Mecklenburg | 545 | 127 | 72 | 22 |
| Rügenwaldermünde, Prussia | $54 \quad 26$ | $16 \quad 23$ | 13 | 4 |
| Schneekoppe, Prussia | 5044 | 1544 | 5259 | 1603 |
| Strassburg, Alsace | $48 \quad 35$ | 745 | 472 | 144 |
| Stuttgart, Württemberg | $48 \quad 47$ | 9 10 | 879 | 268 |
| *Swinemünde, Prussia | $53 \quad 56$ | $14 \quad 16$ | 33 | Iо |
| Wendelstein, Bavaria. | $47 \quad 42$ | 12 I | 5666 | 1727 |
| Wilhelmshaven, Oldenburg | $53 \quad 32$ | 89 | 26 | 8 |
| Würzburg, Bavaria | 4948 | 956 | 587 | 179 |
| * Wustrow, Mecklenburg | $54 \quad 21$ | $12 \quad 24$ | 23 | 7 |
| HOLLAND. <br> (See Belgium.) |  |  |  |  |

Smitheonian Tables.

Table 100.
LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)


Smithsonian Tables.

LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)


LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)

| RUSSIA. (Continued.) | Latitude. | Longitude from Greenwich. | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| Tjumen, Siberia | $57^{\circ} 10^{\prime} \mathrm{N}$. | $65^{\circ} 32^{\prime} \mathrm{E}$. | 272 | 83 |
| Tobolsk, Siberia | 58 12 | 68 14 | 171 | 52 |
| Tomsk, Siberia | 5630 | 8458 | 305 | 93 |
| Tunka, Siberia. | 51 45 | 10233 | 2434 | 742 |
| Uman | 4845 | $30 \quad 13$ | 735 | 224 |
| Uralsk | 5 I 12 | $5 \mathrm{I} \quad 22$ | 98 | 30 |
| Urjupinskaja | 5048 | 420 | 302 | 92 |
| Ust-Ssyssolsk | 6140 | $50 \quad 51$ | 413 | 126 |
| Walaam, Finland | 6123 | 3057 | 141 | 43 |
| Warschau | 5213 | 212 | 390 | 119 |
| Wernyj, Siberia | 43 16 | 7653 | 2402 | 732 |
| Wilna | 54 4I | 25. 18 | 348 | 106 |
| Wjatka | $58 \quad 36$ | 49 4I | 587 | 179 |
| Wladikawkas. | 432 | 44 4I | 2244 | 684 |
| Wologda | 5914 | 3953 | 387 | 118 |
| Wyschnij-Wolotschek | $57 \quad 35$ | 3434 | 545 | 166 |
| SPAIN AND PORTUGAL. |  |  |  |  |
| Barcelona, Spain . . . . . . . Cádiz, Spain . . . . . . . . . | $\begin{array}{lll} 4 \mathrm{I} \cdot & 22 & \mathrm{~N} . \\ 36 & 3 \mathrm{I} & \end{array}$ | $\begin{array}{lll} 2 & \text { Io } & \mathrm{E} . \\ 6 & \text { I8 } & \mathrm{W} . \end{array}$ | 69 | 2 I |
| * Coimbra, Portugal | $40 \quad 12$ | 825 W . | 459 | 140 |
| Gibralter. | 366 | 5 2I W. | 53 | 16 |
| * Lisboa, Portugal | 3843 | 99 W . | 312 | 95 |
| Madrid, Spain | $40 \quad 24$ | 3 4I W. | 2149 | 655 |
| Oporto, Portugal | $4 \mathrm{I} \quad 9$ | 827 W. | 279 | 85 |
| Oviedo, Spain . | $43 \quad 23$ | 548 W. | 801 | 244 |
| San Fernando, Spain. | $36 \quad 28$ | - 25 W . | 92 | 28 |
| * Sierra da Estrella, Portugal | $40 \quad 25$ | 735 W . | 4728 | 1441 |
| Valencia, Spain . | $39 \quad 28$ | - 22 W . | 59 | 18 |
| SWEDEN. <br> (See Denmark.) |  |  |  |  |
| SWITZERLAND. |  |  |  |  |
| Altstätten | 4723 N. | 933 E. | 1542 | 470 |
| Altdorf. | $46 \quad 53$ | 839 | I588 | 484 |
| Basel . | $47 \quad 33$ | $7 \quad 35$ | 912 | 278 |
| * Bern | $46 \quad 57$ | 726 | 1880 | 573 |
| Castasegna | $46 \quad 20$ | 931 | 2297 | 700 |
| Chaumont. | 47 I | 659 | 3701 | 1128 |
| Gäbris | $47 \quad 23$ | $9 \quad 28$ | 4III | 1253 |
| Genf | $46 \quad 12$ | 69 | 1339 | 408 |
| Lugano | 46 o | 857 | 902 | 275 |
| Neuenburg | 47 ○ | 657 | 1601 | 488 |
| Rigi-Kulm . | 473 | 830 | 5873 | 1790 |
| * St. Bernhard. | $45 \quad 52$ | 7 II | 8130 | 2478 |

Table 100.
LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)

| $\begin{gathered} \text { SWITZERLAND. } \\ \text { (Continued.) } \\ \text { * Säntis . . . . . . . . . . } \end{gathered}$ | Latitude. | Longitude Greenwich Greenwich. | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
|  | $47^{\circ} 15^{\prime} \mathrm{N}$. | $9^{\circ} 20^{\prime} \mathrm{E}$. | 8202 | 2500 |
| Sils-Maria | $46 \quad 26$ | 946 | 5938 | 18ı0 |
| Zürich | $47 \quad 23$ | 833 | 1542 | 470 |
| TURKEY. (See Greece.) |  |  |  |  |
| ASIA. |  |  |  |  |
| [The Stations are in India unless otherwise indicated. For Siberian Stations, see Russia.] |  |  |  |  |
| Aden, Arabia . . . . . . . . . . . . | 1245 N. | 453 E. | 94 | 29 |
| Ajmere | $26 \quad 28$ | 7437 | 1611 | 491 |
| Akyab. | $20 \quad 28$ | 9257 | 20 | 6 |
| * Allahabad | $25 \quad 26$ | 8 5 5 | 309 | 94 |
| Amini Divi | II 6 | 7248 | 15 | 5 |
| Bangalore . | 1259 | $77 \quad 38$ | 2981 | 909 |
| Belgaum | $15 \quad 52$ | $74 \quad 42$ | 2524 | 769 |
| Bellary | 159 | $76 \quad 57$ | 1475 | 450 |
| Benares | $25 \quad 20$ | $83 \quad 2$ | 267 | 81 |
| Berhampore | $24 \quad 6$ | 88 17 | 66 | 20 |
| Bhamo | $24 \quad 12$ | $96 \quad 58$ |  |  |
| * Bombay | $18 \quad 54$ | 7249 | 37 | 11 |
| Bushire, Persia | $28 \quad 59$ | $50 \quad 49$ | 25 | 8 |
| * Calcutta | $22 \quad 32$ | 8820 | 21 | 6 |
| Chamba | 3234 | 76 ıо | 3005 | 916 |
| Chemulpo, Corea | 3729 | 12633 | 30 | 9 |
| Chittagong | 22 21 | 9150 | 87 | 26 |
| Colombo | 656 | $79 \quad 52$ | 40 | 12 |
| Cuttack | $20 \quad 29$ | 8554 | 80 | 24 |
| Dacca | 2343 | $90 \quad 27$ | 22 | 7 |
| Deesa | $24 \quad 16$ | 7214 | 466 | 142 |
| Delhi | 2840 | 77 16 | 718 | 219 |
| Dhubri | $26 \quad 7$ | 8950 | 115 | 35 |
| Diamond Island | $15 \quad 52$ | $94 \quad 19$ | 41 | 12 |
| Fusan, Corea | 356 | 12930 |  |  |
| Hakodate, Japan | $4 \mathrm{I} \quad 46$ | 14044 | ıо | 3 |
| Hiroshima, Japan | 3423 | 13227 | 14 | 4 |
| * Hong-Kong, China | $22 \quad 18$ | 114 II | 110 | 34 |
| Hyderabad | $25 \quad 25$ | $68 \quad 27$ | 117 | 36 |
| Indore | 2244 | $75 \quad 53$ | 1823 | 556 |
| Jeypore | $26 \quad 55$ | 75 50 | 1431 | 436 |
| Jhansi | $25 \quad 27$ | $78 \quad 37$ | 840 | 256 |
| Jubbulpore | $23 \quad 9$ | 7959 | 1341 | 409 |
| Kagoshima, Japan | 3135 | 13033 | 13 | 4 |
| Kanazawa, Japan | 3633 | 13640 | 95 | 29 |
| Kandy | $7 \quad 18$ | 80 | 1696. | 517 |
| Kaschgar, China | 3925 | $76 \quad 7$ | 3999 | 1219 |
| Katmandu | $27 \quad 42$ | $85 \quad 12$ | 4388 | 13388 |
| Kelung, China | $25 \quad 20$ | 12146 | 33 | Iо |

LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)

| ASIA. <br> (Continued.) | Latitude. | $\begin{gathered} \text { Longitude } \\ \text { from } \end{gathered}$ $\begin{gathered} \text { Grom } \\ \text { freenwich. } \end{gathered}$ | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| Kioto, Japan | $35^{\circ} \quad \mathrm{I}^{\prime} \mathrm{N}$. | $135^{\circ} 46^{\prime} \mathrm{E}$. | 161 | 49 |
| Kurrachee | 2447 | $67 \quad 4$ | 49 | 15 |
| * Lahore | 3134 | 7420 | 702 | 214 |
| Leh | 34 1о | 7742 | 11503 | 3506 |
| Lucknow | 2650 | 8 I o | 369 | 112 |
| Madras | 134 | 8014 | 22 | 7 |
| Mandalay | 2159 | 968 |  |  |
| Mangalore | 1252 | 7454 | 26 | 8 |
| Matsuyama, Japan | 3350 | 13245 | 105 | 32 |
| Mergui | 12 II | $98 \quad 38$ | 96 | 29 |
| Moulmein | $16 \quad 29$ | 9740 | 94 | 29 |
| Mussooree | $30 \quad 28$ | $78 \quad 7$ | 6881 | 2097 |
| Nagasaki, Japan | 3244 | 12952 | 190 | 58 |
| Nagoya, Japan | 35 10 | 13655 | 49 | 15 |
| Nagpur | 219 | 79 II | 1025 | 312 |
| Nemuro, Japan . | 4320 | 14535 | 89 | 27 |
| Niigata, Japan | 3755 | 1393 | 85 | 26 |
| Oita, Japan | 3313 | 13136 | 26 | 8 |
| Osaka, Japan | 3442 | 135 31 | 23 | 7 |
| Patna | $25 \quad 37$ | 8514 | 183 | 56 |
| Peking, China | 3957 | 11628 | 125 | 38 |
| Peshawar | $34 \quad 2$ | 7137 | 1110 | 338 |
| Poona | $18 \quad 28$ | 74 1о | 1840 | 56I |
| Quetta, Beluchistan | 3011 | $67 \quad 3$ | 5502 | 1677 |
| Raipur | $21 \quad 15$ | 8 rar | 960 | 293 |
| Rajkot. | $22 \quad 17$ | 7052 | 429 | 131 |
| Rangoon | 1646 | $96 \quad 12$ | 4 I | 12 |
| Sakai, Japan | $35 \quad 33$ | 13314 | 7 | 2 |
| Sapporo, Japan | $43 \quad 4$ | 14122 | 56 | 17 |
| Saugor Island | 2 Cl | 88 | 25 | 8 |
| Silchar | 2449 | 9250 | 104 | 32 |
| Simla | 316 | $77 \quad 12$ | 7048 | 2148 |
| Si-wan-tse, China | 4059 | $115 \quad 18$ | 3904 | 1190 |
| Söul, Corea | $37 \quad 35$ | $127 \quad 7$ | 118 | 36 |
| Soya, Japan | $45 \quad 31$ | 14155 | 79 | 24 |
| Surat | $21 \quad 13$ | 7246 | 36 | 11 |
| Taku, China | $38 \quad 59$ | 11740 | 33 | 10 |
| Tezpur | $26 \quad 36$ | 9250 | 251 | 76 |
| Tokio, Japan | 3541 | 13945 | 69 | 21 |
| Trichinopoly | 10 50 | $78 \quad 44$ | 255 | 78 |
| Udan, China | 4435 | 11110 |  |  |
| Urga, China | $47 \quad 55$ | 10650 | 3773 | 1150 |
| Vizagapatam | 1742 | $83 \quad 22$ | 31 | 9 |
| Wakayama, Japan | $34 \quad 14$ | 1359 | 49 | 15 |
| Yuensan, Corea | 39 וо | 12725 |  |  |
| * Zi-Ka-Wei, China | $31 \quad 12$ | 1196 | 23 | 7 |

## LIST OF METEOROLOGICAL STATIONS.

(The asterisk * designates stations of the first order.)

| AUSTRALASIA. <br> Adelaide, South Australia . | Latitude. | Longitude Greenwich Greenwich | Height above Sea-level. |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $34^{\circ} 57^{\prime} \mathrm{S}$. | $138^{\circ} 35^{\prime} \mathrm{E}$. | Feet. | m. |
| Albany, West Australia | $35 \quad 2$ | 11754 | 88 | 27 |
| Alice Springs, South Australia | $23 \quad 38$ | 13337 | 2100 | 640 |
| Auckland, New Zealand | 3650 | 174 51 | 258 | 79 |
| * Batavia, Java. | 6 II | 10650 | 26 | 8 |
| * Boulia, Queensland | 2255 | 13938 |  |  |
| Bourke, New South Wales | 303 | 14558 | 347 | 106 |
| * Brisbane, Queensland. | $27 \quad 28$ | 1536 | 137 | 42 |
| * Burketown, Queensland | 1748 | 13934 |  |  |
| * Cooktown, Queensland | $15 \quad 28$ | 14517 |  |  |
| Derby, West Australia | 178 | 12339 | 17 | 5 |
| Eucla, South Australia | 3145 | 12858 | 7 | 2 |
| Hobart, Tasmania. | 4253 | 14720 | 190 | 58 |
| * Mackay, Queensland | 219 | 149 I3 |  |  |
| Malacca, Straits Settlements | 2 10 N. | 10214 | 12 | 4 |
| * Manila, Philippine Islands . | 1435 N. | 12058 | 46 | 14 |
| Melbourne, Victoria . | 3750 S . | 145 o | 91 | 28 |
| Penang, Straits Settlement. | 52 N . | 10020 | 20 | 6 |
| Perth, West Australia . | $3 \mathrm{I} \quad 57 \mathrm{~S}$. | $115{ }^{1} 5$ | 47 | 14 |
| Port Darwin, South Australia | 1228 S . | 13051 | 70 | 21 |
| Province Wellesley, Straits Settlement. | 522 N. | 10030 | 43 | 13 |
| Singapore, Straits Settlement | 17 N. | 103 51 | 10 | 3 |
| * Sydney, New South Wales . | $33 \quad 52 \mathrm{~S}$. | 15112 | 155 | 47 |
| * Thargomindah, Queensland | 27. $5^{8} \mathrm{~S}$. | 14343 |  |  |
| * Thursday Island, Queensland | 10 34 S . | 14212 |  |  |
| Wellington, New Zealand | 41 I 6 S. | 17447 | 140 | 43 |
| AFRICA AND NEIGHBORING ISLANDS. |  |  |  |  |
| Alexandria, Egypt | $3 \mathrm{I} \quad 12 \mathrm{~N}$. | 2953 E . | 62 | 19 |
| Assab, Abyssinia | 1259 | 4245 | 36 | 11 |
| Alger, Algeria | 3647 | 34 | 125 | 38 |
| Biskra, Algeria | 34 51 | 540 | 400 | 122 |
| Bizerte, Tunis | 3717 | 950 | 20 | 6 |
| Cairo, Egypt . | 305 | 3117 |  |  |
| Cape Town, Cape Colony | 3356 S . | $18 \quad 29$ | 40 | 12 |
| Ceres, Cape Colony | $33 \quad 22 \mathrm{~S}$. | 1920 | 1493 | 455 |
| Constantine, Algeria | $36 \quad 22 \mathrm{~N}$. |  | 2165 | 660 |
| Cradock, Cape Colony . | 32 Ir S. | $25 \quad 38$ | 2856 | 870 |
| Fort Napier, Natal . | 2936 S. | 3023 | 2200 | 671 |
| Fort National, Algeria | $36 \quad 38 \mathrm{~N}$. | 412 | 3005 | 916 |
| Gabès, Tunis | 3353 N. | 10 7 | 33 | 10 |
| Ghardaia, Algeria | 3235 N . | 340 | 1706 | 520 |
| Grahamstown, Cape Colony | 3320 S . | 2633 | 1800 | 549 |
| Ismailia, Egypt | $30 \quad 36 \mathrm{~N}$. | 3216 | 30 | 9 |
| Kimberley, Cape Colony | $28 \quad 43 \mathrm{~S}$. | 2646 | 4050 | 1234 |

LIST OF METEOROLOGICAL STATIONS.
(The asterisk * designates stations of the first order.)

| AFRICA AND NEIGHBORING ISLANDS. (Continued.) | Latitude. | Longitude Greenwich <br> Greenwic | Height above |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet. | m. |
| Laghouat, Algeria | $33^{\circ} 48^{\prime} \mathrm{N}$. | $2^{\circ} 55^{\prime} \mathrm{E}$. | 2454 | 748 |
| Memours, Algeria | 356 N. | 15 W . | 13 | 4 |
| Oran, Algeria | 3542 N. | - 39 W . | 197 | 60 |
| Port Elizabeth, Cape Colony | 3357 S . | 2537 E . | 18 r | 55 |
| Port-Saïd, Egypt . | $3 \mathrm{I} \quad 16 \mathrm{~N}$. | 3218 E . | 20 | 6 |
| Queenstown, Cape Colony | 3 I 51 S. | 26 51 E. | 3500 | 1067 |
| * St. Paul de Loando, Angolo | 849 S . | 137 E . | 194 | 59 |
| Sierra Leone, Senegambia | 830 N. | 139 W . | 224 | 68 |
| Sidi-Bel-Abbes, Algeria | $35 \quad 2 \mathrm{~N}$. | - 39 W. | 1562 | 476 |
| Suez, Egypt | 2959 N. | 3230 E . | ıо | 3 |
| Tamatave, Madagascar | 18 10 S. | 4925 E . | го | 3 |
| Tananarive, Madagascar | 1855 S. | 4736 E . | 4593 | 1400 |
| Tripoli | 3253 N. | 13 II E. | 66 | 20 |
| Vivi, Congo | 540 S . | 1349 E . | 364 | 111 |
| INTERNATIONAL POLAR STATIONS. |  |  |  |  |
| Bossekop, (Norway) | ${ }_{69} 97 \mathrm{~N}$. | 2315 E . |  |  |
| Dicksonhavn, (Holland) | $73 \quad 30$ | 8 I ○ E. |  |  |
| Fort Rae, (Great Britain) | 6239 | 11544 W. |  |  |
| Godthaab, (Denmark) | 64 II | 5144 W. |  |  |
| Jan Mayen, (Austria) | $70 \quad 59$ | 828 W. |  |  |
| Kingua-Fjord, Cumberland Sound, (Germany). | $66 \quad 36$ | 679 W . |  |  |
| Lady Franklin Bay, (United States) | 8I 44 | 6445 W. |  |  |
| Nowaja Semlja, (Russia) | 7230 | 5245 E . |  |  |
| Orange Baie, Cape Horn, (France) | 5531 S . | 7025 W . |  |  |
| Point Barrow, (United States) | $7 \mathrm{7} \quad 23 \mathrm{~N}$. | 15640 W. |  |  |
| Sagastyr, Lena River, (Russia) | 73 ll 23. | 1245 E . |  |  |
| Sodankylä, (Finland) | $\begin{array}{ll}67 & 27 \mathrm{~N} .\end{array}$ | 2636 E . |  |  |
| Spitzbergen,(Sweden), Cap Thordsen | $78 \quad 28 \mathrm{~N}$. | 1542 E . |  |  |
| Suid-Georgien, (Germany) | 5431 S . | 36 ○ W. |  |  |
| MISCELLANEOUS ISLANDS. |  |  |  |  |
| Barbados | $13 \quad 8 \mathrm{~N}$. | 5940 W. | 31 |  |
| Honolulu, Hawaiian Islands | 21.18 | 15750 W. | 50 | 15 |
| La Canee, Crête | 3530 | 24 o E. | 141 | 43 |
| Las Palmas, Canaries | 2728 | 1527 W. | 30 |  |
| Malta, Mediterranean | 3554 | $14 \mathrm{3I} \mathrm{E}$. | 70 | 2 I |
| Massaua, Red Sea | 1536 | 3927 E . | ıо | 3 |
| * Port Louis, Mauritius | 206 S. | 5733 E . | 180 | 55 |
| *St. Helena | 1555 S. | 543 W . | 40 | 12 |
| Sainte-Croix, Teneriffe | 2829 N. | 1621 W. | 118 | 36 |
| Stanley, Falkland Islands | 514 S . | 575 Fl W. |  |  |
| Stykkisholm, Iceland | $65 \quad 5 \mathrm{~N}$. | 2246 W. | 36 | 11 |
| Thorshavn, Färoë Islands | $62 \quad 2 \mathrm{~N}$. | 644 w . | 30 | 9 |

## APPENDIX.

## CONSTANTS.

## Numerical Constants.

Base of natural (Naperian) logarithms, Log $e$, modulus of common logarithms, Circumference of circle in degrees,
" " " " in minutes,

Circumference of circle, diameter unity,

> Number. Logarithm.

| $2 \pi$ | $=6.2831853$ | 0.7981799 |
| ---: | :--- | ---: | :--- |
| $\frac{\pi}{3}$ | $=1.0471976$ | 0.0200286 |
| $\frac{1}{\pi}$ | $=0.3183099$ | 9.5028501 |
| $\pi^{2}$ | $=9.8696044$ | 0.9942997 |


| $e=2.7182818$ | 0. 4342945 |
| :---: | :---: |
| $M=0.4342945$ | 9.6377843 - 10 |
| 360 | 2.5563025 |
| 21600 | 4.3344538 |
| $=1296000$ | 6.1126050 |
| $\pi=3.14159265$ | 0.4971499 |
| 1/ $\boldsymbol{\pi}^{2}=0.1013212$ | 9.0057003 - Io |
| $\sqrt{\bar{\prime}}=1.7724539$ | 0.2485749 |
| $\frac{\mathrm{I}}{\sqrt{\bar{\pi}}}=0.5641896$ | 9.751425 I - 10 |
| $\sqrt{2}=1.4142136$ | 0.1505150 |
| $\sqrt{3}=1.7320508$ | 0.2385607 |

The arc of a circle equal to its radius is in degrees, $\rho^{\circ}=180 / \pi$ in minutes, $\rho^{\prime}=60 \rho^{\circ}$ in seconds, $\rho^{\prime \prime}=60 \rho^{\prime}$
For a circle of unit radius, the arc of $I^{\circ}=1 / \rho^{\circ}$ arc of $\mathrm{I}^{\prime}=\mathrm{I} / \rho^{\prime}$ arc (or sine) of $\mathrm{I}^{\prime \prime}=1 / \rho^{\prime \prime}$
$=57.29578 \quad$ 1.7581226
$=3437.7468^{\prime} \quad 3.5362739$
$=206264.8^{\prime \prime} \quad 5.3144251$

## Geodetical Constants.

Dimensions of the earth (Clarke's spheroid, 1866) and derived quantities :

Equatorial semi-axis in feet,
in miles,
Polar semi-axis in feet,
in miles,
$a=20926062$.
$a=3963.3$
7.3206875
$b=2085512 \mathrm{I}$.
3.5980536
$b=\quad 39498$
$(\text { Eccentricity })^{2}=\frac{a^{2}-b^{2}}{a^{2}}$
Flattening $=\frac{a-b}{a}$
Perimeter of meridian ellipse,
Circumference of equator,
Area of earth's surface,
Mean density of the earth (Harkness)
Surface density "
Acceleration of gravity (Harkness) :
$g_{\phi}(\mathrm{cm}$. per second $)=980.60(\mathrm{I}-0.002662 \cos 2 \phi)$, for latitude $\phi$ and sea level. $g$, at equator $=977.99 ; g$, at Washington $=980.07 ; g$, at Paris $=980.94$. $g$, at poles $=983.2 \mathrm{I} ; g$, at Greenwich $=98 \mathrm{I} .17$;
Length of the seconds pendulum (Harkness) :
$l=39.012540+0.208268 \sin ^{2} \phi$ inches $=0.990910+0.005290 \sin ^{2} \phi$ metres.

## CONSTANTS.- Continued.

## Astronomical Constants (Harkness).

Sidereal year $=365.2563578$ mean solar days.
Tropical year $=365.2422 \mathrm{~d}$. Sidereal day $=23^{h} 5^{6 m} 4$. Ioos mean solar time. Mean solar day $=24^{h} 3^{m} 56.546 s$ sidereal time.
Mean distance of the earth from the sun $=92800000$ miles.

## Physical Constants.

Velocity of light (HARKNESS $)=186337$ miles per second $=299878 \mathrm{~km}$. per second. Velocity of sound through dry air $=1090 \sqrt{\mathrm{I}+0.00367 t^{\circ} C}$. feet per second. Weight of distilled water, free from air, barometer 30 inches:

## Volume.

r cubic inch (determination of 1890 )
x cubic centimetre ( 1890 )
I cubic foot (1890) at $62^{\circ} F$.

| Weight in grains. |  |
| :--- | :---: |
| $62^{\circ} \mathrm{F}$. | $4^{\circ} \mathrm{C}$. |
| 252.286 | 252.568 |
| 15.3953 | 15.4125 |
| 62.2786 lbs. |  |

Weight in grammes. $62^{\circ} \mathrm{F}$. $\quad 4^{\circ} \mathrm{C}$.
$16.3479 \quad \mathrm{I} 6.3662$ $0.9976 \quad 0.9987$ 62.2786 lbs .

A standard atmosphere is the pressure of a vertical column of pure mercury whose height is 760 mm . and temperature $0^{\circ} C$., under standard gravity at latitude $45^{\circ}$ and at sea level.
r standard atmosphere $=1033$ grammes per sq. $\mathrm{cm} .=14.7$ pounds per sq. inch.
Pressure of mercurial column I inch high $=34.5$ grammes per sq. $\mathrm{cm} .=0.49 \mathrm{I}$ pounds per sq. inch.
Weight of dry air (containing 0.0004 of its weight of carbonic acid) :
I cubic centimetre at temperature $32^{\circ} \mathrm{F}$. and pressure 760 mm . and under the standard value of gravity weighs 0.00129305 gramme.
Density of mercury at $o^{\circ} C$. (compared with water of maximum density under atmospheric pressure) $=13.5956$.
Freezing point of mercury $=-38^{\circ} .5 \mathrm{C}$. (REGNAULT, I862.)
Coefficient of expansion of air (at const. pressure of 760 mm ) for $\mathrm{I}^{\circ} \mathrm{C}$. (DO.): 0.003670 .
Coefficient of expansion of mercury for Centigrade temperatures (BROCH):
$\Delta=\Delta_{0}$ ( $1-0.00018 \mathrm{I} 792 t-0.000000000 \mathrm{r}^{7} \mathrm{t}^{2}$-. $000000000035 \mathrm{II} 6 t^{3}$ ).
Coefficient of linear expansion of brass for $I^{\circ} C$., $\beta=0.0000174$ to 0.000 orgo.
Coefficient of cubical expansion of glass for $\mathrm{r}^{\circ} C$., $\gamma=0.000021$ to 0.000028.
Ordinary glass (Recknagel): at $10^{\circ} C ., \gamma=0.0000255$; at $100^{\circ}, \gamma=0.0000276$.
Specific heat of dry air compared with an equal weight of water :
at constant pressure, $K_{p}=0.2374$ (from $0^{\circ}$ to $100^{\circ} C_{\text {., Regnaulit). }}$ at constant volume, $K_{v}=0.1689$.
Ratio of the two specific heats of air (RÖNTGEN): $K_{p} / K_{v}=1.4053$.
Thermal conductivity of air (GraETz) : $k=0.0000484$ ( $\mathrm{I}+0.00185 t^{\circ} \mathrm{C}$.) $\frac{\text { gramme }}{\mathrm{cm} . \mathrm{sec} .}$.
[The quantity of heat that passes in unit time through unit area of a plate of unit thickness, when its opposite faces differ in temperature by one degree.]
Latent heat of liquefaction of ice (BUNSEN) $=80.025$ mass-degrees, $C$.
Latent heat of vaporization of water $=606.5-0.695 t^{\circ} \mathrm{C}$.
Absolute zero of temperature (Thomson, Heat, Encyc. Brit.): -273.0 C. $=-459.4$ F.
Mechanical equivalent of heat*:
I pound-degree, $F$. (the British thermal unit) $=$ about 778 foot-pounds.
I pound-degree, $C$. $=1400$ foot-pounds.
r calorie or kilogramme-degree, $C$. $=3087$ foot-pounds $=426.8$ kilogrammetres $=4187$ joules (for $g=98 \mathrm{Icm}$.).

[^10]APPIENDIX.

## SYNOPTIC CONVERSION OF ENGLISH AND METRIC UNITS. English to Metric.

## Units of length.

I inch.
I foot.
I yard.
I mile.

## Units of area.

I square inch.
I square foot.
I square yard.
I acre.
I square mile.

## Units of volume.

I cubic inch.
I cubic foot.
I cubic yard.

## Metric equivalents.

2.54000
0.304801
0.914402

## 1. 60935

6.4516 929.034 0.83613 0.404687
2.5900 259
centimetres.
metre.
kilometres.
square centimetres.
square metre.
hectares.
square kilometres. hectares.
16.3872 cubic centimetres.
0.028317 cubic metres or steres.
0.76456

## Logarithms.

0.404835
9.484 OI6 - 10
9.96 I 137 - 10
0.206650
0.809669
2.968032
9.922274 - 10
9.607120 - 10
0.413300
2.413300

1. 214504
8.452047 - 10
9.883 4II - IO

## Units of capacity.

1 gallon (U.S.) $=231$ cubic inches.
I quart (U. S.)
I Imperial gallon (British).
277.463 cubic inches (1890).

I bushel (U. S.) $=2150.42$ cubic inches.
I bushel (British).
Units of mass.
I grain.
I ounce avoirdupois.
I ounce troy.
I ton ( 2240 lbs.).

## Units of velocity.

I foot per sec. ( 0.68 I 8 miles per hr. $)=0.30480$ metres per sec. $=1.0973 \mathrm{~km}$. per hr.
I mile per hr. ( 1.46667 feet per sec. $)=0.44704$ metres per sec. $=1.6093 \mathrm{~km}$. per hr.

## Units of force.

1 poundal. 13825.5 dynes. 4.140682
Weight of I grain (for $g=98 \mathrm{Icm}$.). $\quad 63.57$ dynes. 1.803237
Weight of 1 pound av. (for $g=98 \mathrm{Icm}$.). $4.45 \times 10^{5}$ dynes. 5.648335

## Units of stress-in gravitation measure.

I pound per square inch $=70.307$ grammes per sq. centimetre. $\quad 1.846997$
I pound per square foot $=4.8824$ kilogrammes per sq. metre.
0. 688634

## Units of work-in absoiute measure.

I foot-poundal.
421403 ergs.
5.624697
-in gravitation measure.
I foot-pound (for $g=98 \mathrm{Icm}$.) $=1356.3 \times 10^{4}$ ergs $=0.138255$ kilogram-metres.
Units of activity (rate of doing work).
I foot-pound per minute (for $g=98 \mathrm{Icm}$.) $=0.022605$ watts.
r horse-power ( 33000 foot-pounds per min.) $=746 \mathrm{watts}=1.01387$ force de cheval.

## Units of heat.

I pound-degree, $F$.
$=252$ small calories or gramme-degrees, $C$.
I pound-degree, $C$.
$=\mathrm{r} .8$ pound-degrees, $F$.

APPENDIX.

## SYNOPTIC CONVERSION OF ENGLISH AND METRIC UNITS.

## Metric to English.

## Units of length.

1 metre ( $10^{6}$ microns).
"
I kilometre.
Units of area.
I square centimetre.
I square metre.
1 are ( $=$ Ioo square metres).
I hectare.
I square kilometre.
Units of volume.
I cubic centimetre.
I cubic metre or stere.

## Units of capacity.

I litre ( 61.023 cubic inches).
"،
hectolitre.

## Units of mass.

I gramme.
I kilogramme.
،
I tonne.

## Units of velocity,

I metre per second.
I km. per hr. ( 0.2778 m . per sec.)

English equivalents.
39.3700
3.28083
1.09361
0.62137

0.15500
10.7639
1.19599
19.599
2.47104
0.38610

## Logarithms.

1. 595165
0.515984
0.038863
9.793350 - 10
2. 19033 I - 10
I.03I 968
0.077726
2.077726
0.392880
9.586700 - 10

| 0.06 Io234 | cubic inches. | $8.785496-$ Iо |
| :---: | :--- | :--- |
| 35.3145 | cubic feet. | I. 547953 |
| I.30794 | cubic yards. | 0.116589 |

I. 30794 cubic yards.
0.26417 gallons (U. S.). 9.42I 884 - 10
$\begin{array}{ll}\text { I. } 05668 & \text { quarts (U. S.). } \\ 0.21993 & \text { Imp. gallons (British). }\end{array}$

$$
0.023944
$$

9.342 291 - 10
2.7512 bushels (British)
0.452973
0.439523

| 15.4324 | grains. | I. 188432 |
| :---: | :--- | :--- |
| 2.20462 | pounds avoirdupois. | 0.343334 |
| 35.274 | ounces avoirdupois. | I.547454 |
| 32.1507 | ounces troy. | 1.507191 |
| 0.9842 I | tons (2240 1bs.). | $9.993086-$ Io |

3.2808 feet per second. 0.5 I 5984
2.2369 miles per hour. 0.349653
0.62137 miles per hour.
9.793350 - 10

## Units of force.

I dyne (weight of $(98 \mathrm{I})^{-1}$ grammes, for $g=98 \mathrm{rcm}$.) $=7.2330 \times 1 \mathrm{o}^{-5}$ poundals.
Units of stress-in gravitation measure.

I gramme per square centimetre.
I kilogramme per square metre. I standard atmosphere.
0.014223 pounds per sq. inch.
0.20482 pounds per sq. foot.
14.7 pounds per sq. inch. (See def. p. 259.)

## Units of work-in absolute measure.

1 erg.
$2.3730 \times 10^{-6}$ foot-poundals.
I megalerg $=10^{6}$ ergs; r joule $=10^{7}$ ergs.
-in gravitation measure.
I kilogram-metre (for $g=98 \mathrm{rcm}$.) $=98 \mathrm{r} \times 10^{5} \mathrm{ergs}=7.2330$ foot-pounds.
Units of activity (rate of doing work).
I watt.
44.2385 foot-pounds per minute, for $g=98 \mathrm{Icm}$.

I watt $=1$ joule per sec. $=0$. 10194 kilogram-metre per sec., for $g=98 \mathrm{Icm}$.
r force de cheval $=75$ kilogram-metres per sec. $=735^{\frac{3}{4}}$ watts $=0.98632$ horse-power.
Units of heat.
I calorie or kilogramme-degree $=3.968$ pound-degrees, $F=\mathbf{2 . 2 0 4 6}$ pound-degrees, $C$. I small calorie or therm, or gramme-degree $=0.001$ calorie or kilogramme-degree.

## DIMENSIONS OF PHYSICAL QUANTITIES.

$\mathrm{L}=$ length $; \mathbf{M}=$ mass ; $\mathrm{T}=$ time .


## INTERNATIONAL METEOROLOGICAL SYMBOLS.

The International Meteorological Congress, held at Vienna, in September, 1873, decided that it was desirable to introduce for various meteorological conditions, symbols which should be independent of any national language and therefore universally intelligible. From the symbols and abbreviations then in use among different nations, the Permanent Committee of the Congress selected a number for international use. The symbols were modified by the Congress at Munich, in 189r, and the abbreviations for clouds by the Conference at Upsala, in 1894.

References :
"Summary of Resolutions of the Vienna Congress, Appendix K." p. 64. Prepared by Mr. Robert H. Scott, Secretary.
" Bericht über die Int. Meteor. Conferenz in München, I89r," p. 19.
"Report of the Int. Met. Conference at Munich," p. 20.
" Circular of the U. S. Weather Bureau, January I, 1894.
The intensity of the condition is indicated by the small figures ${ }^{\circ}$ and ${ }^{2}$ which are used as exponents of the symbols. Zero $\left({ }^{\circ}\right)$ denotes very slight intensity; two ( ${ }^{2}$ ) strong or marked. Absence of an exponent indicates moderate intensity. A dash ( - ) indicates continuance.

Example.


Translation.
Light rain. Moderate rain. Heavy rain.
rst. Silent lightning from 9-10 p. m. in the E .
4th. Heavy rain ended io a. m.; thunderstorm from 3 to $5 \mathrm{p} . \mathrm{m}$.
16th. Dense haze in the morning; heavy snow from ir. $30 \mathrm{a} . \mathrm{m}$. to $2.50 \mathrm{p} . \mathrm{m}$.

The time of occurrence is expressed in hours; morning and afternoon by a. and p. respectively. The hours are counted from o to 12 commencing with midnight.

Where tables are printed, maximum and minimum values will be in heavy-faced type.

Absence of precipitation is denoted by a dot (.), and amounts less than .or inch (formerly marked $T$ ) are recorded .oo.

| - | means | Degree. | Mi. | means | Miles. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| F | " | Fahrenheit. | Kil. | " | Kilometers. |
| C | " | Centigrade. | N. | " | Nimbus. |
| Ci. | " | Cirrus. | AS. | " | Alto-stratus. |
| Ci. Cu . | " | Cirro-cumulus. | CuN . | " | Cumulo-nimbus. |
| Ci. S. | " | Cirro-stratus. | Fr. Cu . | " | Fracto-cumulus. |
| A. Cu . | " | Alto-cumulus. | Fr. N. | " | Fracto-nimbus. |
| Cu . | " | Cumulus. | Fr. S. | ، | Fracto-stratus. |
| S. Cu. | " | Strato-cumulus. | Scf. | " | Stratus cumuliformis. |
| S | " | Stratus. | Ncf. | " | Nimbus cumuliformis |
| Max. | " | Maximum. | MCu . | " | Mammato cumulus. |
| Min. | " | Minimum. |  |  |  |

1. Rainfall-Indicates that an appreciable quantity of rain (one hundredth of an inch or more) has fallen during the day or since the last observation; also, that the day is a rainy day as distinguished from snowy or clear days.
2.     * Snowfali-Indicates that an appreciable quantity of snow has fallen during the day. *o may be used to denote flurries of snow.
3.     - Hailstones-Hard semi-transparent ice, whether small or large, crystalline or rounded. $\boldsymbol{\Lambda}^{\circ}$ small quantity of hailstones; $\boldsymbol{\Delta}^{2}$ large quantity of hailstones.
4. $\triangle$ SleET-Or pellets of snow or soft hail without any crystalline structure. This symbol is used by the Germans for Graupeln, or snow pellets, and for the semi-transparent mixture of snow and ice that in the dry weather of Central Europe nearly corresponds to the sleet of the coasts of England and America. $\Delta^{\circ}$ small quantity of sleet; $\Delta^{2}$ much sleet.
5. V Silver Frost-(English, "silver thaw," French, givre, German, Rauhfrost or duft-anhang); this refers to an accumulation of snow and sleet on the limbs of trees, in which the snow is the main feature, so that the external appearance is silvery white and rough.
6. $\bigcirc$ Glazed Frost-(French, verglas, Germàn, Glatteis); this refers to an accumulation of snow and ice on the trees, in which the ice is in excess and the external appearance is smooth and transparent. In using the symbols for "silver frost" and "glazed frost," the Munich Conference requests that these terms be considered as descriptive of the resulting phenomena, no matter how they are brought about, therefore the definitions avoid any statement as to the conditions attending the formation of the depositions. The same rule applies to the use of the symbol for "hoar frost."
7. $\leftarrow$ Ice-needles-(Not yet well defined by international usage).

8．$\uparrow$ Drifting snow－（German，schneegestober）；this symbol indicates that strong winds are raising the snow from the ground，filling the air with it like dust，and transporting it horizontally；this may occur under a clear sky．The symbol does not refer to snow falling from the clouds，nor to the mere fact that the snow is lying in drifts on the ground．When the air is filled with blinding snow－dust，use the symbol $\hat{\rightarrow}^{2}{ }^{2}$ ，but for light winds and light snow－dust use $\hat{\uparrow}>0$ ．
9．図 Snow－covering－Or quantity of snow lying on the ground；when more than half the soil in the neighborhood of any station is covered with snow this is indicated by $⿴ 囗 大$ ，if the snow covering is thin，use $\mathbb{Z}^{0}$ ，but if it is considered deep for that station use $\mathbb{Z}^{2}$ ．
1．$\equiv$ FoG $\equiv$ Ground fog not exceeding height of a man；$\equiv{ }^{\circ}$ thin fog or mist enveloping and above the observer ；$\equiv^{2}$ heavy fog or mist， such as the Scotch mist，drizzling down upon the observer． Fog symbols should not be used when an observer at a high station notices fog in the valley below him；this should be expressed by a note in the daily journal．
if．$\infty$ High haze－Such as makes distant mountains appear hazy，or such as covers the sky in the case of Indian summer haze or prairie fires；German，Moorrauch．If clouds are also prevalent in connection with this haze，the additional cloud signal should be given．The intensity，or density，of the haze is expressed by $\infty^{\circ}$ for light haze and $\infty^{2}$ for dense haze．The symbol $\infty$ indi－ cates merely the hazy condition，or the optical result，without considering whether the haze is caused by dust or moisture．
12．$ص$ Dew；$\perp^{0}$ light Dew；$ص^{2}$ heavy DEw－As the formation of dew depends upon the nature and exposure of the horizontal surface on which dew is deposited，the observer should use the same horizontal object uniformly throughout the season．
13．$\square$ Hoar frost ；$\square^{0}$ light hoar frost ；$\square^{2}$ heavy hoar frost， injurious to vegetation－The expression＂frosty weather＂refers to the low temperature as such；but the expression＂hoar frost＂to the crystalline ice deposited upon the surface of solids in the open air．Hoar frost is deposited on horizontal objects generally under a clear sky at night．
14．Strong wind－An arrow with four feathers indicates a wind whose strength is 8,9 ， 10 ， 11 ，or 12 on the Beaufort scale，or 8,9 ，or ro，on the international scale，or anything in excess of 50 miles per hour or 20 metres per second in absolute measures； $\boldsymbol{-}^{2}$ a remarkably strong wind or one exceeding ir on the Beaufort scale，or 80 miles per hour，or 35 metres per second．
15．I．Thunderstorm－Namely thunder，whether with or without light－ ning，rain，hail，or wind．
16. \& Lightning-Distant lightning or any form of lightning that occurs without audible thunder, even when it occurs in the zenith, which is sometimes the case (this latter occurrence should be especially described in the journal of the observer); $x^{\circ} 0$ infrequent lightning, or lightning that is confined to a small region of the sky; $\mathbb{L}^{2}$ lightning that occurs very frequently or extends over a large region of the sky. When distant lightning appears at a definite direction in the horizon, the observer should add the letters indicating the points of the compass, for instance, $5^{\circ}$ NW. וo p. indicates that occasional distant lightning occurred in the northwest at ten $\mathrm{p} . \mathrm{m}$.
17. (1) Solar aureola, corona, or glory-German, Kranz Lichtkron, "Corona," Sonnenhof. These are small circles of prismatic colors surrounding the sun, the radii of these circles are usually less than six degrees, but in the extreme case of Bishop's ring, its radius was fifteen degrees. Several concentric circles are sometimes visible ; each circular band of prismatic colors has its red on the outside, and its blue, violet, or purple on the inside, with respect to the sun; such rings are generally formed when the sun shines through a thin cloud and may be seen if the sun is viewed through neutral-tinted glass or by reflection in water. Similar circles surrounding the shadow of the observer's head are called '"anthelia," "aureolæ," "glories," or "fog-shadows," (German, Gegensonne, Brockenspectra).
18. $U$ Lunar aureola or corona-(German, Mondhof); circles surrounding the moon similar to the solar corona.
19. $\bigoplus$ Solar halo-(German, Sonnenring); these are larger circles surrounding the sun whose sizes are quite definite, namely, about twenty-two degrees and about forty degrees radius from the sun; they are easily distinguishable from the coronæ by the fact that the colors are feebler and are so arranged that the red light is inside or nearest the sun and the blue light is outside; the greater part of the breadth of the halo is white. Complex combinations of halos, parhelia, horizontal circles, and vertical columns sometimes occur, all of which may be indicated in general by the symbol $\oplus^{2}$, where the figure ${ }^{2}$ indicates that the display is more brilliant than usual ; a detailed statement of the radii or diameters of the rings and columns and of their arrangements should be given in the text.
20. $\mathbb{T}$ Lunar halo-(German, Mondring); phenomena surrounding the moon similar to the solar halo.
21. $\sim$ Rainbow-Double rainbows and those with adjacent supernumerary bows may be indicated by $\frown^{2}$.
22. $\sim$ AURORAL LIGHTS-Namely, any display of the Aurora Borealis.

## INDEX.

Abbe, C., work cited ..... xxxiii, lv
Absolute measure ..... 260, 261
zero of temperature. ..... 259
Acceleration, dimensions of ..... 262
of gravity ..... 258
Activity, units of. ..... 260, 26I
Air, coefficient of expansion of. ..... 259
density of, at different humidities,British.liv-1v, 221-223
Metric ..... liv-1vi, 225-228
density of, at different pressures, British liv, 1v, 1vi, ..... 22I-223
Metric. ..... liv-1vi, 225-228
density of, at different temperatures, British ..... liv-1v, 220
Metric. ..... liv-lvi, 224-225
specific heat of dry. ..... 259
thermal conductivity of. ..... 259
weight of, dry ..... 259
Ampere, dimensions of. ..... 262
Angle, ..... 262
conversion of days into ..... 212-215
Angular velocity, dimensions of. ..... 262
Angot, A., treatise cited. ..... xxii
Aqueous vapor, decrease of pressure with altitude ..... xliii, 146
pressure of,British......xxxviii, xxxix, 134, I35Metric.......................xli, 142, 143pressure of, at low temperature,
xxxvi, 130 , 13 ..... 131
in saturated air,
British. .xxxv, xxxvi, 122-127
Metric. xxxv, xxxvi, 128, ..... 129
weight of, British xxxvii, 132
weight of, Metric. xxxvii, 133
Arc, conversion into time. ..... 1i, 210
of circle equal to its radius. ..... 258
Area, dimensions of. ..... 262
of surface of earth. ..... 258
units of. ..... 260, 261
Astronomical constants. ..... 259
Atmosphere, standard pressure of...259, 261
weight of unit of volume ..... 259
Aureola, solar ..... 266
Aureola, lunar
Aureola, lunar ..... 266 ..... 266
Auroral lights ..... 266
Avoirdupois, conversion into metric, 1vi, 229-230, 260
Babinet, barometric formula of....xxxii, II8
Barometer, correction for average de-gree of humidity,xxviii, xxix, xxx, 108, I12, II3latitude and weight of mercury,
xxviii, xxx, 106, 107, 114
variation of gravity with altitude,
xix, 109, 115
determination of heights by,British measures,xxvi-xxix, xxxii, 100-109, 118Metric measures,
xxix-xxxi, xxxii, IIO-115, II8
difference of height corresponding
to .or inch change. ..... xxxi, 116
1 mm . ..... xxxii, 117
Barometric readings,
reduction to standard gravity,xviii-xx, 58-59
sea level, British. ..... xx-xxv, 60-77
Metric ..... xx-xxvi, 78-98
standard temperature,British.xv-xvii, $14-33$
Metric. ..... xvii-xviii, 34-56
when below $\mathrm{O}^{\circ} \mathrm{C}$ ..... xviii
pressures corresponding to tempera-
ture of boiling water, ..... xxxv, 119
Beaufort, Admiral, wind, scale xlvi, 160, 265Belli, work cited.xxxviii
Bessel, " " ..... lii
Bishop's ring. ..... 266
Boiling point, of water. ..... 119
corresponding barometric pressures,
XXXV, II9
Brass, coefficient of linear expansion. ..... 259
Broch, work cited ..... xxxv, 1v, 259
Brockenspectra ..... 266
Bunsen, work cited ..... 259

Caloric 259, 260, 26I
Capacity, electromagnetic........................ 262
magnetic inductive............................. 262
measures of, British............................. 260
" Metric..............................26r
of an accumulator............................... 262
specific inductive................................. 262
units of.........................................260, 261
Centigrade, conversion into Fahrenheit, xii, 7-9
when near the boiling point........xii, 9 of differences into Fahrenheit.....xiii, 9
C. G. S. unit of magnetic intensity...1vii, 23 I

Circle, arc of.................................................. 258
circumference of.................................. 258
diameter................................................... $25^{8}$
circumference of earth....................... 258
equator............................................ 258
Clarke, A. R., treatise cited.........xxii, xlvii
Clarke's spheroid...............................xlvii, 258
Clouds, names and abbreviations.......... 264
Coefficient of expansion of air................ 259
linear 6 " brass............ 259
cubical " 6 glass............. 259
expansion of mercury......................... 259
Conductivity, dimensions of, thermal... 262
specific, electromagnetic.................. 262
thermal, of air...................................... 259
Conductor, resistance of........................... 262
C'onstants, astronomical................................ 259
geodetical................................................... 258
numerical................................................ 258
physical.................................................... 259
Continental measures of length and
equivalents
208
Conversion of measures of time and
angle.....................................1i, 209-218
linear measures...............xlix, 180-208
British and Metric units...........260-26I
thermometric scales....................xi, 2-9
Correction, for air temperature in determining heights by barometer, British...................xxvii-xxviii, 104-105
for air temperature in determining heights by barometer, Metric, xxix-xxx, III
for temperature of the Mercury in the thermometer stem. .xiv, 12
for gravity, in determining heights by the barometer, British, xxviii, 109 for gravity, in determining heights by the barometer, Metric...xxxi, II5
for humidity in determining heights by the barometer, British, xxviii, 108

Correction (Continued).
for humidity in determining heights
by the barometer, Metric, Xxx, II2-I I 3
for latitude, in determining heights by the barometer, British, xxviii, 106-107
for latitude, in determining heights by the barometer, Metric.....xxx, II4
Corona ................................................ 266
Cosines, table of natural...........lix, 236-237
Cotangents, table of natural.....lix, 238-239
Coulomb.................................................. 262
Current, intensity of............................ 262
Days, conversion into decimals of year
and angle..............................lii, 212-215
Day decimals of, into hours, minutes
and seconds................................liii, 216
mean solar....................................... 259
sidereal............................................ 259
Declination of sun................. ......xlix, 177
Degree, length of, of meridian and any
parallel.............................xlvii, 164, i65
length of, of meridian and any parallel at different latitudes, xlvii, 164,165
Degrees, Centigrade into Fahrenheit
and Reaumur...................xi, xii, 7, 8, 9
Fahrenheit into Centigrade xi, xii, 3-6
Reaumur into Fahrenheit and Cen-
tigrade......................................xi, 2
Density, of air.............liv-lvi, 220-228, 259
of earth, mean ................................ 258
surface...................................... 258
dimensions of ................................. 262
surface...................................... 262
of mercury....................................... 259
Depth of rainfall, corresponding quan-
tity of water..............................1viii, 232
Determination of heights by barometer,
British measures.....xxvi-xxix, 100-109
Metric measures.....xxix-xxxi, IIO-II5
Depression of dew-point..................138-14r
Dew........................................................ 265
Dew-point................................xxxviii-xli
Difference of heights by barometer, xxxi, xxxii, II6, II7
of potential 262
Differences Fahrenheit to Centigrade, xiii, 9
Centigrade to Fahrenheit............xiii, 9
Dimensions, in electrostatic system...... 262
electromagnetic system.................... 262
of the earth...................................... 258
physical quantities........................... 262
Distance, mean of earth from sun. ..... 259
Division tables of, for 28,29 and 31 ,1viii, lix, 233-235
Dove's pentades. ..... 1viii, 232
Dry air, weight of. ..... 259
Drifting snow ..... 265
Duft-anhang ..... 265
Duration of sunshine. ..... xlviii, $166-177$
Dyne .1vii, 23I, 260, 26I
Earth, area of surface of ..... 258
density of. ..... 258
dimensions of. ..... 258
eccentricity of. ..... 258
elliplicity of. ..... 258
equatorial semi-axis. ..... 258
flattening of ..... 258
mean distance from the sun ..... 259
El, value of the ..... 208
Electricity quantity of ..... 262
Electric force or electro-motive intensity,262
Electrostatics, quantities in. ..... 262
Electromagnetics ' ..... 262
Energy, dimensions of. ..... 262
Equator, circumference of. ..... 258
Equator, length of semi-axis. ..... 258
Erg. ..... 260, 26I
Espy, treatise cited. ..... xxxviii
Expansion, coefficient of, air. ..... 259
brass. ..... 259
glass. ..... 259
mercury. ..... 259
Fahrenheit, conversion into Centigrade
and Reaumur. ..... xi, xii, 3-6
differences into differences Centi-
differences into differences Centi- grade ..... xiii, 9
Farad, dimensions of. ..... 262
Fathom, Swedish, value of. ..... 208
Ferrel, Wm., treatise cited, xxii, xxxi, xxxix, xlix
Feet, conversion into metres. ..... 1, 200-20I
per second into miles per hour, $\mathrm{xlv}, \mathrm{I}_{55}$
metres per second ..... 260
kilometres per hour. ..... 260
Flattening of the earth ..... 258
Fog, symbol for. ..... 265
Foot, value of, Austrian ..... 208
old French. ..... 208
Russian. ..... 208
Rhenish ..... 208
Spanish ..... 208
Swedish. ..... 208
Foot-pound. ..... 260, 26 I
Foot-poundal. ..... 260, 26I
Force, dimensions of. ..... 262
units of. ..... 260, 26 I
electric. ..... 262
magnetic ..... 262
electromagnetic. ..... 262
Force-de-cheval. ..... 260, 26I
Formula, Babinet's barometric....xxxii, 118
Lambert's, wind direction, xliii, 148 -I 53
Freezing point of mercury ..... 259
Frost, glazed, hoar, silver,symbols, 264, 265
Gallon (U. S.) and Imperial ..... 260, 26I
Gaussian units. ..... 1vii, 23 I
Gegensonne, symbol for ..... 266
Geodetical constants. ..... 258
tables. ..... I6I
Givre or silver frost. ..... 264
Glass, coefficient of cubical expansion. ..... 259
Glatteis, or glazed frost. ..... 264
Glazed frost ..... 264
Glory or corona, symbol for. ..... 266
Graetz, work cited. ..... 259
Grains, conversion into grammes...1vii, 230
Grammes, conversion into grains...lvii, 231
Gramme-degree or therm ..... 26I
Grammes per square centimetre. ..... 26I
Graupeln ..... 264
Gravitation measure, units in. ..... 260, 26I
Gravity, acceleration of. ..... 258
correction for variation of, withaltitude,..............xix, xxxi, IO9, II5correction for variation of, withlatitude.................xix, xxx, 106, II4
reduction of barometric readings to standard................xviii-xxiv, 58-98
relative acceleration of, in different latitudes xlvi, 162,163
Guyot, A., treatise cited. ..... xxii
Hailstones, description and symbol for.. 264Halo, solar and lunar.266
Hann, J., treatise cited ..... xliii
Harkness, Wm., treatise cited,
xix, xxii, xlvi, 258, ..... 259
Haze, symbol for ..... 265
Hazen, H. A., treatise cited..xliv, xlv, 1viiiHeat, dimensions of.262
latent, of liquefaction of ice. ..... 259
vaporization of water. ..... 259
mechanical equivalent of. ..... 259
Heat (Continued).
specific, of dry air ..... 259
ratio of the two, of air ..... 259
units of. ..... 260, 26 I
Hectare ..... 260, 261
Hectolitre ..... 261
Heights, determinatian of, by barometer,British.xxvi-xxix, 100-109
Metric. xxix-xxxi, 110-115
thermometrical measurement of,xxxiii, 119
Hoar-frost, symbol for ..... 265
Horse-power ..... 260, 261
Hours, conversion into decimals of aday.lii, 216
of minutes and seconds into deci- mals of. ..... liii, 217
Humidity relative, British,
xxxviii-xlii, 138 - 14 I
Metric,
xxxviii-xlii, 144-145
term for ..... 1vi, 225
Hygrometrical tables. xxxv, 122-146
Hypsometry xxxiii, xxxiv, 119
Ice, latent heat of liquefaction of ..... 259
needles, symbol for. ..... 264
Inches, conversion into millimetres, xlix, 180-186
Inductive capacity, magnetic ..... 262
specific ..... 262
Inertia, moment of. ..... 262
Intensity, electro-motive ..... 262
of current ..... 262
of field. ..... 262
of magnetization ..... 262
Interconversion, of British and Metric units. ..... 260, 26I
nautical and statute miles. ..... 1i, 208
sidereal and solar time ..... liii, 218
International meteorological symbols. ..... 263
James, H., treatise cited. ..... 160
Joule, value of ..... 259, 26I
Kilogramme-degree. ..... 259
Kilogrammes, conversion into avoirdu- pois 1vi, 230, 260
Kilogram-metres ..... 260, 26I
Kilogramme, prototype. ..... 1vi
Kilometres into miles. ..... 1i, 206, 207
per hour into metres per second,
xlvi, ..... 159miles per hour.26I
Klafter, Wiener, value in metres and feet. ..... 208
Kranz or corona ..... 266
Lambert's formula, mean wind direc- tion. .xliii, $148-153$
Laplace, formula of. ..... xx
Latent heat of liquefaction of ice. ..... 259
vaporization of water. ..... 259
Latitude, gravity correction for, xix, xxx, 106, ..... II4
Laughton, J. K. treatise cited ..... 160
Length of arc of meridian ..... xlvii, 16
parallel. ..... xlvii, 165
dimensions of. ..... 262
of equator of earth ..... 258
meridian circumference of. ..... 258
second's pendulum ..... 258
measures of, Continental with met-
ric and British equivalents......1i, 208units of.260
Libby, Wm., work cited,
xxxviii, xlviii, lvii
Lichtkron or corona ..... 266
Light, velocity of. ..... 259
Lightning, symbol for ..... 266
Line, old French, value of. ..... 208
Linear measures ..... 179-208
Litre, value of. ..... 260, 261
Logarithms, table of. ..... lix, 240-241
Naperian base. ..... 258
Modulus of common ..... 258
Lunar aureola, halo, corona. ..... 266
Magnetic force ..... 262
inductive capacity ..... 262
intensity, units of. ..... 1vii
table for converting ..... 231
moment ..... 262
potential ..... 262
Magnetism, quantity of ..... 262
Magnetization, intensity of. ..... 262
Marek, M., treatise cited ..... xxi
Marvin, C. F., treatise cited ..... xxxvi
Mass, dimensions of. ..... 262
units of ..... 260, 261
Mean density of the earth ..... 258
Mean distance of earth from sun. ..... 259
Mean solar time, conversion into sidereal, ..... 1iii, 218
Mean time at apparent noon. ..... liii, 217
Measures of angle ..... li, 209
of length, continental, Metric and British. ..... 1i, 208
Measures (Continued).
time.li, 209
tables for interconversion of. ...260, 261
Mechanical equivalent of heat ..... 259
Megalerg. ..... 261
Mercury, coefficient of expansion...xvi, ..... 259
density of ..... 259
freezing point of. ..... 259
Mercurial column, one inch high, pres-
sure of. ..... 259
Meridian, arcs of terrestrial ..... xlvii
length of a degree. ..... xlvii, 164 ..... xlvii, 164
ellipse, perimeter of ..... 258
Meteorological stations, list of...lix, 243-257
$\qquad$vi, xlix, 260, 261
Metres, conversion into feet, 1, 202-203, 261per second into kilometres per hour,xlvi, 158,159
miles per hour....xlv, $156,157,261$
Micron. ..... 26I
Mile, Austrian post, value of. ..... 208
Danish, ..... 208
German sea, ..... 208
Nautical, ..... li, 208
Netherlands (migl), ..... 208
Norwegian, ..... 208
Prussian, ..... 208
Swedish, ..... 208
Statute (British), ..... 208
Miles, conversion into kilometres,
1i, 204-205, 26I
nautical1i, 208
statute ..... 1i, 208
per hour into feet per second,

$$
\mathrm{xlv}, \mathrm{I} 54, \mathrm{I} 55
$$

metres per second, $\mathrm{xlv}, \mathrm{I} 54, \mathrm{I} 57,260$kilometres per hour...xlv, 154,260Millimetres, conversion into inches,1, 187-199
Minutes of time, into arc ..... lii, 2 II
into decimals of a day ..... lii, 216
conversion of day into ..... liii, 2 I6
conversion into decimals of an hour,liii, 217
Moment of inertia ..... 262
Momentum, dimensions of. ..... 262
Mondhof or lunar corona. ..... 266
Mondring or lunar halo. ..... 266
Moorrauch or high haze. ..... 265
Moritz, A., treatise cited ..... xxxv
Munich Conference. ..... 263, 264
Naperian base of logarithms ..... 258
Nautical mile, equivalent in statute, li, 208
Neumayer, G., treatise cited ..... 160
Numerical constants ..... 258
Numbers, logarithms of. lix, 240, ..... 241
Ohm, dimensions of. ..... 262
Ounces, conversion into kilogrammes, ..... 1vi, 229
kilogrammes into.......1vi, 1vii, 230, 26I
Palm, Netherlands, value of. ..... 208
Parallel, length of a degree on.....xlvii, ..... 65
Pendulum, length of second's. ..... 258
Pentades, Dove's ..... 1viii, 232
Perimeter of meridian ellipse ..... 258
Physical constants ..... 259
quantities, dimensions of. ..... 262
Potential, difference of ..... 262
in electro-magnetics ..... 262
magnetic ..... 262
Pound, avoirdupois, conversion into kilogramme ..... 1vi, 229, 260
imperial standard ..... 1vi
Pounds, per square foot ..... 260
inch ..... 260
Poundal. ..... 260, 261
Pound-degree 259, 260, ..... 261
Power or rate of working. ..... 262
Pressure of aqueous vapor, British, xxxviii, 122, 128 , 134 , 135
Pressure of aqueous vapor, Metric,
xli, 128, 129, 142
Pressure of aquenus vapor at low tem-peratures.
I3IPressure of standard atmosphere
decrease of vapor pressure with alti- tude ..... xliii, 146
Prototype kilogramme ..... 1vi
Psychrometer, whirled ..... xxxviii, xxxix
Psychrometric observations,
reduction of, British.....xxxix, 134, 137
Metric. xli, 142-143
Quantity of electricity ..... 262
conveyed by current. ..... 262
magnetism ..... 262
Quantities physical, dimensions of. ..... 262
Quantity of water corresponding to given depths of rainfall ..... 1viii, 232
Rainbow, symbol for ..... 266
Rainfall, conversion of depth of, into gallons and tons ..... 1viii, 232
symbol for. ..... 264
Rate of decrease of vapor pressure with altitude ..... xliii, 146
Rate of working, dimensions of. ..... 262
Ratio of specific heats of air ..... 259
yard to metre ..... vi
Rauhfrost, or silver frost ..... 264
Reaumur, conversion to centigrade... ..... xi, 2
Fahrenheit ..... xi, 2
Regnault, treatise cited...xxxiv, xxxv, ..... 259
Recknagel, work cited ..... 259
Reduction of barometer to sea level, xx-xxiv, 60-98
standard temperature, xv-xix, $14-56$gravity.......................xxxi, 58, 59psychrometric observations, xli, 142, I43of snowfall measurement.........xlii, 146Relative humidity,xxxviii, xlii, r38-141, 144-145
Relative intensity of solar radiation,xlix, 178
Resistance of a conductor ..... 262
specific ..... 262
Rode, Danish, value of. ..... 208
Röntgen, work cited. ..... 259
Rowland, H. A., treatise cited. ..... 259
Ruthe, Prussian, value of. ..... 208
Norwegian, ..... 208
Sagene (Russian), value of ..... 208
Scales, comparison of thermometric. ..... xi
Reaumur to Fahrenheit. ..... 2
Ceutigrade ..... 2
Fahrenheit to Centigrade ..... 3-6
Centigrade to Fahrenheit ..... 7-9
Schott, C. A., treatise cited ..... 160
Scott, R. H., treatise cited ..... 160
Schneegestober or drifting snow ..... 265
Sea-level, reduction of barometer to,British.$. x x-x x y, 60-77$
Metric. ..... xx-xxvi, 78-98
Seconds, of time into arc ..... $21 I$
decimals of a day ..... lii, 216
conversion of decimals of a day into, ..... liii, 216
of time into decimals of an hour,
liii, 217
pendulum, length of. ..... 258
reduction for, sidereal or solar time, ..... liv, 218
circumference of circle in ..... 258
arc of circle in ..... 258
Sidereal day and year. ..... 259
time, conversion to mean solar,
Silver frost264
Sines, table of natural. ..... 237
Sleet, symbol for. ..... 264
Snowfall, symbol for ..... 264
weight of and corresponding depth of water ..... 146
Solar, day mean ..... 259
time, mean, conversion to sideral, liii, liv, 218
aureola, symbol for ..... 266
corona ..... 266
halo ..... 266
radiation, relative intensity of, ..... xlix, 178
Sonnenhof, symbol for ..... 266
Sonnenring ..... 266
Sound, velocity of. ..... 259
Specific heat of dry air ..... 259
heats, ratio of, of air ..... 259
conductivity. ..... 262
inductive capacity ..... 262
resistance ..... 262
Spheroid, Clarke's. ..... xlvii, 258
Standard atmosphere ..... 259, 261
Stations, International Polar. ..... 257
list of meteorological ..... 1ix, 243-257
of first order ..... lix
in Africa ..... 256-257
Asia, 254-255, Australasia, 256,Europe, 247-254, North America,244-246, South America, 246-247,Austro-Hungary, 247-248, Bel-gium, 248, British Isles, 248-249,Canada, 244, Central America, 244,Denmark, 249, France, 249, Ger-many, 250, Greece, 248, Green-land, 244, Holland, 248, Italy,25I, Mexico, 244, Norway, 249,Portugal, 253, Roumania, 248,Russia, 25I-253, Spain, 253,Sweden, 249, Switzerland, 253,254, Turkey, 248, United States,245-246, West Indies, 244.
Statute miles, conversion of. ..... 1i, 208
Stere, value of. ..... 260, 26I
Strength of field ..... 262
pole, in magnetics. ..... 262
Stress, dimensions of. ..... 262
units of. ..... 260, 261
Sun, declination of. ..... xlix, 17
mean distance from the earth ..... 259
Sunshine, duration of, at different lati-
tudes and declinations......xlviii, 166-177
Surface (area), units of. ..... 260, 26 rSurface (Continued).density of the earth258
in electro-statics ..... 262
Symbols, International Meteorologic,

$$
263-266
$$

Synoptic conversion of British and Metric units ..... 260-26I
Table for conversion of arc into time li, 210linear measures180-208
mean solar into sidereal.....liii, liv, 218
measures of weight. ..... 229-23I
sidereal into mean solar.....liii, liv, 218time into arc...........................lii, 211
Centigrade readings into Fahren-heit and Reaumur.......xi, xii, 7, 8, 9near boiling point....... .........xii, 9
velocities ..... 154-159
differences F to differences C .......xiii, 9
F......xiii, 9
Fahrenheit readings into Centi-grade.xi, xii, 3-6
Reaumur readings into F and $\mathrm{C} . . . \mathrm{xi}, 2$determination of heights by baro-meter, British.100-109
determination of heights by baro-meter, Metric.IIO-II5
decrease of vapor pressure with al- titude ..... 146
dividing by 28 . ..... lviii, lix, 233
29. .1viii, lix, 234
30. lviii, lix, ..... 235
density of air ..... 220, 228
reduction of barometer to standardtemperature14-56
gravity ..... 58-59
sea-level ..... 60-98
psychrometric observations,
136-145
snowfall measurements ..... 146
temperature to sea-level. ..... Io, II
of duration of sunshine ..... 166-177
intensity of solar radiation. ..... 178
lengths of degree. ..... 164-165
natural cosines and sines. ..... 236-237
cotangents and tangents. ..... 238-239
pressure of aqueous vapor ..... 122-13I
pressures and corresponding boil-ing points.119
quantity of rainfall and corres- ponding depths. ..... 232
of relative acceleration of gravity,162, 163

Tables of relative humidity,

$$
\text { I38-141, } 144-145
$$

Table of weight of aqueous vapor...132-133
Tangents, table of natural......1ix, 238, 239259
of freezing point of mercury ..... 259
decrease of, with altitude,
xiii, xiv, 10,11
reduction to sea level, British,xiii, xiv, 10
reduction to sea level, Metric,
xiii, xiv, II
Thermometer, hypsometric. ..... xxxiv
stem, correction for temperature of mercury ..... xiv, 12
Therm or gramme degree ..... 26I
Thermal conductively of air ..... 259
Thermometric scales ..... -9
Thomson, W., treatise, cited ..... 259
Thorpe, T. E., ..... xiv
Thunderstorm, symbol for. ..... 265
Time, conversion into arc. ..... lii, 211
of arc into ..... 1i, 210
dimensions of ..... 262
mean, at apparent noon. ..... liii, 217
mean solar into sidereal......liii-liv, ..... 218
minutes of, into arc. .....  21
seconds of, ..... 211
sidereal into mean solar.....liii-liv, ..... 218
Toisè, old French. ..... 208
Ton ..... 260
Tonne ..... 261
Tropical year ..... liii, 259
Units of magnetic intensity ..... 1vii, 23 I
interconversion of British and Met-
ric. 260, 261
Vapor aqueous, pressure of, British,XXXV, I22-I27
Metric, xxxvi, 128 -129
at low temperature ......xxxvi, 130,131decrease of pressure with altitude,

$$
\text { xliii, } 146
$$

weight of........xxxvii, xxxviii, I32, I33
Vaporization, latent heat of, of water... 259
Vara, Mexican, value of. ..... 208
Spanish, ..... 208
Velocity, dimensions of. ..... 262
of light. ..... 259
sound ..... 259
units of ..... 260, 261
Velocities, conversion of...xlv, xlvi, 154-159Verglas or glazed frost, symbol for.264
Versta or Werst (Russian) ..... 208
Volt, dimensions of. ..... 262
Volume, dimensions of. ..... 262
units of. ..... 260, 26I
of distilled water. ..... 259
Water, distilled, volume and weight of,259
latent heat of vaporization of ..... 259
specific heat of, compared with air... 259
Watt. ..... 260, 26I
Weight of aqueous vapor,
xxxvii, xxxviii, 132, I33
distilled water ..... 259
dry air ..... 259
one grain in dynes. ..... 260
pound in dyres. ..... 260
dyne ..... 26I
Werst or versta, Russian ..... 208
Wind, mean direction by Lambert'sformula...............................xliii, I48-I53
scale, Beaufort, conversion.....xlvi, 160
symbols for. ..... 265
tables. ..... xliii, $148-160$
Work, dimensions of ..... 262
units of, in absolute measure... 260 , ..... $26 I$
Working, rate of ..... 262
Yard, ratio of to metre. ..... vi
Year, conversion of days into decimalsof, and angle.lii, 212-215
bissextile, days into decimals of,lii, 212-215
length of tropical ..... liii, 259
sidereal ..... 259
Zero, absolute, of temperature ..... 259

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[^0]:    *Wm. Harkness: The solar parallax and its related constants. Washington, 1891, $4^{\circ}$, pp. 169 .

[^1]:    *A. Angot : Annales du Bureau Central Météorologique. Année i878, t. I, p. C. 13.

[^2]:    * Due to the use of a slightly different value for the coefficient of expansion, Prof. Ferrel's formula, upon which the table is computed, is

    $$
    d Z=-\frac{2628.4}{B}\left(\mathrm{r}+0.002034\left(\theta-32^{\circ}\right)\right)(\mathrm{r}+\beta)
    $$

[^3]:    * Comptes Rendus, Paris, 1850, vol. xxv., page 309.

[^4]:    *The table has been computed with the factor II.7449; which results from Clarke's value for the conversion of the metre, instead of with the value II. 7459 above derived.

[^5]:    * From Hand-book of Meteorological Tables. By H. A. Hazen. Washington, 1888. With permission of the author.

[^6]:    * Comparisons of standards of length, made at the Ordnance Survey office, Southampton, England, by Capt. A. R. Clarke, R. E., 1866.

[^7]:    *The length of the tropical year is not absolutely constant. The value here given is for the year 1800 . Its decrease in 100 years is about 0.6 s .

[^8]:    Smithbonian Tables.

[^9]:    Smithbonian Tables.

[^10]:    * Based on Prof. Rowland's determinations. (Proc. Am. Acad. Arts and Sci., 1880.)

